

OFFICE OF
BAMSEY COUNTY ENGINEER
CONSTRUCTION NOTES
PRESCOTT CONNECTION
CO. PROJECT 23-60
FILE No. 4

~~Ed Nesbitt~~

ENGINEERS
FIELD BOOK
No. 10403

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

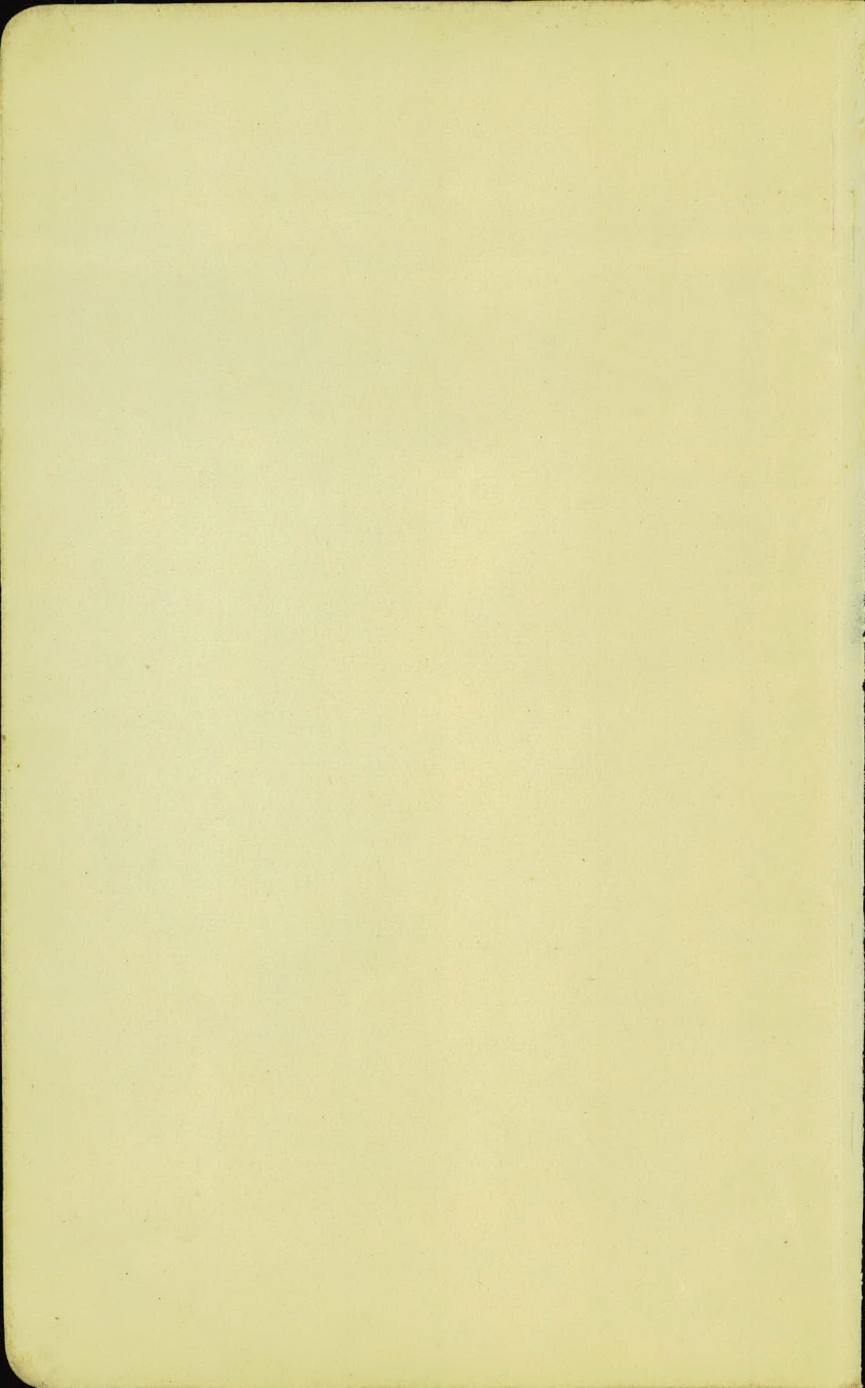
H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

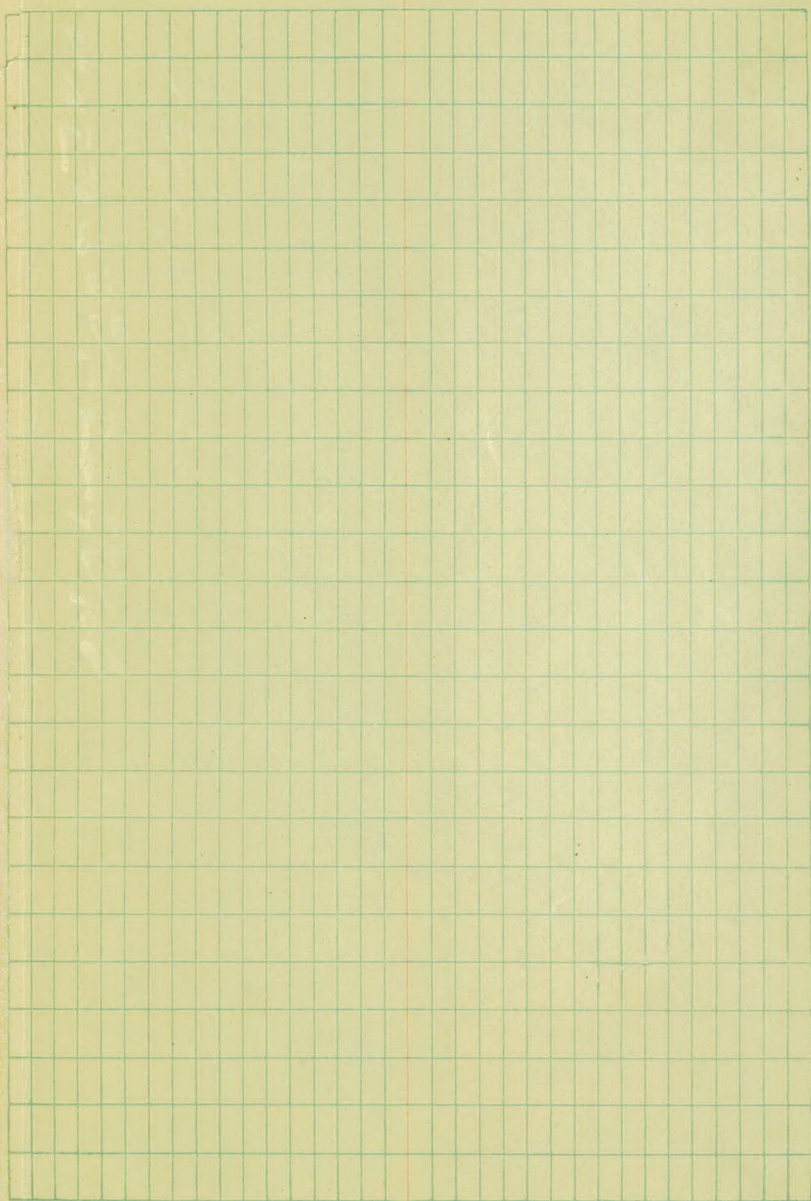
Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \times 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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Book No 4

Proj. 23-60





Sta.	Sta.		Book	Page	Page
80+00	93+50	↑ 153+50	5	3	9
93+75	108+00		4	✓	6
103	106		5	17	17
108+25	118		5	19	16
117+20	153+50		4	7	23
61	79+75		4	24	33
M ^{rs} Betts F.E.			4	36	37
Farm Entr.			4	34	35
✓	✓		4	39	39
✓	✓		5	18	19
Borris St. Conned.		4	40	42	
Culv. Inst.		4	76	77	
0+75	15700	Finals	4	43	50
44+00	67+75	✓	4	51	68

Grades
Final

Sta.	B. S.	H. I.	F. S.	Cross Sections Elev. Grade	Gr. R.
B.M.	7.19	884.52	✓	87738	✓
93+75	875.30			88	9.22
94	876.7			81	8.35
+25				77	
+50	877.17			74	7.35
+75				74	
B.M.			1.41	883.09 (883.11) ✓	
95	877.00			8	7.52 ✓
+25				7.8	
+50	876.30			7.9	8.22
+75	875.96 0.00 pitch 15'			8.3	8.66
96	875.55				8.99
+15	875.40				9.12 ✓
+14	Inv. El. Rt 24" R ₃			77	

Inst. Nesbill
 Rod. A. Baer - No 12011
 Chain. 94.11

9/24/24

Left				BL	Right			
End Board Rail R93+50								
$\frac{5.5}{29}$	$\frac{10.0}{23}$	$\frac{10.3}{18.5}$	$\frac{8.7}{7.5}$	(42) 88	$\frac{9.2}{2.0}$	$\frac{10.3}{2.2}$	$\frac{10.4}{26.5}$	$\frac{5.7}{31}$
$\frac{4.1}{30}$	$\frac{9.5}{22.5}$	$\frac{9.5}{18.5}$	$\frac{7.6}{1.5}$	(43) 81	$\frac{8.6}{1.8}$	$\frac{9.8}{2.2}$	$\frac{9.8}{2.7}$	$\frac{8.5}{5.4}$
$\frac{3.6}{28.2}$	$\frac{8.8}{22.5}$	$\frac{8.6}{1.8}$	$\frac{7.3}{1.5}$	(44) 77	$\frac{8.2}{1.5}$	$\frac{9.2}{2.0}$	$\frac{9.6}{2.6}$	$\frac{3.0}{3.3}$
$\frac{1.0}{27.5}$	$\frac{8.1}{21}$	$\frac{8.2}{17}$	$\frac{6.4}{1.5}$	(45) 74	$\frac{8.0}{1.7}$	$\frac{9.3}{2.0}$	$\frac{9.4}{2.6}$	$\frac{3.4}{3.3}$
$\frac{4.3}{2.7}$	$\frac{7.9}{21.6}$	$\frac{7.7}{17.2}$	$\frac{6.6}{1.5}$	(46) 74	$\frac{7.8}{1.5}$	$\frac{9.5}{1.9}$	$\frac{9.2}{2.4}$	$\frac{3.9}{3.3}$
Noil 12 Oak - 75'R - 94+75								
$\frac{4.5}{2.7}$	$\frac{8.4}{2.6}$	$\frac{8.2}{1.8}$	$\frac{6.7}{1.5}$	(47) 77	$\frac{8.1}{1.6}$	$\frac{9.4}{1.8}$	$\frac{9.4}{2.3}$	$\frac{4.6}{2.6}$
$\frac{5.7}{25.6}$	$\frac{8.6}{21.2}$	$\frac{8.3}{17.5}$	$\frac{7.0}{1.5}$	(48) 78	$\frac{8.1}{1.5}$	$\frac{9.7}{1.8}$	$\frac{9.7}{2.2}$	$\frac{5.1}{2.8}$
$\frac{7.7}{25.3}$	$\frac{9.8}{22.7}$	$\frac{9.6}{19.8}$	$\frac{7.5}{1.6}$	(49) 79	$\frac{8.1}{15.5}$	$\frac{9.7}{19.5}$	$\frac{9.5}{23.5}$	$\frac{5.4}{2.8}$
$\frac{12.7}{28.7}$	$\frac{12.4}{22.5}$	$\frac{8.0}{1.5}$		(50) 83	$\frac{8.3}{1.8}$	$\frac{10.2}{1.9}$	$\frac{10.2}{22.5}$	$\frac{5.6}{26.7}$
	$\frac{8.4}{1.7}$			(51) 84	$\frac{8.6}{1.5}$	$\frac{10.9}{1.9}$	$\frac{10.9}{2.3}$	$\frac{6.0}{2.7}$
		$\frac{8.3}{18.5}$		(52) 86	$\frac{8.7}{7.5}$	$\frac{11.2}{17.5}$	$\frac{10.8}{2.4}$	$\frac{8.9}{26.7}$

Sta.	B. S.	Cross Sections		Grade	Gr. R.
		H, L	F, S.		
		884.52 ✓			
96+35	875.33		8.6		9.19
+50-	00 Ditch Lt.				
+65	875.30		8.9		9.22 ✓
TP	0.12	872.35 ✓	12.29	872.23	
96+35	875.33				(-2.98)
96+15	875.40				(-3.05)
+14-	1st. El. Lt 24' P ₃		13.90		
96	875.55				(-3.2)
TP	12.99	885.12 ✓	0.22	872.13	
97 ✓	875.55				9.59
+25 ✓					
+50-	876.30				8.8
+75					
98 ✓	877.05				8.07
+25					
+50-	877.30				7.82 ✓

Inst.
 Rod.
 Chain.

Left

C L

Right

✓

$$\frac{86}{18.6}$$

$$\frac{9.2}{8.6}$$

$$\frac{86}{15} \frac{10.2}{18} \frac{10.3}{23} \frac{8.2}{26.3} \frac{7.6}{30}$$

$$\frac{11.1}{266} \frac{1.9}{24.5} \frac{1.7}{20.5} \frac{8.8}{16}$$

$$\frac{9.2}{8.9}$$

$$\frac{8.8}{14} \frac{10.5}{18} \frac{10.6}{23} \frac{5.3}{28.8}$$

$$\frac{10.5}{30.5}$$

$$\frac{-2.9}{}$$

$$\frac{1.6}{42.5} \frac{8.6}{40}$$

$$\frac{-3.0}{}$$

$$\frac{7.6}{35}$$

$$\frac{-3.2}{}$$

$$\frac{2.9}{27} \frac{10.7}{22} \frac{10.5}{18} \frac{9.2}{15}$$

$$\frac{9.5}{9.2}$$

$$\frac{9.2}{15} \frac{10.7}{17.5} \frac{10.9}{23.5} \frac{3.0}{32}$$

$$\frac{7.5}{27} \frac{10.8}{22} \frac{10.6}{17.5} \frac{9.0}{15}$$

$$\frac{9.0}{9.0}$$

$$\frac{9.0}{14.5} \frac{10.3}{18} \frac{10.5}{23} \frac{3.0}{31}$$

$$\frac{7.4}{27} \frac{10.5}{22} \frac{10.2}{17.5} \frac{8.8}{15.5}$$

$$\frac{8.8}{8.8}$$

$$\frac{8.6}{18} \frac{9.9}{17} \frac{9.9}{22} \frac{5.6}{30.5}$$

$$\frac{10.0}{21.5} \frac{10.0}{18} \frac{8.6}{15}$$

$$\frac{8.0}{8.7}$$

$$\frac{8.5}{15} \frac{10.0}{18} \frac{10.0}{23}$$

$$\frac{10.5}{20} \frac{8.0}{15}$$

$$\frac{8.0}{8.2}$$

$$\frac{8.0}{14.5} \frac{9.7}{18} \frac{9.8}{23} \frac{5.3}{27.5}$$

$$\frac{7.8}{16}$$

$$\frac{8.0}{8.0}$$

$$\frac{7.8}{15} \frac{9.5}{17.5} \frac{9.6}{22.5}$$

$$\frac{11.5}{23} \frac{7.7}{16}$$

$$\frac{7.8}{7.9}$$

$$\frac{7.7}{15} \frac{9.3}{18} \frac{9.3}{22} \frac{2.6}{30.5}$$

Sta.	B. S.	Cross Sections			
		H. I.	F. S.	Grade	Gr. R.
		885.12	✓		
98+75				8.0	
99 ✓	877.05 End Ditch Lt.			8.3	8.07
+25				8.6	
+50 ✓	876.30			8.8	8.80 ✓
+75				9.4	
100 ✓	875.17			9.8	9.95
+25				10.5	
+50 ✓	873.80			11.3	11.32
B.M.	3.61	877.90 ✓		10.83	874.29 ✓
+75				4.9	
101 ✓	872.17			5.8	5.73
+25				6.6	
+50 ✓	870.30			7.6	7.60

Inst.
 Rod.
 Chain.

Left

C L

Right

$\frac{76}{16}$ 80 $\frac{78}{18.5}$ $\frac{93}{18.5}$ $\frac{24}{22.5}$

8.0

$\frac{132}{24.5}$ $\frac{80}{16}$ 83 $\frac{8.3}{15}$ $\frac{10.5}{18}$ $\frac{10.6}{22.5}$ $\frac{42}{28.2}$

$\frac{10.5}{21}$ $\frac{84}{16}$ 86 $\frac{86}{24.5}$ $\frac{107}{20}$ $\frac{10.9}{24.5}$

8.8

$\frac{116}{68}$ $\frac{90}{39}$ $\frac{109}{30}$ $\frac{102}{23}$ $\frac{101}{19}$ $\frac{89}{15}$ 88 $\frac{9.2}{24.5}$ $\frac{11.0}{19}$ $\frac{11.3}{24.2}$ $\frac{3.5}{30.5}$

$\frac{10.8}{21}$ $\frac{100}{18}$ $\frac{93}{15}$ 94 $\frac{9.7}{15}$ $\frac{11.6}{19}$ $\frac{11.8}{25}$

9.9

$\frac{122}{69}$ $\frac{101}{50}$ $\frac{75}{41}$ $\frac{102}{29}$ $\frac{111}{22.5}$ $\frac{96}{16}$ 9.8 $\frac{10.1}{15}$ $\frac{11.5}{17.5}$ $\frac{12.3}{22.2}$ $\frac{3.4}{32}$

$\frac{10.3}{15}$ 10.5 $\frac{10.8}{15}$ $\frac{12.2}{18}$ $\frac{12.9}{22.5}$

11.3

$\frac{141}{56}$ $\frac{114}{38}$ $\frac{121}{27.5}$ $\frac{126}{22.5}$ $\frac{108}{16}$ 11.3 $\frac{11.9}{15}$ $\frac{13.3}{18}$ $\frac{13.4}{22.5}$ $\frac{3.5}{33}$

Spike 12" Oak - 33' L - 99 + 15

$\frac{6.5}{22.7}$ $\frac{4.5}{15}$ 4.9 $\frac{5.5}{15}$ $\frac{7.2}{18.1}$ $\frac{7.2}{23}$

5.7

$\frac{7.2}{35.5}$ $\frac{7.1}{22}$ $\frac{6.6}{18.1}$ $\frac{5.2}{15}$ 5.8 $\frac{6.3}{16}$ $\frac{8.0}{19.5}$ $\frac{7.9}{22.9}$

$\frac{7.3}{18}$ $\frac{5.9}{15}$ 6.6 $\frac{7.4}{15.7}$ $\frac{8.9}{18.8}$ $\frac{8.9}{22}$

7.6

$\frac{7.0}{39.7}$ $\frac{8.8}{32}$ $\frac{9.2}{23}$ $\frac{8.5}{20}$ $\frac{6.9}{15}$ 7.6 $\frac{8.4}{15}$ $\frac{9.8}{18}$ $\frac{10.0}{23}$

Cross Sections

Sta. B. S. H. I. F. S. Grade Gr. R;

877.90 ✓

101+75

8.7

102 ✓

868.17

98

9.13

+25

TP

305

869.80 ✓

11.5

866.75 ✓

+50 ✓

865.80

4.00

+75

103 ✓

863.30

6.4

863.4

6.50

B17

1210

886.39 ✓

874.29

101

872.17

14.22

+50 ✓

870.30

16.09

102

868.17

18.24

+50

865.80

TP

0.26

880.94 ✓

5.71

880.68 ✓

20.59

103

863.30

17.64

+50

860.80

20.14

Inst.
 Rod.
 Chain.

Left					G L	Right			
				$\frac{9.5}{19.5}$ $\frac{28}{15}$	8.7	$\frac{7.7}{15.5}$ $\frac{11.1}{18.5}$ $\frac{11.2}{22}$			
$\frac{11.4}{44}$	$\frac{11.4}{38}$	$\frac{11.4}{31}$	$\frac{10.6}{20.4}$	$\frac{8.8}{15}$	(9.7)	$\frac{10.8}{15}$ $\frac{12.5}{19}$ $\frac{12.5}{21}$ $\frac{9.8}{24}$			↓ T.R
			$\frac{12.1}{21.5}$	$\frac{10.3}{15}$	10.8	$\frac{11.6}{14.7}$ $\frac{13.1}{19.4}$ $\frac{13.1}{22.5}$ $\frac{10.3}{25.6}$			↓ T.R
$\frac{6.0}{5.8}$	$\frac{6.4}{5.0}$	$\frac{6.0}{5.45}$	$\frac{5.2}{21.5}$	$\frac{8.2}{15.}$	(4.0)	$\frac{4.6}{14}$ $\frac{5.7}{18.5}$ $\frac{5.7}{23}$ $\frac{2.0}{27.5}$			↓ T.R
				$\frac{4.8}{15}$	5.1	$\frac{5.7}{12}$ $\frac{7.1}{18}$ $\frac{7.2}{23}$			
$\frac{7.5}{63}$	$\frac{7.5}{50}$	$\frac{7.7}{39}$	$\frac{7.9}{20}$	$\frac{5.7}{15.5}$	(6.5)	$\frac{6.8}{14.5}$ $\frac{8.1}{18}$ $\frac{8.3}{23}$			↓ T.R
SPK 12" Co C-33 1/2 - 99 + 15									
					(14.2)	$\frac{5.0}{35.0}$			
					(16.1)	$\frac{5.1}{36.5}$			
					(18.2)	$\frac{5.6}{39}$			
					(20.6)	$\frac{7.3}{40}$			
					(17.6)	$\frac{3.1}{42}$			
			$\frac{6.3}{40}$		(20.1)	$\frac{4.9}{42}$			

..... Cross Sections

Sta.	B.S.	H. I.	F. S.	Grade	Gr. R.
		880.94 ✓			
104	858.30				22.64
+25					
+50	855.80				25.16
+75	854.55				26.39
105	853.30				27.64
TP	2.54	870.90 ✓	12.58	868.36 ✓	
105+25	852.05				18.85
+50.	850.80				20.10
P	0.96	859.86 ✓	12.00	858.90 ✓	
B.M.	2.25	850.88 ✓	11.23	848.63 ✓	
106	848.30				21.58
+30	846.80				4.08
+50	845.81				6.07
+75					

Inst.
 Rod.
 Chain.

5

See Page 17 Book 5

Left

C L

Right

$\frac{61}{42}$

22.6

$\frac{41}{41}$

$\frac{67}{23}$

$\frac{49}{42}$

$\frac{80}{44}$

25.7

$\frac{74}{43}$

$\frac{108}{40.5}$

26.5

$\frac{108}{41}$

$\frac{139}{39}$

27.6

$\frac{15.5}{38}$

$\frac{71}{37}$

19.8

$\frac{41}{32}$

$\frac{109}{53}$

20.1

To S.E. Cor. Surveying Cattle Past 105+78

$\frac{24}{18}$

2.3

$\frac{21}{18}$

2.6

4.1

$\frac{34}{19}$

$\frac{38}{20}$

5.1

5.1

$\frac{44}{19}$

$\frac{45}{21}$

7.4

$\frac{56}{19}$

5.6

$\frac{5.9}{21}$

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		850.88 ✓			
107	843.41				2.47
	+25				
	+50	841.26			9.62 ✓
	+75				
108	839.22 ✓				11.66 ✓
TP			11.56	839.32	

Inst.

Rod.

Chain.

Left

G L

Right

✓

$\frac{6.6}{20}$

74

6.8

$\frac{6.7}{20}$

✓

$\frac{7.8}{20}$

7.9

$\frac{7.9}{20}$

✓

$\frac{8.9}{20}$

91.6

8.9

$\frac{9.1}{20}$

✓

$\frac{9.8}{19}$

10.2

$\frac{10.5}{20}$

$\frac{10.6}{20}$

117

11.2

$\frac{11.6}{19.5}$

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
BM. (C)	1178	836.66 ✓		824.88	
117+20 ✓	827.10		8.4	828.13	9.56
+35 ✓	827.60				9.06
+50 ✓	828.20				8.46
+80 ✓	829.20				7.46
118 ✓	829.75		2.9		6.91
+20 ✓	830.41 Ditch L		4.9	31.8	6.25
+50 ✓	831.41		3.6	33.1	5.25
+75					
119 ✓	832.99		1.4	835.3	3.61
TP	11.66	846.47 ✓	1.85	834.81 ✓	
+25 ✓	833.80				12.67
TP	9.45	844.26 ✓	11.66	834.81 ✓	
+50 ✓	834.04		7.1	837.2	9.67

Inst.
Rod.
Chain.

Left

C L

Right

End Guard Rail Lt 1750

$\frac{6.1}{28}$	$\frac{9.8}{22}$	$\frac{9.9}{18}$	$\frac{8.5}{15}$	9.6	$\frac{8.5}{14.5}$	$\frac{10.1}{18}$	$\frac{10.2}{22.5}$	$\frac{7.8}{26}$	$\frac{7.8}{31}$
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$\frac{5.0}{29}$	$\frac{9.4}{22}$	$\frac{9.5}{18}$	$\frac{7.9}{15}$	9.1	$\frac{7.6}{15}$	$\frac{9.7}{19}$	$\frac{9.6}{22.5}$	$\frac{7.1}{25.5}$	$\frac{7.1}{32}$
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$\frac{8.6}{30}$	$\frac{9.1}{24.5}$	$\frac{8.9}{17.5}$	$\frac{7.3}{15}$	8.5	$\frac{7.2}{15}$	$\frac{9.1}{19}$	$\frac{9.1}{22.5}$	$\frac{8.1}{30.5}$	$\frac{7.8}{31}$
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$\frac{3.1}{29}$	$\frac{8.2}{23}$	$\frac{8.3}{17.5}$	$\frac{6.2}{14.5}$	7.5	$\frac{6.1}{14}$	$\frac{7.9}{18}$	$\frac{8.1}{26.5}$	$\frac{0.7}{25.5}$	
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$\frac{6.1}{25}$	$\frac{8.2}{22}$	$\frac{8.1}{19.5}$	$\frac{5.3}{15}$	7.2	$\frac{5.4}{15}$	$\frac{7.9}{18.5}$	$\frac{7.8}{28.5}$		
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$\frac{7.7}{22}$	$\frac{5.0}{16}$	6.3	$\frac{4.9}{15}$	$\frac{7.4}{19}$	$\frac{7.4}{28}$				
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$\frac{7.2}{23}$	$\frac{4.1}{18}$	$\frac{3.5}{16}$	5.3	$\frac{3.5}{15}$	$\frac{6.5}{19}$	$\frac{7.0}{30}$			
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$\frac{2.5}{17}$	2.5	$\frac{2.4}{15}$							
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$\frac{3.8}{22}$	$\frac{2.1}{18}$	$\frac{1.3}{15}$	3.7	$\frac{1.1}{15}$	$\frac{4.9}{20}$	$\frac{5.5}{35.5}$	$\frac{4.4}{26.5}$	$\frac{0.3}{32}$	
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$\frac{13.2}{22}$	$\frac{11.1}{18}$	$\frac{10.4}{16}$	11.7	$\frac{10.1}{14.5}$	$\frac{13.2}{20}$	$\frac{11.2}{25.5}$			
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$\frac{11.2}{28}$	$\frac{9.9}{21}$	$\frac{7.1}{15}$	9.9	$\frac{7.1}{15}$	$\frac{8.8}{19}$	$\frac{8.9}{24}$			
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Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		842.26 ✓			
119+70	835.10				9.16
120	835.76				8.50
+10	Baying Dolite Lt.				
+25	836.40		46	839.7	7.86
+50	836.94		47	840.0	7.3 ✓
(+65 int.)	(37.27)				(7.00)
+80	837.60				6.66
121					
121+35	838.60		25	841.8	5.66
+65	839.17		20		5.09
+85	839.31		16		4.95
TP ⊙	8.84	849.89 ✓	3.21	841.05 ✓	
122+20	840.10				9.79
+40	840.28				9.61
+75	841.02				8.87
123	841.46		5.3	844.6	8.43

Inst.
 Rod.
 Chain.

Left				C L	Right			
$\frac{106}{31}$	$\frac{105}{27}$	$\frac{85}{19.5}$	$\frac{6.4}{15}$	$\frac{9.2}{6.2}$	$\frac{60}{15}$	$\frac{72}{18}$	$\frac{70}{22}$	$\frac{3.0}{29}$
$\frac{79}{22}$	$\frac{84}{19}$	$\frac{5.8}{15}$		$\frac{8.5}{5.5}$	$\frac{5.2}{15}$	$\frac{6.5}{19.5}$	$\frac{6.5}{24.5}$	$\frac{1.4}{31.5}$
$\frac{72}{33}$	$\frac{65}{19}$	$\frac{5.7}{17.5}$	$\frac{5.2}{15}$	$\frac{7.9}{4.6}$	$\frac{4.6}{7.6}$	$\frac{5.8}{20}$	$\frac{5.9}{24}$	$\frac{0.8}{32}$
	$\frac{71}{37}$	$\frac{6.6}{22}$	$\frac{4.5}{15.5}$	$\frac{7.4}{4.3}$	$\frac{4.0}{7.6}$	$\frac{5.4}{18.5}$	$\frac{5.2}{23.5}$	$\frac{1.8}{26}$
	$\frac{67}{39}$	$\frac{6.3}{21.5}$	$\frac{4.1}{16.0}$	4.0	$\frac{3.6}{15.5}$	$\frac{5.0}{18}$	$\frac{4.9}{22}$	$\frac{1.0}{26}$
	$\frac{64}{40.5}$	$\frac{6.0}{21}$	$\frac{3.8}{16.5}$	$\frac{6.7}{3.7}$	$\frac{3.2}{15}$	$\frac{4.7}{18}$	$\frac{4.6}{20}$	$\frac{0.2}{26}$
	$\frac{55}{42}$	$\frac{5.6}{20.5}$	$\frac{3.4}{15}$	3.4	$\frac{2.7}{15.5}$	$\frac{4.2}{18.5}$	$\frac{4.1}{21.5}$	$\frac{0.1}{24.5}$
$\frac{52}{41}$	$\frac{5.6}{37}$	$\frac{4.5}{19}$	$\frac{2.8}{14.5}$	$\frac{5.7}{2.5}$	$\frac{2.3}{15}$	$\frac{3.5}{19}$	$\frac{3.5}{21}$	$\frac{0.4}{24.5}$
$\frac{48}{47}$	$\frac{5.0}{39}$	$\frac{4.3}{2.0}$	$\frac{2.1}{15.5}$	$\frac{5.1}{2.0}$	$\frac{1.6}{16}$	$\frac{2.5}{18.5}$	$\frac{3.8}{20.5}$	$\frac{1.4}{22}$
$\frac{47}{50}$	$\frac{4.4}{37}$	$\frac{3.7}{20}$	$\frac{1.9}{15.5}$	$\frac{4.8}{1.6}$	$\frac{1.2}{17}$	$\frac{2.4}{19.5}$	$\frac{2.4}{22.5}$	
Rock 50' L-122								
	$\frac{8.7}{39}$	$\frac{8.1}{33}$	$\frac{8.3}{18}$	$\frac{6.8}{14}$	$\frac{9.8}{6.4}$	$\frac{5.9}{15.5}$	$\frac{7.0}{19}$	$\frac{7.0}{23}$
								$\frac{1.5}{31}$
$\frac{8.2}{43}$	$\frac{9.4}{42.5}$	$\frac{8.3}{29}$	$\frac{7.8}{19}$	$\frac{6.2}{14.5}$	$\frac{9.1}{6.0}$	$\frac{5.7}{7.6}$	$\frac{6.4}{18.5}$	$\frac{6.3}{21.5}$
								$\frac{0.3}{31}$
	$\frac{9.8}{38}$	$\frac{11.0}{35}$	$\frac{10.8}{28}$	$\frac{9.4}{22}$	$\frac{5.9}{15}$	$\frac{5.0}{16}$	$\frac{6.2}{19}$	$\frac{5.5}{25}$
								$\frac{6.7}{32}$
			$\frac{5.4}{17}$	$\frac{8.4}{5.3}$	$\frac{4.8}{7.5}$	$\frac{6.2}{18.5}$	$\frac{5.5}{26}$	$\frac{0.3}{32}$

(int.)



..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
BM	1178	836.66 ✓		824.88	
TP	1200	846.81 ✓	1.85	834.81 ✓	
117+20	827.10				19.70
+35	827.60				19.21
+50	828.20				18.61
118	829.75				17.06
+20	830.41				16.40
+50	831.41				15.40
+75					
119	832.99				13.82
TP	1200	858.62 ✓	0.19	846.62 ✓	
119	832.99				21.63
TP	10.42	868.66 ✓	0.38	858.24 ✓	
+25	833.80				24.86
+50	834.44				24.22

Inst.
Rod.
Chain.

Left C L Right

End Guard Rail L 117+50

19.7

$\frac{8.5}{36}$

19.2

$\frac{7.5}{36}$

18.6

$\frac{8.3}{36}$

17.0

$\frac{10.1}{37.5}$

16.4

$\frac{8.5}{38}$

15.4

$\frac{4.8}{39.8}$

$\frac{0.1}{42.5}$

13.8

$\frac{10.9}{37.5}$ $\frac{4.7}{36}$

25.6

$\frac{3.8}{54}$

34.9

$\frac{14.5}{51}$ $\frac{8.6}{58}$

34.3

$\frac{12.3}{52}$ $\frac{7.9}{59}$

Sta.	B.S.	Cross		Grade	Gr. R.
		H. I.	F. S.		
		868.66 ✓			
119+70	835.10				33.56
120	835.76				32.90
+25	836.40				32.26
+50	836.94				31.72
+80	837.60				31.06
TP	9.08	872.63 ✓	5.11	863.55 ✓	
121+35	838.60				34.03
121+65	839.17				33.46
121+85	839.31				33.32
122+20	840.10				32.53
+140	840.28				32.35
TP	2.99	866.38 ✓	9.211	863.39 ✓	
+75	841.02				25.36
123	841.46				24.92

Inst.
 Rod.
 Chain.

Left

C L

Right

33.6

$\frac{10.3}{51}$ $\frac{5.8}{5.8}$

32.9

$\frac{4.3}{57}$

32.3

$\frac{140}{24}$ $\frac{11.2}{26}$ $\frac{8.8}{49}$ $\frac{5.0}{55}$

31.8

$\frac{6.0}{48}$ $\frac{6.0}{51}$ $\frac{2.5}{55}$

31.1

$\frac{11.5}{42}$ $\frac{4.5}{50}$ $\frac{0.3}{55}$

34.0

$\frac{12.7}{46}$ $\frac{8.6}{51}$ $\frac{5.4}{52}$

33.4

$\frac{12.0}{46}$ $\frac{7.1}{52}$ $\frac{4.3}{53}$

33.1

$\frac{12.8}{45}$ $\frac{7.1}{54}$ $\frac{3.8}{56}$

32.5

$\frac{11.2}{46}$ $\frac{5.2}{53}$

32.3

$\frac{7.7}{52}$ $\frac{4.3}{52}$

25.4

$\frac{4.4}{47}$ $\frac{1.6}{49}$

24.9

$\frac{10.2}{40}$ $\frac{6.5}{43}$

Cross Sections

Sta.	B.S.	H. I.	F.S.	Grade	Gr. R.
		866.38 ✓			
TP	0.91	855.49 ✓	11.20	854.58 ✓	
123+50	842.44				13.06
+75					
TP	7.10	852.45 ✓	10.14	845.35 ✓	
123+75	842.97				9.48
124+07	843.71				8.74
+25	844.23				8.24
+41	844.60				7.95
+50	844.94				7.51
+75	845.70				6.75
125	846.51				5.94
BM			1.30	856.15 ✓	
TP	0.84	46.19	7.10	45.35	
123+75	842.97				
124+07	843.71				
124+50	End Ditch Rt.				

Inst.
 Rod.
 Chain.

Left

C. L

Right

$\frac{101}{18}$

$\frac{131}{103}$

$\frac{101}{15}$

$\frac{122}{18}$

$\frac{130}{26}$

$\frac{91}{30}$

W 1/2 S 1/1

$\frac{68}{19.5}$

$\frac{95}{6.9}$

$\frac{68}{15}$

W 1/2 S 1/1 Slope

$\frac{62}{20}$

$\frac{81.8}{6.2}$

$\frac{6.2}{16}$

$\frac{60}{20}$

$\frac{83}{6.0}$

$\frac{5.7}{16}$

$\frac{57}{19.5}$

$\frac{71.9}{5.6}$

$\frac{5.5}{17}$

$\frac{54}{20}$

$\frac{75}{5.2}$

$\frac{5.8}{17}$

$\frac{48}{19.5}$

$\frac{68}{4.8}$

$\frac{4.7}{18}$

$\frac{42}{19}$

$\frac{60}{4.1}$

$\frac{4.1}{18}$

Cotton Pass 1267

$\frac{62}{23}$

$\frac{56}{25}$

$\frac{6.2}{30}$

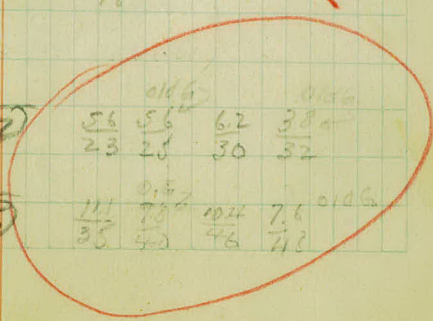
$\frac{38}{32}$

$\frac{21.5}{35}$

$\frac{111}{40}$

$\frac{10.4}{46}$

$\frac{7.6}{48}$



Sta.	Cross Sections			Grade	Gr. R.
	B. S.	H. I.	F. S.		
B.M. 1 -	6.05	857.86 ✓		851.81	
125+00					
+25					
+50					
+75					
126					
+25					
+50					
T.P.	RT.		12.51	845.35 ✓	
T.P.	LT.		11.66	846.20 ✓	
+75					
127					
+25					
+50					
T.P.			0.28	857.59 ✓	

Inst. Galvin
 Rod. Stang
 Chain. Attaberg

Comer

10-6-24 - P.M.

12

Left

C L

Right

B 14 Cattle Pens (marked 851.81)

✓	9.2 19.0	9.0 00	(11.4)	8.8 18.0	✓
✓	8.5 19.0	8.5 00	(10.5)	8.4 18.0	✓
✓	7.9 18.0	7.9 00	(9.6)	7.9 18.0	✓
✓	7.2 17.0	7.2 00	(8.6)	7.4 18.0	✓
✓	7.0 16.0	6.6 00	(7.6)	6.6 17.0	✓
	36 112 12.0 430 370 24.0 6.1	6.1 00	(6.6)	5.9 10.9 14.4 10.8 1.60 250 470 50.0	
	00 74 84 5.2 300 220 20.0 14.0	4.8 00	(5.4)	4.9 8.4 10.3 7.8 170 230 370 430	
✓	4.7 5.3 3.8 220 165 140	3.8 00	(4.3)	4.0 7.6 5.7 17.0 350 390	
✓	4.0 2.6 190 15	2.7 00	(3.0)	2.7 5.7 3.9 21.0 30.0 32	
✓	2.5 2.5 1.6 20 170 100	1.6 00	(1.0)	1.0 17.0 FE RE	
✓	1.4 1.4 0.3 220 170 150	0.3 00	(0.5)	0.7 1.1 170 18 24.0	✓

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
T.P. 126	1.36	846.71 ✓		845.35 ✓	
125+75					
125+50					
T.P. 125+25	0.01	834.87 ✓	11.85	834.86 ✓	
125					
T.P. 126	0.02	846.22 ✓		846.20 ✓ <u>carried</u>	
125+75					
125+50					
135+25					
125					
T.P. 126+75	10.22	867.80 ✓		857.58 ✓ <u>carried</u>	
127					

Inst.
 Rod.
 Chain.

10-6-24-PM-

Left

G L

Right

(-3.6) 3.8 5.2 5.7 7.3 6.8 4.0
 31.0 41.0 57.0 59.0 64.0 66.0

(-6.9) 8.2 9.7 10.3 9.5
 37.0 52.0 55.0 60.0

(-1.6) 11.3 12.4 12.7
 40.0 52.0 60.0

(-12.5) 30
 46.0

(-11.6) 5.4
 45.0

+1.3 1.3 2.4 1.5 (-4.1)
 34.0 40.0 33.0 27.0

3.2 6.4 4.3 4.4 (-3.1)
 43.0 38.0 36.0 32.0

7.6 (-2.1)
 36.0

9.9 (-1.2)
 40.0

12.4 11.7 (-0.3)
 46.0 41.0

5.6 (14.2)
 31.0

17 (12.9)
 33.0

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
127+15		867.80 ✓			
+50					
+75					
128					
+25					
+50					
+75					
129					
+25					
+50					
T.P.	11.82	879.07 ✓	0.55	867.25 ✓	
128					
+25					
+50					

Inst.
 Rod.
 Chain.

10-6-24 - PM.

14

Left

G L

Right

00
35.0

10.4

5.5	11.3	11.4	10.2	10.2	10.0	10.6	11.0	5.5
30.5	22	17.5	15.0	00	16	18	24.0	31.0

9.2

2.5	10.1	10.0	9.3	9.1	8.9	9.6	9.6	1.8
51.5	23.0	18.0	16.0	00	14.0	15.0	23.5	32.0

7.9

0.7	9.3	9.2	8.0	7.7	7.4	8.7	8.7	
33	23.0	18.0	15.0	00	15	17.0	23.5	✓

6.7

	8.0	8.1	6.8	6.7	6.3	7.6	7.7	
✓	21	16.5	13.5	00	16.0	18.0	23.5	✓

5.4

	6.9	6.9	5.4	5.3	4.9	6.3	6.1	
✓	20.5	17.0	14.0	00	16.0	18.5	23.0	✓

	5.2	5.5	4.1	4.0	3.4	4.3	4.4	
✓	22	17.0	14.5	00	15.0	18.0	23.0	✓

2.9

	4.0	4.2	3.0	2.7	2.3	3.4	3.4	
✓	21.5	17.0	15.0	00	16.5	18.5	23.0	✓

	3.4	3.3	1.7	1.5	1.0	2.3	2.3	
✓	21.0	17.5	15	00	15	17.0	23.5	✓

0.4

	2.1	1.9	0.2	0.2	00	1.2	1.1	
	21.0	17.5	15.0	00	15.0	17.0	24.0	✓

19.2

8.0
37.5

18.0

3.9
40.0

16.7

2.0
40.5 STK

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
129		879.07	✓		
+50					
128+25					
+50					
129					
+50					
+75					
130					
+25					
+50					
T.P.	9.87	886.18	✓	2.76	876.31 ✓
130+50					
+75					
131					
+25					

Inst.
 Rod.
 Chain.

10-6-24 - P. 17

15

Left

G L

Right

14.2

0.9
39.0

stk

11.7

1.2
36

stk

10.1
33.5

18.0

6.7
34.5

16.7

stk 5.0
34.5

14.2

3.4
33.0

11.4

stk

12.3	12.3	10.2	10.3	10.1	11.3	11.3
21.0	18.0	15.0	00	14.5	16.5	24.0
26	11.1	11.2	9.2	9.0	10.3	10.1
30.5	20.0	17.0	14.5	9.0	17.0	24.0
			00	15.5		0.7
						33.0

9.4	9.5	7.3	7.5	7.4	9.3	9.3
22	19.0	15.5	00	15.5	18.0	24.0

6.7

16	8.2	8.1	6.6	6.2	6.4	7.9	7.7
30.0	22.5	20.0	15.5	00	15.0	18.0	23.0

13.8

8.6
32

14.1	14.3	12.2	12.1	12.0	14.0	13.8
24.5	21.0	16.0	00	14.0	19.0	21.0

11.3

7.8	12.6	12.4	11.1	11.1	11.1	13.2	12.6	3.7
29.5	23.5	20.0	16.0	00	14.5	17.5	22.0	33

11.7	11.2	10.0	10.1	10.0	11.9	11.6
23.0	19.5	15.5	00	14.5	18.0	23.5

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
131		886.18 ✓			
+50					
+75					
132					
+25					
+50					
+75					
133					
+25					
+50					
+75					
134					
T.P.	hub PC $\frac{1}{4}$		1.10	885.08 ✓	

Cross Sections

Sta. B. S. H. I. F. S. Grade Gr. R.

7.00

892.08

885.08

134+25

+50

+75

135

+25

+50

+75

136

+25

+50

+75

137

Inst. Skopfen
 Rod. Galvin
 Chain. Althberg

Curve

10-7-24 A.M.

Left

C L

Right

9.0 6.0 68 7.7 9.3 9.6
 22.0 16.5 00 16.0 19.5 25.0

8.6 5.4 6.5 7.6 9.4 9.5 7.6
 20.0 15.0 00 17.0 21.0 25.5 28.0

6.5

8.2 5.3 6.3 7.3 8.9 9.1
 20.5 16.0 00 17.0 20.5 27.0

6.2

F.E. 8.1 5.2 6.0 7.2 9.3 9.3 6.6
 21.5 15.0 00 17.5 22.0 25.0 29.5 - FE

7.7 4.9 5.8 7.0 7.8 7.7
 20.0 16.0 00 17.0 19.0 33.5

5.9

7.5 4.8 5.6 6.9 7.7 7.4 4.4
 20.0 15.8 00 18.0 19.5 34.0 35.5

7.3 5.1 5.6 6.7 7.4 7.3
 19.0 15.5 00 17.0 19.0 32.0

5.5

6.8 4.9 5.5 6.4 7.2 6.9 2.7
 19.0 16.0 00 17.0 18.5 25.0 33.0

6.9 5.1 5.5 6.4 6.8 6.7
 19.0 16.9 00 18.0 20.0 25.5

5.6

6.4 5.0 5.5 6.1 6.8 7.0 0.3
 18.0 16 00 18.5 21.5 25.0 33.5

6.4 6.4 5.0 5.4 6.0 6.7 7.0
 22.0 18.0 15.6 00 19.5 21.5 25.5

5.5

3.0 6.0 6.1 4.8 5.3 5.7 7.0 7.0 ✓
 27.0 23.0 20.0 16 00 18.0 21.0 24.0

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
137+25		892.08 ✓			
+50					
+75					
138					
+25					
+50					
+75					
T.P.	12.22 ✓	899.72 ✓	4.58	887.50 ✓	*
137					
+50					
138					
+50					
T.P.	7.79	895.29 ✓	12.22	887.50 ✓	*
139					

Inst.
Rod.
Chain.

Left			C L			Right	
5.8	5.9	4.8	5.0	5.2	6.8	6.7	
22.5	18.0	16.0	00	17.0	20.0	24.0	

(5.3)

1.4	5.4	5.6	4.8	5.0	5.0	6.5	6.6
28.0	22.0	18.5	16.5	00	16.0	19.5	22.5

✓

5.7	5.7	4.7	5.0	5.2	6.7	6.9
22.0	18.0	15.0	00	15.0	18.5	23.0

(5.2)

1.8	6.0	6.1	4.8	5.1	5.1	6.2	6.6
28.0	22.0	17.5	15.0	00	15.0	17.5	23.5

✓

6.4	6.5	5.1	5.0	4.9	6.4	6.4
22.5	17.0	14.5	00	15.5	19.0	23.0

(5.0)

2.8	6.6	6.8	5.0	4.8	4.7	6.2	5.9
27.5	22.5	18.0	15.5	00	15.5	19.0	22.5

✓

6.6	6.5	5.1	4.8	4.6	5.7	5.6
23.0	18.0	15.0	00	14.5	18.0	23.5

(13.1)

4.5
36.0

(12.9)

4.2
34.0

(12.8)

5.0
33.5

(12.6)

6.2
32.0

7.0

11.0	10.4	9.8	8.6	7.8	7.5	8.5	8.2	3.3
27.0	23.0	19.0	15.0	11.8	00	16.0	19.0	24.5
				8.1				30.0

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
+35		895.29 ✓			
+50					
+75					
140					
+25					
+50					
+75					
141					
+25					
+50					
+70					
142 ✓					
+25					

Inst.
 Rod.
 Chain.

Left				CL	Right			
10.5	10.0	8.8	8.0	11.7	8.6	8.5		
24.5	19.0	17.0	00	16.0	18.5	24.5		

(7.9)

8.4	10.2	10.1	9.0	8.1	7.4	8.4	8.2	5.0
28.5	25.0	19.5	17.0	00	15.5	18.0	24.0	27.5

10.4	10.1	8.7	8.0	7.2	8.3	8.2	
25.5	20.5	17.7	00	16.0	19.5	26.5	

(7.8)

9.6	10.3	9.8	9.0	7.9	6.7	7.9	7.9	6.0
27.5	25.5	19.0	18.0	00	15.5	18.5	23.5	26.0

10.3	10.0	9.0	7.8	6.5	7.6	7.7	
25.0	19.5	17.5	00	15.0	18.0	23.0	

(7.6)

9.0	10.2	10.0	8.8	7.8	6.6	7.6	7.7	6.0
27.5	25.0	21.0	18.5	00	15.5	18.0	24.0	26.0

10.5	10.2	8.8	7.6	6.7	7.9	7.9	6.1
26.0	21.5	18.5	00	15.5	18.5	24.0	26.0

(7.5)

9.8	10.8	10.4	9.1	7.7	6.8	8.2	8.1	6.4
30.0	27.5	22.0	19.5	00	16.0	18.5	22.5	25.0

11.3	10.9	9.0	7.9	7.2	8.3	8.3	
28.0	24.0	20.0	00	16.0	19.0	24.0	

(7.3)

10-7-24 P.M.

14.0	13.0	12.2	9.6	8.1	7.4	8.4	8.7	6.7
50.0	31.0	25	19.5	00	18.5	22.0	25.5	28.5

(7.3)

15.4	13.3	10.0	8.0	7.5	8.6	9.0	7.2
50.0	28.0	22.0	00	22.5	27.5	32	36.0

(7.2)

13.0	10.2	8.4	7.6	7.0		
50.0	27.0	00	30.0	50.0		

(7.1)

12.6	10.0	8.7	7.6	7.1		
50.0	25.0	00	30.0	50.0		

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
142+50		895.29 ✓			
BM			6.36 ✓	888.93 ✓	888.89
T.P.	4.07	893.98	5.34	889.95	889.91
+75					
143					
+25					
+50					
+75					
144					
+25					
+50					
+75					
145					
+25					

Inst.

Rod.

Chain.

	Left		CL (7.0)		Right	
86	12.0	12.0	10.5	8.8	7.7	7.0
42.5	39.0	36.0	32	00	28.0	50.0

(5.7)

8.3	10.0	9.5	8.5	7.5	5.9	8.1	8.1	5.9
33.0	27.0	23.0	20.0	60	400	47.0	49.0	51.0

(5.6)

6.2	9.7	9.6	8.3	7.2	6.5	7.8	7.6	2.5
30.0	26.0	21.0	17.0	00	19.0	22.0	25.0	33.0

9.4	9.2	7.9	7.0	6.2	7.8	7.8
25.0	21.0	18.0	00	15.5	19.0	22.5

(5.5)

6.8	9.2	9.0	7.7	6.5	6.0	7.4	7.5	4.0
27.0	24.0	20.0	16.5	00	17.0	19.0	23.0	27.0

8.6	8.6	7.2	6.0	5.3	6.6	6.7
25.0	21.5	17.5	00	16.0	18.5	23.0

(5.4)

6.9	8.3	7.8	7.0	5.6	5.0	6.4	6.4	5.2
27.0	25.0	21.0	18.5	00	17.0	19.5	22.5	25.0

(5.3)

8.1	7.7	6.9	5.2	5.0	6.4	6.8
25.5	21.5	19.0	00	16.0	18.5	22.0

(5.3)

7.4	8.2	7.6	6.7	5.3	5.0	6.4	6.9	5.7
27.0	25.5	20.5	19.0	00	15.5	18.5	22.0	24.0

8.0	7.6	6.3	5.3	4.8	6.7	6.7
25.0	20.5	18.0	00	14.5	18.5	22.0

(5.2)

6.3	7.7	7.3	6.1	5.2	4.8	6.6	6.7	5.9
25.0	23.5	19.0	16.5	00	15.5	19.0	23.0	24.0

7.6	7.3	6.0	5.3	4.9	6.6	6.6
23.0	19.5	16.0	00	16.0	19.0	23.5

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
145+50		893.98 ✓			
+75					
146					
+25					
+50					
+75					
147					
+25					
+50					
+75					
148					
+25					

Inst.
 Rod.
 Chain.

Left				C	Right			
5.5	7.5	7.1	5.6	5.1	4.9	6.8	7.0	5.4
25.0	19.0	18.5	15.5	00	16.0	19.5	23.5	25.0
	7.0	6.9	5.5	5.0	4.9	6.6	6.8	
	23.0	18.0	15.0	00	15.5	19.0	24.0	
				5.0				
4.8	6.9	6.6	5.4	4.8	5.0	6.5	6.6	4.7
25.5	23.5	17.5	15.0	00	15.5	19.0	24.0	26.0
	7.1	6.7	5.2	5.0	4.9	6.8	6.7	
	24.0	18.0	15.0	00	15.5	19.0	24.0	
				4.9				
5.2	6.9	6.7	5.2	5.0	4.8	6.4	7.0	5.1
26.0	24.0	18.5	15.5	00	16.0	18.0	24.0	25.5
	6.7	6.4	5.1	4.8	4.7	6.3	6.6	5.3
	24.0	18.5	15.0	00	15.0	18.5	24.0	25.0
				4.8				
5.9	6.4	6.1	5.1	4.7	4.8	6.3	6.5	5.3
25.0	24.0	19.0	16.5	00	15.5	19.0	23.0	24.0
	6.4	6.2	5.0	4.7	4.7	6.2	6.3	
	24.0	20.0	16.0	00	15.5	19.0	23.0	
				4.7				
6.2	6.6	6.0	5.0	4.8	4.8	6.2	6.5	6.0
24.5	23.5	18.0	15.5	00	16.0	19.0	23.0	24.0
	6.8	6.3	5.0	4.6	4.9	6.4	6.7	6.2
	32.5	18.0	15.0	00	15.0	19.0	22	30.0
				4.7				
FF	6.7	4.9	4.8	4.8	6.8			FF
	20.5	15.5	00	15.5	19.5			
7.2	7.6	6.6	5.0	4.9	5.0	6.6	6.7	
33	28.0	18.0	14.0	00	15.5	19.0	29.0	

Sta.	Cross			Sections	
	B. S.	H. I.	F. S.	Grade	Gr. R.
148+50		893.98 ✓			
+75					
T.P. 149	0.51	889.32 ✓	5.17	888.81 ✓	
+25					
+50					
+75					
150					
+25					
+50					
+75					
157 T.P. +25	4.16	882.97 ✓	10.51	878.81 ✓	
+50					

Inst.
 Rod.
 Chain.

Left			C L	(4.0)		Right		
	6.8	5.3	5.0	5.2	6.7	7.1	6.6	
	19.0	15.0	00	16.0	19.0	23.0	24.0	

	7.3	7.0	5.6	5.2	5.7	7.1	7.5	
	23.0	19.0	16.0	00	15.0	19.0	22.0	

	7.6	3.0	2.7	1.3	(1.0)	1.3	2.6	3.1	2.5
	24.0	23.0	19.0	16	00	16.0	19.0	23.0	24.0

	3.7	3.5	2.0	1.7	2.0	3.4	3.7	
	23.0	19.0	16.0	00	17.0	20.5	23.0	

	3.1	4.6	4.0	2.6	(2.4)	2.6	4.2	4.4	2.8
	25.0	23.0	18.0	15.5	00	17.0	21.0	23.0	25.0

	5.5	5.0	3.4	3.0	3.4	4.3	4.6	
	23.0	18.5	16.0	00	15.0	17.0	23.0	

	3.9	6.2	5.6	4.2	(4.0)	3.9	4.1	5.4	5.2	3.6
	25.0	23.0	18.0	15.0	00	15.0	18.0	24.0	25.5	

	6.8	6.7	5.1	4.9	4.8	6.5	7.3	
	23.0	18.5	15.0	00	14.5	17.5	24.0	

	5.9	8.6	7.0	6.0	(6.1)	5.9	7.6	8.3	6.8
	26.0	24.0	19.0	16.0	00	14.5	17.0	23.0	24.5

	9.5	8.9	7.3	7.2	7.7	8.6	9.2	
	25.0	20.0	15.5	00	15.5	18.0	23.5	

	11.5	8.3		8.1	(8.6)	8.4	10.6	9.0
	22.0	16.0		00	15.0	22.0	24.0	

	6.0	3.1	3.1	(3.4)	3.5	5.5	5.8	
	21.0	16.0	00	14.5	20.0	24.5		

	5.7	6.4	6.1	4.5	(4.8)	4.3	6.7	6.6	0.6
	23.0	22.0	18.0	14.0	00	14.0	20.0	24.0	29.0

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
151+75		882.97			
152					
+21				875.9	7.1
+50				875.2	7.4
+75				875.0	8.0
153				875.4	7.6
+18				876.4	6.6
+37				869.3	13.1
T.P.	1.97	876.38	8.56	874.41	
152+75				875.0	1.4
153				875.4	1.0
+18				876.4	0.0
+37				869.3	7.1
153+50 = Zero		Excav.			
T.P.	2.90	877.31		874.41	
Bm.			4.28	873.03	<u>872.86</u>

Inst.
Rod.
Chain.

.....

Left				C L		Right		
8.0	7.5	5.6	5.5	5.6	7.6	7.7		
22.5	18.5	15.0	00	15.5	21.0	24.5		

(7.3)

7.3	9.5	8.9	7.2	6.8	6.6	7.7	8.5	2.8
24.5	23.0	19.0	15.5	00	14.0	17.0	26.0	30.0

(7.1)

9.0	11.2	10.6	8.6	7.9	8.0	9.3	9.3	3.3
25.0	24.0	20.0	16.0	00	14.5	17.5	24.5	30.0

(7.8)

11.4	12.3	12.3	10.0	9.5	9.4	10.4	10.5	4.0
26.0	25.0	22.0	17.0	00	15.0	17.0	25.0	30.0

(8.0)

4.5
31.0

(7.6)

4.7
31.0

(6.6)

4.4
33.5

2.0
60.0

(11.7)

5.1	6.8	6.6	4.4	4.0	3.8	5.0	5.1	
29.0	26.5	22.5	18.0	00	14.5	19.0	23.0	

(11.4)

5.4	7.6	7.0	5.3	4.8	4.7	6.4	6.3	
34.0	29.0	23.0	19.0	00	15.0	19.5	23.0	

(11.0)

6.0	5.1	4.9	6.6	6.3
27.0	00	16.0	23.0	27.0

(0.0)

8.0	7.0	5.8	3.7	4.6	4.3
45.0	20.0	6.0	35.0	38.0	50.0

(7.1)

Cross Sections

Sta.	B.S.	H. I.	F. S.	Grade	Gr. R.
0					
B.M.	11.19	848.90		837.71	
61				841.2	
+25				842.1	6.8
+50				843.0	5.9
+75				844.0	
62				844.9	4.0
+25				845.8	
+50				846.7	2.2
+75				847.6	
T.P.	7.73	156.03	0.60	848.30	
63				848.5	7.5
+20				849.2	6.8
+50				850.2	
+75				851.0	
T.P. (top of 4 studs 121.00)			3.00	853.03	

Inst. Galvin.....
 Rod. Stacglu
 Chain. Frit.....

Conner.

10-15-24

24

Left

C L

Right

Sta 60 + 60 T.D.

✓	4.8		4.2	3.8	✓
	22.2		50	14.4	

(See page 26) 21.8 3.9 (6.8) 3.6 (See page 25)

✓	4.4		3.5 (5.9)	2.8	✓
	20.2		00	16.8	

✓	4.0		3.2	2.4	✓
	19.0		00	16.6	

✓	3.6		2.6 (4.0)	2.2	✓
	19.0		00	16.6	

✓	2.9		2.2	2.0	✓
	19.8		00	16.4	

✓	2.0		1.7 (2.2)	1.3	✓
	19.0		00	15.0	

✓	1.0		0.8	0.4	✓
	18.6		00	14.4	

(See page 27) 7.6 7.7 (7.8) 6.9

	19.6		00	14.4	✓
--	------	--	----	------	---

✓	6.8		6.4 (6.8)	6.0	✓
	19.0		00	16.0	

✓	6.0		5.6 (5.4)	5.2	5.7	6.5	2.9
	16.6		00	15.0	20.0	22.6	26.6

8.7	8.0	7.3	5.2	4.7 (5.1)	4.5	5.4	6.0
27.0	23.2	20.0	15.6	00	15.0	19.4	21.8

✓

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M.	1.84	839.55 ✓		837.71	
61				841.2	
+15					
+25				842.1	(-2.5)
+50				843.0	(-3.4)
62				844.9	(-5.3)
T.P.	11.98	849.89 ✓	1.64	837.71 ✓	
+50				846.7	3.2
63				848.5	1.4
T.P.	12.97	862.17 ✓	0.69	849.20 ✓	
+20				849.2	13.0
+75				851.0	
T.P.	9.72	871.26 ✓	0.63	861.54 ✓	
64					
+10					
+50					

Inst.
 Rod.
 Chain.

10-15-24

24

Left

C L

Right

11.8
 39.0

collected.

16.8
 47.0

(-2.5)

11.5
 39.0

(-3.4)

5.7
 33

(-5.3)

2.5
 31.4

(3.2)

10.0 11.0 9.4
 28.0 31.0 30.0

(1.7)

5.2 6.3 3.0
 22.2 25.4 30.4

8.0
 30.4

(13.0)

15.4 15.2 13.0
 21.4 25.8 27.4

(11.3)

3.8
 30.4

7.4
 35.4

(19.1)

5.7
 37.6

(17.7)

4.6
 37.6

Sta.	B: S.	Cross		Grade	Gr. R.
		H. I.	F. S.		
65		876.26			
+50					
+90					
66					
(+25 see p. 38)					
+30 ⁷ P.T.					
T.P.			10.75	860.51	
67					
P.M.	6.00	843.71		837.71	
T.P.	0.66	831.99	12.38	831.33	
61				841.2	
+15					
+25				842.1	(-10.1)
T.P.	1.39	842.79	0.59	831.42	
+50				843.0	(0.2)
62				844.9	(-2.1)
+50				846.7	(-3.9)

Inst.
 Rod.
 Chain.

10-15-24

26

Left

GL

Right

16.0

5.3
31.6

14.3

4.9
33.5

13.0

6.1
31.2

6.0
31.2

6.5 5.8 3.1
31.0 37.8 43.0

SW cor. copping Cattle pass Sta. 67+10

60+60 Rk

12.7
53.8

culvert.

14.9
61.0

7.0
52.0

-10.1

9.5
38.2

-0.2

5.5
30.8

-2.1

5.4
33.0

-3.9

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
63		842.79 ✓		848.5	(-5.7)
T.P.	5.21	835.92 ✓	12.08	830.71 ✓	
+20				849.2	(-13.3)
+50				850.2 ✓	
T.P.	12.23	847.62 ✓	0.53	835.39 ✓	
T.P.	12.62	859.69 ✓	0.55	47.07 ✓	
T.P. (by stake 9/64 + 00)			6.70	52.99 ✓	0.15-
64					
+25					
+50					
+75					
65					
+25					
+50					
+75					
66					

In
 Rod
 Chain

10-15-24

27

Left

C L

Right

12.2
45.6

(-57.4)

15.0
62.2

(-13.3)

2.6
42.8

(-14.3)

(7.5)

7.8 9.6 9.2 8.2
24.8 21.8 18.4 15.5

7.5
00

7.2 8.7
14.5 20.5

✓

3.8 8.8 8.5 7.5
27.2 22.2 18.0 16.0

4.8
00

6.5 7.8 7.6
13.8 17.6 19.8

✓

(6.1)

3.9 7.7 7.7 6.5
27.8 23.2 18.0 16.0

6.0
00

5.6 7.1 7.0
15.0 18.4 21.8

✓

6.7 6.8 5.8
22.8 17.8 15.2

5.3
00

4.8 6.3 6.0
10.6 17.8 22.0

✓

(4.4)

3.5 6.7 6.7 5.0
24.6 21.0 17.4 15.4

4.3
00

3.9 5.4 5.4
14.6 17.4 22.6

✓

1.3 6.8 5.9 4.3
26.6 22.4 16.8 14.4

3.6
00

3.0 4.4 4.4
13.8 18.0 20.0

✓

(2.7)

0.9 5.0 5.0 3.4
26.8 21.9 17.3 15.2

2.6
00

2.1 3.9 3.6
14.4 17.4 20.7

✓

2.4 4.8 3.9 2.3
25.0 20.7 18.4 15.2

1.5
00

1.3 2.9 2.8
14.6 17.2 21.2

(1.1)

1.7 3.2 3.2 1.4
24.8 21.3 18.4 15.8

0.7
00

0.5 1.8 1.5
14.8 17.8 22.4

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		159.69 ✓			
T.P. 66+30 ⁷ -P.T.	9.33	162.81 ✓	0.21	859.48 ✓	
+50					
+75					
67					
+25					
B.M.			8.38	860.43 ✓	
+50					
+75					
68					
+25					
+50					
+75					
69					

Inst.
 Rod.
 Chain.

10-15-24

28

Left

C L

Right

8.2 11.7 11.5 9.4 9.1
 24.8 21.0 18.4 16.6 00

2x 8.5 11.1 11.1 8.9 8.7 8.9 10.0 9.6 6.4 5.8 00
 27.0 22.8 18.7 15.0 00 15.8 19.0 23.6 30.4 40.8 47.2
 9.2 10.3 10.8 8.2 5.0 8.1 9.8 10.2 9.5 8.4
 26.0 21.9 19.0 14.4 00 14.4 19.0 25.6 29.3 41.8 ✓

7.0 16.5 13.9 7.4 7.0 7.4 13.0 12.1
 34.8 24.0 13.0 00 13.8 23.0 34.6

13.6 11.9 6.9 6.2 6.8 8.6 9.2
 40.4 22.8 13.8 00 15.0 19.2 33.0 ✓

S.W. Co. Cutlerpass

5.7 4.9 7.4 8.4 6.2 5.7 5.9 7.7 7.9
 42.7 37.4 28.7 20.2 14.6 00 15.4 18.5 21.8 ✓

7.6 6.5 6.5 7.5 5.2 5.0 5.1 6.4 6.5
 41.8 36.2 26.0 21.6 14.8 00 16.5 19.8 22.4 ✓

4.4 5.7 5.0 5.9 5.7 4.5 4.3 4.5 5.9 5.6
 39.1 28.0 24.0 20.4 14.9 00 15.0 18.0 22.8 ✓

2.9 5.3 5.1 6.0 3.9 3.8 5.1 4.5
 30.4 25.7 18.0 15.0 00 14.1 17.2 22.3 ✓

3.3 1.5 4.5 4.6 3.3 3.1 3.4 4.0 4.0
 27.2 22.7 19.1 15.3 00 14.7 18.1 21.1 ✓

2.0 4.4 4.4 2.7 2.3 2.5 3.3 3.5
 27.0 22.3 17.6 14.4 00 15.3 18.5 21.3 ✓

2.1 7.0 4.0 4.0 2.0 2.0 1.9 2.8 2.6
 26.1 21.8 17.6 14.3 00 15.3 19.0 21.7

Cross Sections

Sta.	B. S.	I. I.	Grade	Gr. R.
69+25		868.81 ✓		
+30	see p. 38)			
+50				
T.P.	9.5	877.15 ✓	1.18	867.63 ✓
67				
+25				
+50				
+75				
68				
+50				
69				
+25				
69+50				
+75				

Inst.
 Rod.
 Chain.

10-15-24

29

Left			C L			Right		
1.0	3.2	3.1	1.6	1.4	1.5	2.5	2.1	
25.2	21.0	17.7	13.8	00	15.0	18.2	20.9	
				(1.0)				
	2.4	2.9	1.2	0.8	1.0	2.3	2.1	
	21.7	17.8	13.3	00	14.4	17.3	21.1	

(15.4)

6.3
50.0

(12.2)

8.7
33.0

(14.2)

8.7
31.0

7.5
33.0

(12.8)

7.7
31.0

(11.2)

5.5
31.0

(10.5)

4.6
31.3

4.8
30.2

(9.4)

4.7	11.1	11.1	9.5	9.2	9.3	10.6	10.5	4.7
28.6	20.6	17.3	13.0	00	14.4	18.0	21.4	29.8

6.0	10.4	10.3	8.9	8.7	8.9	10.4	10.1	4.9
24.2	19.0	17.1	13.6	00	15.1	18.0	22.0	27.8

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. H.
70		877.15 ✓			
+25					
+50					
+75					
71					
+25					
+50					
T.P.	7.70	881.93 ✓	2.92	874.23 ✓	
+75					
72					
+25					
+50					
+75					

Inst.
 Rod.
 Chain.

10-15-24

30

Left				CI	Right			
4.1	9.7	8.3	8.1	6.2	8.1	9.9	10.0	5.5
25.8	18.0	14.5	00	00	15.1	15.8	21.6	27.4
5.0	8.1	8.3	7.3	7.0	7.6	9.2	9.0	6.9
28.5	22.6	19.8	14.2	00	16.0	19.5	24.4	26.8
2.5	8.0	8.1	7.1	7.0	6.6	7.5	7.8	6.4
28.7	21.8	18.0	15.7	00	16.0	19.8	23.2	26.7
2.5	7.7	7.8	6.3	6.2	6.7	7.6	7.1	5.3
30.5	22.8	18.3	15.2	00	15.4	20.5	24.0	28.1
2.2	6.9	6.8	6.0	5.9	5.6	6.8	6.7	4.9
31.4	24.6	18.4	16.0	00	16.0	19.5	23.3	27.0
2.0	6.0	6.3	5.7	5.3	5.6	6.5	6.4	4.3
30.4	24.5	17.8	15.5	00	16.1	18.7	23.0	26.3
1.7	6.1	6.1	5.0	4.7	4.8	5.6	6.0	3.7
29.4	23.5	17.4	15.0	00	14.3	15.1	21.8	26.6
5.9	10.6	10.5	9.5	9.0	9.4	10.4	10.6	8.6
29.1	23.6	17.4	14.6	00	16.2	19.0	23.6	26.3
5.5	10.2	10.2	9.0	8.6	8.8	10.1	10.2	8.2
28.6	22.6	17.0	14.4	00	15.9	19.3	23.9	27.2
5.5	9.5	9.8	8.2	8.1	8.3	9.7	9.6	7.5
27.0	22.0	17.7	14.4	00	15.6	19.5	21.5	28.0
5.1	9.0	8.9	7.8	7.6	7.8	9.1	9.2	5.7
27.2	22.4	18.0	15.2	00	15.6	19.5	23.2	26.8
4.9	8.2	8.2	7.5	7.2	7.4	8.5	8.6	5.4
26.9	22.0	18.9	16.0	00	15.5	18.8	23.0	27.1

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
73		881.93	✓		
	+25				
	+50				
	+75				
74					
	+25				
	+50				
	+75				
75					
	+25				
	+50				
	75				

Inst.
 Rod.
 Chain.

10-15-24

21

REVERSE SIDE OF RECORD SHEET

Left			G L		Right			
50 263	7.5 73.2	7.6 19.5	6.9 17.0	6.7 00	6.7 14.5	8.2 17.4	8.2 21.7	5.2 26.3
54 253	7.2 72.5	7.0 19.0	6.5 17.2	6.2 00	6.2 15.5	7.8 19.6	4.7 24.5	
57 259	6.7 23.3	6.6 19.2	5.6 16.8	5.7 00	5.5 15.7	6.8 18.4	6.9 21.3	5.0 24.4
58 258	6.5 22.8	6.3 19.7	5.5 16.5	5.3 00	5.4 16.0	6.5 18.3	6.6 22.0	5.0 24.5
54 249	6.2 22.3	6.0 19.0	5.3 16.8	4.9 00	5.2 15.5	6.3 18.0	6.4 22.4	5.1 24.1
56 266	6.1 23.0	5.7 18.4	4.8 15.8	4.7 00	5.0 16.3	6.2 19.0	6.4 22.4	5.4 24.3
53 258	5.9 22.5	5.7 19.0	4.5 15.4	4.5 00	4.5 15.0	5.7 18.7	6.0 23.3	5.3 25.9
51 266	5.9 24.0	5.6 19.0	4.2 16.1	4.2 00	4.2 14.7	5.9 19.8	6.2 24.0	5.4 25.9
55 274	5.7 22.8	5.5 19.0	4.1 16.5	3.9 00	4.0 14.9	5.3 17.7	6.2 23.6	5.5 25.9
60 280	5.4 19.4	3.9 15.3	3.8 00	3.8 15.5	5.3 18.7	5.8 26.5		
61 312	5.5 19.0	3.8 15.5	3.7 60	3.8 15.3	5.4 19.2	5.5 33.5		
64 345	6.1 20.4	3.8 15.6	3.7 00	3.8 16.4	5.7 19.8	5.6 33.0		

6.2

4.6

4.1

3.7

3.4

..... Cross Sections

Sta.	B. S.	H I	F. S.	Grade	Gr. R.
------	-------	-----	-------	-------	--------

76

881,93 ✓

+25

+50

+75

77

T.P.

4.88

883,28 ✓

3,53

878,40 ✓

+25

+50

+75

78

+25

(+40 see p 38)

+50

+75

Inst.
 Rod.
 Chain.

10-15-24

2

Left		G.L		Right
6.1	3.7	3.7	3.6	5.8
21.0	14.8	00	16.0	20.0

6.3	3.6	3.7	3.6	6.1
21.4	14.7	00	15.6	21.4

6.8	3.8	3.8	3.8	6.4
21.7	15.2	00	16.3	21.6

6.3	3.8	3.7	3.5	5.7
24.8	15.0	00	15.6	22.0

5.8	3.6	3.8	3.6	5.8
20.3	14.7	00	14.4	19.8

8.1	4.8	4.0	5.9	7.9
22.1	16.5	00	15.0	21.4

8.6	4.7	4.7	4.9	8.2
22.1	15.4	00	15.8	21.8

9.2	4.8	4.6	4.8	8.5
23.8	15.9	00	16.0	21.6

9.5	4.7	4.7	4.9	8.9
23.6	16.0	00	16.1	22.9

10.2	4.5	4.6	4.7	9.2
23.0	16.2	00	16.2	23.7

11.2	11.2	9.8	4.9	4.5	5.0	9.7	10.0	9.3
42.0	28.0	24.6	16.0	00	16.7	24.8	30.5	31.3

10.6	11.3	10.7	9.4	4.9	4.9	5.0	10.4	8.5
43.8	43.0	26.0	22.8	15.2	00	16.5	27.0	29.6

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
79		883.28			
+25					
(+30 +40)	} see p. 38)				
+50					
+75					
B.M.			11.53	871.75	
<u>Finals Cont. Book No 5 page 3</u>					
B.M.	11.53	883.52		871.99	
T.P.	0.97	877.08	2.41	876.11	
T.P.	1.07	866.05	12.10	864.98	
B.M.			5.44	60.61	60.46
T.P.	0.95	854.10	12.90	53.15	53.00
T.P.	2.16	847.52	9.14	44.96	
B.M.			9.66	837.86	837.71
B.M.	9.25	869.71		860.46	
T.P.	8.88	876.93	1.66	868.05	
	6.54	862.48	0.99	875.94	
	4.97	883.51	3.94	878.54	
	4.55	879.28	8.78	874.73	
B.M.			7.42	871.86	

Inst.
Rod.
Chain.

10-15-74

33

Left		GL	Right	
9.9	10.3	47	4.8	10.8
47.6	42.0	00	14.9	26.0
9.3	4.8	47	10.6	7.6
23.7	15.0	00	28.4	32.0
6.5	5.0	4.9	6.8	11.2
20.3	13.7	00	14.2	11.1
6.6	5.0	4.9	5.1	8.3
15.3	14.7	00	14.1	22.7
7.7	4.9	4.8	5.0	7.4
21.4	14.7	00	15.0	20.8

Spike 36" tree 65 ft. Lt. 79+50 El. 871.99

Cathartes 67-10 SW cor.

Top of spike to 65 ft

Rt. 60+60 Nail in tree

10-16-74 AM corrected from yesterday work

Spike 36" tree Lt 79+50

Farm Entrances ect.

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
------	-------	-------	-------	-------	--------

Farm Entrances

148 4.8

16 ft Rt = 0+00

0+00 = Zero embank.

0+04

0+08 = Zero Embankment.

16 ft Lt = 0+00

0+00 = Zero embankment.

0+05

0+13 = Zero Embankment.

Inst. Parkin
Rod. Steepleton
Chain. Fritz Conner

10-20-24

34

Left

G L

Right

west. 6.8 5.8 5.6 6.0 6.8 (East.)
 11.0 7.0 00 10 12

west. 7.0 6.0 5.7 5.7 6.8 (East.)
 15.0 12.0 00 5 8

Farm Entrances Ect.

Cross Sections

Sta.	B.S.	H. I.	F. S.	Grade	Gr. R.
135	5.7				
18 ft	0+00				
	0+00				Zero Embankment.
	0+05				
	0+10				Zero Embank
135-16 ft	0+00				
	0+00				Zero Emb.
	0+05				
	0+16				Zero Embankment.
127					
127+26	18	0+00			
	0+05				
	0+13				Zero Exc & Emb.
	0+25				
	0+46				
	0+60				Zero Exc.

Inst. 9
 Rod. S
 Chain. F

10-20-24

36

Left

G L

Right

ditch E. 30. ^{Notes} E refilled

(West)

8.0 6.7 6.9
 13.0 10.0 00

7.3 9.0
 11.0 13.0

East. ←

(West)

7.8 6.1
 13.0 10.0 5.9
 00

6.2 8.1
 9.0 12.0

(East)

(West)

12.3 10.3 11.0 11.9
 12.0 9.0 00 11.0

14.0
 14.0

East

✓

6.5 7.6 7.4 7.9 6.3
 8.0 6.0 0.0 5.0 7.0

✓

3.0 3.7 3.7 3.4 2.2
 7.0 6.0 00 6.0 5.0

✓

M^c Beths F.E.

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
------	-------	-------	-------	-------	--------

Sta	124+50	RT	at end	B ₃	46 off
✓	✓	✓	LT	✓	P ₃ none

B.M.	3.51	836.49		832.98	
------	------	--------	--	--------	--

0+16

+25

+50

+75

1

T.P.	1.02	826.49	11.02	825.47	✓
------	------	--------	-------	--------	---

+25

+50

+75

2

+25

+50

T.P.	2.12	816.08	12.53	813.96	✓
------	------	--------	-------	--------	---

Inst. 9
 Rod. S
 Chain. F

10-20-24

36

UNIVERSITY MICROFILMS

Left

G L

Right

Ridge

Trail in 12" Oak Lt Sta/10+00

4.6 4.6 47.1
 7.0 0.0 5.0

(6.4)

OG 5.1 6.4 6.4 5.6 5.5 5.6 6.5
 Lt 10.0 8.5 5.0 0.0 12.5 16.0

(8.2)

OG 6.7 7.8 6.9 7.3 7.4 8.3
 Lt 15.0 11.5 8.0 0.0 7.0 10.0

(10.0)

9.0 8.8 9.2 9.3 10.4
 10.0 7.0 0.0 8.0 11.0

(11.0)

11.5 10.7 11.1 11.1 12.6
 10.0 7.5 0.0 8.0 11.0

5.6 3.6 3.6 3.4 5.9
 12.0 7.0 0.0 8.0 12.0

(5.4)

7.5 5.2 5.3 5.6 7.8
 11.0 7.0 0.0 7.0 12.0

7.7 7.0 6.9 7.2 11.0
 10.0 7.0 0.0 7.5 12.0

(9.0)

9.5 8.2 8.4 8.7 9.8
 9.5 7.0 6.0 6.0 9.5

(10.0)

10.4 9.5 9.6 9.9 10.7
 9.5 7.0 0.0 7.5 9.5

11.4 11.2 11.2 11.2 11.9
 9.5 6.5 0.0 6.5 9.0

Mr. Betty's F.E.

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
2+75		816.08			
3					
4+25					
4+35	Zero Exc.				
			3.95	814.23	0.63
Connelly FE Lt. 104 ±	Copied from B.3P54				
BM	2.69	876.90		874.21	
I.P.	8.35	874.94	10.31	866.59	
0+00	= Zero Exc.				
0+07					
0+25					
0+50					
0+75					
1+00					
1+15	Zero Exc.				

Inst. 9
 Rod. 5
 Chain. F

10-20-24

37

Left

O.I. 3.2

Right

3.9	2.6	2.7	2.3	3.2
8.5	6.0	0.0	6.5	8.5
		(1.0)		
5.1	3.8	3.6	3.3	3.9
9.5	6.0	0.0	6.5	9.5
		(1.4)		
4.8	3.7	3.6	4.0	
7.5	5.0	0.0	6.0	

Slope stake Lt

$\frac{F 0.8}{8.0}$

(Sta 3400) El. 112.3

9-30-24

Sept 12" oak 33' Lt 99+15

O.G. → 12.5
8

12.1 12.4 3.1 ← O.G.
0.0 6.0 19.0

O.G. → 10.4
6.0

10.8 10.9 2.9 ← O.G.
0.0 6.0 18.0

O.G. → 7.7
8.0

7.7 7.7 8.8 1.6 ← O.G.
0.0 6.0 8.0 15.0

O.G. →

4.7 4.7 5.6 1.0 ← O.G.
0.0 6.0 8.0 14.0

O.G. → 3.4
0.0

3.5 1.0 ← O.G.
8.0 10.0

Add. X Sect. for finals

Sta.	Cross			Grade	Gr. R.
	B. S.	H. I.	F. S.		
B.M. 78+40	11.44	883.43		871.99	
79+30					
79+40	W.C.B.				
B.M.	9.45	870.02		860.57	
T.P. 69+30	6.93	874.40	2.58	867.47	
B.M. 66+25	8.32	868.89		860.57	

Inst. 9
 Rod. S
 Chain. F

10-20-24

38

Left

C L

Right

10.2 4.7 4.6 4.7 9.2
 24.8 16.1 0.0 16.0 23.7

(4.8)

6.3 4.9 4.7 4.9 6.5 11.4 11.7 6.0
 18.5 13.7 0.0 14.3 18.0 24.4 28.5 32.6

(4.8)

13.5 13.1 4.9 4.7 4.9 12.2 11.3 8.6 6.2 0.0
 37.0 24.0 14.6 0.0 13.7 21.8 27.9 33.4 43.0

(4.8)

top S.W. cor coping cutting grass str 67+10

50.0
 2.0 4.7 8.6 8.4 7.0 6.7 6.7 8.3 7.7 1.9
 79.2 25.8 21.1 17.3 13.4 0.0 15.0 19.0 22.2 30.8

(7.0)

8.8 11.8 11.8 9.5 9.2 8.8 9.9 9.5 3.8 2.2 0.8
 75.0 22.0 18.7 15.0 0.0 16.4 20.0 24.0 31.2 39.0 42.4

(9.4)

F.E. Oct.

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
70+25	7.4				
70+25	Lt 14 ft = 0+00				ditch filled over culv.
0+6.3	= Zero Exc & Emb.				
0+14.3					
0+45	= Zero Exc				
70+50	Rt. Ditch has been filled over culv.				
77+00	4.9				
76+85	Lt. 16 ft = 00				Zero Emb.
0+07					
0+21	= Zero Emb.				
76+85	Rt. 16 ft = 00				Zero Emb.
0+07					
0+30	= Zero Emb.				
P.M.	12.56				860.57
67+87	- 16 ft RT = 0.0				
0+06					
0+12	Zero Exc.				
0+16					
0+41					
0+50	= Zero Exc				

Inst. G
 Rod. S
 Chain. F

10-20-24 39

Left

G L

Right

East. 3.6 6.7 6.2 6.3 6.3 6.9 2.6
 19.0 13.5 0.5 0.0 6.5 10.0 15.5 west

East. 7.6 6.0 5.5 5.8 7.5
 16.0 14.0 0.0 8.5 11.5 west

East. 6.7 5.1 5.0 5.0 7.1
 12.5 8.5 0.0 16.0 19.5 West

West 10.4 8.6 8.5 8.6 10.1
 8.0 5.5 0.0 4.5 7.0 East

✓ 3.6 7.9 7.5 7.7 3.3
 14.0 8.0 0.0 6.0 10.5 ✓

✓ 1.7 3.2 3.3 4.0 1.7
 9.0 6.0 0.0 8.0 10.0

Burriss St. Connection Final

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M. 0+58	9.31	753.10	✓	743.79	
1+00					
+25					
T.P. +50	5.87	758.85	✓	749.78	✓
+75					
✓					
+25					
+50					
T.P. +86	3.64	752.54	✓	748.90	✓
3					
+50					
4					

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
4+50		752.54 ✓			
5					
+50					
6					
+50					
T.P.	9.82	759.91 ✓	2.45	750.09 ✓	
7					
+50					
+75					
8					
T.P.	8.63	766.46 ✓	2.08	759.83 ✓	
+50					
+75					
+88.5					

Inst. 9.
 Rod. S.
 Chain. F.

10-21-24

41

Left.

C L

Right

5.0 6.6 6.5 4.9
 16.7 14.4 9.7 7.3

4.3
 4.5
 00

4.3 4.7 7.2
 5.5 16.3 21.0

5.3 6.3 6.7 5.2
 18.2 16.2 11.0 7.6

4.3

4.6

4.6 5.7 5.5 4.5
 16.8 15.3 11.6 8.6

2.3

2.7

2.9 4.7 4.5 3.8
 15.6 13.1 9.6 6.9

4.7

1.3 3.2 3.2 2.7
 15.0 12.5 8.7 6.4

5.9

6.7 9.0 9.2 8.1
 17.7 15.8 12.0 9.0

4.2

4.6 6.5 6.6 6.1
 21.0 19.1 15.2 11.8

2.4

3.2 5.4 5.6 4.7 4.4
 18.5 16.0 12.8 10.7 00

7.3

1.0 2.8 2.8 2.6
 18.3 16.3 12.8 9.9

5.5

6.6 7.0 7.3 6.9
 17.6 16.5 12.8 10.6

2.8

5.5 6.0 5.9 5.5
 20.2 19.2 14.0 12.6

4.5 3.9 3.5
 15.2 11.7 4.4

2.5 3.9 3.0 2.6
 18.4 16.4 13.4 4.8

3.1 3.5 3.7
 7.3 4.4 6.0

Cross Sections

Sta.	B.S.	H. I.	F. S.	Grade	Gr. R.
		766.46			
T.P.	0.74	754.87	12.33	754.13	
T.P.	0.30	743.48	11.69	743.18	
Bm			5.48	738.00	738.00

Inst. 9
Rod. 3
Chain. F

10-21-24

42

Left. G L Right

spike in stump 1st Sta 30 - 0.12-

Final

Cross Sections

Sta.	B.S.	H. I.	F. S.	Grade	Gr. R.
B.M. 0+75	2.61	701.86 ✓		699.25 ✓	
1+00					
+50					(End of Rip Rap Lt.)
2+00					
+50					
3+00					
T.P. +50	8.3	708.80 ✓	1.19 ✓	700.67 ✓	
4+00					
+50					
5+00					
+50					
6+00					
T.P.	6.15	709.93 ✓	5.12 ✓	703.68 ✓	

Inst. Galvin
 Rod. Skoplen.
 Chain. Fritz

Conner

11-10-24

43

Left

C L

Right

Nail in T-P near bridge 150' Lt. Sta. 1 + 26

7.8
 57.3 27.0 (Br 16 Br 10)

7.8
 52.2 29.0 (GR 17.0 GR 16.4) (+11.6)

7.3
 47.2 26.0 (GR 17.9 GR 15.6) (+10.6)

4.4
 46.3 27.7 (GR 18.7 GR 14.7) (+10.0)

3.3
 45.6 28.6 (GR 19.6 GR 13.7) (+9.3)

2.5
 45.1 29.2 (GR 20.8 GR 13.9) (+8.8)

8.4
 42.7 28.3 (GR 21.7 GR 13.6) (+1.6)

8.1
 40.0 28.4 (GR 21.6 GR 14.1) (+1.4)

7.6
 40.7 27.5 (GR 21.3 GR 14.2) (+1.4)

7.5
 38.4 26.8 (GR 21.4 GR 15.2) (+1.3)

7.5
 38.3 25.8 (GR 21.3 GR 16.9) (+1.3)

7.0
 36.0 25.0 (GR 21.0 GR 17.9) (+1.2)

Final

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
6+50	PT	709.83			
7+00					
7+50	✓				
8+00					
8+50	✓				
9+00					
9+50					
10+00					
T.P.			0.48	709.35	✓

Inst. G
 Rod. S
 Chain. F

11-10-24

44

Left		L		Right
8.0 36.2	24.4	(GR 21.0)	(GR 17.2)	(+0.2)
7.8 36.0	25.4	(GR 21.0)	(GR 17.4)	(+0.2)
7.6 35.9	24.9	(GR 20.9)	(GR 17.6)	
7.6 35.6	24.5	(GR 20.8)	(GR 17.8)	(+0.2)
7.7 36.9	25.1	(GR 20.6)	(GR 17.9)	
7.8 37.9	26.6	(GR 20.9)	(GR 17.2)	(+0.2)
8.3 39.4	28.4	(GR 20.8)	(GR 16.8)	(0.1)
8.1 38.3	26.7	(GR 20.7)	(GR 16.4)	(+0.2)

Rock 10+15 Lt.

Final Cross Sections

Sta.	B. S.	H. I. ✓	F. S.	Grade ✓	Gr. R. ✓
B.M. → T.P. →	0.34 6.34	699.59 ✓ 698.89 ✓	7.04	699.25 ✓ 692.55 ✓	
0+75					
1+00					
+50					
T.P.	7.11	705.62 ✓	0.38	698.51 ✓	
2+00					
+50					
3+00					
+50	(End of R.P. Range RT)				
T.P.	1.92	705.07 ✓	2.47	703.15 ✓	
4+00					
+50					
5+00					
+50					
T.P.	10.16	714.09 ✓	1.14	703.93 ✓	
6+00					

Inst. G
 Rod. S
 Chain. F

11-10-24

44

Left

C L

Right

Left	C L	Right
Nail in T.P. Near Bridge	Sta. No. 1 of Sta. 1450 G.R.) 10.2) 23.0	5.3 48.4
(+14.6)	G.R.) 16.4) 25.0	4.4 48.4
(+12.8)	G.R.) 15.6) 22.6	0.8 42.6
(+6.4)	G.R.) 14.7) 20.3	6.8 39.3
(+5.6)	G.R.) 13.7) 18.2	5.4 33.2
(+5.1)	G.R.) 13.9) 16.4	5.4 33.4
(+4.8)	G.R.) 13.6) 16.6	5.4 28.6
(+5.1)	G.R.) 14.1) 17.1	4.3 29.1
(+5.1)	G.R.) 14.2) 16.8	3.6 28.4
(+5.0)	G.R.) 15.2) 22.8	3.7 34.2
(+5.0)	G.R.) 16.9) 25.9	3.5 36.2
(4.1)	G.R.) 17.9) 25.9	12.6 35.3

Final

Sta.	B. S.	H. I.	F. S.	Cross Sections	Grade	Gr. R.
6+405		714.09				
7						
+50	✓					
8						
+50	✓					
9						
+50						
10						
T.P.	4.84	714.13	4.80		709.29	
10+50						
11						
+50						
12						
12						

Inst. 9
 Rod. S
 Chain. F

11-10-24

46

Left.

C L

Right

(4.1) (G.R. 17.2) 27.5 12.6
 32.9

(4.1) (G.R. 17.4) 20.0 11.8
 29.0

(G.R. 17.6) 20.9 12.2
 30.9

(4.2) (G.R. 17.8) 22.0 12.2
 33.0

(G.P. 17.9) 21.9 11.1
 31.5

(4.4) (G.R. 17.2) 20.8 10.8
 29.6

(4.4) (G.R. 16.8) 19.4 10.6
 27.4

(4.5) (G.R. 16.4) 19.4 10.8
 28.1

Rock 10+15 Lt.

12.2
 36.5 27.5 (G.R. 20.8) (4.5) (G.R. 16.6) 20.9 10.6
 29.9

12.2
 35.9 26.9 (G.R. 20.7) (4.6) (G.R. 16.7) 23.1 10.7
 29.1

12.3
 36.2 26.6 (G.R. 20.8) (4.6) (G.R. 16.8) 26.4 10.7
 33.0

12.0
 33.3 24.8 (G.R. 20.8) (4.7) (G.R. 17.5) 26.5 10.7
 34.5

Final

Cross Sections

Sta.	B.S.	H. I.	F. S.	Grade	Gr. R.
12 +50		714.13			
13					
+50					
14					
+50					
15					
T.P.	5.78	713.75	6.16	707.97	
B.M.			8.57	705.24	705.14

Inst. *G*
 Rod. *S*
 Chain. *F*

11-10-24

47

Left	C L	Right
11.5 32.4	24.4 (GR. ^{4.9} GR.) (20.7 18.1)	28.9 10.3 36.6
11.5 32.8	23.8 (GR. ^{4.8} GR.) (20.7 18.7)	30.4 10.1 35.2
11.2 32.3	23.3 (GR. ^{4.8} GR.) (19.8 19.0)	28.0 9.6 34.5
10.8 31.1	22.1 (GR. ^{4.9} GR.) (19.1 19.7)	26.9 9.8 33.6
10.4 30.6	23.1 (GR. ^{4.9} GR.) (18.7 19.9)	26.5 10.0 33.5
10.0 28.6	22.2 (GR. ^{5.0} GR.) (18.2 19.5)	25.5 10.1 32.5

Rock Pt. 15+15

Cottonwood tree 48" R-Sta 21.

Inst. G
 Rod. S
 Chain. F

11-20-24

48

Left		C L		Right	
3.6			3.0		3.5
7.0			00		23.0
	x		(3.2)		
4.7	4.0	3.6	3.2	3.6	3.6
9.0	18.0	17.0	00	11.0	16.6
			(4.0)		
4.3		x	4.2		4.8
6.0		4.0	00	4.7	4.6
		18.0		15.8	16.0
			(4.8)		
4.8		x	5.2		5.5
7.7		4.4	00	5.5	5.5
		18.7		14.8	20.3
			(5.5)		
5.1		x	6.0		6.6
8.6		5.0	00	6.2	6.6
		19.6	4.8	13.7	18.2
			(6.0)		
5.6		x	6.5		7.0
9.2		5.6	00	7.0	7.0
		20.8	5.3	13.9	16.4
			(6.3)		
5.7		x	6.8		7.5
8.3		5.8	00	7.3	7.5
		21.7	5.5	13.6	16.6
			(6.5)		
6.0		x	6.9		7.8
8.4		5.9	00	7.3	7.8
		21.6	5.8	14.1	17.1
			(6.5)		
5.8		x	7.0		8.1
7.5		6.1	00	7.3	8.1
		21.3	5.8	8.8	14.2
			(6.8)		
5.8		x	7.0		7.5
5.8		6.0	00	7.7	7.5
		21.4	5.8	15.2	22.8
			(6.8)		
5.1		x	7.0		7.8
5.8		6.4	00	7.4	7.8
		21.3	4.9	10.2	16.9
			(4.8)		
5.0		x	5.1		5.9
		4.2	00	5.4	5.9
		21.0	3.9	13.0	17.9

Center bridge

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
6+40.5	P.T.	714.75			
7					
+50	✓				
8					
+50	✓				
9					
+50					
10					
T.P.	4.95	714.26	5.44	709.31	
+50					
11					
+50					
12					

Inst.
 Rod.
 Chain.

G
 S
 F

11-20-24

49

	Left		C L		Right	
4.4	4.2	4.3	(4.9)	5.2	5.4	5.8
24.4	21.0	14.7	00	11.2	17.2	22.5
4.8		x	(4.8)	5.1	5.0	5.5
25.4		21.0	00	12.2	17.4	20.0
4.7		x		4.9	4.8	5.0
24.9		20.9	100	00	9.5	17.6
4.7		x	(5.0)	4.9	4.9	4.9
24.5		20.8	128	00	80	15.3
5.0		x		4.9	4.9	5.1
25.1		25.6	168	00	8.8	14.0
5.3		x	(5.1)	4.8	4.6	5.0
26.6		20.9	00	12.8	17.2	20.8
6.2		x	(5.1)	4.9	4.9	5.1
28.4		20.8	11.3	00	16.8	19.4
5.5		x	(5.2)	4.8	4.8	4.9
26.7		20.7	00	12.2	16.4	19.4
4.7		x	(4.7)	4.4	4.4	4.4
27.5		20.8	16.0	00	16.6	20.9
4.8		x	(4.8)	4.5	4.7	4.7
26.9		20.7	00	12.2	16.7	23.1
5.4		x	(4.8)	4.8	4.6	5.0
26.6		20.8	00	11.2	16.8	26.4
5.1		x	(4.9)	4.9	4.7	5.0
24.8		20.8	11.1	00	15.6	17.5

Cross Sections

Sta.	B.S.	H. I.	I. S.	Grade	Gr. R.
12	+50	714.26			
13					
	+50				
14					
	+50				
15					
	T.P.		6.27	707.99	

Inst. S
 Rod. F
 Chain. F

11-20-24

10

	Left X		C L		Right X	
5.5 24.4	5.0 20.7	4.7 13.0	4.9 00	(4.9)	4.7 18.1	5.6 28.9
5.6 23.8		5.0 20.2	4.7 12.8	4.9 00	X 4.9 18.4	5.4 30.4
5.5 23.3	X 5.2 19.8	5.1 11.0	5.0 00	(5.0)	4.8 12.3	X 5.0 19.0
5.5 22.1		X 5.2 19.1	5.0 10.2	5.1 00	(5.1)	4.7 13.3
5.6 23.1	X 5.0 18.7	4.8 13.2	5.0 00	(5.1)	4.9 11.4	X 5.0 19.9
5.0 22.2	X 4.6 18.2		4.8 00	(5.2)	4.8 12.0	X 5.1 19.5

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M.	3.00	795.34 ✓		792.34 ✓	
T.P.	0.70	794.26 ✓	11.78	783.56 ✓	
44+00					
+50					
45+00					
+50					
T.P.	8.73	782.46 ✓	10.53	773.73 ✓	*
46+00					
+50					
47	End of Hanson's FF				
T.P.	11.80	785.53 ✓		773.73 ✓	*
+50					
48					
+25					
+45					
		W46			

Inst. Galv. In.
 Rod. Steel 1/4"
 Chain. 112

11-18-24

51

Canner

Left

CL

Right

Sta 45+90 Top of Guard Rail Post, Lt.

14.0 11.9 ^(11.8) 11.8 11.8 12.9 12.9 2.4
 21.5 18.0 00 15.0 15.0 18.7 21.5

(9.4)

11.7 9.4 9.3 9.4 10.4 10.2 4.5
 19.6 16.3 00 15.0 15.0 18.6 22.3

(7.0)

11.0 7.1 7.0 7.0 7.4 7.0 2.7
 23.4 18.0 00 15.4 16.8 18.2 21.0

(4.6)

13.6 4.5 4.8 4.6 5.2 4.5 0.0
 38.3 26.3 00 15.0 16.2 18.7 21.4

Top of end of R.R. Post Hanson's F.E. Sta 47+00 Lt.

11.8 2.0 1.2 00
 46.6 33.2 19.0 14.5 (0.4)

12.8 7.4 6.5 7.3
 53.4 45.5 31.5 28.3 (+2.0)

14.0 10.7 9.9 8.6 ⁰⁶
 65.0 58.0 42.0 35.0 (+4.4)

9.5
 37.0 (+3.8)

7.6
 37.6 (+6.2)

7.6 5.5
 41.0 36.0 (+7.4)

4.8
 34.0 (+8.0)

Cross Sections

Sta.	B.S.	H I.	F S.	Grade	Gr. R.
48+62		785.53			
+75					
T.P.	3.69	776.35	12.87	772.66	
+88					
49+00					
+10					
T.P.	11.93	788.09	0.19	776.16	
+25					
+38					
T.P.	8.52	796.28	0.33	787.76	
+50					
T.P.	10.63	806.70	0.21	796.07	
+75					
50+00					
+25					
+50					
T.P.	4.29	798.78	12.21	794.49	

Inst. G
 Rod. S
 Chain. F

11-18-24

52

Left

CL

Right

7.9
45.0

+8.5

12.9
58.0

+9.8

Bottom of dunes → 16.0
73.0

+19.5

↙ 16.0
73.0

+20.1

1.6
59.0

+20.7

4.6
47.0

+9.5

0.0
44.0

+10.0

OG → 6.4
41.7

+2.3

OG → 7.0
33.7 5.0
30.0

7.0

OG → 8.8
41.6 4.3
35.0

6.0

OG → 12.1
44.6 3.8
33.0

5.0

OG → 13.3
41.4

4.0

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
50+75		798.78			
51+00					
+25					
+50					
B.M.			9.29	789.49	89.49
+75					
T.P.	6.21	792.05	12.94	785.84	
52+00					
+15					
B.M.				789.50	789.49
B.M.	6.46	798.80		792.34	
46+00					
+50					
47+00					
+50					

Inst. E
 Rod. S
 Chain. F

11-18-24

53

Left

C L

Right

8.6
43.0

(+4.8)

9.4
44.4

(+5.7)

6.6
40.3

(+6.6)

6.0
40.3

(+7.5)

Page 65 ok O.K.

15.5
50.3

(+8.5)

9.7
54.0

(+16.1)

5.9
49.0

(+16.6)

Cattle pass 48 + 50 S.E. Cor. parapet wall

(16.7)

16.5

16.6 17.9 17.9 12.3

00

14.0 16.2 18.6 22.0

(14.3)

12.5

14.6

14.4 15.9 15.9 9.8

17.3

00

14.5 16.8 18.9 23.5

(11.9)

12.0

11.8

11.6 13.2 13.2 7.2

17.0

00

14.6 17.2 20.0 24.0

(8.3)

9.2

9.3

9.4 10.6 10.7 6.2

17.3

00

15.0 17.0 18.9 22.0

(7.1)

6.6

7.4

7.6 9.0 8.8 3.5

18.0

00

14.4 17.0 19.3 22.0

Sta. Cross Sections			Grade	Gr. R.
	B. S.	H. I.	F. S.		
48+25		798.80 ✓			
+45					
+62					
+75					
+88					
49+00					
+10					
T.P.	12.04	810.82 ✓	0.02 ✓	798.78 ✓	
48+62 ✓					
+75					
+88					
49					
+10					
T.P.			0.37	810.45 ✓	

Inst. S
 Rod. S
 Chain. F

11-18-24

54

Left		C L	Right					
5.6 20.0		(5.9) 6.3 00	6.7 14.1	8.1 17.7	7.6 21.4	9.3 26.0		
	4.1 16.0	(6.3) 5.3 00	5.8 14.5	7.2 17.6	6.6 22.2	0.0 27.0		
3.2 17.0		(4.8) 4.3 00	Cattle pass		4.9 15.1	8.0 22.3	10.7 25.4	10.7 32.3
	3.7 24.0	(3.5) 2.9 00	3.8 15.5	4.4 24.2	5.2 34.4	6.5 44.4	6.0 44.4	
2.7 25.4	1.9 20.3	(2.9) 3.2 00	3.5 14.5	4.7 30.2	4.5 48.0			
	1.4 26.0	(2.3) 1.2 00	2.6 1.40	3.4 30.0	3.8 50.0	3.7 59.0	2.3	
0.5 26.0	0.6 22.3	(1.7) 2.0 0.0	2.8 14.8	3.0 30.4	5.8 43.7	6.8 53.6	1.8 58.9	0.8 64.8
		(16.8)			5.0 38.0	O.G.		
		(15.5)			5.3 47.3	O.G.		
		(14.9)			4.3 54.2	O.G.		
		(14.3)			3.8 63.5	O.G.		
		(13.7)			4.4 67.3	O.G.		

Zero S.R.
 15 ft more for
 app. to Cattle pass

Top of rock Pt. Sta 49+

Cross Sections

Sta.	B. S.	H. I. ✓	F. S.	Grade ✓	Gr. R. ✓
T.P. 49+50	12.98	823.43 ✓		810.45 ✓	
+75					
50+00					
+25					
+50					
T.P. +75	6.08	829.17 ✓	0.34	823.09 ✓	
51+00					
+25					
+50					
+75					
52+00					
52+15					
52+60					

Inst. Galvina
 Rod. Stouglon
 Chain. Fritz

Conner

11-19-24

55

Left

C L

Right

24.8

16.4
26.0 O.G.

23.7

10.4
26.0 O.G.

22.7

6.1
28.2 O.G.

21.7

4.0
28.9 O.G.

20.7

1.7
29.5 O.G.

25.6

6.6
29.0 O.G.

24.7

7.3
28.8 O.G.

23.8

7.9
31.0 O.G.

22.9

9.0
32.0 O.G.

21.9

7.1
38.0 O.G.

21.0

5.2
40.0 O.G.

20.5

4.3
39.0 O.G.

18.9

2.0
39.0

..... Cross Sections

Sta.	B. S.	H. I. ✓	F. S.	Grade	Gr. R.
		829.17			
52+75					
T.P.	9.08	837.44 ✓	0.81 ✓	828.36 ✓	
53+00					
53+25					
53+50					
53+75					
54+00					
54+25					
T.P.	2.77	827.30 ✓	12.91 ✓	824.53 ✓	
54+55					
54+75					
54+90					
55+00					

Inst. G
 Rod. S
 Chain. F

11-19-24

56

Left

C L

Right

16.5

3.7
36.0

2.0
39.0 0 G

25.8

2.9
34.5 0 G

24.9

5.4
37.5 0 G

24.0

4.6
36.0 0 G

23.0

6.0
32.5 0 G

22.1

10.5
27.0

21.2

14.0
25.0

10.0

8.4
25.0

9.3

8.1
26.0

8.9

5.1
23.0

8.3

4.2
23.0

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
------	-------	-------	-------	-------	--------

827.30 ✓

55+25

T. P.	1.67	816.17 ✓	12.80	814.50 ✓	
-------	------	----------	-------	----------	--

T. P.	6.64	810.56 ✓	12.25	803.92 ✓	
-------	------	----------	-------	----------	--

55+50

55+68

55+80

T. P.	12.97	823.31 ✓	0.22	810.34 ✓	
-------	-------	----------	------	----------	--

56+00

T. P.	12.52	835.61 ✓	0.22	823.09 ✓	
-------	-------	----------	------	----------	--

56+25

T. P.	11.48	846.84 ✓	0.25	835.36 ✓	
-------	-------	----------	------	----------	--

56+50

T. P.	10.71	956.55 ✓	1.00	845.84 ✓	
-------	-------	----------	------	----------	--

+75

57

+25

Inst. G
 Rod. S
 Chain. F

9

11-19-24

57

Left

C L

Right

7.4

12.0
27.0

+10.2

8.1
49.0

+10.9

14.3
57.0

+11.4

7.0
47.0

0.4

10.6
38.0

12.0

4.0
43.0

22.3

3.2
116.0

31.2

13.6
44.0

4.6 06
51.0

30.2 13.5
37.0

3.8
49.0

29.2 11.7
39.0

Cross Sections

Sta.	B. S.	H. I. ✓	F. S.	Grade	Gr. R.
57+50		856.55 ✓			
+75					
58					
+30					
T.P.	10.98	866.79 ✓	0.74	855.81 ✓	
57+25					
57+50					
+75					
58+00					
+30					
+60					
+85					
59+05					
59+25					

Inst. *G*
 Rod. *S*
 Chain. *F*

11-19-24

58

Left

CL

Right

28.3

11.7
37.0

27.4

14.0
33.0

26.5

10.1
36.0

25.4

7.7
37.0

39.4

8.2
54.0

38.5

11.9
47.0

37.6

12.6
45.0

36.7

9.7
47.0

35.6

6.5
48.0

34.5

10.4 4.4
42.0 46.0

33.6

10.2 3.6
42.0 45.0

32.8

10.1 3.7
40.0 43.5

32.1

10.0 4.9
41.0 43.7

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
59+50		866.79 ✓			
T.P.	6.67	860.49	12.97	853.82 ✓	*
58+30					
+60					
+85					
59+05					
+25					
+50					
T.P.	2.64	858.46 ✓		853.82 ✓	
+75					
60+00					
T.P.	1.57	845.65 ✓	12.38	844.08 ✓	
B.M.			7.93	837.72 ✓	837.71

Inst. G
 Rod. S
 Chain. F

11-19-24

59

Left

C L

Right

31.2

8.3
40.7

29.3

5.1
46.0

28.2

11.5
33.0

27.3

9.2
34.5

26.5

7.3
34.5

25.8

11.2
32.0

24.9

11.8
33.0

20.0

4.1
35.7

19.0

8.2
43.0

Cross Sections

Sta.	B. S.	H. I. ✓	F. S.	Grade ✓	Gr. R.
Bm 49+25	1243	804.77		792.34	
+38					
+75					
50+00					
+25					
T.P. +50	9.03	813.17 ✓	0.63	804.14 ✓	
+75					
51+00					
+25					
+50					
+75					
52+00					

Inst. 9
 Rod. S
 Chain. F

Corner

11-20-24

60

Left		C L		Right				
S.A. Con. Cont. Jan 48-50								
6.3	6.1	6.7	7.4	7.7	7.7	10.0	10.3	4.2
28.0	24.5	100	00	9.5	19.0	24.0	27.0	32.0
(6.7)								
5.1	4.8	6.0	6.7	7.7	8.6	8.6		0.3
27.5	26.0	100	00	14.0	15.5	17.5		26.0
(5.1)								
3.2	3.2	3.3	4.3	5.1	6.2	6.9	6.9	4.7
31.0	27.5	22.0	10.0	00	15.0	16.4	18.5	20.0
(4.1)								
4.6	2.8	3.3	3.2	3.9	4.8	5.2	5.2	3.0
35.5	27.8	25.0	100	00	15.0	16.0	18.0	20.0
(3.1)								
2.0	1.2	2.1	3.0	3.8	4.3	4.2	2.2	
33.0	26.6	100	00	15.3	16.6	18.7	21.0	
(10.5)								
9.4	8.9	8.7	9.8	10.5	11.4	12.4	12.0	
27.8	25.0	20.0	100	00	14.3	16.0	19.7	
(9.6)								
8.8	8.2	8.9	9.6	10.4	11.3	11.0		
23.0	21.4	100	00	15.2	17.1	22.0		
(8.1)								
8.1	7.7	7.9	8.5	9.2	10.0	9.9		
22.2	19.3	100	00	14.2	16.3	21.0		
(7.8)								
6.9	6.9	7.4	7.9	8.2	9.2	9.1		
19.8	17.0	100	00	13.0	15.5	21.0		
(6.9)								
6.5	6.6	6.7	7.0	7.4	8.5	8.5		
20.0	16.0	100	00	13.7	15.8	22.0		
(5.9)								
6.0	5.8	6.0	6.0	6.2	7.6	7.5		
20.0	14.5	100	00	14.6	15.0	24.0		
(5.0)								
5.2	5.2	5.1	5.3	5.3	6.6	6.1		
20.0	14.0	100	00	15.0	18.6	26.0		

Cross Sections

Sta.	B.S.	H. I.	F. S.	Grade	Gr. R.
------	------	-------	-------	-------	--------

52 +15

813.17

Equation

+60

+75

53 +00

+25

+50

T.P.

10.96

823.33

0.50

812.37

+75

54

+25

+50

+75

+90

55 +00

ns. G
 Rod. S
 Chain. F

11-20-24

61

Left				Right			
4.4	4.6	4.7	4.8	4.8	7.5	6.2	
20.0	14.0	10.0	00	15.0	18.4	25.4	

				(2.9)			
3.5	3.7	3.7	3.6	3.6	5.1	5.0	
20.3	13.8	10.0	00	15.2	18.4	24.0	

				(2.5)			
3.2	3.2	3.2	3.1	3.1	4.4	4.4	
20.0	13.8	10.0	00	16.0	19.3	23.7	

				(1.6)			
2.8	2.5	2.4	2.3	1.9	3.4	3.4	
23.0	13.9	10.0	00	15.0	17.7	22.6	

				(0.9)			
	1.5	1.6	1.7	1.2	2.8	2.6	
	23.0	14.0	00	14.2	17.4	21.7	

				(10.2)			
	1.0	0.9	0.7	0.3	1.6	1.6	
	22.6	13.7	00	16.0	18.0	21.0	

				(8.9)			
	10.1	10.3	10.0	9.4	10.8	10.7	
	20.8	14.0	00	15.5	17.5	20.1	

				(6.9)			
9.5	9.3		8.8	8.3	9.4	9.4	
20.0	13.6		00	15.3	17.3	19.6	

				(11)			
8.5	8.2		7.9	7.4	8.9	8.8	
19.0	13.6		00	15.0	17.7	20.8	

				(6.0)			
	7.0	7.0	6.7	6.1	7.5	7.5	4.7
	19.1	13.7	00	15.9	18.0	23.0	25.0

				(5.3)			
	6.2	6.3	5.8	5.1	6.8	6.5	4.1
	19.0	13.9	00	16.5	19.4	24.6	26.5

				(4.9)			
	5.6	5.6	5.1	4.3	5.4	5.3	1.3
	19.8	13.5	00	15.4	17.5	21.0	23.0

				(11.2)			
5.4	5.0	4.6		3.7	4.7	4.3	0.3
21.0	13.7	00		15.5	17.9	21.0	23.0

Cross Sections

Sta.	B.S.	H. I.	F. S.	Grade	Gr. R.
55+25		823.33			
+50					
T.P.	10.70	833.01	1.02	822.31	
+68					
+80					
56					
+25					
+50					
+75					
57+00					
+25					
+50					
+75					
T.P.	10.86	843.61	0.26	832.75	

Inst. G
 Rod. S
 Chain. F

11-20-24

62

Left	x	CL	(3.4)	Right	x
4.7	4.1	3.6		2.7	2.5
23.8	14.0	00		13.9	18.0

3.4	x	(2.5)	x	
24.0	3.0	2.5	1.7	1.4
	13.8	00	14.0	22.3

11.9	x	(11.5)	x	
24.4	11.7	11.2	10.5	10.2
	14.2	00	13.7	20.6

11.2	x	(11.0)	x	
24.0	11.1	10.6	9.9	9.7
	14.2	00	13.9	19.0

10.7	x	(10.3)	x	
23.2	10.1	9.5	8.9	8.9
	14.2	00	13.8	19.0

9.3	x	(9.4)	x	
72.0	9.1	8.3	7.6	7.5
	14.2	00	13.9	17.0
			22.2	29.1
			10.5	10.6
			6.8	6.4
			34.9	41.6

(10.9)	x	(6.5)	x	
25.0	8.0	7.8	7.0	6.4
	20.0	14.0	00	13.7
				16.7
				20.8
				28.6
				34.6
				41.2

6.6	x	(7.6)	x	
17.6	6.5	5.9	5.0	6.3
	14.0	00	16.4	19.2
				26.0

5.4	x	(6.6)	x	
17.5	5.4	4.8	3.8	4.8
	14.0	00	17.0	18.3
				26.0

4.6	x	(5.6)	x	
19.0	4.3	3.4	2.9	3.8
	14.2	00	15.9	18.0
				23.0

3.3	x	(4.7)	x	
24.0	3.0	2.4	1.6	3.0
	14.2	00	15.0	18.0
				23.4

2.8	x	(3.8)	x	
23	1.8	1.1	0.7	1.9
	14.2	00	15.7	18.0
				24.0

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
58+00		843.61			
+30		Zero borrow Lt.			
+60			Row 99.0	OG → 9.0 71.5	
+85			Row 98	OG → 3.2 88.0	14.3 74.0
59+05			Row 98.5	OG → 3.8 90.0	14.5 54.0
+25			Row 98.0	OG → 4.3 92.5	13.7 82.9
+50			Row 100	OG 8.8 87.7	13.2 80.2
+75				OG → 13.4 89.0	11.1 85.0
60+00				OG → 12.9 64.2	5.8 50.5
B.M.			5.98	837.63 ✓	
+25		Zero borrow Lt.			
+50					
+75					
B.M.	8.7 ✓	846.43		837.71 ✓	
60+75					

Inst. G
 Rod. S
 Chain. F

11-20-24

63

Left	X	C L	Right
12.3	1.1	10.5	9.9 10.9 10.6
22.6	1.0	00	15.5 18.0 24.5

		X	(12.4)			
12.4	11.0	9.9	9.4	8.7	9.9	10.0
33.0	16.3	1.0	00	15.2	17.7	23.7

		X	(11.3)			
13.7	12.6	12.0	9.4	8.5	7.8	7.4
20.5	20.8	18.6	14.0	00	17.0	18.2

		X	(10.4)			
13.4	11.5	11.2	7.6	7.6	6.9	6.3
48.0	42.0	23.5	17.8	14.0	00	16.0

		X	(1.6)			
10.2	10.0	6.3	5.6	5.5	5.2	6.3
47.5	29.5	23.7	14.0	00	14.0	17.5

		X	(8.9)			
9.6	9.5	4.9	4.4	4.7	4.2	5.7
50.2	34.5	26.0	14.0	00	14.0	17.5

		X	(8.0)			
8.8	8.7	5.4	3.8	3.7	3.4	5.7
49.8	36.0	31.2	14.0	00	14.5	18.5

		X	(7.1)			
8.6	7.5	3.9	3.1	2.8	2.5	4.8
46.8	32.6	27.8	14.0	00	15.0	19.0

		X	(6.1)			
6.4	4.5	2.7	2.4	1.8	1.4	3.8
42.7	25.5	17.8	14.0	00	15.0	18.5

		X	(9.5)			
8.6	8.3	7.1	0.5	1.1	0.6	2.6
21.0	16.5	14.0	00	00	14.4	20.0

		X	(4.2)			
9.8	0.9	0.5	0.2	0.0	0.2	6.6
30.0	16.5	14.0	00	00	14.2	15.4

		X	(3.0)			
28.0						12.8
50.0						34.0

		X	(5.8)		
3.0	2.8		2.3	1.8	2.0
19.4	13.8		00	14.2	16

..... Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M. ✓	11.12	871.69 ✓		860.57	
67+75		Zero Borrow Rt.			
67+50					
67+00					
66+50					
+25					
66+00					
+50					
65					
+50					
64					
63+50					
T.P.	1.62	860.96 ↓	12.35	859.34 ↓	
63+00		Zero borrow Rt.			
		<u>Const. on</u>			<u>page 68</u>

Inst. G
 Rod. S
 Chain. F

Comps: 11-20-24

64

Left

C L

Right

SW Cor. Copying Cattle pass 67 x 10

9.6

8.5	10.6	10.4	7.6	2.3
14.0	20.5	29.0	34.5	38.0

10.1	15.5	14.8	6.3	1.2
14.0	24.0	33.5	45.6	50.0

11.2	13.0	13.0	9.5	8.1	2.6
14.0	20.5	24.2	29.0	43.0	47.8

12.2

11.5	12.7	12.3	6.4	5.4	3.4
16.0	20.0	23.8	31.7	39.0	41.9

13.3

12.2	13.9	13.6	5.6
16.5	20.0	34.1	41.3

14.7

4.0	7.2
46.0	45.5

16.4

11.1	4.5
43.5	45.8

18.1

11.0	3.8
48.0	49.0

19.5

14.3	6.6
45.5	47.8

21.5

12.4
48.5

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M.	9.17	802.31 ✓		792.34	
T.P.	7.07	796.78	12.60	789.71 ✓	
B.M.			7.29	789.49 ✓	
T.P.	3.36	787.39 ✓	12.75	784.03 ✓	
52+60					
+75					
T.P.	12.54	799.81 ↓	0.12 ✓	787.27 ✓	
T.P.	7.29	805.66 ✓	1.44	798.37 ✓	
53					
+25					
+50					
T.P.	1.55	794.68 ↓	12.53	793.13 ↓	
+75					
54					
+25					
T.P.			8.39	786.29 ↓	
T.P.	8.43	801.96 ↓	1.15	793.53 ✓	
+55					
+90					

Inst. Galvin
Rod. Skooglund
Chain. Fritz

Conner

11-17-24

65

Left

C L

Right

Rock 50 ft Lt Sta 7+25

10.2
61.0

+22.9

1.1
55.0

+23.3

4.6
35.0

+5.9

0.6
33.0

+6.8

4.6
36.0

+7.7

10.0
60.0

+19.7

13.0
62.0

+20.6

6.9
61.3

+21.5

Tree 100 ft Lt Sta 5+50

2.0
44.3

+15.3

5.4
50.0

+16.4

Cross Sections

Sta. B. S. H. I. F. S. Grade Gr. R.

T.P. 1.72 801.96 790.79 12.89 789.07

55+00

T.P. 2.81 780.75 12.85 777.94

55+50

55+68

T.P.

0.12 780.63 *

T.P.

3.16

771.23

12.68

768.07

55+75

T.P.

12.65

793.28

780.63 *

55+80

T.P.

12.68

805.55

0.41

792.87

56+00

56+25

T.P.

11.44

816.81

0.18

805.37

T.P.

14.05

828.69

0.17

816.64

56+50

56+75

57+00

Inst. G
 Rod. S
 Chain. F

11-17-24

Left

C L

Right

4.0
 67.0

$\frac{4.0}{67.0}$

+28.2

$\frac{6.7}{92}$

+40.0

$\frac{0.0}{77}$

+40.7

13.8
 113.0

5.3
 96.0

+48.7

6.0
 70.0

+28.7

9.1
 64.0

+17.1

0.0
 47.0

+18.0

0.6 11.5 7.4 6.7
 75.0 47.0 25.0

4.2

0.8 8.1 6.1 6.0 5.8
 55.0 32.2 36.0 23.0

3.3

0.8 4.2 5.1 4.4
 56.0 49.0 24.0

2.3

Sta.	B.S.	Cross Sections			Gr. R.
		H. I.	F. S.	Grade	
57+25		828.69			
T.P.	0.18	816.24	12.63	816.06	
57+50					
57+75					
58+00					
T.P.	10.86	826.42	0.68	815.56	
58+30					
T.P.	12.68	837.99	1.11	825.31	
T.P.	9.47	844.76	2.70	835.29	
BM			7.08	837.68	837.71

Inst. G
Rod. S
Chain. F

11-17-24

67

Left

C

Right

OG → 6.7 24 2.0
38.0 30.0 21.4

(1.3)

OG → 2.6 00
47.0 43.0

(+12.1)

9.0
56.0

(+13.0)

4.7
50.0

(+13.9)

OG → 4.4
46.0

(+4.8)

Cont. from page 64

Sta.	B.S.	Cross Sections		Gr. R.
		H. I. ✓	F. S.	
63+50		860.96		
+75		Zero	borrow	Lt.
64				
+50				
65				
+50				
+75				
66				
+25				
+50				
67+00	Zero	borrow	Lt. ✓	
T.P.	5.99	866.47	0.48	860.48
B.M.			5.88	860.59 ✓
67+00				860.57

Inst. G
 Rod. S
 Chain. F

11-20-24

68

Left

G L

Right

10.8

10.1 11.7 11.5
 15.2 20.8 41.0

8.8

8.6 13.1 10.1 10.5 10.1 9.4 8.5 10.9 11.0
 40.2 34.7 29.0 17.2 15.1 15.3 21.2 34.3

7.4

11.4 9.1 10.6 10.3 7.6 6.8 10.0 9.9
 48.5 45.0 42.5 23.4 15.0 14.5 22.0 35.6

6.7

9.3 8.1 10.3 10.0 5.8 4.8 7.4 6.8
 47.5 44.5 41.5 22.4 14.0 15.4 19.7 34.5

4.0

5.7 4.7 8.4 8.2 4.4 3.0 5.4 5.3
 46.5 41.3 38.0 20.8 15.3 15.0 19.5 33.5

9.3 7.2 7.1 3.1
 45.4 41.2 20.2 14.0

2.1

4.6 6.9 6.4 2.6 2.8
 46.7 43.0 22.4 17.6 14.0

1.5

5.3 6.0 2.2 1.4
 45.0 23.0 17.2 14.0

6.7

7.9 5.0 4.8 1.0 0.9
 44.5 39.5 22.0 16.5 14.0

7.8 8.5 6.9 6.3
 39.3 33.0 30.0 25.7

ok.

5.1
 14.0

..... Cross Sections
Sta. B. S. H. I. F. S. Grade Gr. R.

Inst.

Rod.

Chain.

Left

C L

Right

Cross Sections

Sta.

B. S.

H. I.

F. S.

Grade

Gr. R.

Inst.
Rod.
Chain.

Left

C L

Right

..... Cross Sections.

Sta.

B. S.

H. I.

F. S.

Grade

Gr. R.

Inst.
Rod.
Chain.

Left

C L

Right

Cross Sections

Sta. B. S. H. I. F. S. Grade Gr. R.

Inst.
Rod
Chain.

Left

C L

Right

Cross Sections

Sta. B. S. H. I. F. S. Grade Gr. R.

Inst.
Rod.
Chain.

Left

C L

Right

Inst.
Rod.
Chain.

Left

C L

Right

Final Guard Rail

~~Cross~~ Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
105-110		LT		464	✓
105-110		RT		480	✓
110	117	RT		704	✓
110	117	LT		697	✓
118	120	LT		224	✓
123	127	LT		400	✓
123	127	RT		385	✓
134	133	LT		177	✓
136	137	LT		151	✓
142		LT		96	✓
barricade		142		32	✓
142		RT		135	✓
143		RT		176	✓
143		LT		159	✓
barricade				32	✓
153		RT		65	✓
153		LT		72	✓
barricade				32	✓
				4481	
				9258	
				13739	✓

Inst.
Rod.
Chain.

Holmes
Johnson

Comer

11-11-24

75

Left

C L

Right

Cont. from page 72

12

15

18
Cross

24
Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
142 Rt			30	30	
135 Rt	24				
135 Lt	24				
127+75 Rt			24		
117+50 R	24				
104 Lt	20				
96+20 Rt	24				
91+00 Lt	24				
87+80 Rt	24				
76+75 Lt	24				
70+25 Lt	24				
70+50 Rt			24		
67+90 Rt			12		
67+90 Lt	24				

Inst.
Rod.
Chain.

Left

C L

Right

Final Guard Raib

0+70	- 18+60	LT	1771	✓
✓	✓	RT	1790	✓
26	27	RT	72	✓
26	27	LT	140	✓
41	43	RT	104	✓
41	43	LT	64	✓
Hanson FE 45-48		LT	240	✓
Baracka 46			32	✓
48	49	RT	89	✓
55	57	RT	160	✓
60	63	RT	304	✓
46	68	LT	2165	✓
Baracka 68			32	✓
67	68	RT	104	✓
77	Baracka		32	✓
77	90	LT	289	✓
✓	✓	RT	280	✓
83+50	84+50	RT	97	✓
83	86	LT	240	✓
87	89	LT	216	✓
89	94	RT	345	✓
91+50	94+50	LT	296	✓
95+50	96+50	RT	49	✓
95	97	LT	169	✓
97+50	99+50	LT	178	✓
			<hr/>	
			9258	

Holmes
Johnson

Conner

11-11-24

(77)

~~cont on page 75~~

600
G.R.

5/9					8371.71	11.86
B.M.	12.54	850.25			8371.71	11.86
60+00				Zero class.	Mat. Ex =	12.7
	10.90	859.66	1.49		848.76	
59+75					836.50	23.2
59+50					835.60	24.1
T.P.	7.73	867.01	0.38		859.28	
59+05					834.00	33.0
T.P.	1.35	856.06	12.30		854.71	
T.P.	3.93	847.83	12.16		843.90	
59+75					836.5	11.3
59+50					835.6	12.2
59+25					834.70	13.1
B.M.			10.15		837.68	

Zero class. Mat. = sta 59+05

class. Mat.

Cornor
Galvin
Schoenlund

10/2/24.

78

Nail in tree 60+80 Pt.

10.0
0.0

2.2
30.5 (+5.5
30.5)

R.
25.0

R
137
15.0

10.6 R
7.6
35.7 (+10.7
35.7)

+89
38.3

30.0 R.

4.9 R
25.5

4.0 R
43.1 (+18.1
43.1)

+13.6
38.6

21.0 4.0 48 (+35.0
48.0)

7.5 R
25.0

66 R
30.0

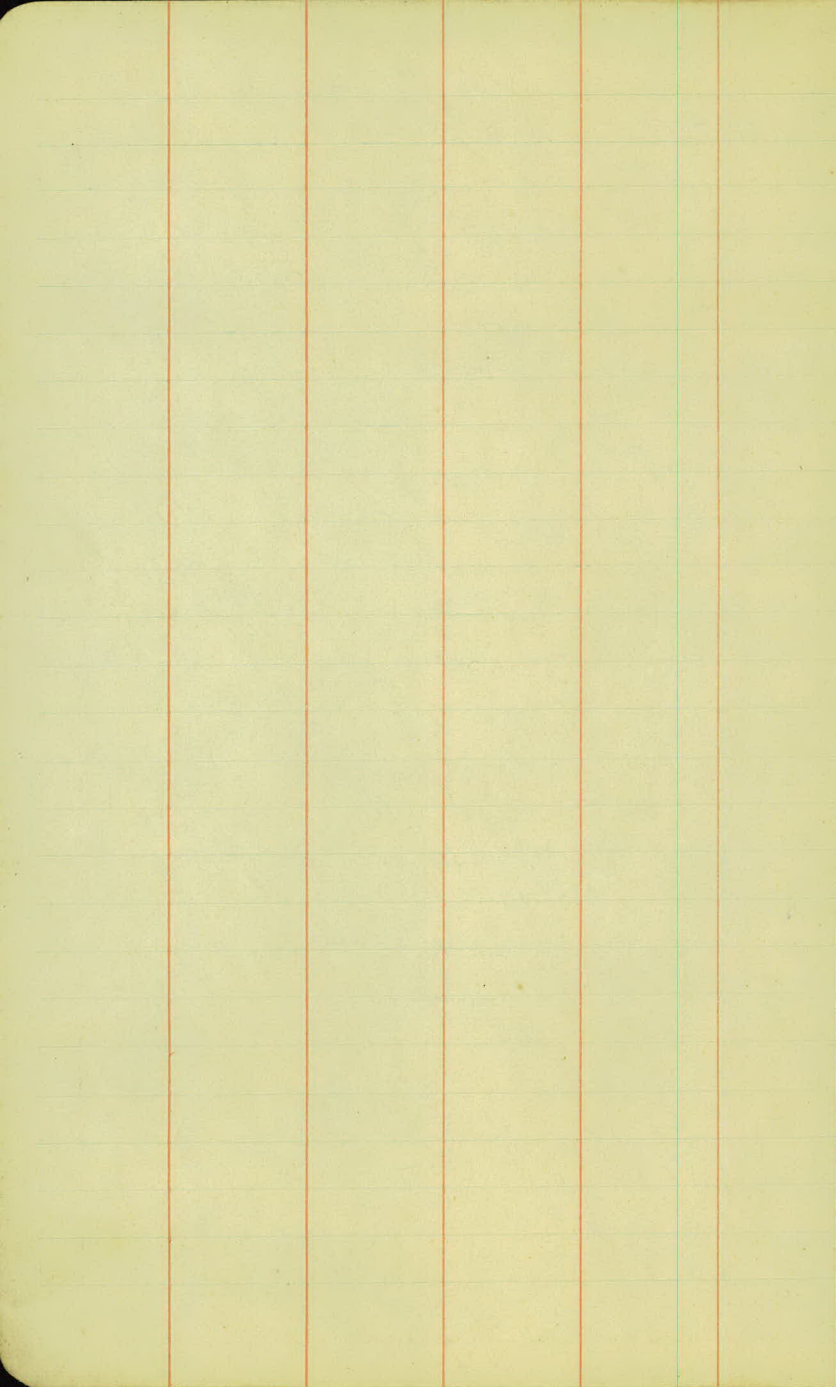
4.5 R
10.0

2.7 R
6.0

6.0 R
0.0
2.7 R
0.0

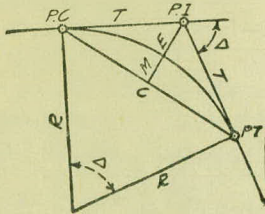
5.1 R
6.5

R indicated Rock



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

Radius= $R = \frac{50}{\sin. D/2}$ (1) Degree of Curve= D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos. \frac{\Delta}{2})$ (5) = $R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) = $R \div \cos. \frac{\Delta}{2} - R$ (8) = $R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin. \frac{\Delta}{2}$ (10) Δ = Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. - $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = def. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 91.27$ and from Table V correction = .10 or $E = 91.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

TABLE I.—MINUTES IN DECIMALS OF A DEGREE.

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

TABLE II.—INCHES IN DECIMALS OF A FOOT.

1-16	3-32	1/8	3-16	1/4	5-16	3/8	1/2	5/8	3/4	7/8
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III.—RADI, ORDINATES AND DEFLECTIONS.

Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot
0° 10'	34377.5	.036	.145	0.05'	7°	819.02	1.528	6.105	2.10'
20	17188.8	.073	.291	0.10	20'	781.84	1.600	6.395	2.20
30	11459.2	.109	.436	0.15	30	764.49	1.637	6.540	2.25
40	8594.42	.145	.582	0.20	40	747.89	1.673	6.685	2.30
50	6875.55	.182	.727	0.25					
1	5729.65	.218	.873	0.30	8	716.78	1.746	6.976	2.40
10	4911.15	.255	1.018	0.35	20	688.16	1.819	7.266	2.50
20	4297.28	.291	1.164	0.40	30	674.69	1.855	7.411	2.55
30	3819.83	.327	1.309	0.45	40	661.74	1.892	7.556	2.60
40	3437.87	.364	1.454	0.50	9	637.28	1.965	7.846	2.70
50	3125.36	.400	1.600	0.55	20	614.56	2.037	8.136	2.80
					30	603.80	2.074	8.281	2.85
2	2864.93	.436	1.745	0.60	40	593.42	2.110	8.426	2.90
10	2644.58	.473	1.891	0.65					
20	2455.70	.509	2.036	0.70	10	573.69	2.183	8.716	3.00
30	2292.01	.545	2.181	0.75	30	546.44	2.292	9.150	3.15
40	2148.79	.582	2.327	0.80	11	521.67	2.402	9.585	3.30
50	2022.41	.618	2.472	0.85	30	499.06	2.511	10.02	3.45
3	1910.08	.655	2.618	0.90	12	478.34	2.620	10.45	3.60
10	1809.57	.691	2.763	0.95	30	459.28	2.730	10.89	3.75
20	1719.12	.727	2.908	1.00	13	441.68	2.839	11.32	3.90
30	1637.28	.764	3.054	1.05	30	425.40	2.949	11.75	4.05
40	1562.88	.800	3.199	1.10	14	410.28	3.058	12.18	4.20
50	1494.95	.836	3.345	1.15	30	396.20	3.168	12.62	4.35
					15	383.07	3.277	13.05	4.50
4	1432.69	.873	3.490	1.20	30	370.78	3.387	13.49	4.65
10	1375.40	.909	3.635	1.25	16	359.27	3.496	13.92	4.80
20	1322.53	.945	3.718	1.30	30	348.45	3.606	14.35	4.95
30	1273.57	.982	3.926	1.35	17	338.27	3.716	14.78	5.10
40	1228.11	1.018	4.071	1.40	18	319.62	3.935	15.64	5.40
50	1185.78	1.055	4.217	1.45	19	302.94	4.155	16.51	5.70
5	1146.28	1.091	4.362	1.50	20	287.94	4.374	17.37	6.00
10	1109.33	1.127	4.507	1.55	21	274.37	4.594	18.22	6.30
20	1074.68	1.164	4.653	1.60	22	262.04	4.814	19.08	6.60
30	1042.14	1.200	4.798	1.65	23	250.79	5.035	19.94	6.90
40	1011.51	1.237	4.943	1.70	24	240.49	5.255	20.79	7.20
50	982.64	1.273	5.088	1.75					
6	955.37	1.309	5.234	1.80	25	231.01	5.476	21.64	7.50
10	929.57	1.346	5.379	1.85	26	222.27	5.697	22.50	7.80
20	905.13	1.382	5.524	1.90	27	214.18	5.918	23.35	8.10
30	881.95	1.418	5.669	1.95	28	206.68	6.139	24.19	8.40
40	859.92	1.455	5.814	2.00	29	199.70	6.360	25.04	8.70
					30	193.18	6.583	25.88	9.00

Note. Chord Deflection=2 times tangent deflection.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
1°	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
2	100.01	.87	12	602.21	31.56	22	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3	150.04	1.96	13	652.81	37.07	23	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4	200.08	3.49	14	703.51	43.03	24	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5	250.16	5.46	15	754.32	49.44	25	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6	300.28	7.86	16	805.25	56.31	26	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7	350.44	10.71	17	856.30	63.63	27	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8	400.66	13.99	18	907.49	71.42	28	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9	450.93	17.72	19	958.81	79.67	29	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10	501.28	21.89	20	1010.3	88.39	30	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

IV

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
31°	1589.0	216.3	41°	2142.2	387.4	51°	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
32	1643.0	230.9	42	2199.4	407.6	52	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
33	1697.2	246.1	43	2257.0	428.5	53	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
34	1751.7	261.8	44	2314.9	450.0	54	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
35	1806.6	278.1	45	2373.3	472.1	55	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.8	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
36	1861.7	294.9	46	2432.1	494.8	56	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
37	1917.1	312.2	47	2491.3	518.2	57	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
38	1972.9	330.2	48	2551.0	542.2	58	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
39	2029.0	348.6	49	2611.2	566.9	59	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
40	2085.4	367.7	50	2671.8	592.3	60	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
61°	3375.0	920.2	71°	4086.9	1308.2	81°	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
62	3442.7	954.8	72	4162.8	1352.6	82	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
63	3511.1	990.2	73	4239.7	1398.0	83	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
64	3580.3	1026.6	74	4317.6	1444.6	84	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
65	3650.2	1063.9	75	4396.5	1492.4	85	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
66	3720.9	1102.2	76	4476.5	1541.4	86	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
67	3792.4	1141.4	77	4557.6	1591.6	87	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
68	3864.7	1181.6	78	4639.8	1643.0	88	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
69	3937.9	1222.7	79	4723.2	1695.8	89	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
70	4011.9	1265.0	80	4807.7	1749.9	90	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.8	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
91°	5830.5	2444.9	101°	6950.6	3278.1	111°	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.1	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
92	5933.2	2518.5	102	7075.5	3374.9	112	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
93	6037.8	2594.0	103	7203.2	3474.4	113	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.6	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
94	6144.3	2671.6	104	7333.6	3576.8	114	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
95	6252.8	2751.3	105	7467.0	3682.3	115	8993.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.3
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
96	6363.4	2833.2	106	7603.5	3791.0	116	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
97	6476.2	2917.3	107	7743.2	3902.9	117	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
98	6591.2	3003.8	108	7886.2	4018.2	118	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
99	6708.6	3092.7	109	8032.7	4137.1	119	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	6808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
100	6828.3	3184.1	110	8182.8	4259.7	120	9924.0	5729.7
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

TABLE V.—CORRECTIONS FOR TANGENTS AND EXTERNALS.

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table IV) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

TABLE VI.—CORRECTIONS FOR SUB-CHORDS AND LONG CHORDS.

FOR SUB-CHORDS ADD										Excess of arc per 100 ft.	LONG CHORDS				
D	10	20	30	40	50	60	70	80	90		D	200	300	400	500
4°	.00	.00	.01	.01	.01	.01	.01	.01	.00	.02	1	199.99	299.97	399.92	499.85
6	.00	.01	.01	.02	.02	.02	.02	.01	.01	.05	2	199.97	299.88	399.70	499.39
8	.01	.02	.02	.03	.03	.03	.03	.02	.01	.08	3	199.93	299.73	399.32	498.63
10	.01	.02	.03	.04	.05	.05	.05	.04	.02	.13	4	199.88	299.51	398.78	497.57
12	.02	.04	.05	.06	.07	.07	.07	.05	.03	.18	5	199.81	299.24	398.10	496.20
14	.02	.05	.07	.08	.09	.10	.09	.07	.04	.25	6	199.73	298.90	397.26	494.53
16	.03	.06	.09	.11	.12	.12	.12	.09	.05	.33	7	199.63	298.51	396.28	492.57
18	.04	.08	.11	.14	.15	.16	.15	.12	.07	.41	8	199.51	298.05	395.14	490.31
20	.05	.10	.14	.17	.19	.20	.18	.15	.09	.51	9	199.38	297.54	393.86	487.75
22	.06	.12	.17	.21	.23	.24	.22	.18	.10	.62	10	199.24	296.96	392.42	484.90
24	.07	.14	.20	.25	.28	.28	.26	.21	.12	.74	12	198.90	295.63	389.12	478.34
26	.09	.17	.24	.29	.32	.33	.31	.25	.15	.86	14	198.51	294.06	385.22	470.65
28	.10	.19	.27	.34	.37	.38	.36	.29	.17	1.00	16	198.05	292.25	380.76	461.86
30	.11	.22	.31	.39	.43	.44	.41	.33	.19	1.15	18	197.54	290.21	375.74	452.02
32	.13	.25	.36	.44	.49	.50	.47	.38	.22	1.31	20	196.96	287.94	370.17	441.15
34	.15	.28	.40	.50	.55	.57	.53	.43	.25	1.48	22	196.32	285.44	364.06	429.30
36	.17	.32	.45	.56	.62	.64	.59	.48	.28	1.66	24	195.63	282.71	357.43	416.53
38	.18	.36	.51	.62	.70	.71	.66	.53	.31	1.86	26	194.87	279.76	350.30	402.89
40	.21	.40	.56	.69	.77	.79	.73	.59	.35	2.06	28	194.06	276.59	342.69	388.43
42	.23	.44	.62	.76	.85	.87	.81	.65	.38	2.28	30	193.18	273.20	334.61	373.20
44	.25	.48	.68	.84	.94	.96	.89	.72	.42	2.50	32	192.25	269.61	326.08	357.28
46	.27	.52	.75	.92	1.02	1.05	.98	.78	.46	2.74	34	191.26	265.81	317.12	340.73
48	.30	.57	.81	1.00	1.12	1.14	1.06	.86	.50	2.99	36	190.21	261.80	307.77	323.61
50	.32	.62	.89	1.09	1.21	1.24	1.15	.93	.55	3.24	38	189.10	257.60	298.03	305.99
52	.35	.67	.96	1.18	1.31	1.35	1.25	1.01	.59	3.52	40	187.94	253.21	287.94	287.94
54	.38	.73	1.04	1.28	1.42	1.46	1.35	1.09	.64	3.80	42	186.72	248.63	277.51	269.54
56	.41	.78	1.12	1.38	1.53	1.57	1.46	1.17	.69	4.09	44	185.44	243.87	266.78	250.85
58	.44	.84	1.20	1.48	1.65	1.69	1.57	1.26	.74	4.40	46	184.10	239.93	255.78	231.95
60	.47	.91	1.29	1.59	1.76	1.81	1.68	1.35	.80	4.72	48	182.71	233.83	244.51	212.92

NOTE.—When a chord of less than 100 ft. is used the corrections given in the above table should be added to the nominal length of chord to get the length which should be used in order that the 100 ft. points will check with those obtained by using the standard 100 ft. chord. Thus in locating a 14° curve by 25 ft. chords measure 25'.06 for each chord. Long chords are useful in passing obstacles.

TABLE VII.—MIDDLE ORDINATES FOR RAILS IN FEET.

Deg. of Curve	LENGTH OF RAILS							Deg. of Curve	LENGTH OF RAILS.						
	32	30	28	26	24	22	20		32	30	28	26	24	22	20
1°	.022	.020	.016	.013	.011	.009	.008	16°	.356	.313	.273	.236	.200	.170	.139
2	.045	.038	.034	.029	.025	.021	.017	17	.378	.333	.290	.252	.213	.180	.148
3	.037	.058	.051	.044	.037	.031	.026	18	.400	.351	.306	.265	.225	.190	.156
4	.089	.079	.069	.060	.050	.042	.035	19	.423	.371	.324	.280	.238	.201	.165
5	.112	.099	.086	.074	.063	.053	.044	20	.445	.392	.341	.296	.250	.212	.174
6	.134	.117	.102	.088	.076	.064	.052	21	.466	.410	.357	.309	.262	.222	.182
7	.156	.137	.120	.104	.088	.074	.061	22	.487	.430	.375	.325	.275	.233	.191
8	.179	.158	.137	.119	.100	.085	.070	23	.509	.450	.390	.338	.287	.243	.199
9	.201	.175	.153	.133	.112	.095	.078	24	.531	.469	.408	.354	.299	.253	.208
10	.223	.196	.171	.148	.125	.106	.087	25	.552	.486	.424	.367	.311	.263	.216
11	.245	.216	.188	.163	.139	.117	.096	26	.573	.506	.441	.382	.323	.274	.225
12	.268	.236	.206	.179	.151	.128	.105	27	.594	.524	.457	.396	.335	.284	.233
13	.290	.254	.222	.192	.163	.138	.113	28	.618	.545	.475	.411	.348	.294	.242
14	.312	.275	.239	.207	.175	.148	.122	29	.638	.564	.491	.424	.361	.303	.250
15	.334	.295	.257	.223	.188	.159	.131	30	.660	.583	.508	.438	.374	.313	.259

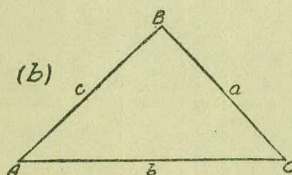
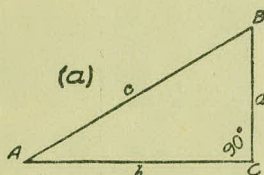
SLOPE REDUCTIONS.

When distances are measured on a slope they may be reduced to the equivalent horizontal distance by the following approximate rule:— subtract from the slope distance the square of the rise divided by twice the slope distance. Thus for a slope distance of 250.3 ft. and a rise of 15 ft. correction= $15^2 \div 2 \times 250.3 = .45$ (by slide rule) or horizontal distance= $250.3 - .45 = 249.85$. When vertical angle= $V. A.$ is measured horizontal distance= $\text{slope distance} - \text{slope distance} (1 - \text{Cos. } V. A.)$. Thus for slope distance of 248.7 ft. and $V. A.$ of $4^\circ 20'$ from Table VIII $\text{Cos.} = .99714$ and correction= $1 - .99714 = .00286$ per foot or total of $.286 \times 2\frac{1}{2}$ (near enough) = .57 and horizontal distance= $248.7 - .57 = 248.13$ ft.

See fig. (a).

TRIGONOMETRICAL FORMULAS.

$$\begin{aligned} \sin. & A = \frac{a}{c} \\ \cos. & A = \frac{b}{c} \\ \tan. & A = \frac{a}{b} \\ \cot. & A = \frac{b}{a} \\ \sec. & A = \frac{c}{b} \\ \text{cosec.} & A = \frac{c}{a} \end{aligned}$$



FORMULA FOR SOLVING TRIANGLES.

Given	Sought.	Right triangles. See fig. (a).
a, c	A, B, b	$\sin. A = \frac{a}{c}, \cos. B = \frac{a}{c}, b = \sqrt{(c+a)(c-a)}$
a, b	A, B, c	$\tan. A = \frac{a}{b}, \cot. B = \frac{a}{b}, c = \sqrt{a^2 + b^2}$
A, a	B, b, c	$B = 90^\circ - A, b = a \cot. A, c = \frac{a}{\sin. A}$
A, b	B, a, c	$B = 90^\circ - A, a = b \tan. A, c = \frac{b}{\cos. A}$
A, c	B, a, b	$B = 90^\circ - A, a = c \sin. A, b = c \cos. A$
Given	Sought.	Oblique triangles. See fig. (b).
A, B, a	b	$b = \frac{a \sin. B}{\sin. A}$
A, a, b	B	$\sin. B = \frac{b \sin. A}{a}$
a, b, C	$A - B$	$\tan. \frac{1}{2}(A - B) = \frac{(a - b) \tan. \frac{1}{2}(A + B)}{a + b}$
a, b, c	A	$\left\{ \begin{aligned} \text{If } s = \frac{1}{2}(a + b + c), \sin. \frac{1}{2} A &= \sqrt{\frac{(s - b)(s - c)}{bc}} \\ \cos. \frac{1}{2} A &= \sqrt{\frac{s(s - a)}{bc}}, \tan. \frac{1}{2} A = \sqrt{\frac{(s - b)(s - c)}{s(s - a)}}, \\ \sin. A &= \frac{2 \sqrt{s(s - a)(s - b)(s - c)}}{bc} \end{aligned} \right.$
A, B, C, a	area	$\text{area} = \frac{a^2 \sin. B \sin. C}{2 \sin. A}$
A, b, c	area	$\text{area} = \frac{1}{2} b c \sin. A$
a, b, c	area	$s = \frac{1}{2}(a + b + c), \text{area} = \sqrt{s(s - a)(s - b)(s - c)}$

TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.		Angle	Sine.	Tan.	Cotg.	Cosin.	
0	0	0	∞	1	90	0	0	∞	1	90	
10	.0029	.0029	343.8	1	50	8	.1392	.1405	7.115	.99027	82
20	.0058	.0058	171.9	.99998	40	10	.1421	.1435	6.968	.98986	50
30	.0087	.0087	114.6	.99996	30	20	.1449	.1465	6.827	.98944	40
40	.0116	.0116	85.94	.99993	20	30	.1478	.1495	6.691	.98902	30
50	.0145	.0145	68.75	.99989	10	40	.1507	.1524	6.561	.98858	20
						50	.1536	.1554	6.435	.98814	10
1	.0175	.0175	57.29	.99985	89	9	.1564	.1584	6.314	.98769	81
10	.0204	.0204	49.10	.99979	50	10	.1593	.1614	6.197	.98723	50
20	.0233	.0233	42.96	.99973	40	20	.1622	.1644	6.084	.98676	40
30	.0262	.0262	38.19	.99966	30	30	.1650	.1673	5.976	.98629	30
40	.0291	.0291	34.37	.99958	20	40	.1679	.1703	5.871	.98580	20
50	.0320	.0320	31.24	.99949	10	50	.1708	.1733	5.769	.98531	10
2	.0349	.0349	28.64	.99939	88	10	.1736	.1763	5.671	.98481	80
10	.0378	.0378	26.43	.99929	50	10	.1765	.1793	5.576	.98430	50
20	.0407	.0407	24.54	.99917	40	20	.1794	.1823	5.485	.98378	40
30	.0436	.0437	22.90	.99905	30	30	.1822	.1853	5.396	.98325	30
40	.0465	.0466	21.47	.99892	20	40	.1851	.1883	5.309	.98272	20
50	.0494	.0495	20.21	.99878	10	50	.1880	.1914	5.226	.98218	10
3	.0523	.0524	19.08	.99863	87	11	.1908	.1944	5.145	.98163	79
10	.0552	.0553	18.07	.99847	50	10	.1937	.1974	5.066	.98107	50
20	.0581	.0582	17.17	.99831	40	20	.1965	.2004	4.989	.98050	40
30	.0610	.0612	16.35	.99813	30	30	.1994	.2035	4.915	.97992	30
40	.0640	.0641	15.60	.99795	20	40	.2022	.2065	4.843	.97934	20
50	.0669	.0670	14.92	.99776	10	50	.2051	.2095	4.773	.97875	10
4	.0698	.0699	14.30	.99756	86	12	.2079	.2126	4.705	.97815	78
10	.0727	.0729	13.73	.99736	50	10	.2108	.2156	4.638	.97754	50
20	.0756	.0758	13.20	.99714	40	20	.2136	.2186	4.574	.97692	40
30	.0785	.0787	12.71	.99692	30	30	.2164	.2217	4.511	.97630	30
40	.0814	.0816	12.25	.99668	20	40	.2193	.2247	4.449	.97566	20
50	.0843	.0846	11.83	.99644	10	50	.2221	.2278	4.390	.97502	10
5	.0872	.0875	11.43	.99619	85	13	.2250	.2309	4.331	.97437	77
10	.0901	.0904	11.06	.99594	50	10	.2278	.2339	4.275	.97371	50
20	.0929	.0934	10.71	.99567	40	20	.2306	.2370	4.219	.97304	40
30	.0958	.0963	10.39	.99540	30	30	.2334	.2401	4.165	.97237	30
40	.0987	.0992	10.08	.99511	20	40	.2362	.2432	4.113	.97169	20
50	.1016	.1022	9.788	.99482	10	50	.2391	.2462	4.061	.97100	10
6	.1045	.1051	9.514	.99452	84	14	.2419	.2493	4.011	.97030	76
10	.1074	.1080	9.255	.99421	50	10	.2447	.2524	3.962	.96959	50
20	.1103	.1110	9.010	.99390	40	20	.2476	.2555	3.914	.96887	40
30	.1132	.1139	8.777	.99357	30	30	.2504	.2586	3.867	.96815	30
40	.1161	.1169	8.556	.99324	20	40	.2532	.2617	3.821	.96742	20
50	.1190	.1198	8.345	.99290	10	50	.2560	.2648	3.776	.96667	10
7	.1219	.1228	8.144	.99255	83	15	.2588	.2679	3.732	.96593	75
10	.1248	.1257	7.953	.99219	50	10	.2616	.2711	3.689	.96517	50
20	.1276	.1287	7.770	.99182	40	20	.2644	.2742	3.647	.96440	40
30	.1305	.1317	7.596	.99144	30	30	.2672	.2773	3.606	.96363	30
40	.1334	.1346	7.429	.99106	20	40	.2700	.2805	3.566	.96285	20
50	.1363	.1376	7.269	.99067	10	50	.2728	.2836	3.526	.96206	10
					82						74
	Cosin.	Cotg.	Tan.	Sine.	Angle.		Cosin.	Cotg.	Tan.	Sine.	Angle.

TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.	Angle	Sine.	Tan.	Cotg.	Cosin.		
°					°						
16	.2756	.2867	3.487	.96126	74	.4067	.4452	2.246	.91355		
10	.2784	.2899	3.450	.96046	50	10 .4094	.4487	2.229	.91236		
20	.2812	.2931	3.412	.95964	40	20 .4120	.4522	2.211	.91116		
30	.2840	.2962	3.376	.95882	30	30 .4147	.4557	2.194	.90996		
40	.2868	.2994	3.340	.95799	20	40 .4173	.4592	2.177	.90875		
50	.2896	.3026	3.305	.95715	10	50 .4200	.4628	2.161	.90753		
17	.2924	.3057	3.271	.95615	73	25 .4228	.4663	2.145	.90631		
10	.2952	.3089	3.237	.95545	50	10 .4253	.4699	2.128	.90507		
20	.2979	.3121	3.204	.95459	40	20 .4279	.4734	2.112	.90383		
30	.3007	.3153	3.172	.95372	30	30 .4305	.4770	2.097	.90259		
40	.3035	.3185	3.140	.95284	20	40 .4331	.4806	2.081	.90133		
50	.3062	.3217	3.108	.95195	10	50 .4358	.4841	2.066	.90007		
18	.3090	.3249	3.078	.95106	72	26 .4384	.4877	2.050	.89879		
10	.3118	.3281	3.048	.95015	50	10 .4410	.4913	2.035	.89752		
20	.3145	.3314	3.018	.94924	40	20 .4436	.4950	2.020	.89623		
30	.3173	.3346	2.989	.94832	30	30 .4462	.4986	2.006	.89493		
40	.3201	.3378	2.960	.94740	20	40 .4488	.5022	1.991	.89363		
50	.3228	.3411	2.932	.94646	10	50 .4514	.5059	1.977	.89232		
19	.3256	.3443	2.904	.94552	71	27 .4540	.5095	1.963	.89101		
10	.3283	.3476	2.877	.94457	50	10 .4566	.5132	1.949	.88968		
20	.3311	.3508	2.850	.94361	40	20 .4592	.5169	1.935	.88835		
30	.3338	.3541	2.824	.94264	30	30 .4617	.5206	1.921	.88701		
40	.3365	.3574	2.798	.94167	20	40 .4643	.5243	1.907	.88566		
50	.3393	.3607	2.773	.94068	10	50 .4669	.5280	1.894	.88431		
20	.3420	.3640	2.747	.93969	70	28 .4695	.5317	1.881	.88295		
10	.3448	.3673	2.723	.93869	50	10 .4720	.5354	1.868	.88158		
20	.3475	.3706	2.669	.93769	40	20 .4746	.5392	1.855	.88020		
30	.3502	.3739	2.675	.93667	30	30 .4772	.5430	1.842	.87882		
40	.3529	.3772	2.651	.93565	20	40 .4797	.5467	1.829	.87743		
50	.3557	.3805	2.628	.93462	10	50 .4823	.5505	1.816	.87603		
21	.3584	.3839	2.605	.93358	69	29 .4848	.5543	1.804	.87462		
10	.3611	.3872	2.583	.93253	50	10 .4874	.5581	1.792	.87321		
20	.3638	.3906	2.560	.93148	40	20 .4899	.5619	1.780	.87178		
30	.3665	.3939	2.539	.93042	30	30 .4924	.5658	1.767	.87036		
40	.3692	.3973	2.517	.92935	20	40 .4950	.5696	1.756	.86892		
50	.3719	.4006	2.496	.92827	10	50 .4975	.5735	1.744	.86748		
22	.3746	.4040	2.475	.92718	68	30 .5000	.5774	1.732	.86603		
10	.3773	.4074	2.455	.92609	50	10 .5025	.5812	1.720	.86457		
20	.3800	.4108	2.434	.92499	40	20 .5050	.5851	1.709	.86310		
30	.3827	.4142	2.414	.92388	30	30 .5075	.5890	1.698	.86163		
40	.3854	.4176	2.394	.92276	20	40 .5100	.5930	1.686	.86015		
50	.3881	.4210	2.375	.92164	10	50 .5125	.5969	1.675	.85866		
23	.3907	.4245	2.356	.92050	67	31 .5150	.6009	1.664	.85717		
10	.3934	.4279	2.337	.91936	50	10 .5175	.6048	1.653	.85567		
20	.3961	.4314	2.318	.91822	40	20 .5200	.6088	1.643	.85416		
30	.3987	.4348	2.300	.91706	30	30 .5225	.6128	1.632	.85264		
40	.4014	.4383	2.282	.91590	20	40 .5250	.6168	1.621	.85112		
50	.4041	.4417	2.264	.91472	10	50 .5275	.6208	1.611	.84959		
				66					58		
	Cosin.	Cotg.	Tan.	Sine.	Angle.		Cosin.	Cotg.	Tan.	Sine.	Angle.

TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.		Angle	Sine.	Tan.	Cotg.	Cosin.	
°						°					
32	.5299	.6249	1.600	.84805	58	30	.6225	.7954	1.257	.78261	30
10	.5324	.6289	1.590	.84650	50	40	.6248	.8002	1.250	.78079	20
20	.5348	.6330	1.580	.84495	40	50	.6271	.8050	1.242	.77897	10
30	.5373	.6371	1.570	.84339	30						
40	.5398	.6412	1.560	.84182	20	39	.6293	.8098	1.235	.77715	51
50	.5422	.6453	1.550	.84025	10	10	.6316	.8146	1.228	.77531	50
						20	.6338	.8195	1.220	.77347	40
33	.5446	.6494	1.540	.83867	57	30	.6361	.8243	1.213	.77162	30
10	.5471	.6536	1.530	.83708	50	40	.6383	.8292	1.206	.76977	20
20	.5495	.6577	1.520	.83549	40	50	.6406	.8342	1.199	.76791	10
30	.5519	.6619	1.511	.83389	30						
40	.5544	.6661	1.501	.83228	20	40	.6428	.8391	1.192	.76604	50
50	.5568	.6703	1.492	.83066	10	10	.6450	.8441	1.185	.76417	50
						20	.6472	.8491	1.178	.76229	40
34	.5592	.6745	1.483	.82904	56	30	.6494	.8541	1.171	.76041	30
10	.5616	.6787	1.473	.82741	50	40	.6517	.8591	1.164	.75851	20
20	.5640	.6830	1.464	.82577	40	50	.6539	.8642	1.157	.75661	10
30	.5664	.6873	1.455	.82413	30						
40	.5688	.6916	1.446	.82248	20	41	.6561	.8693	1.150	.75471	49
50	.5712	.6959	1.437	.82082	10	10	.6583	.8744	1.144	.75280	50
						20	.6604	.8796	1.137	.75088	40
35	.5736	.7002	1.428	.81915	55	30	.6626	.8847	1.130	.74896	30
10	.5760	.7046	1.419	.81748	50	40	.6648	.8899	1.124	.74703	20
20	.5783	.7089	1.411	.81580	40	50	.6670	.8952	1.117	.74509	10
30	.5807	.7133	1.402	.81412	30						
40	.5831	.7177	1.393	.81242	20	42	.6691	.9004	1.111	.74314	48
50	.5854	.7221	1.385	.81072	10	10	.6713	.9057	1.104	.74120	50
						20	.6734	.9110	1.098	.73924	40
36	.5878	.7265	1.376	.80902	54	30	.6756	.9163	1.091	.73728	30
10	.5901	.7310	1.368	.80730	50	40	.6777	.9217	1.085	.73531	20
20	.5925	.7355	1.360	.80558	40	50	.6799	.9271	1.079	.73333	10
30	.5948	.7400	1.351	.80386	30						
40	.5972	.7445	1.343	.80212	20	43	.6820	.9325	1.072	.73135	47
50	.5995	.7490	1.335	.80038	10	10	.6841	.9380	1.066	.72937	50
						20	.6862	.9435	1.060	.72737	40
37	.6018	.7536	1.327	.79864	53	30	.6884	.9490	1.054	.72537	30
10	.6041	.7581	1.319	.79688	50	40	.6905	.9545	1.048	.72337	20
20	.6065	.7627	1.311	.79512	40	50	.6926	.9601	1.042	.72136	10
30	.6088	.7673	1.303	.79335	30						
40	.6111	.7720	1.295	.79158	20	44	.6947	.9657	1.036	.71934	46
50	.6134	.7766	1.288	.78980	10	10	.6967	.9713	1.030	.71732	50
						20	.6988	.9770	1.024	.71529	40
38	.6157	.7813	1.280	.78801	52	30	.7009	.9827	1.018	.71325	30
10	.6180	.7860	1.272	.78622	50	40	.7030	.9884	1.012	.71121	20
20	.6202	.7907	1.265	.78442	40	50	.7050	.9942	1.006	.70916	10
							.7071	1.	1.	.70711	45
											°
	Cosin.	Cotg.	Tan.	Sine.	Angle.		Cosin.	Cotg.	Tan.	Sine.	Angle.

TABLE IX.—CALCULATION OF EARTHWORK.

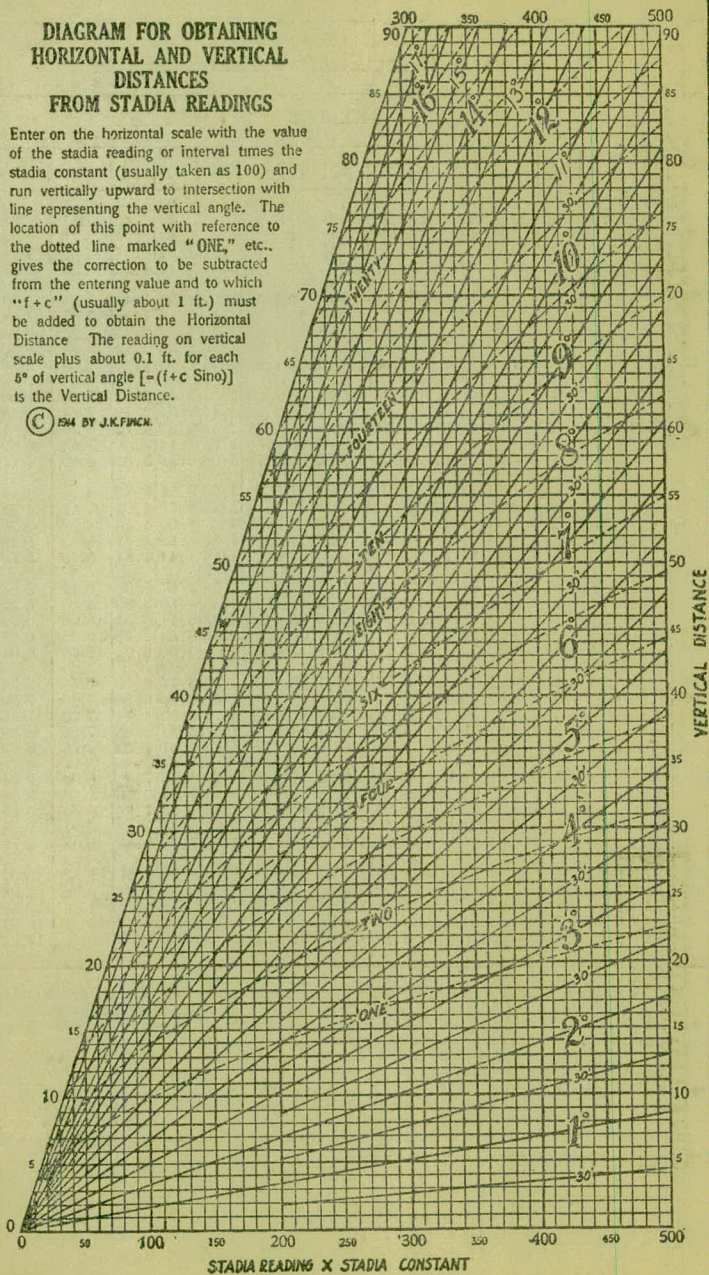
Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

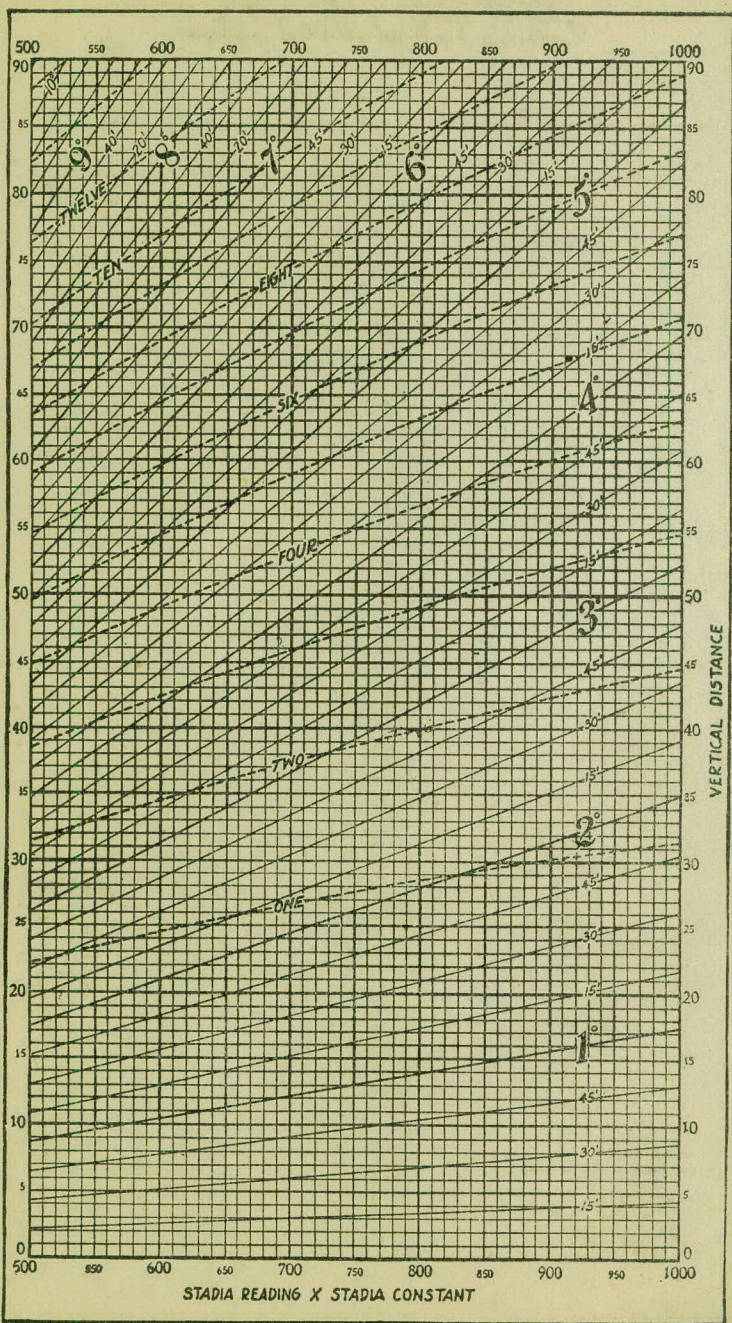
Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w=16.2$ and $h=5.3$, cu. yds. $=1.48+.028+.089=1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) $=h$, and $\frac{1}{2}$ the roadbed $=v$, add the triangles formed by taking the distance out to each break in turn ($=w$'s) by the difference between the cuts (or fills) on each side of it ($=h$'s) always subtracting the outer from the inner.

DIAGRAM FOR OBTAINING HORIZONTAL AND VERTICAL DISTANCES FROM STADIA READINGS

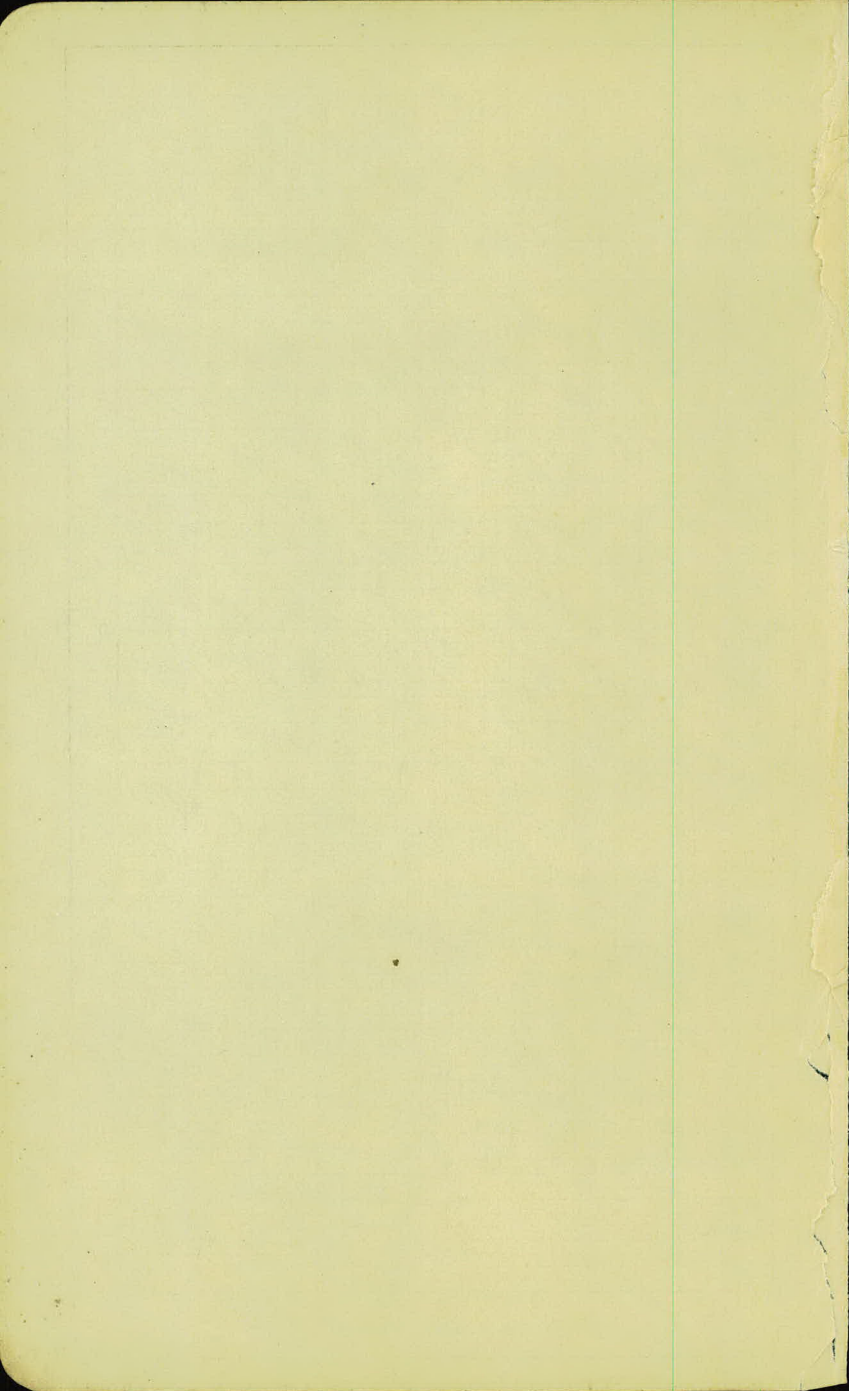
Enter on the horizontal scale with the value of the stadia reading or interval times the stadia constant (usually taken as 100) and run vertically upward to intersection with line representing the vertical angle. The location of this point with reference to the dotted line marked "ONE," etc., gives the correction to be subtracted from the entering value and to which "f+c" (usually about 1 ft.) must be added to obtain the Horizontal Distance. The reading on vertical scale plus about 0.1 ft. for each 5° of vertical angle [$=(f+c) \text{ Sino}$] is the Vertical Distance.

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STADIA READING X STADIA CONSTANT



795.74

12.87 +

.18

808.61 π

0.23 -

808.38 π

12.32 +

820.70 π

0.25

820.35 π

9.20

829.55

5.04

824.51

3.8

Sta 96 - 18" - 72" cm

Camp. 2 - 12" cm 12"
1 - 15" cm 12"

6.5 + 50 1 - 18" - cm 12"

Stewart

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

77.6
15.7
5.8

Roadway 16 feet wide. Side Slopes 1 on 1 1/2.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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