

PLANS SURVEY
LEXINGTON AVENUE

From City Limits
To County Rd. "E"
CO. PROJ. 24-01
RD. % No. 3.

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

File Filed 12-28-23
"10"
File No.

ADJUSTED &
ALIGNMENT

LEXINGTON AVE.

Proj. 124-01

SECTION 3, T29, R23

R.M.

Nov. 25, 1980

$\Delta = 29-49-42$

NE Cor.

$\frac{1070.28}{N 22-43-47 W}$

---2859.67---
N 0-33-12 W

$\Delta = 16-26-13$

E 1/4 Cor.
Sec. 3-29-23

$\frac{470.67}{N 39-10 W}$

309.4

$\Delta = 39-10$

See Section folder

---2326.02---
North

SE Cor.
Sec. 3-29-23

NE Cor
Sec. 3-29-23

N 0-01-55 E

40.78

$\Delta = 30-45$

1141.32
N 30-46-55 E

$\Delta = 23-41$

• = 5/8" Rebar

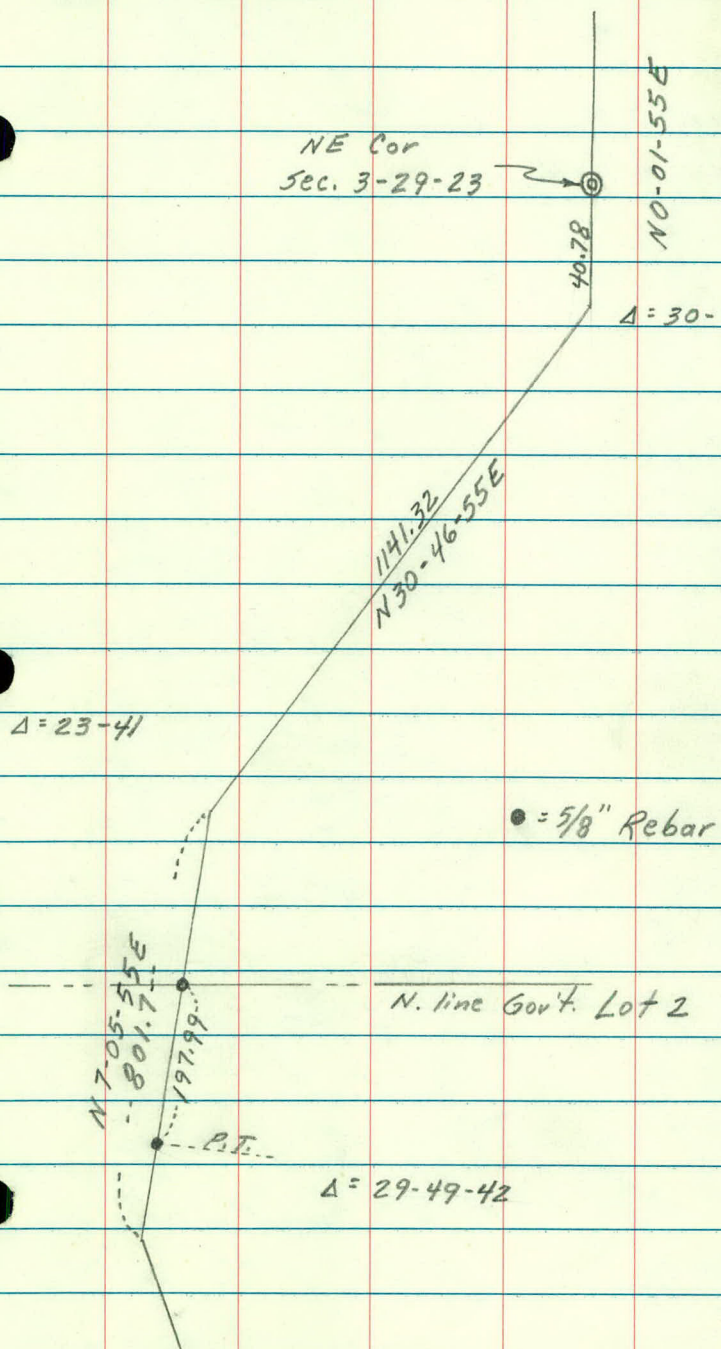
N. line Gov't. Lot 2

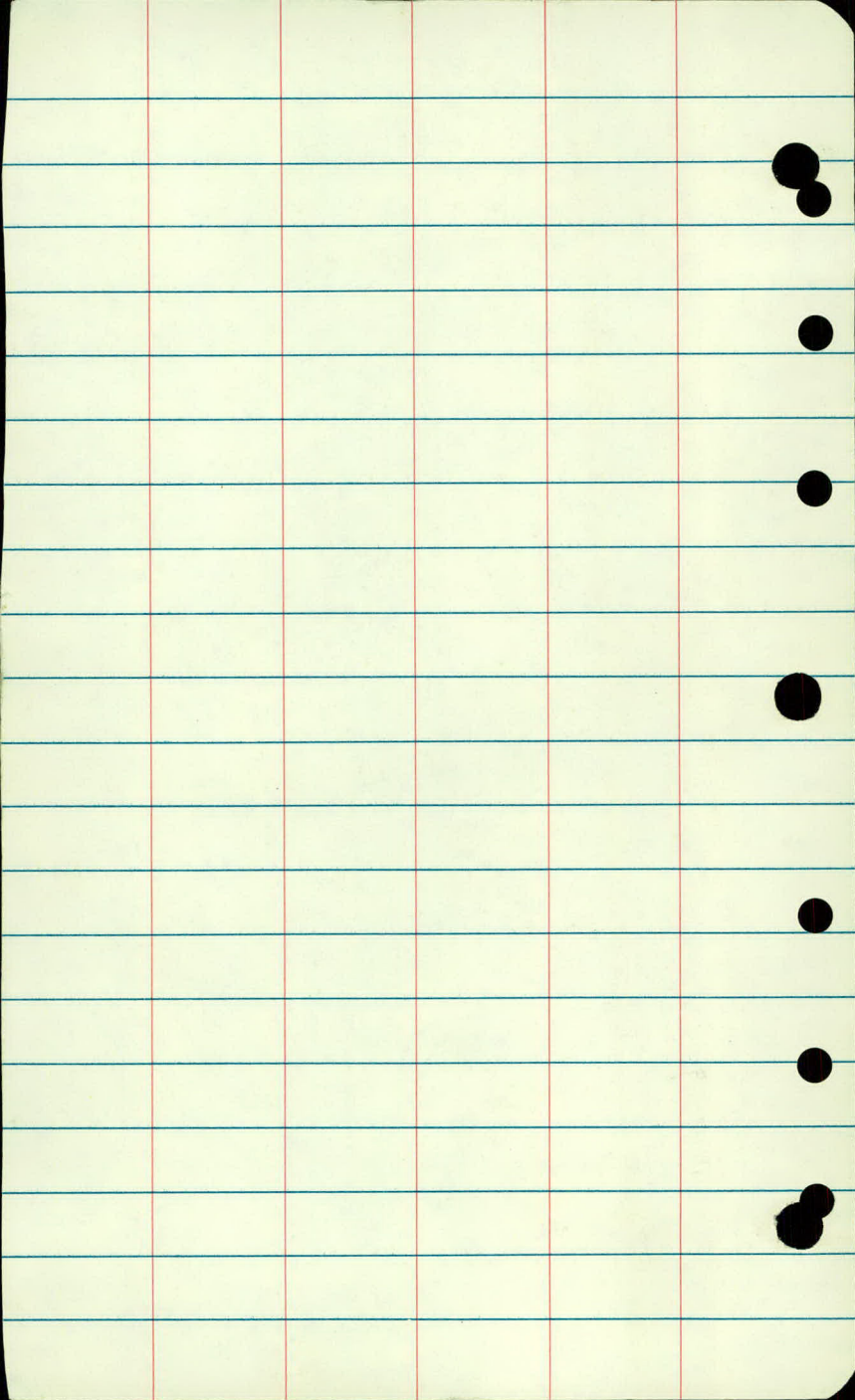
N 7-05-55 E
801.7

197.99

P.T.

$\Delta = 29-49-42$





24-01

Date Filed 12-28-23

Lexington Avenue "10"

	Page	to	Page
Alignment	1		10
Topography	11		50
Drainage	51		53
Levels & Cross-Sec.	54		91
Check Levels	92		94

Grade Separation

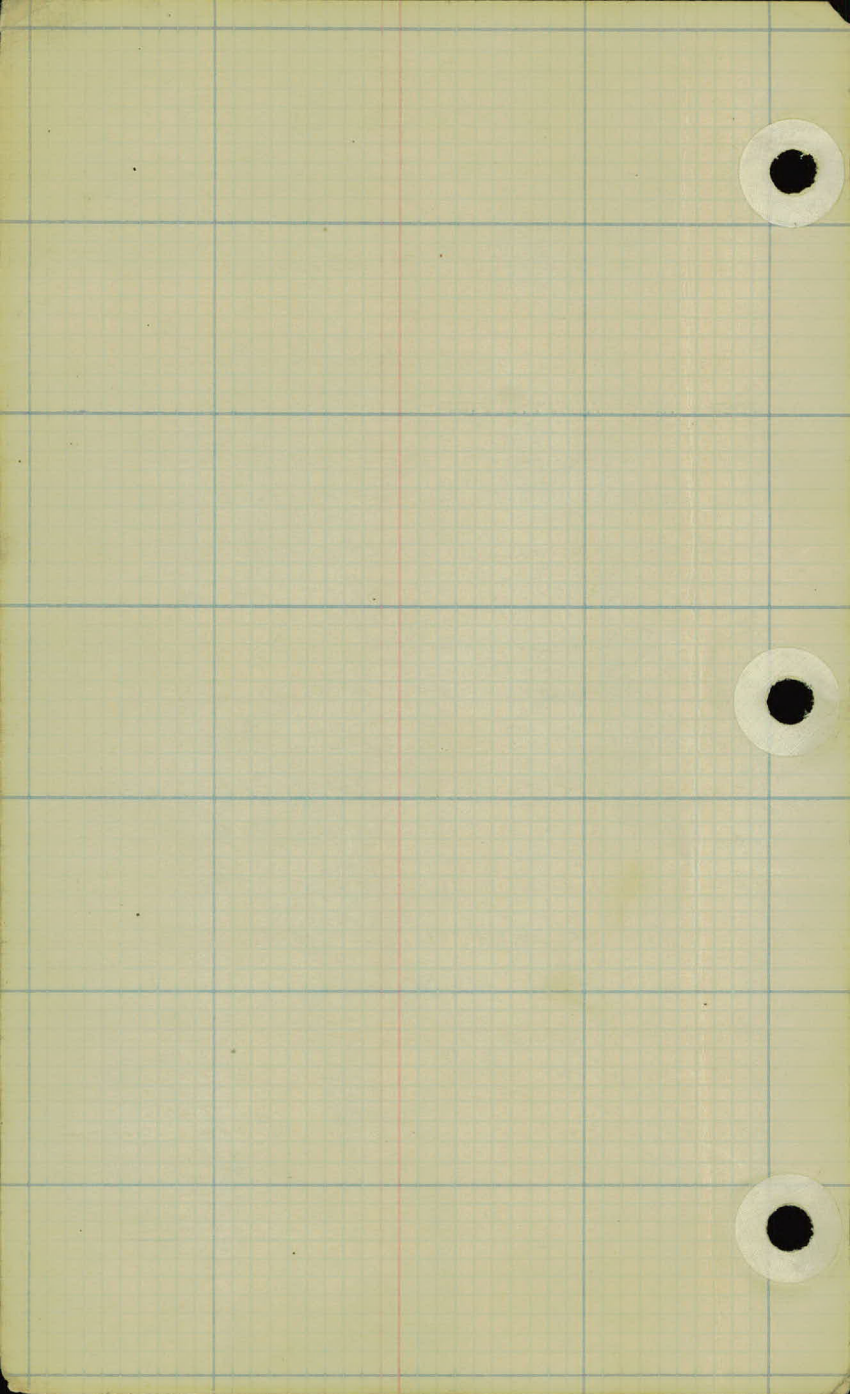
Run-around (Sta. 96 to 110)

Alignment	95		97
Topograph	98		101
Levels	102		104
Cross-Sections	105		109

Anoka Cut-off Connection

Sta. 0 to 8

Alignment	110		111
Topography	112		114
Levels	115		116
Cross-Sections	116		119



(1)

Proj. # 24-01

Lexington Ave.

Alignment Notes

Sta. Point Left Right.

Calc
Beating

66 + 12.0 P.O.T.

N 1°-18' W.

52 + 66.1 P.I. 0°-39' Mont. Δ 0°-39' L.

43 + 28.0 P.O.T.

N 0°-39' W.

26 + 39.55 P.I. 0°-39' Mont. Δ 0°-39' L.

15 + 83.4 P.O.T.

N 00°-00' E

0 + 00 Mont.

T. 29 N

15 14

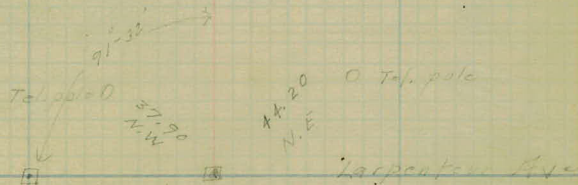
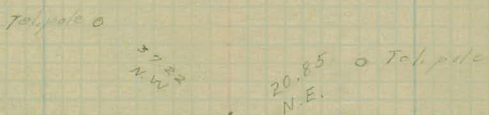
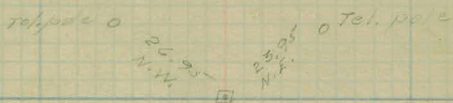
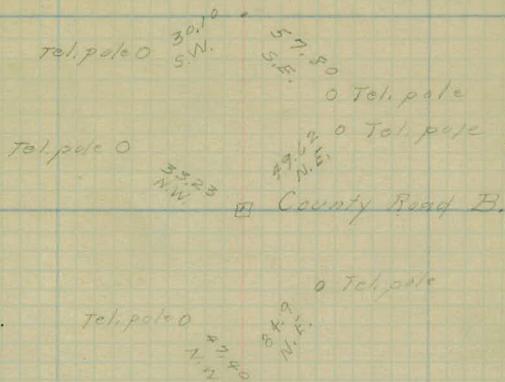
22 23

R. 23 W.

Cor. Carpentier & Lexington Aves.

P.C. Crane - Transit Proj. # 24-01
Simmons - Rodman Sept. 21, 1923
Althberg - Ranchman

(2)



Hamling

Sta. Point Left Right.

116 + 47.8 P.O.T.

111 + 86.8 P.O.T.

N⁰ - 56 W.

104 + 73.2 P.I. Mont. $0^{\circ} - 22'$ $\Delta 0^{\circ} - 22'$ R.

102 + 45.7 $\frac{1}{2}$ of N.P. Ry. Tracks

83 + 09.4 P.O.T.

78 + 72.1 P.O.T. Mont.

N¹ - 18 W.

Proj. # 24-01.

Lexington Ave.

Alignment from Sta. 78+92.1
to Sta. 215+71.6

$$\begin{array}{r} 104+73.2 \\ 102+45.7 \\ \hline 2 \quad 27.5 \end{array}$$

Sta.	Point	Left.	Right.	Calc Bearing
------	-------	-------	--------	-----------------

114+49.7	P.O.T.			
----------	--------	--	--	--

111+86.8	P.O.T.			
----------	--------	--	--	--

N 0°-56' W

104+73.2	P.E.	Ment	0°-22'	
----------	------	------	--------	--

102+45.7	q of	N.P. Ry. Tracks.		
----------	------	------------------	--	--

83+09.4	P.O.T.			
---------	--------	--	--	--

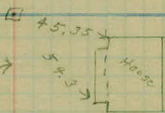
78+92.1	P.O.T.	Ment		N. 1°-18' W
---------	--------	------	--	-------------

30.9' @ 15" Tree

28.9' @ 4" Tree

34.1' @ T.P.

46.1' → STAIR



19.1' @ Tel. pole

Mail Box

@ Tel. pole

Tel. pole

31.1' N.W.

41.8' N.E.



5+9 Point Left Right

date
Bearing

N 23°-38' W

133 + 49.85 P.T.

8°-14'

133

5°-49 1/2' Δ 14°-28'

+682 P.T.

D. 10° R.

+50

3°-14 1/2' T. 83.02 ✓

132

0°-44 1/2' L. 109.07 ✓

131 + 85.18 P.C.

N 40°-00' W

+2536 P.T.

19°-35'

129

17°-33'

Δ 37°-10'

+50

13°-33'

D. 10° L.

+108.9 P.I.

T. 122.83 ✓

128

9°-33'

L. 249.77 ✓

+50

5°-33'

127

1°-33'

124 + 80.57 P.C.

N 0°-56' W

126 + 72.57 = 126 + 80.57 - P.C.

Tel. pole 15.3' P.I.

6.1'

12" Oak Tree 0

Mont.

30.7'

12.55' o Tel. pole

54.4'

Guy post for fence



Sta. Point Left. Right

Calc.
Bearing

N. 30°-1'E.

152+23.26 ✓ P.T.	11°-50 1/2'	
152+00	10°-24 1/2'	12° 0.
151+50	7°-24 1/2'	Δ 23°-41'
151+00	4°-24 1/2'	P.I. 151+26.8
150+50	1°-24 1/2'	S.T. 100.30 ✓
150+26.5 ✓ P.C.	0°-00'	L.C. 197.36 ✓

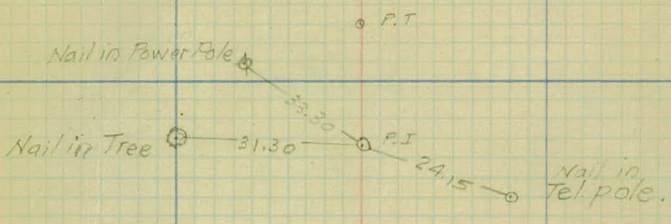
07 cut - 50' ch.

N. 6°-20'E

144+10.4 ✓ P.T.	14°-59'	
144	14°-01 1/2'	Δ 29°-55'
+50	9°-31 1/2'	D. 18° R.
143+29.7 P.I.		T. 85.54 ✓
143	5°-01 1/2'	L. 166.48 ✓
+50	0°-31 1/2'	15 cut 50' ch.

142+44.14 ✓ P.C.

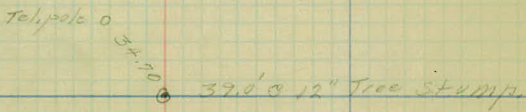
N. 35°-38' W.



P.T.

P.C.

W.H.C.
 P.C. Nov. 18, 23
 A.N.
 M.A.



○

○

Station Point Left Right Calc. Bearing

N. 0° 45' W.

175+69.8 P.O.T.

N. 0° 45' W.

162+39.45 ✓ P.T. 15° 20' 0"

20° C.

163+00 11° 25.8"

Δ 30° 45'

P.I. 162+64.88

162+50 6° 55.8"

S.T. 79.18 ✓

L.C. 153.25 ✓

162+00 1° 25.8"

0.19' cor. -50' ch.

161+15.7 ✓ P.C. 0° 00' 0"

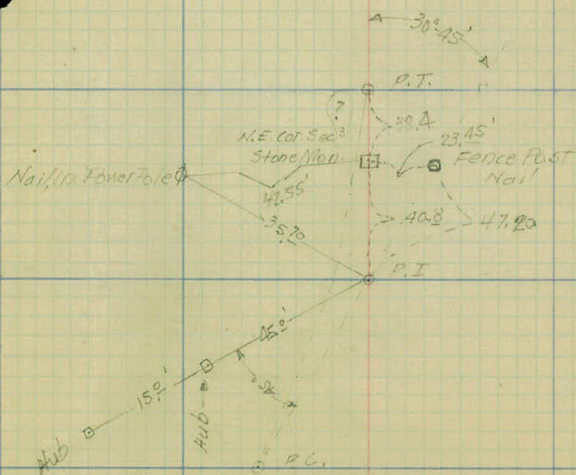
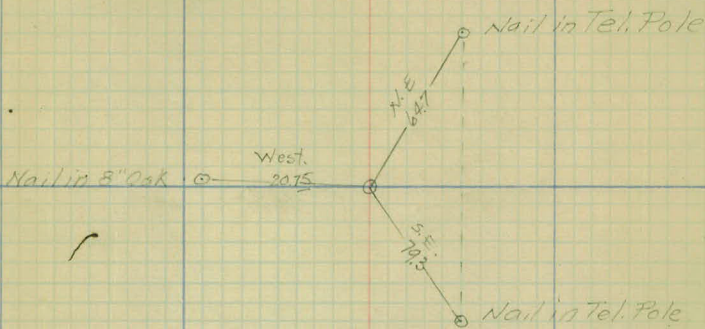
N. 30° 15' E.

W.H. Carlsson
 Paul Crane
 A. Nelson
 M. Alberg

Nov. 19-23
 Rod
 Ch. Fair & Clear.
 Ch.

Proj # 24-01

7



Station Point Left Right Calc. Bear.
N. 0° 56' W.

215+71.0 P.I. ^{Stone} Mon. 0° 11' NE. Cor. Sec. 34

N. 0° 45' W.

212+00 P.O.T.

N. 0° 45' W.

189+37.15 P.O.T. Pipe Mon. 1/4 Cor. bet Sec. 34-35

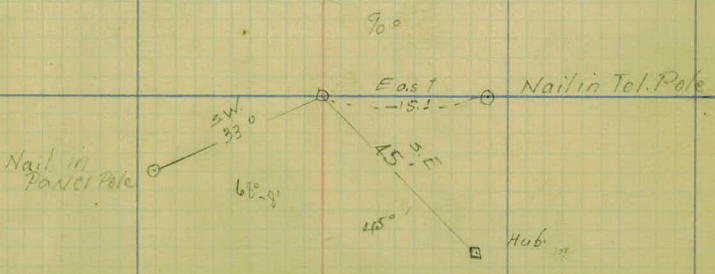
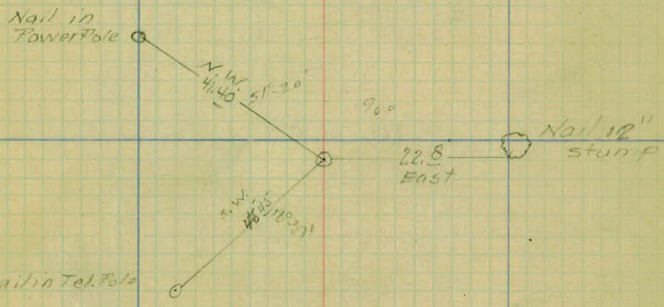
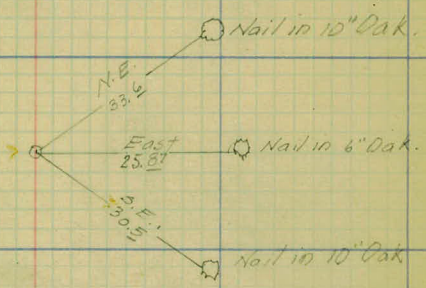
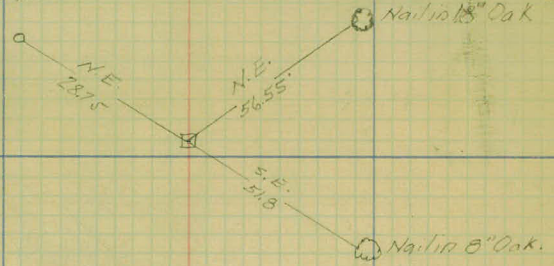
N. 0° 45' W.

182+31.7 P.O.T.

W.H.C. Fair & Clear
 P.O.
 A.N. Nov. 20, 23
 M.A.
 Nail in Guy
 Pole.

715) 27-01

8



Station Point Left Right

Calc
Bear

stone Mod 14 Col. bet Sec 26-27

218+848 S W.B. 50°

2187 6855 S.E.B. 70°

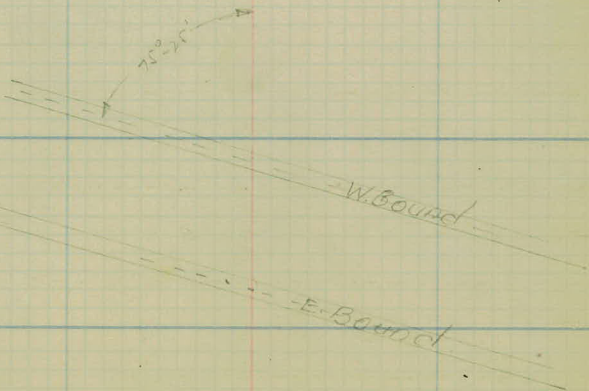
N. 0° 57' W.

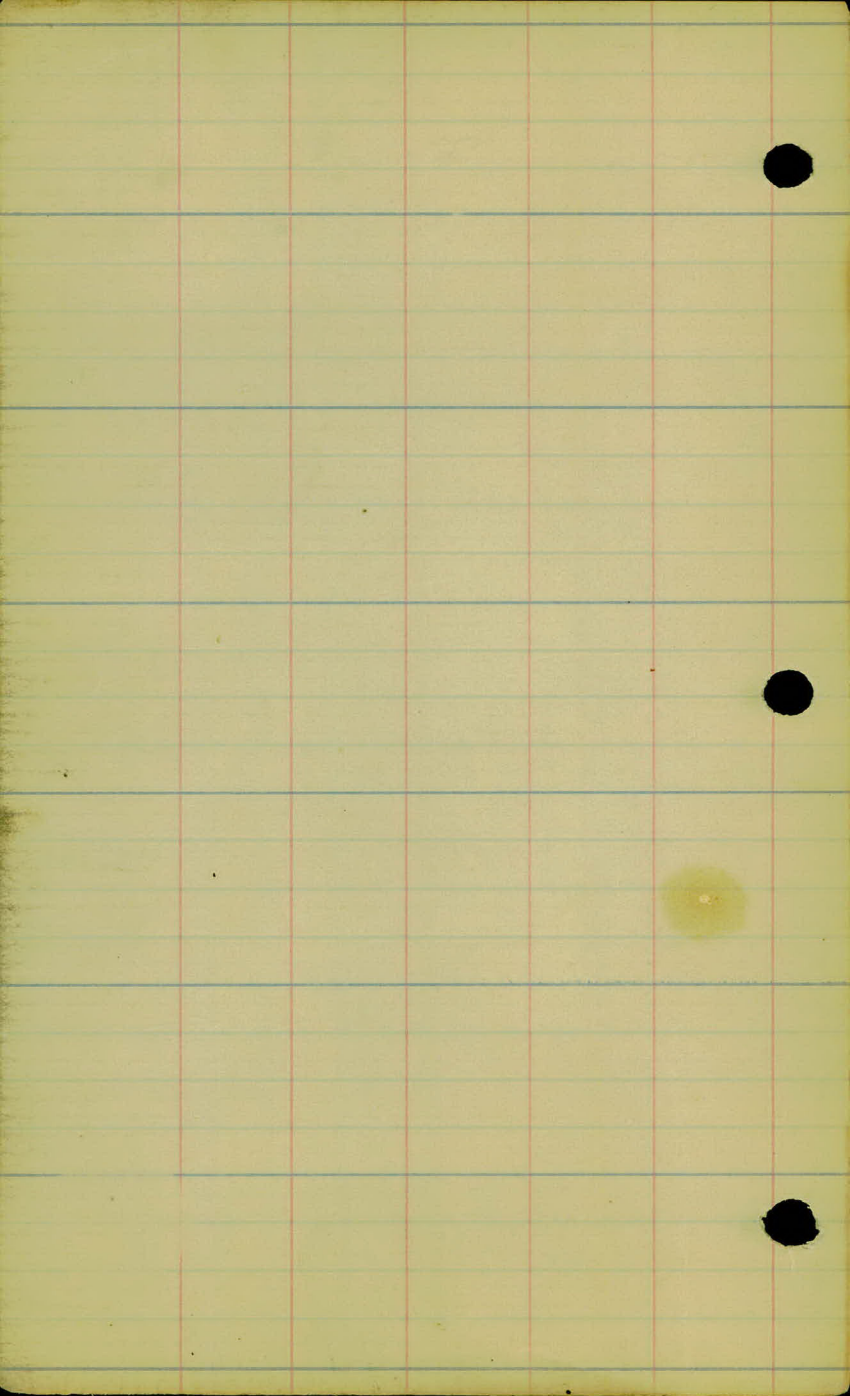
Nail in.
10" Oak Tie

N.W.
25.7

21.95'
S.W.

Nail in
Tel Pole





Lake Josephine

Lake

N. 6°-20' E

N. 33°-38' W

N. 30°-1' E

N. 40°-6' W

N. 1°-21' W

2640' ±

34

35

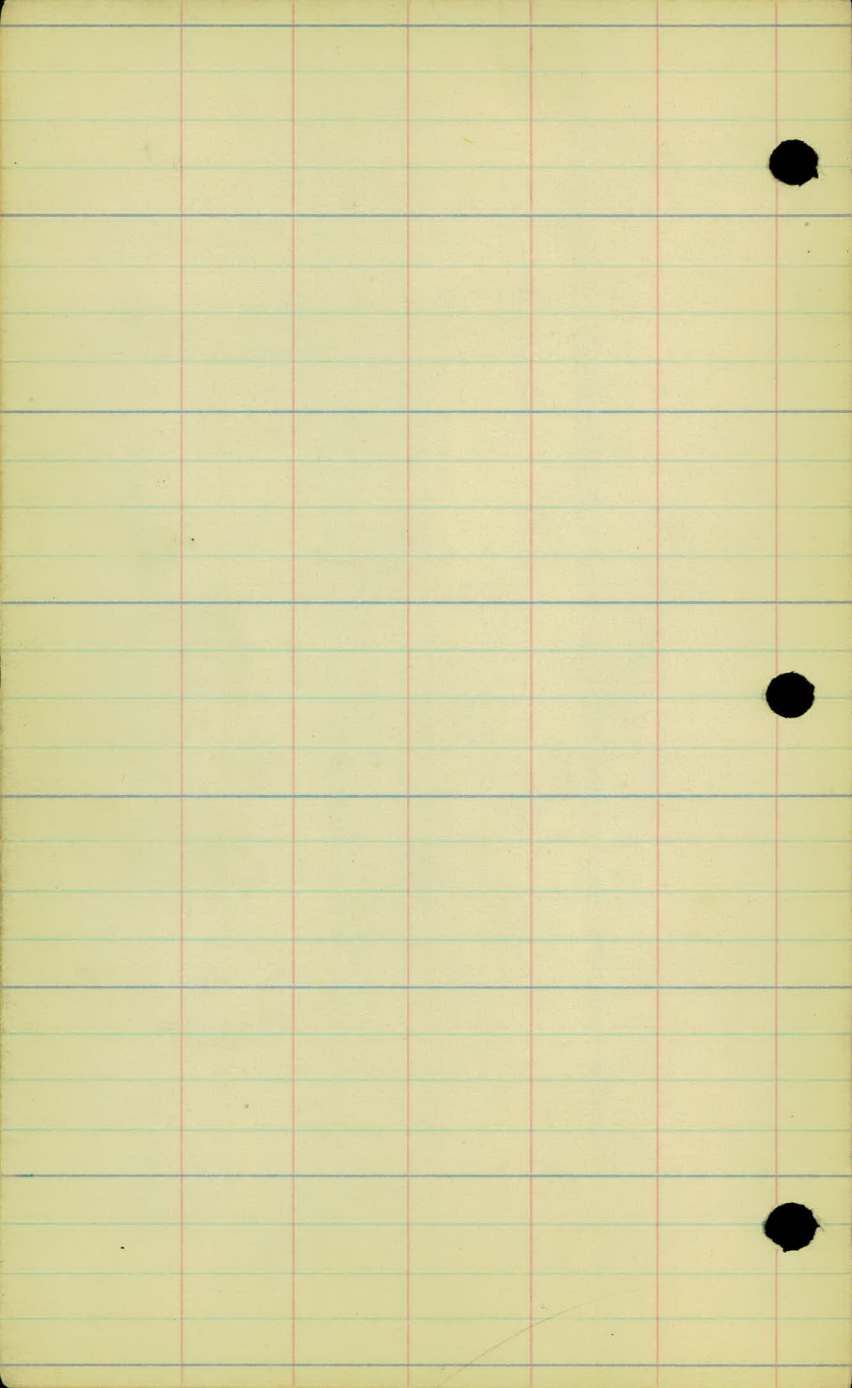
3

2

N. 0°-45' E
N. 0°-47' E

N. 0°-56' W





Art Topog.

Proj. # 24-01.

Lexington Ave

From Sta. 00 to Sta. 56+00

stan

4

3

2

1

0700

-1700

+41 24" Tree 30' L.

+46 T.P. 17' R.

+90 10" Tree 31.5 L.

+43 T.P. 15' L.

+43 P.P. 17.5' R.

+05 Beginning of Garden 35' L.

+14 T.P. 14' R.

+02 15" Tree 34' L.

Corn Field

+30 18" Tree 36' L.

+04 26" Tree 36' L.

+84 T.P. 15' R.

+80 P.P. 16' R.

+72 T.P. 17' L.

+54 Tree Stump 18' L.

+37 18" Tree 48' L.

+30 Iron Pole 19' L.

+27 Iron Road sign 19' L.

+24 Iron Road sign 27' L.

+21 T.P. 32' L.

+36 Sign post 27' R.

+30 T.P. 16' R.

+50 Beginning of Corn Field 25' R.

County Road A.

-62 Front of store 40' L.



Lexington Ave.

-20 T.P. 29' R.

-26 8" Tree 31' R.

-60 8" Tree 32' R.

-80 6" Tree 33' R.

-92 8" Tree 33' R.

stg,

9

8

7

6

5

4

+70 T.P. 16.5' R.

+14 19" Tree 34' L.

+61 T.P. 15.5' L.

+62 Beg. of Truck Bed 25' R.
+62 End of Corn Field 25' R.
+55 T.P. 16' R.

+39 P.P. 17' R.

+11 16" Tree 33' L.

+18 T.P. 16.5' R.

+86 T.P. 15' L.
+70 P.P. 17' R.

+47 15" Tree 34' L.

+87 T.P. 16.5' R.

+20 10" Tree 32' L.

+13 T.P. 14.5' L.

+07 P.P. 17' R.

Sta.

14

13

12

11

10

9

Garden

+227 11" Cor. I.P. 16' Long 16' R.
+21 T.P. 17' R.

Garden

+71 T.P. 15' L.

+88 P.P. 18' R.

+56 Mail Box 15' R.
+25 R. 10" Cor. I.P. 16' Long
+42 End of P. Ent 10' W.

+66 Beg of Garden

+12 End of Garden

+718" Tree 34' L.

+77 T.P. 19' R.

16" Vit. Col. 30' Long 20' L.
+48 12" Tree 34' L.
+38 Fawn Post, 12' Wide
+30 12" Tree 34' L.
12" Tree 35' L.
T.P. 15.5' L.

+57 T.P. 18' R.

+58 Mail Box 11.5' R.

+91 P.P. 17.5' R.

+26 14" Tree 34' L.

+27 T.P. 16.5' R.

Garden

+32 15" Tree, 34' L.
+30 T.P. 15.5' L.

+64 P.P. 17.5' R.

Sta.

20

19

18

17

16

15

14

Carfield

+07 T.P. 16' L.

+65 T.P. 16' R.

+34 P.P. 18' R.

Garden

+90 T.P. 15' L.

+96 T.P. 16.5' R.

+62 P.P. 18' R.

Garden

+118 Sign Post 30' R.

+16 T.P. 17' R.

+10 18' Tree 36' R.

+30 8" Tree 37' R.

+46 P. Ent. 12' Wide

+17 T.P. 15' L.

+21 Mail Box 17' R.

+99 P.P. 19' R.

+45 T.P. 17' R.

+36 T.P. 18' R.

+34 Mail Box 14' R.

+95 T.P. 16' L.

12" Con. I.P. 32' Long 15' R.
+21 F. Ent. 12' Wide

Sta.

26

25

24

23

22

21

20

+93 P.P. 16' R.

+77 T.P. 15.5' L.

+77 T.P. 17' R.

+54 +12" C.I.P. 37.4 Long.

Corn Field

+21 P.P. 17' R.

+06 T.P. 15.5' L.

+07 T.P. 16' R.

+56 T.P. 17.5' R.

+33 T.P. 16' L.

+37 T.P. 15' R.

Carden

+92 P.P. 17' R.

o

+56 Cross Drain 12" C.I.P. 37.2 Long

sta.

32

31

30

29

28

27

26

+69 T.P. 17.5' L.

+94 P.P. 17' R.

+97 T.P. 14' L.

+67 End of fence

+25 P.P. 17' R.

+24 T.P. 13.5' L.

Plough field

Fence Pasture Garden

+62 P.P. 16.3' R.

+66 T.P. 14.5' L.

+39.5 Cross Rd.

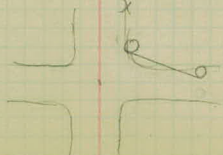
+26 T.P. 45.5' L.

+25 Guy Wire 25' L.

+58 T.P. 14' R.

+45 Guy Wire 35' R.

+44 P.P. 53.5' R.



579

38

37

36

35

34

33

32

+30 P.P. 17' R.

+84 T.P. 14' L.

12" Cor. I.P. 16' Long 15' L.
+23 Pri. Ent. L. 10' wide

Cult. Field

Cult. Field

+65 P.P. 17' R.

12" Cor. I.P. 19' Long 16' L.
+35 Pri. Ent. L.

+88 T.P. 14' L.

12" Cor. I.P. 16' Long 14.5' L.

+74 Pri. Ent. L. 10' Wide

+77 Mail Box 15' L.

+96 Mail Box 15' L.

12" Cor. 20' Long 15.5' R.
+13 Pri. Ent. R. 10' Wide12" Cor. I.P. 20' Long 15' R.
+67 Pri. Ent. R. 10' Wide

+13 P.P. 17' R.

+41 T.P. 14' L.

Plough Field

LAWN

+64 P.P. 17.5' R.

+13 Mail Box 10' L.

12" Cor. I.P. 26' Long 15.5' R.
Pri. Ent. 10' Wide

Sta.

44

43

42

41

40

39

38

+74 T.P. 13' L.

Cult. Field

+26 Mail Box 115' L.

Pasture Field

+58 Mail Box 115' L.

1. 12" C.I.P. 16' Long 16' R.
+69 Pri. Ent. R.

+74 P.P. 17' R.

+99 T.P. 125' L.

+29 T.P. 125' L.

Pasture

+75 P.P. 17.5' R.

+36 Mail Box 11' L.

side Walk
+34 12" C.I.P. 4' Long 17' R.
12" C.I.P. 20' Long 19.5' R.
+07 Pri. Ent. R. 10' Wide
+95 P.P. 17.5' R.

+50 T.P. 125' L.

Cult Field

Pasture

sta.

50

49

48

47

46

45

44

+15 Goy P. 16' L.

+97 T.P. 14.5' L.

Cult. field

Pasture

+15 P.P. 17' R.

+35

+25 T.P. 14' L.
12" C.I.P. 16' Long 14' L.
Pr. Ent L. 10 Wide

59
23
10
10
10

+52 P.P. 17' R.

+28

16

+30 P.P. 17.5' R.

+72 Iron Sign post 16'

+55 T.P. 13' L.

Cult. field

Pasture

+12 P.P. 17.5' R.

sta.

56

55

54

53

52

51

50

+97 P.P. 28' L.



+84 T.P. 17 1/2' R.
27' R. Fence

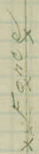
+80 P.P. 29' L.

+77 Mail Box 15' L.

+42 Sign 23' R.
+28 Pri Ent 15' Wide

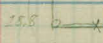
+66 P.P. 29' L.
+49 Guy Wire 30' L.

Cul. Field



+89 Sign Post 19' R.
+32 Guy Wire 18' R.
+3 R.P. 12' R.

+75 Iron Rd Sign 19' L.
+85 P.P. 24'5" R.P.L.
+66.1



+92 Beginning of Run
+92 Iron Rd 21' 3/4

Co. Rd. B.

+20 Mail Box 14' L.
+17 14' Tree 34' L.
+10 6" Tree 34' L.
+83 T.P. 15' L.
+75 14' Tree 34' L.

+41 T.P. 16' R.
+11 R.P. 17' R.

Garden

+68 T.P. 16' L.
+46 Mail Box 14' L.

Cul. Field

+83 P.P. 17'5" R.
12" C.I.P. 4' Long 10' R.
+46 Side Walk

+23 Pri. Ent. R. 10' Wide

62

61

60

59

58

57

56

Proj. # 24-01.

Lexington Ave.

Art Topog from Sta.
56+00 to Sta. 218

62

61

60

59

58

57

54

68

67

66

65

64

63

62

+10 12" Culvert.

74

73

72

71

70

69

68

240 265

+15 P.P. 18' L.

+96 18" Tree 32' R.

Col. Field

+39 T.P. 13.5' R.
+21 30" Tree 32' R.

+71 P.P. 18' L.

+10 18" Tree 31' R.
10" Vit 20' Long 19.5' R.
+77 Pri Ent. 10' Wide

+24 End of Fence 17.

+41 20" Tree 26.5'
12" C.I.P. 18' Long 19' R.
+19 Pri Ent R.
+09 End of Fence 35

+89 Mail Box 11.5' L.

+78 T.P. 16' R.

+31 Fence 19.5'
+24 P.P. 18' L.

12" C.I.P. 20' Long 17.5' L.
+89 Pri Ent. 12' Wide

+62 Mail Box 10.5' L.

+09 T.P. 16' R.
+06 Beginning of F 34.5'
12" C.I.P. 20' Long 20' R.
+94 Pri Ent. 10' Wide

+51 Mail Box 12' L.
+79 P.P. 27.8' L.

80

79

78

77

76

75

74

+57 10" Tree 33 L.
 +35 12" Stump 38 L.
 +30 Nail Box 11, 1 L.
 +19 16" Tree 38 L.
 +04 P.P. 28 L.
 12" C.I.P. 26 Long 15 L.
 +87 Pri. Ent 15 Wide

+29 T.P. 19.5 R.
 +19 Guy Wire 19.5

+82 Sign Post 29 R.

+31 Sign Post 29.5 R.
 12" C.I.P. 12 Long 12 R.
 +22 Farm Ent 16 Wide

+03 14" Tree 24.5 L.
 +82 12" Tree 27 L.
 12" C.I.P. 18 Long 12 L.
 +72 P.C. Ent 10 Wide
 +62 10" Tree 26 L.
 +61 8" Tree 25.5 L.
 +53 P.P. 28 L.

+29 T.P. 17.5 R.

+16 P.P. 2.5 L.

+10 P.P. 17.5 R.

+67 Mail Box 10.5 L.

+72 T.P. 14.5 R.

+58 Farm Ent 10 Wide

+27 6" Tree 29.5 L.

+80 6" Tree 26.5 L.

+64 P.P. 28 L.

Pasture

Old Field

+09 T.P. 13 R.

84

85

84

83

82

81

80

+57 T.P. 19.5 R.

+30 T.P. 19.5 R.

+54 Mail Box 113 L.

12' C.I.P. 20' Long 16' R.
+65 P.I. Ent 15' Wide

+04 T.P. 19.6 R.

+54 Mail Box 115 L.

+50 P.I. Ent 10' Wide

+11 Guy Wire 24 R.

+78 P.P. 29.5 R.
End of Power Line

+31 T.P. 19.1 R.

Cul. Field

+07 P.I. Ent 10' Wide

+37 Mail Box 114 L.

+54 P.P. 28 L.

+53 T.P. 19 L.

92

91

90

89

88

87

86

+66 P.P. 10' L
 +47 Guy Wire = 10' L

+84 T.P. 15.5 R

+60 P.P. 15' R

Hay Field

+62 T.P. 16.5 R

+01 30' Tree 32.5 R

Hay Field

+54 10' 8" Tree 26.5 R

+37 T.P. 17.5 R

+39 30' Tree 32.5 R

+28 30' Tree 31 R

+54 Farm End
 12" V.L.C. 18' Long 19.5' R

+11 T.P. 15' R

Cul Field

Cul Field

+24 T.P. 17.5 R

98

97

96

95

94

93

92

Lake

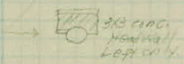
+93 T.P. 13.5 R.

+47 P.P. 13' L.

12" Cor. Cyl. 24" Long 38" h.
+23 Pri Ent 10' Wide

+73 Mail Box 13' L.
+X+ Concrete Mail Wall L.
+20 15" Cor. T.P. 42' Long

+61 T.P. 14" R.



+01 P.P. 13' L.
+7+ Mail Box 12.4' L.

+10 12" Tree 25' L.
+06 12" Tree 27' L.
12" C.I.P.H. Long 21.5 R.
+96 Pri Ent 10' Wide

+57 24" Tree 35' L.
+57 Sign 31' L.

+36 T.P. 14.5 R.

+77 12" Tree 30' L.
+76 12" Tree 30' L.

+46 2 10" Trees 27' L.
+34 P.P. 11.5' L.

+16 14" tree 29' L.
+06 8" Tree 27' L.

+12 T.P. 15" R.

+12 10" Tree 30' L.

+95 11" Tree 22' L.
+96 10" Tree 25' L.

Cul. Field

Hay Field

+25 Over Road Power Line

104

103

+79 15" CIV.

102

101

100

99

78

+99 8" Tree 16' R

+92 Guy Wire 17' R

+98 T.P. 14.5' R

+87 Guy Wire 25' R

✓ +87 Guy Pole 15.5' L

✓ +61 Sign Board 13' R

+45.7 Cattle Guard 33' L

+36 Battery Top 17' R

✓ +34 X Signal 10.5' R

+98 Guy Pole 15' L

+87 P.P. 13' L ✓

10 3x3 Planks 16 Long

+45.7 Cattle Guard 33' L

+45.7

+33 X Sign 13' L ✓



+77 Guy Wire 25' L

+77 Guy Pole 13.5' L

+59 P.P. 12.5' L ✓

+49 Guy Wire 11.5' L

✓ +97 T.P. 15' R

+74 Guy Wire 15' R

+40 T.P. 15' R

+60 Guy Wire 23' R

✓ +75 T.P. 13.5' R

+74 P.P. 13' L ✓

✓ +44 T.P. 13.5' R

Lake

+56 Sign Board 35' L

+31 P.P. 13' L ✓

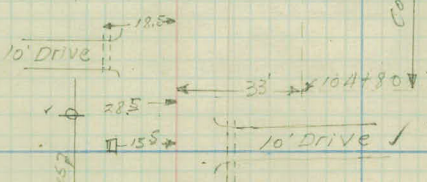
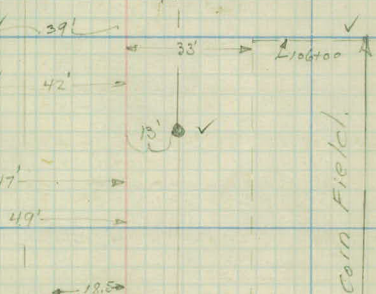
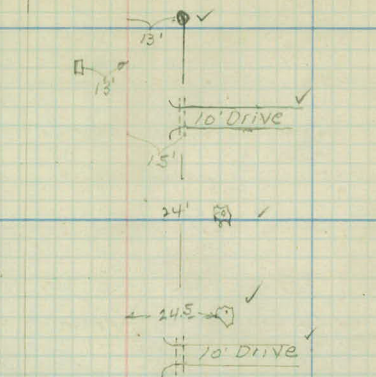
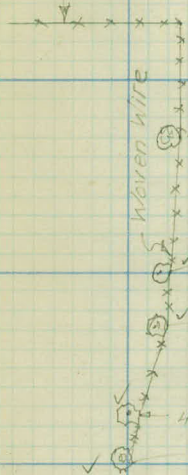
✓ +18 T.P. 13.5' R

- 107 +85 Power Pole. L.
 +75 Bill Board. R.
 107 Fence Corner R.
 +85 Tel Pole R.
 +59 Mail Box L.
 +57 Priv Ent. R., 12" C.M. culv. 16' lq.
 +37 Fence Corner L.
 107 +35 4" Tree R.
 +18 30" Tree L.
 +16 4" Tree R.
 +06 Priv Ent. R., 12" Cor. M. culv. 16' lq.
 106 Tree L.
 +76 12" Tree L.
 +56 Tel. Pole. R.
 +52 14" Tree L.
 105 +37 12" Tree L.
 105
 +26 Priv Ent., 12" Cor. M. culv. 20' lq. L.
 +73 Power Pole L.
 104 +71 Priv Ent. & Mail Box - 12" Cor. M. culv. 14' lq.
 +66 Mail Box L.
 +62 Mail Box L.
 +59 6" Tree R.
 104 +49 4" Conc. Walk, 12" Cor. M. culv. 4' lq.
 +41 6" Tree R.
 +23 6" Tree R.
 +20 Tel. Pole R.

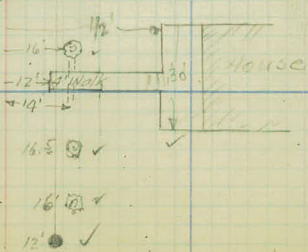
104

Survey here Nov 27, 1923

Cornfield.



Power Wires

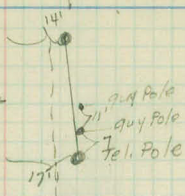
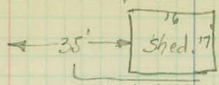


Corn Field.

- 114+46 Beg of Grove of Trees Right.
- 114 +43 Bldg. (Shed) R.
- 114 +33 Priv Ent. R
- +91 Tel. pole
- 112 Fence Corner
- +92 Tel. Pole R.
- +89 Stump L.
- 112+23 E Co. Road @ C.
- 112+05 Tel. Pole R.
- +92 Tel. Pole R.
- +87 Iron Road Sign. L.
- +77 Power Pole L.
- +68 s. end of Gas pump platform. R.
- 111+28 Tel. Pole R.
- +82 Power Pole L.
- +66 Fence corner s end of trees R.
- +62 Tel. Pole R.
- 110+05 Sign Post R.
- +52 Beg. of cluster of trees & stumps. R.
- +40 Tel. Pole R.
- +38 Power Pole L.
- 109+00 Fence R.
- +98 End of Grove R.
- +68 Beg of Grove of Trees & Stumps. R.
- +13 Tel. Pole R.
- 108 Fence R

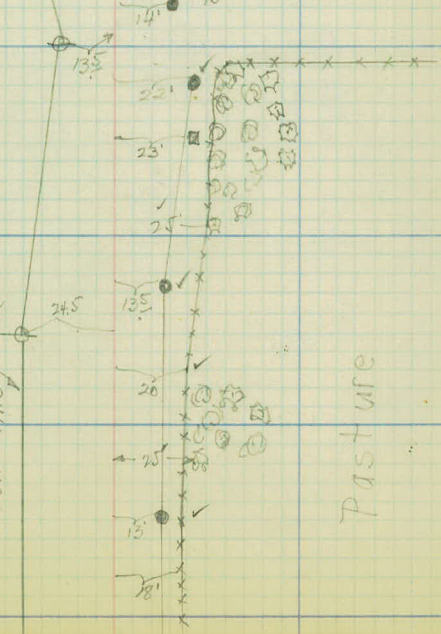
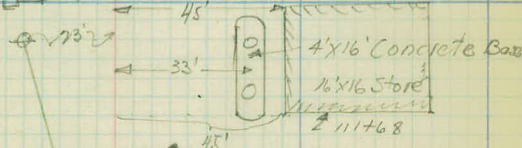
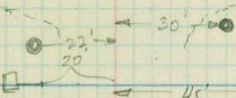
Scattered
Timber
Pasture

36" Woven Wire Samba Wires



County

Road (E) C.



Cultivated

Power line

Pasture

122+00

+75 Fence Corner Right

+60 Tel. Pole Right.

121+00 Fence L.

20+35 Tel. Pole R.

118+22 End of Grove Right

117+77 Tel. Pole R.

117+23 End of Timber left

+50 Tel. Pole R.

116

+64 Beg. of Fence R.

115+44 End of Fence R.

115+18 Tel. Pole R.

114+85 Beg Woven Wire Fence R.

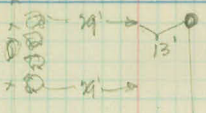
Pasture
Scattered Timber



Woven Wire

Barb Wire

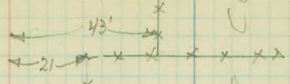
5 Trees
+56
+41



34'



31'



Pasture

Cultive-
Ted
↑

- 129+25 P.T. + Fence L.
+96 Tel. pole R.
128+00 Tel. Pole R.
127+67 Fence L.
127+42 Fence Corner L.
127+04 Tel. Pole R.
126+80.57 P.C.
+69 Side Drain R. 12" Cor. M. Culv. 10/9,
126+50
+49 Sign Board R.

+52 Tel. Pole R.

+30 End of Fence R.

125+00

+12 Tel. Pole R.
124

+18 Sign Board R.
123+00
122+84 Tel. Pole R.
+32 Sign Board R.
122+06 Tree left.

134

133+49.8 P.T.

132 Fence L.

+70 Tel. Pole R.

132+50 Fence L.

+15 12" tree L.

132 Fence corner L.

131+85 P.C.

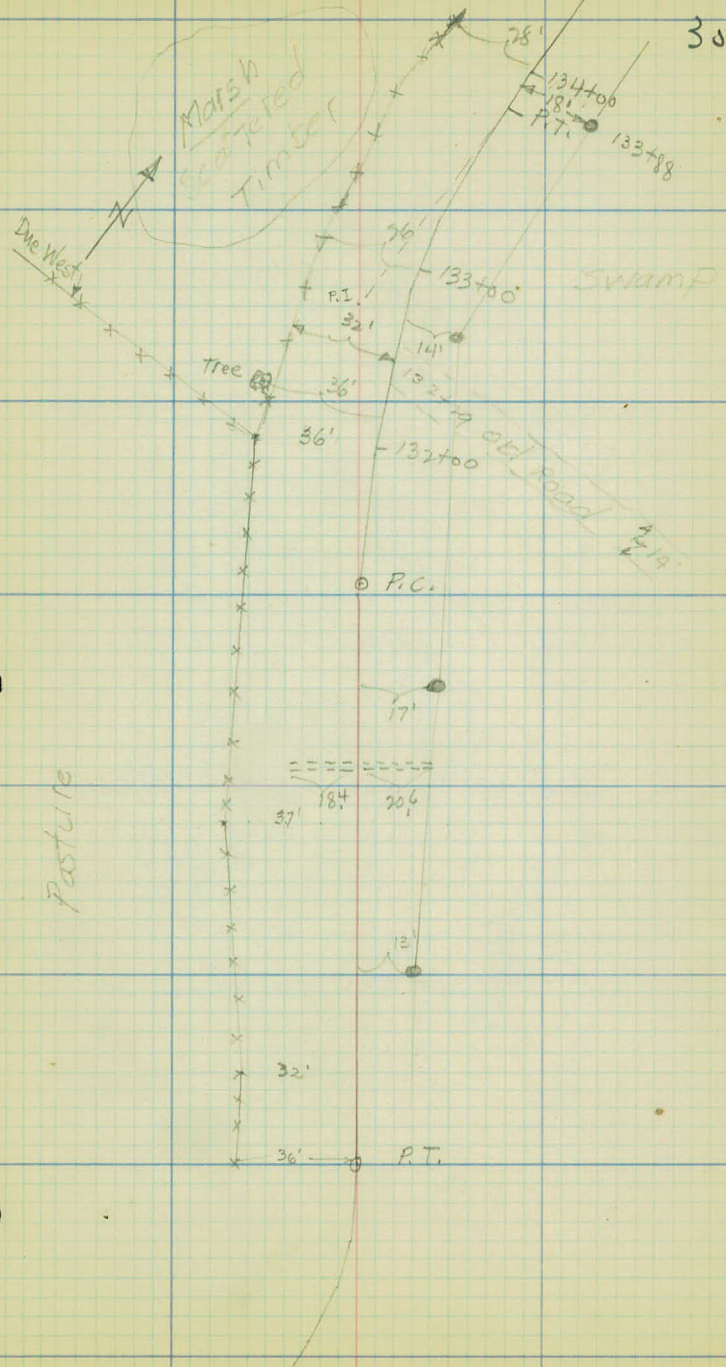
131+53 Tel. Pole R.

+39 12" Culv.

131 Fence L.

130+73 Tel. Pole R.

129+56 Fence left.



140

+95

2- 10" Trees L.

139

+87 Tel. Pole R.

138

+59

Tel. Pole R.

137+00

Fence L.

136+36

Tel. Pole R.

136

135+08

Tel. Pole R.

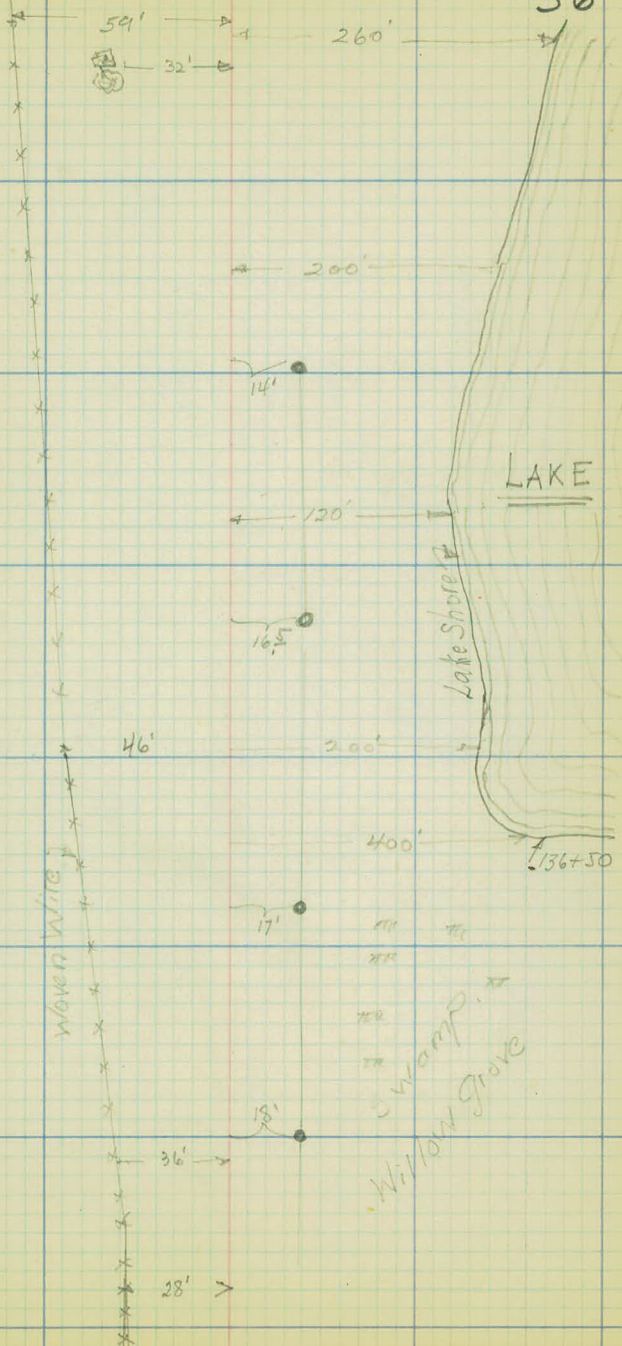
135

Fence L.

134+00

Fence L.

Timber



144+00

+97 Tel. Pole R.

+59 Power Pole L.

143

+75 Tel. Pole R.

142+44.5 P.C.

+35 Mail Box L.

²⁰³
142+00 12" Culvert

141+44 Tel Pole R.

141+40 Int of Road.

141+00

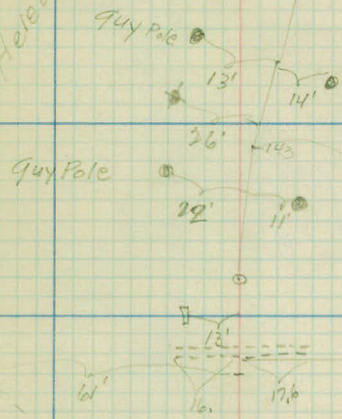
140+70 End of Bill Board

+26 Sign Board L.

140

Scattered Oaks

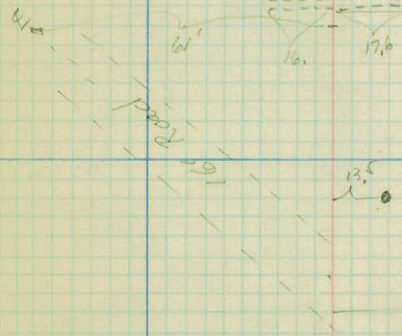
144+1064 P.T.



235'

258'

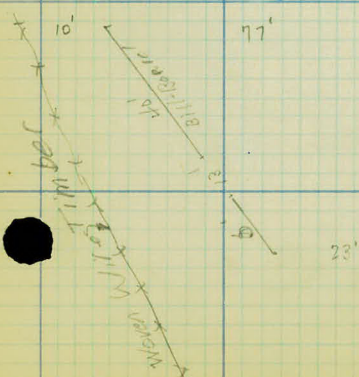
250'



Nat's h.

260'

Lake



77'

23'

260'

149792

149762 Fence cor.

+50

149700

+72 Tel. Pole R.

+28 Power Pole L.

148

139 Tel. Pole R.

147

+91 Power Pole L.

146 +72⁵ Culvert 18"

146 +71 Culvert 18"

+24 Tel. Pole R.

146 Lake L & R.

+70 Power Pole L.

+06 Tel. Pole R.

145

152723.86 P.T.

152702 Fence L.

151 + 52 Power Pole L.

+ 17 Tel. Pole

151

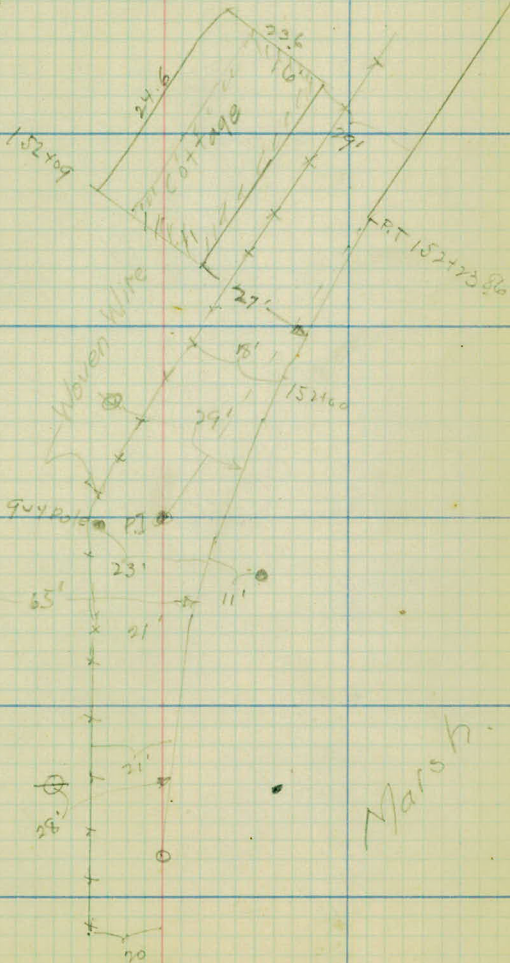
+ 50 Fence

+ 30 Power Pole

+ 26

150700 Fence L.

Lake Josephine



Marsh

156+14 Tel. Pole R.

156+00 End of fence

155 +84 Fence

155 +68 Priv Ent L. 12" C.M. culv 26' Lg

+53 Fence Cor. L.

+14 Priv Ent R. 12" C.M. culv. 16' Lg.

155+00 Fence L.

+98 Power Pole L.

+86 Tel Pole R.

154+11

12" C.M. culv 4' Lg.

153 +81

Steps. 12" C.M. culv 4' Lg.

+68 Tel. Pole R.

153+13 Power Pole L

+01 Store R.

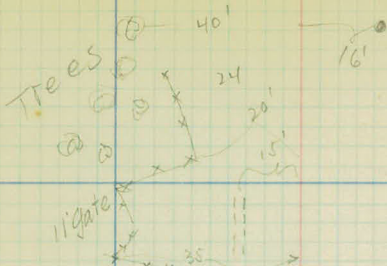
153+00 Fence L.

+65 Fence Cor. L.

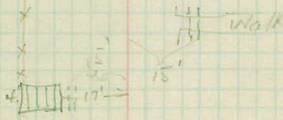
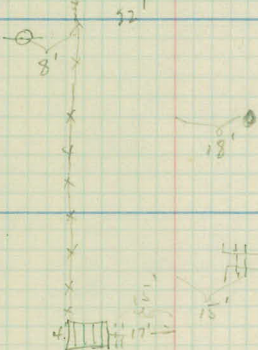
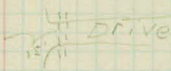
+60 Fence Cor. L.

152+47 Tel Pole R

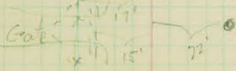
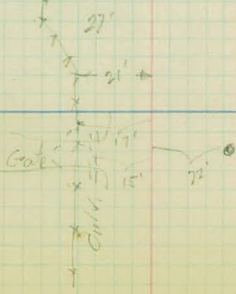
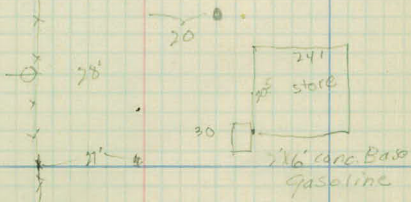
152 +44 Priv Ent. L. 12" C.M. culv 19' Lg.



Private grounds



Cottages
Wooded



161+857 P.C.

161+75 Bill Board s. End.

161+34 Tel. Pole R.

160+86 Power Pole L.

160+24 Priv Ent L. 12" Cor. M. cu N 16' Lg.

160+02 Tel Pole R.

159+95 12" C.M. cu N. 16' Lg.

159+50

159+00

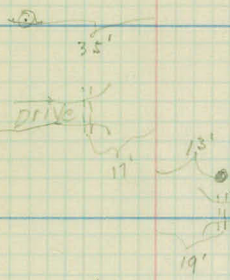
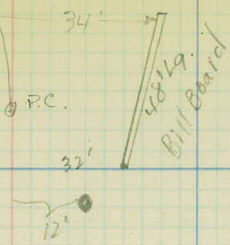
+75 Power Pole L.

+64 Tel Pole R.

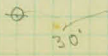
158+00

157+34 Tel. Pole L.

156+92 Power Pole L.



Cultivated



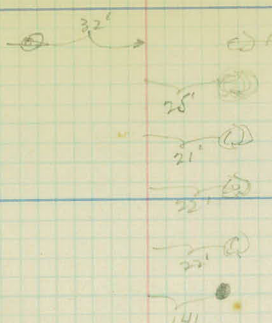
Cultivated

165+69 Postier Pole
166415 36" Tree R.
165442 10" Tree R.
165433 10" Tree R.
165411 14" Tree R.
165403 Tel. Pole R.
164491 Mail Box L.
164490 Fence E&W.
164485 PRIVENT. R.
164480 Fence
163493 Tree & Fence corner R.
163480 Tel. Pole R.
163439.42 P.T.

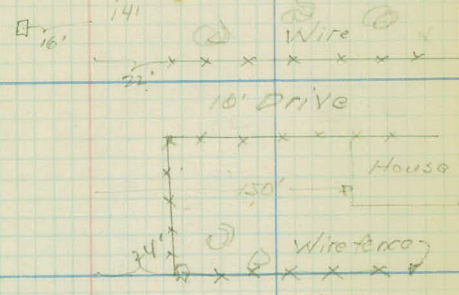
163406 PRIV. ENT. L. 12" Cor M. culv. 16' Lg.

162469 Power Pole L.
162462 Tel Pole R.

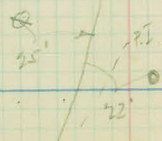
cultivated



Marsh
106
cultivated



10 Drive 11 11 17 17
Stone Monument
cultivated



174+91 Tel. Pole R.
174+62 Power Pole L.
173+70 Tel. Pole R.
173+55 Priv. Road L. 12" Cor. M. cul V. 16' Lg.

172+83 Power Pole L.

172+52 Tel. Pole R.

171+26 Tel. Pole R.

171+10 Power Pole L.

170+00 Tel. Pole R.

169+99 Tel. Pole L.

169+86 Priv. Road L. 12" C. M. cul V. 32' Lg.

169+35 Power Pole L.

+77 Tel. Pole R.

168

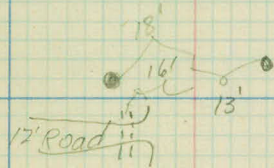
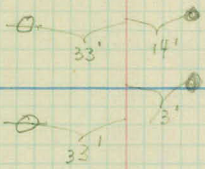
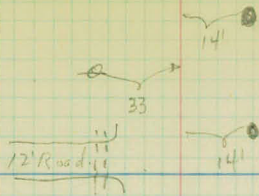
+58 Power Pole

+57 Tel. " R.

167+00

166+68 12" Cor. M. cul V. 99' Lg.

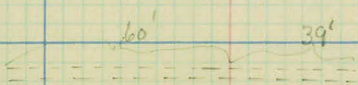
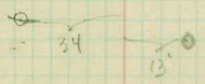
166+29 Tel. Pole R.



⊙ 33' × 14' ⊙ Guy Pole

cultivated

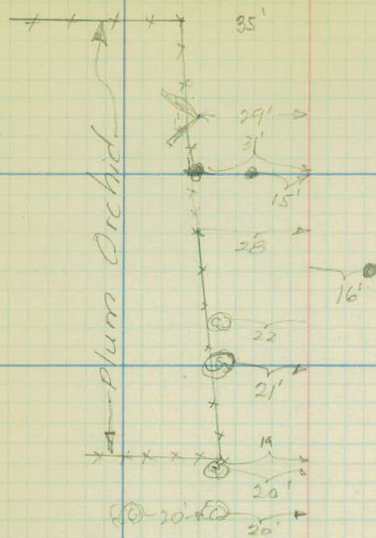
cultivated



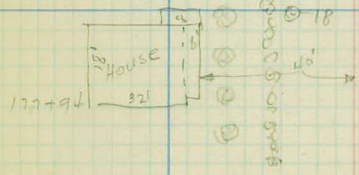
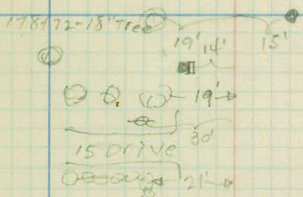
* Marsh



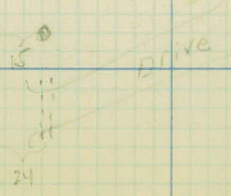
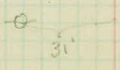
- 181400 End of Fence
- 180493 Sign Board
- 180437 Tel. & Power Pole L
- 180 Fence L.
- 496 Tel. Pole R.
- 179465 30" Stump L.
- 179453 36" Stump. L.
- 179412 Bag Fence L.
- 179411 18" Stump L.
- 178496 18" Tree
- 178472 Tel. Pole R.
- 178463 Tel. Pole L & Mail Box
+56 Power Pole L.
- 178454 12" Tree L.
- 178442
- 178429 End of Hedge L.
- 177461 Bag Hedge L.
- 177449 Tel. Pole R.
- 176460 Culv. 12" Vitrified
- 176450 Power Pole L.
- 176433 Tel. Pole R.
- 176417 Priv. Ent. R. 12" C.M. Culv. 17' Lg.
- 175470 10" Oak L.



cultivated.



cultivated



Cultivated.



- 187+29 12" Tree L.
187+21 Tel. Pole L.
+06 Tel. Pole R.
187 12" Tree L.
186+72 12" Tree L.
186+45 14" Tree L. & beg of fence L.
186+00
185+98 15" Tree L.
185+88 Tel & Power Pole L & R.
185+56 Tel. Pole L.
185+53 20" Tree L.
185+38 15" Tree R.
185+05 14" Tree L.
184+78 6" Tree
184+63 Tel. Pole R.
184+16 Power Pole L.
184 Fence R.
183+83 Tel. Pole L.
183+50 Tel. Pole R.
183+29 14" Stump L.
182+32 Tel. Pole R. & beg of fence
182+18 Power Pole L.
182+12 Tel. Pole L.
181+66 Sign Board
181+64 12" Tree R.
181+44 12" Tree R.
181+14 Tel. Pole R.
181+00

cultivated

cultivated



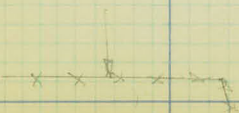
Scattered Timber

Pasture

cultivated

6" Tree
4" Tree
4" Tree

bag pot hole



+24 Power Pole L. Tel. Pole R.

193

+21 Beg Fence L.

+43. Tel. Pole L.

+01 Tel. Pole R.

192

+50 Power Pole L.

191

+81

Tel. Pole R.

+70

Tel. Pole L.

190 100

+65

Tel. Pole R.

+62

Power Pole L.

+375 Stone Mon. end of fence R.

189 100

+92

Tel. Pole L.

188+11

18" Tree L.

187+34

Tel. Pole R.

187+97

14" Tree L. end of fence.

187+80

Power Pole L.

187+75

12" Tree 23' L.

187+53

8" Tree L.

200

+02 Fence Jog
+25 Tel. Pole R.
+32 Tel. Pole L.

199+00

+76 Fence Corner
+61 Mail Box L.
+37 PRIV ENT R.
+14 End of Grove R. Tel. Pole R.

198

+58 Power Pole.

197+00

+90 Power Pole L. & Tel. Pole R.
+77 Fence corner
+51 Fence Jog
+13 Beg of Grove R.

196+00

+87 Tel. Pole L.
+69 Tel. Pole R.
+03 Power Pole L.

195+00

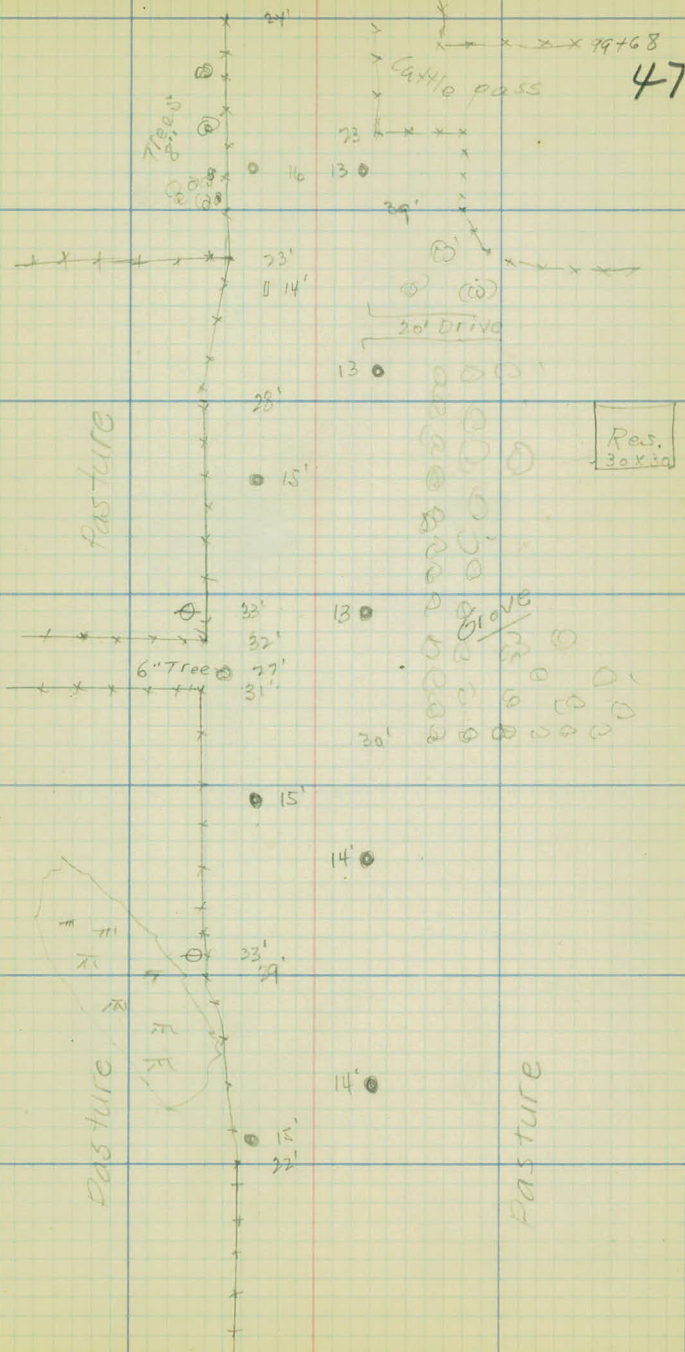
+03 Tel. Pole R.

+13 Tel. Pole L.

194

193

47



Tree

Cattle pass 19+68

23'

16

13

29'

23'

14'

20' Drive

13

28'

15'

Res. 30x10

33'

13

32'

6" Tree

27'

31'

30'

15'

14'

33'

14'

14'

15'

22'

Pasture

207

+89 Tel Pole R.

+22 Tel Pole L.

206

+90
+75 18" Vitrified 41' Lg.
Fence corner R.

+52 Tel Pole R.

151 End of Tile Left

205

+50 Tel Pole L.

+76 15" Tree & Tel Pole R.

204 +60 FTN ENT L.

+88 Mail Box L

+04 Tel Pole R.

203

+77 Tel Pole L.

+11 6" Tree L.

202

+80 Tel Pole R.

+20 End of Tile L.

201+04 End of Fence L.

+56 Tel Pole R.

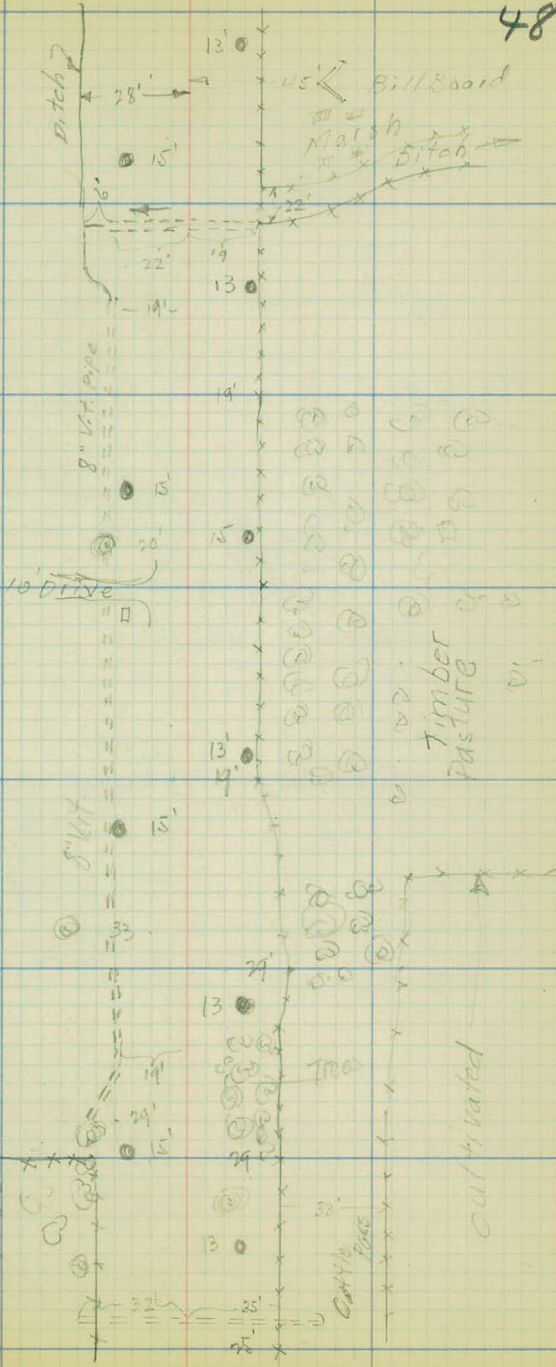
200 +08 20" Vit 67' Lg.

200 35'

Pasture cultivated

Trees

Hay



Billboard
Marsh
Ditch

Timber
Pasture

Cultivated

Tree

Cultivated
Trees

5' Vt. ave

10' Drive

ditch

214+00

+75 Fence L.

+09 Tel. Pole L.

213 Tel. Pole R.

212

+75 Tel. Pole R.

+39 Tel. Pole L.

211

+53 Tel. Pole R.

210

+65 Tel. Pole L.

+27 Tel. Pole R.

209+00

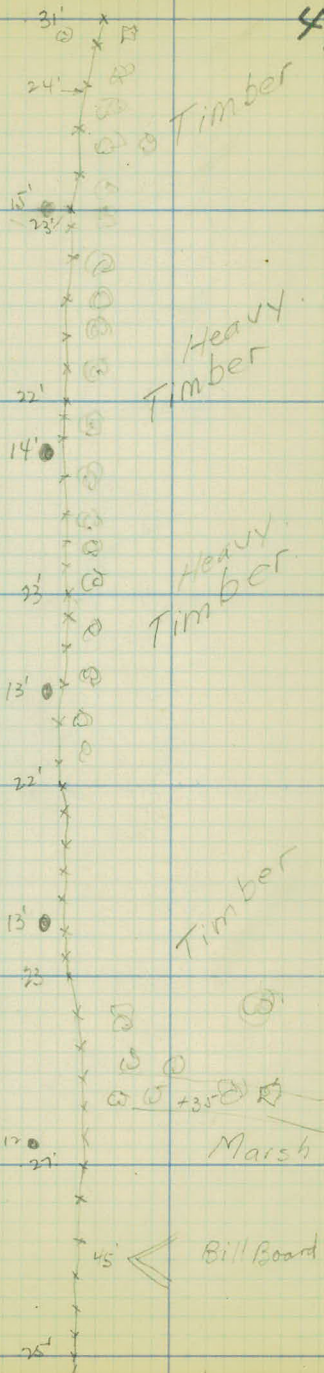
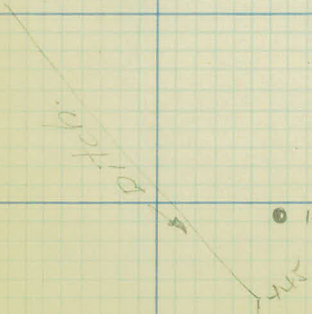
208+08 Tel. Pole R.

+95 Tel. Pole 15' L.

207

Cultivated.

cultivated.



Timber

Heavy Timber

Heavy Timber

Timber

Marsh

Bill Board

+30'

+47 RR Xing S 1/4
218+23 End of fence
218+12 Tel. Pole Left.
218+03

217+63 S. end of Oil Tank R.

217+10 Beg Fence x corner

217+00

750 Tel Pole L

216
+89 Poles L.
+72 E County Road "E"
+57 12" culv. 77 Lg. 455 Tel. Pole Left
+51 Fence R.

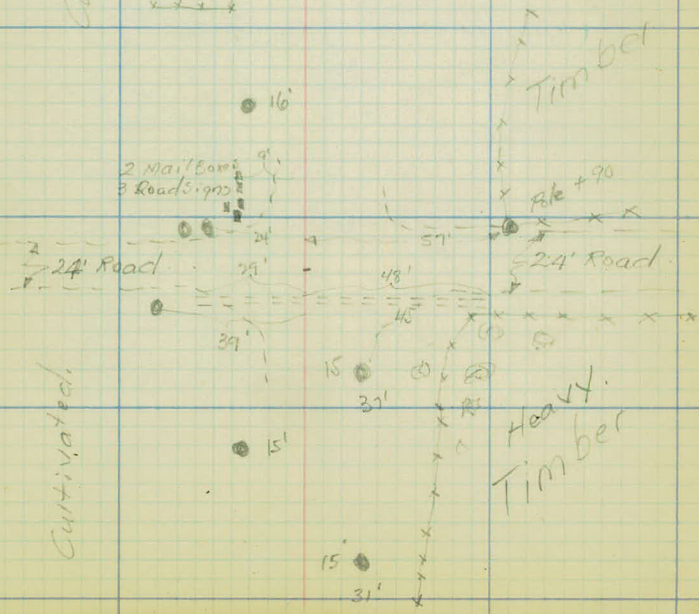
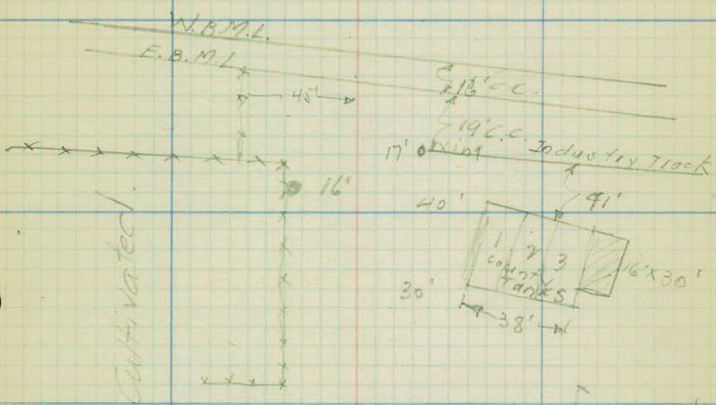
+14 Tel. Pole R.

215 Fence R.

+79 Tel. Pole L.

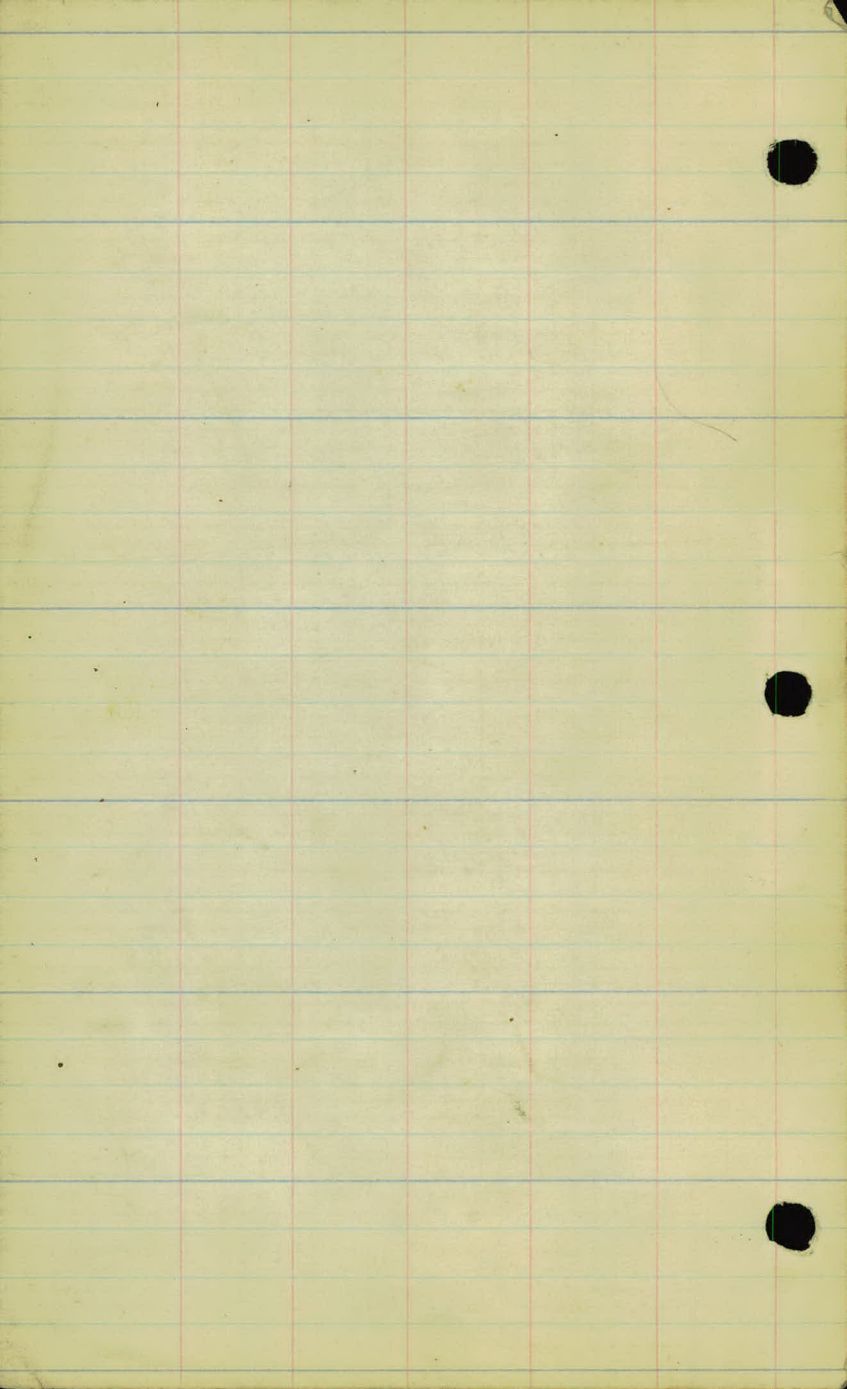
+12 Tel. Pole R.

214 Fence.



2 Mail Boxes
3 Roads 1920

Heavy
Timber



Drainage Notes
Project 24-01
Cross Drains to L.

Lexington Ave
Sta 0+00 to Sta 2+15

Dec. 1, 1973 Job 24-01

station	Present C.M.	Recommended C.M.
20+56	12" X 39' C.M. Extends 18.6' R & 20.6' L.	
24+54	12" X 37.4' C.M. Extends 18.6' R. & 18.8' L.	
74+10	12" X 47.5' C.M. Extends 26.5' R. & 21.0' L.	
95+69	15" X 42' C.M. Extends 22' R. & 20' L.	
102+79	15" X 42' C.M. Extends 22' R & 20' L.	
131+39	12" X 39' C.M. Extends 20.6' R & 18.4' L.	
142+03	12" X 33.6' C.M. Extends 17.6' R & 16' L.	
146+71	18" X 70.5' C.M. 14ft + 1/4 ft. R. Extends 17' R & 53.5' L.	

Inv. El.	299.0	298.9	298.3	297.8
Drains L.	$\frac{20.6}{}$	$\frac{35}{}$	$\frac{50}{}$	$\frac{100}{}$

Inv. El.	298.6	298.5
Drains L.	18.8	100

Inv. Elev.	270.0	269.1	268.8	266.8
Drains R.	$\frac{26.5}{}$	$\frac{25}{}$	$\frac{50}{}$	$\frac{100}{}$

Inv. El.	249.2	247.7	247.2	To Lake →
Drains R.	$\frac{22}{}$	$\frac{50}{}$	$\frac{100}{}$	

Inv. El.	260.9	260.5	260.0
Drains R.	$\frac{22}{}$	$\frac{25}{}$	$\frac{50}{}$

Inv. El.	243.4	242.3	242.1	Drains to Lake.
Drains R.	$\frac{20.6}{}$	$\frac{33}{}$	$\frac{50}{}$	

Inv. El.	243.5	243.6	243.7	243.6	Drains to Lake.
Drains R.	$\frac{17.6}{}$	$\frac{25}{}$	$\frac{50}{}$	$\frac{100}{}$	

Inv. Elev	242.8	243.1	242.2 = Top of Ice.
Drains R.	17	25	30

Dec. 3, 1923 Job 24-01

Station Present Culvert

146+73.5^S 18" x 70.5' C.M. 20ft Vit. R.
Extends 17' R. + 53.5' L.

166+68 12" x 99.0' C.M.
Extends 39.0' R. + 60' L.

176+60 12" x 62' Vit. culv.
Extends 28' R. + 34' L.

200+08 20" x 62' Vit. culv.
Extends 35' R. + 32' L.

205+90 15" x 41' Vit. culv.
Extends 19' R. + 22' L.

215+60 15" x 78' C.M. culv.
Co. Road 2" Extends 29' L. + 43' R.

Inv. El. $\frac{242.7}{17}$ $\frac{243.1}{25}$ $\frac{242.2}{30} = \text{Top of Ice.}$
 Drains. R.

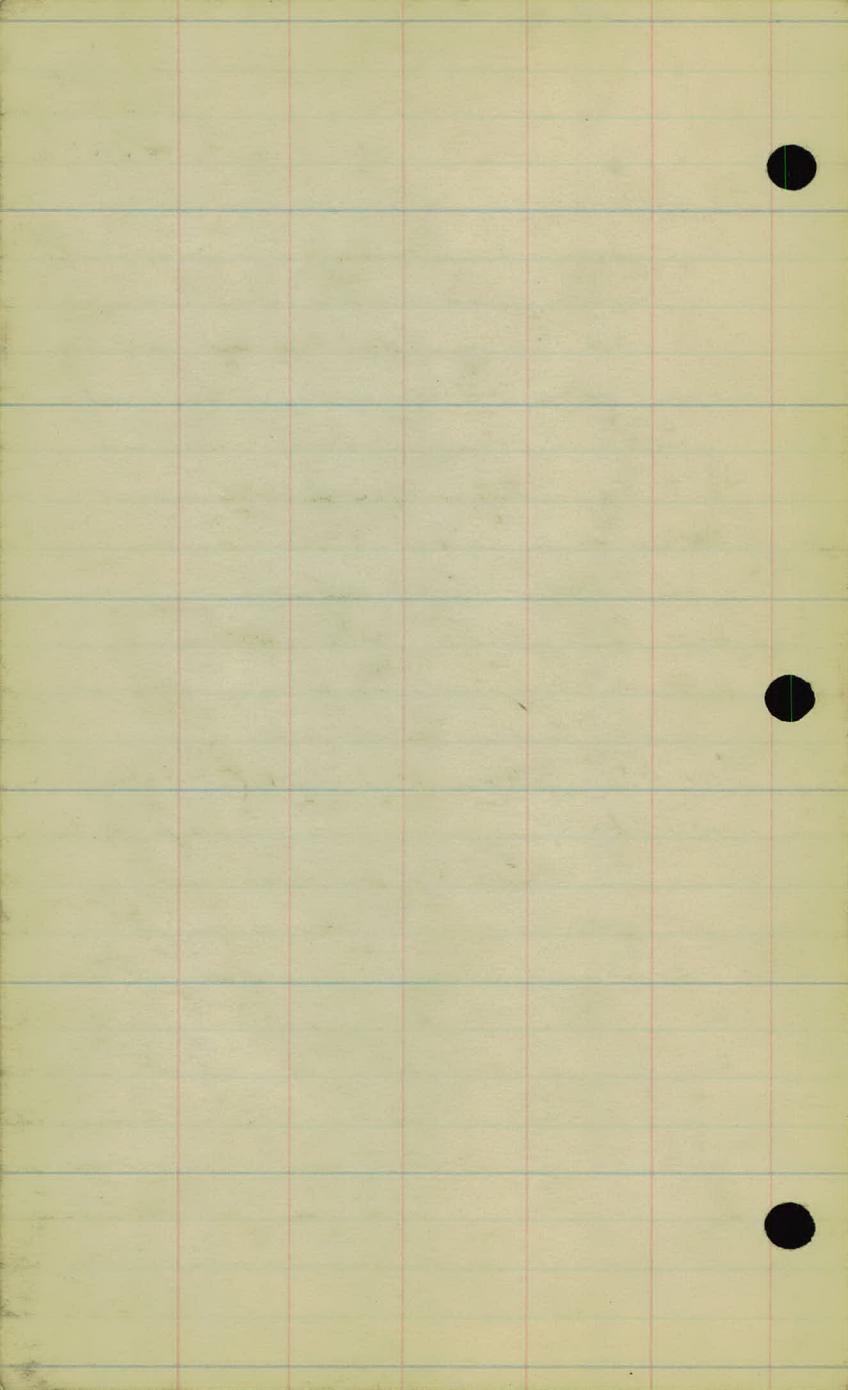
Inv. Elev. $\frac{277.8}{60}$ $\frac{278.3}{65}$ $\frac{279.0}{75}$ $\frac{278.0}{100}$ $\frac{277.0}{125}$
 Drains. L.

Inv. El. $\frac{293.8}{34}$ $\frac{293.2}{50}$ $\frac{292.2}{75}$
 Drains L.

Inv. El. $\frac{275.4}{32}$ $\frac{275.4}{50}$ $\frac{274.4}{100}$
 Drains. L.

Inv. El. $\frac{289.2}{22}$ $\frac{289.8}{28}$ $\frac{289.6}{50}$ $\frac{289.4}{75} = \text{flow line}$
 Drains L. $\frac{75 \text{ of } 8" \text{ Tile}}$
 see topog. for loc.

Inv. El. $\frac{303.7}{29}$ $\frac{303.2}{50}$
 Drains. L.



Proj # 24-01
Lexington Ave.

Center line levels and X Sections.

	+	H.I. ✓	-	Elev. ✓
B.M.	7.02	304.02		300.00
- 3+00			5.7	98.3
- 2+00			5.1	98.9
- 1+00			5.0	99.0
- 0+20			4.6	99.4
- 0+10			4.5	99.5
0+00	Q of Laportese		4.5	99.5
+ 20	Pitcher H.		5.0	99.0
+ 15			5.0	99.0
+ 50			4.9	99.1
1+00			5.2	98.8
2			5.4	98.4
3			6.0	97.4
T.P.	2.38	297.65 ✓	8.75	295.27 ✓
4			2.4	95.9
5			4.0	93.1
6			5.3	92.4
7			5.3	92.4
8			4.9	92.8
9			4.4	93.3
10			3.0	96.7
11			1.0	96.7
B.M.	8.65	305.02 ✓	0.98	296.04 ✓
+ 24			8.3	97.0
+ 32			8.3	97.0
+ 37	Center of Private Ent. on H.			
+ 47			7.7	97.4

R. 10/9/20

(Assumed Elev)

SpK in Tel. pole S.E. Cor of Lex. & Larp.

6.0	5.6	4.7	5.0 ²	4.8	4.7	4.7	5.0				
33	23	12	10	17	21	33					
4.5				4.8							
33				33							
9.7	7.4	4.5	4.2	4.1	4.7	4.3	4.3	4.6	5.5		
300	200	100	80	33	33	100	200	300			
3.4	2.6	5.7	5.3	5.5	5.0	5.3	5.9	5.8	6.3	6.5	7.7
200	150	100	50	20	73	60	100	150	200	2.50	
3.5	3.7	5.5	5.2	5.0	5.2	5.9					
33	27	23	12	15	33						
3.7	3.7	6.1	6.2	5.4	4.9	5.2	6.0	5.1	5.1		
33	27	21	17	14	13	22	30	33			
3.3	3.3	6.1	6.2	5.5	5.2	5.3	7.1	6.5			
33	27	21	18	15	13	18	33				
4.2	4.2	7.5	7.5	6.4	6.0	5.6	6.1	7.0	7.3	6.6	
33	30	25	23	18	14	12	15	17	33		
4.6	4.6	7.3	7.7	7.0	6.6	6.1	7.2	8.0	7.3		
33	30	24	19	10	13	19	33				

3.1	4.9	2.7	2.7	5.1	6.2	5.6					
33	21	14	13	20	25	33					
3.4	9.7	9.0	4.5	5.1	2.8	10.1	7.4				
33	37	20	13	13	20	25	33				
10.2	10.3	5.7	5.3	5.6	10.0	10.8	10.1				
33	20	13	12	17	20	33					
10.2	11.0	5.6	5.3	5.6	10.5	10.3					
33	23	12	14	22	33						
9.7	10.4	10.1	5.4	4.7	5.4	9.6	10.6	10.0			
33	24	20	12	12	20	24	33				
8.8	9.8	9.6	4.9	4.9	4.4	5.0	8.7	7.7	5.7		
33	25	21	15	12	11	18	22	33			
6.3	4.7	3.8		3.0	3.4	3.8	6.0	6.6	6.0		
33	20	13		12	14	18	25	33			
4.7	4.7	4.8	1.0	1.0	1.4	2.7	4.1	4.2	3.2		
33	24	20	13	11	15	21	27	33			

SpK in Tree Lt 510, 11 + 72

11.4	11.7	9.8	8.3	8.5	11.2	11.1				
33	21	15	13	11	21	33				
11.0	10.8	10.0	9.1	8.8	8.8	11.2	11.1			
7.5	5.0	3.9	1.5	1.3	3.1	4.3				
11.1	10.7	7.6	8.4	7.7	7.7	10.7	10.6			
7.5	5.0	3.3	1.5	1.2	2.1	3.3				

Sta	T	H.I.	-	Elev.
11+51		305.32	7.7	297.6
12			6.1	292.2
+33			5.2	300.1
+44	Center of Private Ent.	510		00.3 on Rt.
+61			4.9	00.5
13			3.2	02.1
T.P.	9.75	314.15 ✓	0.94	304.38 ✓
14			9.3	04.8
+22	Center of Private Ent.		8.8	05.3 on Rt.
15			7.4	06.5
16			7.1	07.0
+35			7.3	06.8
+40			7.3	06.8
+46	q. of Private Ent. on Rt.		7.4	06.7
+52			7.5	06.6
+58			7.4	06.5
17			7.9	06.2
B.M.			5.20	308.90
+15			8.1	06.0
18			9.0	04.5
19			11.0	03.1
T.P.	2.8+	306.01 ✓	10.76	303.17 ✓
20			3.8	02.2
20+56	culvert		4.1	01.9
	12" C.I.P. 37.2' Long.			

308.93

10/9/23

	L				R			
	107	161	3,177	7.9	107	106		
	33	20	13	12	31	33		
	24	96	2,761	6.5	78	91	97	7.0
	33	18	13	13	19	23	23	33
6.0	48	7.0	5.8	5.8	7.2	6.1	5.8	
33	27	17	13	14	24	33	50	
5.2	6.2	6.3	5.4	5.0	5.2	5.9	4.9	
33	33	16	7.0		14	33	50	
4.5	6.0	5.8	5.0	4.8	5.2	6.3	4.6	4.1
33	23	17	12	14	23	33	50	
2.0	3.2	3.4	4.5	3.7	3.7	4.5	3.0	
33	27	17	15	12	12	16	17	33

67	8.2	9.2	10.5	9.8	9.3	10.0	11.1	9.0	6.6	6.0	
33	28	18	14	12	12	16	18	18	27	33	
			6.5	7.4	8.7	8.8	9.4	10.2	8.0	5.8	5.3
			5.0	3.3	7	7.3	7.6	19	2.8	3.5	
37	6.5	7.4	8.8	8.3	7.6	7.1	8.8	6.0	4.2	5.4	
33	27	18	15	13	13	16	19	24	33		
4.3	6.7	7.0	8.2	7.5	7.1	7.4	7.8	2.3	2.0		
33	27	18	14	12	12	15	20	33			
			7.2	2.9	8.5	7.7	7.3	7.0	3.4	2.1	1.6
			3.3	1.8	1.7	1.9	2.1	3.5	5.0	7.5	
			7.2	7.9	8.5	7.7	7.3		6.5	4.4	
			3.3	1.8	1.7	1.3			5.1	7.5	

20	2.0	3.2	2.0	4.5		6.5	4.5	
33	20	17	12			30	7.5	
20	2.0	3.2	2.0	7.6		7.1	3.0	1.6
33	20	17	12			24	4.0	7.5
10.0	10.2	8.8	8.7	8.4	9.1	9.0	5.1	
33	24	19	14	13	14	24	36	

Spr. in tree 36' R of Sta. 17+12

109	10.9	8.6	8.1	8.6	9.3	9.3	7.1
33	22	14	12	15	24	33	
11.7	12.0	10.9	10.9	6.7	11.5	11.7	11.6
33	22	14	10	13	19	25	33
14.0	14.3	11.0	11.4	11.0	11.2	14.2	14.3
33	21	15	10	13	18	33	

Spr. in Tol. oak R. Sta. 18+50

7.5	7.0	4.3	3.8	3.7	5.9	4.4	6.5
33	18	13		7.2	17	24	33

7.8	8.3	7.8	7.2	4.1	6.7	6.5	6.1	5.6
200	100	50	10.6		18.4	50	100	200

Sta.	+	H.I.	-	Elev
		306.01		
21			4.4	301.6
22			4.5	301.5
23			4.0	302.0
24			4.2	301.8
	+ 54	Colvert	4.0	302.0
		12" Cor. 37.4' Long		
25			3.9	302.1
24			3.6	302.4
T.P.	5.18	307.54	3.65	302.90 ✓
	+ 25		5.1	302.4
	+ 37.5	E. of Cross Road	5.2	302.3
	+ 55		5.2	302.3
	+ 60		5.2	302.3
27			5.2	302.3
28			4.7	302.6
B.M.			3.33	304.21 ✓

L.

R.

$$\begin{array}{r} 7.5 \\ 33 \end{array} \quad \begin{array}{r} 7.7 \\ 22 \end{array} \quad \begin{array}{r} 7.2 \\ 17 \end{array} \quad \begin{array}{r} 4.7 \\ 12 \end{array} \quad \begin{array}{r} 4.8 \\ 8 \end{array} \quad H.4$$

$$\begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 4.0 \\ 14 \end{array} \quad \begin{array}{r} 6.5 \\ 24 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 6.9 \\ 20 \end{array} \quad \begin{array}{r} 6.7 \\ 18 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 5.0 \\ 9 \end{array} \quad H.5$$

$$\begin{array}{r} 4.9 \\ 9 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 6.1 \\ 17 \end{array} \quad \begin{array}{r} 6.5 \\ 24 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 6.1 \\ 19 \end{array} \quad \begin{array}{r} 5.5 \\ 18 \end{array} \quad \begin{array}{r} 5.3 \\ 15 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 4.6 \\ 9 \end{array} \quad (4.0)$$

$$\begin{array}{r} 4.4 \\ 9 \end{array} \quad \begin{array}{r} 4.2 \\ 13 \end{array} \quad \begin{array}{r} 5.0 \\ 20 \end{array} \quad \begin{array}{r} 5.0 \\ 22 \end{array} \quad \begin{array}{r} 5.5 \\ 23 \end{array} \quad \begin{array}{r} 5.1 \\ 27 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 20 \end{array} \quad \begin{array}{r} 6.9 \\ 9 \end{array} \quad \begin{array}{r} 6.7 \\ 17 \end{array} \quad \begin{array}{r} 4.6 \\ 13 \end{array} \quad \begin{array}{r} 4.6 \\ 9 \end{array} \quad (4.2)$$

$$\begin{array}{r} 4.8 \\ 10 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 7.0 \\ 19 \end{array} \quad \begin{array}{r} 7.4 \\ 25 \end{array} \quad \begin{array}{r} 7.0 \\ 33 \end{array}$$

Invert

$$\begin{array}{r} 7.2 \\ 100 \end{array} \quad \begin{array}{r} 6.9 \\ 50 \end{array} \quad \begin{array}{r} 7.5 \\ 133 \end{array} \quad H.0$$

Invert

$$\begin{array}{r} 7.1 \\ 134 \end{array} \quad \begin{array}{r} 7.2 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 100 \end{array} \quad \begin{array}{r} 6.1 \\ 200 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 22 \end{array} \quad \begin{array}{r} 6.7 \\ 18 \end{array} \quad \begin{array}{r} 4.3 \\ 13 \end{array} \quad \begin{array}{r} 4.7 \\ 10 \end{array} \quad (4.1)$$

$$\begin{array}{r} 4.2 \\ 8 \end{array} \quad \begin{array}{r} 4.2 \\ 13 \end{array} \quad \begin{array}{r} 6.5 \\ 18 \end{array} \quad \begin{array}{r} 7.1 \\ 25 \end{array} \quad \begin{array}{r} 6.5 \\ 33 \end{array}$$

$$\begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 22 \end{array} \quad \begin{array}{r} 6.2 \\ 17 \end{array} \quad \begin{array}{r} 4.0 \\ 14 \end{array} \quad (3.0)$$

$$\begin{array}{r} 4.0 \\ 12 \end{array} \quad \begin{array}{r} 5.7 \\ 17 \end{array} \quad \begin{array}{r} 5.9 \\ 27 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \end{array}$$

$$\begin{array}{r} 6.8 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 24 \end{array} \quad \begin{array}{r} 5.6 \\ 11 \end{array} \quad (5.1)$$

$$\begin{array}{r} 5.7 \\ 19 \end{array} \quad \begin{array}{r} 6.3 \\ 31 \end{array} \quad \begin{array}{r} 5.2 \\ 30 \end{array}$$

$$\begin{array}{r} 8.5 \\ 300 \end{array} \quad \begin{array}{r} 8.0 \\ 200 \end{array} \quad \begin{array}{r} 6.6 \\ 100 \end{array} \quad \begin{array}{r} 6.0 \\ 50 \end{array} \quad (5.0)$$

$$\begin{array}{r} 4.3 \\ 50 \end{array} \quad \begin{array}{r} 4.2 \\ 100 \end{array} \quad \begin{array}{r} 5.1 \\ 200 \end{array} \quad \begin{array}{r} 5.5 \\ 300 \end{array}$$

$$\begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 24 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 5.5 \\ 10 \end{array} \quad (5.2)$$

$$\begin{array}{r} 5.4 \\ 12 \end{array} \quad \begin{array}{r} 4.6 \\ 30 \end{array} \quad \begin{array}{r} 4.6 \\ 50 \end{array}$$

$$\begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 22 \end{array} \quad \begin{array}{r} 6.4 \\ 18 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 5.7 \\ 8 \end{array} \quad (5.2)$$

$$\begin{array}{r} 5.4 \\ 12 \end{array} \quad \begin{array}{r} 7.5 \\ 17 \end{array} \quad \begin{array}{r} 7.5 \\ 25 \end{array} \quad \begin{array}{r} 5.0 \\ 31 \end{array} \quad \begin{array}{r} 7.8 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 25 \end{array} \quad \begin{array}{r} 7.0 \\ 19 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad \begin{array}{r} 5.6 \\ 9 \end{array} \quad (5.2)$$

$$\begin{array}{r} 5.5 \\ 8 \end{array} \quad \begin{array}{r} 5.2 \\ 11 \end{array} \quad \begin{array}{r} 8.1 \\ 17 \end{array} \quad \begin{array}{r} 8.7 \\ 24 \end{array} \quad \begin{array}{r} 8.4 \\ 25 \end{array} \quad \begin{array}{r} 5.8 \\ 30 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array}$$

$$\begin{array}{r} 8.1 \\ 33 \end{array} \quad \begin{array}{r} 8.2 \\ 20 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad \begin{array}{r} 5.4 \\ 10 \end{array} \quad (4.9)$$

$$\begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 5.2 \\ 19 \end{array} \quad \begin{array}{r} 8.9 \\ 25 \end{array} \quad \begin{array}{r} 8.1 \\ 33 \end{array}$$

Spk. 111 Tree 105' Lt. of Sta 28+10

Sta	+	H.I.	-	Elev.
		307.54		
29			4.5	303.0
30			4.1	303.4
31			3.2	304.8
32			2.5	305.0
				Center of Private Ent. on R.
33			1.9	305.4
T.P	6.72	312.58	1.08	305.76
34			6.4	306.2
+64			5.8	306.8
				Center of Private Ent. on R.
+94			5.4	307.0
				Center of Private Ent. on L.
35			5.4	307.0
+13			5.5	307.1
				Center of Private Ent. on R.
36			5.0	307.4
+32			4.8	307.8
				Center of Private Ent. on L.

Sta	+	H.I.	-	Elev.
		312.58		
37			4.4	308.2.
38			5.8	308.8.
39			2.9	309.7.
+08			2.8	309.8.
	Center of Private Ent. on R.			
40			2.5	310.1.
41			1.7	310.9.
T.P.	5.81	314.71	1.63	310.90 ✓
42			4.8	311.9.
+09			4.2	312.5.
	Center of Private Ent. on R.			
43			4.0	312.7.
44			4.3	312.4.
45			4.7	312.0.
46			6.1	310.6.
47			7.5	309.2.
	Center of Private Ent. on L.			

$\frac{48}{33} \frac{6.5}{20} \frac{4.7}{12} \frac{4.7}{8}$

4.8

$\frac{4.7}{13} \frac{5.8}{21} \frac{5.7}{33}$

$\frac{4.7}{33} \frac{5.9}{20} \frac{4.6}{16} \frac{4.4}{8}$

3.8

$\frac{4.3}{16} \frac{5.5}{22} \frac{5.8}{33}$

$\frac{4.1}{33} \frac{4.3}{17} \frac{3.7}{13} \frac{3.5}{8}$

2.9

$\frac{3.8}{11} \frac{3.3}{18} \frac{4.3}{20} \frac{3.6}{23} \frac{3.7}{33}$

$\frac{4.1}{33} \frac{4.3}{18} \frac{3.7}{13} \frac{3.5}{8}$

2.8

$\frac{3.1}{10} \frac{3.0}{27} \frac{3.6}{50} \frac{5.0}{110}$

$\frac{5.9}{33} \frac{5.6}{20} \frac{3.0}{13} \frac{3.0}{8}$

2.5

$\frac{2.6}{12} \frac{3.3}{14} \frac{3.5}{18} \frac{3.7}{28} \frac{3.0}{33}$

$\frac{4.7}{33} \frac{4.1}{18} \frac{2.0}{10}$

1.7

$\frac{2.0}{11} \frac{2.5}{15} \frac{2.8}{16} \frac{3.3}{18} \frac{2.9}{23} \frac{2.8}{33}$

$\frac{4.5}{33} \frac{4.7}{18} \frac{5.2}{19} \frac{4.7}{9}$

4.8

$\frac{5.0}{12} \frac{5.8}{16} \frac{5.8}{17} \frac{4.8}{19} \frac{5.5}{25} \frac{5.5}{31} \frac{4.6}{33}$

$\frac{1.2}{33} \frac{3.9}{30} \frac{4.5}{17} \frac{5.5}{14} \frac{4.5}{9}$

4.2

$\frac{4.4}{14} \frac{4.5}{33} \frac{3.0}{43} \frac{3.1}{50} \frac{1.1}{100}$

$\frac{1.2}{33} \frac{3.3}{30} \frac{4.0}{16} \frac{5.0}{15} \frac{5.0}{13} \frac{4.1}{9}$

4.0

$\frac{4.3}{13} \frac{5.2}{15} \frac{5.2}{17} \frac{4.4}{19} \frac{3.8}{33} \frac{1.1}{38}$

$\frac{5.0}{33} \frac{4.7}{21} \frac{5.5}{14} \frac{4.7}{12}$

4.3

$\frac{4.6}{14} \frac{5.3}{16} \frac{5.3}{19} \frac{4.6}{12} \frac{4.0}{33}$

$\frac{5.4}{33} \frac{5.2}{17} \frac{4.7}{14} \frac{5.8}{13} \frac{5.1}{8}$

4.7

$\frac{5.2}{12} \frac{5.9}{15} \frac{5.9}{17} \frac{5.0}{18} \frac{4.4}{33}$

$\frac{7.0}{33} \frac{8.6}{20} \frac{9.7}{17} \frac{6.7}{9}$

6.1

$\frac{6.6}{13} \frac{7.2}{15} \frac{6.4}{17} \frac{6.7}{33}$

$\frac{7.7}{100} \frac{8.0}{50} \frac{7.9}{23} \frac{8.0}{7}$

7.5

$\frac{8.0}{8} \frac{7.1}{13} \frac{8.8}{14} \frac{8.0}{18} \frac{6.9}{33}$

Sta	T	H.L.	-	R/100
		316.71		
T.P.	3.03	311.12 ✓	8.02	308.09 ✓
48			5.2	307.9.
49			4.2	306.9.
+45			4.3	306.8.
50			4.5	306.6.
+23			4.5	306.6.
				Center of Private Ent. in R.
51			4.5	306.4.
52			4.8	306.3.
B.M.	3.54	310.98 ✓	3.68	307.44 ✓
+38			4.7	306.3.
+67.5			4.8	306.2.
				Center of County Road B.
53			5.2	305.8.
54			4.1	306.2.
+22			4.9	306.1.
				Center of Private Ent. in R.

L.

R.

$$\begin{array}{r} 5.2 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 24 \end{array} \quad \begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 3.5 \\ 16 \end{array} \quad \begin{array}{r} 3.8 \\ 8 \end{array} \quad (3.2) \quad \begin{array}{r} 3.6 \\ 9 \end{array} \quad \begin{array}{r} 3.6 \\ 14 \end{array} \quad \begin{array}{r} 4.8 \\ 17 \end{array} \quad \begin{array}{r} 5.6 \\ 24 \end{array} \quad \begin{array}{r} 5.6 \\ 33 \end{array}$$

$$\begin{array}{r} 7.1 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 4.5 \\ 8 \end{array} \quad (4.2) \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 6.9 \\ 19 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array}$$

$$\begin{array}{r} 9.1 \\ 33 \end{array} \quad \begin{array}{r} 8.7 \\ 24 \end{array} \quad \begin{array}{r} 4.6 \\ 14 \end{array} \quad \begin{array}{r} 4.8 \\ 7 \end{array} \quad (4.3) \quad \begin{array}{r} 4.6 \\ 13 \end{array} \quad \begin{array}{r} 7.8 \\ 21 \end{array} \quad \begin{array}{r} 7.5 \\ 33 \end{array}$$

$$\begin{array}{r} 8.2 \\ 33 \end{array} \quad \begin{array}{r} 7.8 \\ 25 \end{array} \quad \begin{array}{r} 7.3 \\ 30 \end{array} \quad \begin{array}{r} 4.7 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 9 \end{array} \quad (4.5) \quad \begin{array}{r} 4.8 \\ 11 \end{array} \quad \begin{array}{r} 5.6 \\ 18 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array}$$

$$\begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 30 \end{array} \quad \begin{array}{r} 7.6 \\ 22 \end{array} \quad \begin{array}{r} 7.6 \\ 30 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 4.7 \\ 9 \end{array} \quad (4.5) \quad \begin{array}{r} 4.8 \\ 6 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 3.2 \\ 50 \end{array}$$

$$\begin{array}{r} 3.3 \\ 33 \end{array} \quad \begin{array}{r} 4.1 \\ 24 \end{array} \quad \begin{array}{r} 6.5 \\ 21 \end{array} \quad \begin{array}{r} 4.8 \\ 13 \end{array} \quad (4.5) \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 5.4 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 18 \end{array} \quad \begin{array}{r} 3.8 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 6.1 \\ 30 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad (4.8) \quad \begin{array}{r} 5.3 \\ 11 \end{array} \quad \begin{array}{r} 6.5 \\ 14 \end{array} \quad \begin{array}{r} 8.6 \\ 23 \end{array} \quad \begin{array}{r} 8.8 \\ 33 \end{array}$$

Top of lower School House step at the South End.

$$\begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 6.3 \\ 19 \end{array} \quad \begin{array}{r} 5.1 \\ 7 \end{array} \quad (4.7) \quad \begin{array}{r} 5.4 \\ 12 \end{array} \quad \begin{array}{r} 5.7 \\ 2.7 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array}$$

$$\begin{array}{r} 4.9 \\ 300 \end{array} \quad \begin{array}{r} 4.7 \\ 200 \end{array} \quad \begin{array}{r} 5.1 \\ 100 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array} \quad (4.8) \quad \begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 100 \end{array} \quad \begin{array}{r} 3.5 \\ 200 \end{array} \quad \begin{array}{r} 1.9 \\ 300 \end{array}$$

$$\begin{array}{r} 7.3 \\ 33 \end{array} \quad \begin{array}{r} 8.3 \\ 27 \end{array} \quad \begin{array}{r} 5.7 \\ 21 \end{array} \quad (5.2) \quad \begin{array}{r} 5.3 \\ 17 \end{array} \quad \begin{array}{r} 7.9 \\ 27 \end{array} \quad \begin{array}{r} 7.9 \\ 33 \end{array}$$

$$\begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 14 \end{array} \quad \begin{array}{r} 5.4 \\ 12 \end{array} \quad (4.8) \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 17 \end{array} \quad \begin{array}{r} 5.1 \\ 18 \end{array} \quad \begin{array}{r} 5.1 \\ 38 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 6.4 \\ 14 \end{array} \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad (4.0) \quad \begin{array}{r} 4.7 \\ 9 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array}$$

Sta. T H.I. - Elev.

310.98

53 5.1 305.9

54 5.4 305.4

T.P. 1.79 306.27 ✓ 5.90 305.08 ✓

+2.9

Center of Private Est on L.

57 1.5 304.4

58 4.7 303.0

59 5.7 301.0

+5.0

6.6 300.3

60 7.2 299.7

61 2.0 298.9

T.P. +9.4 304.14 ✓ 7.67 299.20 ✓

62 5.3 298.9

B.M. 2.13 304.36 ✓ 1.73 302.23 ✓

+7.9

5.0 299.4

Center of Private Est on R.

63 4.7 299.0

299.0

+5.0

4.7 299.7 ✓

Proj. # 24-01

Lexington Ave.

Center line levels and
X sections from Sta. 55+00
to Sta. 104+00

Center line levels sta 104.-
215+71.6

Sta	+	H.I.	-	Elev.
		310.98	✓	
55			5.1	305.9 ✓
56			5.0	305.9 ✓
T.P.	1.79	306.87	5.70	305.08 ✓
+29	Pri. Ent. L.		1.6	305.3
57			2.5	309.4 ✓
58			3.9	303.0 ✓
59			5.9	311.0 ✓
+50			4.4	310.3 ✓
60			7.2	299.7 ✓
61			8.0	298.9 ✓
T.P.	4.96	309.14	7.67	299.20 ✓
62			5.3	298.9 ✓
B.M.	2.13	304.36	1.93	302.23 ✓
+79	Pri. Ent. R.		5.0	299.4 ✓
63			5.9	299.5 ✓ <u>298.5</u> ✓
+50			4.7	299.7 ✓

L.

R.

$\frac{3.6}{33}$	$\frac{3.6}{29}$	$\frac{5.1}{25}$	$\frac{5.7}{18}$	$\frac{6.5}{14}$	$\frac{5.4}{13}$	5.1	$\frac{5.2}{13}$	$\frac{6.0}{15}$	$\frac{5.4}{17}$	$\frac{5.2}{18}$	$\frac{6.2}{33}$
------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{5.0}{33}$	$\frac{5.2}{18}$	$\frac{6.5}{14}$	$\frac{5.6}{13}$	5.6	$\frac{5.9}{10}$	$\frac{6.0}{13}$	$\frac{6.2}{17}$	$\frac{6.6}{26}$	$\frac{6.6}{33}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{1.0}{50}$	$\frac{1.4}{22}$	$\frac{1.7}{8}$	1.6	$\frac{2.2}{11}$	$\frac{3.1}{15}$	$\frac{3.3}{17}$	$\frac{2.7}{24}$	$\frac{2.7}{33}$
------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{2.5}{33}$	$\frac{3.1}{18}$	$\frac{3.7}{15}$	$\frac{3.7}{14}$	$\frac{2.7}{10}$	2.5	$\frac{2.8}{12}$	$\frac{3.6}{16}$	$\frac{2.0}{18}$	$\frac{0.7}{24}$	$\frac{0.3}{33}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{3.9}{33}$	$\frac{4.8}{22}$	$\frac{5.6}{14}$	$\frac{4.5}{10}$	3.9	$\frac{4.6}{12}$	$\frac{5.4}{16}$	$\frac{5.0}{26}$	$\frac{5.6}{33}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{8.4}{33}$	$\frac{9.2}{27}$	$\frac{9.0}{17}$	$\frac{6.3}{12}$	5.9	$\frac{6.2}{11}$	$\frac{7.7}{17}$	$\frac{8.4}{26}$	$\frac{7.4}{33}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{7.5}{33}$	$\frac{7.4}{28}$	$\frac{9.2}{18}$	$\frac{7.2}{12}$	6.6	$\frac{6.9}{12}$	$\frac{9.8}{17}$	$\frac{10.7}{33}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	-------------------

$\frac{8.6}{33}$	$\frac{16.1}{27}$	$\frac{10.0}{17}$	$\frac{7.8}{11}$	7.2	$\frac{7.5}{13}$	$\frac{16.8}{17}$	$\frac{10.8}{21}$	$\frac{10.0}{24}$	$\frac{10.0}{33}$
------------------	-------------------	-------------------	------------------	-----	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{15.2}{33}$	$\frac{13.5}{22}$	$\frac{8.3}{11}$	8.0	$\frac{8.3}{12}$	$\frac{13.1}{20}$	$\frac{15.0}{33}$
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$\frac{9.7}{33}$	$\frac{8.7}{24}$	$\frac{6.0}{14}$	5.3	$\frac{5.6}{12}$	$\frac{8.7}{19}$	$\frac{9.1}{26}$	$\frac{9.1}{33}$
------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

SpA in Tree

R. Stg. 63 + 94

$\frac{9.0}{33}$	$\frac{7.1}{22}$	$\frac{6.3}{18}$	$\frac{5.5}{10}$	5.0	$\frac{5.6}{10}$	$\frac{7.1}{22}$	$\frac{8.4}{20}$	$\frac{7.2}{50}$	$\frac{9.2}{100}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	-------------------

$\frac{8.3}{33}$	$\frac{8.6}{28}$	$\frac{5.5}{15}$	$\frac{5.3}{9}$	5.9	$\frac{5.6}{12}$	$\frac{8.2}{20}$	$\frac{10.2}{33}$
------------------	------------------	------------------	-----------------	-----	------------------	------------------	-------------------

$\frac{5.9}{33}$	$\frac{5.4}{20}$	$\frac{6.5}{17}$	$\frac{6.5}{16}$	$\frac{5.2}{12}$	4.7	$\frac{5.2}{10}$	$\frac{6.3}{17}$	$\frac{6.3}{19}$	$\frac{5.2}{22}$	$\frac{4.8}{27}$	$\frac{2.2}{31}$	$\frac{2.2}{33}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	------------------	------------------

Sta	T	H.I.		Elev.
		304.36 ✓		
64			4.7	299.7 ✓
+12			4.8	299.4 ✓
				Center of Pri. Ent on L.
T.P.	7.05	308.79 ✓	2.42	301.92 ✓
65			7.7	299.3 ✓ 300.3 ✓
+85			10.0	299.0 ✓
				Center of Pri. Ent on L.
+90			10.0	299.0 ✓
+95				Center of Pri. Ent on R.
+96			10.0	299.0 ✓
66			10.0	299.0 ✓
+97			10.0	299.0 ✓
67			11.2	298.8 ✓
+50			12.1	296.9 ✓
68			13.0	296.0 ✓
T.P.	0.08	296.60 ✓	12.47	296.52 ✓
+95			2.8	293.8 ✓
				Center of Pri. Ent on R.
69			3.1	293.5 ✓

$$\frac{0.8}{33} \quad \frac{5.3}{24} \quad \frac{6.1}{19} \quad \frac{5.2}{17} \quad 4.7$$

$$\frac{5.3}{10} \quad \frac{6.0}{15} \quad \frac{6.0}{17} \quad \frac{1.6}{25} \quad \frac{1.0}{33}$$

$$\frac{2.7}{50} \quad \frac{4.4}{22} \quad \frac{5.1}{8} \quad 4.8$$

$$\frac{5.4}{13} \quad \frac{6.1}{15} \quad \frac{6.1}{17} \quad \frac{2.8}{19} \quad \frac{3.3}{24} \quad \frac{0.3}{27} \quad \frac{2.6}{33}$$

$$\frac{5.8}{35} \quad \frac{9.6}{19} \quad \frac{10.9}{16} \quad \frac{11.9}{15} \quad \frac{10.0}{13} \quad 9.7$$

$$\frac{10.0}{12} \quad \frac{11.0}{16} \quad \frac{11.0}{17} \quad \frac{9.7}{19} \quad \frac{9.2}{24} \quad \frac{5.1}{27} \quad \frac{1.2}{33}$$

$$\frac{7.0}{50} \quad \frac{10.0}{8} \quad 10.0$$

$$\frac{9.8}{14} \quad \frac{8.9}{24} \quad \frac{4.2}{29} \quad \frac{1.6}{31} \quad \frac{1.0}{40}$$

$$\frac{8.5}{33} \quad \frac{10.0}{8} \quad 10.0$$

$$\frac{10.0}{10} \quad \frac{7.3}{19} \quad \frac{8.1}{35} \quad \frac{7.5}{45}$$

$$\frac{7.7}{33} \quad \frac{10.0}{8} \quad 10.0$$

$$\frac{10.0}{10} \quad \frac{9.3}{19} \quad \frac{8.1}{35} \quad \frac{7.5}{45}$$

$$\frac{7.8}{33} \quad \frac{7.9}{27} \quad \frac{2.0}{18} \quad \frac{10.6}{14} \quad \frac{10.6}{15} \quad \frac{10.2}{12} \quad 10.0$$

$$\frac{10.2}{10} \quad \frac{10.4}{7} \quad \frac{9.8}{18} \quad \frac{9.8}{23} \quad \frac{4.3}{31} \quad \frac{1.8}{32} \quad \frac{2.1}{40}$$

$$\frac{8.0}{33} \quad \frac{10.9}{18} \quad \frac{12.0}{16} \quad \frac{12.0}{15} \quad \frac{11.3}{2} \quad \frac{11.4}{7} \quad 11.2$$

$$\frac{11.7}{12} \quad \frac{12.3}{16} \quad \frac{12.3}{18} \quad \frac{11.5}{17} \quad \frac{10.0}{24} \quad \frac{4.0}{33}$$

$$\frac{9.8}{33} \quad \frac{11.8}{19} \quad \frac{12.7}{16} \quad \frac{12.3}{10} \quad 12.4$$

$$\frac{12.6}{13} \quad \frac{12.3}{16} \quad \frac{12.7}{19} \quad \frac{12.2}{33} \quad \frac{5.0}{34} \quad \frac{4.0}{45}$$

$$\frac{13.2}{33} \quad \frac{12.8}{27} \quad \frac{14.0}{17} \quad \frac{13.3}{10} \quad 13.0$$

$$\frac{13.5}{13} \quad \frac{14.1}{17} \quad \frac{11.5}{33} \quad \frac{11.5}{40}$$

$$\frac{5.3}{33} \quad \frac{5.5}{22} \quad \frac{4.9}{17} \quad \frac{3.2}{12} \quad 2.8$$

$$\frac{3.2}{10} \quad \frac{3.1}{22} \quad \frac{3.0}{33} \quad \frac{2.5}{50}$$

$$\frac{5.3}{33} \quad \frac{5.5}{22} \quad \frac{4.9}{17} \quad \frac{3.2}{12} \quad 3.1$$

$$\frac{3.5}{11} \quad \frac{3.4}{33}$$

570	7	H.I.	-	K/100	
			296.60	✓	
+70		Pr. Ent. 10 L.	6.2	290.4	✓
70			6.6	290.0	✓
+65			7.0	287.4	✓
71			10.5	286.2	✓
+15		Pr. Ent. R.	10.7	285.7	✓
+35		✓	11.4	285.0	✓
T.P.	1.27	285.72	12.12	284.47	✓
72		Pr. Ent. R.	2.8	282.9	✓
73			5.6	280.1	✓
74			6.0	279.1	✓
+10			6.6	279.1	✓
		12" Vit. Culvert. 474' Long			
75			7.0	278.7	✓
+55		Pr. Ent. R.	6.8	278.7	✓
74			5.9	279.8	✓

L.

R

5.7	4.1	6.3	6.5	6.2
5.0	3.3	2.1	8	

6.7	8.8	7.2
14	20	33

8.0	7.7	6.7	6.6
3.3	1.4	8	

7.2	7.1	7.4	7.7
14	22	27	33

6.1	6.3	10.3	9.7	9.2	9.0
3.3	2.9	1.4	1.5	1.0	

7.6	9.7	11.4	11.0	8.5
10	15	23	28	33

5.0	5.1	11.6	11.6	10.8	10.8	10.4
3.3	3.0	1.7	1.5	1.2	8	

10.8	10.8	11.9	11.0	9.2
7	15	21	28	33

5.0	5.1	12.3	12.3	11.1	11.3	10.9
3.3	3.0	1.9	1.7	1.2	8	

11.3	11.2	10.7	10.5
8	16	33	50

5.6	13.3	13.3	12.0	11.6
3.3	2.1	1.6	1.2	

12.1	13.3	11.5	10.8
14	28	24	33

4.4	7.0	4.6	3.2	3.1	2.8
3.3	2.8	1.9	1.3	7	

3.1	4.2	5.7	7.0
12	19	33	50

10.8	10.4	5.6	5.9	5.6
3.3	1.8	1.1	1.4	

6.0	11.9	12.7
12	23	31

13.5	13.5	13.2	4.7	6.8	6.6
3.3	2.7	2.0	1.1	7	
Invert 15.1					
21					

7.0	13.9	15.3
13	24	33
15.0 Invert		
16.5		

12.5	12.0	7.2	7.0
3.3	2.0	1.2	

7.5	13.2	13.9
13	23	33

12.7	12.4	6.7	6.0
3.3	2.0	1.4	

7.2	7.7	11.6
14	33	50

12.8	12.8	11.7	5.8	6.0	5.9
3.3	2.8	2.2	1.1	7	

6.4	7.2	13.3	14.2
13	17	29	33

Sta.	+	H.I.	-	Elev.
		285.72	✓	
77			3.0	282.7 ✓
T.P.	11.44	272.72	✓	281.24 ✓
+75	Pri. Ent. L.		7.8	285.1 ✓
78			6.8	286.1 ✓
B.M.	9.88	299.78	✓	290.00 ✓
+70	Pri. Ent L.		10.3	289.4 ✓
79			10.0	289.9 ✓
80			8.1	291.8 ✓
81			7.0	292.9 ✓
+07	Pri. Ent R.		7.0	292.9 ✓
82			6.8	293.1 ✓
+50	Pri. Ent R.		6.9	293.0 ✓
83			7.4	292.5 ✓
+65	Pri. Ent. R.		2.2	291.7 ✓
84			8.7	291.2 ✓

$\frac{7.6}{33} \frac{7.6}{28} \frac{7.1}{20} \frac{3.7}{13}$

3.0

$\frac{3.4}{18} \frac{4.4}{18} \frac{9.0}{25} \frac{10.8}{33}$

$\frac{8.5}{50} \frac{8.0}{15} \frac{8.1}{8}$

7.8

$\frac{8.2}{15} \frac{10.8}{22} \frac{12.3}{29} \frac{12.6}{33}$

$\frac{5.9}{33} \frac{7.1}{18} \frac{8.0}{14} \frac{7.7}{15} \frac{7.1}{12} \frac{7.2}{7}$

6.8

$\frac{7.3}{14} \frac{8.9}{22} \frac{9.3}{28} \frac{11.2}{33}$

SPK in Tree 33 R. of Sta. 78+55

$\frac{8.4}{50} \frac{9.4}{33} \frac{10.4}{8}$

10.3

$\frac{10.7}{9} \frac{10.7}{13} \frac{11.6}{14} \frac{11.6}{17} \frac{10.2}{18} \frac{10.5}{28} \frac{9.8}{34}$

$\frac{4.2}{33} \frac{7.7}{21} \frac{10.2}{9}$

10.0

$\frac{10.6}{9} \frac{10.5}{13} \frac{11.4}{15} \frac{11.4}{14} \frac{10.7}{18} \frac{10.0}{29} \frac{6.7}{37}$

$\frac{2.4}{33} \frac{3.2}{25} \frac{3.0}{21} \frac{8.0}{19} \frac{9.2}{15} \frac{8.4}{11}$

8.1

$\frac{8.5}{12} \frac{9.5}{15} \frac{7.5}{14} \frac{8.7}{18} \frac{9.2}{27} \frac{8.5}{30} \frac{3.8}{38}$

$\frac{2.4}{33} \frac{3.8}{20} \frac{8.0}{15} \frac{7.3}{11}$

7.0

$\frac{7.3}{11} \frac{7.2}{23} \frac{3.4}{36}$

$\frac{2.4}{33} \frac{3.8}{20} \frac{4.0}{15} \frac{7.3}{11}$

7.0

$\frac{7.2}{12} \frac{7.6}{15} \frac{6.7}{24} \frac{6.1}{50}$

$\frac{2.2}{33} \frac{2.0}{24} \frac{5.7}{17} \frac{7.7}{15} \frac{7.7}{14} \frac{7.0}{10}$

6.8

$\frac{7.2}{12} \frac{7.7}{15} \frac{7.7}{14} \frac{7.1}{15} \frac{5.9}{21} \frac{4.7}{33} \frac{2.7}{41}$

$\frac{2.3}{33} \frac{1.7}{23} \frac{5.1}{17} \frac{2.7}{14} \frac{2.9}{13} \frac{7.1}{11}$

6.9

$\frac{7.0}{13} \frac{6.2}{24} \frac{6.1}{33} \frac{5.5}{50}$

$\frac{2.3}{33} \frac{2.2}{23} \frac{6.1}{17} \frac{8.3}{15} \frac{8.3}{12} \frac{2.7}{10}$

7.4

$\frac{7.8}{11} \frac{8.5}{15} \frac{7.8}{17} \frac{5.6}{33}$

$\frac{2.4}{33} \frac{2.0}{27} \frac{6.3}{17} \frac{9.3}{15} \frac{9.3}{13} \frac{8.5}{11}$

8.2

$\frac{8.4}{9} \frac{7.5}{21} \frac{6.3}{36} \frac{5.1}{50}$

$\frac{2.3}{33} \frac{2.1}{27} \frac{7.7}{15} \frac{8.7}{12}$

8.7

$\frac{7.2}{9} \frac{2.1}{14} \frac{10.3}{17} \frac{10.3}{19} \frac{9.2}{24} \frac{6.7}{33}$

Sta.	T.	H.I.		Elev.	
		292.88	✓		
T.P.	1.14	291.61	✓	9.43	290.45 ✓
85				2.2	289.4 ✓
86				4.7	286.9 ✓
87				8.1	283.5 ✓
88				11.9	279.7 ✓
T.P.	0.55	281.22	✓	10.97	280.67 ✓
+54	Farm Ent. L.			4.9	276.5 ✓
89				5.7	275.5 ✓
T.P.	0.35	271.82	✓	9.75	271.49 ✓
90				0.2	271.6 ✓
91				4.3	267.5 ✓
92				3.0	263.8 ✓
T.P.	0.77	261.20	✓	11.39	260.43 ✓
93				1.0	260.2 ✓
94				4.0	257.2 ✓
+92	Pri. Ent. R.			4.8	254.4 ✓
95				7.0	254.2 ✓

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Sta.	+	H.I.	-	Elev.	
		241.20	✓		
+69	15° 21' 42" Long.		8.0	252.9	✓
76			8.4	252.4	✓
+22	Per. Ent. L.		8.6	252.4	✓
77			8.2	253.0	✓
B.M.	3.66	258.65	6.11	254.99	✓
88			5.3	253.4	✓
99			5.2	253.5	✓
100			5.0	253.7	✓
101			4.7	253.8	✓
102			3.1	255.4	✓
+30			1.8	254.9	✓
			12.10	246.55	✓
+38			1.2	257.5	✓
T.P.	5.74	262.05	1.34	257.01	✓
+42A	Top of So. Rail.		5.21	257.87	✓
+55			5.2	257.7	✓

$\frac{9.7}{50}$ $\frac{10.5}{33}$ Invert $\frac{11.32}{20}$ $\frac{8.4}{16}$ 8.3 $\frac{8.1}{13}$ $\frac{12.15}{22}$ Invert $\frac{12.4}{22}$ $\frac{12.7}{33}$ $\frac{14.0}{50}$

$\frac{9.0}{33}$ $\frac{9.4}{22}$ $\frac{8.7}{15}$ 8.6 $\frac{8.7}{15}$ $\frac{12.4}{19}$ $\frac{14.0}{33}$

$\frac{8.7}{50}$ $\frac{9.0}{33}$ $\frac{8.9}{14}$ 8.6 $\frac{8.5}{14}$ $\frac{12.3}{20}$ $\frac{13.7}{26}$ $\frac{14.0}{33}$

$\frac{11.7}{33}$ $\frac{11.4}{20}$ $\frac{8.1}{14}$ 8.2 $\frac{8.5}{13}$ $\frac{13.4}{21}$ $\frac{14.2}{33}$

Spk 111 Tree 60' L. Sta. 97+25

$\frac{9.0}{33}$ $\frac{8.7}{22}$ $\frac{5.4}{15}$ 5.3 $\frac{5.1}{13}$ $\frac{10.8}{23}$ $\frac{11.7}{33}$

$\frac{7.8}{33}$ $\frac{8.7}{22}$ $\frac{5.9}{15}$ 5.2 $\frac{5.2}{14}$ $\frac{11.1}{23}$ $\frac{11.4}{33}$

$\frac{6.5}{33}$ $\frac{8.4}{21}$ $\frac{5.2}{14}$ 5.0 $\frac{5.0}{14}$ $\frac{9.5}{21}$ $\frac{11.7}{33}$

$\frac{10.4}{33}$ $\frac{10.2}{23}$ $\frac{5.0}{14}$ 4.9 $\frac{5.3}{14}$ $\frac{9.7}{21}$ $\frac{11.0}{29}$ $\frac{11.7}{33}$

$\frac{10.7}{33}$ $\frac{10.2}{25}$ $\frac{3.1}{15}$ 3.1 $\frac{3.1}{14}$ $\frac{7.3}{23}$ $\frac{9.9}{33}$

$\frac{7.1}{33}$ $\frac{8.3}{25}$ $\frac{1.8}{13}$ 1.8 $\frac{1.8}{15}$ $\frac{7.2}{22}$ $\frac{7.3}{33}$

Water Elev. of Lake on Right

$\frac{3.1}{33}$ $\frac{1.3}{12}$ 1.2 $\frac{1.5}{15}$ $\frac{2.7}{33}$

$\frac{0.42}{500}$ $\frac{1.47}{400}$ $\frac{2.53}{300}$ $\frac{3.40}{200}$ $\frac{4.33}{100}$ 5.21 $\frac{6.06}{100}$ $\frac{6.85}{200}$ $\frac{7.44}{300}$ $\frac{8.19}{400}$ $\frac{8.85}{500}$

$\frac{6.5}{33}$ $\frac{5.1}{14}$ 5.2 $\frac{5.6}{15}$ $\frac{6.6}{33}$

Sta.	+	H.2.	-	Elev.
		263.05 ✓		
+67			5.1	258.0 ✓
+79	15" O.P. 42 Long		5.0	258.0 ✓
103			4.4	258.7 ✓
+60			2.1	261.0 ✓
104			0.1	263.0 ✓
T.P.	10.95	273.85 ✓	0.15	262.90 ✓
+70	TRIV ENT R.		7.4	266.5 ✓
+86	" " L.		6.8	267.1 ✓
105			6.2	269.7 ✓
106			1.4	272.5 ✓
+66	TRIV ENT R.		1.1	272.8 ✓
T.P.	11.36	285.07 ✓	0.12	273.73 ✓
+56	TRIV ENT R.		10.0	275.1 ✓
107			8.0	277.1 ✓
108			3.6	281.5 ✓
T.P.	10.81	295.56 ✓	0.34	284.75 ✓
109			9.7	285.9 ✓
110			5.6	290.0 ✓
111			2.6	293.0 ✓
112			0.4	295.2 ✓
T.P.	6.23	300.93 ✓	0.86	294.70 ✓

Sta		H.I. 300.93 ✓		Elev.	
+73			5.2	295.7	✓
B.M.			3.31	297.62	✓
113			4.7	296.2	✓
114			4.8	296.1	✓
+38 Priv Ent R.			5.0	295.9	✓
115			6.1	294.8	✓
116			8.6	292.3	✓
117			11.4	289.5	✓
T.P.	1.27	289.67 ✓	12.53	288.40	✓
118			3.0	286.7	✓
119			5.8	283.9	✓
120			8.1	281.6	✓
121			10.7	279.0	✓
122			12.9	276.8	✓
T.P.	1.51	278.18 ✓	13.00	276.67	✓
123			4.1	274.1	✓
124			6.9	271.3	✓
125			10.2	268.0	✓
T.P.	0.75	266.18 ✓	12.75	265.43	✓
126			1.5	264.7	✓
127			4.9	261.3	✓
128			8.3	257.9	✓
B.M.			7.51	258.67	✓
129			12.3	253.9	✓
T.P.	0.47	253.67 ✓	12.98	253.20	✓

2 County Road "G"

50' left Sta 112150 Nail in 15" Oak.

Spike in Tel. Pole 30' R 128100

Sta	+	H.I	-	Elev.
		253.67 ✓		
130			3.9	249.8 ✓
131			6.4	247.3 ✓
+39	12" Cor. pipe.		6.7	247.0 ✓
132			6.5	247.2 ✓
133			6.5	247.2 ✓
134			6.5	247.2 ✓
135			6.3	247.4 ✓
T.P.	445	252.17 ✓	595	247.72 ✓
136			4.6	247.6
137			4.8	247.4
138			4.9	247.3
139			4.7	247.5
140			4.8	247.4
141			5.6	246.6
134	↳ Road to left.		5.7	246.5
142			5.6	246.6
+03	12" Cor. pipe.		5.6	246.6
143			4.7	247.5
144			4.8	247.4
T.P.	450	251.56 ✓	5.11	247.06 ✓
145			4.2	247.4
146			4.3	247.3
+71	^{Cor.} 18" V.I.T. pipe		4.8	246.8 247.0
+73.5	^{Cor.} 18" V.I.T. pipe.		4.8	246.8 247.8

Left \pm Right

70

$$\frac{9.35}{12.4} \leftarrow \text{Invert} \rightarrow \frac{10.4}{20.6}$$

Top of Stake.

$$\frac{8.88}{16.0} \leftarrow \text{Invert} \rightarrow \frac{8.82}{17.6}$$

$$\frac{7.8}{53.5} \leftarrow \text{Invert} \rightarrow \frac{8.5}{17.0}$$

$$\frac{7.8}{53.5} \leftarrow \text{Invert} \rightarrow \frac{8.9}{17.0}$$

\pm

	+	H.I	-	E/eV
34a		251.56		
			9.30	242.26 ✓
			10.05	241.51 ✓
147			5.7	245.9
148			4.3	247.3
149			3.4	248.2
150			2.1	249.5
151			1.1	250.5
T.P.	9.88	260.84 ✓	0.60	250.96 ✓
152			8.9	251.9
+43	Priv Ent Left		8.7	252.1
153			7.9	252.9
154			7.1	253.7
155			6.6	254.2
+44	Priv Ent Right		6.4	254.4
+66	" " Left		5.6	255.2
156			4.9	255.9
157			2.7	258.1
T.P.	12.06	272.30 ✓	0.60	260.24 ✓
158			10.6	261.7
159			6.5	265.8
+97	Farm Ent R.		2.4	269.9
160			2.2	270.1
+25	Farm Ent Left		0.9	271.4
T.P.	11.24	282.64 ✓	0.90	271.40

Water Level Lake on Right. }
" " Lake Josephine } Nov. 21, 23

Top of P.I

Nail in Telpole 14' Right 157730

Top of Cor. pipe 160430 N.E. rd.

Sta		H.I		Elev.
		282.64		
161			8.3	274.3
162			3.6	279.0
+50			1.8	281.8
163			0.2	282.4
+07	Priv Ent left		0.0	282.6
T.P.	7.29	289.57 ✓	0.36	282.22 ✓
164			4.5	285.1
+63	Priv Ent left		4.1	285.5
+86	" " Right		4.0	285.6
165			39	285.7
B.M.	5.40	292.72 ✓	2.25	287.32 ✓
166			6.8	285.9
+68	12" Cor. Pipe.		6.5	286.2
167			5.3	287.4
168			4.5	288.2
169			1.8	290.9
T.P.	11.32	303.84 ✓	0.20	292.52 ✓
+25	Priv Ent. left.		10.9	292.9
170			10.6	293.2
171			8.0	295.8
172			5.6	298.2
173			3.1	300.7
+57	Form Ent. left.		2.0	301.8
174			1.7	302.1

Top of Culvert S. end.

Spike in 12" Birch Tree 22' Right 164+93

$$\begin{array}{r} 141 \triangleleft \\ \hline 60.2 \end{array} \quad \text{Invert} \quad \begin{array}{r} \rightarrow 13.8 \\ \hline 39 \end{array}$$

Top of Culu. S. end.

Sta	+	H.S	-	Elev.
		303.84		
175			1.4	302.4
176			1.0	302.8
+17	Priv Ent. Right.		0.9	302.9
T.P.	3.44	306.26 ✓	0.42	303.42 ✓
+60	12" Vit. pipe		3.9	302.9
177			3.7	303.2
178			3.4	303.5
+44	Priv Ent Left		3.3	303.6
179			3.7	303.2
180			4.6	302.3
181			5.4	301.5
182			6.2	300.7
183			7.4	299.5
184			9.7	297.2
185			12.8	294.1
T.P.	0.69	294.98 ✓	12.57	294.29 ✓
186			4.1	290.9
187			7.3	287.7
188			11.0	284.0
T.P.	0.04	284.37 ✓	10.65	284.33 ✓
189			3.8	280.6
+37			4.6	279.8
B.M.			3.97	280.40 ✓
190			5.5	278.9

$\frac{13.24}{34.0}$ Invert $\frac{19.30}{28.0}$

Top of stake.

Top of stake.

Spike in 4" Oak stump 15' R. 194+37

Sta	+	M.I	-	Elev.
		284.37		
191			6.0	278.4
192			5.5	278.9
193			4.3	280.1
194			3.4	281.0
T.P.	8.90	290.48 ✓	2.79	281.58 ✓
195			2.1	282.4
196			6.7	283.8
197			5.8	284.7
198			4.6	285.9
+80	Priv Ent. Right.		4.0	286.5
199			3.5	287.0
200			3.0	287.5
+88	20" Vit. Cult.		2.9	287.6
201			1.8	288.7
T.P.	10.77	300.84 ✓	0.41	290.07 ✓
202			10.0	290.8
203			3.3	292.5
204	Priv Ent. Left.		7.1	293.7
205			5.9	294.9
+90	15" Vit Cult.		5.7	295.1
206			5.7	295.1
207			4.9	295.9
208			2.2	298.6
T.P.	11.42	311.84 ✓	0.42	300.42 ✓

L £ R

74

Top of Stake.

15.1 Invert 13.1
32 35

18.55 Invert 11.13
22 19

Sta	+	H.I	-	Elev.
		311.84		
209			10.7	301.1
210			7.8	304.0
211			5.1	306.7
212			3.8	308.0
213			3.8	308.0
214			4.0	307.8
215			5.3	306.5
	+60	15" Corr Ck N.	6.9	304.9
	+71.6	2 County Rd "E"	7.0	304.8
B.M.	1.23	307.38 ✓	5.69	306.15 ✓
216			3.2	304.1
217			4.1	303.3
218			5.0	302.4
	+	E. Bound Top of Rail	4.81	302.57 ✓
	+84	W " " " "	4.92	302.46 ✓
190			5.1	302.3
219			6.0	301.4
220			9.4	298.0
221			12.2	295.2
222			15.3	292.1

$$\frac{8.11}{19}$$
$$\text{Direct} \rightarrow \frac{7.17}{48}$$

Spike in 16" Oak N.E. corner of Road Inter section.
45°R. Sta 216.

Sta

+

H.I

-

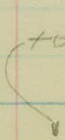
Elev.

Project 24-01
Lexington Avenue.

X-sections from station
104+00 to

Station	Elev.
109	285.9 ✓
108	281.5 ✓
107	277.1 ✓
+56 Priv. Ent. R.	275.1 ✓
+06 Priv. Ent. R.	272.8 ✓
106	272.5 ✓
+50	270.2
105	267.7 ✓
+86 Priv. Ent. L.	267.1 ✓
+70 Priv. Ent. R.	266.5 ✓
+20	262.2 ✓
104+00	263.0 ✓

+0.8



262.2

263.8

L. E. R.

 W.H.G. } Nov 22, 23
 P.G. }
 A.N. } cold.
 M.A. }
 = }
 77

$$\begin{array}{cccccccccccc} +2.7 & +2.1 & -0.2 & -1.0 & -0.4 & 0.0 & -0.3 & -1.0 & -1.1 & +1.2 & +0.3 \\ 33 & 23 & 19 & 18 & 14 & & 13 & 14 & 16 & 19 & 33 \end{array}$$

$$\begin{array}{cccccccccccccccc} +3.2 & +2.5 & -0.1 & -0.4 & -1.2 & -1.2 & -0.6 & -0.3 & 0.0 & -0.3 & -0.3 & -1.2 & -1.2 & -0.2 & +0.3 & +0.1 \\ 33 & 26 & 23 & 19 & 18 & 16 & 15 & 8 & & 7 & 11 & 12 & 14 & 16 & 27 & 33 \end{array}$$

$$\begin{array}{cccccccccccccccc} +3.0 & +2.0 & -0.4 & -1.1 & -1.7 & -0.8 & -0.4 & 0.0 & -0.4 & -0.4 & -1.5 & -1.5 & -0.8 & +0.4 \\ 33 & 26 & 24 & 18 & 17 & 13 & 8 & & 8 & 11 & 13 & 15 & 17 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +1.8 & +1.4 & -0.4 & -0.9 & -1.5 & -0.5 & -0.4 & & -0.3 & -0.5 & -1.0 & -1.7 \\ 33 & 26 & 23 & 17 & 15 & 13 & 8 & 6 & 8 & 15 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} +3.2 & +1.4 & +0.4 & -0.5 & -1.1 & -1.9 & -1.0 & -0.6 & & -0.5 & -0.3 & -0.9 \\ 33 & 29 & 25 & 24 & 17 & 16 & 13 & 7 & & 8 & 15 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} +3.2 & +1.1 & +0.8 & -0.8 & -1.0 & -1.8 & -0.6 & -0.5 & & -0.4 & -0.2 & -1.0 \\ 33 & 27 & 25 & 24 & 17 & 16 & 13 & 9 & & 8 & 15 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +0.9 & -0.9 & -1.0 & -2.0 & -0.5 & & -0.4 & -1.2 & -1.2 & -0.7 & -1.2 \\ 33 & 28 & 18 & 16 & 12 & & 12 & 14 & 16 & 17 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} -0.4 & 0.0 & -1.2 & -0.3 & & -0.1 & -1.0 & -1.0 & +0.3 & +0.2 \\ 33 & 18 & 15 & 12 & & 11 & 13 & 15 & 17 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +1.2 & +0.3 & 0.0 & & & -0.1 & -1.2 & -1.2 & +0.2 & +0.7 \\ 50 & 33 & 70 & & & 12 & 14 & 15 & 17 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +2.0 & +0.5 & -0.7 & 0.0 & -0.3 & & -0.3 & -0.5 & -1.0 & -2.1 \\ 33 & 24 & 19 & 15 & 11 & & 8 & 18 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} -2.2 & -1.8 & -0.2 & & & -0.3 & -0.9 & 0.0 & -0.7 \\ 33 & 18 & 15 & & & 11 & 15 & 16 & 33 \end{array}$$

Note: see level notes for X-sections
bet. sta 0100 to sta 10400

Station	Elev.
115	294.8 ✓
+43	295.9
+33 $\frac{1}{2}$ Farm Ent. R.	295.9 ✓
+22	295.9
114	296.1 ✓
+40	296.1 ✓
113	296.2 ✓
+50	295.8
+23 $\frac{1}{2}$ Co. Rd "C"	295.7 ✓
	295.2
112	295.1 ✓
111	293.0 ✓
110	290.0 ✓

$$\begin{array}{cccccc} +2.5 & +0.2 & -0.5 & -1.2 & -1.2 & -0.6 \\ +2.2 & 24 & 26 & \frac{1}{17} & \frac{1}{16} & \frac{1}{15} & \frac{1}{13} \\ \hline 33 & & & & & & \end{array}$$

$$\begin{array}{cccccc} -0.3 & -0.8 & -0.8 & +4.0 & +4.7 & +4.7 \\ \hline \frac{1}{11} & \frac{1}{13} & \frac{1}{15} & \frac{1}{23} & \frac{1}{30} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccccc} +0.8 & +1.3 & -0.3 & -0.4 & -1.2 & -0.4 \\ \hline \frac{1}{33} & \frac{1}{28} & \frac{1}{25} & \frac{1}{15} & \frac{1}{13} & \frac{1}{11} \end{array}$$

$$\begin{array}{cccc} -0.3 & +0.1 & +2.8 & +2.7 \\ \hline \frac{1}{12} & \frac{1}{20} & \frac{1}{26} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccccc} +0.8 & +1.1 & -0.3 & -0.6 & -1.2 & -0.4 \\ \hline \frac{1}{33} & \frac{1}{28} & \frac{1}{26} & \frac{1}{16} & \frac{1}{14} & \frac{1}{11} \end{array}$$

$$\begin{array}{cccc} -0.1 & +0.2 & +0.6 & +0.9 \\ \hline \frac{1}{8} & \frac{1}{13} & \frac{1}{23} & \frac{1}{50} \end{array}$$

to here 11/22/23

$$\begin{array}{cccccc} +0.9 & +1.5 & -0.6 & -0.7 & -1.2 & -0.5 \\ \hline \frac{1}{33} & \frac{1}{28} & \frac{1}{25} & \frac{1}{15} & \frac{1}{13} & \frac{1}{11} \end{array}$$

$$\begin{array}{ccc} +0.1 & +2.6 & +2.9 \\ \hline \frac{1}{20} & \frac{1}{26} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccccc} +1.0 & +1.7 & -0.4 & -0.5 & -1.2 & -0.5 \\ \hline \frac{1}{33} & \frac{1}{29} & \frac{1}{26} & \frac{1}{19} & \frac{1}{14} & \frac{1}{12} \end{array}$$

$$\begin{array}{cccccc} -0.4 & -0.9 & -0.9 & -0.5 & -0.2 & +2.0 & +2.2 & +2.4 \\ \hline \frac{1}{12} & \frac{1}{13} & \frac{1}{15} & \frac{1}{16} & \frac{1}{20} & \frac{1}{24} & \frac{1}{30} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccccc} +4.1 & +4.8 & 0.0 & 0.0 & -1.0 & -0.4 \\ \hline \frac{1}{33} & \frac{1}{25} & \frac{1}{22} & \frac{1}{16} & \frac{1}{14} & \frac{1}{12} \end{array}$$

$$\begin{array}{cccccc} -0.3 & -1.4 & -1.4 & -1.1 & +1.0 & +1.5 \\ \hline \frac{1}{12} & \frac{1}{14} & \frac{1}{16} & \frac{1}{17} & \frac{1}{21} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccc} +3.4 & +4.2 & 0.0 & -0.3 \\ \hline \frac{1}{33} & \frac{1}{25} & \frac{1}{20} & \frac{1}{10} \end{array}$$

$$\begin{array}{cccccc} -0.6 & -1.7 & -1.7 & +0.5 & +0.7 \\ \hline \frac{1}{16} & \frac{1}{19} & \frac{1}{20} & \frac{1}{23} & \frac{1}{33} \end{array}$$

$$\begin{array}{cc} -0.7 & -0.4 \\ \hline \frac{1}{33} & \frac{1}{18} \end{array}$$

$$\begin{array}{ccc} -0.4 & -0.9 & -1.9 \\ \hline \frac{1}{9} & \frac{1}{20} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccccc} -6.8 & -4.8 & -3.2 & -2.0 & -0.8 & -0.7 \\ \hline \frac{1}{400} & \frac{1}{300} & \frac{1}{200} & \frac{1}{100} & \frac{1}{50} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccccc} -0.8 & -2.7 & -4.9 & -2.4 & +13.0 & -17.0 \\ \hline \frac{1}{18} & \frac{1}{50} & \frac{1}{100} & \frac{1}{200} & \frac{1}{300} & \frac{1}{400} \end{array}$$

$$\begin{array}{cc} -1.2 & -0.6 \\ \hline \frac{1}{33} & \frac{1}{15} \end{array}$$

$$\begin{array}{ccc} -0.7 & -1.2 & -1.8 \\ \hline \frac{1}{16} & \frac{1}{30} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccc} -2.2 & -1.6 & -1.8 & -0.7 \\ \hline \frac{1}{33} & \frac{1}{22} & \frac{1}{16} & \frac{1}{12} \end{array}$$

$$\begin{array}{ccc} -0.5 & -1.2 & -1.4 \\ \hline \frac{1}{9} & \frac{1}{19} & \frac{1}{33} \end{array}$$

$$\begin{array}{cccc} +1.6 & +0.9 & -1.2 & -0.7 \\ \hline \frac{1}{33} & \frac{1}{18} & \frac{1}{15} & \frac{1}{14} \end{array}$$

$$\begin{array}{ccccc} -0.3 & -1.2 & -1.2 & +1.2 & +1.2 \\ \hline \frac{1}{13} & \frac{1}{15} & \frac{1}{17} & \frac{1}{20} & \frac{1}{33} \end{array}$$

Station	Elev.
124	271.3 ✓
+60	272.4
123	274.1 ✓
122	276.8 ✓
+60	277.8
121	279.0 ✓
120	281.6 <u>281.7</u> ✓
119	283.9 ✓
118	286.7 ✓
117	289.5 ✓
+50	290.9
116	292.3 ✓
115+67	293.5

Station	Elev.	
132	247.2	✓
+39	247.0	✓
131	247.3	✓
130	249.8	✓
129	253.9	✓
+50	255.7	
128	257.9	✓
+50	260.7	259.7
127	261.3	✓
+80 P.C.	262.1	
126	264.7	✓
125	268.0	✓

Left. £ Right 80

$$\frac{-1.5}{33} \quad \frac{-2.4}{30} \quad \frac{-2.0}{16} \quad \frac{-0.4}{12} \quad \frac{-0.2}{13} \quad \frac{-1.4}{33}$$

$$\frac{-3.4}{32} \quad \frac{-2.8}{22} \quad \frac{-0.3}{13} \quad \frac{-0.4}{13} \quad \frac{-3.2}{18} \quad \frac{-3.8}{33}$$

$$\frac{-1.7}{33} \quad \frac{-2.8}{31} \quad \frac{-2.4}{17} \quad \frac{-0.1}{13} \quad \frac{-0.2}{13} \quad \frac{-3.6}{19} \quad \frac{-4.0}{33}$$

$$\frac{-2.4}{33} \quad \frac{-2.4}{31} \quad \frac{-3.5}{30} \quad \frac{-3.4}{17} \quad \frac{-0.3}{12} \quad \frac{-0.1}{14} \quad \frac{-2.7}{20} \quad \frac{-3.5}{33}$$

$$\frac{-1.8}{33} \quad \frac{-4.0}{30} \quad \frac{-3.4}{25} \quad \frac{-0.6}{20} \quad \frac{-0.3}{13} \quad \frac{-0.4}{10} \quad \frac{-1.5}{14} \quad \frac{-1.1}{21} \quad \frac{-1.1}{33}$$

$$\frac{-1.0}{33} \quad \frac{-3.2}{30} \quad \frac{-3.4}{25} \quad \frac{-0.3}{20} \quad \frac{-0.2}{13} \quad \frac{-0.3}{12} \quad \frac{-0.6}{15} \quad \frac{-2.2}{18} \quad \frac{-2.2}{22} \quad \frac{0.0}{26} \quad \frac{+0.5}{33}$$

$$\frac{-0.3}{33} \quad \frac{-0.1}{30} \quad \frac{-3.4}{26} \quad \frac{-3.5}{22} \quad \frac{-0.5}{15} \quad \frac{-0.2}{12} \quad \frac{-0.1}{30} \quad \frac{-0.2}{33}$$

$$\frac{-0.7}{33} \quad \frac{-1.7}{26} \quad \frac{-3.5}{19} \quad \frac{-0.8}{14} \quad \frac{-0.1}{10} \quad \frac{0.0}{18} \quad \frac{-0.7}{20} \quad \frac{-0.7}{21} \quad \frac{0.0}{23} \quad \frac{+1.3}{33}$$

$$\frac{-1.7}{33} \quad \frac{-4.0}{24} \quad \frac{-4.0}{23} \quad \frac{-0.3}{15} \quad \frac{-0.1}{13} \quad \frac{-0.6}{15} \quad \frac{-0.6}{16} \quad \frac{+0.2}{18} \quad \frac{+1.0}{28} \quad \frac{+3.7}{29} \quad \frac{-4.0}{33}$$

$$\frac{-1.8}{33} \quad \frac{-4.1}{22} \quad \frac{-0.5}{14} \quad \frac{+0.1}{12} \quad \frac{-0.6}{14} \quad \frac{-0.6}{16} \quad \frac{+0.8}{17} \quad \frac{+1.5}{33}$$

$$\frac{-3.9}{33} \quad \frac{-4.2}{19} \quad \frac{-0.5}{12} \quad \frac{-0.2}{11} \quad \frac{-1.6}{16} \quad \frac{-0.6}{32}$$

$$\frac{-3.3}{33} \quad \frac{-3.4}{30} \quad \frac{-3.9}{17} \quad \frac{-0.6}{12} \quad \frac{-0.4}{11} \quad \frac{-4.2}{17} \quad \frac{-3.6}{33}$$

Station Elevation

141 246.6 ✓

+33 Road L. 247.4

140 247.4 ✓

+50 247.4

139 247.5 ✓

138 247.3 ✓

137 247.4 ✓

136 247.6 ✓

135 247.4 ✓

134 247.2 ✓

133 247.2 ✓

132+50 247.5

$\frac{-0.4}{70} \frac{-2.5}{100} \frac{-2.6}{22} \frac{-2.7}{17} \frac{0.0}{15} \frac{-0.2}{9} \quad \frac{-0.6}{9} \frac{-0.5}{13} \frac{-2.9}{18} \frac{-2.1}{33} \frac{-4.0}{100} \frac{-4.3}{180} \frac{-5.0}{290}$ W.E.

$\frac{4.0}{55} \frac{4.7}{46} \frac{-1.3}{33} \frac{-2.0}{18} \frac{-0.1}{14} \quad \frac{-0.5}{8} \frac{-0.3}{12} \frac{-3.1}{18} \frac{-3.4}{28} \quad \frac{-4.3}{175} \frac{-5.0}{270}$ W.E.

$\frac{+16.9}{65} \frac{+11.7}{40} \frac{+12}{35} \frac{+5.0}{33} \frac{0.0}{27} \frac{-0.4}{21} \frac{-1.5}{19} \frac{-1.5}{17} \frac{0.0}{15} \frac{-0.2}{9} \quad \frac{-0.7}{9} \frac{-0.5}{13} \frac{0.0}{18} \frac{-3.4}{33} \frac{-4.4}{100} \frac{-4.5}{180} \frac{-5.0}{290}$ W.E.

$\frac{+22.0}{75} \frac{+20.0}{55} \frac{+8.0}{47} \frac{+6.0}{46} \frac{-0.3}{21} \frac{-1.5}{18} \frac{-1.5}{16} \frac{-0.1}{13} \frac{-0.3}{9} \quad \frac{-0.7}{9} \frac{-0.4}{15} \frac{-2.9}{20} \frac{-3.4}{33} \frac{-4.4}{100}$

$\frac{+21.0}{75} \frac{+9.3}{55} \frac{+7.4}{41} \frac{+5.0}{40} \frac{-1.1}{20} \frac{-1.5}{17} \frac{-1.5}{16} \frac{-0.2}{14} \frac{-0.3}{8} \quad \frac{-0.5}{10} \frac{-0.4}{15} \frac{-2.3}{19} \frac{-2.3}{33}$

$\frac{+17.0}{47} \frac{+18.0}{50} \frac{+15.1}{40} \frac{+12.0}{60} \frac{-0.5}{21} \frac{-1.8}{20} \frac{-1.2}{18} \frac{-0.2}{15} \frac{-0.3}{9} \quad \frac{-0.4}{15} \frac{-2.7}{19} \frac{-3.4}{33}$

$\frac{+18.7}{60} \frac{+15.6}{46} \frac{+12.6}{34} \frac{+8.0}{33} \frac{-0.2}{21} \frac{-1.6}{17} \frac{-1.6}{16} \frac{-0.1}{12} \frac{-0.2}{8} \quad \frac{-0.3}{15} \frac{-3.0}{19} \frac{-3.4}{33}$

$\frac{+6.3}{46} \frac{+4.5}{28} \frac{-0.3}{23} \frac{-2.1}{18} \frac{-2.1}{16} \frac{-0.1}{11} \frac{-0.2}{8} \quad \frac{-0.5}{13} \frac{-3.0}{19} \frac{-3.4}{33}$

$\frac{48.1}{36} \frac{+2.3}{27} \frac{-0.4}{20} \frac{-1.1}{18} \frac{-1.1}{16} \frac{0.0}{14} \quad \frac{-0.2}{14} \frac{-2.2}{18} \frac{-3.1}{33}$

$\frac{-1.2}{33} \frac{-1.3}{19} \frac{-1.8}{15} \frac{-0.2}{12} \quad \frac{-0.5}{14} \frac{-2.1}{17} \frac{-1.8}{25} \frac{-1.8}{33}$

$\frac{-0.3}{33} \frac{-0.2}{24} \frac{-1.4}{21} \frac{-1.8}{17} \frac{-0.1}{13} \quad \frac{-0.4}{14} \frac{-1.8}{17} \frac{-2.7}{33}$

$\frac{-0.2}{33} \frac{-2.5}{28} \frac{-2.6}{23} \frac{-0.2}{15} \quad \frac{-0.5}{13} \frac{-2.2}{23} \frac{-2.6}{33}$

Station	Elev
149	248.2 ✓
148	247.3 ✓
147	245.9 ✓
+71	246.8 <u>247.8</u>
146	247.3 ✓
145	247.4 ✓
144	247.4 ✓
+50	247.4 ✓
143	247.5 ✓
+03	246.6 ✓
142	246.6 ✓
141+34	246.5 ✓

$$\begin{array}{ccc} -2.0 & -1.4 & -0.2 \\ \hline 33 & 15 & 12 \end{array} \quad \begin{array}{ccc} -0.4 & -4.4 & -4.6 \\ \hline 15 & 23 & 33 \end{array}$$

$$\begin{array}{ccc} -0.8 & -1.0 & -0.2 \\ \hline 33 & 14 & 11 \end{array} \quad \begin{array}{cc} -0.1 & -0.8 \\ \hline 13 & 33 \end{array}$$

$$\begin{array}{ccc} -0.8 & -1.3 & -0.4 \\ \hline 33 & 15 & 11 \end{array} \quad \begin{array}{ccc} -0.3 & -3.4 & -3.9 & -4.5 \\ \hline 16 & 21 & 33 & 45 = \text{W.E.} \end{array}$$

$$\begin{array}{ccc} -5.2 & 3.8 & -1.0 & -1.1 & -1.5 & -0.3 \\ \hline 83 & 65 & 50 & 33 & 16 & 11 \end{array} \quad \begin{array}{ccc} -0.7 & -3.4 & -4.2 \\ \hline 14 & 20 & 33 = \text{W.E.} \end{array}$$

Lake Josephine

$$\begin{array}{ccc} -5.6 & -1.9 & -1.5 & -1.6 & -0.5 \\ \hline 58 & 40 & 23 & 17 & 10 \end{array} \quad \begin{array}{ccc} -0.6 & -4.4 & -4.2 & -4.2 \\ \hline 12 & 18 & 33 & 46 = \text{W.E.} \end{array}$$

$$\begin{array}{ccc} -2.0 & -1.7 & -0.4 \\ \hline 33 & 16 & 13 \end{array} \quad \begin{array}{ccc} -0.9 & -3.7 & -4.6 & -4.8 & -4.8 \\ \hline 13 & 21 & 33 & 100 & 200 = \text{W.E.} \end{array}$$

$$\begin{array}{ccc} +7.6 & +3.4 & -0.4 & -1.2 & -1.2 & -0.4 & -0.1 \\ \hline 50 & 33 & 22 & 21 & 19 & 17 & 11 \end{array} \quad \begin{array}{ccc} -0.4 & -2.1 & -3.0 & -4.0 & -4.2 & -4.9 \\ \hline 13 & 17 & 33 & 100 & 200 & 235 = \text{W.E.} \end{array}$$

$$\begin{array}{ccc} +7.2 & +3.5 & +0.1 & -0.8 & -0.6 & 0.0 \\ \hline 50 & 33 & 22 & 18 & 16 & 11 \end{array} \quad \begin{array}{ccc} -0.5 & -0.4 & -1.2 & -1.2 & -0.9 & -2.1 & 4.5 & -4.9 \\ \hline 9 & 13 & 15 & 16 & 18 & 33 & 200 & 270 \end{array}$$

$$\begin{array}{ccc} -0.0 & -0.6 & -1.3 & -1.4 & -0.6 & -0.1 \\ \hline 66 & 33 & 20 & 19 & 17 & 11 \end{array} \quad \begin{array}{ccc} -0.6 & -0.6 & -1.8 & -1.8 & -2.8 & -3.5 & -2.7 & -4.6 \\ \hline 9 & 13 & 15 & 16 & 33 & 50 & 160 & 258 = \text{W.E.} \end{array}$$

$$\begin{array}{ccc} -1.3 & -1.1 & -0.4 \\ \hline 33 & 17 & 10 \end{array}$$

$$\begin{array}{ccc} -0.3 & -3.0 & -3.1 & -3.2 & -3.6 & -3.6 \\ \hline 14 & 19 & 33 & 100 & 200 & 250 = \text{W.E.} \end{array}$$

$$\begin{array}{ccc} -0.2 & -0.6 & -1.2 & -1.0 & -0.2 \\ \hline 56 & 44 & 33 & 17 & 11 \end{array}$$

$$\begin{array}{ccc} -0.3 & -3.0 & -3.1 & -3.3 & -3.6 & -3.6 \\ \hline 14 & 19 & 33 & 100 & 200 & 250 = \text{W.E.} \end{array}$$

$$\begin{array}{ccc} & & & \text{E.d.} \\ -2.8 & -2.8 & -0.1 & -0.2 \\ \hline 33 & 23 & 17 & 9 \end{array}$$

$$\begin{array}{ccc} -0.6 & -0.4 & -2.8 & -3.0 & -4.0 & -4.0 \\ \hline 09 & 19 & 19 & 33 & 200 & 260 = \text{W.E.} \end{array}$$

Note: (W.E. = Waters Edge)

Station	Elev.
155 + 53	255.0
+14 PIVENT R.	254.4 ✓
155	254.2 ✓
154	253.7 ✓
153	252.9 ✓
+68	252.3
+43 PIVENT L.	252.1 ✓
152	251.9 ✓
+50	251.4
151	250.5 ✓
+50	250.0
150	249.5 ✓

$$\begin{array}{ccccc} +3.1 & +2.1 & -2.1 & -2.1 & 0.0 \\ \hline 33 & 20 & 14 & 13 & 11 \end{array} \quad \begin{array}{ccccc} -0.5 & -2.4 & -2.4 & -0.5 & -0.5 \\ \hline 16 & 21 & 23 & 27 & 33 \end{array}$$

$$\begin{array}{ccccc} +4.5 & +4.3 & -1.5 & -1.5 & -0.2 \\ \hline 33 & 21 & 14 & 13 & 11 \end{array} \quad \begin{array}{cc} -0.1 & -0.2 \\ \hline 11 & 33 \end{array}$$

$$\begin{array}{ccccc} +5.8 & +5.2 & -1.3 & -1.3 & 0.0 \\ \hline 33 & 27 & 15 & 14 & 11 \end{array} \quad \begin{array}{ccccc} -0.2 & -1.5 & +5 & +1.0 & 0.0 \\ \hline 12 & 14 & 15 & 18 & 33 \end{array}$$

$$\begin{array}{ccccc} +6.6 & +6.6 & -0.8 & -0.8 & 0.0 \\ \hline 33 & 25 & 16 & 14 & 12 \end{array} \quad \begin{array}{ccccc} -0.1 & -1.1 & -1.1 & +1.4 & +2.4 \\ \hline 11 & 13 & 15 & 19 & 33 \end{array}$$

$$\begin{array}{ccccc} +7.7 & +7.7 & -1.1 & -1.1 & -0.1 \\ \hline 33 & 25 & 16 & 14 & 12 \end{array} \quad \begin{array}{cc} -0.4 & +0.8 \\ \hline 14 & 30 \end{array} \text{ face of Bidg.}$$

$$\begin{array}{ccccc} +6.7 & +6.7 & -1.0 & -1.0 & 0.0 \\ \hline 33 & 26 & 17 & 15 & 12 \end{array} \quad \begin{array}{cc} -0.4 & +0.5 \\ \hline 12 & 33 \end{array}$$

$$\begin{array}{ccccc} +2.5 & +2.4 & +0.1 & & \\ \hline 33 & 30 & 12 & & \end{array} \quad \begin{array}{ccccc} -0.5 & -0.8 & +0.9 & +0.6 & \\ \hline 14 & 14 & 23 & 33 & \end{array} \text{ To here Nov 23, 23}$$

$$\begin{array}{ccccc} +2.5 & +3.0 & -0.7 & -1.2 & -1.2 & -0.3 \\ \hline 33 & 22 & 17 & 16 & 15 & 13 \end{array} \quad \begin{array}{ccccc} -0.2 & -1.3 & -1.3 & +0.1 & +0.1 \\ \hline 17 & 19 & 22 & 24 & 33 \end{array}$$

$$\begin{array}{ccccc} +1.7 & +0.2 & -0.9 & +0.2 & \\ \hline 33 & 19 & 17 & 14 & \end{array} \quad \begin{array}{ccccc} -0.5 & -0.3 & -1.2 & & \\ \hline 8 & 18 & 33 & & \end{array}$$

$$\begin{array}{ccccc} +0.8 & -0.6 & -4.2 & -0.2 & \\ \hline 33 & 19 & 17 & 13 & \end{array} \quad \begin{array}{ccccc} -0.7 & -5.8 & -6.4 & & \\ \hline 16 & 29 & 33 & & \end{array}$$

$$\begin{array}{ccccc} -0.9 & -0.7 & -1.0 & -1.0 & 0.0 \\ \hline 33 & 18 & 17 & 16 & 13 \end{array} \quad \begin{array}{ccccc} -0.5 & -5.9 & -6.1 & & \\ \hline 17 & 28 & 33 & & \end{array}$$

$$\begin{array}{ccccc} -0.7 & -0.9 & -0.8 & -0.8 & -0.2 \\ \hline 33 & 19 & 15 & 13 & 11 \end{array} \quad \begin{array}{ccccc} -0.8 & -5.5 & -5.8 & & \\ \hline 13 & 21 & 33 & & \end{array}$$

Station	Elev.
+50	280.8 <u>281.8</u> ✓
162	279.0 ✓
161	274.3 ✓
+25	271.4 ✓
160	270.1 ✓
+75	269.8
159	265.8 ✓
158	261.7 ✓
157	258.1 ✓
156	255.9 ✓
+79	255.5
155+66 PrivEnt.L.	255.2 ✓

$$\frac{+5.0}{34} \frac{+0.6}{29} \frac{-0.2}{19} \frac{-1.2}{17} \frac{-1.2}{15} \frac{-0.7}{14}$$

$$\frac{-0.3}{15} \frac{-0.7}{16} \frac{-0.7}{18} \frac{+0.8}{20} \frac{+7.6}{33}$$

$$\frac{+5.1}{36} \frac{+0.9}{31} \frac{+0.2}{19} \frac{-1.1}{17} \frac{-1.1}{16} \frac{-0.2}{15}$$

$$\frac{-0.3}{10} \frac{-1.2}{13} \frac{-1.2}{14} \frac{-0.1}{15} \frac{+1.0}{21} \frac{+7.3}{30} \frac{+7.6}{33}$$

$$\frac{+1.2}{34} \frac{+0.1}{30} \frac{+0.2}{21} \frac{-0.8}{18} \frac{0.0}{13}$$

$$\frac{-0.1}{13} \frac{-0.6}{14} \frac{-0.6}{15} \frac{+0.9}{18} \frac{+1.2}{23} \frac{+5.8}{28} \frac{+7.1}{33}$$

$$\frac{-0.8}{33} \frac{-0.5}{12}$$

$$\frac{+0.2}{14} \frac{-0.9}{15} \frac{-0.9}{16} \frac{+0.1}{19} \frac{+1.2}{28} \frac{+2.2}{30} \frac{+2.4}{33}$$

$$\frac{-2.5}{33} \frac{-1.9}{26} \frac{-0.7}{18}$$

$$\frac{-0.3}{7} \frac{+0.8}{33}$$

$$\frac{-6.2}{33} \frac{-6.0}{32} \frac{-0.5}{24}$$

$$\frac{0.9}{18} \frac{-2.2}{26} \frac{-1.7}{33}$$

$$\frac{-10.7}{34} \frac{-1.0}{20}$$

$$\frac{-0.6}{15} \frac{-11.2}{30} \frac{-11.3}{33}$$

$$\frac{-7.4}{33} \frac{-6.6}{29} \frac{-0.5}{19}$$

$$\frac{-0.1}{15} \frac{-6.7}{25} \frac{-7.6}{33}$$

$$\frac{-11.0}{40} \frac{-11.0}{33} \frac{-10.4}{32} \frac{-0.5}{15}$$

$$\frac{-0.3}{16} \frac{-10.6}{31} \frac{-11.6}{33} \frac{-11.6}{40}$$

$$\frac{-3.4}{33} \frac{-2.7}{20} \frac{-3.3}{18} \frac{-3.3}{17} \frac{-0.5}{14}$$

$$\frac{-0.3}{21} \frac{-4.8}{33}$$

$$\frac{+0.2}{33} \frac{+0.3}{18} \frac{-2.6}{16} \frac{-2.6}{15} \frac{-0.2}{12}$$

$$\frac{-0.4}{21} \frac{-3.2}{24} \frac{-2.6}{33}$$

$$\frac{+1.4}{50} \frac{+1.4}{33} \frac{+0.3}{12}$$

$$\frac{-0.4}{13} \frac{-2.8}{17} \frac{-2.8}{19} \frac{-1.0}{21} \frac{-1.5}{33}$$

Station	Elev.
+85 Priv. Ent. L.	292.9 ✓
169	290.9 ✓
168	288.2 ✓
167	287.4 ✓
+68	286.2 ✓
166	285.9 ✓
165	285.7 ✓
+86 Priv. Ent. R.	285.6 ✓
+63	285.5 ✓
164	285.1 ✓
+07 Priv. Ent. L.	282.6 ✓
163	282.4 ✓

L

4

R

85

$$\begin{array}{r} +2.1 \\ 50 \end{array} \quad \begin{array}{r} +2.2 \\ 33 \end{array} \quad \begin{array}{r} +0.2 \\ 10 \end{array}$$

$$\begin{array}{r} +0.1 \\ 14 \end{array} \quad \begin{array}{r} -0.8 \\ 16 \end{array} \quad \begin{array}{r} -0.8 \\ 17 \end{array} \quad \begin{array}{r} +0.7 \\ 19 \end{array} \quad \begin{array}{r} +1.4 \\ 27 \end{array} \quad \begin{array}{r} +5.8 \\ 33 \end{array}$$

$$\begin{array}{r} +2.5 \\ 33 \end{array} \quad \begin{array}{r} +0.7 \\ 30 \end{array} \quad \begin{array}{r} +0.2 \\ 20 \end{array} \quad \begin{array}{r} -0.9 \\ 18 \end{array} \quad \begin{array}{r} -0.9 \\ 16 \end{array} \quad \begin{array}{r} +0.2 \\ 14 \end{array}$$

$$\begin{array}{r} +0.3 \\ 13 \end{array} \quad \begin{array}{r} -0.3 \\ 15 \end{array} \quad \begin{array}{r} -0.3 \\ 17 \end{array} \quad \begin{array}{r} +0.4 \\ 19 \end{array} \quad \begin{array}{r} +0.8 \\ 30 \end{array} \quad \begin{array}{r} +2.0 \\ 31 \end{array} \quad \begin{array}{r} +2.0 \\ 33 \end{array}$$

$$\begin{array}{r} -2.7 \\ 33 \end{array} \quad \begin{array}{r} -2.2 \\ 28 \end{array} \quad \begin{array}{r} +0.1 \\ 26 \end{array}$$

$$\begin{array}{r} -0.2 \\ 22 \end{array} \quad \begin{array}{r} -1.9 \\ 26 \end{array} \quad \begin{array}{r} -2.4 \\ 33 \end{array}$$

$$\begin{array}{r} -4.5 \\ 33 \end{array} \quad \begin{array}{r} -0.3 \\ 25 \end{array}$$

$$\begin{array}{r} -0.4 \\ 20 \end{array} \quad \begin{array}{r} -6.3 \\ 29 \end{array} \quad \begin{array}{r} -6.4 \\ 33 \end{array}$$

$$\begin{array}{r} -4.7 \\ 33 \end{array} \quad \begin{array}{r} -4.7 \\ 32 \end{array} \quad \begin{array}{r} -0.1 \\ 24 \end{array}$$

$$\begin{array}{r} -0.2 \\ 20 \end{array} \quad \begin{array}{r} -6.5 \\ 32 \end{array} \quad \begin{array}{r} -7.8 \\ 40 \end{array}$$

$$\begin{array}{r} -3.4 \\ 33 \end{array} \quad \begin{array}{r} 3.0 \\ 30 \end{array} \quad \begin{array}{r} -0.7 \\ 24 \end{array}$$

$$\begin{array}{r} -0.3 \\ 18 \end{array} \quad \begin{array}{r} -5.1 \\ 28 \end{array} \quad \begin{array}{r} -5.3 \\ 33 \end{array}$$

$$\begin{array}{r} -2.1 \\ 33 \end{array} \quad \begin{array}{r} -2.0 \\ 27 \end{array} \quad \begin{array}{r} -0.7 \\ 25 \end{array}$$

$$\begin{array}{r} +0.3 \\ 19 \end{array} \quad \begin{array}{r} +0.1 \\ 33 \end{array}$$

$$\begin{array}{r} -1.6 \\ 33 \end{array} \quad \begin{array}{r} -0.3 \\ 11 \end{array}$$

$$\begin{array}{r} +0.5 \\ 33 \end{array} \quad \begin{array}{r} +0.9 \\ 50 \end{array}$$

$$\begin{array}{r} +0.5 \\ 50 \end{array} \quad \begin{array}{r} +0.3 \\ 33 \end{array} \quad \begin{array}{r} +0.1 \\ 27 \end{array}$$

$$\begin{array}{r} 0.9 \\ 19 \end{array} \quad \begin{array}{r} -0.4 \\ 22 \end{array} \quad \begin{array}{r} +1.5 \\ 26 \end{array} \quad \begin{array}{r} +2.0 \\ 33 \end{array}$$

$$\begin{array}{r} +4.9 \\ 33 \end{array} \quad \begin{array}{r} +4.4 \\ 31 \end{array} \quad \begin{array}{r} +0.2 \\ 26 \end{array} \quad \begin{array}{r} -0.1 \\ 19 \end{array} \quad \begin{array}{r} -1.0 \\ 17 \end{array} \quad \begin{array}{r} -1.0 \\ 16 \end{array} \quad \begin{array}{r} -0.3 \\ 12 \end{array}$$

$$\begin{array}{r} -0.2 \\ 13 \end{array} \quad \begin{array}{r} -1.0 \\ 15 \end{array} \quad \begin{array}{r} -1.0 \\ 16 \end{array} \quad \begin{array}{r} +2.8 \\ 22 \end{array} \quad \begin{array}{r} +2.8 \\ 33 \end{array}$$

$$\begin{array}{r} +3.9 \\ 57 \end{array} \quad \begin{array}{r} +1.9 \\ 33 \end{array} \quad \begin{array}{r} -0.4 \\ 9 \end{array}$$

$$\begin{array}{r} +0.2 \\ 14 \end{array} \quad \begin{array}{r} -0.9 \\ 17 \end{array} \quad \begin{array}{r} -0.9 \\ 19 \end{array} \quad \begin{array}{r} +4.4 \\ 24 \end{array} \quad \begin{array}{r} +5.0 \\ 33 \end{array}$$

$$\begin{array}{r} +5.4 \\ 35 \end{array} \quad \begin{array}{r} +1.6 \\ 36 \end{array} \quad \begin{array}{r} -0.1 \\ 14 \end{array} \quad \begin{array}{r} -0.6 \\ 9 \end{array}$$

$$\begin{array}{r} +0.2 \\ 14 \end{array} \quad \begin{array}{r} -0.8 \\ 16 \end{array} \quad \begin{array}{r} -0.8 \\ 18 \end{array} \quad \begin{array}{r} 0.0 \\ 19 \end{array} \quad \begin{array}{r} +4.8 \\ 26 \end{array} \quad \begin{array}{r} +5.0 \\ 33 \end{array}$$

Station	Elev.
178	303.5 ✓
+65	303.4
177	303.2 ✓
+60	302.9 ✓
+17 Priv. Ent. R.	302.9 ✓
176	302.8 ✓
175	302.4 ✓
174	302.1 ✓
+57 Priv. Ent. L.	301.8 ✓
173	300.7 ✓
172	298.2 ✓
171	295.8 ✓
170	293.2 ✓

$$\begin{array}{cccc} -0.3 & -0.1 & -0.8 & -0.3 \\ \hline 33 & 22 & 20 & 18 \end{array} \quad \begin{array}{cccc} +0.2 & -0.3 & +0.6 & +1.8 \\ \hline 21 & 22 & 29 & 33 \end{array}$$

$$\begin{array}{ccc} -2.8 & -2.3 & 0.0 \\ \hline 33 & 25 & 22 \end{array} \quad \begin{array}{ccc} -0.2 & -1.2 & -0.1 \\ \hline 20 & 23 & 25 \end{array} \quad \begin{array}{c} -0.2 \\ \hline 33 \end{array}$$

$$\begin{array}{ccc} -8.4 & -8.4 & -0.6 \\ \hline 33 & 31 & 21 \end{array} \quad \begin{array}{ccc} -0.7 & -3.7 & -3.8 \\ \hline 22 & 26 & 33 \end{array}$$

$$\begin{array}{ccc} -8.0 & -8.0 & -0.5 \\ \hline 33 & 32 & 20 \end{array} \quad \begin{array}{ccc} -0.1 & -5.0 & -5.0 \\ \hline 22 & 27 & 33 \end{array}$$

$$\begin{array}{ccc} -7.9 & -7.7 & -0.8 \\ \hline 33 & 31 & 22 \end{array} \quad \begin{array}{ccc} -0.2 & -1.1 & -1.0 \\ \hline 11 & 33 & 50 \end{array}$$

$$\begin{array}{ccc} -7.9 & -7.4 & -0.9 \\ \hline 33 & 29 & 22 \end{array} \quad \begin{array}{cccc} -0.2 & -1.2 & -1.2 & -0.5 \\ \hline 18 & 19 & 21 & 22 \end{array} \quad \begin{array}{c} +0.8 \\ \hline 33 \end{array}$$

$$\begin{array}{cccc} +0.4 & +0.4 & -0.3 & -0.2 \\ \hline 33 & 31 & 29 & 21 \end{array} \quad \begin{array}{ccc} -1.2 & -1.2 & -0.4 \\ \hline 20 & 18 & 17 \end{array} \quad \begin{array}{cccc} +0.5 & -0.2 & -0.2 & +0.9 \\ \hline 15 & 16 & 18 & 20 \end{array} \quad \begin{array}{ccc} +1.7 & +2.0 & +7.5 \\ \hline 25 & 31 & 33 \end{array}$$

$$\begin{array}{cccc} +0.2 & +0.2 & -0.2 & -0.2 \\ \hline 33 & 30 & 29 & 21 \end{array} \quad \begin{array}{ccc} -1.1 & -1.1 & -0.2 \\ \hline 20 & 18 & 17 \end{array} \quad \begin{array}{cccc} -0.2 & -0.9 & -0.9 & 0.0 \\ \hline 15 & 16 & 18 & 19 \end{array} \quad \begin{array}{ccc} +0.8 & +3.8 & +3.6 \\ \hline 26 & 30 & 33 \end{array}$$

$$\begin{array}{ccc} -2.1 & 0.0 & -0.1 \\ \hline 50 & 35 & 20 \end{array} \quad \begin{array}{ccc} 0.0 & -0.9 & -0.9 \\ \hline 18 & 20 & 22 \end{array} \quad \begin{array}{ccc} +0.2 & +0.9 \\ \hline 23 & 33 \end{array}$$

$$\begin{array}{ccc} -2.3 & -1.1 \\ \hline 33 & 30 \end{array} \quad \begin{array}{ccc} -0.3 & -1.2 & -1.1 \\ \hline 25 & 27 & 33 \end{array}$$

$$\begin{array}{cccc} +0.8 & +0.8 & +0.1 & 0.0 \\ \hline 33 & 30 & 28 & 21 \end{array} \quad \begin{array}{ccc} -1.1 & -1.1 & -0.3 \\ \hline 20 & 18 & 13 \end{array} \quad \begin{array}{ccc} -0.1 & +0.1 \\ \hline 18 & 33 \end{array}$$

$$\begin{array}{cccc} +1.4 & +1.4 & 0.0 & 0.0 \\ \hline 53 & 30 & 27 & 18 \end{array} \quad \begin{array}{ccc} -1.2 & -1.2 & -0.2 \\ \hline 16 & 15 & 13 \end{array} \quad \begin{array}{cccc} -0.1 & -1.0 & -1.0 & 0.0 \\ \hline 15 & 17 & 18 & 19 \end{array} \quad \begin{array}{ccc} +0.6 & +1.6 & +1.6 \\ \hline 30 & 32 & 33 \end{array}$$

$$\begin{array}{cccc} +6.3 & +1.4 & +0.7 & -1.0 \\ \hline 33 & 27 & 18 & 17 \end{array} \quad \begin{array}{ccc} -1.0 & -1.0 & 0.0 \\ \hline 16 & 16 & 12 \end{array} \quad \begin{array}{cccc} +0.1 & -0.7 & -0.7 & +0.6 \\ \hline 14 & 17 & 18 & 20 \end{array} \quad \begin{array}{ccc} +1.4 & +5.6 \\ \hline 27 & 33 \end{array}$$

Station	Elev.	
189	280.6	✓
188	284.0	✓
187	287.7	✓
+55	289.1	
186	290.9	✓
185	294.1	✓
184	297.2	✓
183	299.5	✓
182	300.7	✓
181	301.5	✓
180	302.3	✓
179	303.2	✓
178+44 Priv. Ent. L.	303.6	✓

L.

#

R

87

$$\begin{array}{ccccc} -5.6 & -4.0 & -1.1 & -0.12 & -1.2 & +0.7 & +2.1 \\ \hline 33 & 26 & 21 & 16 & 18 & 21 & 33 \end{array}$$

$$\begin{array}{ccccc} -3.7 & -2.4 & -2.8 & -2.8 & -1.1 & -0.1 & -1.2 & -1.2 & +3.2 & +4.0 \\ \hline 33 & 24 & 21 & 20 & 19 & 12 & 18 & 20 & 24 & 33 \end{array}$$

$$\begin{array}{ccccc} +2.7 & +4.0 & -1.7 & -1.5 & -0.8 & -0.8 & -1.0 & -1.0 & +6.3 & +5.8 \\ \hline 33 & 24 & 20 & 19 & 18 & 11 & 16 & 17 & 19 & 25 & 33 \end{array}$$

$$\begin{array}{ccccc} +4.8 & +4.7 & -1.4 & -1.2 & -0.6 & -0.4 & -1.5 & -1.5 & +1.6 & +2.0 \\ \hline 33 & 31 & 24 & 23 & 22 & 16 & 18 & 20 & 24 & 33 \end{array}$$

$$\begin{array}{ccccc} -1.7 & -1.8 & -0.8 & -0.4 & -0.5 & -4.1 & -4.5 \\ \hline 33 & 30 & 24 & 11 & 19 & 26 & 33 \end{array}$$

$$\begin{array}{ccccc} -7.8 & -1.1 & -0.6 & -0.5 & -0.9 & -4.2 & -5.0 \\ \hline 33 & 22 & 11 & 12 & 24 & 30 & 33 \end{array}$$

$$\begin{array}{ccccc} -8.0 & -7.4 & -1.4 & -0.4 & -1.6 & -2.0 \\ \hline 33 & 31 & 23 & 24 & 25 & 33 \end{array}$$

$$\begin{array}{ccccc} -3.0 & -3.4 & -0.8 & -2.2 & -2.2 & -1.0 & -0.4 & -0.2 & -1.0 & -1.0 & +4.0 & +4.4 \\ \hline 33 & 27 & 23 & 21 & 20 & 19 & 16 & 18 & 19 & 20 & 28 & 33 \end{array}$$

$$\begin{array}{ccccc} -2.0 & +0.7 & -1.5 & -1.5 & -0.8 & -0.4 & -1.0 & -1.0 & +5.8 & +6.0 \\ \hline 33 & 25 & 20 & 19 & 18 & 16 & 17 & 18 & 28 & 33 \end{array}$$

$$\begin{array}{ccccc} +2.0 & +3.0 & -1.2 & -1.2 & -0.9 & +0.1 & -0.5 & -0.5 & +5.2 & +5.4 \\ \hline 33 & 26 & 19 & 18 & 17 & 16 & 17 & 18 & 27 & 33 \end{array}$$

$$\begin{array}{ccccc} +0.9 & +1.1 & -1.2 & -0.7 & -0.3 & -0.9 & -0.9 & -0.1 & -0.4 \\ \hline 33 & 29 & 24 & 20 & 19 & 20 & 21 & 23 & 33 \end{array}$$

$$\begin{array}{ccccc} -0.5 & -0.3 & -0.4 & -1.4 & -1.6 & -0.9 & -0.5 \\ \hline 33 & 20 & 22 & 23 & 27 & 29 & 33 \end{array}$$

$$\begin{array}{ccccc} -1.0 & -0.8 & -0.2 & 0.0 & -1.2 & -1.4 & +1.0 \\ \hline 50 & 33 & 21 & 19 & 22 & 27 & 33 \end{array}$$

Station	Elev	
198 +14	286.1	
198	285.9	✓
+55	285.3	
197	284.7	✓
196	283.8	✓
195	282.4	✓
+70	282.1	
194	281.0	✓
193	280.1	✓
192	278.9	✓
191	278.4	✓
190	278.9	✓
89+37	279.8	✓

Station	Elev.
205	294.9 ✓
+64	294.6
204 ^{Priv.} Ent. L.	293.7 ✓
203	292.5 ✓
202	290.8 ✓
+80	290.4
+50	289.8
201	288.7 ✓
+08	287.6 ✓
200	287.5 ✓
199	287.0 ✓
+30 Priv. Ent. R.	286.5 ✓
198+22	286.3

$$\frac{-0.4}{33} \quad \frac{-1.6}{19} \quad \frac{-2.5}{16} \quad \frac{-0.4}{13} \quad \frac{-0.2}{13} \quad \frac{-1.0}{15} \quad \frac{-1.0}{16} \quad \frac{-0.3}{17} \quad \frac{-0.3}{33}$$

$$\frac{-0.1}{33} \quad \frac{-1.3}{18} \quad \frac{-1.6}{16} \quad \frac{-0.3}{14} \quad \frac{-0.2}{13} \quad \frac{-0.8}{14} \quad \frac{-0.8}{16} \quad \frac{+2.9}{19} \quad \frac{+3.1}{33}$$

$$\frac{-1.2}{50} \quad \frac{-1.2}{33} \quad \frac{-0.8}{13} \quad \frac{-0.4}{12} \quad \frac{-1.6}{15} \quad \frac{-1.6}{16} \quad \frac{+0.2}{19} \quad \frac{+0.5}{33}$$

where Nov. 26, 23

$$\frac{-0.5}{33} \quad \frac{0.0}{21} \quad \frac{-2.7}{17} \quad \frac{-2.7}{16} \quad \frac{-0.7}{13} \quad \frac{-0.4}{12} \quad \frac{-1.2}{15} \quad \frac{-1.2}{17} \quad \frac{-0.5}{18} \quad \frac{-1.0}{33}$$

$$\frac{+7.1}{33} \quad \frac{+7.1}{30} \quad \frac{-2.4}{20} \quad \frac{-2.5}{17} \quad \frac{-0.5}{14} \quad \frac{-0.5}{12} \quad \frac{-1.3}{14} \quad \frac{-1.2}{16} \quad \frac{+6.8}{24} \quad \frac{+6.5}{33}$$

$$\frac{+5.8}{33} \quad \frac{+6.3}{30} \quad \frac{-2.1}{20} \quad \frac{-2.1}{16} \quad \frac{-0.5}{15} \quad \frac{-0.7}{14} \quad \frac{-1.2}{15} \quad \frac{-1.1}{18} \quad \frac{+8.7}{28} \quad \frac{+8.5}{33}$$

$$\frac{-1.5}{33} \quad \frac{-1.0}{29} \quad \frac{-4.7}{24} \quad \frac{-4.7}{21} \quad \frac{-0.4}{13} \quad \frac{0.0}{12} \quad \frac{-1.2}{14} \quad \frac{-1.2}{16} \quad \frac{+4.3}{22} \quad \frac{+5.6}{33}$$

$$\frac{-10.6}{33} \quad \frac{-10.3}{30} \quad \frac{-0.4}{14} \quad \frac{-0.2}{14} \quad \frac{-6.9}{23} \quad \frac{-7.9}{33}$$

$$\frac{-10.5}{33} \quad \frac{-10.0}{29} \quad \frac{-0.4}{15} \quad \frac{-0.6}{15} \quad \frac{-8.5}{28} \quad \frac{-9.0}{33}$$

$$\frac{-10.3}{33} \quad \frac{-10.0}{29} \quad \frac{-0.4}{14} \quad \frac{-0.6}{15} \quad \frac{-8.7}{27} \quad \frac{-9.1}{33}$$

$$\frac{-9.0}{33} \quad \frac{-8.7}{29} \quad \frac{-0.6}{16} \quad \frac{-0.6}{16} \quad \frac{-5.1}{24} \quad \frac{-4.9}{33}$$

$$\frac{-1.9}{33} \quad \frac{-0.7}{21} \quad \frac{-1.6}{19} \quad \frac{-1.6}{17} \quad \frac{-0.7}{16} \quad \frac{0.0}{10} \quad \frac{+1.0}{33} \quad \frac{+2.0}{50}$$

$$\frac{0.0}{33} \quad \frac{+0.9}{22} \quad \frac{-1.5}{19} \quad \frac{-1.7}{16} \quad \frac{-0.9}{15} \quad \frac{-0.2}{16} \quad \frac{+0.1}{24} \quad \frac{+0.3}{33}$$

Station	Elev	
215	306.5	✓
214	307.8	✓
+50	307.7	
213	308.0	✓
212	308.0	✓
211	306.7	✓
210	304.0	✓
209	301.1	✓
+50	299.8	
208	298.6	✓
207	295.9	✓
206	295.1	✓
+90	295.1	✓

L.

E

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90

$$\begin{array}{cccccc} +1.3 & +0.8 & -1.8 & -0.8 & -0.4 & - \\ \frac{33}{33} & \frac{23}{23} & \frac{20}{20} & \frac{15}{15} & \frac{9}{9} & - \end{array} \quad \begin{array}{cccccc} -0.3 & -0.8 & +0.3 & -0.6 & -0.1 & +3.2 \\ \frac{15}{15} & \frac{17}{17} & \frac{24}{24} & \frac{21}{21} & \frac{31}{31} & \frac{33}{33} \end{array}$$

$$\begin{array}{cccccc} -0.3 & +0.3 & -1.8 & -1.8 & -0.8 & - \\ \frac{33}{33} & \frac{23}{23} & \frac{20}{20} & \frac{18}{18} & \frac{14}{14} & - \end{array} \quad \begin{array}{cccccc} -0.4 & -1.5 & -1.5 & +0.8 & -0.9 & - \\ \frac{15}{15} & \frac{17}{17} & \frac{21}{21} & \frac{23}{23} & \frac{33}{33} & - \end{array}$$

$$\begin{array}{cccccc} +0.9 & +0.6 & -1.5 & -0.8 & - & - \\ \frac{33}{33} & \frac{23}{23} & \frac{20}{20} & \frac{14}{14} & - & - \end{array} \quad \begin{array}{cccccc} -1.0 & -1.6 & -1.8 & - & - & - \\ \frac{15}{15} & \frac{20}{20} & \frac{33}{33} & - & - & - \end{array}$$

$$\begin{array}{cccccc} -2.1 & -1.5 & -2.1 & -1.1 & -0.7 & - \\ \frac{33}{33} & \frac{23}{23} & \frac{22}{22} & \frac{16}{16} & \frac{10}{10} & - \end{array} \quad \begin{array}{cccccc} -0.2 & -0.9 & -0.9 & +1.2 & +1.5 & - \\ \frac{15}{15} & \frac{17}{17} & \frac{20}{20} & \frac{22}{22} & \frac{33}{33} & - \end{array}$$

$$\begin{array}{cccccc} -0.7 & -0.7 & -2.1 & -2.1 & -1.4 & -0.7 \\ \frac{33}{33} & \frac{23}{23} & \frac{21}{21} & \frac{19}{19} & \frac{17}{17} & \frac{10}{10} \end{array} \quad \begin{array}{cccccc} -0.6 & -1.1 & -1.1 & +0.4 & +0.9 & - \\ \frac{15}{15} & \frac{17}{17} & \frac{19}{19} & \frac{20}{20} & \frac{33}{33} & - \end{array}$$

$$\begin{array}{cccccc} +1.8 & +1.0 & -1.9 & -1.9 & -1.0 & - \\ \frac{33}{33} & \frac{24}{24} & \frac{20}{20} & \frac{18}{18} & \frac{15}{15} & - \end{array} \quad \begin{array}{cccccc} -0.5 & -1.0 & -1.0 & +2.9 & +3.9 & - \\ \frac{15}{15} & \frac{17}{17} & \frac{18}{18} & \frac{21}{21} & \frac{33}{33} & - \end{array}$$

$$\begin{array}{cccccc} +0.4 & +0.2 & -1.8 & -1.8 & -0.8 & - \\ \frac{33}{33} & \frac{23}{23} & \frac{20}{20} & \frac{18}{18} & \frac{16}{16} & - \end{array} \quad \begin{array}{cccccc} -0.4 & -1.0 & -1.0 & +0.7 & +1.0 & - \\ \frac{15}{15} & \frac{16}{16} & \frac{18}{18} & \frac{20}{20} & \frac{33}{33} & - \end{array}$$

$$\begin{array}{cccccc} -4.7 & -3.9 & -0.6 & - & - & - \\ \frac{33}{33} & \frac{21}{21} & \frac{16}{16} & - & - & - \end{array} \quad \begin{array}{cccccc} -0.3 & -1.2 & -0.9 & +1.6 & +3.6 & - \\ \frac{14}{14} & \frac{17}{17} & \frac{19}{19} & \frac{22}{22} & \frac{33}{33} & - \end{array}$$

$$\begin{array}{cccccc} -5.7 & -3.9 & -0.7 & - & - & - \\ \frac{33}{33} & \frac{20}{20} & \frac{15}{15} & - & - & - \end{array} \quad \begin{array}{cccccc} -0.5 & -2.2 & -2.2 & -1.3 & 0.9 & - \\ \frac{15}{15} & \frac{18}{18} & \frac{20}{20} & \frac{22}{22} & \frac{33}{33} & - \end{array}$$

$$\begin{array}{cccccc} -5.9 & -4.8 & -0.6 & - & - & - \\ \frac{33}{33} & \frac{22}{22} & \frac{14}{14} & - & - & - \end{array} \quad \begin{array}{cccccc} -0.5 & -4.9 & -4.1 & - & - & - \\ \frac{17}{17} & \frac{24}{24} & \frac{33}{33} & - & - & - \end{array}$$

$$\begin{array}{cccccc} -5.3 & -5.3 & -6.3 & -6.3 & -5.1 & -4.9 & -0.4 \\ \frac{33}{33} & \frac{30}{30} & \frac{29}{29} & \frac{28}{28} & \frac{27}{27} & \frac{21}{21} & \frac{13}{13} \end{array} \quad \begin{array}{cccccc} -0.4 & -4.8 & -4.8 & - & - & - \\ \frac{18}{18} & \frac{20}{20} & \frac{33}{33} & - & - & - \end{array}$$

$$\begin{array}{cccccc} -4.2 & -4.1 & -5.4 & -5.4 & -4.2 & -4.0 & -0.4 \\ \frac{33}{33} & \frac{29}{29} & \frac{28}{28} & \frac{27}{27} & \frac{25}{25} & \frac{18}{18} & \frac{13}{13} \end{array} \quad \begin{array}{cccccc} -0.4 & -4.0 & -3.8 & - & - & - \\ \frac{13}{13} & \frac{19}{19} & \frac{33}{33} & - & - & - \end{array}$$

$$\begin{array}{cccccc} -4.2 & -4.1 & -5.4 & -5.4 & -4.2 & -4.0 & -0.4 \\ \frac{33}{33} & \frac{29}{29} & \frac{28}{28} & \frac{27}{27} & \frac{25}{25} & \frac{18}{18} & \frac{13}{13} \end{array} \quad \begin{array}{cccccc} -0.5 & -4.5 & -4.5 & - & - & - \\ \frac{13}{13} & \frac{19}{19} & \frac{23}{23} & - & - & - \end{array}$$

Station

Elev.

+84 W. Bound

+62^{E Bound} Top of Rail

302.6

✓

+50

302.1

218

302.4

✓

217

303.3

✓

216

304.1

✓

215 + 71 1/2 E Co. Rd. "E"

304.8

✓

+60

304.9

✓

+40

305.5

W.H. Carlsons T

Nov, 27, 23

Paul J. Crane Red

Fair & Cold.

A.S. Nelson Ch.

M. Alberg "

General Note:

Soil conditions from
sta 000 to 215, sandy clay.

top of Rail

$\frac{-1.6}{400}$ $\frac{-1.2}{300}$ $\frac{-0.8}{200}$ $\frac{-0.4}{100}$ $\frac{+0.4}{100}$

$\frac{-4.8}{33}$ $\frac{-4.0}{22}$ $\frac{-0.4}{11}$ $\frac{-0.1}{9}$ $\frac{-0.5}{23}$

$\frac{-3.3}{33}$ $\frac{-2.1}{20}$ $\frac{-0.4}{14}$ $\frac{-0.4}{9}$ $\frac{-0.6}{33}$

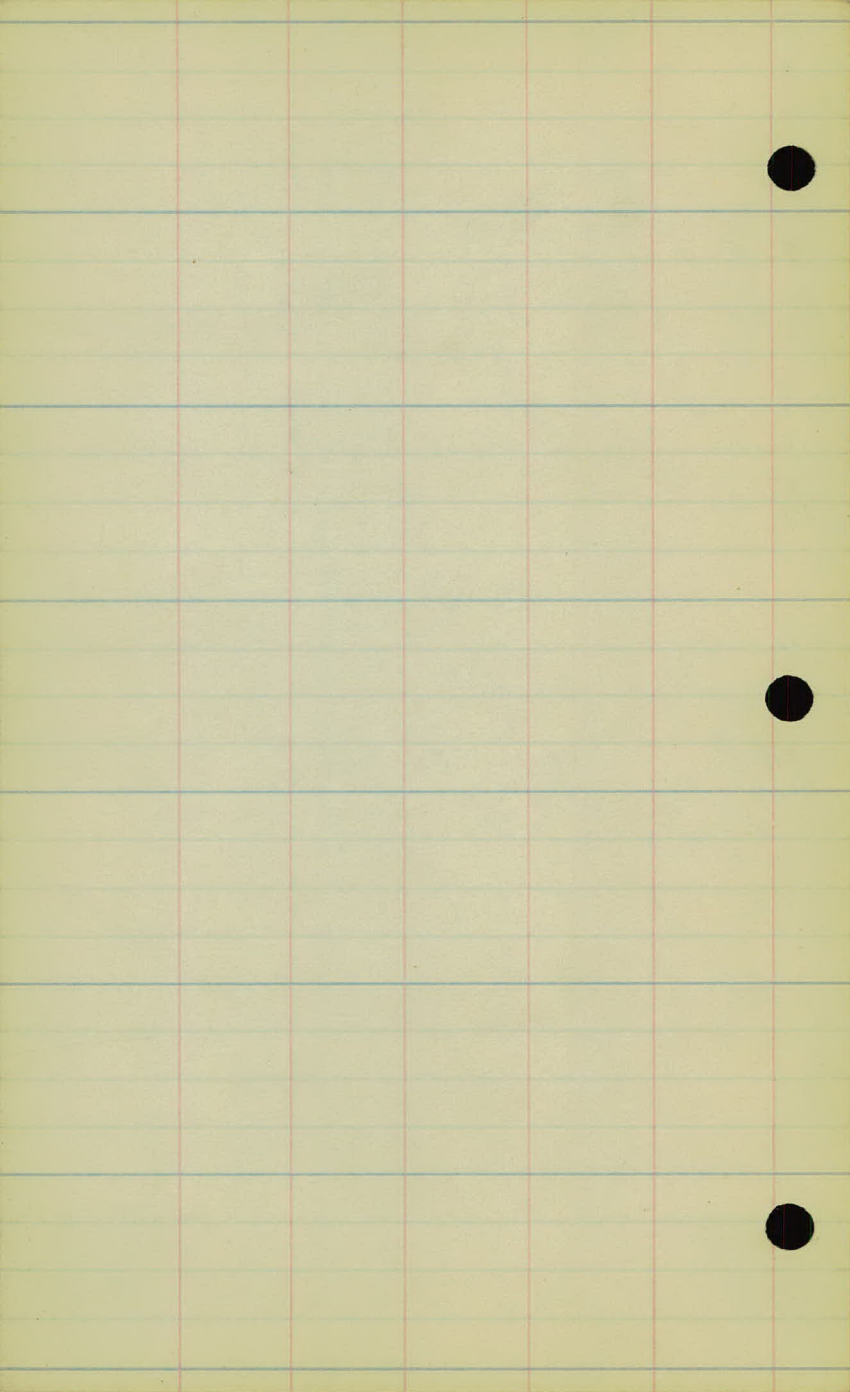
$\frac{-4.7}{33}$ $\frac{-5.0}{18}$ $\frac{-0.8}{11}$ $\frac{-0.5}{7}$ $\frac{-0.8}{13}$ $\frac{-1.8}{33}$

$\frac{-1.8}{33}$ $\frac{-1.7}{20}$ $\frac{-0.5}{10}$ $\frac{-0.1}{8}$ $\frac{-0.1}{20}$ $\frac{-0.7}{45}$ $\frac{+1.0}{50}$

$\frac{-6.5}{400}$ $\frac{-5.5}{300}$ $\frac{-4.0}{200}$ $\frac{-1.8}{100}$ $\frac{-0.8}{33}$ $\frac{+0.3}{33}$ $\frac{+1.4}{100}$ $\frac{+2.9}{200}$ $\frac{+3.0}{300}$ $\frac{+2.6}{400}$

$\frac{-2.7}{33}$ $\frac{-1.3}{30}$ $\frac{-0.7}{16}$ $\frac{0.0}{21}$ $\frac{-0.5}{16}$ $\frac{-1.7}{48}$

$\frac{+0.4}{33}$ $\frac{+0.6}{23}$ $\frac{-1.6}{21}$ $\frac{-0.6}{12}$ $\frac{-0.3}{13}$ $\frac{-0.7}{23}$ $\frac{-1.3}{25}$ $\frac{-1.3}{27}$ $\frac{-0.3}{28}$ $\frac{+2.6}{36}$



PROJECT 24-01

Alignment Notes:

Proposed Grade Separation

Lexington Ave & N.P.R.R.

Sta. 96+52.28 "A" Line - 111+49.05 "A" Line. =
Sta 110+49.05 Lexington Ave Location

Station	Point	L	R	Calc. Bear.
102+58.67 ✓	P.T.		20°16'	20° C.
102			140°24'	Δ 40°-32' R
+50			7°-24'	P.I 10462.32
101			4°-24'	S.T 106.32 ✓
100+56 ✓	P.C.		0°-00'	L.C. 202.67 ✓
				cor. .19

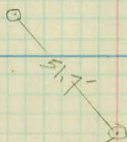
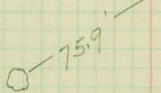
N. 38°18'

98+98.95 ✓	P.T.	18°30'		
98+50		14°49.2		15° C.
98+00		11°04.2		Δ 37°-00' L
+50		7°-19.2		P.I 97780.45
97+00		3°-34.2		S.T. 128.11 ✓
96+52.28 ✓	P.C.	0°-00'		L.C. 246.67 ✓
				cor. .10

N. 1°-18' W.

①

Nail in Pole

R.R. Spike
in 24" Oak

W.H. Carlson }
P.C. Crane } Dec. 17, 23
M.S. Ahlberg }
A.S. Nelson }

Station	Point	L	R	Calc. Bear.
				N. 0°-56' W.
				N. 0°-55' W.
110+49.6	→ Lexington Ave.			
111+49.1	✓ P.T.	11°46' 50"		
111+00		9°19' 20"		10°-C.
110+50		6°49' 20"		Δ 23°-33' L
110+00		4°19' 20"		P.T. 110+33.2
109+50		1°49' 20"		S.T. 119.59 ✓
109+13.61	✓ P.C.	0°-00' 00"		L.C. 235.50 ✓ (Cor., 05)

N. 22°-38' E.

106+00.77	✓ P.T.		10°-12' 00"	
106+00			10°-09' 10"	10° C.
105+50			7°39' 20"	Δ 20°-24' R
105+00			5°09' 20"	P.T. 105+00
104+50			2°-39' 20"	S.T. 103.23 ✓
103+46.77	✓ P.C.		0°-00' 00"	L.C. 204.00 ✓ (Cor., 05)

103+19.08 S.N.P.R.R.

N. 2°14' E.

Equation

④ Nail in 16" Oak.

34.57

①

40.05

⑧ Nail in 8" Oak

⑨ Nail in top 6" stump.

③ 3.8

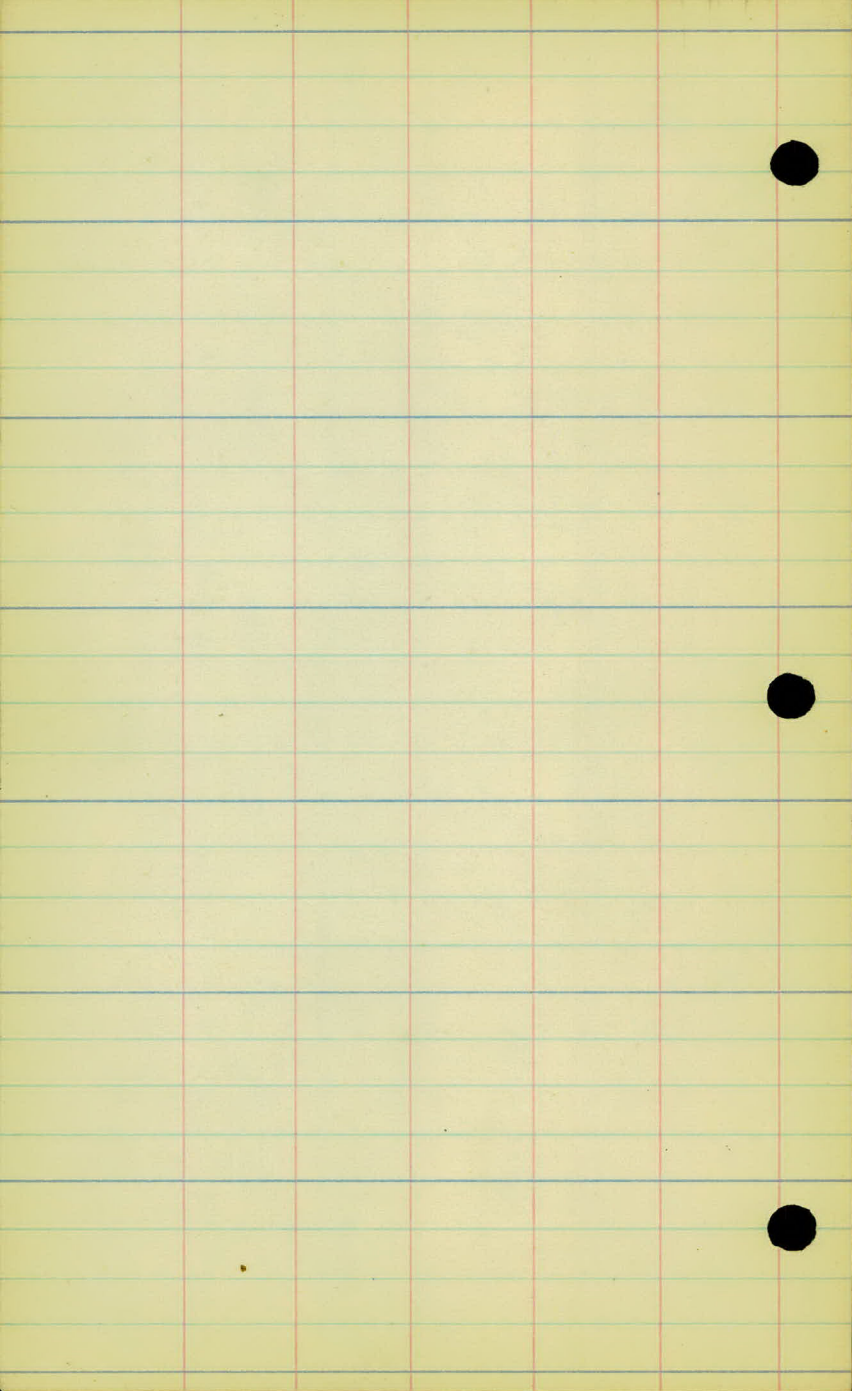
② 18.1

10" tree

④



90°



98

PROJECT 2401

Art. Topography.

Proposed Grade Separation
Lexington Ave. & N.P.R.R.

+58.67 = P.T.

102

101

+56 = P.C.

100

+50 End of grave 30' R

99

+48.95 =
+59

P.T.

Fence Cor. 4' L. + Req of Grave
Various sizes C.O.

98

+98

Fence Corner 40.5 L.

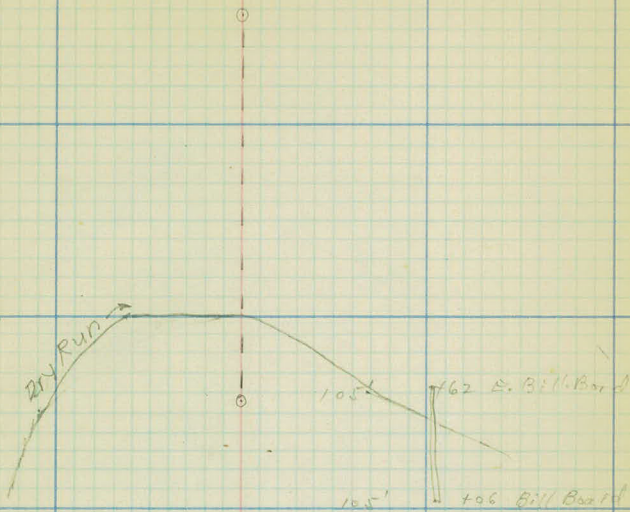
97

+52.28 = P.C.

96

cultivated





5" Tree +17-29' L.
10" Tree +07-29' L.

10' Oak +77-7' L.

8" Oak +67-11' L.
6" Oak +41-21' L.

6" Stump +08-31' L. ✓

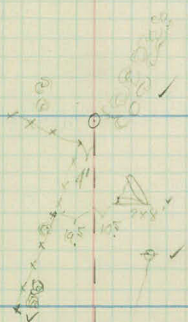
8" Oak +03-33' L. ✓

20' Oak +05-46' L. ✓

12" Oak +20-43' L. ✓

14" Oak +00-53' L. ✓

Po hole +67'



+54 Edge = 20' R.

+28 P.R. 29' R.

+42 T.P.

Scale 1" = 100'

108

+06 Fence Line E.W.

107

+00.77 = P.T.

106

+97 20" tree 52' L.

+87-24 Tree 60' L.

+86 S.E. cor of No. 110 Left.

+45 210' Drive E. & West.

+15 End of Hedge Left. 24' Left.

105

S.E. Cor. of

+25 House 19' Left. Part to Lexington.

+33 Hedge on R.

104

+96.77 = P.C.

+92 19.5' 26" maple 11' R.

+75 80' Hedge 17' R.

+68 R.W. Fence

+19.08 R.M.B.R.R.

103

+70 R/W Fence ✓
- 75' R old Road

102

Equation 17

$$110 + 49 \frac{1}{2} \\ + 49.05 = P.T.$$

111

110

$$+ 13.55 = P.C.$$

109

108

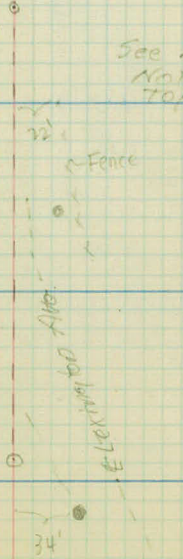
W.H. Carlson
P.C. Crane
M. Ahlberg
A. Nelson
12/18/23

See Lexington
Notes for addi.
topog.

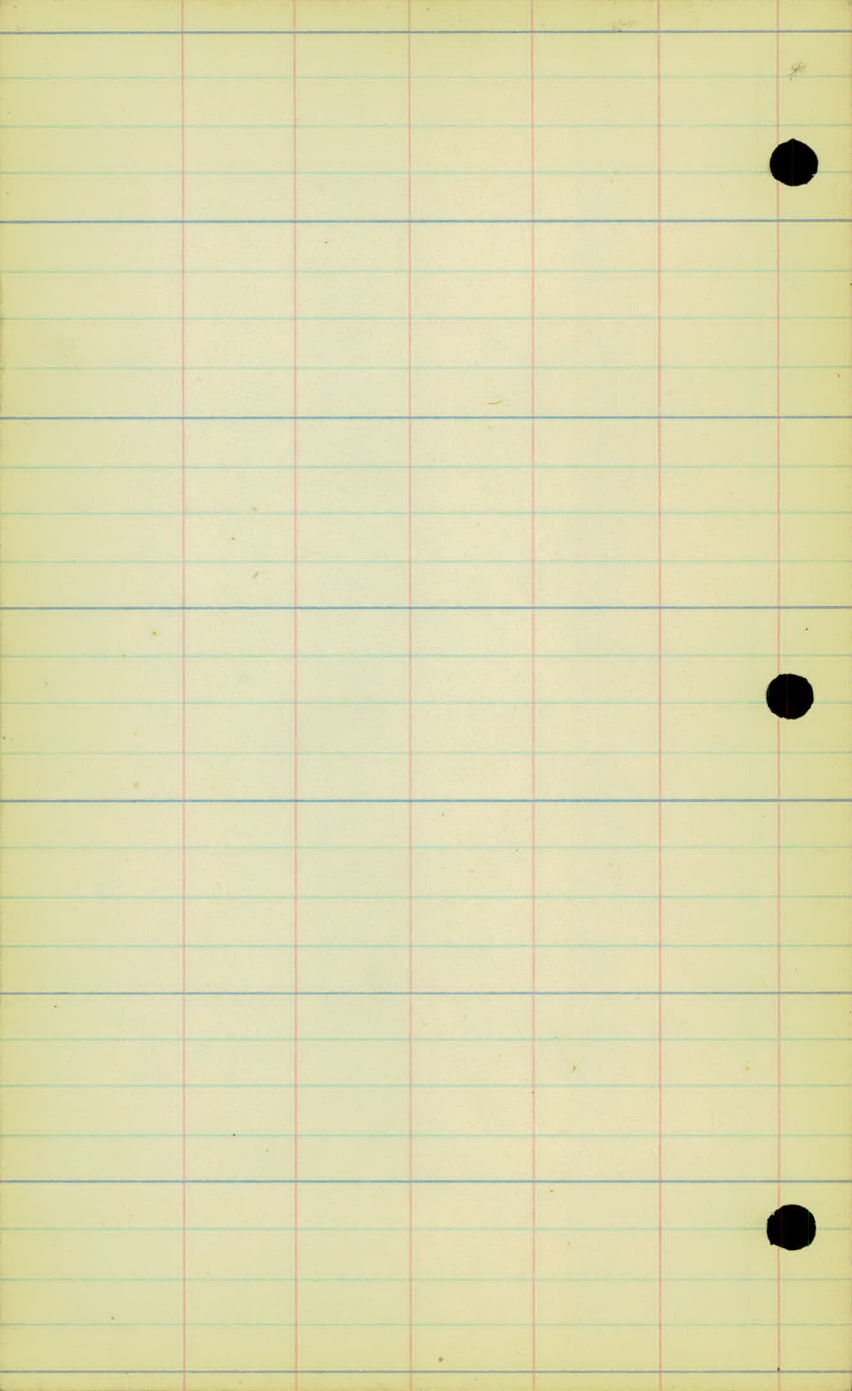
433 T.P. 13'L.

437 R. 23'R.

Cultivated



21 - 0.



PROJECT 24-01

Center Line Levels

Proposed Grade Separation

Lexington Ave, & N.P.R.R.

Station	B.S	H.I	-	Elev.	
B.M.	2.08	257.07 ✓		254.99 ✓	
96+52			4.4	252.7 ✓	
97			4.0	53.1 ✓	
+50			4.0	53.1 ✓	
			10.08	46.79 ✓	
+60			4.1	53.0 ✓	
+80			6.4	50.7 ✓	
98			7.2	49.9 ✓	
+50			6.0	51.1 ✓	
99			1.1	56.0 ✓	
+50			2.0	55.1 ✓	
100			1.7	55.4 ✓	
+56			1.4	55.7 ✓	
101			2.8	54.3 ✓	
+50		✓	0.7	56.4 ✓	
T.P.	12.04	267.19	1.92	255.15 ✓	
102			9.3	57.9 ✓	
+50			6.6	60.6 ✓	
+73			4.7	62.5 ✓	
+82			9.6	57.6 ✓	
103			2.6	58.6 ✓	
+12			3.7	58.5 ✓	
+19.08			7.30	59.89 ✓	
			7.75	59.44 ✓	
+27		✓	9.0	58.2 ✓	
T.P.	11.82	278.76	0.31	266.88 ✓	

W.H. Carlsson }
R.C. Crane } 12/18/23
A. Nelson }
M. Hillberg }
R.R. Spike 10 24" Oak 60' L. Sta 97+25

163

Top of Ice Lake on R. Dec. 18, 1923

Top of Stake 101

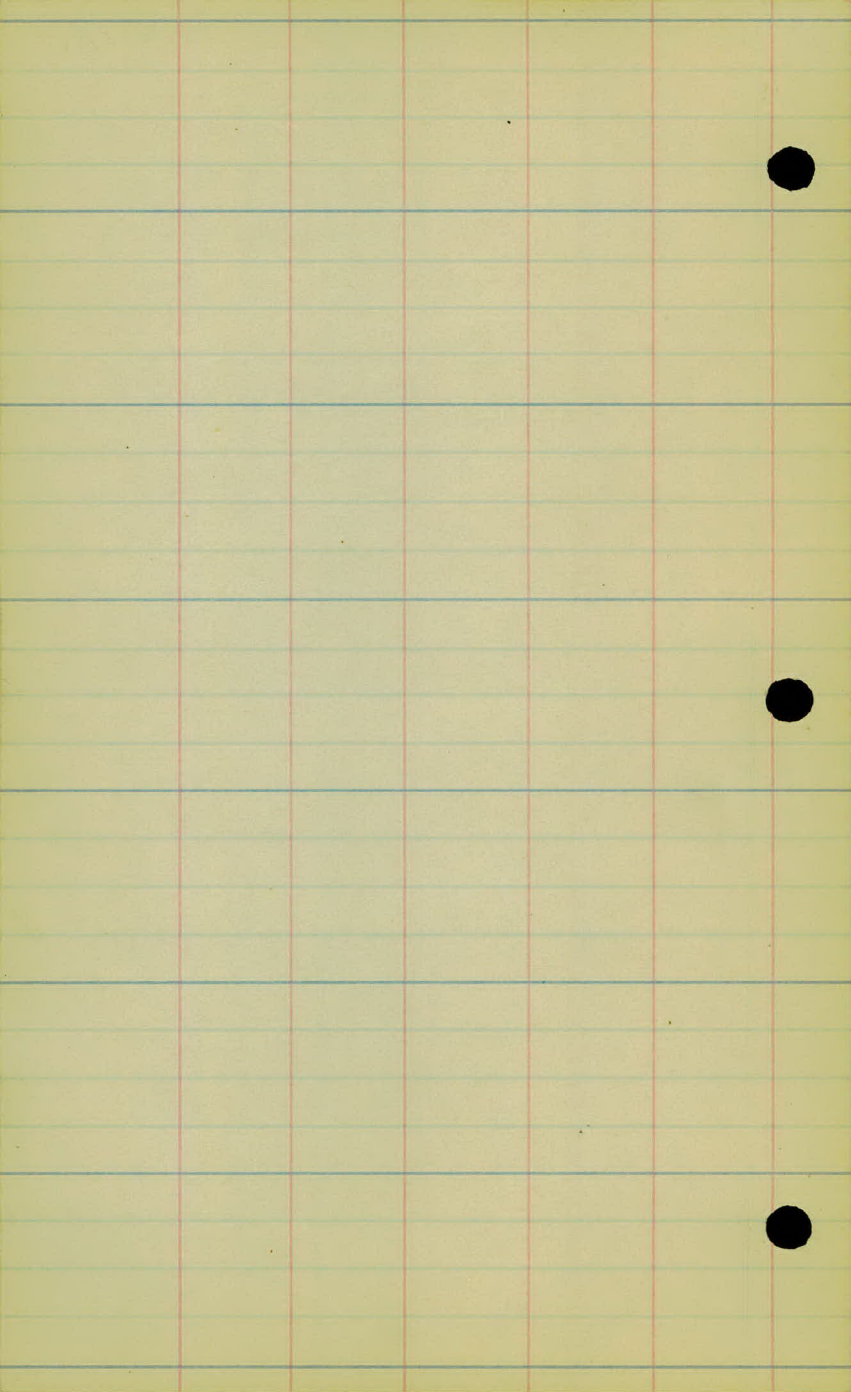
Top. of Rail

Base of Rail

Sta	+	H.F		Elev.	
		278.76	✓		
103+43				8.0	270.8 ✓
+62				6.8	72.0 ✓
104				6.5	72.3 ✓
+25				6.2	72.6 ✓
+50				6.4	72.4 ✓
105				7.0	71.8 ✓
+25				4.7	74.1 ✓
+46				4.1	74.7 ✓
B.M	12.57	291.16	✓	0.17	(288.59) 278.59
+54				11.9	79.3 ✓
+75				10.8	80.4 ✓
106				11.5	79.7 ✓
+25				13.0	78.2 ✓
107				10.5	80.7 ✓
108				9.1	82.0 ✓
109				5.1	86.0 ✓
+50				4.7	86.5 ✓
+87				3.9	81.3 ✓
110				5.4	85.8 ✓
+05				6.0	85.2 ✓
T.P.	11.74	298.22	✓	4.68	286.48 ✓
+50				10.7	87.5 ✓
111				8.2	90.0 ✓
+49.4 = 110+49.6				6.6	91.6 ✓
B.M. for check.				0.62	297.60 ✓ 297.62

Spike in 10" Oak 105425 - 25' Right.

R.R. Spike in 10" Oak 105425 - 25' Right.



PROJECT 24-01

Cross Section Notes

Proposed Grade Separation

Lexington Ave, & N.P.R.R.

Station	Elev.
+50	256.4
101	254.3
+56	55.7
100	55.4
+50	55.1
99	56.0
+50	51.1
98	49.9
+80	50.7
+50	53.1
97	53.1
96 + 52.28	252.7

$$\begin{array}{cccccc} +1.4 & & & & & \\ \hline 100 & & & & & \end{array} \quad \begin{array}{cccccc} 0.0 & -0.8 & -0.7 & -1.3 & -1.8 & -7.3 \\ & 42 & 100 & 124 & 133 & 200 \end{array}$$

$$\begin{array}{cccccc} +2.2 & & +1.1 & & & \\ \hline 100 & & 65 & & & \end{array} \quad \begin{array}{cccccc} 0.0 & -0.2 & -0.1 & +0.1 & -3.9 & -6.3 \\ & 12 & 49 & 110 & 122 & 189 \end{array}$$

$$\begin{array}{cccccc} 0.0 & +2.3 & +2.0 & & & \\ \hline 100 & 62 & 37 & & & \end{array} \quad \begin{array}{cccccc} 0.0 & -1.1 & -1.6 & -2.3 & -1.7 & -5.0 & -7.6 \\ & 20 & 67 & 68 & 107 & 121 & 177 \end{array}$$

$$\begin{array}{cccccc} +2.1 & +2.4 & +2.2 & +1.1 & & \\ \hline 100 & 60 & 36 & 16 & & \end{array} \quad \begin{array}{cccccc} 0.0 & -1.7 & -1.9 & -2.5 & -3.3 & -2.6 & -5.6 \\ & 20 & 53 & 71 & 100 & 105 & 124 \end{array}$$

$$\begin{array}{cccccc} +1.9 & & +1.6 & & & \\ \hline 70 & & 35 & & & \end{array} \quad \begin{array}{cccccc} 0.0 & -0.6 & -1.4 & -3.0 & -3.5 & \\ & 15 & 33 & 60 & 91 & \end{array}$$

$$\begin{array}{cccccc} +1.5 & +1.0 & +0.3 & & & \\ \hline 50 & 33 & 18 & & & \end{array} \quad \begin{array}{cccccc} 0.0 & 0.0 & -3.0 & -3.0 & -1.8 & -4.3 & -6.0 & -2.5 \\ & 2 & 9 & 14 & 30 & 54 & 80 & 95 \end{array}$$

$$\begin{array}{cccccc} +7.5 & +6.0 & +2.0 & +2.0 & +1.0 & & \\ \hline 50 & 21 & 15 & 11 & 9 & & \end{array} \quad \begin{array}{cccccc} 0.0 & -1.0 & -1.1 & +2.4 & +2.4 & \\ & 18 & 36 & 42 & 60 & \end{array}$$

$$\begin{array}{cccccc} +7.8 & +6.3 & +2.7 & +0.8 & +0.6 & & \\ \hline 50 & 38 & 31 & 17 & 7 & & \end{array} \quad \begin{array}{cccccc} 0.0 & -0.4 & +3.3 & +3.4 & +3.1 & +3.5 \\ & 8 & 16 & 31 & 38 & 45 \end{array}$$

$$\begin{array}{cccccc} +7.3 & +6.2 & +2.7 & +0.7 & & & \\ \hline 50 & 41 & 36 & 12 & & & \end{array} \quad \begin{array}{cccccc} 0.0 & +3.6 & +3.3 & +3.5 & +3.1 & +3.2 \times 0.2 \\ & 6 & 12 & 21 & 28 & 33 & 39 \end{array}$$

£. Cox.

$$\begin{array}{cccccc} +3.5 & +3.0 & +2.2 & -3.5 & -4.4 & -3.3 & & & \\ \hline 60 & 50 & 45 & 38 & 30 & 8 & & & \end{array} \quad \begin{array}{cccccc} 0.0 & +0.2 & +0.2 & 0.0 & +4.2 & -5.1 \\ & 2 & 20 & 25 & 21 & 33 \end{array}$$

$$\begin{array}{cccccc} +2.4 & -3.2 & -3.6 & -2.3 & & & & & \\ \hline 60 & 47 & 33 & 18 & & & & & \end{array} \quad \begin{array}{cccccc} 0.0 & -0.3 & & & & & & & \\ & 12 & 7 & & & & & & \end{array} \quad \begin{array}{cccccc} 0.0 & -0.5 & -0.2 & -5.4 & -6.0 & \\ & 11 & 17 & 24 & 33 & \end{array}$$

$$\begin{array}{cccccc} -2.4 & -2.4 & +0.2 & & & & & & \\ \hline 33 & 22 & 16 & & & & & & \end{array} \quad \begin{array}{cccccc} 0.0 & -0.2 & +0.1 & -4.0 & -5.0 & -5.4 \\ & 9 & 13 & 18 & 23 & 33 \end{array}$$

Station

Elev.

750

72.4

+25

72.6

104

72.3

+62

72.0

+43

70.8

+27

58.2

103+19

259.89

103+12

58.5

103

258.6

102+82

57.6

+73

62.5

102

257.9

Floor of
House

$\frac{+2.5}{70}$ $\frac{+4.1}{46}$ $\frac{+4.1+17}{37}$ $\frac{17}{13}$ $\frac{0.43}{9}$ $\frac{-5.2}{44}$ $\frac{-19.2}{74}$ $\frac{-19.8}{100}$ $\frac{-22.0}{190}$

$\frac{+4.7}{100}$ $\frac{+3.0}{41}$ $\frac{+1.4}{33}$ $\frac{0.0}{1}$ $\frac{-0.7}{7}$ $\frac{-6.2}{15}$ $\frac{-6.8}{50}$

$\frac{+1.4}{100}$ $\frac{+1.1}{33}$ $\frac{0.0}{13}$ $\frac{-0.9}{34}$ $\frac{7.5}{42}$ $\frac{-7.2}{56}$ $\frac{-8.0}{78}$ $\frac{-19.8}{100}$ $\frac{-21.1}{100}$ $\frac{-27.3}{192}$

$\frac{-1.7}{100}$ $\frac{-1.4}{50}$ $\frac{-1.6}{25}$ $\frac{0.0}{0}$ $\frac{-0.1}{7}$ $\frac{-1.6}{13}$ $\frac{3.3}{26}$ $\frac{10.1}{39}$ $\frac{-11.2}{71}$ $\frac{-18.7}{89}$ $\frac{-20.3}{125}$ $\frac{-23.1}{188}$ $\frac{-20.8}{200}$

$\frac{-0.9}{100}$ $\frac{-0.3}{65}$ $\frac{-0.7}{33}$ $\frac{0.0}{9}$ $\frac{-1.1}{19}$ $\frac{-4.0}{39}$ $\frac{-10.1}{47}$ $\frac{-10.9}{71}$ $\frac{-14.9}{92}$ $\frac{-17.7}{115}$ $\frac{-21.3}{190}$

$\frac{+1.1}{100}$ $\frac{+0.3}{50}$ $\frac{0.0}{0}$ $\frac{-0.7}{40}$ $\frac{-1.9}{100}$ $\frac{-1.4}{213}$

Top of Rai $\frac{+0.8}{100}$

$\frac{0.0}{1}$ $\frac{-1.0}{100}$ $\frac{-1.9}{200}$

$\frac{+0.7}{100}$ $\frac{+0.2}{50}$ $\frac{0.0}{1}$ $\frac{-0.7}{50}$ $\frac{-1.1}{100}$ $\frac{-2.0}{213}$

$\frac{+0.6}{100}$ $\frac{0.0}{55}$ $\frac{0.0}{1}$ $\frac{0.0}{33}$ $\frac{-0.6}{70}$ $\frac{+1.5}{79}$ $\frac{+1.7}{94}$ $\frac{-4.4}{124}$ $\frac{-7.7}{150}$ $\frac{-9.0}{200}$

$\frac{+6.0}{100}$ $\frac{+6.5}{85}$ $\frac{+5.0}{40}$ $\frac{+4.2}{33}$ $\frac{0.0}{9}$ $\frac{-1.3}{29}$ $\frac{-1.8}{62}$ $\frac{-4.4}{80}$ $\frac{-5.6}{111}$ $\frac{-10.9}{135}$ $\frac{-12.6}{150}$ $\frac{-14.3}{195}$

$\frac{+3.3}{100}$ $\frac{+2.7}{50}$ $\frac{0.0}{1}$ $\frac{-0.8}{20}$ $\frac{-0.1}{57}$ $\frac{-1.3}{100}$ $\frac{+1.7}{126}$

Sta.	Elev.
787	287.3
+50	86.5
109	86.0
108	82.0
107	80.7
+75	78.2
106	79.7
+75	80.4
+54	79.3
+46	74.7
+25	74.1
105	71.8

Station

Elev.

Equation
 $+49\% = 110 + 49.6$ 291.6

111 290.0

450 87.5

110 85.8

(See Lexington Ave Notes)

W.H. Carlson
R.C. Crane
M. Ahlberg

Dec. 19, 1923

-2.8	-2.0	00	-1.3	-1.5	00	-0.4	-1.2	-1.2	00	00
$\frac{75}{}$	$\frac{50}{}$	$\frac{33}{}$	$\frac{19}{}$	$\frac{15}{}$	$\frac{00}{}$	$\frac{13}{}$	$\frac{15}{}$	$\frac{17}{}$	$\frac{18}{}$	$\frac{33}{}$

-0.2	+2.0	+1.0	+1.0	-1.1	-0.5	00	00	-0.4	-1.0	-1.0	+1.3	+1.3
$\frac{71}{}$	$\frac{33}{}$	$\frac{23}{}$	$\frac{18}{}$	$\frac{15}{}$	$\frac{11}{}$	$\frac{00}{}$	$\frac{1}{}$	$\frac{15}{}$	$\frac{17}{}$	$\frac{19}{}$	$\frac{22}{}$	$\frac{33}{}$

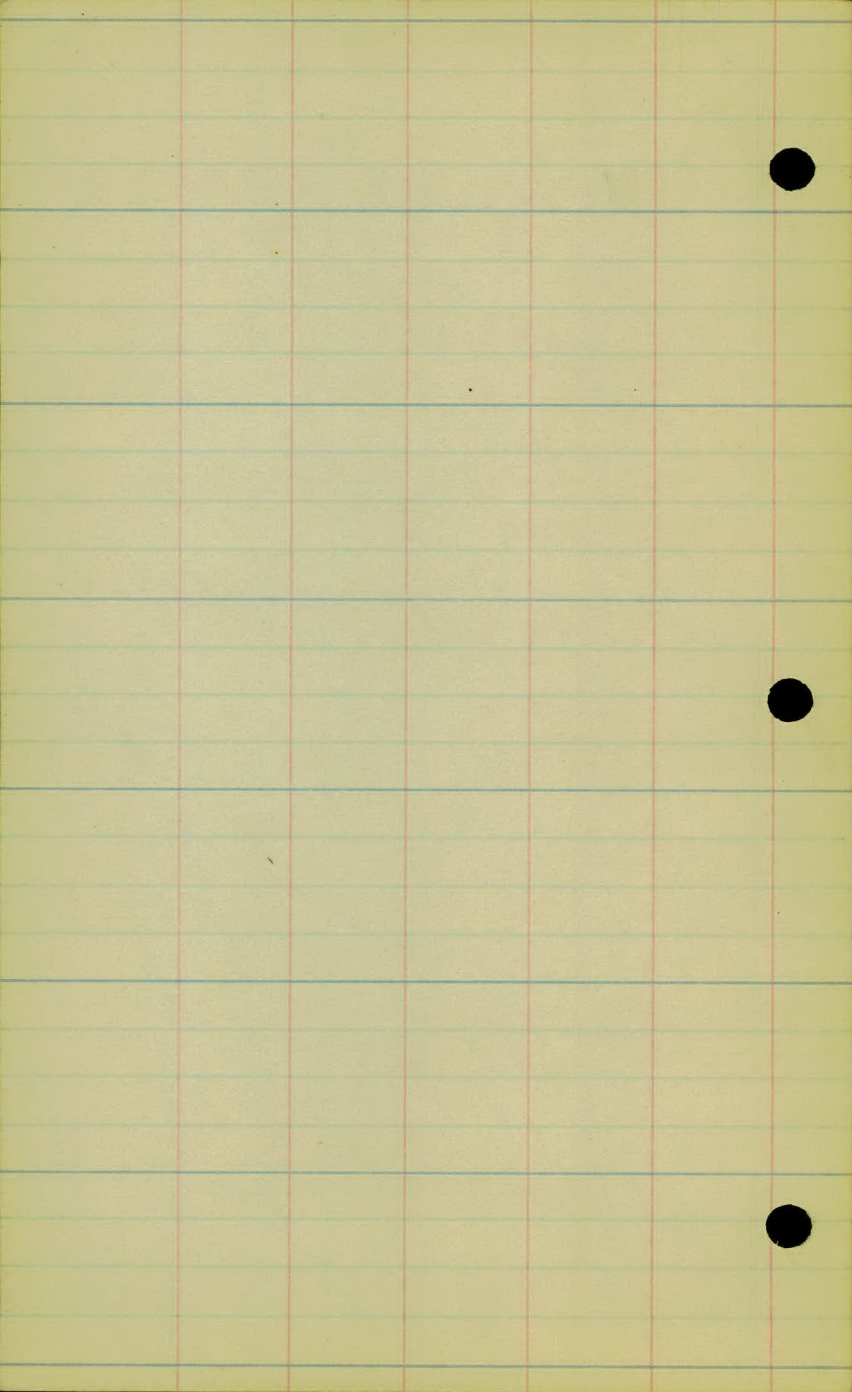
£Lex.

+2.8	+4.6	+4.5	+2.4	+2.0	-0.6	+0.4	00	-0.6	-0.6	+2.0	+2.0
$\frac{100}{}$	$\frac{61}{}$	$\frac{33}{}$	$\frac{18}{}$	$\frac{12}{}$	$\frac{10}{}$	$\frac{7}{}$	$\frac{21}{}$	$\frac{24}{}$	$\frac{26}{}$	$\frac{29}{}$	$\frac{33}{}$

£Lex.

+4.8	+4.6	+2.2	+2.0	00	-0.2	-0.8	-0.4	-0.3	-1.1
$\frac{100}{}$	$\frac{33}{}$	$\frac{9}{}$	$\frac{2}{}$	$\frac{00}{}$	$\frac{1}{}$	$\frac{2}{}$	$\frac{5}{}$	$\frac{28}{}$	$\frac{33}{}$

£Lex



Alignment Notes
 St. Paul-Anoka & Lexington Ave.
 Connection.
 "I" Line.

Station 0+00 = 33+21 "A" Line = Intersection of
 Larpenteur Ave — to Station 8+61.53 P.T. =
 7+11.8 Lexington Ave. Location.

W.H. Carlson. Jr

Nov. 30, 1923

P.C. Crane Rad.

Fair & Clear.

A.S. Nelson Ch.

M.S. Alberg Ch.

Station Point Left Right Bear.

N. 10° 05' E.
= 10° 0' E.

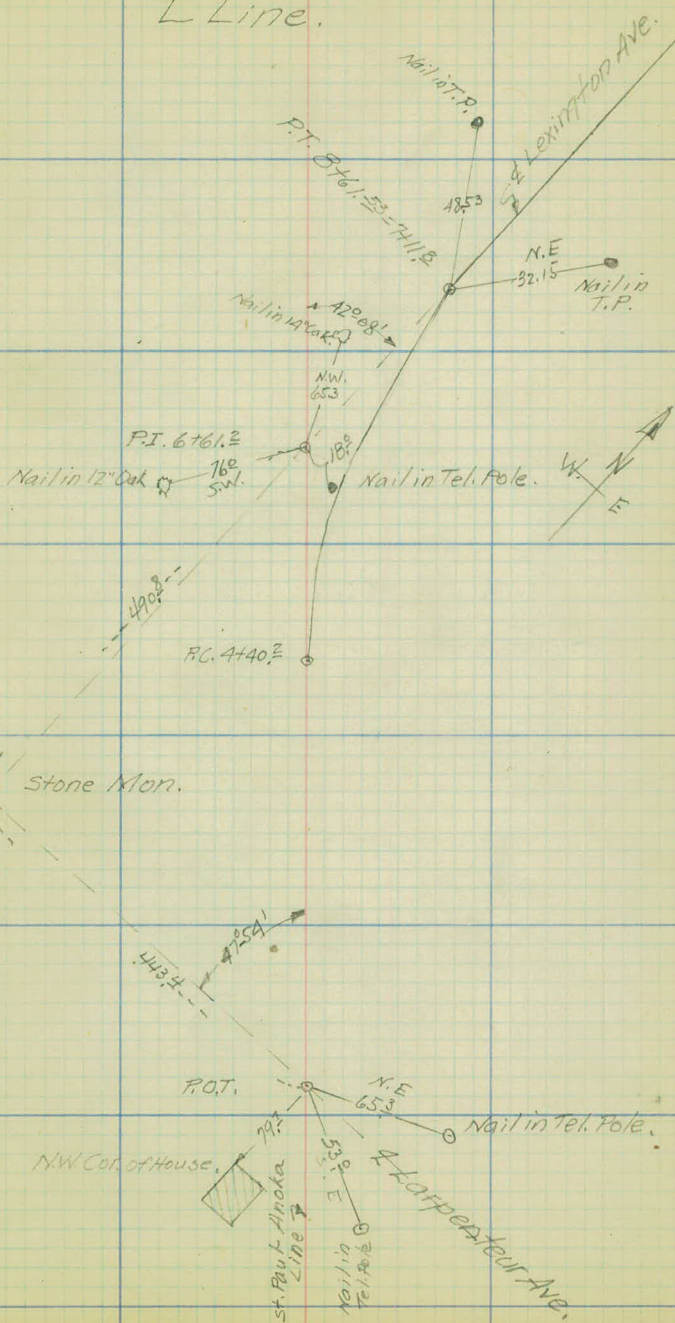
8 + 61.53 ✓ + 50	P.T. = 7+11.8	21° 04'	
8		20° 29.4'	
+ 50		17° 59.4'	10° C.
7		15° 29.4'	Δ 42° 08'
+ 50		12° 59.4'	P.I. 6+61.20
6		10° 29.4'	S.T. 221.00' ✓
+ 50		7° 59.4'	L.C. 421.33' ✓
5		5° 29.4'	Cor. 05' - 50' ch.
4 + 50		2° 59.4'	
4 + 40.2 ✓	P.C.	0° 29.4'	
		0° 00'	

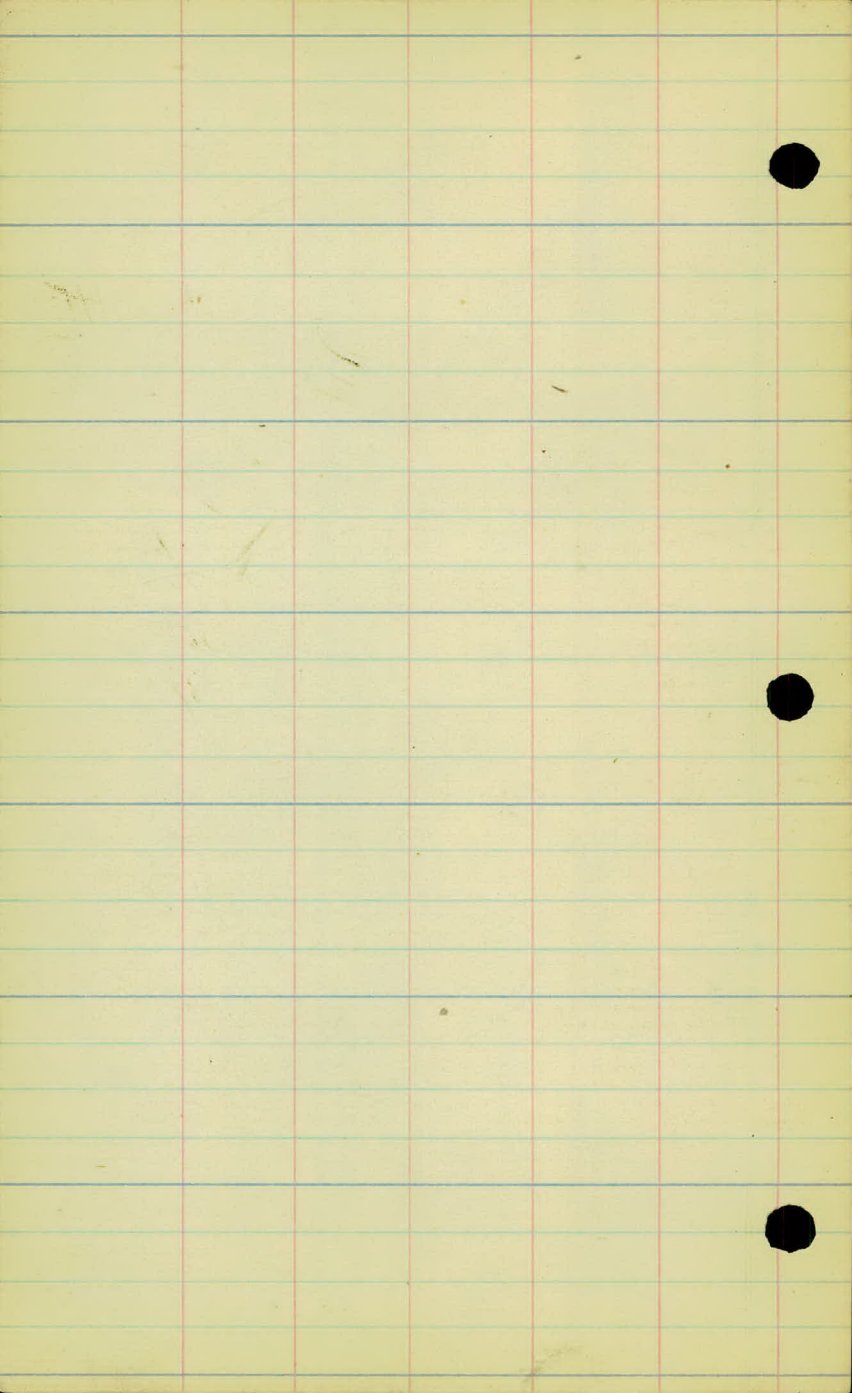
N. 41° 03' W.

Choo = 33721' P.O.J.

"L" Line.

111





Art Topography.

St. Paul-Anoka & Lexington Ave
Connection

5

4

3

2

1

0100

P.C. O

N.A. Lebens.

cultiva tech.

N.A. Lebens.

Cultivated

atol Tel Pole

110' 54"

40'

↳ Lappenstraße

- 021-MailBox B'L.

75'

32'

Ave



(Equation)

$$8 + 61.53 \text{ P.T} = 7 + 11.8$$

8

7

6

5

4

4 Lexington Ave.

P.T. ○



7168 T.P. ●

7119 T.P. ●

6470 Edge of cornfield R

S. Skinnington Ave.

114'

6495 Tel pde ● 78'

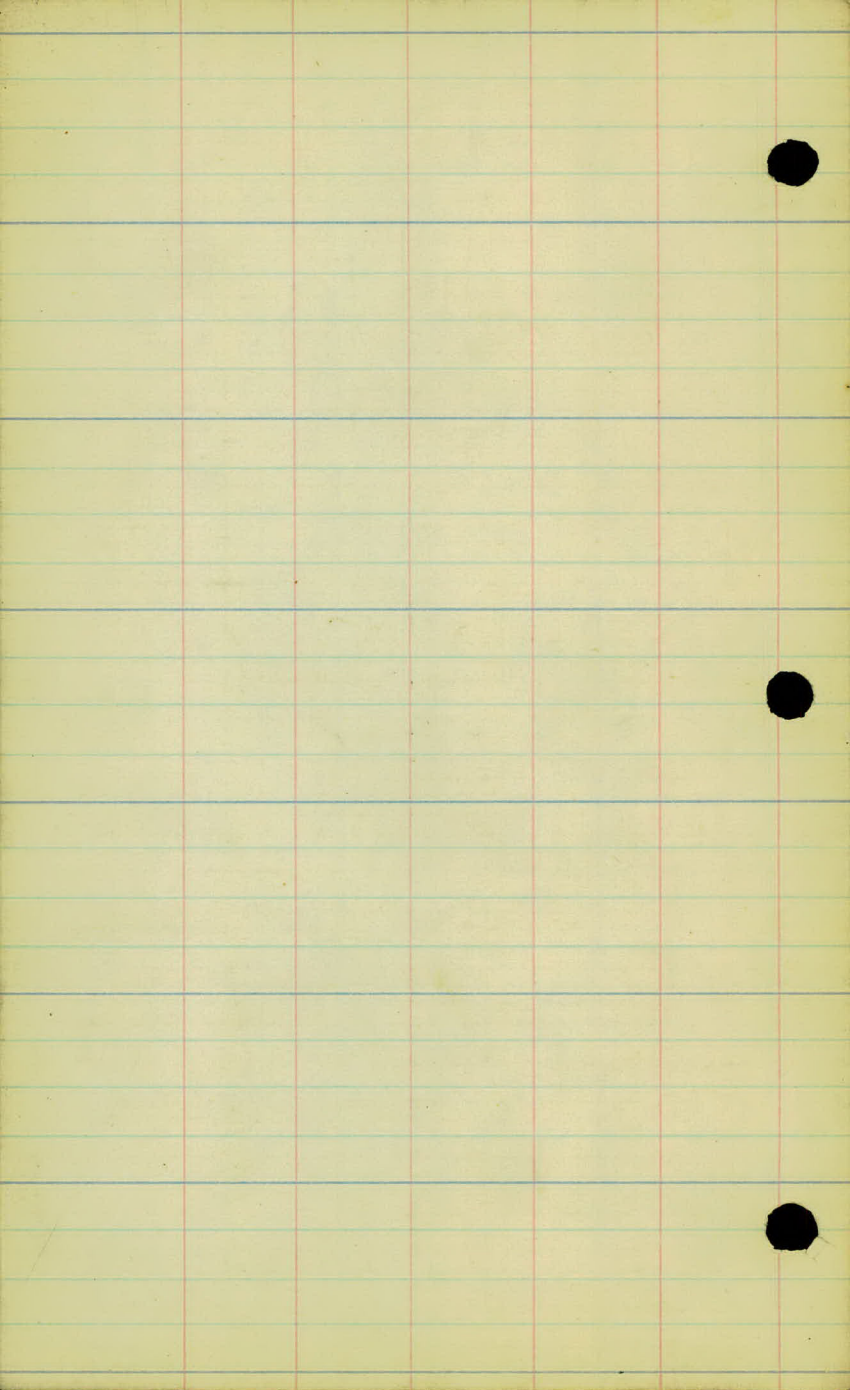
68'

Cultivated.

N.H. Lebens

Cultivated.

P.C. ○



Center Line Levels,
St. Paul-Anoka & Lexington Ave.
Connection.

2" Line.

Sta. 0+00 = 33+21 "A" Line to sta 8+61.53 =
sta. 7+11.8 Lexington Ave Location.

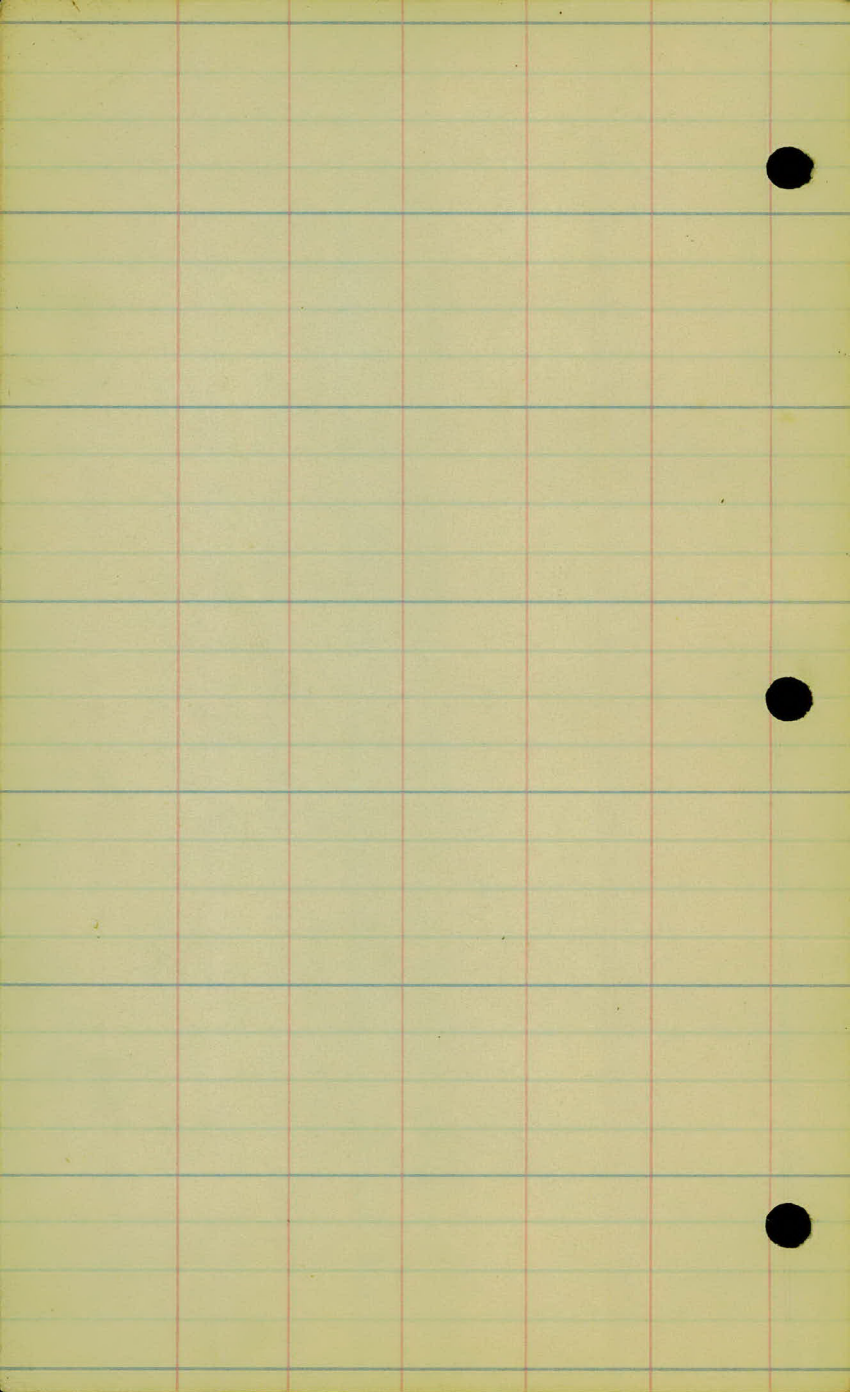
Station	+	H.I	-	Elev.
B.M.	4.28	304.28 ✓		300.00
0+00			6.33	297.95 ✓
+18			7.0	297.3
+30			8.7	295.6
1			9.3	295.0
2			8.9	295.4
3			7.2	297.1
+50			6.0	298.3
4			5.5	298.8
T.P.	1.77	300.94 ✓	5.11	299.17 ✓
+40 ² P.C.			7.6	298.3
5			5.6	295.3
+50			9.2	291.7
6			11.3	289.6
+50			11.6	289.3
7			13.5	287.4
+15			12.7	288.2
+50			9.1	291.8
8			8.7	292.2
+50			8.5	292.4
8+61.5 = 7+118			8.5	292.4
T.P.	8.27	305.09 ✓	4.12	296.82 ✓
For check.			5.07	300.00 ✓

Initial B.M. (assumed) Lexington Ave Datum.
R.R. spike in Tel. pole, S.E. Corner Larpenieur & Lexington
E Larpenieur Ave.

Top of stake -

E Lexington Ave.

(Initial B.M.)



Cross Sections Notes

St. Paul-Anoka & Lexington Ave.
connection.

"L" Line.

Sta	Elev.
6+50	289.3
6+00	289.6
+50	291.7
5+00	295.3
+40% P.C.	298.3
4+00	298.8
+50	298.3
3+00	297.1
2+00	295.4
1+00	295.0
+30	295.6
+18	297.3
0+00 = 33+21	298.0

L

£

R

118

$$\begin{array}{cccccccc} +4.1 & +3.6 & +3.1 & +0.6 & +1.5 & +1.5 & +0.1 & \\ 44 & 33 & 30 & 22 & 17 & 14 & 12 & \end{array}$$

$$\begin{array}{r} -0.9 \\ 33 \end{array}$$

$$\frac{1}{4} \text{ Lex. Ave.}$$

$$\begin{array}{r} +0.5 \\ 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{r} +0.8 \\ 33 \end{array}$$

$$\begin{array}{r} +0.3 \\ 33 \end{array}$$

$$\begin{array}{r} -0.4 \\ 33 \end{array}$$

$$\begin{array}{r} +1.0 \\ 33 \end{array}$$

$$\begin{array}{r} +0.2 \\ 22 \end{array}$$

$$\begin{array}{r} -1.0 \\ 33 \end{array}$$

$$\begin{array}{r} +0.9 \\ 33 \end{array}$$

$$\begin{array}{r} -0.8 \\ 33 \end{array}$$

$$\begin{array}{r} +0.5 \\ 33 \end{array}$$

$$\begin{array}{r} +0.6 \\ 14 \end{array}$$

$$\begin{array}{r} -1.0 \\ 33 \end{array}$$

$$\begin{array}{r} +0.7 \\ 33 \end{array}$$

$$\begin{array}{r} -0.8 \\ 33 \end{array}$$

$$\begin{array}{r} +0.7 \\ 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ 16 \end{array}$$

$$\begin{array}{r} -0.2 \\ 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{ccc} +2.5 & +2.0 & +0.2 \\ 33 & 14 & 2 \end{array}$$

$$\begin{array}{cc} 0.0 & +3.0 \\ 10 & 33 \end{array}$$

$$\begin{array}{r} +0.3 \\ 33 \end{array}$$

$$\begin{array}{r} +0.8 \\ 18 \end{array}$$

$$\begin{array}{ccc} +1.0 & -1.9 & -1.6 \\ 7 & 17 & 33 \end{array}$$

$$\begin{array}{r} -1.0 \\ 33 \end{array}$$

$$\begin{array}{r} -0.5 \\ 17 \end{array}$$

$$\begin{array}{cccc} -0.4 & -0.5 & -2.3 & -2.6 \\ 15 & 23 & 30 & 38 \end{array}$$

Sta

Elev.

8+61.5 = 7+11.8

292.4

8+50

292.4

8

292.2

+50

291.8

+15

288.2

7+00

287.4

L.

£

R

119

$\frac{-5.0}{32}$	$\frac{-5.0}{21}$	$\frac{-0.5}{14}$	$\frac{-0.3}{10}$	$\frac{4}{4}$	$\frac{-0.4}{10}$	$\frac{-0.4}{13}$	$\frac{-4.5}{20}$	$\frac{-5.0}{23}$	$\frac{-5.7}{25}$	$\frac{-5.0}{33}$
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Lex.

$\frac{-5.0}{33}$	$\frac{-5.3}{22}$	$\frac{-0.5}{15}$	$\frac{-0.4}{10}$	$\frac{-0.4}{8}$	$\frac{-0.4}{12}$	$\frac{-4.7}{20}$	$\frac{-5.7}{26}$	$\frac{-5.1}{33}$
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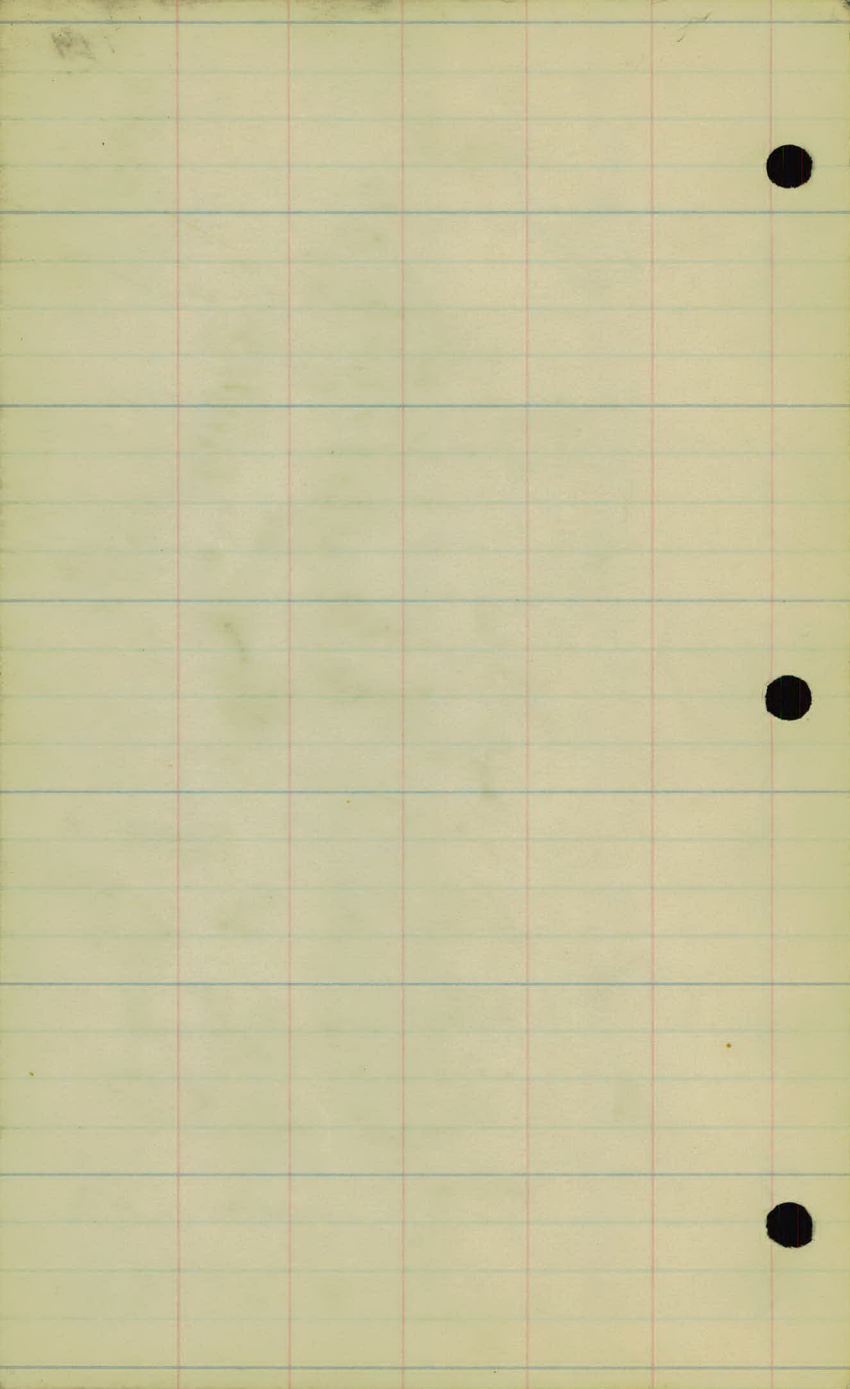
$\frac{-5.1}{33}$	$\frac{-4.8}{24}$	$\frac{-0.6}{17}$	$\frac{-0.4}{14}$	$\frac{+0.1}{4}$	$\frac{-0.5}{10}$	$\frac{-4.8}{17}$	$\frac{-5.5}{27}$	$\frac{-4.8}{33}$
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$\frac{-4.4}{35}$	$\frac{-0.1}{26}$	$\frac{+0.1}{23}$	$\frac{+0.6}{12}$	$\frac{-4.4}{10}$	$\frac{-5.0}{19}$	$\frac{-4.4}{33}$
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$\frac{+4.0}{33}$	$\frac{+4.0}{31}$	$\frac{+4.2}{20}$	$\frac{+4.0}{7}$	$\frac{-0.5}{4}$	$\frac{-1.0}{6}$	$\frac{-1.0}{10}$	$\frac{-0.5}{11}$	$\frac{-1.0}{17}$	$\frac{-0.3}{33}$
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$\frac{+8.4}{33}$	$\frac{+5.3}{27}$	$\frac{+4.8}{12}$	$\frac{+1.0}{5}$	$\frac{-0.2}{4}$	$\frac{+0.5}{7}$	$\frac{+0.2}{33}$
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Lex.

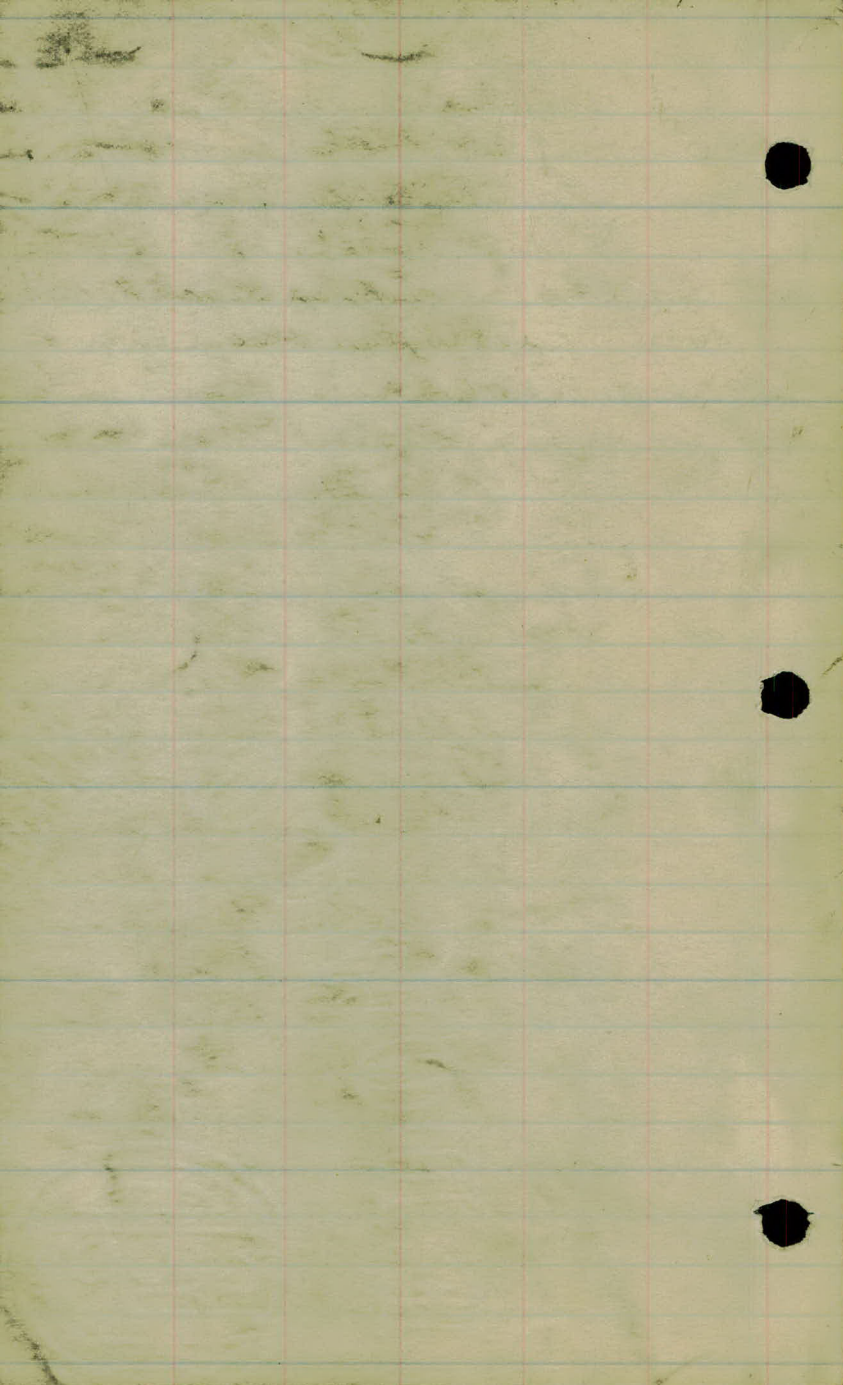


Proj. # 24-01.

The relative Elev. of
Larpenteur Ave. and Lexington
Ave. surveys.

Nail in T.P. N.W. Cor. of Lex. & Larp. from
survey on Larpenteur Ave.

Spk. in T.P. S.E. Cor. of Lex. & Larp. from
survey on Lexington Ave. assume.
Elev. of 300.00.



Check Levels.

Project 24-01

Lexington Ave.

Station 0+00 - Sta. 2+15

	B.S.	H.I	F.S.	Elev.	Orig. Elev.	
B.M.	3.00	303.00		300.00	300.00	
T.P.	6.56	299.36	10.20	292.80		
T.P.	12.69	311.73	0.32	299.04		
B.M.	1.63	310.53	2.83	308.90	308.93	-03
T.P.	5.42	307.13	8.82	301.71		
B.M.	5.49	309.75	2.87	304.26	304.21	+05
T.P.	7.47	315.05	2.17	307.58		
T.P.	0.54	312.56	3.03	312.02		
B.M.	3.41	310.93	5.04	307.52	307.44	+08
T.P.	1.74	304.10	8.57	302.36		
B.M.	2.82	305.15	1.77	302.33	302.23	+10
T.P.	0.38	293.70	11.83	293.32		
T.P.	2.41	283.49	12.62	281.08		
T.P.	9.71	291.28	1.92	281.57		
B.M.	6.64	296.73	1.19	290.09	290.00	+09
T.P.	0.31	288.98	8.06	288.67		
T.P.	0.22	276.74	12.46	276.52		
T.P.	0.40	264.65	12.49	264.25		
T.P.	3.67	257.51	10.81	253.84		
B.M.	3.21	258.34	2.38	255.13	254.99	+14
T.P.	7.62	265.63	0.33	258.01		
T.P.			2.59	263.04	262.90	+14
T.P.						
	25.34		122.30	300.00		
			85.34	263.04		
			36.96	36.96		

(Over)

W.H.C.
A.J.C. } Dec. 1, 1923
A.S.N.
M.S.A.

93

R.R. spike in Tel. Pole S.E. corner Lex. & Larp.

R.R. spike in Tree 36' R. of Sta. 17+12.

R.R. spike in Tree 105' L. of Sta. 28+16

Top of Lower school House step, south end. Sta 52.

R.R. spike in Tree R. Sta. 63+74

R.R. spike in Tree 33' R. Sta. 78+35

R.R. spike in Tree 60' L. Sta 97+25

Spike in Tree 16' R. Sta. 109.

	B.S.	H.I	F.S.	Elev.	Orig. Elev.
	9.29	272.33		263.04	
T.P.	12.31	284.08	0.56	271.77	
T.P.	11.36	295.33	0.11	283.97	
T.P.	6.65	301.20	0.78	294.55	
B.M.			3.47	297.73	297.62 +.11
T.P.	1.54	293.00	9.74	291.46	
T.P.	0.70	282.97	10.73	282.27	
T.P.	0.30	272.27	11.00	271.97	
T.P.	2.06	265.08	9.25	263.02	
B.M.	0.55	259.33	6.30	258.78	252.67 +.11
T.P.	4.03	252.25	11.11	248.22	
T.P.	4.51	252.20	4.56	247.69	
B.M. (New)	2.59	252.37	2.42	249.78	249.66
T.P.	8.62	255.93	5.06	247.31	
T.P.	11.28	266.00	1.21	264.72	
T.P.	12.62	278.20	0.42	265.58	
T.P.	11.33	288.73	0.80	277.40	
B.M.	4.58	292.05	1.26	287.47	289.32 +.15
T.P.	12.70	304.31	0.44	291.61	
T.P.	5.25	308.27	1.29	303.02	
T.P.	0.88	301.37	7.78	300.49	
T.P.	0.64	299.54	12.47	288.90	
B.M.	4.30	284.89	8.95	280.59	280.40 +.19
T.P.	6.85	291.19	.55	284.34	
T.P.	8.79	299.98	0.00	291.19	
T.P.	11.85	310.65	1.18	298.80	
B.M.	155.58 113.29 48.29	306.23 263.04 42.29	4.32	306.33	306.15 +.18
			11.29		

94
W. H. Carlson } Dec 3, 1923
P. C. Crane }
A. S. Nelson } Fair
M. S. Alberg }

Nail in 15" Oak, 50' L. Sta 112+50

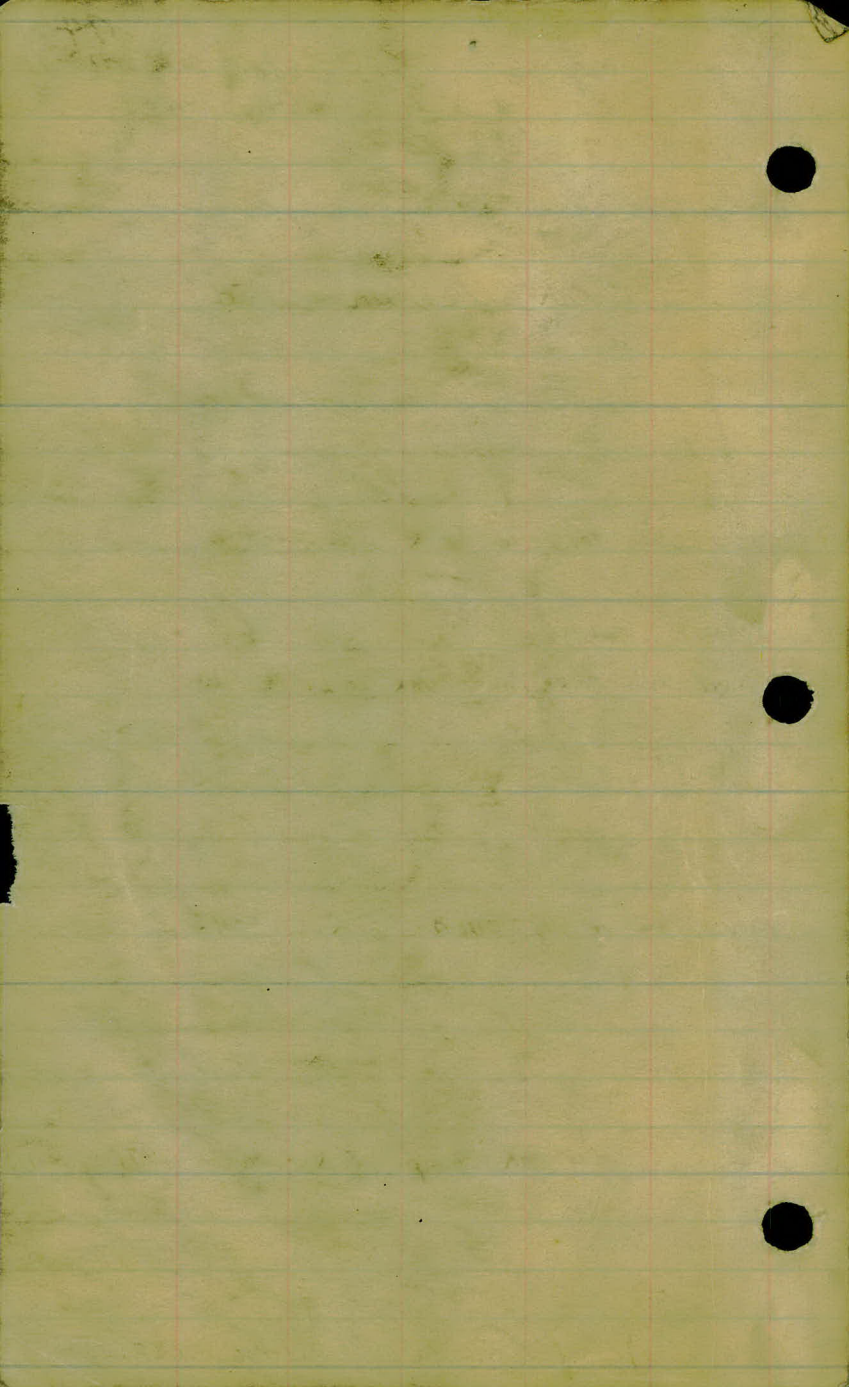
Spike in Tel. Pole 30' R. Sta 128+00

(New B.M.) spike in 14" Oak 60' L. Sta 143.

R.R. spike in 12" Birch 22' R. 164+93

R.R. spike in 14" Oak Stump, 25' R. Sta. 189+37 (Opp. Man.)^{none}

R.R. Spike in 18" Oak 45' R. Sta 216 N.E. cor. Co. Rd. E. Inter.



$$\begin{array}{r} 215 + 71.6 \\ 189 + 37.15 \\ \hline 4634.45 \end{array} \text{ for the } N \frac{1}{2} \text{ of Sec } 34$$

measured along the East line thereof
is = 2634.45' taken from Co Surveyors
notes on project #24-01

694.6 City of

122413