PLANS SURVEY

PRESCOTT CONN.

From Prescott Wis.

To Minn. Trunk Highway No. 3

CO. PROJ. Nº 23-60

4-16-24

"4" (23-60)

Burris Str. Conn.-

23-60

Burris St. Connection (1)
Proj 23-60

X sections pages 1 — 3
Align Notes pages 5 — 6
s/Ketch/Map. page 4

Sta	+ HI	—	El.
BM	6.25	744.29	738.04
33		5.8	38.5
32		7.8	36.5
31		10.0	34.3
T.P.	7.30	741.78 9.81	734.48
30		8.1	33.7
29		12.9	28.9

RL RL

5.8	6.3	6.0	5.7	3.7	2.6	2.4	1.8
00	7.5	9.0	13.0	17.6	23.6	30	50

7.8	7.7	8.7	5.0	3.4
00	2.0	14.4	23.6	50

10.0	9.3	9.3	8.7	6.5	5.4	Poop	5.2
00	6.0	13.4/15	21.4	25.5	32.2	31	50

wall

8.1	7.6	8.4	8.4	8.1	7.8	7.9	7.3	5.7	4.9	3.7	3.0	2.6
00	8.0	10	18.4	20.2	28.5	32.5	39.7	44.0	48.6	49.06.00		70.0

12.9	12.7	11.0	11.5	11.5	11.1	9.8	6.7	4.3	1.8	Pump
00	1.0	24.3	27.0	31.5	31.5	44	60	70	90	70

741.78

2+76.6 PC		7.2	34.6
3+00		9.0	32.8
3+25		8.1	33.7
3+49? PT		6.7	35.1
T.P.	12.44 751.88	2.34	739.44
℄		12.6	39.3
4+20		10.5	41.4
5		4.7	47.2
5+16 =		3.2	48.9

PT other location
8+5~~2~~

Lt.

3

1.9 3.4 5.3 7.2 9.2 10.1
30 20 10 0.0 10 20

Rt.

2.9 4.8 9.0 9.5 10.5 11.2 12.4 13.3
25 10.0 6.0 14 16.7 21 23 38

1.5 5.5 7.9 8.1 8.6 9.3 10.7 12.1
30 20.5 11.6 6.0 11.0 19.6 25 33

(+0.4) 4.2 5.5 6.4 7.0 6.7 6.5 7.2 8.4 7.6 5.7
37 24 17.4 15.6 10 0.0 2.0 12.0 19 28 30

8" Elm

Copied

3 FP

70.60

0+00

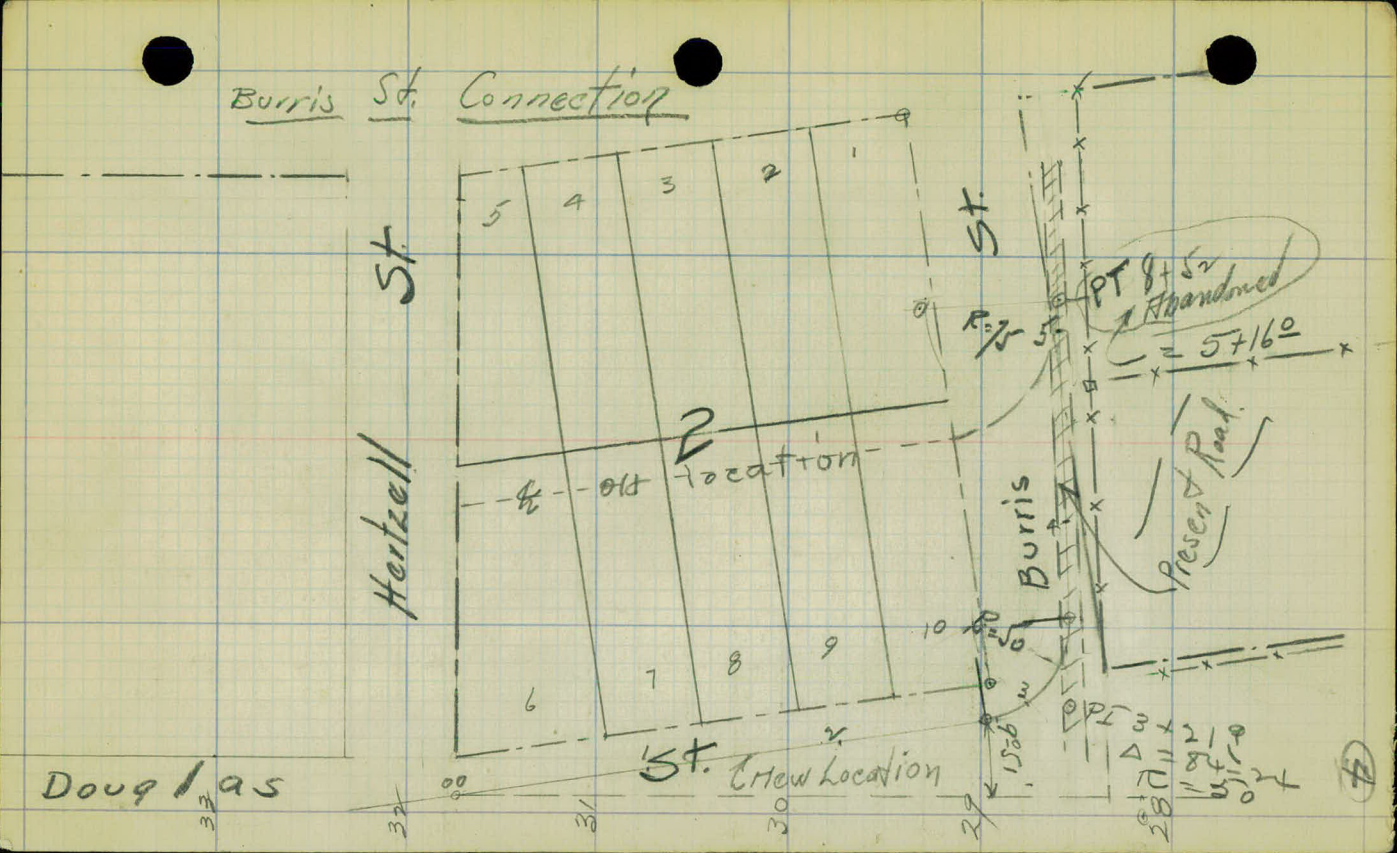
FP

16.35

PI

Copied

12" Elm.


Burris St. Connection
Hartzell St.
St.
PT 8+52
Abandoned
= 5+16.0
Present Road
Burris
Old location
New Location
Douglas
5
4
3
2
1
6
7
8
9
10
2

page 57

Sta Point Lt Δ Rt Calc.

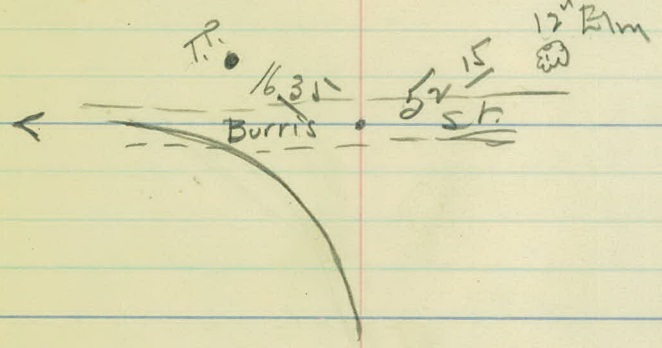
3+21.9 PI 84.24

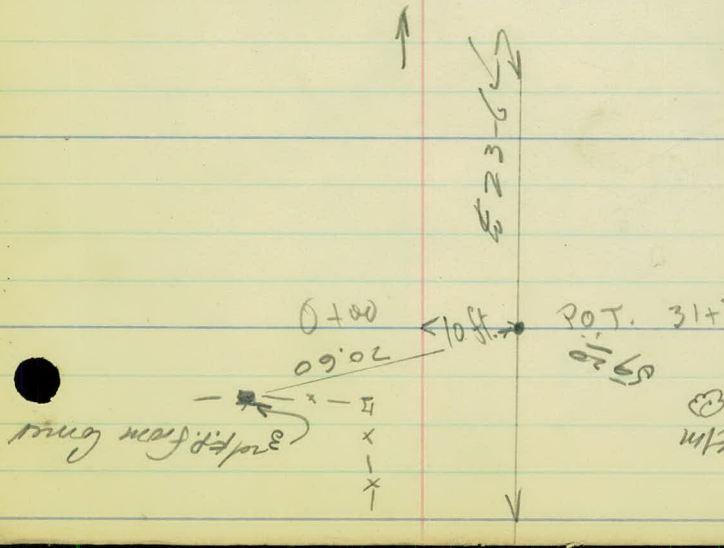
8+55 (?) T.T.
5+160

3+50.3 P.T.

3+45.0
3+00
2+166 PC

6+00 - 10ft. Rt. Beginning
31+73 POT


T.P.
16.31
Burris
12" Elm
15
5 ft.


0+00
70.60
10ft.
P.O.T. 31+73
8" Elm

General layout

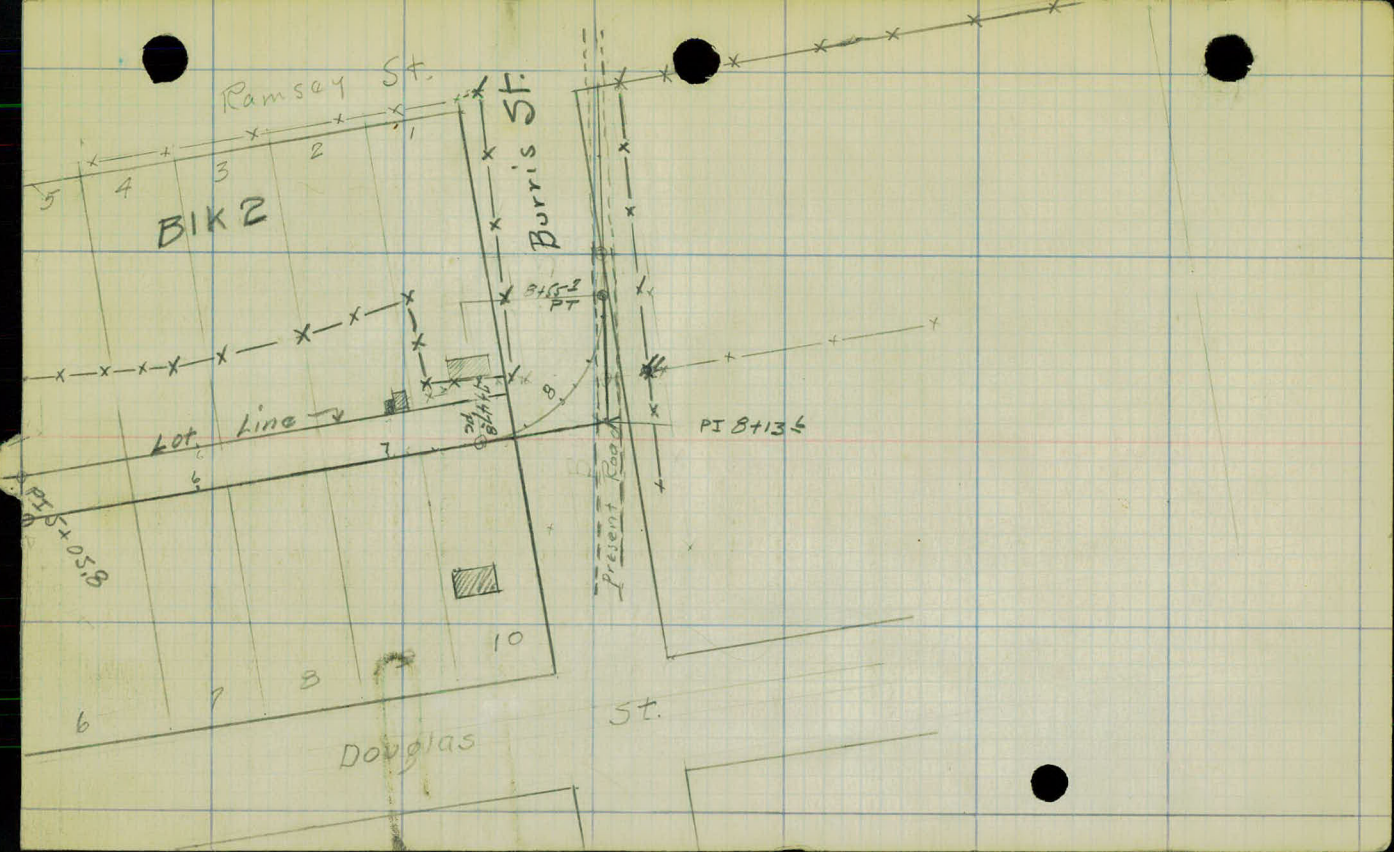
Borris St

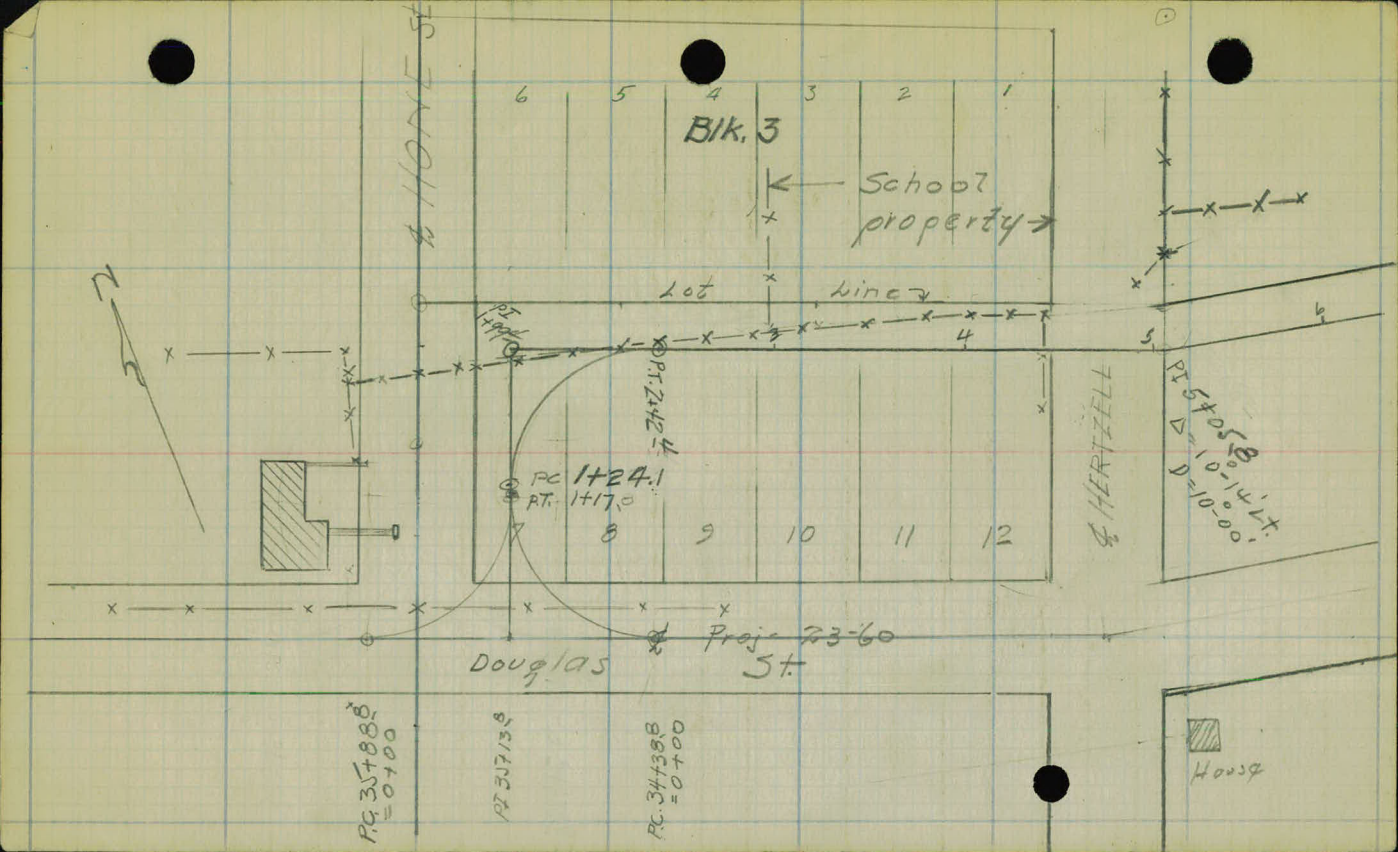
Connection

Proj - 23-60

FMC

Feb-1924


Ramsey St.
Burris St.
BLK 2
Lot Line
PI 8+13.6
Present Road
Douglas St.
1
2
3
4
5
6
7
8
9
10


Blk. 3
6
5
4
3
2
1
School property
Lot lines
4
5
8
9
10
11
12
PC 1+24.1
PT. 1+17.0
PT 1+24.4
HERTZELL
Douglas St.
Proj. 23-60
House
PC 3+88.8
=0+00
PT 3+13.8
PC 3+38.8
=0+00

Alignment Notes
Burris St.
Connection
Proj. - 23-60
FMC 7/11/24

Sta Point Lt. Δ Rt. Calc:

1+17.8 P.T.

1+00

+75

+50

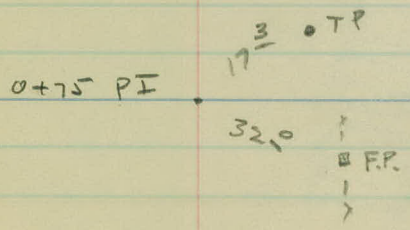
+25

0+00 P.C.

curve Rt

PI = 0+75
Δ = 90-00 Rt
T = 75.00
L = 117.8
R = 75.00

00


17 3/4
TP
0+75 PI
32,0
F.P.

Sta. Point Lt Δ Rt Calc

1+17.8 PC

curve Lt. 1+00

+75

+50

+25

0+00 PC 00

PI = 0+75.0
Δ = 90°-00' Lt
T = 75.01
L = 117.8
R = 75.0

Same PI as curve to Rt.

5+56.8 PT.

5

4+54.5 PC

2+42.4 PT

+25

2+00

+75

+50

1+24.4 PC

PI = 5+05.8

Δ = 10-14

T = 51.3

L = 102.3

D = 10-00 Lt

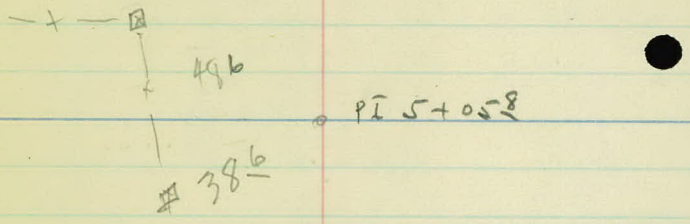
PI = 1+99.4

Δ = 90-12

T = 75.3

L = 118.5 ✓

R = 75'



16" oak.

PI 1+99.4

32.5

48.1

12" oak

28.0

12" oak

$8+39^{0} = 8+57.4$

$8+55.7$ PT

$+50$

$+25$

$8+80$

$+75$

450

$9+47.8$ PC.

$PI = 8+13.6$

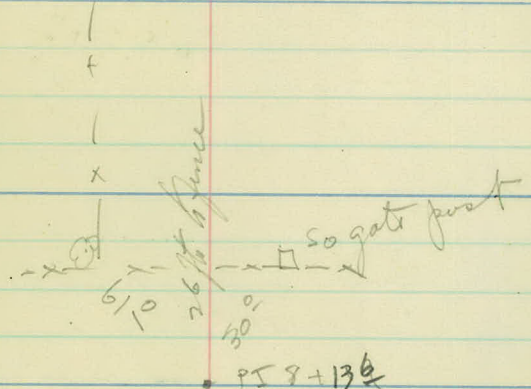
$\Delta = 82-30$

$T = 65.8$

$L = 107.9$

$R = 75^{0}$

9+47



Cross-sections
&
& levels
Burris St. Connection
Proj. 23-60

FMC 7/11/24

Sta	+	HI	−	El.	El
BM	5.30	743.34			738.04
T.P.	11.29	753.40	1.23		742.11
0+00 PC			12.3		41.10
0+25			11.0		42.4
0+75			10.0		43.4
1+00			8.3		45.1
0+00 PC			10.0		43.4
0+25			10,3		43.1
0+50			10.0		43.4
0+75			9.6		43.8
1+00			8.3		45.1

curve to Rt.

curve to Lt.

Spike in Cottonwood 45 ft. Rt Sta 30+30

12.1	12.3	11.0	10.5
25.0	00	12.6	30.0
11.1	11.0	10.0	
30.0	00	30.0	
10.4	10.0	9.5	
23.0	00	30	
8.3	8.3	8.7	
2	00	30.0	

8.0	9.0	10.0	9.8	10.5	9.7
30.0	18.0	00	15	19.4	30.0
8.3		10.3	10.7		
30.0		00	30.0		
8.4		10.0	10.8		
30		00	30.0		
7.6		9.6	10.4		
30.0		00	30.0		
7.2		8.3	8.3		
30.0		00	2.0		

Sta	+	HI	−	El.	El.
		753.40			
1+17.8 P.T.			7.2		46.2
1+50			3.9		49.5
T.P.	10.54	763.71	0.23		753.17
1+50					
1+75			11.1		52.6
2+00			9.6		54.1
B.M.	5.37	743.41	?		738.04
T.P.	11.51	754.33	0.59		742.82
2+42.4 P.T.			1.2		53.1
3+00			3.8		50.5
4+00			6.5		47.8
4+54.5 P.C.			7.5		46.8
5+00			8.2		46.1
5+56.8 P.T.			9.2		45.1
6+00			8.8		45.5

6.2	7.2		8.3
30.0	00		30.0
12.8	3.9		5.5
13.0	00		30.0
10.9			
30.0			
6.0	11.1	14.0	14.3
30.0	00	19.0	30.0
4.6	9.6	13.1	13.8
30.0	00	19	30.0

Spike in Cottonwood 45 ft Rt. Sta. 30+30

+4.0	+0.5	1.2	5.3
25.0	9.7	00	30.0
+0.7	2.3	3.8	7.0
25.0	12.0	00	30.0
4.0	5.0	6.5	8.7
31.0	26.6	00	30.0
4.9		7.5	9.0
30.0		00	30.0
6.1		8.2	10.0
30.0		00	30.0
6.8		9.2	7.1
30		00	30
7.0		8.8	11.0
30.0		00	30.0

Sta	+	HI	−	El.	El.
		754.33			
7+00			8.9		445.4
T.P.	3.82	751.02	7.13		747.20
7+47.8 PC			5.8		45.2
7+75			5.5		45.5
8+00			6.3		44.7
8+25			5.2		45.8
8+55.7 P.T			2.3		48.7
8+80			0.2		50.8
T.P.	1.09	748.29	3.82		747.20
B.M.			10.24		738.05
9+30				757.4	
10+20				765.7	
10+70				770.6	
10+80				771.7	
11+30				776.9	
11+80				783.4	
12+00				786.5	
12+30				789.5	
12+80				795.3	

Stations continue in center of road.

7.2	8.9	9.4
30.0	00	30.0
4.0	5.8	6.9
30.0	00	30.0
3.8	5.5	7.0
30.0	00	30.0

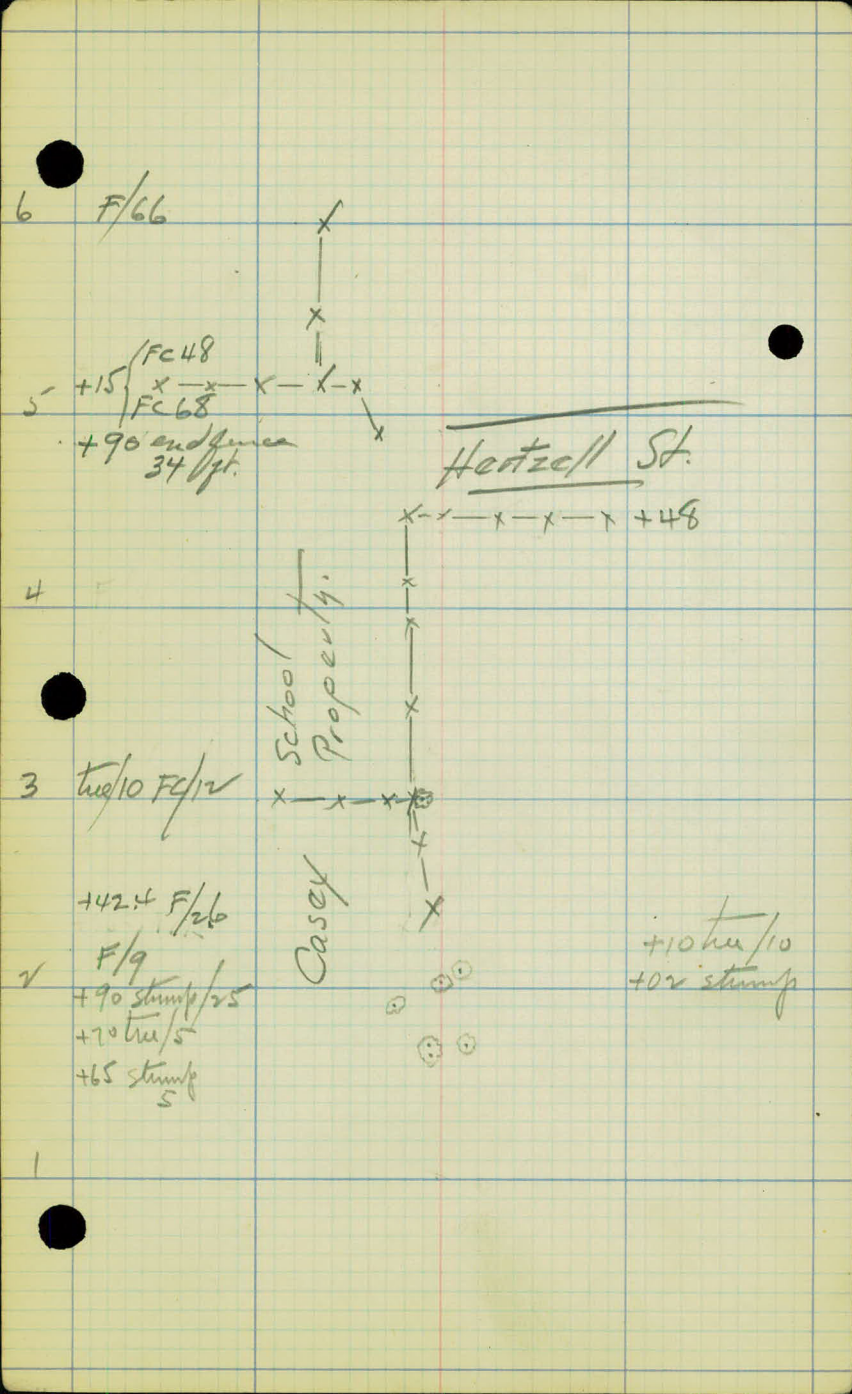
4.4	5.2	6.3	8.8
30.0	25.0	00	30.0

3.5	5.0	5.2	4.3
30.0	26.0	00	28.0

3.1	2.9	2.3	2.3
30.0	26.0	00	20

Spike in Cottonwood tree 45 ft Rt Sta 30+30

Art. Topog.
Burris St. connection
Proj. 23-60
F.M.C. 7/11/24


6
F/66
FC48
+15
FC68
+90 end fence
34 ft.
Hertzell St.
+48
4
School Property
3
tree/10 FC/12
+42.4 F/26
F/9
+90 stump/25
+70 tree/5
+65 stump
5
Casey
+10 tree/10
+02 stump
1

9

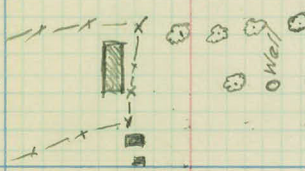
+55 F/49

+55 F/20

+25 F/28

8

+68 tree/24
+65 shed 36
+25 FC/365
+40 F/31 shed/365
+15 corncrib 27
+04 toilet-265



+68 tree/18-36-60
+46 tree 26 well 42
+53
+24 } house 63

7

6 F/66

Cross-Sections
Hartzell St
South of Proj-23-60
to R.R. tracks

F.M.C 7/6/24

Sta	+	HI	−	El.
B.M.		4.85	742.89	738.04
0+00 = 32+03.8				
0+25				
0+50				
0+80				
1+10				
1+50				
1+90				
2+21	C m & S & P R.R.			
2+40	C B & Q			

Note

Sta 32+03.8 Δ = 90°-00 Lt.

Hertzell St. (South)

Rod Readings

Lt (East)

Rt (west)

			7.0 30°		6.1 00	5.9 25°	6.3 30°		
			6.3 30	8.6 14°	8.4 00	8.2 10°	10.1 14.6	10.1 17°	5.7 24° 5.0 30°
wood pile	4.6 30°	6.6 27	10.6 21°	11.3 14°	11.0 00	12.1 6.0	11.5 11°	8.1 20°	6.4 3.0
wood pile		8.0 30	12.8 20°	12.7 14°	12.7 00	12.0 19°	11.9 30		
			13.6 30°	13.4 14°	13.3 00	14.4 30°			
			16.8 30°	13.8 13°	14.1 00	15.3 30°			
					14.2 08				
					13.2 00				

738.04 BM
4.00
742.04 = ±

742.0
729.2
12.8

12.8
5.2
7.6

31+73.5

23-60

Connection
Bridge - (Sta 0+71) to
Old Location - 23+60

Cross-sections
Sta 24-0+00
Proj 23-60

Sta	+	HI	−	El.
B.M.	7.80	712.94 ✓		705.14 ✓
23+96½ Pc.			4.1	708.8 ✓
23			3.8	09.1 ✓
22 ✓			4.3	08.6 ✓
21			4 ✓	08.7 ✓
20			4.1	08.8 ✓
19		✓	3.6	09.3 ✓
T.P.	4.06	713 5/9	3.41	709.53 ✓
18			4.4	09.2 ✓
17			5.7	07.9 ✓
16			4.5	09.1 ✓
15 ✓			4.6	09.0 ✓
14		✓	4.7	08.9 ✓
T.P.	5 11/19	714 29/41	4.41	709 18/41 ✓

Lt R+

Cottonwood line Rt Sta 20+80

Taken on Lt ft. snow

		4.7	7.9	7.3	4.5	4.1	4.3	10.1	12.5
		42	37	18.2	13	00	9	22	54
6	4.4	7.2	8.0	7.2	4.5	3.8	4.5	9.2	12.7
10	4.42	40	27	17	11	03	12	25	64

Soundings Shoved 4 Sta 24 — 11

4.7	7.6	7.5	4.8	4.3	5.1	7.9	10.3	
46	38	19	12	00	15	22	58	
3.9	7.2	8.2	4.7	4.2	4.2	7.2	10.1	
49	43	20	13	00	10	20	55	
4.7	6.8	8.2	7.6	4.8	4.1	4.4	7.6	10.5
48	42	30	19	11	00	11	21	52
4.0	7.8	8.6	8.2	5.1	3.6	4.5	8.7	11.6
52	44	25	21	15	00	12	25	59
4.7	8.4	9.0	8.6	5.0	4.2	4.4	4.6	8.6	12.6
55	50	36	27	20	9	00	3	15	50
5.0	8.8	9.5	9.2	5.1	4.4	5.7	10.1	13.5	
66	57	41	31	26	13	00	15	50	
5.3	8.4	8.7	8.6	5.0	4.5	4.9	8.6	7.0	
55	48	29	19	13	00	10	20	42	
4.2	9.6	8.6	7.2	3.2	4.6	4.3	5.0	8.6	10.2
50	39	21	10	4	00	8	14	27	48
5.6	10.4	10.1	4.0	4.1	4.2	4.8	7.6	10.0	
44	32	12	2	00	12	23	30	57	

Sta	+	HI	−	El.	El.
13		714.29 ✓	6.7	07.6 ✓	
12 ✓			7.5	06.8 ✓	
11			5.8	08.5 ✓	
10			4.9	09.4 ✓	
9		✓	5.2	09.1 ✓	✓
T.P.	8.39	712.80	9.88		704.41
8			3.7	09.1 ✓	
7			8.2	04.6 ✓	
6			10.2	04.6 ✓	
5			9.2	03.6 ✓	
4			4.0	08.8 ✓	
3			4.4	08.4 ✓	
2		✓	3.8	09.0 ✓	
	9.72	719.60	3.92		709.88 ✓
1			5.2	13.4 ✓	

Lt Rt

7.8 11.0 11.5 6.7 5.2 4.7 5.3 9.4 10.7
40 30 10 00 3 17 26 36 62

6.4 12.0 11.6 7.5 5.7 5.2 5.7 10.2 10.8
45 29 8 00 6 16 28 40 52

4.2 12.1 12.1 5.8 5.0 4.8 5.0 10.6 11.9
49 32 11 00 4 14 26 39 66

6.2 11.2 12.0 5.4 4.9 4.8 4.9 10.7 12.0
53 40 17 6 00 7 16 33 61

7.6 12.0 11.5 5.4 5.2 5.5 10.9 12.2
58 35 24 12 00 10 25 50

5.4 9.8 10.2 3.4 3.4 3.7 10.6 11.0
70 60 38 22 11 00 22 50

7.2 10.2 10.7 3.8 3.6 3.7 8.2 11.0 11.5
80 74 50 34 21 12 00 9 54

7.0 10.4 10.8 3.6 3.4 3.1 10.2 10.9 11.7
93 88 60 40 27 21 00 2 52

6.5 10.4 10.8 4.1 3.8 4.4 5.5 9.2 11.5 13.0
112 100 73 37 23 14 9 00 6 50

5.1 11.7 11.4 4.6 4.0 4.3 12.0 13.1
123 108 36 16 00 7 27 51

8.1 12.1 13.3 11.9 5.4 4.4 4.2 4.7 13.1 13.4
140 130 36 19 5 00 10 21 43 56

4.1 11.7 14.3 12.0 4.6 3.8 4.5 6.0 14.2 15.4
200 183 45 35 10 00 7 14 35 57

8.6 5.9 5.2 5.8 9.0 21.2 25.0
34 16 00 8 17 40 87

Sta

0+71 = Minn. End of bridge

-30		718.60 ✓	3.2	15.1 ✓
-130			1.5	17.1 ✓
		(712.80)		
TP	3.59	704.85 ✓	11.54	701.26 ✓
B.M.			5.61	699.24

1

Note 1+50 on Lt end of Rip Rap
10+50 " Rt "

} stubs on bridge

699 25 } spike in power pole 2 ft. above ground
} 200 Lt. sta 1+50

1.4	9.0	10.6
248	235	57
	95.8	94.2

Alignment & Distance
from
PI 25+69.2 to Prescott Bridge
Proj - 23-60

2/7/24
F.M.C.

Lt △ Rt.

25+69.2 PI 13-37 (13-44') Rt.

17+00 11°-30'

3+35 37°-30'

0+71 ± End of Bridge 7°-08'

Sta. 0+00 ↑

↓ Wisc. end of bridge

23-60

Town Road
at Sta. 142

Alignment for Town road

Sta. 141+97.3

Proj - 23-60

F.M.C. 2-5-24

+92.2	P.T.	43-50
+50		37-30
2		30-00
+50		22-30
1		15-00
+50		7-30
0+00	P.C.	0-0

185.48

P.I. = 1+85.3

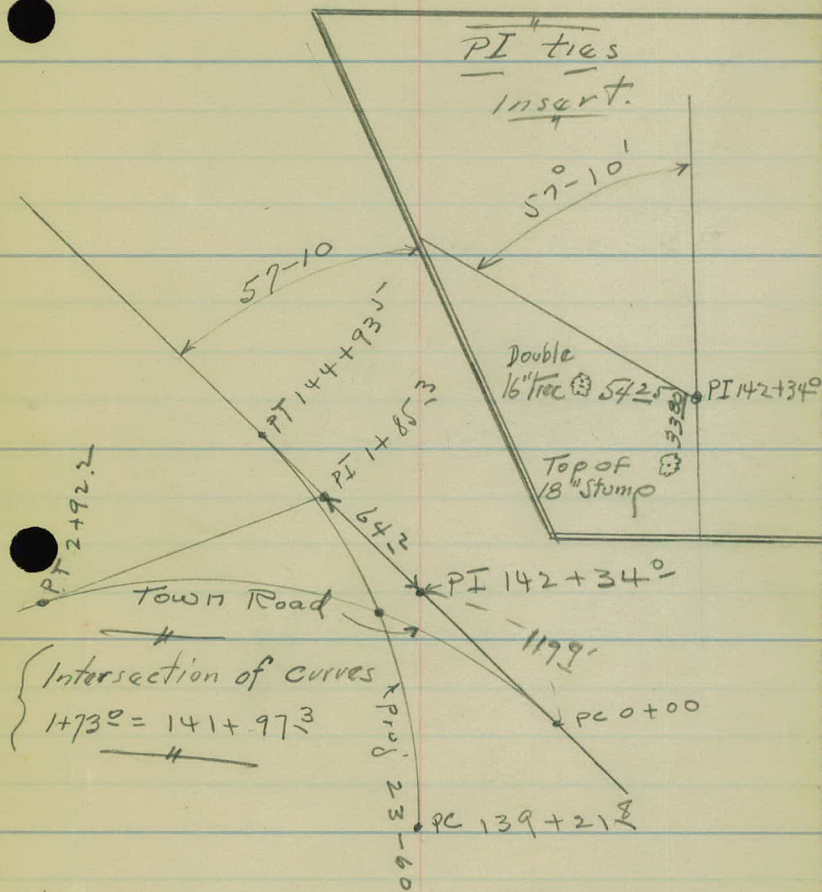
Δ = 87-40

D = 30-00 Lt.

T = 185.3 185.48

L = 292.2

R =



142+34.0
139+21.8
3 12.2 = T

Artifical Topog for Town road.
sta 141 + 97.3
Proj 23-60

FMC 2-5-54

P.T. 144+93
St Paul
144
143
Cut Wated
97°-40'
51°-10'
P.T. 2+92
To 17th Ave
142
Brush & Woods
P.I. 142+34
141
Cultivated
Prescott
140
Pasture
PC 0+00
Prescott
PC 139+
09-25 Rd

Cross-sections for Town road

Sta 141+97.3

Proj. 23-60

FMC 2-5-24

Sta	+	HI	-	Elev.	Elev.
BM.	11.55	896.39			884.84
TP	8.65	902.49	2.55		893.84
0+00			8.8	93.7	
0+50			11.3	91.2	
T.P.	2.21	893.42	11.28		891.21
1+00			6.1	87.3	
1+50			7.9	85.5	
2+00			11.3	82.1	
T.P.	7.06	889.91	10.57		882.85
2+50			11.1	78.8	
T.P.	2.46	882.37	10.00		879.91
2+92.2			6.7	75.7	
3+50			11.5	70.9	

Lt Rod Readings Rt

RR spike 24" oak 15' Lt Sta 142+24

7.1	6.7	9.2	8.8	8.8	8.1	5.8	5.5
33	28	22	15	00	13	18	33

9.7	11.3	12.0	12.0	11.3	11.3	10.9	8.7	8.4
33	19	15	10	7	00	21	27	33

3.8	5.0	6.1	5.9	3.8	3.3
33	1	00	10	16	31

5.5	6.6	7.9	8.2
33	20	00	31

12.8	11.7	12.3	11.3	10.9	8.9
33	15	12	00	51	33

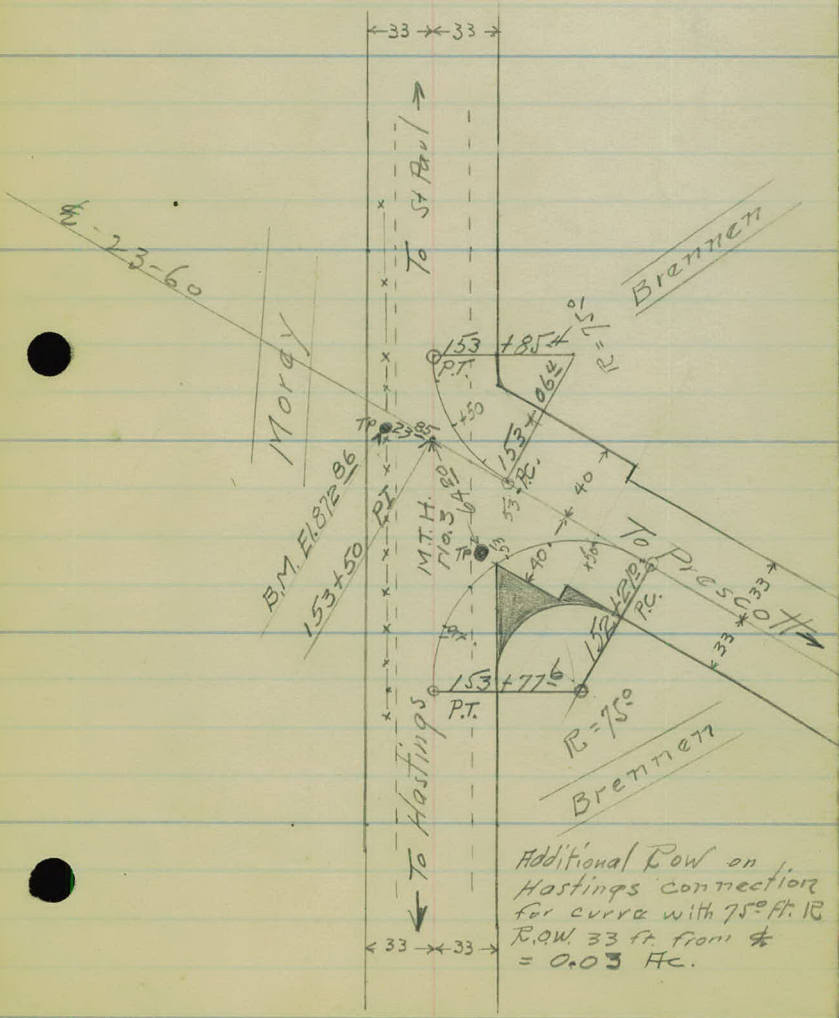
12.3	12.1	13.4	12.5	11.1	9.7	10.4	5.5
33	22	19	7	00	14	29	34

7.6	7.3	9.2	8.7	7.6	6.7	7.2	4.6	4.4
34	26	24	15	10	00	17	28	33

11.5
00

Alignment Notes
M.T.H. No. 3 Connection
Proj - 23-60
FMC 2/12/24

Sta	+	HI	−	Elev. Ft.
B.M.	9.60	882.46		872.86
		Lt.		
152+21 = P.C.			6.4	876.1
+50			8.1	874.4
+75			9.4	873.1
153+00			9.8	872.7
+25			14.0	868.5
+50			15.2	867.3
153+77.6 P.T.			15.6	866.9
		Rt.		
153+06.4 P.C.		882.46	6.3	876.2
+25			9.5	873.0
+50			11.0	871.5
153+85.4 P.T.			8.5	874.0


33 33
℄ 23-60
To St Paul
Mordy
Brennen
153+85
P.T.
R=75°
153+06
153+50
P.T.
B.M. El 872.86
TP 23.85
M.T.H. No. 5
TP 53
153+40
153+42
P.C.
To Proctor
33
153+77.6
P.T.
R=75°
Brennen
To Hastings
33 33
Additional R.O.W. on Hastings connection for curve with 75° ft. R. R.O.W. 33 ft. from ℄ = 0.03 Ac.

Cross-section Notes
M.T.H. No. 3 Connection
Proj-23-60
FMC 2/12/24

Sta Point Lt Δ Rt. Calc.

153 +85.4 P.T.

153 + 75

153 + 50

153 + 25

153 + 06.4 P.C.

PI = 153 + 50
Δ = 60° 20' Lt
T = 43.6
L = 79.0
R = 75.0

153 + 77.6 P.T.

153 + 50

153 + 25

153 + 00

152 + 75

152 + 50

152 + 21.0 P.C.

PI = 153 + 50
Δ = 119° 40' Lt
T = 129.04
L = 156.6
R = 75.0

R.R. Spike in T.P. 10 ft. Lt. of Sta. 153+75

8.6	6.4		3.0	
30.0	00		30.0	

El. 872.8

9.6	8.1		5.4
30.0	00		30.0
11.3	9.4		7.6
30.0	00		30.0
12.0	9.8	9.9	12.5
30.0	00	13.0	27.0

12.9	14.1	14.0	14.2
30.0	20.0	00	30.0
15.7	15.8	15.2	15.0
30.0	20.0	00	30.0
15.7		15.6	16.9
30.0		00	23

12.7	11.7	7.2	6.3	4.4
30.0	24.0	11.4	00	30.0
13.2	12.8	9.5	5.2	4.4
30.0	12.0	00	8.0	30.0

10.5	12.1	11.0	9.1	3.0	3.1
30.0	23.0	00	13.0	24.0	30.0
7.6	8.9	8.5	7.6	1.0	1.6
23.0	15.0	00	19.0	28.0	40

Revisions

23-60

Project 23-60

Change of line
Sta. 59+53 to 99+59
Transit Notes.
2-Pages.

R.E. Austin
A.N. Skooglan.
W. Maloney
M. Galvin.
} Party

12-18-23

℄ Fwg. ht. Fwg. Rt. Calc. Bearing

76+00 P.O.S.T

64+70 E.C. N 0°03' W

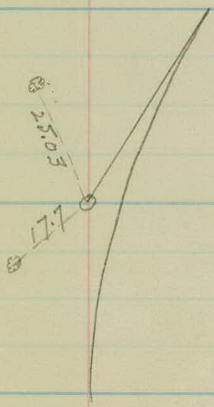
63+40 P.I 57°44'

61+81.3 T.C. N 58°15' W

61+50 P.O.T

59+53 P.O.T = B.C. 5° Curve. ht. Old line

Sta.	Def.
61+81.3	0°00'
62+00	1°52'
+50	6°52'
63+00	11°52'
+40	15°52' ⊙
+50	16°52'
64+00	21°52'
64+70	26°52'



20° Curve R
Δ = 57°44'
S.T. = 158.7
B.C. = 61+81.3
Length = 288.7
E.C. = 64+70

℄

Ang. ht. Ang Rt.

99+59.2 P.I. 7°54'

98+85 P.O.T.

95+74.8 P.O.T.

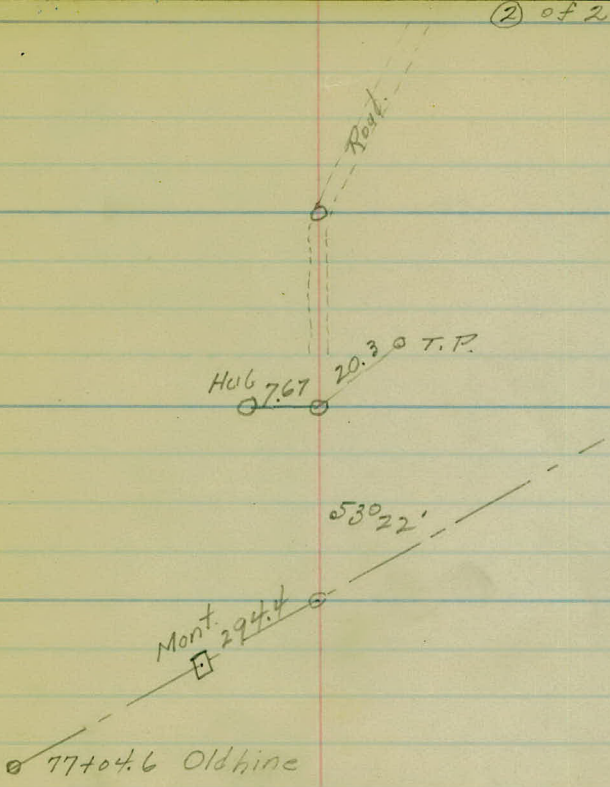
93+00 P.O.T.

N 53° 55' W

82+34.3 ✓ E.C.

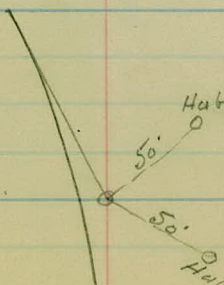
79+27.2 P.I. 53°24'

75+66.8 ✓ B.C.



Sta. - Def

75+66.8 - 0°00'
76+00 - 1°20'
77+00 - 5°20'
78+00 - 9°20'
79+00 - 13°20'
80+00 - 17°20'
81+00 - 21°20'
82+00 - 25°20'
+34.3 - 26°42'



8° Curve ht.

Δ = 53°24'
P.C. = 75+66.8
length = 667.5
E.C. 82+34.3
S.T. = 360.2?

360'

Project 23-60

Levels + X-sections
Line Change.
Sta. 59+53.2 To 99+59.2
5-Pages

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M. Galvin
} Party.

Station	+	HI	—	Rod	Elev.
B.M.	10.33	848.16			837.83
T.P.	8.33	856.38	0.11	848.05	
59+53				0.8	55.6
60+00				9.7	46.7
+13				12.8	43.6
T.P.	0.58	844.12	12.84	843.54	
+41				4.9	39.2
+56				10.3	33.8
T.P.	0.51	831.82	12.81	831.31	
+75				7.2	24.6
+98				10.9	20.9
61+00				10.9	20.9
+10				10.8	21.0
+16				6.0	25.8
+34				0.0	31.8
T.P.	12.53	843.93	0.42	831.40	
+50				10.9	33.0
62+00				8.0	35.9

LT

RT.

Spike in Oak 20' left Sta. 60+36

35.6	40.6	45.6	50.6	52.1	54.0	55.4	57.3	58.6	59.2	60.6	61.0
-20.0	-15.0	-10.0	-5.0	-3.5	-1.6	-0.2	+1.7	+3.0	+3.6	+5.0	+5.4
78.0	68.0	46.0	30.0	24.0	13.0	5.0	16.0	30.0	50.0	85.0	100.0

21.7	26.7	31.7	36.7	41.7	44.9	47.7	49.2	49.7	51.7	53.8
-25.0	-20.0	-15.0	-10.0	-5.0	-1.8	+1.0	+2.5	+3.0	+5.0	+7.1
75.0	71.0	57.0	46.0	30.0	20.0	15.0	30.0	50.0	75.0	100.0

-23.6	-28.6	33.6	38.6	42.2	45.5	47.1	48.6	48.9
-20.0	-15.0	-10.0	-5.0	-1.4	+1.9	+3.5	+5.0	+5.3
70.0	61.0	49.0	35.0	22.0	23.0	50.0	70.0	100.0

19.2	24.2	29.2	34.2	37.4	39.9	40.7	42.0	44.2	48.2
-20.0	-15.0	-10.0	-5.0	-1.8	+0.7	+1.5	+2.8	+5.0	+9.0
68.0	57.0	50.0	36.0	18.0	20.0	41.0	50.0	71.0	100.0

08.8	13.8	18.8	23.8	25.1	28.8	32.0	34.4	36.3	37.3	38.8	40.6	41.8	43.8
-25.0	-20.0	-15.0	-10.0	-8.7	-5.0	-1.8	+0.6	+2.5	+3.5	+5.0	+6.8	+8.0	+10.0
74.0	67.0	60.0	53.0	50.0	37.0	23.0	8.0	16.0	24.0	31.0	50.0	70.0	85.0

08.6	16.6	16.8	19.6	22.6	27.7	29.6	33.4	34.6	36.8	39.6	40.9	43.1
-16.0	-8.0	-7.8	-5.0	-2.0	+3.1	+5.0	+8.8	+10.0	+12.2	+15	+16.3	+18.5
56.0	54.0	50.0	30.0	17.0	13.0	21.0	31.0	40.0	50.0	70.0	75.0	100.0

20.9	23.8	25.2	25.9	28.2	21.2	22.0	24.9	25.9	28.9	34.4	35.9	39.1
0.0	+2.9	+4.3	+5.0	+7.3	+0.3	+1.1	+4.0	+5.0	+8.0	+13.5	+15.0	+18.2
65.0	50.0	42.0	35.0	6.0	3.0	10.0	16.0	23.0	47.5	76.0	87.0	100.0

27.0	26.2	26.4	27.7	26.0	21.6	26.0	28.0	31.0	34.8
+6.0	+5.2	+5.0	+6.7	+5.0	+0.6	+5.0	+7.0	+10.0	+13.8
71.0	50.0	45.0	23.0	10.0	15.0	36.0	50.0	75.0	100.0

28.1	28.8	27.8	28.4	21.6	22.0	23.8	26.8	26.8	29.8	30.8	35.8
+2.3	+3.0	+2.0	+2.6	-4.2	-3.8	-2.0	+1.0	+1.0	+4.0	+5.0	+10.0
17.0	50.0	33.0	14.0	8.0	24.0	40.0	42.0	50.0	73.0	82.0	111.0

168	19.8	21.3	29.8	28.3	28.1	27.3	30.8	36.3
-15.0	-12.0	-0.5	-2.0	-8.5	-3.7	-4.5	-1.0	+4.5
75.0	50.0	22.0	16.0	46.0	84.0	100.0	111.0	136.0

38.0	35.0	34.1	33.0	34.3						
Root of Tree	10' RT Sta 61+			30	33.7	35.5	35.6	36.3	33.5	
+5.0	+2.0	+1.1	0.0	+1.3	+0.7	+2.5	+1.6	+3.9	+0.5	
70.0	50.0	49.0	24.0	38.0	50.0	71.0	100.0	117.0	142.0	

38.9	39.5	38.1	35.7	37.9	39.9	40.9	43.8	44.9	44.9
+5.0	+3.6	+1.2	-0.2	+2.0	+4.0	+5.0	+7.9	+9.0	+9.0
76.0	67.0	50.0	18.0	25.0	50.0	64.0	100.0	125.0	150.0

Station	+	H I	−	Rod.	Elev.
		843.93			
62 +40				4.2	39.7
+50				1.8	42.1
T. P.	12.59	856.19	0.33	843.60	
+70				8.0	48.2
63 +00				0.4	55.8
T. P.	11.55	867.68	0.06	856.13	
+40				3.9	63.8
T. P.	6.52	874.08	0.12	867.56	
64 +00				4.6	69.5
65 +00				8.2	65.9
+54				10.9	63.2
66 +00				9.5	64.6
+50				9.0	65.1
67 +00				6.4	67.7
68 +00				2.1	72.0
T. P.	4.55	877.20	1.43	872.65	
69 +00				4.3	72.9

4 2 4

35.8	37.1	39.5	45.1	47.1	50.5	51.1	48.9	49.1	49.5
-6.3	-5.0	-2.6	+3.0	+5.0	+8.4	+9.0	+6.8	+7.0	+7.4
75.0	50.0	25.0	5.0	25.0	50.0	66.0	100.0	132.0	150.0

50.3	50.8	54.2	57.8	59.8	58.3	55.8	57.8	50.8	50.2
-5.5	-5.0	-1.6	+2.0	+3.0	+2.5	0.0	-4.0	-5.0	-5.6
75.0	46.0	16.0	16.0	41.0	50.0	82.0	100.0	114.0	150.0

60.3	61.8	64.0	65.1	63.5	62.3	62.6	59.1	58.8	55.8	55.3
-3.5	-2.0	-1.8	+1.3	+1.7	+1.5	-1.2	-4.7	-5.0	-8.0	-8.5
71.0	50.0	31.0	19.0	39.0	50.0	75.0	100.0	100.0	122.0	150.0

70.5	70.1	68.9	67.9	64.5	62.2	59.5	52.7
+1.0	+0.6	-0.6	-1.6	-5.0	-7.3	-10.0	-12.8
50.0	26.0	30.0	50.0	85.0	100.0	120.0	150.0

70.0	68.7	64.4	60.9	55.9	50.9	
+4.1	+2.8	-1.5	-5.0	-10.0	-15.0	
38.0	24.0	16.0	57.0	119.0	181.0	

67.6	65.1	61.9	59.8	58.2	56.4	54.4	53.2
+4.1	+1.9	-1.3	-3.4	-5.0	-6.8	-8.8	-10.0
38.0	18.0	36.0	50.0	70.0	100.0	150.0	190.0

68.3	67.1	60.7	60.6	61.6	64.3	
+4.7	+2.5	-3.9	-4.0	-3.0	-0.3	
39.0	18.0	41.0	50.0	100.0	150.0	

(60.9)	63.3	64.8	65.1	68.1	70.1		
-4.2	-1.8	-0.3	0.0	+3.0	+5.0		
38.0	16.0	21.0	50.0	100.0	125.0		

69.2	68.2	69.2	69.9	71.9	72.7	73.8	
+1.5	+0.5	+1.5	+2.2	+4.2	+5.0	+6.1	
37.0	20.0	29.0	50.0	100.0	117.0	150.0	

72.5	72.5	72.9	73.3
+0.5	+0.5	+0.9	+1.3
37.0	20.0	50.0	100.0

74.1	73.8	72.9	73.9
+1.2	+0.9	0.0	+0.1
36.0	18.0	50.0	100.0

Station	+	H.I.	—	Rod.	Elev.
		877.20 ✓			
70 + 00				7.5	69.7
71 + 00				5.5	71.7
+ 50				5.0	72.2
72 + 00				5.8	71.4
+ 50				6.1	71.1
B.M.	9.31	884.51	2.00	875.20	
73 + 00				11.4	73.1
74 + 00				7.9	76.6
75 + 00				5.6	78.9
76 + 00				2.0	82.5
+ 50				2.0	82.5
77 + 00				4.2	80.3
+ 50				6.2	78.3
78 + 00				4.6	77.9
T.P.	4.30	882.99	5.82	878.69	

Rt.	71.4	70.6	69.3	69.3 Rt.
	+1.7	+0.9	-0.4	-0.4
	35.0	17.0	50.0	100.0

72.7	72.5	71.2	69.7
+1.0	+0.8	-0.5	-2.0
35.0	20.0	50.0	100.0

74.9	73.6	67.0	66.4	64.8
+3.5	+2.2	-4.4	-5.0	-4.6
35.0	16.0	50.0	76.0	100.0

75.4	73.9	67.1	67.1	66.8
+4.3	+2.8	-4.0	-4.0	-4.3
33.0	19.0	46.0	50.0	100.0

Nail in 16" Elm 33 [illegible] 72 x 6.5

75.9	74.9	69.0	68.1
+2.8	+1.8	-4.1	-5.0
33.0	19.0	50.0	70.0

77.6	77.4	76.6	75.6
+1.0	+0.8	-0.0	-1.0
33.0	17.0	50.0	100.0

79.5	79.5	79.1	79.2
+0.6	+0.6	+0.2	+0.3
33.0	15.0	50.0	100.0

+0.4	+0.3	-0.4	-1.3
33.0	17.0	50.0	100.0

0.0	+1.0	+1.2	-2.8	-4.6
100.0	50.0	23.0	50.0	100.0
			-2	
+3.2	+2.2	+1.7	-2.5	
100.0	50.0	19.0	50.0	

+3.6	+1.0	-1.0
100.0	50.0	50.0

Station	+	H.I.	—	Rod.	Elev.
		882.99			
79+00				5.3	77.7
80+00				5.1	76.9
81+00				4.6	78.4
82+00				4.6	78.4
83+00				4.8	78.2
84+00				3.9	79.1
T.P.	8.99	888.93	3.05	879.94	
85+00				8.6	80.1
86+00				7.9	81.0
87+00				6.0	82.9
88+00				3.9	85.0
89+00				1.9	87.0
90+00				0.4	88.5
T.P.	12.57	900.96	0.54	888.39	
91+00				7.5	93.5

LH	RH
+7.2/200.0 +5.0/144.0 +4.0/150.0 +2.0/100.0 +0.2/30.0	+1.1/50.0
+1.0/100.0 +0.6/100.0	+0.4/50.0
+1.0/100.0 +0.3/50.0	+0.5/50.0
+1.3/100.0 0.0/50.0	+1.0/50.0
+3.8/200.0 +2.2/150.0 +1.1/100.0 +1.0/50.0	+0.9/50.0
+0.6/100.0 0.0/50.0	+1.8/50.0
+0.5/100.0 +0.2/50.0	+1.7/50.0
+1.7/200.0 +0.8/150.0 +0.2/100.0 0.0/50.0	+1.6/50.0
0.0/100.0 +0.2/50.0	+1.0/30.0 +1.9/50.0
-1.0/100.0 -0.5/50.0 +0.2/32.0	+1.8/50.0
-0.7/100.0 -0.6/50.0 -0.4/30.0	+0.5/23.0 +1.5/50.0
-1.5/200.0 -1.0/150.0 -1.0/100.0 -0.4/50.0	+2.3/33.0 +3.5/50.0
-4.2/30.0 -1.7/50.0	+0.2/25.0 +0.7/50.0

Station	+	H.I.	−	Rod.	Elev.
		900.96			
92+00				4.3	96.7
93+00				2.2	98.6
T.P.	5.10	903.75	2.31	898.65	
94+00				5.2	98.6
95+00				8.1	95.7
96+00				8.3	95.5
B.M.				7.20	896.55
97+00				6.8	97.0
+25				6.1	97.7
98+00				2.1	901.7
T.P.	10.75	912.73	1.77	901.98	
99+00				7.3	905.4
+59.2				5.9	906.8

Lt. Rt.

-2.1 / 100.0 -1.0 / 50.0 +1.3 / 50.0

-4.5 / 200.0 -1.1 / 150.0 -0.3 / 100.0 +0.2 / 50.0 +1.1 / 50.0

-1.1 / 100.0 0.0 / 50.0 +1.0 / 50.0

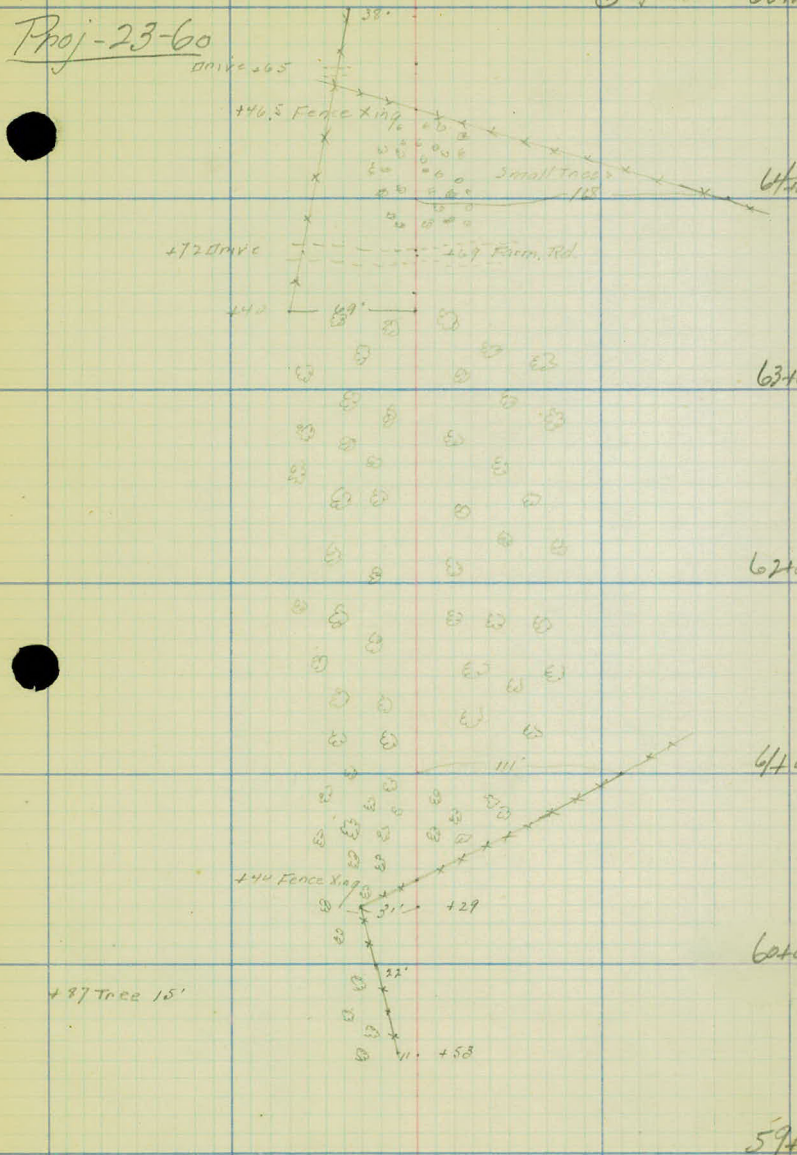
℄ Road → -0.3 / 78.0 +0.5 / 49.0 +1.0 / 50.0

Nail in Cor. Fence Post Rt. Sta. 95+60

Check-levels

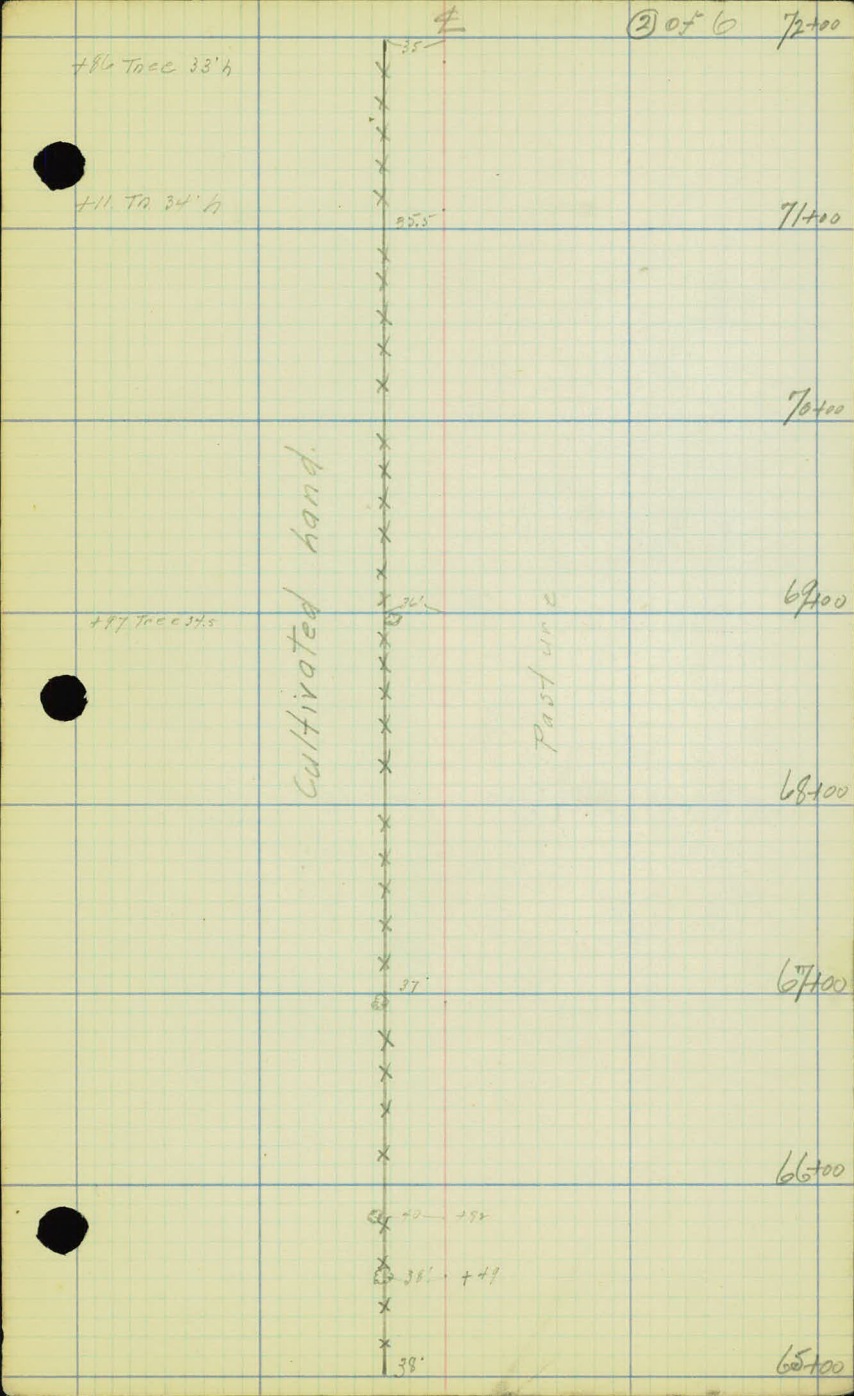
	+	H.I	−	Rod	Elev	
H.I		912.73				
T.P.	0.34	900.60	12.47	900.26		
T.P.	0.99	891.27	10.32	890.28		
T.P.	3.49	889.05	5.91	885.56		
T.P.	1.44	886.00	4.69	884.56		
T.P.	1.77	881.73	6.04	879.96		
B.M.			5.71	876.02		Spike in Elm 30' Rt. St. 72+25

Proj-23-60

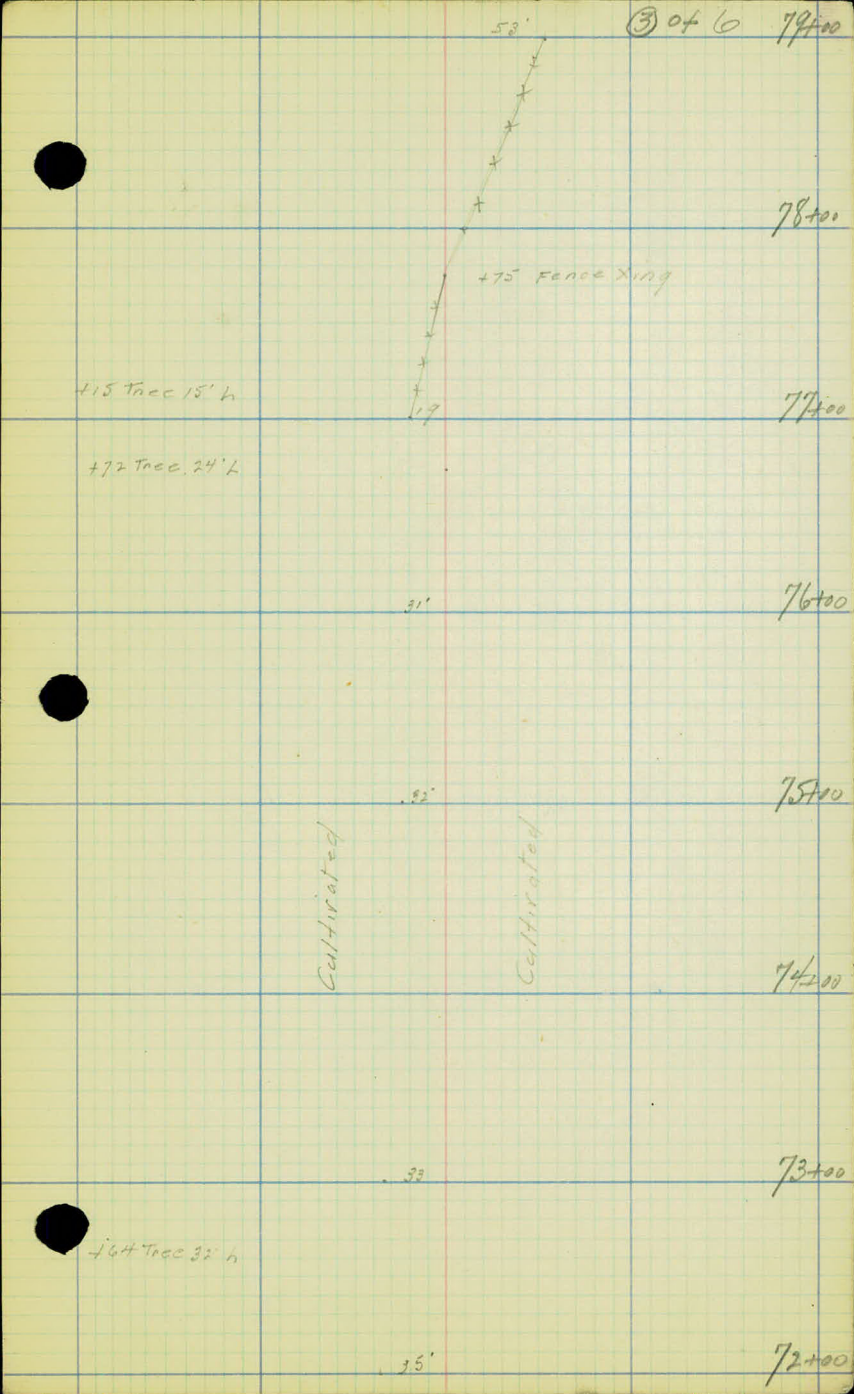

65+00
64+00
63+00
62+00
61+00
60+00
59+00
38'
Drive
+46.5 Fence Xing
Small Trees
18'
+72 Drive
Farm Rd.
+44
69'
111'
+40 Fence Xing
31'
+29
22'
+87 Tree 15'
11'
+58

(2)

Proj - 23-60


4
(2) 05° 6
72+00
+86 Tree 33' h
+11 Tree 34' h
35
35.5
71+00
70+00
Cultivated land.
Past ure
69+00
+97 Tree 34.5
34'
68+00
37'
67+00
66+00
40
+82
38' + 49
38'
65+00

(3)
Proj. 23-60


3 of 6
79+00
58'
78+00
+75' Fence Xing
+15 Tree 15' L
77+00
67
+72 Tree 24' L
76+00
31'
75+00
82'
Cultivated
Cultivated
74+00
73+00
33
+64 Tree 32' L
35'
72+00

4

Proj. -23-60

(4) of 6

86+00

85+00

84+00

92'

+85 Fence Xing

83+00

41'

82+00

81+00

80+00

79+00

5
Proj-23-60

(5) of 6

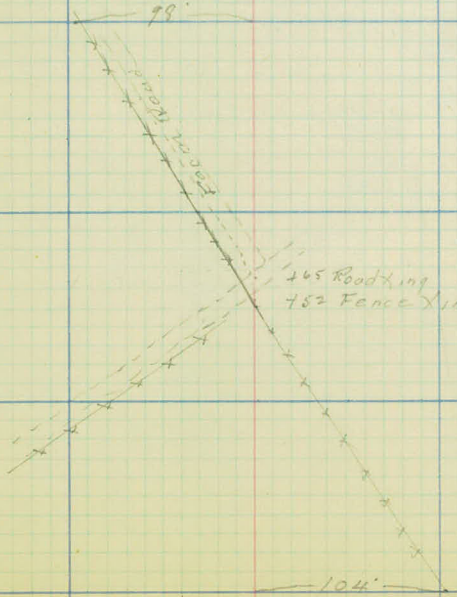
93+00

92+00

91+00

90+00

89+00



88+00

87+00

86+00

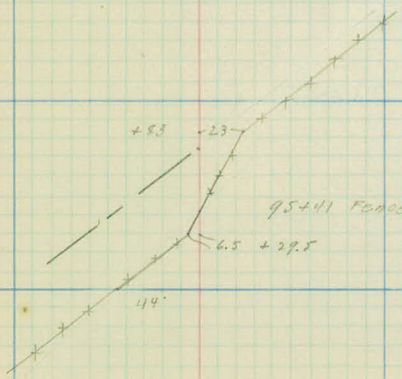
Proj - 23-60

99+00

98+00

97+00

96+00



95+00

94+00

93+00

Proj No 23-60

Change of line
Sta. 68+32 to 118+79.6
X-Sections + Level Notes
5 Pages
10/1/23

R.E. Austin
D. Stooglin
W. Maloney
M. Galvin
} Party.

Station	+	H.I	−	Rod	Elev.
B.M	3.00	879.03			876.03
68+32				8.0	71.0
+80				7.7	71.3
69+00				10.9	68.1
+50				10.4	68.6
70+00				9.7	69.3
+40				9.0	70.4
+72				6.4	72.6
+78				4.9	74.1
71+00				4.2	74.8
72+00				2.1	76.9
T.P	5.91	881.84	3.00	876.03	
73+00				4.6	77.2
74				5.1	76.7
75				5.3	76.5
76				5.7	76.1
77				6.1	75.7
79				8.0	73.6
T.P	6.12	882.99	4.97	876.87	
+40				9.6	73.4
79				6.9	76.1
B.M.				11.00	871.99
+31				5.2	77.6
+40				7.7	75.3
+50				5.7	77.3
80+00				6.6	76.4
81				5.5	77.5
82				4.3	78.7

Sp. in Blk. Elm 30' Rt. Sta 12+25

-4.7	-4.6	-1.5	-0.8	+0.2					+0.8		
38.0	27.0	24.0	17.0	12.0					33.0		
		-4.0	-3.5						+1.5		
		33.0	17.0						33.0		
		-0.5	-0.5					+3.9	+4.8		
		33.0	7.0					11.0	33.0		
	+4.6	+4.0	0.0			0.0	0.0	+3.4	+4.0		
℄ Rd	33.0	20.0	10.0			9.0	17.0	28.0	33.0		
+5.0	+5.0	+4.0	+0.3			+1.0	0.0	+2.3	+4.0		
33.0	23.0	18.0	11.0			10.0	30.0	33.0	39.0		
+5.0	+4.4	+0.5				+1.2	+1.4	+1.0	+1.7		
33.0	15.0	6.0				9.0	15.0	26.0	33.0		
+3.0	+2.2	+2.1				-0.6	+0.2	0.0			
33.0	19.0	7.0				9.0	17.0	33.0			
	+1.5	+1.2				0.0	-1.9	-1.5	-1.0		
	33.0	9.0				4.0	9.0	15.0	33.0		
	+1.8	+1.0				-0.5	-2.4	-1.9	-1.0		
	33.0	8.0				8.0	10.0	18.0	38.0		
	-0.2	-0.5				-1.1	-2.9	-2.3			
	33.0	20.0				24.0	27.0	33.0			

	-0.1	-1.0				+0.1	-0.5	-0.7			
	33.0	18.0				18.0	29.0	33.0			
	+0.1	+0.1				+0.1	+0.2				
	33.0	21.0				17.0	33.0				
	0.0	+0.2				+0.2	+0.3				
	33.0	19.0				18.0	33.0				
	-0.1	-0.1				+0.2	+0.2				
	33.0	16.0				18.0	33.0				
℄ Lane	+0.2	+0.1				+0.3	+0.4				
	33.0	18.0				19.0	33.0				
	0.0	-0.6				+0.1	+0.5				
	33.0	18.0				18.0	33.0				

	-1.1	-0.8				+0.7	+0.7				
	33.0	20.0				20.0	33.0				
	-1.5	-0.6				+0.2	0.0				
	33.0	17.0				15.0	33.0				
Nail in 24" tree 65' Rt. Sta 99+50											
	-6.1	-4.8	-2.9	-1.1			+0.1	-0.1			
	30.0	33.0	24.0	14.0			15.0	33.0			
	+0.1	+0.5	-0.2				+1.4	+1.7			
	33.0	28.0	14.0				13.0	33.0			
	-1.6	-0.9					0.0	0.0			
	33.0	23.0					17.0	33.0			
-1.0	-0.4	0.0					+0.4	+0.8			
33.0	29.0	21.0					17.0	33.0			
	-0.4	-0.5					+0.1	+0.6			
	33.0	27.0					21.0	33.0			
	-0.2	-0.2					+0.2	+0.2			
	33.0	22.0					19.0	33.0			

Station	+	H.I.	—	Rod	Elev.
		982.99 ✓			
83+00				5.8	77.2 ✓
+50				7.2	75.8 ✓
84				11.8	71.2 ✓
+25				11.1	71.9 ✓
+50				9.8	73.2 ✓
T.P.	8.99	884.76 ✓	7.22	875.77 ✓	
85+00				9.9	74.9 ✓
+70				6.4	78.4 ✓
86+00				6.4	78.4 ✓
+50				7.1	77.7 ✓
87+00				5.6	77.0
+94				11.0	73.8
95+00				9.6	75.2
+50				5.2	79.6
97				5.0	79.8
+50				4.4	80.4
90+00				3.9	80.9
+30				2.5	82.3
T.P.	1.3	884.41 ✓	1.72	883.02 ✓	
91+00				5.5	78.9
92+00				5.0	79.4
B.M.				5.57	(878.84) ✓
+60				9.5	74.9
93+00				7.1	77.3
+25				6.0	78.0
+50				7.3	77.1

Sec Connor's Loc.

Lt

		-2.5	-1.0	+1.0	+1.4
		33.0	28.0	25.0	33.0
	-2.8	-1.4	-1.4	+1.3	+1.8
	33.0	26.0	18.0	23.0	33.0
-7.4	-7.3	-3.4	-1.0	+2.6	+4.0
33.0	30.0	26.0	14.0	13.0	33.0
-23.3	-13.8	-9.5	-8.0 -5.8	-2.8	+2.7 +4.5
70.0	50.0	33.0	27.0 25.0	14.0	16.0 33.0
-19.1	-15.1	-12.7	-9.6 -8.0	-5.8 -4.4	+2.7 +4.0
61.0	50.0	45.0	33.0 30.0	25.0 13.0	17.0 33.0
	-9.0	-4.6	-2.8	-1.0	+2.6 +3.9
	50.0	33.0	24.0	17.0	22.0 33.0
	-3.4	-2.1	-1.2	+0.1	+0.8 +1.0
	50.0	33.0	22.0	15.0	20.0 33.0
	-6.2	-3.8	-2.0	-0.6	+1.2 +1.6
	50.0	33.0	19.0	14.0	21.0 33.0
	-6.4	-3.6	-2.1	-0.7	+0.8 +1.9
	50.0	28.0	16.0	12.0	18.0 33.0
-12.7	-9.5	-7.3	-5.1	-3.1	+1.3 +3.3
60.0	50.0	42.0	32.0	18.0	14.0 33.0
	-7.0	-5.7	-3.6	-1.0 -0.4	+0.3 +1.5
	50.0	33.0	22.0	17.3 10.0	16.0 33.0
	-5.0	-2.9	-0.2	+0.7	+1.5
	50.0	33.0	18.0	10.0	33.0
		-5.0	-3.1	-0.5	+1.8
		45.0	31.0	18.0	27.0
		-5.0	-2.5	-1.3	+1.5
		48.0	38.0	26.0	33.0
		-5.0	-2.4	-0.6	+1.1
		67.0	50.0	33.0	33.0
	-5.0	-3.0	-1.5	-0.9	-1.1 -1.3
	64.0	50.0	33.0	13.0	26.0 33.0
+10.0	-5.0	-4.5	-2.1	-0.3	+1.0 +2.5 +2.6
78.0	54.0	50	33.0	16.0	15.0 28.0 33.0
-10.0	-8.0	-5.0	-2.0	-0.9	+0.6
99.0	72.0	76.0	50.0	38.0	32.0
Nail 20° Chk 46 Rt 92+30					
	-5.0	-3.0	-1.6	-0.9	+1.5 +2.4 +2.5
	74.0	50.0	33.0	12.0	17.0 26.0 33.0
		-10.0	-5.0	-2.4	+1.4 +2.3
		70.0	42.0	33.0	13.0 32.0
		-5.0	-2.2	-1.1	+0.5 +1.0
		61.0	50.0	33.0	17.0 33.0

Rt

Station	+	H.I.	−	Rod.	Elev.
		884.41			
93 +75				10.7	73.7
T.P.	7.05	879.35	12.11	872.30	
94 +00				10.2	69.0
+07				11.8	67.6
+25				6.3	73.1
+50				1.9	77.5
T.P.	11.45	887.67	1.8	876.22	
95 +00				7.1	82.6
+50				4.7	85.0
96 +00				5.9	83.8
+60				9.9	80.8
97 +00				8.8	80.9
98 +00				6.0	84.7
T.P	1.92	887.25	4.34	885.33	
99 +00				3.1	84.2
+50				3.4	83.9
100 +00				2.6	84.7
+50				5.0	82.3
101 +00				6.4	80.9
+50				5.2	81.1
102 +00				5.0	81.3
+50				6.2	81.1
B.M.	4.09	885.17	6.17	881.08	
103 +00				4.9	80.2
+50				4.2	80.8
104 +00				5.0	80.2

③ of 5

Lt	℄	Rt
$\frac{-0.4}{50.0}$ $\frac{-0.2}{33.0}$		$\frac{+1.0}{17.0}$ $\frac{+1.4}{33.0}$
$\frac{+2.0}{75.0}$ $\frac{-1.1}{50.0}$ $\frac{-1.4}{33.0}$		$\frac{+0.9}{15.0}$ $\frac{+0.8}{21.0}$ $\frac{+1.2}{23.0}$ $\frac{+2.1}{33.0}$
$\frac{-1.8}{50.0}$ $\frac{-2.9}{45.0}$ $\frac{5.8}{44.0}$ $\frac{-6.1}{35.0}$ $\frac{-5.0}{32.0}$ $\frac{-4.1}{25.0}$ $\frac{-2.5}{25.0}$ $\frac{-1.8}{17.0}$ $\frac{0.0}{9.0}$		$\frac{+2.1}{15.0}$ $\frac{+3.3}{23.0}$ $\frac{+3.0}{33.0}$
$\frac{-9.6}{68.0}$ $\frac{12.5}{63.0}$ $\frac{-12.8}{58.0}$ $\frac{-10.0}{52.0}$ $\frac{-7.5}{50.0}$ $\frac{-6.0}{46.0}$ $\frac{-5.0}{41.0}$ $\frac{-3.1}{35.0}$ $\frac{-2.5}{33.0}$ $\frac{-2.0}{27.0}$ $\frac{+0.1}{12.0}$		$\frac{+0.5}{16.0}$ $\frac{-0.5}{24.0}$ $\frac{0.0}{33.0}$
$\frac{-15.6}{78.0}$ $\frac{-17.8}{71.0}$ $\frac{-15.0}{64.0}$ $\frac{-13.4}{62.0}$ $\frac{-10.0}{51.0}$ $\frac{-8.0}{45.0}$ $\frac{-5.0}{33.0}$ $\frac{-2.5}{24.0}$ $\frac{-1.1}{16.0}$		$\frac{+1.6}{20.0}$ $\frac{+0.9}{33.0}$
$\frac{-15.0}{73.0}$ $\frac{-10.0}{60.0}$ $\frac{-6.5}{50.0}$ $\frac{-5.0}{44.0}$ $\frac{-3.1}{33.0}$ $\frac{-1.7}{22.0}$		$\frac{+2.0}{33.0}$
$\frac{-10.0}{91.0}$ $\frac{-5.0}{60.0}$ $\frac{-4.2}{50.0}$ $\frac{-2.1}{33.0}$ $\frac{-1.1}{22.0}$		$\frac{+1.3}{33.0}$
$\frac{-1.3}{50.0}$ $\frac{-0.2}{33.0}$		$\frac{0.0}{20.0}$ $\frac{-0.[illegible]}{33.0}$
$\frac{+1.0}{33.0}$		$\frac{-1.2}{33.0}$
$\frac{+2.3}{33.0}$		$\frac{-1.7}{33.0}$
$\frac{-1.0}{33.0}$		$\frac{+1.1}{24.0}$ $\frac{+0.9}{33.0}$
$\frac{-0.7}{33.0}$ $\frac{-0.7}{18.0}$		$\frac{+1.5}{18.0}$ $\frac{+2.3}{33.0}$
$\frac{-2.0}{33.0}$ $\frac{-0.8}{16.0}$		$\frac{+2.1}{33.0}$
$\frac{-5.0}{45.0}$ $\frac{-3.0}{33.0}$ $\frac{-1.1}{16.0}$		$\frac{+1.0}{13.0}$ $\frac{+1.2}{33.0}$
$\frac{-5.0}{45.0}$ $\frac{-3.0}{33.0}$ $\frac{-0.6}{12.0}$		$\frac{+1.4}{20.0}$ $\frac{+1.4}{33.0}$
$\frac{-5.0}{48.0}$ $\frac{-3.0}{33.0}$ $\frac{-1.6}{20.0}$		$\frac{+0.7}{20.0}$ $\frac{+0.4}{33.0}$
$\frac{-5.0}{70.0}$ $\frac{-2.0}{50.0}$ $\frac{-0.5}{33.0}$ $\frac{0.0}{22.0}$		$\frac{0.0}{18.0}$ $\frac{-1.1}{33.0}$
$\frac{-5.0}{58.0}$ $\frac{-2.7}{45.0}$ $\frac{+0.[illegible]}{30.0}$ $\frac{0.0}{17.0}$		$\frac{-0.2}{19.0}$ $\frac{-0.6}{33.0}$
$\frac{-15.0}{70.0}$ $\frac{-10.0}{60.0}$ $\frac{-7.3}{50.0}$ $\frac{-5.0}{39.0}$ $\frac{-2.2}{24.0}$		$\frac{+0.7}{19.0}$ $\frac{0.0}{33.0}$

So. Side Tree
Nail in 8" Oak Lt. Sta 102+30

Lt	℄	Rt
$\frac{-15.0}{62.0}$ $\frac{-10.0}{48.0}$ $\frac{-5.0}{31.0}$ $\frac{-4.1}{28.0}$ $\frac{-1.7}{14.0}$		$\frac{+1.1}{15.0}$ $\frac{+0.7}{33.0}$
$\frac{-15.0}{65.0}$ $\frac{-10.0}{54.0}$ $\frac{-8.6}{50.0}$ $\frac{-5.0}{36.0}$ $\frac{-4.2}{33.0}$ $\frac{-1.5}{18.0}$		$\frac{+0.5}{15.0}$ $\frac{0.0}{33.0}$
$\frac{-15.0}{77.0}$ $\frac{-10.0}{65.0}$ $\frac{-5.0}{47.0}$ $\frac{-3.1}{33.0}$ $\frac{-1.1}{20.0}$		$\frac{0.0}{21.0}$ $\frac{-1.0}{33.0}$

75% Rock

See Corrected Loc.

Station	+	H.I.	−	Rod	Elev.
		885.1 ✓			
105 + 00				9.3	75.9
+ 30				10.1	75.1 ✓
+ 60				9.5	75.7 ✓
106 + 00				11.0	74.2 ✓
T.P.	0.17	875.16 ✓	10.11	(774.99)	✓
+ 20				2.9	72.3 ✓
+ 50				8.1	67.1 ✓
T.P	0.14	862.40 ✓	12.90	(862.26)	✓
+ 90				3.4	59.0 ✓
107 + 00				6.9	55.5 ✓
T.P	0.58	850.69 ✓	12.24	(850.11)	✓
+ 25				2.7	48.0 ✓
+ 50				12.6	38.1 ✓
T.P	0.80	839.2 ✓	12.25	838.42	✓
+ 65				6.9	32.3 ✓
108 + 00				11.6	27.6 ✓
+ 35				11.6	27.6 ✓
109 + 00				15.0	24.2 ✓
110 + 00				17.3	21.9 ✓
+ 50				17.1	22.1 ✓ ✓
111 + 00				13.2	(24.0) 26.0
+ 50				9.5	29.7 ✓
T.P	2.73	833.04 ✓	8.93	830.31	✓
112 + 00				2.5	30.5
B.M.				0.30	(332.74) ✓
+ 50				4.8	28.2 ✓

Rt. Rt. (4) 0 - 5

(105 + 0)

(+30)

+80)

(106)

75% Rock

(+20)

(+50)

(+90)

(107)

(+25)

(+50)

(+65)

(108)

(+35)

(109)

(110)

(+50)

(111)

(+50)

(112)

Spin 24" Oak 28' Rt 12 + 0 0

(+50)

Station	+	H.I.	−	Rod	Elev.
		833.04 ✓			
113 +00				11.1	821.9 ✓
T.P.	1.79	823.51 ✓	11.32	821.72 ✓	
+50				4.4	819.1 ✓
114 +00				3.5	820.0 ✓
115 +00				6.7	816.8 ✓
+50				9.4	814.1 ✓
		✓			
T.P.	0.73	811.60	12.64	810.87 ✓	
116 +00				2.0	809.6 ✓
+08				2.2	809.4 ✓
+19				9.2	802.4 ✓
+32				10.3	801.3 ✓
+46				4.8	806.8 ✓
+60				5.3	806.3 ✓
+90				12.1	799.5 ✓
117 +00				12.7	798.9 ✓
+11				12.5	799.1 ✓
T.P.	3.11	802.69 ✓	12.02	799.58 ✓	
+18				8.6	794.1 ✓
B.M.				(7.04)	(795.65) ✓
+45				10.4	791.3 ✓
+50				8.1	794.6 ✓
T.P.	12.17	814.37 ✓	0.49	802.20 ✓	
					✓
+65				7.5	806.9 ✓
+71				4.1	810.3 ✓
T.P.	5.92	818.49 ✓	1.80	812.57 ✓	
118 +00				3.1	815.4 ✓
+29½				2.0	816.5 ✓

Lt. | Rt.

-1.1 0.0 | +0.3 +0.5 +2.0 0.0
50.0 23.0 | 16.0 29.0 32.5 50.0

-0.9 -0.5 | +0.9 +2.0
50.0 28.0 | 18.0 45.0
-1.5 -0.4 | +0.8 +0.5
50.0 24.0 | 25.0 50.0
0.0 -0.2 | +1.0 +1.0
50.0 26.0 | 18.0 50.0
-0.1 +0.4 +0.7 | -0.2 -0.5
50.0 39.0 18.0 | 19.0 50.0

+1.0 +0.4 | +0.7 -0.8 -1.5 -2.1 -2.6 +0.3 16
50.0 19.0 | 26.0 35.0 44.0 50.0 57.0 59.0
+0.5 0.0 | -0.3 -1.4 -2.5 -3.8 -2.0 +1.0 +08
50.0 17.0 | 9.0 27.0 32.0 45.0 50.0 -2.5
+6.6 +6.1 +5.0 +2.6 | 0.0 +2.0 +5.0 +7.5 +7.8 +19
50.0 21.0 17.0 9.0 | 10.0 27.0 38.0 42.0 50.0
+7.4 +6.7 +5.0 | +5.0 +7.3 +6.5 +9.2 +32
50.0 24.0 20.0 -0.2 | 10.0 14.0 31.0 50.0
0.0 -7.6 -7.0 -5.0 -0.9 | +1.5 +2.9 +3.0 +46
45 21.0 14.0 9.0 4.0 | 15.0 30.0 50.0
-2.5 -4.5 -8.0 -9.7 -5.0 -2.0 | +1.7 +2.3 +3.1 +60
50.0 45.0 35.0 24.0 19.0 13.0 | 12.0 27.0 50.0
-6.8 -6.6 -5.0 -1.3 -0.7 | +3.1 +4.8 +5.0 +90
50.0 44.0 38.0 24.0 10.0 | 14.0 32.0 41.0

-1.0 -8.5 -8.8 -7.1 -6.8 -5.0 -4.0 -0.2 | +1.8 +3.0 +3.7 17
74.0 67.0 60.0 57.0 58.0 33.0 24.0 14.0 | 15.0 32.0 50.0
-6.9 -8.8 -8.2 -6.2 -5.0 -1.4 | +1.4 +2.6 +3.0 (+11)
50.0 46.0 39.0 32.0 12.0 3.0 | 14.0 33.0 50.0

+4.0 -1.0 -1.3 -3.9 -3.5 -1.7 -1.0 | +3.4 +5.0 +6.3 +7.5 +8.0 +18
61.0 50.0 42.0 35.0 24.0 15.0 10.0 | 10.0 15.0 26.0 33.0 50.0

Sp. in 14" Pop 10' Rt Sta 117+20 = (Sp. in blz, free 3' R. 114+05 / Conner's orig. survey · El. 795.73)
+15.0 +13.1 +11.7 +10.0 +7.8 +5.0 +3.2 | +0.5 +0.8 +1.6 +3.3 +5.0 +7.0 +45
62.0 45.0 32.0 17.0 17.0 12.0 10.0 | 11.0 29.0 43.0 50.0 54.0 66.0

-0.4 -0.3 +0.2 | -0.4 -1.1 -0.5 -1.0 +11
50.0 30.0 12.0 | 12.0 33.0 34.0 50.0

-2.3 -1.3 -0.3 | +0.2 -0.4 -1.4 (16)
50.0 34.0 20.0 | 19.0 33.0 50.0

Project 23-60

Station 86+70.3 to 93+98.8
Connection #2
Between North and South Lines
Transit Notes
1-Page.

R.F. Austin
A.N.S Kooglun } Party.
W. Maloney
M. Galvin

11-6-23

Abandoned

		Ang. ℄ Lt	Ang. Rt	
(93+98.8	E.C. = 92+76.5 Conner's line)			
				N. 17° 40' W.
92+85±	P.I	48°57'		
				N. 64° 22' W.
91+54.0	B.C.			
90+11.1	E.C.			
89+25.0	P.I	55°21'		
				N. 81° 01' W.
88+20.3	B.C.			
81+00	P.I	5°00'		

11-6-23

Sta.	Def.
91+54	0°00'
92+00	4°36'
+50	9°36'
93+00	14°36'
+50	19°36'
+98.8	24°28½'

20° Curve Rt.
Δ = 48°57'
Tang = 131.05
B.C. = 91+54 ±
Length = 244.8
E.C. = 93+98.8 ±

Sta.	Def.
88+20.3	0°00'
+50	4°18½'
89+00	11°33½'
+50	18°48½'
90+00	26°03½'
+11	27°40½'

29° Curve Rt.
Δ = 55°21'
S.T. = 104.7
B.C. = 88+20.3 ±
Length = 190.8
E.C. = 90+11.1

Project 23-60

Station 88+20.3 — 93+98±
Connection #2
Between North and South lines
Level Notes
1-Page.
11/6/23

R.E. Austin
H.N. Skooglan
W. Maloney
M. Galvin
} Party.

Abandoned

(6)

Station	+	H.I.	—	Rod	Elev.
B.M	7.17	886.01			878.84
85+20.8				8.9	77.1
+50				6.6	79.4
89+00				5.4	80.6
+50				5.0	81.0
90+00				4.9	81.1
+50				4.1	81.9
91+00				4.9	81.1
+50				5.6	80.4
92+00				8.1	77.9
+50				7.5	78.5
93+00				7.4	78.6
+50				12.7	73.3
T.P.	1.32	875.66	11.67	874.34	
+73				8.0	67.7
+77				10.6	65.1
+85				8.6	67.1
(93+98.5	=92+76.5)			5.9	69.8
93+00	Orig. line			2.6	73.1

Nail in 20" Oak. RH 92+30

Ft Alignment.

Proj - 23-60

Prescott Connection

Jan. 1924

Party

Conner

Wilshusen

Rittenberg

Fritz

Sta	PT.	∠ from ↗ Rt
89+17.5	EC	16-09
+50		14-47
89		12-17
+50		9-47
88		7-17
+50		4-47
87		2-17
86+54.3	BC	00 Corners Lines
=86+54.3	P.O.T.	↗ Haustus Curve

PI = 88+20.3
Δ = 32-19
10° C Rt.
T = 166.0
LC = 323.2
166.1


10" oak

30 RT

PI 58+20.3

34 LT


10" oak

Sta	PT	Lt △ Rt.
92+65.1 EC		26°08½'
+50		24-38
92		19-38
+50		14-38
91		9-38
+50		4-38
90+03.1 BC		00

PI = 91+44.3
△ = 52-17
20° C Lt
T = 140.6
LC = 261.4
T = 141.3

30" Double Oak.

23'5"

PI 91443

39'3"

30" Oak

Sta.	PT	∠	Δ	Rt.
94+83.8	EC		11-59	
+50			9-17	
94			5-17	
+50			1-17	
93+34	BC		00	

PI = 94+10
Δ = 23-58
16° C Rt.
T = 76.2
LC = 149.8
76.2

8" oak

24' 19.9 10" oak

PI 94+10

Sta PT ∠ Δ Rt.

103+52.4 EC Austin's Line
[illegible]01+95.5 POT corner's Line

100+63.6 EC 6-34

PI = 99+81.8
Δ = 13-08
8° C Rt.
T = 82.4
LC = 164.2
82.5

+50 6-01½

100 4-01½

+50 2-01½

98+99.4 BC 00

6" oak

@ 39.8

6" oak @ 39.8 PI 99+81.8

Ft Levels

Proj-23-60

Prescott Connection

Jan. - 1924.

Party

Conner

-Wilshusen *

Luttenberg *

Fritz

Sta	+	H.I.	−	Elev.	
B.M.	6.82	88566	✓	87884	✓
86+54⅔ B.C.			7.7	78.0	✓
87			6.5	79.2	✓
+50			8.9	76.8	✓
88			9.9	75.8	✓
+50			5.5	80.2	✓
89			4.1	81.6	✓
+50			3.8	81.9	✓
89+77.5 E.C.			3.8	81.9	✓
90+03.7 B.C.			3.7	82.0	✓
+50			4.2	81.5	✓
91			5.2	80.5	✓
+50			6.7	79.0	✓

Nail in 20" Oak 4.0' R. 92+30 Austin's Survey (R.J.W) 1-25-24

Sta	+	H.I. 885.66	−	Elev
9			10.3	75.4
+15			11.8	73.9
T.P.	0.10	876.2	9.54	876.12
+50			12.5	63.7
T.P.			2.71	873.51
T.P.	1.70	865.96	11.96	864.26
9+65.1	E.C.		9.2	56.8
T.P.	4.20	858.08	12.08	853.88
9+88			17.6	40.4 40.5
93			9.9	48.2
T.P.	1093	884.44		873.51
93+340	B.C.		17.0	61.4
+50			11.9	72.5
94			3.7	80.7
+50			3.5	80.9
94+83.8	E.C.		3.6	80.8
95			3.9	80.5

Top of stake at Stg. 93+50

Sta	+	H.I	−	Elev	
		884.44 ✓			
95+50		✓	7.2	77.2	✓
T.P.	0.99	879.09	6.34	878.10	✓
96			10.7	68.4	✓
+35			14.2	64.9	✓
+50			9.5	69.6	✓
~~T.P.~~					
97		✓	1.4	77.1	✓
T.P.	5.98	883.58	1.49	877.60	✓
+50					
+50			4.8	78.8	✓
98			7.9	75.7	✓
+50			10.2	73.4	✓
98+99+	B.C.		10.5	73.1	✓
99+50			5.8	77.8	✓
T.P.	7.96	886.0 ✓	4.94	878.6	✓
99+78			6.4	80.2	✓
100			5.3	81.3	✓
+50			5.0	81.6	✓
+63.6	E.C.		4.9	81.7	✓
13 N.J.			5.3	881.07	880.06

878.64
7.96
886.60
5.53
881.07

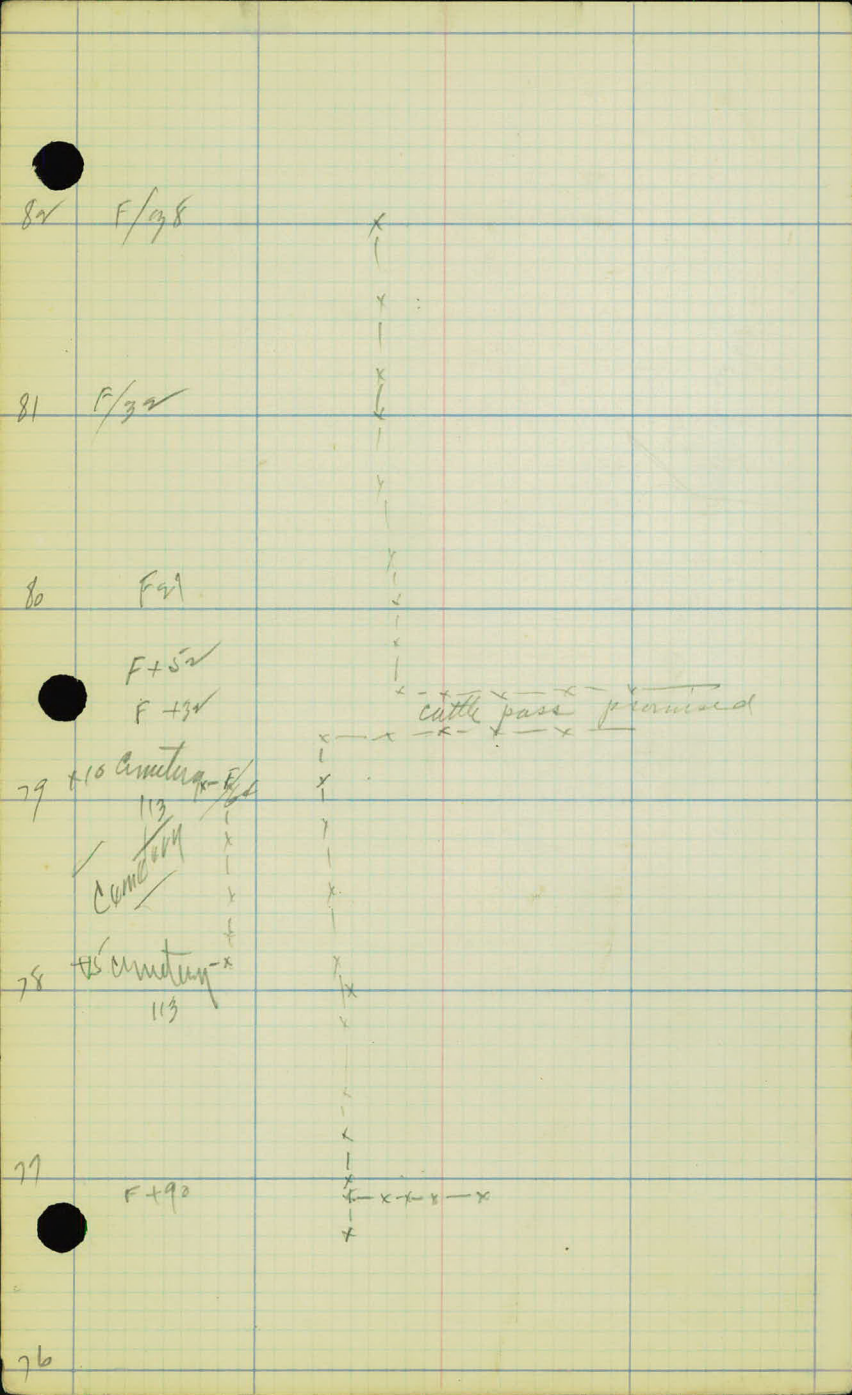
Nail in 8" Oak L. 102+30 Austin's Survey (R.J.W. 1-25-52)

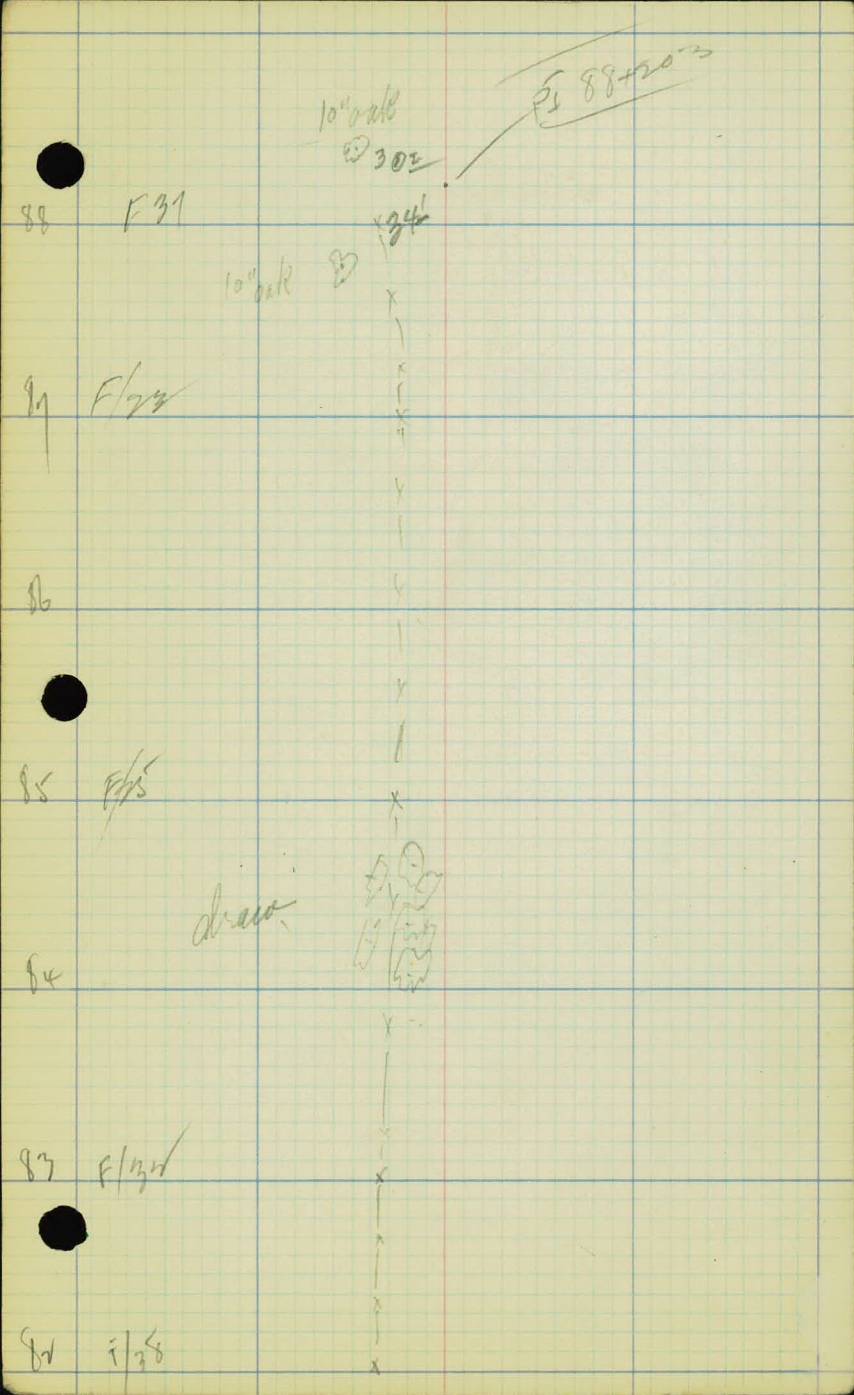
101	116.60	6.2	80.4
+50		6.3	80.3
101 +50		5.8	80.8

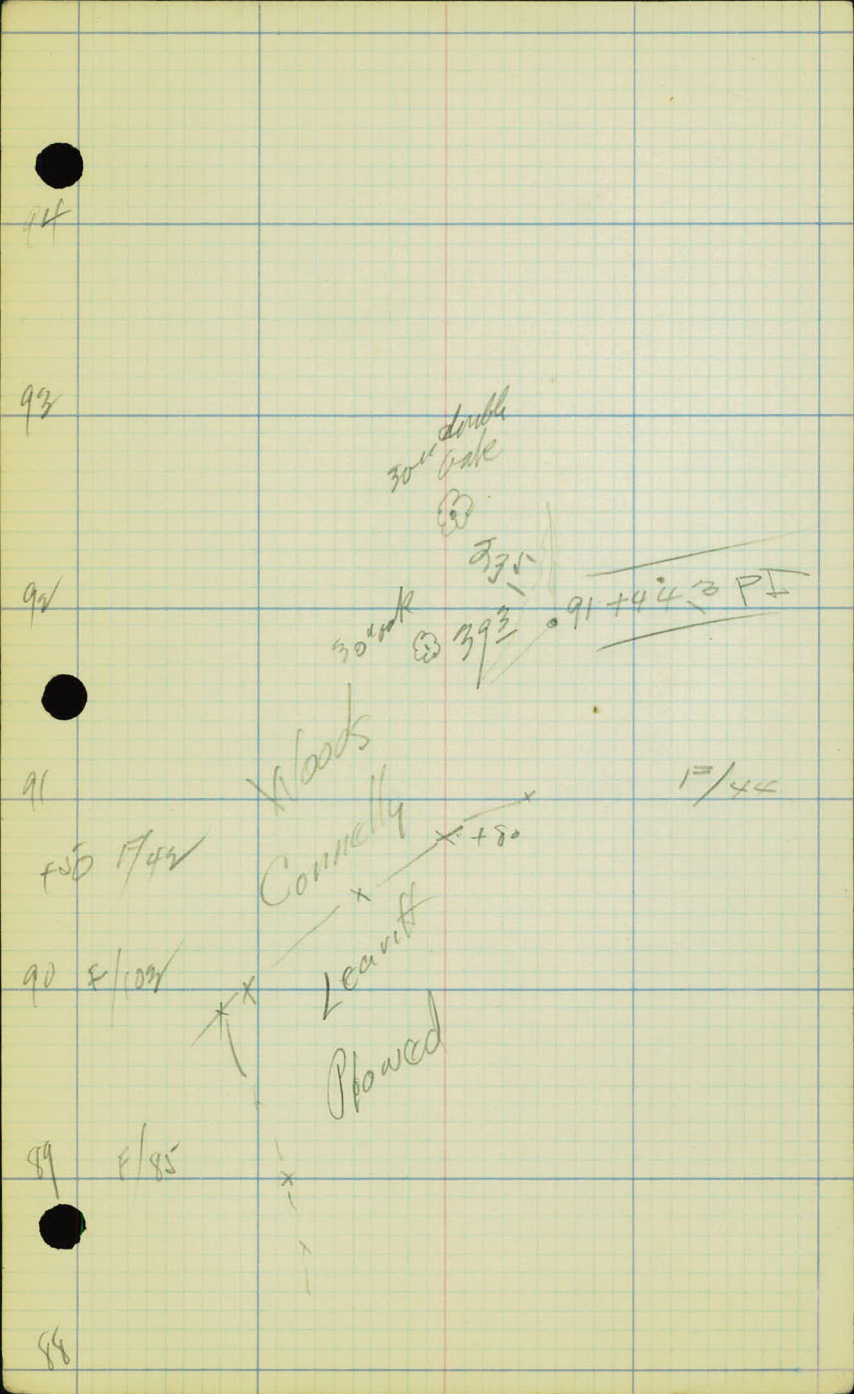
Art. Topog

Proj. - 23-60
Prescott Connection
Jan. - 1924.

Party
Conner *
Wilshusen
Ruttenberg
Fritz *


82
F/38
81
F/32
80
F29
F+5
F+3
cattle pass provided
79
+10 Crushing
113
Camp
78
+15 Crushing
113
77
F+92
76


10" pole
302
E 88+20
88
E 31
10" pole
89
E 32
86
85
E 33
drain
84
83
E 34
82
E 35


94
93
30" double gate
92
30" dbl
91
Woods
Connelly
Leavitt
Plowed
89
88

100

99

98

97

96

95

94

8" oak @ 34' PS 19 @ 9 @ 10" oak

94+10

Cross-Sections
Proj.-23-60
Prescott Connection
Jan.-1924

Party
Conner
Wilshusen
Rothenberg
Fritz

Prescott Project

86+54.3 to 101+95.5

86+54.3	B.C.	78.0	
87+00		79.2	
+50		76.8	
+75		75.2	
88+00		75.8	
+50		80.2	
89+00		81.6	
+50		81.9	
90+03.7	B.C.	82.0	-10.0/160
+50		81.5	-10/150
91+00		80.5	-10/145
+50		79.0	

Connors
Wilshusen
Rottenberg
Fritz

1/9/24 L

R.

-11.0	-7.5	-4.1	-1.6	00	+1.1	+2.0
75	60	30.0	150	00	75.0	50
-6.8	-5.4	-2.4	00	+1.3	+1.5
56	47.0	23.0	00	37.0	51.0
-10.4	-3.6	-1.7	00	+1.0	+2.6
56	26.0	16.0	00	19.0	44
	-8.0	-4.6	-1.6		+2.7
	46.0	31.0	00		33
	-4.5	-1.1	00		+1.6
	37	28.0	00		33
-10.0	-5.0				
105	81	-2.0	00		+0.4
		57	00		33
-11.0	5.0				
115	100	-4.0	00		+0.6
		79.0	00		33
-6.0					
140	-3.5		00		00
	101		00		33
-1.5					
-140	00	-1.0	00		+0.4
	83	51	00		33
-2.0					
-1.5					
140	-1.6		00		-0.5
100	2.0		00		33
-3.5					
110	-4.8	-1.6	00		+0.5
	70.0	35.0	00		33
	-8.8	-2.7	00		+0.7
	54	17.0	00		33

93+00	75.4
+50	63.7
+88	40.5
93+50	72.5
94+00	880.7
+50	80.9
95+00	80.5
+50	77.2
96+00	68.4
+35	64.9
+50	869.6

Connors
Wilkinsen
Rutenberg
Fritz

	C	R
-10.4 / 43	-5.0 / 27.0	00 / 00	+1.0 / 33
-7.7 / 44.0	-4.0 / 23.0	00 / 00	+1.0 / 40	+0.5 / 46
-18.0 / 130	-12.0 / 100	-10.0 / 80	-8.5 / 72	-6.0 / 65	-3.8 / 34.0	00 / 00	+2.7 / 87	+4.0 / 40	+4.0 / 52	+6.0 / 60
-1.0 / 75	00 / 00	00 / 31	-1.1 / 45
-14.4 / 116	-10.0 / 100	-6.0 / 79	-2.6 / 67	00 / 00	00 / 50
-10.6 / 89	-4.0 / 57	00 / 00	0.0 / 48
-10.0 / 67	-2.6 / 27.0	00 / 00	-1.1 / 52
-8.0 / 67	-4.2 / 54	00 / 00	-0.6 / 26.0	+4.2 / 68
-5.0 / 61	-0.5 / 27	-1.6 / 6.0	00 / 00	+2.0 / 12.0	+9.7 / 48
-16.0 / 60	-10.0 / 42.0	-3.8 / 00	+4.0 / 14.0	+12.0 / 46
-15.0 / 56.0	-10.0 / 41.0	00 / 00	+2.0 / 21.0	+8.8 / 49.0

97+00	77.7
+50	78.8
98+00	75.7
+50	73.4
99+00	873.1
+50	77.8
100+00	81.3
+50	81.6
101+00	880.4
+50	80.3
+95 ±	80.8

Commons
Wilshusen
Ruttenberg
Fritz

snowy
×cold

L R

-12.0 / 54	-5.0 / 32.0	0-0 / 0-0	+1.5 / 16.0	+3.4 / 46.0
-10.0 / 59.0	-7.2 / 46.0	0-0 / 0-0		+2.2 / 47
-10.0 / 69	-6.5 / 50	0-0 / 0-0	+1.7 / 26.0	+4.4 / 58
-10.0 / 38.0		0-0 / 0-0	+3.2 / 15.0	+11.0 / 71.0
-9.2 / 66	-8.0 / 12.0	0-0 / 0-0	+0.8 / 7.0	+3.8 / 41.0
-3.2 / 42.0		0-0 / 0-0		+2.4 / 42
-9.2 / 54	-4.4 / 33	0-0 / 0-0		0-0 / 44.0
-10.0 / 54.0	-5.0 / 33	0-0 / 0-0		0-0 / 38
-11.4 / 46.0	-5.6 / 28.0	0-0 / 0-0	+2.5 / 8.0	+0.8 / 26.0	0-0 / 69
-8.8 / 47.0	-5.0 / 29.0	0-0 / 0-0	+0.4 / 12.0	-0.4 / 39.0
-10.0 / 51.0	-3.6 / 24.0	0-0 / 0-0	0-0 / 3.8.0	-1.6 / 47.0

Project 23-60

Station 12+418 to 14+432

Connection between North and South lines.

Transit Notes

1-Page

11-2-23

D. F. Hoxton
H. N. Shipton
W. [illegible]
H. Curtin.
} Party.

File

℄

Station	Ang. L.	Ang. Rt.	Calc. Bearing

Equation { 94+43.3 South line
= 93+02.2 North line

94+43.3 E.C.

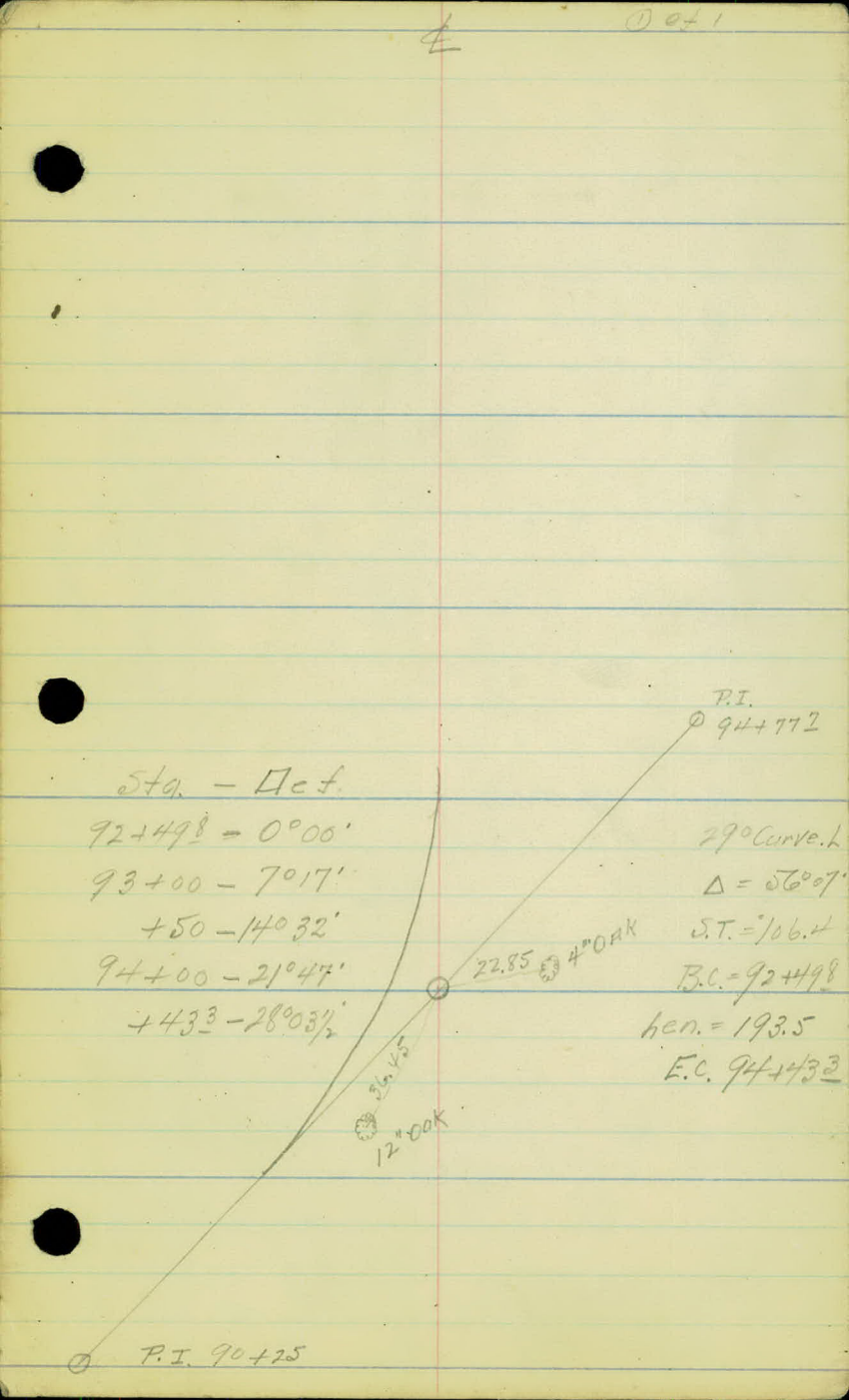
93+56.2 P.I 56°07'

92+49.8 B.C.

90+25 P.I

N 41°11' W

N 94°51' W


P.I.
94+77.2
Sta. – Inc.
92+49.8 – 0°00'
93+00 – 7°17'
+50 – 14°32'
94+00 – 21°47'
+43.3 – 28°03½'
29° Curve.
Δ = 56°07'
S.T. = 106.4
B.C. = 92+49.8
Len. = 193.5
E.C. 94+43.3
22.85
4" OAK
36.45
12" OAK
P.I. 90+25

Project 23-60

Station 92+49.8 to 94+43.3
Connection between North + South lines.

Level Notes
1 Page.

R.E. Austin
D.N. Skooglum
W. Maloney
M. Galvin
} Party.

11/2/23

Station	+	H.I.	−	Rod.	Elev.	
B.M.	1.07	879.91			(878.84)	Pt. 92+30
92+50				4.2	75.7	
93+00				3.2	76.7	
7+25				2.3	77.6	
+50				3.7	76.2	
+75				4.4	75.5	
+96				12.8	67.1	
94+00				15.9	64.0	
+03				14.7	65.2	
+25				8.5	71.4	
+48				8.9	71.0	

Project No 23-60

Change of line
Sta. 68+32± – 118+29±
Transit Notes.
4-Pages.

R. E. Austin.
H. Skooglun
W. Maloney
M Galvin
} Party.

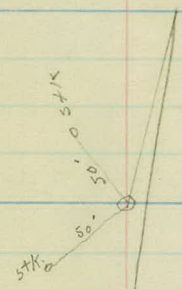
10/31/23

Station	Ang. h.	Ang R	
82+24.9 E.C.			N 18° 10' W 925.2'
81+00 P.I	5° 00'		
77+74.9 B.C.			N 83° 10' W 1154.6'
72+21.6 P.O			
70+59.2 E.C.			
69+45.9 P.I	9° 05'		
68+32.1 B.C.			S 87° 45' W 312.9'
66+~~38~~ 32.9 E.C.			

Austin
Skoglund
Maloney
Galvin

Sta. - Ref

79+74.9 - 0°00'
80+00 - 0°15'
81+00 - 1°15'
82+00 - 2°15'
+24.9 - 2°30'



2° Curve, Rt.
Δ = 5°00'
S.T. 125 -
B.C. = 79+74.9
Length 250.0
E.C. 82+24.9

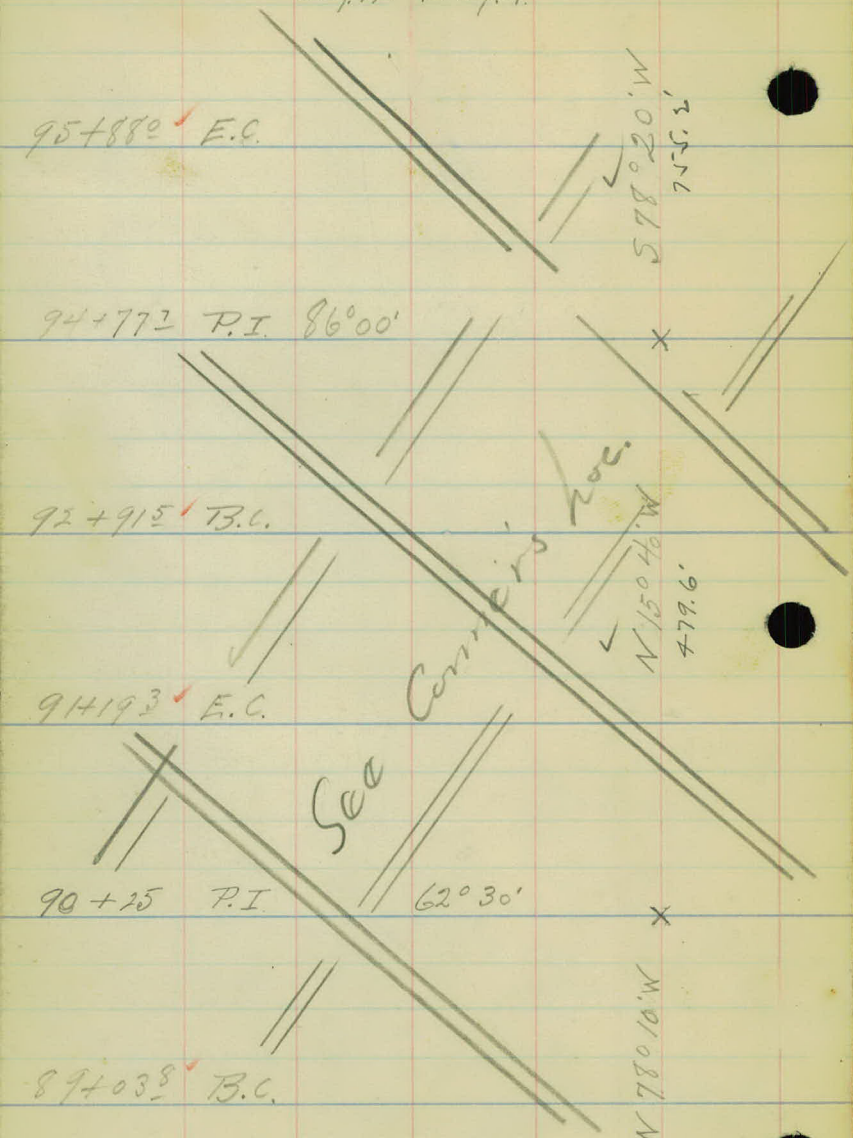
Sta. - Ref

68+32 - 0°00'
+50 - 0°21½
69+00 - 1°21½
+50 - 2°21½
70+00 - 3°21½
+59.2 - 4°32½

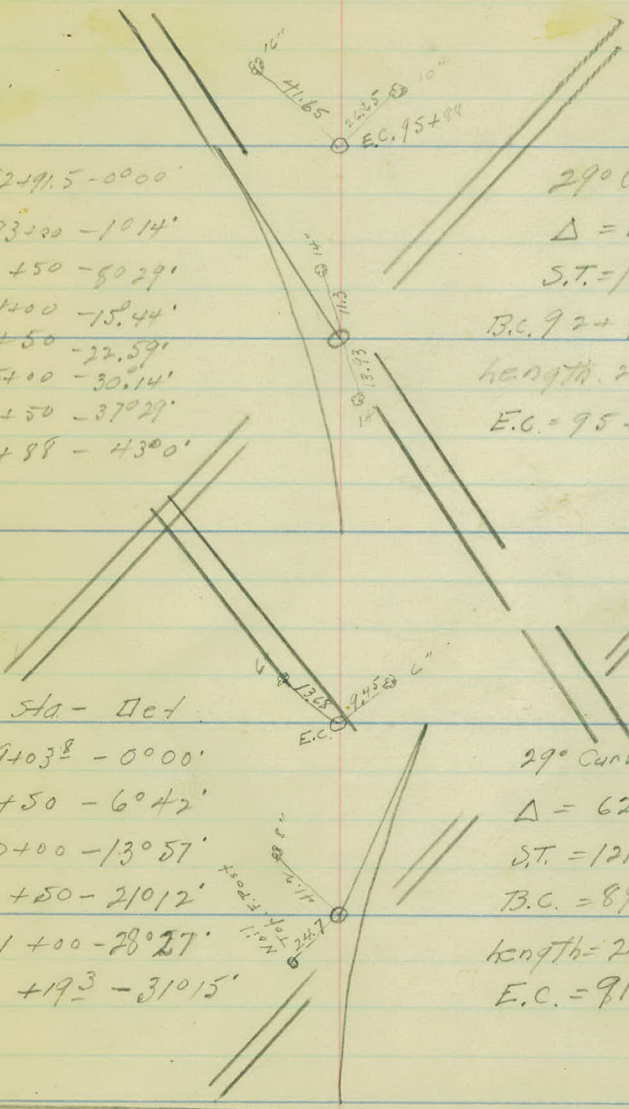
4° Curve Rt.
Δ = 9°05'
S.T. = 113.8
B.C. = 68+32
Length = 227 -
E.C. = 70+59.2

℄

Ang. h. Ang. R.


95+88.2 E.C.
S 78°20' W
1.5.5.
94+77.2 P.I. 86°00'
92+91.5 B.C.
N 15°40' W
479.6'
See Carrier's Loc.
91+93 E.C.
90+25 P.I.
62°30'
N 78°10' W
87+03.8 B.C.

10-30-23


16"
41.65
2435
10"
E.C. 95+88
Sta - Det
92+91.5 - 0°00'
93+00 - 1°14'
+50 - 5°29'
94+00 - 15°44'
+50 - 22.59°
95+00 - 30.14'
+50 - 37°29'
+88 - 43°0'
29° Curve Lt.
Δ = 86°00'
S.T. = 186.2
B.C. 92+91.5
length. 296.5
E.C. = 95+88
Sta - Det
89+03.8 - 0°00'
+50 - 6°42'
90+00 - 13°57'
+50 - 21°12'
91+00 - 28°27'
+19.3 - 31°15'
29° Curve Rt.
Δ = 62°30'
S.T. = 121.2
B.C. = 89+03.8
length = 215.5
E.C. = 91+19.3

3 4

Ang L Ang. R

105+60.9 P.O.T.

N 60° 42' W

1005.7'

103+52 ± E.C.

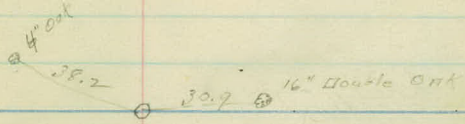
101+57 P.I 40°58'

S 81°02' E

99+42.7 B.C.

SEE Conner's Location

10-31-23



Sta - Def

99+42.7 - 0°00'

100+00 - 2°52'

+50 - 5°22'

101+00 - 7°52'

+50 - 10°22'

102+00 - 12°52'

+50 - 15°22'

103+00 - 17°52'

+52.7 - 20°29'

10° Curve Rt.

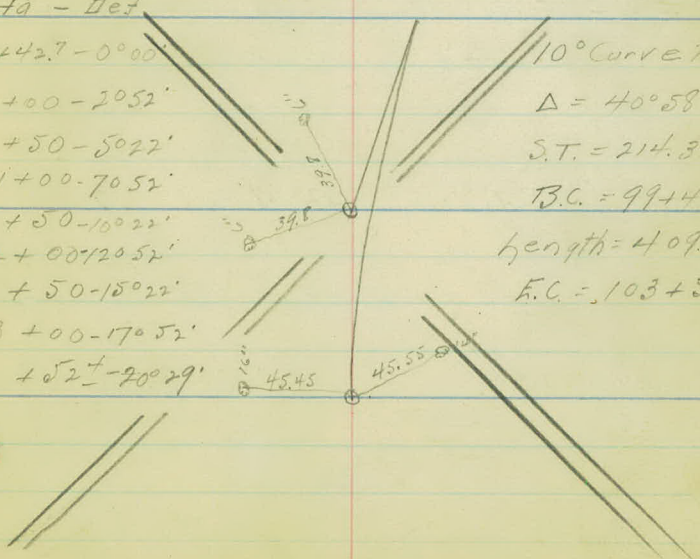
Δ = 40°58'

S.T. = 214.3 ✓

B.C. = 99+42.7

Length = 409.7 ✓

E.C. = 103+52.4



℄

Ang b Ang R

118+29.6 = (115+09.9 "Connects line)

N. 37° 40' E.

9.956

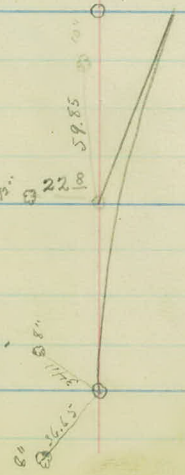
113+03.8 E.C.

111+43.8 P.I. 32° 59'

109+74.0 B.C.

N. 27° 40' E.

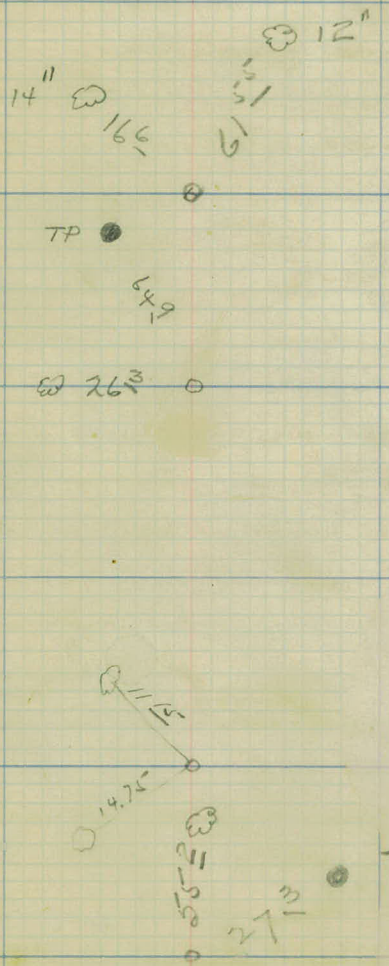
Sta	Def.
109+74	0°00'
110+00	1°18'
+50	3°48'
111+00	6°18'
+50	8°48'
112+00	11°18'
+50	13°48'
113+00	16°18'
+03.8	16°29½'



10° Curve Rt.
Δ = 32°59'
S.T. = 169.8
B.C. = 109+74
Length = 329.8
E.C. = 113+03.8

PRESCOTT CONNECTION FMC 9/4/23

L-Lime.

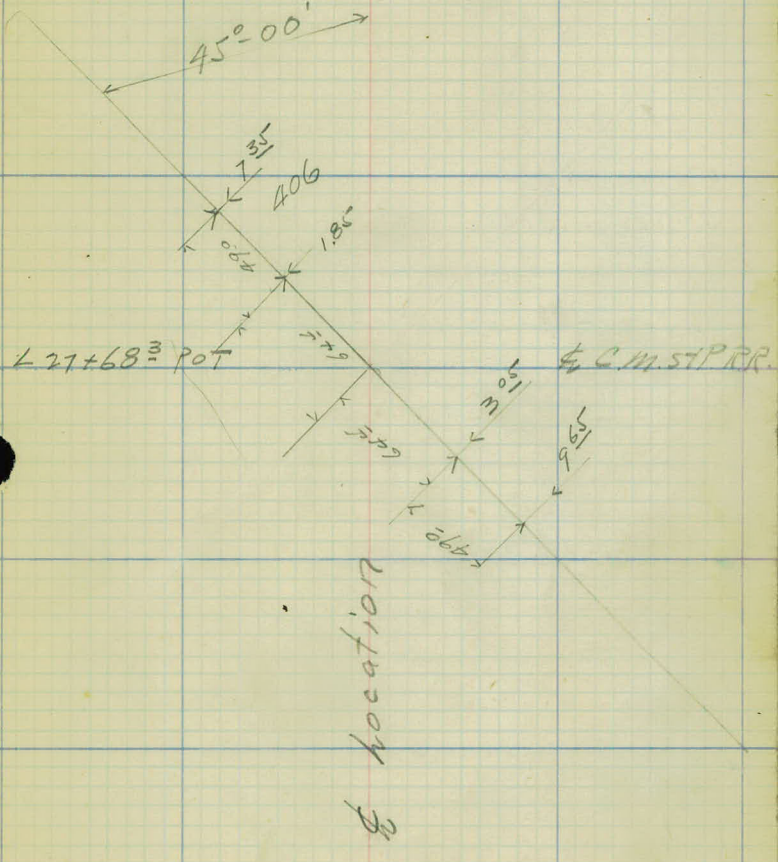


Sta. Pt. Lt. Δ Rt. Calc. Bear.

PRESCOTT CONNECTION
L-Line

4/3/23
FMC

CM & St.P R.R. Xing



Stat. Pt. Lt. Δ Rt. Calc. Bear.

PRESCOTT CONNECTION FMC

L-Line

Equations

Revision

N24-05' W

Short Station - 52+00 to 53+00
= 92.6 ft.

(52+50 ± EC		
52 + 43.0 EC)	23-55	
52	21-33	
+50	18-48	PI - 50+39.1
		Δ = 47°50'
51	16-03	11° C Rt.
		T = 231.0
+50	13-18	LC = 434.9
		Def. pr. ft = 3.3 min.
50 POC	10-33	
+50	7-48	
49	5-03	
+50	2-18	
48+08.1 BC	00	

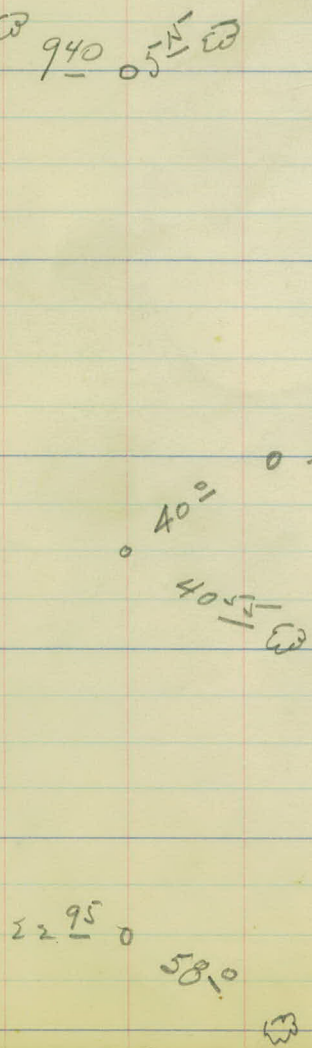
N71°55' W

Engr. Off. 210

PRESCOTT CONNECTION 4/13/23 FHC

L-Line

same tie as used on BC ahead.



PRESCOTT CONNECTION FMC
L Line

S/G- Pt. Lt. Δ Rt. Cafe Bear

52+60 BC

N24-05W

Note - this curve was re staked 4/17/23
Stakes are in ground for both this and
11°C. X sect. are taken independent on
each. - Computations will decide which to use.

+78.7 EC 23-55 Δ = 47°50'

T = 159.3

+50 21-37 LC = 298.9

PI 50+39.1

51 17-37 16° C Rt Δ

+50 13-37

50 9-37

+50 5-37

49 1-37

49+79.8 BC 00-00

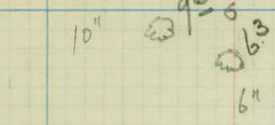
11°C Run

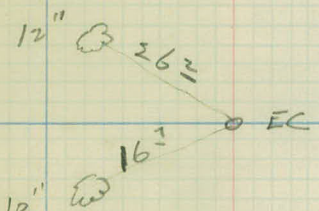
Void

Error in chaining
50' Ch. 1.1 ft. Short of Dist.
Correct. added at
to Tang Dist.

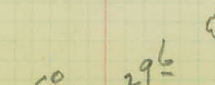
N71-05W

PRESCOTT CONNECTION FMC 4/4/23
2-Line





Sta 50+15.5 Ct. 3.8 B PI 50+13.7



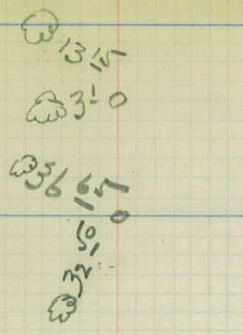
Sta.	Pt.	Lt. Δ Rt.	Calc. Bear.
63+03.5	PI	34°-00	
			N 50°-10' W
42.94	EC	17-05	
58		16-12	
			PI - Not Set
+50		14-42	Δ = 34°-10'
			T = 293.5
57	POC	13-12	∠C = 66.94
			6° C LT
+50		11-42	
56		10-12	
54+99.5			
+50		8-42	
+40		8-24	
55	POC	7-12	
+50		5-42	
54		4-12	
+50	POC	2-42	
53		1-12	
52+60	BC	00	N 24°-05' W

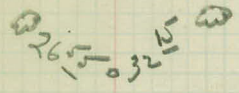
PRESCOTT
CONNECTION
L-Line

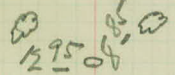
8"

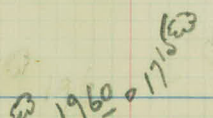
8"

FMC 4/8/23









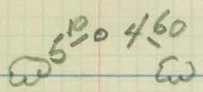
Sta.	PT.	Lt △ Rt.	Calc. Bear.
65		13-40½	
+50	POC	12-25½	
64		11-10½	
+50		9-55½	
63		8-40½	
+50		7-25½	PI = 63+03.5 △ = 34°-00'
62	POC	6-10½	5° C Lt. T = 350.5
+50		4-55½	Lc = 680°
61		3-40½	
+50		2-25½	
60		1-10½	
59+53°	BC		

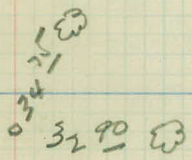
N58°-15W

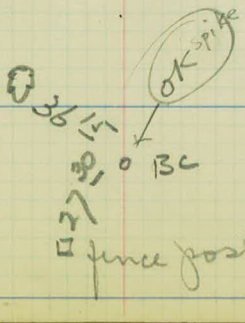
PRESCOTT CONNECTION
L- Line

(46)

FMC 4/5/23







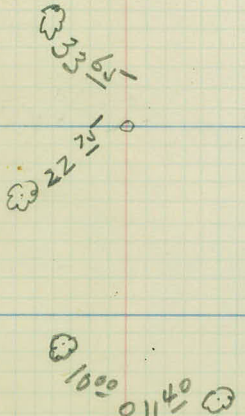
Sta.	PT.	Lt. Δ Rt.	Calc. Bear.
			N 7 L° - 20' W
69+45.9	PI	17°-55' L	
			S 87-45 W
+ 33.9	EC	17-00 / 16°-55	
66		16-10½	
+50		14-55½	

Curve clgs 18 FT to match deflt.

PRESCOTT CONNECTION
L - Line

FMC 4/5/23

30
59+53.7
6+77
66+30.7
16-36
30.7



Sta.	PT.	Lt. Δ	Rt.	Calc. Bear.
				N 7° 20' W
68+	EC	8-57½		
+50		8-35		
71		7-35		PI = 69+45.9
				Δ = 17-55
+50		6-35		4° Crv
				T = 225.8
70		5-35		LC = 447.9
+50		4-35		
69		3-35		
+50		2-35		
68		1-35		
+50		0-35		
67+20	BC	00		
				S. 87° 45' W

PRESCOTT CONNECTION
L-Line

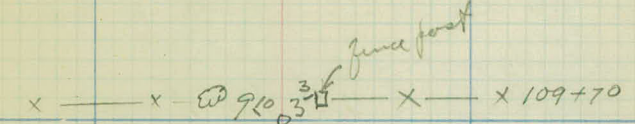
FMC 9/6/23

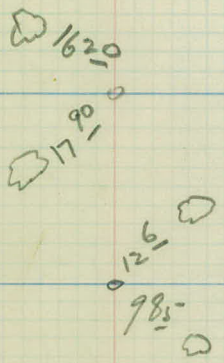
T3 9S- 0 15 1/2

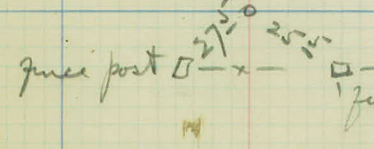
Sta.	PT.	Lt. Δ Rt.	Calc. Bear.
			N 27°36' W
109+86.9	PI	44°10' Rt.	
99+00	POT		
			N 71-46 W
94+00	POT		
80+00	POT		
77+04.6	PI	2°34' Rt	
			N 74°20

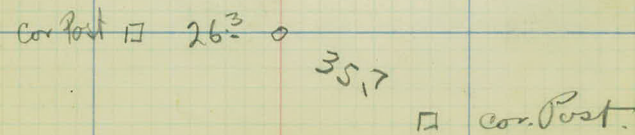
PRESCOTT CONNECTION
L- Line

FMC 4/6/23









Sta	PT.	Lt. Δ Rt.	Calc. Bear.
110		11-53	
+50		10-53	
109		9-53	
+50		8-53	4° C Rt.
108		7-53	PI = 109+86.9
			Δ = 44-10
+50		6-53	T = 581.2
			Lc = 1104.2
107		5-53	
+50		4-53	? D
106		3-53	
+50		2-53	
105		1-53	
+50		0-53	
104+05.7 BC		00	
			N 71°-46' W

PRESCOTT CONNECTICUT FHC 9/10/23
L - Line

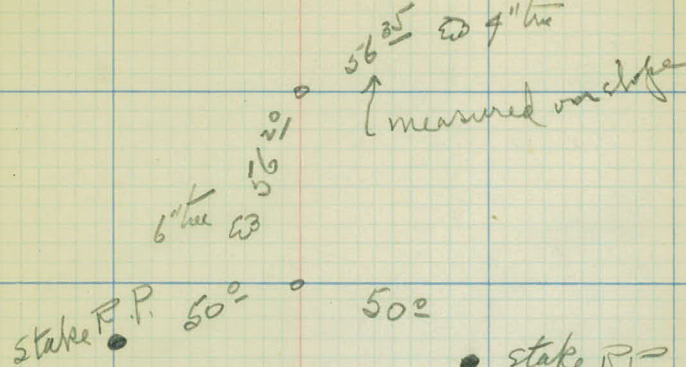
BC 104+05.71

7.10 11.50 BM used for RP

Sta.	PT.	Lt. Δ	Rt.	Calc. Bear.
				N 62°-50' W
124+14.6	PI	35°-14'		
				N 27-36 W
+09.9	EC			22-05
115				21-53
+50				20-53
114				19-53
+50				18-53
113				17-53
+50				16-53
112				15-53
+50				14-53
111				13-53
110+50				12-53

Curve d 0.00

PRESCOTT CONNECTION FMC 9/10/23
L-Line



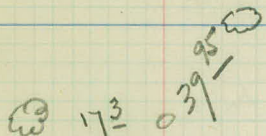
1075 06 29

Sta	PT.	Lt. Δ Rt.	Calc. Bear.
+50		7-02½	
122	POC	6-25	
+50		5-47½	
121		5-10	
+50		4-32½	PI = 122 + 16
			Δ = 35°-14'
120		3-55	2°-30' C Lt.
			T = 727.8
+50		3-17½	LC = 1409.3
			Def. pr. St. 0.75 Min.
119		2-40	
+50		2-02½	
118		1-25	
+50		0-47½	
117		0-10	
116+86.8	BC	0-0	

N 21°-36' W

PRESCOTT CONNECTION
L-line

FMC 9/10/23



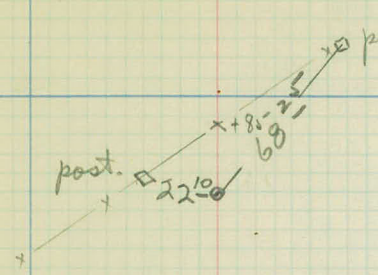
stake RP • 50' 50' • stake RP

Sta.	PT	Lt. Δ Rt.	Calc. Bear.
129		15-10	
	+50 POC	14-32½	
128		13-55	
	+50	13-17½	
127		12-40	
	+50 POC	12-02½	
126		11-25	
	+50 POC	10-47½	
125		10-10	
	+50	9-32½	
124		8-55	
	+50	8-17½	
123		7-40	

Dist in curve is 1.3 ft short.
Dist. Sta 126 & 126+50

PRESCOTT CONNECTION
L-Line

FMC 4/10/23



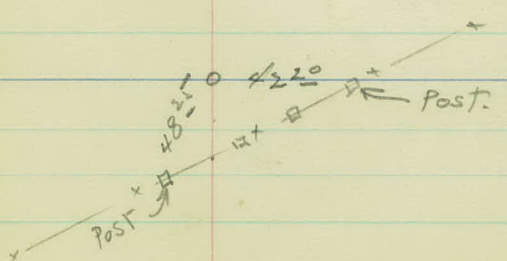
Sta.	Pt.	∠	Δ	Rt.	Calc Bear.
					S 80°-04' W
135+68.5	PI	37°-06			
					N 62°-50' W
+96	EC	17-37			
+50		17-02½			
130		16-25			
129+50		15-47½			

PRESCOTT CONNECTION

L-Line

FMC 4/10/23

Not Referenced
in center field



+50	14-09	
137	12-54	
+50	11-39	
136	10-24	
+50	9-09	PI = 135+68.5
		Δ = 37-06
135	7-54	5° C Lt.
		T = 384.6
+50	6-39	∠C = 742.2
134	5-24	
+50	4-09	
133	2-54	
+50	1-39	
132	0-24	
131+83.9 BC	00	

N62°-50'W

PRESCOTT CONNECTION
L-Line

FMC 9/10/23

8" Not Referenced in cultivated field

S. 80° 04' W

140+08 POT

S 80°-04'W

139+90. POT W. edge Town Rd.

S 80°-04'W

+258 EC 18-33

139 17-54

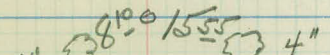
+50 16-39

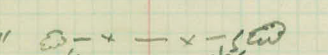
138 15-24

Error in chaining 0.00

PRESCOTT CONNECTION FMC 9/11/23

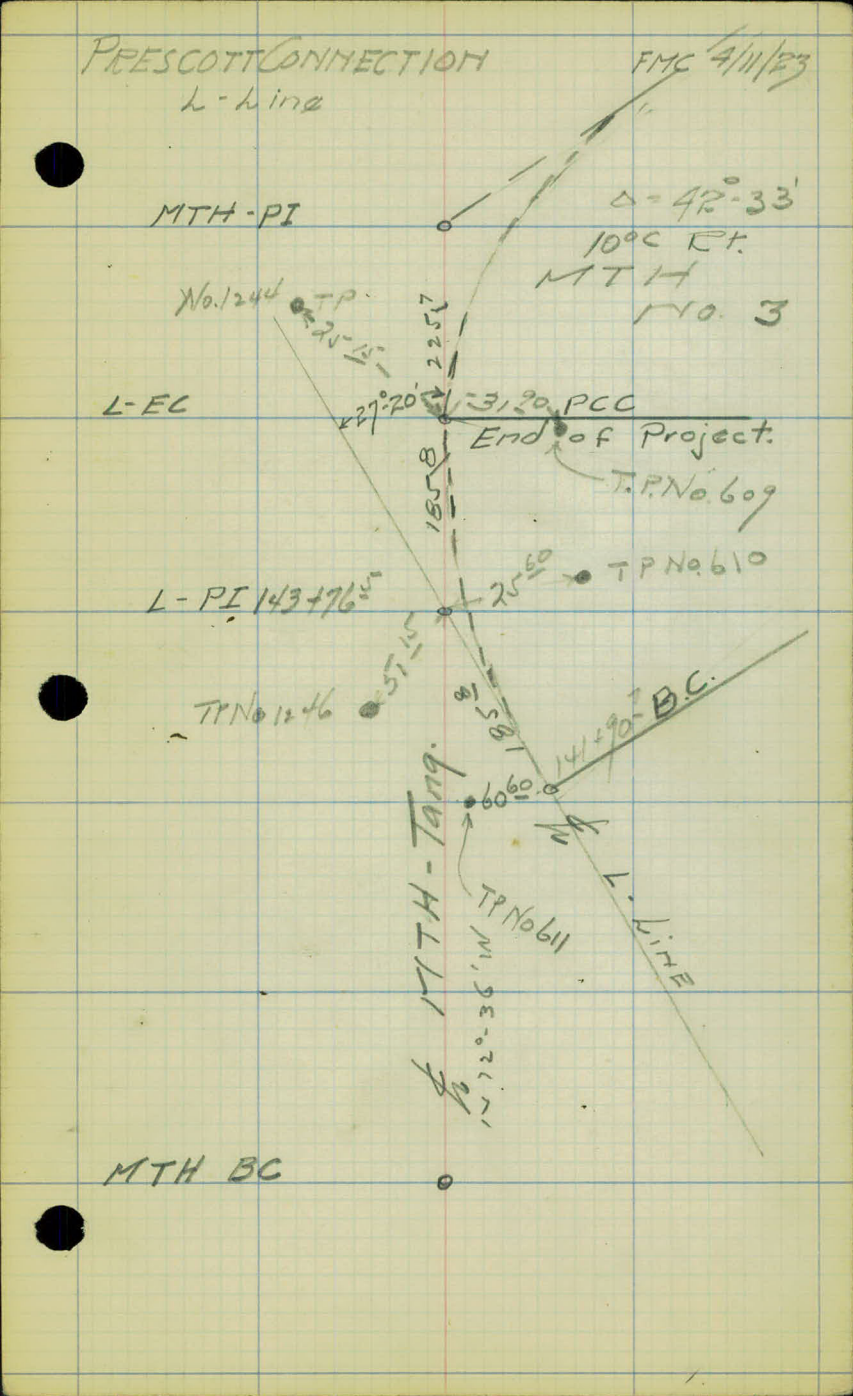
L-Line





near Sta 138+40

Sta.	P.T.	Lt. Δ	Ct.	Calc. Bear.
				N 72° - 36' W
	+55.1' EC		13-40	PI = 143+76.5
				Δ = 27° - 20'
145			11-36	7° - 30' C Rt.
				T = 185.8
	+50		9-43½	LC = 364.4
				Def. for ft = 1.25 min
144			7-51	
	+50		5-58½	
143			4-06	
	+50		2-13½	
142			0-21	
141+90.7	BC		0 0	
				S 80° - 04' W


PRESCOTT CONNECTION
L - Line
FMC 4/11/23
MTH - PI
Δ = 42° 33'
10°C Ct.
MTH
No. 3
No. 1244 TP
25 - 12
22.57
L - EC
27° 20'
31.90 PCC
End of Project.
T.P. No. 609
165.78
TP No. 610
L - PI 143+76.54
25.60
TP No. 1246
57.44
158.81
141+90 - BC
60.60
MTH - Tang.
TP No. 611
N 11° 36' 21" W
L - Line
MTH BC

Sta	Pt.	Lt. Δ Rr	Cal. Bear.
123		7-30½	
+50		6-53	
122		6-15½	
+50		5-38	
121		5-00½	
+50		4-23	
120		3-45½	
+50		3-08	
119		2-30½	
+50		1-53	
118		1-15½	
117+50		0-38	
116+99.3	BC	00	

PI=
Δ = 36°-00'
R = 30' C Lt.
T = 744?
LC = 1440?
Def. pr. ft. = 0,75 / Min.

PRESCOTT CONNECTION
LA line

F.M.C. 4/16/23

Lt Δ Rt

N32°-50' W

135+68.5 PT 30-00

PI = 135+68.5
Δ = 30°-00
10°C Rt
T = 153.5
Lc = 300.0
Deg of Curve = 3 min

137+15.0 EC 15-00

137 14-15

+50 11-45

136 9-15

+50 6-45

135 4-15

+50 1-45

134+15.0 EC 00

N62°-50' W

L 131+83.9 = L H 131+83.9

PRESCOTT CONNECTION
LA line

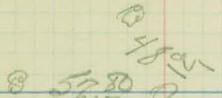
FMC 9/16/23

142+34.0 PT	57.10
+93.5 ✓ EC	28.35
+50	26.25
144	23.55
+50	21.25
143	18.55
+50	16.25
142	13.55
+50	11.25
141	8.55
+50	6.25
140	3.55
+50	1.25
139+21.5 BC ✓	00

PT = 142+34.0
Δ = 57° 10'
10° C
T = 312.2 ✓
LC = 571.7 ✓

PRESCOTT CONNECTION
LH - line

F.M.C. 9/16/23.



168+50 POT on pole line W. of road on Sec. line Aprox 1300 ft. N.

153+68 = MTH 257+93

153+50 POT Aprox Center MTH No. 3

PRESCOTT CONNECTION
LA Line

F.M.C. 4/16/23

89-60
59-58
N 30-02 W

TP
1410
TP
N 59°-58'-
N 30-02 W
MTH N 29-53 W
+12

TP
93.8
N 21 E
TP

station line
sta 156 POT

ARTIFICAL TOPOG.
PRESCOTT-CONNECTION
Sta 23+00 to 145+50 55.1
4/11 to 4/12 - 1923
PARTY - Conner
Railing
Franke

29

28

27

26

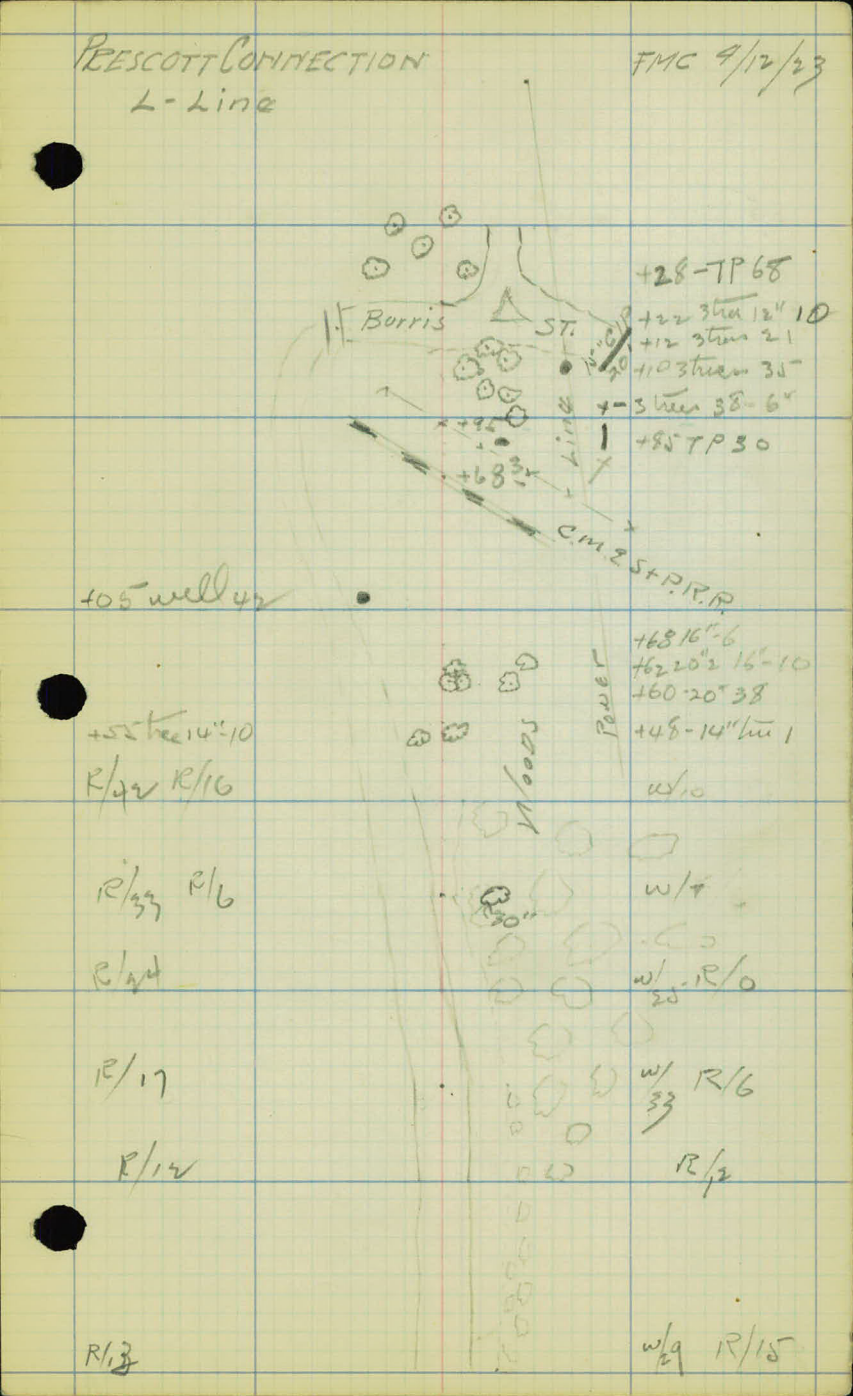
25

24

23

PRESCOTT CONNECTION
L-Line

FMC 9/12/23



35

34

33

32

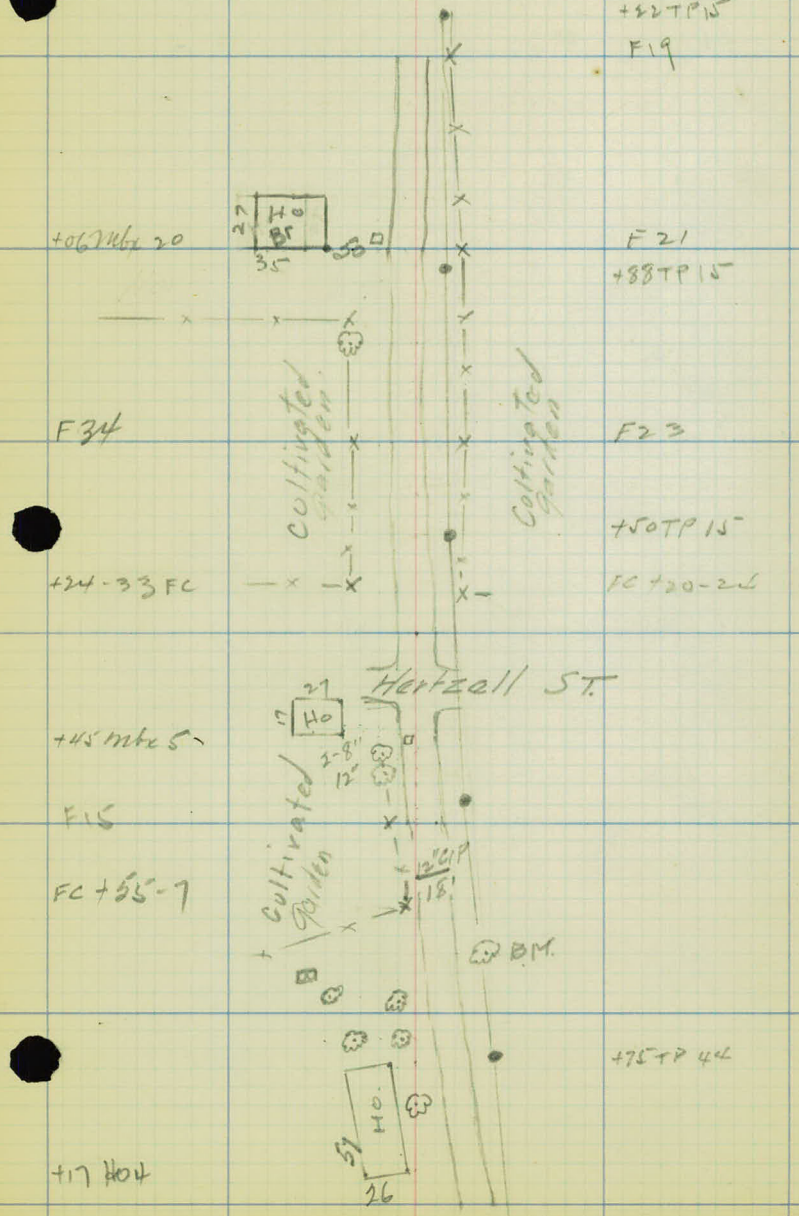
31

30

29

PRESCOTT CONNECTION
L - Line

FMC 9/12/23



41

40

39

38

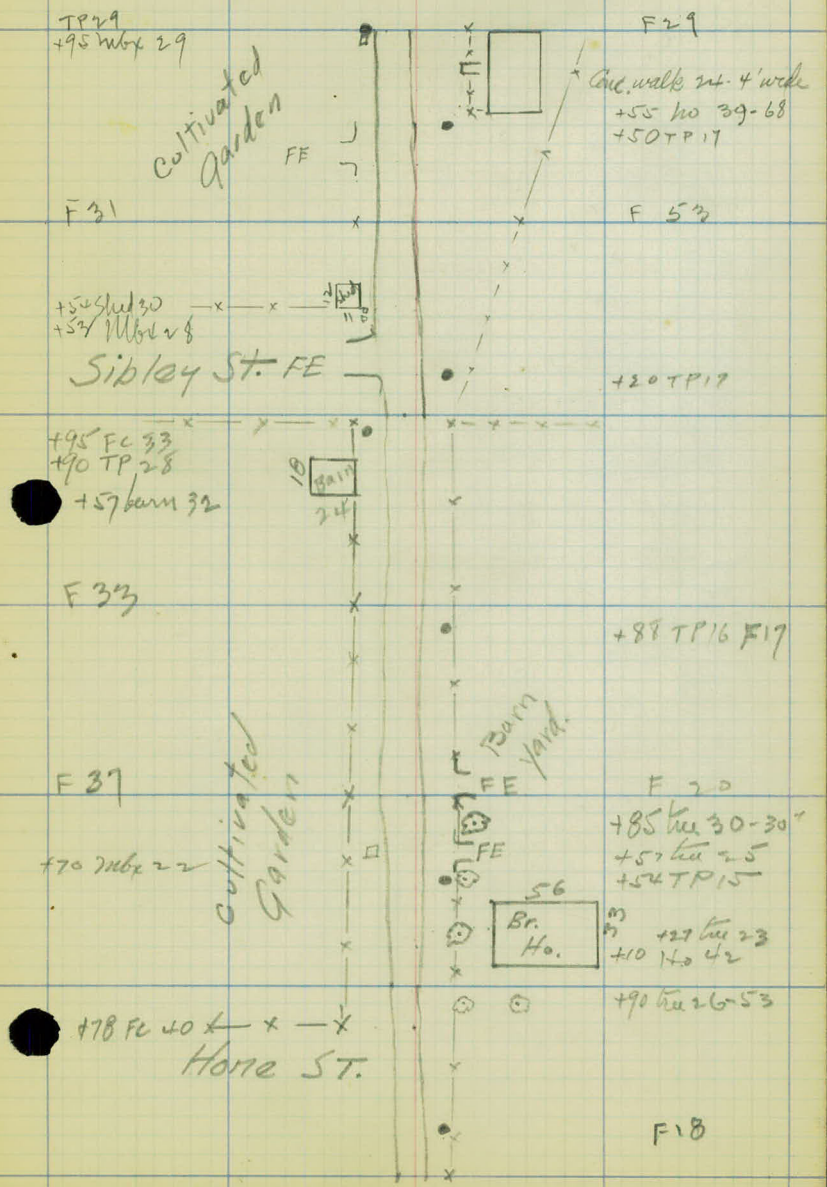
37

36

35-

PRESCOTT CONNECTION
2- Line

FMC 4/12/23



47

46

45

44 PI

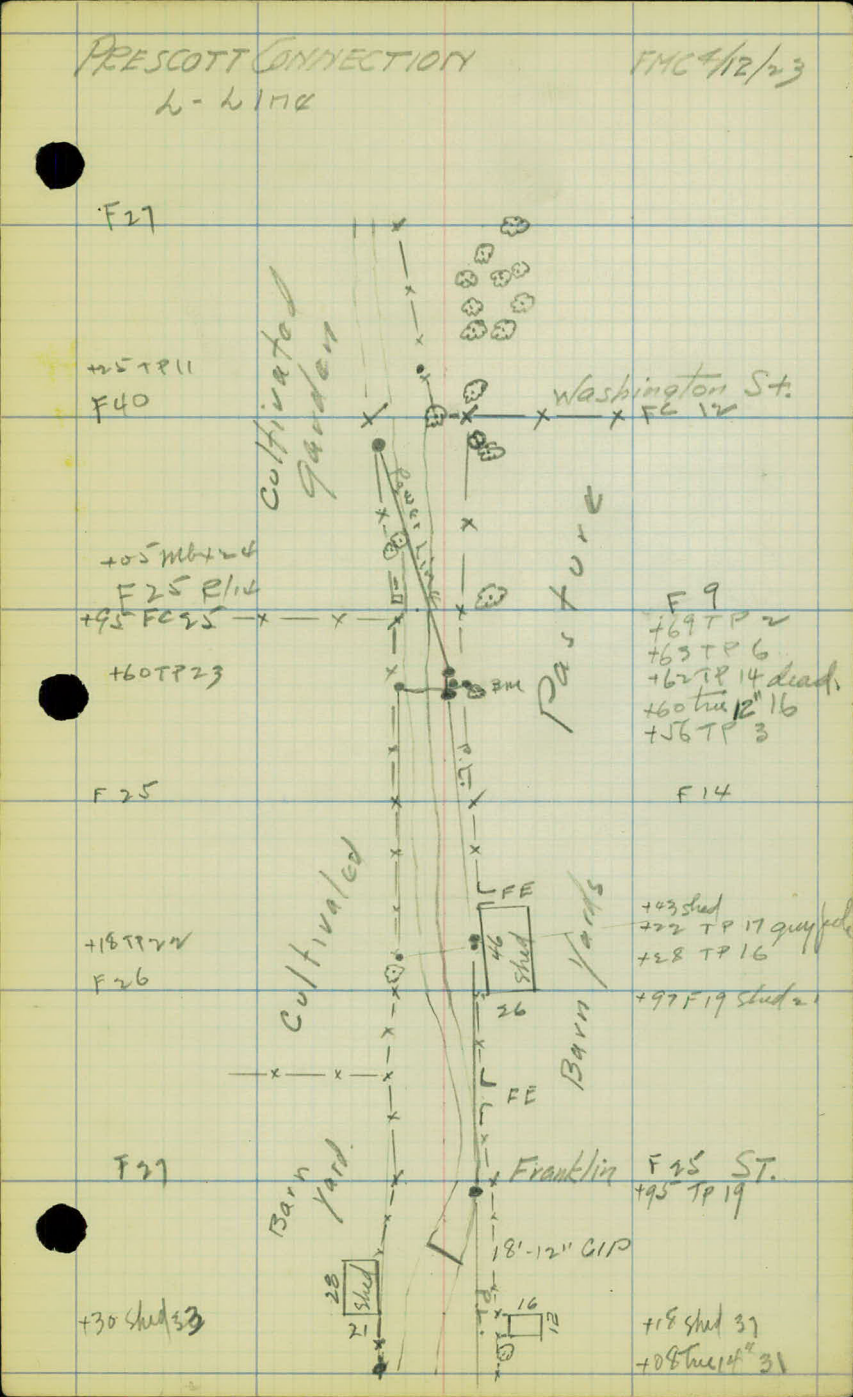
43

42

41

PRESCOTT CONNECTION — FMC 4/12/23

2 - 2 line



53

52

51

50

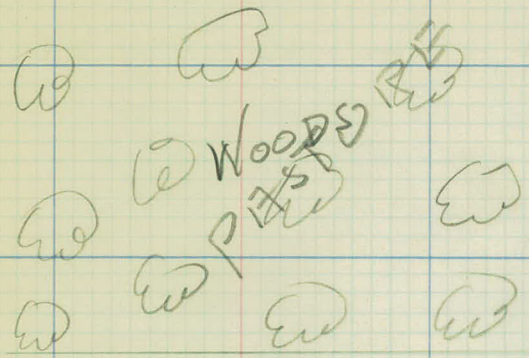
49

48

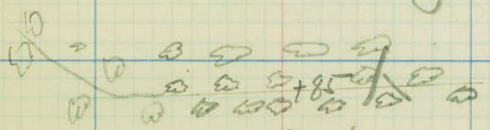
47

PRESCOTT CONNECTION
2 - Line

FMC 9/12/23



OAK. St.
(+25' on plan.)



F60

+12 - 18" tree 13

59

58

57

56

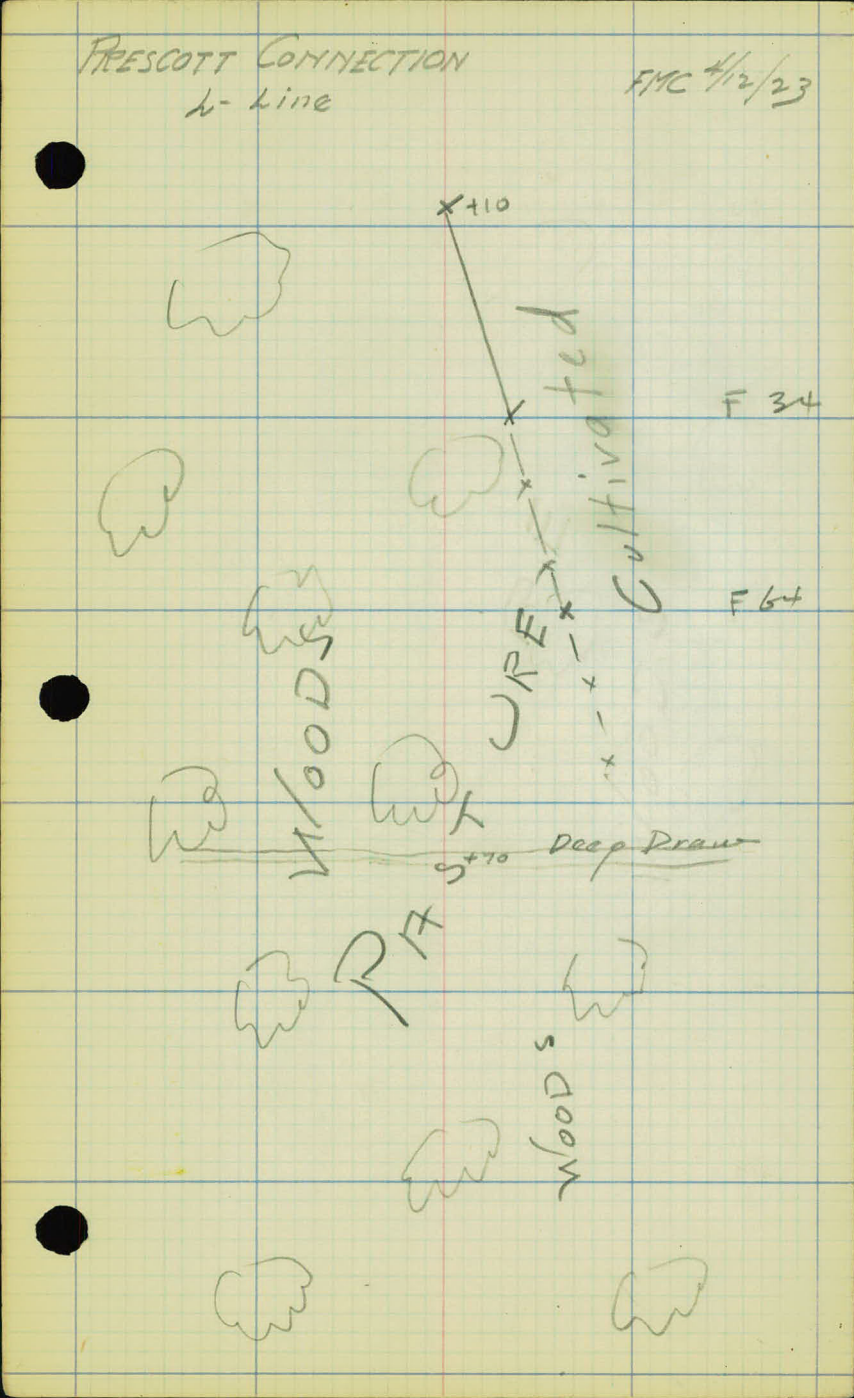
55

54

53

PRESCOTT CONNECTION
L- Line

FMC 4/12/23



65

64

63

62

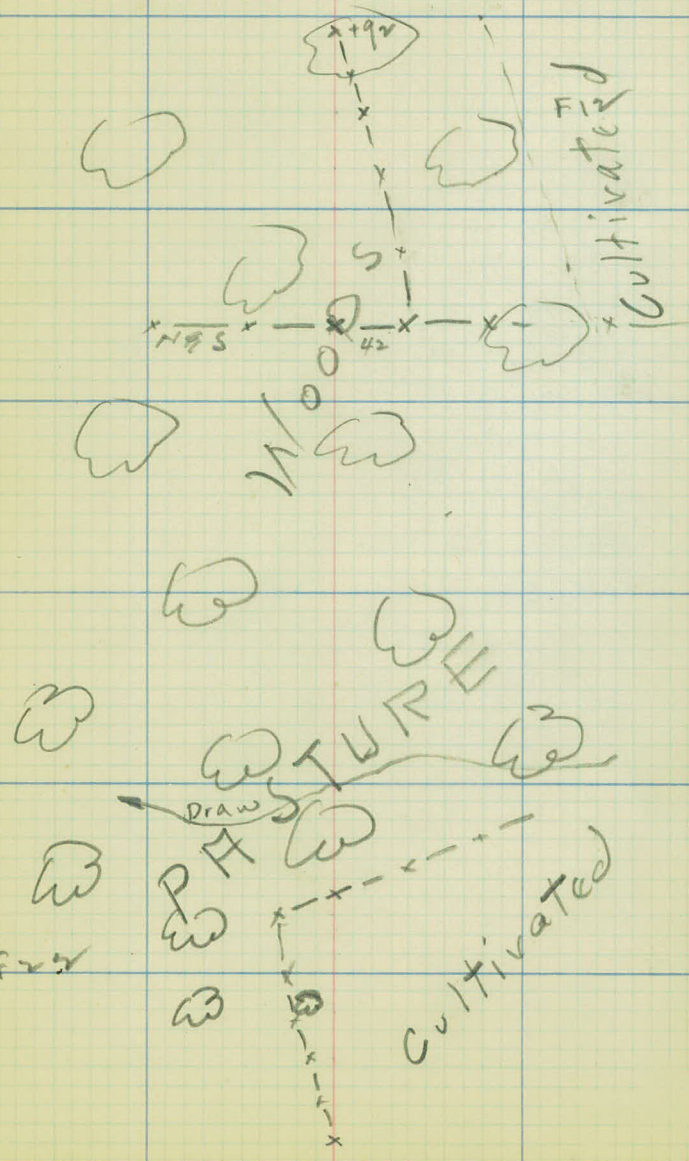
61

60

59

PRESCOTT CONNECTION
L-Line

FMC 4/12/23



71

70

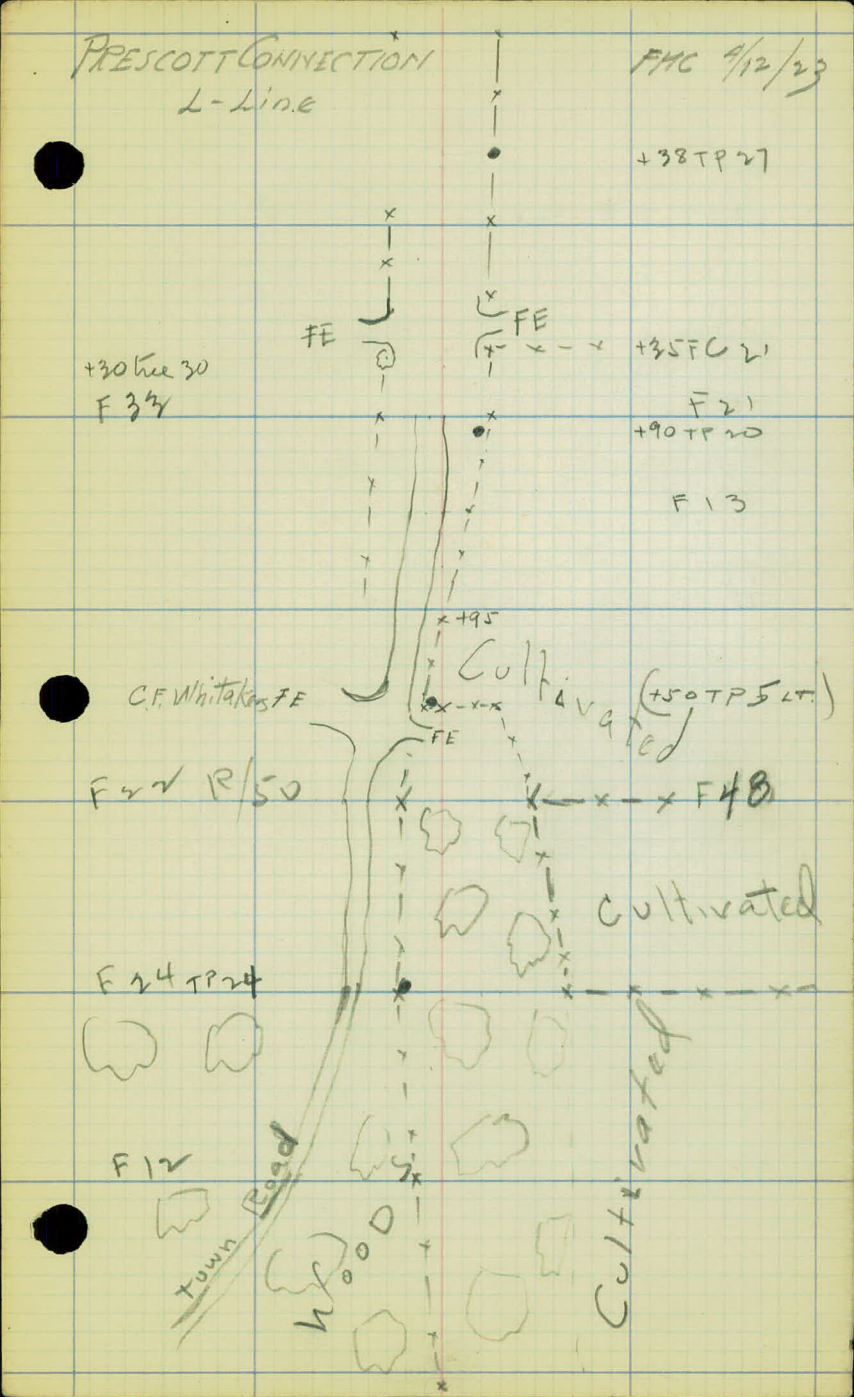
69

68

67

66

65


PRESCOTT CONNECTION
L-Line
FHC 9/12/23
+38 TP 27
FE
FE
+35 FC 21
+30 Tree 30
F 33
F 21
+90 TP 20
F 13
+95
C.F. Whitaker's FE
Cultivated
(+50 TP 5 Lt.)
FE
F 48
Cultivated
F 24 TP 24
F 12
Town Road
Cultivated

77

76

75

74

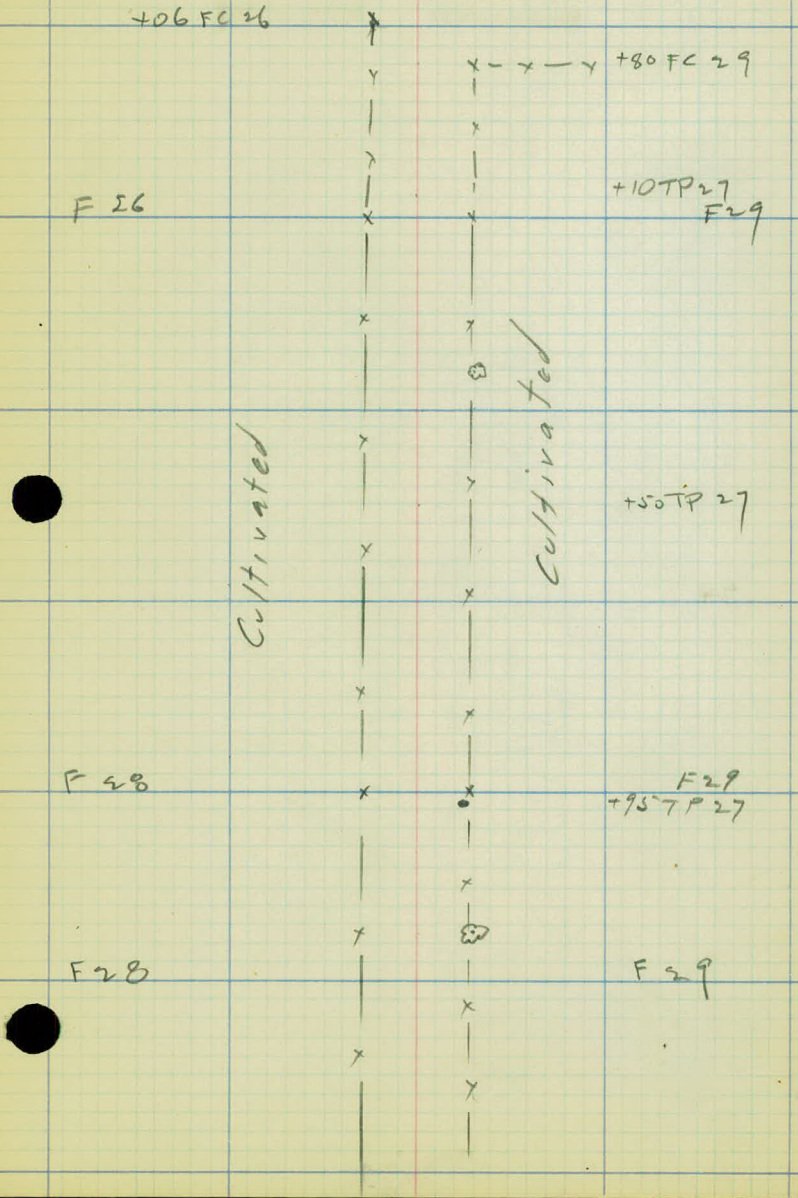
73

72

71

PRESCOTT CONNECTION
2 - Line

FMC 9/12/23



83

82

81

80

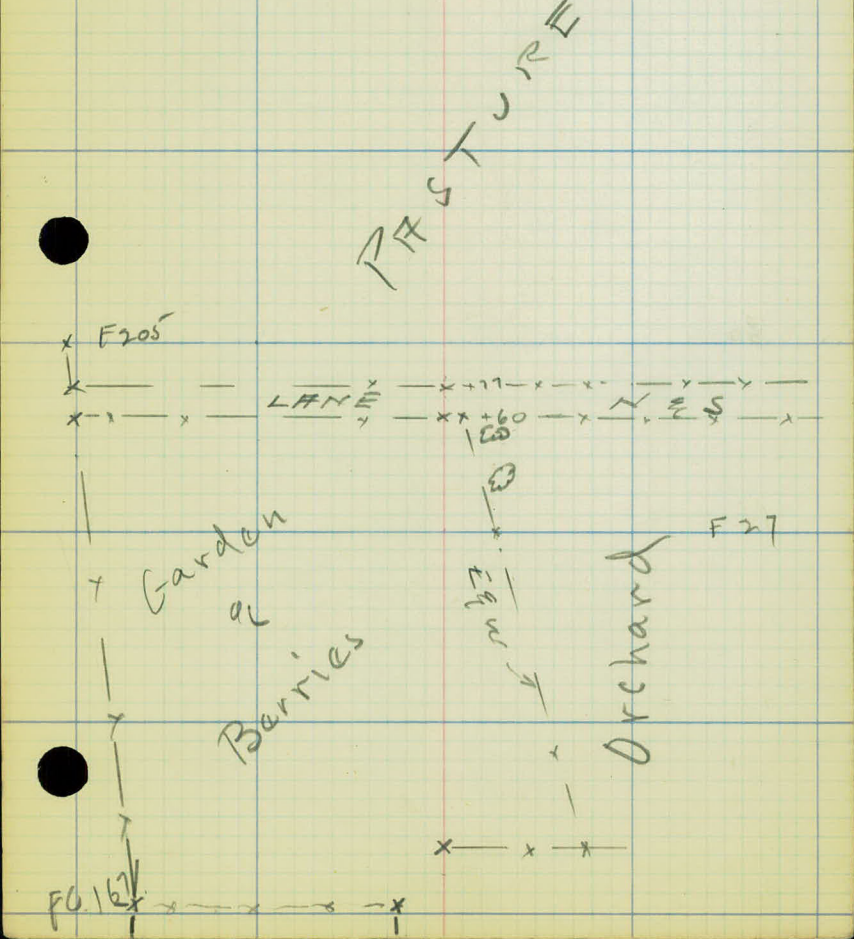
79

78

77

PRESCOTT CONNECTION
L-Line

FMC 9/12/23



89

88

87

86

85

84

83

Prescott Connection
L-Line

FMC 9/12/23

Pasture

95

94

93

92

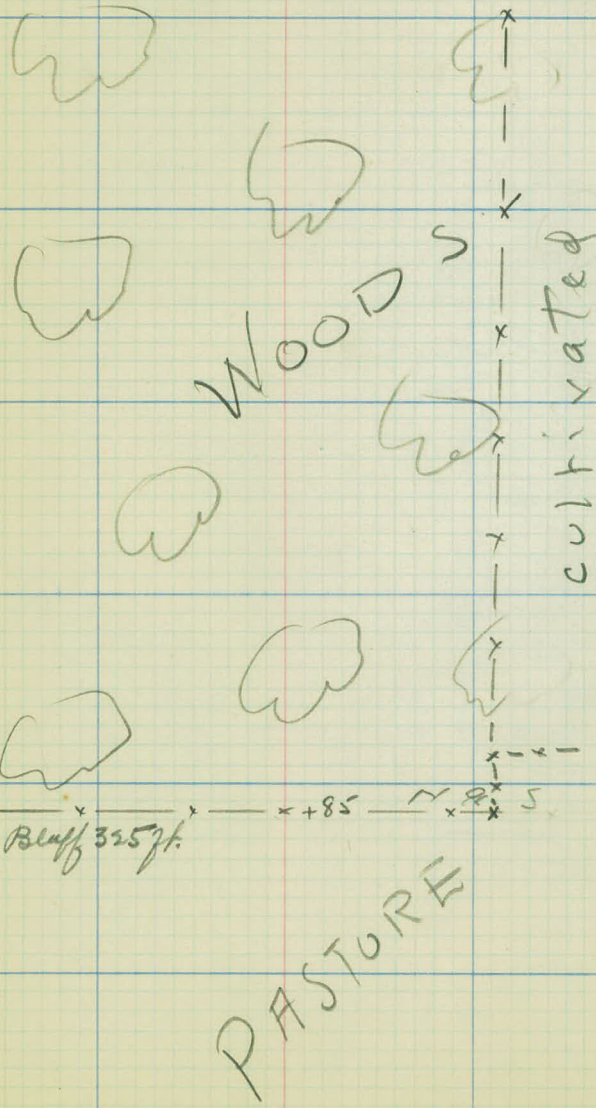
91

90

89

PRESCOTT CONNECTION
L - Line

FMC 9/12/23



101

100

99

98

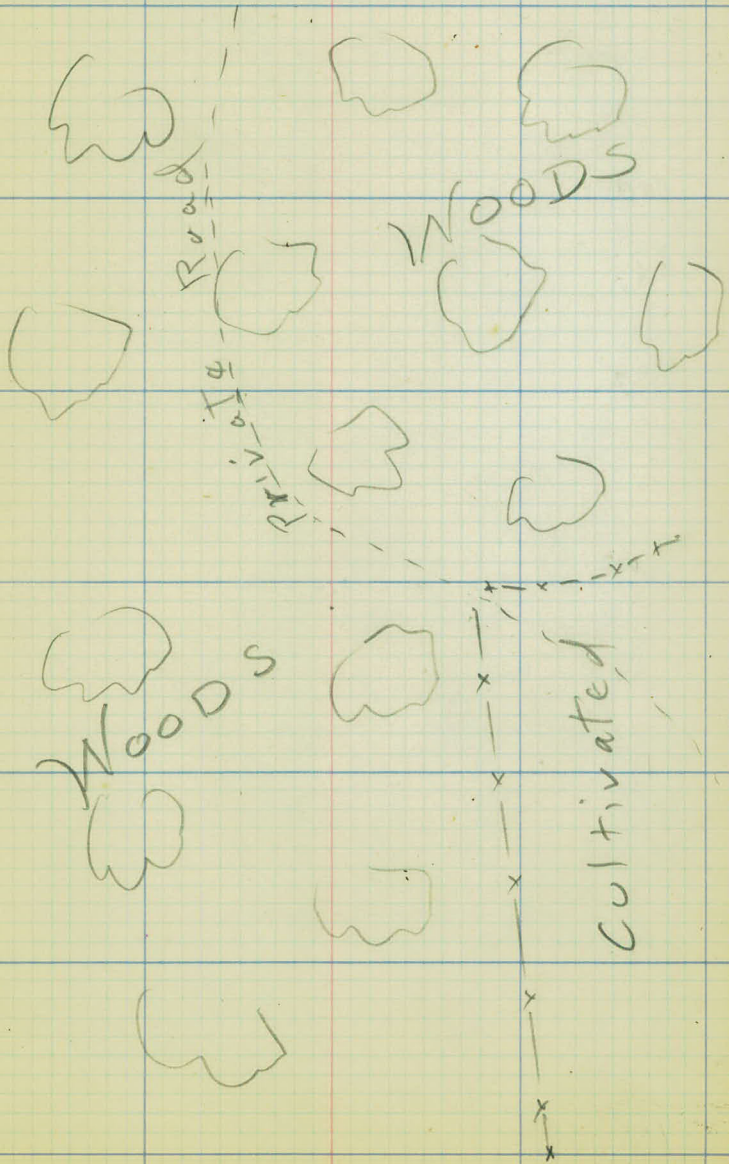
97

96

95

PRESCOTT CONNECTION
L-Line

FMC 4/2/23



107

106

105

104

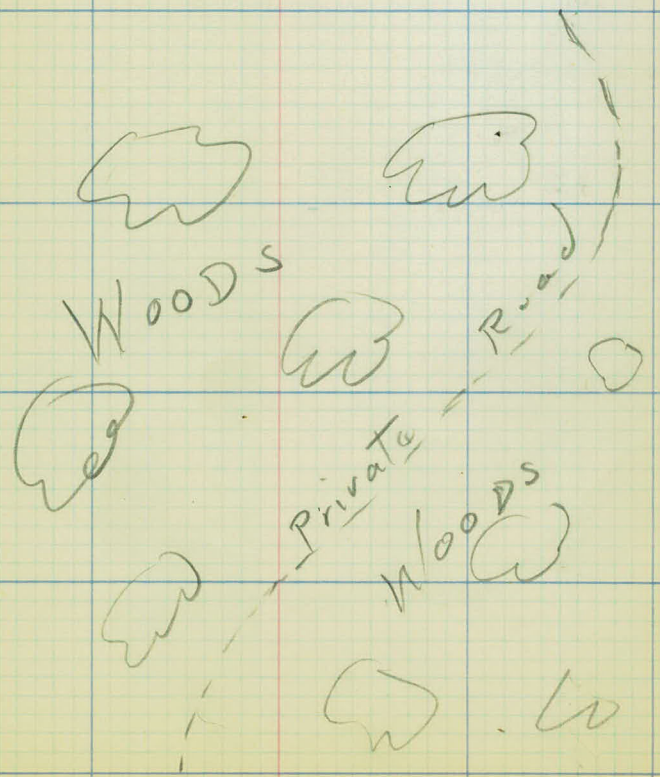
103

102

101

PRESCOTT CONNECTION
L-Line

FMC 4/12/23



109

108

107

106

105

104

103

PRESCOTT CONNECTION
L-Line

FMC 4/11/23

F/50

1K 107+75

Road to Private Cut.

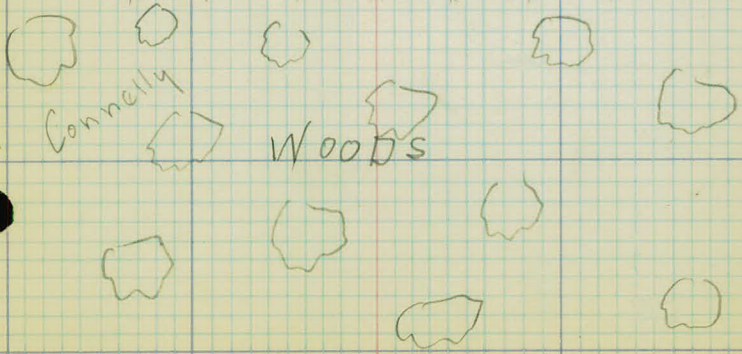
Cultivated

Connelly

x — x — x — x — x — x — x + R/150

Connelly

Woods



115

114

113

112

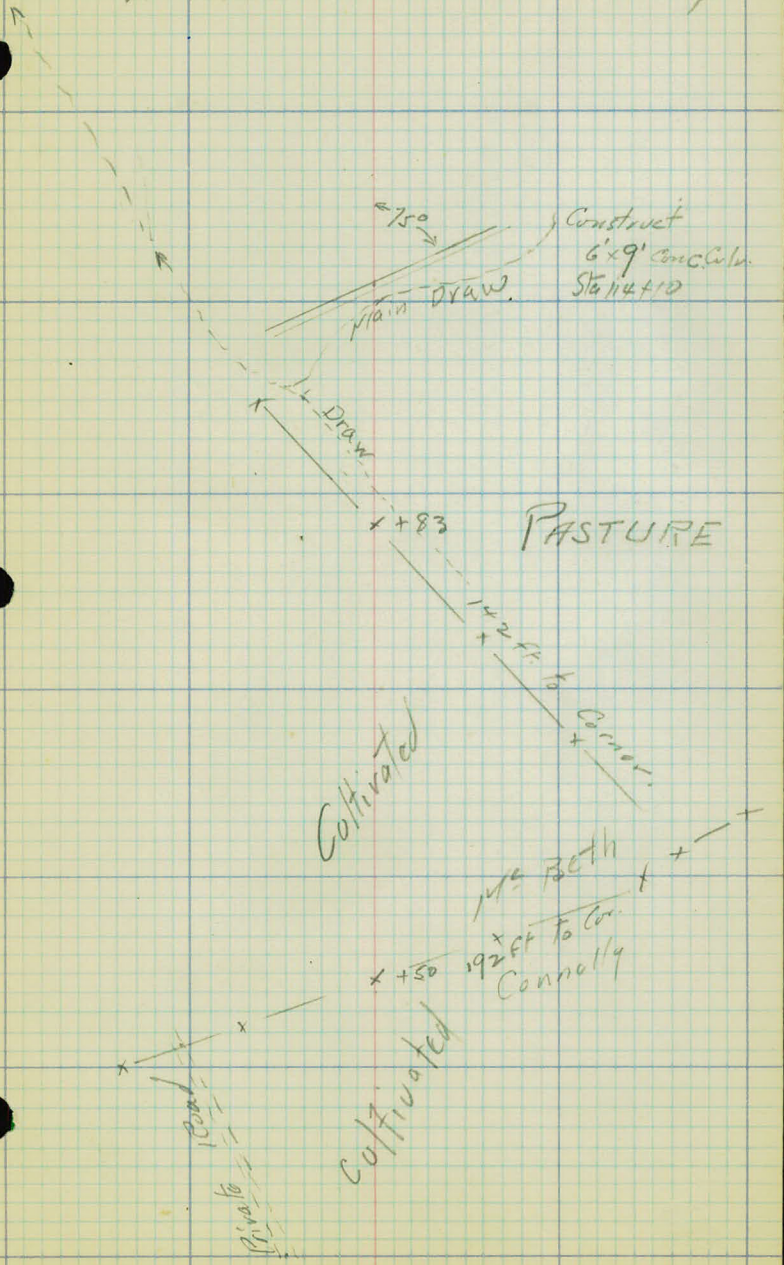
111

110

109

PRESCOTT CONNECTION
L - Line

FMC 9/11/23



121

120

119

118

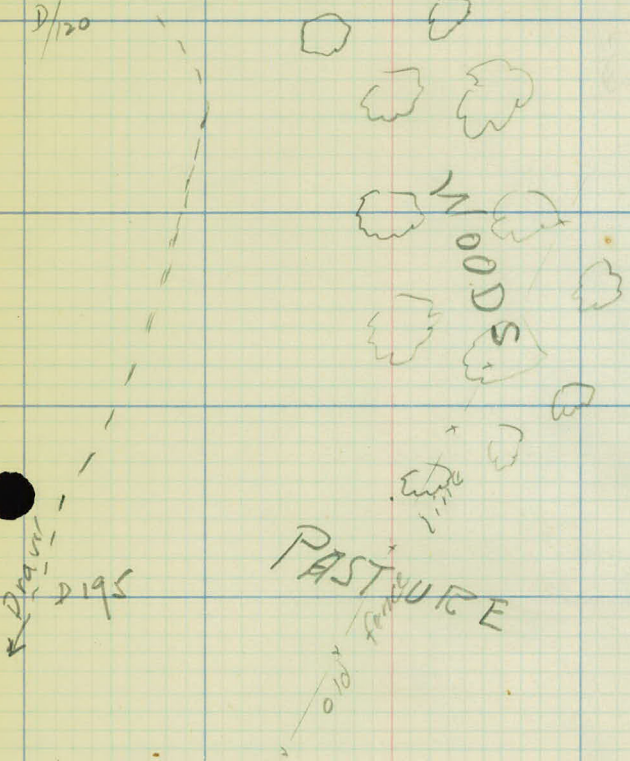
117

116

115

PRESCOTT CONNECTION
L-LINE

FMC 9/11/23



127

126

125

124

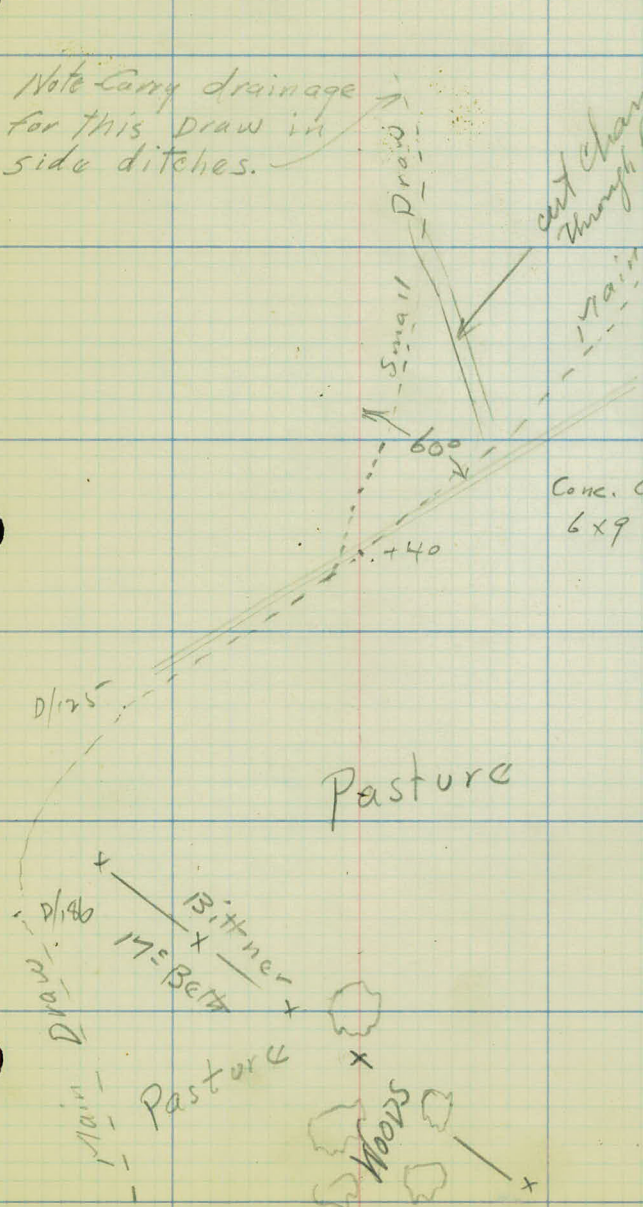
123

122

121

PRESCOTT CONNECTION
2-Line

FMC 4/11/23



133

132

131

130

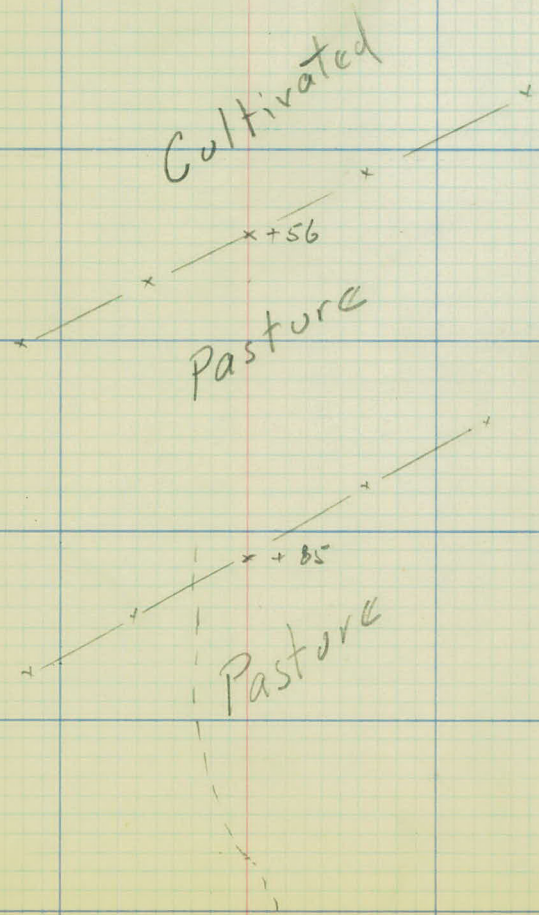
129

128

127

PRESCOTT CONNECTION
L-Line

FMC 9/11/23



139

138

137

136

135

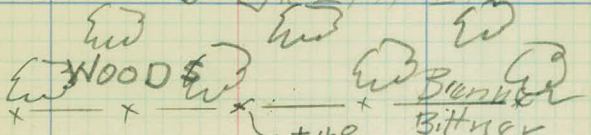
134

133

PRESCOTT CONNECTION
L - Line

FMC 3/11/23

J. BRENNEN



Cultivated

Cultivated

145

144

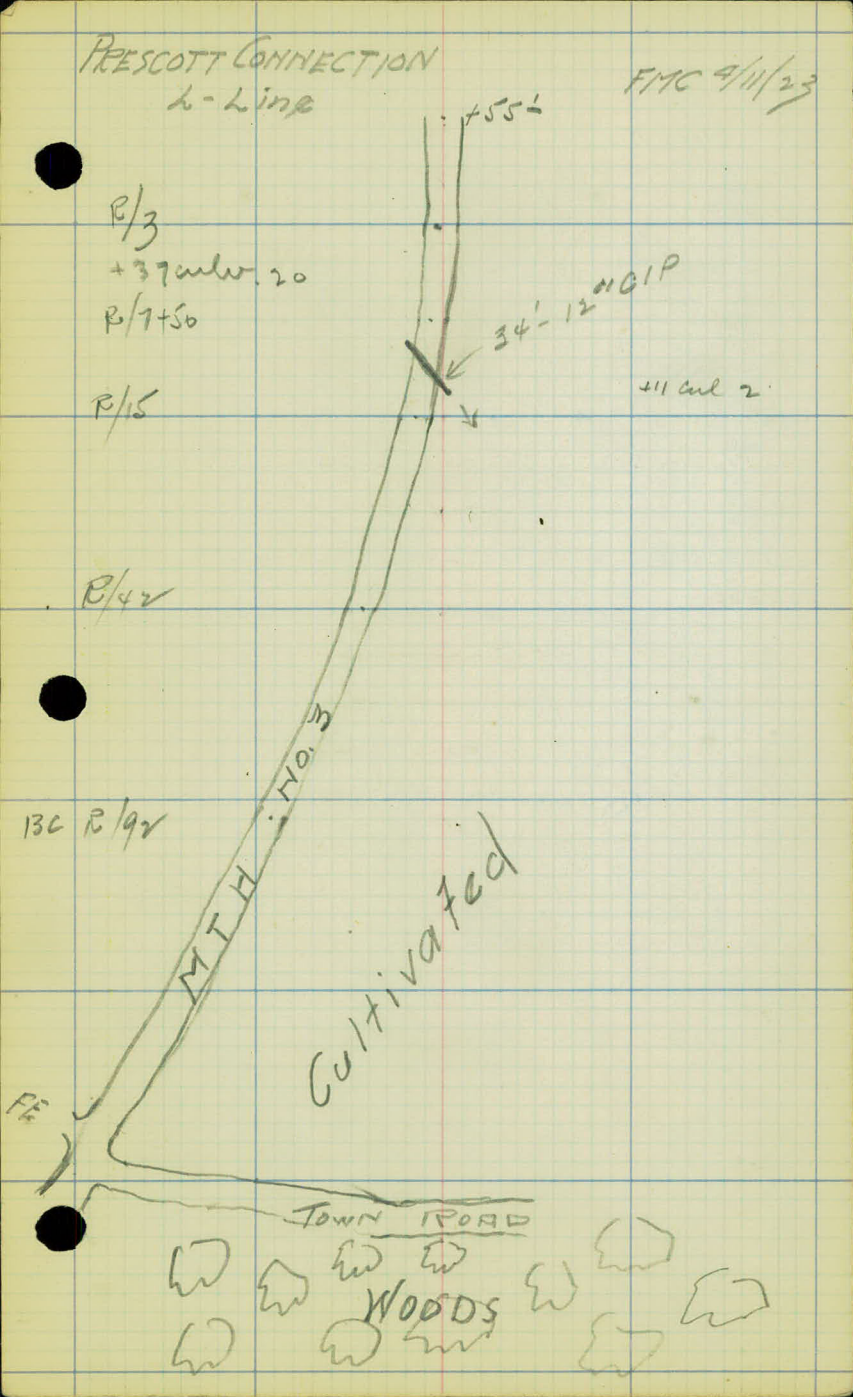
143

142

141

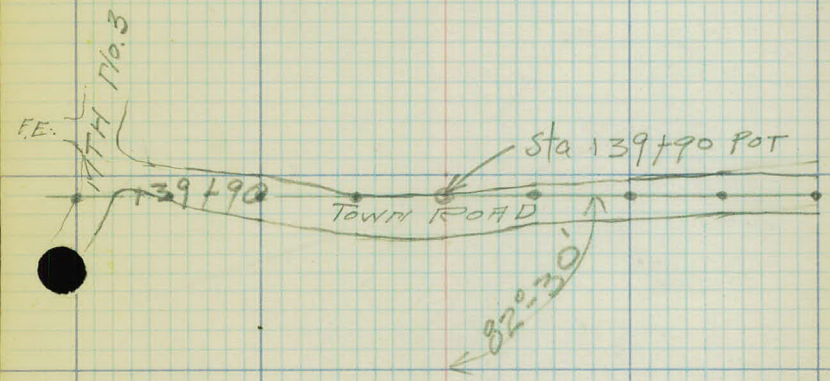
140

139


PRESCOTT CONNECTION
L-L Line
FMC 9/11/23
+55±
R/3
+37 curv. 20
R/7+56
34'-12" HGIP
+11 curv 2
R/15
R/42
MTH No. 3
13C R/92
Cultivated
PE
TOWN ROAD
WOODS

PRESCOTT CONNECTION
R-Line R. line
FMC 9/11/23

OVERHEAD ROAD X ING
Aprox Sta 139+80 - L line



139+25 ± EL

PRESCOTT CONNECTION
LA Line

FMC 4/16/23

138

137

136

135

134

133

132

PRESCOTT CONNECTION
LA - Line

F.M.C. 4/16/23

CENTIGRADE

FAHRENHEIT

144

143

142

141

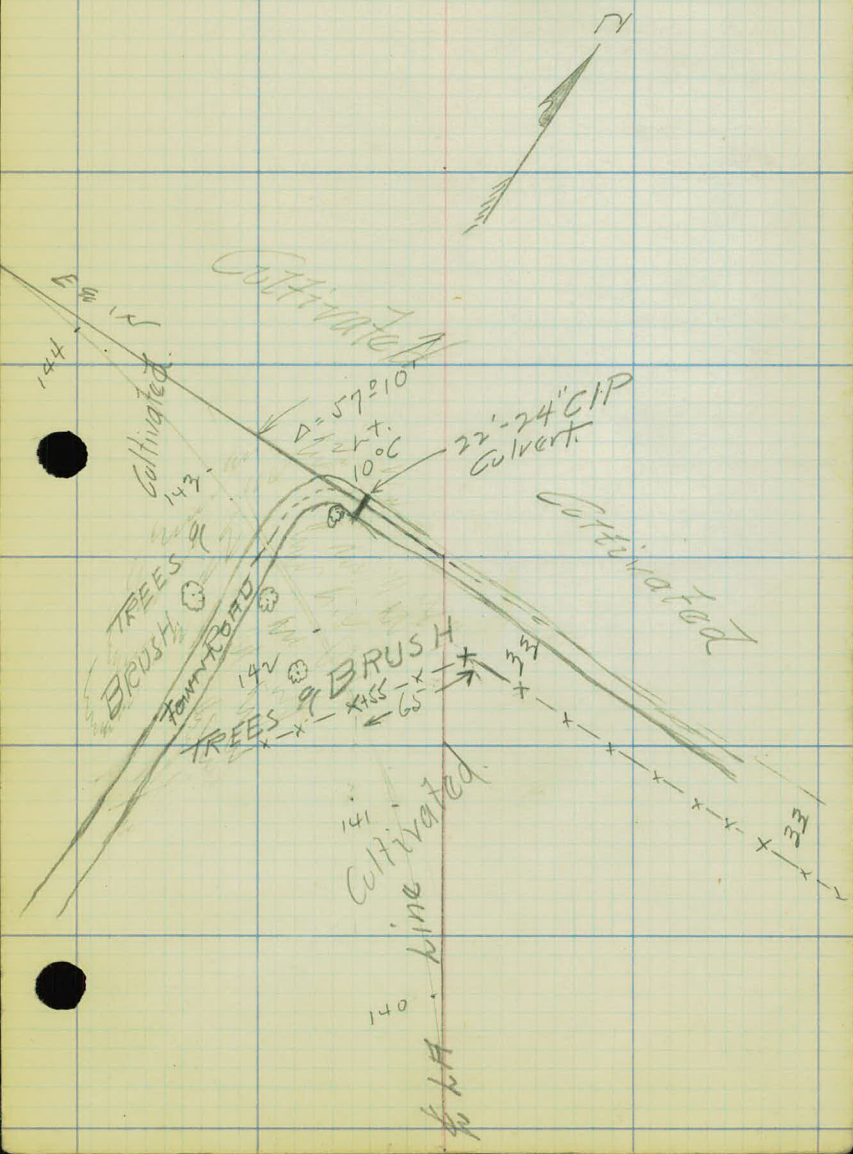
140

139

138

Prescott Connection
L.A. - Line

FMC 9/16/23



150

149

148

147

146

145

144

PRESCOTT CONNECTION
L7 - Wing

FMC 4/16/23

156

155

154

153

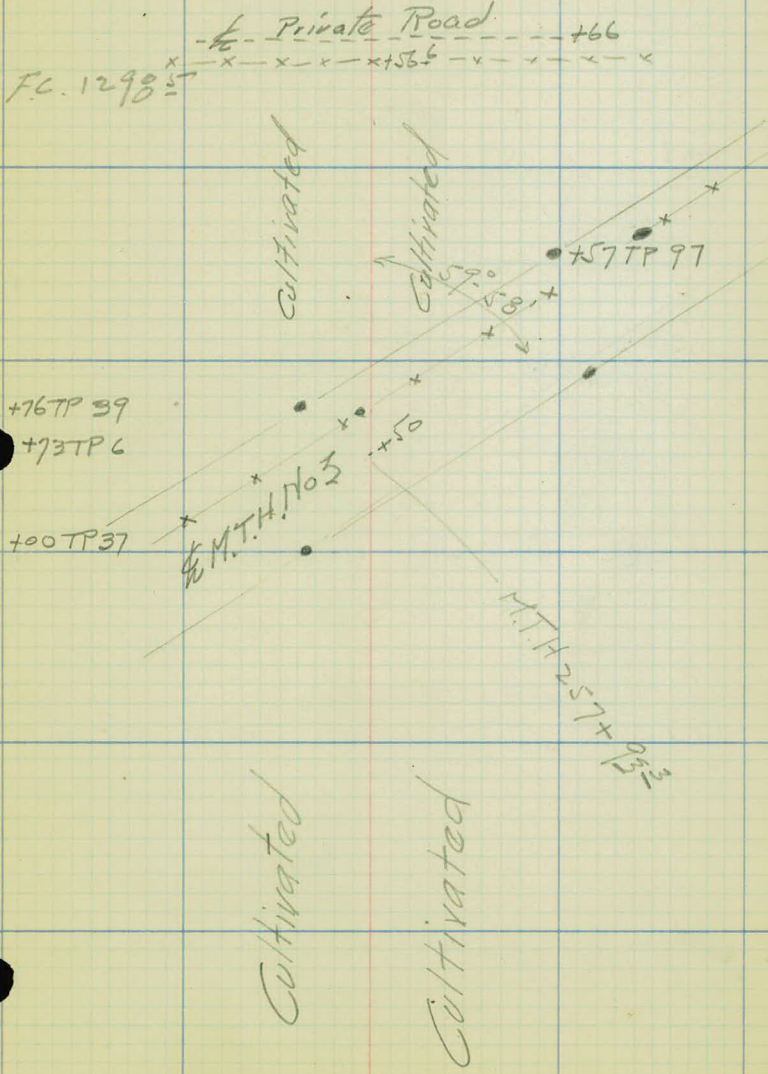
152

151

150

PRESCOTT CONNECTION
LA - Line

FMC 9/16/23



162

161

160

159

158

157

156

RESCOTT CONNECTION
47 Line

Cultivated

Cultivated

FMC 4/16/23

168

167

166

165

164

163

162

PRESCOTT CONNECTION
LA-2 line

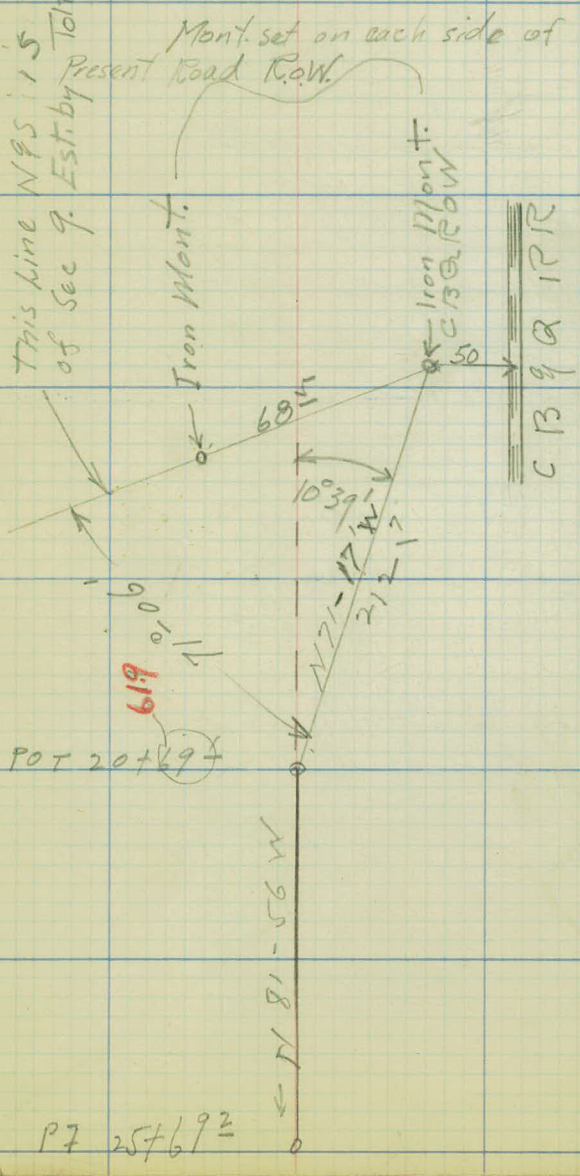
FMC 4/16/23

Cultivated

Cultivated

Section Ties
L-Line

F.M.C. 4/17/23



South on sec line from ¼ Cor
between Sec 8 & 9
465 ft. to fence E & W thence
71 ft. East to Large Cor. Post ⅞

Commencing at Sec Cor
4-5-8-9 Thence west.

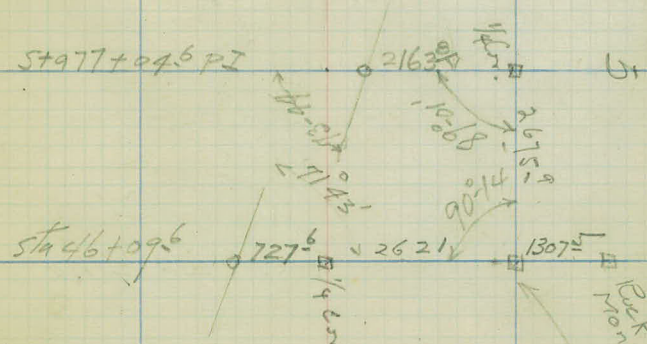
674 ft. west to fence N E S
1336 " " " " N E S
3644 " " " " N 9 S
2675 ft. 1/4 Cor but Sections 5/8

Thence South to ∠ PI Sta 77+06
2163.8 ft. Thence angle
Lt. 73°-14' sighted at
E C Sta 71+68.2

(Dist from 1/4 Cor to Stone on
sect line North 25.95 ft.
Re chained 9/18/23.
but Sec. 8 & 9

Section Ties
½-Line

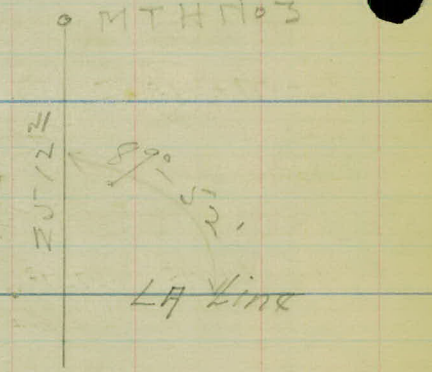
FMC 9/7/23



Cross Roads in Wisconsin

4/17/23

Commencing at PI on MTH No 3 a pool 296 and thence South on tang 2 North produced 1160 ft. good find corner possibly 1/4 Cor 65 ft. to East or west. 1500 ft. bottom of dup draw 2S 12 E 2 ft. to LA Hunt Site/68+27 Sur ∠ = 89° 52'



1160
1320
160

P.J.C. 4/4/23

Center Elev. on the
Prescott Connection
L. Line.
April 4, to April 11, 1923.

Crane Level,
Stark Rod.

Proj. 23 - 60

Sta	B.S.	H.I.	F.S.	Rod	Elev.
B.M.	7.92	713.06			705.14
21				4.2	708.9
22				4.2	708.9
23				3.9	709.2
23+95.7 B.C.				4.1	709.0
24+50				4.6	708.5
25				5.4	707.7
25+50				8.6	704.5
T.P.	11.00	719.28	4.78		708.28
26				13.6	705.7
+36				13.3	706.0
+50				10.2	709.1
27				4.5	714.8
+28				0.3	719.0
T.P.	12.25	731.38	0.15		719.13
27+50				3.8	727.6
27+65				2.95	728.43
27+73				3.19	728.19
				2.78	728.60
				3.24	728.14
27+79				3.7	727.7
27+87				7.3	724.1
28				7.1	724.3
28+32				8.4	723.0
28+45				7.6	723.8

Prescott Cont. P.J.C. 4/4/23

L. Line

On blazed Cottonwood tree Sta. 20+80 to. right

Top of S. Rail

Top of N Rail

Top of N. Rail 100' L. of ℄

Top of N. Rail 100' R. of ℄

Center of Road

Sta.	B.S.	H.I.	F.S.	Rod	Elev.
		731.38			
28+70				3.9	727.5
29				2.4	729.0
T.P.	9.23	739.91	0.70		730.68
29+45				7.5	732.4
30+01.4	R.O.T.			6.1	733.8
B.M.				1.87	738.04
31				5.0	734.9
32				3.3	736.6
33				1.4	738.5
T.P.	9.03	748.07	0.85		739.06
34				7.6	740.5
35				6.3	741.8
36				4.3	743.8
37				1.8	746.3
T.P.	12.47	760.04	0.52		747.57
38				11.2	748.8
39				9.4	750.6
39+50				8.1	751.9
40				3.1	756.9
41				3.4	756.6
T.P.	11.62	771.11	0.55		759.49
42				9.4	761.7
42+21				6.2	764.9
43				2.5	768.6
B.M.				4.24	766.87

Prescott Cont. P.J.C. 4/4/23

L. Line

Sp. in Cottonwood tree 45' R Sta 30+30

Sp. in Elm tree 25' L. Sta 43+10

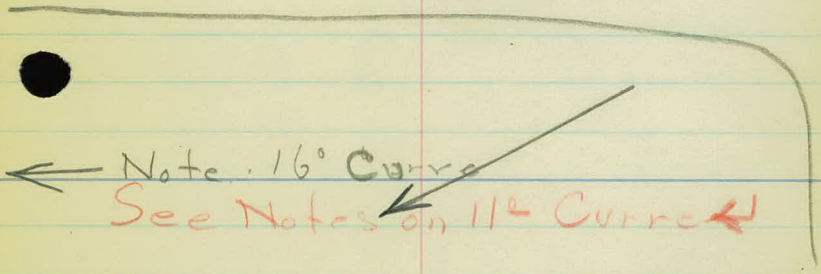
Sta.	B.S.	H.I	F.S.	Rod	Elev.
		771.11			
T.P.	12.65	783.04	0.72		770.39
44 P.I.				10.8	772.2
B.M.				3.72	779.32
45				6.8	776.2
46				2.7	780.3
T.P.	10.92	793.55	0.41		782.63
47				9.5	784.1
48				5.5	788.1
T.P.	4.27	795.94	1.88		791.67
48+30				4.7	791.2
48+59 P.O.T.				6.0	789.9
48+70				8.7	787.2
T.P.	3.77	786.81	12.90		783.04
48+79.8 B.C. 16° Curve			See →	10.9	775.9
T.P.	1.17	775.08	12.90		773.91
48+82				4.8	770.3
48+97				4.9	770.2
49				3.1	772.0
T.P.	12.92	804.59			791.67
49+25				10.6	794.0
49+50				4.4	800.2
T.P.	7.39	811.54	0.44		804.15
50				4.4	807.1
+50				6.4	805.1

Prescott Cont. P.J.C. 4/4/23

L. Line

Sp. in blazed tree 15' R, Sta 44+60

On Rock 4' L. Sta. 49+25



On Rock. 6' L. Sta. 49+25

Sta.	B.S.	H.I	F.S.	Rod	Elev.
		811.54			
51				8.0	803.5
51+50				6.9	804.6
51+78.7 E.C.				6.9	804.6
52				5.6	805.9
52+25				2.0	809.5
52+43.1 = E.C. of 11° Curve					
52+60 B.C.				2.1	809.4
T.P.	8.54	819.93	0.17		811.37
53				8.2	811.7
53+27				2.4	817.5
53+50 P.O.C.				2.4	817.5
54				7.0	812.9
54+30				10.0	809.9
54+50				12.2	807.7
54+55				12.9	807.0
54+75				9.3	810.6
55 P.O.C.				9.0	810.9
T.P.	8.53	814.19	12.27		807.66
B.M.				0.47	815.72
55+30				11.6	804.6
T.P.	0.18	803.83	12.54		803.65
55+40				3.1	800.7
T.P.	1.16	792.46	12.53		791.30
T.P.	3.73	784.03	12.16		780.30
B.M.				5.11	778.92
55+70				5.00	779.0

Prescott Cont. P.J.C. 4/17/23

L. Line

Center Elev. from
Sta. 48+00 to 51+43.1 E.C.
on 11° Curve.

Crane Level
Stark Rod.

Sta.	B.S.	H.I.	F.S.	Rod.	Elev
B.M.	11.24	790.56			779.32
48				2.3	788.3
+08.1 B.C.				1.9	788.7
T.P.	3.00	792.87	0.69		789.87
48+30				2.1	790.8
+50				2.3	790.6
+60				1.8	791.1
+75				2.1	790.8
B.M.				1.16	791.71
T.P.	1.76	782.87	11.76		781.11
48+82				8.3	774.6
+86				10.0	772.9
+93				12.3	770.6
+98				11.7	771.2
49.				9.3	773.6
+10				7.7	775.2
+15				2.7	780.2
T.P.	13.01	795.78	0.10		782.77
T.P.	11.23	806.15	0.86		794.92
49+21				10.7	795.5
+35				6.4	799.8
+50				3.0	803.2
T.P.	9.84	815.56	0.43		805.72
50				3.3	812.3
+10				2.2	813.4

Prescott Cont. P.T.C. 4/17/23

L. Line 11° Curve

Sp. in blazed tree 15' R. Sta. 44+60

On Rock 4'L. Sta 49+25 on 16° Curve

Sta,	B.S.	H.I.	F.S.	Rod	Elev.
		815.56			
50+40				2.2	813.4
+50				4.0	811.6
51				7.5	808.1
+15				8.8	806.8
+50				8.0	807.6
+90				8.5	807.1
52				7.6	808.0
+13				5.8	809.8
+43.1 P.T. E.C. = Equation?				5.7	809.9
Sta. 50 on 16° Curve				8.4	807.2

Prescott Cont. P.J.C. 4/17/23

L. Line 11° Curve

Check, O.K.

ELEV.

Prescott Cont. P.J.C. 4/5/23

L. Line.

Sp. in blazed Oak tree 10' R. Sta 54+95

Sp. in ground on ℄ at Sta 55+35

Sp. in blazed tree 15' L. 55+70

Sta.	B. S.	H. I	F. S.	Rod	Elev
B. M	0.06	815.78			815.72
56				13.3	802.5
56+25				1.2	814.6
T. P.	11.96	827.47	0.27		815.51
56+50				4.7	822.8
T. P.	12.49	839.68	0.28		827.19
T. P.	4.33	843.03	0.98		838.70
56+90				2.2	840.8
57 P.O.C.				0.6	842.4
57+15				1.0	842.0
57+50				8.0	835.0
57+70				11.5	831.5
58				7.3	835.7
B. M.				7.45	835.58
58+29.4 E.C.				0.2	842.8
T. P.	12.14	855.00	0.17		842.86
58+50				5.8	849.2
T. P.	7.38	862.11	0.27		854.73
59 P.O.T.				0.5	861.6
59+25				1.6	860.5
59+53.0 B.C.				6.4	855.7
T. P.	0.77	850.13	12.75		849.36
60				3.5	846.6
60+18				7.4	842.5
60+42				11.6	838.5

Prescott Cont. P.J.C. 4/5/23

L. Line

Sp. in blazed Oak Tree 10' R. Sta. 54+95

Sp. in blazed Elm tree 5' L. Sta. 57+95

Stg.	B.S.	H.I.	F.S.	Rod.	Elev
		850.13			
B.M.	0.62	838.45	12.30		837.83
60+50				2.4	836.1
T.P	7.48	830.21	12.72		825.73
60+80				7.4	822.8
60+85				7.8	822.4
60+87				9.6	820.6
60+90				9.7	820.5
60+95				7.9	822.3
61				7.0	823.2
61+25				0.4	829.8
T.P.	11.89	841.76	0.34		829.87
61+50				8.9	832.9
62 P.O.C.				6.3	835.5
62+50				5.5	836.3
63				3.4	838.4
63+06				2.8	839.0
T.P.	12.90	854.38	0.28		841.48
63+50				7.1	847.3
63+70				2.4	852.0
T.P.	11.12	864.99	0.51		853.87
64				6.3	858.7
64+09				5.4	859.6
64+50				2.2	862.8
65				3.3	861.7
65+50				2.5	862.5

Prescott Cont. P.J.C. 4/5/23

L. Line

Sp. in blazed Oak tree 20'L. 60+36

Sta.	B.S.	H.I. 864.99	F.S.	Rod	Elev.
65+70				3.3	861.7
65+90				4.7	860.3
66				3.4	861.4
66+18				1.0	864.0
T.P.	10.60	875.07	0.52		864.47
66+33				9.8	865.3
67				9.8	865.3
67+20 B.C.				9.1	866.0
67+50				7.8	867.3
68				4.9	870.2
68+50				4.0	871.1
69				3.3	871.8
69+30				4.6	870.5
69+75				6.6	868.5
69+50				7.0	868.1
70				5.1	870.0
B.M.	5.73	879.11	1.69		873.38
70+50				7.5	871.6
71				6.2	872.9
71+50				5.4	873.7
71+68.0 E.C.				5.2	873.9
72				4.3	874.8
B.M.	5.40	881.43	3.08		876.03
73				5.2	876.2
74				4.9	876.5

Prescott Cont. P.J.C. 4/6/23

L. Line

Sp. in blazed Elm tree 25' L. Sta. 70 + 33.

Sp. in blazed Elm tree 30' R. 72 + 25

Sta.	B.S.	H.I.	F.S.	Rod	Elev.
		881.43			
75				4.7	876.7
76				4.4	877.0
77				3.9	877.5
77+04.6 P.I.				3.9	877.5
T.P.	7.21	883.87	4.77		876.66
78				4.7	877.2
79				5.3	878.6
B.M.				4.33	879.54
80 P.O.T.				4.7	879.2
81				4.9	879.0
82				4.9	879.0
83				4.1	879.8
84				2.8	881.1
T.P.	6.60	887.82	2.05		881.82
85				5.3	882.5
86				4.8	883.0
87				4.9	882.9
88				4.2	883.6
89				3.8	884.0
89+45				3.9	883.9
90 P.O.T.				5.2	882.6
91				7.0	880.8
T.P.	0.53	881.49	6.84		880.96
B.M.				0.54	880.95
91+64				2.5	879.0

Prescott Cont. P.J.C. 4/6/23

L. Line

Sp. in fence post 10' R. Sta. 79+70

Sp. in blazed Elm tree 13' R. Sta. 91+33

Sta.	B.S.	H.I.	F.S.	Rod	Elev.
		881.49			
92				4.9	876.6
92+30				9.4	872.1
T.P.	6.32	876.25	11.56		869.93
92+45				8.5	867.8
92+50				10.8	865.5
92+53				9.0	867.3
92+85				4.2	872.1
93				3.1	873.2
T.P.	10.63	886.56	0.32		875.93
93+30				3.1	883.5
94 P.O.T.				2.3	884.3
94+25				2.4	884.2
95				7.3	879.3
96 P.O.T.				9.2	877.4
97				9.3	877.3
97+50				9.5	877.1
98				7.5	879.1
T.P.	4.78	883.93	7.41		879.15
98+12				4.2	879.7
98+13				4.9	879.0
98+20				4.7	879.2
98+22				3.2	880.7
98+80				1.5	882.4
99				2.4	881.3
100				11.4	872.5

Prescott Cont. P.J.C. 4/6/23

L. Line

Sta.	B.S.	H.I.	F.S.	Rod	Elev.
		883.93			
T.P.	0.65	872.07	12.51		871.42
101				7.1	865.0
+25				10.2	861.9
B.M.	0.56	862.17	10.46		861.61
101+70				7.7	854.5
+75				9.8	852.4
102				12.2	850.0
+05				10.8	851.4
+50				8.5	853.7
103				3.7	858.5
T.P.	2.10	863.87	0.40		861.77
103+86				1.2	862.7
103+61.5 P.S.T.				2.4	861.5
103+75				4.8	859.1
104				10.1	853.8
B.M.	0.21	853.40	10.68		853.19
104+05.7 B.C.				1.1	852.3
T.P.	0.77	841.75	12.42		840.98
104+50				3.1	838.7
104+80				11.0	830.8
T.P.	0.75	830.18	12.32		829.43
B.M.				1.86	828.32
105				2.6	827.6
+45				6.0	824.2
+50				5.4	824.8

Prescott Cont. P.J.C. 4/9/23

L. Line

Sp. in blazed 12" Oak 27' L. Sta. 101+25

Sp. in blazed tree 10' R. Sta 104

On fence Post 33' R. Sta. 104+72.

Sta.	B.S.	H.I. 830.18	F.S.	Rod	Elev.
106				6.1	824.1
+50				7.8	822.4
107				8.8	821.4
+50				5.3	821.9
108				4.5	823.7
+40				5.6	824.6
+50				5.7	824.5
109				4.5	823.7
+50				8.2	822.0
110				10.2	820.0
+50				10.0	820.2
111				10.4	819.8
T.P.	1.22	820.90	10.50		819.68
111+50				2.1	818.8
111+65				2.7	818.2
112				5.1	815.8
+50				9.1	811.8
+60				10.0	810.9
+80				11.3	809.6
T.P.	1.27	809.67	12.50		808.40
112+95				6.6	803.1
113				6.3	803.4
+10				2.0	807.7
+40				2.1	807.6
+50				4.0	805.7

Prescott Cont. P.J.C. 4/10/23

L. Line

Sta.	B.S.	H.I.	F.S.	Rod.	Elev.
		809.67			
113+75				10.0	799.7
113+95				10.3	799.4
T.P.	2.17	799.69	12.15		797.52
114				5.0	794.7
B.M.				3.96	795.73
114+15				7.0	792.7
114+18				8.0	791.7
114+25				7.9	791.8
T.P.	11.58	810.01	1.26		798.43
114+50				0.4	809.6
T.P.	12.90	822.34	0.57		809.44
114+55				7.6	814.7
115				6.0	816.3
115+09.9 E.C.				5.7	816.6
115+65				4.3	818.0
116				1.8	820.5
T.P.	12.89	834.71	0.52		821.82
116+86.8 B.C.				4.3	830.4
117				2.9	831.8
T.P.	9.11	843.19	0.63		834.08
117+50				6.4	836.8
117+80				9.4	833.8
118				10.1	833.1
+34				10.5	832.7
+50				9.3	833.9

Prescott Cont. P.J.C. 4/10/23

L. Line

Sp. in blazed tree 3'R. Sta 114+05

Sta.	B.S.	H.I.	F.S.	Rod	Elev
		843.19			
119				4.5	838.7
T.P.	12.40	854.62	0.97		842.22
119+50				10.8	843.8
119+70				8.5	846.1
120				9.3	845.3
+15				10.9	843.7
+25				5.9	848.7
+50				3.3	851.3
+95				0.6	854.0
121				1.0	853.6
+50				1.5	853.1
B.M.	8.77	859.36	4.03		850.59
121+70				4.1	855.3
122 P.O.C.				5.0	854.4
+25				6.3	853.1
+35				5.7	853.7
+50				6.9	852.5
123				12.9	846.5
T.P.	0.88	847.68	12.56		846.80
123+50				8.8	838.9
T.P.	0.51	835.31 (835.81)	12.38		835.30
124				5.8	829.5 (830.0)
+10				7.5	827.8 (826.3)
B.M.	2.24	825.62	12.45		823.38
124+35				11.6	814.0

Prescott Cont. P.J.C. 4/10/23

L. Line

Sp. in blazed 14" Oak 15' L. Sta 122+10

Sp. in blazed 6" poplar 30' L. Sta 124+20

Sta.	B.S.	H.I	F.S.	Rod	Elev
		825.62			
124+40				13.3	812.3
124+47				13.2	812.4
124+48				12.2	813.4
124+50				11.7	813.9
124+52				11.1	814.5
124+60				5.1	820.5
124+64				8.9	816.7
124+70				9.8	815.8
124+73				9.9	~~814.7~~ 815.7
124+75				9.6	816.0
124+80				8.8	816.8
125				3.5	822.1
T.P.	12.60	837.59	0.63		824.99
125+20				7.9	829.7
+30				4.3	833.3
+50				1.7	835.9
T.P.	12.75	850.05	0.29		837.30
125+94				10.5	839.6
126				9.3	840.8
+40				0.7	849.4
T.P.	6.28	855.85	0.48		849.57
126+50				4.5	851.4
+75				0.6	855.3
127				1.8	854.1
+10				1.5	854.4

Prescott Cont. P.J.C. 4/10/23

L. Line

Sta.	B.S.	H.I. 855.85	F.S.	Rod	Elev.
127+25				3.1	852.8
+28				3.5	852.4
+30				1.4	854.3
T.P.	13.94	869.44	0.35		855.50
127+50				8.3	861.1
T.P.	12.38	880.87	0.95		868.49
128				9.4	871.5
+30				5.8	875.1
+50				5.0	875.9
129				4.0	876.9
+50				4.1	876.8
130				3.7	877.2
+50				2.4	878.5
B.M.	6.88	885.27	2.48		878.39
130+96.1 E.C.				5.9	879.4
131				5.8	879.5
+83.9 B.C.				4.3	881.0
132				4.2	881.1
+50				3.7	881.6
133				3.5	881.8
+50				2.9	882.4
134				2.7	882.6
+50				2.5	882.8
135				2.2	883.1
T.P.	5.22	889.09	1.40		883.87

Prescott Cont. P.J.C. 4/11/23

L. Line

Sp. in fence post 42' L. Stg. 130+30

Sta.	B.S.	H.I	F.S.	Rod	Elev.
		889.09			
135+50				5.3	883.8
136				4.5	884.6
+50				3.3	885.8
137				2.5	886.6
+50				2.4	886.7
138				4.7	884.4
+45				7.9	881.2
+50				9.5	879.6
B.M..				11.16	877.93
T.P.	0.32	877.43	11.98		877.11
138+70				2.7	874.7
139				12.9	864.5
T.P.	0.18	864.87	12.74		864.69
139+25.9 E.C.				8.4	856.5
139+40				11.8	853.1
T.P.	1.63	853.65	12.85		852.02
139+45				9.3	844.4
+50				8.7	845.0
+55				7.9	845.8
T.P.	9.07	862.43	0.29		853.36
139+64				8.8	853.6
+70				8.7	853.7
+78				8.6	853.8
+87				9.5	852.9
+88				8.7	853.7

Prescott Cont. P.J.C. 4/11/23

L. Line

Center of Road

Sta.	B.S.	H.I. 862.43	F.S.	Rod	Elev.
139+90				10.0	852.4
B.M.				11.99	854.44
T.P.	8.70	870.49	0.64		861.79
140				7.4	863.1
+08.5 P.O.T.				5.4	865.1
+85				8.1	862.4
141				9.1	861.4
+15				8.9	861.6
T.P.	1.46	859.38	12.57		857.92
141+90.7 B.C.				3.5	855.9
142				4.4	855.0
+50				7.8	851.6
143				8.4	851.0
+48				8.4	851.0
+50				9.0	850.4
+65				9.5	849.9
+80				9.3	850.1
B. 146+20.4				12.7	846.7
144				8.3	851.1
+15				6.7	852.7
+50				5.5	853.9
145				3.4	855.8
+55.1 P.C.C.	End of Project			2.0	857.4
T.P.	12.04	870.70	0.72		858.66
B.M.				1.05	869.65

Prescott Cont. P.J.C. 4/11/23

L. Line

Spin blazed 8" Oak. 27' R. Sta. 139+65

On B. Line. On Road Check. O.K.

On Road

On Road

On Rock

Nail in T.P. No. 1241 L. M.T.H. #3

Sta.	B.S.	H.I.	F.S.	Rod	Elev.
T.P.	0.38	859.04			858.66
B.M.			2.82		856.22

Center Elev. on town Road

B.M.	7.20	861.64			854.44
T.P.	1.01	849.81	12.84		848.80

Prescott Cont. P.J.C. 4/11/23

L. Line

On Rock

Sp. in T.P. No. 609 Sta. 145+30. 21' R.

Sp. in blazed 8" Oak 27' R. Sta. 139+65

139+80 = Center of Road

L.				℄				
2+00	1+50	1+00	0+50	0 0	0+50	1+00	1+50	2+00
840.6	842.4	846.7	850.4	853.7	856.3	857.7	858.9	860.1

Prescott Cont.
L. Line

X Sections on the
Prescott Cont.
L. Line.

Crane. Recording
Wilshusen. Hand Level
Sterk. Rod
McManus Tape

Sta	Elev.
145+55	857.4
145	855.8
+50	853.9
144	851.1
+50	850.4
143	851.0
+50	851.6
142	855.0
141	861.4
140+12	865.1
139+90	852.4

Prescott Cont. P.J.C. 4/11/23

L. Line ℄

L.				R.				
+5.5	+5.5	-1.0	-1.0	-0.3	-1.3	-1.7	-0.8	00
33	24	15	12	9	11	22	26	40

145	+5.5	+5.5	-0.5	-0.6	-0.5	-1.9	-1.8	-0.5
	33	31	20	13	9	14	21	33
		-1.5	-1.5	-0.7	-0.3	-1.0	-1.7	-0.6	00
		33	22	17	5	11	16	24	36
	+0.7	00	+1.0	+1.3	+0.5	+1.7	+1.5	
	35	28	24	2	17	19	37	
	-1.0	00	+0.5	-0.7	+1.0	+2.5		
	41	38	18	14	4	41		
-2.2	-3.1	-2.0	-1.4	-1.0	+0.7	+2.5		
33	30	28	18	16	22	35		
		-2.1	-1.5	+0.5	+5.0			
		37	30	5	33			
		-5.0	-3.0	+5.0	+7.0			
		34	17	16	33			
		-5.5	-3.8	-2.5	+5.0	+8.8		
		38	29	14	18	35		
		-3.8	-2.0	+2.8	+4.0			
		33	14	27	39			
	-1.8	-1.8	-1.1	-0.4	-1.0	00	+0.6	
	33	29	9	6	5	24	33	

Sta.	Elev.
139+65	853.6
139+44	844.4
139+40	853.1
139+25	856.5
139	864.5
+50	879.6
+40	881.2
138	884.4
+50	886.7
137	886.6
+50	885.8
136	884.6

Prescott Cont. P.J.C. 4/11/23

L. Line

L.			R.	
-2.5	-2.5 -1.0		+0.6	+1.4
33	26	19	20	33
-2.8	-2.2		+0.5 00	+0.4
33	28		11 20	33
-2.8	-2.2		+0.5 00	+0.4
33	28		11 20	33
-2.5	-2.0	-1.5	+0.3	+1.0
33	25	19	25	33
139 -2.0	-1.0	-1.5	-2.0	
33	20	31	33	
+1.3		-2.2	-2.5	
33		28	33	
+1.0	+0.8	-2.0		
33	21	34		
+1.5		-2.0		
33		33		
+1.8		-2.8		
33		33		
+3.0		-2.0		
33		33		
+2.3		-1.5		
33		33		
+1.8		-1.0	-1.0	
33		17	33	

Sta	Elev.
+50	883.8
135	883.1
+50	882.8
134	882.6
+50	882.4
133	881.8
+50	881.6
132	881.1
131	879.5
+50	878.5
130	877.2
+50	876.8

Prescott Cont. P.J.C. 4/11/23

L. Line

L.		R.	
+1.4	−0.8	00	
33	18	33	
+0.5	+0.7		
33	33		
00	+0.6		
33	33		
−0.3	+1.0		
33	33		
−0.8	+1.0		
33	33		
−0.5	+0.3	+1.4	
33	18	33	
−1.2	+1.0	+2.0	
33	20	33	
−1.2	+0.5	+2.0	
33	14	33	
−1.5	+1.0	+2.5	
33	16	33	
−1.8	+2.8		
33	33		
−1.4	+1.7		
33	33		
−2.2	+1.0		
33	33		

Sta.	Elev.
129	876.9
+50	875,9
128	871.5
+50	861.1
+25	852.8
127	854.1
+50	851.4
126	840.8
+50	835.9
125	822.1
+50	813.9
+32	814.0

Precott Cont. P.T.C. 4/11/23

L. Line

	L.	R.
129	-3.4 -0.8	+1.2 +1.3
	33 10	25 33
	-5.0 -1.5	+1.7
	33 15	33
	-5.0 -5.5 -5.5 -4.0 -1.2	+0.6
	33 31 28 24 12	37
	+2.6 -0.2 -3.1 -3.2 -1.1 -2.5 -0.1	+1.4 +3.0
	33 16 23 20 14 12 5	20 33
	+15.0 +10.0 +4.6 +1.8 -0.1	+0.3 +3.6 +5.0 +10.0
	50 33 18 13 7	7 25 34 60
	+15.0 +9.5 +5.0 +3.4 +1.8	-1.0 -3.5 -3.0 +3.0 +5.0
	50 25 10 8 2	5 11 20 38 50
	+12.5 +10.0 +5.0	-5.0 -11.0 -10.0 -4.5 -2.0
	50 40 18	14 28 29 40 60
	+5.0 +3.5 +4.0	-1.6 -6.6 -9.1 -14.1 -14.1 +0.3
	40 33 23	21 26 36 41 45 58
	+10.0 +5.0 +3.0	-0.6 -10.7 -15.5 -15.5 -2.7
	65 50 38	6 23 24 27 40
	+12.5 +10.0 +5.0	-4.0 -5.0 -4.0 +7.0 +6.0
	50 14 9	6 10 16 22 33
	+8.5 +8.0 +0.3 +0.3 -1.0 -1.0 0.0	-0.7 -1.5 -0.4
	50 34 24 18 15 13 12	14 16 40
	-1.8 -1.5	+0.4 +3.2 +5.0 +10.0 +12.0
	39 13	8 31 37 50 60

Sta.	Elev.	
124	829.5	830.0
+50	838.9	✓
123	846.5	✓
+50	852.5	✓
122	854.4	✓
+50	853.1	✓
121	853.6	✓
+50	851.3	✓
120	845.3	✓
+50	843.8	✓
119	838.7	✓
+50	833.9	✓

Prescott Cont P.J.C. 4/11/23

L. Line

	L.	R.
124	-5.5 +5.0 +10.0 50 31 70	
	-10.0 -5.0 +5.0 +10.0 +15.0 50 25 22 41 60	
	-10.0 +5.0 +10.0 +15.0 50 17 41 60	
	-15.0 -10.0 -5.0 +5.0 +10.0 +15.0 55 41 19 12 39 60	
	-15.0 -10.0 -5.0 +3.8 +10.0 +12.5 55 40 18 17 39 50	
	-14.5 -10.0 -5.0 -3.6 +5.0 +10.0 +12.8 12.8 54 41 16 12 16 31 42 50	
	-20.0 -15.0 -10.0 -5.0 +5.0 +10.0 +13.5 +14.0 55 41 27 12 12 30 42 55	
	-20.0 -15.0 -7.0 -4.0 +5.0 +10.0 +15.0 Level 50 41 14 11 14 29 45	
	-20.0 -15.0 -10.0 -5.0 +5.0 +10.0 +15.0 +18.4 Level 50 42 34 15 15 33 50 55	
	-20.0 -15.0 -10.0 -5.0 +5.0 +10.0 +15.0 +18.7 55 43 29 14 17 34 50 60	
	-14.5 -10.0 -5.0 +5.0 +10.0 +15.0 +20.0 60 42 18 14 30 40 55	
	-10.0 -15.0 -13.5 -8.0 -5.0 +5.0 +10.0 +15.0 69 63 50 41 23 21 41 60	

Sta.	Elev.	
118	833.1	✓
+50	836.8	✓
117	831.8	✓
116	820.5	✓
115	816.3	✓
+70	815.1	
+50	809.6	✓
+25	791.8	✓
114	794.7	✓
+95	799.4	✓
+72	799.7	✓
+35	807.4	✓

Prescott Cont. P.J.C.

L. Line 7/12/23

	L.	R.
118	-2.0 +3.3 +5.0 34 34 50	
	-11.0 -6.0 -1.0 +0.6 00 60 40 8 18 50	
	-8.5 -5.0 -2.6 +5.0 +7.0 50 35 20 35 50	
	-3.0 -2.2 +2.0 50 37 50	
	-2.2 -2.3 -2.3 50 45 50	
	Level -3.2 -0.5 -2.0 33 32 50	
	-2.8 00 +1.8 +1.0 44 17 22 .50	
	+1.0 +0.8 -0.7 00 +1.2 +5.0 +13.0 +18.0 34 24 17 10 13 21 41 60	
	-2.0 -1.8 00 -0.5 50 35 35 44	
	-6.5 -5.5 -1.2 +0.3 -5.0 -5.0 50 34 17 17 30 50	
	00 -5.0 -1.5 +0.5 +2.2 50 44 34 18 50	
	-1.0 -8.5 -8.5 -2.6 +1.2 00 60 40 31 22 24 50	

Sta.	Elev.
113+08	807.7
113	803.4
+95	803.1
+78	809.6
+50	811.8
112	815.8
+69	818.2
111	819.8
+50	820.2
110	820.0
+50	822.0
109	823.7

Prescott Cont. P.S.C. 4/12/23

L. Line

	L.			R.	
	00	-0.8	-6.5	-6.5	+1.7	+2.2
	50	38	25	14	32	50
113	+6.0	+4.5	-0.5	-1.6	+5.0	+6.2
	-50	22	14	5	12	50
	+6.0	+5.0	+0.3	+1.3	+5.0	+5.0
	50	22	11	14	29	50
	-1.0	-0.6	+0.5	00	00	
	50	19	18	28	50	
	+1.5	+1.5	+0.5	-0.8	-1.0	
	50	39	13	18	37	
	00	00	+0.4	-1.0	-1.8	
	50	38	21	22	50	
	-0.8	-0.8	-0.5	-1.3		
	50	31	18	42		
	00	+0.4	00	00	-1.6	-2.5
	50	22	16	28	33	50
	00	+0.5	00	-1.6	-3.2	
	50	25	22	22	50	
	+1.5	+0.4	-0.5	-1.6		
	50	24	34	50		
	-2.0	+0.5	-1.0	-2.2		
	50	19	41	50		
	+3.3	+2.2	-2.3	-4.0	-4.5	
	50	28	18	43	50	

Sta.	Elev.
+50	824.5
108	823.7
+50	821.9
107	821.4
+50	822.4
106	824.1
+50	824.8
105	827.6
+50	838.7
104	853.8
+75	859.1
+50	861.9

Prescott Cont. P.S.C. 4/12/23

L. Line

	L.			R.		
	+1.5	+1.0		-1.8	-5.0	
	50	33		22	50	
108	+1.0	+1.2	+0.8	-2.0	-4.0	
	50	38	25	35	50	
	+0.8	+0.5		-1.0	-2.3	-2.3
	50	36		14	44	50
	00	+0.5		-0.8	-1.5	
	50	35		17	50	
	+0.5	+0.8		-0.8	-1.0	
	50	26		22	50	
	+1.5	+0.8		-1.0	-1.5	
	50	27		22	50	
	+1.5	+1.0		-1.2	-1.8	
	50	29		24	50	
	+5.0	+3.8	+1.0	-2.5	-2.0	
	50	37	13	46	50	
	+12.5	+10.0	+5.0	-4.5	-10.0	
	50	38	18	17	50	
	+13.0	+11.0	+5.0	-5.0	-10.0	-14.5
	50	42	18	21	41	50
	+9.5	+5.0		-3.2	-8.2	
	54	29		16	50	
	+5.0	+2.2		-5.5	-7.0	
	50	21		43	50	

Sta.	Elev.
103+21	862.5
102+64	855.0
102	850.0
+76	852.4
+26	861.9
101	865.0
+50	868.5
100	872.5
+50	877.0
99	881.3
+58	881.0
98	879.1

Prescott Cont. P.T.C. 4/12/23

L. Line

	L.				R.				
	+11.0	+4.0			-3.2	-6.0	-8.0		
	52	27			25	45	50		
	+15.0	+10.0	+5.0		-4.0	-10.0			
	60	38	18		17	50			
					-3.0				
102	+15.0	+10.0	+5.0	+1.5	-2.4^	-2.8	-3.0		
	60	41	21	4	17	40	50		
	+6.0	+5.0	+3.2	+1.8	+0.8	+0.8	+1.0		
	50	44	38	22	11	42	50		
	+1.1	-0.2	+1.0		0.0	-1.1			
	50	44	38		25	50			
	+2.0	+1.8			0.0	-1.5			
	50	44			27	50			
	+4.2	+1.2			-1.0	-0.3			
	50	34			42	50			
	+4.0	+1.5			+1.0	+2.2			
	50	24			35	50			
	+2.0				0.0	+2.2			
	46				35	50			
	-3.0				+2.0	+2.0			
	50				35	50			
	-3.0	-3.0	-2.2		+0.4	-0.5			
	50	38	33		37	50			
	+2.8	0.0			-1.0	-2.0			
	50	20			22	50			

Sta.	Elev
+50	877.1
97	877.3
96	877.4
95	879.3
94+25	884.2
93+80	883.5
+35	877.7
93	873.2
+54	867.3
92	876.6
+49	879.0
91	880.8

Prescott Cont. P.J.C. 4/12/23

L, Line

	L.					R.				
	+10.0	+5.0	+0.5	00						
	67	42	11	50						
97	+10.0	+5.0	+0.3	-0.2						
	66	41	13	50						
		+5.0	+0.7	-1.1	-1.1					
		50	16	35	50					
			+2.1	-1.2	-2.2					
			60	24	50					
		-3.0	-0.6	00						
		50	15	50						
		-5.0	-3.0	+2.0	+3.7					
		50	27	22	50					
	-15.0	-10.0	-5.0	+3.5	+5.0					
	50	38	23	33	50					
-5.0	-10.5	-13.8	-10.0	-5.0	+5.0	+7.2	+8.6			
50	35	30	25	15	29	40	60			
	+7.5	+4.0	-0.4	+1.5	+5.0	+10.0				
	60	29	8	4	21	47				
	-1.4	00	+1.0	-4.0						
	50	45	18	50						
		-1.8	00	-0.8	-4.2					
		50	18	23	50					
		-1.1	-1.1	-0.2	-2.0					
		50	43	24	50					

Sta.	Elev.
90	882.6
89	884.0
88	883.4
87	882.9
86	883.0
85	882.5
84	881.1
83	879.8
82	879.0
81	879.0
80	879.2
79	878.6

Prescott Cont. P.J.C. 4/12/23

L. Line

	L.	R.
90	00	-1.0
	33	33
	-0.2	-0.5
	33	33
	00	-0.8
	33	33
	00	-0.2
	33	33
	00	-0.2
	33	33
Flat	-0.6	00
	33	33
Flat	-0.4	00
	33	33
	00	00
	33	33
	00	-0.2
	33	33
	00	-0.3
	33	33
	-0.8	+1.0
	33	33
	-1.5	-1.2
	33	33

Sta.	Elev.
78	877.2
77	877.5
76	877.0
75	876.7
74	876.5
73	876.2
72	874.8
71	872.9
+50	871.6
70	870.0
+50	868.1
+30	870.5

Prescott Cont. P.J.C. 4/12/23

L. Line

	L.	R.
78	-0.6 -1.5 33 33	
	-1.0 -0.7 00 00 35 27 16 34	
	00 00 +0.2 -0.6 -0.6 +0.3 33 16 14 12 16 33	
	+0.5 -0.2 -0.8 -1.0 -0.5 -0.5 35 16 14 18 19 33	
	+0.8 +0.8 00 -0.5 00 34 30 16 18 33	
	+0.4 +0.4 -0.2 -0.5 -0.7 -0.2 00 33 28 16 15 13 16 33	
	+2.2 +1.0 -0.9 -1.0 +0.5 +1.0 33 14 13 20 22 33	
	+2.5 +1.0 -0.7 -0.5 -1.0 -1.3 +1.0 +1.8 +1.8 34 19 15 8 15 20 15 26 33	
	+2.4 +2.4 -0.1 00 -0.9 00 33 30 22 7 12 35	
	+4.0 +2.4 -0.3 00 -0.5 +2.8 +3.0 43 34 28 10 11 20 33	
Level	+1.5 +0.5 -0.2 +1.0 +1.8 +2.8 40 30 13 11 15 33	
	+1.2 -2.0 -2.0 -2.4 +1.2 +2.0 +2.5 35 28 20 5 6 25 33	

Sta.	Elev.
69	871.8
+50	871.1
68	870.2
+50	867.3
67	865.3
66+53	865.2
65+90	860.3
+50	862.5
65	861.7
+50	862.8
64	858.7
+50	847.3

Prescott Cont. P.J.C. 4/12/23

L. Line

	L.				R.		
69	-0.3	-4.5	-4.2	-4.2	+1.0	Level	
	46	36	20	10	33		
	-4.5	-3.5	-0.4	-0.3	-1.0		
	50	30	16	15	33		
	-7.5	-7.0	-3.0	-1.0	-0.8	+1.0	
	50	35	30	24	16	46	
				-3.4	+0.8	+3.0	
				33	20	45	
	-14.0	-6.0	-2.2	+1.8	+4.0	+5.0	
	35	29	11	16	34	46	
	-10.0	-7.0	-1.8	+1.6	+3.0	+3.0	
	50	44	15	16	41	50	
	-9.0	-5.0	-2.5	+2.0	+5.0		
	50	30	13	14	41		
	-7.0	-3.0	-1.0	+2.5	+5.0		
	50	25	8	25	46		
	-15.0	-10.0	-5.0	+2.8	+5.0		
	50	33	23	22	50		
	-15.0	-10.0	-5.0	+3.5	+5.0		
	50	40	25	25	50		
	-15.0	-10.0	-5.0	-2.5	+3.5	+6.0	+7.0
	50	34	24	14	20	43	50
	-15.0	-10.0	-5.0	-3.5	+5.0	+10.0	+15.0
	50	33	18	13	23	38	55

Sta.	Elev.
63	838.4
+50	836.3
62	835.5
+50	832.9
61+08 +2.5	825.7
61 823.2	
60+87 -3.2	820.6 820.0
60+50	836.1
60	846.6
+53	855.7
59	861.6
58+69 -3.0	858.6
58+50	849.2

Prescott Cont. P.J.C. 4/13/23

L. Line

	L.				R.			
63	00	-4.0	-5.0		+5.0	+10.0	+15.0	
	55	46	36		21	44	62	
	+5.0	+4.0	+1.5	00	+2.5	+5.0	+9.0	
	60	46	38	21	25	39	64	
	+5.0	+1.0			+4.0			
	50	26			50			
	-1.3	-0.5			+2.5			
	50	37			50			
	-10.0	-5.0	-2.4	-0.5	+0.5	-1.6	-5.0	-3.0	-2.0
	72	50	40	28	13	5	15	46	56
	-13.0	-5.0	-1.2	+1.5	+0.8	+1.0	+3.8	+10.0	
	53	52	40	21	12	7	17	50	
	-20.0	-15.0	-10.0	-5.0	-2.2	00	+1.3	+2.5	+4.0
	75	65	50	35	25	18	25	32	50
	-20.0	-15.0	-10.0	-5.0	-3.8	-2.0	+1.5	+3.5	
	75	60	50	36	25	17	25	50	
	-23.2	-20.0	-10.0	-4.0	-2.0	-0.5	+1.5	+2.8	+4.0
	100	80	48	25	12	8	12	25	50
	-20.0	-16.0	-11.8	-2.0	+1.0	+1.0	+2.0		
	100	70	50	12	6	10	50		
	-20.0	-18.5	-15.0	-10.0	+3.2	+3.5	+4.5		
	100	90	50	35	13	25	50		
	-15.5	-14.5	-14.5	-15.0	-10.0	-5.0	+1.8	+9.8	+12.5	+14.0
	100	80	65	43	22	9	4	25	37	50

Sta.	Elev.
57+89 -2.2 (58 → 835.7)	833.5
+50	835.0
57	842.4
+25 -10.0	832.4
+50	822.8
56	802.5
+70 779.0	
+45 +3.5	782.5
+40	800.7
+25 +5.0	805.7
55	810.9

Prescott Cont. P.S.C. 4/13/23

L. Line

	L.				R.			
57+85	-32.0	-27.8	-20.0	-0.5	+10.0	+21.3	+24.0	+27.2
	100	80	43	9	15	40	45	50
52	-36.0	-30.0	-15.0	-10.0	+15.0	+19.0	+20.0	
	100	80	35	25	95	45	50	
47	-31.0	-30.0	-20.0	-10.0	+5.0	+6.1	+10.0	+10.0
	100	90	58	27	16	19	31	50
42	-22.3	-20.0	-9.0	-8.0	-4.0	+3.8	+5.0	+20.0
	100	92	50	42	20	15	18	55
37	-10.0	-9.2	-10.0	-11.0	+15.0	+21.7		
	100	92	62	50	35	50		
	-1.0	-2.0	-9.7	-9.2	-8.3	-4.5	+2.4	+10.0	+11.8	+16.8
	100	91	60	50	45	30	14	33	40	50
765	-2.0	-3.8	-7.8	-7.5	-10.0	-5.5	-3.7	-3.2	+0.5	+4.5	+5.0	+10.0	+13.2	+15.0
	100	88	50	28	25	14	12	7	9	17	30	43	55	65
	-36.2	-32.0	-30.0	-21.8	-20.0	-15.0	-9.4	+5.5	+10.0	+12.0	+14.2
	100	95	90	60	45	33	19	15	32	50	60
	-32.0	-30.0									
	105	125									
	-42.5	-37.8	-35.0	-30.0	-20.0	-12.3	-1.3	+5.0	+10.0	+12.2	+15.0	+14.3
	16	107	100	80	57	30	5	13	23	35	49	61
	-40.5	-39.0									
	129	124									
	-45.0	-38.0	-30.0	-15.0	-8.2	-5.0	+1.0	+5.0	+10.0	+14.4	+19.5
	125	105	86	50	30	21	5	12	20	26	50
	-50.0										
	150										

Sta.	Elev.	
55		
54+89 +0.5	811.4	
+57 -1.3	806.4	
+50	807.7	
+25 -3.0	809.9	
54	812.9	
53+50	809.0	817.5
53+25 -0.5	809.5	817.0
53 811.7		
52+91 -2.5	809.2	
52+43.1 E.C. 11° Curve	809.9	
52+17 +1.3	809.0	809.3
52 808.0		

Prescott Cont. P.S.C. 4/17/23

L. Line

L.						R.				
-31.8	-30.0	-25.0	-15.0	-5.0	-0.2	+2.5	+5.0	+10.0	+15.0	+18.5
110	100	74	50	17	9	12	15	28	42	50
-39.0										
125										
-30.0	-20.0	-10.0	-7.4	-5.0	-3.2	+5.0	+10.0	+15.0	+27.2	
126	100	65	50	30	8	15	28	36	50	
-30.0	-20.0	-13.2	-10.0	-7.8	-7.5	-4.5	+5.0	+15.0	+25.0	
127	100	70	48	20	12	9	12	35	50	
-34.2	-30.0	-25.0	-24.2	-26.5	-22.0	-15.0	-5.0	+5.0	+10.0	+15.0	+25.0
125	100	58	55	50	44	34	11	9	20	30	50
-25.0	-20.0	-15.0	-10.0	-5.0	+5.0	+10.0	+13.2	+20.0	+27.1		
50	43	34	20	10	12	22	28	40	50		
-40.0	-45.0	-50.0	-52.0								
78	86	100	115								
-50.0	-41.6	-35.0	-30.0	-15.0	-10.0	+5.0	+10.0	+23.5			
112	97	85	75	34	25	12	24	50			
-45.0	-40.0	-35.0	-25.0	-13.5	-5.0	+5.0	+12.8	+19.3			
112	100	90	68	36	15	15	35	50			
-30.0	-25.0	-20.0	-15.0	-10.0	-5.0	+5.0	+10.0	+15.0	+20.0	+24.4	
89	78	63	50	27	12	11	21	33	42	50	
-40.0	-35.0	-27.1	-25.0	-15.0	-10.0	-5.0	+5.0	+13.1	+15.0	+20.0	
83	74	67	48	30	20	11	14	33	39	50	
-35.0	-30.0	-20.0	-15.0	-5.0	+5.0	+12.4	+19.2				
75	65	43	33	12	11	33	50				

Sta.	Elev.	
52 ←		
51+91 -0.8	807.2 ✓	
+50	807.6 ✓	
51	808.1 ✓	
+50	811.6 ✓	
50	812.3 ✓	
+50	803.2 ✓	
+20 -0.5	796.7 ✓	
49 793.6 ✓ ←		
48+98 -2.6	771.0	771.2
+90 -2.9	771.6 ✓	
48+70 +0.8	791.8	791.9
48+59.6 791.1 ✓		

48+08.1 B.C. 11° Curve

Prescott Cont. P.J.C. 4/17/23

L. Line

	L					R				
	-25.0	-20.0	-13.7	-10.0	-5.0	+5.0	+10.	+13.0	+15.0	+19.5
	55	46	33	25	12	13	24	33	39	50
	-20.0	-15.0	-10.0	-5.0		+5.0	+10.0	+12.9	+19.0	
	55	40	25	14		14	28	35	50	
51	-20.0	-18.4	-13.1	-10.0	-5.0	+5.0	+10.0	+15.0	+20.0	+21.5
	50	44	33	25	12	12	22	33	46	50
	-23.2	-20.0	-14.1	-10.0	-5.0	+5.0	+10.0	+11.2	+15.0	
	55	45	33	22	11	10	27	33	50	
	-18.6	-15.0	-11.1	-10.0	-5.0	+3.5	+0.5	+6.5	+9.5	
	50	42	33	29	12	14	26	33	50	
	-17.6	-15.0	-11.6	-10.0	-5.0	-3.3	+5.0	+6.5	+10.0	
	50	46	33	30	23	12	25	33	50	
	-14.0	-10.0	-5.0	-2.5		+3.5	+5.0	+6.3	+6.7	+6.2	+0.5
	50	33	19	13		15	22	29	33	37	48
	-9.5	-8.7	-5.0	-4.0	-4.0	-1.5	+0.7	+0.3	+7.9	+9.1	+14.8	+15.0
	60	55	46	33	19	9	10	15	16	33	40	50
	-9.5	-8.7	-5.0	-4.0	-4.0	-1.5	+0.7	+0.3	+7.9	+9.1	+14.8	+15.0
	60	55	46	33	19	9	10	15	16	33	40	50
	-13.5	-12.8	-10.0	-8.0	-5.0	+3.5	+5.0	+7.1	+10.8	+15.0	+16.3
	55	48	33	35	10	14	17	22	33	48	50

25

Prescott Cont.
L. Line.

P.J.C. 4/13/23.

Sta.	Elev.
	(on 16° Curve)
48+60	789.9
48	788.1
+41	785.8
47	784.1
+50	782.0
46	780.3
+50 -2.0	778.3
45	776.2
44	772.2
43+50 -1.2	771.0
43 768.6	
42+96	768.6
42+50 -1.8	766.8

Prescott Cont. P.J.C. 4/13/23

L. Line

	L.				R.			
	-20.0	-15.0	-10.0	-5.0	+5.0	+10.0	+15.0	
	80	60	38	21	16	38	60	
48		-15.0	-10.0	-5.0	+5.0	+10.0	+15.0	
		58	38	15	20	37	52	
	-15.0	-10.0	-8.0	-5.0	+5.0	+10.0	+15.0	+17.0
	50	36	21	16	18	29	44	50
	-11.0	-11.0	-6.0	-3.5	+5.0	+10.0	+15.0	+20.0
	50	37	27	12	18	33	48	63
	-12.0	-9.0	-9.0	-8.0	-5.0	+5.0	+10.0	+15.0	+18.0
	60	43	34	26	19	18	33	48	50
	-10.0	-9.0	-6.0	-6.0	-1.5	+5.0	+10.0	+15.0	+20.0
	50	42	27	19	6	19	29	39	54
	-9.0	-4.0	-3.4	-2.6	+3.0	+5.0	+10.0	+15.0	
	50	22	12	10	10	20	40	55	
45		-8.0	-2.5	-2.5	+2.5	+5.0	+10.0	+15.0	
		50	16	8	13	23	43	63	
	-5.0	-3.0	-1.5		+2.0	+5.0	+10.0	+15.0	
	50	29	25		14	26	43	58	
	-6.0	-4.2	-2.5	-3.0	+2.2	+5.0	+10.0	+15.0	
	54	34	30	25	15	34	54	74	
	-7.0	-2.5	-8.0		00	+1.1	+3.8	+7.8	
	40	24	8		6	9	18	38	
	-8.0	-5.0	-4.1	-0.9	+0.2	+1.8	+5.0		
	44	30	14	3	10	14	40		

Sta.		Elev.
42		761.7
+50	-4.0	757.7
41		756.6
+50	-1.1	755.5
40		756.9
+45	-5.0	751.9
39		750.6
38		748.8
37		746.3
36		743.8
35		741.8
34		740.5

Prescott Cont. P.S.C. 4/13/23

L. Line R.

L

42

-7.0	-3.6	-1.5					+2.2	+2.5	+5.0	+10.0			
44	28	14					5	17	22	47			
-4.2	-3.2	-1.2					+0.5	+1.8	+5.0	+10.0			
47	28	19					5	16	30	50			
-2.2	-2.2	-1.0					+3.2	+4.3					
40	33	30					13	27					
-2.2	-1.2	-1.4	-1.5				+0.5	+2.0	+5.0	+10			
38	28	24	22				2	5	30	45			
-5.0	-5.0	-4.2	-5.0	-1.3			+1.1	+5.0	+7.4				
40	33	31	15	7			13	41	50				
00	00	-0.3					+2.1	+5.0	+9.0				
50	30	27					4	20	40				
+0.5	+0.5	-0.3					+1.7	+3.5	+5.0	+9.0			
50	30	18					8	13	27	51			
-0.5	00	00					-1.0	+2.8	+3.2	+4.2	+5.0		
34	32	21					10	17	19	29	40		
-0.1	-0.3	-0.8					+0.5	+1.2	+3.2				
38	24	21					13	20	45				
-0.5	-0.1	-0.7					-0.5	00	+0.6	+1.8	+38		
40	22	19					6	10	18	26	45		
00	00	-0.5					-0.3	+0.4	+0.7	+0.7	+1.7		
50	25	21					5	7	18	21	40		
+1.2	+0.3	00	-0.5				-0.3	+0.7	+1.2	+2.5			
43	31	23	21				5	21	23	40			

Sta.		Elev.
33		738.5 ✓
32		734.6 ✓
31	←	734.9 ✓
+60	-0.2	734.7 ✓
30	←	733.8 ✓
29+79	+0.3	734.1 ✓
+45		732.4 ✓
+16	+1.2 →	730.2 ✓
29		729.0 ✓
+67		727.5 ✓
+62	-3.6	(731.1) 723.9
+38	-1.2	723.1 ✓
28		724.3

Prescott Cont. P.S.C. 4/13/23

L. Line

	L.	R.
33	+0.8 00 -0.8 00 46 34 27 23 18	-0.8 00 +1.8 +3.0 +3.0 +3.8 8 12 17 22 26 40
	-1.4 -0.6 -0.4 45 30 14	-0.8 -1.4 00 +2.5 +4.2 10 12 16 23 50
	+1.8 +1.8 0.0 -0.8 -1.0 50 30 18 14 10	+0.4 +1.5 +3.3 +4.5 17 24 27 50
	-4.2 -2.8 -1.4 46 28 8	+0.5 +1.6 +2.0 +3.0 +4.0 +5.0 5 8 25 27 34 50
	-6.0 -4.0 -1.5 50 34 18	+0.4 -0.3 +0.6 +1.8 +2.5 8 14 38 45 50
	-6.0 -4.0 -1.4 60 34 15	-0.2 -1.2 -1.8 -1.0 00 +2.0 9 28 30 34 45 60
	House 00 8	-0.2 -0.6 00 +1.0 +4.0 21 23 38 45 60
	-10.0 -7.5 -4.5 -2.0 63 54 50 33	+1.0 +1.3 +3.8 13 36 50
	-10.0 -5.0 -3.5 -1.6 -1.1 60 50 38 28 15	+1.4 +0.8 +2.2 +3.4 24 28 38 45
	0.7 -1.5 -5.5 -5.0 -2.5 -1.3 70 65 55 45 24 11	+0.4 -1.0 00 +2.0 +4.4 13 19 31 45 60
	-6.0 -4.5 -2.5 60 36 18	+1.8 +3.0 +5.0 +8.0 10 21 43 63
	-6.0 -3.7 -2.4 -1.3 55 36 29 14	+1.5 +3.6 +5.0 +8.5 18 39 50 60

Sta.	Elev.
+15 00	724.3 ✓
28	724.3 ✓
+79 +32	727.7 ✓
+68 +3.5	727.8 ✓
+50	727.6 ✓
+28	719.0 ✓
27	714.8 ✓
+64 -2.5	717.3 ✓ 712.3
+40 70.6	706.3 ✓
26	705.7 ✓
+50	704.5 ✓
25	707.7 ✓

Prescott Cont. P.S.C. 4/13/23

L. Line

L.	R.
+1.3 +.2 +4.0 +3.8 -0.2 -0.9 -0.8	+1.6 +2.7 +4.0 +5.0
54 44 38 31 22 19 11	24 41 55 60
28	
+1.2 +3.8 +3.8 +3.3 -0.2	+1.6 +1.8 +3.0 +4.5
43 33 26 20 9	29 43 50 60
-15.0 -10.9 -10.0 -5.0 -2.5 -1.0 +0.5	-0.8 -4.0 -3.5 -3.0 -0.8 00
73 62 58 42 33 25 15	3 12 23 41 55 60
-20.0 -15.0 -10.0 -3.8 -0.7	-0.7 -1.6 -4.3 -3.8 -2.8 -0.2
65 50 43 24 14	10 15 23 31 43 55
-13.5 -12.5 -9.0	00 00 -1.5 00
65 50 25	17 45 54 75
-7.0 -9.5 -4.0 -3.2	+1.7 +9.0 +9.5 +9.8 +8.5
62 52 46 32	11 29 46 47 78
-5.0 -5.0 -4.0 -2.5 -0.8	+1.0 +2.0 +11.0 +11.0
62 54 29 40 14 40 29	10 32 58 70
-4.0 -3.8 -2.4 -1.3	-0.8 -2.9 -1.8 +2.0 +4.5
50 44 34 15	21 30 35 50 60
+2.0 +1.6 +1.0 +0.7	00 +1.8 +5.0 +10.0
46 38 33 26	19 33 46 66
+1.2 +3.0 +3.4 -2.5 00	-2.0 -2.5
50 40 31 20 14	34 55
+1.0 +3.7 +4.5 +3.8	-2.0 -2.5 -3.0
44 38 21 9	15 31 45
-2.6 -2.6 +0.5 +1.0	-5.0 -9.0 -12.0 -12.0
40 33 24 15	10 34 40 50

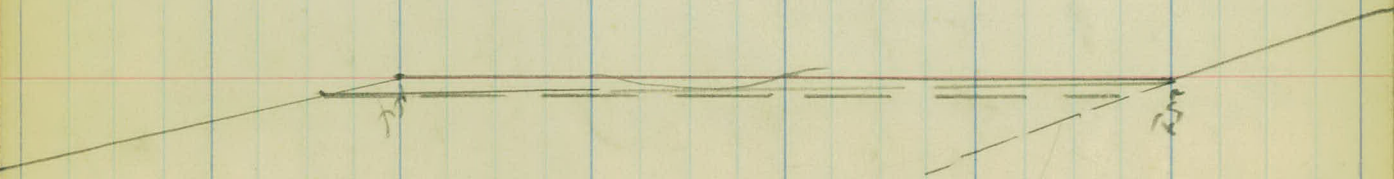
Sta.	Elev.
24+50	708.5
23+95	709.0
23	709.2
22	708.9

Prescott Cont.

L. Line

	L.			R.		
	-3.5	-3.5	-0.6	-0.7	-5.0	-7.0
	34	24	15	7	17	50
	-4.4	-4.2	-0.6	-1.1	-6.0	-8.0
	40	19	12	11	21	50
23	-3.8	-4.2	-4.2	-0.8	-1.2	-5.5	-6.0
	38	29	20	12	15	24	35
	-3.2	-4.0	-3.6	-0.9	-1.3	-5.0	5.0
	41	29	19	12	15	24	35

X sections



Prescott Cont P.J.C. 4/16/23

L. A. Line

Center Elev. From
Sta 132+00 to 171+00
on the A. L. Line

Sta.	B.S.	H.I.	F.S.	Rod.	Elev.
B.M.	10.63	889.02			878.39
132				8.1	880.9
+50				7.4	881.6
133				7.0	882.0
+50				6.4	882.6
134				5.9	883.1
+15.0 B.C.				5.8	883.2
+50				5.4	883.4
T.P.	11.69	895.64	5.07		883.95
135				11.6	884.0
+50				10.7	884.9
136				9.3	886.3
+12				8.9	886.7
+50				6.9	888.7
137				3.6	892.0
+15.0 E.C.				3.3	892.3
+88				2.9	892.7
138				3.5	892.1
+85				5.9	889.7
139				5.9	889.7
+80 +21.2 B.C.				8.2	887.4
140				7.9	887.7
T.P.	5.15	893.48	7.31		888.33
+50				5.4	887.9
141				6.2	887.3

Prescott Cont. P.J.C. 4/16/23

L.A. Line

SP, in fence post 42" L. Sta. 130+30 on L. Line

Stg.	B.S.	H.I.	F.S.	Rod	Elev.	
		893.48				
141.+50				7.1	886.4	
+65				9.0	884.5	
142				9.8	883.7	
+03				10.0	883.5	
+05				11.0	882.5	
+25				9.9	883.6	
B.M.	8.02	892.86	8.64		884.84	
+35				7.9	884.8	885.0
+50				6.9	885.8	886.0
+75				8.0	884.7	884.9
+80				4.1	888.~~6~~.8	
+95				4.1	888.~~6~~	
143				3.1	889.~~7~~.9	
+12				4.4	888.~~3~~.5	
+50				4.5	888.~~2~~.4	
144				4.7	888.~~0~~.2	
+50				4.7	888.~~0~~2	
+93.5 E.C.				4.5	888.~~2~~4	
145				4.6	888.~~4~~.3	
146				3.1	889.~~6~~.8	
147				4.0	888.~~7~~.9	
148				5.2	887.~~5~~7	
T.P.	6.93	889.14	4.65		882.21	
149				2.3	886.8	
150 P.O.T.				3.7	885.4	

Prescott Cont
L.A. Line

P.J.C. 4/16/23

Spin blazed 24" Oak. Sta. 142+24 Lt. 15'

Center of road

Sta.	B.S.	H.I. 889.14	F.S.	Rod	Elev.
150 +24				4.7	884.4
+85				10.4	878.5
151				11.4	877.5
+40				9.4	879.5
152				11.5	877.6
+33				14.2	874.9
T.P.	2.25	879.75	11.64		877.50
153				4.4	875.4
+15				3.2	876.6
+35				10.4	869.4
+50				8.6	871.2
+61				8.6	871.2
+65				9.8	870.0
+67				8.1	871.7
+73				7.2	872.6
+74				6.3	873.5
B.M.	3.98	876.84	6.89		872.84
154				5.4	871.4
+65				8.8	868.0
155				8.6	868.2
+63				6.0	870.8
+66				4.8	872.0
156				5.4	871.4
157				4.3	872.5
+95				3.0	873.8

Prescott Cont.
L. A. Line

P.J.C. 4/16/23

Center of road

Sp. in T. P. 10' L. Sta. 153+75

Sta.	B.S.	H.I.	F.S.	Rod.	Elev.
		876.84			
T.P.	11.66	887.56	0.94		875.90
158				7.3	880.3
+60				2.9	884.7
159				1.2	886.4
T.P.	8.47	895.49	0.54		887.02
160				6.8	888.7
161				4.8	890.7
162				4.6	890.9
163				5.2	890.3
164				5.2	890.3
T.P.	1.73	891.91	5.31		890.18
165				2.6	889.3
166				4.2	887.7
167				5.2	886.7
168				5.5	886.4
+36				5.0	886.9
169				3.6	888.3
170				3.7	888.2
+45				2.1	889.8
171				2.2	889.7
B.M.			1.40		890.51

Prescott Cont.
L. A. Line

P. S. C. 4/18 p3

Top of Hub in ground at Stg. 171

E/a V

Prescott Cont. 4/18/23
L. A Line

X sections on the
L. A. Line From Sta.
171+00 to 132+00.

Sta.	Elev.
171	889.7
745	889.8
170	888.2
169	888.3
736	886.9
168	886.4
167	886.7
166	887.7
165	889.3
164	890.3
163	890.3
162	890.9

Prescott Cont. P.J.C. 4/18/23

L. A. Line

	L.	℄	R.	
171	-0.8 -0.5	0.7 -1.0		
	33 21	25 33		
	+0.2 +0.4	-1.0 -2.5		
	33 23	19 33		
	+1.5 +1.1	-1.0 -1.8		
	33 27	15 33		
	+0.4 +0.2	-0.7 -1.3		
	33 23	23 33		
	+0.9 +0.2	-0.7 -1.0		
	33 14	24 33		
		+0.2 -0.2 00		
		33 19 33		
	00 -0.2	+0.5 +0.6		
	33 22	21 33		
	00 -0.3	+0.2 +0.8		
	33 30	19 33		
	-0.4	00 +0.3		
	33	17 33		
	-0.7	00		
	33	33		
	-0.8	00		
	33	33		
	-0.3	-0.3		
	33	33		

Cultivated field

Cultivated field

Sta.	Elev.	
161	890.7	✓
160	888.7	✓
159	886.4	✓
+60	884.7	✓
158	880.3	✓
+35	873.8	✓
157	872.5	✓
156	871.4	✓
+66	872.0	✓
+63	870.8	✓
155	868.2	✓
+65	868.0	✓

Prescott Cont. P.J.C. 4/18/23

L. A. Line

	L.	R.
161	+0.2 -1.0 33 33	
	+0.9 -1.2 33 33	
	+1.2 +0.5 -1.3 -2.7 33 20 19 33	
	+1.3 +0.4 -1.3 -2.8 33 18 17 33	
	+3.5 +1.6 -2.1 -4.0 33 18 14 33	
Cultivated field	+6.3 +4.5 +2.5 +0.8 -0.7 -1.0 45 33 23 12 20 33	Cultivated field
	+2.5 +0.7 -0.5 34 14 133	
	+0.6 00 -0.4 33 20 33	
	+0.5 -0.5 33 33	
	+0.5 00 00 00 34 19 23 35	
	-0.8 -0.3 +0.8 +1.5 35 25 14 35	
	-1.0 -0.5 +0.7 +1.6 34 20 21 35	

Sta.	Elev.
154	871.4
+74	873.5
+65	870.0
+61	871.2
+50	871.2
+40 - 0.8	870.4
+35	869.4
+15	876.6
153	875.4
+33	874.9
152	877.6
+40	879.5

Prescott Cont. P.S.C. 4/18/23

L. A. Line

	L.	R.
1.54	-1.8 -1.0	+1.2 +2.3
	37 22	20 34
	-1.8 -1.4	+1.2 +1.8 +2.0
	33 13	13 32 35
	-1.0 -0.6	+0.9 +1.8
	34 19	17 33
	-2.8 -2.0 -1.2	+1.2 +2.5 +4.0
	50 33 17	18 34 50
	-2.2 -1.6 -1.0	+1.6 +2.2 +3.8
	50 33 17	25 33 50
	-2.5 -1.5 -1.0	+1.4 +2.2 +3.5
	50 33 17	18 33 50
	-1.3 -0.7	+0.8 +1.8
	33 19	21 33
	-2.2 -1.4	+0.9 +2.5
	33 16	15 33
	-2.5 -1.2	+2.1 +2.5
	33 15	23 33
	-3.3 -1.6	+2.5 +4.4
	33 17	19 33
	-3.7 -1.9	+1.4 +2.6
	33 18	14 33
	-3.6 -1.5	+1.8 +3.0
	33 16	17 33

Sta.	Elev.	
151	877.5	✓
+14	884.4	✓
150	885.4	✓
149	886.8	✓
148	~~887.5~~	887.7
147	~~888.7~~	888.9
146	~~889.6~~	889.8
145	~~888.1~~	888.3
+50	~~888.0~~	888.2
144	~~888.0~~	888.2
+50	~~888.2~~	888.4
143	~~889.7~~	889.9

Prescott Cont. P.J.C. 4/18/23

L. A. Line

	L.		R.	
151	-1.7	-0.8	+1.7	+3.2
	33	17	17	33
	00	00	-0.3	-0.7
	33	17	19	33
	00		+0.2	
	33		33	
	-0.2		00	
	33		33	
	-0.7		00	
	33		33	
	-0.6		-0.3	
	33		33	
	-0.6		00	
	33		33	
	-0.2		00	
	33		33	
	-1.3		+0.1	
	33		33	
	-1.1		+1.0	
	33		33	
	-1.8		+1.4	
	33		33	
	-1.7	-0.8	+1.0	+1.2
	33	18	14	33

Cultivated field

Cultivated field

Sta.	Elev.	
+80	~~888.6~~	888.9
+75	~~884.7~~	884.9
+50	~~885.8~~	886.0
+25	883.4	✓
+05	882.5	✓
142	883.7	✓
+65	884.5	✓
+50	886.4	✓
141	887.3	✓
+50	887.9	✓
140	887.7	✓
+50 +0.2	887.9	✓

Prescott Cont. P.J.C. 4/18/93

L.A. Line

L					R			
-0.1	00	+0.4	00		-1.5	-3.0	-1.5	
37	26	12	8		10	30	36	
+3.7	+3.0	+1.2	+0.5	+1.0				
34	23	17	18	34				
+1.3	-2.3	-1.7	+0.3	+0.5				
37	32	24	29	37				
-0.5	00	+0.2	+0.8	00	-0.7	+0.7		
39	30	17	10	18	30	36		
-0.5	+0.5	-0.5	+0.5	+1.7	+3.0			
40	33	18	9	12	39			
-1.5	-0.7	-2.0	-1.8	-0.8	+0.8	+2.0	+2.5	
40	33	20	15	8	12	28	41	
-4.0	-3.0	-1.2	+2.2	+3.5	+4.0	+3.8		
33	25	10	11	28	33	42		
-7.5	-7.0	-5.0	-3.2	-1.4	+1.5	+2.5		
35	33	28	21	14	25	33		
-1.4	-1.5	+2.0	+1.6					
33	20	29	33					
-2.3	-1.0	+1.2	+1.5					
34	14	24	33					
-1.4	-1.2	+1.0	+2.0					
33	19	21	33					
-1.4	-0.7	+1.1	+2.0					
33	18	19	35					

Sta.	Elev.
140+50	
139+21.8 B.C.+0.9	888.8 ✓
139	889.7 ✓
138	892.1 ✓
+15.0 E.C.	892.3 ✓
137	892.0 ✓
+50	888.7 ✓
136	886.3 ✓
+50	884.9 ✓
135	884.0 ✓
+50	883.4 ✓
+15.0 B.C.	883.2 ✓
134	883.1 ✓

Prescott Cont. F.M.C. 4/18/23

L. A. Linc

L.			R.	
-2.0	-1.2	+0.7	+1.4	
34	20	28	33	
-1.7	-0.9	+1.0	+1.8	
33	16	19	34	
-2.3	-1.2	+1.3	+2.0	
33	17	21	33	
-4.3	-2.0	+1.2	+2.7	
35	17	19	34	
-4.1	-2.6	+1.7	+3.4	
34	20	19	33	
-3.2	-1.7	+1.2	+2.6	+3.2
35	15	19	30	34
-1.8	-1.0	+1.5	+2.8	
37	16	22	34	
-1.2	-1.1	+1.4	+3.0	
35	19	19	34	
-0.7	-0.5	+0.7	+2.0	
34	21	19	34	
-0.8	-0.5	+0.7	+1.3	
36	19	18	34	
-0.8	-0.7	+0.6	+1.2	
34	18	22	33	
-1.0	-0.7	+0.6	+1.5	
34	20	18	33	

Sta.	Elev.
133	882.0
132	880.9

Prescott Cont.

F.M.C. 4/18/23

L. A. Line

L.		R.	
-0.5	-0.5	+0.3	+1.6
32	17	18	34
-1.2		+0.5	+2.0
33		14	33

Prescott Cont. P.S.C. 4/17/23

L. Line,

X sections on the
16° Curve From Sta.
51+78.7 E.C. to 48+70

Sta.	Elev.
51+78.7 E.C. Curve	804.6
+50	804.6
51	803.5
+50	805.1
50	807.1
+50	800.2
+25	794.0
49 772.0	
48+95 -3.0	769.0
48+85 -2.8	769.2
48+79.8 B.C. 16° Curve	
48+70 -2.5	787.4
48+59 787.9	

Prescott Cont. P.T.C. 4/17/23

L. line

	L.					R.				
	-20.0	-15.0	-13.6	-10.0	-5.0	+5.0	+10.0	+12.4	+15.0	+19.4
	50	38	33	24	12	13	28	33	40	50
		-17.3	-11.7	-5.0		+5.0	+10.0	+11.5	+15.0	+19.5
		50	33	14		15	29	33	41	50
51		-19.5	-14.2	-10.0	-5.0	+5.0	+10.0	+13.3	+15.0	+20.0
		50	33	22	11	12	23	33	38	50
	-20.5	-20.0	-13.2	-10.0	-5.0	+5.0	+10.0	+13.3	+15.0	+17.6
	50	48	33	24	13	12	22	33	41	50
		-17.2	-15.0	-12.7	-8.5	-5.0	+3.0	+5.0	+8.5	+10.0	+11.5
		50	39	33	24	14	10	15	33	43	50
	-17.8	-15.0	-11.7	-10.0	-4.5	-1.5	+5.0	+7.6	+10.0	+11.0	
	50	44	33	28	14	10	21	33	45	50	
	-15.9	-15.0	-11.5	-10.0	-5.0	-2.4	+2.9	+5.0	+8.0	+10.0	
	50	45	33	28	12	2	14	26	33	50	
	-7.0	-7.0	-4.0	-3.0	-2.6	-0.5	+1.1	+1.7	+1.4	+10.0	+12.5	+12.2	+15.5
	50	47	39	20	7	6	8	15	23	27	38	40	50
	-7.0	-7.0	-4.0	-3.0	-2.6	-0.5	+1.1	+1.7	+1.4	+10.0	+12.5	+12.2	+15.5
	50	47	39	20	7	6	8	15	23	27	38	40	50
		-11.6	-10.0	-9.3	-5.0	-3.4	+3.8	+5.0	+7.3	+10.0	+13.0	+19.8	
		50	45	33	14	9	7	12	21	26	33	50	

X sections

114+40 PW #6

124+50 PW #6

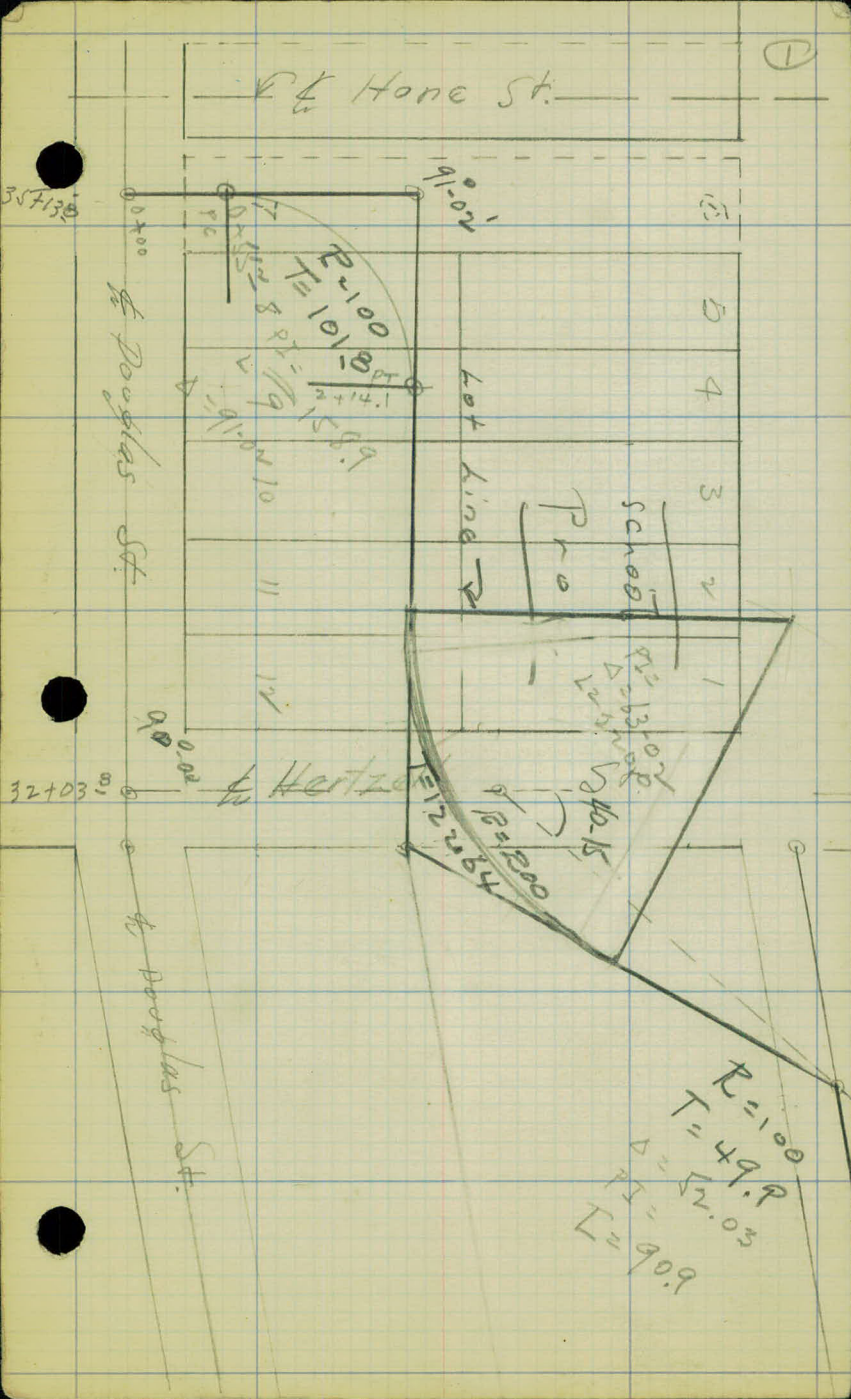
139+45 P. 30" P3

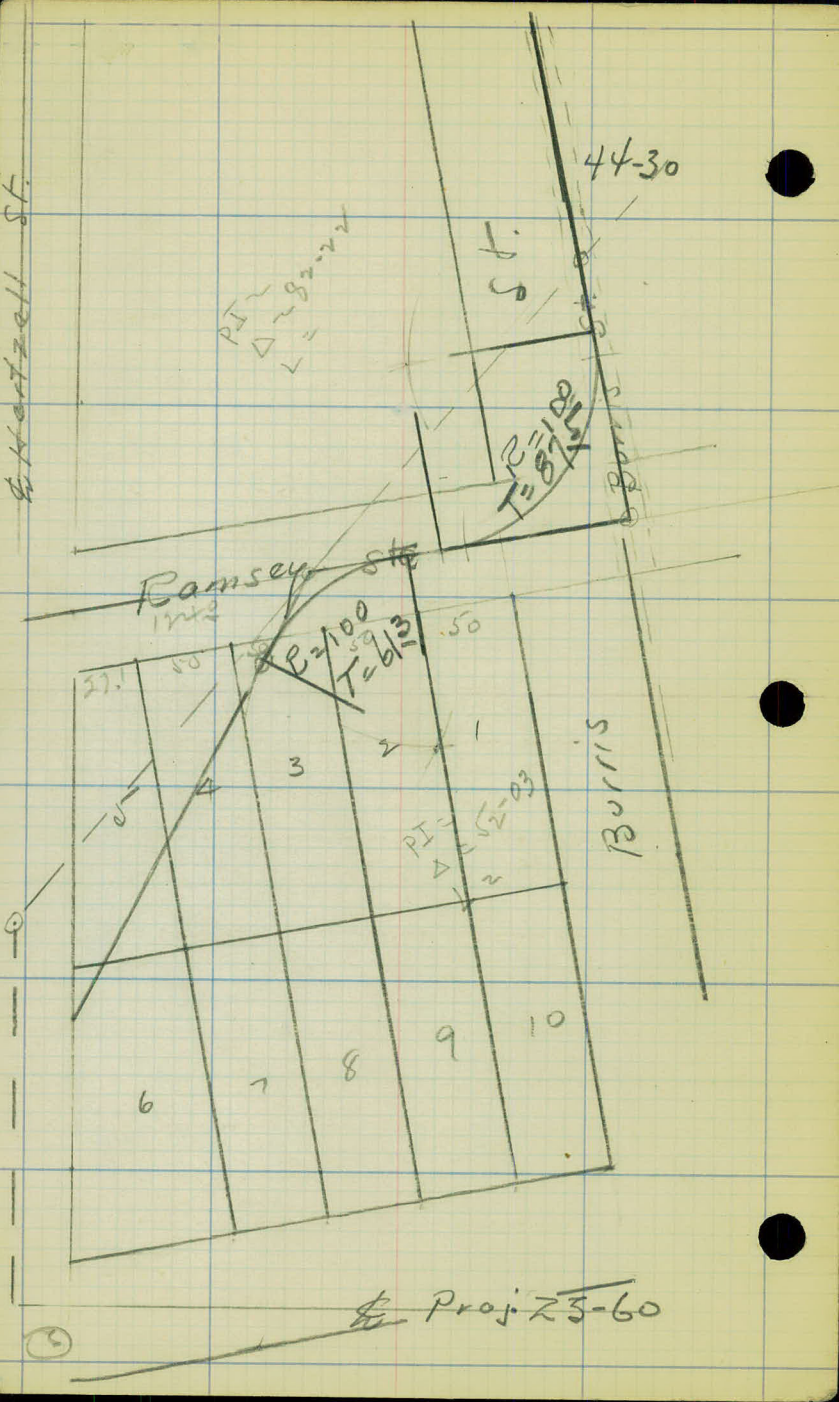
Burris St. Connection
Proj - 23-60

INDEX

Sheet to Sheet	
1 — 2	General Layout.
3 — 6	Align.- Red line
7 — 9	X sects ✓ ✓
10 — 11	Align.- Blue line
12 — 14	X sections - ✓ ✓

Conner
Wilshusen
Mahoney
Keogh
Apr. 14 '15 - 1924


Hone St.
Douglas St.
Hertzel
Douglas St.
School
Pro
Lot Line
R=100
T=101.8
R=100
T=49.8
R=2200
T=12.64
R=1300
T=40.15
91°02'
90°00'
35+71.38
32+03.8
1
2
3
4
5
12


44-30
Hartzell St.
Ramsey St.
Burris
PI~
Δ~82-22
L=
R=100
T=81.3
PI~
Δ~52-03
L=
50
1
2
3
4
5
6
7
8
9
10
Proj. 73-60

Alignment
Red line

Burris Street Connection
Proj - x3-60

Stg. Point Lt △ Rt.

2+14± PT

45-31

PI = 1+57.0

△ = 91-0

R = 100 ft. Rt.

T = 101.8

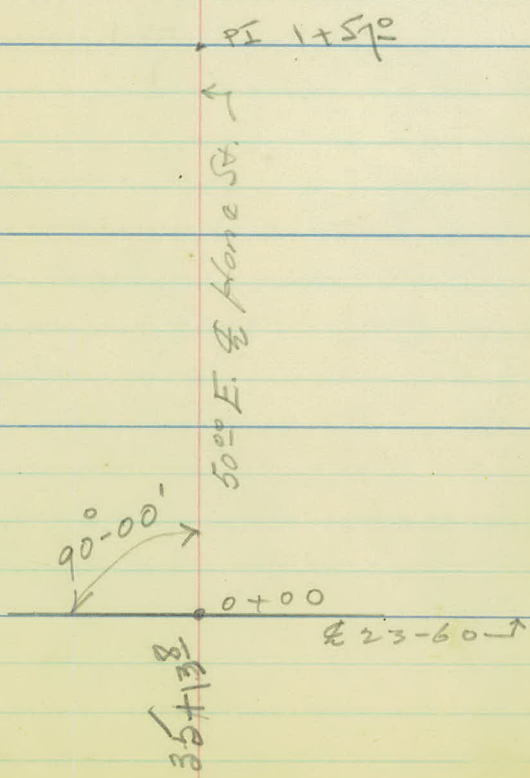
L = 158.9

0+55 PC.

00

0+00 = Stg 35+13.8 Proj 23-60

Red line (4)



Sta Point Lt. Δ Rt.

7+31.1 = 7+29.9

~~+31~~ PT 26-01½ PI = 6+90.2

+25 24-07 Δ = 52-03 Rt.

7 16-58 R = 100'

+75 9-49 T = 49.9 48.8

+50 2-40 L = 90.8 ✓

6+~~41.2~~ 40 P.C. 00

+50.3 ✓ PT 31-31 PI = 4+52.9

5 24-19½ ✓ Δ = 63-07 ✓

+50 17-09½ ✓ R = 200 ft Rt Lt.

4 9-59½ ✓ T = 122.6 ✓

+50 2-49½ ✓ L = 220.0 ✓

3+30.3 ✓ PC 00

Red Line (5)

Note P.I 6+90 Red line = P.O.T. 4+33.8
Blue line

Sta Point Lt. Δ Rt.

+08 3 P.T. 41-11

9+00

+75

+50

+25

8

+75

7+64 5 PC 00

PI = 8+52.0

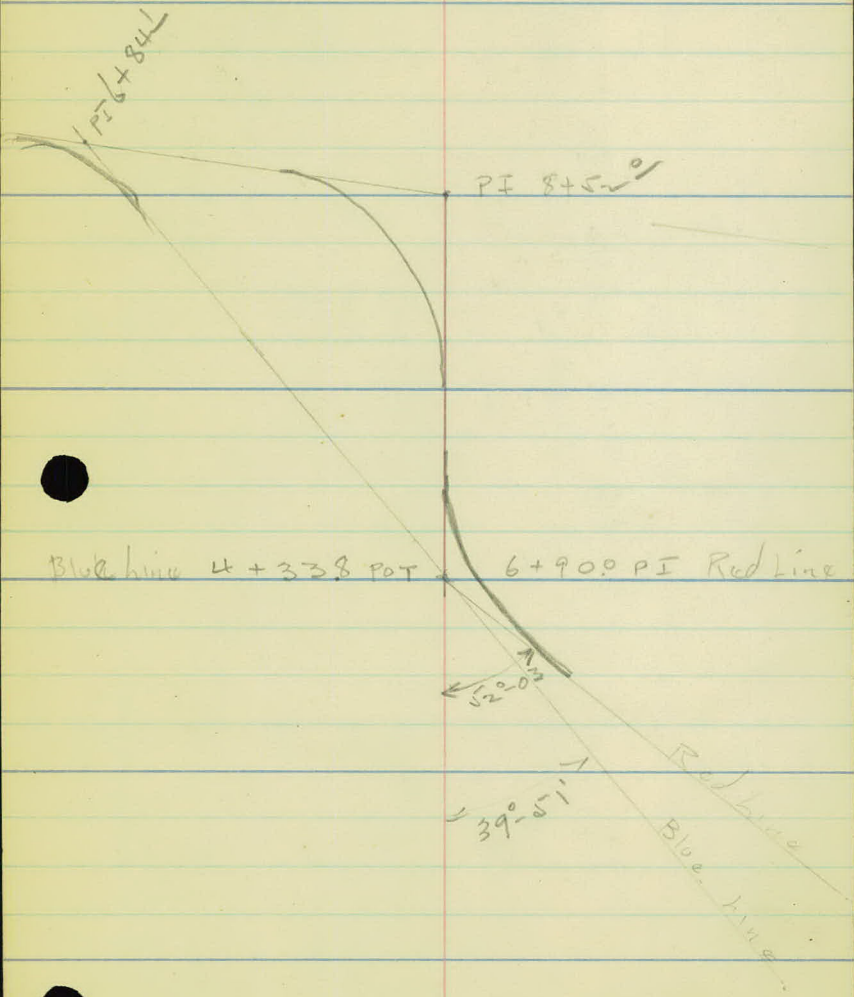
Δ = 82°22'

R = 100° Lt.

T = 87.5

L = 143.8

Red Line


PI 6+84
PI 8+5
Blue line 4+338 POT
6+900 PI Red Line
52°-0'
39°-5'
Red line
Blue line

(7)

& levels & X sections
of
Burris St. Connection
Red line

Proj - 23-60

Sta.	+	HI	-	El.
T.P.	11.66	859.21		847.55
T.P.	1.80	852.48	8.58	850.63
0+00			12±	840.4
0+55.2	P.C.		8.7	43.8
1+00			5.3	47.2
	9.37	858.86	2.99	849.49
1+50			8.4	50.5
2+00			8.0	50.9
2+50			9.8	49.1
3+00			11.8	47.1
3+50			12.3	46.6
T.P.	12.21	859.73	11.34	847.52
4+00			13.5	46.2
4+50			13.0	46.7
5+00			11.3	48.4
5+50	3 PT		4.0	55.7
T.P.	11.06	869.49	1.30	858.43

Lt. Ct. Red Line (8)

Sta 4+50 Top of stake Red line -

11.0	12.1	11.9
33	00	33
7.8	8.7	9.4
33	00	33
1.8	5.3	7.6
33	00	33

top of stake 1+25 Red line -

2.8	3.9	7.7	8.4	10.6	12.3
33	24	6	00	28	30
2.0	6.5	8.0		11.7	
33	12	00		33	
3.4	8.7	9.8		13.3	
33	14	00		33	
6.9	9.9	11.8		14.1	
33	19	00		33	
10.6	10.9	12.3		14.6	
33	28	00		33	
9.8		13.5		15.6	
33		00		33	
9.0		13.0	14.0	15.6	
33		00	10	33	
6.6		11.3	13.4		
33		00	33		
00	0.9	4.0	10.7		
33	22	00	33		

Sta.	+	HI	−	El.
6+00		69.49	9.4	60.1
+50			5.6	63.9
7+00			3.7	65.8
T.P.	5.96	71.19	4.26	65.23
7+75			9.6	64.6
8+00			10.2	64.0
8+50			10.3	63.9
9+00			5.6	68.6
B.M.			3.76	67.43

Lt.		℄	Rt.	
Lt.			Rt.	
6.5 / 33		9.4 / 00	11.9 / 33	Red Line
2.2 / 33		5.6 / 00	8.8 / 33	
0.0 / 33		3.7 / 00	7.2 / 33	
5.5 / 33	9.5 / 11	9.6 / 00	13.7 / 33	
6.5 / 33	9.5 / 13	10.2 / 00	13.5 / 33	
5.4 / 33	8.9 / 5.0	10.3 / 00	10.1 / 17	10.8 / 33
3.9 / 33	4.4 / 17	5.6 / 10	5.6 / 00	6.3 / 13	6.9 / 33

Nail on 8" Elm 12'-Lt sta 9+00 Red Line

Alignment
Blue Line
Burris Street Connection
Proj - 23-60

Sta. Point Lt. Δ Rt.

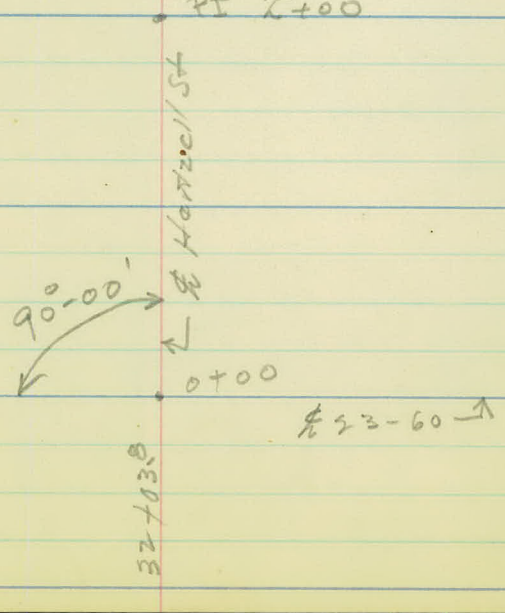
7+20.9 ✓ P.T. 32-15 PI = 6+84.1
7+00 Δ = 44-30
+75 R = 100 ft Lt.
+50 T = 40.9 ✓
6+43.2 ✓ P.C. 00 L = 77.7 ✓

4+33.8 P.O.T. = PI 6+90 Bed line.

2+33.6 = ~~2+33.9~~
~~2+33.9~~ P.T. 20-07½ ✓ PI = 2+00
+25 Δ = 40-15
✓ R = 100 ft. Lt.
+75 T = 36.7 ✓
1+63.3 P.C. 00 L = (70.6) 70.3

0+00

Blue line (11)



℄ levels & X sections
Burris St. Connection
Blue line

Proj-23-60

Sta.	+	H.I.	-	Elev
B.M.	10.64	847.68		837.04 = 738.04
0+00			12.1	35.6
0+14			13.2	34.5
0+25			9.4	38.3
0+50			7.7	40.0
1+00			5.3	42.4
1+50			2.7	45.0
1+75			1.0	46.7
T.P.	11.66	859.21	0.13	847.55
2+00			10.4	48.8
2+25			8.2	51.0
2+50			5.9	53.3
T.P.	9.76	867.44	1.53	857.68
2+85			8.5	58.9
3+00			8.2	59.2
3+50			5.6	61.8

Blue Line

Lt ℄ Rt. Blue Line

Sp. in Cottonwood · 45° R. of 30+20

Lt	℄	Rt.
11.2 / 33	12.1 / 00	12.8 / 33
11.8 / 33	13.2 / 00	13.3 / 33
8.8 / 33	9.4 / 00	9.5 / 33
6.8 / 33	7.7 / 00	8.2 / 33
4.4 / 33	5.3 / 00	4.9 / 15 — 5.7 / 33
2.1 / 33	2.7 / 00	3.3 / 33
0.1 / 33	1.0 / 00	1.9 / 33

Top of stake 4+50 - R-LINE

8.6 / 33 — 9.0 / 27 — 8.3 / 25 — 10.4 / 00 — 12.7 / 26 — 12.2 / 33

3.7 / 33 — 5.2 / 23 — 8.2 / 00 — 8.9 / 12 — 11.5 / 33

0.1 / 33 — 2.3 / 24 — 4.4 / 13 — 5.9 / 00 — 7.6 / 13 — 9.5 / 22 — 10.7 / 33

Top Rock

5.3 / 33 — 7.0 / 20 — 8.5 / 00 — 10.4 / 6.0 — 11.4 / 15 — 14.6 / 33

4.7 / 33 — 8.2 / 00 — 9.5 / 17 — 11.0 / 30 — 12.2 / 33

1.6 / 33 — 5.6 / 00 — 6.6 / 17 — 7.6 / 23 — 8.4 / 33

Sta	+	HI	−	El.
		867.44		
TP	9.46	875.31	1.59	865.85
4+00			10.0	65.3
4+50			7.5	67.8
5+00			4.7	70.6
T.P.	6.88	881.13	1.06	874.25
5+50			7.8	73.3
6+00			6.0	75.1
6+20			2.8	78.3
T.P.	5.36	881.53	4.96	876.17
6+50			3.6	77.9
+75			4.8	76.7
7+00			1.8	79.7
B.M.			11.10	870.43
T.P.	9.50	890.51	0.5	881.01
7+20.9 P.I			7.8	82.7

Blue Line

top of stake L+00 blue line

6.7 33 | 10.0 00 | 13.5 33

3.4 33 | 4.5 25 | 7.5 00 | 9.5 14 | 10.1 26 | 11.2 33

1.4 33 | 3.7 8 | 4.7 00 | 7.5 26 | 8.4 33

Rock S.E. Cor. Church.

1.1 33 | 5.0 22 | 7.8 00 | 9.4 8 | 12.0 33

(+5.4) 33 | 0.8 19 | 1.7 5 | 6.0 00 | 7.8 12 | 10.3 21 | 11.0 33

(+6.4) 33 | (+3.6) 15 | (+0.3) 12 | 00 8 | 2.8 00 | 5.7 8 | 6.8 12 | 9.2 16 | 10.5 33

(+7.6) 33 | (+0.8) 16 | 00 13 | 3.6 00 | 6.2 11 | 8.3 14 | 9.4 33

(+7.4) 33 | (+4.6) 10 | 4.8 00 | 6.8 24 | 7.4 27 | 6.8 28 | 6.7 33

(+8.0) 33 | (+7.0) 28 | (+4.5) 18 | 1.8 6 | 1.8 00 | 1.6 9 | 0.9 11 | 1.0 20 | 1.4 33

one nail 8" Elm. 12 ft Lt 9+00 Red line

+1.6 33 | 1.7 21 | 3.2 14 | 8.1 8 | 7.8 00 | 7.7 19 | 8.6 33

(0)

Proj 23-60

Align Notes

Sta. 82+24.9 P.T. to 112+71.3 P.T.

F.M. Conner
H.L. Wilshusen
Jos. Mahoney
Warren H. Sleeger

April 22-23-1924

0 - 5 - Sheets

(Alignment taken over proper location)

RJH

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 4-28-24

File No.

Sta	Point	∠t	△	Rt	Calc Bear.
					N45-51W ✓
89+17.4 ✓	P.T				16-09½
+50					14-47½
89					12-17½
+50					9-47½ PI 88 +20.3 ✓
					△ = 32°-19' ✓
88					7-17½ D = 10-00 PT
					T = 166.1 ✓
+50					4-47½ L = 323.2 ✓
					R = 573.69
87					2-17½
86+54.2 ✓	P.C.				00
					N78-10W
82+24.9	EC ✓				

10" Oak

30 ± 0

PI 88+20.3

3 + 10

10" Oak

88+20.3
+66.1
8654.2

Sta	Point	Lt Δ Rt	Calc Bear.
			S 81°-49' W
			S 89-41 W
9+64.6	P.R.C.	26-10	
+50		24-42½	
9		19-42½	
+50		14-42½	
91		9-42½	PI = 91+44.3 Δ = 52-20 T = 141.44 ✓
+50		4-42½	L = 261.67 ✓
90+03.9	P.C.	00	D = 20°-00' Lt R = 287.94
			N 45-51 W ✓

Double Oak

23 50

PS 91 + 44.3

39 30

30" Oak.

Sta	Point	Lt Δ Rt	Calc Bear.
			N72°-58'W
			PI = 93+71.6
			Δ = 25°-13'
94+74.7	P.T.	12-36½	D = 12°-00' Rt.
			T = 107.0
+50		11-07½	L = 210.14
			R = 478.34
94		8-07½	
+50		5-07½	
+25		3-37½	
93		1-07½	
92+64.6	PRC	00	
			S89-41W
			S 81°-49' W

10" Oak
3 nails near ground
70 00

PI 93+71.6

6" Elm
53 26
3 nails 7 ft. above ground

Sta	Point	Lt.	Rt.	Calc. Bear.
104+50	POT			
				N55-45W.
103+56.3	PT		8-36½	PI = 102+14
				Δ = 17°13'
103			6-55	D = 6-00 Rt.
				T = 144.56
	+50		5-25	L = 286.94
				R = 955.37
102			3-55	
	+50		2-25	
101			0-55	
100+69±	PC		00	
				N72-58W

15" Oak
3 nails

47 10

90 T 104 + 50

12" oak
3 nails

70 60

PI 102 + 140

10" oak
3 nails
up 8 ft.

48 24

15" oak
3 nails

68 30

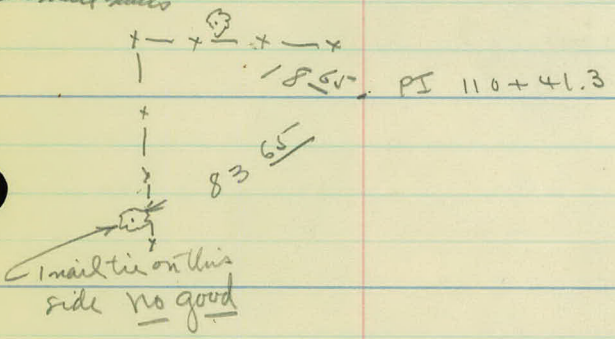
Sta	Point / Equation	∠ Δ Rt.	Calc Bear
114+45.6			N27-34 W = ✓
112+71.3 ✓	P.T.	14-05½	
+50		13-27	
112		11-57	
+50		10-27	
111		8-57	P I = 110+41.3
			Δ = 28°-11'
+50		7-27	D = 6°00 Rt
			T = 239.7 ✓
110		5-57	L = 469.7 ✓
			R = 955.37
+50		4-27	
109		2-57	
+50		1-27	
108+01.6 ✓	P.C.	00	
			N55-45W ✓

N 27-36' W.

~~N 28° 03' W~~

(5)

1 large nail 30" oak
2 small nails



Project 23-60

Level Notes

Sta. 86+00 to 112+71 3/4

Sta	+	H.I.	−	Elev.	
B.M.	480	885.73 ✓		880.93 ✓	
86+00				78 2/5 ✓	
+54 2/5	P.C.			78 0/0 ✓	
87+00				79 0/0 ✓	
+50				76 6/10 ✓	
88+00				75 7/10 ✓	
+50				80 2/10 ✓	
89+00				81 4/10 ✓	(20/72)
+50				81 4/10 ✓	
90+02 9/10	P.C.			81 7/10 ✓	(0.0/15.2)
+50				81.4 ✓	
91+00		✓		80 5/10 ✓	
T.P.	0.82	881.89	4.66	881.07 ✓	
+50				78 9/10 ✓	

Lt. Rt. O.K. F.W.C.

??? Spain Blessed Elm 13' R. Sta. 91+33 (Conner's Orig. Line)

R.J.W. 4-26-24

7.5/00

7.7/00

6.7/00

9.1/00

10.0/00

(00/80) 11.5/80 10.8/75 9.5/66 6.2/52 5.8/47 5.5/00 5.2/33

11.3/97 10.3/90 8.8/81 7.3/76 6.2/70 4.9/34 4.3/00 3.6/33

(00/13) 11.3/131 9.0/118 8.1/108 6.6/100 5.7/66 4.8/45 4.3/00 3.5/33

11.0/152 8.6/131 6.9/145 5.1/115 5.0/106 4.4/100 4.0/68 4.6/33 4.0/00 2.8/33

(00/142) 11.3/142 6.4/100 5.5/80 5.4/57 4.5/52 4.8/29 4.3/00 3.7/33

(00/111) 12.7/111 11.0/97 8.7/68 6.5/28 5.2/00 4.1/23 4.3/33

15.5/100 11.6/70 7.7/46 5.0/20 3.0/00 1.9/38 3.3/62 3.4/70

Sta	+	H.I	-	Elev.
		881.89 ✓		
92+00				75 3/10 ✓
+25				72 1/10 ✓
T.P.	2.16	871.80 ✓	12.25	869.64 ✓
+50				
T.P.	1.93	862.91 ✓	10.82	860.98 ✓
+64 6/10				56 6/10 ✓
+75				49 2/10 ✓
+86				40 2/10 ✓
93+00				49 7/10 ✓
T.P.	10.79	873.10 ✓	0.60	862.31 ✓
+25				64.9 ✓
T.P.	11.72 ✓	884.63 ✓	0.19	872.91 ✓
+50				73 6/10 ✓
+56				
94+00				81 10/10 ✓
+50				81 10/10 ✓
+74 7/10	P.T.			81 00/10 ✓

Lt ℄ Rt.
Windy · cold

16.3/49 11.6/28 6.6/00 5.2/26 7.1/52 9.4/70

9.8/00 8.1/21 9.0/40

(Bottom draw)

14.3/40 11.6/28 8.8/00 9.4/39 13.0/65 14.5/70

6.3/00

13.7/00

28.7/65 22.7/00 18.1/25

DOWN HILL 11.6/75 14.4/61 13.2/00 10.1/33 15.9/61

11.3/35 8.2/00 7.8/22 9.2/36

13.2/82 11.0/20 11.0/00 10.9/15 12.3/30

(0.0/86) 11.0/86

(0.0/99) 11.0/99 5.2/60 4.0/38 3.5/00 3.3/36

(0.0/87) 11.0/87 5.6/55 4.2/30 3.5/00 3.3/35

(0.0/79) 11.0/79 5.4/43 4.2/24 3.6/00 4.1/35

Sta.	+	H.I.	-	Elev.
		884.63 ✓		
B.M.			0.80	883.83 ✓
	1.02 ✓	884.85 ✓		
95+00				80.1 ✓
+50				76.1 ✓
96+00				72.7 ✓
+10				72.0 ✓
+75				78.4 ✓
97+00				80.7 ✓
+50		✓		80.4 ✓
T.P.	5.85	885.45	5.25 ✓	879.60 ✓
98+00				76.6 ✓
+50				78.3 ✓
99+00				77.3 ✓
+50				80.3 ✓

Lt. ℄ Rt.

Spike in 1: 09K 70' Rt 95+50 · 3No16

5.3 / 35	5.0 / 29	4.8 / 00	4.5 / 35
(0.0 / 70) 11.8 / 70	9.1 / 45	7.9 / 31	8.8 / 00	4.7 / 35
20.9 / 40	20.2 / 28	12.2 / 00	7.6 / 20	5.4 / 35
28.9 / 60	24.3 / 35	12.9 / 00	5.6 / 35
(0.0 / 38) 11.8 / 38	10.9 / 35	6.5 / 00	4.2 / 35
(0.0 / 57) 11.8 / 57	8.9 / 35	4.2 / 00	2.7 / 35
(0.0 / 62) 11.8 / 62	7.9 / 35	4.5 / 00	3.1 / 35
	13.0 / 35	8.9 / 00	4.7 / 35
	15.2 / 35	7.2 / 00	2.2 / 35
	14.8 / 35	8.2 / 00	3.8 / 35
	7.2 / 35	5.2 / 00	4.0 / 35

Sta	+	H.I.	-	Elev
		885.45 ✓		
100+00				82.4 ✓
			4.31	881.14 ✓
101			6.2	79.3 ✓
+50			6.5	79.0 ✓
T.P.	6.05	883.18 ✓	8.32	877.13 ✓
102			4.3	78.9 ✓
+50			4.8	78.4 ✓
103			6.2	77.0 ✓
+56 3	P.T.		8.7	74.5 ✓
104			5.4	74.8 ✓
T.P.	1.51	877.04 ✓	7.65	875.53 ✓
+50			4.9	72.1 ✓
T.P.	0.96	865.92 ✓	12.08	864.96 ✓
105			2.1	63.8 ✓
+25			6.4	59.5 ✓
+40			11.6	54.3 ✓

Lt. | ℄ | Rt.

4.0 / 35 | 3.1 / 40 | 3.5 / 35

Austins B.M. (881.08) R.J.W. 4-26-24

10' L · 100+65 - 8" Oak.

4.2 / 40

Sta	+	H.I.	−	Elev	
		865.92			
T.P.	0.52	854.58	11.86	854.06	
105+50			35	51.1	
+75		843.54	12.1	42.5	
T.P.	0.37	843.84	11.41	843.47	843.17
106			10.8	33.0	32.7
+30		833.15	14.1	29.7	29.4
T.P.	0.62	833.45	11.01	832.83	832.53
B.M.			4.83	828.32 / 828.62	828.32
107			6.5	27.0	26.6
108			10.0	23.5	23.1
+50			11.3	22.2	21.8
109			9.8	23.7	23.3
+50			5.8	27.7	27.3
110		831.52	3.4	30.1	29.7
T.P.	1.37	831.82	3.00	830.45	830.15
+50			2.8	29.0	28.7
111			5.7	26.1	25.8

nail in EP 33' Rt 105+00

Sta.	+	H.I.	−	Elev.	
		831.52 ✓			
		831.82			
111+50		822.24 ✓	11.0	810.8	20.5 ✓
T.P.	7.60	827.51	11.91	819.91	819.61 ✓
112 ✓			3.2 ✓	19.3	19.0 ✓
+50			2.7	19.8	19.5 ✓
=114+56					
112+73	P.T.	812.78 ✓	3.6	18.9	18.6 ✓
T.P.	7.31	813.08	11.74	810.77	810.47 ✓
T.P.	7.62 ✓	803.47	12.23	801.85	800.55 ✓
		803.17 ✓	7.62 ✓	795.55	795.23 ✓
				795.55 ✓	

6 pike in 10" Cottonwood 10' Rt sta 117+25

Hail Cottonwood 45'R-30+30-23-60

	+	∆ 755.88 ✓	−	Elev.
			4.9	751.0 ✓
1+25			7.6	748.3 ✓
1+08 3 P.T			9.5	746.4 ✓
0+75 8 P.I.			13.9	742.0 ✓

Nail in 10" elm tree - 15' Lot E of Rd at 9+65

738.04

Sta.	+	I	−	Elev.
		753.75		
6+50			4.3	749.5
6			5.8	748.0
5+53.7			6.6	747.2
4+77.0 Ext.			7.7	746.1
T.P.	8.55	749.90	12.40	741.35
BM		749.90	11.86	738.04
4+00			3.3	746.3
3			1.7	748.2
T.P.	6.88	755.88	0.90	749.00
2+13			4.3	751.6
2			3.2	752.7
1+75			3.0	752.9

6/2/24 Murphy
Ahlberg

℄ Elev. New Borris St. Connection

	+	IT	−	Elev.
B.M.				
	1.07	772.48 ✓		771.41
9+50			4.5	768.0 ✓
9			8.2	764.3 ✓
8+88 PT			8.7	763.8 ✓
8+50			12.1	760.4 ✓
8+25			13.7	758.8 ✓
T.P.	2.16	761.73 ✓	12.91	759.57 ✓
8+00			5.7	756.0 ✓
+75			8.1	753.6 ✓
+50			9.9	751.8 ✓
7+30 PC			10.2	751.5 ✓
7			11.3	750.4 ✓
T.P.	5.00	753.75 ✓	12.98	748.75 ✓

1 Mag Bearing

PT. 8 +88½ 31°35'

+50 23° 58'

Δ=63°10'L +75 18° 58'

8+20=. P.I. D=40° L 8 13° 58' N12°00' E

℄ old Rd. Burris St. T=89⅝ +75 8° 58'

L=157.9 +50 3° 58'

R=

PC 7+30⅞ 0° 00'

PT. 5 +53⅞

+25

Δ 30°30' δ

4+79⅞ P.I. D=20°

T=78.5 +75

L=152.5

R=287.94 +50

E=10.41

+25

PC 4+01⅜

6/2/25

Norbitt

Murphy

Ahlberg

Nelson

Alignment - Burris St. Connection

PT +13$\frac{01}{}$ 45° 00'

2 39° 23'

Δ = 90° 00' +75 28° 38'

D = 86° R

1+81$\frac{67}{}$ PI T = 73.31 +50 17° 53'

L = 104$\frac{65}{}$

R = 73.31 +25 7° 08'

PI = 1+08$\frac{31}{}$

PT. +07$\frac{14}{}$

1+00

Δ = 90° 00'

0+75$\frac{5}{}$ = PI D = 84° R +75

3.5+13$\frac{6}{}$ Main Line T = 75.41

L = 107$\frac{14}{}$ +50

R = 75.41

+25

PC 0+00 =

Revised —

See other location

other locations made

Apr. 14-15-1924 Comm

Village of Point Douglas

B.M. Sp. in Cottonwood
45' Rt. Sta. 30+30
Elev. 738.04

P.O.T. 27+68.3
℄ C.M.+St. P. Ry.

Cross-Sec. to —
29 - 90'
30 - 70'
31 - 50'
32 - 50'

Scale 1" = 100'