

PLANS SURVEY
LAKE DEMONTREVILLE ROAD
From East County Line
To Long Lake Road
CO. PROJ. N^o 24-52

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 8-19-24

File No. 11

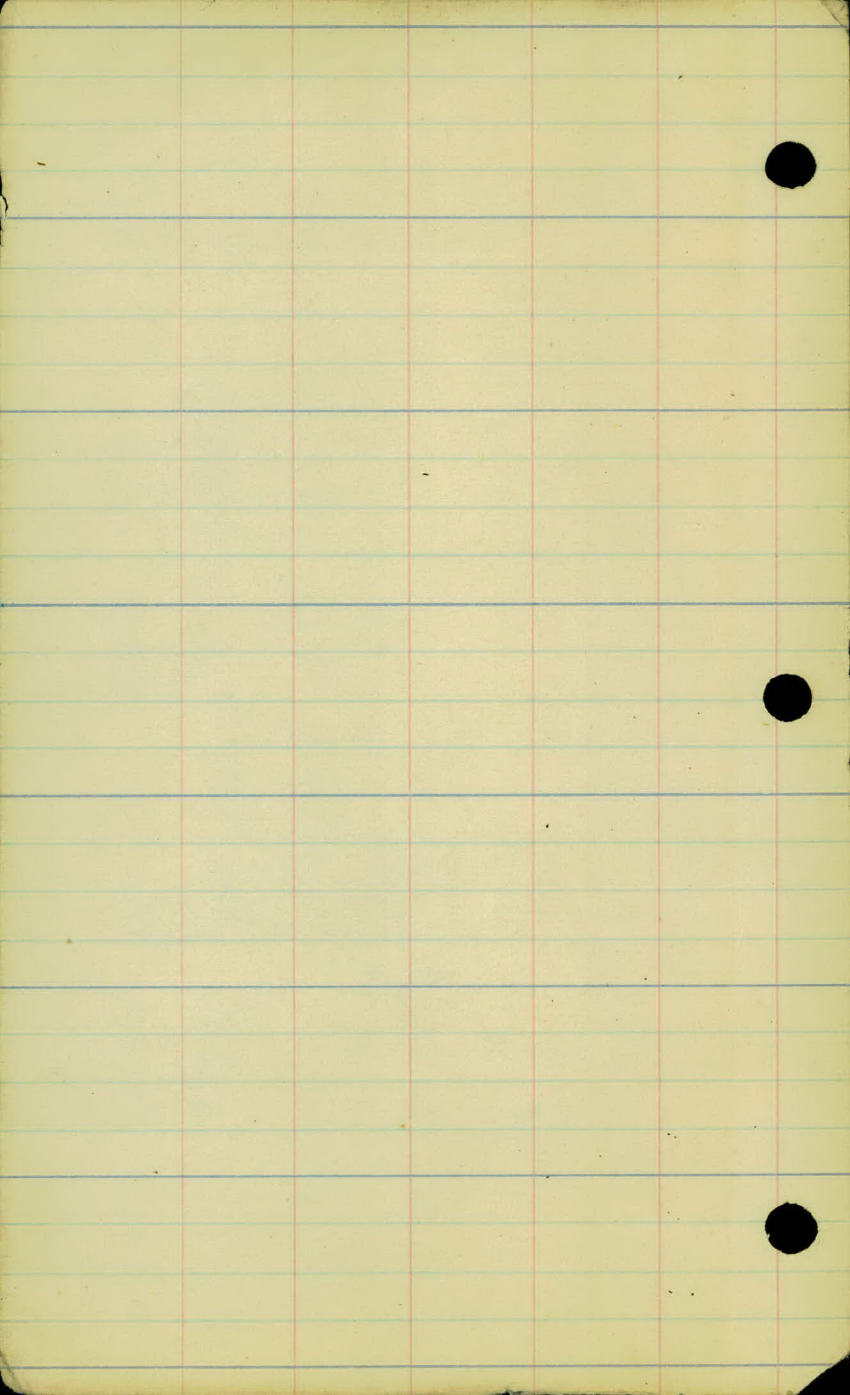
Line Change
 &
Line Extension

Proj- 24-52

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Office of Ramséy Co. Engineer
ST. PAUL, MINN.
Date Filed 8/19/24
File No. "11" (24-52)



Alignment

Station 148+29.4 : 202+73

Proj- 24-52

Station Point L R Bear.

N. 59° 32' E.

156+14.07 ✓ P.T.

5° 30.1'

156+00

5° 13.1'

155+50

4° 13.1'

4° C.R.

155+00

3° 13.1'

Δ 11° 00'

154+50

2° 13.1'

P.I. 154+77

154+00

1° 13.1'

T. 137.93 ✓

153+50

0° 13.1'

L. 275.00 ✓

153+39.07 ✓ P.C.

0° 00.1'

N. 48° 32' E. ✓

149+63.98 ✓ P.T.

13° 26.5'

20° C.L.

149+50

12° 03.6'

Δ 26° 55'

149+00

7° 03.6'

P.I. 148+98.3

148+50

2° 03.6'

T. 68.90 ✓

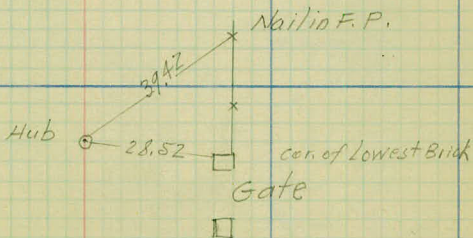
148+29.4 ✓ P.C.

0° 00.1'

L. 134.58 ✓

N. 75° 27' E.

○ Hub.



W.H.G.
Eck.
GAVIO
Fiorde

July 25-1924

Station Pt. L R. Bear.
N. 2° 48' W. ✓

171+49.99 P.T. 26° 35'

171+49.77 ✓
171+00 20° 20.1' 25° C.L.

170+50 14° 05.1' Δ 53° 10'

170+00 7° 50.1' P.I. 170+52.7

169+50 1° 35.1' T. 115.38 115.60 ✓

169+37.32 ✓ P.C. 0° 00' L. 212.67 ✓
169+37.1 ✓

N. 50° 22' E. ✓

167+14.3 ✓ P.T. 15° 30'

167+00 14° 47.1'

166+50 12° 17.1' 10° C.R.

166+00 9° 47.1' Δ 31° 00'

165+50 7° 17.1' P.I. 165+63.4

165+00 4° 47.1' T. 159.10 ✓

164+50 2° 17.1' L. 310.00 ✓

164+04.3 ✓ P.C. 0° 00'

N. 19° 22' E. ✓

160+78.2 ✓ P.T. 20° 05'

160+50 17° 16.7' 20° C.L.

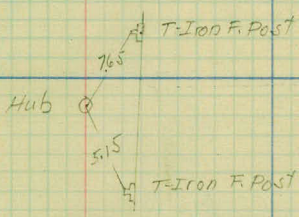
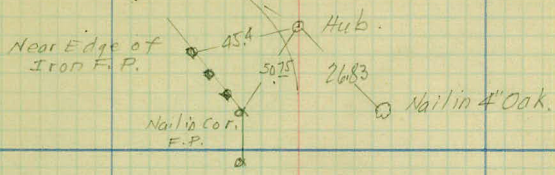
160+00 12° 16.7' Δ 40° 10'

+50 7° 16.7' P.I. 159+82.5

159 2° 16.7' T. 105.28 ✓

158+77.22 ✓ P.C. 0° 00' L. 200.83 ✓

N. 59° 32' E. ✓



Hub.

A single point labeled 'Hub.' is located in the lower right quadrant of the page.

Station Pt. L R. Bear.

202+73.⁰⁰ \pm Long Lake Road.

192+11.⁰⁰ P.O.T.

N. 1° 03' W. ✓

188+14.¹ P.I. 96° 10'

182+11.³⁵ P.O.T.

N. 89° 07' E. ✓

175+12.¹ P.I.

91° 55'

N. 2° 48' W. ✓

~~10101~~

W.H.C. July 28-1924
Eck.
Gallio
Frank

4

Nail in 6" oak

21.58

49.38 Nail in T.P.

Nail in 6" Oak

21.6

Nail

Nail in 6" oak

21.85

Nail in T.P.

42.25

Nail in Nail Box

19.22

Hub.

Nail in 6" Oak

18.10

Nail in 3" Oak

14.95

Hub.

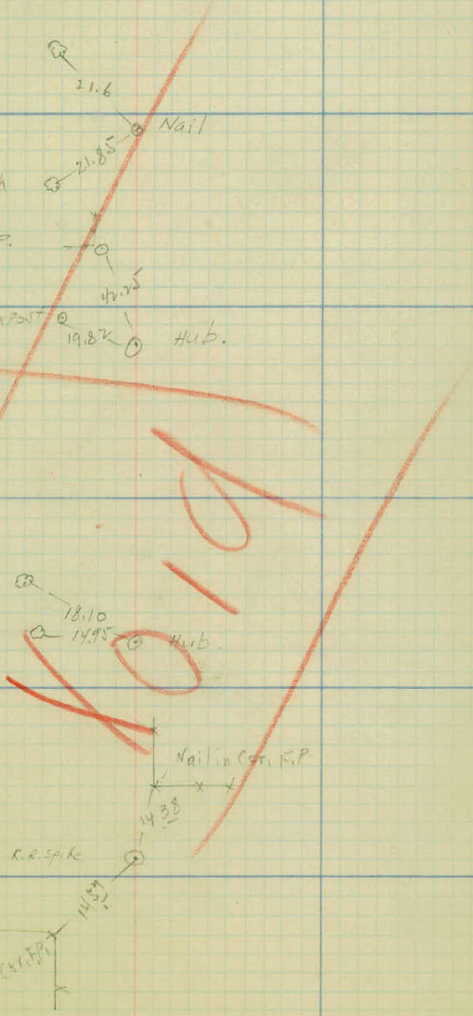
Nail in Cor. F.P.

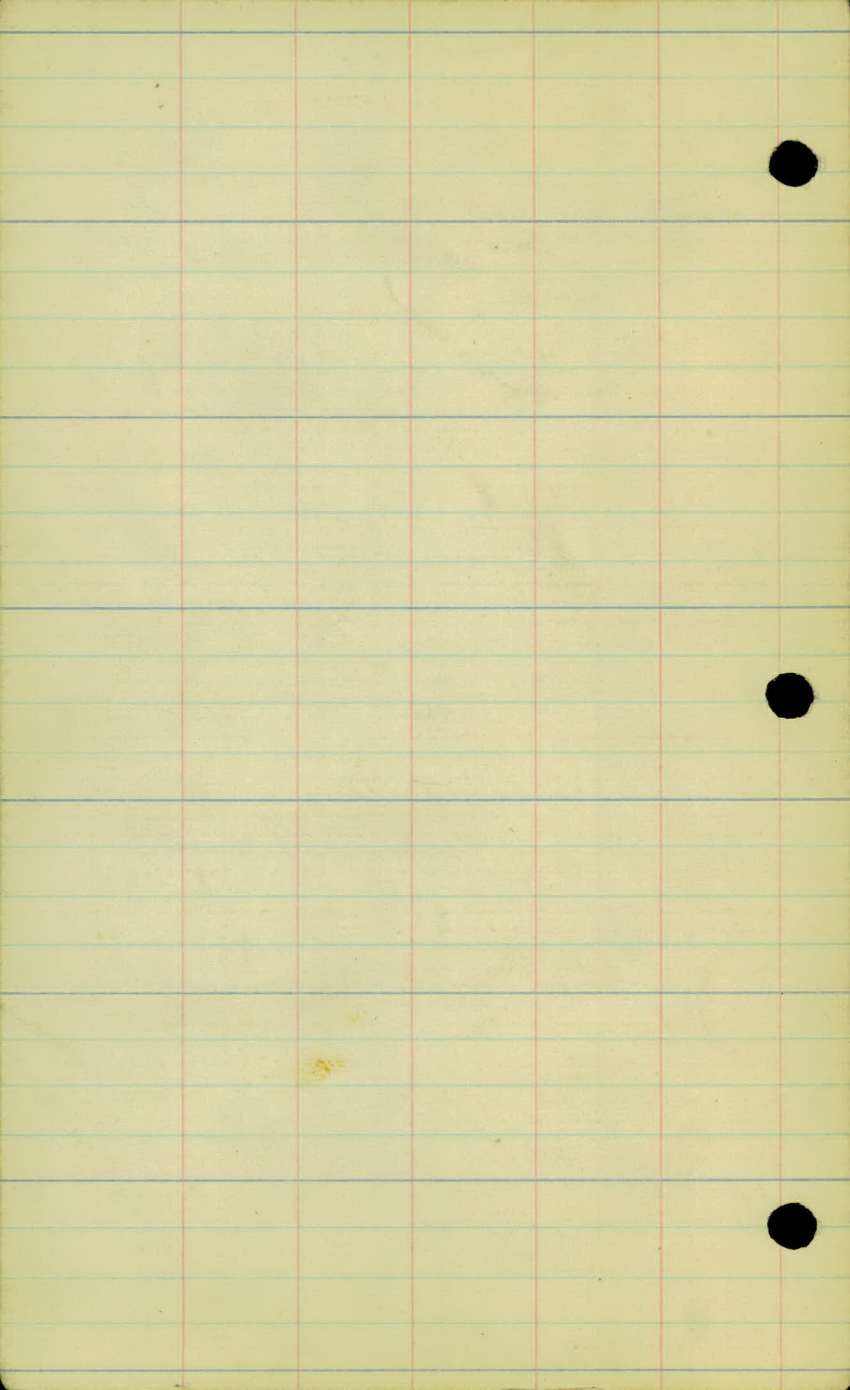
14.38

r.e. spike

14.57

Nail in Cor. F.P.





Art. Topog.

Proj - 24-52

station.

153

152

151

150

149

148

cultivated.

Willows

+183-Brick Post 7A
+69-Brick Post 43

+150-Brick P. 43'
+28 2-M. Br. 3 each 19'
+35-Brick Post 79N

Fence Col. 136-27'

Waldorf Estate

Heavy Oaks.

Hedge 99 Rt

108-A Fence 18'

Hedge

Heavy Oaks

Fence 41' Rt.
+11-End Br. of Post

164-30' Oak 16'

50' 50'

N.H.C.
Eck. July 28, 24
Ealyin
Frank.

station.

159

158

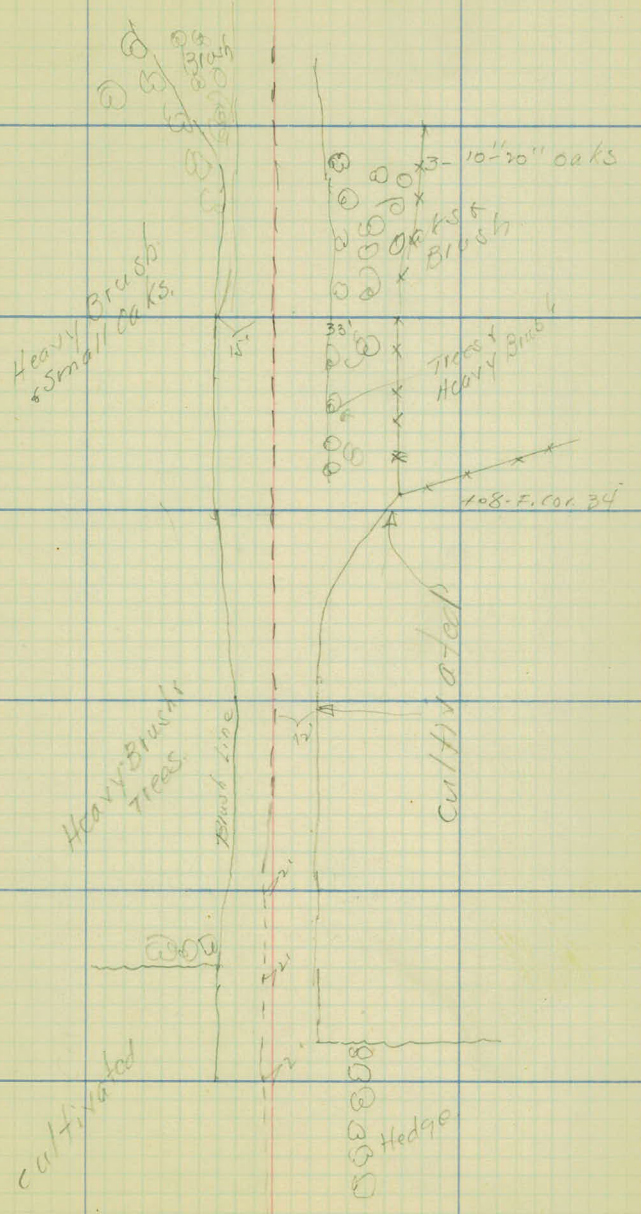
157

156

155

154

153



station.

165

164

163

162

161

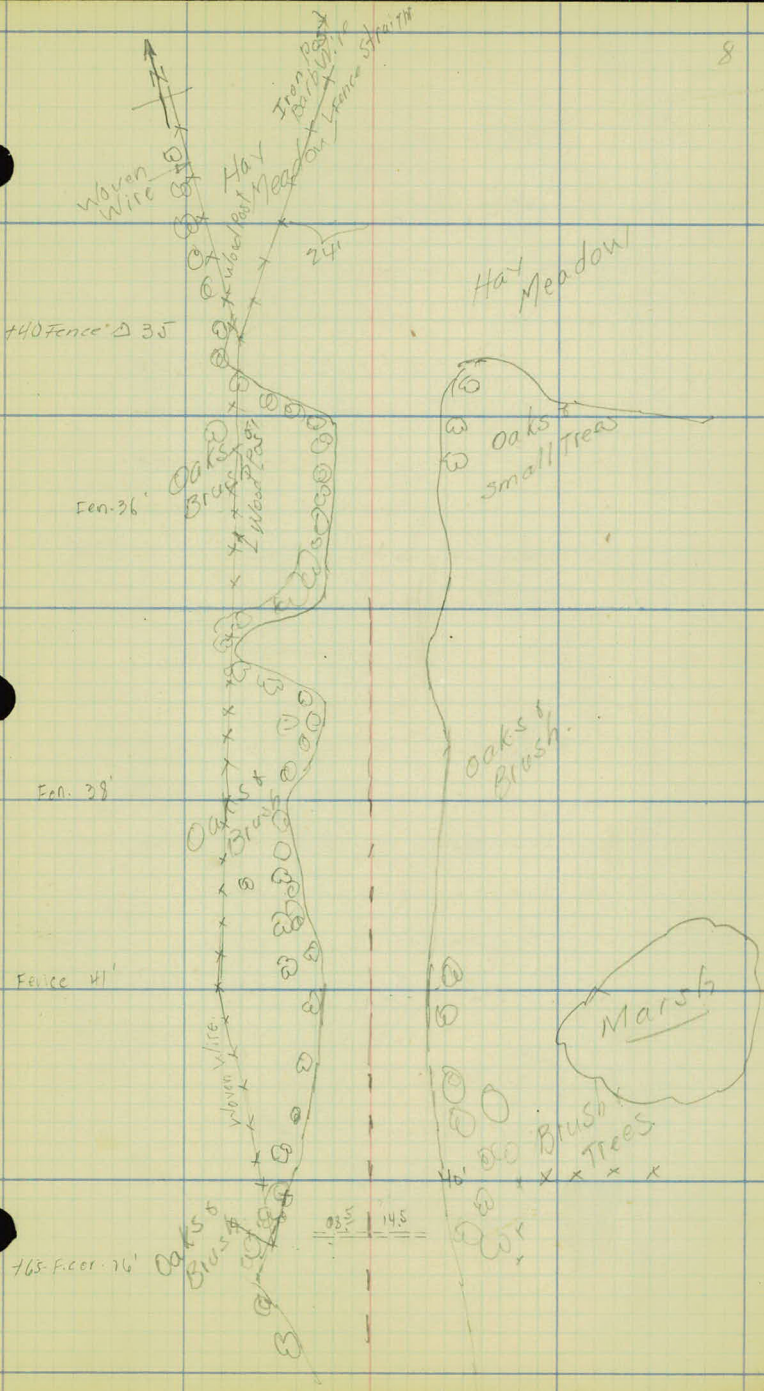
160

172

12' x 23' Vit.

Small Lake on
Left

159



Woven Wire

Iron post
Barbed Wire
Fence Strait

Hay Meadow

24

Fence 35

Hay Meadow

Fence 36

Oaks & Brush

Oaks & small Trees

Fence 38

Oaks & Brush

Fence 41

Oaks & Brush

Marsh

Woven Wire

Oaks & Brush
Trees

Fence 41
Oaks & Brush

22.5 14.5

station

171

170

169

168

167

166

165

2

+11 - en. Δ 18'

+12 - F. Δ 12'

F. 21

Fence 18'

+24 - en. Δ 21'

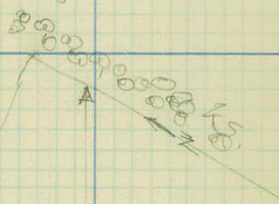


Hay Meadow

Hay Meadow

Fence Straight Iron Posts

Cultivated.



Hay Meadow

24'

station

cont'd next page

~~175+12-10 RI~~

~~175~~

~~178 12" x 28.5 c.M.~~

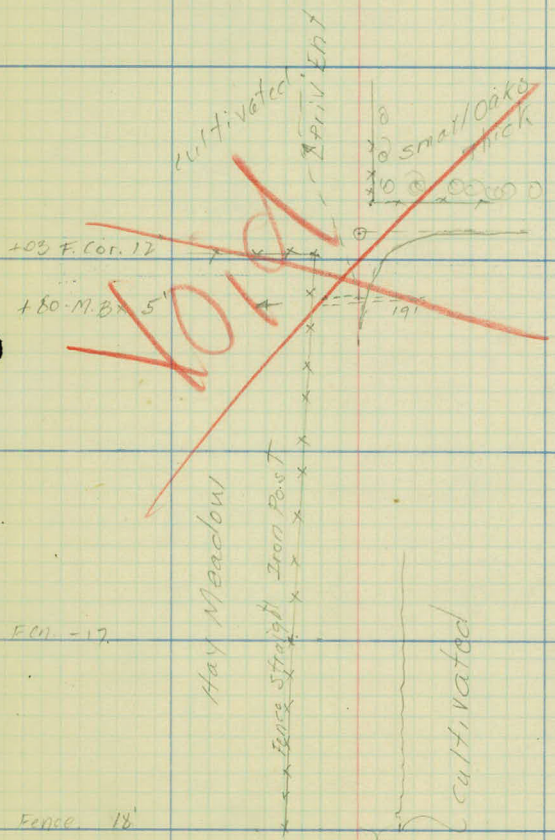
174

173

172

171

E



+03 F. Cor. 12

+80 M.B. 5'

FCI -17

Fence 18'

cultivated
SPRINT

5mat/Oaks
10
191

Hay Meadow
Fence Straight Iron Post

cultivated

Station

180

179

178

177

176

175+12.1 RI

175

Z

Small-Oaks
Thick

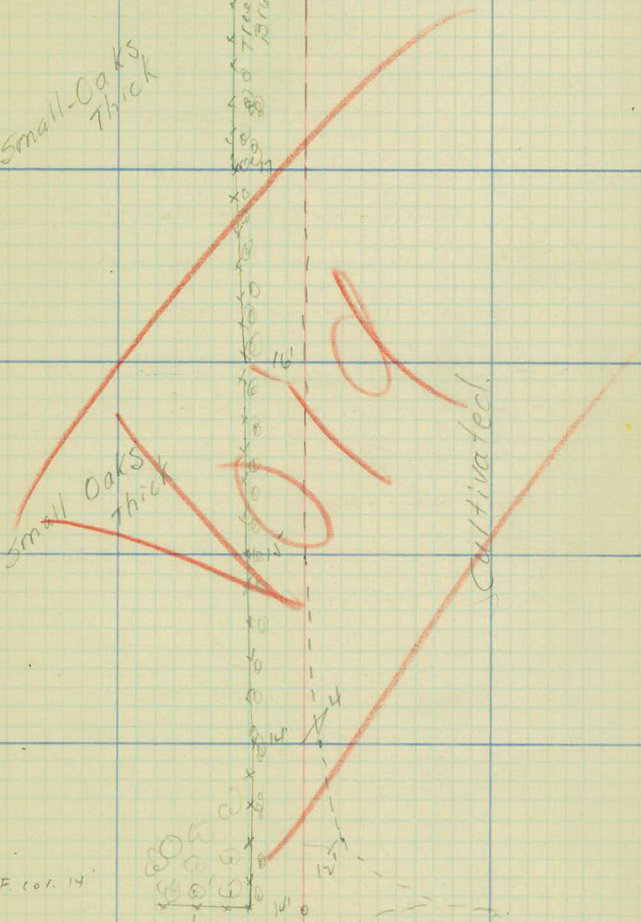
100
90
80
70
60
50
40
30
20
10
0
10
20
30
40
50
60
70
80
90
100

Small Oaks
Thick

Cultivated.

715-E. Col. 14'

Cultivated



station

186

185

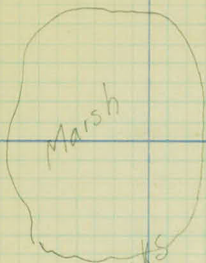
184

183

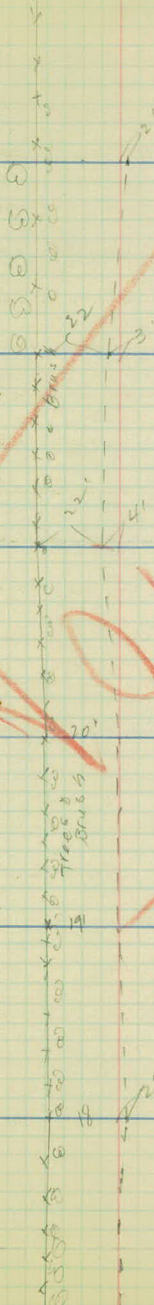
182

181

180



Oaks
thick



Oaks
thick

010

Cultivated.

Oaks
thick



station

190

189

188+14.1 P.I.

188

188+14.1 P.I.

188

187

186

F-16'

F 35'

Heavy Oaks 13

746-T.P. 15

Small Oaks
Thick

Small
Brush

Small
Brush

Heavy Oaks

752-F. Cor. 17'

16'

2'

39'

730-2-M. 30 14'

723-F. Cor. 41'

722-T.P. 41'

795 F. Cor. 36'

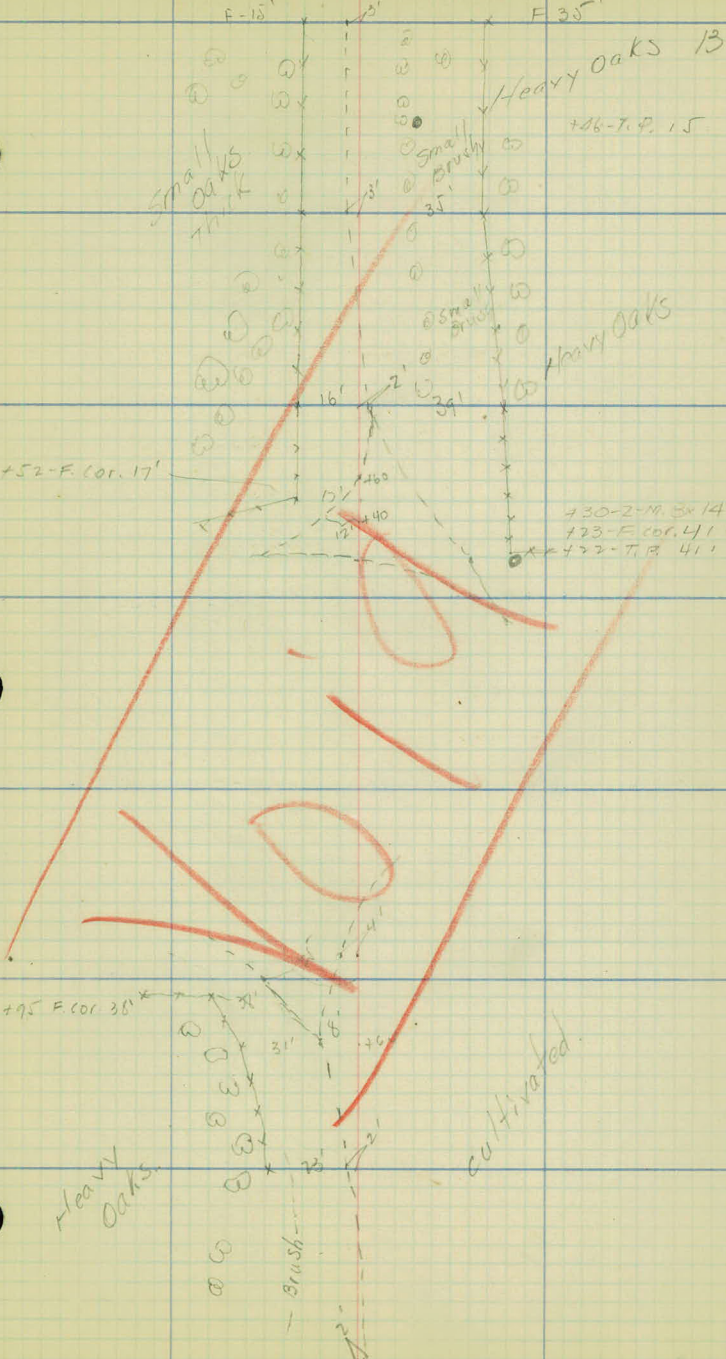
31'

26'

Heavy Oaks

Brush

cultivated



station

197

196

195

194

193

192

191

station

202+73 End. of Long Lake Road.

+25' 12x30' C.M.

202

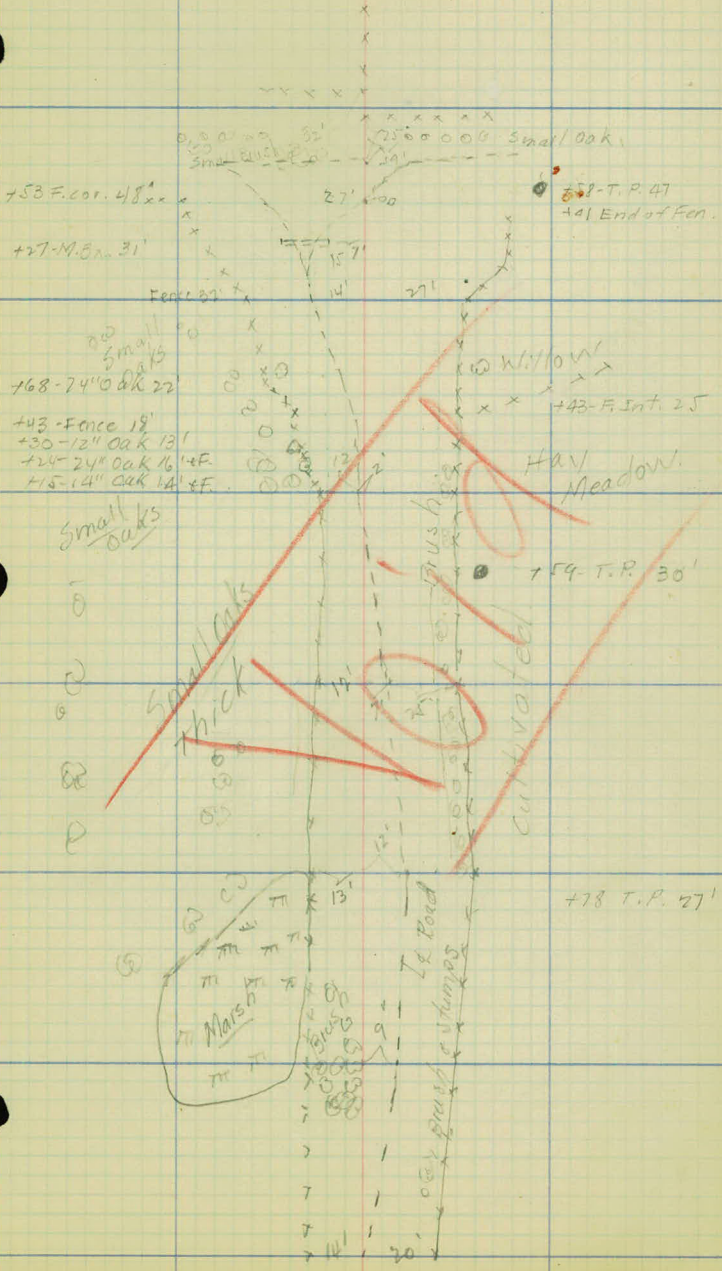
201

200

199

198

197



753-F. cor. 48' x 22'

727-M. 51' x 31'

768-74" oak 22'

743-Fence 18'
 730-12" oak 13'
 724-24" oak 16' 1/2"
 715-14" oak 14' 1/2"

Small oaks

Small oaks
thick

Brush

Cultivated

Willow

Hay Meadow

758-T.P. 47
End of Fence

759-T.P. 30'

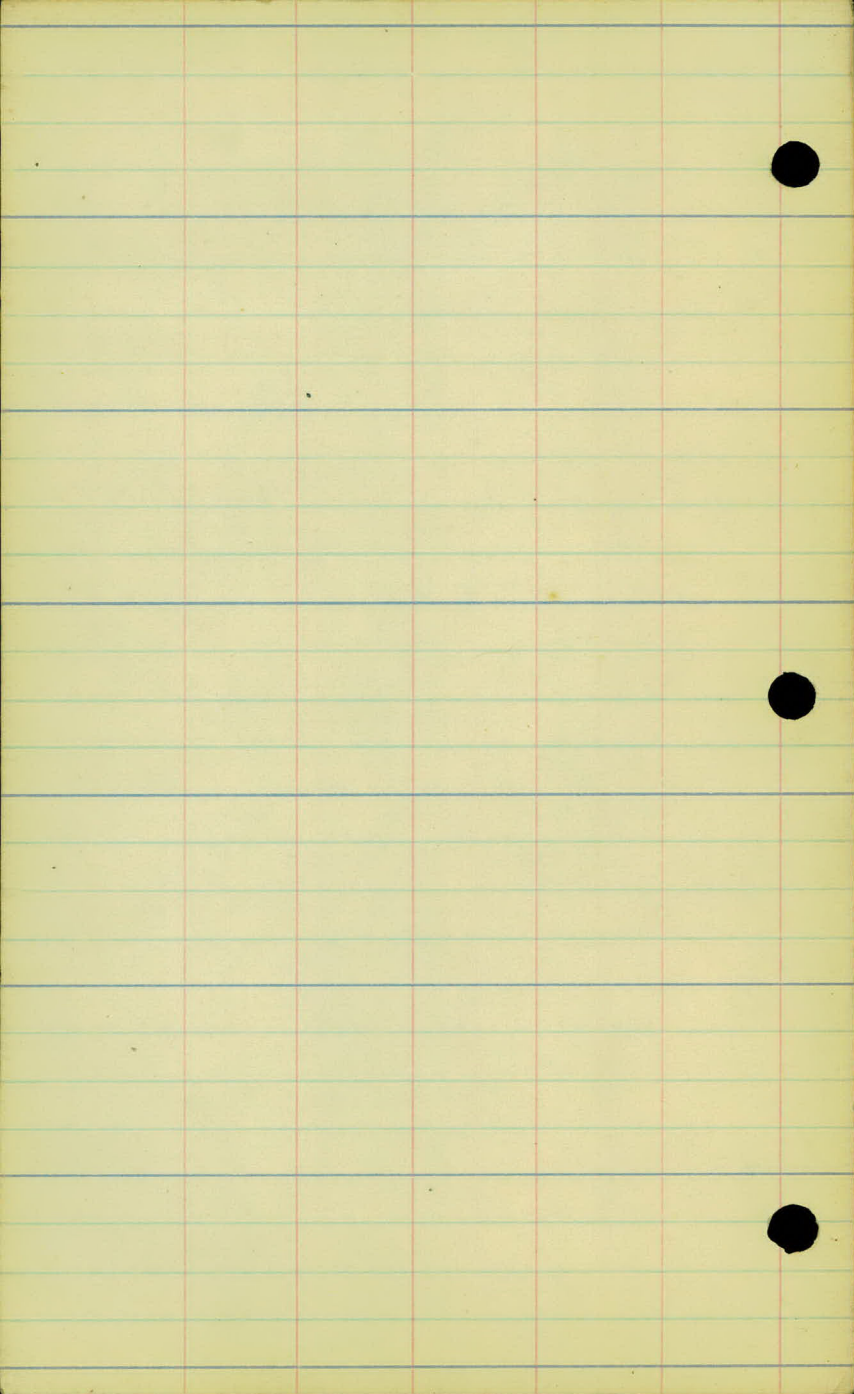
778 T.P. 27'

Marsh

Is Pond
oak brush & stumps

Stumps

20'



Surveyed on 7/30/27/16

Center Line Levels.

Proj - 24-52-Extension

Station	+	H. I	-	±lev.
				958.6 ✓
B.M.	6.26	964.88 ✓		958.52
148+50			11.7	53.2 ✓
149			6.0	58.9 ✓
+50			2.8	62.1 ✓
150			0.0	64.9 ✓
T.P.	9.80	974.50 ✓	0.18	964.70 ✓
+50			7.0	67.5 ✓
151			5.9	68.6 ✓
152			4.4	71.1 ✓
+60			3.7	70.8 ✓
153			3.1	71.4 ✓
T.P.	4.73	978.48 ✓	0.75	973.75 ✓
154			2.5	76.0 ✓
+50			1.1	77.4 ✓
155			2.9	75.6 ✓
+50			5.6	72.9 ✓
156			7.6	70.9 ✓
157			9.4	69.1 ✓
+60			8.9	69.6 ✓
158			7.4	71.1 ✓
+60			5.5	73.0 ✓
159			5.4	73.1 ✓
T.P.	4.48	977.42 ✓	5.54	972.94 ✓
+50			6.1	71.3 ✓
160			6.3	71.1 ✓

W.H.C.
Eck.
Gavin
Frank

17

July 29, 24

R.R. spike in 16" Oak 35' Lt. Sta. 149+00
(Iron sign on tree)

L. $\frac{1}{2}$ R

$\frac{1}{2}$ Drive Rt.

$\frac{5.0}{50}$

station	+	H.I	-	Elev.
		977.42 ✓		
160+50			54	973.0 ✓
161			46	72.8 ✓
162			46	72.8 ✓
+50			48	72.6 ✓
163			42	73.2 ✓
+50			2.3	75.1 ✓
T.P.	11.73	988.66 ✓	0.49	976.93 ✓
164			11.0	77.7 ✓
+50			8.2	80.5 ✓
B.M.			59.2	982.74 ✓
165			59	82.8 ✓
+50			3.9	84.7 ✓
166			1.2	87.5 ✓
T.P.	4.32	992.45 ✓	0.53	988.13 ✓
+50			3.3	89.2 ✓
167			3.3	89.2 ✓
+45			3.2	89.3 ✓
168			4.4	88.1 ✓
169			5.6	86.9 ✓
+50			5.9	86.6 ✓
170			6.6	85.9 ✓
+50			7.4	85.1 ✓
171			7.9	84.2 ✓
+50			8.6	83.9 ✓
172			9.1	83.4 ✓

84.7 84.8 ✓

R.R. spike 20" Oak 60' Lt. 164+85

Station	+	H.I.	-	Elev.
		992.45 ✓		
T.P.	3.80	987.40 ✓	8.85	983.60 ✓
173			5.0	82.4 ✓
174			5.5	81.9 ✓
+80			5.7	81.7 ✓
175			6.5	80.9 ✓
+12.1			6.6	80.8 ✓
176			4.2	83.2 ✓
B.M.			4.75	982.65 ✓
177			0.0	87.4 ✓
T.P.	11.31	998.51 ✓	0.20	987.20 ✓
178			6.5	92.0 ✓
179			4.0	94.5 ✓
180			2.1	96.4 ✓
T.P.	5.62	1003.69 ✓	0.50	998.01 ✓
181			4.6	99.1 ✓
182			2.3	1001.4 ✓
+80			2.1	1001.6 ✓
183			2.5	1001.2 ✓
184			8.5	95.2 ✓
T.P.	0.80	993.40 ✓	11.09	992.60 ✓
185			4.0	89.4 ✓
186			7.1	86.3 ✓
187			7.2	86.2 ✓
188			5.8	87.6 ✓
+14.1			5.5	87.9 ✓

VOID

P.I.

R.R. Spike in 24" Cott. 12' Lt. 175+80 { Line Revised
B.M. at Sta. 174+00

P.I.

station	+	H. I	-	E/ev.
		993.40 ✓		
B.M.	7.07	997.45 ✓	3.02	990.38 ✓
189			4.7	92.8 ✓
+70			1.6	95.9 ✓
190			1.7	95.8 ✓
+70			1.3	96.2 ✓
191			0.4	97.1 ✓
T.P.	7.46	1004.69 ✓	0.22	997.23 ✓
192			7.7	1004.0 ✓ / 1002.0 ✓
+50			2.2	1002.5 ✓
193			3.6	1001.1 ✓
+50			6.1	998.6 ✓
194			6.8	997.9 ✓
195			7.6	997.1 ✓
196			8.7	96.0 ✓
197			8.8	95.9 ✓
T.P.	7.00	1002.67 ✓	9.02	995.67 ✓
+85			6.6	96.1 ✓
198			8.5	94.2 ✓
+50			10.2	92.5 ✓
199			10.0	92.7 ✓
+55			6.8	95.9 ✓
200			6.3	96.4 ✓
+75			5.4	97.3 ✓
201			5.7	97.0 ✓
+30			6.4	96.3 ✓

R.R. Spike in T.P. Lt. Sta 188122

L. L. R.

85

6.7
Fres. Road

10.0

7.0
Fres. Road.

Station	+	H.I	-	Elev.
		1002.67 ✓		
201+70			9.0	993.7 ✓
202			11.4	991.3 ✓
135			10.6	992.1 ✓
160			9.0	993.7 ✓
173			9.4	993.3 ✓
B.M.	9.45	1003.73 ✓	8.19	994.48 ✓
			<u>48.58</u>	994.48 ✓
				45.86 ✓

Levels East on Long Lake Road

0+00 = 202+73			10.6	93.3 ✓
0+50			7.0	96.9 ✓
1+00			2.5	1001.4 ✓
1+30			0.0	1003.9 ✓

Levels West on Long Lake Road

B.M.	3.75	998.23 ✓		994.48 ✓
0+00 = 202+73				93.3 ✓
0+50			7.6	90.6 ✓
1+00			9.4	88.8 ✓
1+50			11.0	87.2 ✓
2+00			12.4	85.8 ✓

check Levels following page.

Checked
 RW
 7-30-24

& Long Lake Road.

R.R. spike in T.P. Rt. Sta 202+58

+ H.I - Elev.

Check-Levels

B.M.	7.60	1002.08		994.48
T.P.	9.54	1005.02	6.60	995.48
T.P.	0.53	993.78	11.77	993.25
B.M.			3.41	990.37 = 90.38
T.P.	11.46	1004.81	0.43	993.35
T.P.	0.40	996.06	9.15	995.66
T.P.	1.33	987.93	9.46	986.60
B.M.	4.61	987.24	5.30	982.63 = 87.65
T.P.	8.88	993.95	2.17	985.07
B.M.	2.89	985.63	11.21	982.74
T.P.	1.47	975.73	11.37	974.26
T.P.	8.34	978.65	5.42	970.31
T.P.	0.11	968.34	10.42	968.23
B.M.			9.75	958.59 = 52.62

W.H.C.
Eck
Galin
Flanke

July 29, 24

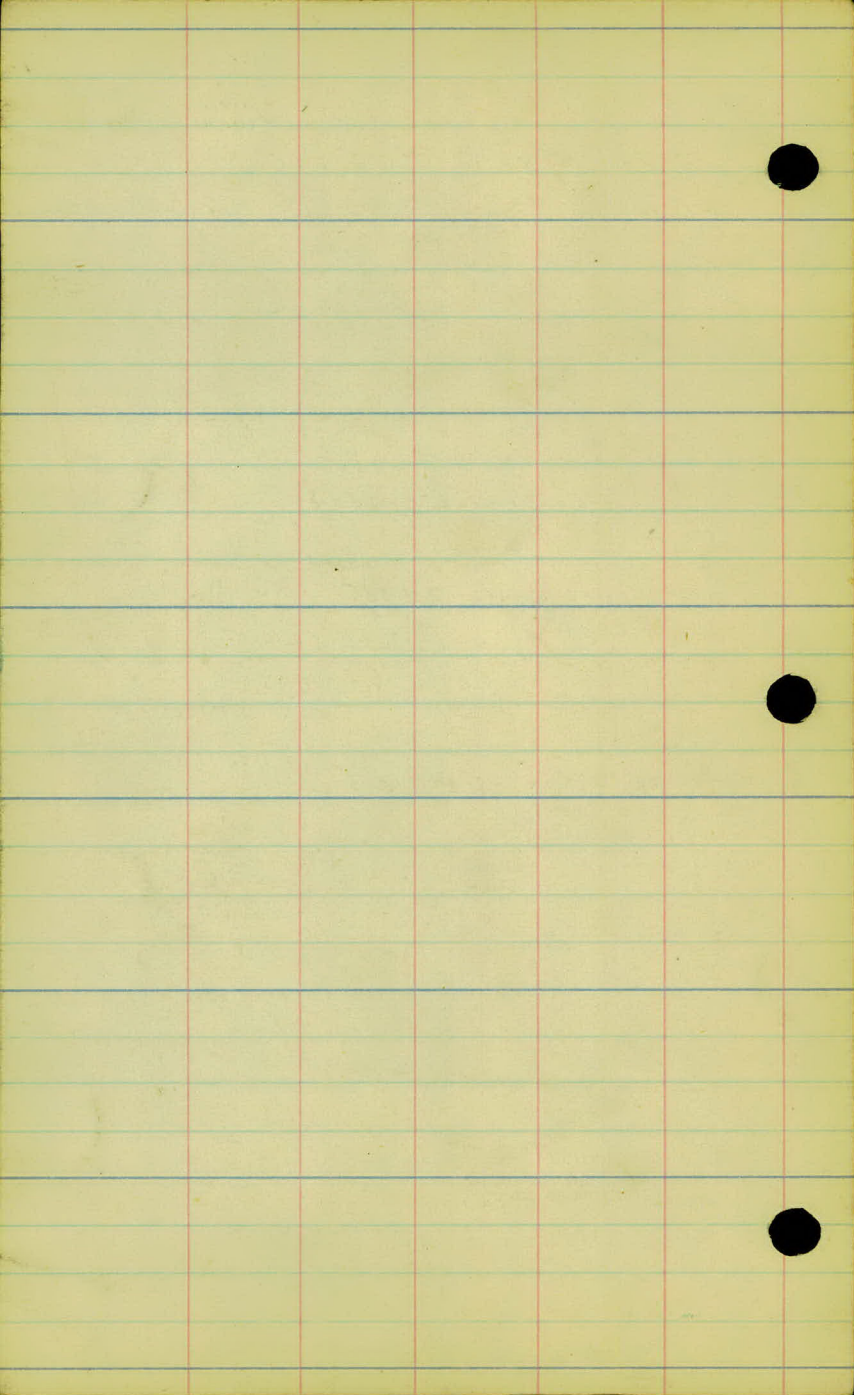
R.R. Spike in T.P. Rt. Sta. 202+58

R.R. Spike in T.P. Lt. Sta. 188+22

R.R. in 24" Co. H. 12' Lt. 175+80 $\left\{ \begin{array}{l} \text{Line Revised} \\ \text{E.M. Rt. Sta. 175+00} \end{array} \right.$

R.R. in 20" Oak 60' Lt. 164+85

R.R. Spike 16" Oak 35' Lt. 149+00



Cross Sections.

Proj. 24-52

Station

Elev.

155

75.6 ✓

+50

77.4 ✓

154

76.0 ✓

153

71.4 ✓

+60

10.6

70.8 ✓

152

70.1 ✓

151

68.6 ✓

+50

67.5 ✓

150

64.9 ✓

+50

62.1 ✓

149+00

58.9 ✓

148+65

-2.7

56.2 ✓

Lt.

E

Rt.

24

$$\begin{array}{r} -3.7 \\ \hline 33 \end{array} \quad \begin{array}{r} -2.2 \\ \hline 22 \end{array} \quad \begin{array}{r} -1.1 \\ \hline 17 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 14 \end{array} \quad \begin{array}{r} -0.4 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -0.2 \\ \hline 7 \end{array} \quad \begin{array}{r} -0.6 \\ \hline 10 \end{array} \quad \begin{array}{r} +2.1 \\ \hline 13 \end{array} \quad \begin{array}{r} +3.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 33 \end{array} \quad \begin{array}{r} +0.8 \\ \hline 12 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 14 \end{array}$$

$$\begin{array}{r} +0.1 \\ \hline 7 \end{array} \quad \begin{array}{r} +2.6 \\ \hline 13 \end{array} \quad \begin{array}{r} +2.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +1.1 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.0 \\ \hline 16 \end{array} \quad \begin{array}{r} -0.2 \\ \hline 10 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 9 \end{array} \quad \begin{array}{r} +0.6 \\ \hline 12 \end{array} \quad \begin{array}{r} -0.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.9 \\ \hline 33 \end{array} \quad \begin{array}{r} +0.4 \\ \hline 14 \end{array}$$

$$\begin{array}{r} +0.4 \\ \hline 8 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 13 \end{array} \quad \begin{array}{r} -0.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.7 \\ \hline 33 \end{array} \quad \begin{array}{r} -0.5 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 16 \end{array} \quad \begin{array}{r} -0.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +1.2 \\ \hline 33 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 15 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -1.5 \\ \hline 17 \end{array} \quad \begin{array}{r} -1.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +3.4 \\ \hline 33 \end{array} \quad \begin{array}{r} +2.2 \\ \hline 20 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 15 \end{array}$$

$$\begin{array}{r} -1.5 \\ \hline 19 \end{array} \quad \begin{array}{r} -1.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +2.1 \\ \hline 33 \end{array} \quad \begin{array}{r} +2.8 \\ \hline 18 \end{array} \quad \begin{array}{r} -1.1 \\ \hline 13 \end{array}$$

$$\begin{array}{r} -0.8 \\ \hline 19 \end{array} \quad \begin{array}{r} +0.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.2 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.4 \\ \hline 17 \end{array} \quad \begin{array}{r} -1.1 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -0.6 \\ \hline 18 \end{array} \quad \begin{array}{r} +2.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -2.2 \\ \hline 33 \end{array} \quad \begin{array}{r} -0.3 \\ \hline 17 \end{array} \quad \begin{array}{r} -1.3 \\ \hline 15 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 12 \end{array} \quad \begin{array}{r} -0.9 \\ \hline 19 \end{array} \quad \begin{array}{r} +0.2 \\ \hline 29 \end{array} \quad \begin{array}{r} +0.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.2 \\ \hline 16 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 12 \end{array} \quad \begin{array}{r} -0.9 \\ \hline 7 \end{array}$$

$$\begin{array}{r} -0.1 \\ \hline 13 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 18 \end{array} \quad \begin{array}{r} -1.3 \\ \hline 20 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 22 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.7 \\ \hline 35 \end{array} \quad \begin{array}{r} +1.4 \\ \hline 19 \end{array} \quad \begin{array}{r} -0.6 \\ \hline 16 \end{array} \quad \begin{array}{r} -1.4 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -0.6 \\ \hline 14 \end{array} \quad \begin{array}{r} +2.0 \\ \hline 17 \end{array} \quad \begin{array}{r} +2.1 \\ \hline 19 \end{array} \quad \begin{array}{r} +1.1 \\ \hline 33 \end{array}$$

(Head Level)

 W.H.C.
 F.C.
 Galvin
 Frank
 July 31, 1924

Station

Elev.

161 72.8 ✓

+50 72.0 ✓

160 71.1 ✓

+50 71.3 ✓

159 73.1 ✓

+60 -0.2 73.0 ✓

158 71.1 ✓

+60 -1.7 69.6 ✓

157 69.1 ✓

+55 +0.2 69.3 ✓

156 70.9 ✓

155+50 72.9 ✓

Lt.

E

Rt.

25

$$\begin{array}{r} -2.0 \\ 33 \end{array} \quad \begin{array}{r} -1.7 \\ 13 \end{array} \quad \begin{array}{r} -0.8 \\ 10 \end{array}$$

$$\begin{array}{r} -1.1 \\ 12 \end{array} \quad \begin{array}{r} -2.0 \\ 20 \end{array} \quad \begin{array}{r} -0.7 \\ 21 \end{array} \quad \begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{r} -0.6 \\ 33 \end{array} \quad \begin{array}{r} -0.6 \\ 70 \end{array} \quad \begin{array}{r} -0.2 \\ 13 \end{array} \quad \begin{array}{r} -0.1 \\ 12 \end{array}$$

$$\begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} -1.1 \\ 15 \end{array} \quad \begin{array}{r} +0.6 \\ 16 \end{array} \quad \begin{array}{r} -2.0 \\ 33 \end{array}$$

$$\begin{array}{r} -2.3 \\ 33 \end{array} \quad \begin{array}{r} -2.1 \\ 15 \end{array} \quad \begin{array}{r} -0.7 \\ 7 \end{array}$$

$$\begin{array}{r} -0.4 \\ 10 \end{array} \quad \begin{array}{r} -1.8 \\ 16 \end{array} \quad \begin{array}{r} -1.3 \\ 20 \end{array} \quad \begin{array}{r} -1.4 \\ 33 \end{array}$$

$$\begin{array}{r} -4.2 \\ 33 \end{array} \quad \begin{array}{r} -3.7 \\ 14 \end{array} \quad \begin{array}{r} -0.5 \\ 7 \end{array}$$

$$\begin{array}{r} -1.1 \\ 14 \end{array} \quad \begin{array}{r} -2.0 \\ 18 \end{array} \quad \begin{array}{r} -1.8 \\ 33 \end{array}$$

$$\begin{array}{r} -1.8 \\ 33 \end{array} \quad \begin{array}{r} -1.8 \\ 17 \end{array} \quad \begin{array}{r} -0.6 \\ 12 \end{array}$$

$$\begin{array}{r} -0.7 \\ 10 \end{array} \quad \begin{array}{r} +2.5 \\ 14 \end{array} \quad \begin{array}{r} +4.0 \\ 25 \end{array} \quad \begin{array}{r} +5.5 \\ 33 \end{array}$$

$$\begin{array}{r} +2.5 \\ 33 \end{array} \quad \begin{array}{r} +1.5 \\ 17 \end{array} \quad \begin{array}{r} -1.0 \\ 13 \end{array}$$

$$\begin{array}{r} -0.3 \\ 10 \end{array} \quad \begin{array}{r} +4.5 \\ 14 \end{array} \quad \begin{array}{r} +4.2 \\ 33 \end{array}$$

$$\begin{array}{r} +1.0 \\ 33 \end{array} \quad \begin{array}{r} +0.8 \\ 24 \end{array} \quad \begin{array}{r} +0.6 \\ 18 \end{array} \quad \begin{array}{r} -0.9 \\ 14 \end{array} \quad \begin{array}{r} -0.5 \\ 9 \end{array}$$

$$\begin{array}{r} -1.0 \\ 12 \end{array} \quad \begin{array}{r} +0.5 \\ 14 \end{array} \quad \begin{array}{r} -0.2 \\ 33 \end{array}$$

$$\begin{array}{r} +0.5 \\ 33 \end{array} \quad \begin{array}{r} 0.0 \\ 18 \end{array} \quad \begin{array}{r} -1.3 \\ 15 \end{array} \quad \begin{array}{r} -0.4 \\ 10 \end{array}$$

$$\begin{array}{r} -0.7 \\ 8 \end{array} \quad \begin{array}{r} -1.7 \\ 13 \end{array} \quad \begin{array}{r} -2.2 \\ 33 \end{array}$$

$$\begin{array}{r} -1.7 \\ 33 \end{array} \quad \begin{array}{r} -1.7 \\ 16 \end{array} \quad \begin{array}{r} -0.2 \\ 9 \end{array}$$

$$\begin{array}{r} -0.6 \\ 8 \end{array} \quad \begin{array}{r} -1.4 \\ 9 \end{array} \quad \begin{array}{r} -2.3 \\ 14 \end{array} \quad \begin{array}{r} -3.2 \\ 33 \end{array}$$

$$\begin{array}{r} -3.5 \\ 33 \end{array} \quad \begin{array}{r} -2.2 \\ 17 \end{array} \quad \begin{array}{r} -0.2 \\ 9 \end{array}$$

$$\begin{array}{r} -0.3 \\ 7 \end{array} \quad \begin{array}{r} -1.5 \\ 11 \end{array} \quad \begin{array}{r} -2.0 \\ 33 \end{array}$$

$$\begin{array}{r} -3.2 \\ 33 \end{array} \quad \begin{array}{r} -3.2 \\ 17 \end{array} \quad \begin{array}{r} -0.8 \\ 10 \end{array} \quad \begin{array}{r} -0.5 \\ 8 \end{array}$$

$$\begin{array}{r} -0.5 \\ 10 \end{array} \quad \begin{array}{r} 0.0 \\ 15 \end{array} \quad \begin{array}{r} +0.3 \\ 23 \end{array} \quad \begin{array}{r} +1.0 \\ 33 \end{array}$$

$$\begin{array}{r} -1.8 \\ 33 \end{array} \quad \begin{array}{r} -1.7 \\ 20 \end{array} \quad \begin{array}{r} -0.8 \\ 14 \end{array} \quad \begin{array}{r} -0.4 \\ 9 \end{array}$$

$$\begin{array}{r} -0.5 \\ 10 \end{array} \quad \begin{array}{r} +1.8 \\ 16 \end{array} \quad \begin{array}{r} +3.0 \\ 33 \end{array}$$

Station

Elev.

168

88.1 ✓

167

89.2 ✓

+50

89.2 ✓

166

87.5 ✓

+50

84.8 ✓

165

82.8 ✓

+50

80.5 ✓

164

77.7 ✓

+50

-3.2

74.5 ✓

163

73.2 ✓

+50

-1.0

72.6 ✓

162

72.8 ✓

Lt.

L

Rt.

26

$$\frac{-1.1}{33} \quad \frac{-1.0}{18} \quad \frac{-1.0}{11}$$

$$\frac{-0.6}{12} \quad \frac{0.0}{14} \quad \frac{+1.2}{33}$$

$$\frac{-2.0}{33} \quad \frac{-1.2}{12}$$

$$\frac{-0.4}{12} \quad \frac{+0.3}{14} \quad \frac{+1.0}{33}$$

$$\frac{-1.0}{33} \quad \frac{-0.9}{22} \quad \frac{-1.5}{13}$$

$$\frac{-0.6}{12} \quad \frac{+0.4}{14} \quad \frac{+0.8}{33}$$

$$\frac{-0.5}{33} \quad \frac{-0.2}{26} \quad \frac{-0.6}{17} \quad \frac{-1.5}{16}$$

$$\frac{-0.5}{10} \quad \frac{0.0}{18} \quad \frac{0.0}{33}$$

$$\frac{+0.4}{33} \quad \frac{+0.5}{26} \quad \frac{-1.0}{16}$$

$$\frac{-0.4}{8} \quad \frac{-0.8}{12} \quad \frac{-1.2}{33}$$

$$\frac{-1.0}{33} \quad \frac{-0.3}{24} \quad \frac{-0.9}{13}$$

$$\frac{-1.4}{12} \quad \frac{-0.9}{33}$$

$$\frac{+1.0}{33} \quad \frac{+1.0}{24} \quad \frac{-0.8}{13}$$

$$\frac{-1.0}{10} \quad \frac{-1.1}{12} \quad \frac{+0.2}{17} \quad \frac{-0.3}{33}$$

$$\frac{+5.8}{33} \quad \frac{+5.2}{16} \quad \frac{-1.1}{12}$$

$$\frac{-0.8}{11} \quad \frac{-1.5}{13} \quad \frac{+1.0}{17} \quad \frac{+5.2}{21} \quad \frac{+5.0}{33}$$

$$\frac{-1.1}{33} \quad \frac{-0.7}{14}$$

$$\frac{-0.8}{11} \quad \frac{-0.9}{18} \quad \frac{0.0}{20} \quad \frac{+1.0}{33}$$

$$\frac{-5.2}{33} \quad \frac{-5.2}{25} \quad \frac{-2.0}{17} \quad \frac{-0.6}{10}$$

$$\frac{-0.6}{7} \quad \frac{-2.2}{14} \quad \frac{-4.4}{19} \quad \frac{-4.8}{33}$$

$$\frac{-5.0}{33} \quad \frac{-3.3}{18} \quad \frac{-0.5}{10}$$

$$\frac{-1.2}{10} \quad \frac{-1.9}{14} \quad \frac{+0.7}{17} \quad \frac{+1.0}{33}$$

$$\frac{-1.5}{33} \quad \frac{-1.8}{13} \quad \frac{-0.9}{9}$$

$$\frac{+1.0}{12} \quad \frac{-1.1}{16} \quad \frac{-0.7}{19} \quad \frac{+0.3}{33}$$

Station

Elev.

175+12

80.8 ✓

175+00

80.9 ✓

+79

~~80.4~~

81.3 ✓

174

81.9 ✓

173

82.4 ✓

172

83.4 ✓

+50

83.9 ✓

171

84.6 ✓

+50

85.1 ✓

170

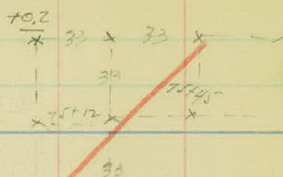
85.9 ✓

+50

86.6 ✓

169

86.9 ✓



Plan of X-sections

@ P.I.

Same @ Sta. 188+14

E.
 $\frac{-1.8}{33}$ $\frac{-0.5}{13}$

W.
~~2 Road.~~

~~E.~~
 ~~$\frac{-2.0}{33}$ $\frac{-1.2}{13}$ $\frac{-0.5}{7}$~~

~~W.~~
 ~~$\frac{-0.2}{15}$ $\frac{-0.2}{17}$ $\frac{-0.9}{22}$ $\frac{-1.0}{33}$~~

~~$\frac{-2.0}{33}$ $\frac{-1.9}{14}$ $\frac{-0.8}{8}$~~

~~$\frac{-0.2}{5}$ $\frac{-0.9}{11}$ $\frac{-0.4}{33}$~~

~~$\frac{-3.4}{33}$ $\frac{-2.0}{17}$ $\frac{-1.1}{13}$~~

~~$\frac{-0.9}{13}$ $\frac{0.0}{15}$ $\frac{+0.8}{33}$~~

~~$\frac{-3.0}{33}$ $\frac{-1.7}{18}$ $\frac{-0.9}{10}$~~

~~$\frac{-0.3}{8}$ $\frac{-1.2}{12}$ $\frac{-0.3}{14}$ $\frac{-0.0}{33}$~~

~~$\frac{-2.1}{33}$ $\frac{-0.3}{13}$~~

~~$\frac{-0.7}{12}$ $\frac{-0.0}{14}$ $\frac{+0.3}{33}$~~

~~$\frac{-1.7}{33}$ $\frac{-0.4}{10}$~~

~~$\frac{-0.3}{8}$ $\frac{-0.9}{13}$ $\frac{0.0}{15}$ $\frac{+0.2}{33}$~~

~~$\frac{-1.3}{33}$ $\frac{-1.0}{18}$ $\frac{-0.5}{12}$~~

~~$\frac{-0.2}{16}$ $\frac{+0.3}{18}$ $\frac{+0.1}{33}$~~

~~$\frac{-2.0}{33}$ $\frac{-0.9}{14}$ $\frac{-0.6}{8}$~~

~~$\frac{+0.1}{11}$ $\frac{-0.6}{16}$ $\frac{+0.6}{17}$ $\frac{+0.6}{33}$~~

~~$\frac{-1.5}{33}$ $\frac{-1.5}{20}$ $\frac{-1.1}{11}$~~

~~$\frac{-0.3}{12}$ $\frac{+0.7}{14}$ $\frac{-0.6}{33}$~~

~~$\frac{-1.6}{33}$ $\frac{-1.4}{20}$ $\frac{-1.1}{11}$~~

~~$\frac{-0.7}{12}$ $\frac{0.0}{14}$ $\frac{+0.5}{33}$~~

Station		Elev.
+40	-3.2	92.0 ✓
184		95.2 ✓
+50	-3.5	97.7 ✓
183		101.2 ✓
182		1001.4 ✓
181		99.1 ✓
180		96.4
179		94.5
178		92.0 ✓
177		87.4 ✓
176		83.2 ✓
175+45	+0.5	81.3 80.6
175+12		80.8

Lt.

L

Rt.

$$\frac{-2.0}{33}$$

$$\frac{-0.5}{12}$$

$$\frac{-0.4}{12}$$

$$\frac{+1.8}{17}$$

$$\frac{+3.0}{33}$$

$$\frac{0.0}{33}$$

$$\frac{+1.0}{20}$$

$$\frac{0.0}{15}$$

$$\frac{-0.2}{8}$$

$$\frac{+3.1}{17}$$

$$\frac{+4.5}{33}$$

$$\frac{+2.0}{33}$$

$$\frac{+2.1}{17}$$

$$\frac{0.0}{13}$$

$$\frac{-0.2}{7}$$

$$\frac{+0.2}{11}$$

$$\frac{+3.0}{18}$$

$$\frac{+3.4}{33}$$

$$\frac{+0.6}{33}$$

$$\frac{+0.7}{20}$$

$$\frac{+1.1}{15}$$

$$\frac{-0.5}{13}$$

$$\frac{0.0}{8}$$

$$\frac{-0.3}{5}$$

$$\frac{0.0}{13}$$

$$\frac{+0.9}{18}$$

$$\frac{+1.0}{33}$$

$$\frac{0.0}{33}$$

$$\frac{-0.2}{18}$$

$$\frac{-0.5}{8}$$

$$\frac{0.0}{7}$$

$$\frac{-0.6}{12}$$

$$\frac{-1.4}{17}$$

$$\frac{-2.7}{33}$$

$$\frac{+2.6}{33}$$

$$\frac{+2.3}{20}$$

$$\frac{+1.9}{12}$$

$$\frac{+0.3}{9}$$

$$\frac{-0.2}{9}$$

$$\frac{-1.1}{14}$$

$$\frac{+2.0}{33}$$

$$\frac{+2.7}{33}$$

$$\frac{+1.6}{20}$$

$$\frac{+1.4}{12}$$

$$\frac{+0.4}{9}$$

$$\frac{+0.1}{5}$$

$$\frac{+0.2}{7}$$

$$\frac{-0.9}{12}$$

$$\frac{-2.2}{33}$$

$$\frac{+2.5}{33}$$

$$\frac{+1.6}{18}$$

$$\frac{+1.4}{12}$$

$$\frac{-0.1}{7}$$

$$\frac{+0.2}{7}$$

$$\frac{-0.8}{12}$$

$$\frac{-2.0}{33}$$

$$\frac{+2.7}{33}$$

$$\frac{+2.4}{20}$$

$$\frac{+2.2}{14}$$

$$\frac{+0.5}{11}$$

$$\frac{-0.4}{7}$$

$$\frac{0.0}{6}$$

$$\frac{+0.4}{8}$$

$$\frac{-0.3}{14}$$

$$\frac{-1.0}{33}$$

$$\frac{+2.3}{33}$$

$$\frac{+1.5}{14}$$

$$\frac{+1.5}{12}$$

$$\frac{0.0}{10}$$

$$\frac{0.0}{7}$$

$$\frac{0.0}{7}$$

$$\frac{+0.4}{9}$$

$$\frac{-1.0}{13}$$

$$\frac{-1.5}{33}$$

$$\frac{-0.5}{33}$$

$$\frac{-1.2}{14}$$

$$\frac{+0.5}{3}$$

$$\frac{-0.8}{18}$$

$$\frac{-1.4}{33}$$

$$\frac{-0.5}{33}$$

$$\frac{-0.5}{14}$$

$$\frac{-0.6}{14}$$

$$\frac{+0.4}{7}$$

$$\frac{0.0}{17}$$

$$\frac{-0.2}{22}$$

$$\frac{-1.0}{33}$$

= same as

7A19-33' RT

N.

S.

$$\frac{4.0}{33}$$

$$\frac{+0.6}{14}$$

- - 2' Road - -

Station	Elev.
+50	+17 → 94.5 ✓
189	→ 92.8 ✓
188+47	+14 → 89.3 ✓
188+14	→ 87.9 ✓
188+14	→ 87.9 ✓
187+81	-12 → 86.7 ✓
+37	-12 → 85.0 ✓
187	→ 86.2 ✓
+50	-1.0 → 85.3 ✓
186	→ 86.3 ✓
+60	+0.4 → 86.7 ✓
+18	-1.0 → 88.4 ✓
185	→ 89.4 ✓

100

Lt. £ Rt.

$\frac{-0.5}{33}$	$\frac{-1.6}{18}$	$\frac{-0.8}{15}$	$\frac{-0.9}{10}$	$\frac{-0.7}{9}$	$\frac{+2.9}{13}$	$\frac{+3.2}{33}$
-------------------	-------------------	-------------------	-------------------	------------------	-------------------	-------------------

$\frac{+0.2}{33}$	$\frac{+2.6}{12}$	$\frac{0.0}{8}$	$\frac{-0.6}{13}$	$\frac{-0.5}{33}$
-------------------	-------------------	-----------------	-------------------	-------------------

W. E.

3 amo 22 18781
32 Lt.

$\frac{+0.7}{33}$	$\frac{+0.9}{17}$	$\frac{-1.2}{13}$	$\frac{0.0}{14}$	$\frac{-0.3}{23}$	$\frac{-0.5}{33}$
-------------------	-------------------	-------------------	------------------	-------------------	-------------------

W. E



$\frac{0.0}{17}$	$\frac{+0.2}{33}$
------------------	-------------------

N S (187114) S.E. $\frac{-0.6}{46}$

$\frac{-0.5}{4}$	$\frac{-1.5}{8}$	$\frac{-3.2}{33}$
------------------	------------------	-------------------

N S

$\frac{+3.5}{33}$	$\frac{+1.5}{24}$	$\frac{0.0}{18}$	$\frac{1.0}{9}$	$\frac{-3.2}{12}$	$\frac{-5.0}{33}$
-------------------	-------------------	------------------	-----------------	-------------------	-------------------

$\frac{+2.0}{33}$	$\frac{+2.9}{18}$	$\frac{-0.5}{4}$	$\frac{0.0}{6}$	$\frac{-0.2}{5}$	$\frac{-1.9}{8}$	$\frac{-5.5}{33}$
-------------------	-------------------	------------------	-----------------	------------------	------------------	-------------------

$\frac{-2.8}{33}$	$\frac{-1.0}{25}$	$\frac{+1.8}{15}$	$\frac{-0.5}{12}$	$\frac{-0.3}{7}$	$\frac{-1.8}{13}$	$\frac{-4.8}{33}$
-------------------	-------------------	-------------------	-------------------	------------------	-------------------	-------------------

$\frac{-7.2}{33}$	$\frac{-5.0}{25}$	$\frac{1.1}{9}$	$\frac{-0.7}{7}$	$\frac{-2.6}{7}$	$\frac{-4.5}{33}$
-------------------	-------------------	-----------------	------------------	------------------	-------------------

$\frac{-14.0}{33}$	$\frac{-12.0}{27}$	$\frac{-5.0}{14}$	$\frac{-1.7}{10}$	$\frac{-0.4}{6}$	$\frac{-1.1}{10}$	$\frac{-3.2}{17}$	$\frac{-4.8}{33}$
--------------------	--------------------	-------------------	-------------------	------------------	-------------------	-------------------	-------------------

$\frac{-15.0}{20.0}$	$\frac{-12.0}{33}$	$\frac{-5.0}{12}$	$\frac{-0.2}{8}$	$\frac{-0.8}{8}$	$\frac{-2.1}{16}$	$\frac{-2.5}{33}$
----------------------	--------------------	-------------------	------------------	------------------	-------------------	-------------------

$\frac{-0.7}{33}$	$\frac{+0.5}{19}$	$\frac{-1.1}{15}$	$\frac{-0.4}{10}$	$\frac{-0.6}{8}$	$\frac{-1.2}{24}$	$\frac{-1.0}{33}$
-------------------	-------------------	-------------------	-------------------	------------------	-------------------	-------------------

$\frac{+4.1}{33}$	$\frac{+4.0}{22}$	$\frac{-0.5}{14}$	$\frac{0.0}{9}$	$\frac{-0.3}{8}$	$\frac{-0.8}{24}$	$\frac{-0.3}{33}$
-------------------	-------------------	-------------------	-----------------	------------------	-------------------	-------------------

Station

Elev.:

197

95.9 ✓

+50

-1.4

94.6 ✓

196

96.0 ✓

195

97.1 ✓

+60

-1.2

~~96.7~~

194

97.9 ✓

+50

-3.3

98.6 ✓

193

01.1 ✓

+50

-0.6

02.5 ✓

192

02.0 ✓

+50

+1.8

38.9 ✓

191

97.1 ✓

+50

-0.8

95.0 ✓

190

95.8 ✓

Lt.

E

Rt.

$$\begin{array}{r} -7.0 \\ 33 \end{array} \quad \begin{array}{r} -3.9 \\ 20 \end{array} \quad \begin{array}{r} -0.2 \\ 8 \end{array}$$

$$\begin{array}{r} -0.3 \\ 9 \end{array} \quad \begin{array}{r} +5.0 \\ 15 \end{array} \quad \begin{array}{r} +8.2 \\ 20 \end{array} \quad \begin{array}{r} +8.3 \\ 33 \end{array}$$

$$\begin{array}{r} -5.3 \\ 32 \end{array} \quad \begin{array}{r} -4.0 \\ 17 \end{array} \quad \begin{array}{r} -0.1 \\ 7 \end{array}$$

$$\begin{array}{r} -0.2 \\ 7 \end{array} \quad \begin{array}{r} -0.5 \\ 10 \end{array} \quad \begin{array}{r} +2.1 \\ 23 \end{array} \quad \begin{array}{r} +2.1 \\ 33 \end{array}$$

$$\begin{array}{r} -5.2 \\ 33 \end{array} \quad \begin{array}{r} -1.1 \\ 15 \end{array} \quad \begin{array}{r} -0.4 \\ 10 \end{array} \quad \begin{array}{r} +0.3 \\ 2 \end{array}$$

$$\begin{array}{r} +0.2 \\ 10 \end{array} \quad \begin{array}{r} +1.8 \\ 12 \end{array} \quad \begin{array}{r} +2.2 \\ 17 \end{array} \quad \begin{array}{r} +2.2 \\ 33 \end{array}$$

$$\begin{array}{r} -2.8 \\ 33 \end{array} \quad \begin{array}{r} -1.1 \\ 16 \end{array} \quad \begin{array}{r} 0.0 \\ 11 \end{array} \quad \begin{array}{r} +0.5 \\ 5 \end{array}$$

$$\begin{array}{r} +0.5 \\ 7 \end{array} \quad \begin{array}{r} +1.1 \\ 8 \end{array} \quad \begin{array}{r} +1.9 \\ 16 \end{array} \quad \begin{array}{r} +1.9 \\ 33 \end{array}$$

$$\begin{array}{r} -2.6 \\ 33 \end{array} \quad \begin{array}{r} -1.5 \\ 16 \end{array} \quad \begin{array}{r} -0.5 \\ 13 \end{array} \quad \begin{array}{r} +0.4 \\ 5 \end{array}$$

$$\begin{array}{r} +0.3 \\ 4 \end{array} \quad \begin{array}{r} -1.1 \\ 6 \end{array} \quad \begin{array}{r} -1.2 \\ 16 \end{array} \quad \begin{array}{r} -1.4 \\ 33 \end{array}$$

$$\begin{array}{r} -4.8 \\ 33 \end{array} \quad \begin{array}{r} -1.6 \\ 17 \end{array} \quad \begin{array}{r} -0.1 \\ 13 \end{array} \quad \begin{array}{r} +0.6 \\ 5 \end{array}$$

$$\begin{array}{r} 0.0 \\ 3 \end{array} \quad \begin{array}{r} 3.2 \\ 5 \end{array} \quad \begin{array}{r} 4.1 \\ 20 \end{array} \quad \begin{array}{r} -4.1 \\ 33 \end{array}$$

$$\begin{array}{r} -2.5 \\ 33 \end{array} \quad \begin{array}{r} -0.8 \\ 18 \end{array} \quad \begin{array}{r} 0.0 \\ 13 \end{array} \quad \begin{array}{r} +0.6 \\ 6 \end{array}$$

$$\begin{array}{r} -0.1 \\ 4 \end{array} \quad \begin{array}{r} 0.0 \\ 15 \end{array} \quad \begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{r} -2.0 \\ 32 \end{array} \quad \begin{array}{r} +0.6 \\ 18 \end{array} \quad \begin{array}{r} -0.2 \\ 16 \end{array} \quad \begin{array}{r} +0.6 \\ 10 \end{array} \quad \begin{array}{r} +0.4 \\ 9 \end{array}$$

$$\begin{array}{r} +0.3 \\ 6 \end{array} \quad \begin{array}{r} +4.6 \\ 9 \end{array} \quad \begin{array}{r} +5.0 \\ 20 \end{array} \quad \begin{array}{r} +5.6 \\ 33 \end{array}$$

$$\begin{array}{r} -0.1 \\ 33 \end{array} \quad \begin{array}{r} +1.3 \\ 18 \end{array} \quad \begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} +0.5 \\ 5 \end{array}$$

$$\begin{array}{r} 0.0 \\ 6 \end{array} \quad \begin{array}{r} +3.5 \\ 9 \end{array} \quad \begin{array}{r} +4.6 \\ 20 \end{array} \quad \begin{array}{r} +4.6 \\ 33 \end{array}$$

$$\begin{array}{r} +1.8 \\ 33 \end{array} \quad \begin{array}{r} +1.8 \\ 18 \end{array} \quad \begin{array}{r} +0.5 \\ 16 \end{array} \quad \begin{array}{r} -0.3 \\ 13 \end{array} \quad \begin{array}{r} +0.5 \\ 5 \end{array}$$

$$\begin{array}{r} -0.4 \\ 6 \end{array} \quad \begin{array}{r} +2.6 \\ 10 \end{array} \quad \begin{array}{r} +3.0 \\ 18 \end{array} \quad \begin{array}{r} +3.0 \\ 33 \end{array}$$

$$\begin{array}{r} +1.0 \\ 33 \end{array} \quad \begin{array}{r} +0.8 \\ 17 \end{array} \quad \begin{array}{r} 0.0 \\ 15 \end{array} \quad \begin{array}{r} -0.3 \\ 9 \end{array}$$

$$\begin{array}{r} -0.4 \\ 8 \end{array} \quad \begin{array}{r} +0.9 \\ 11 \end{array} \quad \begin{array}{r} +0.9 \\ 20 \end{array} \quad \begin{array}{r} +0.9 \\ 33 \end{array}$$

$$\begin{array}{r} -1.3 \\ 33 \end{array} \quad \begin{array}{r} -1.4 \\ 16 \end{array} \quad \begin{array}{r} -0.5 \\ 11 \end{array}$$

$$\begin{array}{r} -0.7 \\ 9 \end{array} \quad \begin{array}{r} -0.7 \\ 20 \end{array} \quad \begin{array}{r} -1.0 \\ 33 \end{array}$$

$$\begin{array}{r} -4.8 \\ 33 \end{array} \quad \begin{array}{r} -4.2 \\ 20 \end{array} \quad \begin{array}{r} -0.5 \\ 10 \end{array} \quad \begin{array}{r} +0.2 \\ 2 \end{array}$$

$$\begin{array}{r} -1.1 \\ 7 \end{array} \quad \begin{array}{r} -2.6 \\ 12 \end{array} \quad \begin{array}{r} -3.1 \\ 19 \end{array} \quad \begin{array}{r} -3.0 \\ 33 \end{array}$$

$$\begin{array}{r} -6.0 \\ 33 \end{array} \quad \begin{array}{r} -4.4 \\ 25 \end{array} \quad \begin{array}{r} -0.8 \\ 16 \end{array} \quad \begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} +0.2 \\ 3 \end{array}$$

$$\begin{array}{r} +0.2 \\ 9 \end{array} \quad \begin{array}{r} +3.6 \\ 12 \end{array} \quad \begin{array}{r} +4.8 \\ 20 \end{array} \quad \begin{array}{r} +5.5 \\ 33 \end{array}$$

Station

Elev.

202+73

93.3 ✓

+41

-12

92.1 ✓

202

91.3 ✓

+70

-3.1

93.7 ✓

+37

-1.7

95.3 ✓

201

97.9 ✓

+43

-0.3

96.1 ✓

200

96.4 ✓

+50

-1.8

94.6 ✓

199

92.7 ✓

198

94.2 ✓

+80

+22

96.4 ✓

197+40

0.0

95.9 ✓

197

Lt. R Rt.

$$\frac{-2.2}{33}$$

$$\frac{+1.8}{33}$$

$$\frac{-1.1}{33}$$

$$\frac{+0.4}{13}$$

$$\frac{-0.7}{6}$$

$$\frac{-1.0}{33}$$

$$\frac{+0.5}{33}$$

$$\frac{+0.2}{27}$$

$$\frac{+1.4}{13}$$

$$\frac{+0.9}{7}$$

$$\frac{-0.9}{33}$$

$$\frac{+2.8}{33}$$

$$\frac{-0.8}{19}$$

$$\frac{+0.6}{8}$$

$$\frac{-2.5}{8}$$

$$\frac{-2.5}{33}$$

$$\frac{+2.8}{33}$$

$$\frac{+2.3}{20}$$

$$\frac{+1.7}{10}$$

$$\frac{-0.7}{11}$$

$$\frac{-0.6}{8}$$

$$\frac{-2.8}{18}$$

$$\frac{-3.2}{21}$$

$$\frac{-4.0}{33}$$

$$\frac{+0.5}{33}$$

$$\frac{+1.1}{8}$$

$$\frac{+2.8}{10}$$

$$\frac{-0.3}{7}$$

$$\frac{+0.4}{3}$$

$$\frac{+0.5}{18}$$

$$\frac{+6.3}{20}$$

$$\frac{+6.9}{33}$$

$$\frac{+0.2}{33}$$

$$\frac{-1.5}{15}$$

$$\frac{-1.2}{7}$$

$$\frac{+0.6}{6}$$

$$\frac{-0.2}{20}$$

$$\frac{+2.2}{23}$$

$$\frac{+3.5}{28}$$

$$\frac{+5.0}{33}$$

$$\frac{0.0}{33}$$

$$\frac{-1.0}{15}$$

$$\frac{-0.9}{4}$$

$$\frac{+0.8}{8}$$

$$\frac{+0.2}{19}$$

$$\frac{+2.4}{21}$$

$$\frac{+4.9}{33}$$

$$\frac{+0.8}{33}$$

$$\frac{-0.7}{18}$$

$$\frac{-0.5}{8}$$

$$\frac{+0.7}{10}$$

$$\frac{-10.2}{19}$$

$$\frac{+4.2}{24}$$

$$\frac{-5.7}{33}$$

$$\frac{-1.5}{33}$$

$$\frac{-1.0}{15}$$

$$\frac{+2.5}{7}$$

$$\frac{+2.8}{13}$$

$$\frac{+3.0}{26}$$

$$\frac{+6.0}{33}$$

$$\frac{3.4}{33}$$

$$\frac{-1.3}{10}$$

$$\frac{+1.6}{4}$$

$$\frac{+1.9}{9}$$

$$\frac{+1.2}{20}$$

$$\frac{+2.8}{23}$$

$$\frac{+4.1}{28}$$

$$\frac{+4.1}{33}$$

$$\frac{-5.2}{33}$$

$$\frac{-3.2}{11}$$

$$\frac{+0.2}{6}$$

$$\frac{0.0}{15}$$

$$\frac{-13.4}{19}$$

$$\frac{-15.2}{28}$$

$$\frac{+1.2}{33}$$

$$\frac{-3.5}{33}$$

$$\frac{+0.1}{11}$$

$$\frac{-0.8}{8}$$

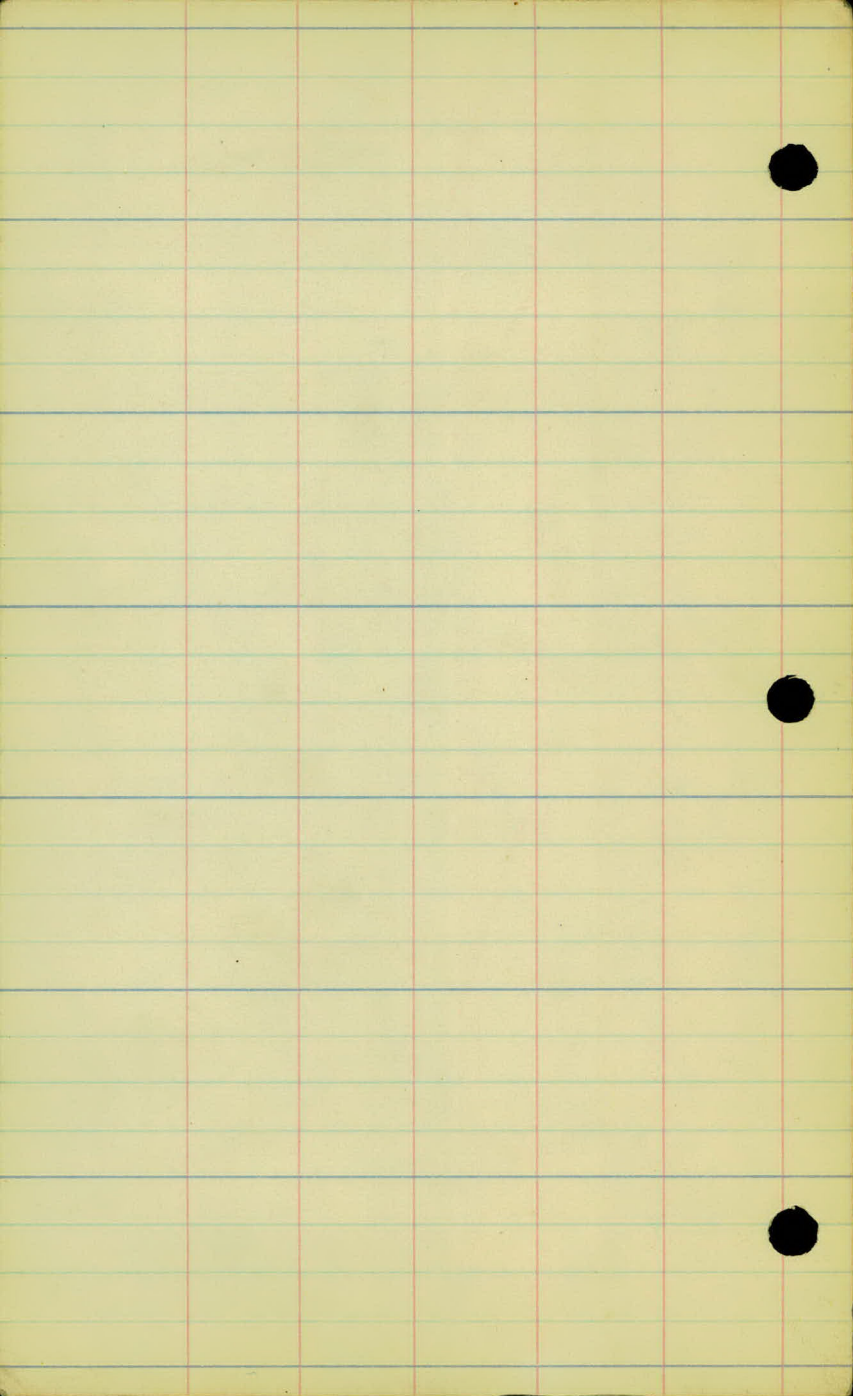
$$\frac{+0.3}{8}$$

$$\frac{0.0}{10}$$

$$\frac{+5.0}{24}$$

$$\frac{+1.00}{23}$$

$$\frac{+10.5}{33}$$



Drainage

Proj. 24-52

Station Present Cully Rec'd Cully.

159+72 12" x 73' Vit
Ext. 14.5 R. + 8.5 L.

174+78 12" x 285 C.M.
Ext. 19' R. 9.5 L.

Note: Not near Revised Line!

202+75 12" x 30' C.M.
200+82
Rev. Aug 24 Ext.

W.H.C.
Eck.
Galvin
Franke } July 31, 1924

Inv. Elev. - 3.1 - Elev. 160

Drains L. to Lake

Inv. Elev. - 2.1 & Elev. Sta. 175

Drains. L.

Inv. Elev. - 3.2 & Elev. Sta 204178

Drains. L. End of Pipe 6' Lt. of L.

1787

1917

Line Revision

Proj. 24-52

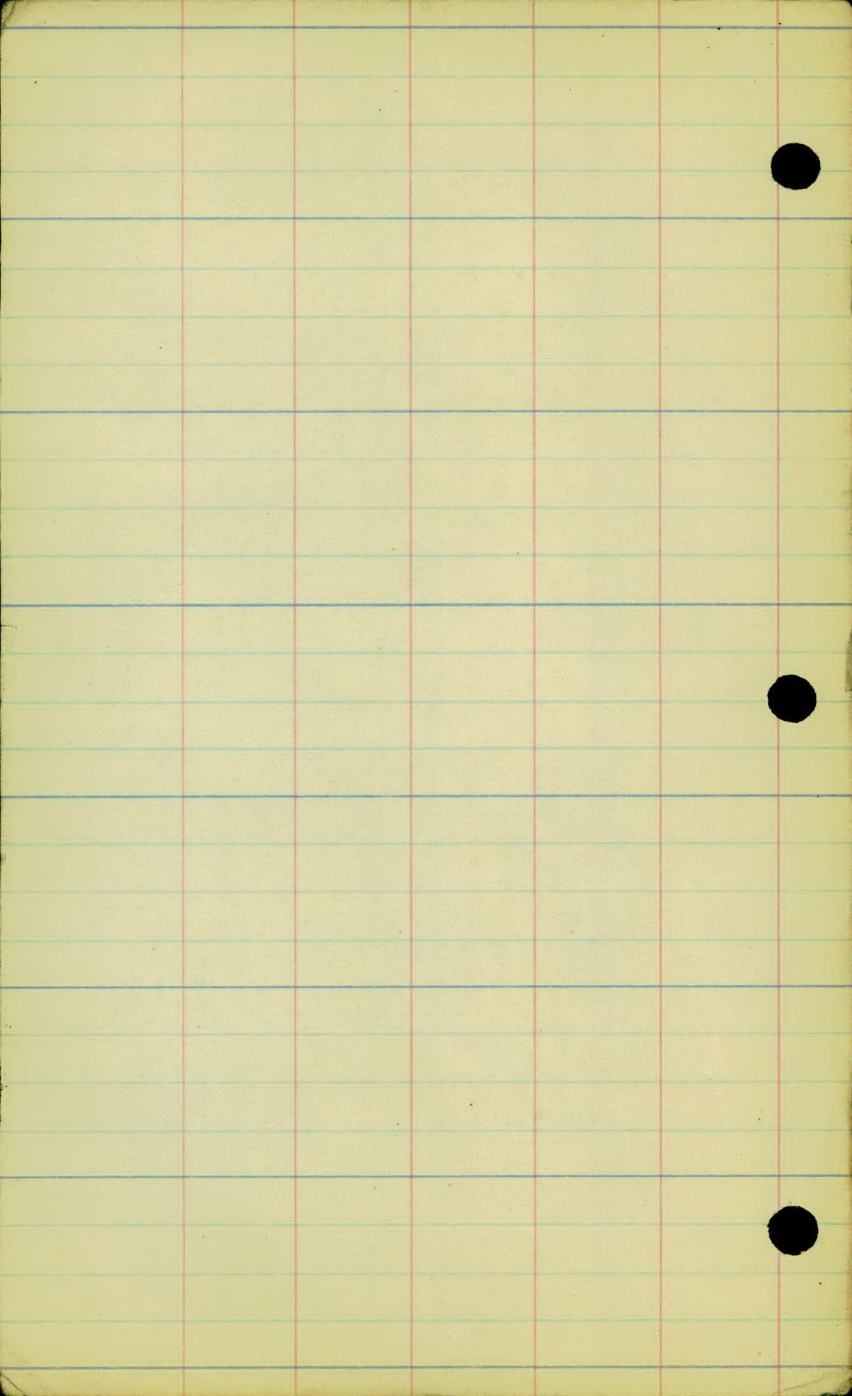
Sta. 172+98¹⁵ to 200+85.6

Index

Alignment	1	3
Art. Topog.	4	9
E Levels	10	13
X-sections	15	19

Aug 9 - 1924

Office of Ramsey Co. Engineer
ST. PAUL, MINN.
Date Filed 8/19/24
File No. "11" (24-52)



1

Line Revision

Proj. 24-52

Alignment.

Aug 8, 1924

Station Point L R Bear.

N. 88° 32' E ✓

180+63.2 ^{1812?} P.O.T

N. 88° 32' E ✓

+13.05 ✓ P.T.

45° 40'

176

43° 46.1

+50

36° 31.1

29° C.R.

175

29° 16.1

Δ 91° 20'

+50

22° 01.1

P.I 175+02.5

174

14° 46.1

T. 204.35 ✓

+50

7° 31.1

L. 314.9 ✓

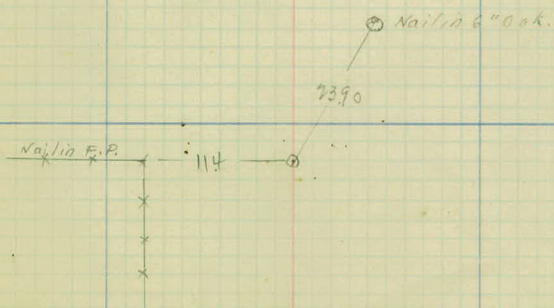
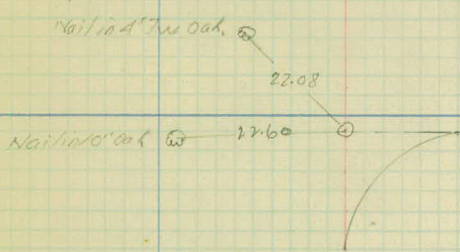
173

0° 16.1

172+98.15 P.C.

0° 00'

N. 2° 48' W ✓



Station Point L R Bear

End of Proj

300125.6

Iron.
Men

N. 1° 01' W. ✓

190+17.70

P.O.T.

N. 1° 01' W. ✓

+22.0 ✓

P.T

44° 46.5'

188

41° 35'

29° C.L.

+50

34° 20'

Δ 89° 33'

187

27° 05'

P.I 187+11.30

+50

19° 50'

T 198.08 ✓

186

12° 35'

L. 308.79 ✓

185+50

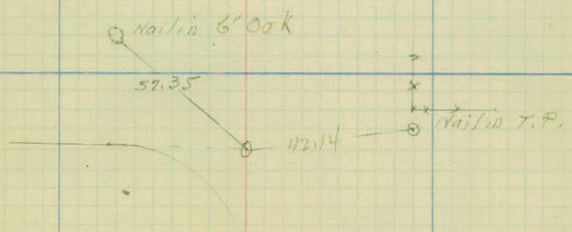
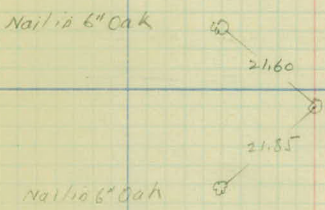
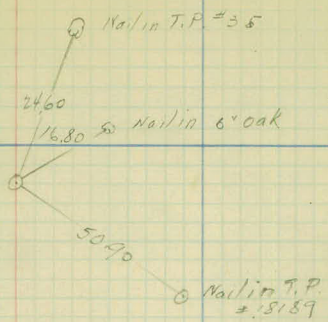
5° 20'

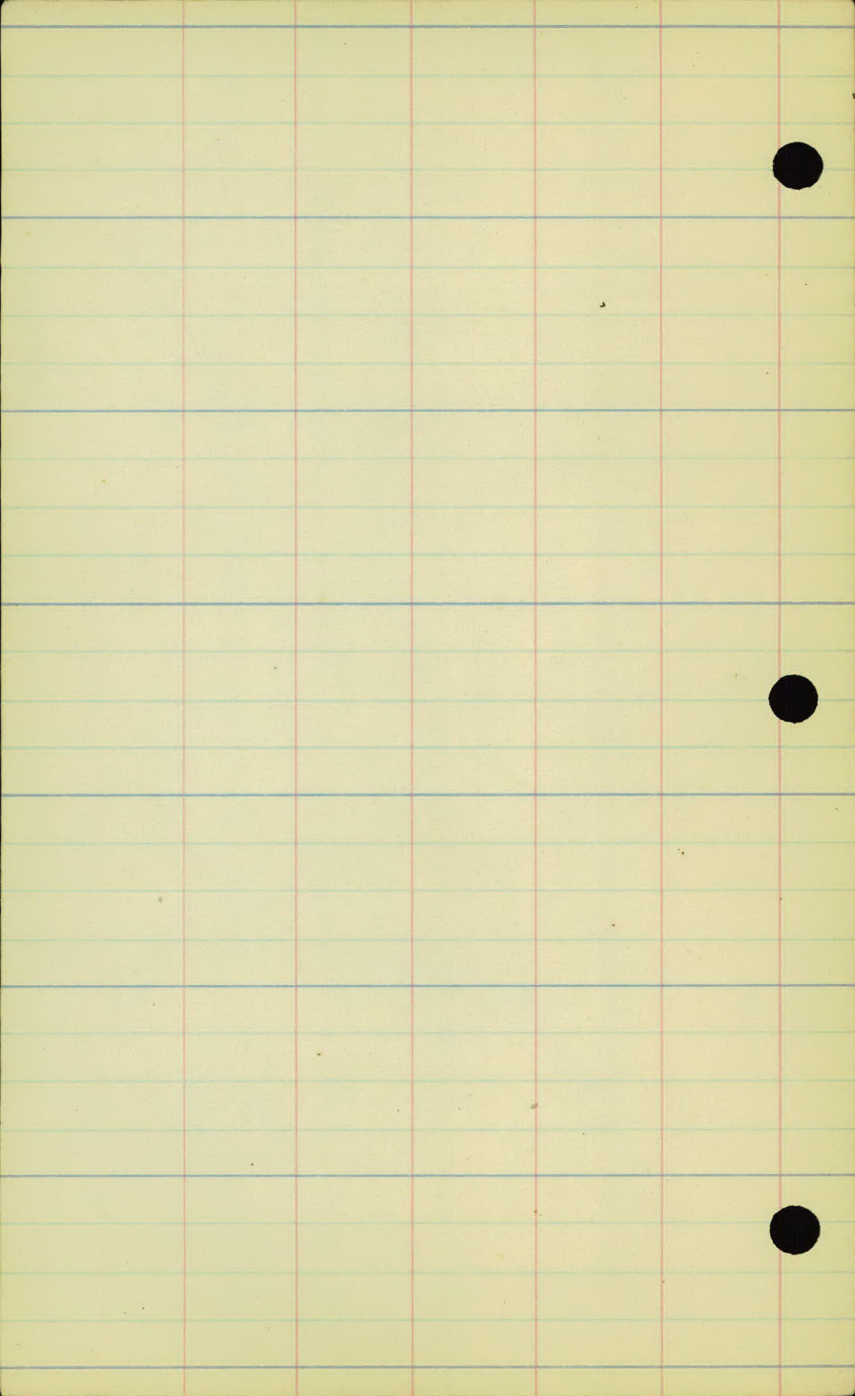
185+13.23 ✓

P.C

0° 00'

N. 88° 32' E. ✓





Line Revision.

Art. Topog

Proj - 2457

W.H.C.
Eck. Aug 11, 24
Galvin
Frank

Station

177

413.09

P.T.

176

175

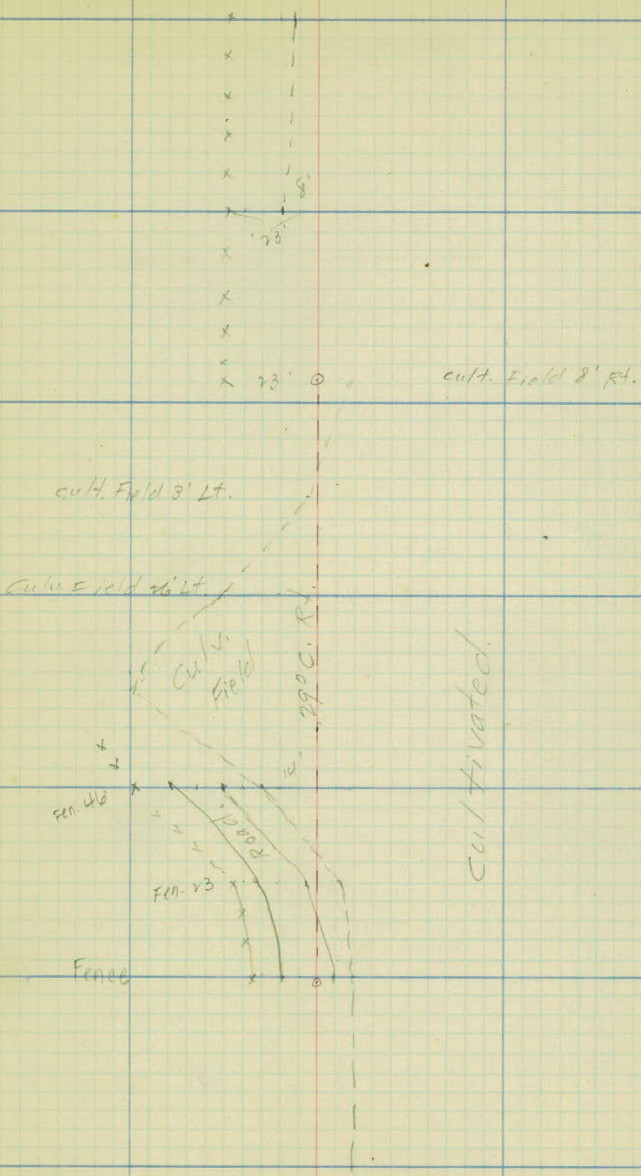
174

173

498.15

P.C.

172



183

182

181

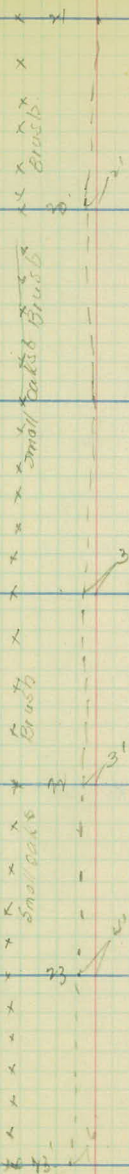
180

179

178

177

Heavy
Oaks
Brush
(Thick)



cultivated

189

+22.01 P.T.

188

187

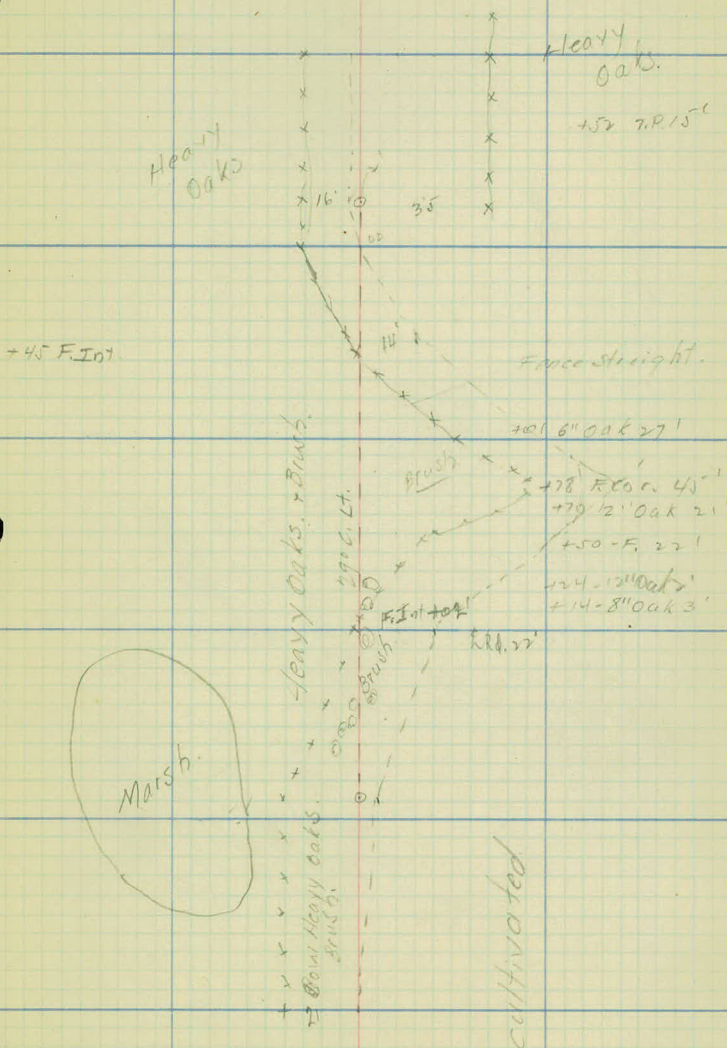
186

+13.22 P.C.

185

184

183



195

784

Po. Line Xing.

194

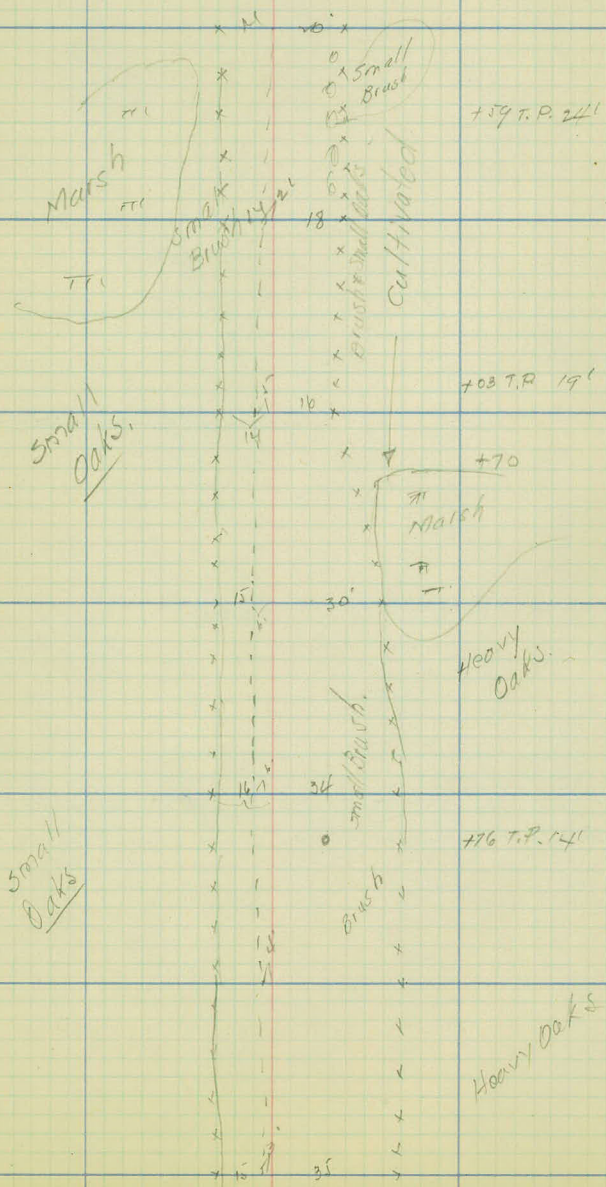
193

192

191

190

189



200 + 85.6 End of 1961 Iron Mon.

200

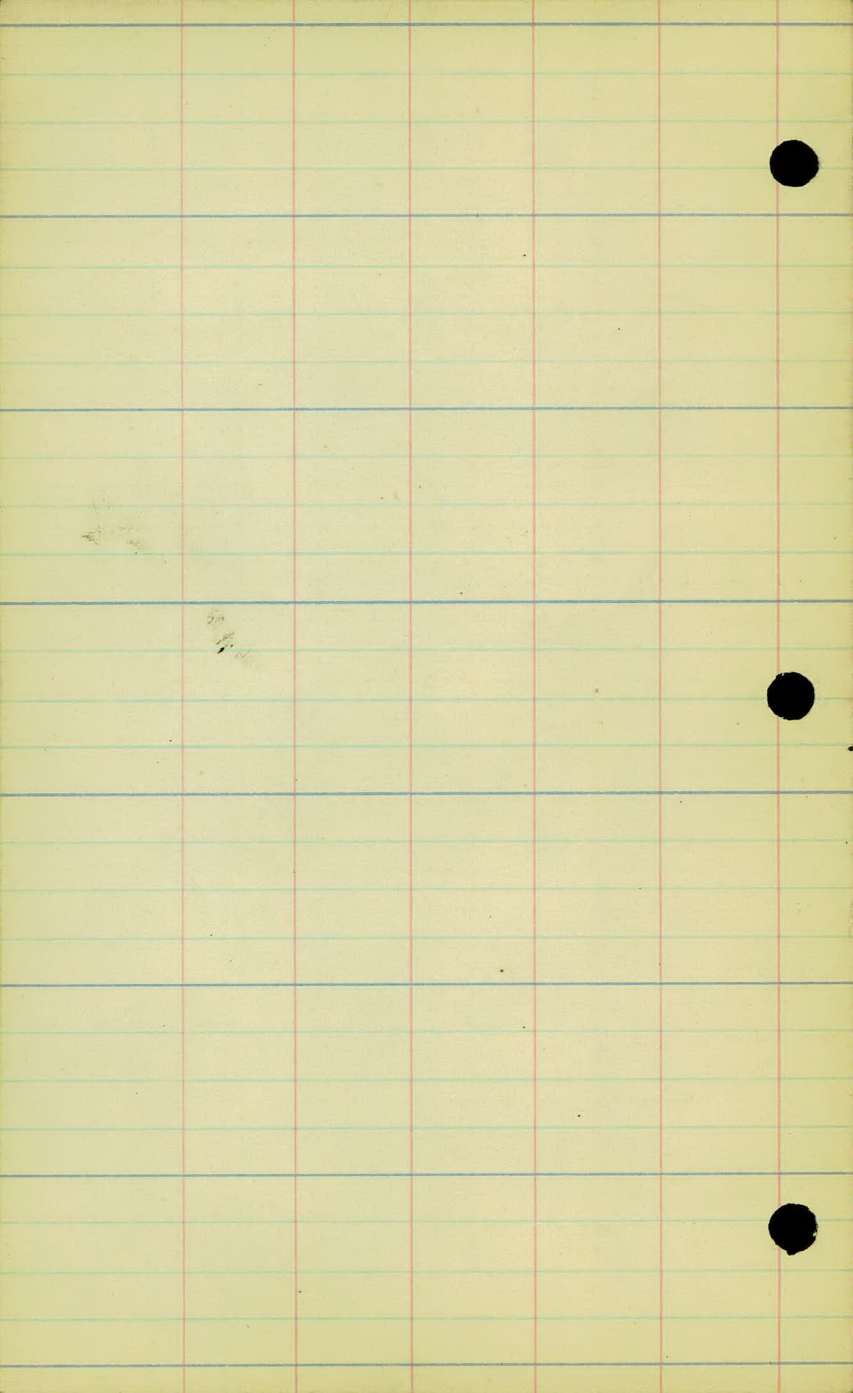
199

198

197

196

195



Line Revision.
2 Levels

Proj. 2452

Station	+	H.I. ✓	-	Elev. ✓
B.M.	5.90	988.55		982.65
17400			6.2	82.4
+50			6.7	81.9
174			7.0	81.6
+50			6.8	81.8
175			6.4	82.2
+50			4.3	84.3
176			0.9	87.7
T.P.	9.36	997.08 ✓	0.83	987.72
+40			7.5	89.6
177			4.9	92.2
178			2.4	94.7
179			0.5	96.6
T.P.	6.37	1002.90 ✓	0.55	996.53
180			3.8	99.1
+60			2.1	100.8
181			1.5	01.4
+50			1.4	10.5 1.5
182			2.1	100.8
+50			5.0 4.5	97.9
183			6.3	94.6
+50			11.0	99.9
T.P.	0.49	993.11 ✓	10.28	992.62
184			3.6	89.5 89.5
+30			4.8	88.3
+55			5.7	87.4

W.H.C.
Eck. Aug 11, 1924
Calvin
Fronke

R.R. Spike 24' Coff. at Sta. 12500

Station	+	HI	-	Elev.
		993.11 ✓		
185			7.1	996.0 ✓ 86.0
+50			7.5	995.6 ✓ 85.6
B.M.	5.82	996.21 ✓	2.72	990.39, 990.38
186			9.7	86.5
+50			6.4	89.8
187			3.3	92.9
+50			1.3	94.9
188			0.4	95.8
T.P.	9.05	1004.88 ✓	0.38	995.83
188+60			9.0	95.9
189			8.1	96.8
+50			5.6	999.3
190			3.2	1001.7
+55			2.3	02.6
191			3.7	1001.2
+57			6.3	998.6
192			7.0	97.9
+65			7.2	97.7
193			7.7	97.2
194			8.8	96.1
+54			9.4	95.5
195			9.1	95.8
T.P.	5.62	1001.87 ✓	8.63	996.25
+50			5.5	95.1 ✓ 96.4
+85			5.9	96.0 ✓ 98.0

R.R. spike in T.P. Rt. sta. 186195

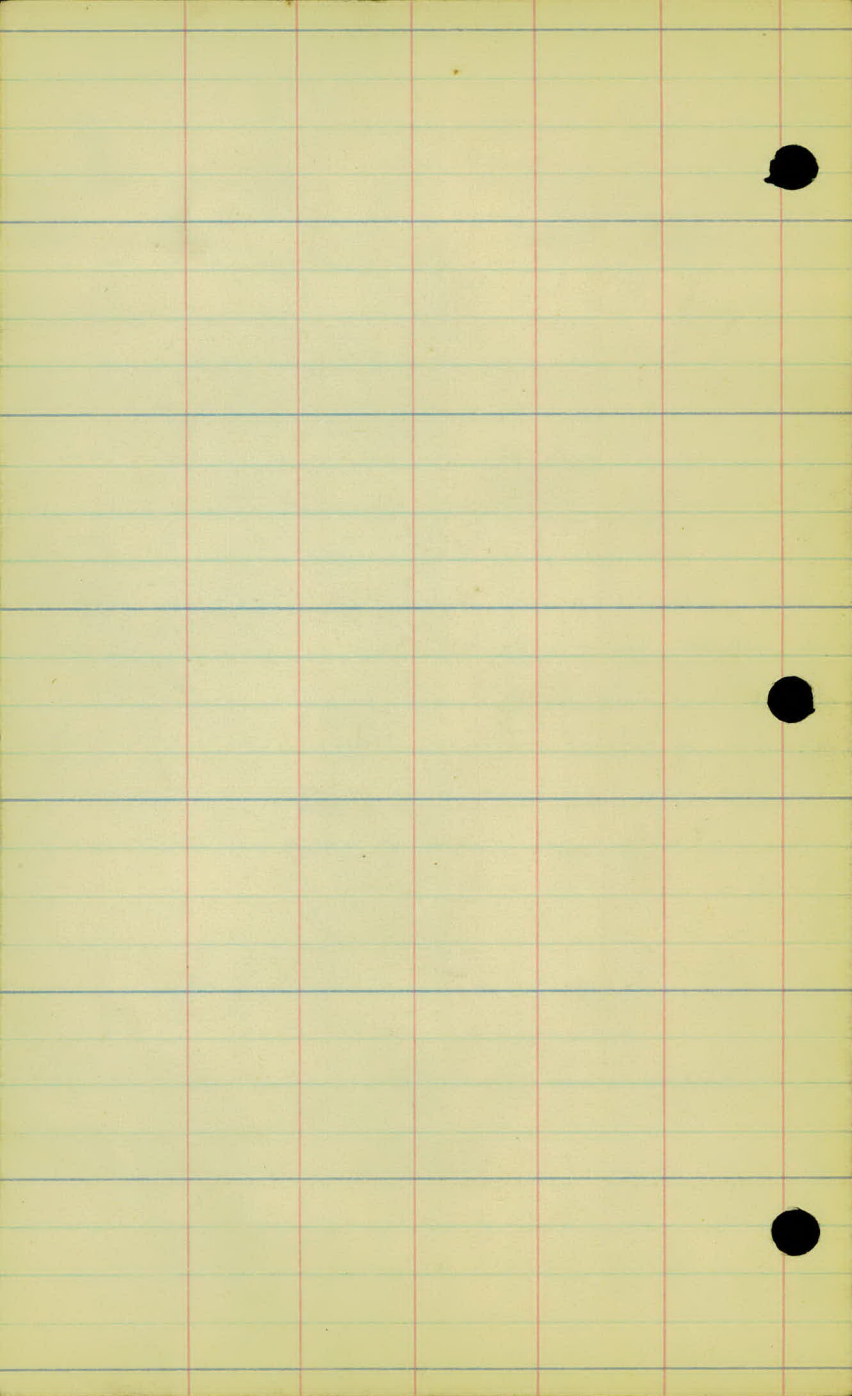
Station	+	H.S	~	Elev.
		1001.87		
186			6.0	995.9
197			9.2	92.7
+60			6.2	95.7
198			5.6	96.3
+50			5.2	96.7
199			4.8	97.1
+45			6.0	95.9
+77			8.7	93.2
200			10.6	91.3
+50			9.0	92.9
+80			8.5	93.4
+91			8.3	93.6
B.M.			7.40	994.47

Note: for Σ Levels of Long Lake Road see
original Level Notes.

check Levels P 42 orig. Notes

↳ Long Lake Road

R.R. Spike in T.P. at Sta. 200+64



Line Revision

X-Sections

Proj - 24-52

station	Elev
180 + 60	1000.8
180	999.1
179	996.6
178	994.7
177	992.2
+ 40	989.6
176	987.7
+ 50	984.3
175	982.2
+ 50	981.8
174	981.6
+ 50	981.9
173	982.4

Lt. 2

Rt.

$$\begin{array}{r} +2.0 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.4 \\ \hline 14 \end{array} \quad \begin{array}{r} +0.1 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 6 \end{array} \quad \begin{array}{r} -1.3 \\ \hline 14 \end{array} \quad \begin{array}{r} -2.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -2.1 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.9 \\ \hline 25 \end{array} \quad \begin{array}{r} +1.5 \\ \hline 15 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 7 \end{array} \quad \begin{array}{r} -1.1 \\ \hline 10 \end{array} \quad \begin{array}{r} -1.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +2.0 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.0 \\ \hline 16 \end{array} \quad \begin{array}{r} +0.1 \\ \hline 14 \end{array} \quad \begin{array}{r} -0.3 \\ \hline 9 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 5 \end{array} \quad \begin{array}{r} -1.2 \\ \hline 14 \end{array} \quad \begin{array}{r} -2.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +2.1 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.5 \\ \hline 24 \end{array} \quad \begin{array}{r} +1.0 \\ \hline 16 \end{array} \quad \begin{array}{r} -0.3 \\ \hline 12 \end{array}$$

$$\begin{array}{r} -0.1 \\ \hline 5 \end{array} \quad \begin{array}{r} -1.1 \\ \hline 9 \end{array} \quad \begin{array}{r} -2.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +2.6 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.9 \\ \hline 20 \end{array} \quad \begin{array}{r} -0.5 \\ \hline 14 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 8 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 1 \end{array} \quad \begin{array}{r} -0.2 \\ \hline 7 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +3.1 \\ \hline 33 \end{array} \quad \begin{array}{r} +2.6 \\ \hline 21 \end{array} \quad \begin{array}{r} -0.4 \\ \hline 16 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 1 \end{array} \quad \begin{array}{r} -0.6 \\ \hline 7 \end{array} \quad \begin{array}{r} -1.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +1.0 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.4 \\ \hline 21 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 18 \end{array}$$

$$\begin{array}{r} +0.4 \\ \hline 7 \end{array} \quad \begin{array}{r} -0.6 \\ \hline 6 \end{array} \quad \begin{array}{r} -1.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.1 \\ \hline 10 \end{array} \quad \begin{array}{r} +0.4 \\ \hline 7 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -1.6 \\ \hline 33 \end{array} \quad \begin{array}{r} -0.8 \\ \hline 26 \end{array} \quad \begin{array}{r} +0.1 \\ \hline 9 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 6 \end{array} \quad \begin{array}{r} +1.4 \\ \hline 33 \end{array}$$

Same as Originals

W.H.C.
ack. Aug 1924
Davis
Smith

Station.	Elev.
186 +50	989.8 .
186	986.5 .
+50	995.6 85.6
185	996.0 86.0
+55	987.4 .
+30	988.3 .
184	988.5 89.5
+50	991.9 .
183	994.6 .
+50	997.9 .
182	1000.8 .
+50	1010.5 1001.5
181	1001.4 .

$$\begin{array}{r} \text{L1} \\ -150 \quad -5.0 \quad -1.4 \\ 33 \quad 16 \quad 5 \end{array}$$

$$\begin{array}{r} \text{R1} \\ +1.2 \quad +0.8 \quad 0.0 \\ 8 \quad 16 \quad 33 \end{array}$$

$$\begin{array}{r} -10.0 \quad -1.6 \\ 33 \quad 6 \end{array}$$

$$\begin{array}{r} -1.8 \quad -0.2 \quad -0.2 \quad -0.8 \quad -1.8 \\ 7 \quad 9 \quad 21 \quad 30 \quad 33 \end{array}$$

$$\begin{array}{r} -9.2 \quad -3.8 \quad -0.8 \\ 33 \quad 15 \quad 5 \end{array}$$

$$\begin{array}{r} +0.8 \quad -0.5 \quad -2.8 \quad -4.0 \\ 7 \quad 13 \quad 22 \quad 33 \end{array}$$

$$\begin{array}{r} -13.5 \quad -11.0 \quad -5.0 \quad -1.4 \quad -0.1 \\ 33 \quad 25 \quad 12 \quad 10 \quad 6 \end{array}$$

$$\begin{array}{r} +0.2 \quad -0.6 \quad -3.1 \quad -4.2 \\ 3 \quad 10 \quad 18 \quad 33 \end{array}$$

$$\begin{array}{r} -14.6 \quad -12.0 \quad -5.0 \quad 0.0 \quad 0.5 \\ 37 \quad 26 \quad 11 \quad 6 \quad 3 \end{array}$$

$$\begin{array}{r} 0.0 \quad 0.7 \quad -1.9 \quad -2.6 \\ 2 \quad 9 \quad 17 \quad 33 \end{array}$$

$$\begin{array}{r} -5.0 \quad -4.6 \quad -2.1 \quad -0.5 \\ 33 \quad 25 \quad 14 \quad 8 \end{array}$$

$$\begin{array}{r} -0.6 \quad -1.2 \quad -1.7 \\ 9 \quad 24 \quad 33 \end{array}$$

$$\begin{array}{r} +3.6 \quad +4.0 \quad -1.0 \quad -0.2 \\ 33 \quad 31 \quad 21 \quad 8 \end{array}$$

$$\begin{array}{r} -0.4 \quad -1.2 \quad -1.2 \\ 8 \quad 26 \quad 33 \end{array}$$

$$\begin{array}{r} -0.9 \quad -1.1 \quad -0.1 \\ 33 \quad 21 \quad 12 \end{array}$$

$$\begin{array}{r} -0.4 \quad +0.8 \quad +2.0 \\ 12 \quad 16 \quad 33 \end{array}$$

$$\begin{array}{r} -0.0 \quad +1.2 \quad +0.3 \quad 0.0 \\ 33 \quad 22 \quad 17 \quad 10 \end{array}$$

$$\begin{array}{r} -0.1 \quad +3.2 \quad +4.0 \\ 8 \quad 15 \quad 33 \end{array}$$

$$\begin{array}{r} +1.9 \quad +2.5 \quad 0.0 \quad +0.5 \\ 33 \quad 18 \quad 15 \quad 11 \end{array}$$

$$\begin{array}{r} 0.0 \quad +3.1 \quad +4.0 \\ 8 \quad 16 \quad 33 \end{array}$$

$$\begin{array}{r} +0.8 \quad +1.5 \quad -0.6 \quad -0.2 \\ 33 \quad 17 \quad 15 \quad 10 \end{array}$$

$$\begin{array}{r} 0.0 \quad +1.2 \quad +0.9 \\ 8 \quad 16 \quad 33 \end{array}$$

$$\begin{array}{r} 0.0 \quad +1.4 \quad -0.4 \quad 0.0 \\ 33 \quad 16 \quad 14 \quad 8 \end{array}$$

$$\begin{array}{r} 0.0 \quad 0.0 \quad 0.0 \\ 6 \quad 15 \quad 33 \end{array}$$

$$\begin{array}{r} -0.1 \quad -1.1 \quad -0.2 \\ 33 \quad 17 \quad 9 \end{array}$$

$$\begin{array}{r} -0.4 \quad -0.9 \quad -2.7 \\ 8 \quad 11 \quad 33 \end{array}$$

Station	Elev.
193	997.2
+65	997.7
192	997.9
+57	998.6
191	1001.2
+55	1002.6
190	1001.7
+57	999.3
189	996.8
+60	995.9
188	995.8
+50	994.9
+30	993.7
187	992.9

+0.8

$$\begin{array}{cccc} -2.8 & -1.1 & 0.0 & +0.5 \\ \hline 33 & 16 & 11 & 5 \end{array}$$

$$\begin{array}{cccc} +0.5 & +1.7 & +1.9 & +1.9 \\ \hline 7 & 8 & 16 & 33 \end{array}$$

$$\begin{array}{cccc} -2.6 & -1.5 & -0.5 & +0.4 \\ \hline 33 & 16 & 13 & 5 \end{array}$$

$$\begin{array}{cccc} +0.3 & -1.1 & -1.2 & -1.4 \\ \hline 4 & 6 & 16 & 33 \end{array}$$

$$\begin{array}{cccc} -4.8 & -1.6 & -0.1 & +0.6 \\ \hline 33 & 11 & 13 & 5 \end{array}$$

$$\begin{array}{cccc} 0.0 & -3.2 & -4.1 & -4.1 \\ \hline 3 & 9 & 20 & 33 \end{array}$$

$$\begin{array}{cccc} -2.5 & -0.8 & -0.0 & -0.6 \\ \hline 33 & 18 & 13 & 6 \end{array}$$

$$\begin{array}{ccc} -0.1 & -0.0 & 0.0 \\ \hline 4 & 15 & 33 \end{array}$$

$$\begin{array}{ccccc} -2.0 & +0.6 & -0.2 & -0.6 & +0.4 \\ \hline 33 & 18 & 16 & 10 & 9 \end{array}$$

$$\begin{array}{cccc} +0.3 & +4.6 & +5.0 & +5.6 \\ \hline 6 & 9 & 20 & 33 \end{array}$$

$$\begin{array}{cccc} -0.1 & +1.3 & -0.5 & +0.5 \\ \hline 33 & 18 & 12 & 5 \end{array}$$

$$\begin{array}{cccc} 0.0 & +3.9 & +4.6 & +4.6 \\ \hline 6 & 9 & 20 & 33 \end{array}$$

$$\begin{array}{ccccc} +1.8 & +1.8 & +0.5 & -0.3 & +0.5 \\ \hline 33 & 18 & 16 & 13 & 5 \end{array}$$

$$\begin{array}{ccccc} -0.4 & -0.0 & +2.6 & -3.0 & -5.0 \\ \hline 6 & 8 & 10 & 18 & 33 \end{array}$$

$$\begin{array}{cccc} +1.0 & +0.8 & -0.0 & -0.3 \\ \hline 33 & 17 & 15 & 9 \end{array}$$

$$\begin{array}{cccc} -0.4 & +0.9 & +0.7 & +0.9 \\ \hline 8 & 11 & 20 & 33 \end{array}$$

$$\begin{array}{ccc} -1.3 & -1.4 & -0.5 \\ \hline 33 & 16 & 11 \end{array}$$

$$\begin{array}{ccc} -0.7 & -0.9 & -1.0 \\ \hline 9 & 20 & 33 \end{array}$$

$$\begin{array}{cccc} -4.8 & -4.2 & -0.5 & -0.2 \\ \hline 33 & 20 & 10 & 2 \end{array}$$

$$\begin{array}{cccc} -1.1 & -2.6 & -3.1 & -3.0 \\ \hline 7 & 12 & 19 & 33 \end{array}$$

$$\begin{array}{ccccc} -4.7 & -4.8 & -2.1 & -1.0 & -0.8 \\ \hline 33 & 25 & 17 & 14 & 9 \end{array}$$

$$\begin{array}{cccc} -0.2 & +4.8 & +5.2 & +5.8 \\ \hline 10 & 13 & 18 & 33 \end{array}$$

$$\begin{array}{ccc} -10.6 & -3.6 & -1.5 \\ \hline 33 & 11 & 4 \end{array}$$

$$\begin{array}{ccccc} -0.6 & 0.9 & -1.1 & +1.7 & +1.7 \\ \hline 6 & 15 & 26 & 29 & 33 \end{array}$$

$$\begin{array}{ccc} -8.9 & -5.0 & -1.8 \\ \hline 33 & 18 & 10 \\ -10.8 & -2.0 & -1.7 \\ \hline 33 & 17 & \end{array}$$

$$\begin{array}{ccccc} +2.0 & +2.0 & +0.4 & 0.0 & -0.6 \\ \hline 6 & 11 & 12 & 8 & 33 \\ +1.6 & +1.2 & +0.9 & & \\ \hline 10 & 21 & 33 & & \end{array}$$

Station	Elev.
199 +77	993.2
+45	995.9
199	997.1
+50	996.7
198	996.3
+60	995.7
197	992.9 .92.7
196	995.9
+85	996.0
+50	995.4 .96.4
195	995.8
+54	995.5
194	996.1

$$\begin{array}{r} +2.8 - 0.8 \\ \hline 33 \quad 19 \end{array} \quad \begin{array}{r} +0.6 \\ \hline 8 \end{array}$$

$$\begin{array}{r} -2.5 \\ \hline 8 \end{array} \quad \begin{array}{r} -2.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +2.8 \\ \hline 33 \end{array} \quad \begin{array}{r} +2.3 \\ \hline 20 \end{array} \quad \begin{array}{r} +1.7 \\ \hline 14 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 11 \end{array}$$

$$\begin{array}{r} -0.6 \\ \hline 8 \end{array} \quad \begin{array}{r} -2.8 \\ \hline 18 \end{array} \quad \begin{array}{r} -3.2 \\ \hline 20 \end{array} \quad \begin{array}{r} -4.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.8 \\ \hline 18 \end{array} \quad \begin{array}{r} +2.8 \\ \hline 16 \end{array} \quad \begin{array}{r} -0.3 \\ \hline 7 \end{array}$$

$$\begin{array}{r} +0.4 \\ \hline 3 \end{array} \quad \begin{array}{r} +0.5 \\ \hline 18 \end{array} \quad \begin{array}{r} +6.3 \\ \hline 20 \end{array} \quad \begin{array}{r} +6.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.2 \\ \hline 33 \end{array} \quad \begin{array}{r} -1.5 \\ \hline 15 \end{array} \quad \begin{array}{r} -1.3 \\ \hline 7 \end{array}$$

$$\begin{array}{r} +0.6 \\ \hline 6 \end{array} \quad \begin{array}{r} -0.3 \\ \hline 20 \end{array} \quad \begin{array}{r} +2.2 \\ \hline 23 \end{array} \quad \begin{array}{r} +3.950 \\ \hline 28 \quad 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 33 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 15 \end{array} \quad \begin{array}{r} -0.9 \\ \hline 4 \end{array}$$

$$\begin{array}{r} +0.8 \\ \hline 8 \end{array} \quad \begin{array}{r} +2.2 \\ \hline 19 \end{array} \quad \begin{array}{r} +2.4 \\ \hline 21 \end{array} \quad \begin{array}{r} +4.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.8 \\ \hline 33 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 18 \end{array} \quad \begin{array}{r} -0.5 \\ \hline 8 \end{array}$$

$$\begin{array}{r} +0.7 \\ \hline 10 \end{array} \quad \begin{array}{r} +0.2 \\ \hline 19 \end{array} \quad \begin{array}{r} +4.2 \\ \hline 24 \end{array} \quad \begin{array}{r} +5.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -1.5 \\ \hline 33 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 15 \end{array}$$

$$\begin{array}{r} +2.1 \\ \hline 7 \end{array} \quad \begin{array}{r} +2.8 \\ \hline 13 \end{array} \quad \begin{array}{r} +3.0 \\ \hline 26 \end{array} \quad \begin{array}{r} +6.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -3.5 \\ \hline 33 \end{array} \quad \begin{array}{r} -3.1 \\ \hline 8 \end{array}$$

$$\begin{array}{r} +0.2 \\ \hline 8 \end{array} \quad \begin{array}{r} -0.3 \\ \hline 18 \end{array} \quad \begin{array}{r} +3.2 \\ \hline 26 \end{array} \quad \begin{array}{r} +3.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -5.2 \\ \hline 33 \end{array} \quad \begin{array}{r} -3.2 \\ \hline 11 \end{array}$$

$$\begin{array}{r} +0.2 \\ \hline 6 \end{array} \quad \begin{array}{r} -0.0 \\ \hline 15 \end{array} \quad \begin{array}{r} +3.4 \\ \hline 19 \end{array} \quad \begin{array}{r} +5.2 \\ \hline 28 \end{array} \quad \begin{array}{r} +5.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -3.5 \\ \hline 33 \end{array} \quad \begin{array}{r} +0.4 \\ \hline 11 \end{array} \quad \begin{array}{r} -0.8 \\ \hline 8 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 3 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 10 \end{array} \quad \begin{array}{r} +5.0 \\ \hline 14 \end{array} \quad \begin{array}{r} +10.0 \\ \hline 20 \end{array} \quad \begin{array}{r} +10.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -7.0 \\ \hline 33 \end{array} \quad \begin{array}{r} -3.9 \\ \hline 20 \end{array} \quad \begin{array}{r} -0.2 \\ \hline 8 \end{array}$$

$$\begin{array}{r} -0.5 \\ \hline 10 \end{array} \quad \begin{array}{r} +3.8 \\ \hline 15 \end{array} \quad \begin{array}{r} +2.0 \\ \hline 21 \end{array} \quad \begin{array}{r} +1.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -5.3 \\ \hline 33 \end{array} \quad \begin{array}{r} -4.0 \\ \hline 17 \end{array} \quad \begin{array}{r} -0.1 \\ \hline 7 \end{array}$$

$$\begin{array}{r} -0.2 \\ \hline 7 \end{array} \quad \begin{array}{r} -0.5 \\ \hline 16 \end{array} \quad \begin{array}{r} +2.0 \\ \hline 23 \end{array} \quad \begin{array}{r} +2.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -5.2 \\ \hline 33 \end{array} \quad \begin{array}{r} -1.1 \\ \hline 15 \end{array} \quad \begin{array}{r} -0.4 \\ \hline 10 \end{array} \quad \begin{array}{r} +0.3 \\ \hline 2 \end{array}$$

$$\begin{array}{r} +0.2 \\ \hline 10 \end{array} \quad \begin{array}{r} +1.8 \\ \hline 12 \end{array} \quad \begin{array}{r} +2.2 \\ \hline 17 \end{array} \quad \begin{array}{r} +2.2 \\ \hline 33 \end{array}$$

station.

Elev.

201+10

220

995.6

+91

993.6

Mon 20014.50 End of Proj

+80

993.4

+48

992.9

200

991.3

2 Extended

completed
Aug 11, 24

$$\frac{-1.6}{33} \quad \frac{+0.4}{17}$$

$$\frac{0.0}{33}$$

$$\frac{-2.3}{33}$$

$$\frac{+1.1}{33}$$

$$\frac{-2.2}{33}$$

$$\frac{-1.8}{33}$$

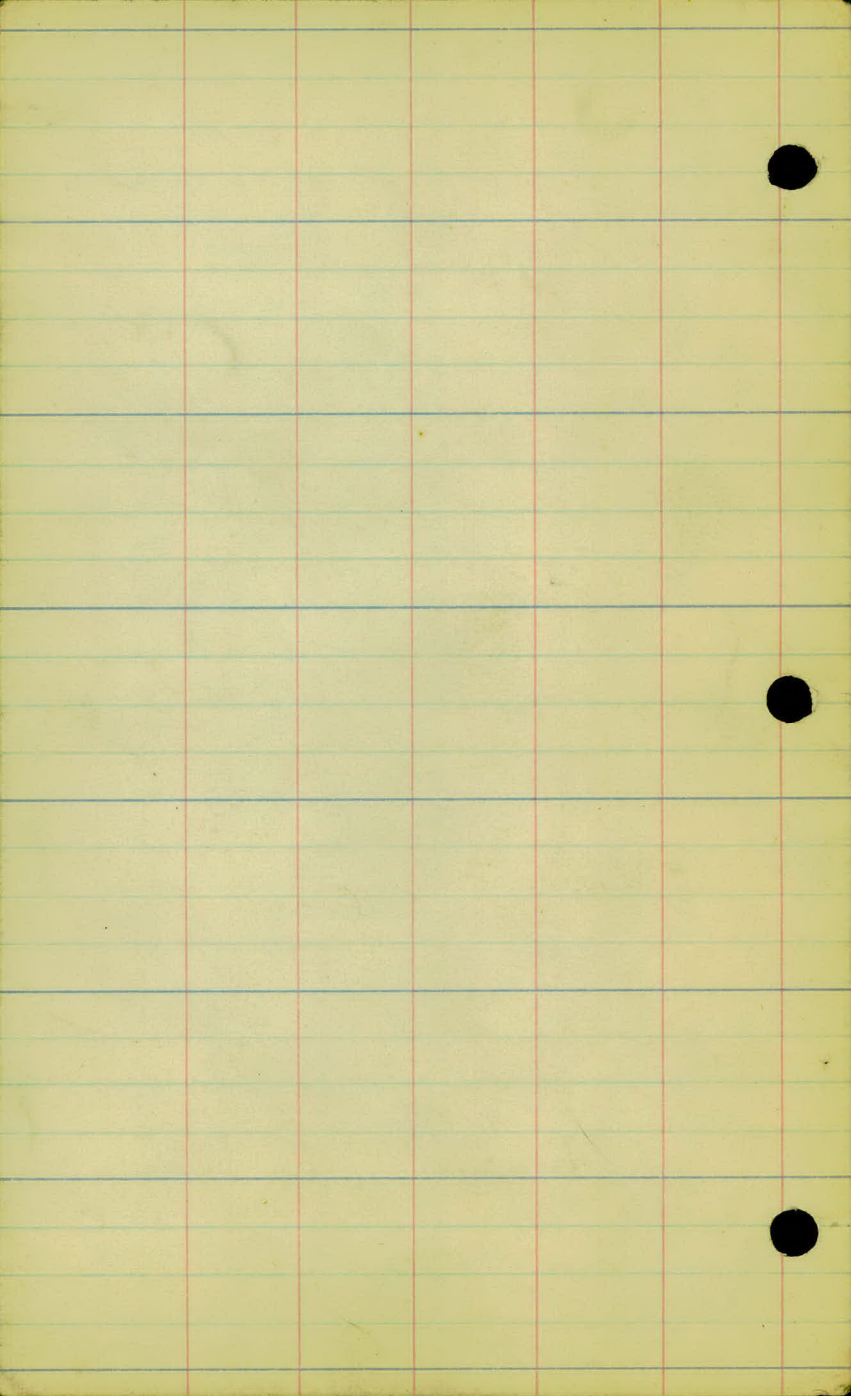
$$\frac{-1.1}{33} \quad \frac{+0.4}{13}$$

$$\frac{-0.7}{6} \quad \frac{-1.0}{33}$$

$$\frac{+0.5}{33} \quad \frac{+0.2}{17} \quad \frac{+1.4}{33} \quad \frac{+0.9}{7}$$

$$\frac{-0.7}{33}$$

23



200+60

Proj. 24" ✓

12" x 21' C.M. in p, remove ✓

Pl- 24" C.M., @ Sta 200+00

~~199+00 199+70 8' near bridge L~~

197+00 No culv to be placed

Pot hole left of E ✓

~~to the bridge 195 to 196 L~~

~~191~~

192+15 Pl. 24" C.M. ✓

186+75 F.E.R.

7.12" C.M. No culv reqd. ✓

Etc. for in cut, 30 cy.

186+85 Pl 24" C.M. ✓

194+50 Pl 24" C.M. ✓

175+00 F.E.L

12" C.M. 24' long under old road at corner - use it under form cut. ✓

163+00 Drainage both ways from E. no culv reqd. ✓

159+72 ✓

Pl. 24" C.M. ✓

157+00

Drains to R of E ✓
no x-drain reqd

152+55

Pl. 12" x 60 C.M. ✓
Ent. R.

Change grade ✓
next above ent.

10 trees per
100 lin. ft.

200+85 - 188+22
~~Cl. Br. 10' wide~~
Cl. Br. 10' wide

2+52

188+22 ——— 185+13

60 trees Cl. Br. ✓

185+13 - 176+13

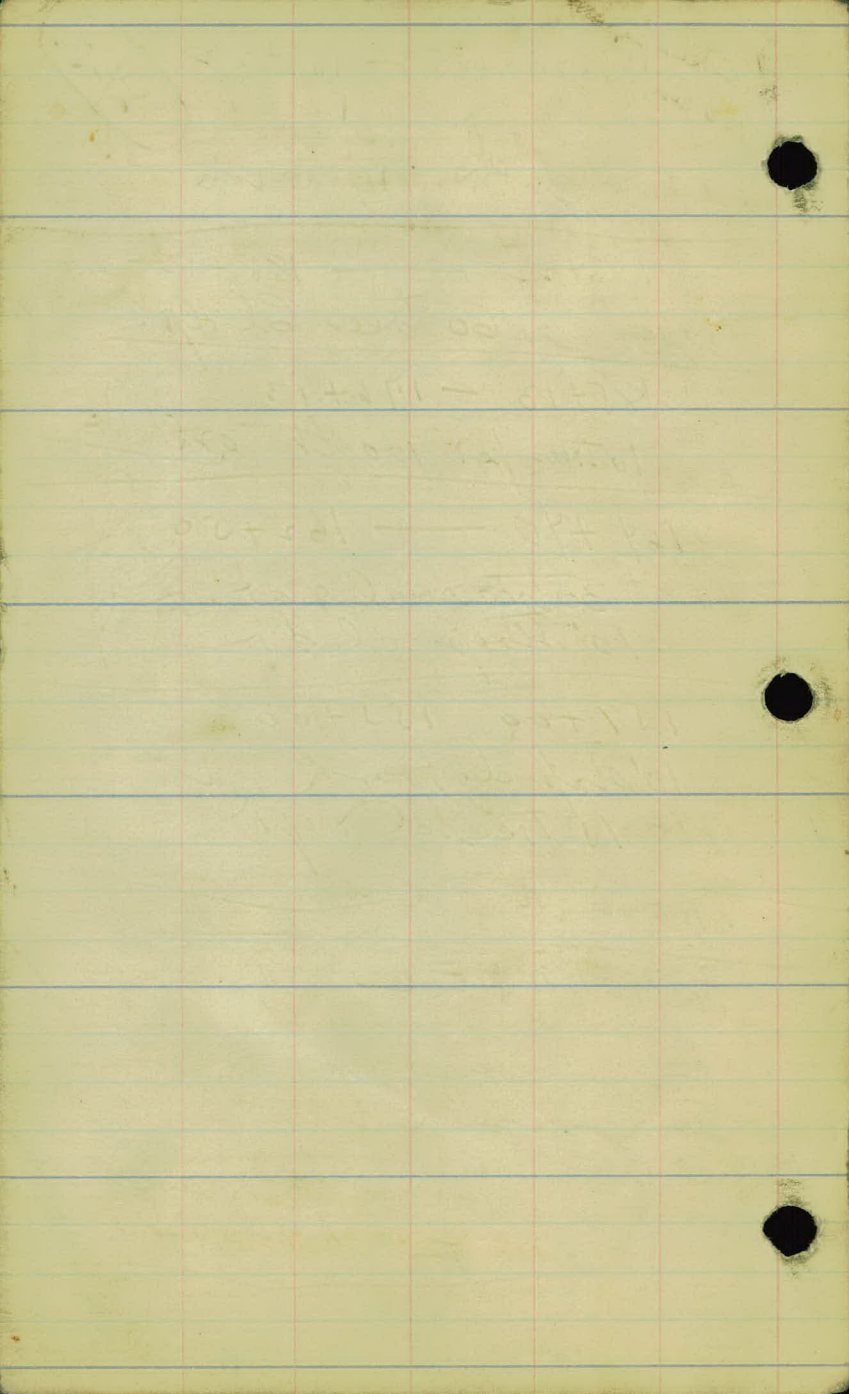
10 trees per 100 ft - 0.25 A Br. ✓

164+40 ——— 162+50

30 trees cl x gr. ✓
10' strip sl. Br.

159+00 155+00

10' strip sl. brush ✓
15 trees cl x gr.



Faint, illegible ghosting of text from the reverse side of the paper, appearing as light blue and grey marks across the page.

Alignment Notes.

Project 24-52. 24-52

From County Road C and the
East County Line, West into
Washington County.

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Rec'd 2/27/24 Rec. 2-27-24

Date Filed APR. 15th '24

11 11-24-52

LAKE DE MONTREVILLE ROAD

Station Pt. L. R. Calc. Bear.

35+96.⁸ P.O.T.

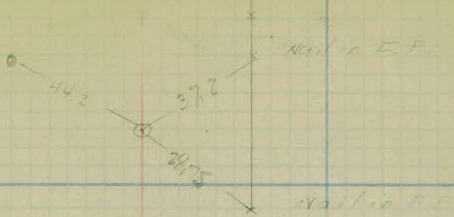
75+79.8 1/4 Corner Iron Pipe. 0°-02' ~~N. 90°-02' E.~~ S 89° 58' E.

7497.⁰⁰ 4 3/4" Pipe

N. 90°-00' E.

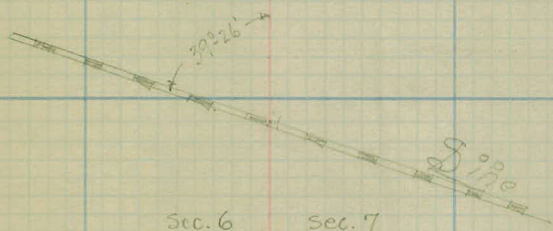
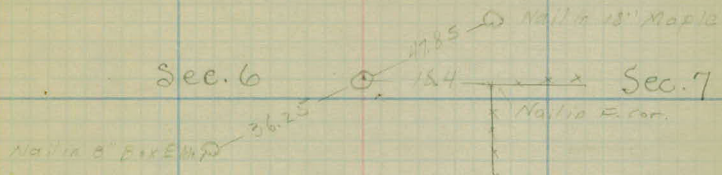
0+00 3rd Corner Mark. (stone)

Nail in T.F.



Sec. 6

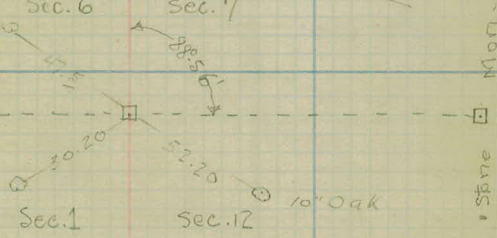
Sec. 7



Sec. 6 Sec. 7

Wash Co. ↑
Ramsey Co. →

3 Nails
12" Oak.



Sec. 1

Sec. 12

Se County Road "C"

W.C. ↑
 G.E.J. Rod
 E.H.R. Ch.
 T.F. Ch.

station Pt. L. R. Calc. Bearing.

57+42.3 P.O.T.

N. 87° 26' E. ✓

53+05.50 P.T. 0° 48'

53+00 0° 46.4'

1° C.L.

52+50 0° 31.4'

A. P. 36' - L.

52+25.5 ^{2"x2"} PI stake.
Sec. corner.

S.T. 80.00' ✓

52+00 0° 16.4'

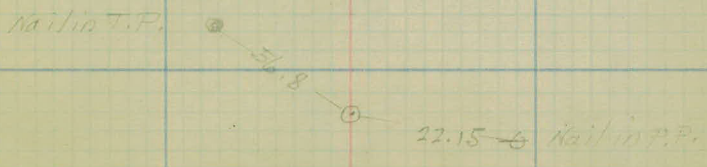
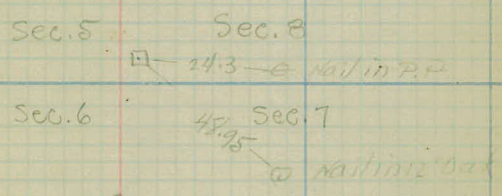
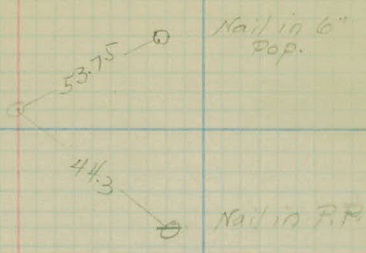
C.L. 160.00' ✓

51+45.5 ✓ P.C. 0° 00'

PI 52+25.5

46+97.4 P.O.T.

589.56 E.
N. 77° 02' E.



Station Pt. L. R. calc. Bear.

N 88° 10' E
~~N 88° 20' E~~

91-42.2 P.O.T.

N 88° 10' E ✓

87-64.80 P.O.T.

78-63.40
P.I.
2 1/2" stake 0-16'
1/4 Cor. Sec. 5 and 8

~~N 88° 20' E~~ ✓

○ Nail in 24" Pop.
33.6
○
32.6 — Nail in 4" Blk Oak
30 — 3-4" Blk Oaks.

○ Nail in 8" White Oak
19.30
○
23.25 — Nail in 14" Twin Oak

Nail in T.P. ○ 30.3 — ○ 20.95 — ○ Nail in F.P.

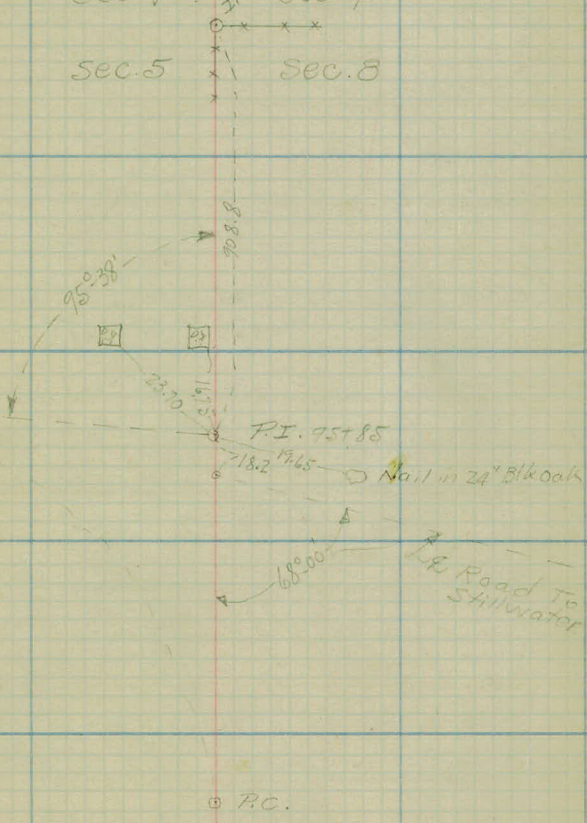
Station	P.T.	L	R	Calc. Bear.
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N 7° ²⁸ W

96+94.48 ✓	P.T.	47° 49'		
96+50		41° 22'		29° C.L.
96+00		34° 07'		Δ 95° 38'
95+50		26° 52'		S.T. 220.36. ^{220.29}
95+00		19° 37'		C.L. 329.77 ✓
94+50		12° 22'		P.I. 95+85'
94+00		5° 07'		at Cor. 50' Ch.
93+64.71	P.C.			

N 8° ^{10 E} E.

Sec. 4 Iron Mon.
Sec. 9.
Sec. 5
Sec. 8



Station Pt. L R Calo. Bear.

N. 40° ²³ W.

102+22.56 ✓ P.T. 14°30'

102+00 12°14.6' 20° C.L.

101+50 7°14.6' Δ 29°-00'

101+00 2°46' P.I. 101+52.03

100+77.56 ✓ P.C. 0°00' S.T. 74.47 ✓

L.C. 145.00

Cor. 19-50' ch.

N 11° ²³ W

100+02.68 ✓ P.T. 12.57 1/2

4°-C.L.

99+50 0°54.3'

Δ 3°-55'

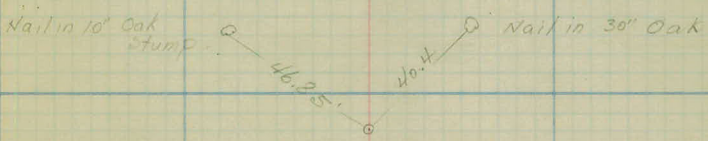
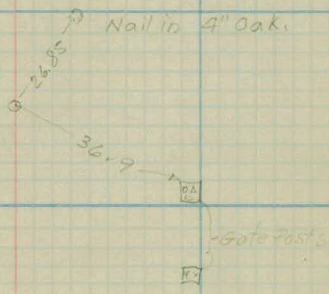
P.I. 99+53.7 ✓

99+04.72 P.C. 0°00'

S.T. 48.98 ✓

C.L. 97.91 ✓

N 7° ²⁸ W



Station PT. L R Calc
Bear
N. 11° ~~37~~ E

113+95⁴⁶ ✓ P.T. 15° 45'
 113+50 11° 39.5' 18' C.R.
 113+00 7° 09.5' Δ 31° - 30'
 112+50 2° 39.5' P.I. 113+10.6
 112+20⁴⁶ ✓ P.C. 0° - 00' S.T. 90.14 ✓
 C.L. 175.00 ✓
 Cor. 15' - 50' ch.

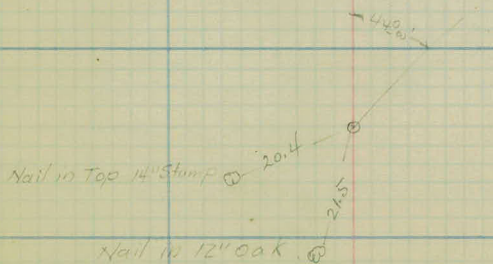
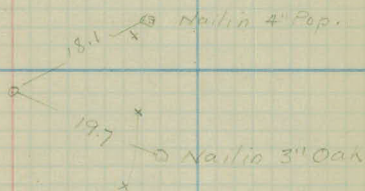
N. 19° ~~53~~ W

111+32³⁰ ✓ P.T. 11° 45'
 111+00 9° 19.5' 15' C.L. -
 110+50 5° 34.6' Δ 23° - 30'
 110+00 1° 49.6' P.I. 110+55.3
 109+75.63 ✓ P.C. 0° - 00' S.T. 79.67 ✓
 L.C. 156.67 ✓
 Cor. 12. - 50' ch.

N. 13° ~~37~~ E

105+44⁶² ✓ P.T. 22° 00'
 105 17° 32.3' 20' C.R.
 104+50 12° 32.3' Δ 44° - 00'
 104+00 7° 32.3' P.I. 104+40.9
 103+50 2° 32.3' S.T. 116.28 ✓
 103+24.62 ✓ P.C. 0° - 00' L.C. 220.00 ✓
 Cor. 19 - 50' ch.

N. 48° ~~23~~ W



Station	Pt.	L	R	Calc, Bear.
123+52.10	✓ P.T.		24°-45'	N 11°-57' E N 12°-00' E
123+00			19°-01'	22° C.R.
122+50			13°-31'	Δ 47°-30'
122+00			8°-01'	P.I 122+47.92
121+50			2°-31'	S.T 120.80 ✓
12+27.12	✓ P.C.		0°-00'	L.C. 225.00 ✓ 0.23 cor. - 50 ch.
121+25.82	✓ P.T.		7°-30'	N 12°-27' E 12° C.R.
121			5°-57'	Δ 15°
120+50			2°-57'	P.I 120+68.8
120+00.82	✓ P.C.		0°-00'	S.T, 62.98 ✓ L.C. 125.00 ✓ 0.06 cor. 50 ch.
116+25.37	✓ P.T.	7°-05'		N 12°-33' W
116		5°-49'		10° C.L.
115+50		3°-19'		Δ 14°-10'
115		0°-16'		P.I 115+55.0
114+83.20	✓ P.C.	0°-00'		S.T, 71.30 ✓ C.L. 141.67 ✓ .05 cor. 50 ch.

N 11°-37' E

Nail in 6" Pop

Nail in 8" Pop

10.1

15.65



Nail in E.P.

27.35



Nail in E.P.

25.45

Nail in 5" Birch

22



Nail in 5" Oak

34.7



Stat 100 Pt. L R Calc. Bear.
 S. 27°33' E
 S 20°13' W

136+92.9 ✓	P.T.		20°40'	
136+50			17°40'	
136			14°10'	14° C.R.
+50			10°40'	Δ 41°20'
135+0.0			7°10'	P.I. 135.524
134+50 ✓			3°40'	S.T. 154.25 ✓
133+97.6 ⁵ ✓	P.C.		0°00'	L.C. 295.24 ✓ 69° 10' 10" ✓

S. 64°-53' E
 N. 11°13' E

129+56.56 ✓	P.T.		21°25'	
+50			20°50'	18° C.R.
129			16°20'	Δ 42°50'
+50			11°50'	P.I. 128+43.9 ✓
128			7°20'	S.T. 125.36 ✓
+50			2°50'	L.C. 237.96 ✓
127+18.6 ✓	P.C.		0°00'	0.15 cm - 50' h.

N. 68°-17' E

127+05.25 ✓	P.T.		3°10'	5° C.R.
127			8°02'	Δ 6°20'
+50			1°47'	P.I. 126+42
126			0°32'	S.T. 63.4 ✓
125+78.5 ✓	P.C.		0°00'	L.C. 126.65 ✓

61-57
 N. 62° E

Nail in 18" B/K Oak — 33.8

Nail in 24" Bir Oak

9°

Nail in 8" Oak

42° 50'

24.1

Nail in 8" oak

26.9

Nail in 4" Willow — 24.1

Nail in 8" Willow

Station Pt. L. R.

N 75° 27' E
~~S 56° 47' E~~

147+94 ^{8.54} P.T. 18° 25' 29° C.L.

147+50 11° 58' Δ 36° 50'

147+00 42° 43' P.I. 147+34°

146+67 ^{7.53} P.C. S.T. 66. ⁴⁷

L.C. 127.01 ✓

S 67° 43' E
~~S 19° 57' E~~

144 = 85.42 = 144 = 85.05

144+85 ⁴² P.T. 11° 30' 20° C.R.

144+50 7° 57' Δ 23° 00'

144+00 22° 57' P.I. 144+29

143+70 ^{70.05} ⁴² P.C. S.T. ^{52.95}

L.C. 115.00
Cor. 19, 50' Ch.

145
14499.63

N 81° 17' E
S 42° 57' E

142+44 ⁷ P.T. P.C. 31° 35' 43° C.L.

142+00 18° 01' Δ 63° 10'

141+50 7° 21' P.I. 142+00

141+14 ³ P.C. S.T. 15.78 ^{85.70}

L.C. 150.40 ✓

137+55 P.O.T.

S 27° 33' E
S 20° 13' W

Nail in 20" oak. \odot 46.8 \odot Nail in 16" oak
 \ominus 10.22

\odot Nail in 14" Birch
 \ominus 27.35
 \ominus 27.45
 \ominus 27.42
 \ominus 27.46
 \odot Nail in TW. Birch^{10'}

\odot Nail in 4" oak
 \ominus 30.7
 \ominus 30.9
 \odot Nail in B. Birch
 \odot 37.05

\odot Nail in 14" oak.
 \ominus 31.9
 \odot Nail in 12" oak.
 \ominus 30.9

Station pt. L R

1494 77. ⁰⁰ P.T. 13° 31.5'

1494 50 10° 48'

149 5° 48'

148441 ⁷⁵ 96 P.C.

N 48° 24 E

~~S 85° 50 E~~

20° C.L.

A 27° 03'

P.I 149411

S.T. (69.04) 69.25

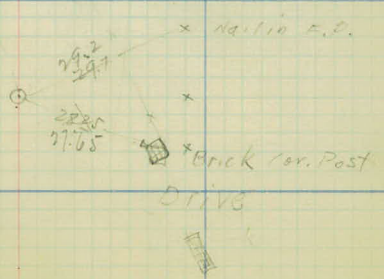
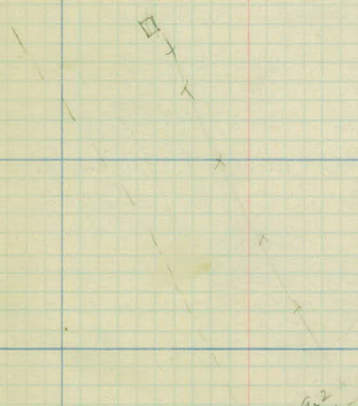
L.C 135 25' ✓

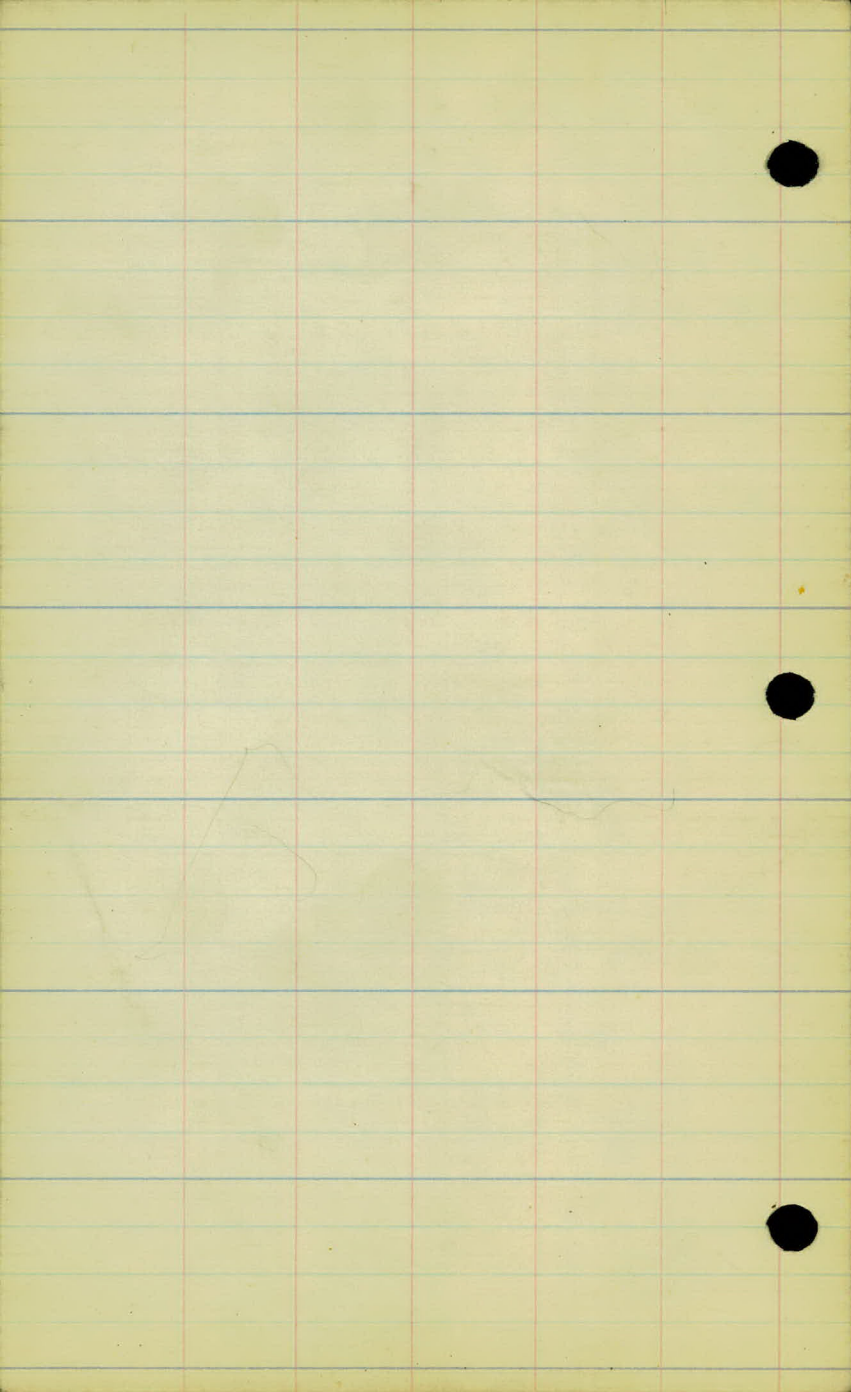
N 75° 27 E

~~S 56° 47 E~~

Eastman
150
149 } 100.21

ENT to Walnut Ridge AL





Center Line Levels.

Project 24-52

station + H.I. - Elev.

B.M. 496 996.13 991.17

West along Co. Rd. "C"

0+00	4.56	991.57	✓
+14	4.9	91.2	✓
+20	4.9	91.2	✓
+50	5.7	90.4	✓
1+00	6.4	89.7	✓
2+00	6.1	90.0	✓

So. along E. Co. Line

0+00	4.56	991.57	✓
1	4.8	91.3	✓
2	4.5	91.6	✓
3	4.5	91.6	✓
4	3.4	92.7	✓

No. along E. Co. Line.

0+00	4.56	991.57	✓
1	4.7	91.4	✓
2	3.8	92.3	✓
3	2.6	93.5	✓
#10 Approx	1.7	94.4	✓

W.H.C.
C.E.J. } Feb 6, 1924.
E.H.R.
T.F. }

Lake Imp B.M. #23, Spike in T.R. N.W. cor. of C. & E. Cal line

Top Stone Man. Co. Road "G" & E. County Line.

Stone Man. Co. Rd "C"

Stone Man. Co. Rd "C"

Top of Rail

Station + H.I - Elev.

996.13

0100			456	991.57	✓
125			55	90.6	✓
+34			56	90.5	✓
1			41	92.0	✓
+44			33	92.8	✓
2			39	92.2	✓
3			54	90.7	✓
T.P.	485	995.81	5.17	990.96	✓
4			55	90.3	✓
5			56	90.2	✓
6			58	90.0	✓
7			57	90.1	✓
+56			49	90.9	✓
+97			408	91.73	✓
8			41	91.7	✓
+27			51	90.7	✓
9			73	88.5	✓
10			76	88.2	✓
11			63	89.5	✓
T.P.	190	992.56	5.15	990.66	✓
12			2.2	90.4	✓
13			43	88.3	✓
14			49	87.7	✓
+62			53	87.3	✓

E. Co. Line Top of Mon.

Top of Stake Sta. 3.

Top of Rail 3° line left

$\frac{5.2}{300}$	$\frac{5.1}{200}$	$\frac{4.6}{100}$
-------------------	-------------------	-------------------

Right:

$\frac{3.6}{100}$	$\frac{2.1}{200}$	$\frac{2.3}{300}$
-------------------	-------------------	-------------------

Top of Stake Sta. 11.

Farm Ent. L.

Station	+	H.I	-	Elev.
		792.56		
15			5.2	987.4 ✓
16			5.1	87.5 ✓
+37			4.9	87.7 ✓
17			5.7	86.9 ✓
18			7.4	85.2 ✓
19			10.2	82.4 ✓
T.P.	5.79	989.16 ✓	7.19	983.37 ✓
20			2.3	80.9 ✓
21			7.1	82.1 ✓
22			5.5	83.7 ✓
+77			4.9	84.3 ✓
23			4.7	84.5 ✓
+50			4.1	85.1 ✓
24			2.5	86.7 ✓
T.P.	9.69	997.07 ✓	17.8	987.38 ✓
25			5.4	91.7 ✓
+10			4.63	92.44 ✓
26			4.8	92.3 ✓
B.M.	8.00	1002.75 ✓	2.22	994.75 ✓
27			2.8	94.0 ✓
28			5.6	97.2 ✓
29			3.6	99.2 ✓
30			2.6	1000.2 ✓
T.P.	12.10	1013.27 ✓	15.8	1001.17 ✓
31			10.2	1003.1 ✓

Top of stake sta. 19.

↳ Road Left.

£

Top stake 24

Top of Mon. (Iron)

where 2/6/24

R.R spike in 30' Maple 30' R. Sta 26+70

Top 3

Station	+	H.I.	-	Elev.
		1013.27 ✓		
32			6.2	1007.1 ✓
33			2.5	1010.8 ✓
T.P.	10.95	1022.92 ✓	13.0	1011.97 ✓
34			9.2	13.7 ✓
35			5.4	17.5 ✓
36			4.0	18.9 ✓
37			5.5	17.4 ✓
+60			9.6	13.3 ✓
38			11.8	11.1 ✓
T.P.	2.56	1014.19 ✓	10.59	1012.33 ✓
39			6.5	08.4 ✓
+66			6.8	08.1 ✓
40			6.8	08.1 ✓
+73			8.4	06.5 ✓
41			9.8	05.1 ✓
+50			12.0	02.9 ✓
T.P.	4.92	1008.19 ✓	11.62	1003.27 ✓
42			6.1	02.1 ✓
43			5.5	02.7 ✓
+35			6.1	02.1 ✓
44			6.2	02.0 ✓
45			5.6	02.6 ✓
46			4.4	03.8 ✓
47			5.6	02.6 ✓
+55			4.3	00.9 ✓

top of Stake 33

Top of Stake 38

top of Rock.

Station	+	H.I.	-	Elev.
		1008.19 ✓		
48			2.1	999.1 ✓
T.P.	0.17	996.85	11.51	996.68 ✓
49			3.8	93.1 ✓
50			8.6	88.3 ✓
51			12.0	84.9 ✓
T.P.	0.48	986.93 ✓	10.40	986.45 ✓
52			4.1	82.8 ✓
B.M.			4.52	982.41 ✓
+50			4.7	82.2 ✓
53			5.2	81.7 ✓
54			6.1	80.8 ✓
55			6.5	80.4 ✓
56			6.5	80.4 ✓
T.P.	4.28	985.73 ✓	5.58	981.35 ✓
57			2.8	82.9 ✓
+42			2.2	83.5 ✓
58			3.7	82.0 ✓
+55			7.1	78.6 ✓
59			8.5	77.2 ✓
60			9.7	76.0 ✓
61			10.3	75.4 ✓
62			10.2	75.5 ✓
T.P.	3.22	979.64 ✓	9.31	976.42 ✓
63			5.9	73.7 ✓
64			7.4	72.4 ✓ 72.2

Top of rock

Top of shale 81

RR spike in Power Pole 22' R. sta 52+17

Top of shale 56

Top shale

Station	+	H.I	-	E/ev.
		979.64		
65			7.7	(970.9) 71.9
66			7.2	72.4 ✓
138				
67			5.6	71.0 ✓
406			3.6	71.0 ✓
68			8.9	70.7 ✓
69			8.2	71.4 ✓
70			2.1	72.5 ✓
T.P.	0.47	973.70	6.41	973.23 ✓
71			1.9	71.8 ✓
72			3.7	70.0 ✓
73			5.3	68.4 ✓
74			5.7	68.0 ✓
75			6.3	67.4 ✓
76			2.0	66.7 ✓
77			7.0	66.7 ✓
78			6.5	67.4 ✓
B.M.	12.01	980.51	5.20	968.50 ✓
79			10.9	69.6 ✓
80			7.8	72.7 ✓
81			5.4	75.1 ✓
82			4.9	75.6 ✓
83			5.0	75.5 ✓
84			1.7	78.8 ✓
T.P.	11.30	990.76	1.05	979.46 ✓

Int of Road Right

Farm Ent. Left

Top of Stake

318 spike in Power Pole 78143 75 Left

Top of Stake

Station	H.I	Elev
	990.76	
85	✓	5.3 985.5 ✓
T.P.	11.25 1001.55	0.46 990.30 ✓
86		9.5 92.1 ✓
+50		6.4 95.2 ✓
87		4.0 97.6 ✓
+50		2.5 99.1 ✓
88		3.2 98.4 ✓
T.P.	0.95 997.61	4.92 996.63 ✓
89		2.7 94.7 ✓
90		6.3 91.3 ✓
91		8.5 88.8 ✓
+42		10.7 86.9 ✓
T.P.	0.30 986.53	11.38 986.23 ✓
92		2.7 83.8 ✓
93		7.7 78.6 ✓
T.P.	1.28 975.89	11.92 974.61 ✓
+64		6.3 69.6 ✓
94		7.1 66.8 ✓
T.P.	0.72 964.95	11.66 964.23 ✓
+50		2.9 62.1 ✓
95		7.0 58.0 ✓
+50		8.9 56.1 ✓
96		10.2 54.8 ✓
T.P.	2.94 956.10	11.79 953.16 ✓ 11.79
96.50		5.9 52.2 ✓

top P. Post.

P.C.

Top No. 10 7450

Station	+	H.I. ✓	-	Elev.
		956.10		
97			6.0	950.1 ✓
98			10.3	945.8 ✓
T.P.	1.45	946.00 ✓	11.55	944.55 ✓
99			2.5	43.5 ✓
+50			3.4	42.6 ✓
100			4.2	41.8 ✓
B.M.			5.21	940.79 ✓
101			5.3	40.7 ✓
+50			5.3	40.7 ✓
102			4.5	41.5 ✓
+50			3.4	42.6 ✓
103			2.6	43.4 ✓
+50			4.9	41.1 ✓✓
104			6.1	39.9 ✓
+50			6.5	39.5 ✓
T.P.	4.48	943.99 ✓	6.49	939.51 ✓
105			4.4	39.6 ✓
+4d			3.8	40.2 ✓
106			4.2	39.8 ✓
107			7.8	36.8 ✓
108			9.1	34.9 ✓
+50			8.7	35.3 ✓
109			6.8	37.2 ✓
110			2.1	41.9 ✓
T.P.	4.40	945.82 ✓	2.57	941.42 ✓

700 stake 99

R.R. Spike in 14" Tree 22' R. 100+13

station	+	HI	-	E/cv.
---------	---	----	---	-------

945.82 ✓

110 +50			58	940.0 ✓
111			7.9	37.9 ✓
112 +50			8.4	37.4 ✓
112			8.8	37.0 ✓
+50			8.2	37.6 ✓
113			7.0	38.8 ✓
+50			5.1	40.7 ✓
114			4.6	41.2 ✓
+25			5.4	40.4 ✓
115			9.1	36.7 ✓
B.M.			8.23	937.59 ✓

125.53

179.13 99.07

125.55 937.59

53.68 ✓ 53.58 ✓

B.M.

Levels.

Proj. 24-52

Nail in 8" White Oak 20' R 11/5/10

To here 2-7/24

Station	+	H.I	-	Elev.
B.M.	0.54	938.13 ^v		937.59
(115)				
115+50			3.8	934.3 ^v
116			5.2	32.9 ^v
+40			5.6	32.5 ^v
117			5.5	32.6 ^v
118			6.2	31.9 ^v
119			6.0	32.1 ^v
T.P.	6.21	939.43 ^v	5.91	932.22 ^v
+50			6.3	32.1 ^v
120			6.4	32.0 ^v
+50			6.5	31.9 ^v
121			6.2	32.2 ^v
+50			6.4	32.0 ^v
122			6.4	32.0 ^v
+50			6.7	31.7 ^v
123			6.4	32.0 ^v
+50			6.1	32.3 ^v
T.P.	2.50	937.48 ^v	3.45	934.98 ^v
124			4.8	32.7 ^v
+50			5.4	32.1 ^v
125			5.6	31.9 ^v
126			5.4	32.1 ^v
+30			4.7	32.8 ^v
127			5.5	32.0 ^v
+50			5.0	32.5 ^v

W.H.C.

C.E.J.

M.S.A.

T.F.

} Feb 27, 24

Top of Stake 119

Nail in B. Poplar W.R. Sta. 123153

Station	+	H. I	-	Elev.
		937.48		
128			.46	932.9 ✓
+50			.46	932.9 ✓
129			.49	32.6 ✓
T.M.	1.05	937.43 ✓	1.10	936.38 ✓
+50			.56	31.8 ✓
130			.56	31.8 ✓
+65			.47	32.7 ✓
131			.54	32.0 ✓
132			.57	31.7 ✓
133			.48	32.6 ✓
134			16.00	921.43 ✓
			3.5	33.9 ✓
+50			2.0	35.4 ✓
T.P.	10.52	947.08 ✓	0.87	936.56 ✓
135			10.0	37.1 ✓
+50			7.9	39.2 ✓
136			.48	42.3 ✓
+50			1.3	45.8 ✓
T.P.	5.53	952.09 ✓	0.52	946.56 ✓
137			3.7	48.4 ✓
+55			1.2	50.9 ✓
+70			1.8	50.3 ✓
138			3.8	48.3 ✓
+60			2.9	43.2 ✓
139			10.3	41.8 ✓
140			11.7	40.4 ✓

P.N. spike in 6" Oak. 33'-4". Sta. 127+40

Top of Ice Lake De-Monteville Feb 27, 1924

Top stake 34+50

Top stake 136+50

Station + H.I - Elev.

952.09

T.P. 142 942.86 ✓ 10.65 941.44 ✓

141 3.5 39.4 ✓

+50 4.2 38.7 ✓

142 4.9 38.0 ✓

+65 5.2 37.7 ✓

143 5.4 37.5 ✓

+70 5.5 37.4 ✓

144 5.4 37.5 ✓

+50 5.9 37.0 ✓

145 5.6 37.3 ✓

T.P. 965 948.09 ✓ 4.42 938.44 ✓

146 9.8 38.3 ✓

+67 9.3 40.8 ✓

147 6.7 41.4 ✓

+50 4.6 43.5 ✓

148 0.3 47.8 ✓

T.P. 10.94 958.34 ✓ 0.19 947.90 ✓

+41 6.5 52.3 ✓

B.M. 10.24 968.86 ✓ 0.22 958.62 ✓

149 9.9 59.0 ✓

+50 6.9 62.0 ✓

150 4.0 64.9 ✓

151 0.5 68.4 ✓

T.P. 9.08 975.69 ✓ 0.25 968.61 ✓

Top of stake 140

top stake 145

Top of stake 148+00

R.R. spike in 16" Oak 35' Lt. Sta. 149+00
(Find sign on Tree priv. Gals.)

Station + H.I - Elev.

975.69 ✓

152 60 69.7 ✓

162 5.1 70.6 ✓

158 4.4 71.3 ✓

Across Lake

checking back to sta. 115.

B.M. 0.35 958.97 ✓ 958.62

T.P. 0.13 948.04 ✓ 11.06 947.91 ✓

T.P. 0.28 936.93 ✓ 11.29 936.65 ✓

T.P. 3.44 930.38 ✓ 2.99 926.94 ✓

T.P. 4.89 926.48 ✓ 8.79 921.59 ✓

T.P. 10.38 931.99 ✓ 4.87 921.61 ✓

T.P. 8.26 939.94 ✓ 0.31 931.68 ✓

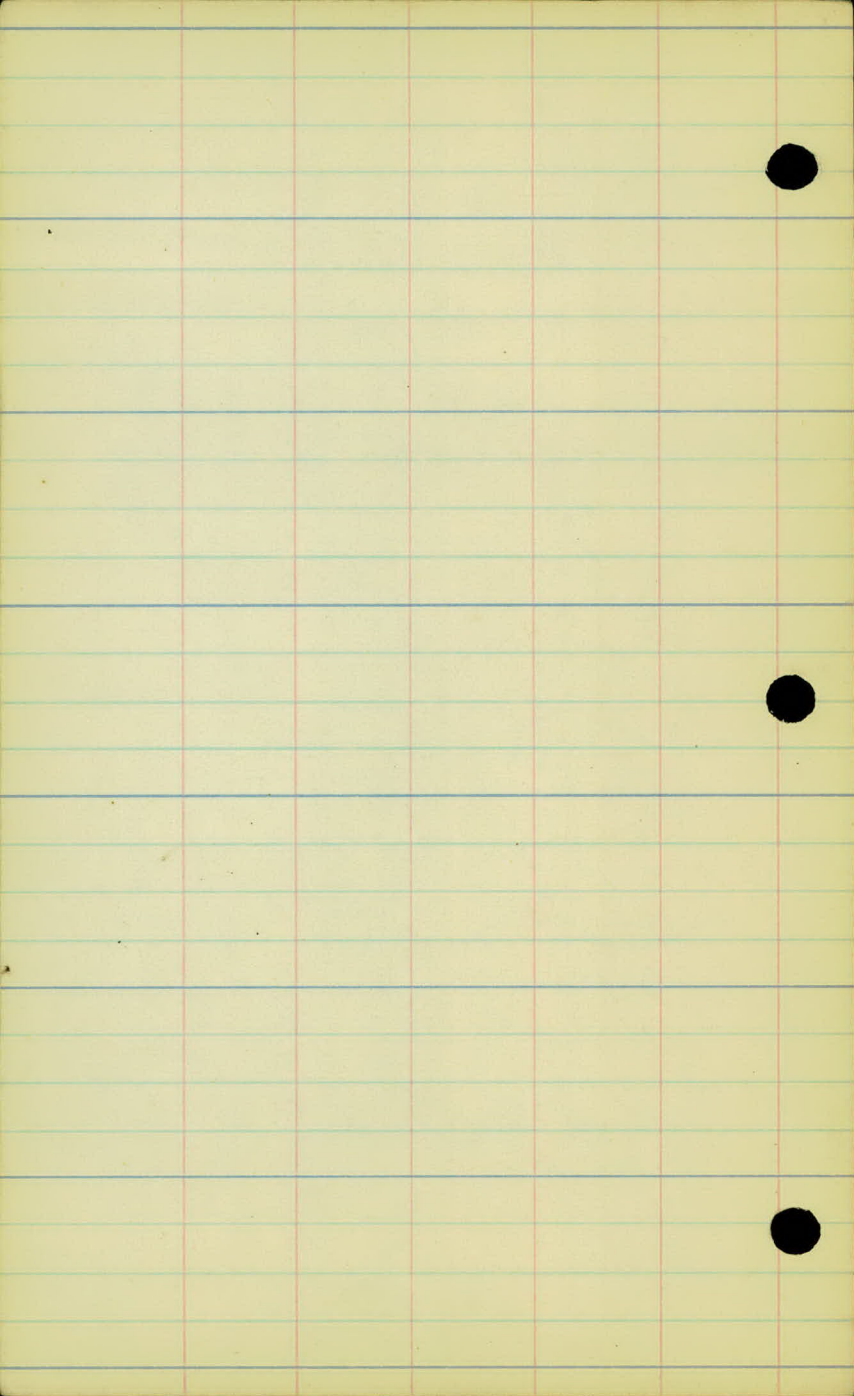
B.M. 2.33 937.61 = 935.28

Forcheck Levels from Sta etc.

to Sta 115 to see following page

£ Drive to Estate Left.

Nail in 8" Oak 20' R. 115+10



Check Levels

Project - 24-52.

W.H.C. }
G.E.J. } Feb 25, 24.
M.S.A. }
T.F. }

Sta.	+	H.I	-	E/ev.	
B.M.	5.68	996.85		991.17	
T.P.	5.54	996.25	6.14	990.71	
T.P.	2.16	992.83	5.58	990.67	
B.M. (new)			4.29	988.54	
T.P.	5.22	988.66	9.45	985.38	
T.P.	9.16	996.56	1.26	987.40	
B.M.	9.33	1004.09	1.80	994.76	94.75
T.P.	10.82	1014.80	0.11	1003.98	
B.M. (new)	7.32	1021.15	0.97	1013.83	
T.P.	3.01	1012.49	11.67	1009.48	
T.P.	5.60	1008.88	9.21	1003.28	
T.P.	0.66	1000.29	9.25	999.63	
T.P.	0.90	990.78	10.41	989.88	
B.M.	4.35	986.78	8.35	982.43 = 982.41	
T.P.	4.37	985.74	5.41	981.37	
T.P.	3.28	979.71	9.31	976.43	
T.P.	0.92	974.17	6.46	973.25	92.42
B.M. (new)			1.25	972.92	
T.P.	10.87	979.35	5.69	968.48	962.50
T.P.	11.06	990.22	0.19	979.16	
T.P.	10.67	1000.87	0.02	990.20	
B.M. (new)	2.94	1000.31	3.50	997.37	
T.P.	0.24	988.72	11.93	988.38	
T.P.	0.79	977.81	11.70	977.02	
T.P.	0.30	966.50	11.61	966.20	
T.P.	0.34	954.86	11.98	954.52	

Lake Imp B.M. #23, R.R. Spike in T.P. N.W. Cor.

Co. Rd "C" E. Co. Line.

Top of Large Rock - 15' Lt. Sta 15+72

R.R. spike in 30" Maple 30' R. 26+70

Nail in Po. Pole Rt. Sta 54

Top of Rock

Nail in Po. Pole

R.R. spike in Po. Pole, 22' R. Sta. 52+17

R.R. spike in 18" Poplar 55' Rt 70+36

" " " Po. Pole 75' Lt. 78+63

Nail in T.P. Lt. Sta 84+00

Nail in 8" Oak 87+70 R. 18'

	+	H.I	-	Elev
		954.86		
T.P.	3.34	946.82	11.38	943.48
B.M.	6.91	947.72	6.01	940.81
T.P.	4.33	944.77	7.28	940.44
T.P.	2.82	945.38	2.21	942.56
B.M.			7.77	937.61 = 937.59

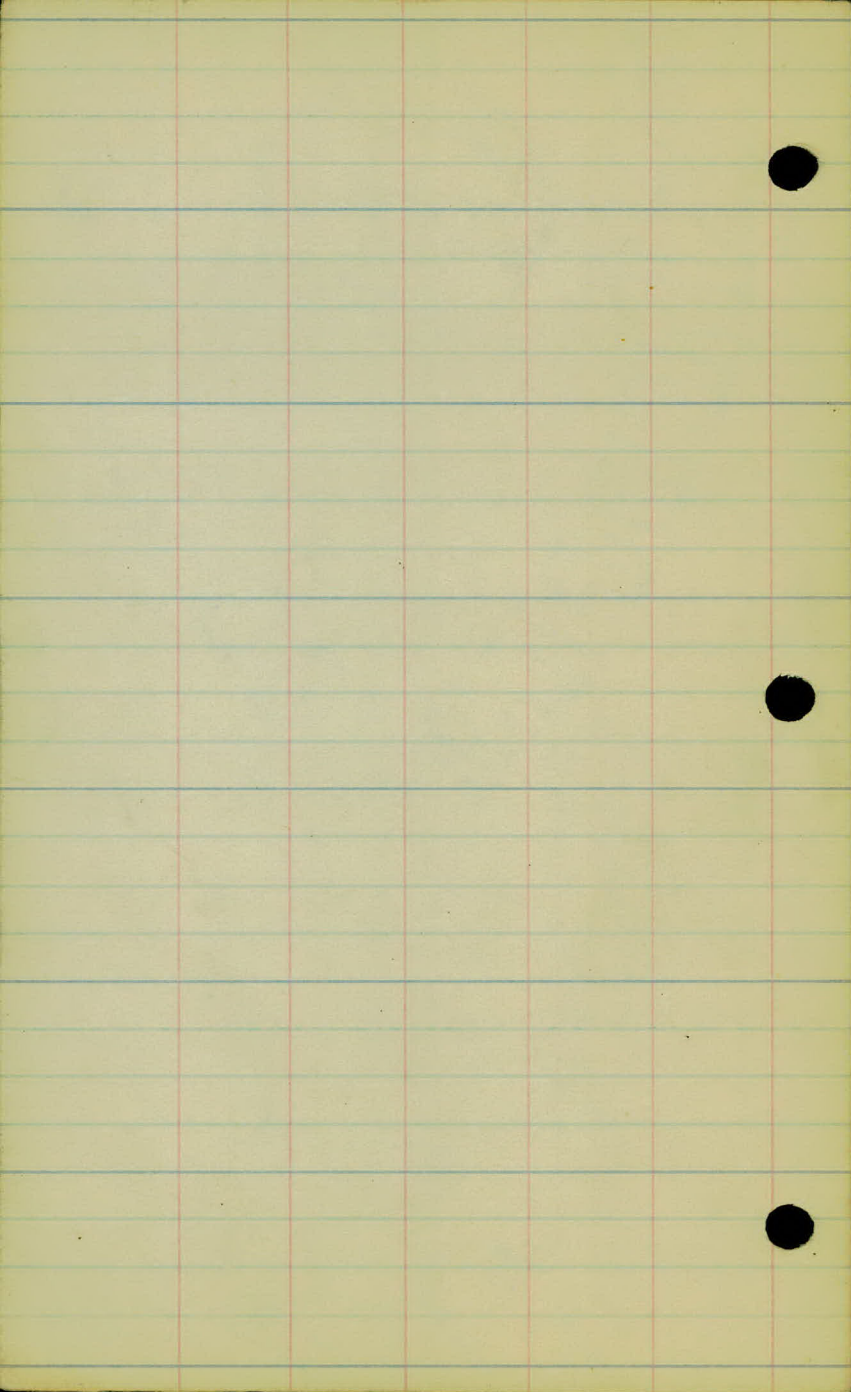
133.09

186.65
133.09
53.56

991.17
937.61
53.56

R.R. spike 14" Tree 22' R. 100+13

Nail in 8" Oak 20' R 115+10



Proj. #24-52

Art. Topog. from Sta.
0+00 to End of Proj.

Sta.

3

2

1

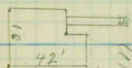
0+00 Center of East Co. Line Road.

-1

+45 Cor. of F. 27 L.
+24 T. 30 L.



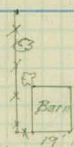
+45 T. 39 L.
+37 T. 37 L.
+12 Tree 48 L.
+10 steps 30 L.
+86 House 57



Lawn

+67 T. 32
+55 T. 32
+36 T. 32
+18 P.P. 50 L.
+18 Road sign 40 L.

-26 T. 18
-32 Hyd. 21 L.

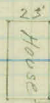


+82 11" T. 30 R.
+63 12" T. 30 R.
+60 Barn 34 R.
+87 Barn 37 R.
+57 F. 20 R.

+07 T. 27 R.

+48 P.P. 17 R.

+45 10 Drive Way
+57 T. 30 R.



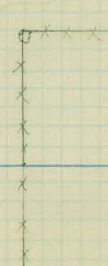
+17

+106 T. 22 R.

+59 T. 29 R.

+78 House 53 R.

+73 Thru T. 22
+46 T. 23 R.
+45 P.T. 17 R.



-26 6" T. 29 R.
-30 6" T. 29 R.
-32 15" T. 23 R.
-54 2" T. 29 R.

Fence 29 R.

sta.

9

8

7

6

5

4

3

+21 Fence 32

+95 Fence Cor 44' R

+87 T.P. 24' L.

+41 F. Cor. 42'

+49 F. Cor. 56' L.

+25 P.P. 21' R.

Fence 44' R

+97 Sign Post 20' R

7 3x10" P/20' R.
+97.0 R.R. Tract
500 Line

+65 F. 62' L.

+64 P. 42' R
End. +51 F. 32' R

+36 Cor. F. 26' L.
+34 T.P. 26' L.

+01 T.P. 26' R
Fence 26' R

+83 Private Lot 15' W.

+94 P.P. 19' R.

+97 T.P. 25' L.

Fence 26' R

+77 P.P. 20' R

+20 18" T. 30' L.
Fence 25' L.

Fence 24' R

+64 T.P. 24' L.

+68 C.T. 32' R.
+45 P.P. 20' R

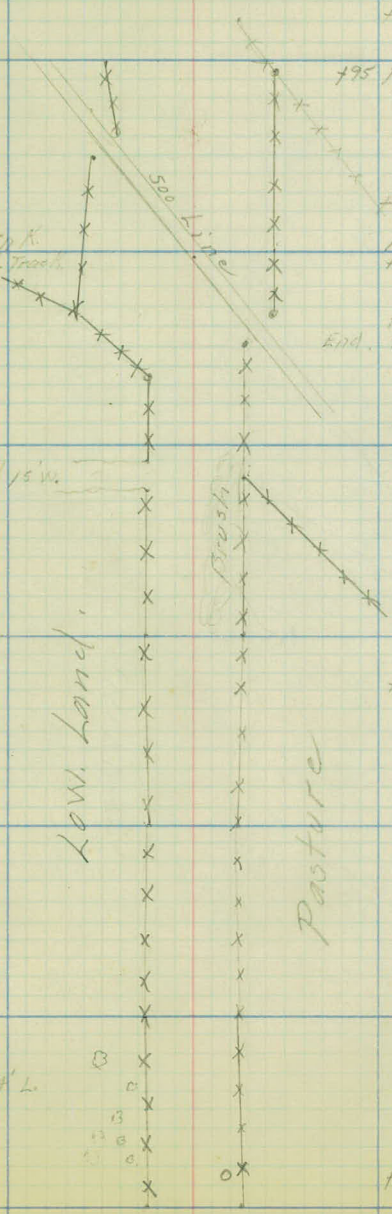
+25 8" T. 27' L.

F 15' R

+62 12" Tree 34' L.

+14 P.P. 19' R.

+20
26' F.



Sta.

15

14

13

12

11

10

9

+62 P. Ent. R.

+23 T.P. 24' L.
+25 Mail Box 2' L.

Fence 29'

+30 6" Tree 31' L.

Fence 24'
+96 T.P. 27'

+01 6" Tree 35' L.

+60 T.P. 24' L.

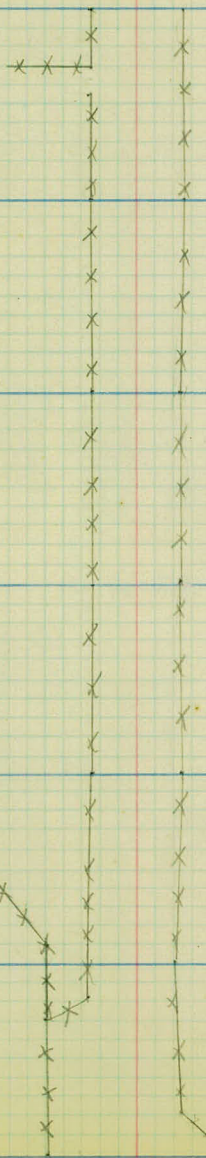
+21 6" Tree 35' L.

Fence 44' L.

+22 T.P. 26'
+10 F. Cor 49' L.

+81 F. Cor 26'

Fence 49' L.



Cultivated field

+64 P.P. 25' R.

F. 25' R.

Fence 32'
+01 P.P. 22'

Fence 22'

+50 P.P. 22'

Fence 33' R.

Fence 20' R.
+95 P.P. 30' R.

+21 F. Cor 22' R.

Sta.

21

20

19

18

17

14

15

23, 5, 8

+95 18' T. 28'
+92 F. Cor. 27'

+34 P.P. 27'R

F. 27'R

+57 Mai/Box 2'R

F. 17'R

+33 P.P. 26'R

+78 sign Post 22'R

+39 P.P. 25'R

Fence 26'
+97 P.P. 26'

+06 Cross P.
Fence 24'R

+98 T.P. 21'L
+34 Mai/Box
+78 Road
+62 Cor F. 20

Road

+56 T.P. 22'

+22 6" T. 19'L

F. 21'L

+27 T.P. 21'L
+03 12 T. 31'L
Fence 21

Swamp
10
11
12
13
14
15
16
17
18
19
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21
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89
90
91
92
93
94
95
96
97
98
99
100

54 Timber
13

Fence 22'
+95 10 T. 19'
+78 T.P. 22'
+99 6 T. 15'
+68 6 T. 18'
+50 8 T. 10 L
+34 6 T. 20'
+33 12 Tree 19 L

Fence 26'L

Cultivated field

Sta.

27

26

25

24

23

22

21

+98 Mail/Box 9 L.

+23 T.P. 18' L.
+18 P.P. 18' L.
+18 Sign Post 15' L.
F. Ent.

+65 6" T. 30' L.
+42 Sidewalk 30' L. 4" Wide
+36 14" T. 30'
+28 Post 15' L.
+12 14" T. 30'
+05 House 30' L.
+91 T.P. 18' L.
+88 5" T. 30'

+55 6" T.
+25 6" T. 27' L.
+24 Mail Box 8' L.
+16 F. Cor. 30' L.

+67 T.P. 15' L.

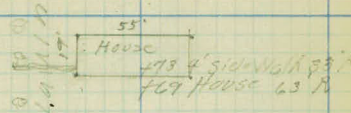
+40 F. Cor. 10' L.

+03 Guard rail
+90 Guard rail 9' L.

+77 Farm Ent 44' Wide
+50 Mail Box R.
+51 T.P. 19'

+71 9" T. 20' L.

+24 T.P. 21' L.



+13 27" T. 32' R.
+15 P.P. 27' R.
F. Ent.

+80 F. Cor. 20' R.

+25 5" T. 15' R.
+05 House 1
F. 25' R.

+81 P.P. 27'
+80 4" T. 12' R.

F. 25' R.

+13 P.P. 25' R.
F. 25' R.
+10 End of G. Rail

+93 Cross Drain
18" C.T.P. 25' Long
16' L. 2. 15' R.
+24 Guard rail 13' R.

+11 Cor. F. 30' R.
+17 12" T. 30' R.
+85 P.P. 20' R.



+22

Lawn

Cultivated Field

Mare/W.

Sta.

33

32

31

30

29

28

27

F. 26' R



House
 +41 House
 +37 F. Cor. 27' R

+14 P.P. 19' L
 +15 T.P. 19' L

P. Line. Crossed

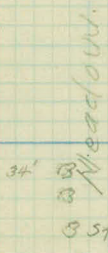
+14 P.P. 27' R.

Cultivated Field

+02 P.P. 19' L.

+35 R' T. 35' R.

+18 R' T. 35' R.

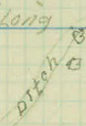


+48 T.P. 18' L
 +17 R' T. 19' L.

Cobble stone Wall with Plank roof. +23 30" T. 34' P

+10 Cross Drain
 6' Wide 4' Deep 16' Long

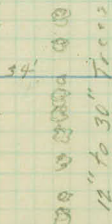
+95 3 1/2" T. 21' L
 +80 6' T. 15' L.



35' B → 13' L. & 13' R.
 3 stump
 12" to 25" trees

+39 P.P. 19' L.

+90 T.P. 19' L.



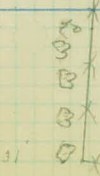
Mail Box 6' L.

32' X X +12 F. Cor 52' R

+89 P.P. 19' L.

+57 T.P. 19' L.

Cultivated Field



18" T. 31' R
 +19 F. Cor 46' R.

Sta.

39

38

37

36

35

34

33

+15 P.P. 28' R.
+18 End of F. 28' R.

+82 T.P. 19' L.

Cultivated field

Cultivated field

+72 P.P. 28' R.

+37 T.P. 19' L.

+24 P.P. 27' R.
F 27' R.

+14 T.P. 18' L.

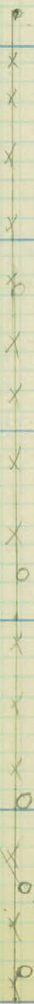
+52 P.P. 27' L. Cross Line

+05 P.P. 26' R.

+62 T.P. 18' L.

Crossline +59 P.P. 29' R.

+15 P.P. 26' R.
F. 24' R.



sta.

45

44

43

42

41

40

39

+50 F. 29' L.
+79 T.P. 29' L.

Cultivated field



+57 Cross F. 15' L.
+87 T.P. 27' L.



+06 F. Cor 15' L.
+88 3" T. 17' L.



+72 3" T. 17' L.
+56 4" T. 17' L.
+40 4" T. 17' L.
+23 6" T. 17' L.
Farm Ent. L.

Farmyard



+67 T.P. 24' L.

Barra

+47 T.P. 23' L.

Cultivated field

+18 T.P. 22' L.

+96 P.P. 26' R.

Cultivated field

+93 P.P. 28' R.

+02 P.P. 29' R.

+68 P.P. 29' R.

sta.

51

50

49

48

47

46

45

X
X
o
X
X
X
X
X
X
X
X
X
X
X
X



Needs
B
B

+29 F. Cor 19' R.

+78 P.P. 16' R.

Cultivated field

Cultivated field

+33 P.P. 19' R.

+92 P.P. 21' R.

+36 P.P. 14' R.

+05 T.P. 40' L.

+77 T.P. 36' L.
+77 F. 36' L.

+46 T.P. 34' L.
+46 F. 34' L.

+15 T.P. 32' L.
F. 32' L.

sta.

57

54

53

54

53

52

51

+82 T.P. 41' L.

+58 T.P. 41' L.

+33 T.P. 41' L.

+59 15" Stump 33' L.

+97 T.P. 43' L.

+25 F. Cor 43' L. * * *
+18 High power cross line

+38 T.P. 42' L.



+66 F. 19' R.
+66 P.P. 16' R.

+01 Cross Drain 12" C.T.P.
22' long 17' L. & 5' R.

+18 P.P. 14' R.
F. 19' R.

+72 P.P. 13' R.

+31 Cross F. 21' R.
+17 P.P. 24' R.
F. 22' R.

+83 10" T. 22' R.

+63 8" T. 22' R.

+54 5" T. 22' R.

+20 F. 20' R.
+17 P.P. 14' R.
F. 20' R.

Cultivated field
Brush

SWAMP

Woods

Stumps

Sta.

63

62

61

60

59

58

57

+99 24" T. 20' R.

Meadow

+19 T.P. 37' L.

F. 27' R.

+82 F. Cor. 48' L.
+87 Mail Box 3' L. X
+71 F. Ent. 10' Wide

+58 12" T. 23' R.
+55 P.P. 22' R.

Cultivated Field

F. 27' R.

+99 T.P. 37' L.

+07 P.P. 20' R.
F. 27' R.

~~SWAMP~~

+44 T.P. 37' L.

F. 25'

+61 3 6" T. 19' R.
+54 P.P. 19' R.

+04 T.P. 39' L.

F. 32' R.
+93 5" T. 24' R.

SWAMP

+05 P.P. 15' R.
F. 30' R.

Sta.

69

68

67

66

65

64

63

F. 14' L.

F. 14' R.

+86 P.P. 25' R.

F. 12' L.

+87 T.P. 34' L.

SWAMP

SWAMP

+54 P.P. 25' R.
+57 F. 25' R.
+48 F. Cor. 48' R.
+24 F. Cor. 55' R.
+23 Nail Box 3' R.
+14 Farm. 40' R.
+02 8' T. 40' R.

F. 12' L.

+66 C.T. 10' L.

+30 T.P. 34' L.

+30 6" T. 3' L.

F. 8' L.

+66 P.P. 25' R.
F. 36' R.

+67 12" T. 11' L.

+51 F. 9' L.

+46 Willows 32' R.
+41 Cor. F. 36' R.

F. 30' L.

+73 T.P. 34' L.

Meadow.

F. 34' R.
+73 Willows

+52 P.P. 24' R.

+39 4 5" T. 29'

F. 33' R.

+55 T.P. 34' L.

Brush

SWAMP

F. 35' L.

+18 T.P. 35'
F. 32' R.

578

75

74

73

72

71

70

69

F. 29' L
+71 T.P. 33' L
+63 30" T. 20' L

+44 T.P. 33' L

F. 33' L

F. 33' L
+94 T.P. 33' L

+54 F. Cor. 30'

+66 12" Stump 21' L
+58 T.P. 32' L

+46 10" T. 25' L

+22 Mail Box 6' x 12" C.I.P. 28' Long 12' L

+18 6" T. 22' L

+85 F. Ent. 15' Wide

+94 14" T. 13' L

+85 F. Cor. 17' L

+25 T.P. 33' L

Meadow

Farm yard

Brush

Cultivated Field

Cultivated Field

Swamp

+26 M.P. 24' R

Fence Posts

+67 F. Post 18' R

+14 F. Cor. 15' R
F. 16' R

+83 P.P. 23' R

F. 20' R
+70 24' T. 8' R

+55 8" T. 24' R

+32 P.P. 24' R

F. 30' R

+37 18" 22' R
+21 P.P. 24' R

F. 26' R

Sta.

81

80

79

78

77

76

75

+05 T.P. 30'L
F. 30'L.

+15 P.P. 22'R

Cultivated field

+79 F. Cor. 25'L
+68 F. Cor. 25'L
+68 T.P. 31'L



+68 Cross F. 18'R

+62 12" T. 28'L

+42 T.P. 31'L

F. 28'L.

Meadow

Cultivated field

+27 P.P. 22'R

+06 T.P. 32'L
F. 24'L.

+76 P.P. 13'R.

+03 24" T. 29'

brush

Sta.

87

86

85

84

83

82

81

+4' 10" T. 22' L.

+59 T.P. 26' L.

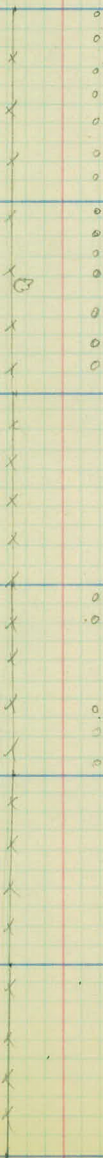
+19 12" T. 25' L.
F. 26' L.
+91 24" T. 25' L.

+60 24" T. 21' L.

+21 T.P. 28' L.
F. 28' L.

F. 28' L.
+85 T.P. 28' L.

+44 T.P. 28' L.



Unimproved field

Swamp

C. Field

+82 24" T. 46' R.
+77 24" T. 36' R.

+30 4 2" T. 15' R.

T.P. 23' R.

+52 3" T. 13' R.

+50 40" T. 8' R.

+14 F. Post 19' R.

+79 15" T. 35' R.

+33 P.P. 23' R.

F. Post 19' R.

+66 F. Post 19' R.

+77 P.P. 22' R.

+38 P.P. 22' R.

sta.

93

92

91

90

89

88

87

come to here.

F. 24' R.

+33 30" stump 17' L.

+58 10" T. 21' R.

F. 23' R.

+99 15" T. 22' R.

+76 30" T. 22' R.

F. 23' R.

F. 20' R.

F. 21' R.

+45 T. P. 27' L.

+82 Mail Box 21' L.

+64 Farm Ent.
+50 F. Cor 27' L.

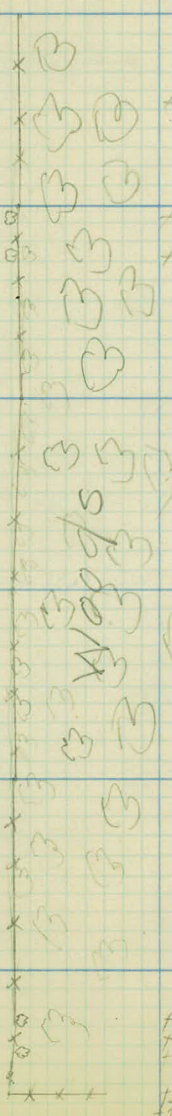
+03 T. P. 27' L.
F. 27' L.

+74 8" T. 22' R.
+51 10" T. 22' R.
+51 P. R. 23' R.

+31 F. Cor 15' R.
+27 Three 12" T. 14' R.

cultivated field

road



Sta.

99

98

97

96

95

94

93

105

104

103

102

101

100

99

111

110

109

108

107

106

105

115

114

113

112

111

121

120

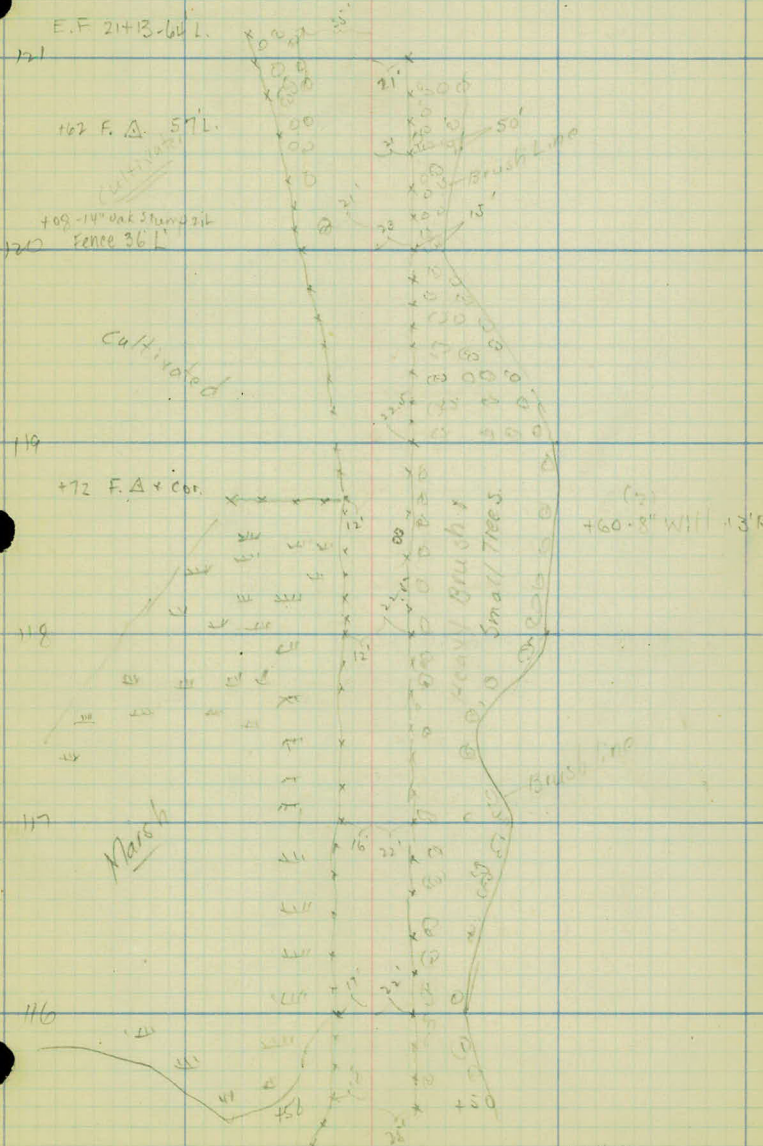
119

118

117

116

115



W.H.C.
 C.E.J. } 2/25/74
 M.S.A.
 T.F.

station

127

+58 ± F.E. L.

+38 culvert

126

125

124

123

122

+98 10' x 22' ± Vit. Ext. 10'R.

121

Thick Poplar
Oaks

+84 E.F. 20'L.

+27-18" Oak 16'

+28-24" Oak - 24'
+18-10" Spruce 12'

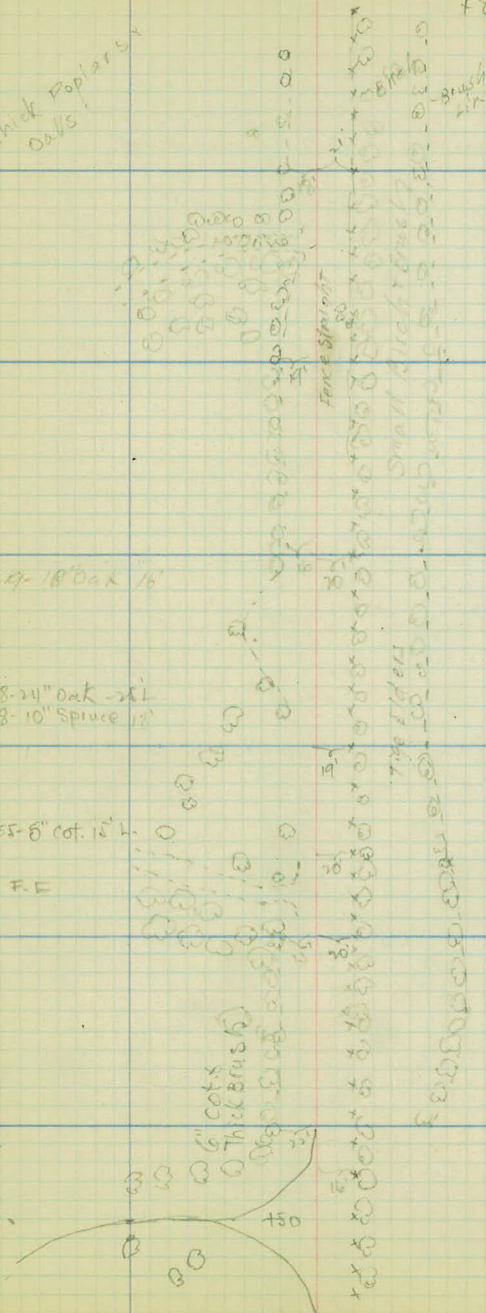
+55-8" Cot. 16'L.
+L
+29 F.E.

+45- F.A. - 20'R

+61 F.A. 16'R

+78 F. Δ 16'P.

F.E.



+31 Wil
+HR

station

133

132

131

130

129

128

127

Large Trees

- +65 - 8" Oak
- +55 - 28" Oak
- +35 - 8" Oak

Heavy Oaks

Scattered Oaks

+15 - Old 24" Oak
Rotten

- +52 - 12" Oak 15' L
- +45 12" Oak 12' L
- +05 8" " 70'
- +35 - 15" Oak 15'
- +50 - 8" Oak 11' L

Scattered Oaks



Lake Shore

Small Birch & Bush



Station

139

138

137

136

135

+58 12" X 24' conc. cu l. EXT P'R.

+25 Int. of Road

134

+83 ± F.I.E. Left.

133

Cultivated.

+50-8" Oak 12' L.
+42 7" " 12' L.

+62-4" Oak 18' L.
Cultivated.

Small Branch
0.5' x 1.0' x 0.5'

+14-18" Oak 12' R
+092 40 " 11' R

+71-24" Oak 14' R

+06-8-8" Pop. 7' R

to here 2/28/24

Woodsy Oaks.

+55 Mail Box 8' L.

+45 6" Oak 18' L.

+28-20" Oak 18' L.

+08 17" Oak 24' L.

Heavy
oak Maple
Branch

Tree line

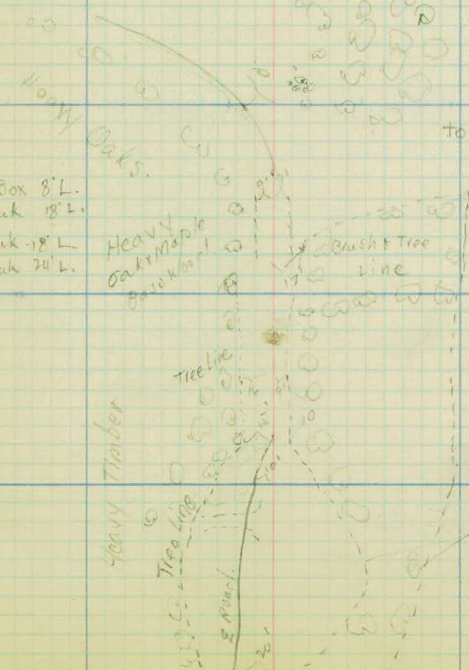
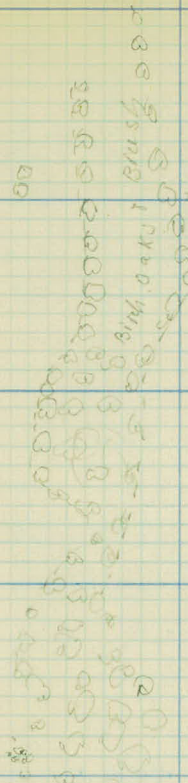
Heavy Timber

Tree line

Brush Tree
line

Brush line

Brush Tree
Line



Station

145

144

143

142

141

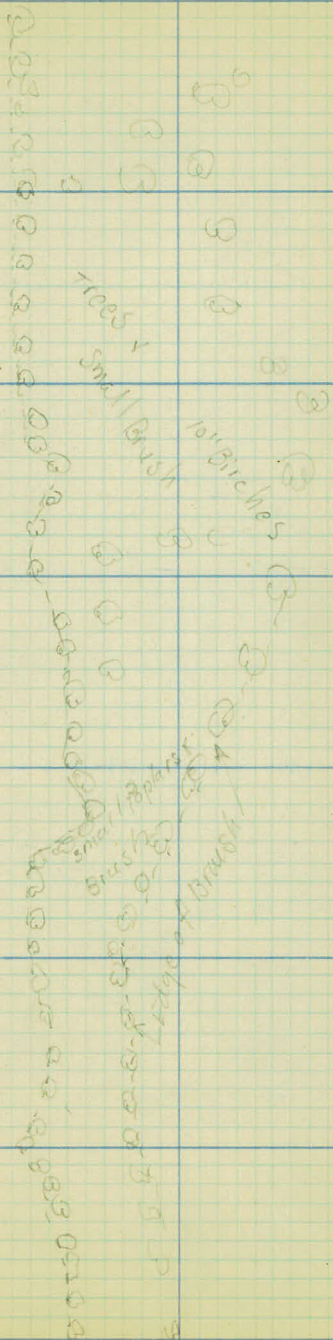
140

139

A

cultivated

cultivated



station

151

150

149

148

147

774 - ~~24~~" X 31' galv. culv.

146

145

station

151

152

740 Mail/Box 20 Bank

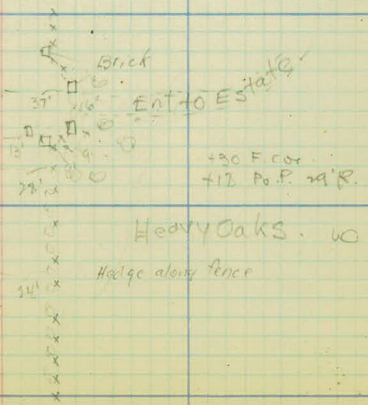
726

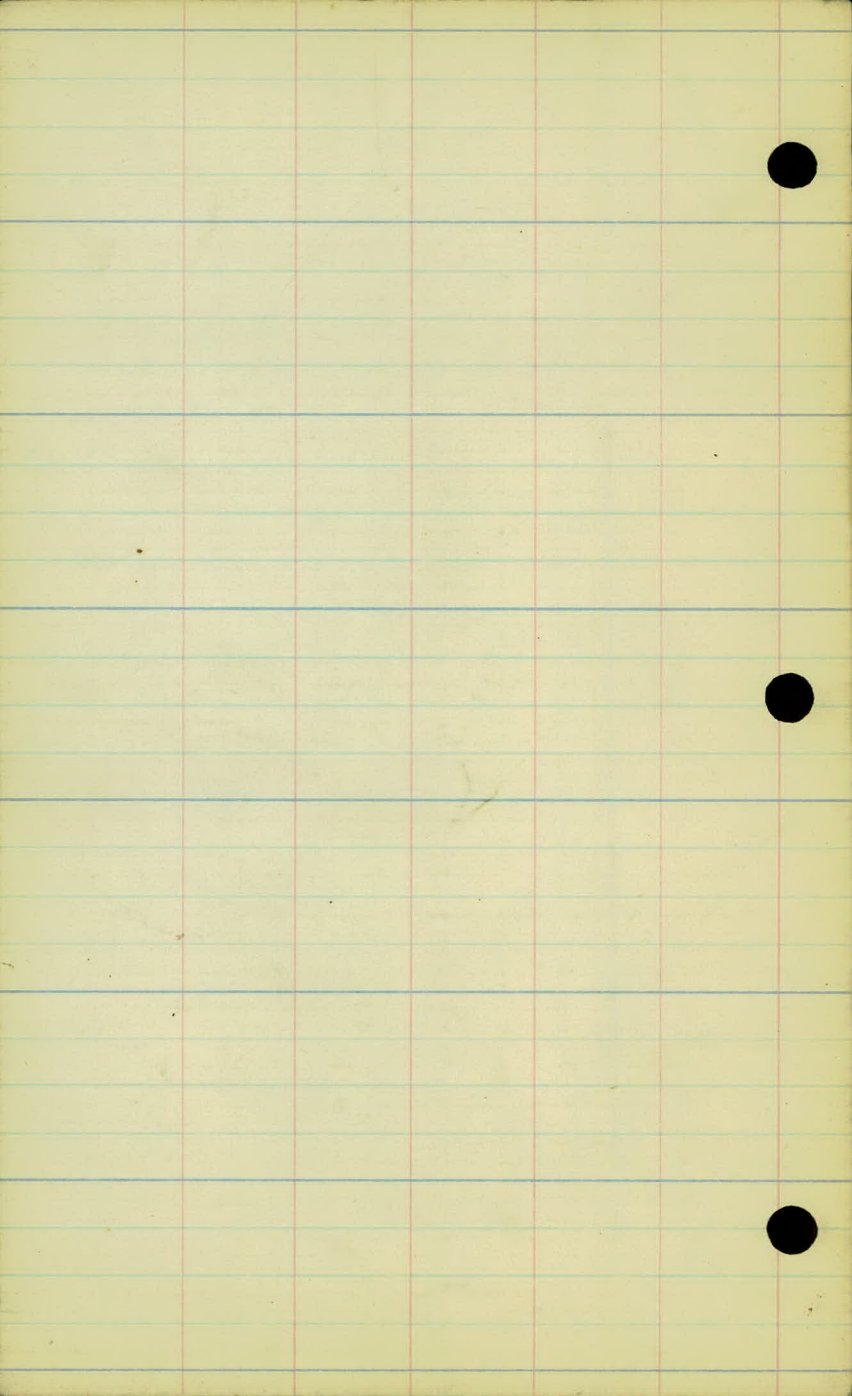
152

151

To here 2/29/24

Cultivated





24-52

Proj. # 23-52.

X sections from Sta 0+00
to

Sta.

Elev.

5

4

3

2

+44 10.9

Pr. Ent

1

+34 00

+25 -12.5

90.6

0 +00

-14

-0.6

-20

-0.1

-50 -0.2

L

R.

902

-2.0	-2.1	00	+0.3	-0.3	-2.0	-1.8	-1.4
33	20	14	7	3	8	18	33

903

-2.2	-1.7	+0.2	+0.4	-0.3	-1.2	-1.1	-0.9
33	21	15	70	2	7	20	33

907

-0.6	-0.5	+0.1	-0.9	-1.2	+0.4	+0.4
33	22	13	10	18	24	33

922

+1.2	+1.6	-0.5	-0.1	-0.5	-0.4	+0.2
33	31	26	15	11	19	33

728

+2.2	+2.5	-0.2	00	10	+0.8	+0.2	+0.7
33	31	25	12	15	26	40	50

920

+2.2	+2.1	-0.3	+0.2	-0.8	+2.7	+2.9
33	31	26	12	13	21	33

905

+0.2	+0.6	-0.4	-0.4	-0.7	-0.4	+2.6	+3.1
33	31	26	13	15	23	28	34

90.61

-1.0	-0.6	-0.2	-0.3	-0.7	-0.8
33	28	16	13	25	33

91.57

+1.6	+0.5	-0.4	-0.3	-1.2	-0.4	-0.1	00
300	200	100	33	33	100	200	300

-1.8	-1.4	-0.1	-0.2	-1.0	-1.3
33	20	8	14	30	33

-1.8	-1.3	-0.1	-1.1	00
33	15	9	24	33

-2.2	-1.7	-1.1	-0.1	-1.2	-0.4
33	79	11	9	18	33

Sta.

Elev.

11 ←
+ 90 - 0.7

10

9

+ 27 - 1.0

8 ←

+ 77 + 1.4

+ 54 + 1.0

+ 35 + 0.5

+ 20 + 0.2

7

6

L:

R

89.5

-0.2	+0.1	-0.8	-0.8	+0.1	00	-1.4	-1.7	+1.6	+1.7
43	37	33	17	9	10	19	26	33	35

88.8

-1.1	-1.0	+0.1	+0.1	+0.1	-1.3	-0.6
33	18	11	3	8	20	33

88.2

-2.6	-1.2	+0.3	+0.2	-0.1	-1.7	-1.8	-1.5
33	16	11	4	4	9	20	33

88.5

-1.8	-1.1	00	+0.2	00	-1.2	-1.7	-1.9
33	17	12	4	4	8	19	33

90.7

00	00	+0.1	00	-2.9	-3.5
33	15	7	6	18	33

91.7

-1.4	-1.1	-1.6	00	-0.9	-1.2	-3.5
33	27	20	9	10	23	35

91.5

-1.2	-0.9	-0.1	00	+0.1	00	-0.6
33	14	11	4	4	16	33

90.9

-3.7	-4.2	-0.1	+0.2	-0.1	+0.2	+0.4
34	20	11	5	5	24	33

90.6

-3.9	-5.2	-3.2	-4.0	-3.6	-0.2	00	00	-0.5	+0.4	-0.1	+0.2
34	33	29	25	17	11	5	5	6	10	25	33

90.3

-4.1	-5.4	-3.6	-3.6	-3.4	+0.1	+0.2	+0.1	-2.7	-3.2	-2.4	-0.6
34	32	28	24	18	11	4	5	11	24	28	33

90.1

-2.7	-3.4	-2.6	+0.2	+0.3	+0.2	-3.1	-3.0	-3.1
33	23	19	12	6	2	10	22	33

90.0

-3.4	-3.0	-0.1	+0.1	-0.4	-2.3	-2.2	-2.2
33	20	14	7	3	8	16	33

Sta.

Elev.

19

18

+40 - 01 68

17

+37 + 01 41

16

15

14

13

+32 + 01 42

12

+40 + 01 42

11

895

L.

R.

824

-41	-28	-19	+0.3	+0.2	-0.4	+0.1	+0.5
33	13	5	9	18	23	27	33

85.2

-17	-0.4	-1.0	+0.2	+0.1	+0.1	+2.2	+3.0
33	16	10	6	13	22	24	33

85.7

-0.2	+1.0	-1.0	-0.1	+0.3	-0.1	-0.8	+1.5	+2.3
33	22	14	5	4	11	19	27	33

86.9

+0.2	-0.2	-0.2	+0.1	-0.3	-1.1	+0.1	+0.4
33	20	9	7	15	19	24	33

87.7

-0.4	+0.1	+0.4	00	00	-0.1	-1.2	+1.8	+2.0
33	23	14	8	8	13	20	23	33

87.5

-0.9	00	+0.3	+0.1	-0.8	+1.3	+1.3
33	23	10	8	19	24	33

87.4

-2.5	-2.1	-1.6	-0.3	+0.3	+0.4	-1.9	-1.9	-1.4
33	18	6	3	7	15	21	24	33

87.7

-1.4	-1.9	-1.7	-0.4	-0.2	-0.2	-1.3	-0.9
24	17	7	2	4	16	22	33

88.3

-2.4	-2.2	-1.2	00	00	-0.1	-1.0	-0.9
33	14	7	3	4	13	11	33

89.5

-1.6	-1.4	-1.3	-0.7	+0.1	00	-1.3	-1.3
34	29	20	11	4	9	19	33

90.4

+2.0	+2.2	-1.4	-1.4	00	00	-0.5	-0.7	-2.0	+1.3	+1.3
40	33	25	14	4	10	15	22	29	35	40

90.7

+5.0	+5.0	-1.1	-1.8	-3.5	-3.3	-0.1	-0.5	-1.9	-1.9	+5.2	+5.2
45	41	33	35	23	15	10	11	19	25	35	40

Sta.

Elev.

25

+76 -1.0

+24 +1.2

24

+50 +1.5

23

+93 +0.1

Cross Drain

+77 +1.8

Farm Road L

22

21

20

+78 +1.3 HL

Farm Road L.

L.

R.

4.7

91.7
 +3.9 +3.2 +1.0 -0.3 00 +0.8 +6.5 +6.0
 33 20 14 10 9 15 21 33

90.7
 +4.7 +3.7 -0.1 -0.1 +0.4 +7.7 +7.4
 33 20 10 8 15 25 33

87.9
 +1.1 +1.0 -0.3 -0.1 -0.8 +0.5 +0.8
 33 14 10 10 19 22 30

86.7
 -2.7 -2.2 -1.0 -0.2 -0.2 -2.1 -2.8 -3.8
 33 22 14 9 4 16 25 33

85.1
 -4.2 -3.0 -0.2 00 -3.0 -4.2 -3.8
 33 12 4 10 17 23 33

84.5
 -2.7 -2.9 -1.7 +0.1 +0.1 00 -2.3 -4.0 -3.1
 33 23 12 6 3 12 18 26 33

invert invert
 84.6
 -4.5 -4.0 -4.2 -4.1 -0.3 -0.1 -3.9 -4.5 -5.5 -3.0
 50 33 22 10 8 11 15 22 33 50

84.3
 -0.4 -1.2 -1.2 -0.9 00 -0.9 -9.4 -3.0
 50 34 29 11 9 15 21 32

83.7
 -0.7 -0.5 -0.8 +0.2 -0.1 00 +0.4 +0.2
 33 23 14 5 15 24 26 33

82.1
 -9.3 -1.3 -1.8 +0.1 -0.6 -0.2
 33 19 6 9 20 33

80.9
 -4.0 -2.7 -1.7 +0.7 +0.9 +0.8 -0.5 -0.1
 33 16 5 4 10 19 22 33

81.2 -H.L.
 -2.1 -2.7 -1.3 -1.2 +0.7 +0.7 +0.5 -0.8 +0.2
 50 33 20 9 6 11 19 24 33

sta.

Elev.

33

32

31

+10 +0.2

30

+49 +0.3

29

28

27

+50 +0.5

26

Pr. Ent. L. & R.

+80 +0.2

10.8

+1.3	+1.4	+0.4	-0.1	-0.2	-1.2
33	22	7	8	15	33

1007.1

+2.4	+1.2	+0.9	0.0	+0.2	+0.1	+1.2
33	14	4	8	19	27	33

03.1

+2.0	+0.7	-0.4	+1.3	0.0	-0.1	-3.3	+0.9	+1.1
33	19	9	5	11	14	27	32	34

Ditch → Invert

00.6

-3.4	-3.2	-3.4	-6.4	-5.8	-0.2	-0.1	-0.1	-4.0	-2.4	-2.0	-1.8
32	29	24	20	13	13	3	13	13	12	33	50

Ditch

1000.2

-3.5	-3.2	-6.2	-6.2	-4.9	+0.1	+0.2	0.0	-1.0	-1.2
33	29	24	20	13	4	4	12	21	33

Ditch

99.5

-5.3	-7.0	-6.7	-5.7	-4.2	+0.1	+0.2	+0.1	-0.2	+1.0
51	48	42	39	13	4	5	14	20	33

99.2

-4.3	-3.6	0.0	-0.2	-0.1	+1.4	+2.9
33	14	4	10	20	33	37

97.2

-0.9	+0.2	+0.5	+0.2	+0.8	+2.6
33	15	7	15	22	33

94.0

-1.0	-0.4	+0.3	0.0	+0.3	+1.7	+1.8
33	18	7	8	21	28	33

92.8

-4.8	-4.3	+0.4	+0.1	-0.2	+0.4	+2.0
33	20	8	5	17	29	33

92.3

0.0	+0.4	+0.1	+0.3	-0.3	-0.6	-0.8
50	33	20	9	16	33	50

92.4

+1.8	+1.8	+0.1	-0.4	-0.7	+0.1	-1.4
33	23	11	11	15	19	33

Sta

Elev.

41 ←
+73 +13

40

+64 -03

39

+64 -13

38

+60 +21

37

36

35

+50 +17

34

h.

R

06.5

-0.5	-3.2	-0.6	+0.9	-0.7	+4.5	+5.1
33	17	5	12	24	28	33

.081

+1.2	+2.7	+1.0	+0.9	+0.4	+0.2	+2.3	+2.4
33	18	7	12	19	26	30	33

08.1

-0.2	00	-0.4	+1.0	+0.2	+1.0	+1.0
33	18	4	11	24	29	33

08.4

-2.7	-2.9	-2.8	=0.3	+0.4	+0.3	+1.0
33	22	9	4	11	23	33

9.3

-8.1	-4.4	-0.5	+0.4	+0.3	-0.2	+1.0	+1.1
33	12	4	10	17	22	27	33

11.1

-6.8	-2.5	-0.4	+0.6	00	00	+2.8
33	11	7	9	17	22	33

13.3

-4.5	-1.9	-1.0	+0.6	+0.2	-0.1	+2.6	+3.0
33	21	9	7	15	21	27	33

17.4

-2.1	-0.1	-0.9	+0.1	-0.3	+1.3	+2.8
33	13	7	7	19	22	33

18.9

-1.4	-0.6	+0.1	00	-0.4	00	-0.8
33	24	10	6	17	24	33

17.5

-0.3	+1.1	+0.6	+0.2	-0.1	00	-0.4	-1.2	-1.8
33	17	7	6	15	23	29	30	33

15.4

+2.1	+2.0	00	00	-0.3	-1.5	-2.4	-3.2
33	17	6	6	15	28	30	37

13.7

-0.4	+0.1	+0.1	-0.3	-0.3	-2.2	-2.9	-4.1
33	22	4	7	13	25	29	33

Sta.

Elev.

48

+ 55 + 2'

47

46

+ 75 + 16'

45

+ 61 + 10'

44

+ 35 - 03'

43

42

Pr. Ent. L.

+ 50 + 06'

41

L.

R.

00.9

-2.6	+0.7	-0.8	0.0	-0.2	+2.7	+4.6
33	16	8	7	15	25	33

02.6

-5.7	-2.3	+0.4	+0.2	+1.7	+2.5
33	15	8	17	27	33

03.8

-3.7	-0.9	+0.1	+0.2	+1.8
33	18	10	23	33

03.2

-4.5	-3.4	-2.4	+0.9	+0.7	+0.9
33	18	7	11	21	33

02.6

-4.0	-5.1	-3.2	+0.7	+0.4	+1.6
33	15	4	11	22	33

02.7

-7.6	-5.2	-2.5	+0.3	+0.2	+2.7
33	22	7	11	22	33

02.0

-2.1	-2.4	-2.4	+0.5	+0.3	+0.7
33	20	6	10	22	33

02.1

+1.1	+1.0	+0.6	+0.4	0.0	+0.5
33	13	11	17	25	33

02.7

0.0	+0.3	+0.4	0.0	-0.4	+1.2
33	10	11	18	27	33

02.1

-0.8	-0.5	-0.3	+0.8	+0.6	-0.1	+1.0
50	25	9	9	14	28	33

02.9

-3.1	-2.8	-0.1	+0.5	+0.2	+0.1	+5.3	+5.6
33	15	4	10	19	14	31	33

05.1

-8.8	-7.8	-2.0	-0.3	+0.4	-0.5	+5.2	+5.9
33	27	14	8	12	22	27	33

Sta.

Elev.

57

+40.29

56

55

54

+40.05

53

52

51

50

49

48

L

R.

82.9

+1.1	+0.5	-0.7	-0.7	-0.2	+3.2	-3.0
33	23	9	10	27	33	40

82.0

+1.5	+0.6	-0.4	-0.3	-0.5	-0.7	-1.6
33	20	13	5	6	14	33

80.4

+0.3	-0.4	+0.2	-0.2	-2.3	-3.0	-3.0
33	14	4	3	10	20	33

80.4 invert

-2.4	-2.4	-2.9	-0.6	+0.2	00	-2.8	-3.0	-3.5	-3.5
33	28	17	15	6	3	5	17	33	50

80.8

00	-1.4	-1.6	00	+0.7	-2.1	-3.1	-3.5
33	30	20	14	8	4	18	33

81.2

-0.2	-1.0	+1.1	+0.5	-2.2	-2.9	-3.0
32	23	17	8	5	18	33

81.7

-1.9	-1.6	00	+0.4	-2.3	-2.8	-3.0
33	24	17	7	7	14	33

82.8

-1.9	-1.9	-0.5	00	-0.3	-1.3	-1.5
33	24	15	8	10	21	33

84.9

-1.0	-1.1	-0.2	00	+2.4	+2.3
33	28	14	12	17	33

88B

-4.3	-3.5	-0.7	-0.3	+1.0	+2.0
33	23	12	12	20	30

93.1

-5.3	-3.0	-0.5	-0.4	+1.0	+2.9
33	21	10	15	25	33

99.1

-1.2	+0.5	-1.1	-0.6	+0.1	+0.6	+4.8	+6.1
33	13	14	8	7	17	28	33

Sta.

Elev.

67

+884.3

64

65

64

63

62

+71.21

Edm Cut h: 15' to 10' wide

61

60

59

58

+42.10

57

82.9

L.

R.

72.3

+0.7	+0.2	-1.2		+2.1	+2.4	+1.9	+1.4	+0.7	+0.7
33	15	3		4	15	25	30	33	30

72.4

+1.4	+1.1	+1.1		+1.4	+3.0	+3.4	+3.2	+1.1	+1.1
33	22	7		5	9	14	24	30	33

71.9

00	-0.1	-0.3	-0.8	+1.2	+1.7	+1.3	+0.1	00
33	26	4	4	4	15	23	29	33

72.2

-0.6	-0.6	+1.0	+1.5	+1.1	-1.1	-0.3	-0.3
33	5	7	13	21	28	30	33

73.7

-1.5	-1.4	-1.5		+0.7	+0.1	+0.6	-1.0	-1.5
33	15	4		3	12	19	23	33

75.5

-0.6	-1.1	-3.0	-0.6	+0.3	-0.2	-2.3	-2.8
33	11	9	6	10	17	23	33

75.4

-0.3	-0.4	-0.4		+0.3	00	-2.4	-2.8
50	33	21		9	16	22	33

75.4

-2.4	-2.9	-2.4		+0.4	+0.3	-2.6	-2.9
33	18	7		7	15	22	33

76.0

-2.7	-2.6	-1.4	00	+0.3	-0.1	-2.7	-3.2
33	17	6	1	7	13	20	33

77.2

+1.4	+0.5	-0.3	00	-0.3	-2.7	-3.8
33	17	4	5	12	21	33

82.0

+4.7	+2.2	+1.1		+0.4	-0.5	-0.1	-0.4
33	19	12		5	12	15	33

83.5

+0.4	+0.2	-0.7		-1.7	-0.1	+0.8
33	20	8		12	16	33

Sta.

Elev.

+40⁰⁰

74

75

72

+55-07

71

+75-02

70

69

68

+14-03

67

Farm Ent. L.

Farm Ent. R.

68.0

-0.9	0.0	-1.4	0.0	+0.6	-1.0	+2.5	+3.6
33	20	19	17	6	11	18	33

68.0

-1.4	-0.9	-1.4	+0.3	+0.8	-1.1	+1.5	+2.4
33	14	21	14	9	9	18	33

68.4

-1.8	-1.6	+0.7	+0.5	-1.3	-2.1	-1.0
33	21	14	8	7	13	33

70.0

-1.5	-1.8	-1.2	+0.1	+0.4	-0.4	-1.8	-0.8	-0.7	-0.8
33	22	19	13	5	6	13	18	26	33

71.1

+0.2	-0.1	-0.3	-0.3	-0.7	-0.2	+0.2	-0.8	-1.9	-0.6	-0.2	-1.8	-0.7
33	23	21	19	15	11	4	6	17	20	26	30	33

71.8

+3.6	+3.2	-3.1	-3.1	-0.6	-0.7	-1.3	-1.7	+0.4
33	24	17	15	11	10	21	30	33

72.3

+4.0	+3.7	-3.2	-3.2	-0.5	-0.7	-1.6	-1.9	+0.3
33	20	13	11	7	12	21	31	33

72.5

+0.2	0.0	-0.3	+0.2	-0.1	-2.2	-2.8
50	33	14	3	10	18	33

71.4

-2.1	-2.1	-1.8	+0.6	-0.5	-1.8	-1.8
33	17	6	11	14	19	33

70.7

-1.6	-1.4	-1.4	+0.9	+1.4	+1.1	-1.4	-1.4
33	12	3	2	11	16	18	33

70.8

-1.5	-1.3	-1.0	+1.5	+2.1	+1.7	+1.8
33	26	9	4	15	33	50

71.0

-1.3	-0.7	+2.2	+2.2	+1.7	-0.3	-1.4	-1.4
33	9	6	14	27	29	32	33

Sta.

Elev.

85

+70

Int. (83.5) ?

84

83

82

81

80

79

78

77

76

75

85.5

+0.4	-0.2	+0.3	-1.7	-3.6	-4.1
33	17	4	14	22	33

83.5

+0.8	10	-0.6	+0.3	-0.6	-2.5	-2.5	-1.0
33	18	12	5	9	21	30	33

78.8

-1.4	-0.3	00	+0.4	-0.5	-1.9	-2.7
33	19	12	5	7	19	33

75.5

-2.3	-0.9	+0.3	+0.6	-2.0	-3.4	-3.5
33	19	13	8	9	21	33

75.6

-2.3	-1.0	+0.5	+0.1	-0.5	+0.1	+1.1
33	18	12	8	4	13	33

75.1

-1.7	-1.6	-0.1	+0.3	10	+0.7	+2.1
33	19	13	7	5	10	33

72.7

-0.3	-1.1	-0.1	+0.2	-0.9	+0.2	+1.3
33	19	11	5	10	18	33

69.6

-0.7	-1.0	-0.3	+0.5	+0.4	+1.1	+2.2
33	21	15	9	11	21	33

67.4

-1.7	-1.9	+0.5	+2.2	-1.1	-0.1	+0.1
33	18	12	7	12	22	33

66.7

-2.3	-1.7	+0.7	+0.7	-0.4	-1.6	-0.3
33	21	14	10	7	19	33

-66.7 66.7

-2.1	-1.4	+0.1	+0.4	-0.9	-0.4	-0.5
33	19	12	7	11	20	33

67.4

00	+0.4	-1.1	+0.3	+0.7	-0.5	+1.4	+1.4
33	23	22	15	8	10	16	33

Sta

Elev.

92

+56 - 0.8

91

90

89

88

+64 + 0.5

Form E-1

+10 + 0.3

87

+40 + 0.1

86

+70 + 0.2

85

L

R.

83.8

+2.0 -0.3 -0.1 -0.4 -1.2 -1.2 +0.1 -0.4
33 18 12 6 11 18 22 33

88.0

+3.6 +1.3 -1.7 -0.8 -1.3 +1.4 +1.4
33 23 11 10 14 14 33

88.8

+1.4 0.0 -0.9 -0.5 -1.0 +1.0 +1.0
33 21 12 9 17 20 33

91.3

+0.8 +0.4 -0.5 -0.8 -1.3 -0.2 -0.2
33 25 13 8 15 19 33

94.7

+3.9 +1.4 +0.3 -0.2 +0.4 -1.5 -1.0 +0.1
33 20 12 7 10 19 25 33

98.4

+3.7 +1.0 +0.4 +0.4 -0.9 -3.2 -4.7 -7.8
33 25 14 3 12 19 29 33

98.9

+2.4 +2.0 +0.1 +0.4 -0.4 -3.8 -5.0
33 33 13 5 12 26 33

97.9

+2.5 +1.4 +0.9 +0.1 -0.1 -0.8 -1.6
33 24 15 2 9 20 33

97.6

+2.4 +1.8 +0.1 +0.3 -0.6 -3.2 -3.6 -1.1
33 25 15 3 8 19 22 33

94.2

+2.5 +1.4 -0.1 +0.4 -1.1 -1.4 +2.0 +2.0
33 21 15 5 11 24 31 33

92.1

+0.8 +0.1 -0.4 +0.1 -1.2 -1.1 +3.2 +1.5
33 18 12 5 9 20 28 33

90.5

+0.1 -0.1 -0.4 +0.3 -0.5 -1.4 -1.0 -0.4
33 18 11 4 7 16 28 33

sta.

Elev.

99

98

97

+50 +1.8

96

+50 -20

95

+50 +3.4

94

+646 P.C. -5.3

93

+50 -5.1

92

L.

R.

43.5

+1.3	+0.2	+0.1	+0.1	-0.8
33	9	7	15	33

45.8

+1.5	+0.8	-1.0	-0.8	-0.5	-0.3
33	24	9	11	17	33

50.1

+2.9	+1.4	-0.7	-0.2	-0.3	+1.7	+1.7
33	16	8	8	13	16	33

52.2

+2.8	+2.6	+1.4	+0.3	+0.2	+1.4	+1.8
33	19	12	7	17	22	33

54.8

+1.3	+0.7	-1.3	-1.0	-1.5
33	16	18	25	33

56.1

+1.3	+0.8	-0.4	-1.3
33	23	17	33

58.0

+1.7	+1.2	-0.7	-1.6
33	20	18	33

62.1

00	-1.0	-0.4	+0.3	-0.5	-1.4
33	15	7	14	26	33

66.8

-1.0	-1.1	-1.4	-1.3	-2.0	-1.6	+0.6	+0.7
33	16	5	13	18	23	28	33

73.3

-2.2	-2.2	-0.5	-0.1	-1.1	-1.8	-0.7	-0.2
33	21	12	8	13	18	22	33

78.6

-1.8	-2.7	-0.3	-0.4	-1.8	-0.8	-0.1
33	21	11	10	18	24	33

78.7

-2.2	-3.6	-0.8	-0.8	-0.4	-1.3	-0.2	-0.5
33	29	14	7	12	14	24	33

Sta

Elev.

104

+90 -31

15" Vit. Culvert 28' Long.

+50 -22

103

+50 +18

102

+50 -07

+10 -10

Pub. Ent. R.

101

+14 -02

15" Vit. Culvert 29' Long.

100

+50 -07

99

X-sections.

P. J. Crane Tohere.

Sta 104

+0.6 -0.1 -0.2 -0.2 -5.4 -9.0
33 20 10 10 21 33

invert

invert

403.

-0.2 -1.5 -1.7 -2.9 -2.9 +0.2 -1.2 -6.0 -7.4 -7.5
33 24 24 19 14 11 14 17 23 33

41.7 ←

+0.9 +0.7 -1.4 -0.6 -0.2 -10.0 -10.5
33 20 14 10 10 35 40

43.4

+4.3 +3.0 -2.4 -0.7 -1.2 -9.0 -10.1 -12.7
33 22 14 7 11 27 33 40

+6.0 +4.0 -1.8 -1.0 -8.6 -10.4 -12.7
33 21 12 12 27 33 40

+5.7 +4.5 +3.5 -0.4 -1.0 -8.7 -9.0
33 23 14 9 14 33 40

+5.3 +2.2 +0.1 -0.3 -0.9 -3.4 -5.3
33 14 12 8 11 24 33

+3.6 +1.3 +0.2 -0.9 -4.0 -4.5 -5.0
33 14 9 9 21 33 50

+3.7 +2.3 +1.2 +0.1 -0.9 -3.6 -4.0
33 22 15 12 12 21 33

Invert

invert

+0.7 -1.7 -2.2 +0.1 -1.0 -9.2 -4.4 -4.5
33 21 13 11 10 11 23 40

+0.7 +0.1 -1.2 -0.4 -1.1 -2.6 -2.6
33 22 14 11 11 18 33

+0.7 -0.2 +0.1 -0.4 -1.5 -1.5
33 20 13 12 20 33

Station Elev.

110+50 6.8

110+20 4.8

110 5.0

X

109 6.7

+50 8.5

X

108 5.8

+55 5.6

107 4.6 103

+53 3.1 145

X

106 5.4 102

+44 5.1 119

105 5.6

104+50 5.8

104 Last 5.2

$$L \quad Z \quad R$$

$$+5.4 \quad +2.2 \quad +0.2 \quad -0.1 \quad 40.0 \quad +0.5 \quad +0.1 \quad -1.3 \quad -4.6$$

$$\frac{33}{33} \quad \frac{10}{10} \quad \frac{7}{7} \quad \frac{4}{4} \quad \frac{40.0}{40.0} \quad \frac{10}{10} \quad \frac{22}{22} \quad \frac{27}{27} \quad \frac{23}{23}$$

$$42.1$$

$$+2.3 \quad +2.3 \quad +1.2 \quad 0.0 \quad -0.6 \quad +0.1$$

$$\frac{33}{33} \quad \frac{16}{16} \quad \frac{14}{14} \quad \frac{12}{12} \quad \frac{7}{7} \quad \frac{2}{2}$$

$$-0.5 \quad -0.5 \quad -0.6 \quad -0.8 \quad -3.0 \quad -9.6$$

$$\frac{2}{2} \quad \frac{10}{10} \quad \frac{14}{14} \quad \frac{18}{18} \quad \frac{23}{23} \quad \frac{33}{33}$$

$$41.9$$

$$+3.9 \quad +2.3 \quad -0.1 \quad 0.0 \quad -0.3 \quad +0.2$$

$$\frac{33}{33} \quad \frac{21}{21} \quad \frac{18}{18} \quad \frac{14}{14} \quad \frac{9}{9} \quad \frac{3}{3}$$

$$-0.6 \quad -0.1 \quad -1.4 \quad -4.4 \quad -9.5$$

$$\frac{10}{10} \quad \frac{15}{15} \quad \frac{18}{18} \quad \frac{24}{24} \quad \frac{33}{33}$$

$$37.2$$

$$+0.2 \quad 0.0 \quad -0.7 \quad -0.6 \quad 0.0 \quad +0.2$$

$$\frac{33}{33} \quad \frac{17}{17} \quad \frac{16}{16} \quad \frac{13}{13} \quad \frac{9}{9} \quad \frac{3}{3}$$

$$-0.2 \quad -0.5 \quad -1.0 \quad -0.7 \quad -2.7$$

$$\frac{4}{4} \quad \frac{8}{8} \quad \frac{11}{11} \quad \frac{16}{16} \quad \frac{33}{33}$$

$$+1.9 \quad -1.6 \quad -1.0 \quad -0.3 \quad +0.2$$

$$\frac{33}{33} \quad \frac{17}{17} \quad \frac{12}{12} \quad \frac{7}{7} \quad \frac{3}{3}$$

$$-0.4 \quad -1.2 \quad -2.0 \quad -3.5$$

$$\frac{5}{5} \quad \frac{8}{8} \quad \frac{14}{14} \quad \frac{33}{33}$$

$$+2.0 \quad -0.4 \quad -1.2 \quad -0.3 \quad +0.1$$

$$\frac{33}{33} \quad \frac{21}{21} \quad \frac{15}{15} \quad \frac{9}{9} \quad \frac{3}{3}$$

$$-0.3 \quad -4.0 \quad -4.5 \quad -5.7$$

$$\frac{6}{6} \quad \frac{42}{42} \quad \frac{19}{19} \quad \frac{33}{33}$$

$$35.8$$

$$+5.4 \quad +2.5 \quad +0.6 \quad -0.8 \quad -0.7 \quad -0.1$$

$$\frac{33}{33} \quad \frac{23}{23} \quad \frac{18}{18} \quad \frac{15}{15} \quad \frac{11}{11} \quad \frac{5}{5}$$

$$-0.5 \quad -2.6 \quad -3.9 \quad -5.1 \quad -6.1$$

$$\frac{6}{6} \quad \frac{11}{11} \quad \frac{15}{15} \quad \frac{25}{25} \quad \frac{33}{33}$$

$$+8.8 \quad +4.8 \quad +3.5 \quad -0.1 \quad -0.1$$

$$\frac{33}{33} \quad \frac{17}{17} \quad \frac{14}{14} \quad \frac{11}{11} \quad \frac{6}{6}$$

$$-0.3 \quad -0.6 \quad -1.6 \quad -3.0 \quad -4.0 \quad -5.4$$

$$\frac{7}{7} \quad \frac{11}{11} \quad \frac{13}{13} \quad \frac{19}{19} \quad \frac{26}{26} \quad \frac{33}{33}$$

$$37.5$$

$$+10.8 \quad +8.0 \quad +5.3 \quad +1.3 \quad +0.1 \quad -0.1$$

$$\frac{33}{33} \quad \frac{20}{20} \quad \frac{14}{14} \quad \frac{11}{11} \quad \frac{8}{8} \quad \frac{4}{4}$$

$$+0.2 \quad -0.2 \quad -0.7 \quad +0.1 \quad -1.2 \quad -2.9$$

$$\frac{8}{8} \quad \frac{10}{10} \quad \frac{16}{16} \quad \frac{18}{18} \quad \frac{24}{24} \quad \frac{33}{33}$$

$$39.8$$

$$+11.3 \quad +7.5 \quad +2.3 \quad -0.2 \quad -0.4$$

$$\frac{33}{33} \quad \frac{18}{18} \quad \frac{14}{14} \quad \frac{10}{10} \quad \frac{5}{5}$$

$$+0.3 \quad -0.4 \quad -1.6 \quad +0.6 \quad -0.8 \quad -6.0$$

$$\frac{9}{9} \quad \frac{9}{9} \quad \frac{15}{15} \quad \frac{16}{16} \quad \frac{20}{20} \quad \frac{33}{33}$$

$$+2.5 \quad +6.0 \quad +5.2 \quad -0.5 \quad -0.5 \quad -0.6$$

$$\frac{33}{33} \quad \frac{22}{22} \quad \frac{21}{21} \quad \frac{14}{14} \quad \frac{11}{11} \quad \frac{7}{7}$$

$$+0.2 \quad -0.4 \quad -0.4 \quad -5.7 \quad -8.1$$

$$\frac{9}{9} \quad \frac{9}{9} \quad \frac{11}{11} \quad \frac{20}{20} \quad \frac{33}{33}$$

$$+4.7 \quad +1.6 \quad +0.8 \quad -0.1 \quad -0.1$$

$$\frac{33}{33} \quad \frac{21}{21} \quad \frac{17}{17} \quad \frac{11}{11} \quad \frac{6}{6}$$

$$-0.6 \quad -1.4 \quad -5.7 \quad -7.3 \quad -8.3$$

$$\frac{9}{9} \quad \frac{12}{12} \quad \frac{21}{21} \quad \frac{27}{27} \quad \frac{33}{33}$$

$$+3.4 \quad +0.5 \quad -0.2 \quad 0.0$$

$$\frac{33}{33} \quad \frac{19}{19} \quad \frac{12}{12} \quad \frac{8}{8}$$

$$-0.2 \quad -0.5 \quad -6.6 \quad -1.7$$

$$\frac{9}{9} \quad \frac{11}{11} \quad \frac{22}{22} \quad \frac{33}{33}$$

W.H.C.
C.E.J.
M.A.
T.F. } 2/27/24

Station

Elev.

117 4.4 932.6

v

116 6.0 932.9

+50 4.6 934.3

x

115 9.3 2.1

x

+80 8.8

114 4.9

+50 5.3

113 7.2

x

+50 4.5

112 5.1

+50 5.7

111 4.2

x

$$\frac{-4.0}{30} \quad \frac{-3.3}{28} \quad \frac{-2.7}{15} \quad \frac{-0.3}{11} \quad \frac{-0.3}{6}$$

$$\frac{-0.4}{5} \quad \frac{-1.1}{8} \quad \frac{-3.4}{13} \quad \frac{-4.1}{20} \quad \frac{-4.2}{33}$$

$$\frac{-3.9}{33} \quad \frac{2.2}{17} \quad \frac{-2.4}{11} \quad \frac{-0.5}{7}$$

$$\frac{-0.2}{10} \quad \frac{-0.8}{16} \quad \frac{-1.8}{20} \quad \frac{-4.9}{33}$$

$$\frac{4.0}{33} \quad \frac{-2.5}{15} \quad \frac{-2.3}{8} \quad \frac{-1.0}{6} \quad \frac{-0.6}{4}$$

$$\frac{+0.4}{9} \quad \frac{-0.2}{14} \quad \frac{-0.6}{16} \quad \frac{-2.4}{19} \quad \frac{-4.2}{28} \quad \frac{-4.9}{33}$$

$$\frac{-1.7}{33} \quad \frac{+0.8}{22} \quad \frac{+1.7}{20} \quad \frac{-0.9}{16} \quad \frac{-0.9}{13} \quad \frac{-0.2}{6}$$

$$\frac{-0.1}{6} \quad \frac{-0.3}{10} \quad \frac{+0.4}{18} \quad \frac{+0.9}{22} \quad \frac{-2.4}{27} \quad \frac{-4.4}{33}$$

$$\frac{+1.8}{33} \quad \frac{+3.8}{29} \quad \frac{+5.1}{21} \quad \frac{-0.2}{17} \quad \frac{-1.3}{14} \quad \frac{-0.2}{9} \quad \frac{0.0}{6}$$

$$\frac{0.0}{6} \quad \frac{-0.6}{19} \quad \frac{+1.1}{23} \quad \frac{-2.5}{27} \quad \frac{-4.6}{33}$$

$$\frac{+8.0}{33} \quad \frac{+1.0}{27} \quad \frac{+5.0}{22} \quad \frac{+0.3}{18} \quad \frac{-0.5}{11} \quad \frac{-0.5}{7}$$

$$\frac{-0.5}{6} \quad \frac{-0.4}{10} \quad \frac{+1.2}{12} \quad \frac{-5.9}{25} \quad \frac{-8.6}{33}$$

$$\frac{+6.6}{33} \quad \frac{+5.3}{23} \quad \frac{+4.2}{19} \quad \frac{+2.3}{17} \quad \frac{-0.4}{14} \quad \frac{0.0}{8}$$

$$\frac{-0.3}{6} \quad \frac{+0.3}{8} \quad \frac{0.0}{11} \quad \frac{-4.8}{20} \quad \frac{-6.5}{26} \quad \frac{-7.8}{33}$$

$$\frac{+4.8}{33} \quad \frac{+2.8}{20} \quad \frac{-0.2}{17} \quad \frac{-0.4}{14} \quad \frac{+0.2}{11} \quad \frac{+0.4}{8}$$

$$\frac{-0.1}{5} \quad \frac{+0.2}{8} \quad \frac{-2.2}{12} \quad \frac{-3.8}{17} \quad \frac{-6.3}{33}$$

$$\frac{+3.7}{33} \quad \frac{+1.5}{19} \quad \frac{-0.8}{15} \quad \frac{-0.1}{8} \quad \frac{-0.1}{5}$$

$$\frac{-0.5}{8} \quad \frac{-0.9}{11} \quad \frac{-2.5}{14} \quad \frac{-4.0}{19} \quad \frac{-5.1}{33} \quad \frac{-7.3}{33}$$

$$\frac{+5.1}{33} \quad \frac{+3.8}{26} \quad \frac{+1.9}{18} \quad \frac{0.0}{16} \quad \frac{-0.3}{11} \quad \frac{-0.3}{7}$$

$$\frac{-0.4}{7} \quad \frac{-1.0}{10} \quad \frac{-2.2}{12} \quad \frac{-3.7}{18} \quad \frac{-4.9}{25} \quad \frac{-6.1}{33}$$

$$\frac{+6.7}{33} \quad \frac{+4.0}{21} \quad \frac{+1.8}{13} \quad \frac{+0.1}{10} \quad \frac{+0.1}{7}$$

$$\frac{-0.2}{9} \quad \frac{-1.0}{13} \quad \frac{-2.3}{17} \quad \frac{-3.6}{22} \quad \frac{-5.2}{29} \quad \frac{6.8}{33}$$

$$\frac{+6.0}{33} \quad \frac{+3.1}{18} \quad \frac{+2.1}{13} \quad \frac{+0.6}{10} \quad \frac{-0.3}{7}$$

$$\frac{+0.2}{8} \quad \frac{-0.8}{14} \quad \frac{-1.7}{20} \quad \frac{-3.0}{25} \quad \frac{-6.0}{20} \quad \frac{-8.0}{33}$$

Station		Elev.
123+50	4.7	932.3
+35	4.6	932.4
	X	
123	5.0	932.0
+50	5.3	931.7
122	5.0	932.0
+50	5.0	932.0
+27	5.0	932.0
	X	
121	4.8	932.2
+50	5.1	931.9
120	5.0	932.0
+60	5.0	932.0
	X	
119	4.9	932.1
118	5.0	931.9

+1.5
50

L

Z

R

+1.5 +1.7 +1.5 +0.5 -0.6 -0.5 -0.2
33 29 26 21 14 11 8

0.0 -0.4 -2.3 -3.0 -3.9
4 7 17 20 33

+2.6 +0.2 +0.3 -0.5 -0.3
33 27 22 15 10

-0.1 -0.9 -2.4 -3.3 -3.8
5 8 13 19 33

+2.5 +0.7 +0.3 -0.5 -0.8 -0.4 -0.1
33 24 18 14 11 8 6

-0.5 -0.8 -2.1 -2.8 -3.7
6 8 12 19 33

+0.4 +0.5 -0.7 -0.5 -0.0
33 19 15 11 7

-0.3 -0.3 -1.3 -2.2 -3.4
5 9 12 17 33

-1.2 -0.7 -1.4 -0.7 -0.2
33 23 19 14 8

-0.4 -0.8 -2.2 -2.5 -3.4
5 9 13 18 33

+1.5 +1.3 +0.7 +0.2
33 29 16 11

-0.4 -0.4 -1.0 -3.0 -3.2 -4.3
5 8 12 16 20 33

+1.8 +1.5 +0.7
33 26 11

-0.3 -0.4 -2.4 -2.9 -3.2
5 10 14 19 33

+3.2 -1.1 -1.4 1.3 0.0 0.0
36 32 25 20 16 9

-0.6 -1.2 -2.8 -3.0 -3.2
6 10 14 19 33

+10.2 +8.3 +5.7 +4.5 -1.2 -1.4 -0.7 -0.2
32 33 28 27 21 16 13 8

-0.2 -0.2 -2.3 -2.9 -3.3
6 10 13 20 33

1.3 +1.7 +6.3 +4.0 -0.4 -1.4 -0.5 -0.3
34 33 25 22 19 13 9 7

-0.4 -0.6 -2.4 -2.9 -3.5
7 10 15 23 33

-0.3 -0.3 -1.0 -1.0 -0.3
33 16 16 11 8

-0.6 -0.7 -2.5 -3.1 -3.6
7 11 14 22 33

-1.7 2.2 2.1 -0.4
33 15 11 7

-0.4 -0.9 -1.5 -2.5 -3.2
8 11 16 22 33

-4.2 -3.1 -3.0 -0.2
33 16 11 5

+0.1 +0.1 -0.7 -2.0 -3.2 -3.7
3 9 11 14 21 33

4

Station		Elev.
129	4.6	937.6
+50	4.3	932.9
128	4.3	932.9
+50	4.5	932.5
127		932.0
+50	4.6	932.5
+30	4.3	932.8
	X	
126	5.0	932.1
	5	
+50	4.9	932.1
125	5.1	931.9
+40	4.8	932.3
124	4.4	932.7

$$\frac{+5.1}{33} \quad \frac{+4.5}{28} \quad \frac{+1.0}{10} \quad \frac{0.0}{8}$$

$$\frac{-0.6}{5} \quad \frac{-0.9}{10} \quad \frac{-2.2}{14} \quad \frac{-4.1}{33}$$

$$\frac{+2.8}{33} \quad \frac{+1.5}{18} \quad \frac{+0.2}{10}$$

$$\frac{-0.9}{6} \quad \frac{-1.1}{9} \quad \frac{-2.0}{11} \quad \frac{-4.2}{33}$$

$$\frac{+1.4}{33} \quad \frac{+1.2}{20} \quad \frac{-0.3}{12}$$

$$\frac{-0.5}{4} \quad \frac{-1.1}{10} \quad \frac{-2.1}{14} \quad \frac{-3.7}{33}$$

$$\frac{-0.7}{33} \quad \frac{+0.8}{24} \quad \frac{+1.2}{10} \quad \frac{-0.2}{7}$$

$$\frac{0.0}{2} \quad \frac{-0.5}{7} \quad \frac{-0.9}{10} \quad \frac{-1.9}{16} \quad \frac{-2.9}{3.1} \quad \frac{-3.6}{33}$$

$$\frac{+0.2}{33} \quad \frac{+1.0}{27} \quad \frac{+1.9}{21} \quad \frac{-1.0}{14} \quad \frac{-0.3}{7}$$

$$\frac{-0.1}{5} \quad \frac{-0.4}{11} \quad \frac{-1.7}{17} \quad \frac{-3.5}{21} \quad \frac{-3.7}{28} \quad \frac{+5}{28} \quad \frac{-2.5}{33}$$

$$\frac{-0.1}{33} \quad \frac{-0.1}{16}$$

$$\frac{-0.1}{8} \quad \frac{-1.8}{14} \quad \frac{-3.6}{33}$$

$$\frac{-2.5}{33} \quad \frac{-2.3}{13} \quad \frac{-0.6}{9}$$

$$\frac{-0.5}{7} \quad \frac{-0.8}{11} \quad \frac{-2.6}{13} \quad \frac{-3.5}{33}$$

$$\frac{-1.5}{33} \quad \frac{+1.1}{28} \quad \frac{+0.4}{26} \quad \frac{+0.5}{16} \quad \frac{-0.8}{13} \quad \frac{-1.2}{11} \quad \frac{0.0}{8}$$

$$\frac{-0.4}{8} \quad \frac{-0.9}{11} \quad \frac{-1.9}{14} \quad \frac{-3.1}{28} \quad \frac{-3.1}{33}$$

$$\frac{+3.4}{33} \quad \frac{+0.6}{19} \quad \frac{-1.1}{17} \quad \frac{-1.2}{14} \quad \frac{-0.8}{12} \quad \frac{-0.5}{8}$$

$$\frac{-0.5}{3} \quad \frac{-0.5}{6} \quad \frac{-1.1}{9} \quad \frac{-2.1}{13} \quad \frac{-2.6}{24} \quad \frac{-3.2}{33}$$

$$\frac{+1.1}{50} \quad \frac{+1.5}{43} \quad \frac{+6.7}{33} \quad \frac{+4.1}{29} \quad \frac{+1.1}{16} \quad \frac{-0.5}{15} \quad \frac{-0.9}{11} \quad \frac{-0.4}{8}$$

$$\frac{-0.5}{8} \quad \frac{-2.1}{12} \quad \frac{-2.8}{20} \quad \frac{-3.5}{33}$$

$$\frac{+1.6}{50} \quad \frac{+1.7}{46} \quad \frac{+8.0}{33} \quad \frac{+3.2}{23} \quad \frac{+1.1}{15} \quad \frac{-0.5}{14} \quad \frac{-0.9}{11} \quad \frac{-0.6}{8}$$

$$\frac{-0.3}{7} \quad \frac{-0.4}{9} \quad \frac{-1.9}{13} \quad \frac{-2.7}{19} \quad \frac{-3.7}{33}$$

$$\frac{+1.6}{50} \quad \frac{+8.0}{33} \quad \frac{+4.0}{28} \quad \frac{-0.3}{19} \quad \frac{-0.8}{13} \quad \frac{-0.4}{9}$$

$$\frac{-0.3}{5} \quad \frac{-0.5}{9} \quad \frac{-2.1}{12} \quad \frac{-2.8}{18} \quad \frac{-3.9}{33}$$

Station		Elev.
136	7.0	942.3
+50	10.1	939.2
	X	
135	4.9	937.1
+50 -	6.6	935.4
134	8.1	933.9
	X	
+60	7.9	933.1
	X	
133	4.5	932.6
132	5.4	931.7
+50	5.3	931.8
131	5.2	932.0
+65	4.5	932.7
130	5.3	931.8
129+50	5.3	931.8
	X	

$$\begin{array}{cccc} +3.6 & +3.7 & +0.5 & +0.7 \\ \hline 33 & 38 & 33 & 11 \end{array}$$

$$\begin{array}{cccc} 0.0 & -0.4 & -0.8 & -2.3 \\ \hline 5 & 15 & 23 & 33 \end{array}$$

$$\begin{array}{cccc} +4.6 & +2.9 & +2.0 & -0.5 \\ \hline 33 & 21 & 11 & 9 \end{array}$$

$$\begin{array}{ccc} -0.2 & -2.0 & -3.7 \\ \hline 11 & 20 & 33 \end{array}$$

$$\begin{array}{cccc} +3.4 & +1.9 & +0.2 & +0.1 \\ \hline 33 & 13 & 10 & 6 \end{array}$$

$$\begin{array}{cccc} 0.0 & -0.1 & -1.5 & -2.4 \\ \hline 7 & 13 & 24 & 33 \end{array}$$

$$\begin{array}{ccc} -0.1 & 0.0 & 0.0 \\ \hline 33 & 18 & 8 \end{array}$$

$$\begin{array}{cccc} -0.1 & -1.1 & -1.7 & -1.7 & -2.0 \\ \hline 7 & 12 & 21 & 20 & 33 \end{array}$$

$$\begin{array}{cccc} +5.8 & +3.4 & +0.6 & +0.1 \\ \hline 33 & 24 & 19 & 10 \end{array}$$

$$\begin{array}{ccc} -0.5 & -1.3 & -2.8 \\ \hline 8 & 12 & 33 \end{array}$$

$$\begin{array}{cccc} +4.7 & +3.1 & +0.7 & +0.1 \\ \hline 33 & 24 & 19 & 8 \end{array}$$

$$\begin{array}{ccc} -0.4 & -1.2 & -2.4 \\ \hline 11 & 17 & 33 \end{array}$$

$$\begin{array}{cccc} +4.8 & +2.3 & +2.3 & +0.5 & -0.1 \\ \hline 33 & 26 & 17 & 10 & 7 \end{array}$$

$$\begin{array}{cccc} -0.2 & -0.4 & -0.7 & -3.5 \\ \hline 3 & 9 & 12 & 33 \end{array}$$

$$\begin{array}{cccc} +5.3 & +4.9 & +4.8 & +2.5 & +0.5 & +0.4 & +0.3 \\ \hline 39 & 33 & 25 & 33 & 19 & 14 & 3 \end{array}$$

$$\begin{array}{cccc} -0.3 & -2.7 & -3.2 & -3.6 \\ \hline 5 & 10 & 28 & 33 \end{array}$$

$$\begin{array}{cccc} +10.0 & +10.3 & +5.3 & +1.5 & -0.1 & +0.3 \\ \hline 39 & 33 & 25 & 18 & 15 & 4 \end{array}$$

$$\begin{array}{ccc} -0.6 & 7 & \\ \hline 0.4 & 1.1 & -2.1 & -3.9 \\ \hline 9 & 9 & 13 & 33 \end{array}$$

$$\begin{array}{cccc} +13.0 & +12.9 & +12.6 & +6.3 & +3.0 & +0.1 \\ \hline 29 & 34 & 30 & 15 & 13 & 8 \end{array}$$

$$\begin{array}{cccc} 0.0 & -0.3 & -1.7 & -1.0 \\ \hline 5 & 8 & 12 & 33 \end{array}$$

$$\begin{array}{cccc} +13.5 & +13.9 & +13.0 & +9.3 & +5.0 & +1.1 & -0.2 \\ \hline 37 & 33 & 30 & 17 & 15 & 9 & 2 \end{array}$$

$$\begin{array}{cccc} -0.4 & -0.7 & -2.7 & -1.9 \\ \hline 6 & 10 & 14 & 33 \end{array}$$

$$\begin{array}{cccc} +20.0 & +20.5 & +14.7 & +9.0 & +3.6 & +0.5 & -0.1 \\ \hline 58 & 48 & 33 & 23 & 18 & 13 & 9 \end{array}$$

$$\begin{array}{cccc} -0.2 & -0.4 & -1.5 & -4.2 \\ \hline 5 & 8 & 12 & 33 \end{array}$$

$$\begin{array}{cccc} +9.7 & +7.7 & +2.9 & +2.1 & -0.4 \\ \hline 33 & 26 & 14 & 13 & 9 \end{array}$$

$$\begin{array}{cccc} -0.3 & -0.5 & -1.8 & -3.0 & -1.3 \\ \hline 5 & 9 & 14 & 25 & 33 \end{array}$$

station E/ev.

142 5.1 938.0

+50 1.4 938.7

141 3.5 939.4

+40 2.2 40.1

X

140 5.8 940.4

+60 5.4 940.9 ✓

139 4.5 941.9

+60 3.1 943.2

X

138 7.0 942.3

+70 8.1 950.3

+35 4.5 950.9

137 6.4 948.1

X

136+50 3.6 945.8

L E R

$$\begin{array}{cccc} +6.1 & +3.5 & +3.5 & -0.2 \\ \hline 33 & 19 & 12 & 9 \end{array}$$

$$\begin{array}{cccc} +0.2 & -0.2 & -1.7 & -1.9 \\ \hline 11 & 19 & 24 & 33 \end{array}$$

$$\begin{array}{cccc} +6.1 & +4.3 & -0.9 & -0.5 & -0.2 \\ \hline 33 & 19 & 14 & 12 & 8 \end{array}$$

$$\begin{array}{ccc} -0.7 & -6.6 & -7.9 \\ \hline 11 & 24 & 33 \end{array}$$

$$\begin{array}{cccc} +6.1 & +4.5 & -0.9 & -0.7 & -0.3 \\ \hline 33 & 18 & 13 & 11 & 9 \end{array}$$

$$\begin{array}{cccc} -0.3 & -0.8 & -7.2 & -9.2 \\ \hline 4 & 10 & 21 & 33 \end{array}$$

$$\begin{array}{cccc} +2.5 & +2.1 & -1.0 & -0.6 & -0.2 \\ \hline 33 & 16 & 13 & 11 & 7 \end{array}$$

$$\begin{array}{cccc} -0.4 & -0.8 & -1.3 & -7.8 \\ \hline 6 & 10 & 15 & 33 \end{array}$$

$$\begin{array}{cccc} +1.4 & +0.7 & -0.3 & -0.4 & 0.0 \\ \hline 33 & 15 & 12 & 11 & 8 \end{array}$$

$$\begin{array}{cccc} -0.3 & -0.2 & -1.0 & -7.8 \\ \hline 6 & 13 & 17 & 33 \end{array}$$

$$\begin{array}{cccc} +0.8 & +0.7 & -0.6 & -0.1 \\ \hline 33 & 14 & 12 & 8 \end{array}$$

$$\begin{array}{cccc} -0.3 & -0.4 & -1.2 & -7.8 \\ \hline 6 & 9 & 23 & 33 \end{array}$$

$$\begin{array}{cccc} +1.7 & +0.8 & -0.8 & -0.4 \\ \hline 33 & 16 & 12 & 9 \end{array}$$

$$\begin{array}{cccc} -0.3 & -0.3 & -0.9 & -6.2 \\ \hline 5 & 10 & 24 & 33 \end{array}$$

$$\begin{array}{cccc} +2.5 & +2.7 & -0.7 & -0.1 \\ \hline 33 & 19 & 13 & 9 \end{array}$$

$$\begin{array}{cccc} -0.5 & -0.7 & -1.7 & -8.6 \\ \hline 6 & 10 & 19 & 33 \end{array}$$

$$\begin{array}{cccc} +5.8 & +4.1 & -0.2 & 0.0 \\ \hline 33 & 20 & 12 & 6 \end{array}$$

$$\begin{array}{cccc} -0.4 & -0.9 & -1.1 & -2.0 \\ \hline 3 & 11 & 16 & 33 \end{array}$$

$$\begin{array}{cccc} +4.3 & +4.0 & -0.5 & -0.7 & -0.5 \\ \hline 33 & 21 & 14 & 9 & 6 \end{array}$$

$$\begin{array}{cccc} -0.3 & -0.9 & -1.0 & -9.1 \\ \hline 5 & 10 & 18 & 33 \end{array}$$

$$\begin{array}{cccc} +2.7 & +3.5 & -0.5 & -0.7 & -0.5 \\ \hline 33 & 20 & 13 & 7 & 11 \end{array}$$

$$\begin{array}{ccc} -0.4 & -1.5 & -2.2 \\ \hline 8 & 20 & 33 \end{array}$$

$$\begin{array}{cccc} +2.5 & +2.8 & -0.1 & -0.7 \\ \hline 33 & 17 & 13 & 9 \end{array}$$

$$\begin{array}{cccc} -0.9 & -1.1 & -8.4 & -5.6 \\ \hline 8 & 12 & 25 & 33 \end{array}$$

$$\begin{array}{cccc} +4.6 & +1.9 & +0.5 & 0.0 \\ \hline 33 & 17 & 12 & 4 \end{array}$$

$$\begin{array}{cccc} -0.4 & -0.8 & -2.1 & -3.0 \\ \hline 6 & 11 & 24 & 33 \end{array}$$

Station E/ev.

+50 7.6 943.5

x

147 2.0 941.4

+88 2.3 941.1

+67 2.6 940.8

+52 3.2 940.2

146 5.2 938.3

145 6.1 937.2

+50 6.4 937.0

144 6.0 937.5

X

+70 5.6 937.4

143 5.5 927.5

142+65 5.3 937.7

L, E R

$$\begin{array}{cccc} +0.2 & 0.0 & -0.5 & -0.6 \\ \hline 33 & 13 & 9 & 11 \end{array}$$

$$\begin{array}{cccc} 0.0 & -0.6 & -1.7 & -2.5 & -4.9 \\ \hline 6 & 11 & 15 & 21 & 33 \end{array}$$

$$\begin{array}{cccc} -4.9 & -3.5 & -2.5 & -0.3 \\ \hline 33 & 24 & 12 & 7 \end{array}$$

$$\begin{array}{ccc} -0.2 & -1.5 & -3.6 \\ \hline 8 & 16 & 33 \end{array}$$

$$\begin{array}{ccccc} -6.2 & -6.7 & -6.0 & -2.3 & -0.3 \\ \hline 33 & 22 & 16 & 14 & 10 \end{array}$$

$$\begin{array}{ccc} -0.2 & -2.9 & -4.8 \\ \hline 8 & 18 & 33 \end{array}$$

$$\begin{array}{cccc} -3.3 & -2.3 & -1.4 & -0.7 \\ \hline 33 & 19 & 15 & 9 \end{array}$$

$$\begin{array}{ccc} -0.4 & -1.4 & -8.0 & -7.9 \\ \hline 7 & 10 & 14 & 33 \end{array}$$

$$\begin{array}{ccccc} -1.5 & -1.0 & -0.4 & 0.0 & -0.2 & -0.4 \\ \hline 33 & 30 & 24 & 21 & 12 & 7 \end{array}$$

$$\begin{array}{ccc} -0.1 & -0.7 & -2.8 & -4.7 \\ \hline 6 & 13 & 18 & 33 \end{array}$$

$$\begin{array}{cccc} +4.1 & +2.1 & -0.4 & -0.1 \\ \hline 33 & 19 & 11 & 10 \end{array}$$

$$\begin{array}{ccc} -0.3 & -0.4 & -3.0 & -3.8 \\ \hline 7 & 10 & 16 & 33 \end{array}$$

$$\begin{array}{ccccc} +4.2 & +3.8 & +1.7 & -0.3 & +0.2 \\ \hline 33 & 25 & 19 & 12 & 8 \end{array}$$

$$\begin{array}{ccc} -0.6 & -1.0 & -3.0 & -5.3 \\ \hline 6 & 10 & 15 & 33 \end{array}$$

$$\begin{array}{ccccc} +5.1 & +5.1 & +1.1 & -0.4 & +0.3 \\ \hline 33 & 23 & 17 & 11 & 7 \end{array}$$

$$\begin{array}{ccc} -0.6 & -1.0 & -3.7 & -5.0 \\ \hline 6 & 11 & 20 & 33 \end{array}$$

$$\begin{array}{cccc} +5.1 & +4.0 & +0.3 & 0.0 \\ \hline 33 & 21 & 13 & 9 \end{array}$$

$$\begin{array}{ccc} -0.7 & -1.4 & -4.1 & -6.0 \\ \hline 7 & 11 & 20 & 33 \end{array}$$

$$\begin{array}{ccccc} +5.4 & +3.8 & +1.3 & 0.0 & -0.2 & 0.0 \\ \hline 33 & 21 & 17 & 12 & 10 & 8 \end{array}$$

$$\begin{array}{ccc} -0.9 & -1.2 & -3.3 & -7.0 \\ \hline 8 & 10 & 16 & 33 \end{array}$$

$$\begin{array}{ccccc} +6.0 & +2.5 & +1.2 & -0.4 & -0.1 \\ \hline 33 & 18 & 14 & 10 & 6 \end{array}$$

$$\begin{array}{ccc} -0.8 & -4.1 & -6.4 \\ \hline 10 & 18 & 33 \end{array}$$

$$\begin{array}{ccccc} +6.2 & +4.2 & +3.0 & -0.1 & -0.4 \\ \hline 33 & 18 & 15 & 12 & 9 \end{array}$$

$$\begin{array}{ccc} -0.2 & -0.2 & -4.7 & -5.9 \\ \hline 6 & 11 & 25 & 33 \end{array}$$

Station.

Elev.

153 4.6 971.3

+62 5.3 970.6

152 6.1 969.7

v

151 2.9 968.4

+50 4.3 967.1

150 6.5 964.9

-

+50 9.2 962.0

x

149 2.9 959.0

/

+65 7.8 962.9- 52.2

x

148 2.4 947.8

L. E. R

Totale 2/29/24

$$\frac{+0.7}{33} \quad \frac{+0.5}{21} \quad \frac{+0.2}{15} \quad \frac{+0.4}{9}$$

$$\frac{-0.2}{5} \quad \frac{-0.6}{10} \quad \frac{-1.2}{21} \quad \frac{-1.4}{33}$$

$$\frac{+1.0}{33} \quad \frac{0.0}{21} \quad \frac{-0.4}{16} \quad \frac{+0.2}{10}$$

$$\frac{0.0}{12} \quad \frac{-0.8}{40}$$

$$\frac{+2.5}{33} \quad \frac{+1.1}{22} \quad \frac{0.0}{18} \quad \frac{-0.4}{15} \quad \frac{+0.1}{11}$$

$$\frac{-0.4}{8} \quad \frac{-1.2}{12} \quad \frac{-1.6}{33}$$

$$\frac{+3.0}{33} \quad \frac{+2.3}{24} \quad \frac{-0.5}{20} \quad \frac{-0.2}{15} \quad \frac{+0.2}{8}$$

$$\frac{-0.2}{4} \quad \frac{-0.8}{11} \quad \frac{-1.3}{23} \quad \frac{-1.5}{33}$$

$$\frac{+2.5}{33} \quad \frac{+2.2}{23} \quad \frac{-0.2}{19} \quad \frac{0.0}{11} \quad \frac{+0.4}{5}$$

$$\frac{-0.2}{8} \quad \frac{-0.2}{14} \quad \frac{+1.2}{24} \quad \frac{+1.2}{28} \quad \frac{+0.8}{33}$$

$$\frac{+0.7}{33} \quad \frac{+1.2}{22} \quad \frac{-0.8}{18} \quad \frac{-0.5}{12} \quad \frac{+0.2}{5}$$

$$\frac{-0.5}{7} \quad \frac{-0.4}{13} \quad \frac{+0.5}{16} \quad \frac{+2.2}{23} \quad \frac{+2.2}{33}$$

$$\frac{-1.6}{33} \quad \frac{-1.0}{27} \quad \frac{-0.3}{21} \quad \frac{-1.2}{19} \quad \frac{-0.9}{13} \quad \frac{+0.2}{9}$$

$$\frac{-0.4}{5} \quad \frac{-0.8}{12} \quad \frac{-0.4}{16} \quad \frac{+1.0}{26} \quad \frac{+0.9}{33}$$

$$\frac{-0.2}{33} \quad \frac{-0.7}{21} \quad \frac{-0.9}{16} \quad \frac{0.0}{8}$$

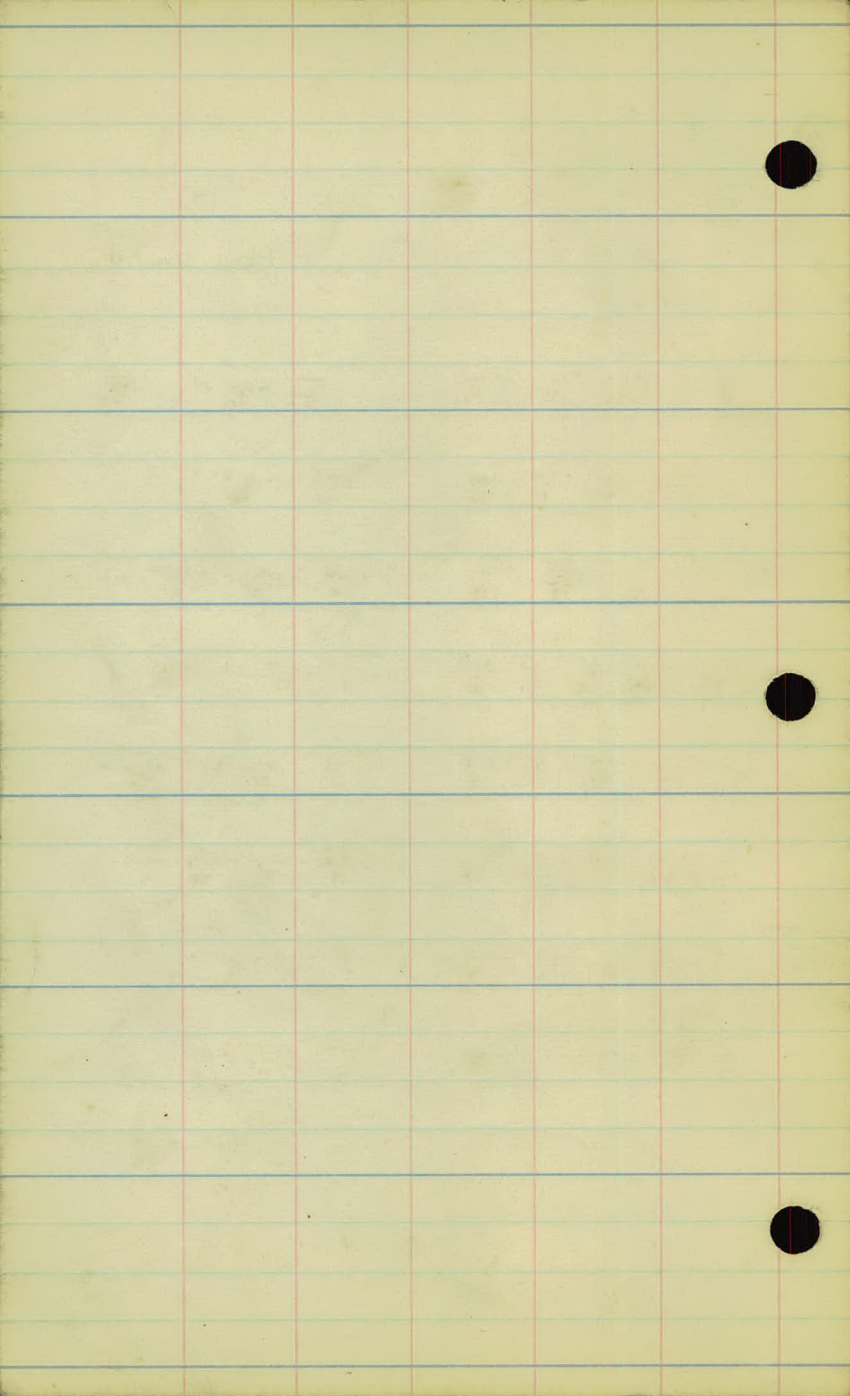
$$\frac{-0.9}{10} \quad \frac{-1.0}{14} \quad \frac{+0.9}{18} \quad \frac{-0.7}{33}$$

$$\frac{+0.8}{33} \quad \frac{+1.5}{30} \quad \frac{-0.7}{16} \quad \frac{-0.6}{9}$$

$$\frac{-0.2}{7} \quad \frac{-0.6}{13} \quad \frac{+2.2}{16} \quad \frac{+0.8}{33}$$

$$\frac{-0.3}{33} \quad \frac{+0.4}{30} \quad \frac{+1.6}{18} \quad \frac{-0.1}{15} \quad \frac{-1.3}{11} \quad \frac{-0.7}{8}$$

$$\frac{-0.4}{7} \quad \frac{-1.1}{10} \quad \frac{-1.6}{13} \quad \frac{-1.1}{15} \quad \frac{-0.2}{18} \quad \frac{-1.8}{31}$$



Drainage Notes

Project 24-52

Station Present Cully, Recommended Cully

146+76 24" X 31' Galv. Metal, 24" C.M.
Extends 15' R. & 16' L. (old very poor)

134+58 12" X 24' conc. Cully.
Extends 7' R. & 17' L. (O.K.)

126+36 18" X 24' C.M. (Half full of dirt.)
Extends 13' R. & 11' L.

121+98 8" X 23' Vitrified
Extends 11' R. & 12' L.

117+? cannot locate account ice
removed, Farmer claims 10" pipe C.M.
is in at this location.

108 10" C.M.
To Drain cuts N.Y.S.

103+90 15" X 28' Vitrified
Extends 12' R. & 14' L.

100+12 18" X 22' Vitrified
Extends 10' R. & 12' L.

83+20 10" X
To Drain Pot hole &
Small area on Rt.

W.H.C. }
 G.E.J. } 34-24
 M.S.A. }
 T.F. }

Inv. Elev. $\frac{932.7}{18}$ $\frac{32.7}{35}$ $\frac{32.6}{40}$
 Drains R.

Inv. Elev. $\frac{932.8}{7}$ $\frac{32.7}{20}$ $\frac{32.1}{40}$
 Drains R.

Inv. Elev. $\frac{929.4}{13}$ $\frac{29.3}{30}$
 Drains R.

Inv. Elev. $\frac{929.2}{11}$ $\frac{29.2}{20}$ $\frac{28.4}{40}$

Inv. Elev.
 Drains R.

117 = 932.6
 118 = 931.8

Drains R.

Inv. Elev. $\frac{933.6}{12}$ $\frac{32.4}{20}$ $\frac{31.3}{45}$
 Drains R.

Inv. Elev. $\frac{937.7}{10}$ $\frac{37.4}{20}$ $\frac{37.3}{30}$
 Drains R.

station Present Culv. Recommended culv.

77+50

12" C.M.

55+02

12" x 22' C.M.

Extends 5' R. & 17' L.

30+09

4' x 5' x 23' lg. stone walls, wood deck
(see detail)

Extends 14' R. & 9' L.

" " " "

22+93

18" x 24.5' C.M.

Extends 10' L. & 14.5' R.

7+06

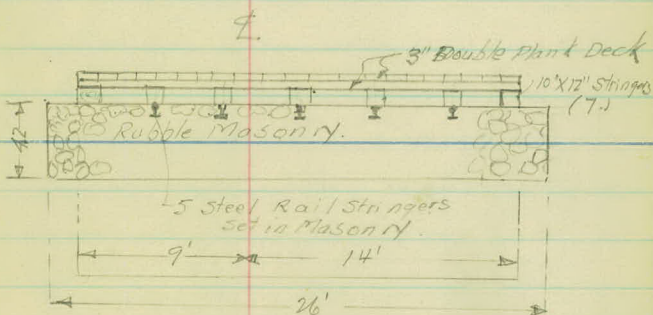
12" x 24' C.M.

Extends 16' L. & 8' R.

Inv. Elev.	977.7	77.6	77.1
Drains R.	$\frac{5}{5}$	$\frac{15}{15}$	$\frac{30}{30}$



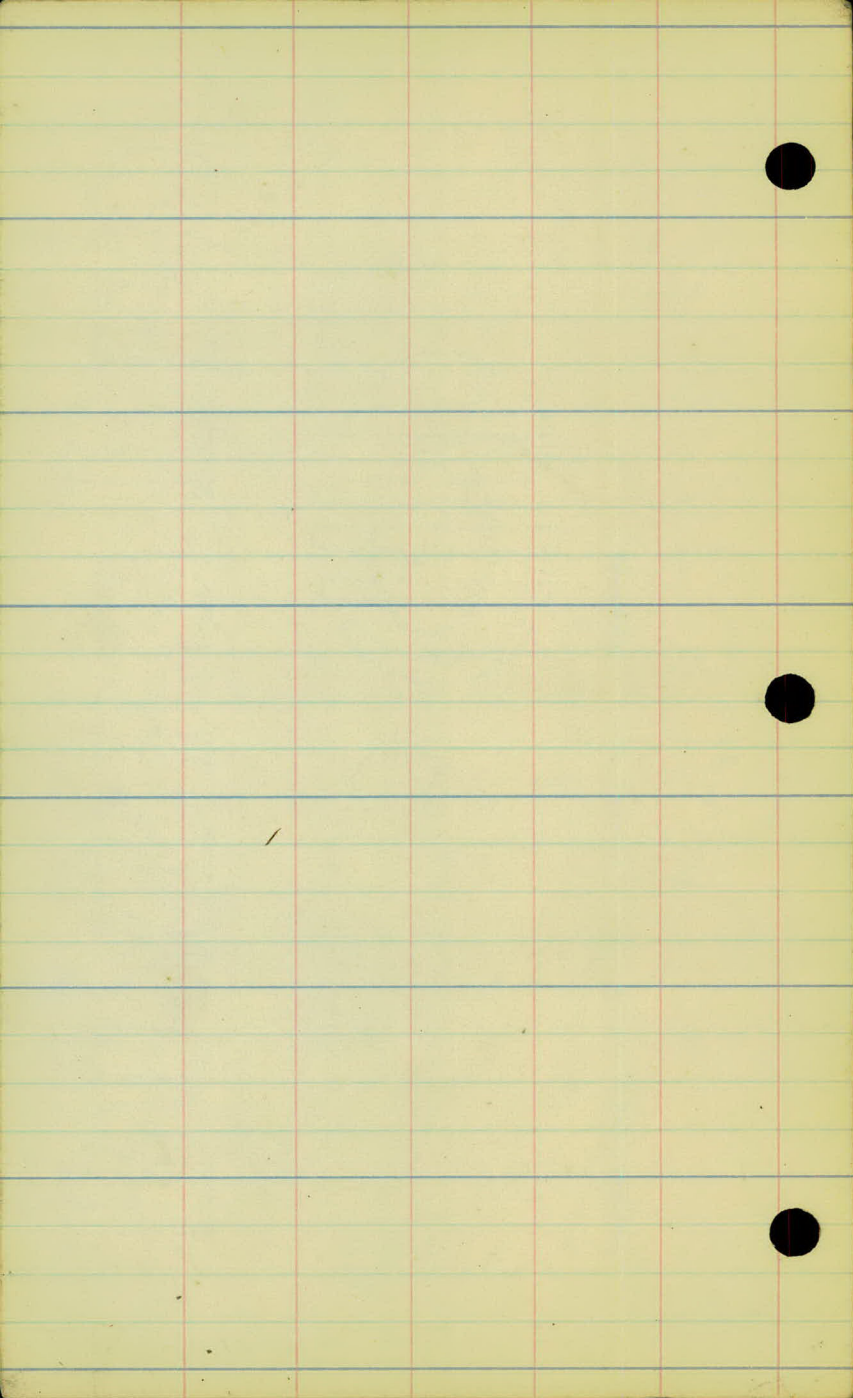
End Section.



Inv. Elev.	994.4	993.5
Drains L.	$\frac{9}{9}$	$\frac{32}{32}$

Inv. Elev.	980.4	10.0	79.9
Drains Lt.	$\frac{10}{10}$	$\frac{25}{25}$	$\frac{35}{35}$

Inv. Elev.	987.8	87.2	84.7
	$\frac{16}{16}$	$\frac{78}{78}$	$\frac{31}{31}$



Ties to Lake Shore

Project 24-52

Station

 W.H.C.
 C.F.J.
 M.S.A.
 T.F.

March 4, 1924

141+00 Lake shore 147' Right

137+55 " " 175' "

134+00 " " 190' "

130+00 " " 148' "

127+00 " " 150' "

125+30 " " 280' "

119+60 " " 335' "

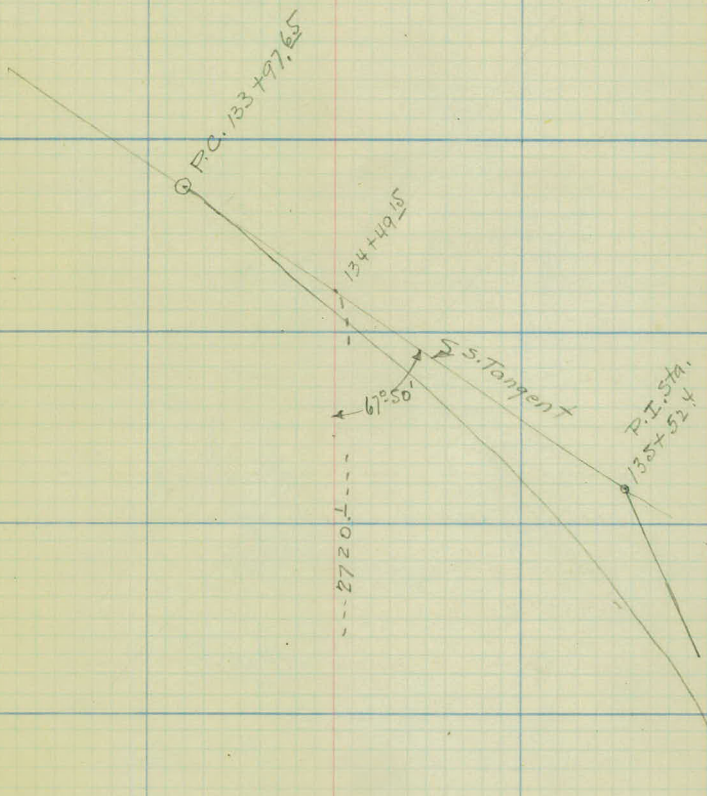
112+00 " " 195' "

107+25 " " 230' "

103+00 " " 345' "

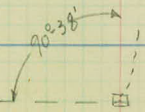
T. 29 N. R. 21. W. 1.
 Sec. 5 N Sec. 4

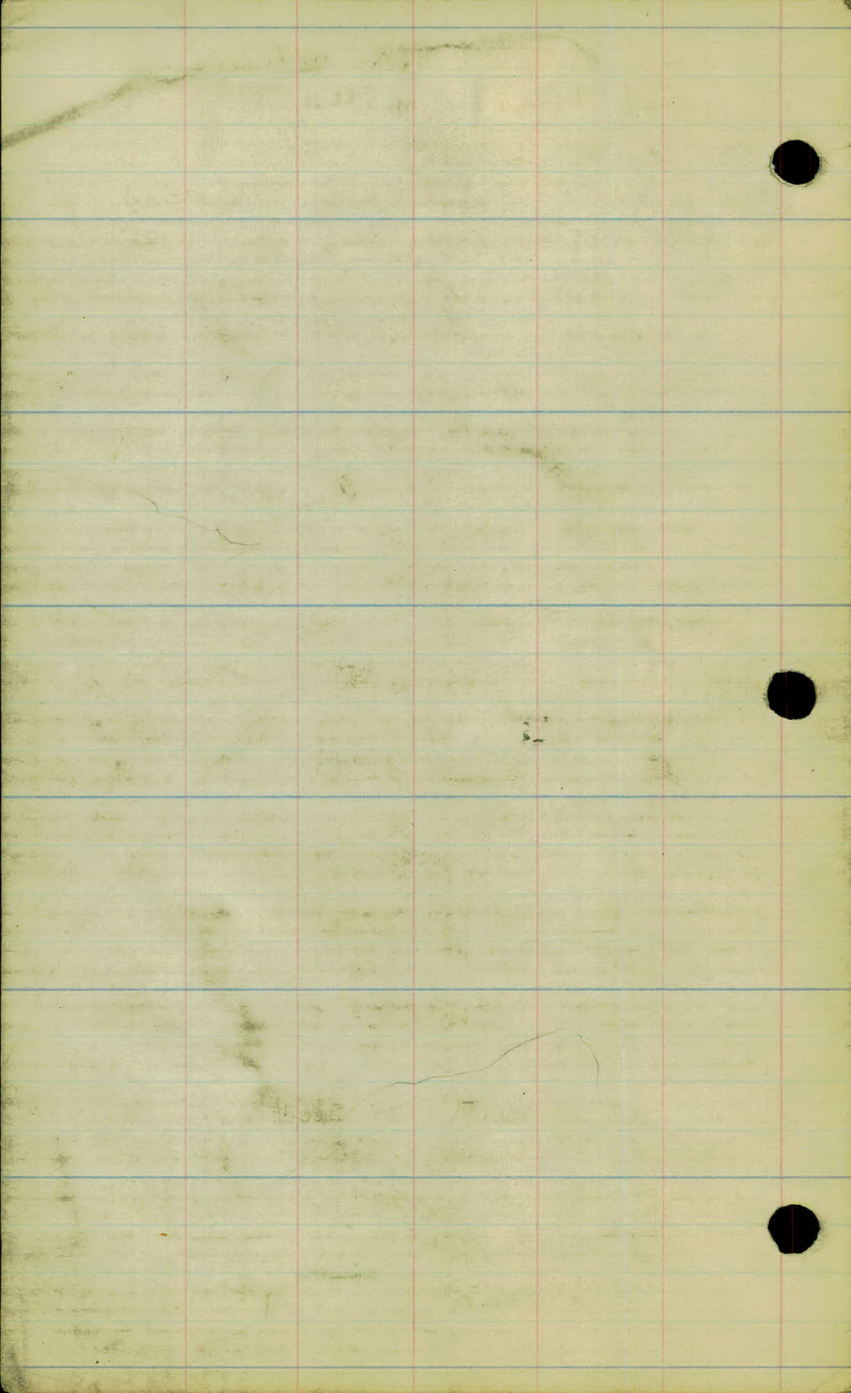
W.H.C.
 C.E.J.
 M.S.A. } 3/6/24
 T.F.



Sec. 5 Sec. 4

Sec. 8 Sec. 9





24-52

Change of grade - raise

0+00 L 1+50

No cult. reqd. at beginning

1+50 F.E.R. No cult. reqd

7+06

Remove 10" x 22' C.M.
P. 18" C.M.

Put in S.R. stem

12" x 22' C.M. imp. remove

P. 15+00

18" C.M. Culv

20+00

12" x 24' C.M. imp. remain

P. 18" x C.M.

21+20 Build Ents. to School Prop.

21+80 12" C.M. Culv

22+93 Remove old culv

P. 24" C.M.

25+30 Ent. to House L.

P. 12" x 12' C.M.

Use old Culv

26+00 F.E.R. ✓
P. 12" x 24' C.M.

26+00 F.E.L. ✓
No Culv. reqd ✓

26+50 No X drainage
required ✓

26+60 Ent. R. to House ✓
P. 12" x 12' C.M. ✓
Place old pipe

30+10 Remove
Plank Floor ✓
P. 24" C.M. Culv

32+40 F.E.R. ✓
P. 12" x C.M.

39+40 Build F.E.R. ✓
P. 12" x 24' C.M.

41+75
18" x 20' C.M. inp. extend ✓
with same

44+15 Build F.E.R. ✓
P. 12" x 24' C.M.

50+20 F.E.R.

P. 12" x 24"

✓

53+50

P. 18" C.M. equalizer

✓

55+0

remove slat beds

P. 18" C.M.

✓

61+70

F.E.L.

12" x 24" C.M. imp.

✓

Rem. & Rep. Cond. O.K.

67+14

F.E.R.

12" x 20" C.M. imp. Cond. O.K.

Rem. & Rep.

67+00

Cut out culv. across
road

✓

68+50

P. 18" x C.M. equalizer

70+00

12" x 24" C.M. imp. Cond. O.K.
Rem. & Rep.

✓

77+22

12" x 22" C.M. imp. rem.

P. 18" C.M.

✓

78+63

F.E.L.

P. 12" x 24" C.M.

✓

95+00

P. 18" C.M. on Curve ✓

Drain to R

100+05

15" x 18" V.P. imp. rom ✓

P. 18" C.M.

108+00

P. 18" x C.M. ✓

Drains R

118+50

P. 24" C.M. equalizer ✓

122+25

10" x 24" V.P. imp. rom ✓

P. 18" C.M.

123+30

F.E.L. ✓

P. 12" x 24"

18" x 24" C.M.

126+36

P. 24" C.M. ✓

126+60

F.E.L.

P. 12" C.M. ✓

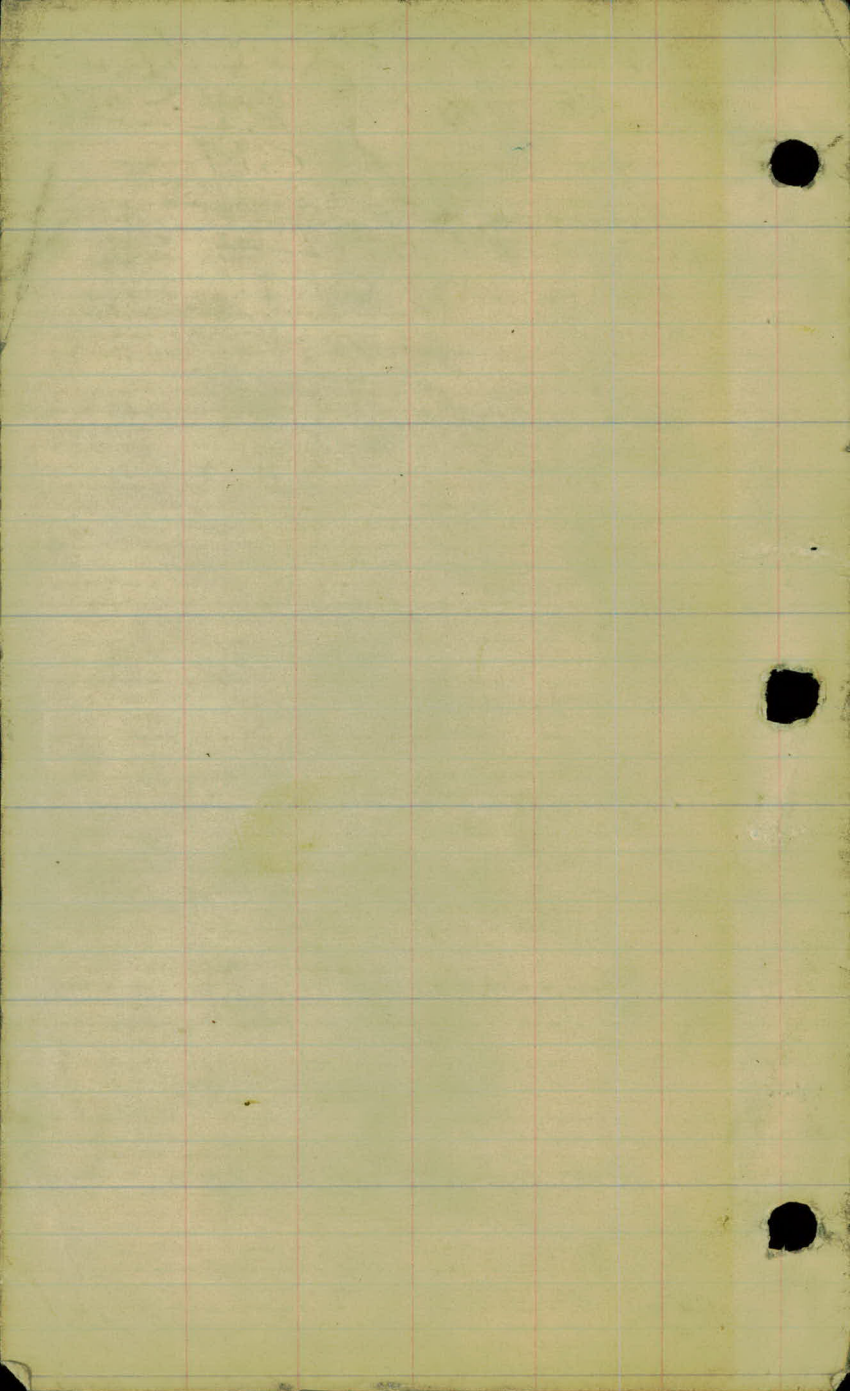
~~134+20~~

~~P. 18" C.M.~~

134 + 58 15" x 24" P.I. 11VP
Remove Cond. OK ✓

134 + 18 P, 18" C.M. ✓

136 + 12 ENTIL ✓
P, 12" x 36" C.M.



LEWIS W. CLARKE, COUNTY SURVEYOR
WASHINGTON COUNTY, MINNESOTA
204 NORTH THIRD STREET
STILLWATER, MINN.

January 31, 1924

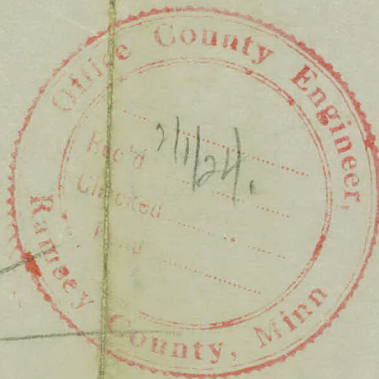
Mr. R. J. Wolfgangle
Designing Engineer
County Surveyors office, Ramsey County,

Dear Sir:

Yours of the 29th in re Sections 4 & 5, Oakdale, received. The sketch on the back of this letter shows all I can do for you. As to the widths of the road you mention, I know of no reason why they should not be made 66 feet. I usually do not try very hard to run out the lines as per original surveys. When I have tried it I generally come further away than if I had taken things as found. You might be able to find the road in question at the County Auditor's office, but I doubt it. It is a Town road and the Town Clerks are not usually very careful about saving such records.

Very truly yours

Lewis W. Clarke
County Surveyor.



Wolfgangle

2-1-24

U Z 466