FINAL SURVEY

BIRCH LAKE RD.

From Centerville Road

To Bald Eagle Ave.

CO. PROJ. Nº 23-56

R.D. % Nº 29

FILE Nº 2

12-14-23

"12"

FINAL CHAINAGE & ALIGNMENT NOTES

Sta 0+00 – 112+18.6 (21 sheets)

PROJECT #2356

A. Deutsche
Hd Ch. Schiosser
Rr. " Mahoney } Party -
Rodman Franke

(23-56) FINAL CHAINAGE

Deutsche
Johnson
Mahoney
Franke
} Jr.

EQUATION 3+11.23 = 2+00.4 P.T.

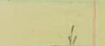
(Shown on Profile as 89°48')

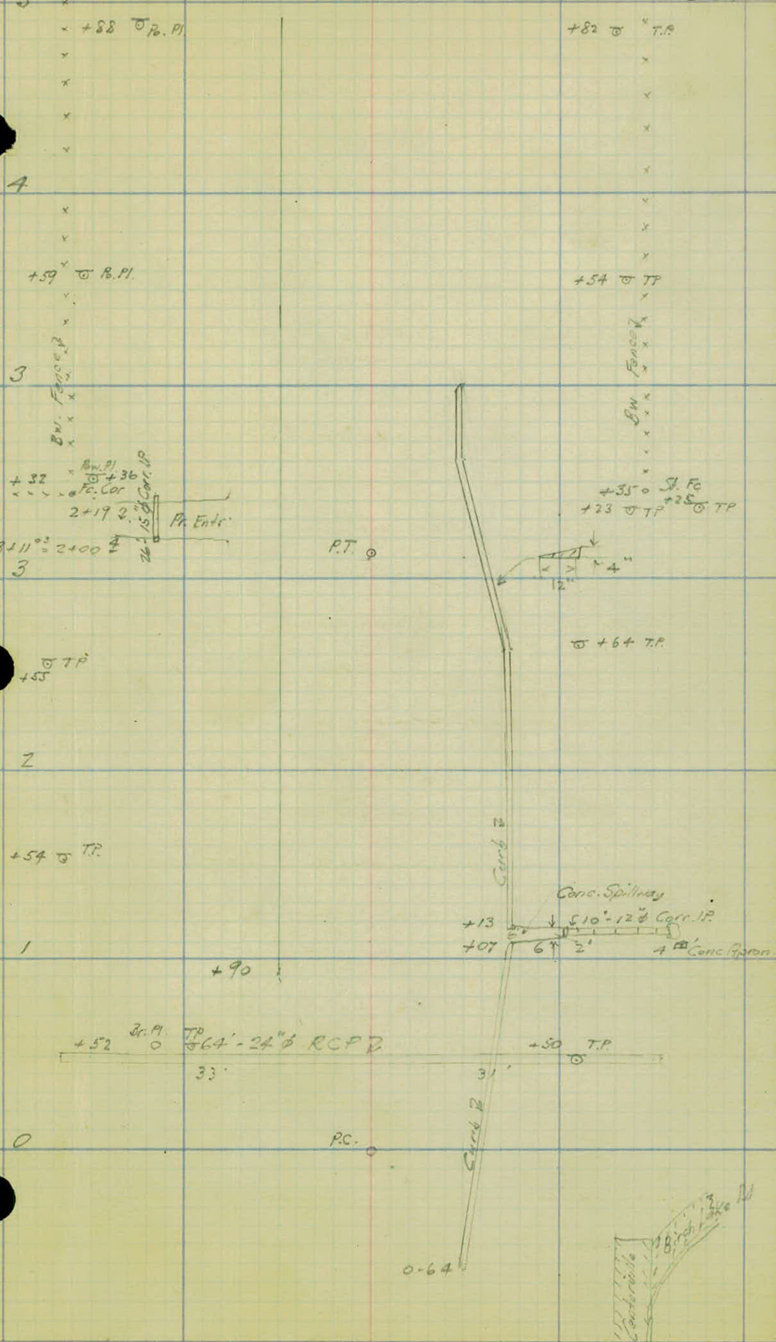
Note:- Evidently interior ∠ instead of Δ was originally measured.

Δ = 90°-12'
T = 200.4
D = 29°00' R
L = 3+11.23

P.I. = Mont Es & Rds extd'd

0+00 P.C. Beginning Project (23-56)

0-64 End Conc Curb Et. Sec. 


5
Lt
℄
Rt.
+88 Po. Pl.
+82 T.P.
4
+59 Po. Pl.
+54 TP
Bw. Fence
3
Bw. Fence
+32
Bw. Pl. +36
Fc. Cor
15" Corr. P.
2+19 2
Pr. Entr.
+35 St. Fc
+23 TP
+25 TP
3+11.03 = 2+00
P.T.
4"
12"
3
+64 T.P.
+55 TP
2
Curb
+54 T.P.
Conc. Spillway
+13
10'-12" Corr. P.
+07
6
2'
4 Conc. Apron
1
+90
+52 Br. Pl.
TP 64'-24" RCP
+50 T.P.
33'
31'
0
P.C.
Curb
0-64
Centerline
Birch Lake Rd

12-12-23 Cold Air

12

11

10

9

8

7

6

5

+15 ⊙ P.P.

+45 ⊙ T.P.

+89 ⊙ P.P.

+13 ⊙ T.P.

+62 ⊙ P.P.

+77 ⊙ T.P.

+77 ⊙ T.P.

+36 ⊙ P.P.

Sw. Fr.

Sw. Fr.

+09 ⊙ P.P.

+12 ⊙ T.P.

23-56 19 Lt. ℄ Rt. 12-11-23 Colol Pair

+96 ⊙ T.P

+87 ⊙ P.o.P.I

18

+87 ⊙ T.P

+53 ⊙ P.o.P.

17

+57 ⊙ T.P

+23 ⊙ P.o.P.I

16

24"-18"-6" Conc. I.P.

+53 P. Entr.

+120'

C.I. & Evergreens

+32 ⊙ T.P

15

+89 ⊙ P.o.P.

+76

+17 Fe Cor

+64 ⊙ T.P

14

+15 Fe Cor

13

Boulders

+64 ⊙ T.P

+51

48"-24"ϕ R.C.P.

23' 25'

+37 ⊙ P.o.P.I

12

$\Delta = 28°30'$
$D = 5°00$ R
$T = 291 \pm$
$L = 570°$

$20+47\frac{1}{2}$ P.C.
5 70
$4+17\frac{1}{2}$

26

25

24 T.P. +04

23

+04 P. Entr.

22

+31 P.C. P.I.

21

+50 T.P.

P.C.

+11 P.C. P.I.

+18 T.P.

20

+79

19

$\Delta = 40^{\circ}-40'$
$D = 17^{\circ}-00'\ L$
$T = 125.4$
$L = 239.2$

EQUATION – $30+72.6 = 30+71.4 = P.C.$

$26+17.4 = P.T.$

23-56 33 Lt ℄ Rt 12-11-23 Cold Fair 6

2'⌀ Conc Apron 10'-12" Corr IP 2' +64 End Curb
+61 ℄ Conc Spillway
+58 End Curb
< 67
+48 ⊙ T.P.

Note
Not installed by contractor
24'-12" V.I.P.

32
+90 Pr. Entr
+80 Mail Box
+64 ⊙ R.R.
Cobble stone to retain
+50 16" Oak
+20 TP.
+17 4" Oak

31
+88 Pr. Entr
26'-15"⌀ Corr. I.P.
EQ = 30+72^6 = 30+71^4
P.C. ⊙
+52 ⊙ Po Pl
4" 12"
Curb 3
+24 24" Oak

30
+00 12" Oak
+86 ⊙ TP
18'-15"⌀ Corr. I.P.
+48 10" Oak
Farm Ent. +39
+34 Farm Entr
+26 ⊙ Po Pl
18'-15"⌀ Corr. I.P.

29
+62 ⊙ Po Pl
+68 12" Oak

28
+02 ⊙ Po Pl
+91 ⊙ Br Pl
Haul Borrow Pit
Old Road
For Shldr Matl.

27
10' 2'
+97 ℄ Spillway - Conc
+94 End Curb
Curb 3
12" 4"
P.T. ⊙

26

38+34.2 P.T.

$\Delta = 35^\circ 26'$
$D = 12^\circ 00$ L
$T = 152.8$
$L = 295.3$

35+38.9 P.C.

33+10.3 P.T.

12" Birch

Farm Entr · +81

+67 ⊙ T.P.

+49 End Curb

39

+12 ⊙ Po Pl

P.T. ⊙ +36 ⊙ T.P.

38

6'-12" Conc P.

2 ⊕ Conc Apron

+69⁵ = End Curb

5'

+67 ℄ Conc Spillw.

+64⁵ = End Curb

2' 6'

+24 ⊙ TP

+23 ⊙

+13 ⊙ 10" Birch

37

+93 ⊙ 10" Broh

+64 ⊙ Po Pl

+70 ⊙ 8" Oak

+64 ⊙ 12" Poplar

+52 ⊙ 8" Oak

+24 ⊙ TP

+16 ⊙ 8" Oak

36

4' 12"

P.C. ⊙

+34 ⊙ Po Pl

35

⊙ TP

+97 End Curb

48'-24" ⌀ RCP ℄

34+03

< 28' +97 End Curb ✕ 20' >

+63 ⊙ T.P.

P.T. ⊙

33

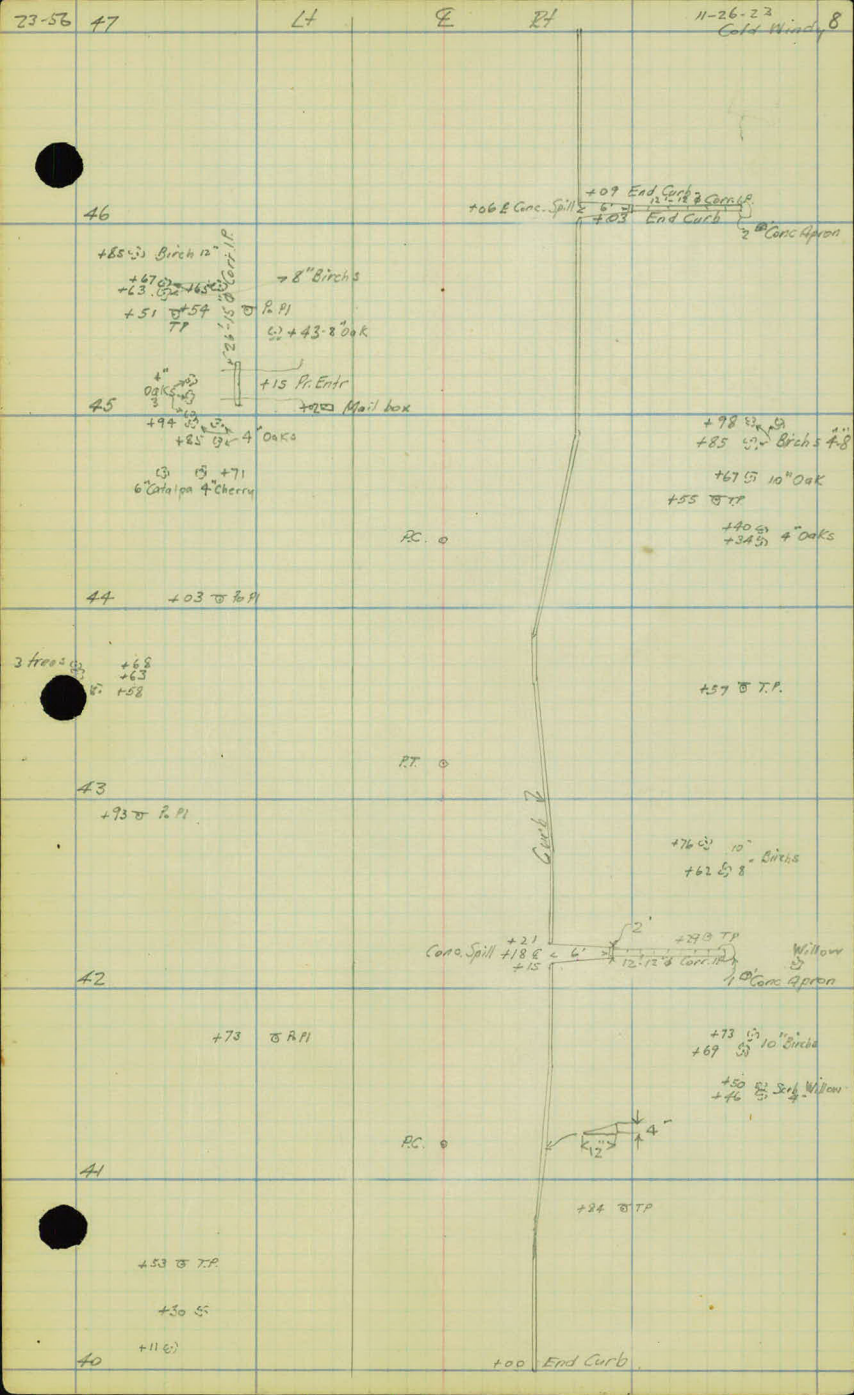
$\Delta = 99°37'$
$D = 29°00'$ R
$T = 236.5$
$L = 343.5$

$44+35.1$ P.C.

$43+19.4$ P.T.

$\Delta = 20°07'$
$D = 10°00'$ R
$T = 101.6$
$L = 201.2$

$41+18.2$ P.C.


73-56 47
Lt
℄
Rt
11-26-23
Cold Windy 8
46
+09 End Curb
+06 ℄ Conc. Spill
+03 End Curb
2 ℄ Conc Apron
+85 Birch 12"
+67
+63
+65
+51
+54
TP
8" Birch
P. Pl
+43 8" Oak
24'-15" Corr. I.P.
+15 Pr. Entr
+20 Mail box
45
4" Oak
+94
+85
4" Oaks
6" Catalpa 4" Cherry
+71
+98
+85 Birch 4-8
+67 10" Oak
+55 T.P.
+40
+34 4" Oaks
P.C.
44
+03 P. Pl
3 Trees
+68
+63
+58
+57 T.P.
P.T.
43
+93 P. Pl
Curb ℄
+76 10" Birch
+62 8"
+21
+18 ℄
+15
Conc. Spill
6'
12'-12" Corr.
+27 TP
2'
Willow
1/4 ℄ Conc Apron
42
+73 P. Pl
+73 10" Birch
+69
+50 Set 4" Willow
+46
P.C.
12"
4"
41
+24 TP
+53 T.P.
+30
+11
40
+00 End Curb

$\Delta = 14°08'$
$D = 5°00'L$
$T = 142.1$
$L = 282.7$

$53+32.8$ P.C.

$52+74.7$ P.T.

$\Delta = 37°20'$
$D = 20°00'L$
$T = 97.3$
$L = 186.7$

$50+88.0$ P.C.

$47+78.6 = 47+87.9$ EQUAT — P.T.

Cold Windy

+96 End Curb

P.C.

+22 14" Oak

+35 15" Oak

+22 6"
+15 4" } Oak
+02 4"

53

48"-24° RCP

24' 24'

P.T.

+76 4 Way Birch

+40 3 Birchs

4"
12"

52

Curb

+34

+32 BM Tree 12" Oak

51

P.C.

+57-18" Oak

+57 24" Oak

+37 End Curb
+34 E Cone Spillway

5'

+15 Pr. Entr

50 24" Oak +04

26'-15" Corr. I.P.

+78 4 Birchs

49

Cone Spillw +02 E

2'

16'-12" Corr. IRP

+99 End Curb

48

EQUAT. 47+78.6 = 47+87.2 P.T.

12"
4"

Curb

47

60+22.2 P.T.

Δ = 9°00'
D = 9°00 L
T = 50.10
L = 100.00

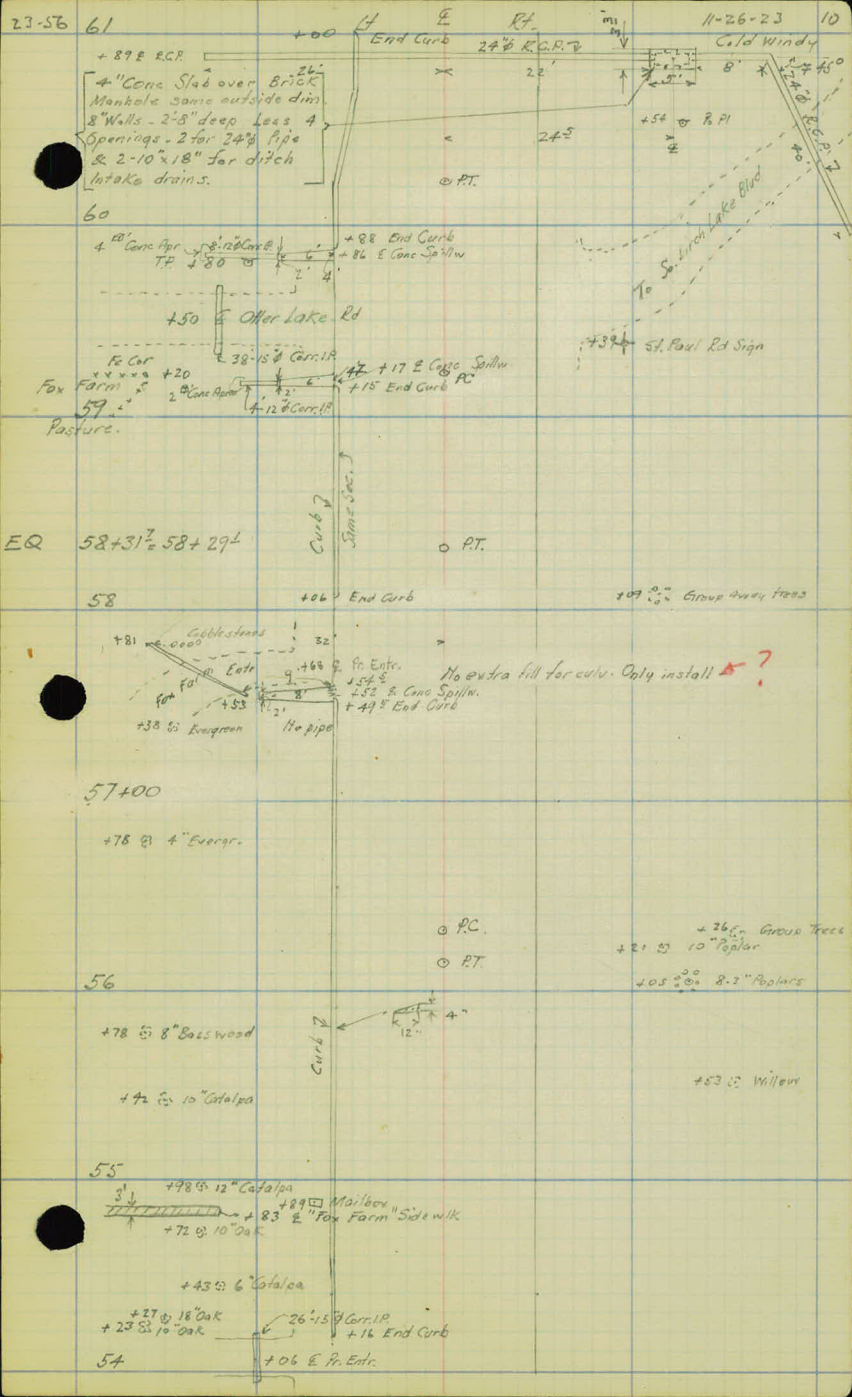
59+22.2 P.C.

EQUAT. 58+31.7 = 58+29.4 P.T.

Δ = 19°54 ✓
D = 10°00 L
T = 100.65
L = 199.0

56+32.7 P.C.

56+15.47 P.T.


+00 End Curb
24"ø R.C.P.
Cold Windy
+89 ℄ R.C.P.
4" Conc Slab over Brick Manhole same outside dim. 8" Walls - 2'-8" deep Less 4 Openings - 2 for 24" Pipe & 2-10"x18" for ditch intake drains.
24"
22'
8'
5'
+54 ℄ P. Pl
24"ø R.C.P.
P.T.
60
4 ea Conc Apr
T.P. +80
8'-12"ø Conc ℄
+88 End Curb
+86 ℄ Conc Spillw
Sycamore Lake Blvd
+50 ℄ Otter Lake Rd
+39 St. Paul Rd Sign
Fe Cor
+20
2 ea Conc Apron
38'-15"ø Corr. I.P.
+17 ℄ Conc Spillw
+15 End Curb
Fox Farm
59
Pasture.
EQ
58+31.7 = 58+29.4
Curb & Same Sec.
P.T.
58
+06 End Curb
+09 Group Young Trees
+81
Cobblestone
32'
Entr
+68 ℄ Fr. Entr.
+54 ℄
+52 ℄ Conc Spillw.
+49 ℄ End Curb
+53
+38 ℄ Evergreen
No pipe
No extra fill for culv. Only install ?
57+00
+78 ℄ 4" Everg.
P.C.
P.T.
+36 ℄ Group Trees
+21 ℄ 10" Poplar
+05 8-3" Poplars
56
+78 ℄ 8" Boxelwood
Curb &
4"
12"
+42 ℄ 10" Catalpa
+53 ℄ Willow
55
3'
+78 ℄ 12" Catalpa
+89 Mailbox
+83 ℄ "Fox Farm" Sidewlk
+72 ℄ 10" Oak
+43 ℄ 6" Catalpa
+27
+23 ℄ 18" Oak
10" Oak
26'-15"ø Corr. I.P.
+16 End Curb
54
+06 ℄ Fr. Entr.

64+43.5 = 64+44.4 EQUAT. P.T.

$\Delta = 8°26'$
$D = D = 7°00$ R
$T = 60.4$
$L = 120.5$

63+23.0 P.C.

Field Grain

Ploughed (N)

Ploughed

Field

67

66

26'-15" Corr. I.P.

+68 Farm Entr.

+45 End Curb

+38 (R) 20" Oak B.M.
+34 (L) 4"

65

EQUATION - 64+43.5 = 64+44.0 P.T.

64

4"

12"

Cond ?

P.C.

63

+58 Pr. Entr

28" Oak +44 (R) T.P.

26'-15" Corr. I.P.

Conc Spillw +56 (R)

+59 End Curb

6'

7'

2'

No pipe

+34 Pr. Entr

26'-15" Corr. I.P.

62

+91 (L) 14" Oak

61

75					11-21-23 Cold Cloudy	12
74						Corn Stubble
73						
72						
71						Ploughed Field in Grain
70						
69						Ploughed Field
68						

81+24.8 P.T.

$\Delta = 15°02'$
$D = 15°00'$ L
$T = 50.5$
$L = 100.2$

80+24.6 PC

23-56 | 82 | Lt | ℄ | Rt | 11-21-23 | 13

Cold Cloudy E.Gr.

+87

P.T.

81

+00 F.Fc

No Curbing

P.C.

80

Ploughed Field in Grain

Ploughed Field.

79

+45

78

77

Corn Stubble

76

75

85+33 P.T.

$\Delta = 14^\circ 56'$
$D = 15^\circ 00$ R
$T = 50^{\pm}$
$L = 99^{\pm}$

84+33$^{\pm}$ PC

89 | 4 | ℄ | Rt | 11-21-23 | 14

Cold Cloudy

88

Stubble

+50

87

Grain

Pasture

15" & 18" Tile Drain

86

End drain +91

Ditch +90 ℄

48'-30" ϕ R.C.P.

Ditch +82

55'

24'

24'

+51 Farm Entr

26'-15" ϕ Conc. I.P.

P.T.

85

No Curbing

P.C.

Pasture

84

Plowed Field in Grain

83

82

23-56 96 +00 ♂ P. Pl   Lt   ℄   Rt   11-21-23 Cold Cloudy 15

+51 ℄   40'-12"ɸ Corr. I.P. Ƶ

95

Pasture

+41 ♂ P. Pl
+31 ℄   38'-12"ɸ Corr. I.P. Ƶ   19±   +31 15" Dr. Inlet C.I. Grate

94

+94 Fc Cor
+87 ⚘ End 4" Trees
+59 ⚘
+30 ⚘   Vacant Lots
93   +08 ⚘

Vacant Lots.

+78 ♂ P. Pl   +72 ⚘
+44 No Pipe Pr. Entr   +54 Pr. Entr. No pipe
+46 End Patch
19±   +32 ⚘ 15" Dr. Inlet C.I. Grate

92

Hse +89 ℄ Hse   +99 ⚘
70'   +70 ⚘
+41 ⚘   Strawberry Patch
Garden   15"ɸ Vit. Drain Tile Ƶ   +09 ⚘ St 4" Row Trees

91   +98 ⚘
+86 ⚘
+76 ⚘ 2" Trees
+64 ⚘
+52 ⚘   Pasture or Vacant Lots

90

Pasture or Vacant Lots

89   +02 ℄   38'-12"ɸ Corr. I.P.

73-56 103 Lt ℄ Rt 11-21-23 Cold Windy 16

+94 ℄ +93 tree 38'-12"∅ Corr. I.P. ℄ TP +93 Fc

18'

+92

+71 tree 6" +86 tree

+75 tree

+62 ℄ Wlk +67 tree

+57 tree

+49 tree

+42 ℄ Pr. Entr +37 tree

+31 tree 8" No pipe +25 ℄ Pr. Entr

13'-12"∅ x 3/8" thk W.I.P. Installed by Property Owner

102

+96 tree 6" 65'

+90 ℄ Wlk Hse etc

70' Hse

+74 Po.Pl +77 TP +74 tree

+65 tree 4" +64 tree Bushes

+41 tree 4" 45' +45 Hse

+39 tree tree

+32 tree 1" tree

+26 ℄ Pr. Entr No pipe

+16 tree 4" 15" Drop Inlet C.I. Grate +19 +19 Fc. Cor.

101

+92 tree 2" Tree

+74 Sidwlk +80 End Br.

+67 tree 4" "

70'

+43 Po.Pl

+39 tree +36 Pr. Entr

+27 tree +31 TP

+13 tree 6' Vit & 6' Corr. I.P. 15"∅. Installed by Property owner.

100

+92 tree 4" Tree

70' Sidewalk

Sidwlk +75 Brush

+59 tree

+48 tree

38' +30 Beg. Br.

+23 tree +21 Po Pl

10" trees +11 tree +13 Fire hyd. +09 Mail box

99 +09 Beg. Sdewlk +00 Pr. Entr +11 Fc. Cor.

℄ Road +95 No pipe

+81 Mailbox +88

+77 tree +76 Wh. O Pipe

+53 tree

+31

+27 tree

Hse 75'

98 tree +05 4" Trees

+59 Po Pl

15" Vit Drain Tile ℄

Ploughed Field

97

+44 Fc Cor.

+40

96

23-58 110 Lt ℄ Rt 11-2-23 Cold Cloudy 17

+70 ℄

+16 ℄

109

Brush ℄ +89 ⊖ Po Pl Side walk

+69 ⊖ TP

108

No pipe +00 Pr. Entr

+09 Pr. Entr No pipe

+00 24" Oak

Hse +75 +70 ℄ 16" Oak +62 ℄ +75 Nik Hse

k 76' +68 ℄ 65' k

+32 ℄

+38 ℄

Fe Cor ⊖ Po Pl +41

x - - x +33 ⊖ TP +21 +31 ℄ 15" Drop Inlet Ct. Grate

No pipe +11 Pr. Entr

107

Hse k 60' Tree ℄ +75 ℄ End Brush

Tree ℄

Fe. Cor. +53

8" Vit. Pipe Drain

1067 03 Wik

Hse k 60' 98+ ℄ +96 ⊖ Po Pl

+87 ⊖ TP

+71 ℄ +56 Hedge

Side walk

Hse k 26 Wik 4 way brick manhole

65' 1'x2'-15" walls & cover

105 +145 ℄ 1" Tree

+98 Fire Hyd. Est. 32'-12" ℄ Corr. RR ℄ 15" 42' 15" Vit. Pipe

+89 ℄ 6" Tree End Vit Pipe +88 ℄ 15" Drop Inlet Ct. Grate +88

+87 End Vit Pipe 48+ Brg. Brush

Road No pipe +67 ℄ Rd Lt & Rt. No pipe Road.

+44 ⊖ Po Pl

+42 ⊖ TP +48 15" Dr. Inlet Ct. Grate etc

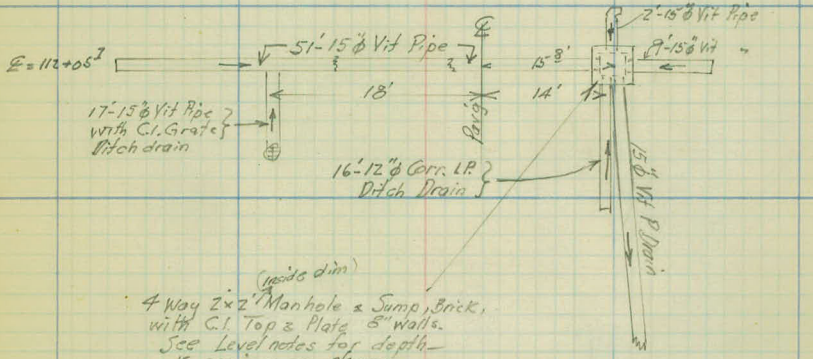
+22 ⊖ TP

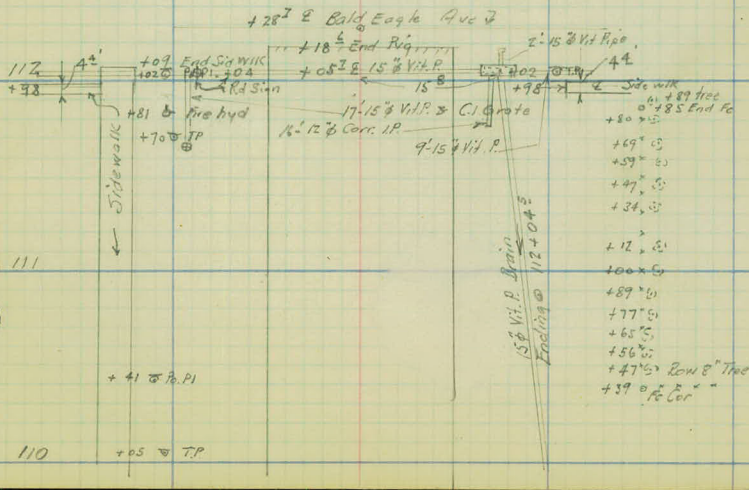
104

Ploughed Garden Side walk 15" ⌀ Vit. Pipe Ploughed Garden

103 +06 ⊖ Po Pl

Detail of Drainage System shown below near end of project 23-56





L ℄ RH

51+85.2 P.I.

10" Oak RP Tack Hub to Grd

50+88 - P.C.

Nail 10" Oak

EQUATION 47+78.6 = 47+87.2

4 12" 4

46+71.6 P.I. Tack Hub

Tack Hubs

Nail Tel. Pl

36+91.7 P.I. Tack 1x2" Hub to Grd

Nail Tree

31+96.5 P.I. Tack 1x2" Hub 20") below surface of Private Entr.

Nail 8" Oak

Nail 10" Oak

EQUATION - 30+72.6 = 30+71.1

Nail 10" Box Elder

23+38.5 P.I. RR spoil road

Tack Hub to Grade

EQUATION - 3+11.63 = 2+00 P.T.

Center Sta/mark Pt. Pl.

P.I. = 2+00 Mont Inters. Rs No. Birch Lake extended & Centerville

Tack 3" Apple Tree

T.P. # 337

P.O.T. 0+00 P.C.

Nail

Tel. Pl # 336

Mont Intr E Co Rds 6 & Centerville See (23-02)(23-55) BK for ties

112+28.1 Nail in Asphalt — Nails Tel. Plt
& Bald Eagle Ave

L 2 Rt.

84+83.1 P.I.

80+75 P.I. — Tacks Hubs to Grd.

EQUATION - 64+43.5 = 64+44.4 P.T.

63+83.4 P.I.

Nail in Lead tree — Tack Hub — Addn Built on Subsequent to Measurement. — Center of Hse

Nail tree

59+73° P.I.

Nail Tree

EQUATION 58+31.7 = 58+29.1

Tack Hub to Grd

57+33.35 P.I.

Tack Hub to Grd.

54+74.9 P.I. — Nail Birch — 3 Nail Birch

STATEMENT OF PAVEMENT WIDTHS

STATION	TO STATION	WIDTH FROM ℄ LEFT (A)	RIGHT (A)
0 - 50		^	10' x From ℄ Centerville
0+00		To be determined	12.48
0+25		Graphically	14.48
+50		v	15.00
0+90	2+61	10.00	15.00
2+86		10.	14.48
EQUAT 3+11²³ = 2+00 ⁴		10	12.48
2+25 ⁴		10	10.50
2+50 ⁴	30+22 ⁶	10.00	10.00
30+47 ⁶		10.37	10.00
EQUAT 30+72 ⁶ = 30+71 ¹		11.63	10.00
30+96 ¹		12.90	10.00
31+21 ¹	32+60 ³	13.29	10.00
32+85 ³		12.90	10
33+10 ³		11.63	10
33+35 ³		10.37	10
33+60 ³	34+88 ⁹	10	10
35+13 ⁹		10.31	10
35+38 ⁹		11.27	10
35+63 ⁹		12.25	10
35+88 ⁹	37+84 ²	12.57	10
38+09 ²		12.25	10
38+34 ²		11.27	10
38+59 ²		10.31	10
38+84 ²	40+68 ²	10	10
40+93 ²		10	10.28
41+18 ²		10	11.13
41+43 ²		10	11.99
41+68 ²	42+69 ⁹	10	12.29
42+94 ⁴		10	11.99
43+19 ⁴		10	11.13
43+44 ⁴	44+10 ¹	10	10.50
44+35 ¹		10	12.48
44+60 ¹		10	14.48
44+85 ¹	47+28 ⁶	10	15.00
47+53 ⁶		10	14.48
EQUAT 47+78 ⁶ = 47+87 ⁹		10	12.48
48+00		10	11.31
48+37 ⁹	50+38	10	10
50+63		11.00	10
50+88			
EQUATION - 58+31² = 58+29 ⁴		12.00	10
	59+69 ⁹		
59+95 ⁴		11.86	10
60+20 ⁴		11.06	10
60+50		10.17	10
60+70 ¹			
EQUAT - 64+43⁵ = 64+44 ⁴		10.00	10.00
79+74 ⁶			
80+00		10.36	10
80+24 ⁶		11.49	10
80+49 ⁶		12.67	10
80+74 ⁷		13.00	10
80+99 ⁸		12.64	10
81+24 ⁸		11.49	10
81+50		10.33	10
81+74 ⁸	83+83 ⁵	10.00	10.00
84+00		10.00	10.14
84+33 ⁵		10.	11.49
84+58 ⁵		10	12.64
84+83 ⁵		10	13.00
85+08 ⁵		10	12.63
85+33		10	11.49
85+50		10	10.62
85+83	112+18 ⁶	10	10

FINAL X-SECTIONS

Sta. 0+00 - 112+18.6 (18 Sheets)

Project No. 23-56

Deutsche
Johnson
Maheney
Franke
} Party

(23-56)

FINAL - X - SECTIONS

Sta.	+ S	H.I.	- S	Elev	
B.M.	168	245.06 ✓		243.38	
Bottom Manhole			7.97		
Intake 9" V.T. P 15"ϕ			7.67		
" 12"-12" Conn. I.R			6.74		
" 51'-15" V.T. "			7.20		
" 11'-15" V.T. P			6.55		
" Long 15" Drain			7.92		
112+00				240.10	239.47
111+00				240.13	39.50
110+00				240.11	39.48
109+00				240.08	39.45
108+00				240.05	39.42
107+00				239.91	39.28
Drop Inlet (Top)			6.66		
T.P	4.70	244.47 ✓	5.29	239.77 ✓	
106+00				239.78	39.15
105+00				239.66	39.03
Bottom Manhole			8.39		
Outlet 15" V.T. P			8.08		
Intake 15" " P			8.25		
Drop Inlet Top			6.15		
" " "			6.32		
T.P.	6.20 Noon	244.19 ✓	6.48	237.99 ✓	
104+00				239.54	38.91
103+00				239.37	238.74
Top 12"ϕ Conn I.R. at Intake			5.71		

11-22-23
Cold. Cloudy

Party { Deutsche, Johnson, Mooney, Franke } L Rf

Top Fire Hydrant L - Sta. 111+80 See p-8 Bk 2 (23-56)

112+05 I

112+05 I

111+90 - 16' Rt

112+05 I - 25' Lt

111+89 - 19' L

Notes:- Sta. 112 - 112+18 I
16 Cu yds Fill dumped 11-23-23 on Rf about manhole & Vit file pipe subsequent to Final X-Sections -
Sta. 112+18 I - a 0+00 Lt & Rt at elev 240.1 -

112+04 S

5.5	5.7	5.2	5.0	4.96	5.0	5.1	5.6	5.0		
19	16	14	10	0	10	14	19	22		(4.9)
5.1	5.3	6.0	5.1	5.0	4.93	5.0	5.1	6.1	4.7	5.0
28	18	17	14	10	0	10	15	19	21	28	(4.2)
5.2	5.1	5.9	5.0	5.0	4.95	5.0	5.0	5.9	4.9	4.5
28	18	17	14	10	0	10	15	19	21	28	(4.2)
5.3	5.5	6.2	5.2	5.0	4.98	5.1	5.0	5.9	4.8	4.8
28	19	18	14	10	0	10	15	19	20	28	(4.3)
5.3	5.3	6.1	5.2	5.1	5.01	5.1	5.1	5.7	5.0	4.8
28	19	18	14	10	0	10	16	19	20	28	(4.3)
5.4	5.7	6.4	5.4	5.2	5.15	5.2	5.3	4.8	6.2	5.7
28	19	18	15	10	0	10	14	20	21	28	(4.8)

107+31 - 19 I Rt

Edge Rd 10' R Sta. 106+40

4.9	5.0	5.9	4.8	4.7	4.69	4.7	4.9	6.0	4.3	4.8
28	18	17	14	10	0	10	14	20	23	27	(4.8)
4.9	4.9	5.9	4.9	4.8	4.81	4.9	4.9	5.7	4.7	4.6
28	19	17	14	10	0	10	14	18	20	28	(5.0)

104+88 - 15 S R

104+88 S - " "

104+87 S " "

104+88 - 20 S "

104+48 - 20 S "

Top Cl Grate Inlet - 104+48

4.7	4.9	5.9	4.7	4.7	4.65	4.7	4.8	5.7	4.7	5.0
28	19	18	15	10	0	10	14	19	20	28	(4.3)
4.8	5.0	6.2	5.0	4.9	4.82	4.9	5.1	6.3	5.4	5.7
28	20	19	15	10	0	10	15	19	20	28	(5.0)

102+94 - 18' L

(23-56) FINAL X-SECTIONS

Sta-	+ S	H.I.	- S	Elev	
		Cont'd fr. prec page			
102+00		244.19		239.26	238.63
101+00				239.15	38.52
Top. Drop Inlet			6.54		
100+00				239.05	38.42
99+00				238.97	38.34
98+00				238.90	38.27
T.P.	4.70	243.53	5.36	238.83	
97+00				238.82	38.19
96+00				238.75	38.12
Intake Culv			7.04		
95+00				238.63	38.00
Intake Culv			7.30		
Top Dr. Inlet			6.84		
94+00				238.51	37.88
93+00				238.41	37.78
Top. Dr. Inlet			6.78		
B.M. x	2.86	242.91	3.45	240.08	240.05
92+00				238.29	37.66
91+00				238.20	37.57
90+00				238.09	37.46
Intake Culv			7.32		
89+00				237.95	37.32
88+00				237.83	37.20
87+00				237.60	36.97
86+00		To Page 9		237.71	237.08
T.P.			5.19	237.72	

Note: Ask me re: this diff. if you're concerned. Say "fire hydrant" REP.

9 an elev

Deutsche, Johnson, Mahoney, Franke } Party Lt ℄ Rt. Cold Flowfg

4.9	5.0	6.3	5.1	5.0	4.93	5.0	5.0	6.4	5.7	5.5	
28	19	18	14	10	0	10	15	20	21	28	(5.1)
4.8	4.9	6.0	5.1	5.1	5.04	5.1	5.1	6.7	4.4	6.0	
28	19	18	14	10	0	10	15	19	21	28	(5.3)

101+19 - 20'R

4.6	4.6	6.1	5.2	5.2	5.14	5.2	5.3	6.9	4.6	3.2	4.5
28	19	18	14	10	0	10	15	19	21	24	28 (4.8)
4.8	4.8	6.0	5.4	5.3	5.22	5.3	5.2	6.1	4.5	4.8	
28	19	18	14	10	0	10	15	19	20	28	(4.4)
5.6	5.9	6.7	5.4	5.4	5.29	5.4	5.4	6.8	6.0	5.8	
28	21	20	14	10	0	10	14	19	20	28	(5.1)

Edge Paving 10'R Sta. 98+00

5.7	5.7	6.8	5.0	4.8	4.71	4.8	4.9	6.4	5.6	5.6	
28	20	19	14	10	0	10	14	19	21	28	(5.1)
6.1	6.1	7.3	5.1	4.9	4.78	4.9	5.0	6.7	5.8	5.7	
28	21	19	14	10	0	10	15	19	21	28	(6.5)

95+51 - 20'L

5.8	5.8	7.0	5.0	4.9	4.90	5.0	5.2	7.0	6.3	6.4	
28	21	20	14	10	0	10	15	20	21	28	(6.5)

94+31 - 18'L

94+31 - 19^{3}R

4.7	5.0	6.6	5.2	5.1	5.02	5.1	5.0	6.4	5.4	5.9	
28	21	19	14	10	0	10	14	19	21	28	(5.3)
4.2	4.2	6.3	5.2	5.2	5.12	5.2	5.2	6.5	5.1	5.4	
28	21	19	15	10	0	10	14	19	20	28	(4.5)

92+32 - 19^{6}R

R.R. Sp. Pow Pl. L Sta. 92+80

4.5	4.6	6.0	4.8	4.7	4.62	4.7	4.8	6.1	5.0	4.9	
28	21	20	14	10	0	10	14	19	20	28	(4.1)
4.8	4.7	6.0	5.0	4.8	4.71	4.8	4.8	6.1	4.5	4.8	
28	21	20	15	10	0	10	14	19	21	28	(4.4)
4.9	4.8	6.1	4.9	4.9	4.82	4.9	5.0	6.4	5.6	5.7	
28	21	19	15	10	0	10	14	20	21	28	(6.0)
5.7	5.3	6.4	5.0	5.0							
28	21	19	15	10	4.96	5.0	5.1	6.1	5.0	5.3	
					0	10	14	19	21	28	(5.0)

89+02 - 18'L

5.5	5.1	6.2	5.2	5.1	5.08	5.2	5.1	6.2	4.9	5.4	
28	20	19	15	10	0	10	15	19	21	28	(5.1)
5.0	5.1	6.4	5.3	5.4	5.31	5.4	5.4	6.6	5.3	4.9	
28	20	19	14	10	0	10	15	20	21	28	(3.6)
5.1	5.0	6.3	5.1	5.1	5.20	5.5	5.5	6.1	5.3	5.1	
28	23	21	15	10	0	10	15	21	23	28	(5.2)

Top stk 30'R Sta 85+72

(2356) PRIVATE ENTRANCES, ROADS ETC.

108+09 P.E. Ditch Section (See X-Sec) x 15' wide

108+00 P.E. Ditch Section (" " ") X 15' " "

107+11 P.E. " " (" " ") x 16' " "

104+67 (Rd) Roadway Rt. 14'Rt = 0+00 H.I. = 244.47

0+00

0+09

104+67 (Rd) Roadway Lt. 14'Lt = 0+00 H.I. = 244.47

0+00

0+05

102+42 P.E. Ditch Sec (See X-Sec) x 12.5' less Culv pipe

102+25 P.E. " " (" " ") X 12.0'

101+26 P.E. " " (" " ") x 13.2

100+36 P.E. " " (" " ") x 12.0 less 15" ϕ Culv "

99+00 P.E. " " (" " ") x 23.2

98+95 (Rd) Roadway Lt 14' Lt. 0+00 HI = 244.19

0+00

0+05 (1½ pipe)

0+32

92+54 P.E. Ditch Sec (See X-Sec) x 20.0

92+44 P.E. " " (" " ") x 18.0

Deutsch
Johnson
Mahoney
Franke
} Party

Lf Cf Rf

11-22-23
Cold Cloudy

5.0 / 16	4.9 / 0	5.0 / 17
5.1 / 10	5.0 / 0	5.3 / 10

4.9 / 16	4.8 / 0	4.9 / 14
5.1 / 9	4.9 / 0	5.0 / 9

		5.3 / 12	5.3 / 0	5.4 / 13		
4.7 / 14	4.5 / 12	5.3 / 11	5.0 / 0	5.2 / 11	4.6 / 12	4.7 / 15
		4.1 / 8	4.5 / 0	4.3 / 6	4.1 / 8	

PRIVATE & FARM ENTRANCES ETC

85+51 F.E. Rt 0+00 = 16'R H.I. = 243.64

0+00

0+08.5 (Less Galv Pipe)

0+11

65+68 Farm E. Rt. 0+00 = 15' Rt. H.I. = 244.92

0+00

0+07

0+13 (Less Galv Pipe)

0+28

62+58 R. Entr. Lt 0+00 = 15' Lt. H.I. = 241.19

0+00

0+08 (Less Galv. pipe)

0+15

0+47

62+34 R. Entr. Rt. 0+00 = 15' Rt H.I. = 241.19

0+00

0+08 (Less Galv Pipe)

0+14

59+50 Outlet Lake Rd Lt 0+00 = 16' Lt H.I. = 235.65

0+00

0+08 (Less Galv Pipe)

0+12

54+06 R. Entr. Lt. 0+00 = 16' L H.I. = 237.03

0+00

0+04 (Less Galv Pipe)

0+15

Reylsche
Johnson
Mahoney
Franko

E

11-23-23
Cold Cloudy

Lt Rt.

6.3 6.3 6.4
13 0 13
8.9 7.1 6.7 7.0 9.0
14 13 0 13 14

6.8 6.6 6.7
13 0 13

7.5 7.3 7.7
13 0 13

10.06 6.6 6.6 7.2 10.42
Intake Culv. 13 9 0 9 13 Outlet Culv. P.
5.5 5.4 6.4 6.2 6.5 5.4 5.5
13 10 7 0 8 11 13
5.6 5.2 5.6 5.8 5.7
10 7.0 6 0 8

7.6 7.2 7.1
13 0 13
9.97 7.8 7.7 7.5 9.46
Outlet 13 12 0 12 13 Intake Culv
8.0 7.5 7.8 7.9 7.6 6.1 5.7
12-10 7 6 0 8 9 13
8.3 7.4 8.0 8.1 6.4 5.3
7 2 0 11 12 16

8.0 8.0 8.1
13 0 13
10.16 8.4 8.6 9.0 10.75
Intake Culv 13 12 0 12 13 Outlet Culv
7.0 8.0 8.8 10.1
15 10 0 13

4.9 5.3 5.2
19 0 18
8.51 7.0 5.8 5.6 6.2 7.6 8.89
Intake Culv 9 18 13 0 14 17 Outlet Culv
5.8 5.5 5.9
12 0 12

5.2 5.2 5.3
13 0 13
7.03 5.2 5.1 5.2 7.04
Outlet Culv 13 12 0 12 13 Intake Culv
6.1 4.7 4.4
10 0 8

(23-56) PRIVATE & FARM ENTRANCES

50+15 Pr. Entr. Lt 0+00 = 15' Lt H.L. = 236.41
0+00 .
0+04 (Less Culv Pipe)
0+37

45+14 Pr. Entr. Lt 0+00 = 15' Lt - H.L. = 237.29
0+00
0+07 (Less Culv Pipe)
0+19

39+81 Farm Entr. Lt. 0+00 = 15' Lt H.L. = 236.82
0+00 No Culv Pipe.
0+07
0+21

31+90 Pr. Entr Rt 0+00 = 19'-8t H.L. = 237.46
0+00 Less Culv Pipe
0+13 Note: This pipe not installed
0+27 by Contractor.

30+88 Pr. Entr. Rt 0+00 = 16'. Rt. H.L. = 237.46
0+00 (Less Culv Pipe)
0+07
0+21

Same party. Lt Rt 11-27-23 Cold Windy 12-11-23 Cold Windy

5.4 5.7 5.6
14 0 11

7.10 5.1 4.8 4.4 6.9.9
Outlet Culv 13 12 0 10 13 Intake Culv

3.8 2.1 1.7
10 0 17

5.0 4.9 4.7
13 0 13

7.96 6.7 5.9 7.0 8.15
Intake Culv 13 12 0 12 13 Outlet Culv

7.1 7.3 7.5
6 0 6

5.1 5.3 5.1
9 0 9

8.7 7.1 6.4 6.4 8.6
12 7 0 7 10

8.7 8.6 8.6
5 0 5

5.0 4.8 4.7
14 0 13

10.9 6.6 6.3 7.2 10.88
Outlet Culv 9 6 0 12 15 Intake Culv.

8.7 8.1 8.4
4 0 12

4.0 3.9 3.9
14 0 11

10.2 5.2 4.9 5.2 10.13
Outlet 14 11 0 8 13 Intake Culv.

7.4 7.6 7.9
16 0 4

(23-56) PRIVATE & FARM. ENTRANCES ETC.

29+39 Farm Entr Lt. 0+00 = 15' Lt. H.I. = 237.46

0+00

0+05 (Less Culv. Pipe)

0+07

29+34 Farm Entr. 0+00 = 16' Rt H.I. = 237.46

0+00

(Less Culv Pipe)

0+06

0+09

23+04 Pr. Entr. Lt 0+00 = 15' Lt. H.I. = 255.97

0+00

(Less Culv pipe)

0+07

0+12

15+53 Pr. Entr Lt. 0+00 = 15' Lt H.I. = 258.39

0+00 (Less Culv pipe)

0+09

0+18

2+19 Pr. Entr Lt 0+00 = 15' Lt H.I. = 266.10

0+00 (Less Culv pipe)

0+08

0+20

Same party. H E Rf 12-11-23 Cold Fair

2.0/10 2.0/0 2.3/9

4.22/9 2.8/9 2.9/0 3.4/9 4.48/9 Intake Culv. / Outlet Culv.

3.2/9 3.1/0 3.5/9

2.0/8 1.8/0 1.7/9

4.22/9 2.7/9 2.3/0 2.7/9 4.08/9 Outlet / Intake Culv

2.4/9 2.4/0 2.0/9

6.0/10 6.0/0 6.0/10

7.73/9 Top Intake Culv. 8.5/9 5.6/7 5.4/0 5.5/8 8.85/9 Outlet Culv

5.7/8 5.1/0 5.1/8

8.5/13 8.4/0 8.2/13

11.95/12 9.4/11 9.2/0 8.9/13 10.65/17 Outlet Culv / Intake Culv

10.6/9 10.1/0 10.2/9

4.0/14 3.8/0 3.9/14

6.59/13 Outlet Culv. 3.4/10 3.3/0 3.4/10 6.40/13 Intake Culv

2.0/10 2.6/0 2.1/10

(23-56) FINAL X-SECTIONS

Sta.	+S	H.I.	-S	Elev	
T.P.	5.92	243.64 ✓		237.72 ✓	
Top Culv (30") 24'L ✓			7.08 ✓		
" " (30") 24'R ✓			6.84 ✓		
Note Use Elev of bottom of Conc Culv - 18"R as elev of outlet of 15"ϕ Vit.P.					
Intake-15"ϕ Corr. I.P. at F.E.			8.93		
Outlet " " " " "			7.00		
85+00				237.94	37.31
84+83.5					
84+50					
84+00				238.32	37.69
83+00				238.74	38.11
82+00				239.17	38.54
81+30					
81+00				239.59	38.96
80+75					
80+24.6 P.C.					
80+00				239.90	39.27
T.P.	4.86	245.33 ✓	3.17	240.47 ✓	
79+00				240.17	39.54
78+00				240.30	39.67
77+00				240.49	39.86
76+00				240.70	40.07
75+00				240.88	40.25
74+00				240.98	40.35
73+00				240.90	240.27
T.P.	3.77	244.92 ✓	4.18	241.15 ✓	

Deutsche
Johnson
Mahoney
Franke
} Party

E

11-23-23
Cold Cloudy
SNOW! ✓

Lt.

Rt

Top stk 30'R Sta. 85+72

85+90

85+90

85+91

85+38-26'R

85+64-26'R

6.5	6.9	7.6	5.1	5.2	5.70	6.3	6.5	8.2	7.0	7.0	
36	33	27	15	10	0	12.8	18	27	32	33	(6.7)
6.5	7.0	7.7	5.1	5.1	5.59	6.2	6.4	8.1	7.1	6.9	
36	33	27	14	10	0	13	18	27	32	35	(7.0)
7.1	7.2	7.6	5.1	5.0	5.50	6.1	6.3	8.1	6.8		
36	33	24	15	10	0	12.5	18	26	32 - 35		(6.9)
6.3	7.1	7.5	5.0	5.0	5.32	5.7	5.7	7.9	7.8	6.8	
36 - 33	32	26	15	10	0	10.5	15	24	30	33-35	(6.8)
6.0	6.2	7.3	4.9	4.9	4.90	5.0	5.2	7.3	7.2	6.1	
33	31	27	14	10	0	10	15	23	30	33-36	(6.0)
5.1	5.1	6.9	6.7	4.8	4.7	4.47	4.4	4.5	6.6	6.4	5.2	4.9	
33	31	27	24	15	10	0	10	14	24	29	32	34	(5.3)
		5.4	6.6	5.1	4.7	4.20	3.9	3.9	6.0	6.1	5.0		
33 -		31	27	18	10	0	10	15	24	30	32-35		(5.3)
		5.5	6.6	4.9	4.6	4.05	3.6	3.8	6.4	6.6	5.2		
33 -		31	27	17	12.5	0	10	15	25	29	32-35		(4.9)
3.5	6.7	6.5	4.9	4.6	3.95	3.4	3.5	6.5	6.5	5.4		
34 - 32	29	26	18	13	0	10	15	24	28	31-33		(5.1)
4.7	6.1	6.2	4.5	4.3	3.82	3.4	3.5	6.5	6.1	4.6		
33 - 30	28	24	14	11.5	0	10	15	23	28	31-33		
4.6	6.0	5.8	4.2	4.1	3.74	3.4	3.5	6.1	5.8	4.4		
33 - 30	27	22	15	10.5	0	10	14	24	28	31-33		(3.9)

Top stk 13'R Sta. 80+00

6.5	7.5	7.6	5.3	5.3	5.16	5.2	5.3	7.4	7.1	6.3	
33 - 29	27	23	14	10	0	10	14	24	27	30-33	(6.0)
5.9	7.0	7.1	5.3	5.1	5.08	5.1	5.0	7.1	7.0	6.1	
33 - 29	27	23	14	10	0	10	7.5	23	28	30-33	(5.7)
6.1	6.7	5.0	4.9	4.84	4.9	4.9	7.4	6.9	6.2		
33 - 31	22	15	10	0	10	14	24	29	30-33		(5.5)
6.4	6.9	6.7	4.8	4.7	4.63	4.7	4.7	7.1	7.1	6.3	
33 - 31	29	22	15	10	0	10	15	23	29	31-33	(5.8)
5.6	6.5	6.6	4.6	4.5	4.45	4.5	4.6	6.6	6.2	5.7	
33 - 31	29	23	15	10	0	10	14	23	29	31-33	(5.1)
5.4	6.5	6.7	4.6	4.4	4.25	4.4	4.4	6.8	6.4	5.4	
33 - 31	29	24	15	10	0	10	14	23	29	31-33	(5.1)
5.7	7.0	7.2	4.5	4.5	4.3	4.5	4.5	7.6 ✓	6.9	6.1	
33 - 31	29	25	15	10	0	10	15	24	29	31-33	(5.3)

Top stk 14'R Sta 73+00

(23-56)

FINAL X-SECTIONS

Sta.	+S	H.I.	-S	Elev	
		Contd fr. prec. page 244.92			
72+00				240.70	240.07
71+00				240.41	39.78
70+00				240.21	39.58
69+00				240.00	39.37
68+00				239.60	38.97
67+00				238.71	38.08
66+00				237.63	37.00
65+00				236.49	35.86
B.M. & T.P.	0.42	241.19 ✓	4.17	240.75 ✓	Plan elev 240.77 ✓
64+48.5					
64+00		℄ EQUATION 64+44.4 = 64+43.5 ✓ 7 - Ft.		235.45	34.82
63+50					
63+00				234.26	33.63
B.M.			0.42	240.77 ✓	
B.M.	0.54	241.31 ✓		240.77	
62+00				233.05	32.42
61+00				231.94	31.31
T.P.	3.65	235.65 ✓	9.31	232.00 ✓	
61+00					
Intake 24ϕ RCP			9.28		
Top. Ctr Conc Slab			6.74		
Top. 24ϕ RCP at Outlet			7.58		
Intake Spillway R.			6.93		
Top. " " S at outlet			6.84		
60+00				231.32	230.69
59+77					

Deutsche, Johnson, Mahoney, Franke } Party. — 11-23-23 Cold Snow 11-26-22 Cold Windy

Lt Ct Rt

	6.1	6.8	7.0	4.3	4.3	4.22	4.3	4.3	6.9	6.7	6.1
33-	30	29	23	14	10	0	10	15	23	29	31-33
	5.4	6.6	6.8	4.6	4.6	4.51	4.6	4.4	6.4	6.7	5.5
33-	31	28	23	14	10	0	10	15	23	29	32-33
	5.6	6.7	6.7	4.8	4.8	4.71	4.8	4.8	6.8	6.9	5.8
33-	31	29	25	15	10	0	10	15	25	29	32-34
	5.6	7.0	6.5	4.9	5.0	4.92	5.0	5.0	6.9	7.0	5.9
33-	31	30	24	14	10	0	10	14	25	29	31-33
	5.3	7.5	7.1	5.4	5.4	5.32	5.4	5.3	7.2	6.8	5.9
33-	28	25	21	15	10	0	10	15	23	28	30-33
	5.7	8.4	8.0	6.3	6.3	6.21	6.3	6.4	8.0	8.0	5.8
30-	27	24	20	15	10	0	10	15	19	22	25-28
	5.6	9.4	9.2	7.4	7.4	7.29	7.4	7.5	9.6	9.6	5.6
33-	30	24	20	15	10	0	10	15	19	23	28-30
	5.6	10.7	10.4	8.2	8.3	8.43	8.26	10.8	11.1	4.9	4.9
33-	32	25	21	15	10	0	10	14	20	23	30	33

Oak

R.R. Sp. Tree Rt. 65+30

	1.6	7.3	1.8	1.8	5.16	5.4	5.4	7.6	2.7	1.9	
35-	32	24	14	10	0	10.2	15	24	31	33-35	
	1.3	7.7	5.3	5.2	5.74	6.1	6.2	7.9	2.3	1.8	
36-	33	25	14	10	0	10.2	15	25	33	36	
	0.4	8.2	5.9	5.8	6.32	6.7	6.7	8.6	2.0	1.4	
36-	34	25	15	10	0	10	+0.14	24	33	36	
	2.1	9.1	6.7	6.6	6.93	7.1	7.1	9.4	3.9	3.5	
36-	32	23	14	10	0	10	15	23	32	36	

RR. Sp. 14" Oak 35' R Sta. 65+30

" " " " " " " " " " " " ← Start 11-26-23 11:30A

	12.1	11.5	11.5	8.4	8.3	8.26	8.4	8.6	11.7	11.1	11.0
33		26	23	15	10	0	10	15	23	26	30-33
						9.37	9.3	9.4	13.0	13.0	12.7
						0	10	15	23	26	27-33

Edge Pavg 10' R Sta 61+00

	9.6	9.1	2.8	3.7
35-	28	15	10	

60+89 26' Lt

60+89 24.5 Rt

See Drainage Notes

59+86

59+86

	9.3	8.2	9.1	7.9	4.8	4.6	4.43	4.2	4.7	5.5	County Gravel Stk. Pile
33		30	29	24	17	12	0	10	15	25	26-40
	8.5	8.3	8.9	5.0	4.9	4.60	4.20	4.0	9.1	9.2	
33		28	24	17	12	0	10	16	24	33	

(23-56) FINAL X-SECTIONS

Sta.	+S	H.I.	-S	Elev	
59+72		235.65			
59+50					
59+34					
59+26					
Intake Spillway P			6.04		
Top " " P. of Outlet " "			6.43		
59+00				231.10	230.47
58+31					
EQUATION — 58+31.7 = 58+29.4 P.T.					
58+00				231.27	30.64
57+50					
57+00 =				231.48	30.85
Intake 15" Con. R.P. P.E. Culv.			6.72		
Outlet 15" " " " "			7.10		
56+50					
56+32.7 P.C.					
56+15.42 P.T.					
56+00				231.69	31.06
T.P.	5.01	237.03	3.63	232.02	
55+50					
55+00				231.87	31.24
54+50					
54+00				231.92	31.29
53+50					
53+00				231.88	231.25
Outlet 24" R.C.P.			7.51		
Intake " "			8.14		

Deutsche
Johnson
Mahoney
Franke
} Forty

11-26-23
Cold Windy

11

L Rt

8.6	8.0	8.8	5.0	4.9	4.49	4.2	4.1	9.0	9.5	
33	29	23	17	12	0	10	16	24	33	(57)
5.7		5.3	4.8	4.50	4.2	4.1	9.2	9.2		
33		16	12	0	10	16	24	33		(57)
8.3	6.7	5.0	4.9	4.52	4.2	4.1	9.4	9.7		
33	21	17	12	0	10	17	24	33		(59)
8.4	7.9	8.4	7.1	5.1	4.9	4.51	4.26	4.2	8.3	9.8
33	26	24	21	17	12	0	10	16	24	33	(59)

59+ 17

59+ 17

8.4	8.4	7.9	7.6	4.85	4.2	4.4	8.8	9.9		
33	24	17	12	0	10	16	23	33		(60)
7.9	7.4	4.5	4.5	4.41	4.1	4.0	8.8	9.8		
33	23	17	12	0	10	15	23	33		(59)
7.7	7.1	4.5	4.5	4.38	4.1	3.9	7.8	9.8		
33	23	18	12	0	10	15	21	33		(58)
5.7	5.6	4.6	4.6	4.25	3.9	3.9	8.8	9.8		
33	20	17	12	0	10	15	23	33		(59)
5.6	5.6	4.2	4.3	4.17	3.9	3.6	8.7	10.0		
33	18	16	12	0	10	16	23	33		(55)

57+ 68 - 22° L

57+ 68 - 33° L

4.0	4.5	5.5	5.3	4.1	4.1	4.06	3.7	3.6	7.8	9.5
33	23	22	20	17	12	0	10	15	22	33	(53)
3.7	4.0	5.2	5.2	4.1	4.1	4.03	3.7	3.4	6.9	9.4
33	25	22	19	17	12	0	10	15	21	33	(51)
3.4	3.6	5.1	5.1	4.0	4.1	3.98	3.7	3.6	6.2	9.0
33	24	22	19	17	12	0	10	15	20	33	(49)
2.6	3.0	4.9	4.9	4.0	4.1	3.96	3.6	3.6	6.3	9.2
33	25	22	19	17	12	0	10	15	21	33	(49)

Edge Pvig. 10° R Std. 56+00

2.2	2.8	6.0	6.0	5.3	5.4	5.23	4.7	4.9	6.7	8.4
38	25	21	19	16	12	0	10	15	21	33	(52)
2.5	2.7	5.7	5.2	5.3	5.16	4.8	4.9	6.6	8.5	
33	24	20	18 16	12	0	10	16	25	33	(44)
2.7	2.6	4.9	5.4	5.3	5.15	4.8	4.8	5.8	6.8	
33	24	18	16	12	0	10	15	19	38	(43)
4.9	4.4	6.9	6.9	5.2	5.4	5.11	4.8	4.8	5.8	7.0
38	25	21	19	16	12	0	10	15	18	33	(49)
4.9	4.8	6.5	5.2	5.2	5.13	4.8	4.9	6.1	7.3	6.9	7.6
38	25	22 19	17	12	0	10	15	19	25	26	33	(54)
6.3	6.7	7.2	6.7	5.3	5.2	5.15	4.9	4.8	6.0	8.1		
33	25	23	18	16	12	0	10	15	18	33		(61)

52+ 75 Rt

52+ 75 L

(23-56) FINAL X SECTIONS

Sta.	+S	H.I.	-S	Elev	
52+50		237.03 ✓			
52+00				231.60	230.97
51+50			S		
51+25					
51+00				231.23	30.60
B.M.			4.98	232.05 ✓	Plan Elev 232.09 232.09 ✓ Rec. Levels by R.E.D.
B.M.	432	236.41 ✓			232.09
50+50					
50+00				231.08	30.45
49+55					
49+00				231.38	30.75
48+00		EQUATION			
		47+78 = 47+87 ?		231.77	31.14
Intake 12"ϕ Corr I.P. Spillway			6.17		
Top 12"ϕ Spill. at outlet			9.41		
TP 2 B.M.	520	237.29 ✓	4.32	232.09 ✓	232.09 ✓
47+00				231.88	31.25
46+50					
46+00				231.89	31.26
Intake 12"ϕ Corr I.P. Spillway			7.39		
Top 12"ϕ Corr I.P. (Spillw) at outlet			11.30		
45+50					
45+00				231.92	31.29
44+00				231.98	31.35
43+50					
43+00				232.04	231.41
T.P.	508	237.32 ✓	5.05	232.24 ✓	

Same party - Cold windy

L. Rt.

9.5	6.2	5.3	5.3	6.26	6.0	5.0	6.3	10.1		
33	18	16	12	0	10	15	19	33		(64)
7.6	6.2	5.5	5.5	5.43	5.1	5.0	7.4	10.6		
33	19	17	12	0	10	15	19	33		(61)
4.2	4.5	6.7	5.7	5.8	5.59	5.3	5.1	6.8	9.6	
33	24	21	16	12	0	10	15	19	33	(58)
3.0	3.2	6.1	5.9	5.9	5.70	5.4	5.2	6.4	7.6	
33	26	21	17	12	0	10	16	19	33	(58)
2.4	3.5	6.4	6.0	6.0	5.80	5.5	5.2	6.2	6.2	
33	27	20	17	12	0	10	16	19	33	(61)

See 1.54. DK2-2856) Sp. 12" Oak 30'R Sta. 51+30

" " " " " " " " Start 11-27-23

12	7.1	6.5	6.5	5.2	5.3	5.28	5.0	4.9	5.8	6.4	5.7	5.6
33	24	20	18	16	16	0	10	16	18	29	23	36	(60)
5.4	6.6	7.1	5.4	5.6	5.33	5.2	5.0	6.9	7.8			
33	22	20	16	10	0	10	15	19	33			(66)
10.7	10.5	5.4	5.4	5.28	5.3	5.2	5.9	7.0	9.5	10.1		
33	24	15.6	16	0	10	16	17	22	28	33		(63)
10.8	9.0	5.0	5.1	5.08	4.9	5.0	10.0	10.7				
33	21	15	10	0	10	15	24	33				(63)
10.1	9.9	4.0	4.2	4.64	4.9	5.0	11.1	12.0				
33	23	16	10	0	11.4	16	26	33				(63)

49+02 - Rt

49+02 "

Sp. 12" Oak 30'R Sta. 51+30

6.9	6.4	4.6	4.8	5.41	6.1	6.2	12.8	13.1	
33	19	17	10	0	15	19.5	30	33	(134)
6.4	6.3	4.5	4.8	5.43	6.1	6.1	13.0		
33	19	16	10	0	15	20	31-33		(121)
6.2	6.0	4.6	4.8	5.40	6.1	6.4	12.0	12.8	
25	18	15.5	10	0	15	19	26	33	(83)

46+06 Rt.

46+06 "

9.6	9.4	4.7	4.8	5.41	6.1	6.1	11.5	12.0		
33	22	15	10	0	15	20	29	33		(68)
5.6	6.2	7.7	4.8	4.7	5.37	6.1	6.1	7.9	9.4	
33	23	20	15	10	0	15	19	25	33	(60)
7.5	6.0	4.9	5.0	5.31	5.5	5.6	6.9	7.0	10.3	
28	17	15	10	0	10.5	15	17	21	33	(60)
7.1	7.4	4.9	5.0	5.31	5.4	5.5	9.6	10.9		
30	27	15	10	0	10.5	15	26	33		(56)
7.4	6.1	4.7	4.9	5.25	5.7	5.8	8.6	11.1		
33 - 28	18	15	10	0	11.7	16	21	33		(60)

Edge Rvg 10'Lt 43+70

(23-56) FINAL X-SECTIONS

Sta.	+S	H.I.	- S		
B.M.		237.32	4.69	232.63	232.64 (Prev determined)
42+50					
Intake 12"ϕ Conc. RCP Silt			7.07		
Top " " " " at outlet			8.53		
42+00				231.96	231.33
41+50					
41+00				231.92	31.29
40+50					
40+14					
40+00				231.95	31.32
B.M.	4.18	236.82	4.69	232.63	232.64
39+50					
39+00				231.85	31.22
38+50					
38+34 ± P.T.					
38+00				231.79	31.16
37+50					
37+00				231.86	31.23
36+50					
T.P.	4.98	237.46	4.34	232.48	
36+00				231.90	31.27
35+85					
35+38 ± P.C.					
B.M.			10.78	226.68	226.69 (Prev. Determined)
				231.92	
35+00					31.29
34+00				231.94	231.31
Top 24" RCPC Outlet				8.38	
Intake " " " Inv				11.30	

Note: These rods are correct. Cult is laid to Elevation of Lake. Instead of Lake.

Deutsche
Johnson
Maloney
Franke
} Party

℄ Rt.

11-27-23
Cold Windy
12-11-23
Cold Fair

See BK #2 Pg. 58

Nail pow pl. 27'L Sta. 42+94

8.0	6.9	4.7	4.8	5.41	5.9	6.3	6.8	10.0	
28	19	14.5	10	0	12	17	19	30-33	(60)

42+18-Rt.

42+18- "

9.4	7.9	4.5	4.8	5.36	5.9	6.1	7.0	8.4	
30-26	21	14.5	10	0	12.4	17	18	28	(60)
9.1	8.3	4.7	4.9	5.40	5.8	5.7	7.2	7.3	
33-28	21	15	10	0	12	16	19	22	(60)
8.7	7.9	4.8	5.1	5.40	5.6	5.5	9.6	10.5	
30-27	20	15	10	0	10.5	14.5	22	26	(62)
9.1	8.6	5.3	5.2	5.36	5.3	5.2	11.1	11.0	
28	20	15	10	0	10	14.5	23	28	(67)
9.6	9.4	5.4	5.4	5.36	5.2	5.1	12.0	12.5	
28	21	15	10	0	10	15.5	25	33	(70)
9.6	9.4	5.5	5.4	5.37	5.5	5.3	12.2	12.8	
33	25	16	10	0	10	15.5	25	33	(72)

Start. 12-11-23

Nail Pow Rt. 27'L Sta. 42+94

10.5	9.8	5.0	5.0	4.88	4.9	4.8	7.2	8.3	11.3	
33	22	15	10	0	10	16	21	25	33	(65)
11.8	11.3	5.0	4.9	4.91	4.9	4.9	9.0	10.6	11.0	
33	24	15	10	0	10	16	23	27	33	(70)
11.7	11.4	5.4	5.2	5.01	4.7	4.9	7.7	6.7	7.4	9.1
33	25	17	10.5	0	10	16	20	23	28	33	(66)
11.1	10.8	5.4	5.3	5.04	4.7	4.7	7.0	7.6		
33	25	17	11.5	0	10	16	20	28			(67)
10.4	9.5	5.5	5.5	5.03	4.5	4.4	7.1	7.8		
33	24	18	13	0	10	17	21	27			(65)
8.5	8.5	5.5	5.6	5.03	4.5	4.4	7.4	7.5		
26	22	17	13	0	10	15	19	25			(64)
10.0	9.1	5.6	5.5	4.96	4.7	4.1	7.3	7.5		
33	23	18	12.5	0	10	16	22	27			(65)

Intake Spillway Inv. = 6.98
Top Outlet P " " = 7.85
@ 37+67

11.7	11.4	5.7	5.5	4.90	4.3	4.1	8.8	8.8	
33	26	18	12.5	0	10	16	23	26	(67)
12.5	12.1	6.2	6.1	5.86	4.9	4.7	8.7	10.6	
33	26	19	12.5	0	10	17	23	31	(77)
12.7	12.1	6.2	6.1	5.86	4.9	4.8	10.5	11.5	
33	27	18	12.5	0	10	17	25	33	(75)
12.5	11.8	5.7	5.7	5.55	5.2	5.1	11.6	12.8	
33	27	17	11.5	0	10	16	26	38	(77)

Edge Pavg 10'R 36+50

Nail TPI. 40'L Sta. 33+37

13.1	11.6	5.6	5.5	5.87	5.3	5.4	12.5	13.9	
33	26	16	10	0	10	16	27	33	(78)
11.9	11.4	5.7	5.7	5.82	5.4	5.4	11.9	12.6	
33	23	16	10	0	10	16	24	33	(77)

Sta 34+03

(23-56)

FINAL X-SECTIONS

Sta.	+ S	H.I.	- S		
		Contd fr. p page			
33+00		237.46 ✓		231.94	231.31
32+00				232.06	31.43
31+90					
31+00				232.87	32.24
30+00		EQUATION		234.38	33.75
29+00		30+72½ = 30+71½		236.43	35.80
B.M.	11.27	247.05 ✓	1.69	235.77 ✓	Prev. Determ'n ✓ 235.78
28+00				238.96	38.33
27+00				241.65	41.02
26+90					
+75					
26+00				244.14	43.51
25+50					
25+00				246.21	45.58
T.P.	9.03	255.97 ✓	0.11	246.84 ✓	
24+50 ✓					
24+00				248.00	47.37
23+00				249.41	48.78
22+00				250.54	49.91
B.M.			4.48	251.49 ✓	Prev. Determ'n 251.50
21+50					
21+00				251.32	50.69
P.C. 20+47½					
20+00				251.85	51.22
19+00				251.82	51.19
18+00				251.59	250.96
T.P.	6.87	258.39 ✓	4.45	251.52 ✓	

Same party — 12-11-23 — 12-12-23 Cold Fair Windy — 14

	Lt.				℄			Rt.			
Intake Spillw. Rod = 7.52	11.3	10.6	5.9	5.8	6.52	5.1	5.0	12.3	12.6		
	33	26	18	12	0	10	16	27	33		78
Top outlet end " " " 9.22	12.1	11.6	5.8	5.9	5.40	4.8	4.9	10.0	10.2		
	33	29	19	13	0	10	18	26	33		76
	11.6	11.3	5.9	5.9	5.36	4.7	4.8				
	33	27	19	13.3	0	10	19	See R.Entr. Data for remainder			75
	7.8	7.7	4.9	5.0	4.89	4.0	4.0	10.2	7.3	7.4	
	33	24	19	13.3	0	10	16	23	26	33	74
	4.8	5.2	3.0	3.1	3.08	3.0	3.0	4.9	4.9	4.1	5.4
	33	20	15	10	0	10	15	19	22	23	33	49
3.7	3.3	3.7	3.1	1.81	1.0	1.03	1.1	0.9	2.9	3.0	0.7	0.7
33	22	21	18	14.5	10	0	10	15	19	22	25	33	16
									Start.	12-12-23		

Sp. Pow. Pl. 36' L Sta. 29+30

8.2	7.7	10.3	10.1	8.2	8.2	8.09	8.2	8.4	10.1	10.4	7.0	6.7
33	25	21	17	14.5	10	0	10	14.5	17	20.5	26	33	78
6.9	6.9	5.4	5.4	5.40	5.5	6.0	7.4	7.6	1.0	1.1		
22	18.8	15	10	0	10	15	17.6	21.6	30	33		28
6.4	6.4	6.1	5.2	5.15	5.0	5.1	7.4	7.6	0.1	0.2		
22	18	15	10	0	10	14.4	18.5	21.3	32	33		03
34	22	6.6	6.6	4.7	4.7	4.74	4.7	4.5	6.9	6.5	0.0	-0.2
33	29	22	19	15	10	0	10	15	18	22	30	33	+04
+1.9	+2.1	0.0		4.7	2.5	2.6	2.91	3.1	2.9	5.8	5.8	3.7	4.0
33	31.6	28.6	22-18.6		15	10	0	10	15	19	23	25	33	28
3.0	3.6	4.3	4.1	1.6	1.5	1.86	2.1	1.7	5.2	5.4		
33	26	25	19	15	10	0	10	15	20	30		5.1
1.1	1.6	3.1	2.7	0.4	0.5	0.84	1.1	1.0	2.8	3.4		
33	29	25	18	15	10	0	10	15	19	20		27

Top. Conc Curb 10' Rt. Sta. 24+50

5.9	6.5	10.4	8.4	8.5	8.85	9.1	8.9	11.4	11.4	7.0	6.9	
33	30	23-19		15	10	0	10	15	19	22	28	33	67
4.1	4.2	9.4	9.1	7.5	7.6	7.97	8.2	8.1	10.5	10.5	1.7	1.7	
33	31	23	18	15	10	0	10	15	19	23	32	35	4.1
5.3	5.0	8.5	6.0	6.2								
33	28	23-20	16	10	6.16	6.8	6.8	9.4	9.6	2.1	1.9		
					0	10	14	18	23	32	35	1.1
6.1	6.8	7.1	7.3	5.1	5.1	5.43	5.7	5.8	8.6	9.0		
33	25	23	19	15	10	0	10	14	20	30		6.4

Sp. Tel. A. L Sta. 22+60

7.1	7.0	7.5	7.1	4.5	4.6	5.02	5.2	5.1	7.6	7.8		
30	24	23	19	15	10	0	10	15	19	25		58
7.1	6.8	7.3	6.9	4.3	4.3	4.25	4.9	4.9	7.4	7.4	6.0	5.4	
33	24	23	19	15	10	0	10	15	18	21	23	33	53
6.3	6.2	6.6	6.3	4.1	4.2	4.39	4.5	4.5	6.9		1.9	1.6	
33	23	22	19	15	10	0	10	14	18	21	28	33	46
5.5	5.1	6.1	5.7	4.1	4.1	4.12	4.1	4.0	6.0	6.6	3.8	2.7	
33	24	22	17	14	10	0	10	14	18	22	28	33	41
3.0	3.8	6.1	5.6	4.3	4.2	4.15	4.2	4.3	6.3	2.3	2.7		
33	25	22	17	14	10	0	10	14	20	26	33		2.9
2.7	2.8	6.1	5.7	4.4	4.1	4.38	4.5	4.6	6.5	0.0	+ 2.0		
33	27	22	18	15	10	0	10	14	20	30	32.35		26

Edge Pavg 10' R Sta 18+80

(23-56)

FINAL X-SECTIONS

Sta-	+S	H.I.	-S		
		258.39			
17+50		Centre of pipe			
17+00				251.17	250.54
16+50					
16+00				250.45	49.82 Prev. Deformed
B.M. & T.P.	4.08	253.55	8.93	249.46	249.47
15+00				249.68	49.05
14+00				248.98	48.35
13+67					
13+00				248.57	47.94
Top Culv Pipe 24"ϕ Outlet End (Lt)			9.20		
" " " " Intake End (Rt)			8.95		

Note:- This Culv drains now from Rt. to Lt although contour of land shows it should drain Lt to Rt.

12+00				248.75	48.12
11+00				249.58	48.95
10+47					
10+00				251.00	50.37
9+00				252.64	52.01
T.P.	9.10	261.59	1.06	252.49	
8+29					
8+00				254.37	53.74
7+00				256.06	55.43
6+61					
6+00				257.77	257.14
Temp B.M.	5.32	266.10	0.81	260.78	
6+00					

Deutsche
Johnson
Mahoney
Franke

Lt. ℄ Rt. 12-12-23 Cold Fair

3.2	3.2	7.8	7.8	7.1	7.0	6.98	7.0	7.1	8.1	8.6	9.0	+ 0.6	+ 0.8
33	29	21	17	15	10	0	10	15	18	21	32.5	33	36

55

3.2	3.5	8.5	8.3	7.4	7.8	7.72	7.3	7.4	8.3	8.8	9.1
33	29	22	18	15	10	0	10	15	17	21	32-33

60

7.5	7.3	9.0	8.4	7.5	7.6	7.53	7.6	7.5	8.3	8.7	4.3
33	24	21	18	15	10	0	10	15	16	20	27-33

67

10.2	9.4	10.0	9.1	8.1	8.1	7.94	8.0	8.1	9.0	9.6	7.8	7.9
33	23	22	17	15	10	0	10	15	18	22	25	33

93

Top SW. Cor. Conc. Hop House 120' L Sta. 15+25

7.0	6.5	4.1	4.0	3.87	4.0	3.8	5.2	5.6	4.8	5.9	
33	19	15	10	0	10	15	18	21	22	33	

54

8.0	7.0	4.6	4.6	4.57	4.7	4.8	6.4	7.0	4.0	4.8	
33	20	15	10	0	10	15	18	21	25	33	

63

8.4	7.8	4.9	4.8	4.78	4.9	4.8	6.5	7.3	5.8	6.9
33	19	15	10	0	10	15	18	22	24	33

69

11.3	10.0	5.0	5.1	4.98	5.1	5.3	9.8	10.1	
33	23	15	10	0	10	15	22	33	

78

Sta. 12+51

" " +51

9.1	7.7	4.9	4.9	4.80	4.9	5.0	8.2	9.0	
33	20	15	10	0	10	15	21	33	

75

4.3	4.5	6.2	5.6	4.1	4.1	3.97	4.1	4.2	7.1	7.8
33	24	22	19	15	10	0	10	15	21	33

58

4.8	4.4	5.3	5.1	3.6	3.3	3.28	3.4	3.5	5.7	5.6	4.5	5.3
33	24	23	20	15	10	0	10	14	19	23	24	33

46

4.2	3.7	4.8	4.7	2.7	2.6	2.53	2.6	2.7	4.4	4.6	2.9	3.7
33	24	22	19	15	10	0	10	15	19	21	24	33

38

4.6	3.8	1.1	1.0	0.91	1.1	1.2	3.4	1.4	1.5	
33	21	14	10	0	10	15	19	24	33	

23

Edge Rd 10'R Sta. 9+00

8.0	7.7	9.5	9.3	8.0	7.8	7.74	7.9	8.0	9.6	9.7	3.9	4.4
33	26	23	19	15	10	0	10	15	18	21	27	33

83

8.5	8.3	9.3	9.2	7.4	7.3	7.22	7.3	7.5	9.6	9.8	6.4	7.2
33	25	23	19	15	10	0	10	15	19	21	26	33

79

8.0	7.6	7.9	5.7	5.6	5.53	5.6	5.7	7.7	8.0	7.4	9.2
33	23	21	14	10	0	10	15	19	23	24	33

63

5.8	5.2	7.2	7.0	5.0	5.0	4.88	5.0	5.1	7.1	7.1	5.7	6.6
33	25	23	19	14	10	0	10	15	19	23	24	33

53

		3.82	3.5	3.9	5.9	1.9	3.4
		0	10	14	20-22	27	33

38

(3:30 P.M.) Start 12-13-23 Cor. broken

Edge Rd 10'R Sta 4+00 (Pulled Up A/o Called for by truck for tow)

4.7	9.5	10.5	9.5	8.5	8.4
33	30	22	17	14	10

83

(23-56) FINAL X-SECTIONS

5+55		266.10 Cont'd fr. p. page			
5+00				259.50	258.87
4+00				261.07	60.44
3+75					
3+00				261.97	61.34
2+50				261.94	61.31
EQUATION 2+00 ℄ = 3+11 03					
BM & T.P.			3.88	262.22	Prev. Determ'd 262.24
3+00				261.38	60.75
	3.87	266.11			
2+50				260.77	60.14
2+00				259.99	59.36
1+50					
1+00				258.86	58.23
0+50					
0+00 P.C.				259.68	259.05
T.P.	5.10	263.76	7.45	258.66	
Top 24" R.C.P. Outlet (Lt)			10.66		
" " " " " Intake (Rt)			10.30		
Top 12" ϕ Corr. P. Spillway outlet			10.43		
Intake " " " " "			5.98		
T.P.	6.83	266.61	3.98	259.78	
BM.			4.36	262.25	262.24

Lt ℄ Rt 12-13-23 Cold! Windy

8.2	7.6	9.5	9.2	7.7	7.6	7.54	7.6	7.8	9.5	9.7	8.1	9.6
33	27	25	18	14	10	0	10	15	20	23	25	33
8.0	7.2	8.8	8.3	6.7	6.7	6.60	6.7	6.7	8.6	9.0	7.9	8.3
33	25	22	18	15	10	0	10	15	19	22	25	33
4.4	4.1	6.6	6.6	5.1	5.1	5.03	5.1	5.2	6.7	6.7	2.8	3.0
33	27	23	19	15	10	0	10	15	19	22	27	33
5.6	5.3	6.3	6.3	4.8	4.8	4.73	4.8	4.7	6.4	6.4	5.4	5.6
33	25	23	19	15	10	0	10	15	19	22	25	33
2.9	2.9	5.7	5.7	4.2	4.2	4.13	4.10	4.2	6.1	6.3	4.0	4.2
33	28	24	20	15	10	0	10	14	19	21	24	33
1.8	1.9		5.8	3.9	4.0	4.16	4.2	4.2	5.5	5.5	2.5	2.4
33	28	23	20	15	10	0	10	14	18	22	26	33

7.6
6.7
5.0
4.5
3.6
3.7

Nail 24" Poplar 40'L Sta. 3+45

1.0	1.1	6.4	6.4	5.5	4.3	4.3	4.72	5.1	5.0	6.9	6.9 - 2.1	+ 0.2
33	31	24	22	18	15	10	0	132	18	21	25 30	33

4.21

As above →

5.7	6.8	7.3	7.5	6.1	6.2	4.7	4.7	5.34	6.0	6.0	7.6	3.7
37	34	33	31	28	23	18	10	0	15	21	25-28	32-33

6.00

8.3	7.7	7.5	6.8	5.7	5.5	4.72	6.7	6.7	11.1	10.9
56	46	45	35	19	10	0	14.6	19	26	33

10.7

7.6	10.4	10.1	5.8	6.2	Cant	7.4	7.5	13.4	
50	33	23	16	10	Set 8 Sun	15	19	25-33	

12.6

12.4	7.8	7.6	6.5	6.7	7.25	7.8	7.6	14.3	14.2
50	39	33	18	10	0	15	20	30	33

12.9

14.4	6.5	6.3	6.82	6.86	7.1	7.0	14.2	14.3	
40	24	Edge 18	10	Centerline 0	15	20	2.8	33	

8.6

14.3	13.8	4.8	6.7	6.43	6.4	6.5	11.3	11.2	
33	27	16	10	0	12.5	17	25	33	

7.7

Top curb 15'R Sta. 0+75

Sta. 0+50

" 0+50

" 1+10

" 1+10

Top curb R Sta. 2+32

Sp 24" Poplar 40'L Sta. 3+45

	5.03	868.63		863.60
0+00			4.9	863.73
24			4.9	3.73
48			4.8	3.83
72			4.8	3.83
96			4.9	3.73
1+20			5.0	3.63
+44			5.1	3.53
+68			5.0	3.63
+92			4.9	3.73
2+16			4.9	3.73
40			4.9	3.73
64			5.0	3.63
88			4.8	3.83
3+12			4.5	4.13
36			4.2	4.43
60			3.7	4.93
84			3.1	5.53
4+08			2.2	6.43
+32			1.2	7.43
T.P.	8.13	875.51	1.25	867.38
56			7.5	68.00
80			6.7	68.81
5+04			6.0	69.51
+28			5.2	70.31
+52			4.6	70.91
+76			3.8	71.71
			1.84	873.67

25

(23-56)

FINAL X-SECTIONS BORROW PIT

Pt. or Sta	+S	H.I.	- S	Elev.
B.M.	1184	247.62		238.78
0+00				
0+38.5				
0+21				
0+43.3				
0+84.3				
0+98.3				
1+09				
1+24				
1+43.3				
"A"				
"B"				
"C"				
T.P.	9.86	253.54	3.94	243.68
"C" +08' to "D"				
"D"				
"D" +08' toward "E"				
"D" +15' " "E"				
"E"				
"E" +17' toward "F"				

Note: - Sections for "F", "G", "H", "J", "K" same as "originals" - Prev. determ'd -

B.M. 204 251.50 ✓ 251.50

Deutsche, Johnson, Mahoney, Franke } Party.

L ℄ R.

See Bk. I.P. 75 for alignment Pls etc.

Nail Pow P. 36' L Sta. 29+30

8.2 — On Pav'g

8.5

6.9

5.4 — On Pav'g

4.5

3.3

2.3

1.9

+0.1

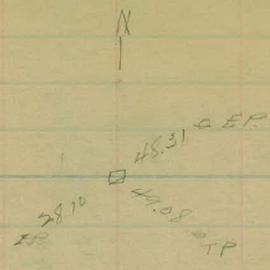
Top rock

4.5

3.9

See Note Left.

To Pow P. L. Sta. 22+60


N
45.31° ER
41.08° TP
38.1° EP