PLANS SURVEY

LAKEVILLE ~ ROSEMOUNT

From Lakeville

To Dakota Co. S.R No. 1

CO. PROJ. 24-02

Proj. 24-02

Notes Used for plans -

Sta. 0 to 82+22.25 "L" Line

Sta. 82+13.9 to 141+05.5 "A" Line

Project 24-02

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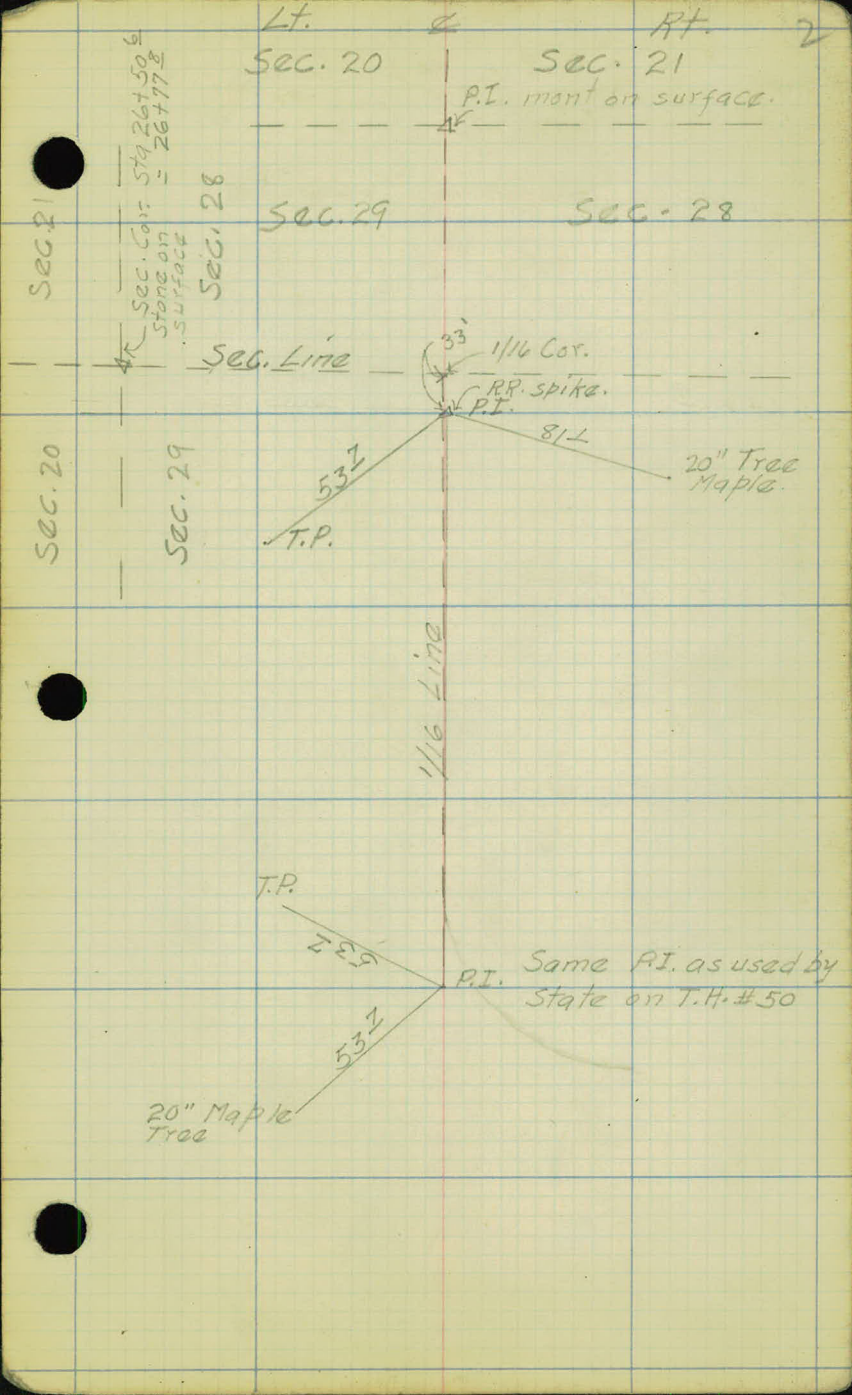
Proj 24-02

"A" Line

Station		∠ Lt.	∠ Rt.	Mag. Br.	
					N.0°15'W
$26+50^{6}$ = $26+77^{8}$ P.I.		2°27'			
				N.9°30'W	N.2°12'E
$16+03^{5}$ ✓	P.T.				
					Δ 86° 55' C. 20° Lt. T. 272^{9} ✓ L. 434^{6} ✓
$14+41^{8}$	P.I.				
$11+68^{9}$ ✓	P.C.				
					N.89°07'E.
$4+45^{6}$ ✓	P.T.				
					Δ 89° 07' C. 20° Rt. T. 283^{6} ✓ L. 445^{6} ✓
$2+83^{6}$	P.I.				
					N.0°00
0+00 ✓	P.C.				

Jorgenson
Persons
Briggs
Eck


Lt.
℄
Rt.
Sec. 20
Sec. 21
P.I. mon't on surface.
Sec. Cor.: Sta 264+50.6
= 267+78
Stone on surface
Sec. 28
Sec. 29
Sec. 28
Sec. 21
Sec. Line
33'
1/16 Cor.
R.R. spike.
P.I.
81 L
20" Tree Maple.
53 1/2
T.P.
Sec. 20
Sec. 29
1/16 Line
T.P.
53 1/2
P.I.
Same P.I. as used by State on T.H. #50
53 1/2
20" Maple Tree

17" L.

∠ Lt. ∠ Rt. M99 Br.

76+17.63 P.O.T.

67+83.7 N. 0°-15' W.

58+06.1 P.O.T.

53+08.5 P.I. 0°03'

N 6° 50' W N. 0°-18' W.

49+14.6 P.O.T.

38+26.9 P.I. 0°03'

Jorgenson
Persons
Briggs
Eck.

N. 0°-15' W.

Lt. ℄ Rt. 3

on Fence line.

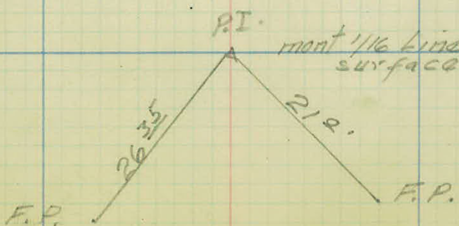
cement. block. on surface
1/16 line mont.

on Fence Line

Stone on surface 1/4 Cor.

on Fence Line.

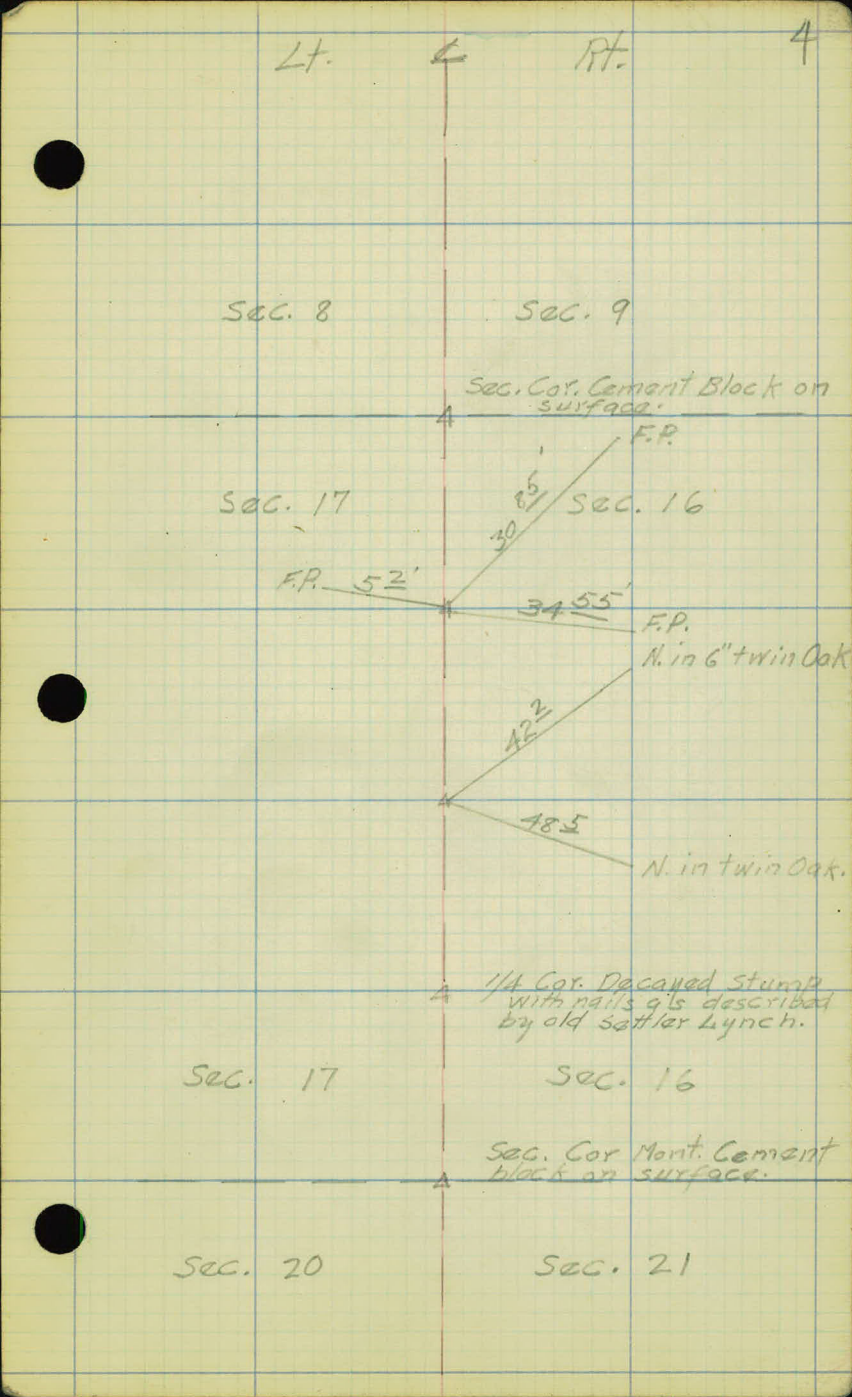
mont 1/16 Line Stone on
surface.



"A" Line

		∠ Lt.	∠ Rt.	
				M99 Br.
132+09.3	P.I.		0°11'	N 1° 12' W
117+85.9	P.O.T.			N 1° 23' W
105+80	P.I.	1°00'		
105+70				N. 0° 25' W.
79+39.8	P.I.	0°10'		
				N. 0° 15' W.

Jorgenson
Persons
Briggs
Eck


Lt.
℄
Rt.
Sec. 8
Sec. 9
Sec. Cor. Cement Block on surface.
F.P.
Sec. 17
Sec. 16
F.P.
F.P.
N. in 6" twin Oak
N. in twin Oak.
1/4 Cor. Decayed Stump with nails q's described by old Settler Lynch.
Sec. 17
Sec. 16
Sec. Cor Mont. Cement block on surface.
Sec. 20
Sec. 21

"A" L.

141+05.5 = 455+18.1 S.R. #I Dakota Co.

141+05.5 P.T. ✓

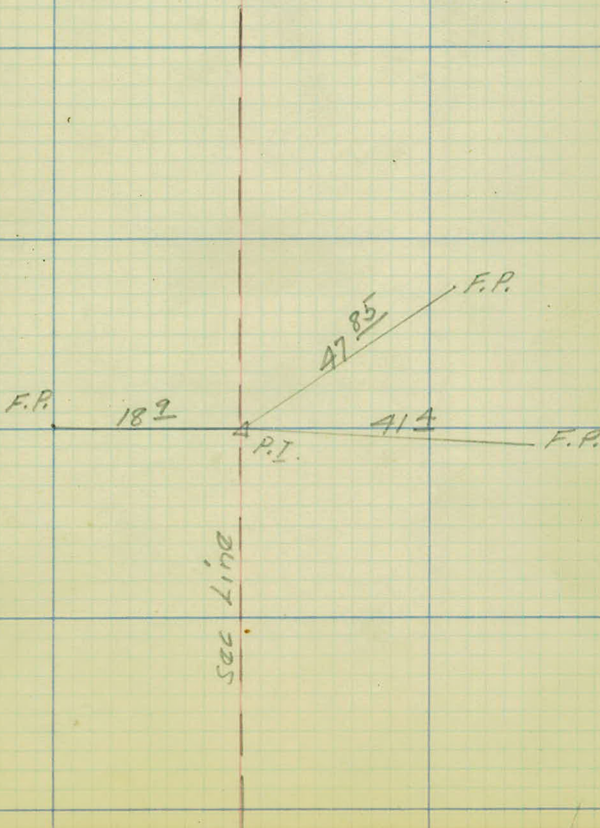
N 73° 02 E

Δ 74° 14'
20° C. Rt. ✓
T. 217.9 ✓
L. 371.1 ✓

139+52.3 P.I.

137+34.4 P.C. ✓

N 1° 12' W


F.P.
47 85
F.P.
18 9
P.I.
41 4
F.P.
Sec Line

12/29/23 Topog 4th Line
Cold & Cloudy. Jorgenson
Briggs
Eck.

24

22

20 & 24" Culv. Req.

18

16

14

12

10

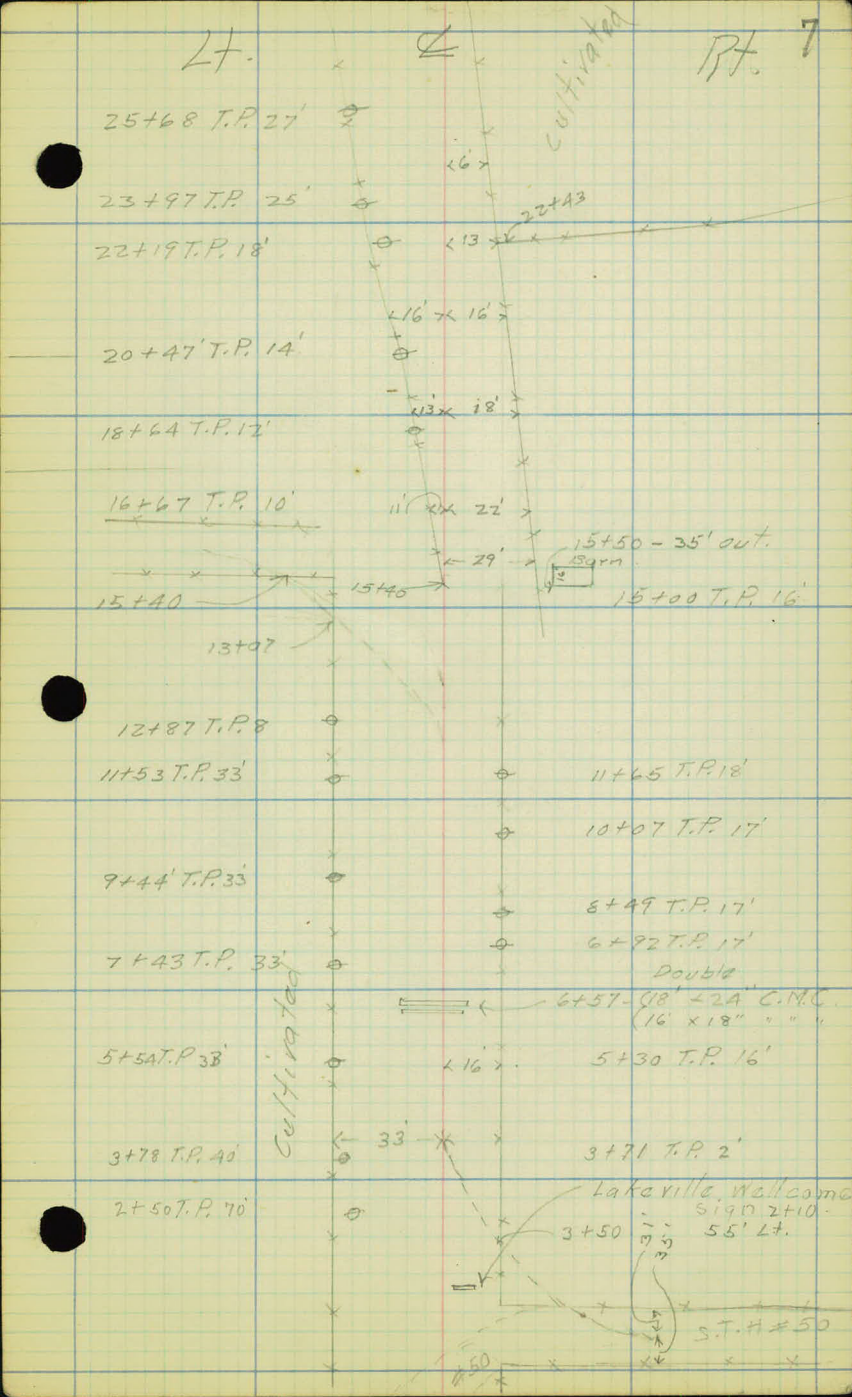
8

6

4

2

0+00 P.C.


Lt.
℄
Rt.
Cultivated
25+68 T.P. 27'
23+97 T.P. 25'
22+19 T.P. 18'
20+47 T.P. 14'
18+64 T.P. 12'
16+67 T.P. 10'
15+40
13+07
12+87 T.P. 8
11+53 T.P. 33'
9+44 T.P. 33'
7+43 T.P. 33'
5+54 T.P. 38'
3+78 T.P. 40'
2+50 T.P. 70'
16'
22+43
13
16' × 16'
13' × 18'
11' × 22'
29'
15+40
15+50 – 35' out.
15 barn
15+00 T.P. 16'
11+65 T.P. 18'
10+07 T.P. 17'
8+49 T.P. 17'
6+92 T.P. 17'
Double
6+57 - 18" ∠ 24" C.M.C.
(16' × 18" " " "
5+30 T.P. 16'
16'
33'
3+71 T.P. 2'
Cultivated
Lakeville, Wellcome
Sign 2+10 -
55' Lt.
3+50
S.T.H. #50
50'

50

48

46

44

42

40

38

36

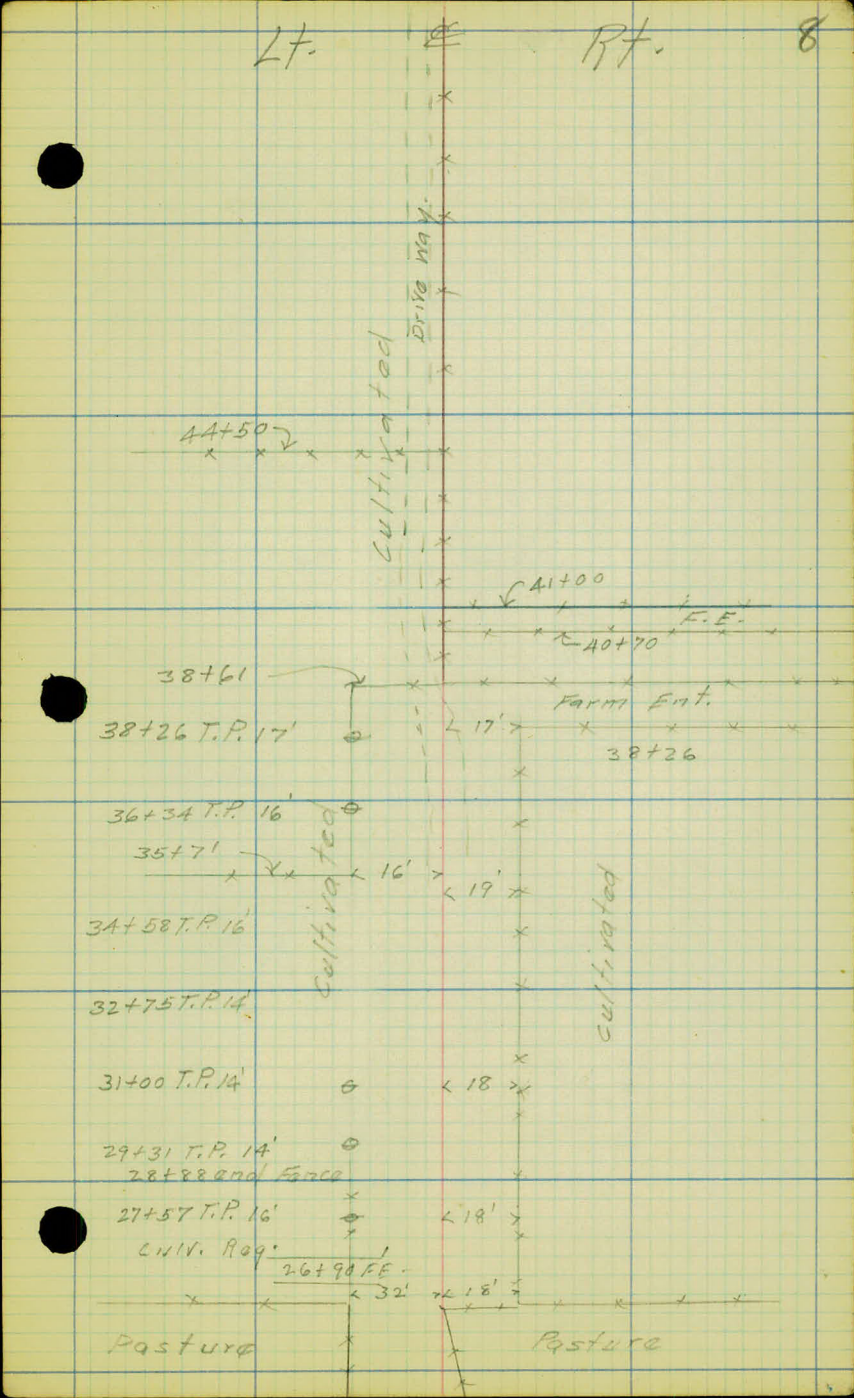
34

32 ℄ Culv. Req. 24"

30

28

26


Lt.
℄
Rt.
Drive Way
Cultivated
44+50
41+00
F.E.
40+70
38+61
Farm Ent.
38+26 T.P. 17'
17'
38+26
36+34 T.P. 16'
35+71
16'
19'
34+58 T.P. 16'
Cultivated
Cultivated
32+75 T.P. 14'
31+00 T.P. 14'
18'
29+31 T.P. 14'
28+88 End Fence
27+57 T.P. 16'
18'
Civ. Rod.
26+98 F.E.
32'
18'
Pasture
Pasture

Topog.

76

74

72

70

68

67+00 24" Culv. Sq. ℄

66

64

62

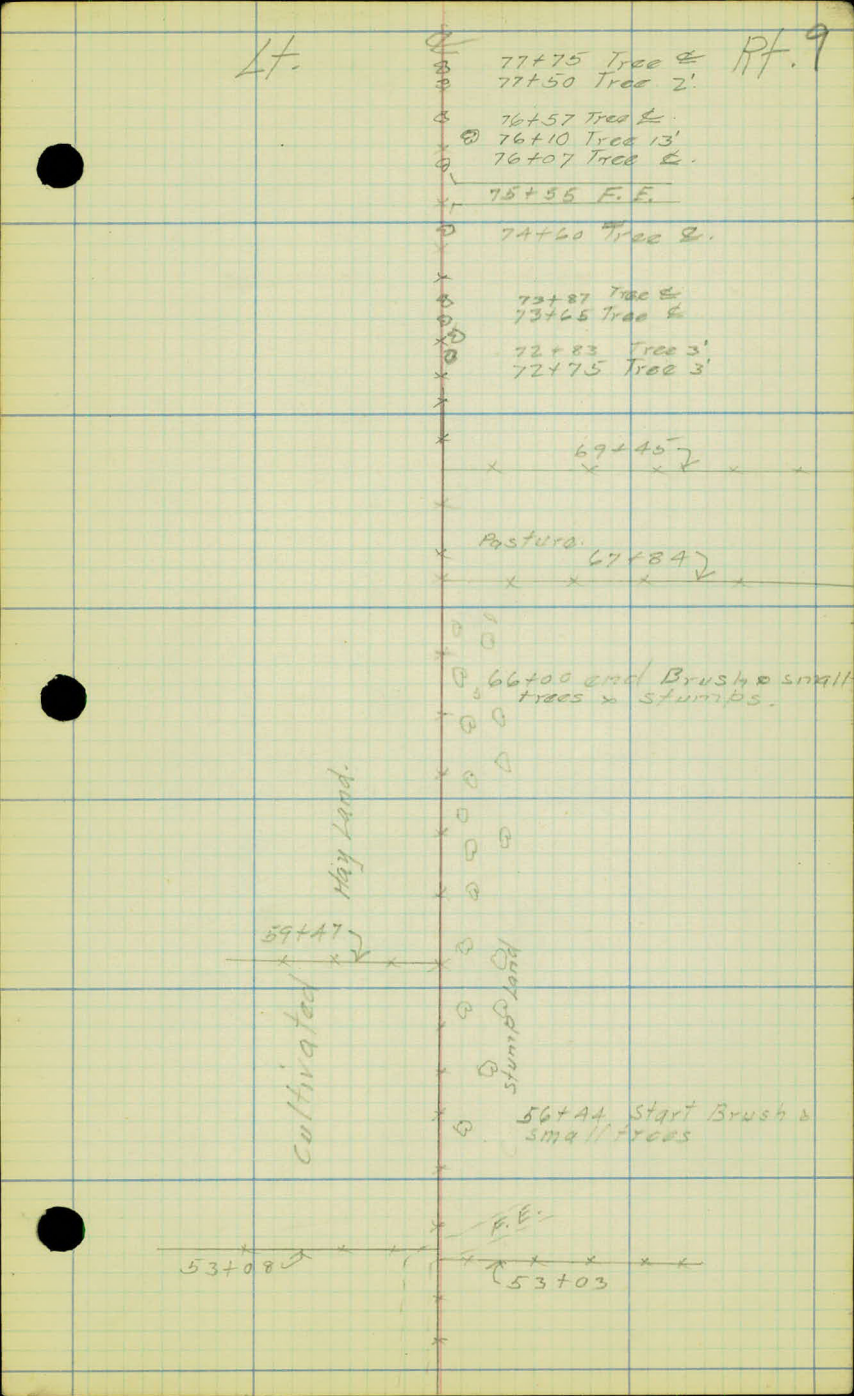
60

58

56

54

52


Lt.
Rt. 9
77+75 Tree &
77+50 Tree 2'
76+57 Tree &
76+10 Tree 13'
76+07 Tree &
75+55 E. E.
74+60 Tree &
73+87 Tree &
73+65 Tree &
72+83 Tree 3'
72+75 Tree 3'
69+45
Pasture.
67+84
66+00 end Brush & small trees & stumps.
High Land.
59+47
Cultivated
Stumps
56+44 Start Brush & small trees
E. E.
53+08
53+03

Topog -

100

8

6

4

2

90

8

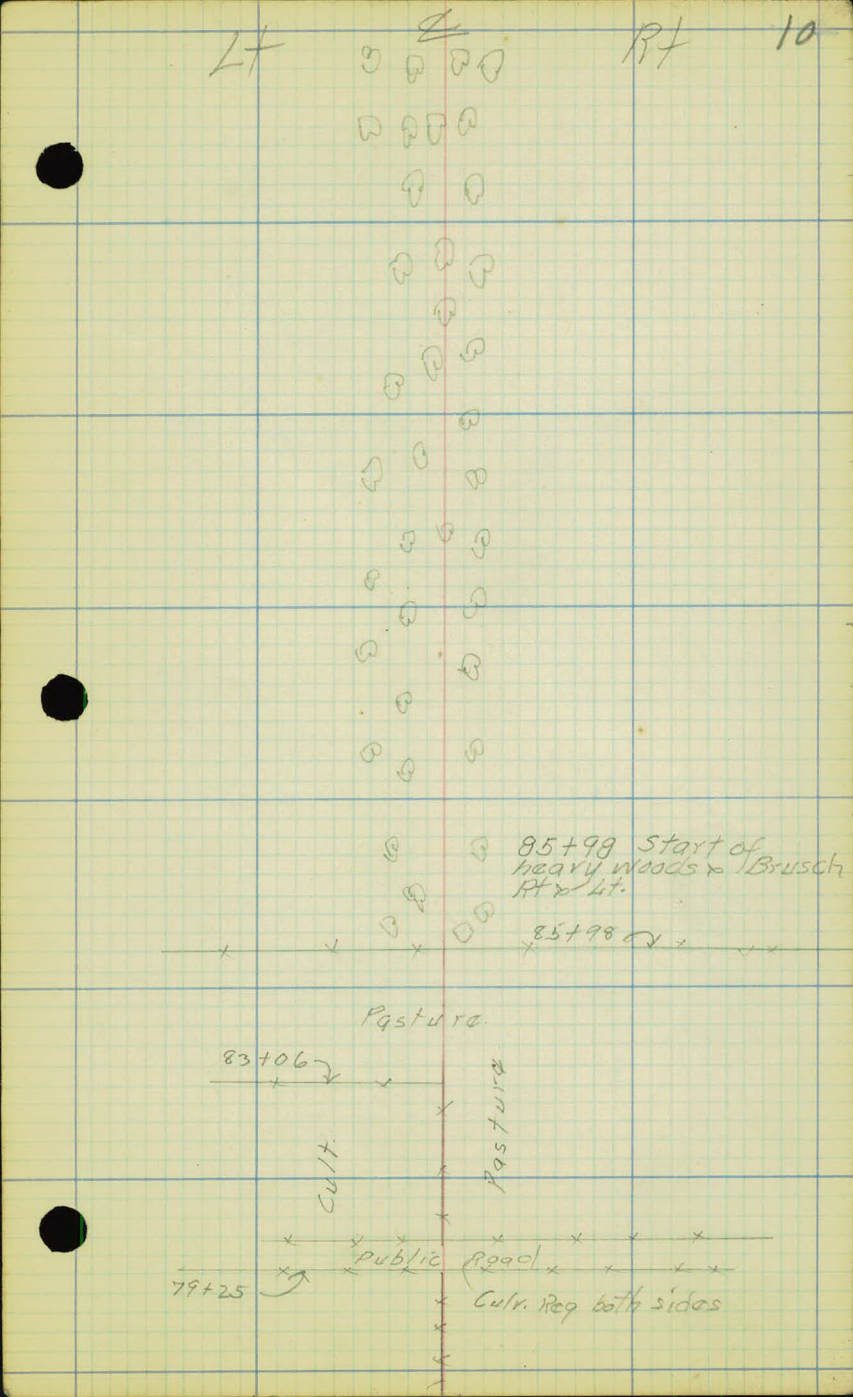
6

84 & Culv. Reg 24"

82

80

78


Lt
℄
Rt
85+99 Start of heavy woods & Brush Rt & Lt.
85+98
Pasture
83+06
Cult.
Pasture
Public Road
79+25
Culv. Req both sides

124

22

20

18

16

14

12

10

109+83 Combination Cattle pass & Culv. Req.

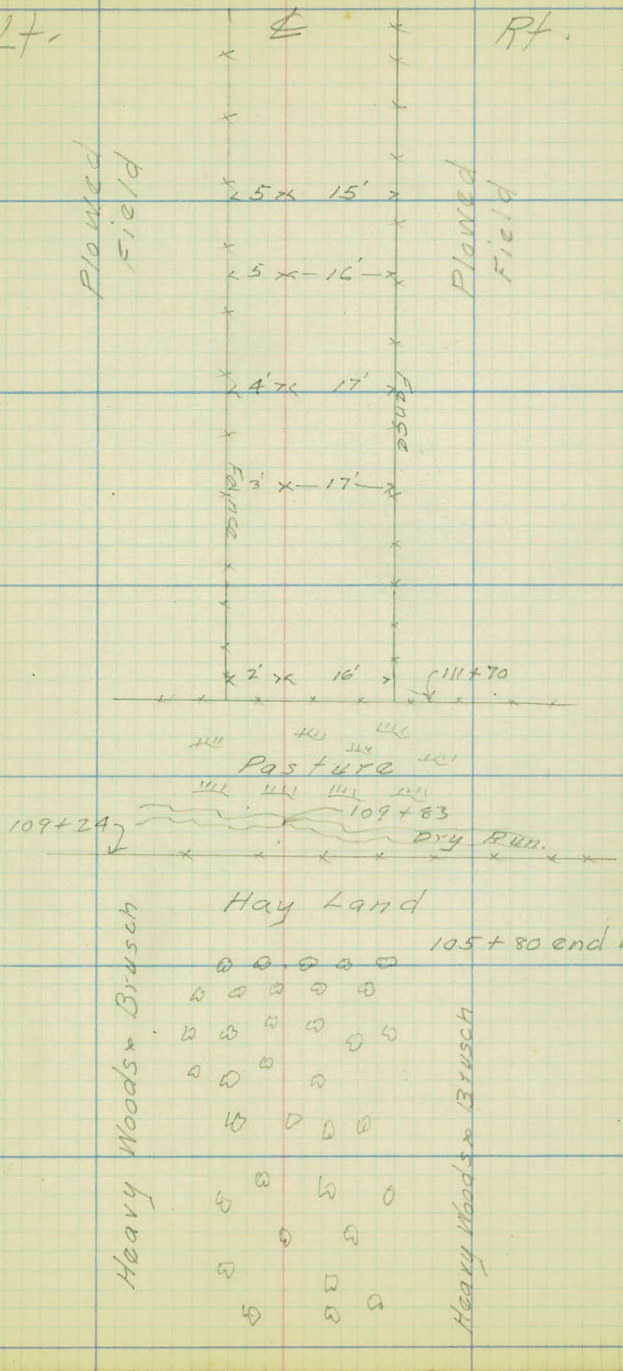
8

6

4

2

100


Lt.
℄
Rt.
Planted Field
Planted Field
5' x 15'
5' x 16'
4' x 17'
3' x 17'
2' x 16'
Fence
Fence
111+70
Pasture
109+24
109+83
Dry Run.
Hay Land
105+80 end Woods
Heavy Woods & Brush
Heavy Woods & Brush

Topog.

141+05.5 P.T.

137+34.4

135

133

132+10

130

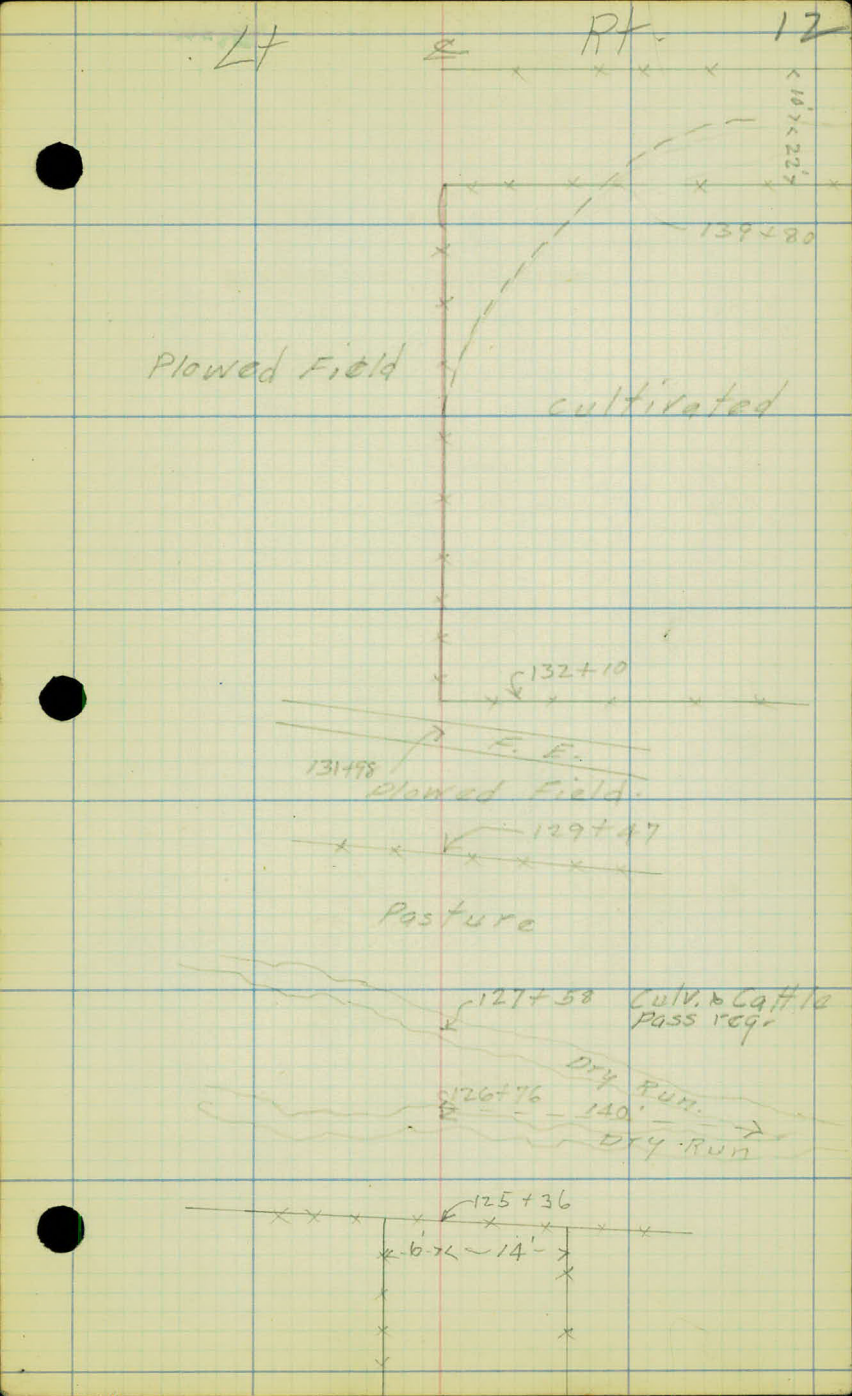
129

128

127

126

125


Lt
℄
Rt
16' x 22'
137+80
Plowed Field
Cultivated
132+10
P. E. E.
131+98
Plowed Field.
129+47
Pasture
127+58
Culv. & Cg. #10
Pass reg.
Dry Run.
126+76
140'
Dry Run
125+36
6' x 14'

"B." Line & Levels.

12			11.1	78.0 ✓
11			12.0	77.1 ✓
10			12.9	76.2 ✓
9			12.6	76.5 ✓
T.P.	11.44	89.10 ✓	2.35	77.66 ✓
8			3.4	76.6 ✓
7			3.1	76.9 ✓
+90			3.0	77.0 ✓
6			3.4	76.6 ✓
5			4.6	75.4 ✓
4			4.4	75.6 ✓
+15			4.1	75.9 ✓
3			4.9	75.1 ✓
+50			4.3	75.7 ✓
2			5.3	74.7 ✓
1			4.4	75.6 ✓
0				73.8 ✓
B. M.	3.11	980.01 ✓		976.90

12-26-23 Unsettled, Cold & Cloudy "A" Line

	+S	H.I	-S	Elv.
+ 55	Cu/v		5.2	74.4
6			5.5	74.1
5			5.2	74.4
+45 6	P.T.		4.6	75.0
4+00			4.6	75.0
+50			4.8	74.8
3+00			4.9	74.7
+50			5.3	74.3
2+00			4.6	75.0
+50			4.1	75.5
1+00			4.1	75.5
+50			4.8	74.81
0+00			5.8	73.8
B. M.	2.71	979.61 ✓		976.90 ✓

Jorgenson
Parsons
Briggs
Eck.

Lt.	℄	Rt.
7.4/33 7.3/15 7.6/inv.C. 5.3/8		5.5/6 8.0/inv.Culv. 8.4/18 8.4/23 8.4/38
5.2/34 5.6/28 6.5/19 5.4/9		5.7/6 6.7/12 6.9/20 7.0/37
5.1/33 5.6/24 5.4/13		5.2/5 6.0/12 5.3/15 5.4/20 5.3/36
4.7/34 5.2/22 4.6/12		5.1/12 4.7/19 4.8/37
4.7/39 5.3/31 4.9/22 4.4/8		5.1/9 4.8/17 4.5/39
4.8/36 4.7/24 5.1/7		4.6/24 4.5/41
5.0/38 5.1/20		5.0/26 5.1/43
4.9/40 5.2/22		5.4/22 5.6/39
4.8/40 4.7/20		5.1/21 5.1/40
4.5/41 4.2/23 4.1/17 3.4/11 3.6/3		3.7/21 3.9/33
4.1/34 3.9/15		3.7/2 3.7/6 4.0/10 3.2/17 3.2/21 3.6/32
4.3/37 4.8/24 5.3/23 4.9/17		4.9/14 4.8/18 5.5/24 3.8/29 4.0/33
6.1/35 5.9/30 6.1/20 6.6/18 6.0/13		5.9/17 5.7/18 6.3/28 4.9/32 4.8/35

Stg.	+S	H.I.	-S	Elv.
+50			6.0	89.8
14			5.6	90.2
+50			4.8	91.0
13			3.7	92.1
+50			4.1	91.7
12+00			4.5	91.3
+68 I	P.C.		5.6	90.2
11+00			8.5	87.3
T.P.	10.66	995.78	0.38	985.12
10			2.9	82.6
9			6.7	78.8
8			9.1	76.4
7+00			11.1	74.4
T.P.	11.50	985.50	5.61	974.00
		979.61		

6.4 6.2 38 21	5.7 6.2 18 35
5.5 5.5 37 22	6.0 6.4 20 34
4.7 4.7 40 20	5.1 5.8 19 37
4.0 3.8 37 21	4.1 5.4 5.6 11 23 40
4.3 3.8 4.2 36 21 15	3.3 3.5 4.2 3.7 6 25 32 40
5.0 4.7 5.3 4.7 33 23 20 6	5.3 4.6 4.7 14 21 36
5.9 5.8 6.7 6.0 32 25 22 8	6.4 5.0 5.6 12 19 35
8.6 8.4 9.3 8.6 34 26 23 9	9.0 8.0 7.9 10 22 37
2.2 2.4 3.3 3.0 34 28 24 10	3.1 1.9 1.6 1.1 12 17 22 35
6.8 6.6 7.2 7.1 6.5 34 28 26 12 9	7.0 5.8 5.8 5.8 12 17 22 36
9.7 9.8 9.6 9.0 33 21 11 8	9.7 9.6 9.1 9.2 7 13 21 35
12.5 123 11.0 33 16 9	11.0 12.5 12.5 11.9 12.0 5 11 15 18 33

	+S	H.I	-S	Elv.
24			9.4	84.9
T.P.	11.35	994.26 ✓	0.00	982.91 ✓
23			1.1	81.8
22			3.2	79.7
21			4.1	78.8
20			4.9	78.0
19			5.3	77.6
18			3.2	79.7
T.P.	1.22	982.91 ✓	11.63	981.69 ✓
17			10.4	82.9
16+00			6.7	86.6
B.M.	1.78	993.32 ✓	4.24	991.54 ✓
+50			6.9	88.9
15+00			6.3	89.5
		995.78 ✓		

Lt & Rt.

9.3/40 9.3/29 9.0/21 9.8/18 8.8/8 | 9.8/3 9.0/4 8.4/15 8.5/33

1.5/40 1.1/27 1.2/17 1.8/16 0.9/5 | 2.3/A 1.1/7 1.0/15 0.3/33

4.5/39 4.1/21 3.4/13 | 3.1/10 3.3/36

5.8/37 5.4/21 4.5/10 5.0/8 | 4.0/9 4.5/21 4.6/35

6.2/35 5.8/16 5.1/6 5.3/5 | 4.3/9 4.9/17 5.3/35

6.2/39 6.0/21 5.4/6 5.7/3 | 4.4/7 5.4/15 5.0/16 4.7/33

3.4/33 3.0/18 3.0/6 3.7/2 | 2.5/8 3.5/16 2.7/17 2.0/27 1.8/36

11.4/33 10.8/20 10.3/5 11.2/4 | 9.7/9 10.3/17 9.5/18 9.0/28 8.1/35

7.6/34 6.8/18 6.2/4 7.0/2 | 5.6/4 5.0/10 5.7/18 4.7/20 3.7/27 4.0/37

R.R. Spk. 20" Maple Rt. Sta. 15+00

8.7/37 7.8/19 | 6.9/4 7.5/6 6.6/11 6.1/30 5.2/33

7.4/33 6.7/15 | 5.7/15 5.5/25 5.9/27 5.1/39

T.P.	11.67	1016.92 ✓	7.48	1005.25 ✓
33			7.5	05.2
32			8.7	04.0
31			7.1	05.6
30			6.1	06.6
29			3.8	08.9
+77			4.3	08.4
T.P.	8.49	1012.73 ✓	0.18	1004.24 ✓
28			0.3	04.1
27			6.6	97.8
26+77 8 / 26+50 6 } short sta.			7.9	96.5
T.P.	10.77	1004.42 ✓	0.61	993.65 ✓
26			1.2	93.1
25			6.1	88.2

994.26 ✓

10.2/33 9.7/14 8.6/15 6.7/19 6.5/36

12.9/33 12.1/14 11.1/12 9.8/4 7.7/3 7.7/15 7.2/19 7.0/35

9.0/33 8.8/17 7.6/14 7.1/15 6.0/16 5.7/24 5.2/36

8.0/27 7.6/14 6.9/12 6.6/2 5.5/11 5.7/15 5.0/16 5.0/25 4.5/36

5.9/33 4.8/18 4.4/6 3.5/9 3.8/13 3.0/14 3.4/23 3.1/37

6.0/35 5.5/25 4.6/10 4.1/9 4.4/13 3.6/13 3.9/18 4.1/22 3.7/36

0.5/35 0.7/27 0.3/15 0.7/9 1.1/12 1.0/14 0.6/22 0.8/35

6.5/34 6.5/15 7.0/10 6.0/12 6.0/17 6.0/33

7.4/33 7.5/21 8.0/19 8.0/12 8.8/8 7.7/17 6.9/33

0.4/34 0.2/31 0.4/21 1.0/20 0.7/9 0.8/6 0.6/23 0.5/35

5.1/37 5.1/24 5.9/21 4.9/10 4.9/1 4.5/13 4.2/33

12/27/23 Cloudy + Fog, Cold. Snow.

	+S	H.I.	-S	Elv.
T.P.	11.43	46.37 ✓	0.78	34.94 ✓
43			4.6	31.1
42			6.2	29.5
41			6.7	29.0
40			4.5	31.2
39			2.5	33.2
+ 43			2.3	33.4
38			5.0	30.7
37			12.2	23.5
T.P.	11.83	35.72 ✓	0.67	23.89 ✓
B.M.	11.72	24.56 ✓	4.08	1012.84 ✓
36			2.2	14.7
35			7.5	09.4
34			10.1	06.8

1016.92 ✓

Jorgenson
Briggs
Eck

Lt & Rt. 18

				6.6 / 35	5.6 / 11	4.1 / 16	3.3 / 35		
8.9 / 38	8.0 / 21	7.2 / 3		5.9 / 16	5.5 / 35				
		10.2 / 42	7.9 / 11			5.6 / 17	4.0 / 38		
		8.6 / 38	6.1 / 14			3.0 / 19	1.6 / 39		
	6.7 / 39	5.4 / 26	4.3 / 13			1.4 / 19	0.6 / 38		
	7.3 / 40	4.2 / 16	3.7 / 7			1.2 / 16	0.3 / 34		
8.9 / 39	6.6 / 17	5.8 / 10		4.6 / 8	4.7 / 15	3.6 / 18	1.0 / 42		
	16.1 / 39	13.4 / 19	13.2 / 10			12.4 / 13	10.8 / 19	9.7 / 33	

R.R. spk. Cor. F.P. Lt. 35 + 75

			4.8 / 33	3.0 / 15	2.4 / A	2.4 / 9	3.1 / 13	1.3 / 18	0.8 / 24	0.0 / 36
		10.3 / 38	8.8 / 18	8.0 / A		7.7 / 13	7.0 / 19	6.3 / 34	
		13.3 / 33	12.0 / 17	10.9 / 2		10.0 / 12	10.2 / 15	9.6 / 19	9.3 / 37

	+S	H.I.	-S	E/V.
55			8.5	77.3
54			7.3	78.5
B.M.			5.30	1080.46 ✓
53			5.6	80.2
52			5.2	80.6
51			5.3	80.5
50			6.4	79.4
49			8.1	77.7
T.P.	8.34	85.76 ✓	2.17	77.42 ✓
+50			3.9	76.0
A8			7.3	72.6
T.P.	11.80	79.89 ✓	0.58	68.09 ✓
A7			4.9	63.8
T.P.	11.55	68.67 ✓	0.24	57.12 ✓
A6			3.8	53.6
T.P.	11.18	57.36 ✓	0.19	46.18 ✓
A5			1.8	44.6
A4			8.8	37.6

1046.37 ✓

Lt & Rt.

9.2 / 36	8.6 / 16	8.5 / 5	8.6 / 18	8.5 / 36
7.6 / 36	7.0 / 13	7.7 / 4	7.9 / 18	8.1 / 36

R.R.Spk Cor E.P. 53+05 ℄

4.8 / 36	6.0 / 8	6.5 / 15	6.8 / 34
5.0 / 36	4.6 / 13	6.3 / 20	6.6 / 36
5.3 / 35	5.4 / 13	6.4 / 17	6.9 / 37
7.0 / 36	6.5 / 13	6.9 / 16	7.4 / 36
9.8 / 37	8.8 / 14	8.3 / 16	8.7 / 36
6.6 / 37	1.9 / 10	3.8 / 18	3.5 / 37
9.8 / 35	8.2 / 7	6.6 / 17	5.8 / 37
7.0 / 35	5.7 / 7	4.1 / 19	3.0 / 37
3.6 / 37	4.5 / 10	3.4 / 20	2.3 / 37
3.9 / 35	2.5 / 7	0.6 / 22	+0.5 / 39
11.1 / 38	9.7 / 14	10.8 / 13	10.1 / 8	8.1 / 15	7.5 / 35

	+s	H.I.	-s	E/V.
67			11.0	47.3
66			7.7	50.6
65			5.0	53.3
64			3.6	54.7
T.P.	2.51	58.31	11.58	55.80
63			11.3	56.1
62			8.1	59.3
61			3.9	63.5
T.P.	1.31	67.38	11.49	66.07
60			8.6	69.0
59			2.2	75.4
T.P.	1.41	77.56	9.61	76.15
58			6.8	79.0
57			6.3	79.5
56			8.1	77.7
		85.76		

Lt. ℄ Rt.

10.9 / 36	10.9 / 18	11.0	11.3 / 16	11.6 / 34
7.7 / 37	7.9 / 18	7.7	8.0 / 15	8.6 / 34
4.5 / 33	5.2 / 10	5.0	5.1 / 15	5.0 / 34
3.2 / 35	3.6 / 16	3.6	3.3 / 14	4.2 / 36
11.7 / 35	11.6 / 17	11.3	11.3 / 9	11.5 / 36
8.5 / 37	8.5 / 20	8.1	8.6 / 12	9.0 / 37
4.2 / 37	3.6 / 15	3.9	4.5 / 21	4.4 / 37
8.5 / 37	7.9 / 16	8.6	8.7 / 12	8.7 / 36
2.4 / 37	2.1 / 17	2.2	2.3 / 21	2.4 / 36
8.0 / 37	7.2 / 19	6.8	7.0 / 16	7.0 / 36
7.9 / 37	7.0 / 17	6.3	6.3 / 16	5.8 / 36
9.2 / 37	8.7 / 16	8.1	8.3 / 11	7.7 / 36

	+S	H.I.	-S	E/V.	
+30			8.4	68.0	68.7
79			7.5	68.9	69.6
78			6.3	70.1	70.7
77			4.2	72.2	72.9
+63			3.5	72.9	73.6
76			4.6	71.8	72.5
75		77.06	8.8	67.6	68.3
T.P.	11.04	76.40	0.40	65.36	66.02
74			3.7	62.1	62.7
73		66.42	8.5	57.3	57.9
T.P.	11.31	65.76	3.86	54.45	
72			4.2	54.1	
71			7.0	51.3	
70			8.8	49.5	
69			9.8	48.5	
68			10.2	48.1	
		58.31			

Lt ≤ Rt.

7.2 / 37	8.0 / 20	8.4 9.0 / 11	10.6 / 34
7.0 / 37	7.5 / 18	7.5 8.3 / 15	8.9 / 35
5.3 / 37	6.0 / 24	6.3 7.5 / 19	8.0 / 34
3.0 / 37	3.7 / 13	4.7 4.7 / 17	5.5 / 34
2.7 / 27	3.1 / 20	3.5 4.2 / 19	4.8 / 36
3.8 / 37	4.3 / 18	4.6 5.0 / 17	5.5 / 36
8.0 / 36	8.9 / 20	8.8 8.8 / 16	9.2 / 33
3.6 / 36	3.9 / 17	3.7 4.0 / 18	3.9 / 34
8.6 / 34	8.5 / 14	8.5 8.5 / 15	8.7 / 34
4.2 / 36	4.5 / 18	4.2 4.7 / 15	5.0 / 35
6.1 / 37	6.7 / 17	7.0 7.4 / 15	7.6 / 35
8.3 / 36	8.4 / 18	8.8 8.9 / 17	8.6 / 35
9.6 / 35	9.6 / 16	9.8 10.1 / 21	9.9 / 36
10.6 / 36	10.4 / 20	10.7 10.6 / 15	10.7 / 35

	+S	H.I.	-S	Elv.	
89			9.0	78.9	79.6
B.M.	9.53	88.59 / 87.93	0.14	1078.40	1079.06
88			4.0	74.5	75.2
87			8.5	70.0	70.7
T.P.	11.23	1079.20 / ~~78.54~~	3.00	67.31	67.97
86			3.7	66.6	67.3
85			5.7	64.6	65.3
84			7.3	63.0	63.7
+34			7.2	63.1	63.8
83			5.6	64.7	65.4
T.P.	1.54	70.97 / 70.31	7.63	68.77	69.43
82			8.2	68.2	68.8
81			6.5	69.9	70.6
80			7.2	69.2	69.9
79+40			9.2	67.2	67.9

76.40

Lt ℄ Rt.

9.4 / 37 — 8.9 / 20 — 90 — 8.8 / 15 — 9.1 / 35

R.R. spk in 20" tree Rt. 88+30

4.4 / 34 — 4.4 / 19 — 4.0 — 3.8 / 17 — 3.7 / 35

8.3 / 35 — 8.5 / 18 — 8.5 — 8.5 / 19 — 8.7 / 37

3.5 / 35 — 3.7 / 16 — 3.7 — 3.7 / 17 — 3.9 / 35

4.3 / 36 — 5.6 / 19 — 5.7 — 6.1 / 19 — 6.5 / 37

6.8 / 37 — 7.1 / 20 — 7.3 — 7.7 / 18 — 8.0 / 34

6.1 / 36 — 6.5 / 19 — 4.7 — 7.9 / 19 — 8.4 / 36

4.8 / 34 — 5.1 / 13 — 5.6 — 6.0 / 5 — 6.8 / 21 — 7.5 / 37

7.4 / 34 — 8.0 / 17 — 8.2 — 8.5 / 4 — 9.7 / 20 — 10.5 / 35

5.6 / 33 — 6.1 / 19 — 6.6 — 7.2 / 2 — 8.1 / 18 — 8.9 / 35

6.4 / 34 — 7.1 / 15 — 7.1 — 7.9 / 2 — 8.5 / 17 — 9.2 / 35

7.7 / 37 — 8.4 / 19 — 8.2 — 10.0 / 23 — 10.8 / 37

	+S	H.I.	-S	E/V.	
101			3.8	58.0	58.7
+50			0.8	61.0	61.7
T.P.	0.20	62.47 / 61.87	10.24	61.61	62.27
100			8.4	63.5	64.1
9			5.5	66.4	67.1
8			4.4	67.5	68.1
7			6.2	65.9	66.3
T.P.	5.20	72.51 / 71.85	11.70	66.65	67.31
6			11.3	67.1	67.7
5			8.7	69.7	70.3
4			5.2	73.2	73.8
T.P.	1.33	79.01 / 78.35	10.91	77.02	77.68
3			11.5	76.4	77.1
2			8.7	79.2	79.9
91			5.1	82.8	83.5
90		88.59 / 87.93	5.4	82.5	83.2

Lt & Rt.

3.8 / 34	3.6 / 15	3.8 / 17	3.8 / 34
1.0 / 37	0.9 / 21	0.8 / 13	1.1 / 34
8.4 / 37	8.2 / 20	8.4 / 15	8.9 / 32
5.6 / 37	5.7 / 20	5.7 / 15	5.7 / 33
4.1 / 32	4.1 / 18	4.6 / 12	4.6 / 32
5.2 / 34	5.9 / 20	7.0 / 17	7.7 / 35
11.2 / 34	11.3 / 23	12.3 / 25	12.7 / 35
7.6 / 37	8.1 / 22	9.2 / 24	9.4 / 35
3.2 / 36	4.1 / 19	6.3 / 19	7.6 / 37
8.4 / 37	9.9 / 20	12.9 / 15	14.3 / 36
6.3 / 37	7.5 / 19	9.8 / 15	10.3 / 34
3.3 / 36	4.2 / 19	5.8 / 16	6.4 / 37
4.7 / 36	4.9 / 16	5.4 / 18	5.6 / 37

3.8
5.5
4.6
6.7
11.3
8.7
5.2
11.4
8.1
5.1
5.4

	+S	H.I.	-S	Elv.	
9			7.8	18.7	19.3
108			1.8	24.7	25.3
T.P.	0.87	27.13 / 26.47	11.70	25.60	26.26
+23			7.3	30.0	30.7
107			6.7	30.6	31.3
+42			3.1	34.2	34.8
T.P.	0.81	37.96 / 37.30	11.55	36.49	37.15
B.M.			5.93	1042.11	42.77
106			9.6	38.4	39.1
+86			7.6	40.4	41.1
+65			6.7	41.3	42.0
T.P.	0.60	48.70 / 48.04	6.83	47.44	48.10
105			8.0	46.3	46.9
T.P.	2.39	54.93 / 54.27	9.93	51.88	52.54
A			10.7	51.1	51.8
31			10.0	51.8	52.5
102		62.47 / 61.81	7.9	53.9	54.6

Lt & Rt.

7.8

7.8 / 37	7.8 / 17	7.8 / 22	8.2 / 37

1.8

2.2 / 37	2.2 / 21	1.8 / 17	1.9 / 34

7.3

8.5 / 37	8.2 / 22	7.5 / 20	7.6 / 36

6.7

7.2 / 37	7.0 / 17	6.4 / 17	6.2 / 36

3.1

3.5 / 37	3.4 / 18	2.7 / 22	2.2 / 37

R.R. spk in 14' O.G. Rt. 105+80

9.6

10.8 / 36	10.2 / 17	9.6 / 18	8.2 / 35

7.6

8.8 / 36	8.0 / 17	7.4 / 18	7.0 / 33

6.7

7.9 / 34	7.3 / 17	6.3 / 17	6.3 / 36

Nail in tree Rt. 105+00

8.0

9.0 / 33	8.5 / 17	7.7 / 17	8.0 / 35

10.7

12.2 / 35	10.9 / 18	10.7 / 19	10.3 / 34

10.0

11.2 / 34	10.2 / 17	10.0 / 18	9.6 / 36

7.9

8.1 / 36	8.3 / 20	8.3 / 16	8.2 / 34

	+S	H.I.	-S	E/V.	
+50			3.5	46.0	46.6
117			5.1	44.4	45.0
T.P.	6.42	50.14 / 49.48	0.26	43.06	43.72
16			3.1	40.2	40.9
115			7.5	35.8	36.5
T.P.	11.80	43.98 / 43.32	0.27	31.52	32.18
14			2.3	29.5	30.1
113			9.0	22.8	23.4
T.P.	10.53	32.45 / 31.79	0.40	21.26	21.92
112			2.7	19.0	19.6
+69			3.5	18.2	18.8
111			5.7	16.0	16.6
+35			5.5	16.2	16.8
110			6.5	15.2	15.8
+82			7.2	14.5	15.1
T.P.	6.42	22.32 / 21.66	11.23	25.24	15.90
109+28		27.13 / 26.47	10.2	16.3	16.9

Lt & Rt.

		3.5			
2.4 / 37	2.9 / 22	3.1 / 6		3.9 / 17	4.7 / 37
		5.1			
3.7 / 37	4.4 / 21	4.9 / 7		5.7 / 16	6.7 / 36
		3.1			
2.0 / 36	2.3 / 21	2.7 / 6		3.7 / 17	4.9 / 36
		7.5			
7.5 / 36	7.3 / 6			7.5 / 17	8.0 / 36
		2.3			
2.9 / 36	2.4 / 5			2.4 / 16	1.4 / 20	2.1 / 36
		9.0			
8.7 / 37	9.2 / 5			9.0 / 16	9.2 / 36
		2.7			
2.3 / 37	2.4 / 5			2.8 / 16	3.4 / 34
		3.6			
2.9 / 37	3.2 / 18			3.3 / 17	3.7 / 36
		5.7			
5.2 / 37	5.4 / 18			5.4 / 16	6.9 / 37
		5.5			
5.2 / 36	5.4 / 20			6.0 / 17	6.2 / 33
		6.5			
6.1 / 37	6.4 / 16			6.5 / 16	6.8 / 35
		7.2			
7.0 / 37	7.1 / 19			7.1 / 18	7.3 / 33
		10.2			
10.2 / 37	10.1 / 13			10.3 / 17	10.3 / 35

	+S	H.I.	-S	E/V.	
+85			7.4	11.0	11.7
+76			8.7	9.7	10.4
+66			7.8	10.6	11.3
126			5.9	12.5	13.2
125		19.07	4.2	14.2	14.9
T.P.	3.63	18.41	11.92	14.78	15.44
124			9.6	17.1	17.7
123			6.4	20.3	21.0
T.P.	0.01	27.36 / 26.70	11.40	26.67	27.35
22			11.8	26.3	27.0
121			5.8	32.3	33.0
T.P.	0.41	38.73 / 38.09	11.80	37.68	38.34
20			11.1	38.4	39.0
19			6.4	43.1	43.7
+48			3.9	45.6	46.2
118		50.14 / 49.48	3.0	46.5	46.1

Lt. ℄ Rt.

7.1 7.2 8.4 7.9 7.4 7.2 7.6
37 37 20 9 15 36

7.1 7.3 7.5 8.7 8.1 7.3 7.6
37 25 17 11 20 37

7.0 7.3 7.8 8.0 8.4 8.6
37 20 10 24 36

3.4 5.5 5.9 6.3 6.6
37 19 18 37

2.6 2.6 3.7 4.7 4.6 4.4 4.9
36 19 9 14 24 37

9.5 8.8 9.8 9.6 13.4 11.4
37 19 9 16 35

5.9 5.6 6.6 6.4 7.3 7.8
36 18 8 16 35

10.8 10.7 11.7 11.8 12.6 13.7
36 16 8 16 35

4.3 4.9 5.3 5.8 6.7 7.5 8.2
35 17 7 16 25 37

9.9 9.9 11.1 11.1 12.3 13.7
35 17 7 16 36

5.4 5.1 6.1 6.4 7.0 7.9
34 18 7 18 37

2.6 3.1 3.7 3.9 4.4 5.5
36 22 7 17 37

3.3 2.5 2.8 3.0 3.5 4.4
37 21 7 17 37

	+S	H.J.	-S	E/V.	
+11			8.5	31.4 ✓	32.0
132		40.52	10.3	29.6 ✓	30.2
T.P.	11.49	39.86 ✓	0.50	28.37 ✓	29.03
31			3.6	25.3 ✓	25.9
130			8.2	20.7 ✓	21.3
+48		29.53	10.5	18.4 ✓	19.0
T.P.	10.82	28.87 ✓	0.36	18.05 ✓	18.71
129			2.6	15.8 ✓	16.5
+43			3.6	14.8 ✓	15.5
128			5.8	12.6 ✓	13.3
+68			6.4	12.0 ✓	12.7
+64			8.0	10.4 ✓	11.1
+57			8.4	10.0 ✓	10.7
+50			7.0	11.4 ✓	12.1
127		19.07	7.1	11.3 ✓	12.0
		10[illegible] ✓			

Lf. & Rt.

8.5
9.1/36 9.7/30 9.5/17 9.5/3 8.4/11 8.1/36

10.3
9.2/37 9.5/28 9.7/9 10.0/7 10.7/23 10.5/37

3.6
3.8/36 3.5/13 3.5/17 3.3/36

8.2
8.1/37 8.1/23 8.4/17 8.6/34

10.5
11.4/35 11.0/14 10.6/10 10.9/23 10.9/36

2.6
3.2/35 2.8/27 2.3/19 2.2/37

3.6
4.7/37 4.6/14 3.5/16 3.4/36

5.8
6.0/37 5.6/14 5.6/19 5.5/37

6.4
6.7/37 7.3/21 8.8/14 7.8/7 6.5/19 6.4/37

8.0
6.7/37 6.6/26 7.4/18 8.7/10 6.3/9 6.6/22 6.4/37

8.4
6.9/37 6.6/23 6.9/10 9.0/6 7.9/16 6.6/24 6.8/37

7.0
6.9/35 6.8/15 8.6/8 9.0/18 8.1/26 6.5/30 6.8/37

7.1
7.2/37 6.8/29 6.9/15 7.4/17 7.6/35

	+S	H.I.	− S	E/L.	
140			5.5	55.2	55.9
+50			7.3	53.4	54.6
139			9.0	51.7	52.4
+50			9.2	51.5	52.2
138			9.1	51.6	52.3
+50			9.4	51.3	52.0
+34?	P.C.		9.6	51.1	51.8
137			9.8	50.9	51.6
136		61.36	10.1	50.6	51.3
T.P.	11.22	60.69	1.58	49.47	50.13
135			1.5	49.6	50.2
+53			3.1	48.0	48.6
134		51.71	6.2	44.9	45.5
T.P.	11.45	51.05	0.26	39.60	40.26
133		40.52	3.5	36.4	37.0
		39.86			

Lt ≤ Rt.

5.5

4.8 5.7 4.7 5.5 6.0
35 25 11 12 37

7.3

5.3 5.8 6.5 7.6 7.7
37 25 17 20 37

9.0

7.1 8.1 9.4 10.4
36 18 19 37

9.2

7.0 8.0 10.2 11.0
37 18 21 37

9.1

7.6 8.4 10.2 11.2
37 12 17 36

9.4

7.9 8.5 8.7 10.5 12.0
36 19 4 17 37

9.6

8.4 8.4 9.2 10.5 12.1
34 21 4 13 37

9.8

8.1 8.7 9.5 10.8 12.3
37 23 4 12 35

10.1

8.5 8.9 10.0 10.6 12.0 13.0
37 19 4 9 23 36

1.5

0.8 0.8 1.1 1.3 2.3 3.3
37 22 5 8 22 37

3.1

3.4 2.8 3.0 2.7 3.2 4.3
37 20 4 7 21 37

6.2

7.1 6.0 5.7 6.0 6.8
36 11 10 23 37

3.5

3.7 2.9 2.7 2.7 3.1
39 14 7 22 37

1062.70 = 956.59

B.M.		65.66 ✓	2.30	1062.70	63.36
T.P.	7.56	65.00	3.25	57.44	58.10
141+05 5			2.8	57.9 ✓	58.6
140+50		61.35	3.9	56.18 ✓	57.5
		60.69 ✓			

Dakota Co. S.R. #I.

Dakota Co. S.R. #I

· Spk in 24" Oak 47' L. Sta. 451+00

0.7 / 39	1.1 / 17	2.1 / 10	3.6 / 6	2.4 / 7	3.2 / 18	2.5 / 24	2.5 / 37

3.8

1.9 / 37	1.8 / 28	2.6 / 15	4.6 / 10	4.8 / 8	4.6 / 14	4.1 / 21	4.4 / 37

3.9

Cold & deep snow.

1/3/24 "B" Line

Jorgenson Peterson's Bridge

	+S	H.I	−S & Rod.	Eck & Flv.
B.M.	5.32	85.78		1080.46
50+58			8.1	1077.7
50			8.5	77.3
49			7.8	78.0
48			5.4	80.4
+78			4.4	81.4
47			3.4	82.4
46			3.7	82.1
+24			5.3	80.5
45			6.4	79.4
+55			9.2	76.6
44			14.3	71.5
T.P.	0.20	74.26	11.72	74.06
43			11.1	63.2
42			15.5	58.8
T.P.	0.83	63.95	11.14	63.12
41			9.9	54.1
+50			13.0	51.0
40			16.5	47.5
+40			18.3	45.7
39			16.1	47.9

& Lovals.

3" Line & Levels

		63.95		
38			7.4	56.6
+50			.8	59.2
37			1.2	57.8
36			3.1	60.9
35			1.4	62.6
T.P.			1.08	62.87
+50			4.8	59.5
T.P.	7.30	64.30	0.05	57.00
34			2.3	54.8
T.P.	10.51	57.05	0.16	46.34
33			0.8	45.9
32			8.6	38.1
T.P.	11.51	46.70	0.65	35.19
+50			1.4	34.4
31			3.1	32.7
30			6.6	29.2
+50			9.0	26.8
T.P.	10.02	35.84	0.40	25.82
29			2.9	23.3
+79			4.6	21.6
28			9.1	17.1
T.P.	11.75	26.22	0.35	14.47
27			1.9	12.9
26			6.5	8.3
T.P.	11.44	14.82	0.46	1003.38
25		1003.84	0.6	03.2

Stg kø 35+00 E.

"B" Line & Levels.

+75			2.3	1001.5
24			5.6	98.2
23			9.9	93.9
T.P.	10.87	1003.84	1.35	92.97
22			2.0	92.3
+60			2.6	91.7
21			4.8	89.5
20			7.2	87.1
19			8.5	85.8
+55			9.8	84.5
18			8.8	85.5
17			7.1	87.2
+12			5.5	88.8
16			4.8	89.5
+36			4.6	89.7
15			5.1	89.2
T.P.	5.96	94.32	0.74	88.36
14			4.9	84.2
13			8.7	80.4
12			11.1	78.0
		89.10		
11				

1/2/24 "B" Line

Damn Cold & Deep snow

∠ Rt ∠ L.

33+74.5 P.T.

31+43.7 P.I.

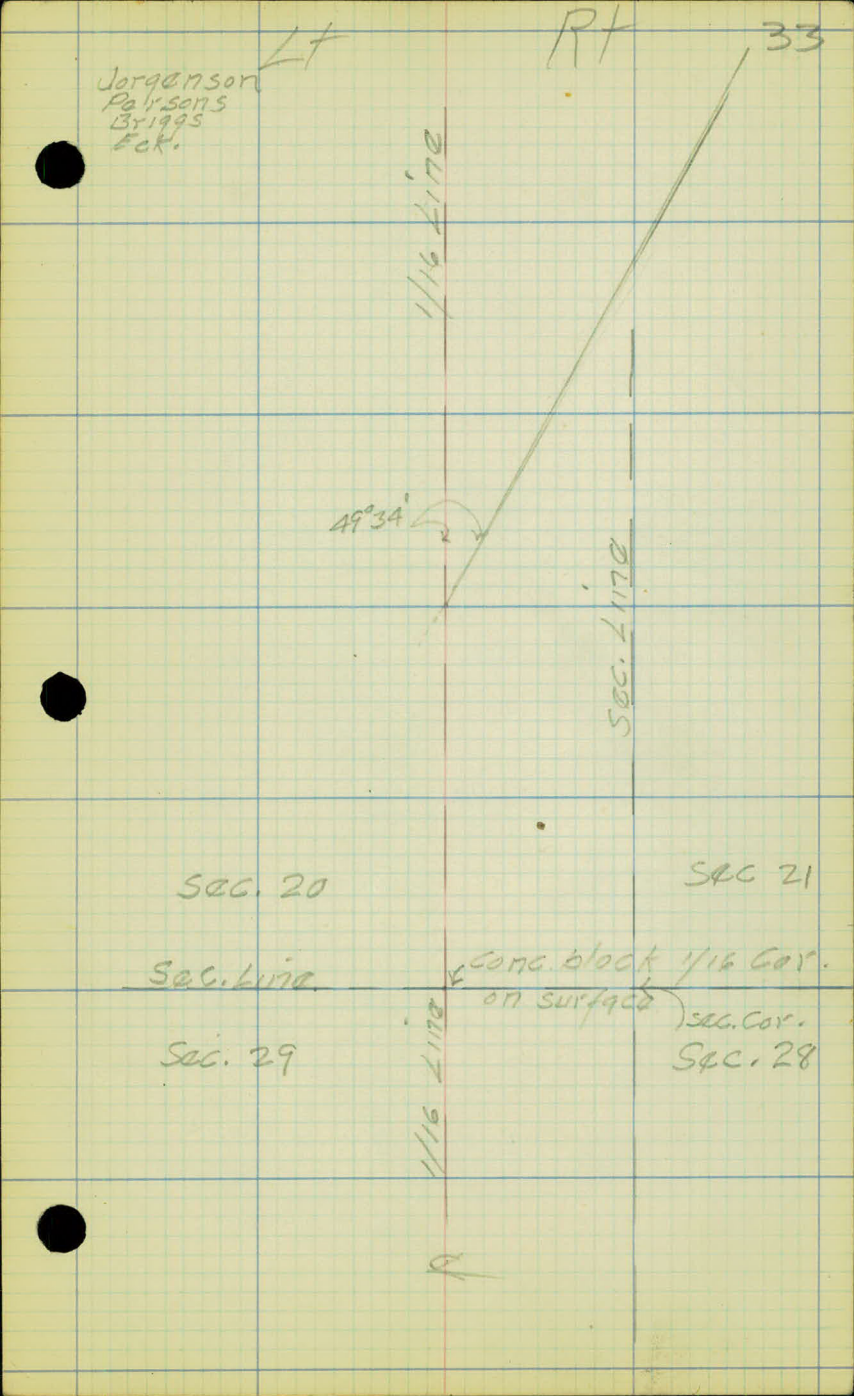
Δ 49° 34'
∠ 10° Rt
T. 264.2
L. 495.7

28+78.8 P.C

16+13.9 P.I. 0°12'

2+83.6 B = 2+83.6 B.

0+00 "B" L. = 0+00 "A" Line.


Lt
Rt
33
Jorgenson
Parsons
Bridges
Ext.
1/16 Line
49°34'
Sec. Line
Sec. 20
Sec 21
Sec. Line
Conc. block 1/16 Cor.
on surface
Sec. Cor.
Sec. 29
Sec. 28
1/16 Line

1/3/24
Cold & Deep snow

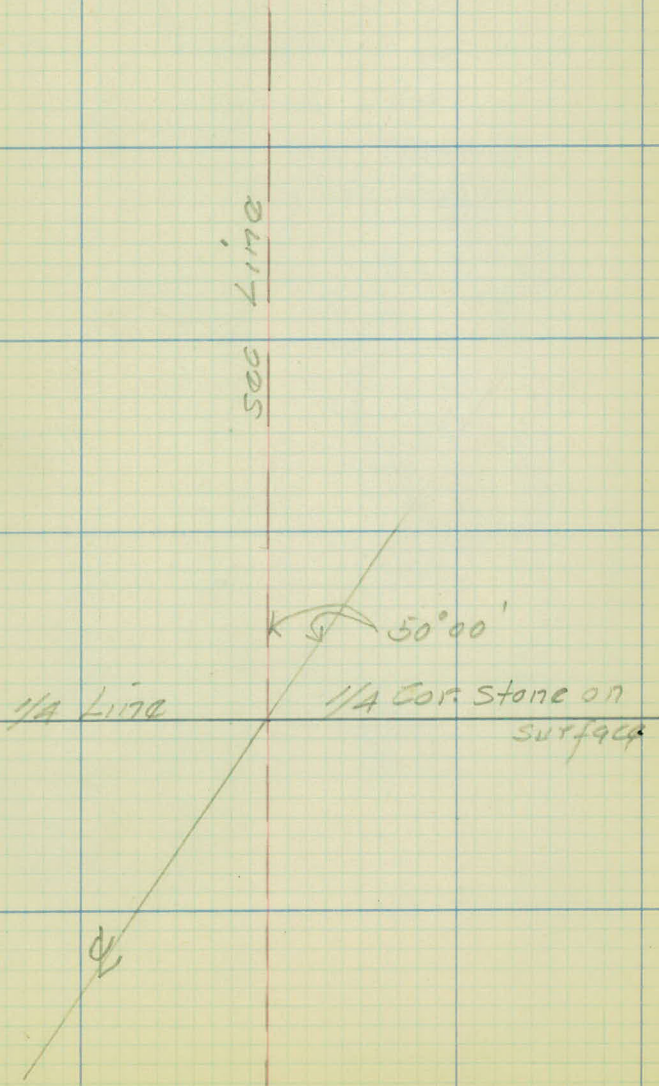
$50+58\frac{8}{}$ "B" Line = $55+76\frac{6}{}$ "A" Line

$48+26\frac{4}{}$ P.I.

$45+58\frac{8}{}$ P.C.

Δ 50° 00'
$\angle$ 10° 0' Lt.
T. $267\frac{6}{}$
L. 500'

Jorgenson
Persons
Briggs
Eck.



B. Line

1/7/24

X Sections on the B. Line from Sta 0+00 to Sta. 50+58.8.

Crane
Persons
Briggs
Lek.

Sta.	Elev.
11	977.1 ✓
10	976.2 ✓
9	976.5 ✓
8	976.4 ✓
7	976.9 ✓
+90	77.0
6	976.4 ✓
5	975.4 ✓
4	975.4 ✓
+15	75.9
3	975.1 ✓
+50	975.7
2	974.7 ✓
-1	975.4 ✓
0+00	973.8 ✓ Beginning of P.Line

B. Line

Lt.			Rt.		
-0.5	-0.3		-0.1	-0.5	
33	17		20	33	
-0.3	-0.5		00	-0.3	
33	22		20	33	
-0.7	-0.8		-0.1	-0.1	
37	19		20	33	
-0.7	00		-0.5	-0.9	
33	21		13	33	
00	00		-0.5	-1.0	
33	21		15	33	
-0.5	00		-1.0	-1.0	
33	17		18	33	
-0.7	-0.4		-0.5	-0.8	
33	20		23	33	
-1.0	-0.7		00	00	
33	21		12	33	
-0.6	-0.3		-0.1	-0.5	
33	22		20	33	
-1.0	-1.0		-0.7	-1.0	
33	18		18	33	
00	00		-0.5	-0.5	
33	19		15	37	
00	-1.5	-1.0	-1.0	-1.0	
33	27	18	21	33	
00	+0.4	00	00	+0.2	-0.4 00
33	27	18	12	21	25 33
-0.5	-0.5	-0.5	-0.5	00	+0.5
33	20	19	18	27	33
-0.7	-0.9	-0.9	-0.5	-1.0	+0.2
33	17	18	17	18	33

Sta.	Elev.
13	993.9
12	992.3
+60	91.7
11	989.5
10	987.1
9	985.8
+55	984.5
8	985.5
7	987.2
+12	88.8
6	989.5
+36	989.7
5	989.2
4	984.2
3	980.4
2	978.0

B. Line

Lt.		Rt.	
+0.5 / 33	−0.3 / 18	+0.5 / 17	+0.3 / 33
−0.5 / 33	−0.5 / 18	−0.2 / 17	−0.5 / 33
−0.7 / 33	−0.5 / 18	−0.2 / 18	−0.5 / 33
0.0 / 33	0.0 / 18	−0.4 / 20	−0.5 / 33
0.0 / 33	+0.5 / 22	−0.2 / 21	−0.5 / 33
0.0 / 33	+0.3 / 21	−1.0 / 20	−1.5 / 33
+1.5 / 33	+0.5 / 18	−0.2 / 18	−0.9 / 33
+1.0 / 33	+0.4 / 18	−1.5 / 19	−2.0 / 34
+0.6 / 33	+0.5 / 22	−1.0 / 18	−1.9 / 33
+0.3 / 33	+0.3 / 18	−1.5 / 18	−2.6 / 33
+0.7 / 34	+0.5 / 18	−1.1 / 19	−1.5 / 33
−0.5 / 33	−0.2 / 18	−1.1 / 18	−2.2 / 33
−1.0 / 33	−0.7 / 19	−0.5 / 19	−1.0 / 33
−1.0 / 34	−0.5 / 18	−0.6 / 22	−1.0 / 33
−0.7 / 33	−0.5 / 22	−0.4 / 21	−0.5 / 33
−0.5 / 33	−0.4 / 21	−0.4 / 21	−0.3 / 33

Sta.		Elev.
34	← -2.5	1054.8 ✓
+79.5	P.T.	1052.3 ✓
33		1045.9 ✓
32		1038.1 ✓
31		1032.7 ✓
30		1029.2 ✓
+50		1026.8 ✓
29		1023.3 ✓
+98.8	P.C.	1021.4 ✓
28		1017.1 ✓
27		1012.9 ✓
26		1008.3 ✓
25		1003.2 ✓
+75		1001.5
24		998.2 ✓

B. Line

Lt.			Rt.	
-2.0 / 33	-0.7 / 18	+1.1 / 18	+2.3 / 36	
-2.1 / 33	-1.5 / 14	+1.6 / 20	+2.5 / 33	
-2.0 / 33	-1.0 / 18	+0.9 / 24	+1.5 / 36	
-2.6 / 33	-1.9 / 17	+1.0 / 24	+2.0 / 36	
-3.5 / 34	-3.0 / 16	-1.0 / 11	+1.0 / 20	+2.0 / 33
-3.1 / 33	-2.0 / 23	-1.5 / 5	+0.5 / 3	+0.8 / 18	+1.5 / 33
	-3.1 / 33	-2.0 / 19	+0.2 / 19	+1.2 / 37	
-2.5 / 33	-1.6 / 21	+0.2 / 22	+1.7 / 33		
-2.5 / 33	-1.7 / 20	+0.1 / 11	+1.0 / 37		
-3.0 / 33	-2.0 / 20	00 / 19	+1.5 / 33		
-2.1 / 34	-1.7 / 18	00 / 20	+1.1 / 33		
-2.5 / 33	-1.5 / 20	-0.9 / 18	00 / 33		
-1.5 / 33	-1.1 / 18	-0.9 / 18	00 / 33		
-1.0 / 33	-1.0 / 14	-1.0 / 19	-1.0 / 33		

Sta.	Elev.
44	1071.5
43	1063.2
42	1058.8
41	1054.1
+50	1051.0
40	1047.5
+40	1045.7
39	1047.9
38	1056.4
+50	1059.2
37	1059.8
36	1060.9
35	1062.4
+50	1059.5
34	1054.8

B. Line

Lt.		Rt.	
00 / 33	00 / 79	-0.8 / 30	-1.0 / 37
+2.0 / 33	+1.0 / 20	-0.5 / 18	-1.0 / 33
+1.5 / 33	+1.0 / 21	-1.0 / 18	-1.6 / 33
+2.5 / 33	+1.0 / 20	-1.5 / 18	-2.5 / 33
38.5 +1.4 / 18	+0.6 / 18	-2.0 / 18	-3.1 / 33
+2.0 / 33	+1.0 / 21	-1.0 / 21	-2.0 / 33
+0.5 / 33	+0.1 / 21	-0.5 / 19	-1.0 / 37
+1.5 / 37	+0.5 / 18	-1.2 / 22	-2.0 / 37
+2.7 / 37	+1.2 / 21	-2.4 / 22	-4.0 / 33
+3.0 / 33	+1.5 / 18	-2.0 / 18	-3.1 / 33
+3.0 / 35	+1.5 / 21	-2.0 / 19	-3.5 / 35
+2.0 / 33	+0.5 / 19	-1.5 / 19	-3.1 / 34
00 / 33	00 / 19	-1.2 / 19	-2.5 / 37
-1.0 / 33	-0.9 / 18	-0.3 / 18	-0.9 / 33
-1.0 / 33	-1.0 / 21	+1.0 / 18	+1.6 / 33

Sta.		Elev.	
		55+74.6 On the A Line	
B. +58.8 =		1077.7✓	End of B. Line
50		1077.3✓	
49		1078.0✓	
48		1080.4✓	
+78		1081.4✓	
47		1082.4✓	
46		1082.1✓	
+58.8	P.C. 00'	1082.1	
+24		1080.5	
45		1079.4✓	
+55		1076.6✓	

B. Line

Lt.		Rt.	
-2.0/33	-1.3/21	-0.5/15	0.0/33
-1.5/33	-1.0/21	-0.4/18	-0.5/33
-0.9/37	-0.5/20	0.0/19	-0.5/33
-1.0/33	-0.5/19	-0.5/19	0.0/33
-1.0/33	-0.2/15	-0.5/18	-1.4/33
-0.5/33	-0.2/18	-0.7/23	-1.0/37
0.0/33	0.0/21	-0.5/18	-0.7/33
0.0/33	0.0/18	-0.5/15	-0.5/33
-0.4/33	-0.1/18	-0.5/18	-1.0/33
+0.2/33	0.0/21	-0.5/22	-0.5/33
0.0/33	0.0/18	-0.5/18	-1.0/33

B. Line

1/7/24

Art. Topog on the B. Line
from Sta 0+00 to Sta. 50+58.8

Crane
Persons
Briggs
Eck.

Sta.

5

4

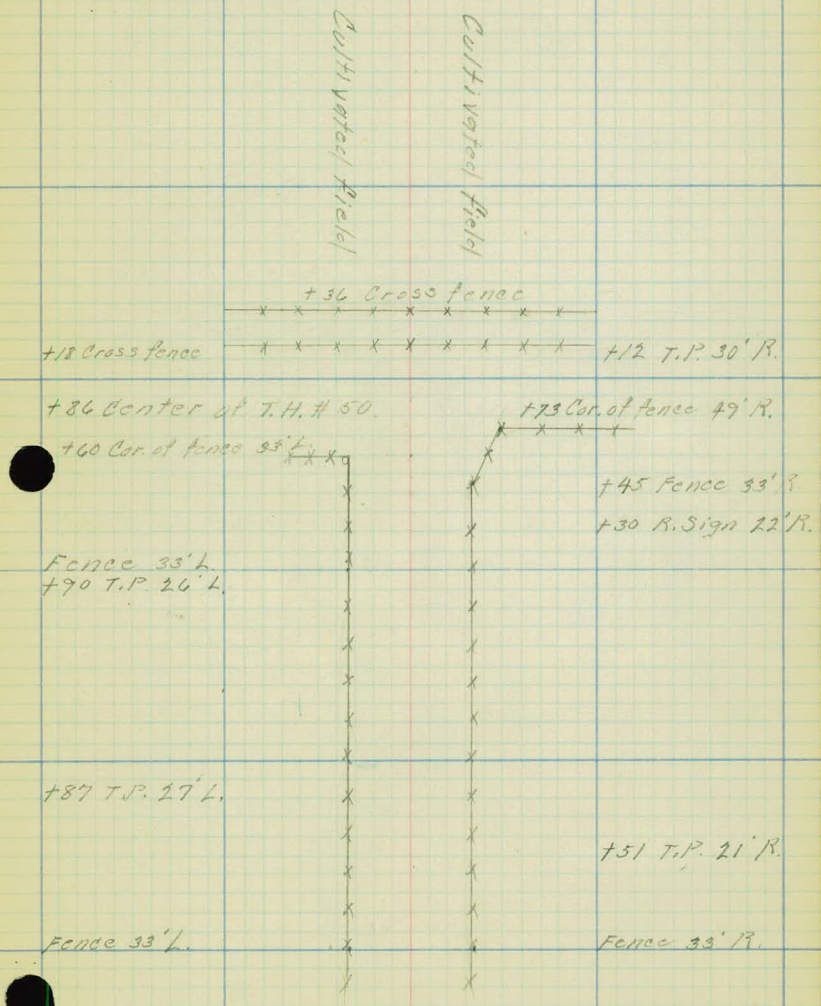
3

2

1 All fences on the B. Line consist of three or four strands of barb wire.

0

B. Line


Cultivated Field
Cultivated Field
+36 Cross fence
+18 Cross fence
+12 T.P. 30' R.
+86 Center of T.H. # 50.
+73 Cor. of fence 49' R.
+60 Cor. of fence 33' L.
+45 Fence 33' R.
+30 R. Sign 22' R.
Fence 33' L.
+90 T.P. 26' L.
+87 T.P. 27' L.
+51 T.P. 21' R.
Fence 33' L.
Fence 33' R.

Sta.

11

10

9

8

7

4

5

43

Cultivated field

Cultivated field

B. Line

Sta.

17

16

15

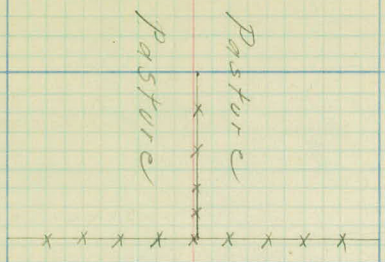
14

13

12

11

B. Line


Fence I. R.
Pasture
Pasture
+12 fence
Cultivated Field
Cultivated Field

Stg.

13

22

21

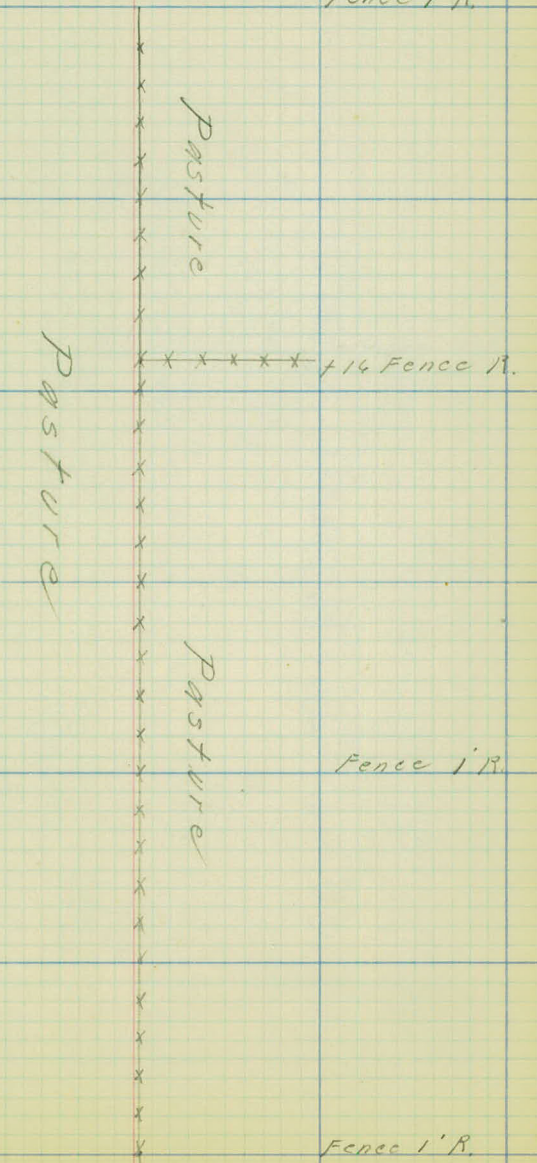
20

19

18

17

B. Line


Fence 1' R.
Pasture
Pasture
#14 Fence R.
Pasture
Fence 1' R.
Fence 1' R.

Sta.

29

28

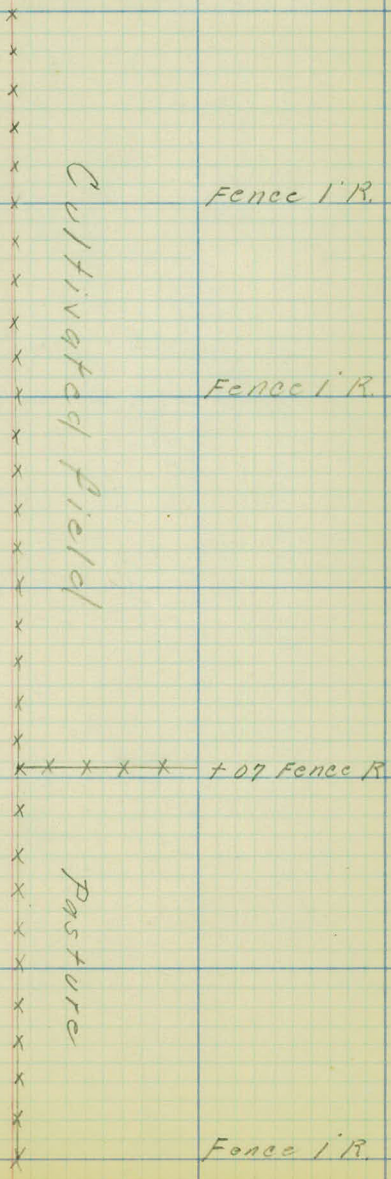
27

26

25

24

23


Fence 1 R.
Cultivated Field
Fence 1 R.
Pasture
+07 Fence R
Pasture
Fence 1 R.

Sta.

35

34

33

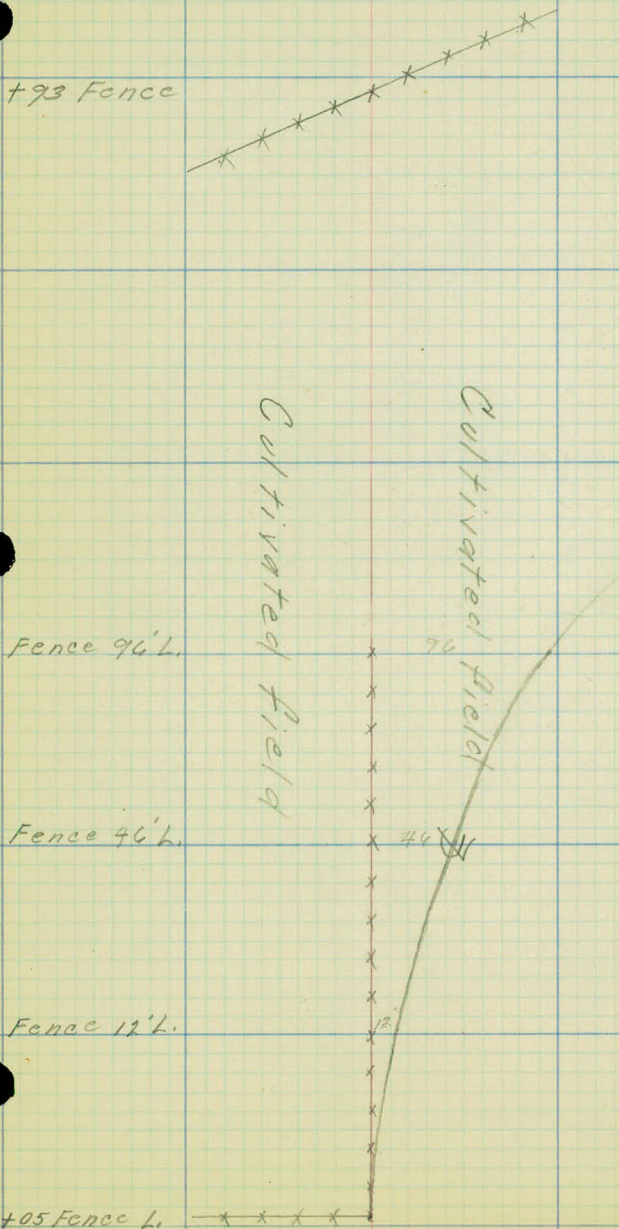
32

31

30

29

B. Line


+93 Fence
Cultivated Field
Cultivated Field
Fence 96'L.
96
Fence 46'L.
46
Fence 12'L.
12
+05 Fence L.

Sta.

41

40

39

38

37

36

35

48

Cultivated field

Cultivated field

B. Line

Sta.

47

46

45

44

43

42

41

49

Cultivated field

Cultivated field

B. Line

579.

+58.8

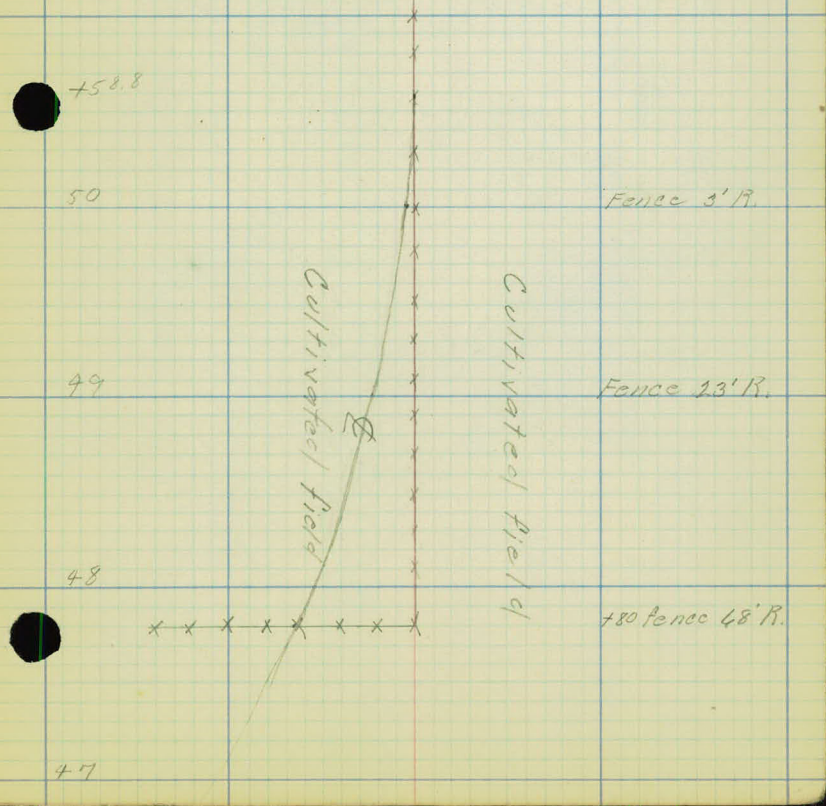
50

49

48

47

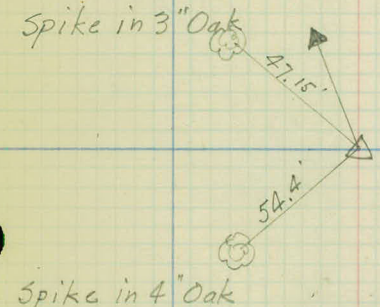
B. Line.

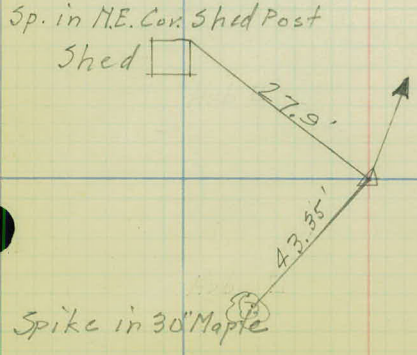

+58.8
50
Fence 3' R.
Cultivated field
Cultivated field
49
Fence 23' R.
48
+80 Fence 48' R.
47

Copy of Dakota Co. Notes
(from book #91)

DODD ROAD
Transit Notes

	ΔL	ΔR	Bearing
P.O.T. 434+00			
			N47°34'E
P.T. 428+06.0			A=8°30'
			D=4° L
			T=106.5'
427+00 P.I. 8°30'			L=212.5'
P.C. 425+93.5			
			N56°04'E
			A=25°30'
PT 414+56.6			D=8°00' R
			T=162.2'
			L=318.8'
413+00 PI	25°30'		
PC 411+37.8			N30°34'E


Spike in 3" Oak
47.15'
54.4'
Spike in 4" Oak


Sp. in N.E. Cor. Shed Post
Shed
27.9'
43.35'
Spike in 30" Maple

Δ L Δ R

N74°14'E

POT 474+00

POT 455+50

N74°14'E

PT 454+79.5 Δ = 26° 40'

D = 8° R

T = 169.9'

P.I. 453+16.0 26°40' L = 333.3'

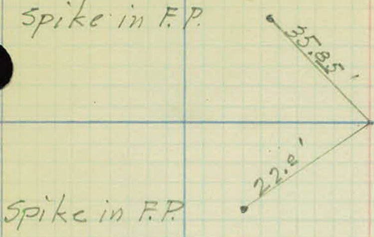
PC 451+46.2

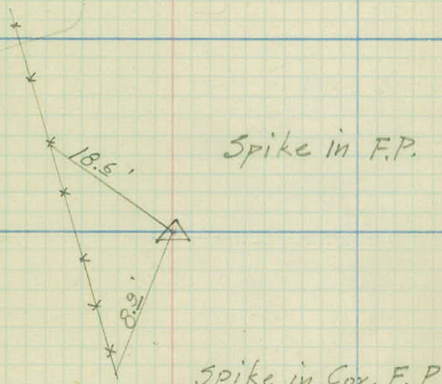
453+05.0 N&S. Sec. Line
bet Sec. 8&9

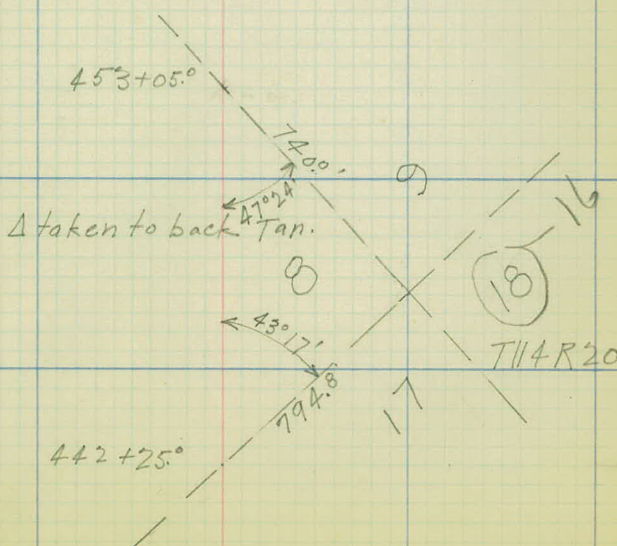
R.O.T. 450+00

N47°34'E

442+25 E&W. Sec Line
bet. Sec. 17&8


Spike in F.P.
35.85'
22.2'
Spike in F.P.


Spike in F.P.
18.5'
8.9'
Spike in Cor. F.P.


453+05.0
74.00'
47°24'
Δ taken to back Tan.
9
16
8
18
43°17'
T114R20
794.8
17
442+25.0

	+	H.I.	−	Elev.
B.M.				880.32
B.M.				956.59

Sp. in Tel. Pole 20'L of Sta. 311+00

310+55 ± is Int. of S.R. Nº1 & S.T.H. #50.

Sp. in 24" Oak - 47'L. of 451+00

Elv. T.H. #50
Lakeville

B.M. 995+00
Spike in 18" Maple 80'L.
El 976.90

Grade T.H. #50

Sta. 993+00 El. 972.3
-0.1% grade

to Sta 1001+54

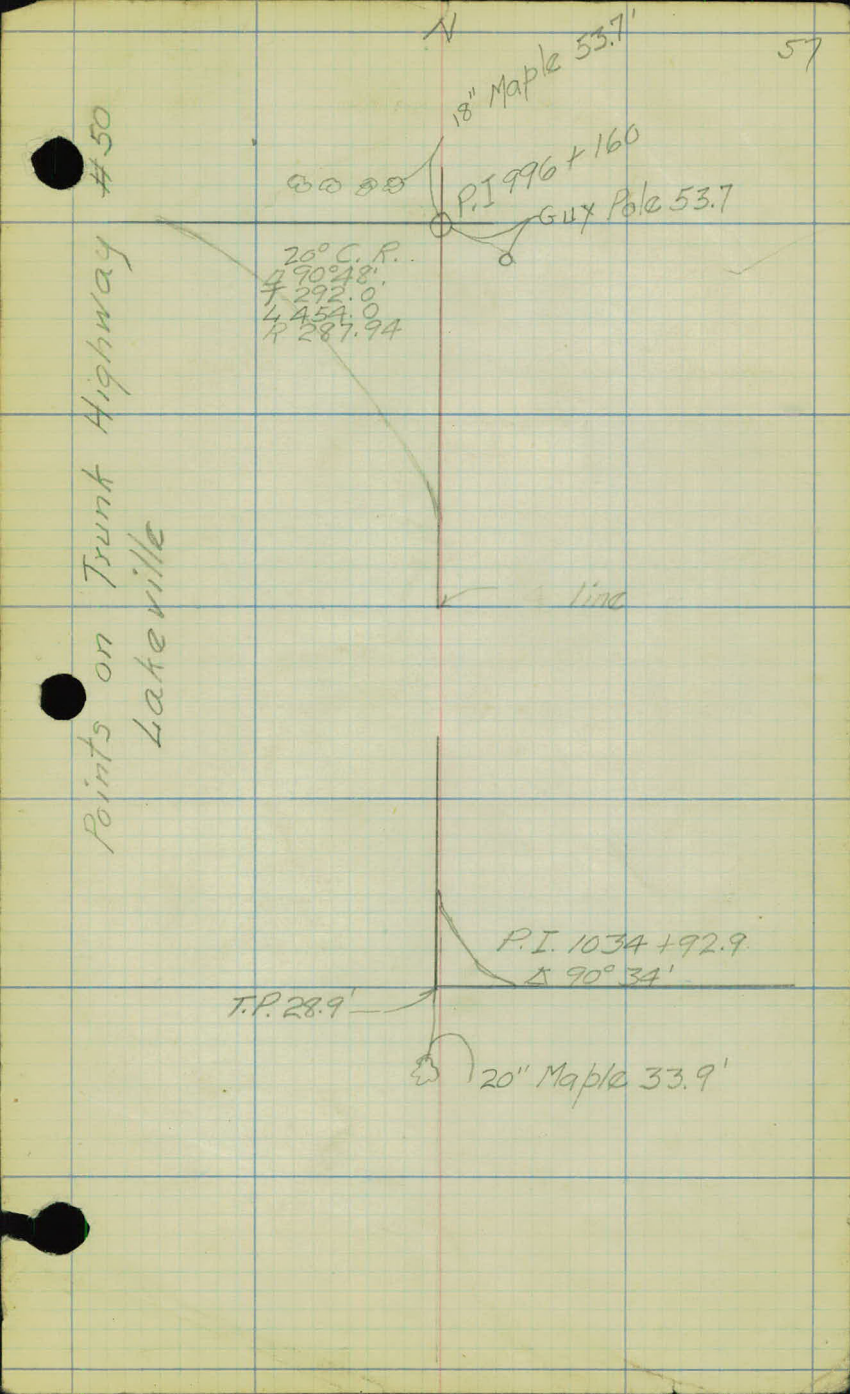
AEA 479.5

38.6

455 ÷ 18 = 1

#50

Points on Trunk Highway
Lakeville



Project 24-02

"L" Line

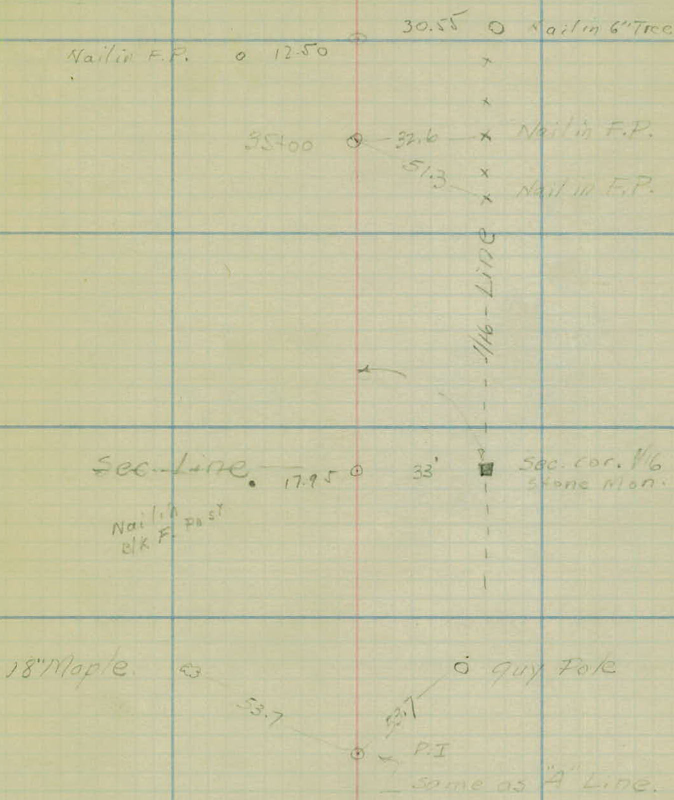
Alignment Notes.

Carlson
Johnson
Ahlberg
Brooke
} Feb. 10-11-24

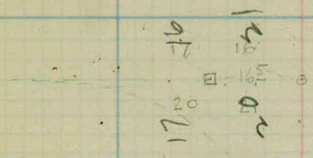
Jorgenson Engr.

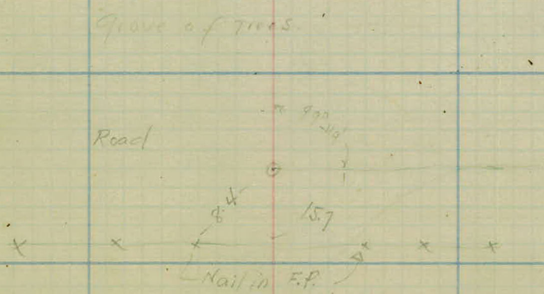
"L" - Line

Station	Ft.	L	R	Bearing	Calc. Coor.
42+42.4	P.I. 1/4 Line		0°-03'		N. 0°-18' E.
35 too	P.O.T.				
					N. 0°-15' E. ✓
16+13.8	P.I		1°-36'		
					N. 1°-21' W. ✓
2+83.6 ↓	P.I	1°-21'			
					N. 0°-00' ✓
0 too	Same as 4 Line				


30.55
Nail in 6" Tree
Nail in F.P.
12.50
35+00
32.6
Nail in F.P.
51.3
Nail in F.P.
1/16 - Line
Sec. Line
17.95
33'
Sec. cor. 1/16
Stone Mon.
Nail in
Blk F. Post
18" Maple
53.7
53.7
Guy Pole
P.I
Same as "A" Line.

Station	Pt	L	R		Calc. Bearing
	"L" Line				N. 0°23'W.
81+13.9 = "A" Line.		45°15'			
82+22.25	P.T.	45°-15'			
82		43°01.5'		20° C.L.	
81		33°01.5'		Δ 90°30'	
80		23°01.5'		P.I. 80+60.2	
79		13°01.5'		S.T. 290.45	
78		3°01.5'		L.C. 452.5	
77+69.75	P.C.	0°00'			
16+00	P.O.T.				~~N.90°00'E~~
					S89.53 E
70+31.55	P.T.		44°54.5'		
70			41°-45'	20° C (L) R	
69			31°-45'	Δ 89°49'	
68			21°-45'	P.I. 68+67.5	
67			11°-45'	S.T. 287.05	
66			1°-45'	L.C 449.1	
65+82.45	P.C				
					N0°18'E.




Grove of Trees.
Road
8.4
15.7
Nail in F.P.

Project 24-02
"L" Line
Art. Topography.

W.H.C.
C.E.S.
M.S.A.
T.F.

Feb. 13, 24

Sta.

5

4

+36 X-Fence
+18 X-Fence

3

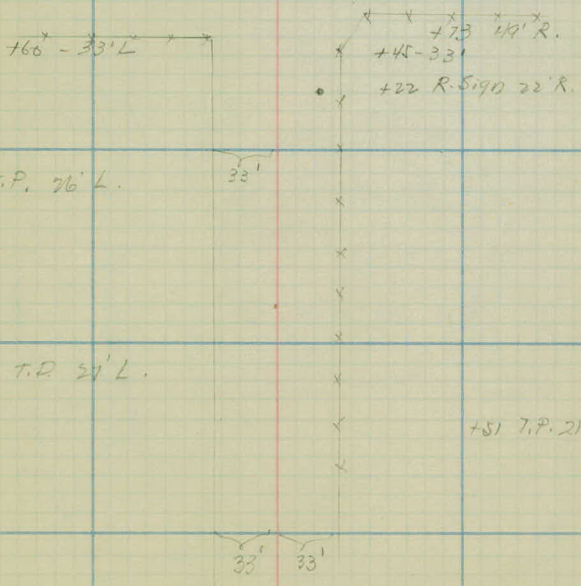
+26 ℄ T.H. #50

2

1

0+00

Cultivated


+66 - 33' L
+90 T.P. 76' L.
+87 T.P. 24' L.
33'
33'
33'
+73 49' R.
+45 - 33'
+22 R.S. 90 22' R.
+51 T.P. 21' R.

18

17

16 + 12 Fences Feet Col. R1

16

15

14

13

12

11

10

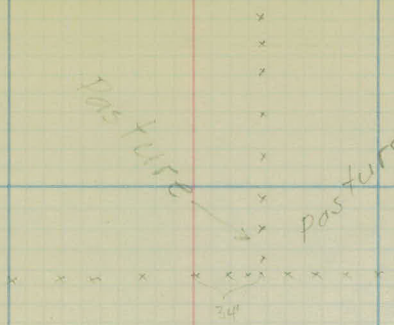
9

8

7

6

5



cultivated

30

+04 Fence & Fence Co.

29

28

27

26

+07 Fence & Fence Co.

25

24

23

22

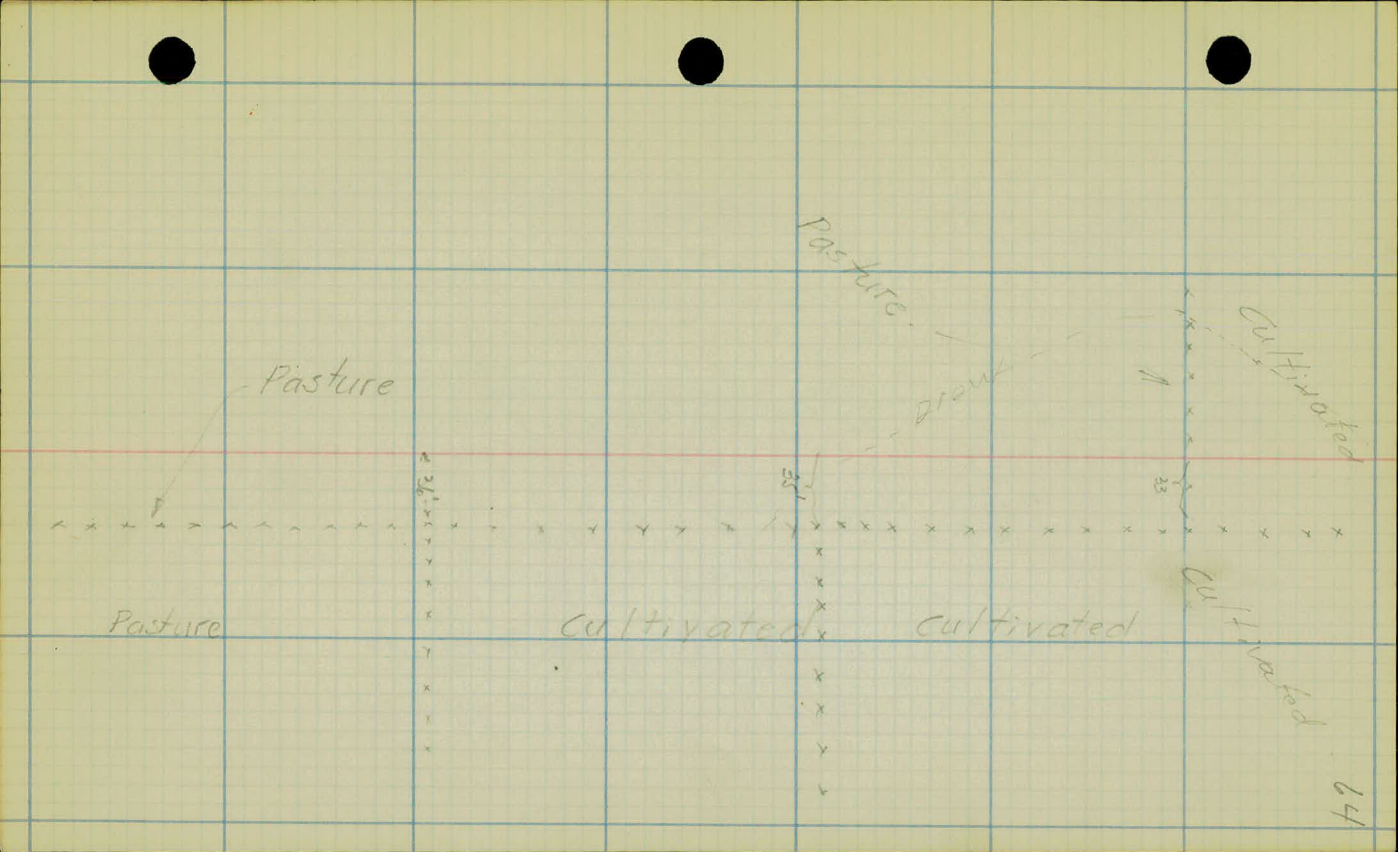
+16 Fence & Fence Co. Inc.

21

20

19

18


Pasture
Pasture
Pasture
Cultivated
Cultivated
Cultivated
Cultivated
Draw
24
23
64

+42 Fence x Fence Cor.

42

41

40

39

38

37

36

35

34

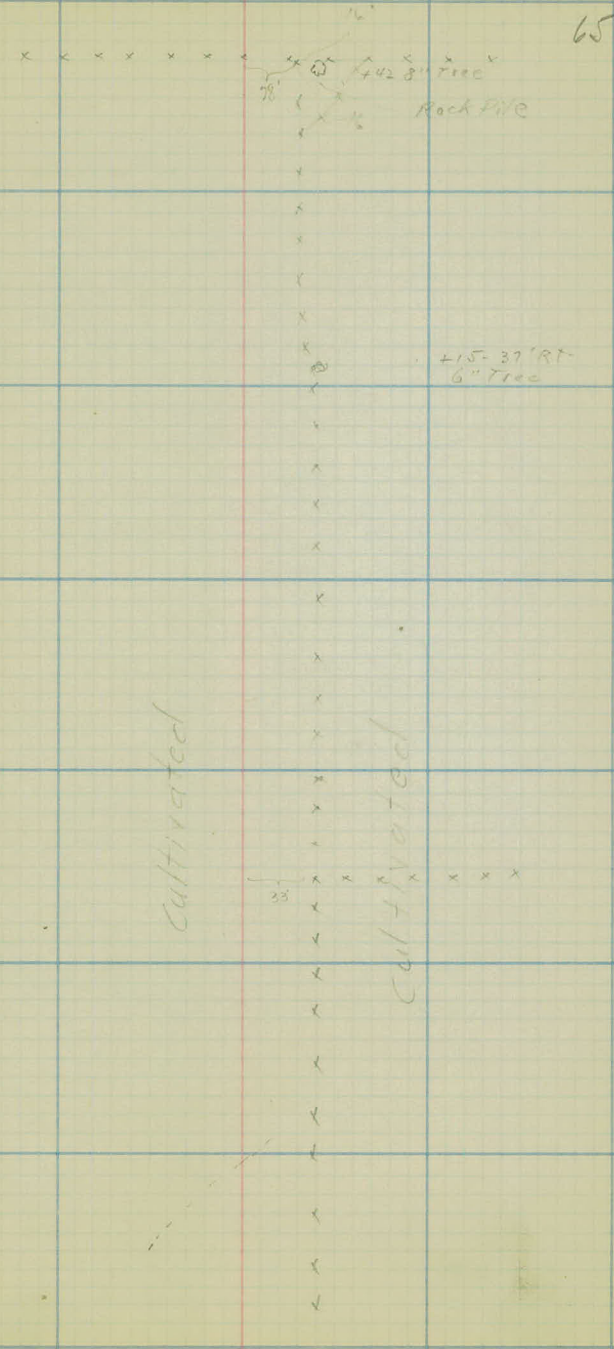
+89 Fence x Fence Cor.

33

32

31

30


+42 8" Tree
Rock Pile
+15- 37' RT-
6" Tree
Cultivated
Cultivated
33'

54

53

52

51

50

+20 Fence Line

49

48

47

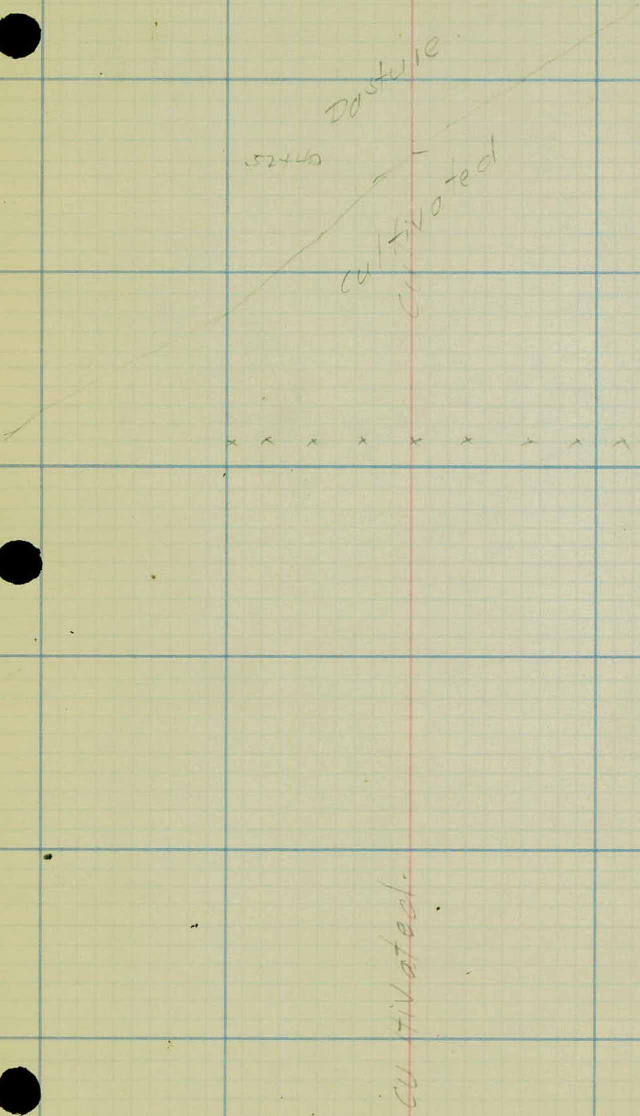
46

45

44

43

42


pasture
.52+40
cultivated
Cultivated
CUltivated.

66
65+82 45 P.C.

cultivated

cultivated

~ 440

Pasture

+69.75 P.C.

77

76

75

74

73

72

71

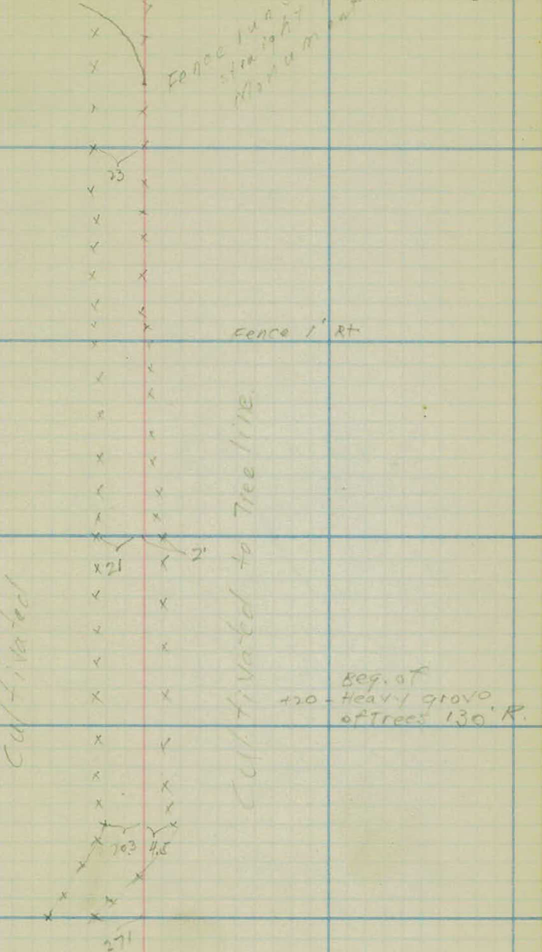
70

69

68

67

66


Fence runs straight to Monument
23
Fence 1' Rt
Cultivated to Tree line
Cultivated
21
2'
+20 - Beg. of Heavy grove of Trees 130' R.
20.3
4.5
27'

83

+22 25 = 82+13.9 "A" Line

82

81

80

79

78

Project 24-02

"E" Line

Center Line Levels
and X-Sections.

Sta.	+	H.I	-	Elev.
"L" Line				
B.M.	3.26	980.16 ✓		976.90 ✓
0+00				
1				
2				
+50				
3				
-36				975.7 ✓
4				975.6 ✓
5				975.4 ✓
6				976.7 ✓
T.P.	3.33	981.29 ✓	2.80	977.96 ✓
7				977.1 ✓
8				976.6 ✓
9				976.3 ✓

L & R W.H.G. E.H.J. M.S.A. T.F. } Feb 18

Spike in 18" Maple 48' Lt. 3+18

See "8" Line X-Sections

5.1 / 33	5.2 / 76	5.1	5.4 / 20	√.2 / 33
5.5 / 33		5.2		5.2 / 33
6.0 / 33		5.4		5.0 / 33
T. Stake				
4.3 / 33		4.1		4.3 / 33
3.8 / 33		4.2		4.6 / 33
4.7 / 33		4.7 @		4.7 / 33
5.1 / 33		5.0		4.8 / 33

Station	+	H.I	−	Elev.
		992.29		
10				976.2 ✓
11				976.9 ✓
12				977.9 ✓
13				980.3 ✓
T.P.	11.19	992.43 ✓	0.05	981.24 ✓
14				983.8 ✓
15				988.4 ✓
+50				989.9 ✓
16				990.7 ✓
+15				990.8 ✓
17				988.5 ✓
18				987.1 ✓
19				986.5 ✓
20				988.0 88.3

	L	℄	R
	4.9 / 3.3	5.1	5.0 / 3.2
	4.2 / 3.3	4.4	4.2 / 3.3
	3.3 / 3.3	3.4	3.4 / 3.3
	0.9 / 3.3	1.0	0.9 / 3.2
Top of stake 12.			
	9.0 / 3.3	8.6	8.2 / 3.3
	4.1 / 3.3	4.0	3.7 / 3.3
	2.8 / 3.3	2.5	2.7 / 3.3
	1.2 / 3.3	1.1	2.7 / 3.3
	1.0 / 3.3	1.6	3.5 / 3.3
	3.6 / 3.3	3.9	5.1 / 3.3
	4.4 / 3.3	5.3	6.6 / 3.3
	4.8 / 3.3	5.9	6.6 / 3.3
	4.3 / 3.3	4.4	5.1 / 3.3

Station	+	H.I.	−	Elev	
		992.43			
21				989.8 ✓	
22				992.0 ✓	
T.P.	11.73	1003.82 ✓	0.34	992.09 ✓	
23				994.4 ✓	
24				997.6 ✓	
25				1001.9 ✓	
T.P.	11.26	1014.39 ✓	0.69	1003.13 ✓	
26				1006.8 ✓	
27				1010.9 ✓	
T.P.	11.90	1025.90 ✓	0.19	1014.20 ✓	
28				1015.4 ✓	
29				1020.9 ✓	
+25				1022.9 ✓	
B.M.	10.25	1035.17 ✓	1.08	1024.82 ✓	✓
30				1024.5 ✓	
+50				1026.2 ✓	
31				1026.9 ✓	

L	℄	R
7.6 / 33	2.6	2.9 / 33
.00 / 33	.04	0.3 / 33
8.7 / 33	9.4	7.6 / 33
6.3 / 33	6.7	5.8 / 33
2.1 / 33	1.9	0.8 / 33
Top Stake 2.5		
8.4 / 33	7.6	6.3 / 33
4.2 / 33	3.5	2.3 / 26 — 1.4 / 33
11.8 / 33	10.5	8.9 / 33
6.7 / 33	5.0	2.2 / 33
4.8 / 33	3.0	0.2 / 33
R.R Spike in Cor. F.E. 33 Rt. Sta 24+04 Not on head of spike 13.0 / 33	10.7	8.1 / 33
11.6 / 33	9.0	6.4 / 33
9.0 / 33	8.3	5.8 / 33

Station	+	H I	−	Elev.	
		1035.17			
31+55				1030.0 ✓	
32				1033.4 ✓	
T.P.	11.43	1045.81 ✓	0.79	1034.38 ✓	
33				1041.3 ✓	
T.P.	11.47	1056.47 ✓	0.81	1045.00 ✓	
34				1050.7 ✓	
+60				1055.5 ✓	
T.P.	3.34	1059.55 ✓	0.76	1056.21 ✓	
35				(1057.0)	56.6
+40				(1056.5)	56.1
36				(1051.2)	50.8
+50				(1048.5)	48.1
T.P.	2.20	1050.92 ✓	1.28	1048.72 ✓	
37				1047.7 ✓	
+70				1044.1 ✓	
B.M.			1.29	1049.63 ✓	3
38				1044.3 ✓	

L	C	R
	3	
5.6 / 33	5.2	4.7 / 33
1.9 / 33	1.8	1.3 / 33
Top of Shale 32		
4.6 / 33	4.5	3.6 / 33
6.0 / 33	5.8	4.5 / 20 · 4.0 / 33
2.0 / 33	1.0	0.0 / 15 · 0.0 / 33
4.3 / 33	3.0	1.6 / 12 · 2.0 / 21 · 1.6 / 33
5.2 / 33	3.8	2.1 / 10 · 2.4 / 29 · 1.5 / 33
11.9 / 33	9.8	6.7 / 10 · 6.0 / 24 · 6.2 / 30 · 4.3 / 33
14.7 / 33 · 13.7 / 12	11.5	9.1 / 15 · 7.8 / 30 · 6.5 / 33
Top of Shale 37		
6.6 / 33	3.2	1.4 / 15 · 1.0 / 30 · 0.0 / 33
9.1 / 33	6.8	5.0 / 12 · 3.7 / 30 · 2.5 / 33
Top of Boulder. 33' Rt 37+70		
9.6 / 33	6.6	5.7 / 18 · 4.7 / 33 · 3.5 / 33

Station	+	H.I	−	Elev
		1050.92		
38+45				1043.2
39				1042.8
+				
+58				1040.6
40				1042.0
+60				1039.9
41				1040.3
+25				1042.1
+70				1046.9
42				1047.4
+42				1043.4
T.P.	1.19	1040.52	11.59	1039.33
+65				1040.9
43				1038.4
44				1035.3

L	S	R
10.6 / 33	7.7	5.7 / 21 — 4.5 / 33
11.5 / 33	8.4	6.1 / 30 — 5.1 / 33
18.0 / 33	10.3	7.0 / 30 — 6.0 / 33
12.1 / 33	8.9	6.6 / 30 — 5.7 / 33
13.3 / 33	11.0	9.8 / 15 — 9.8 / 30 — 8.4 / 33
12.6 / 33	10.6	8.5 / 27 — 6.1 / 33
10.4 / 33	8.8	8.1 / 24 — 7.5 / 33
5.0 / 33	4.0	3.5 / 33
3.7 / 33	3.5	4.3 / 33
7.4 / 33	7.5	8.0 / 33
Top of Stake 4.3		
0.7 / 33	0.2	0.0 / 33
2.5 / 33	2.1	1.1 / 33
7.8 / 33	5.7	2.8 / 33

Station	+	H.I	−	Elev
		1040.52		
45				1031.7
45+50				1029.9
46+00				1029.5
T.P.	2.78	1033.17	10.13	1030.39
47				1028.6
48				1027.5
49				1027.5
50				1030.2
51				1028.5
T.P.	7.35	1037.18	3.34	1029.83
52				1026.9
53				1026.6
+45				1027.3
54				1030.2
+60				1032.3

L	C	R
10.6/33	8.8	7.1/33
12.0/33	10.6	9.3/33
12.5/33	11.0	9.6/33
T. Stk 46		
.59/33	4.6	2.9/33
7.1/33	5.7	4.2/33
7.8/33	5.7	3.4/33
.57/33	3.0	.50/33
6.4/33	4.7	3.1/33
T. Stk. 51		
11.7/33	10.3	9.2/33
11.5/33	10.6	9.4/33
11.2/33	9.9	9.0/33
8.3/33	7.0	5.8/33
5.6/33	4.9	3.1/33

Station	+	H.I	−	Elev.
		1037.18		
T.P.	10.88	1047.61	0.45	1036.73
55				1037.3
+22				1039.2
56				1041.3
57				1043.4
T.P.	12.09	1059.32	0.38	1047.23
58				1047.3
+60				1049.1
59				1052.6
+65				1056.6
T.P.	11.66	1070.82	0.16	1059.16
60				1060.2
+54				1065.1
61				1067.6
62				1070.3

L	S	R
12.3 / 33	10.3	8.5 / 33
11.1 / 33	9.1	6.0 / 33
9.0 / 33	6.8	3.8 / 33
6.1 / 33	4.2	1.6 / 33
14.3 / 33	12.0	9.9 / 33
11.8 / 33	10.7	8.7 / 33
9.0 / 33	7.3	5.9 / 33
3.5 / 33	2.7	2.3 / 33
11.3 / 33	10.6	7.9 / 33
7.2 / 33	5.7	5.0 / 33
4.9 / 33	3.7	3.3 / 33
2.5 / 33	0.5	0.0 / 33

Station	+	H.I	−	Elev
		1070.82		
T.P.	11.90	1082.71	0.01	1070.81
63				1071.7
64				1074.5
65				1079.6
T.P.	11.94	1093.91	0.74	1081.97
66				1084.5
67				1090.3
750				1093.3
T.P.	5.90	1099.30	0.51	1093.40
68				1094.9
69				1095.7
B.M.			2.31	1096.99
70				94.7
71				93.1
72				91.7
73				92.5

L	R	R
8.2 / 33	1.0	2.3 / 33
10.6 / 33	8.7	6.3 / 33
4.3 / 33	3.1	1.3 / 33
11.1 / 33	9.4	7.8 / 33
3.6 / 33	3.6	3.4 / 33
0.0 / 33	0.6	0.9 / 33
3.9 / 33	4.4	4.7 / 33
2.7 / 33	3.4	4.5 / 33

R.R. spike in 8" Tree 21' L. sta 69+00

4.3 / 33	4.0 / 17	4.6	5.7 / 33
5.6 / 33	5.8 / 17	6.7	7.7 / 33
6.6 / 33	6.8 / 17	7.6	8.8 / 33
6.7 / 33	6.6 / 17	6.8	7.6 / 33

Station	+	H. I	−	Elev.
		1099.30		
74				92.5
T.P.	0.90	1094.45	5.75	1093.55
75				90.4
76				88.1
77				85.2
T.P.	0.90	1084.13	11.22	1083.23
78				81.0
79				75.7
80				73.1
T.P.	1.95	1074.22	11.86	1072.27
81				1071.6
82				1069.1
T.P.	12.11	1080.10	6.43	1067.99
B.M.			1.04	1079.06

L	C	R
7.0 / 33	6.8 / 18	6.8	7.2 / 33
4.6 / 33	4.2 / 14	4.1	4.1 / 33
7.0 / 33	6.7 / 14	7.1 / 6	6.6 / 5	6.4	6.3 / 33
9.6 / 33	9.5 / 14	10.1 / 6	9.4 / 5	9.3	9.6 / 33
3.7 / 33	4.0 / 13	3.8 / 13	3.8 / 5	3.4 / 4	3.1	3.6 / 33
	6.8 / 33	8.4	9.0 / 15	9.5 / 25	9.5 / 33
	9.6 / 33	11.0	12.8 / 33
	1.6 / 33	2.6	3.5 / 33
	4.6 / 33	5.1	5.8 / 14	6.9 / 33

88+30 "A" Line R.R. spike Rt. in 22" Tree.

See topog. of "A" Level

Proj 24 02
Check Levels

"L" Line to "A" Line Sta 884.30

Station	+	H.I	-	Elev.	
Check Levels "L" Line.					
	3.25	980.25		976.90	
T.P.	3.90	981.93	2.22	978.03	
T.P.	10.68	991.91	0.70	981.23	
T.P.	8.43	996.93	3.41	988.50	
T.P.	10.72	1006.15	1.50	995.43	
			3.00	1003.15	= 1003.13
T.P.	10.99	1016.85	0.29	1005.86	
T.P.	11.03	1027.59	0.29	1016.56	
B.M.			2.75	1024.84	= 1024.82
T.P.	11.21	1037.98	0.82	1026.77	
T.P.	11.57	1048.87	0.68	1037.30	
T.P.	9.18	1057.70	0.35	1048.52	
B.M. for check			8.05	1049.65	= 1049.63
	91.06		18.31		
	- 18.31			1049.65	
	72.75 ✓			976.90	
				72.75 ✓	
B.M.	0.51	1050.14		1049.63	
T.P.	1.05	1040.39	10.80	1039.34	
T.P.	4.79	1034.26	10.92	1029.47	
T.P.	11.99	1043.68	2.57	1031.69	
T.P.			1.35	1042.33	
	18.34		25.64	1049.63	
			7.30 ✓	1042.33	
				7.30 ✓	

W.H.C.
E.H.J.
M.S.A.
T.F.
} Feb 19 1924.

Spike in 18" Maple 48' Lt. 3+18 "L" Line.
This is State Highway Datum

Old T.P top of Stake Sta. 25

R.R. Spike in Cor. F. Post 33' R. Sta. 29+04.

Top of Boulder 33' Rt. 37+70

Top Stake Sta. 47 +00

	+	H.I	−	Elev.	
	12.01	1054.34		1042.33	
T.P.	11.72	1064.95	1.11	1053.23	
T.P.	11.81	1076.22	0.54	1064.41	
T.P.	11.82	1087.59	0.45	1075.77	
T.P.	11.99	1098.87	0.71	1086.88	
B.M.			1.84	1097.03 = 1096.99	
T.P.	1.39	1094.48	5.78	1093.09	
T.P.	0.80	1084.08	11.20	1083.28	
T.P.			7.40	1076.68	
T.P.	1.80	1075.82	10.06	1074.02	
T.P.	12.07	1079.73	8.16	1067.66	
B.M.			0.65	1079.08 = 1078.40 ("A" Line) (= 1079.06 "Z" Line.)	
	75.41		38.66		
	38.66			1079.08	
	36.75 ✓			1042.33	
				36.75 ✓	

Checking back on "A" Line.

T.P.	0.45	1077.13		1076.68	
T.P.	9.30	1083.77	2.66	1074.47	
B.M.			3.25	1080.52 = 1080.46 ("A" Line) (= 1080.51 "Z" Line)	

R.R. Spike in 8" Tree 72' L. Sta 69+00

Top of Stake Sta 79.

R.R Spike in 22" Tree Rt. Sta. 88+30 "A" Line.

Top Stake Sta 79.

R.R Spike in Cor. F. Post Sta. 53+05 "A" Line.

Project 24-02

"L"-"P" Line

Alignment Notes

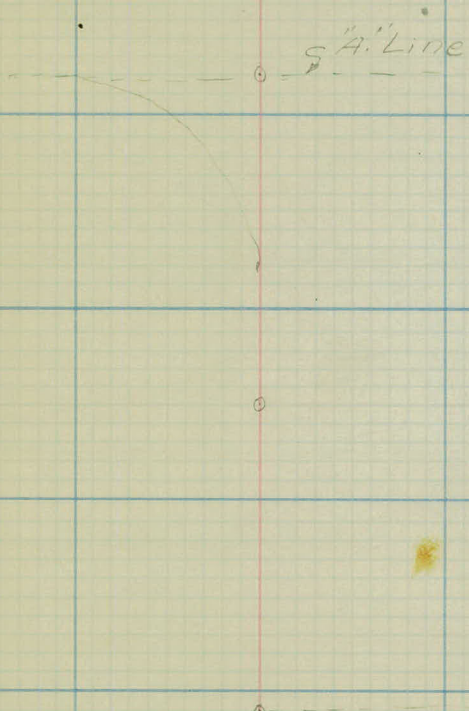
Carlson
Johnson
Ahlberg

Feb 15, 24

Jorgenson Engr.

Station	Point	L	R	Calc. Bear	
					(N. 0° 15' W.)
= 55+96± = "A" Line					
56+21.57	P.T.	44°54'			
56		42°44'			
55		32°44'		20° C.L.	
54		22°44'		Δ 89°48'	
53		12°44'		P.I = 54+59.6	
52		2°44'		S.T 286.93	
51+72.67	P.C.	0°00'		C.L. 449.20	
47+38.7	P.O.T.				
				N. 45°54' E.	
44+04.5	P.T.		44°40.5'		
44			44°13.8'		
43			34°13.8'	20° C. R.	
42			24°13.8'	Δ 89°21'	
41			14°13.8'	P.I. 42+42.4	
40			4°13.8'	S.T. 284.7	
39+57.7	P.C			C.L. 446.75	
					N. 0° 15' E.

"L-P" Line



Project 24-02

L-P Line

Art. Topography.

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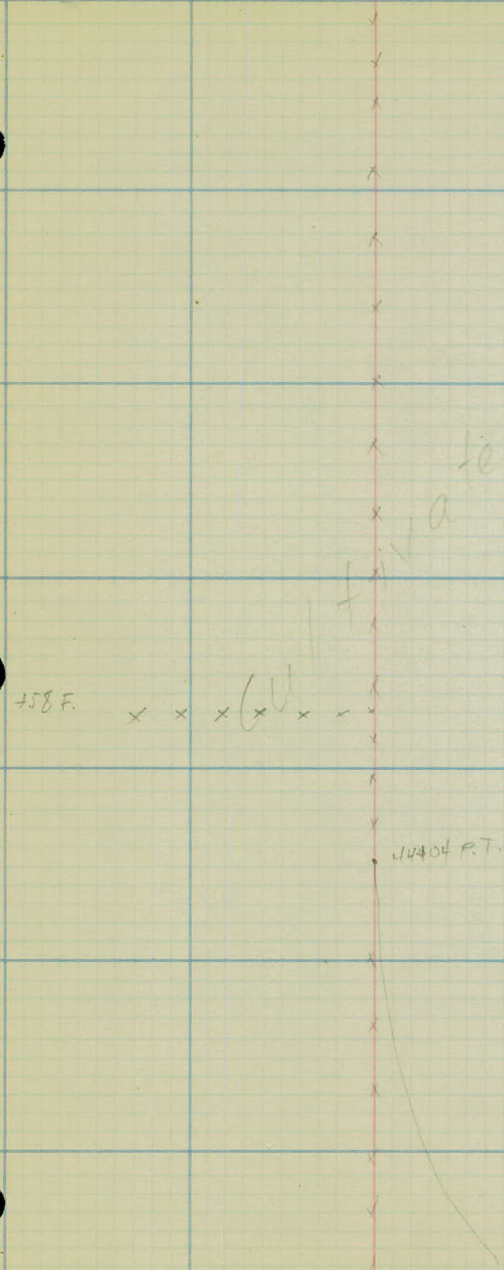

+58 F.
11404 F.T.

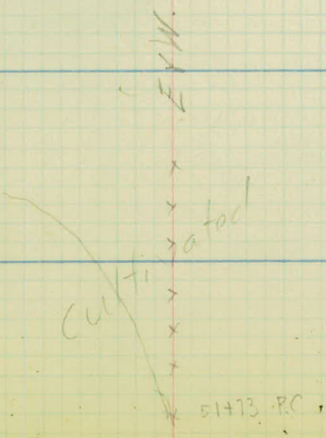
56+26 57 = 55+96 = "A" Line

55

54

53

52



Cultivated
51+73 P.C

Project 24-02

"L" - P. Line.

Center Line Levels
and Cross Sections

Station	+	H.I	−	Elev.
L-P. Line.				
B.M.	6.90	1087.41		1080.51
56+21.5				77.9
56				77.8
55				77.0
54				78.6
53				80.9
52				82.1
51				82.9
50				83.1
49				83.4
48				84.0
T.P.	1.92	1087.00	2.33	1085.08
47+40				84.4

L	E	R
		W.H.C. C.E.S. M.S.A. T.F. Feb 19 34
18+32+20 "A" Line 53+05		
11.1 / 33 — 10.1 / 12 / E	9.5	10.0 / 6 — 9.5 / 33
11.0 / 32 — 10 / 33	9.6	9.9 / 32
11.0 / 33	10.4	9.5 / 13 — 9.9 / 33
9.5 / 32	8.8	8.8 / 33
7.4 / 33	6.5	5.5 / 33
6.5 / 33	5.3	4.9 / 32
5.9 / 33	4.5 / 0	4.8 / 33
4.2 / 33	4.3	5.2 / 33
4.9 / 33	4.0 / 0	3.5 / 33
4.5 / 33	3.4	3.0 / 33
3.7 / 33	2.6	3.0 / 33

Station	+	H.I	−	Elev.
		1087.00		
47				1083.1
+50				79.9
46				75.7
T.P.	030	1075.27	12.03	1074.97
45				66.4
+45				63.5
44				62.6
T.P	0.03	1064.00	11.30	1063.97
+60				63.3
43				56.6
T.P	4.17	1056.12	12.05	1051.95
+35				49.7
42				48.3
41				43.6
40				42.3
BM. for check.			6.18	1049.64
394 577				

L	E	R
5.0 / 33	3.9	3.9 / 33
9.2 / 33	7.1	5.6 / 33
14.0 / 33	11.3	9.3 / 33
12.1 / 33	8.9	7.3 / 5 / 6.4 / 33
15.4 / 33	11.8	10.0 / 5 / 9.0 / 33
17.0 / 33	13.1 / 0	10.7 / 5 / 9.9 / 33
4.6 / 32 / 2.4 / 4	0.7	0.5 / 33
8.0 / 33 / 7.1 / 20	6.4 / 0	6.8 / 33
7.5 / 33	6.4	5.7 / 33
8.8 / 33	7.8	7.3 / 33
13.8 / 33	12.5	12.7 / 33
17.0 / 33	13.8	12.0 / 32

39+70 Rock St.

See 3rd Line

Project 24-02
"L"-"K" Line
Aligment Notes

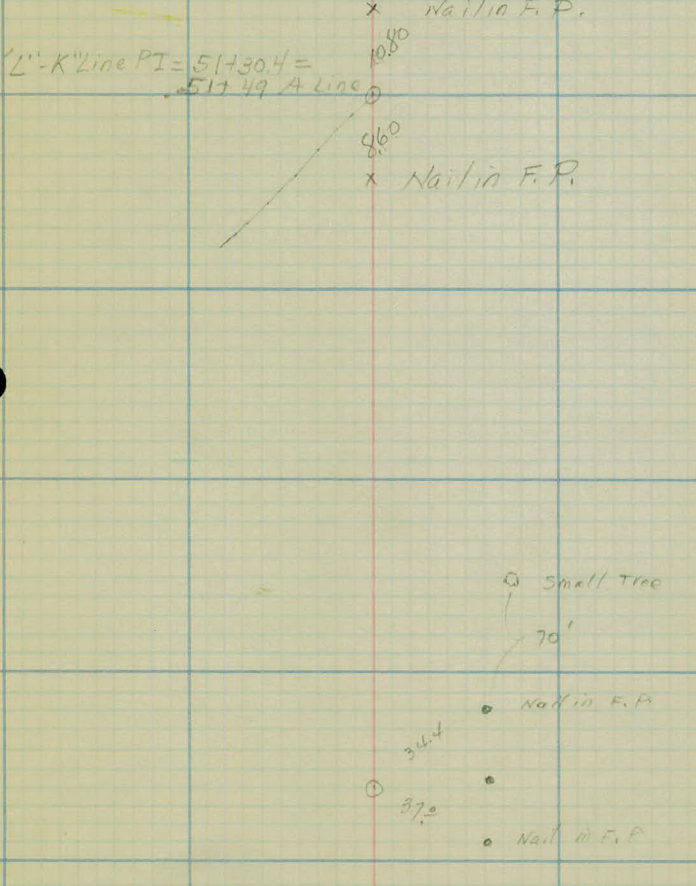
Carlson
Johnson
Ahlberg

Feb 15, 24

Jorgenson Engr.

Station	Point	L	R	Calc. Bear. N 0°15'W. + Δ "A" Line N. 0°-12'W. =
	℄ = 5389.8	"A" Line.		
52+88.65	P.T.	39°54.5'		
52		31°-02.6'		20° C.L.
51		21°-02.6'		Δ 79°49'
50		11°-02.6'		P.I. 51+30.4
49		1°-02.6'		S.T. 240.83
48+89.57	P.C.			C.L. 399.08
41+80	P.O.T.			
				N. 79° 37' E.
40+02.71	P.T.		39°41'	
40			31°-19'	
39			29°-19'	20° C.R.
38			19°-19'	Δ 79°22'
37			9°-19'	P.I. 38+45.8
36+06.83	P.C.			S.T. 238.12
				L.C. 376.83
				N. 0°-15' E.

L-K Line


Nail in F.P.
10.40
"L"-K" Line PI = 51+30.4 =
51+49 A Line
46.0
Nail in F.P.
Small Tree
70'
Nail in F.P.
34.4
37.0
Nail in F.P.

Project 24-02

L-K-Line

Art. Topography.

48

47

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37

406·88 R.C.

36

cultivated

cultivated

37+39 E Xing

Fence N&S

33

+88.65 = 53+89.2 "A" Line.

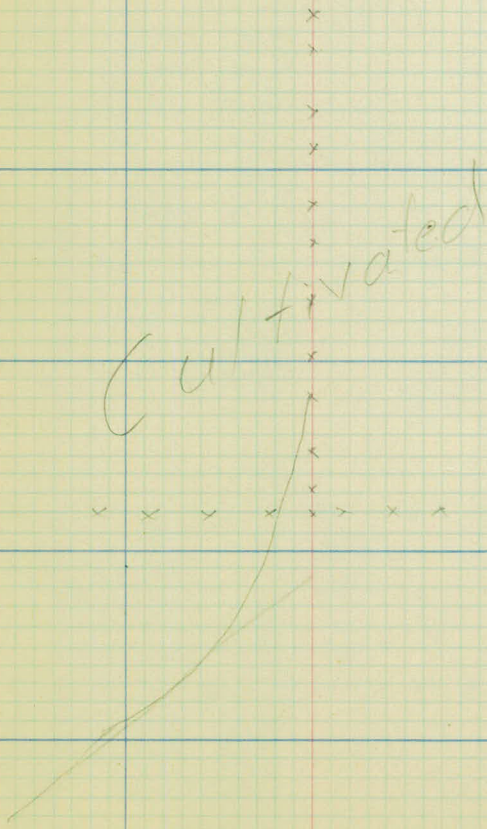
52

51

50

49

48


Cultivated

Project 24-02

"L"-"K" Line

Center Line Levels
and Cross Sections

Station	+	H.I	−	Elev.
B.M.	8.05	1057.68		1049.63
L-K- Line				
37				49.6
+40				49.4
38				49.6
39				55.3
T.P.	12.00	1069.42	0.26	1057.42
40				63.1
T.P.	10.06	1078.84	0.64	1068.78
41				71.4
+60				75.2
42				75.5
+55				71.1
43				68.8
+30				68.8
44				73.9

L Z R

Top of Rock 3770

W.H.C.
C.E.L.
M.S.A
T.F
} Feb 19.24

L	Z	R
11.4 / 33	8.1	7.7 / 1.5 — 6.7 / 2.0 — 4.8 / 33
12.0 / 33	2.3	6.1 / 33
9.5 / 33	8.1 / 6	5.5 / 33
4.4 / 33	2.4	0.0 / 33
8.5 / 33	6.3	5.6 / 33
8.0 / 33	7.4	6.6 / 33
3.5 / 33	3.6	3.7 / 33
2.7 / 33	3.8	5.2 / 33
3.0 / 33	7.7	11.7 / 33
6.5 / 33	10.6	13.5 / 33
6.8 / 33	10.0	12.4 / 33
2.0 / 33	4.9	3.5 / 33

Station	+	H.I	-	Elev.
		1078.84		
44+50				1075.3
H5				74.6
+65				72.1
H6				72.8
+55				73.6
H7				72.4
T.P	T.47	1087.41	0.90	1077.94
+50				73.3
H8				75.7
+60				78.9
H9				80.7
50				82.0
51				81.6

L.	&	R.
0.3 / 33	3.5	6.5 / 33
1.1 / 33	4.7	6.8 / 33
2.9 / 33	6.7	10.0 / 33
3.1 / 83	6.0	9.0 / 32
2.2 / 33	5.7	8.5 / 33
3.1 / 33	6.4	9.4 / 33
11.7 / 33	14.1	16.5 / 33
9.4 / 33	11.7	13.0 / 33
7.4 / 83	8.5	10.3 / 33
6.0 / 83	6.7	9.0 / 33
5.0 / 83	5.4	6.0 / 33
5.5 / 33	5.8	6.5 / 33

Sta	+	H.I	−	Elev	
		1087.41			
52				1080.4	
+88.65				1078.4	
B.M. for check.			6.90	1080.51	1080.46

L	℄	R
$7\frac{4}{33}$	7.0	$7\frac{5}{33}$
$8\frac{9}{33}$	9.0	$9\frac{8}{33}$

R.R. spike in corner Fence Post Sta 53+05 "A" Line.

Project 24-02

"L" "W" Line

Alignment Notes

W.H.C.
E.H.J.A.
N.S.E.
T.E. } 2/22/24

R.J.W Loc. Engr.

Station	Pt.	L	R.	
"L" W. Line.				
		73+78.9 "L" Line		
68+29.63	P.T.	23°-50'		20° C.L.
68		20°-52'		Δ 47°-40'
67		10°-52'		P.I. 67+18.5
66		0°-52'		S.T. 127.20
65+91.3	P.C.			L.C. 238.33
56+10	P.O.T.			
52+88.25	P.T.	16°-45'		10° C.R.
52		12°-20'		Δ 33°-30'
51		7°-20'		P.I. 51+25.9
50		2°-20'		S.T. 172.65
49+53.25	P.C.			C.L. 335.00
47+25.59	P.T.	6°-48'		
47		6°-25'		3° C.R.
46		4°-55'		Δ 13°-36'
45		3°-25'		P.I. 45+00
44		1°-55'		S.T. 227.74
43		0°-25'		C.L. 453.33
42+72.26	P.C.			

42+72.26 "L" Line

⊙ on Fence Line.

Project 24-02

"L"-W Line.

Center Line Levels & Cross-Sections.

W.H.C.
E.H.J.
M.S.A.
T.F.
} Feb. 22, 24

R.J.W. Loc. Engr.

Station	+	H.I	−	Elev.
	11.51	1040.98		1029.47
for check.			1.65	1039.33
42+72.76				1040.0
43				38.4
44				35.7
45				37.7
+50				31.0
46				31.0
47				31.4
48				32.1
49				36.0
+27				38.6
T.P.	9.44	1049.79	0.63	1040.35
49+53				
				40.5

Top stake Sta. 47 "L" Line. (Old T.P.)

" " " 43 " " "

	L	℄	R
	7.2/33	1.0	0.0/33
	4.3/33	2.6	1.3/33
	8.5/33	5.3	2.6/33
	10.8/33	3.3	6.0/33
	11.9/33	10.0	8.2/33
	11.4/33	10.0	7.8/33
	11.3/33	9.6	7.7/33
	1.3/33	8.9	7.0/33
	7.7/33	5.0	3.6/33
49+21 Fence E & W			
	5.5/33	?.4	0.0/33
Top of Rock 15' Rt 49+20			
	12.1/33	9.3	6.7/33

Station	+	H.I	−	Elev.
		1049.79		
50				1042.1
+50				43.2
51				44.8
+50				43.9
52				41.1
+50				38.8
53				39.1
54				40.8
+40				41.8
55				46.4
T.P.	10.06	1057.52	2.33	1047.46
+75				51.8
56				52.4
+70				52.1

L.	℄	R
10.8 / 33	7.7	4.7 / 33
9.6 / 33	6.6	3.7 / 33
8.8 / 33	5.0	2.0 / 33
10.1 / 33	5.9	2.5 / 33
12.2 / 33	8.7	5.3 / 33
12.9 / 33	11.0	8.2 / 33
12.9 / 33	10.7	8.4 / 33
9.6 / 33	9.0	8.3 / 33
8.4 / 33	8.0	7.1 / 33
3.3 / 33	3.4	3.5 / 33
Top of Stake 33		
Rd. 135' Lt. 6.6 / 33	5.7	6.0 / 33
6.7 / 33	5.1	5.0 / 33
7.2 / 33	5.4	4.8 / 33

Station	+	H.I	-	Elev.
		1057.52		
57				1051.4
+75				50.9
58				51.7
+15				51.7
59				52.5
60				53.0
+40				53.2
61				53.7
+45				54.0
62				54.1
T.P.	636	1061.68	2.20	1055.32
+50				56.3
63				56.2
+50				55.7

L	℄	R
7.4 / 33	6.1	4.0 / 33
7.3 / 33	6.6	5.8 / 33
7.3 / 33	6.3 / 10	5.8	5.3 / 10	5.8 / 33
6.8 / 33	5.8	5.1 / 15	4.8 / 33
Rd. 105' L. 3.8 / 105	5.0 / 33	5.0	4.6 / 15	4.6 / 33
3.6 / 33	4.5	5.6 / 33
3.5 / 33	4.3	5.6 / 33
3.7 / 33	3.8	5.4 / 33
1.7 / 33	2.0 / 20	3.5	5.7 / 33
Rd. 21' Lt. 2.3 / 33	2.5 / 21	3.4	3.5 / 33
Top of stake 62		
5.4 / 33	6.4	7.3 / 33
5.7 / 33	5.5	6.0 / 33
4.8 / 33	5.7 / 28	6.0	6.7 / 33

Station	+	H.I	−	Elev.
		1061.68		
64				1055.7
65				54.8
66				54.7
+50				55.2
67				56.0
+50				57.8
68				60.2
+29.6				
(Checking)				
B.M.	9.11	1057.55	13.24	1048.44
T.P.	12.70	1069.59	0.66	1056.89
	13.20	1082.52	0.27	1069.32
			3.6	1076.9 1078.9
B.M.			1.90	1080.62 1080.51

L.	Z	R
5.5 / 33	5.5 / 27 6.0 / 15 6.0	7.3 / 33
6.7 / 33	6.9	7.7 / 33
6.8 / 33	7.0	7.9 / 33
5.8 / 33	6.6	8.0 / 33
4.7 / 33	5.7	6.0 / 25 6.0 / 33
3.4 / 33	3.9	4.0 / 12 4.5 / 33
1.1 / 33 1.5 / 12	1.5	2.0 / 5 2.0 / 33

N.W. Corner
Top of 6"X6" Concrete Monument Sta. 67+83 "A" Line
@ Fence Corner

St. D around "A" Line

R.R. Spike in Corner F.P. Sta. 5370.5 "A" Line

Project 24-02

"Z" [illegible] Line.

Art. Topography.

W.H.C.
C.E.J.
M.S.A.
T.F.
Feb 22, 24

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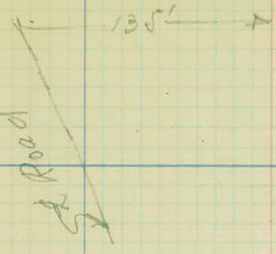

Continued.

+27 Fence Line E & W.

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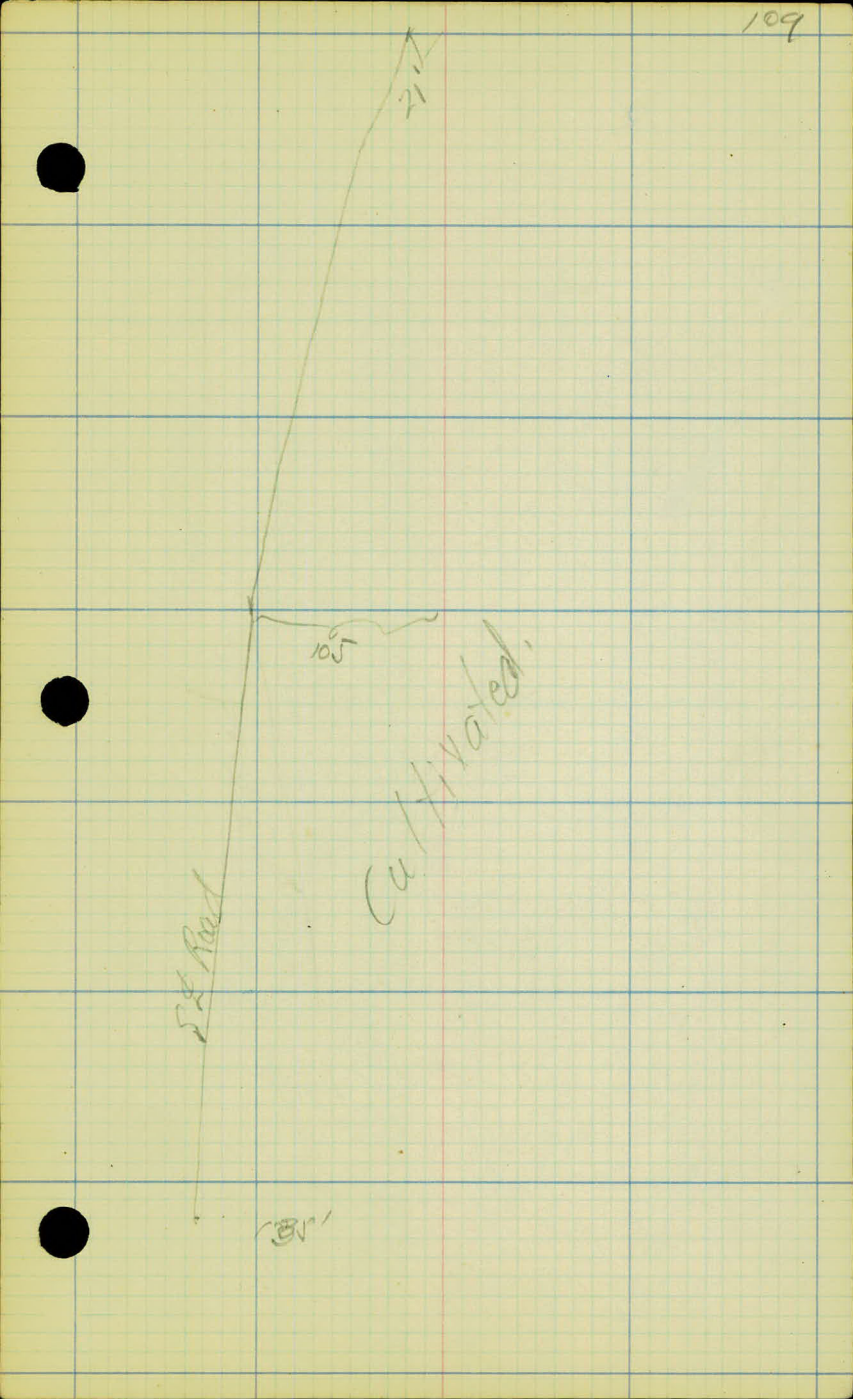

71'
105'
Cultivated.
52' Road
80'

68

67

66

65

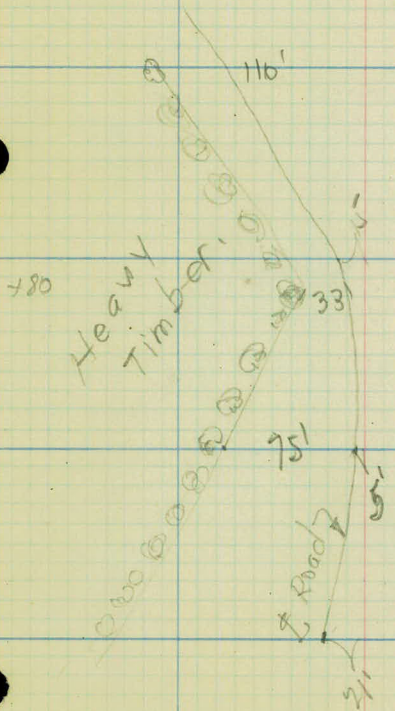
64

63

62

61

+40 8' Tree 18' R.
+30-6" " 21' R.



Check-Levels.

Proj 24-02

Station 53+05 to Station 141+05

"A" Line

	+	H.I	—	Elev.	
B.M.	3.02	1083.48		1080.46	
58			4.6	78.9	
T.P.	0.05	1074.41	9.12	1074.36	
T.P.	1.36	1063.71	12.06	1062.35	
T.P.	2.76	1054.97	11.50	1052.21	
66			4.3	50.7	
B.M.			6.68	1048.29	
T.P.	11.49	1063.73	2.73	1052.24	
73			5.9	57.8	
T.P.	11.91	1075.41	0.23	1063.50	
T.P.	3.32	1074.55	4.18	1071.23	
81			4.1	1070.2	
T.P.	11.54	1079.41	6.68	1067.87	
B.M.	8.55	1087.49	0.47	1078.94	1078.46
T.P.	2.04	1082.57	6.96	1080.53	
T.P.	0.44	1072.41	10.60	1071.97	
T.P.	2.22	1071.12	3.51	1068.90	
T.P.	0.49	1062.29	9.32	1061.80	
T.P.	4.23	1056.76	9.76	1052.53	
T.P	1.27	1048.89	9.14	1047.62	
C/d T.P.			0.85	1048.04	1047.04
B.M.			6.20	1042.69	1042.11
T.P.			9.06	1039.83	
	64.69		105.32	1080.46	
			64.69	1039.83	
(Over)			40.63 ✓	40.63 ✓	

W.H.C.
C.E.J.
M.S.A. } Feb. 23, 24
T.F.

R.R. spike in Cor. F.P. Sta. 53+05
Ground ℄

Ground ℄

Top of Mon: 67+83 ℄ Line

Ground ℄.

Top of Short F.P. @ corner by Mon.
Ground ℄
Top of Stake Sta 86
R.R. spike in 24" Tree Rt. 88+30
Top Stake Sta. 92

Top Stake Sta. 98

Nail in Tree @ Sta 101
Spike R.R. Rt. 105 + 80.

	+	H.I	−	Elev.	
	0.78	1040.61		1039.83	
T.P.	0.79	1032.75	8.65	1031.96	
T.P.	11.08	1042.06	1.77	1030.98	
T.P.	6.22	1047.91	0.37	1041.69	
T.P.	0.29	1037.47	10.73	1037.18	
T.P.	0.19	1027.50	10.16	1027.31	
T.P.	11.33	1028.33	10.50	1017.00	
T.P.	11.65	1039.68	0.30	1028.03	
B.M. (new)			7.86	31.82	
T.P.	11.79	1051.30	0.17	1039.51	
T.P.	11.70	1062.83	0.17	1051.13	
T.P.	4.30	1065.06	2.07	1060.76	
			1.61	1063.45	1062.76
	70.12		46.50	1063.45	
		70.12		1039.83	
		46.50			
		23.62		23.62	

T. Stake 16.

Top Rock. 120+35

Top of Conc. Mon. Sta. 132+09

Sp. Ke in 24" Oak 175' Lt. Sta. 138+00

24-02 R/W

#4201