PLANS SURVEY

NEW BRIGHTON ROAD

From Co. Rd. "D"

To Cleveland Avenue

CO. PROJ. Nº 23-63

S.T.H. No. 62

INDEX

New Brighton Rd.

Page	Title	Sta.
1 – 5	Alignment	0+00 – 108+26?
6 – 18	℄ Elevations	0+00 – 108+26?
19 – 33	X sections	0+00 – 108+26?
34 – 54	Art. Topog.	0+00 – 108+26?
55	Culverts	

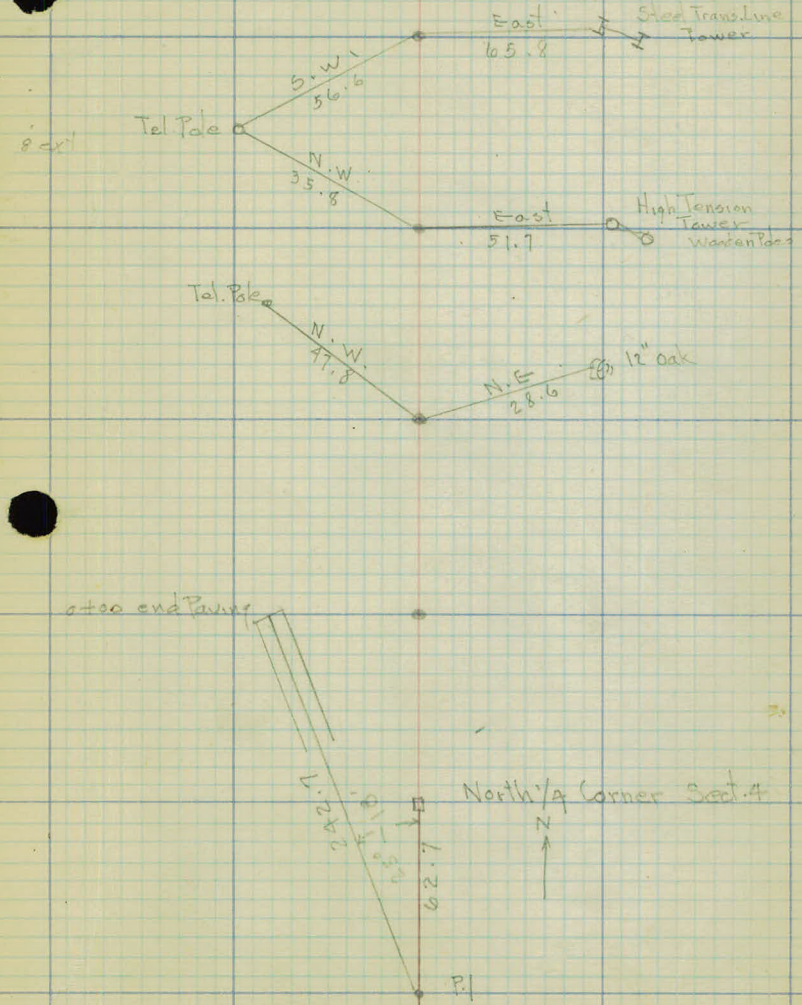
Job 23-63

New Brighton Rd.

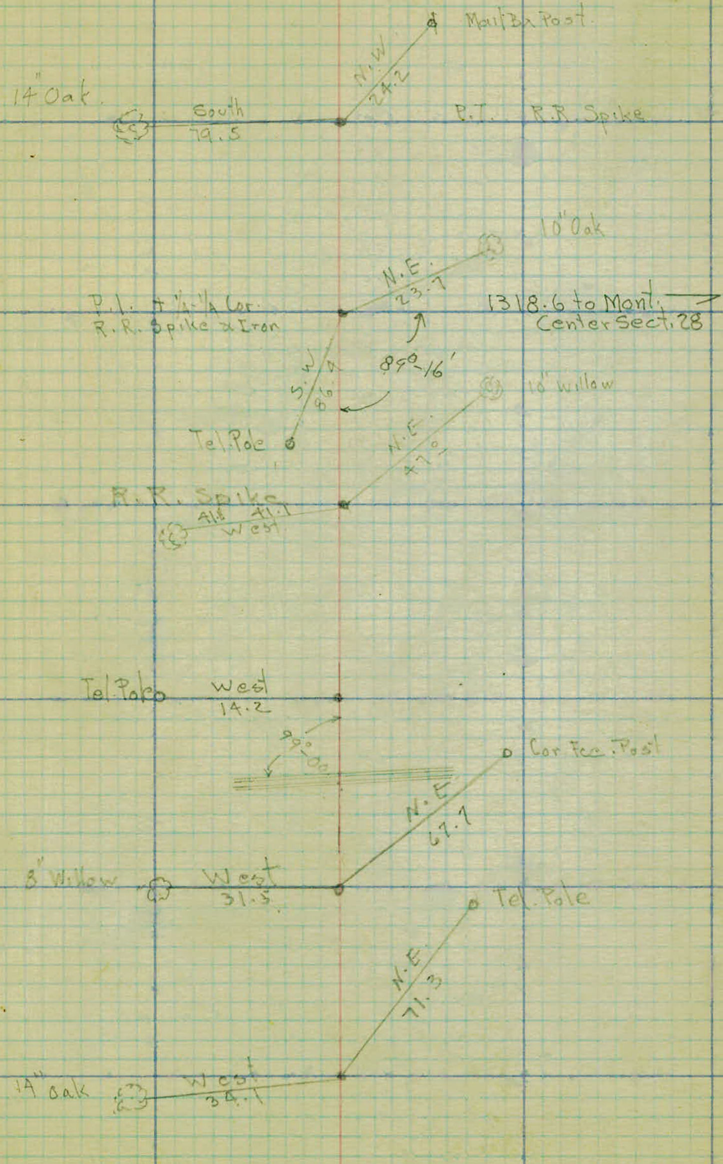
G. Reitler	Inst.
F. Tierney	Level
A. Persons	Rod
W. Wikhusen	Hd. Chain
J. Mahoney	Rr. "
J. Carr	Stakes
M. Galvin	Flag

New Brighton Rd. 3-16-23

Sta.	Point Left & Right		Calc. Mag. Bear
			N00°-39'E N2°-30'W
28+38 17	P.T.		
			Δ 25°-57'
28		12°-58'	C 15°
27+53.4	P.I.		S.T. 88.26
			L.C. 173'
+50		10°-07'	50' C
27		6°-22'	
26+65 14	P.C.	2°-37'	
			N25°-18'W N29°-30'W
0+00	end of Paving		
			N00°00'W
			N4°-30'W


East
65.8
Steel Trans. Line Tower
S.W.
56.6
Tel Pole
8" ±
N.W.
35.8
East
51.7
High Tension Tower
Warren Pole
Tel. Pole
N.W.
17.8
N.E.
28.6
12" Oak
a+00 end Paving
North 1/4 Corner Sect. 4
N
62.7
P.I.

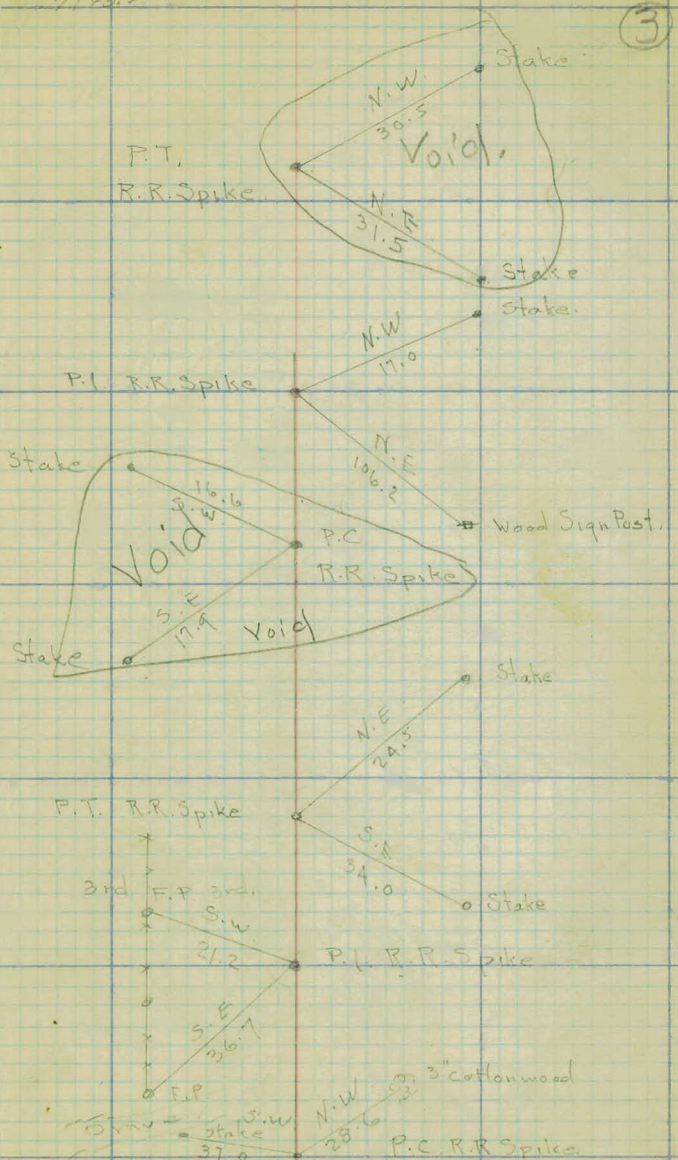
Station	Point	Left & Right	Calc. Mag. Bearing
			N89°-12'W ✓
81+30.9	P.T		
81		44°-38'	
+50		40°-10'	Δ 89°-16'
80		32°-55'	C 29°-0
80+20±	P.I		S.T. 197.10 ✓
+56		25°-40	L.C. 307.80 ✓
79		18°-25'	
+50		11°-10'	
78+23.1	P.C.	3°-55'	
06+63.6	P.O.T.		
			N00-04'E ✓
			N4°-30'W
53+87±	P.I.	0°-35'	
41+13.5	P.O.T.		
			N00-39'E


Mail Bx Post
N.W.
24.2
14" Oak
South
79.5
P.T. R.R. Spike
10" Oak
N.E.
23.7
P.I. + 1/4-1/4 Cor.
R.R. Spike & Iron
1318.6 to Mont.
Center Sect. 28
S.W.
8.6
89°-16'
10" Willow
Tel. Pole
N.E.
47.0
R.R. Spike
41.7
West
Tel. Pole
West
14.2
90°-00'
Cor. Fce. Post
N.E.
67.1
8" Willow
West
31.5
Tel. Pole
N.E.
71.3
14" Oak
West
34.1

3-20-23

Off Brighton Rd

Station	Point	Left.	Right	Calc. Mag Bearing
99+00.30 = 99+01.3	P.T			N88°-58'W
99		23°-53'		
98+50		23°-48'		Δ 47°-46'
98		18°-48'		C 20°-00' 287.49
97+89.2	P.I			S.T 126.92
+50		13°-48'		L.C 238.85
97		8°-48'		
96+61.98	P.C.	3°-48'		
92+51.5	Mont.	on back Tangent Produced		
				N41°-12'W
90+25.7	P.T.			
90		24°-00'		Δ - 48°-00'
+50		21°-24'		C 20'-0
89+13.9	P.I			S.T. 128.2
89		16°-24'		L.C. 240
+50		11°-24'		
88		6°-24'		
87+85.7	P.C.	1°-24'		
				N89°-12'W

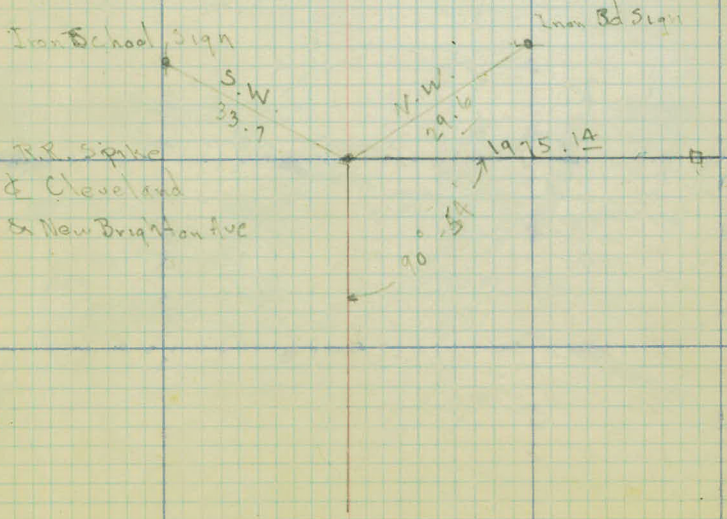

Stake
N.W.
30.5
Void.
P.T.
R.R. Spike.
N.
31.5
Stake
Stake.
N.W
17.0
P.I. R.R. Spike
Stake
N.E
106.2
Wood Sign Post.
S.W.
116.6
Void
P.C
R.R. Spike
S.E
17.1
Void
Stake
Stake
N.E
24.5
P.T. R.R. Spike
S.E
34.0
Stake
3rd F.P. 3rd.
S.W
21.2
P.I. R.R. Spike
S.E
36.1
F.P.
3" Cottonwood
S.W
37.0
N.W
28.6
P.C. R.R Spike.

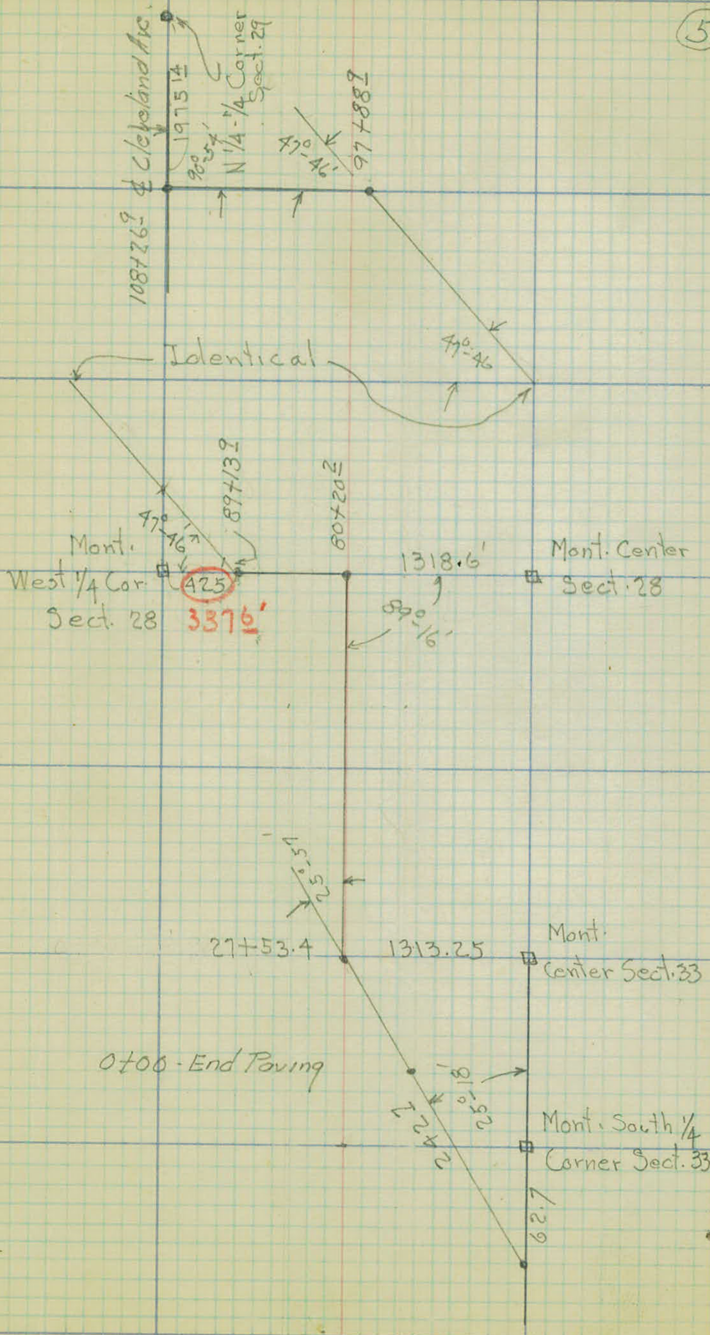
Station	Point	Left	Right	Calc Bearing	Mag.

108+26.9 End Location

N 88°-5[illegible]W

3-21-23 (4)


Iron School Sign
S.W.
33.7
Iron Bd Sign
N.W.
N.E.
N.P. Spike
& Cleveland
& New Brighton Tue
1975.14
90



℄ Cleveland Ave.
N 1/4 - 1/4 Corner Sect. 29
197.5 1/4
90°-57'
47°-46'
97+88.9
108+26.9
47°-46
Identical
47°-46'
89+13.9
80+20.2
Mont.
West 1/4 Cor.
Sect. 28
425
3376'
1318.6'
Mont. Center
Sect. 28
89°-16'
25°-57'
27+53.4
1313.25
Mont.
Center Sect. 33
0+00 - End Paving
25°-18'
2+42
Mont. South 1/4
Corner Sect. 33
62.7

E Levels -

New Brighton Road

B.M. Sp. in 5 piling of first bent E side of Road - El. 196.17

3/16/23

& Levels New Brighton Rd.

B.M.	8.33 ·	235.78 ·		227.45
-4+00			3.9	31.9 ·
-3			3.5	32.3 ·
	5.55 ·	237.83 ·	3.50 ·	232.28 ·
-2			5.2	32.6 ·
B.M			5.87	231.96 ·
-1			5.0	32.8 ·
0+00			4.9	32.9 ·
+50			4.6	33.2 ·
1			4.5	33.3 ·
+50			4.4	33.4 ·
2			4.4	33.4 ·
+50			4.4	33.4 ·
3			4.4	33.4 ·
+50			4.4	33.4 ·
4			4.1	33.7 ·
	6.37	240.02 ·	4.18	233.65 ·
+50			5.8	34.2 ·
5			5.6	34.4 ·
+50			5.4	34.6 ·
6			5.2	34.8 ·
+50			4.8	35.2 ·
7			4.8	35.2 ·
+50			4.8	35.2 ·
8			4.7	35.3 ·

3/16/23

F.P.T
R.P.

(7)

Nail in T.P. ℄ Sta. 129+00 (old survey) 540' S of Cor. (Int. Cty Rd D & N.B. Rd.)

Nail in 12" Oak S.W Cor. Cty Rd D + N.B. Rd.

End pavement — beginning of job

3/16/23

240.02

8+50			4.8	235.2
9			5.5	34.5
+50			6.2	33.8
10			6.8	33.2
B.M	4.32	235.63	8.71	231.31
+50			2.5	33.1
11			3.0	32.6
+50			3.4	32.2
12			4.0	31.6
+50			4.2	31.4
13			4.6	31.0
+50			4.8	30.8
14			4.8	30.8
+50			4.8	30.8
15			4.7	30.9
+50			4.9	30.7
16			5.0	30.6
	4.45	235.01	5.07	230.56
+50			4.5	30.5
17			4.6	30.4
+50			4.5	30.5
18			4.7	30.3
+50			4.8	30.2
B.M			5.99	229.02
19			5.0	30.0
+50			5.1	29.9

3/16/23

F.R.T.
R.P.

(8)

Nail in 15" Oak 25' R. 9+90

Nail in 20" Oak L 18+75

3/16/23

235.01

20			5.1	229.9
+50			5.2	29.8
21			5.7	29.3
+50			5.8	29.2
22	9.45		5.9	29.1
	6.15	23540 · 5.76		229.25
+50			6.2	29.2
23			5.8	29.6
+50			5.4	30.0
24			5.0	30.4
+50			4.7	30.7
25			4.4	31.0
+50			4.3	31.1
26			4.2	31.2
+50			4.1	31.3
B.M	463	236.36 · 3.67		231.73
27			5.2	31.2
+50			5.1	31.3
28			5.0	31.4
+50			5.1	31.3
29	10.60		4.9	31.5
+50	9.43		5.0	31.4
30	1.17		5.0	31.4
+50			5.0	31.4
31			5.0	31.4
+50			4.9	31.5

3/16/23

(9)

F.R.T.
R P

Sp. in T.P L Sta 27+85

3/16/23

236.36

32				5.0	31.4
+50				5.1	31.3
33				5.2	31.2
+50				5.2	31.2
34				5.2	31.2
	5.10	236.40	5.06		231.30
+50				5.1	31.3
35				5.1	31.3
+50				4.9	31.5
36				5.0	31.4
+50				4.9	31.5
37				4.9	31.5
+50				4.9	31.5
38				5.1	31.3
+50				5.1	31.3
39				5.0	31.4
+50				5.0	31.4
40				5.1	31.3
B.M	1.56	233.73	4.23		232.17
+50 +7.6	Pr. Rd. R	232.17 − 231.73 = .44		2.6	31.1
41				2.6	31.1
				3.0	30.7
+50	9.73 − 9.29 = .44	JBN	9.29	3.8	29.9
42				4.5	29.2
+50	Prir. Ent.	R		5.6	28.1
43				6.9	26.8
+50				8.3	25.4

3/16/23

(10)

F.P.T.
R.P.

Sp. in T.P. L 39+50

3/16/23

233.73

44	1.56	10.1	223.6
+50		12.1	221.6
	0.32 222.35 11.70		222.03
45		2.5	19.9
+50		4.4	18.0
46		6.4	16.0
+50		8.0	14.4
47		10.0	12.4
+30	Rtw. Ent. L	11.1	11.3
B.M	9.31		213.04
	1.88		232.17
	21.01		19.13
	1.88		
	19.13		

3/16/23

F.T.?
R.P.?

(11)

Spin T.P L 47+00

3/M/23

B.M	1.24	214.28			213.04
47+50				3.8	211.5
48				5.9	208.4
+50				8.4	205.9
49				10.0	204.3
+50				11.5	202.8
	1.44	204.24	11.48		202.80
50				2.4	201.8
+50				3.3	200.9
51				3.9	200.3
+50				4.5	199.7
52				4.7	199.5
+50				5.1	199.1
53				5.6	198.6
+50				6.1	198.1
54				6.3	197.9
+50				6.5	197.7
55				7.0	197.2
	4.11	201.07	7.28		196.96
				+11.47	212.54
+50				4.6	196.4
56				5.0	196.0
B.M			4.41		196.66
					16.38

6.79

2.17
6.79
16.38

3/17/23

Sp. in T.P L 47+00

(12)

El. bottom of girder at bridge
& bridge. (Soo R.R.)

Sp T.P. L 56+15

3/22/23

B.M.	4.25 200.91		196.66
B.M.		3.75	197.16

3-22-23

Sta. 56+15
196+66

B.M. 196.66

Sta.	B.S	H.I.	F.S.	Rod	Elev.
	8.38	205.04.			
56+50				8.9	196.1.
57				8.4	196.6.
+50				7.1	197.9.
58				5.5	199.5.
+50				3.6	201.4.
59				1.6	203.4.
T.P.			0.87		204.17.
	11.15	215.32.			
59+50				10.1	205.2.
60				8.2	207.1.
+50				6.4	208.9.
61				4.5	210.8.
+50				2.4	212.9.
62				0.9	214.4.
T.P.			0.77		214.55.
	11.62	226.17.			
+50				9.8	216.4.
63				8.1	218.1.
B.M.			5.83		220.34.
+50				6.5	219.7.
64				4.9	221.3.
+50				3.4	222.8.

New. Brighton Road.

(14)

Spike in Tel. Pole on Left.

R.R. Spike in 14" oak Sta. 63+10 ~~Left~~ Right

Sta.	B.S	H. I.	F.S	Rod	Elev.
		226.17			
65				2.2	224.0
+50.				1.2	225.0.
T.P			1.32		224.85
	5.65	230.50.			
66				4.7	225.8
+50				3.9	226.6
67				3.8	226.7
+50				4.0	226.5
68				4.5	226.0
+50				5.5	225.0
69				6.7	224.8 223.8
+50				8.0	222.5
70				9.6	220.9
+50				10.4	220.1
71				10.6	219.9
T.P.			10.57		219.93
	6.40	226.33			
+50				6.8	219.5
72				6.3	220.0
+50				5.3	221.0
73				5.0	221.3
+50				4.8	221.5
74				4.7	221.6
+50				5.0	221.3
75				5.2	221.1

(15)

3-22-23

N. Brighton Rd

Sta.	B.S	H I	F.S	Rod	Elev
		226.33			
75+50				5.3	221.0
76				5.7	220.6
+50				6.6	219.7
77				7.9	218.4
T.P.			7.74		218.59
	0.55	219.14			
+50				1.65	217.5
78				3.3	215.8
+50				5.1	214.0
79				7.1	212.0
+50				9.5	209.6
80				11.2	207.9
B.M.			11.63		207.51
	0.10	208.21			
+50				2.2	206.0
81				4.5	203.7
+50				6.3	201.9
82				8.5	199.7
+50				9.8	198.4
83				10.1	198.1
T.P.			9.47		198.74
	6.80	205.54			
+50				7.5	198.0
84				7.6	197.9
+50				6.6	198.9

3-22-23

(16)

New Brighton Rd

On R.R. Spike in 6" oak to left sta. 80+00

Sta.	B.S.	H.I.	F.S.	Rod	Elev.
		205.54			
85				5.8	199.7
B.M.			0.93		204.61
+50				4.7	200.8
86				3.5	202.0
+50				2.4	203.1
87				1.3	204.2
T.P.			0.30		205.24
	8.52	213.76			
+50				8.7	205.1
88				7.6	206.2
+50				6.7	207.1
89				6.1	207.7
+50				4.9	208.9
90				3.8	210.0
+50				2.8	211.0
91				1.8	212.0
T.P.			1.50		212.26
	11.29	223.55			
+50				10.1	213.4
92				8.6	215.0
+50				7.4	216.1
93				6.3	217.3
+50				4.2	219.3
94				3.3	220.3
+17				2.3	221.3

3-23-23 (17)

On 16" Oak. R.R. Spike 35+75 Left

Sta.	B.S.	H.I.	F.S.	Rod	Elev.
		223.55			
94+30				1.0	222.5
T.P.			1.19		222.36
	10.91	233.27			
+50				9.1	224.2
95				8.1	225.2
+50				7.4	225.9
96				7.4	225.9
+50				6.5	226.8
97				5.6	227.7
+50				5.4	227.9
98				3.6	229.7
+50				3.9	229.4
99				3.7	229.6
	3.57	233.36	3.48		229.79
100				4.3	229.1
101				4.9	228.5
+80				5.4	228.0
102				5.4	228.0
103				6.2	227.2
104				6.9	226.5
	1.80	229.50	5.66		227.70
105				3.8	225.7
106				4.8	224.7
107				5.7	223.8
108				6.6	222.9
+269				6.5	223.0
B.M.			5.35		223.15

224.15

Priv. Ent. L.

Int. Cleve. Ave. End Line
Sp. in T.P. S.E. Cor. Int. Cleve & N.B. Rd.

X Sections New Brighton Rd.

Beginning at End Pave
(Int. Cty Rd. D. & N.B. Rd.

3/19/23

+50	235.2
6	34.8
+50	34.6
5	34.2
+50	34.2
4	33.7
+50	33.4
3	33.4
+50	33.4
2	33.4
+50	33.4
1	33.3
+50	33.2
0+00	232.9

Tierney
Mahoney
Persons

3/19/23

(20)

+0.8/33 +0.5/25 -1.0/22 -1.8/18 00/13 -0.4/15 -1.0/20 -1.5/24 -0.5/28 2.0

+0.5/33 00/25 -1.1/22 -1.1/16 -0.1/12 00/9 -0.5/20 00/27 -0.6/33

-0.6/33 -1.0/26 -2.2/23 -2.0/18 -0.4/13 -0.7/15 -2.0/19 -2.0/21 -0.7/23 00/28 -0.8/33

2.0 -1.5/29 -2.6/24 -2.1/18 -0.7/13 -0.5/15 -1.5/25 -2.0/33

-1.2/29 -2.2/26 -2.1/17 -0.6/13 -0.5/15 -1.5/21 -0.7/26 2.0

2.0. -1.0/30 -2.0/25 -2.1/19 -0.4/13 -0.5/15 -1.5/19 -1.0/23 2.0.

-2.0/33 -2.0/24 -1.8/18 -0.5/13 -0.5/15 -1.5/18 -1.5/23 2.0

-2.4/33 -1.0/23 -1.7/22 -1.3/16 -0.3/13 -0.5/15 -1.0/21 -1.0/27 -1.4/33

2.0. -0.5/30 -0.5/22 -2.1/20 -2.1/16 -0.3/12 -0.8/15 -1.5/18 -2.0/23 -0.6/24 2.0

2.0 +1.0/28 +0.5/21 -1.1/19 -1.1/16 -0.4/12 00/15 -1.0/18 -1.0/22 00/23 2.0

2.0 +1.4/28 +0.5/21 -0.8/19 -1.4/15 -0.2/12 -0.3/15 -0.8/18 -0.8/22 +0.5/23 2.0

+1.0/21 -0.3/20 -0.9/15 -0.1/12 -0.2/15 -0.6/22 +0.8/23 2.0

2.0. +1.0/26 +0.4/21 -0.7/12 -0.4/9 -0.5/19 00/22 2.0.

2.0 +0.5/22 -1.0/19 -0.8/12 -0.3/6 -0.4/11 -0.4/22 +0.4/26 +0.4/33

3/19/23

+50	230.8
13	31.0
+50	31.4
12	31.6
+50	32.2
11	32.6
+50	33.1
10	33.2
+50	33.8
9	34.5
+50	35.2
8	35.3
+50	35.2
7	235.2

3/19/23

(21)

-1.3	-0.3	-0.5	-0.8	-1.6	-3.0	-3.5	
18	14	9	10	17	23	33	
± 0.4	00	-1.7	-1.0	-0.3	-0.3	-0.6	-0.8	-3.7	-4.5
33	27	23	16	11	9	9	16	23	33
+1.5	+1.0	-1.0	-1.7	00	-0.5	-0.6	-2.0	-2.5	-2.5	-4.0	SS
33	27	22	16	14	9	16	21	23	26	33	
+2.5	+1.5	-0.5	-1.0	00	-0.7	-2.5	-2.5	-1.5	-2.5
33	25	22	18	15	16	21	24	26	33
L.0	+2.0	-1.0	-1.0	00	-0.4	-2.2	-2.2	-0.7	-2.0
	27	22	18	15	15	20	24	27	33
+1.5	+1.0	-1.0	-1.6	00	-0.1	-2.2	-2.3	-0.8	-2.6
33	25	21	17	13	15	20	25	28	33
00	00	-1.5	-1.5	-0.5	-0.3	-2.0	-0.7	-2.5
33	24	21	16	13	15	21	29	37
+0.5	01	-1.8	-1.8	+0.3	-0.5	-2.2	-2.5
32	23	21	17	10	15	23	35
L.0	-1.0	-2.0	-2.0	-0.5	-0.5	-2.0	-3.0	-3.7
	25	23	18	13	15	19	26	33
L.0	-0.5	-1.6	-1.6	-0.3	-0.5	-2.1	-2.1	L.0
	25	24	19	14	15	23	26	
L.0	-0.5	-1.5	-1.5	-0.5	-0.3	-1.9	-1.1	-1.6
	30	23	19	15	15	23	25	33
L.0	-1.0	-2.0	-2.0	-0.5	-0.5	-1.0	-2.0	-1.0	L.0
	29	25	19	13	15	20	24	28	
	-1.5	-2.0	-2.0	-0.7	-0.4	-1.5	-1.5	-1.0	L.0
	33	22	17	13	15	20	24	28	
00	00	-1.1	-1.1	-0.4	-0.3	-1.0	00
33	22	21	18	13	15	22	30

3/19/23

+50		~29.8
20		29.9
+50		29.9
19		30.0
+50		30.2
18		30.3
+50		30.5
17		30.4
+50		30.5
16		30.6
+50		30.7
15		30.9
+50		30.8
14		30.8
+74	P.Ent. R	230.8

3/19/23

(22)

+1.5/39 −3.0/24 −2.0/20 −0.5/15 −0.3/9 00/17 −2.5/26 +5.0/46

+5.0/41 −3.5/21 −0.5/15 +5/11 00/9 +0.2/19 −2.0/25 +1.5/37

+1.0/38 −2.0/19 −0.4/13 −0.2/9 00/17 −1.1/22 −2.9/33

L.0. −2.5/19 −0.5/13 −0.3/9 00/18 −2.0/23 −2.5/28 L.0

L.0 −3.0/26 −0.6/12 −0.3/9 −0.5/16 −2.4/21 −2.1/25 −1.2/30 L.0

5.5 −2.5/29 −2.4/24 −2.4/20 −0.5/12 −0.4/9 −0.4/17 −1.1/21 −2.0/27 −0.5/28 00/34

−0.9/33 −0.5/25 −2.1/22 −2.1/17 −0.5/12 −0.5/8 00/16 −1.1/19 −2.0/24 00/28 +0.5/36

L.0 −1.0/23 −2.4/21 −2.0/17 −0.5/12 −0.4/8 −0.5/17 −2.0/21 −2.5/25 00/28 L.0.

L.0 −2.5/28 −2.0/18 −1.0/12 −0.5/10 −0.5/15 −2.3/21 −2.4/25 −1.0/28 L.0

−1.0/33 −2.4/23 −2.5/20 −2.1/17 −0.5/12 −0.3/7 −0.5/10 −0.5/17 −2.5/22 −2.5/25 −2.8/28 −1.7/33

+0.5/33 −0.5/23 −1.5/21 −1.5/16 −0.3/13 −0.3/7 −0.7/16 −0.7/17 −2.5/20 −2.5/24 −1.5/22 L.0

L.0 00/27 −1.5/20 −1.5/14 −0.5/11 −0.7/18 −2.1/21 −2.0/25 −0.5/29 L.0

L.0 00/25 −1.7/21 −1.5/18 −0.5/15 −0.4/8 −1.0/17 −2.5/21 −2.5/24 −1.1/28 L.0.

L.0 −0.5/24 −1.4/22 −1.6/18 −0.5/16 −0.2/9 −0.8/9 −1.2/16 −2.5/20 −3.0/25 −2.1/30 L.0

L.0 −1.0/35 −1.0/25 −1.2/21 −0.5/18 −0.4/14 −1.3/17 −3.0/35

3/19/23

+50	Old driveway L	23.3
27		31.2
+50		31.3
26		31.2
+50		31.1
25		31.0
+50		30.7
24		30.4
+50		30.0
23	12"	29.6
+50		29.2
22		29.1
+50		29.2
21		29.3

3/19/23

(23)

-1.5/45 -1.5/34 00/15 √ -0.2/12 -1.5/22 -2.6/30 L.6

L.6 -0.5/18 00/14 -0.5/16 -1.0/21 -1.3/27 L.6

L.6 +0.5/24 -1.0/22 -1.0/16 +0.2/12 -0.3/16 -1.6/18 -1.6/22 00/24 L.6

L.6 +1.5/28 -1.0/22 -1.5/16 00/12 √ -0.3/15 -1.5/20 -1.5/22 +2.8/25 L.6

L.6 +2.5/28 -2.4/21 -1.5/17 -0.2/12 √ -0.2/15 -1.2/20 +3.8/26 L.6

L.6 +2.8/28 -2.5/19 -0.2/12 -0.5/15 -1.9/21 -3.5/28

L.6 +2.8/28 -2.2/18 -0.5/11 -0.2/17 √ -1.5/20 +4.9/30 L.6

L.6 +2.2/30 -2.2/18 00/11 -0.2/16 √ -2.5/24 -1.5/30 -1.5/35

L.6 +1.8/28 -2.0/17 00/10 +0.2/17 √ +2.5/25 +2.5/30 -1.5/38

-3.0/33 -3.8/19 -0.5/12 00/16 √ -4.5/26 -3.8/32 +0.5/40

L.6 -13.0/35 -0.3/11 00/17 -4.5/33

-16.5/45 -15.0/36 -0.4/18 00/8 √ 00/18 -4.5/34

-16.8/45 -15.0/35 -0.5/13 [illegible] 00/15 -3.8/27 -1.5/33

-6.8/33 -4.0/20 00/13 - √ +0.2/19 00/17 -2.0/23 +4.5/38

3/21/23

+50	31.3	Tierney, Persons, Mahoney, Carr
34	31.2	
+50	31.2	
33	31.2	
+50	31.3	
32	31.4	
+50	31.5	
31	31.4	
+50	31.4	
30	31.4	
+50	31.4	
29	31.5	
+50	31.3	
28	31.4	

3/21/23

41	230.7
+70	31.1 Rdwy R
+50	31.1
40	31.3
+50	31.4
39	31.4
+50	31.3
38	31.3
+50	31.5
37	31.5
+50	31.5
36	31.4
+50	31.5
35	231.3

L.6 +3.5/33 -1.5/26 -1.5/20 +0.2/16 00/15 -1.3/19 -1.3/25 +3.7/36 L.0.

+2.0/35 -1.0/29 -1.0/22 00/18 00/15 +1.0/46

L.0. +1.0/33 -1.0/29 -1.0/20 00/17 00/15 -1.0/15 -1.0/24 +2.0/29 +2.0/35

-1.0/35 +0.5/31 +0.2/27 -1.0/24 -1.0/21 +0.2/17 00/15 -1.0/20 -1.0/24 +1.0/28 L.0

-2.5/35 -1.0/28 -1.7/26 -1.7/22 00/17 00/15 -2.0/20 -2.0/24 -0.5/26 L.0.

-2.5/33 -2.5/25 00/21 00/15 -1.5/16 -1.5/20 -1.5/23 -2.0/25 -3.0/33

-3.0/33 -2.1/27 -2.1/25 00/20 00/16 -1.7/15 21 L.0

-3.0/33 -2.0/27 -2.0/22 -0.5/16 00/15 -1.3/19 -1.3/22 -0.5/24 -1.5/33

-2.0/33 -1.4/26 -1.4/25 -1.4/20 -0.5/14 00/14 00/15 -1.0/20 -1.0/24 +0.2/26 L.0

-1.0/33 -0.5/25 -1.2/21 -1.2/20 -0.2/14 00/13 +0.2/15 -0.6/18 -0.6/22 +0.4/26 L.0

-1.2/32 +0.5/24 -0.2/23 -0.2/20 00/15 √ 00/14 -0.3/18 00/21 +1.2/25 +1.2/33

-0.7/33 00/26 -1.0/22 -1.0/22 00/16 √ 00/14 -0.6/19 -0.6/22 +1.2/24 L.0

-1.0/33 -0.6/26 -1.2/21 -0.2/15 √ 00/15 -1.0/18 -0.8/21 00/25 L.0

-1.0/33 -1.0/25 -1.2/21 -0.2/19 -1.2/15 √ 00/13 -1.0/18 -1.0/21 00/25 -0.4/33

3/21/23

48	208.4
+50	10.5
+30	11.3 Rdwy L (12" Cor. I Culv. 11 to Rd)
47	12.4
+50	14.4
46	16.0
+50	18.0
45	19.9
+50	21.6
44	23.6
+50	25.4
43	26.8
+50	28.1 PR. E-R.
42	29.2
41 +50	229.9

-1.5/33 -1.0/24 -0.5/17 00/15 | +0.2/16 -0.8/20 -1.5/28 L.O.

-0.5/37 -0.8/27 -0.8/21 00/16 | 00/16 -0.9/18 -2.5/35

+1.0/45 +0.3/20 | 00/16 -1.5/20 -2.5/33 L.O

L.O. +0.5/33 +0.5/30 -1.5/26 -1.5/20 00/16 | 00/17 -1.5/23 -3.0/33 L.O

L.O +0.5/31 -1.0/27 -0.8/21 +0.4/17 | -0.5/17 -2.5/23 L.O.

L.O 00/28 -1.5/26 -1.5/20 +0.4/16 | 00/16 -2.5/21 L.O.

00/34 +1.0/26 -1.2/23 -1.2/18 00/15 | 00/17 -1.5/21 L.O

L.O. +0.4/26 -1.3/25 -1.3/20 +0.4/16 | 00/18 -2.0/23 -2.0/27 -0.7/29 -0.7/34 L.O

L.O +2.5/34 -1.3/27 -1.3/21 00/18 | 00/18 -1.6/22 -1.0/29 +1.0/32 L.O

L.O +3.5/43 +4.0/35 -1.0/26 -1.0/21 +0.5/15 | +0.2/18 -1.5/22 -1.5/28 +2.5/33 L.O

L.O +4.0/36 -1.0/26 -1.0/21 +0.2/18 | +0.3/15 -1.2/19 -1.2/23 +2.0/29 L.O.

L.O +3.5/34 -0.8/26 -0.8/21 +0.6/18 | +0.2/16 -1.2/20 -1.2/25 +2.2/29 L.O.

L.O +5.0/34 -1.3/26 -1.3/21 +0.5/14 | 00/15 +0.2/25 +2.0/46

+5.0/33 -1.5/25 -1.5/21 x 0.3/17 | +0.2/15 -1.0/20 -1.0/24 +4.1/32 L.O.

+5.0/34 -1.4/25 -1.4/20 0 0/17 | +0.2/15 -1.3/18 -1.3/25 +4.9/32 L.O

3/21/23

+50	198.1
53	98.6
+50	99.1
52	99.5
+50	199.7
51	200.3
+50	200.9
50	01.8
+50	02.8
49	04.3
+50	205.9

3/21/23 (27)

+1.0/39 -2.0/30 -1.5/22 00/18 -0.4/18 -1.2/26 -2.0/35

L.O. -2.0/22 00/16 00/18 -1.0/21 -2.0/33

L.O. -2.5/26 +0.2/16 -0.5/17 -3.0/22 L.O

L.O. -3.0/24 00/16 -0.4/16 -3.0/25 L.O

L.O -3.2/25 00/16 -0.2/18 -2.5/22 L.O

L.O -3.5/25 +0.3/17 -0.1/17 -2.5/23 -2.5/29 -2.0/33

L.O. -4.0/25 00/16 00/17 -2.5/24 L.O

L.O -4.0/23 00/15 00/17 -2.5/24 L.O

L.O. -4.5/24 -0.2/16 +0.1/17 -3.5/27 L.O

L.O -3.7/25 00/16 00/16 -3.0/26 L.O

-3.0/37 -2.5/27 -2.0/21 00/16 00/15 -0.5/17 -1.0/23 -1.5/26 L.O

59	203.4
+50	201.4
58	199.5
+50	97.9
57	96.6
+50	96.1
56	96.1
+80	96.3
+70	96.4 Along N Edge Br. Emb
+50	℄ Bridge 96.5
+30	96.8 Along S Edge Br. Emb.
+20	97.0
55	97.2
+50	97.7
54	197.9

L.O -9.5/30 +0.2/14 +0.5/15 -7.8/26 L.O

L.O. -7.5/28 00/14 +0.2/15 -7.0/26 L.O.

L.O -5.0/24 00/14 00/15 -2.8/24 L.O

L.O. -4.0/20 00/14 -0.2/16 -4.0/24 L.O.

Marsh

L.O. -2.5/18 00/14 -0.4/16 -2.5/22 L.O

L.O. -2.1/18 00/14 -0.5/16 -2.7/20 L.O

-1.7/18 00/14 00/16 -1.8/19 -1.5/27 L.O

+1.3/33 00/24 +0.5/15 00/16 -1.9/19 -0.5/23 S.S.

+1.0/33 00/25 +0.5/15 +0.1/10 +1.0/19 +3.0/28 S.S.

+2.5/33 +1.0/28 00/21 +0.2/10 -0.5/10 +1.9/20 +3.0/26 +5.0/29 +7.9/33

S.S +6.0/37 +4.0/33 +2.0/26 +0.5/17 +0.1/18 00/21 +4.2/29 +6.0/33 S.S.

-2.0/23 -2.0/21 00/15 -0.4/19 -2.4/23 L.O

-2.1/37 -2.0/20 00/15 -0.2/19 -2.5/24 L.O.

-2.0/38 -2.0/24 +0.2/18 -0.5/20 -3.0/25 L.O.

00/14 -2.0/30 -2.0/23 +0.2/17 -0.4/17 -3.5/25 L.O

Marsh

66	25.8
+50	25.0
65	24.0
+50	22.8
64	21.3
+50	19.7
63	18.1
+50	16.4
62	14.4
+50	12.9
61	10.8
+50	08.9
60	07.1
+50	05.2

+8.5 / 35 | -1.8 / 28 | -2.0 / 23 | 00 / 16 | √ | -0.2 / 15 | -1.2 / 20 | -1.2 / 20 | +11.5 / 38

+4.8 / 36 | 00 / 32 | -2.4 / 22 | -0.1 / 17 | √ | +0.1 / 14 | -1.5 / 18 | -1.2 / 21 | +2.5 / 33 | ss. 4

+1.8 / 33 | -1.4 / 26 | -1.7 / 21 | +0.2 / 16 | √ | 00 / 14 | -1.0 / 17 | -1.0 / 24 | -0.17 / 33 | +3.5 / 38

-6.5 / 36 | -5.0 / 29 | +0.2 / 15 | √ | +0.5 / 14 | -3.5 / 22 | -4.2 / 36 | -4.4 / 33

L.O. | -10.0 / 36 | -0.1 / 15 | √ | +0.2 / 15 | -5.0 / 25 | L.O.

LO | -7.5 / 31 | -0.3 / 15 | √ | +0.5 / 15 | -1.5 / 21 | -1.7 / 36

-5.0 / 33 | -4.0 / 24 | 00 / 15 | √ | +0.3 / 15 | +1.3 / 22 | +2.5 / 28 | +2.6 / 37

+1.0 / 37 | -0.5 / 29 | 00 / 16 | √ | +0.1 / 15 | -0.7 / 19 | +6.5 / 34

+7.5 / 42 | -1.5 / 33 | -1.7 / 21 | +0.2 / 15 | √ | +0.4 / 15 | -1.0 / 17 | +5.0 / 28 | +9.3 / 36

+9.0 / 40 | -1.5 / 25 | -0.7 / 18 | +0.3 / 16 | √ | +0.3 / 16 | -1.0 / 17 | -1.0 / 20 | +8.0 / 33

+5.0 / 23 | -1.2 / 25 | -1.2 / 19 | +0.2 / 17 | √ | +0.3 / 14 | -0.4 / 16 | +1.5 / 23 | +1.5 / 29 | +0.5 / 33

+8.5 / 37 | -2.0 / 25 | -2.0 / 19 | 00 / 15 | √ | +0.4 / 15 | -4.0 / 23 | L.O

L.O. | -5.0 / 24 | +0.2 / 15 | √ | +0.5 / 15 | -7.5 / 27 | L.O

L.O | -8.5 / 30 | +0.2 / 15 | √ | +0.5 / 15 | -9.5 / 29 | L.O

73	21.3
+50	21.0
72	20.0
+50	19.5
71	19.9
+50	20.1
70	20.9
+50	22.5
69	23.8
+50	25.0
68	26.0
+50	26.5
67	27.6
+50	226.6

-0.5/36 -2.0/24 -0.2/15 -0.1/15 -8.0/29 L.O.

-5.0/33 -5.0/29 0.0/15 -0.4/14 -9.0/28 L.O.

-7.0/34 -6.5/29 +0.3/17 +0.1/14 -8.0/29 L.O.

-5.0/35 -5.0/27 +0.5/16 0.0/14 -6.5/25 L.O.

-5.5/36 -5.5/27 +0.2/15 -0.2/14 -8.2/28 L.O.

-5.7/33 -5.7/28 +0.3/16 +0.3/16 +0.1/15 -8.5/29 L.O.

-6.1/33 -6.1/30 +0.2/16 0.0/14 -9.5/27 L.O.

-1.6/33 -1.6/29 -2.0/27 -1.6/21 0.0/16 0.0/14 -9.0/26 L.O.

+3.5/34 -1.0/34 -1.3/20 -0.2/16 0.0/15 -3.2/21 -5.1/27 -6.1/33

+9.5/33 0.0/22 -1.0/17 0.0/15 +0.3/15 -0.9/19 -0.1/22 +5.3/29

+12.0/33 +0.5/22 -0.6/18 +0.3/14 +0.3/15 -0.8/18 -0.5/21 +12.0/34

+12.5/33 -0.6/18 +0.2/15 +0.3/15 -0.3/18 +0.2/21 +14.5/36

+11.5/36 -1.1/23 -1.5/19 +0.2/15 +0.3/15 -0.5/18 0.0/23 +13.5/38

+9.0/30 -1.7/25 -2.0/20 +0.3/15 0.0/15 -1.0/18 +12.5/40

3/23/23

Thackray
Mahaffey
Perkins
Carr

80	07.9
+50	09.6
79	12.0
+50	14.0
78	15.8
+50	17.5
77	18.4
+50	19.7
76	20.6
+50	21.0
75	21.1
+50	21.3
74	21.6
73 +50	22.5

-4.0/48 -3.5/40 -1.7/30 -1.9/26 -0.8/22 +0.2/16 -1.7/23 L.O.

L.O. -9.5/50 -8.0/40 -1.5/21 +0.5/17 -1.0/22 -1.0/34

L.O. -10.5/35 -1.2/19 +0.5/16 -4.5/38

S.S. -8.5/50 -9.0/38 -1.0/21 -0.2/14 -6.0/28 L.O

L.O +1.2/32 -1.4/26 -1.5/22 -0.4/18 +0.1/15 -1.2/20 -0.7/24 +0.5/26 L.O.

L.O. +5.0/34 -0.5/26 -0.6/21 +0.1/16 0.0/15 -0.8/18 -0.4/22 +1.7/26 L.O.

+1.2/32 -0.7/26 -0.6/21 +0.2/17 +0.1/16 -0.8/19 -0.2/23 +1.3/27 L.O

+7.4/35 -1.1/25 -1.0/21 +0.1/16 0.0/15 -0.8/20 -0.7/25 +0.8/28 +0.2/33

+2.3/34 +2.3/32 -1.1/25 -1.0/20 0.0/16 +0.2/15 -0.8/20 -0.9/24 +1.2/28 +0.8/33

-0.7/23 +0.1/28 -0.8/20 +0.2/17 -0.7/15 -1.3/21 -1.2/34

+5.0/35 +3.5/30 -0.7/22 -0.6/20 +0.1/17 -0.3/15 -2.2/21 -2.7/33

+10.5/37 -0.5/24 -0.5/20 +0.2/17 0.0/16 -1.5/21 -1.3/25 +1.7/30 +1.3/33

+9.5/38 -0.5/23 -0.5/19 0.0/16 -0.3/16 -1.2/20 -1.2/29 +1.5/31 +1.3/33

+3.0/34 +1.9/29 -1.0/24 -1.0/20 -0.2/16 -0.3/15 -2.6/25 -2.7/33

+50	203.1
86	02.0
+50	200.8
85	199.7
+50	98.9
84	97.9 30" Corr. I Culv. in place
+50	98.0
83	98.1
+50	98.4
82	199.7
+42	202.3
+30	02.7 Pr. Ent. R
81	03.7
80+50	206.0

+16.0/45 +2.3/24 -0.7/21 -0.8/17 00/15 -0.5/15 -1.5/19 -1.2/24 +2.3/31 L.O.

+11.5/41 +2.7/25 -1.3/23 -1.2/18 00/14 00/15 -1.5/20 -1.5/25 +2.3/30 L.O.

L.O. -1.8/28 -2.0/20 -0.7/14 -0.3/15 -6.0/27 -9.0/40 S.S.

L.O. -12.0/34 00/13 -0.7/14 -15.0/43 -16/50

L.O -16.0/42 -0.7/15 -0.7/15 -17.0/44 L.O

L.O. -14.5/39 -0.3/15 -0.7/15 -18.5/44 L.O

L.O -13.5/39 -0.7/16 -0.7/14 -17.5/43 L.O

L.O -14.5/39 -0.6/15 -0.6/14 -17.5/43 L.O

L.O -14.5/38 -0.5/14 -0.4/14 -15.5/41 L.O

L.O -12.5/37 00/12 -0.1/14 -13.0/33 L.O.

-8.0/39 -7.0/32 -2.0/32 -0.8/17 -0.6/18 -1.8/40 -1.0/50

-4.8/39 -4.0/30 -0.7/18 -0.5/18 -1.0/39 -1.0/50

S.S. -0.5/37 -1.3/27 -1.0/26 -0.7/21 -0.7/18 -0.1/15 -0.5/24 -2.0/33 L.O

S.S. -1.2/40 00/32 -1.5/28 -1.8/23 +0.4/19 -1.3/36 -1.3/31

97	227.7
96	25.9
95	25.2
+30 +17 }	xsections omitted here – See last sheet xsections
94	20.3
93	17.3
92	15.0
91	12.0
90	210.0
+50	208.9
89	07.7
+50	07.1
88	06.2
+50	05.1
87	204.2

00 / 33 | 00 / 33

+0.3 / 33 | −0.3 / 33

−0.5 / 33 | 00 / 33

℄ Rd.

+1.0 / 36 | +0.5 / 25 | +2.0 / 17 | −0.2 / 7 | +0.5 / √11 | −0.5 / 21 | +2.0 / 26 | L.O.

+0.1 / 34 | −0.1 / 25 | −1.0 / 21 | −0.8 / 15 | −0.5 / 12 | −0.5 / 18 | +1.5 / 25 | L.O.

℄ Ditch Drains S

−2.0 / 38 | −5.0 / 34 | −3.0 / 26 | −0.7 / 12 | −0.5 / 12 | −1.2 / 18 | −1.0 / 22 | L.O.

−9.0 / 36 | −7.0 / 24 | −1.0 / 14 | −0.7 / √12 | −1.5 / 19 | −0.8 / 31 | S. S.

−11.0 / 40 | −3.5 / 26 | −1.2 / 12 | −1.0 / 10 | −1.2 / 15 | −0.5 / 18 | +1.0 / 38 | S. S.

℄ R.

−2.8 / 32 | −0.8 / 21 | −0.7 / 18 | +0.5 / 8 | −0.5 / 10 | 00 / 15 | +1.0 / 33 | S. S.

℄ R

00 / 37 | +0.5 / 24 | +0.8 / 15 | −0.3 / 10 | +3.0 / 15 | +3.8 / 33 | S. S.

+2.6 / 34 | +2.5 / 32 | −1.2 / 23 | −0.5 / 21 | −0.7 / 10 | −0.1 / 11 | −0.5 / 18 | +2.5 / 29

+8.0 / 40 | −0.6 / 25 | −1.5 / 20 | −0.3 / 17 | 00 / 14 | −1.8 / 18 | +10.0 / 34

+13.0 / 38 | +3.0 / 26 | −0.2 / 20 | 00 / 15 | 00 / 17 | −1.3 / 21 | +10.0 / 34

+17.0 / 45 | −0.5 / 20 | −0.6 / 15 | −0.1 / 12 | −0.1 / 17 | −1.2 / 21 | −1.2 / 23 | +3.7 / 30 | L.O.

107	23.8
	24.1
+ 70	Alley Ent. R.
106	24.7
	25.7
105 + 04	Int. 5 street.
104	26.5
	26.9
+ 40	Alley Ent. R.
103	27.2
102	28.0
	~~28.0~~
+80	PR. Ent. L
101	28.5
100	29.1 (Short Sta. = 99.0')
99	29.6
+50	29.4
98	29.7

+3.3/35 +0.5/22 +0.7/13 -0.4/9 | -0.3/14 +0.5/15 +1.3/22 +2.5/26 L.O.

+2.5/34 +0.3/22 +0.7/13 -0.4/9 | -0.4/15 00/39 00/100

+3.0/36 +0.4/24 +0.7/13 -0.5/9 | -0.8/13 -0.2/15 -1.7/26 -3.3/30 -3.2/33

+3.0/100 +2.0/50 +0.8/15 | -0.2/9 -2.8/35 -3.1/50 -4.3/100 -5.7/150

L.O. +1.5/26 +0.1/21 -0.2/10 | -0.9/11 -2.0/22 -2.5/33

00/33 | -1.3/16 -2.6/34 -2.9/44

+1.0/33 +0.1/24 00/22 -0.0/15 -0.4/8 | -0.7/12 -0.7/22 -1.7/33

+0.5/28 00/16 -0.5/14 | -0.7/12 -0.4/19 -2.0/27 -2.2/33

+0.7/41 00/15 | -0.7/14 -2.3/28 -2.5/33

L.O. -0.7/16 -0.7/9 | -0.9/15 -1.6/23 -2.5/34

L.O -0.9/26 +0.2/20 -0.8/12 | -1.0/15 -0.3/20 -1.6/26 -2.6/34

+1.0/33 +2.0/22 -0.7/11 | -1.0/12 -0.2/15 +1.0/25 00/35

ER

+1.0/33 +1.8/23 +2.5/19 -0.1/9 | +0.3/6 -0.1/17 +1.1/29 +0.8/35

ERd.

35. 00/33 +0.6/8 | -1.3/7 -0.3/19 -1.5/34

94+30	222.5	
94+17	221.3	
+26.9	223.0	Ant. Cleve. Hve End Line
+10	222.9	
10.8	222.9	

E Rd.

+0.3/34 +0.4/24 −1.4/9 −0.8/23 −1.5/33 −1.6/38

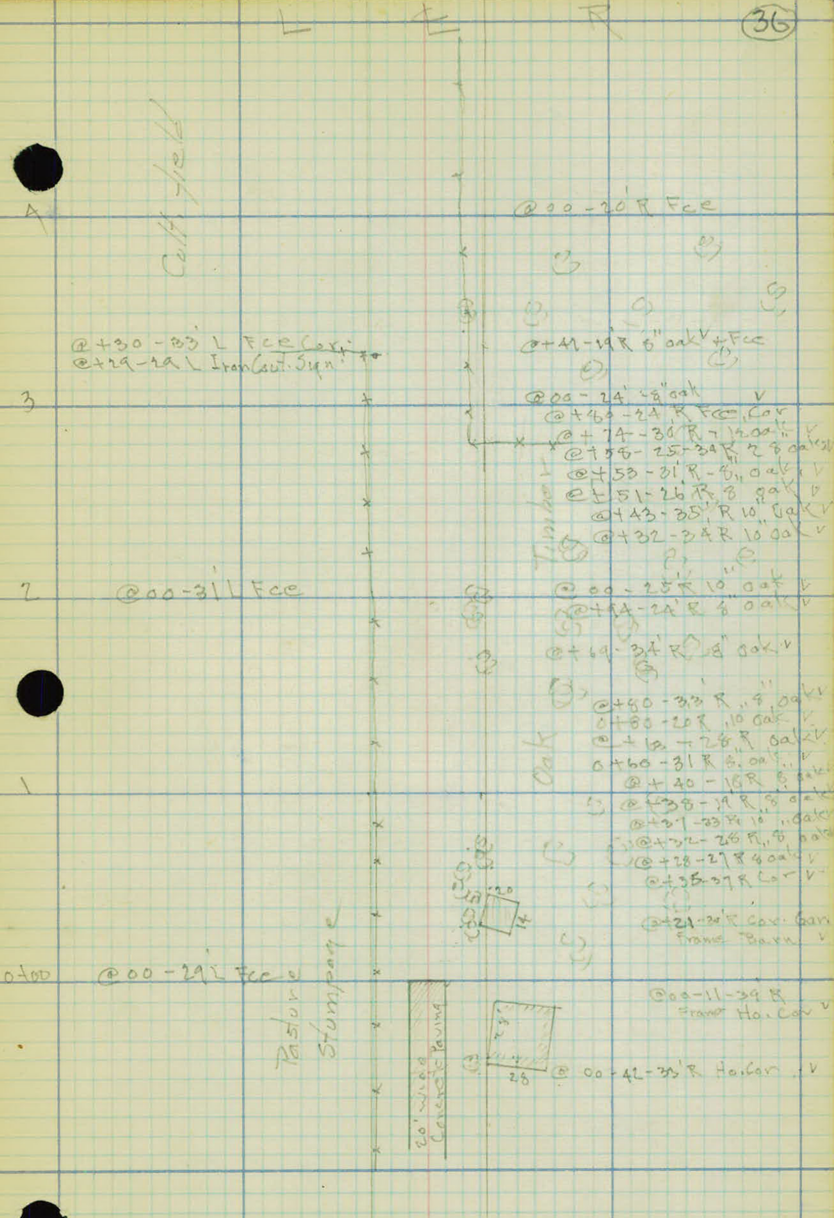
E Rd.

+1.4/34 +1.6/32 +0.9/20 +0.6/5 +1.0/13 −0.1/23 −0.3/28 +2.0/30 +3.6/36 L.O.

−1.8/150 −1.3/100 −0.5/50 −1.0/50 −3.0/100 −5.0/150

−1.5/50. −1.0/30 −0.5/17 −0.6/22 −0.7/35 −0.5/43

+5.5/39 +5.5/34 +3.0/29 +0.5/25 +0.6/18 −0.5/14 −0.5/15 −0.7/20 00/23 +3.0/31 +8.0/38


L
℄
R
Cult. field
@ 00 - 20' R Fce
@ +30 - 33' L Fce Cor.
@ +29 - 29' L Iron Cult. Sign
@ +42 - 19' R 8" oak + Fce
@ 00 - 24' 8" oak
@ +60 - 24' R Fce Cor
@ +74 - 30' R 12" oak
@ +58 - 25 - 34' R 2 8" oak
@ +53 - 31' R - 8" oak
@ +51 - 26' R 8" oak
@ +43 - 35' R 10" oak
@ +32 - 34' R 10" oak
Timber
@ 00 - 31' L Fce
@ 00 - 25' R 10" oak
@ +14 - 24' R 8" oak
@ +69 - 34' R 8" oak
@ +80 - 33' R 8" oak
@ +80 - 20' R 10" oak
@ +18 - 28' R oak
@ +60 - 31' R 8" oak
@ +40 - 16' R 8" oak
@ +38 - 19' R 8" oak
@ +37 - 33' R 10" oak
@ +32 - 26' R 8" oak
@ +28 - 27' R 8" oak
@ +35 - 37' R Cor
Oak
20
14
@ +21 - 38' R Cor. Barn
Frame Barn
0+00
@ 00 - 29' L Fce
Pasture
Stumpage
20' wide Concrete Paving
@ 00 - 11 - 39' R
Frame Ho. Cor
28
@ 00 - 42 - 33' R Ho. Cor

3-17-23

Stump pile

Cult. field

10

@ +98 - 25' R Fce Cor.

@ +46 - 35' R 20" oak ✓

9 @ 00 - 25' R Fce ✓

Oak Timber ✓

@ +41 - 34' R 18" oak ✓

@ 00 - 25' R Fce

8 @ +96 - 25' R - 8" oak ✓

@ +55 - 29' R - 8" oak ✓

@ +42 - 28' R 8" oak ✓

7 @ 00 - 25' R - Fce.

@ +73 - 33' R - 2-16" oak ✓

Cult. field

@ +53 - 24' R 6" oak ✓

@ +50 - 22' R Fce ✓

@ +13 - 26' R 14" oak ✓

6

@ +80 - 25' R 16" oak ✓

@ +61 - 22' R 6" oak ✓

@ +42 - 22' R 8" oak ✓

@ +10 - 25' R 8" oak ✓

5

Cult. field

Oak Timber

4

3-17-23

L ℄ R

(38)

Cult. field

Cult. field

16

15

Cult. field

Cult. field

14

13

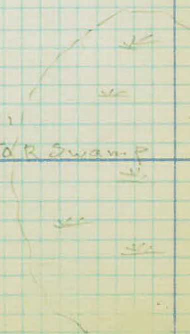
@+61 ℄ Drive L.
Need 20' Culv.

@+72 Drive R
Need 20' Culv.

12

Cult. field

Swamp

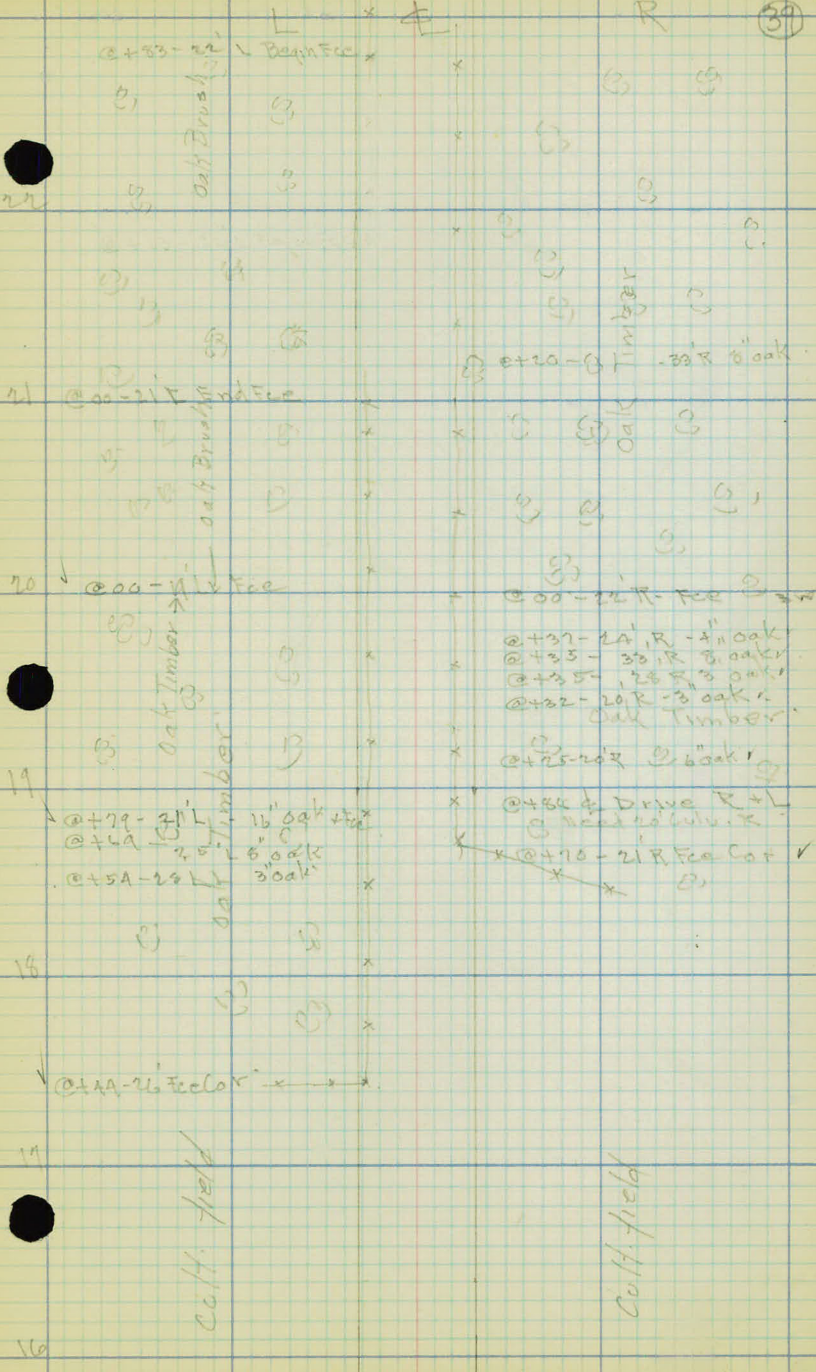


@00-150 R Swamp

11

10

3-17-23



L
℄
R
@+83-22' L Begin Fce
Oak Brush
22
@+20-33'R 8" oak
Oak Timber
21
@00-21'L End Fce
Oak Brush
20
@00-21'L Fce
@00-22'R-Fce
@+37-24',R-4" oak
@+33-33',R 8" oak
@+35-28'R 3" oak
@+32-20'R-3" oak
Oak Timber
Oak Timber
@+25-20'R 6" oak
19
@+79-21'L-16" oak + Fce
@+49-25'L 6" oak
@+54-28'L 3" oak
@+84 ℄ Drive R+L
Oak Timber
@+70-21'R Fce Cor
18
@+44-26' Fce Cor
17
Cult. field
Cult. field
16

3-17-23

New Brighton Rd.

L ℄ R

Cult. field

Cult. field

@ +42 - Steel Tower R

28

@ +83 - 19' L T. Pole
2 w

@ +53 - 40+45 R Trans. L. Poles

@ +43 - 26' L Fce Cor.

@ +69 - Trans. line x Rd.

@ +26 - 35' R Fce Cor

@ +20 - 20' L Iron Post

@ +18 - Trans. line x Rd.

27

@ 00 - 22' L Fce.

@ +99 - 33' L T. Pole

@ +89 ℄ Drive L
Needed Culv.

@ +78 - 27' R 12" oak

@ +75 - 25' R - 16" oak

@ +12 - 26' R + 8" oak

@ +08 - 32' R 8" oak

@ 00 - 26' R 4" oak + Fce

26

@ +87 - 25' R. - 12" oak

@ +69 - 25' R 4" oak

@ +63 - 26' R 4" oak

@ +52 - 25' R. 4" oak

Oak Brush

@ +05 - 34' R 10" oak

25

@ +90 - 30' R 12" oak

@ +80 - 28' R 6" "

@ +46 - 25' R 8" oak + Fce

24

@ 00 - 18' L Fce

@ 00 - 17' R Fce.

Oak Brush

Oak Timber

23

22

N. Br. Rd. 3-17-23

L ⊥ R (41)

@ +26 - 16' L T. Pole 2 W 0

34

33

@ +97 - 15' L L T. Pole 0

32

@ +67 - 15' L T. Pole 2 W 0

Cult field

Cult field

31

@ +38 - 14' L T. Pole 0

30

@ +13 - 13' L T. Pole 2 W 0

29

Cult field

Cult field

28

3-17-23

N. Br. Rd

40

@+41-16' L Tel. Pole
2W

39

@+13-17' L Tel. Pole.

Cult. field

Cult. field

38

37

@+84-17' L T. Pole
2W.

36

@+54-17' L T. Pole

Cult. field

Cult. field

35

34

3-17-23

π Line L ℄ R

@+90-32' R T.Pole
2W

@+39-22' L T.Pole

~~@+25-26'~~

@+25-26' R T.Pole

A6

@+11-11'L T.Pole

~~@+79-19'L T.Pole~~

@+50-21' R T.Pole
2W

2W

A5

@+93-25' R T.Pole

@+57-18'L T.Pole

A4

@+66-42' L ~~Fce Cor~~

@+33-17' L T.Pole
2W

@+37-25' R T.Pole
5W

A3

@+76-34' L 10" Oak

@+72-33' R 10" Tree
@+53-33' R 8" Tree
36x16
@+49-8' R Co. Rd. Pipe Culv
@+43-1' R Drive R
@+34-15' R Mail Bx
@+34-33' R 8" Tree

@+10-14' L Tel.Pole

A2

@+81-29' R begin Tel. Poles

@+10-32' 14' Oak

A1

@+68 ℄ Rd R
Need 20' Culv

@+38-36' L Fce Cor

A0

3-22-23

@ +50 -14' L T. Pole

@ +21 -49' R 8" Tree
Co. Ditch

52

Marsh @ edge fill

51 @ +05 -14' L T. Pole

50

Willow Brush

@ +59 -14' L T. Pole

49

Meadow

@ +39 -15' L T. Pole
2w

48

@ +44 -35' T. Pole
@ +44 -14' L Fnc. Cor.
@ +31 ℄ Rd.

@ +05 -14' L T. Pole

47

Cult. Field

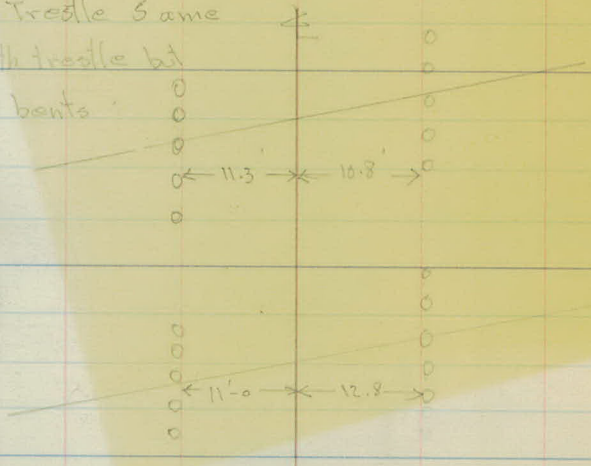
46

3-22-23

N. Brighton Rd

Clearance from present grade
15.67 ft to underside of Girder

North Trestle Same
as South trestle but
has 10 bents



5 Pile to each Bent
9 Bents in So. Bridge
10 - 6"x16" Timber Girders
8x8 sawed Ties
2 - 16x12 Timber Girders
(2 - (2-16" Steel I beams) in Span over Road

@+15 - 17½ L 8" Tree
Marsh @ edge fill

58

@ 00 - 21 R - begin Timber

@+66 - 13 L T. Pole

57

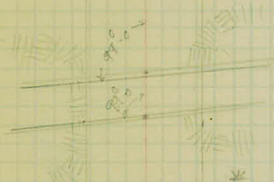
~~@+66 - 13 L~~ Brush

@+37 - 17 R Cor. R.o.W. Fce

Marsh @ edge fill

@+15 - 13 L T. Pole

56



@+58 ℄ Trestle

@+36 ℄ Trestle

55

@+30 - 13 L T. Pole

@+70 - 30 L Cor. R.o.W. Fce

@+44 - 36 R Cor. R.o.W. Fce

Oak Timber

54

@ 00 - 30 L 10" Tree

@+92 - 32 L 6" Tree

@+67 - 14 L T. Pole

Meadow

53

52

New Brighton Rd 3-17-23

0+00 End of Paving

0+00

L ℄ R (46)

Oak Brush

@+69 - 25' R 4" Tree
@+60 - 28' R Fe$ (struck through)

Timber

64

@+90 - 22' R 12" Tree

@+90 - 36' L 14" Oak & Fe color

@+62 - 15' L T. Pole

@+27 - 20' R Cor. Fe
Hedge & Curb (struck through)

@+36 - 26' L - 18" Tree

@+14 ℄ Drive

@+07 - 20' R 16" tree

Oak Timber

@+07 - 20' R Cor. Fe

@00 - 20' R Fe

63

@+71 - 17' L Mail Bx
@+69 - 32' L - 14 Oak

Timber

@+61 ℄ Drive
Hedge & Curb (struck through)

@+13 - 16' L T. Pole
2 w

62 @00 - 20' R - 8" Tree

@+41 - 28' R begin Brush

Cult. Field

61 @00 - 26' R Fe

@+64 - 14' L - T. Pole

60

@+80 - 23' R edge & end Timber

Oak Timber

Field

@+14 - 14' L T. Pole

59 @00 - 25' R Fe

Cult.

58

3-22-23

L ℄ R (47)

Oak Brush & Timber

@+10 - 25' R 8" Willow
@00 - 25 R Fce

70

@+58 - 13' L T. Pole

@+35 - 31' L 12" Oak Fce Cor

69 @+09 - 31' L begin Fce.

@+73 - 29' L 4" Oak

@+12 - 14' L T. Pole

68 @00 - 37' R Fce

Cult. Field

67

@+63 - 15' L T. Pole

Brush

66

Cult. Field

@+13 - 14' L T. Pole

65 @00 - 37' R Fce.

Oak Brush

64

3-22-23

New Brighton Rd

L ℄ R

76

Timber

@ +53 — 14' L T. Pole

75

Oak

Cult. field

74 @ +04 — 13' L T. Pole
2 w

73 @ 00 — 22' R end fce.

@ +57 — 13' L T. Pole
@ +50 — 25' L end
Timber

Cult. field

72

~~@ +57 — 13' L T. Pole~~

@ + 10 — 13' L — T. Pole
2 w.

71

Oak Timber

@ +65 — 22' R Fce. Cor.
@ + 51 — 16 R 2-8 Tree

Cult. field

@ +24 — 20' L begin Timber

70

3-22-23

New Brighton Rd

Topog. Measured off Curve

@+24 – 30' R 3-16" Trees

82

@+80 – 300' R ℄ Ho

@+55 – 18' R Mail Bx

@+25 ℄ Drive

Oak Timber

81

@+51 – 33' L – 10" oak

@+26 – 32' L 8" Tree

@+20 – 32 L – 8" oak

@+15 – 31 L 6" oak

80 @00 – 31 L – 6" Oak

@00 – 150' R T. Pole

@+90 – 36' L 12" Tree

@+84 – 33 L 6" Tree

@+76 – 110 R Fce Cor

Located from Curve

Corn Field

@+30 – 18' R T. Pole 2w

@00 – 38' R Fce

79

@+90 – 30 R – 6 – 8" willows

@+60 – 77' R begin Fce

@+56 – 26 R 6-8 willows

@+20 – 13' L T. Pole

78

Oak Timber

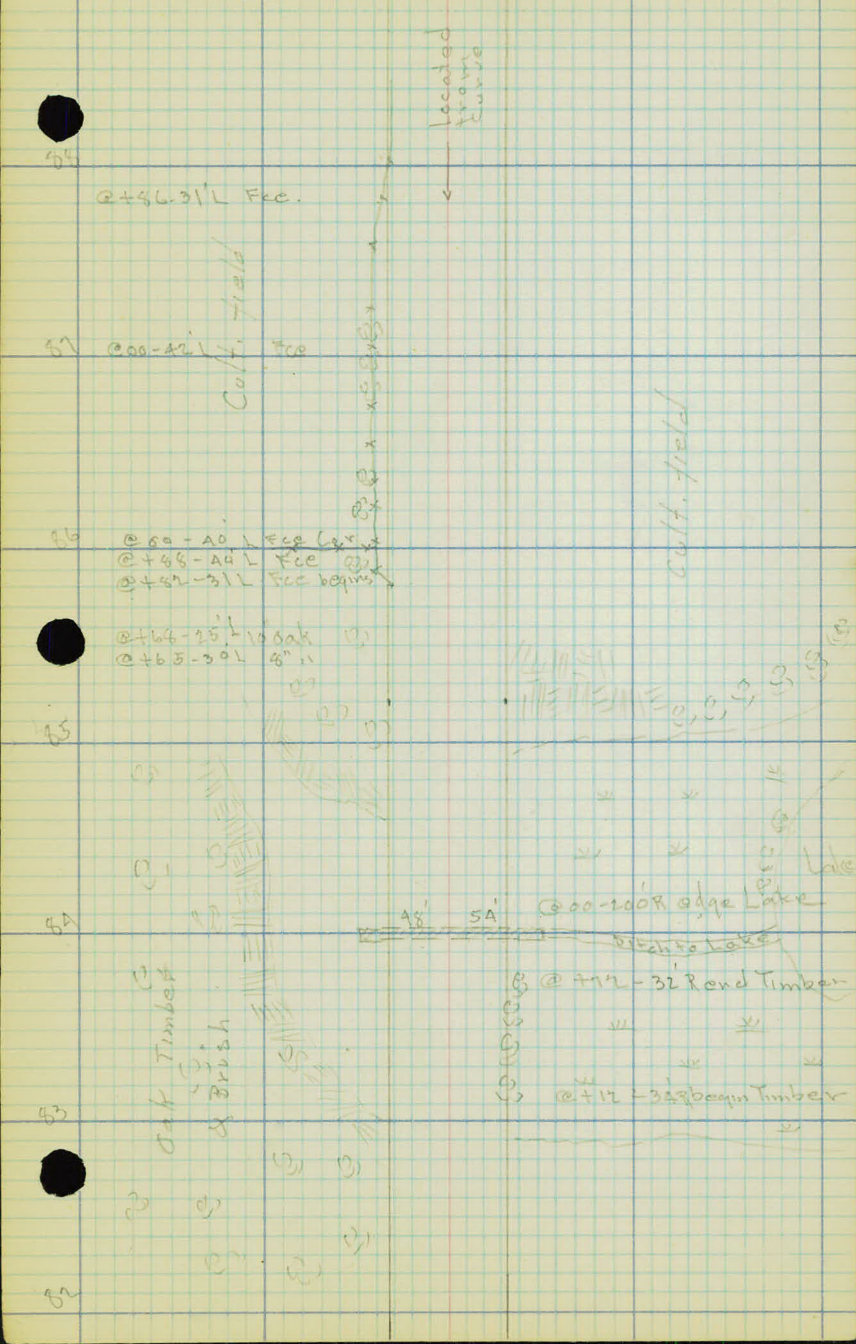
77 @00 – 15' L T. Pole 2w

Corn Field

76

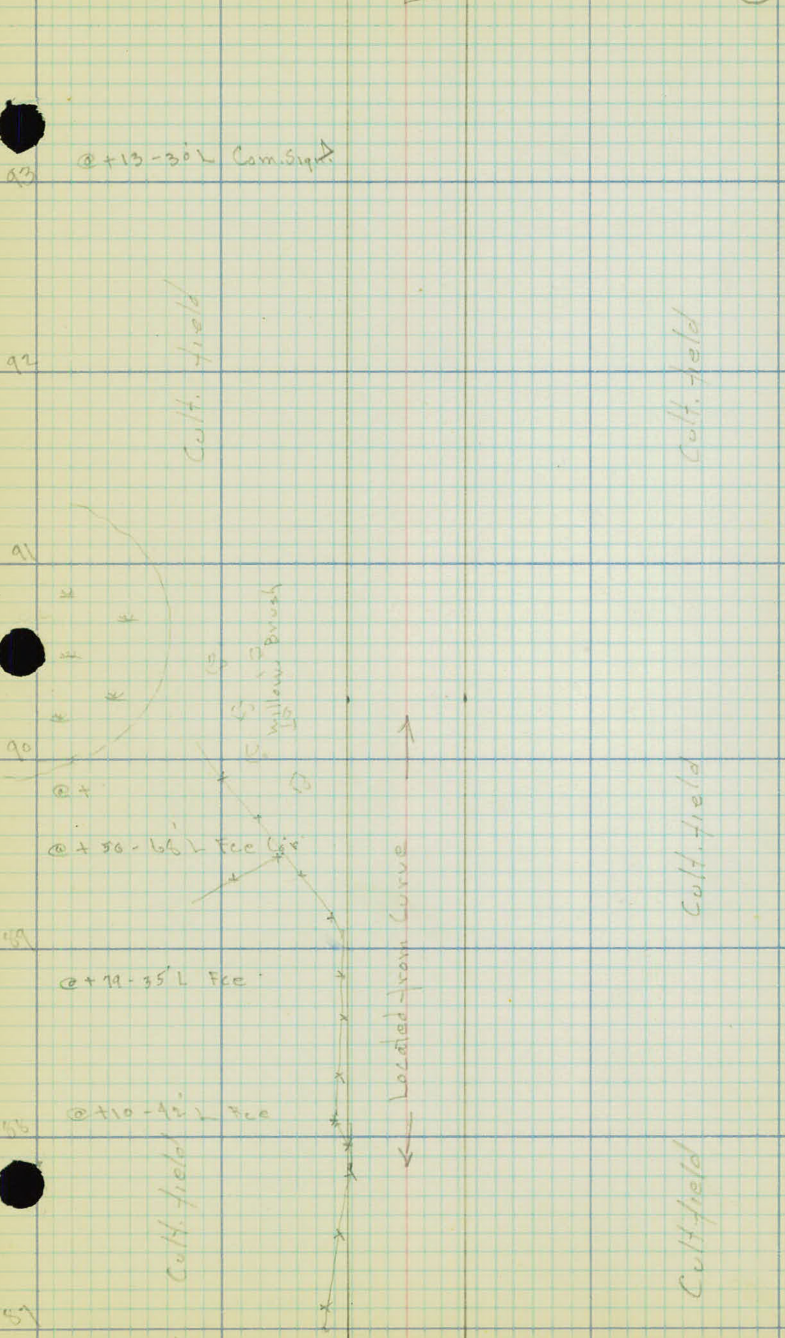
N. Br. Rd 3-22-23

14" - Corr. Iron Culvert



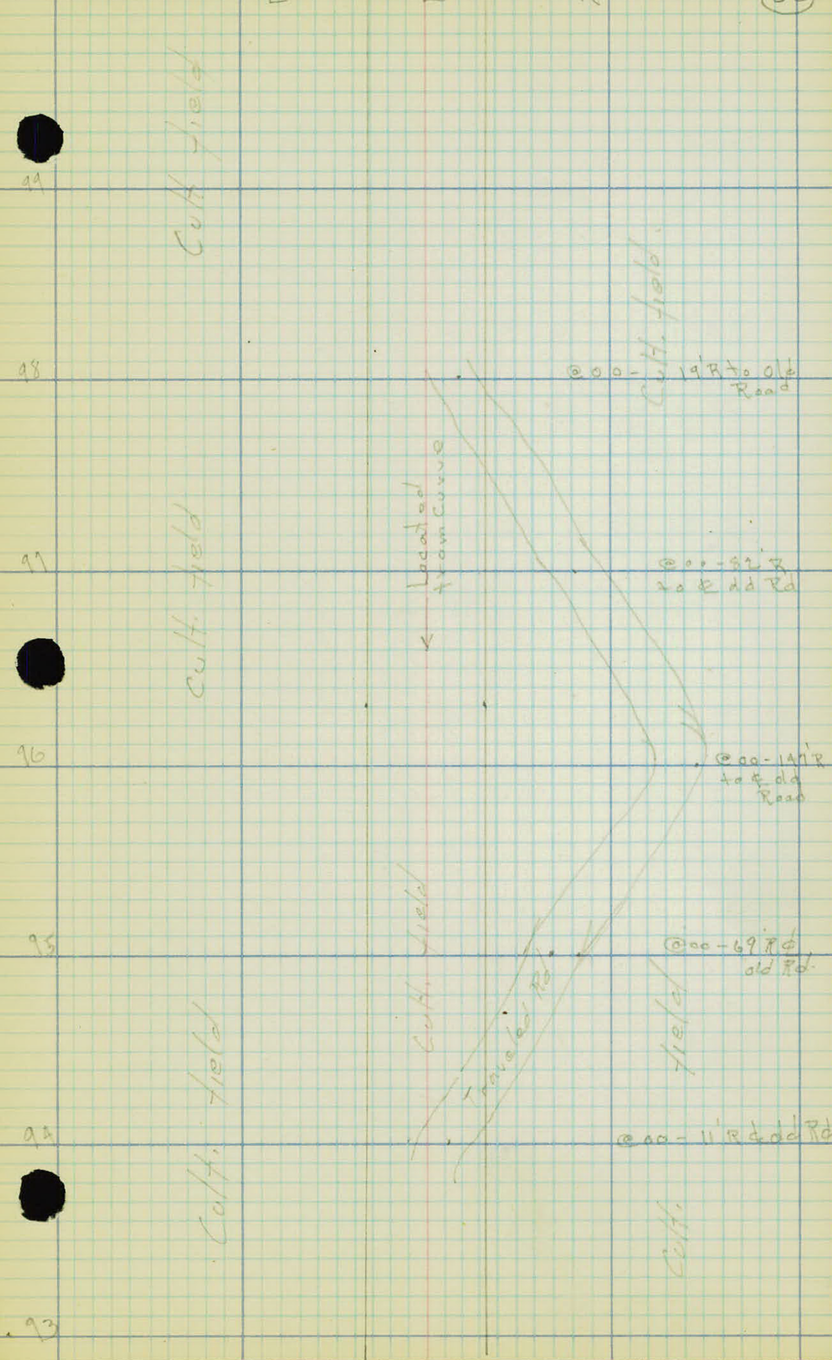
L
℄
R
Located from Carrie
88
@+86-31' L Fce.
87
@00-42' L Fce
Cult. Field
Cult. Field
86
@00-40 L Fce Cor
@+88-44 L Fce
@+82-31 L Fce begins
@+64-25' L 10" oak
@+65-30 L 8" "
85
84
48'
54'
@00-200 R edge Lake
Ditch to Lake
Lake
@+72-32' Rend Timber
@+12-348 begin Timber
Oak Timber & Brush
83
82

N. B. Rd 3-22-23


L
℄
R
@ +13 - 30' L Com. Sign
93
92
Cult. field
Cult. field
91
Willow Brush
90
@ +
@ + 50 - 65' L Fce Cor.
Cult. field
Located from Curve
89
@ + 79 - 35' L Fce
@ +10 - 42' L Fce
88
Cult. field
Cult. field
87

3-21-23

New Brighton Rd.


L
℄
R
99
98
97
96
95
94
93
Cult. field
Cult. field
Cult. field
Cult. field
Cult. field
Cult. field
Located from Curve
Traveled Rd
@ 00 - 19' R to old Road
@ 00 - 82' R to ℄ old Rd
@ 00 - 147' R to ℄ old Road
@ 00 - 69' R ℄ old Rd.
@ 00 - 11' R ℄ old Rd

3-22-23

New Brighton Rd.

L ℄ R (53)

@+32 - 29' L - 18" oak
@+22 - 16' L - T. Pole
@+24 - 18' L - 4' Tile walk
@+32 - 27' R Fce Cor
@+06 - ℄ street
105
@+81 - 16' R - T. Pole

@+54 - 31' L 8" oak
@+49 - 28' L - 12" oak
@+12 - 26' L - 10 oak
104

@+72 - 21' L - 30" oak
@+50 - 22' L 12" oak.
@+43 - 25' L T. Pole
@+36 - ℄ 20' Alley R
@+32 - 46' R Pow. Pole
@+22 - 21' L - 12" oak
103
@+92 - 33' L 10" oak
@+79 - 29' L - 16" oak

36'
@+41 - ℄ Ho 65
@+35 - 44' L 10" oak
@+15 - 32' L 12" oak
102
@+88 - ℄ 10' drive
@+79 - 19' L Fce Cor

101

Cult. field

Cult. field
100

99

3-24-23.

New Brighton Road.

L ℄ R

40
Frame
Church

109 @ +66 - 17' L Fce Cor
@ +63 - 17 L - T. Pole
@ +61 - 26 L Fce Cor
@ +50 - 31' L - School
@ +50 end walk 4

@ +80 - N.E. Cor. Church 47' R
@ +69 - 15 R Guy Pole
Iron Rd Sign
@ +53 - 46' R

106 + 26.9 ℄ Cleveland

@ +10 - 45' R water Hyd.
@ 00 - 24 R Pole
@ 00 - 40' R T. Pole

108 107+99 - 15' L Iron Rd Sign
@ +92 - 15 L Pow Pole
@ +80 - 33' L 4" Tree
@ +60 - 33' L 4" Tree
@ +44 + 52 - 32 L 6" oak
@ +47 ℄ Ho - 53 L
32'
Ho
Tile w.

Oak Trees

@ +33 - 27' R 10" oak

@ +37 - 32' L 4" Tree
@ +21 - 32' L 4" Tree
@ +05 - 32 L 4" Tree
107 @ 00 - 18' L - edge Tile walk
@ +91 - 14' L Pow. Pole
@ +86 - 32 L 4" Tree

@ +80 - 40' R. T. Pole
@ +70 - ℄ 20' Alley R.
@ +63 - 32' R Pow. Pole
@ +61 - 25 R Fce Cor.

@ +22 - 31' L - 30" oak

@ +08 - 20' R - 14" oak

106

@ +95 - Cor. Ho.
@ +54 - 35 L, 10 Tree
@ +54 - 46 L Cor. Ho
@ +49 - 38 L - 12 Tree
20'
40'
Tile walk

@ +50 - 27' R Fce.
@ +45 - 21 R 10" oak
Tile walk

105

104

3-22-23

New Brighton Rd

12+75 Need 38'-18" Culv. under Rd

22+70 Need 55'--18" Culv. " "

52+20 Need 45'-18" Culv. " "

57+00 Need 42'-18" Culv. " "

81+25 12"-40' Cor. Iron Culvert under drive to Right Replace with 18" Culv.

84+00 20"-10'lg. Culv. in place Condit Good

91+00 Need 44'- 18" Culv. under Road

To drain side ditch on left

To drain side ditch on right

To drain marsh on left into ditch on right

@ equalizer

elev. invert Low side. Right. ~20' lower than
℄ @ sta. 84+00 flows right.

Check heads

New Brighton Road.

3/27/23

3/27/23

Check Levels N. B. Rd.

B.M.	8.79	236.24	8.39		227.45
	5.47	238.32	3.39		232.85
B.M				6.37	231.95
	2.67	237.80	3.19		235.13
B.M.				6.47	231.33
	4.17	234.95	7.02		230.78
B.M				5.93	229.02
B.M	4.36	236.09	3.22		231.73
B.M	2.18	234.34	3.93		232.16
	1.34	223.82	11.86		222.48
B.M	0.00	213.03	10.79		213.03
	1.57	202.75	11.85		201.18
B.M				5.55	197.20
B.M				6.03	196.72
	11.46	214.06	0.15		202.60
	11.59	225.47	0.18		213.88
B.M				5.04	220.43
	4.56	229.72	8.31		225.16
	0.03	222.56	7.25		222.47
	1.27	213.42	10.29		212.21
B.M				5.87	207.55
	0.73	203.85	10.30		203.12
	10.01	213.09	0.77		203.08
B.M				8.48	204.61
	11.05	223.78	0.36		212.73
	10.81	233.93	0.66		223.12
	3.64	231.65	5.92		228.01

3/27/23

{Tierney
Persons

Nail in T.P. 50' S. End pave

Nail in 12" Oak SW. Cor Cty R/D + N.B.R.R.

Nail in 15" Oak 25' R 9+90

Nail in 15" Oak L 18+75

Sp. in T.P. L 27+85

Sp in T.P L 39+50

Sp. in T.P. L 47+00

Spin Spiling first bent on E side R.R. Br.

Sp in T.P. L 56+15

Sp. in 14" Oak R 63+10

Sp in 12" Oak L 80+00

Sp in 1

Sp. in 10" Oak L 85+75

		231.65		2
	2.66	228.61	5.70	225.95
B.M			4.42	224.19

Note:- Differs by 1.04' from levels as carried on ℄. (223.15)

Check levels from B.M. Sp. in T.P Cleve. & N.B.Rd to B.M Sp. in 10" Oak ℄ 85+75.

B.M.	4.42	228.61		224.19
	5.94	231.89	2.66	225.95
	6.62	234.63	3.88	228.01
	1.25	224.37	11.51	223.12
	2.22	215.25	11.34	213.03
	4.76	212.90	7.11	228.14
			8.32	284.58

Note. ∴ 1.0' Error in ℄ levels between these benches.

Sp in T.P. S.E Cor. Int N.B.Rd + Cleve. Ave.
Sf

Sp in T.P. Cleve. Ave + N.B. Rd - End of Line.

Sp in 10" Oak L 85+75

New Brighton Road R.J.W.
5-17-23

✓ Field Inspection

✓ 0+25 P. 24" P3

Sent out all drain tile

✓ 10+00 — 12+00
Gr. 3 stamps

✓ 12+61 End R & L
P. 12" x 25' L
No culv. req'd on R.

✓ 18+88 End R & L
No culv. req'd L.
P. 12" x 25' R.

✓ Start G.R. L 20+70
End " L 23+30

✓ Start G.R. R 21+50
End " R 23+30
22+00 P. 24" P3

✓ 26+89 End L
P. 12" x 25'

40+68 E. 1 [illegible]
P. 12" [illegible]

42+43 E. L
P. 12" x 24 C. M.
Haul from 47+31

47+31 Road Int. L
12" x 24 C. M. in place remove
P. 18" x 30 replace
[illegible] C.M. remove at 42+43

52+20 P. 24" P. 3
Inv. Elev. 3.5' below
℄ elevation

55+00 P 24" P. 3
Inv Elev 3' below ℄ elev
56+10 P 24" P. 3

62+60 E. L.
No culv. req.

63+25 E. R.
No culv. req.

81 + 25 Cond OK

12" x 38' C.M. Cond. OK.

84+00 Inp - 24" x 100' C.M Cond OK.

P.I.R. L. 80+50 — 85+75

P.I.R. R. 81+50 — 85+75

107+97

Final Xsections
23-63

Carley - Level
Briggs - Tape
Eck - Rod.

10/27/23
Carley - cold Sta 0 to Sta 39

G.R. - L - 48+44 — 291'

Sta	+	H.I.	−	E/ev	
B.M.	6.01	237.97 ✓			231.96
0			5.0	33.0	32.4
+25					
+50			4.8	33.2	32.55
1			4.6	33.4	32.7
+50			4.4	33.6	32.85
2			4.3	33.7	33.0
+50			4.2	33.8	33.15
3			4.0	34.0	33.3
+50			3.9	34.1	33.45
4			3.7	34.3	33.6
T.P.	5.30	239.50 ✓	3.7 ✓	234.20 ✓	
+50			5.1	34.4	33.75
5			4.9	34.6	33.9

Final Xsections Party (Carley, Briggs, Eck) 10-29-23 Cloudy cold. 12

23-63

Lt ℄ Rt

Nail in 12" oak S.W. Cor. of Xroads

4.3/26 7.6/22 6.7/19 5.2/15 5.2/10 (5.6) 5.1/10 4.5/33 Driveway

18"C.M. pipe Xdrain Invert 230.1 Outlet 229.8

3.7/26 6.8/23 6.4/20 5.1/15 4.7/10 (5.4) 4.7/10 4.8/15 6.3/21 6.7/25 4.9/28 4.7/31

3.3/26 5.8/24 6.4/23 5.8/20 4.7/15 4.7/10 (5.3) 4.7/10 4.8/15 6.8/22 7.2/24 3.9/30

3.2/27 6.3/24 6.0/21 4.4/15 4.5/10 (5.1) 4.5/10 4.6/16 6.7/24 6.1/27 4.4/25

3.3/28 6.3/24 6.1/21 4.2/15 4.4/10 (5.0) 4.4/10 4.7/17 6.4/21 6.5/25 4.0/29

4.7/27 7.0/24 6.6/21 4.1/15 4.3/10 (4.8) 4.3/10 4.5/15 6.5/20 7.0/23 5.1/27

5.5/27 7.1/24 6.6/21 4.0/15 4.1/10 (4.7) 4.1/10 4.4/15 6.6/20 6.8/22 5.5/24

6.3/28 6.9/25 6.4/21 4.1/15 4.0/10 (4.4) 4.0/16 4.0/15 5.7/19 6.1/28

5.2/29 7.1/26 6.9/22 3.6/15 3.8/10 (4.4) 3.8/10 4.0/15 5.7/19 6.1/24

7.5/28 6.6/31 8.3/28 8.0/22 5.1/15 5.2/10 (5.8) 5.1/10 5.1/15 7.3/21 7.3/22 6.9/24

6.0/31 8.3/27 7.7/22 5.0/15 5.0/10 (5.6) 4.9/10 4.9/15 7.3/22 7.4/25

Sta	+	H.I	−	Elev	
	5.30	239.50			
5+50			4.7	34.8	34.05
6			4.5	35.0	34.20
+50			4.4	35.1	34.35
7			4.3	35.2	34.50
8			4.3	35.2	34.5
+50			4.5	35.0	34.3
9			4.8	34.7	34.0
+50			5.2	34.3	33.6
B.M.	4.65	236.00	8.16		231.35
10			5.6	33.9	33.2
+50			4.4	33.6	32.8
11			2.8	33.2	32.4
+50			3.2	36.8	32.0
12			3.7	32.3	31.6

Lt ℄ Rt

5.3	7.9	7.3	4.7	4.8	(5.4) 4.8	5.1	6.7	6.7	5.0
31	26	22	15	10	10	15	20	23	26
4.0	6.8	6.4	4.4	4.6	(5.3) 4.6	4.9	7.1	7.4	5.1
30	27	21	15	10	10	15	20	23	26
3.4	6.6	6.4	4.6	4.6	(5.2) 4.5	4.6	6.9	7.10	4.6
30	26	20	15	10	10	15	20	23	26
4.3	6.3	6.8	4.2	4.4	(5.0) 4.4	4.5	7.1	5.1	
30	28	25	15	10	10	16	23	27	
4.7	7.2	4.4	4.4	(5.0) 4.4	4.4	6.4	6.4	4.9	
31	26	15	16	10	16	22	25	27	
4.9	6.6	4.4	4.6	(5.2) 4.6	4.6	7.1	5.5		
29	25	15	10	10	16	25	27		
5.0	7.4	4.9	4.9	(5.4) 4.9	5.1	7.3	7.4		
30	25	16	10	10	17	23	27		
6.1	7.9	7.5	5.4	5.3	(5.9) 5.3	5.5	8.5	8.3	
30	25	21	15	10	10	16	23	26	

Nail in 14" oak 25' Lt sta 9+90

5.8	8.4	7.9	5.8	5.7	(6.3) 5.7	5.9	9.0	9.1	8.2
29	25	20	15	10	10	16	23	25	26
2.1	4.9	4.6	2.8	2.3	(3.2) 2.5	2.6	5.3	5.4	3.4
30	25	19	15	10	10	15	22	25	27
1.6	5.2	4.7	2.8	2.9	(3.6) 2.9	3.2	5.9	5.5	4.1
30	25	20	15	10	10	16	22	25	27
1.5	5.1	4.7	3.1	3.3	(4.0) 3.4	3.5	6.0	6.4	4.6
30	25	20	15	10	10	16	21	24	26
2.1	5.7	5.0	3.6	3.8	(4.4) 3.8	4.1	6.4	7.2	5.9
32	25	19	15	10	10	15	19	24	26

Sta	+	H.I.	−	Elev	
	4.65	236.00			
12 +50			4.1	31.9	31.2
13			4.3	31.7	31.0
+50			4.5	31.5	30.8
+60			4.6	31.4	30.8
+71			4.6	31.4	30.7
14			4.6	31.4	30.7
+50			4.6	31.4	30.7
15			4.7	31.3	30.6
+50			4.7	31.3	30.6
16			4.8	31.2	30.5
+50			5.0	31.0	30.4
17			5.0	31.0	30.3
+50			5.1	30.9	30.2

Lt ℄ Rt (4

3.2/31 6.5/25 6.0/19 4.1/15 4.2/10 (4.8) 4.2/10 4.3/15 8.2/23 8.4/25 7.2/25

5.0/31 7.0/25 6.4/19 4.5/16 4.5/10 (5.0) 4.4/10 4.7/14 8.8/23 9.2/26

5.9/30 6.7/25 6.7/21 4.8/16 4.7/10 (5.2) 4.6/10 4.7/15 7.6/21 8.0/25

5.8/32 4.9/17 4.7/10 (5.2) 4.6/10 4.9/15 7.9/31

5.5/32 6.1/30 4.8/16 4.7/10 (5.3) 4.7/10 4.8/14 7.4/32

5.3/33 7.6/27 7.2/22 4.9/15 4.7/10 (5.3) 4.7/10 4.8/14 8.1/21 8.2/25 6.9/29

5.0/30 7.0/25 7.0/22 4.6/15 4.7/10 (5.3) 4.7/10 4.6/14 7.9/23 7.7/26 5.8/30

4.2/33 7.6/26 7.6/22 4.9/15 4.8/10 (5.4) 4.8/10 4.6/16 7.7/24 7.6/27 5.5/31

4.7/33 7.4/27 7.2/23 4.9/15 4.9/10 (5.4) 4.8/10 5.0/16 8.2/25 8.2/28 6.6/30

6.8/32 7.6/29 7.7/23 5.0/15 4.9/10 (5.5) 4.9/10 5.1/15 8.4/25 8.4/27 6.9/29

8.8/30 8.4/23 5.2/15 5.1/10 (5.6) 5.1/10 5.4/15 7.9/24 8.4/28 6.4/30

7.0/32 8.1/27 7.8/22 5.3/15 5.1/10 (5.7) 5.1/10 5.2/14 8.6/25 8.7/28 5.3/32

6.5/32 8.3/29 8.3/23 5.1/16 5.2/10 (5.8) 5.2/10 5.3/16 8.5/25 8.4/29 5.0/33

Sta	+	H.I.	−	Elev	
	4.65	236.00			
18			5.2	30.8	30.1
+50			5.3	30.7	29.9
B.M.					
19			5.4	30.6	29.8
T.P.	4.04	234.50 ✓	5.54	230.96 ✓	
+50			4.1	30.4	29.7
20			4.2	30.3	29.5
+50			4.4	30.1	29.4
+88			4.5	30.0	29.3
21			4.5	30.0	29.2
+50			4.6	29.9	29.1
22			4.6	29.9	29.1
+00					
+50			4.4	30.1	29.3
23			4.2	30.3	29.5
+50			3.9	30.6	29.8
24			3.6	30.9	30.1
T.P.	4.68	236.08 ✓	3.10	231.40 ✓	

Lt ℄ Rt

5.9
8.2/28 8.0/22 5.4/15 5.2/10 5.2/10 5.4/15 9.1/26 9.2/29 5.7/33

6.1
8.5/26 8.2/21 5.6/15 5.4/10 5.4/10 5.3/15 9.3/26 9.1/29 6.8/32

spike in 20" conc Lt s℄ 15+75 (Removed)

6.2
8.7/30 9.2/28 8.6/21 5.6/15 5.5/10 5.5/10 5.5/16 8.2/25 8.0/28

4.8
5.2/32 7.9/30 7.7/27 4.3/15 4.2/10 4.2/10 4.3/17 7.2/23 7.4/27 6.4/29

5.0
4.3/32 8.4/29 8.5/24 4.3/15 4.3/10 4.3/10 4.1/17 7.1/24 7.5/27 2.6/34

5.1
4.4/34 9.0/32 8.7/24 4.4/15 4.5/10 4.5/10 4.5/17 7.4/25 7.1/29 (233.1/41)
10.4/37 10.8/35 8.8/26 4.8/16 4.6/10 4.6/10 4.8/17 7.7/24 7.8/27 8.4/39
5.2
5.3
11.9/31 4.8/16 4.6/10 4.6/10 4.7/16 7.6/24 7.6/27 1.4/37

5.4
(213.0/47) (214.9/40) 4.7/17 4.7/10 4.7/10 4.8/16 8.6/27 7.3/31

5.4
(211.0/49) (212.3/43) 4.8/15 4.7/10 4.7/10 4.7/15 9.9/29 10.3/34 9.5/38

outlet Lt Inv. Rt
24" conc. culvert Invert 212.8 Outlet 223.8

5.5
(217.1/34) 4.8/15 4.5/10 4.5/10 4.7/15 9.7/28 9.6/34

5.0
8.7/28 9.1/27 8.5/21 4.7/15 4.3/10 4.3/10 4.2/15 8.0/23 5.8/29 7.9/32

4.7
3.1/28 7.2/26 7.1/21 4.0/15 4.0/10 4.0/10 4.1/15 7.3/23 7.9/28 7.1/30

4.4
1.5/29 6.8/24 6.4/20 3.9/15 3.7/10 3.7/10 3.8/16 6.7/22 7.3/28 5.6/31 5.3/35

Sta	+	H.I. 236.08	−	Elev	
24+20			5.1	31.0	30.2
24+50			5.0	31.1	30.3
25			4.7	31.4	30.6
+50			4.6	31.5	30.7
26			4.6	31.5	30.8
+50			4.6	31.5	
27			4.7	31.4	30.9
B.M.	6.13	236.53	5.62	230.46	230.40
27+50			5.0	31.5	30.95
28			5.0	31.5	31.0
+50			4.9	31.6	31.05
29			4.7	31.8	31.1
+50			4.7	31.8	31.15
30			4.6	31.9	31.2
+50			4.6	31.9	31.25

Note: Equation 26+63.0 = 26+65.14 30.8
26+00 to 27+00 = short sta 97.86'

Lt ℄ Rt

3.1/29 8.1/24 7.8/19 5.5/15 5.2/10 (5.9) 5.2/10 5.5/15 8.6/24 8.9/27 6.7/31 2.9/36

3.7/29 7.9/24 7.4/19 5.1/15 5.1/10 (5.8) 5.1/10 5.4/14 8.2/23 8.2/27 1.5/35

2.8/28 7.7/24 7.3/20 5.1/15 4.9/10 (5.5) 4.8/10 4.6/16 7.2/21 7.3/24 1.2/29

2.8/28 7.5/24 7.0/22 4.7/16 4.7/10 (5.4) 4.8/10 4.7/15 7.2/20 7.5/23 1.7/28

3.2/29 7.7/26 7.2/21 4.4/15 4.4/10 (5.3) 4.7/9 4.5/9.7 4.8/14 7.3/20 7.7/24 3.3/28

4.5/30 7.9/27 7.4/24 4.0/14 4.8/10 (5.3) 5.0/9.4 4.7/10.4 4.7/16 7.6/23 7.8/26 4.6/29

5.5/32 7.7/30 7.6/27 3.7/18 4.0/10 (5.2) 5.2/11.4 5.0/12.4 4.9/19 7.3/25 7.7/28 7.1/30

spike in elec. pole Rt of sta 27+55

6.7/36 8.2/34 8.0/30 4.5/21 4.4/10 (5.5) 5.7/12 5.5/13 5.7/23 8.2/29 8.5/32 7.5/34

6.5/29 8.0/27 4.1/16 4.4/10 (5.5) 5.6/12 5.4/13 5.4/20 7.9/26 8.5/30 7.0/32

6.4/27 7.6/26 7.1/22 4.3/16 4.5/10 (5.4) 5.3/10 5.1/11 5.1/17 7.9/26 5.4/29

5.4/27 7.0/25 6.7/22 4.4/16 4.6/10 (5.4) 5.0/9 4.8/10 5.7/17 7.0/23 7.8/27 5.3/29

5.7/27 6.9/23 4.6/17 4.7/10 (5.3) 4.9/10 4.9/17 7.0/22 7.5/27 5.4/29

5.8/28 7.5/26 7.0/23 4.6/17 4.8/10 (5.3) 4.7/10 4.5/17 7.3/23 7.8/27 5.1/29

5.1/28 7.6/26 7.4/23 4.8/16 4.7/10 (5.2) 4.7/10 4.8/15 7.3/23 8.1/26 5.5/29

Sta	+	H.I.	−	Elev.	
	6.13	236.53			
31			4.5	32.0	31.3
+50			4.5	32.0	31.3
32			4.5	32.0	31.4
+50			4.5	32.0	31.4
33			4.5	32.0	31.4
+50			4.5	32.0	31.4
34			4.5	32.0	31.4
TP	4.90	236.93	4.50	232.03	
+50			4.8	32.1	31.4
35			4.9	32.0	31.4
+50			4.9	32.0	31.4
36			4.8	32.1	31.4
+50			4.8	32.1	31.4
37			4.8	32.1	31.4

L+ E R+ 17

5.4	7.4	7.1	4.7	4.6	(5.2)	5.0	7.5	8.1	5.6
29	26	23	15	10	4.6	15	23	26	28
					10				
6.0	8.1	7.7	4.7	4.6	(5.2)	4.9	7.5	8.3	6.5
29	26	23	15	10	4.6	15	22	26	28
					10				
6.1	8.2	7.9	4.5	4.6	(5.1)	4.7	7.5	8.4	6.4
30	26	23	16	10	4.6	16	23	27	29
					10				
6.2	8.7	8.0	4.7	4.6	(5.1)	4.8	7.9	8.6	6.9
29	26	23	15	10	4.6	16	23	27	29
					10				
5.8	8.3	8.0	4.6	4.6	(5.1)	4.8	7.7	8.6	6.9
27	24	22	15	10	4.5	15	23	28	30
					10				
6.1	8.2	7.7	4.8	4.6	(5.1)	4.8	7.4	8.4	6.3
28	25	21	15	10	4.6	15	22	27	30
					10				
5.4	8.1	7.6	4.5	4.6	(5.1)	4.8	7.1	7.9	6.6
29	25	22	15	10	4.6	15	22	28	30
					10				
6.1	8.2	7.8	4.9	4.9	(5.5)	4.9	7.4	8.3	6.7
29	25	21	15	10	4.9	15	22	27	30
					10				
6.2	8.4	8.1	5.0	5.0	(5.5)	4.9	7.2	7.7	5.9
28	25	22	16	10	4.9	16	23	26	28
					10				
6.3	7.7	7.1	5.1	5.0	(5.5)	4.8	6.9	7.4	5.4
27	25	21	16	10	5.0	16	23	27	29
					10				
5.6	7.7	7.2	5.0	4.9	(5.5)	5.0	7.0	7.5	4.7
28	25	22	16	10	4.9	16	22	26	28
					10				
5.7	7.7	7.2	5.1	4.9	(5.5)	5.1	6.8	7.1	4.7
29	25	21	15	10	4.9	17	22	25	28
					10				
6.0	8.2	7.7	5.0	4.9	(5.5)	5.1	7.0	7.0	5.3
29	25	21	15	10	4.9	16	22	26	27
					10				

Sta	+	H.I.	−	Elev	
37+50	4.90	236.93			
37+50			4.9	32.0	31.4
38			4.9	32.0	31.4
+50			4.8	32.1	31.4
39			4.9	32.0	31.4
B.M.			6.21	230.72 ✓	230.72 ✓
B.M.	4.40	235.12 ✓			230.72 ✓
39+50			3.0	32.1	31.4
40			3.1	32.0	31.3
+50			3.4	31.7	31.0
+62			3.5	31.6	30.9
+77			3.6	31.5	30.8
41			3.9	31.2	30.5

Lt & Rt

4.

6.6	8.2	7.8	5.1	5.0	(5.5)	4.9	5.0	6.9	7.4	5.6
30	26	22	14	10		10	15	20	24	26

7.8	8.3	8.0	5.3	5.0	(5.5)	4.9	5.3	7.0	8.0	6.4
27	25	22	15	10		10	15	19	23	25

9.2	8.9	5.1	4.9	(5.5)		4.9	5.3	7.5	8.2	7.6
28	24	16	10			10	15	20	23	24

8.6	8.1	5.3	5.0	(5.5)		4.9	4.9	7.5	8.2	7.1
28	22	16	10			10	14	19	23	25

Spike in tele pole at sta 39+40 { Moved since original Xsections were taken used for setting Grade stakes.

Started here - 10-30-23
Fair - Hot.

5.8	6.4	5.8	3.6	3.2	(3.7)	3.2	3.2	5.8	6.3	4.6
28	26	22	16	10		10	15	20	24	26

3.3	6.4	5.7	3.5	3.2	(3.8)	3.2	3.6	5.5	5.9	2.9
30	26	22	16	10		10	15	20	24	27

2.5	5.0	7.1	6.4	3.8	3.5	(4.1)	3.4	3.5	5.7	5.7	1.9
34	30	26	24	15	10		10	15	21	25	28
2.3	5.1	7.1	6.4	3.7	3.4	(4.2)	3.6	3.4	5.4	5.3	3.5	3.3	✓
34	30	27	23	17	10		10	16	20	25	29	32	
1.7	5.5	6.9	6.4	4.0	3.7	(4.3)	3.7	3.8	5.6	4.5	4.0	3.7	✓
35	29	26	22	16	10		10	17	20	27	30	35	

1.2	6.9	6.6	3.9	4.0	(4.6)	4.0	4.3	5.7	5.7	0.8
34	27	22	16	10		10	15	19	25	29

Sta	+	H.I	−	Elev	
	4.40	235.12			
41+50			4.6	30.5	29.9
42			5.4	29.7	29.0
+50			6.5	28.6	28.0
43		✓	7.7	27.4	26.7
T.P.	1.00	228.28	7.84	227.28 ✓	227.28 ✓
+50			2.3	26.0	25.3
44			3.9	24.4	23.7
+50			5.7	22.6	21.9
45		✓	7.6	20.7	20.0
T.P.	2.51	219.79	11.00	217.28 ✓	
+50			1.0	18.8	18.1
B.M.			1.76	218.03	
46			2.7	16.9	16.2
+50			4.8	15.0	14.8
47			6.7	13.1	12.3

Lt						℄	Rt					
0.6/34	3.2/32	7.7/26	7.2/21	4.8/16	4.7/10	(5.2)	4.6/10	4.9/15	6.6/19	6.6/23	3.4/29	1.1/31
	0.6/35	8.5/26	8.3/22	5.6/16	5.5/10	(6.1)	5.5/10	5.7/14	7.5/19	7.6/24	3.8/28	1.8/30
	2.2/35	9.6/26	9.3/23	6.5/16	6.6/10	(7.1)	6.6/10	6.4/17	6.3/26	4.3/27		
	5.2/35	10.8/27	10.6/23	7.5/16	7.8/10	(8.4)	7.8/10	8.0/15	10.9/20	11.1/24	8.2/27	6.0/29

Spike in tele pole Rt sta 43+35 used for Grade stakes

Lt						℄	Rt					
	(229.4/35)	5.2/27	5.0/22	2.4/16	2.4/10	(3.0)	2.4/10	2.4/15	5.3/20	2.5/28	0.8/30	
	0.2/35	7.2/26	6.7/21	4.0/16	4.0/10	(4.6)	4.0/10	4.1/15	7.4/22	7.4/26	4.7/30	2.2/32
	4.0/33	9.1/26	8.8/21	6.3/15	5.8/10	(6.4)	5.8/10	6.0/16	9.0/21	9.3/27	7.3/30	5.8/32
	8.1/29	11.0/26	10.4/21	8.0/15	7.7/10	(8.3)	7.7/10	8.0/16	11.5/21	11.4/24	9.6/27	
	1.7/28	4.0/25	3.5/20	1.4/15	1.1/10	(1.7)	1.1/10	1.3/15	3.8/20	4.0/23	3.4/25	4.0/26

Spike in tele pole 29' Rt sta 45+50 (used for T.P. in original Xsec)

Lt						℄	Rt					
	4.0/27	5.7/25	5.4/21	2.9/15	3.9/10	(3.6)	3.0/10	3.0/14	6.2/20	6.3/23	7.0/26	
4.9/29	5.7/28	7.4/26	7.2/18	5.0/15	4.9/10	(5.5)	4.9/10	4.9/14	8.3/20	8.3/22	8.5/25	
6.7/30	7.7/27	9.3/25	9.1/20	6.9/15	6.8/10	(7.5)	6.8/10	6.9/15	9.9/19	9.9/22	9.1/23	9.5/25

Sta	+	H.I.	−	Elev	
	2.51	219.79			
47 +20			7.5	12.3	11.5
+40			8.3	11.6	10.8
+50		✓	8.7	11.1 ✓	10.3
T.P.	1.24	210.83	10.20	209.59	
48			1.7	09.1	08.4
+50			3.7	07.1	06.4
49			5.6	05.2	04.5
+50		✓	7.1	03.7 ✓	03.0
T.P.	3.00	205.35	8.48	202.35	
50			3.00	202.7	01.7
+50			4.0	201.4	200.7
51			4.7	00.7	199.9
+50			5.1	00.3	99.5
52		✓	5.4	00.0 ✓	99.2
T.P.	5.25	203.72	6.88	198.47	
B.M.			4.31	199.41 ✓	199.35

7.5/30 7.6/17 7.6/10 (8.3) 7.6/10 7.8/16 10.9/21 11.1/24 10.6/26

7.8/32 8.8/26 10.6/24 10.9/20 8.2/16 8.4/10 (9.0) 8.4/10 8.5/15 11.4/20 12.3/26 11.5/27

10.2/26 11.2/25 11.4/20 8.8/14 8.8/10 (9.5) 8.8/10 8.8/16 12.0/21 12.5/26 11.7/27

3.6/27 5.6/25 5.5/20 1.9/15 1.8/10 (3.4) 1.8/10 1.9/16 4.7/21 5.2/26 4.3/27

cut ruts out
48+35

6.4/19 4.0/15 3.8/10 (4.4) 3.8/10 3.9/16 6.9/21 7.3/25 6.0/27

cut ruts out
sta 49+00

10.2/21 5.7/15 5.7/10 (6.3) 5.7/10 5.8/16 8.7/22 9.6/25

11.5/22 7.1/16 7.2/10 (7.8) 7.2/10 7.3/15 10.1/20 11.3/23

7.6/21 3.0/15 3.1/10 (3.7) 3.1/10 2.9/15 4.2/18 ~~3.6~~

7.4/20 4.0/16 4.1/10 (4.7) 4.1/10 3.9/16 6.6/20

6.5/19 4.6/16 4.8/10 (5.5) 4.8/10 5.0/16 7.4/21

7.6/20 6.1/18 5.3/16 5.2/10 (5.9) 5.2/10 5.3/15 8.0/21 7.8/28

7.6/20 5.7/16 5.5/10 (6.2) 5.6/10 5.7/16 8.5/21 8.9/28

R.R. spike in 3rd bent Lt sta 55+50

See page 77 of original Notes

Final Xsections

23-63

Carley
Persons
Briggs
Eck

10-31-23

Sta.	+	H.I.	−	Elev	
B.M.	6.99	231.14			224.15
108+04			7.6	23.5	
107+97			7.5	23.6	22.9
+50			7.1	24.0	23.3
107			6.7	24.4	23.8
+50			6.1	25.0	24.3
106			5.6	25.5	24.8
+50			5.2	25.9	25.3
105			4.7	26.4	25.8
+50			4.2	26.9	26.3
104			3.8	27.3	26.7
+50			3.4	27.7	27.0
B.M.	6.10	234.24	2.95	228.19	228.16
103			6.2	28.1	27.4
+50			5.8	28.5	27.7

Nail in tel. pole S.E. cor. Cleveland + 6th str

8.4/19 8.1/14 7.7/25 9.5/31 8.0/37

8.0/18 8.3/16 7.8/15 7.6/10 (8.2) 7.6/10 7.6/20 9.0/23 9.1/28 0.7/37 End of paving

7.4/18 7.9/17 7.3/15 7.3/10 (7.8) 7.3/10 7.2/15 8.5/18 8.4/20 2.6/27

7.0/18 7.4/17 6.8/15 6.7/10 (7.3) 6.8/10 6.8/16 8.5/18 8.4/21 4.8/27

6.5/19 6.9/18 6.1/14 6.2/10 (6.8) 6.3/10 6.3/15 7.8/18 7.6/19 7.0/20

5.9/19 6.6/18 6.5/17 5.6/14 5.7/10 (6.3) 5.8/10 5.9/15 7.3/18 7.9/21

5.4/18 6.0/17 5.9/16 5.4/14 5.3/10 (5.8) 5.3/10 5.4/15 7.2/18 7.1/23 6.6/24

Cut runs out 105+30

4.0/32 4.6/17 4.8/10 (5.3) 4.8/10 4.8/16 6.4/38 X road Rt + Lt

2.2/26 4.0/23 4.4/22 5.1/20 5.1/17 4.3/15 4.3/10 (4.8) 4.3/10 4.3/15 5.8/18

3.1/25 4.3/23 4.9/21 4.9/17 4.0/15 3.9/10 (4.4) 3.9/10 4.0/14 6.7/20 7.3/24

4.0/21 4.7/20 4.6/18 3.7/16 3.5/10 (4.1) 3.5/10 3.3/17 4.5/23 6.0/29 6.3/34

Nail in oak tree 22' Lt sta 103+30

6.8/22 7.8/20 7.8/19 6.4/15 6.3/10 (6.9) 6.3/10 6.3/15 7.9/18 8.5/27

6.5/21 7.4/20 7.4/18 6.0/15 6.0/10 (6.6) 5.9/10 5.9/15 7.4/18 8.0/25

Sta	+	H.I.	−	Elev	
	6.10	234.26			
102			5.6	28.7	28.0
+50			5.3	29.0	28.2
101			5.1	29.2	28.5
+50			4.8	29.5	28.7
100			4.6	29.7	29.0
		Long Sta. 101.0'			
+50		99+01.3 = 99+00.3	4.5	29.8	29.1
Equation		99+00.3 = 99+01.3	Sta 99 to 100 = 99+0		
99			4.5	29.8	29.1
+50			4.6	29.7	28.9
T.P.	4.04	232.97	5.33	228.93	
98			3.8	29.2	28.6
+50			4.3	28.7	28.1
97			4.9	28.1	27.5
+50			5.7	27.3	26.6
T.P.	7.00	228.74	11.23	221.74	
96			2.4	26.3	25.7

Lt ℄ Rt

(6.3) 6.1/22 6.9/20 6.7/18 5.8/16 5.6/10 5.7/10 5.7/15 7.3/18 8.2/22

(6.1) 5.6/26 6.1/22 6.8/21 6.9/18 5.4/15 5.4/10 5.4/10 5.6/15 7.0/18 7.0/21

(5.8) 6.5/28 6.4/23 7.1/22 7.0/19 5.1/15 5.2/10 5.2/10 5.3/15 7.2/19 7.4/22

(5.6) 6.6/30 6.5/24 7.1/23 7.2/20 5.2/16 4.9/10 4.9/10 5.0/15 7.0/19 7.5/25

(5.3) 6.1/30 6.1/25 7.1/23 7.2/20 4.7/15 4.7/10 4.6/10 5.0/15 6.9/19 7.0/21 6.4/24 6.9/27

(5.2) 4.6/32 4.2/28 7.5/24 7.4/22 4.4/15 4.8/10 4.3/10 4.4/15 6.6/20 6.8/25 5.0/27

(5.2) 3.6/36 3.4/32 7.0/26 7.2/23 4.7/18 4.8/11.9 5.0/11.1 4.1/10 3.9/15 6.0/19 5.7/24 3.8/26

(5.4) 3.8/33 7.5/28 7.2/24 4.9/19 5.2/13.5 5.4/12.8 4.1/10 4.7/18 6.0/21 5.8/27 4.7/30 5.2/36

(4.4) 3.8/34 7.1/29 7.1/26 4.2/20 4.3/14.1 4.5/13.3 3.3/10 2.6/16 5.3/22 5.3/26 4.6/28 4.7/33

(4.9) 5.3/32 7.2/28 7.2/25 4.5/20 4.8/13.5 5.0/12.6 3.7/10 3.2/16 6.2/22 4.5/29

(5.5) 5.3/30 7.6/26 7.6/24 5.5/19 5.4/13.5 5.6/12.7 4.3/10 4.0/15 7.2/20 7.1/25 5.4/28

(6.4) 5.4/27 7.7/23 7.8/20 5.9/16 5.9/11.2 6.1/10.3 5.3/10 5.3/15 7.2/19 7.7/25 6.5/27

(3.0) 2.4/26 4.8/22 4.9/19 2.6/15 2.4/10 2.6/8.9 2.3/10 2.0/16 3.5/20 4.3/26 3.1/29

Sta	+	H.I.	−	Elev	
	7.00	228.74			
95 +50			3.6	25.1	24.5
95			4.8	23.9	23.2
+50			6.2	22.5	21.8
94			7.6	21.1	20.4
+50			9.0	19.7	19.0
T.P.	3.14	221.22	10.66	218.08	
93			3.0	18.2	17.6
+50			4.3	16.9	16.2
92			5.7	15.5	14.8
+50			7.0	14.2	13.5
T.P.	5.47	214.83	11.86	209.36	
91			1.9	12.9	12.2
+75.7			2.5	12.3	11.7
+50			3.1	11.7	11.0
90			4.3	10.5	10.0

(4.2)

3.1/26 5.2/22 5.4/20 3.7/15 3.7/10 3.6/10 3.5/16 4.6/20 5.1/27 3.0/30

(5.5)

3.9/26 6.4/22 6.5/19 4.7/15 4.9/10 4.9/10 4.8/18 6.5/23 6.2/28 3.6/31

(6.9)

5.5/27 7.8/23 7.7/20 6.1/16 6.2/10 6.3/10 6.1/17 7.2/22 7.7/25 6.6/27 6.0/34

(8.3)

7.5/28 9.7/24 9.5/21 7.6/16 7.7/10 7.7/10 7.7/17 9.3/21 9.1/24 6.0/29

(9.7)

9.5/31 9.3/27 11.4/24 11.3/21 8.9/16 9.1/10 9.1/10 9.0/15 10.8/20 10.9/23 8.2/27

(3.6)

3.6/25 5.2/23 5.1/20 2.9/16 3.1/10 3.1/10 3.2/15 5.2/19 5.4/22 2.6/26

(5.0)

6.3/25 6.8/23 6.9/20 4.1/15 4.4/10 4.4/10 4.4/15 6.8/20 6.6/23 5.2/25

(6.4)

8.8/22 5.4/16 5.8/10 5.8/10 5.7/15 8.3/20 8.3/23 7.2/25

(7.7)

12.3/24 6.8/16 7.1/10 7.1/10 7.5/15 10.4/21 10.7/24 9.6/26

(2.6)

10.6/30 1.4/16 1.7/10 2.0/9.2 1.8/10 1.9/15 5.1/22 5.4/25 4.0/27

(3.1)

12.1/31 2.0/17 2.3/10 2.7/9.3 2.5/10.2 2.6/15 5.6/22 5.7/26 3.7/30 ✓

(3.8)

12.2/31 2.4/17 2.8/10 3.4/9.5 3.2/10.4 3.5/16 5.8/23 6.2/26 3.5/31

(4.8)

14.0/30 3.3/16 3.7/10 5.0/12.3 4.7/13 4.7/19 6.8/25 7.3/31 3.8/36

Sta	+	H.I.	−	Elev	
	5.47	214.83			
89+75Z			4.8	10.0	09.4
89 +50			5.2	09.6	08.9
89 +25.7			5.8	09.0	08.4
89			6.2	08.6	07.9
+85I			6.6	08.2	07.6
+50			7.2	07.6	06.9
+35I			7.6	07.2	06.6
88		✓	8.2	06.6	05.9
TP	1.44	208.13	8.14	206.69 ✓	
+85Z			1.9	06.2	05.6
+50			2.6	05.5	04.8
+35I			2.8	05.3	04.5
87			3.6	04.5	03.8

Lt & Rt

14.0/29	4.9/16	4.2/10	(5.4)	5.6/12.8	5.3/13.8	5.4/19	7.3/26	7.5/33	4.3/37
12.5/32	11.7/29	4.4/18	4.8/10	(5.9)	6.1/12.6	5.8/13.5	6.0/19	8.2/27	8.2/32	5.0/37
9.8/37	10.2/36	9.3/26	4.4/18	5.2/10	(6.4)	6.5/12.6	6.3/13.6	6.3/19	8.8/26	8.9/32	4.7/38
7.6/36	9.0/34	8.1/23	4.9/17	5.6/10	(6.9)	7.0/12.7	6.8/13.7	7.0/19	9.2/25	9.5/29	3.2/38
7.9/35	9.2/33	8.1/22	5.6/17	6.0/10	(7.2)	7.4/12.8	7.2/13.6	7.1/18	9.7/24	9.8/28	212.9/37.5
5.4/31	6.6/29	9.0/28	10.0/26	10.0/22	6.6/16	6.7/10	(7.9)	8.0/12.5	7.8/13.4	8.0/19	10.2/23	10.2/27	215.3/38
4.1/32	8.0/28	10.4/25	10.4/21	7.0/15	7.0/10	(8.2)	8.4/12.8	8.1/13.6	8.1/19	10.3/23	10.4/27	215.4/38
213.4/37	210.9/34	210.8/32	11.1/24	11.1/20	7.8/15	7.8/10	(8.9)	8.9/11.9	8.6/12.8	8.8/18	10.7/22	10.8/26	215.8/39
214.7/35	4.5/23	4.4/20	1.2/15	1.5/10	(2.5)	2.4/11	2.2/11.7	1.9/18	4.4/23	4.5/26	215.7/39
217.4/37	0.0/29	5.0/23	5.1/19	2.2/15	2.3/10	(3.3)	2.9/9.2	2.6/10.0	2.6/16	5.1/23	5.2/25	214.2/37
218.2/38	0.0/30	5.5/23	5.6/19	2.6/15	2.7/10	(3.6)	3.1/9	2.9/10	3.0/15	5.3/21	5.5/25	212.6/36
220.7/41	0.0/31	6.1/23	3.6/15	3.6/10	(4.3)	3.7/10	3.8/15	6.1/21	6.4/25	208.9/34

Sta	+	H.I	−	Elev	
	1.44	208.13			
86 +85.7			3.9	08.2	03.4 99.9
86 +50			4.7	07.4	02.8 00.7
86 +00		✓	5.6	06.5	01.8 01.6
T.P.	5.59	207.46	6.26	201.87 ✓	
B.M.				✓	204.61
T.P.	0.73	204.22 ✓	3.97	203.49	
85 +60			2.5	01.7	
+50			2.7	01.5	200.7
85			3.8	00.4	199.7
+50			4.7	99.5	98.7
84			5.5	98.7	98.0
+50			5.8	98.4	97.7
83			5.6	98.6	97.9
+50			4.8	99.4	98.6
82			3.5	✓ 00.7	200.0
T.P.	7.07	209.16 ✓	2.13	202.09	

(220.8 / 41) 1.5/31 6.3/25 6.2/20 3.9/15 3.9/10 (4.7) 4.1/10 4.1/15 6.4/21 6.5/25 0.8/33 ✓

(219.3 / 41) 0.7/34 7.2/26 7.2/21 4.5/15 4.7/10 (5.3) 4.8/10 4.8/15 7.4/22 7.8/25 7.0/27 2.6/33

(216.6 / 39) 8.1/24 8.2/21 5.4/15 5.4/10 (6.3) 5.7/10 5.6/15 8.5/21 9.1/26 4.6/34

Nail in 10" oak Lt sta 85+75 Removed.

Top of bottom plank at G.P.

2.3/31 6.2/27 5.8/20 2.5/16 2.4/10 2.5/9.2 2.6/9.3 2.5/10 2.5/16 6.5/23 9.0/29 8.7/31 9.7/33 ✓

5.1/31 7.0/28 6.8/21 2.7/16 2.7/10 2.8/9 (3.5) 2.8/9.4 2.7/10.1 2.8/18 9.2/28 11.6/35

(88.3 / 33) 3.6/15 3.7/10 3.8/9.3 (4.5) 3.9/11 3.7/10 4.1/18 (82.6 / 44)

(83.16 / 40) 4.6/16 4.6/10 4.7/9.1 (5.5) 4.8/9.4 4.6/10.1 4.7/17 (80.6 / 44) (79.5 / 47)

(81.16 / 41) 5.4/15 5.4/10 5.5/9.4 (6.2) 5.6/9 5.5/10 5.5/16 (81.5 / 42)

(84.16 / 36) 5.6/15 5.8/10 5.9/9.5 (6.5) 5.9/9.3 5.8/10 6.3/17 (80.1 / 44)

(83.7 / 39) 5.5/16 5.5/10 5.6/9.3 (6.3) 5.7/9.3 5.6/10 5.9/16 (81.4 / 41)

(84.5 / 38) 4.9/16 4.7/10 4.8/9.2 (5.6) 4.9/9.3 4.7/10.1 4.8/16 (82.8 / 38)

(87.7 / 34) 3.4/15 3.5/10 3.7/9.0 (4.2) 3.4/10 3.5/15 (87.7 / 37)

Top of C.M.P. pipe Rt 9+17 10-31-23

Sta	+	H.I	−	Elev	
	7.07	209.16			
E (C.81+30.9 = 81+33.1)	81+33.1 = 81+30.9 Long Sta. 102.2		6.0	63.2	02.5
81			4.6	04.6	03.8
+50			2.6	06.6	05.9
T.P.	9.47	216.38 ✓	2.25	206.91 ✓	
80			7.8	08.6	07.9
+50			5.7	10.7	10.0
79			3.7	12.7	12.0
+50			1.7	14.7	13.9
B.M.	7.55	223.53 ✓	0.35	216.03 ✓	215.98 ✓ Error 0.05
78			7.2	16.3	15.6
+50			5.7	17.8	17.1
77			4.5	19.0	18.3
+50			3.5	20.0	19.4
76			2.7	20.8	20.1

started here - 11-5-23
same-party Fair-warm

11.1/37 11.9/35 9.7/24 6.0/18 6.3/12.3 6.5/11.3 (6.7) 5.5/10 5.5/16 7.4/37 Driveway

6.2/36 9.2/33 8.5/28 5.2/20 5.3/14.9 5.5/14 (5.4) 4.1/10 4.1/17 6.6/23 7.9/27 7.0/37 7.1/43

3.4/34 6.8/30 6.5/27 3.4/21 3.2/15.1 3.4/14 (3.3) 2.0/10 1.9/18 5.2/25 5.3/29 4.6/30 4.5/33

(8.5)
10.1/31 11.8/29 11.5/26 8.6/21 8.5/15.1 8.7/14.1 7.1/10 6.7/17 11.2/24 11.2/27 10.5/28

(6.4)
13.6/30 6.6/20 6.4/15 6.4/14.1 5.1/10 4.8/16 8.4/22 8.3/26 7.6/28

(4.4)
14.1/35 4.5/20 4.3/15.2 4.6/14.4 3.1/10 2.6/17 5.0/24 5.5/27 5.2/28 5.7/31

(2.5)
9.6/34 2.1/22 2.1/14.4 2.4/13.6 1.3/10 1.2/17 8.2/25

Nail in tree Lt of sta 78+15 used for Grade-stakes.

Cut Ends Rt + Lt Sta 78+23.1 R.C.

6.5/31 7.0/29 8.8/27 8.8/22 6.9/16 6.9/10 (7.9) 7.6/9.2 7.4/10.1 7.3/17 9.6/22 9.8/25 5.1/31

(6.4)
1.3/33 8.0/25 8.0/21 5.6/16 5.7/10 6.0/9.1 5.6/10 5.8/16 7.5/20 7.7/27 4.4/31

(5.2)
(228.5/35) 6.1/24 6.1/20 4.6/15 4.6/10 4.6/10 4.7/15 6.5/22 7.0/28 3.8/32

(4.1)
(227.0/33) 5.5/24 5.3/20 3.4/16 3.6/10 3.6/10 3.5/17 5.7/23 5.8/28 3.4/32

(3.4)
1.2/29 4.7/24 4.7/20 2.6/14 2.9/10 2.8/10 2.7/17 4.8/23 5.0/29 2.0/32

Sta	+	H.I	−	Elev.	
	7.53	223.53			
+50			2.2	21.3	20.7
T.P.	7.04	229.27	1.30	222.23	
75			7.6	21.7	21.0
+50			7.4	21.9	21.1
B.M.					222.37
74			7.4	21.9	21.1
+50			7.5	21.8	21.0
T.P.	4.04	225.71	7.60	221.67	
73			4.3	21.4	20.8
+50			4.6	21.1	20.5
72			4.9	20.8	20.2
+50			5.0	20.7	20.1
+50					
71			4.7	21.0	20.3
+50			4.2	21.5	20.4
70			3.4	22.3	21.7

Lt ℄ Rt

(2.8)

0.8	2.5	4.2	4.0	2.4	2.4	2.2	2.3	4.7	5.1	4.3
29	26	24	20	15	10	10	15	21	28	30

(8.3)

4.6	9.2	9.1	7.6	7.7	7.7	7.8	10.8	11.3	10.5
29	23	18	14	10	10	16	22	27	29

(8.2)

(231.8)	0.0	9.0	9.1	7.5	7.4	7.4	8.0	10.5	10.7	5.8
36	34	22	19	15	10	10	16	20	25	30

Nail in tele. pole Lt of sta 74+05 Removed

(8.2)

(230.4)	9.6	9.5	7.6	7.5	7.5	7.9	10.4	10.6	5.8
36	23	19	16	10	10	17	20	26	32

(8.3)

5.5	11.3	10.7	7.6	7.6	7.6	7.8	12.5	12.6	10.8
37	29	22	16	10	10	16	25	28	32

Cut beg. 175 73+20

(4.9)

5.6	9.2	8.4	4.3	4.3	4.3	4.2	4.2	12.3
36	32	24	16	10	9.3	9.9	16	27

(5.2)

10.3	10.8	7.7	4.6	4.6	4.6	4.6	4.5	4.6	13.8
36	32	24	16	10	9.1	9.5	10	15	28

(5.5)

11.9	4.7	4.8	5.0	4.9	4.8	4.9	14.0
27	17	10	9.0	9.3	10	15	27

(5.6)

11.8	10.6	5.0	5.0	5.1	5.1	5.0	5.1	13.6
32	25	17	10	9.3	9.2	10	16	28

Lt Rt

24" corr. CMP (5.4) Invert - 213.70 Outlet - 212.50

11.2	4.7	4.6	4.8	4.7	4.6	5.0	14.5
25	16	10	9.1	9.3	10	15	29

(5.3)

11.1	4.1	4.2	4.3	4.3	4.2	4.3	14.2
27	15	10	9.2	9.4	10	15	29

(4.0)

6.7	3.6	3.3	3.5	3.4	3.3	3.3	14.3
21	16	10	9.4	9.1	10	15	32

Sta	+	H.I.	−	Elev	
	4.04	225.71			
+50			2.3	23.4	21
69			1.2	24.5	23.8
T.P.	7.23	231.76	1.18	224.53	
+50			6.2	25.6	24.9
68			5.4	26.4	25.7
+50			5.0	26.8	26.2
		66+60.8 = 66+63.6			
67			4.9	26.9	26.2
		Equation 66+63.6 = 66+60.8			
		67 − 66 short sta 77.2'			
+50			5.3	26.5	25.9
66			6.0	25.8	25.1
+50			7.1	24.7	24.0
B.M.					228.55
65			8.5	23.3	22.6
T.P.	2.24	224.82	9.18	222.58	
+50			2.9	21.7	21.2
64			4.3	20.5	19.9

Lt & Rt

119

cut ends
69+75

4.8 / 29	6.7 / 26	6.6 / 22	2.5 / 16	2.3 / 10	2.4 / 9.2	2.3 / 9.2	2.2 / 10	2.5 / 15	13.1 / 30	✓

(1.9)

0.0 / 29	4.0 / 25	4.0 / 20	1.3 / 15	1.3 / 10	1.2 / 9.3	1.1 / 10	1.3 / 16	6.1 / 25	8.4 / 34	8.0 / 35

(6.9)

(2348 / 33)	4.0 / 28	8.8 / 25	8.6 / 20	6.3 / 15	6.2 / 10	6.3 / 10	6.2 / 15	8.9 / 20	9.2 / 25	2.4 / 35

(6.1)

(237.4 / 35)	3.2 / 29	8.1 / 24	7.7 / 19	5.8 / 15	5.4 / 10	5.4 / 10	5.5 / 18	8.0 / 20	7.7 / 24	(236.7 / 37)

(5.6)

(238.1 / 36)	3.4 / 28	8.1 / 24	8.1 / 20	5.4 / 15	5.1 / 10	5.1 / 10	5.2 / 15	7.3 / 19	7.6 / 24	3.6 / 29	(240.5 / 38)

(5.6)

(237.1 / 37)	8.1 / 25	7.5 / 20	5.2 / 15	5.0 / 10	5.0 / 10	4.9 / 15	7.2 / 20	7.3 / 25	(239.4 / 37)

(5.9)

(235.1 / 36)	4.9 / 29	8.3 / 25	8.1 / 21	5.5 / 16	5.4 / 10	5.3 / 10	5.4 / 15	7.9 / 20	7.9 / 26	4.6 / 28	(235.5 / 35)

(6.7)

(234.3 / 38)	5.6 / 31	8.9 / 26	8.6 / 20	6.3 / 15	6.0 / 10	6.0 / 10	6.1 / 14	8.6 / 19	8.8 / 24	5.9 / 27	(236.9 / 40)

(7.8)

(230.7 / 35)	7.3 / 29	10.4 / 27	10.2 / 21	7.2 / 16	7.2 / 10	7.1 / 10	7.1 / 19	9.5 / 21	9.8 / 28	6.9 / 31	(233.6 / 40)

Spike in T.R Lt of sta 65+15 Removed

(9.7)

7.0 / 31	11.5 / 25	11.6 / 22	9.0 / 15	8.4 / 10	8.6 / 10	8.5 / 16	9.9 / 19	11.3 / 23	11.0 / 30	8.9 / 33	4.4 / 38

(3.6)

8.4 / 31	7.5 / 26	4.8 / 21	3.0 / 15	3.0 / 10	3.0 / 10	3.0 / 16	6.1 / 23	7.1 / 26	6.8 / 32	6.8 / 34

(4.9)

12.1 / 29	7.0 / 21	4.7 / 15	4.4 / 10	4.3 / 10	4.5 / 15	8.8 / 26	9.2 / 30	cut ends 64+00	

Sta	+	H.I	−	Elev	
	2.24	224.82			
+50			5.6	19.2	18.5
B.M.					220.34
63		✓	7.1	14.7 ✓	17.0 ✓
	4.06	217.95	10.98	213.84	213.89
+50			1.8	15.2	15.3
62			3.6	14.4	13.7
+50			5.3	12.7	12.0
61		✓	7.1	10.9 ✓	10.2
T.P.	1.83	211.86	7.92	210.03	
+50			2.7	09.2	08.5
60			4.4	07.5	06.7
+50		✓	6.1	05.8	05.1
T.P.	2.20	205.57	8.49	203.37 ✓	
59			1.3	04.3	03.5
+50			2.7	02.9	02.2
58			3.8	01.8	201.1

Lt ℄ Rt

(6.3)

11.8 / 28	8.1 / 20	6.3 / 15	5.7 / 10	5.7 / 10	5.9 / 16	9.2 / 24	9.3 / 27	6.6 / 30

Spike in 14" oak Lt sta 63+10

(7.8)

10.8 / 25	7.1 / 16	7.1 / 10	7.2 / 10	7.4 / 16	10.4 / 21	10.7 / 25	3.1 / 31

R.R. spike in tele. pole Lt of sta 62+20

(2.7)

11.3 / 40	11.8 / 17	11.9 / 10	11.7 / 10	2.1 / 16	4.9 / 21	4.8 / 27

used for Grade stake 3 (224.1 / 36)

(220.4 / 45) (216.0 / 39)

(4.3)

7.2 / 32	7.2 / 21	3.6 / 15	3.6 / 10	3.6 / 10	3.5 / 16	5.8 / 19	5.8 / 23	(224.2 / 35)

(220.3 / 42) (216.5 / 37) +4.5

7.9 / 30

(6.0)

								+7.6 (219.6 / 34)
8.6 / 27	8.4 / 21	3.6 / 16	5.4 / 10	5.4 / 10	5.5 / 14	8.1 / 19	8.1 / 23	

(7.8)

2.6 / 37	4.0 / 35	10.7 / 28	11.0 / 21	7.4 / 15	7.2 / 10	7.2 / 10	7.1 / 16	9.8 / 20	9.7 / 26	5.5 / 31

(3.4)

3.3 / 32	6.2 / 29	6.8 / 27	6.8 / 22	3.0 / 16	2.8 / 10	2.8 / 10	2.8 / 16	6.1 / 22	7.0 / 29	6.8 / 31

(5.2)

9.7 / 35	9.9 / 25	7.8 / 15	4.5 / 10	4.5 / 9.4	4.3 / 10	4.6 / 17	12.5 / 28	

(6.8)

14.5 / 29	11.7 / 23	6.1 / 15	6.1 / 10	6.2 / 9.3	6.2 / 9.7	6.1 / 10	6.3 / 16	11.3 / 22	16.0 / 25

(2.1)

10.6 / 29	1.6 / 16	1.3 / 10	1.4 / 9.2	1.5 / 9.4	1.3 / 10	1.5 / 16	10.8 / 26

(3.4)

11.5 / 28	2.7 / 16	2.6 / 10	2.8 / 9.2	2.7 / 9.2	2.6 / 10	2.9 / 15	10.8 / 24

(4.5)

11.3 / 26	3.7 / 16	3.8 / 10	3.9 / 9.2	3.9 / 7.6	3.8 / 10	4.0 / 15	11.9 / 23

Sta	+	H.I	−	Elev	
	2.20	205.57			
+50			4.9	00.7	200.1
57			5.8	99.8	199.3
+50			6.6	99.0	98.6
+12					
56			7.0	98.0	98.2
T.P.	4.50	203.84	6.23	199.34	
+50			5.4	98.4	97.9
55			5.5	98.3	97.7
+92					
+50			5.4	98.4	97.8
54			5.1	98.7	98.0
+50			4.9	98.9	98.3
53			4.6	99.2	98.6
+50			4.3	99.5	98.9
B.M.			4.50	199.34	199.35

Lt ℄ Rt

(5.5)

11.5 / 24	5.0 / 16	4.9 / 10	5.1 / 9.2	5.0 / 9.2	4.9 / 10	5.3 / 16	11.8 / 24

(6.3)

11.9 / 28	11.0 / 22	6.3 / 15	5.8 / 10	5.9 / 9.3	6.0 / 9.2	5.9 / 10	6.0 / 15	11.0 / 21

(7.0)

11.9 / 27	11.5 / 23	6.6 / 16	6.5 / 10	6.6 / 9.5	6.7 / 9.1	6.6 / 10	6.6 / 15	11.1 / 21	11.8 / 25

24" conc. culvert — Invert 121 Lt 193.5 — Outlet Rt 193.0

11.7 / 35	11.1 / 23	7.1 / 16	7.0 / 10	(7.4)	7.1 / 10	6.9 / 15	11.5 / 22	11.3 / 25

(5.9)

5.7 / 26	7.8 / 23	7.8 / 19	5.7 / 15	5.5 / 10	5.5 / 10	5.4 / 15	9.0 / 20	9.1 / 24	6.6 / 29

(6.1)

7.8 / 37	7.2 / 32	8.6 / 28	7.8 / 21	5.5 / 17	5.9 / 10	5.6 / 10	5.6 / 16	9.4 / 22	9.8 / 28

24" conc culvert (6.0) Invert 194.0 Lt — Outlet 193.8 Rt

8.5 / 25	8.3 / 21	5.6 / 17	5.4 / 10	5.4 / 10	5.8 / 16	8.6 / 20	9.6 / 29

(5.8)

7.7 / 22	5.2 / 16	5.2 / 10	5.3 / 10	5.6 / 16	8.7 / 22	9.8 / 29	

(5.5)

6.9 / 20	5.6 / 18	4.8 / 15	5.0 / 10	5.0 / 10	5.2 / 15	8.1 / 19	8.6 / 28	7.6 / 29

(5.2)

7.0 / 19	4.8 / 17	4.7 / 10	4.7 / 10	4.9 / 16	8.0 / 22	8.4 / 29	7.0 / 30	

(4.9)

5.8 / 20	4.4 / 17	4.4 / 10	4.4 / 10	4.6 / 16	7.7 / 22	8.1 / 25	

R.R. spike in 3rd Bent Lt of sta 55+50

Topography

23-63

Conley
Persons
Briggs
Eck

11-3,4.-23

Fair-Warren

Sta.

17+00

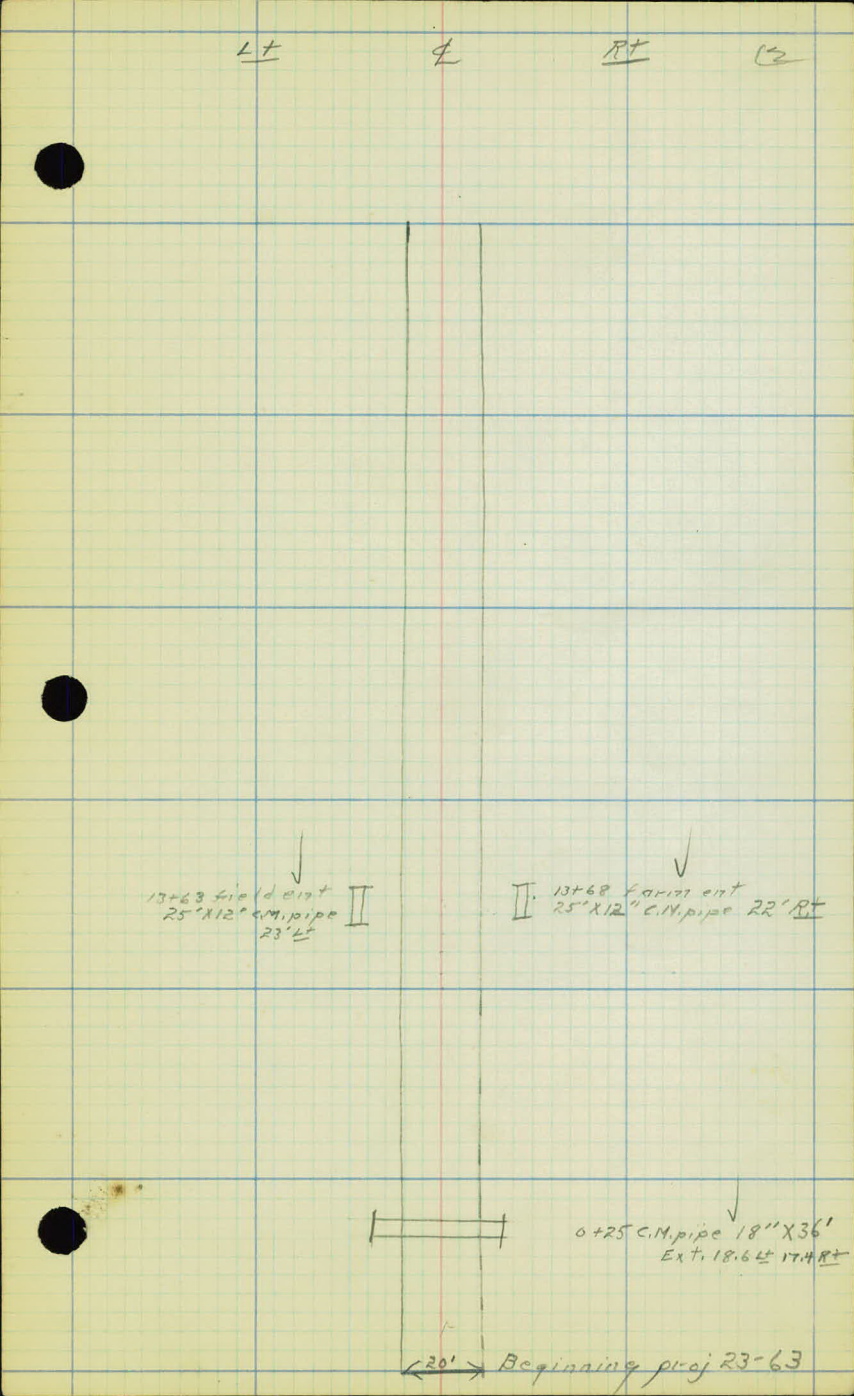
16+00

15+00

14+00

13+00

0+00


Lt
℄
Rt
13+63 field ent
25"X12" C.M. pipe
23' Lt
II
II
13+68 farm ent
25"X12" C.M. pipe 22' Rt
0+25 C.M. pipe 18"X36'
Ext. 18.6 Lt 17.4 Rt
20'
Beginning proj 23-63

5+00

23+00

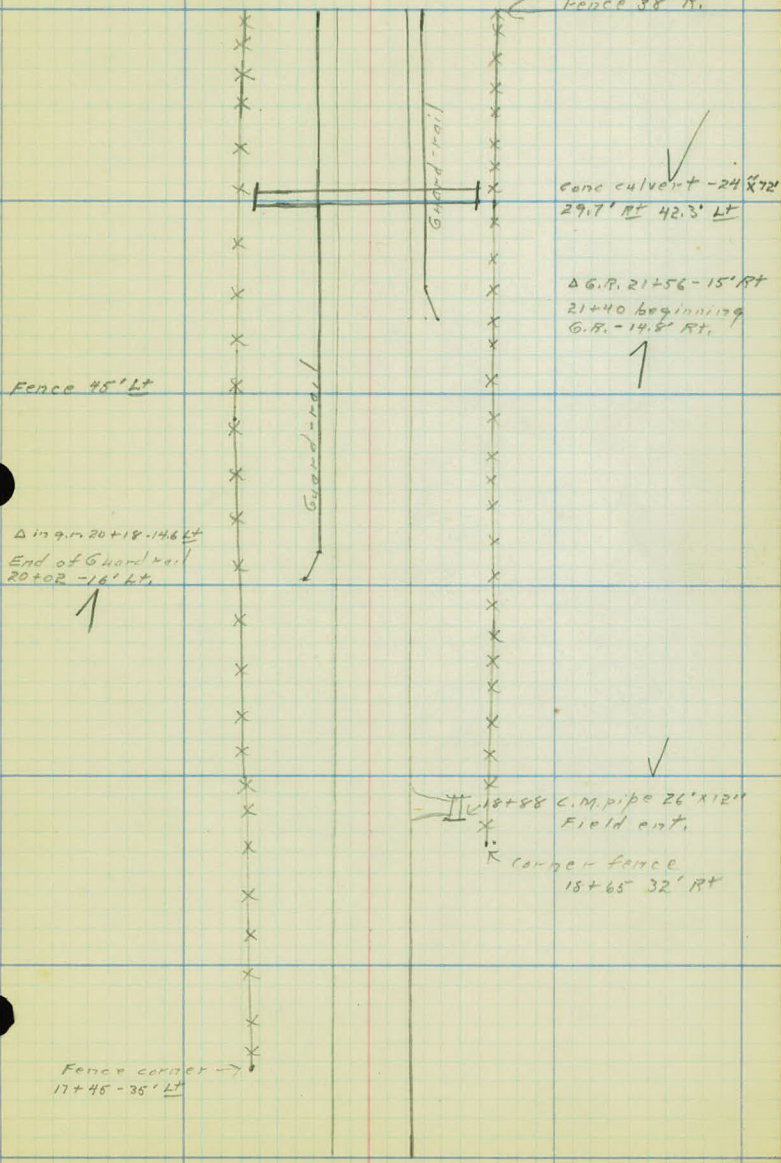
22+00

21+00

20+00

19+00

18+00


Fence 38' Rt.
Guard rail
Conc culvert - 24" x 72"
29.7' Rt 42.3' Lt
Δ G.R. 21+56 - 15' Rt
21+40 beginning
G.R. - 14.8' Rt.
1
Fence 45' Lt
Guard rail
Δ in g.r. 20+18 - 14.6 Lt
End of Guard rail
20+02 - 16' Lt.
1
18+88 C.M. pipe 26" x 12"
Field ent.
Corner fence
18+65 32' Rt
Fence corner
17+46 - 35' Lt

Sta

29

28

27

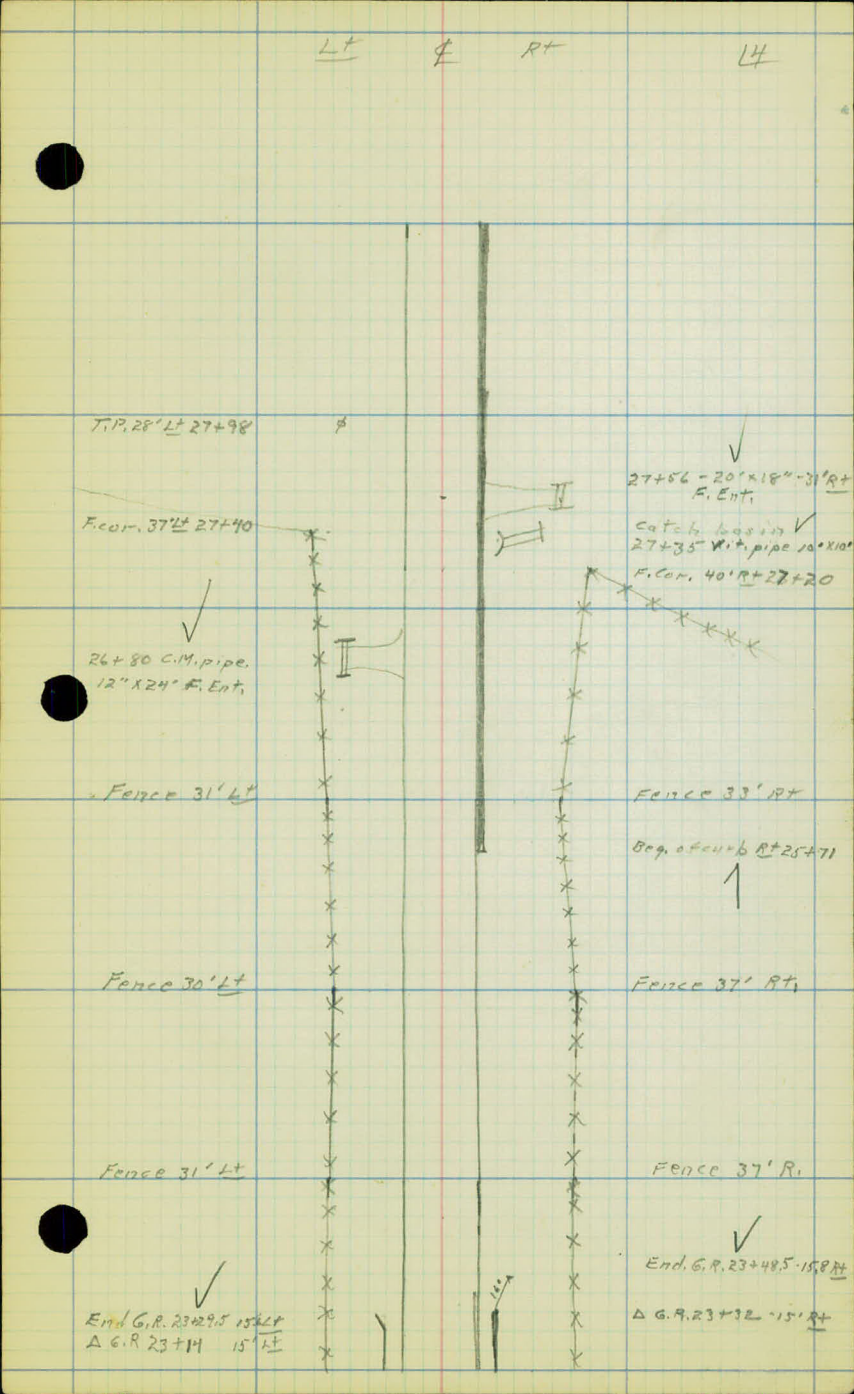
26+00

25+00

24+00

Width of paving on Curve.

Sta	width
25+75	20'
26+00	20'
26+25	20'
26+50	20.7'
26+75	21.8'
27+00	22.7'
+25	23.0'
+50	22.8'
+75	22.8'
28	22.8'
+25	22.1'
+50	20.8'
+75	20.0'


Lt
℄
Rt
14
T.P. 28' Lt 27+98
F. cor. 37' Lt 27+40
26+80 C.M. pipe. 12" X 24" F. Ent.
Fence 31' Lt
Fence 30' Lt
Fence 31' Lt
End G.R. 23+29.5 15' Lt
Δ G.R 23+14 15' Lt
27+56 - 20" x 18" - 31' Rt
F. Ent.
Catch basin
27+35 W. Ft. pipe 10" X 10"
F. Cor. 40' Rt 27+20
Fence 38' Rt
Beg. of curb Rt 25+71
Fence 37' Rt
Fence 37' R.
End G.R. 23+48.5 - 15' Rt
Δ G.R. 23+32 - 15' Rt

5+a

35+00

34+00

33+00

32+00

31+00

30+00

Lt ℄ Rt

T.P. 28' Lt 35+55 ⌀

T.P. 29' Lt 34+39 ⌀

T.P. 29' Lt 32+97 ⌀

T.P. 29' Lt 31+65 ⌀

T.P. 28' Lt 30+39 ⌀

✓

End of curb 29+39.3

T.P. 27' Lt 29+13 ⌀

Sta

41+00

40+00

39+00

38+00

37+00

36+00

Lt ℄ Rt

T.R 28' Lt 40+78

C.M. pipe 25'X12"
21' Rt X Feed 40+68

T.R 28' Lt 39+40

T.R 28' Lt 38+13

T.R 28' Lt 36+83

Sta

47+00

46+00

45+00

44+00

43+00

42+00

G.R. - 4.

48 + 44 + 51 + 41

(≈ 97.)

Lt ℄ Rt

C.M.pipe 34'x18"
22'Lt 47+25

T.P. 28'Lt 27+03

T.P. 20'Lt 46+59

T.P. 28'Rt 46+24

T.P. 28'Lt 45+78

T.P. 28'Rt 44+91

T.P. 28'Lt 44+56

T.P. 28'Lt 43+31

T.P. 27'Rt 43+35

C.M.pipe 26'x12"
F.E.n.t. 42+42 22'R

T.P. 28'Lt 42+05

Sta

57+00

56+00

55+00

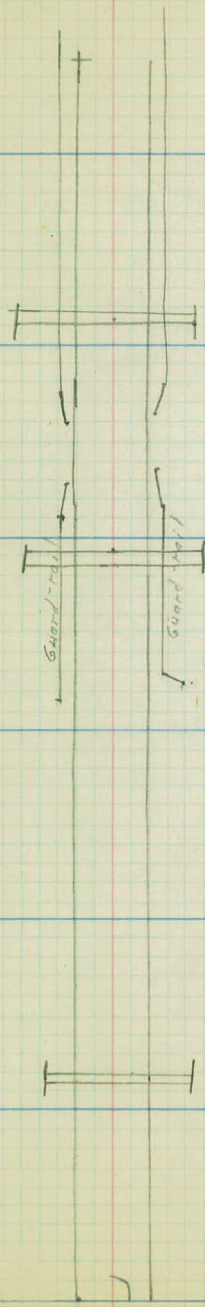
54+00

53+00

52+00

No new topography between
sta 48 and sta 52

Lt ℄ Rt



Conc culvert 24" X 48'
22' Rt 26' Lt 56+11

L G.R. 14.3 Lt 55+76
Beg. G.R 12' Lt 55+60

End of G.R. -12.5' Rt
55+28
L G.R. 55+12 -14.5 Lt

Beg. of G.R. 15' Rt
54+16

L.G.R. 14' Rt 55+79
Beg. G.R 11' Rt 55+63

End G.R. 13' Rt - 55+32

L G.R. 14.3 Rt - 55+16

Conc. culvert 24" X 48'
54+91 - 24' Lt 24' Rt.

L 54+29 - 14.5 Rt
Beg. G.R. 19' Rt
54+23

Conc. Culvert
24" X 40' - 52+19
22' Rt 18' Lt

Sta.

63+00

62+00

61+00

60+00

59+00

58+00

L ℄ R

T.P. 28' Lt 63+62

℄ G.R. 14.5' Rt 63+36
Beg G.R 19' R 63+29
C.M. pipe 18"x20'
63+15 - 25' Rt
Field-ent.

Guard-rail

Guard-rail

℄ G.R. - 14.5 L 63+03

Beg. G.R. 15.5' L. 62+86

F. Cor. 36' Rt 62+52

T.P. 29' Lt 62+14

F. Cor. 61+58 - 36' R.

T.P. 60+63 - 29' Lt

End G.R. 14.4 Lt 60+77

℄ G.R. 14' Lt 60+62

End G.R. 14.5 Rt 60+81

℄ G.R 14' Rt 60+65

Guard-rail

Guard-rail

Sta.

69+00

68+00

67+00

66+00

65+00

64+00

U.O

T.P. 28' R. 69+62

Beg. of curb 69+00
L G.R. 145 R 59+07
Beg of G.R. 15.5' L 68+90

T.P. 28' Lt 68+27

Beg. of curb 68+77
L G.R. 145' Rt 68+67
Beg. G.R 68+51 - 15.7' Rt

T.P. 28' Lt 66+65

T.P. 28' Lt 65+15

End G.R. 15' Lt 64+78
L G.R 64+63 - 14.4 Lt

End G.R. 15' Rt 64+80
L G.R 14.4 Rt 64+63

Sta.

75+00

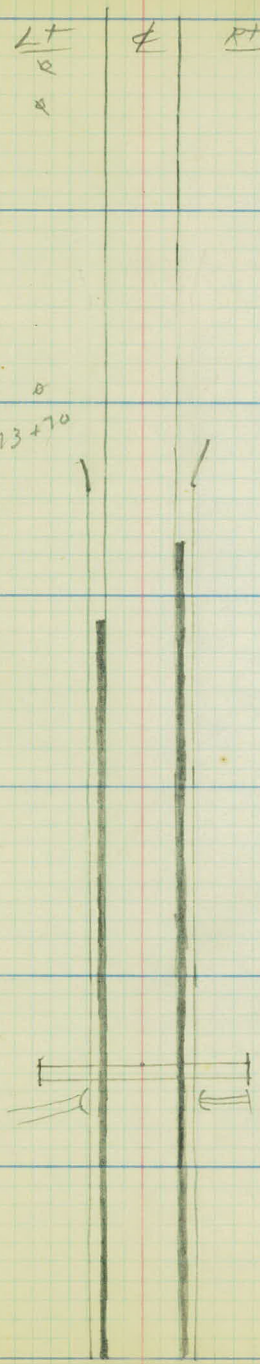
74+00

73+00

72+00

71+00

70+00


Lt
℄
Rt
III
T.P. 28' Lt 75+74
T.P. 28' Lt 75+56
T.P. 74+08 28' Lt
B
73+70
End G.R. 16' Lt 74+77
L.G.R. 14.5 Lt 73+55
End curb 72+85
Catch-basin 74+32
10' X 12" C.M. pipe
End. G.R. 16' Rt 74+77
73+07
L.G.R. 14.5 Rt 73+63
End curb 73+25
Conc. Culvert 24" RCP
28' Rt & Lt 70+54
Catch-basin 70+32
10' X 12" C.M. Pipe

Sta.

81+00

80+00

79+00

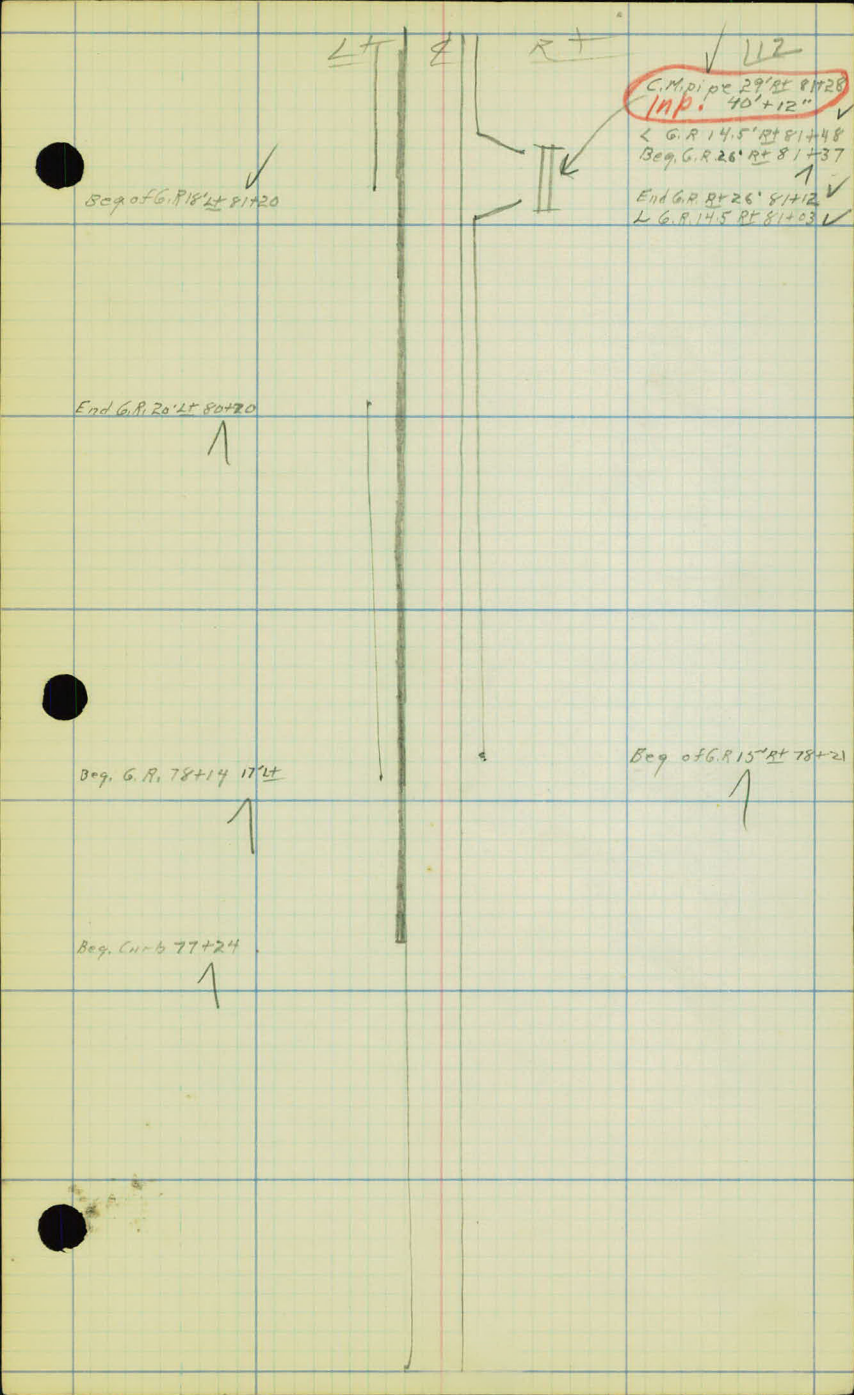
78+00

77+00

76+00

Curve - widths.

77+75		- 20'
78		- 20.5'
	+25	- 22.5'
	+50	- 24.3'
	+75	- 25.0'
79		- 25.2'
	+25	- 25.0
	+50	- 25.0
	+75	- 25.0
80		- 25.0
	+25	- 25.2
	+50	- 25.1
	+75	- 25.1
81		- 24.8
	+25	- 22.8
	+50	- 20.8
	+75	- 20.'


L+
℄
R+
12
C.M.pipe 29' Rt 81+28
Inp. 40'+12"
L G.R 14.5' Rt 81+48
Beg. G.R 26' Rt 81+37
End G.R Rt 26' 81+12
L G.R 14.5 Rt 81+03
Beg of G.R 18' Lt 81+20
End G.R. 20' Lt 80+20
Beg. G.R. 78+14 17' Lt
Beg of G.R 15' Rt 78+21
Beg. Curb 77+24

5+0

87+00

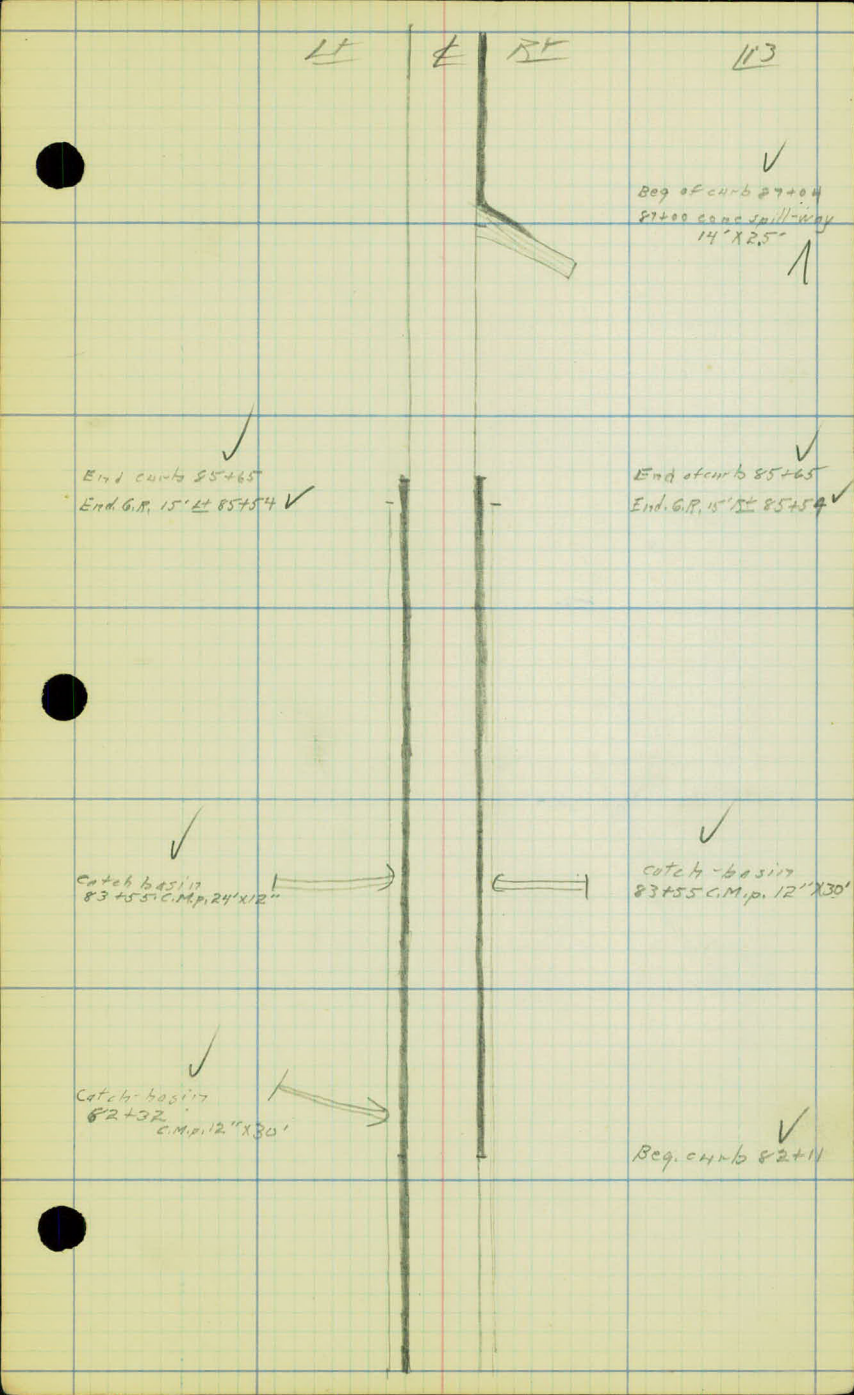
86+00

Curve - width

87	+50	20.1'
	+75	21.1'
88	+00	22.8'
	+25	23.6'
85+00	+50	23.6'
	+75	23.8'
89		23.8'
	+25	23.8'
	+50	23.6'
	+75	23.6'
90.		23.0
	+25	21.7
84+00	+50	20.4
	+75	20.0'

83+00

82+00


Lt
℄
Rt
113
Beg of curb 87+04
87+00 conc spill-way
14' X 2.5'
End curb 85+65
End G.R. 15' Lt 85+54
End of curb 85+65
End. G.R. 15' Rt 85+54
Catch basin
83+55 C.M.p. 24" X 12"
Catch basin
83+55 C.M.p. 12" X 30'
Catch basin
82+32
C.M.p. 12" X 30'
Beg. curb 82+11

STA

93+00

92+00

91+00

90+00

89+00

88+00

93+54 - 23' Lt
C.M.P. 18" X 12"
Field Inlet

End G.R 91+65

End curb 91+03

Beg G.R 15' Lt 88+70

Sta

100+00

99+00

Curve Widths

96+25	20'
+50	21.0'
+75	22.7'
97	23.6'
+25	23.6'
+50	23.6'
+75	23.8'
98	24.3'
+25	23.6'
+50	23.6'
+75	23.0'
99	21.8'
+25	20.3
+50	20.0'

98+00

97+00

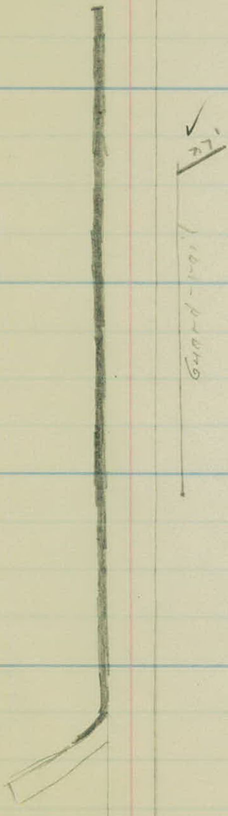
96+00

95+00

94+00

Lt ℄ Rt

99+46 End curb.



< G.R. 98+45

Beg. G.R. 96+93

95+71 Beg. curb
Conc. spillway
3'x12'

II

94+37 -26' Rt.
18'x12" C.M.P.

107+00

106+00

105+00

104+00

103+00

102+00

101+00

107+96.6
End of paving

✓
163+61 C.M.P. pipe
19'± 18"x12"
II

150
8
1200

Woodwood Road
County Road E.
from Co. Line to first Cross
of St Paul Suburban R.R.