

Job N^o 7

No. Birch Lake Road

CO. PROJ. 23-56

FIELD BOOK

360

Office of Survey & Engineering

ST. PAUL, MINN.

Date filed

"2"

KEUFFEL & ESSER CO.

DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

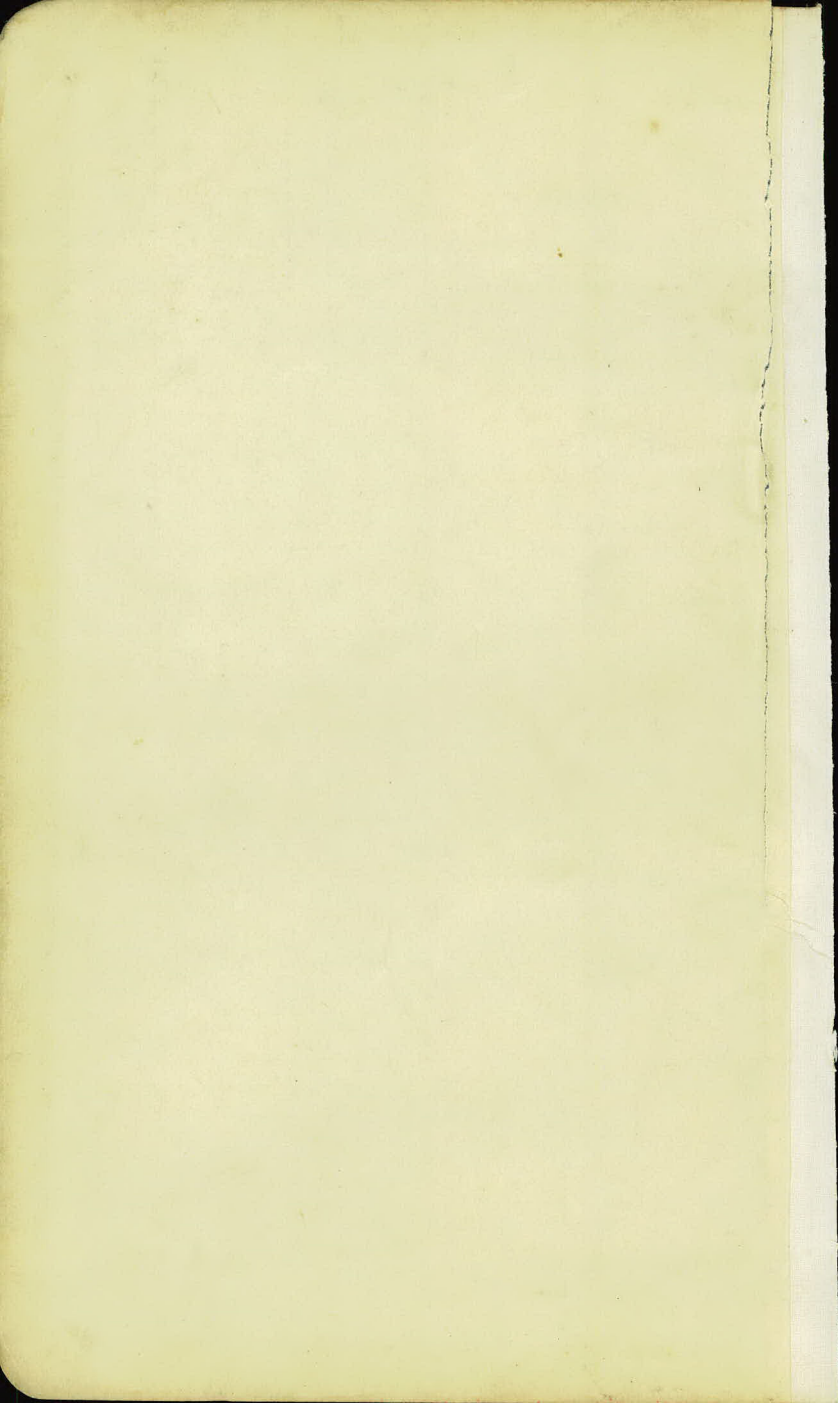
For Keith's Railroad Curve Tables see end of book.

462760

101009

911047
13+225
104,272

911047
26+01.4
117,461



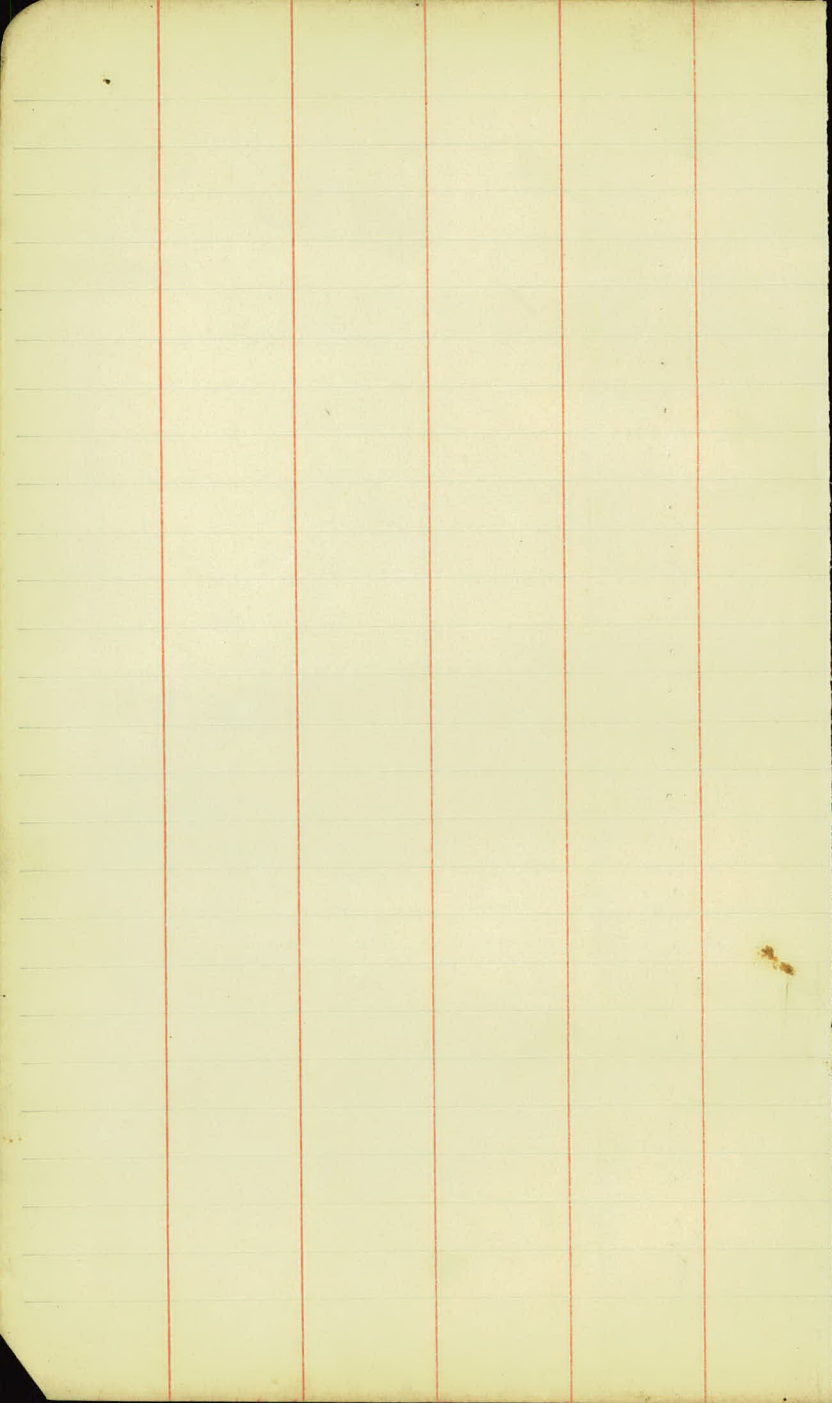
No. Birch Lake Road

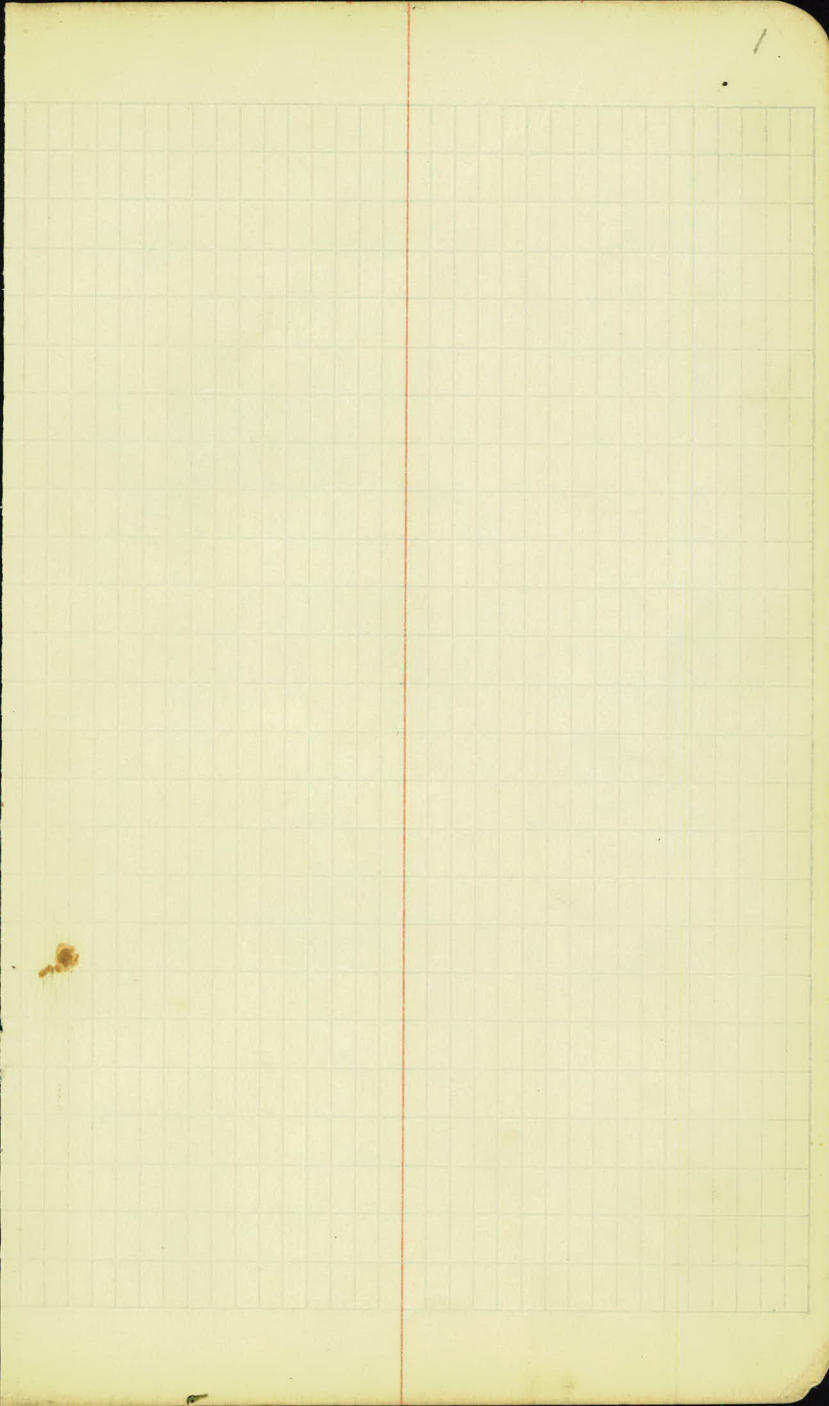
Proj. 23-56

~~Job. N-7~~

Index to Notes

Kind	Sta -	Sta.	Page -	Page
Alignment	0+00 -	117+44.9	2 -	6
Art. Topog	0+00 -	117+44.9	9 -	28
Culv. Notes			29 -	





B.h. line

Transit Notes

279.

Ang. R. Ang. h.

33+103 F.C.

31+96 P.I

40°40'

30+71 B.C.

26+17 F.C.

23+38 P.I

28°35'

20+47 B.C.

17+00 P.O.T

2+32 P.O.T

0+00 Mont Int. Birch Lake + Cent. Rd.

N. 55° - 50' E

X

S. 61° 30' E

N. 90° - 00' E

X

7-13-23

52-
49.4
41-

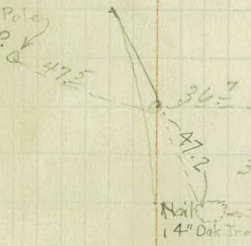
R.G. Austin Transit
Skycapin - Peeling - chain ✓
Johnson - Walsh. J. Carter - D. F. Day



Sta. Def.

- 80+71.1 - 0°00'
- 11+00 - 20°27'
- 24+00 - 10°57'
- 33+00 - 19°27'
- 44+10.2 - 20°20' ✓

L. Pole
T.P. ✓



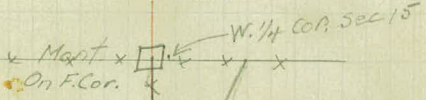
17° Curve, L
Δ = 40' 40"

BC = 80+71.1

Tree Length = 239.2 ✓

FC = 33+10.2 ✓

ST = 125.4 ✓



Sta. Def.

- 0+47.4 - 0°00'
- 11+00 - 10°19'
- 22+00 - 30°49'
- 33+00 - 60°19'
- 44+00 - 90°49'
- 55+00 110°19'
- 66+00 130°49'
- 76+17.4 140°15' ✓



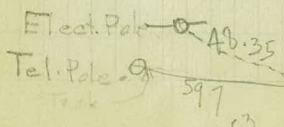
5° Curve, R.
Δ = 79° 30"

BC = 90+47.4 ✓

Length = 570.0 ✓

FC = 26+17.4 ✓

ST = 291.4 ✓



Stone at Surface

3" Dutch Apple Tr.

45.3

Sta

Ang. P. Ang. b

43+287 B.C.

N-61°-00'E

42+360 P.I 18°36'

X

41+427 B.C.



38+347 B.C.

N 42-24 E

36+917 P.I 35°26'

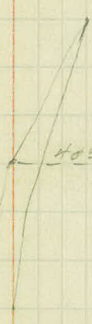
X

35+289 B.C.

N 77-50 E

~~E~~

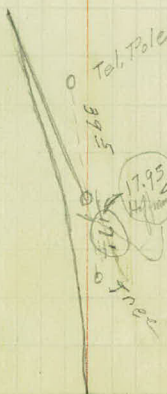
Sta.	Def
41+42.7	0°00'
42+00	2052'
43+00	7052'
43+287	90°18'



100 C. Right
 $\Delta = 18036'$
 $\checkmark S.T. = 93.9 \checkmark$
 $\checkmark B.C. = 41+42.7$
 $\checkmark \text{Length} = 186.0 \checkmark$
 $\checkmark E.C. = 43+287 \checkmark$

T.P.
63.7

Sta.	Def.
35+38.2	0°00' - B.C.
36+00	2040'
37+00	9040'
38+00	15040'
38+34.2	17043' F.C.



120 C. Left
 $\Delta = 35026'$
 $\checkmark S.T. = 152.8 \checkmark$
 $\checkmark B.C. = 35+38.2$
 $\checkmark \text{Length} = 295.3 \checkmark$
 $\checkmark E.C. = 38+34.2 \checkmark$

17.95
14.15
to trees

Sta.

Ang. R. Ang. h

514318
65280

55+86±

E.C. ✓

S 56° 39' E

54+72±

P.I

110±'

S 56° 15' E

53+58±

B.C. ✓

52+77±

E.C. ✓

51+55±

P.I

38° 24'

X

50+86±

B.C. ✓

(Long Sta. 47 to 48 = 97.1')
Equation Sta. 47+82. = 47+76.2

47+79±

E.C. = 47+82.0 ✓

S 17° 51' E

46+76±

P.I

1010±'

X

~~44+33±~~

B.C.

44+33± B.C. ✓

N 61° 00' E

4

Sta - Def.

- 53+58± = 0000'
- 54+00 = 1002'
- 55+00 = 2092'
- 55+86± = 5042' ✓

14111

5° Curve left.

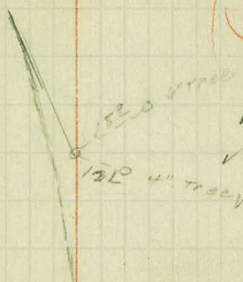
$\Delta = 11024'$

✓ S.T. = 114± = 114.4

✓ B.C. = 53+58± ✓

✓ Length = 2280 ✓

✓ E.C. = 55+86± ✓



Sta. Def.

- 50+95 = 0+00
- 51+00 = 1030'
- 52+00 = 11030'
- 52+77± = 19012' ✓

20° Curve left

$\Delta = 39020'$

✓ S.T. = 100.27 ✓

✓ B.C. = 50+95

✓ Length = 192.0 ✓

✓ E.C. = 52+77.0 ✓



Sta. Def.

- 44+80± - 000'
- 45+00 - 100075
- 46+00 - 240375
- 47+00 - 390075
- +79' - 50035'

Corrected in Field
3/9/23
P.R.B.

29° C. Right.

$\Delta = 101009'$

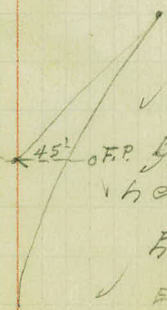
✓ S.T. = 245± = 242.9

✓ B.C. = 44+80±

✓ Length = 348.9 ✓

✓ E.C. = 47+79' ✓

✓ EC = 47+82.0



Sta.

Ang. R. Ang. L.

63+46⁴ E.C. ✓

63+00¹ P.I. 24° 41'

62+51⁵ B.C. ✓

62+08⁰ E.C. ✓

61+13² P.I. 53° 56'

60+00⁶ B.C. ✓

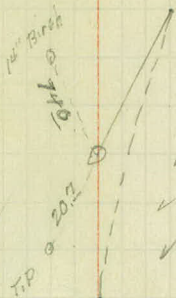
56+96⁵ E.C. ✓

56+50⁴ P.I. 13° 55'

56+03² B.C. ✓

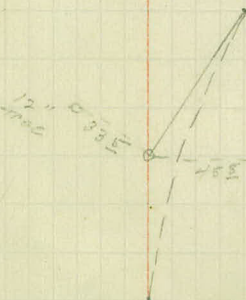
S 2° 57' E ✓
X
S 21° 38' E ✓
X
S 81° 34' E ✓
X
S 67° 39' E ✓

Sta.	Def.
62+51.5	$= 0^{\circ}00'$
63+00	$= 6^{\circ}18'$
63+46.4	$= 12^{\circ}20\frac{1}{2}'$



26° Curve, R.	
Δ	$= 24^{\circ}41'$
✓ S.T.	$= 48.63 \checkmark$
✓ B.C.	$= 62+51.5 \checkmark$
✓ length	$= 94.93 \checkmark$
✓ E.C.	$= 63+46.4 \checkmark$

Sta.	Def.
60+00.6	$= 0^{\circ}00'$
61+00	$= 12^{\circ}55'$
62+00	$= 25^{\circ}55'$
62+08	$= 36^{\circ}58'$



26° Curve, R.	
Δ	$= 53^{\circ}56'$
✓ S.T.	$= 113 \checkmark$
✓ B.C.	$= 60+00.6 \checkmark$
✓ length	$= 207.4 \checkmark$
✓ E.C.	$= 62+08 \checkmark$



15° Curve-L	
Δ	$= 13^{\circ}55'$
✓ S.T.	$= 46.7 \checkmark$
✓ B.C.	$= 56+03.7 \checkmark$
✓ length	$= 92.5 \checkmark$
✓ E.C.	$= 56+96.5 \checkmark$

B.h. pine
Ang. R. Ang. h.

Sta.

117+44² P.O.T. E Bald Eagle Ave

91+04² P.O.T

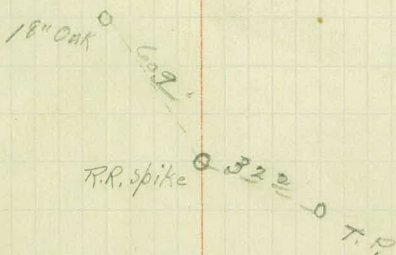
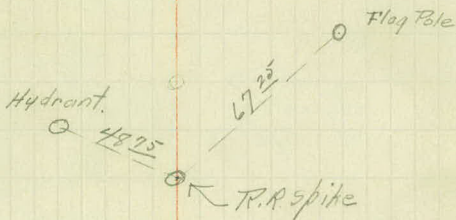
69+57⁴ E.C.

68+46⁹ P.I. 86°47'

66+58' B.C.✓

S 89° 44' E
S 22° 57' E

R. E. Austin - Transit
 Choctaw - Reiling - Chain
 Walsh - Stake Point
 Johnson - Rear Flag

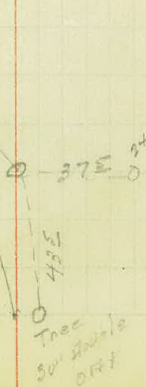


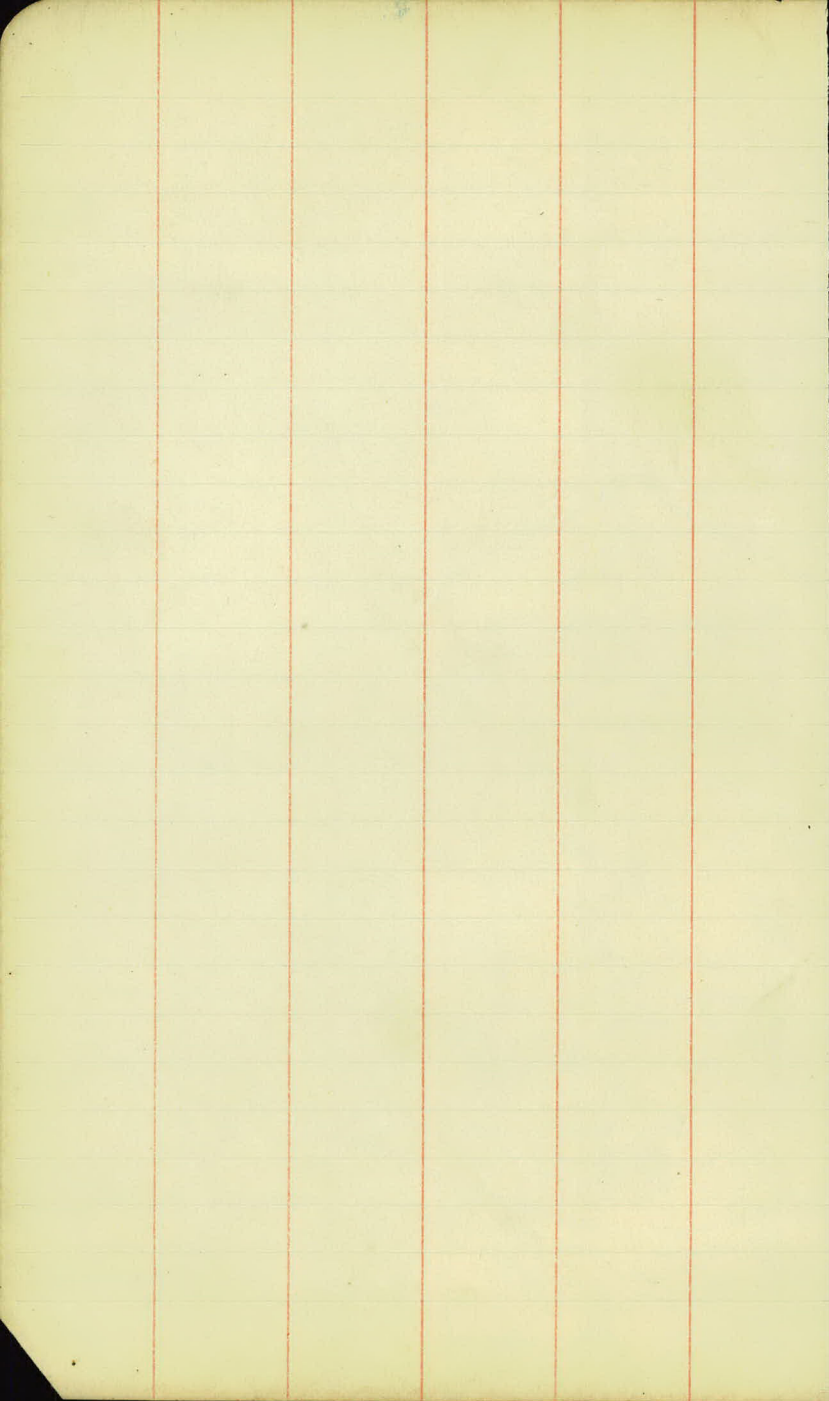
Sta. Def.

66+58± = 0°00'
 67+00 = 60°04 1/2'
 +50 = 130°19 1/2'
 68+00 = 200°34 1/2'
 +50 = 270°49 1/2'
 69+00 = 350°04 1/2'
 69+57± = 430°23 1/2'

90° Curve h

$\Delta = 86^{\circ}47'$
 \checkmark S.T. = 188.8 \checkmark
 \checkmark B.C. = 66+58± \checkmark
 \checkmark length = 299± \checkmark
 \checkmark E.C. = 69+57± \checkmark





FIFTH ST.

Mon. Found.

13175

1319.94

89509. 90001

33

EAGLE AVE

1322.07

672.65' 0' Tol. of Pole

Not Found Replaced with RR Spike

Hydrant

1322.5

BIRCH LAKE AVE

890525

18" OAK

1318.92

60' 0"

33

32.1/32.1' Tel. Pole

2641.42

BALD

1322.07

89001.33

90016

Mon. Not Found

2635.8

B. h. Line
Artificial Topography

228-23

R.K. Hastin
Stooplin - Reitroy } chain.
Walsh. - Johnson }

.9

West

Right

6+00

Callivated Land

Cultivated Land

5+00

4+00

3+00

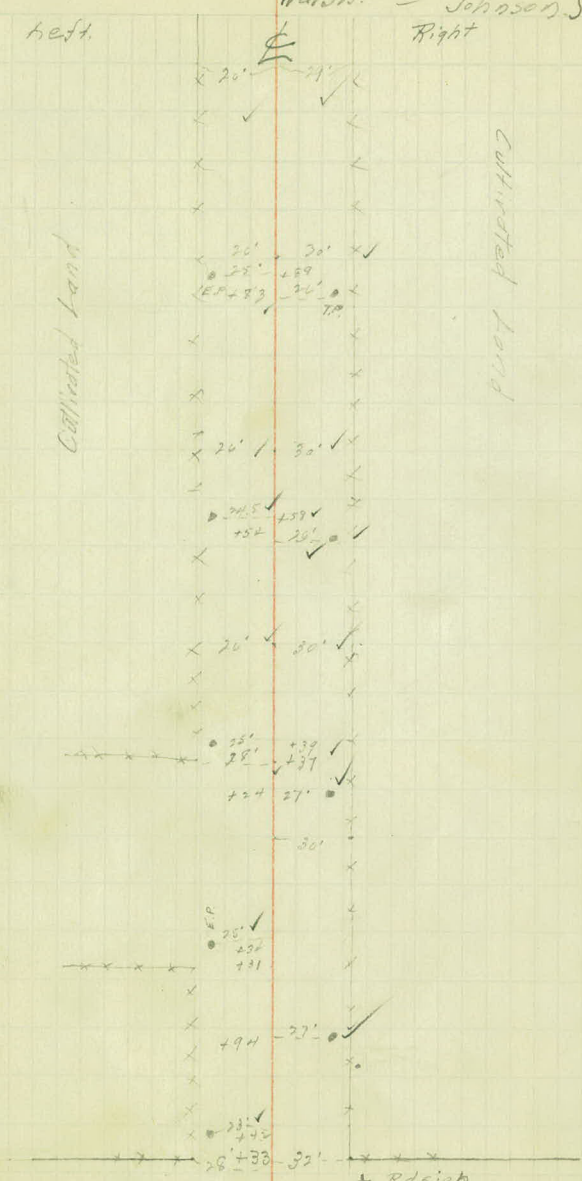
2+00

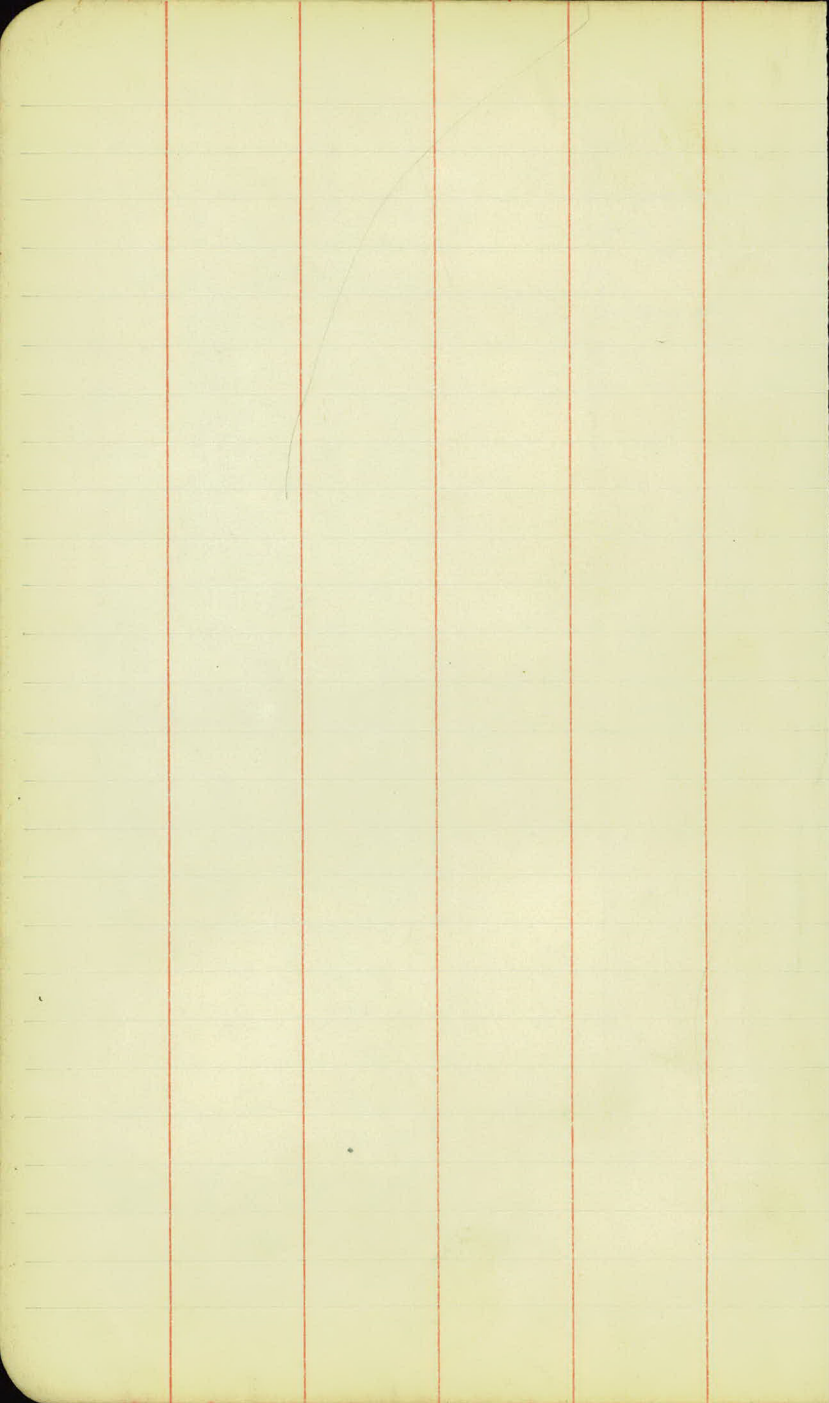
1+00

0+00

Centerville

Rdsigh
Road





Left

E

Right

x 25' - 27' ✓

12+00

x
x
x +44 25' 0 ✓

x 24' - 25' ✓
x 23' - 24' ✓

11+00

x
x
x

x
x +14 25' 0 ✓
x 20' - 21' ✓

10+00

x 23' - 24' ✓
x
x

x 24' - 25' ✓

9+00

x 26' - 25' ✓
x 24' - 25' ✓

x
x 22' - 23' ✓
x 28' - 29' ✓

8+00

x +77 26' 0 ✓

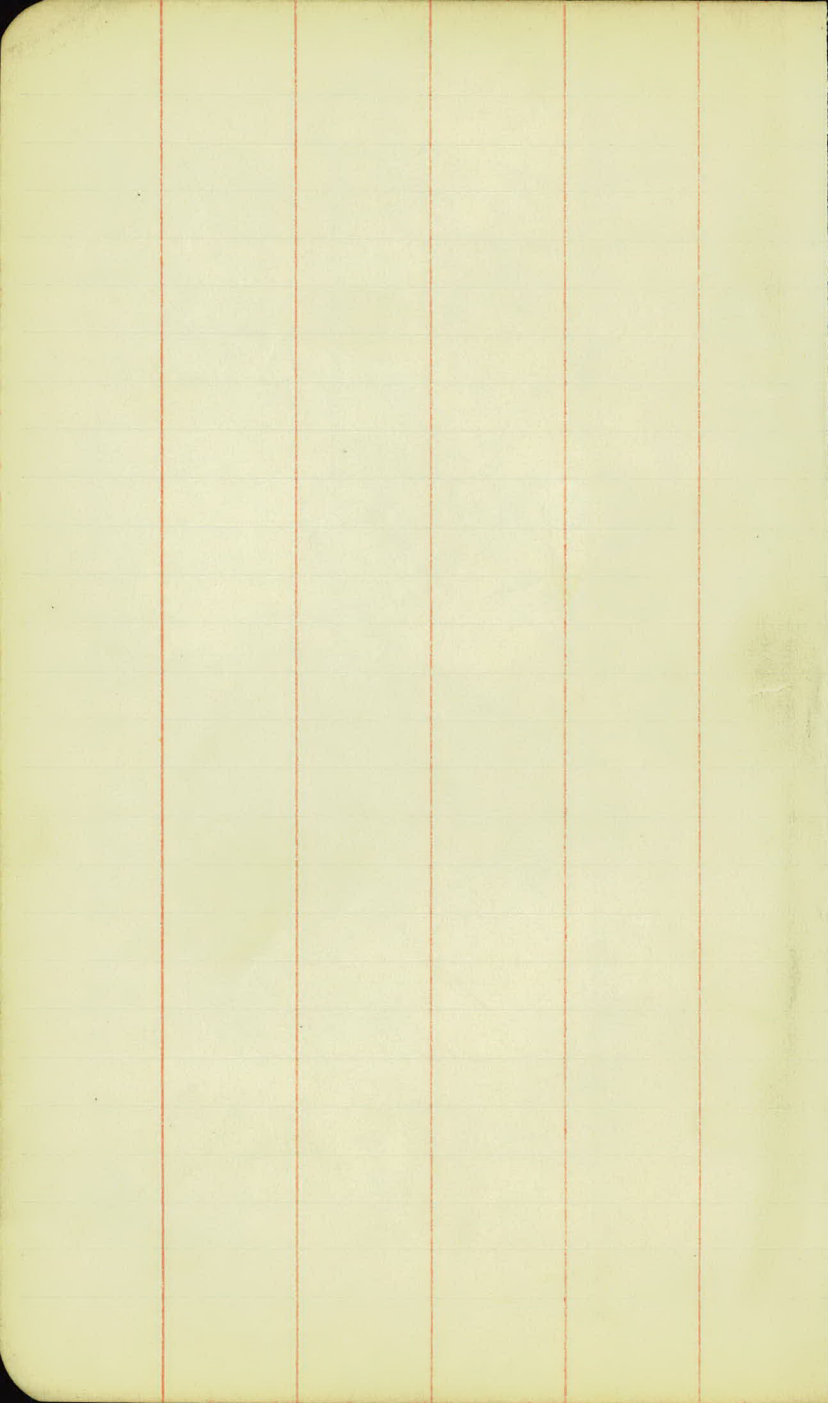
x
x 24' - 25' ✓
x

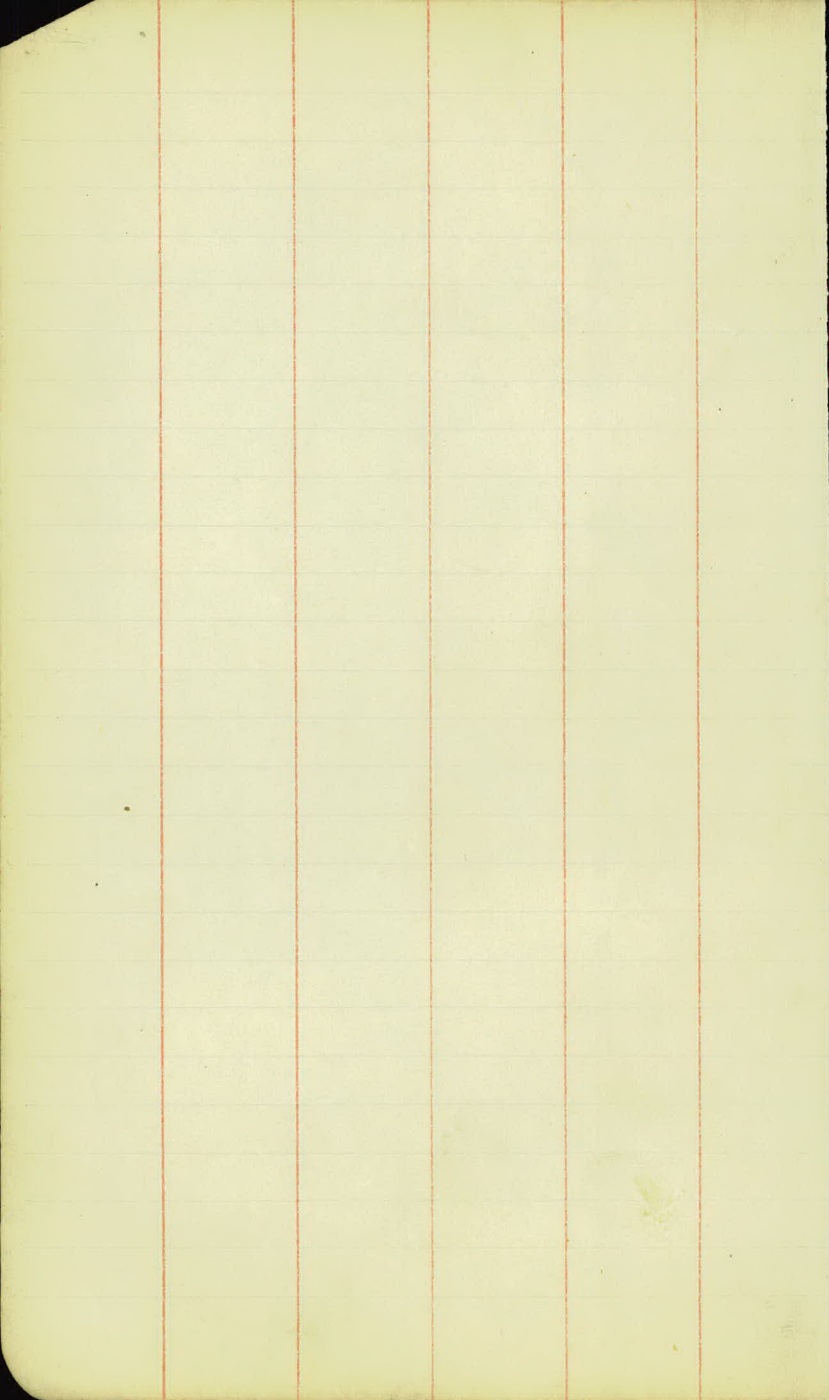
x 25' - 29' ✓

7+00

x
x
x
x
x 20' + 18 25' 0 ✓

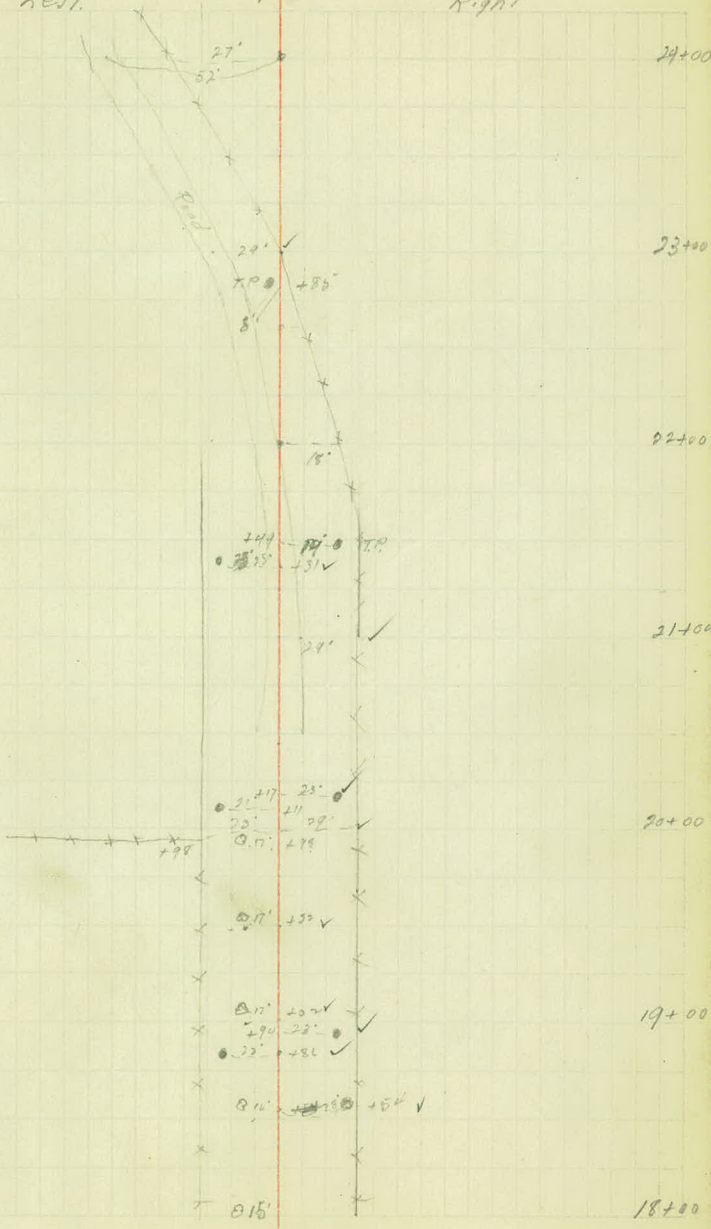
6+00

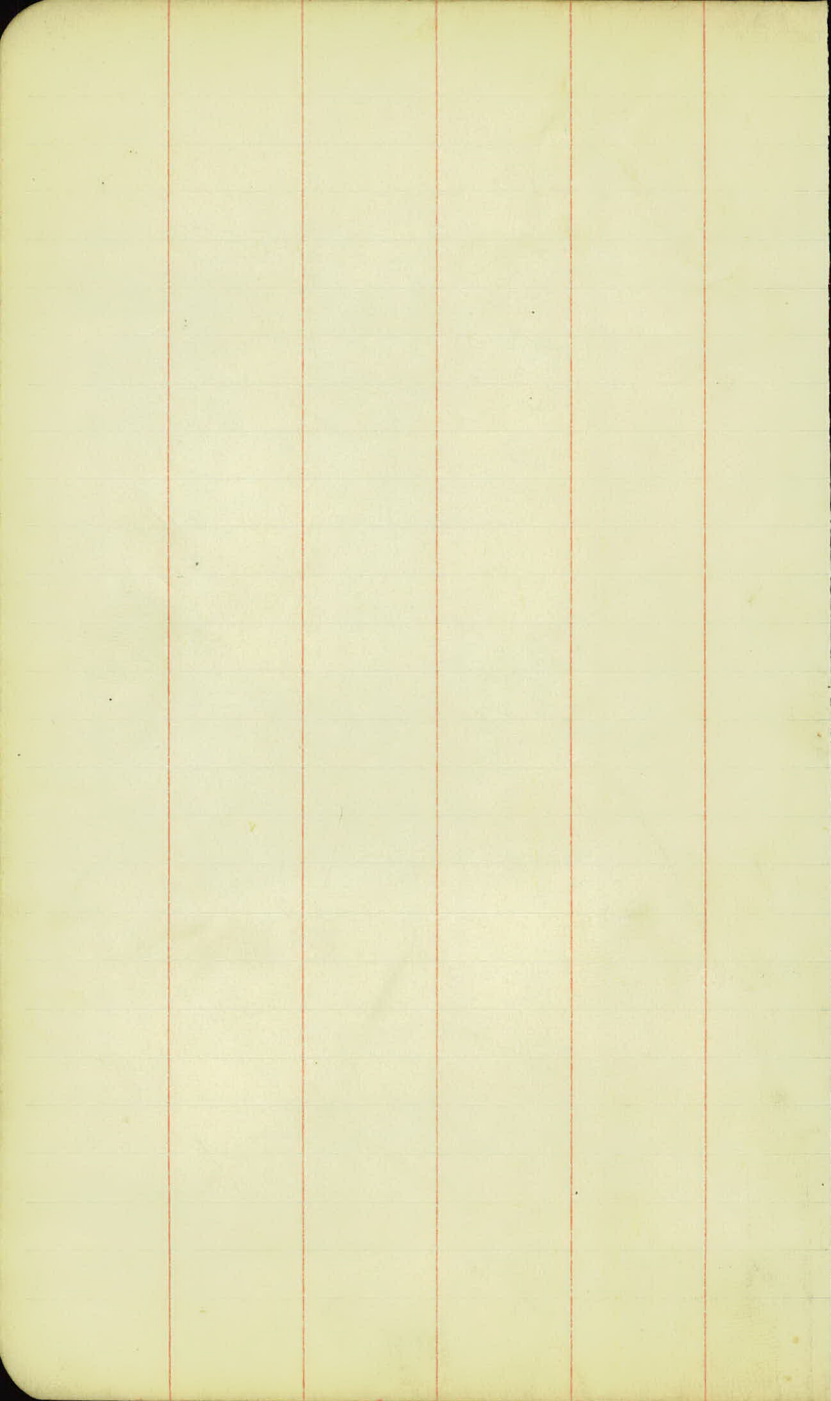


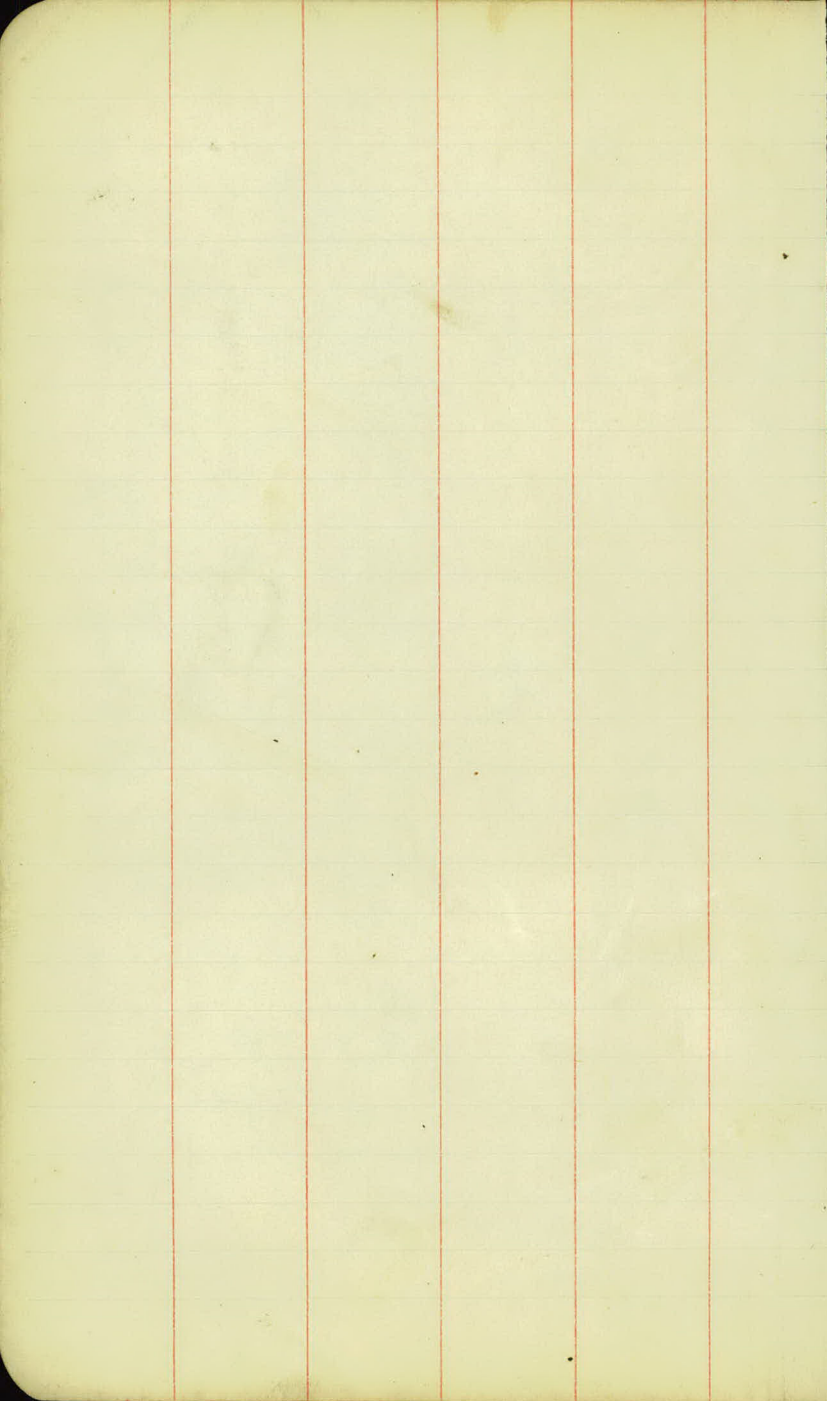


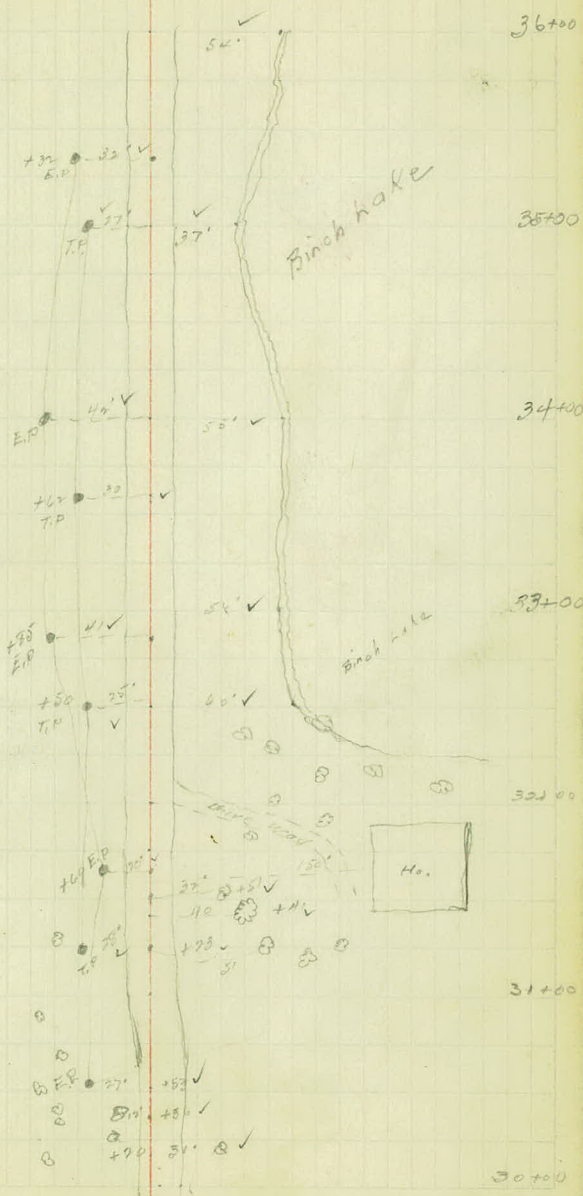
Left

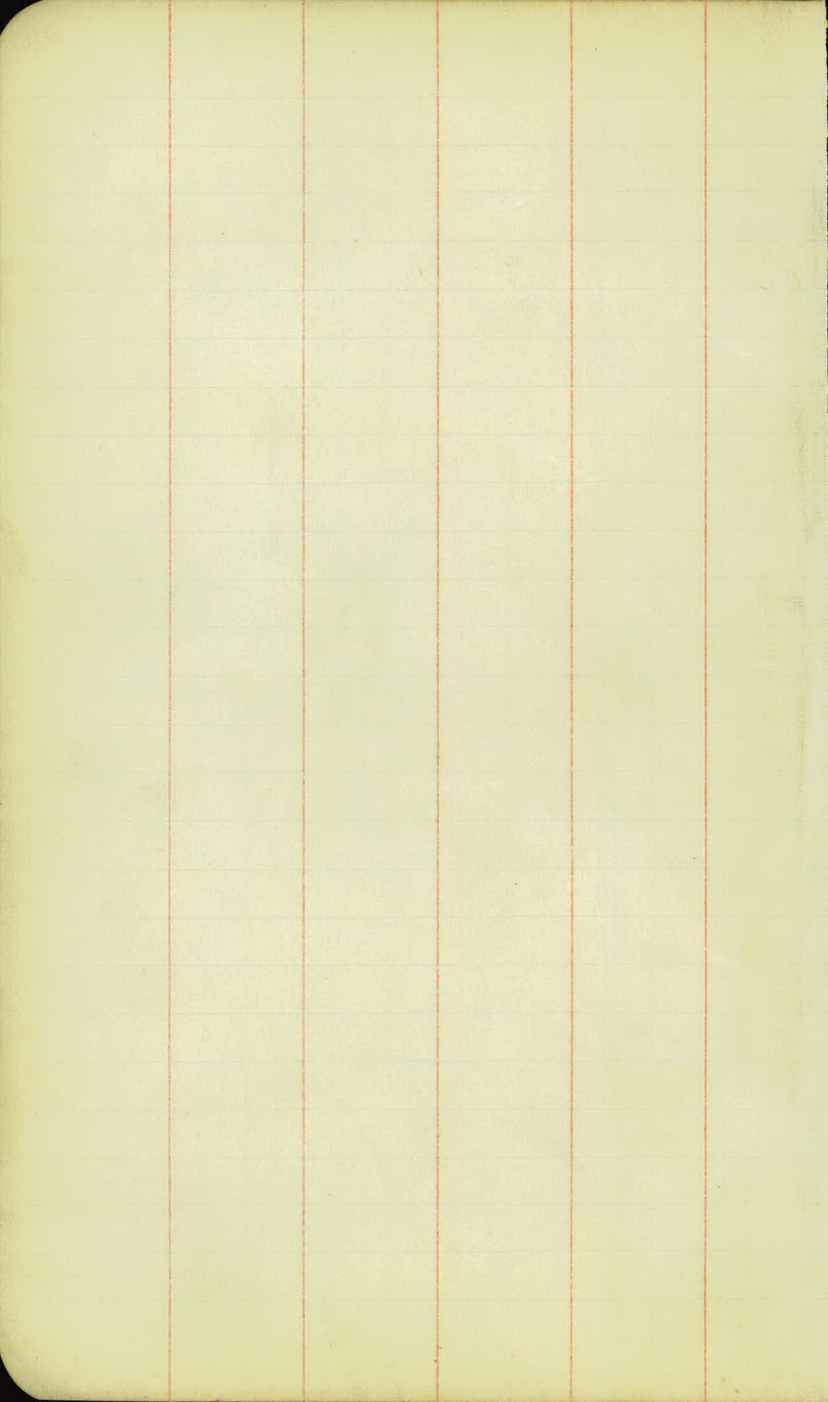
Right

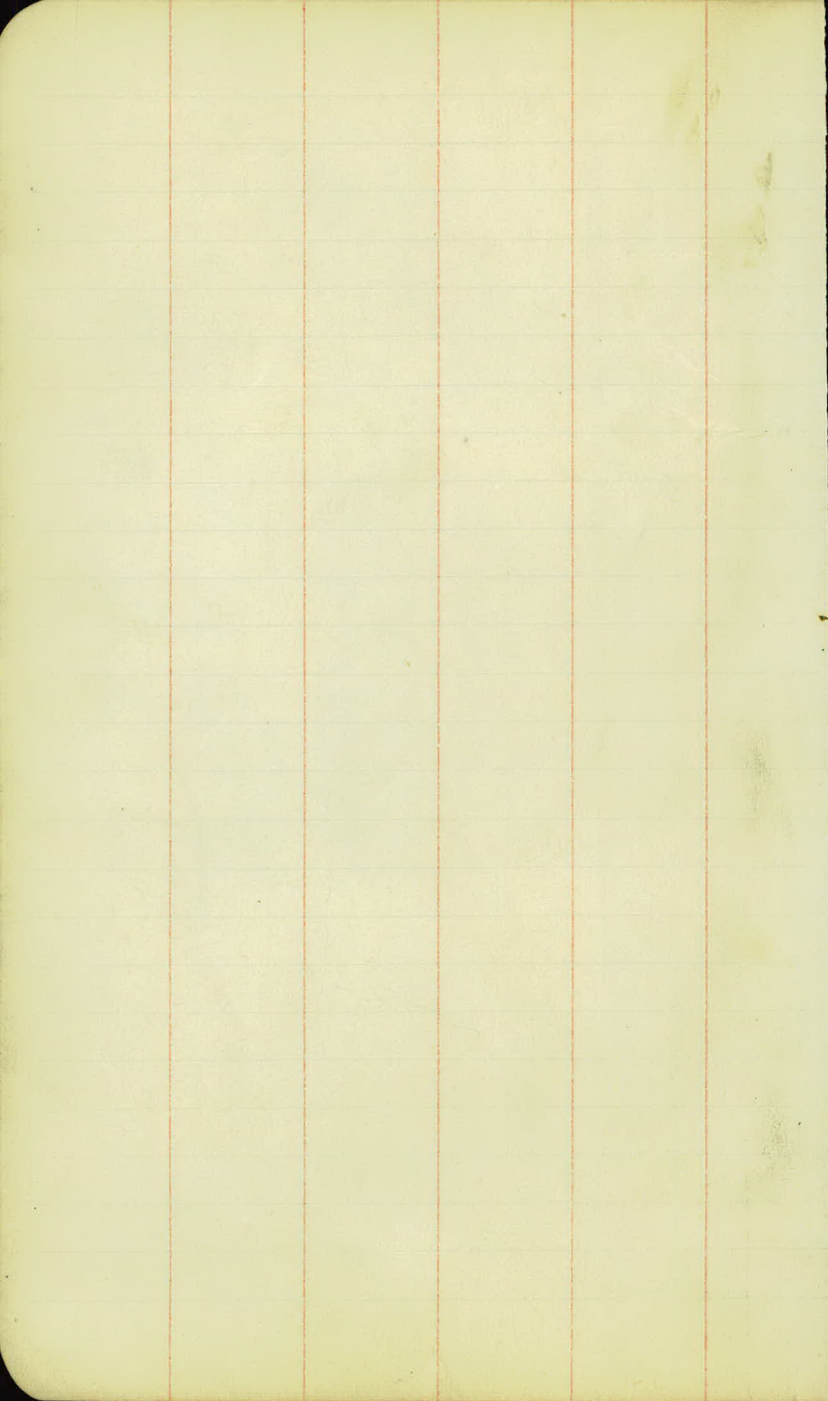


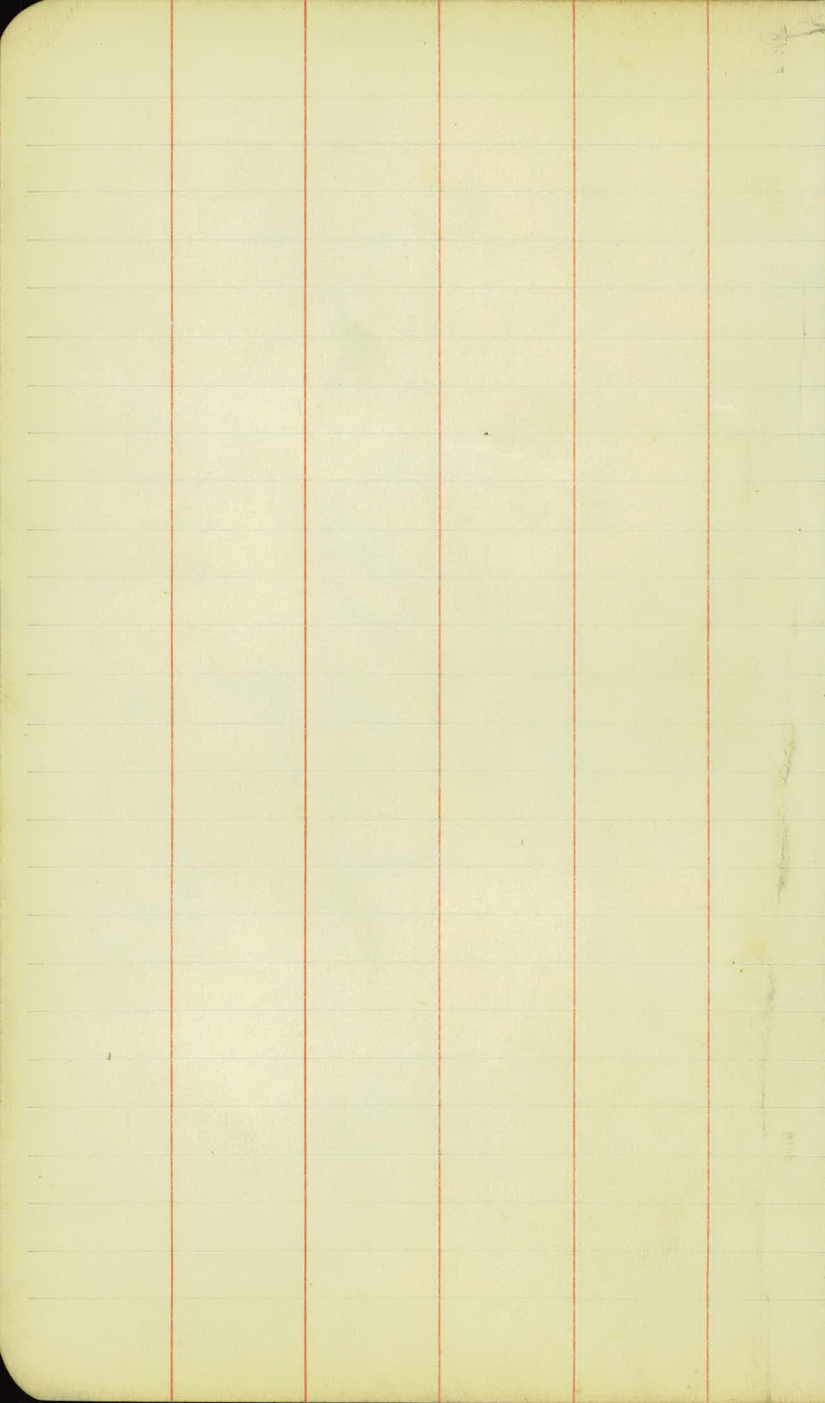


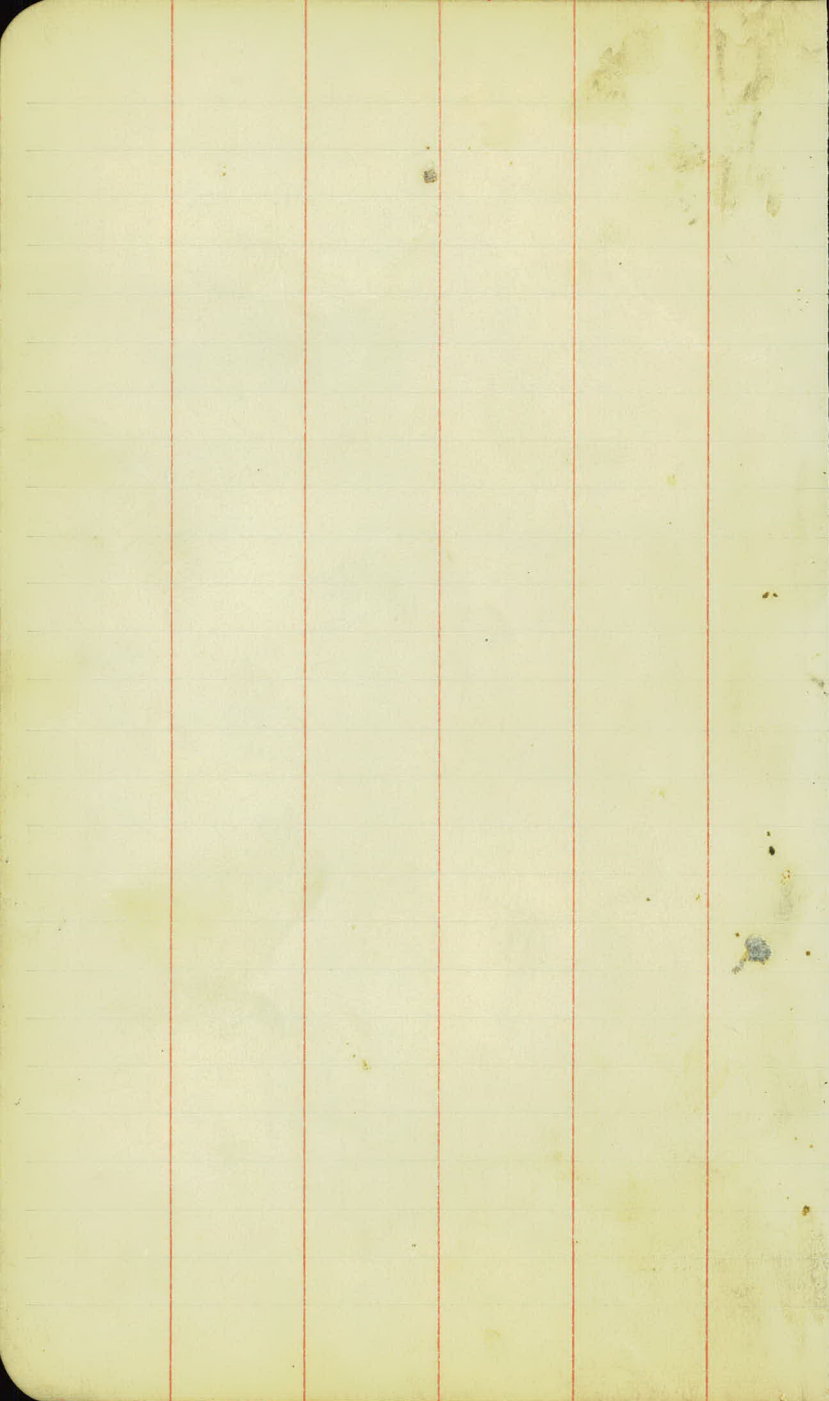












60+00

59+00

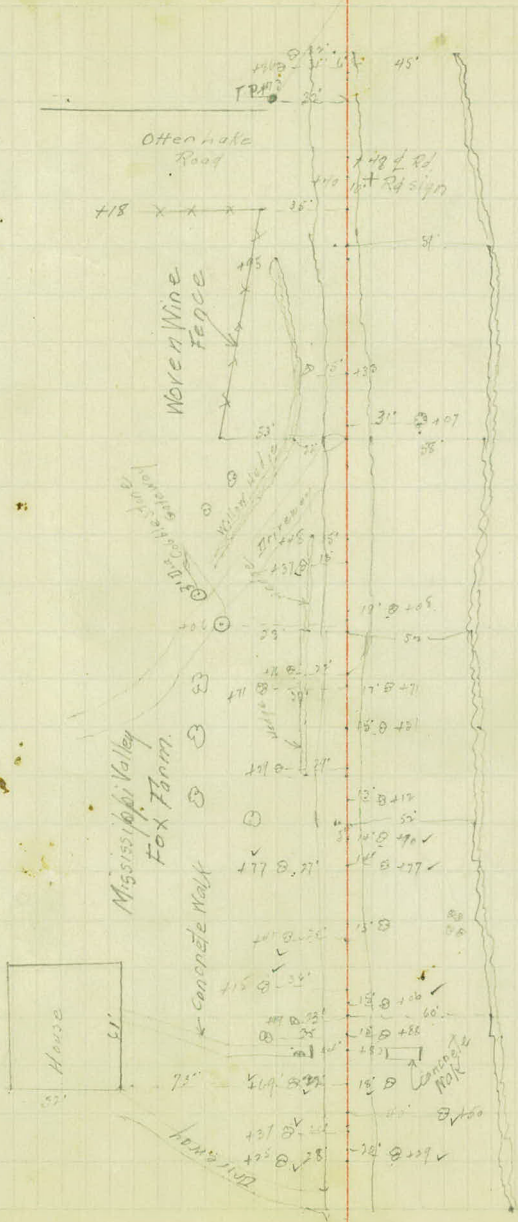
58+00

57+00

56+00

55+00

54+00



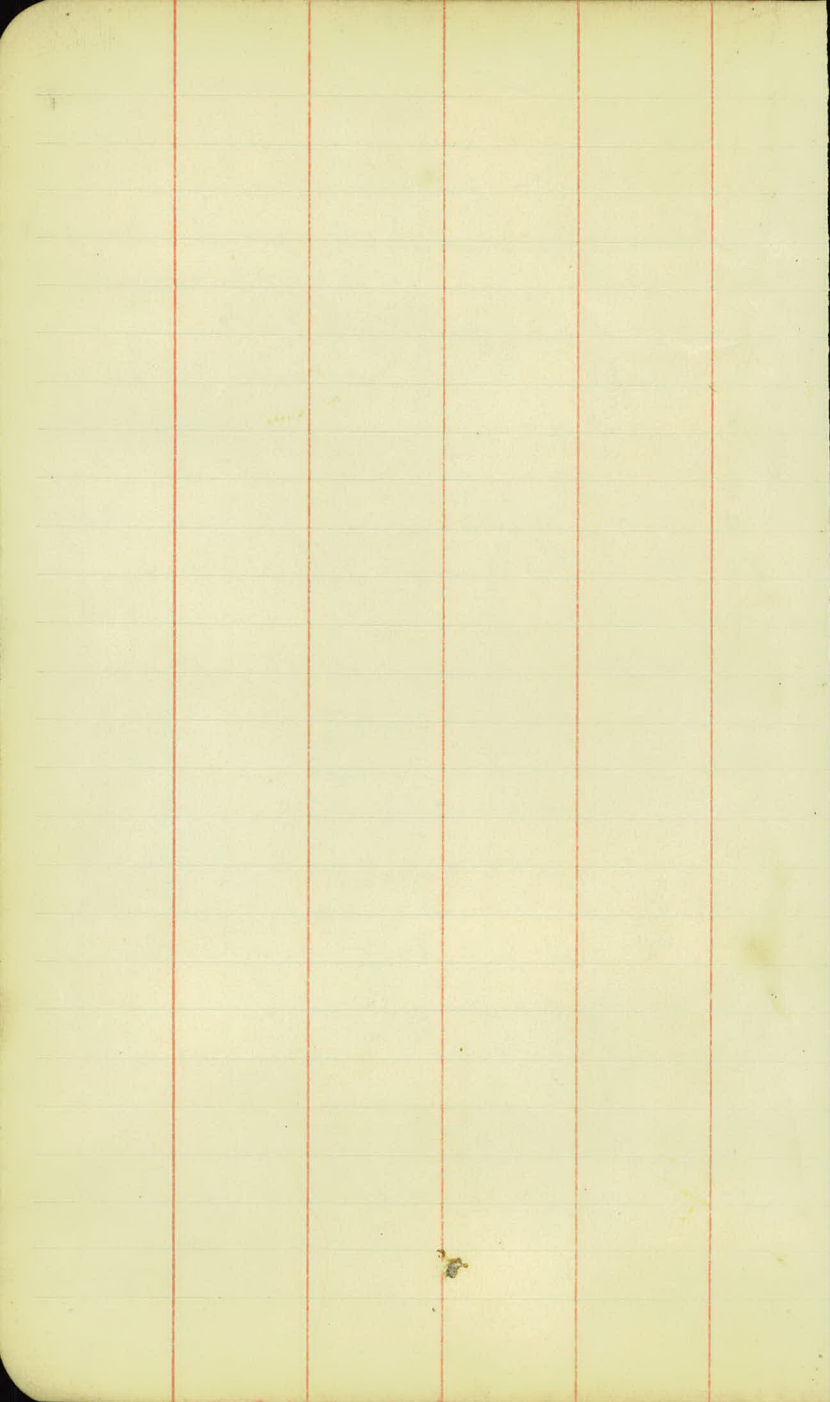
Birch Lake

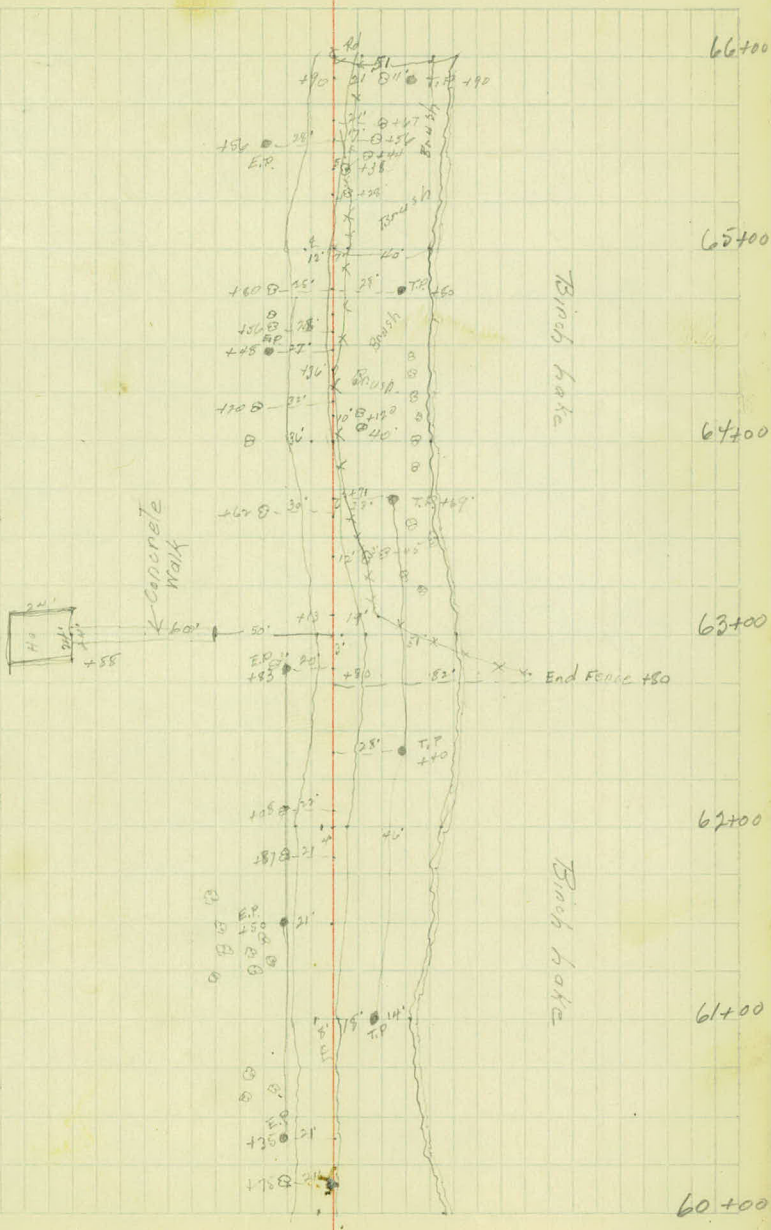
Mississippi Valley Fox Farm

Concrete Walk

House

100' 100'





Concrete Walk

Birch Lake

Birch Lake

66+00

65+00

64+00

63+00

62+00

61+00

60+00

End Face +80

E.P.

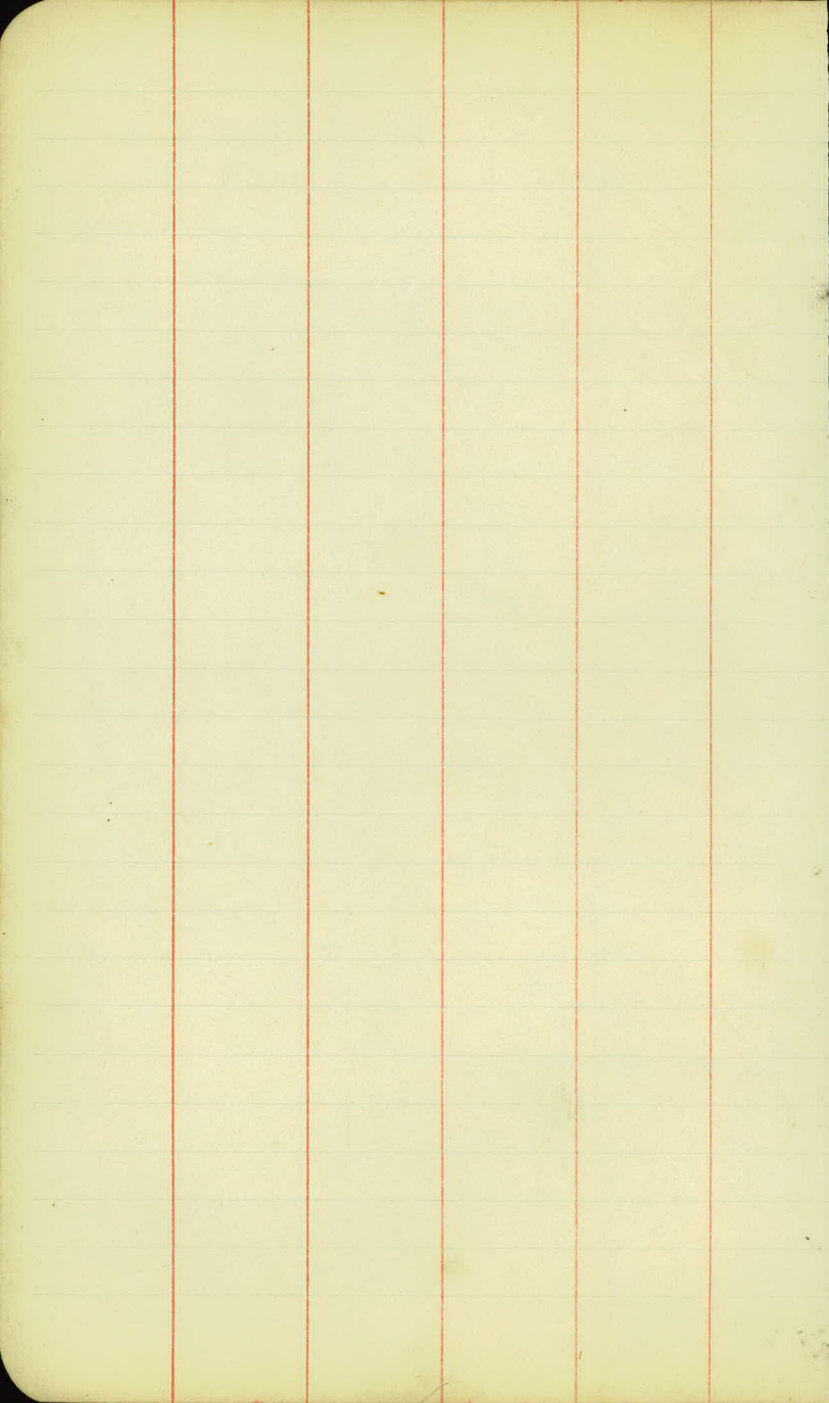
E.P.

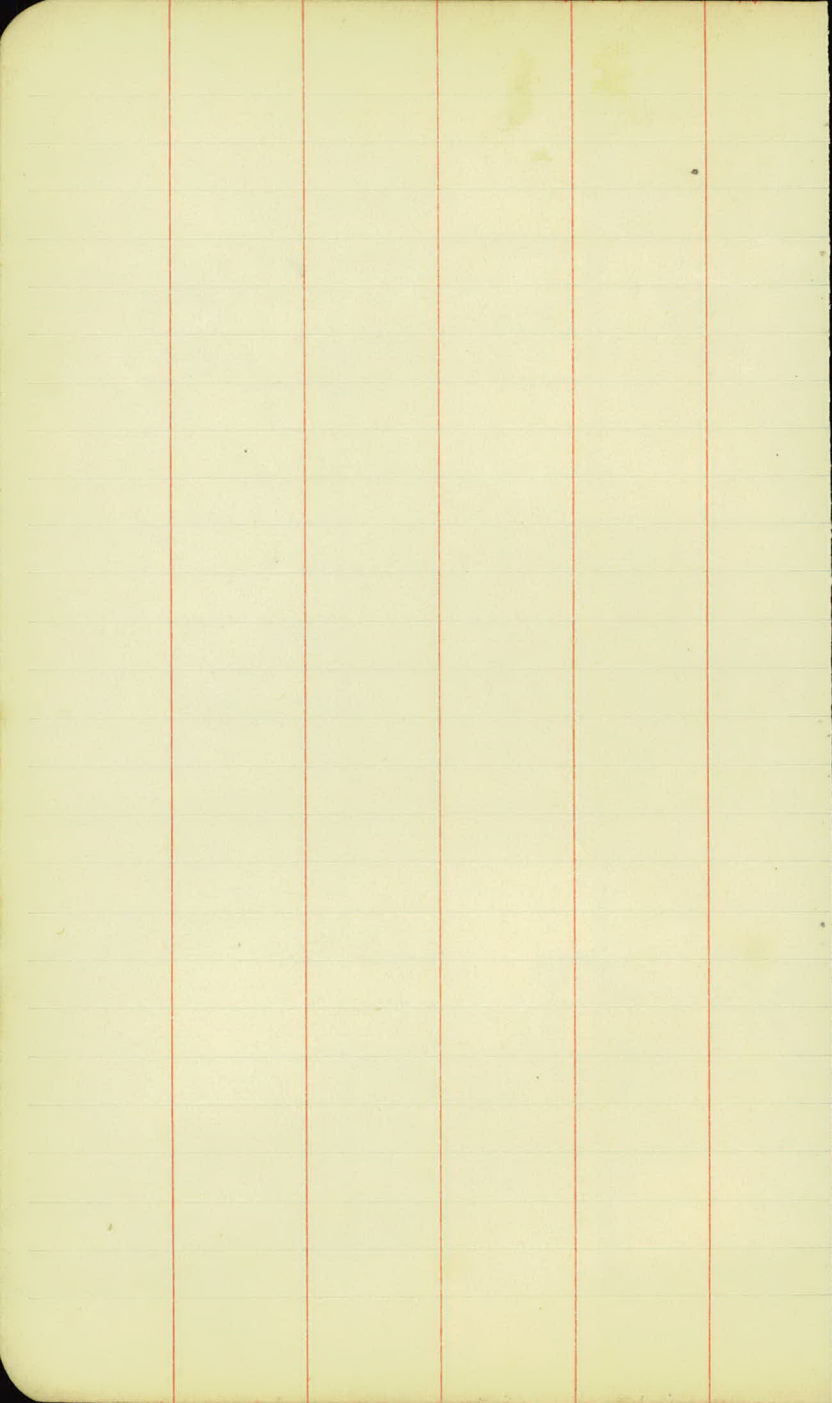
Ad

T.P.

T.P.







5' E.Rd.

78+00

+86 27'

36" ⊕ 24' +47

• 22' +02

77+00

+57 27' • Tel. Pole

76+00

Ele. Pole • 22' +70

+26 27'

75+00

• 22' +36

74+00

+97 27'

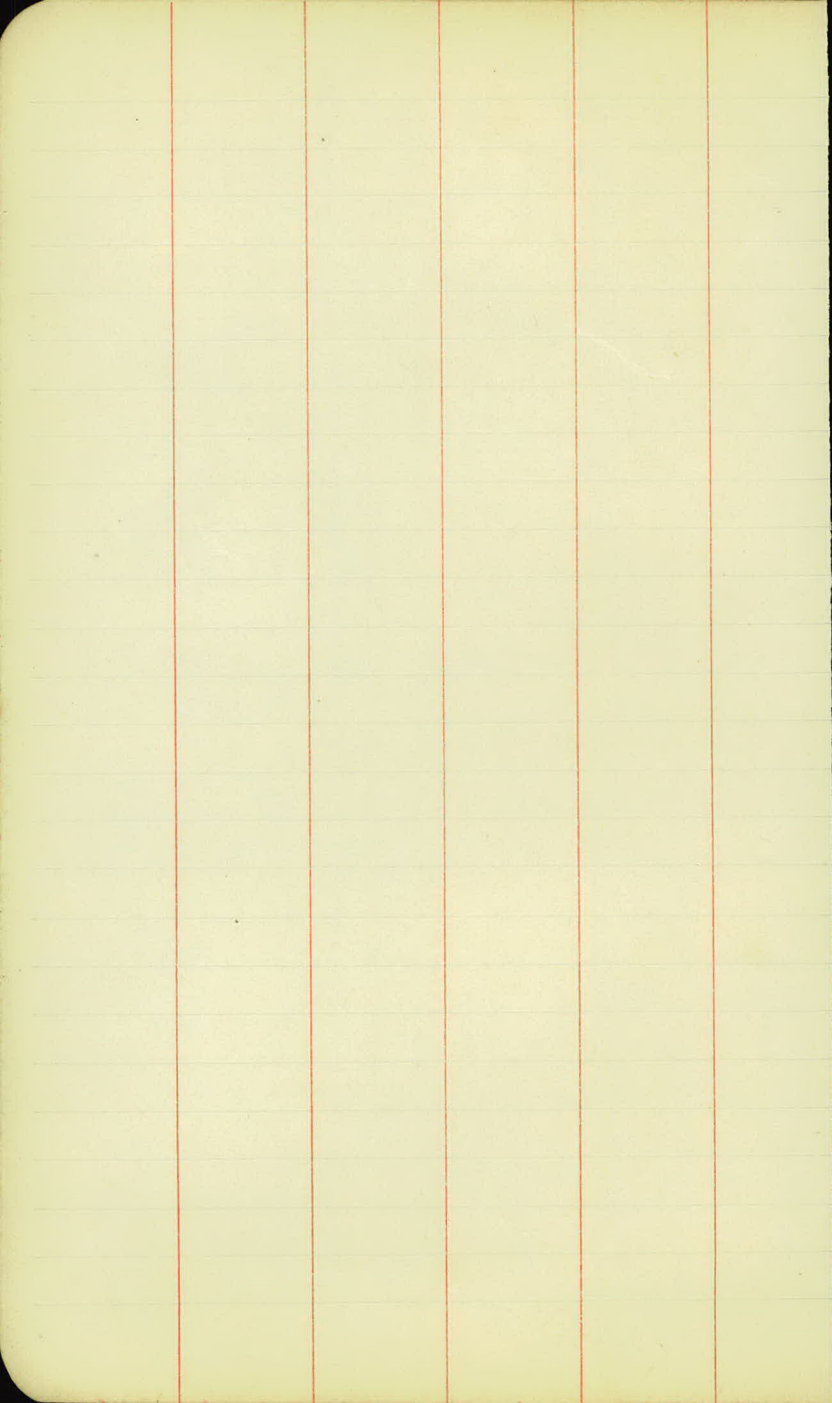
73+00

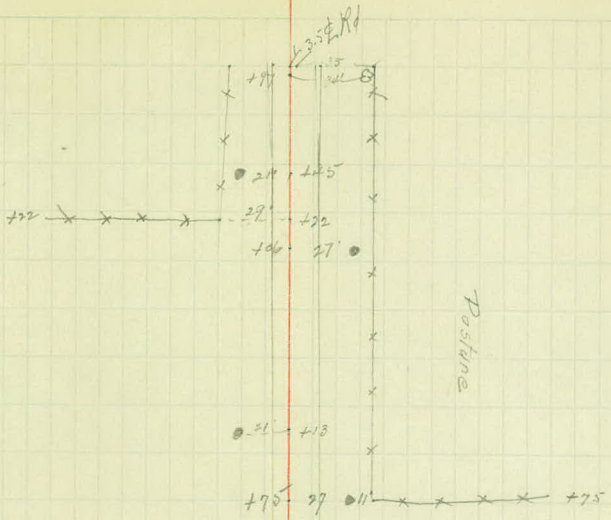
• 22' +02
E.P.

+63 27' • Tel. Pole

72+00

4' E.Rd.





84+00

53+00

52+00

51+00

50+00

49+00

78+00

Postline

Comp. field

Comp. Field

puoy palpatipno

3 1/2 Rd

5 1/2 Rd

E.P. 21' +85

+43 27' • T.P.

• 22' +58

+19 21' •

• 22' +30

+22

+75

+75

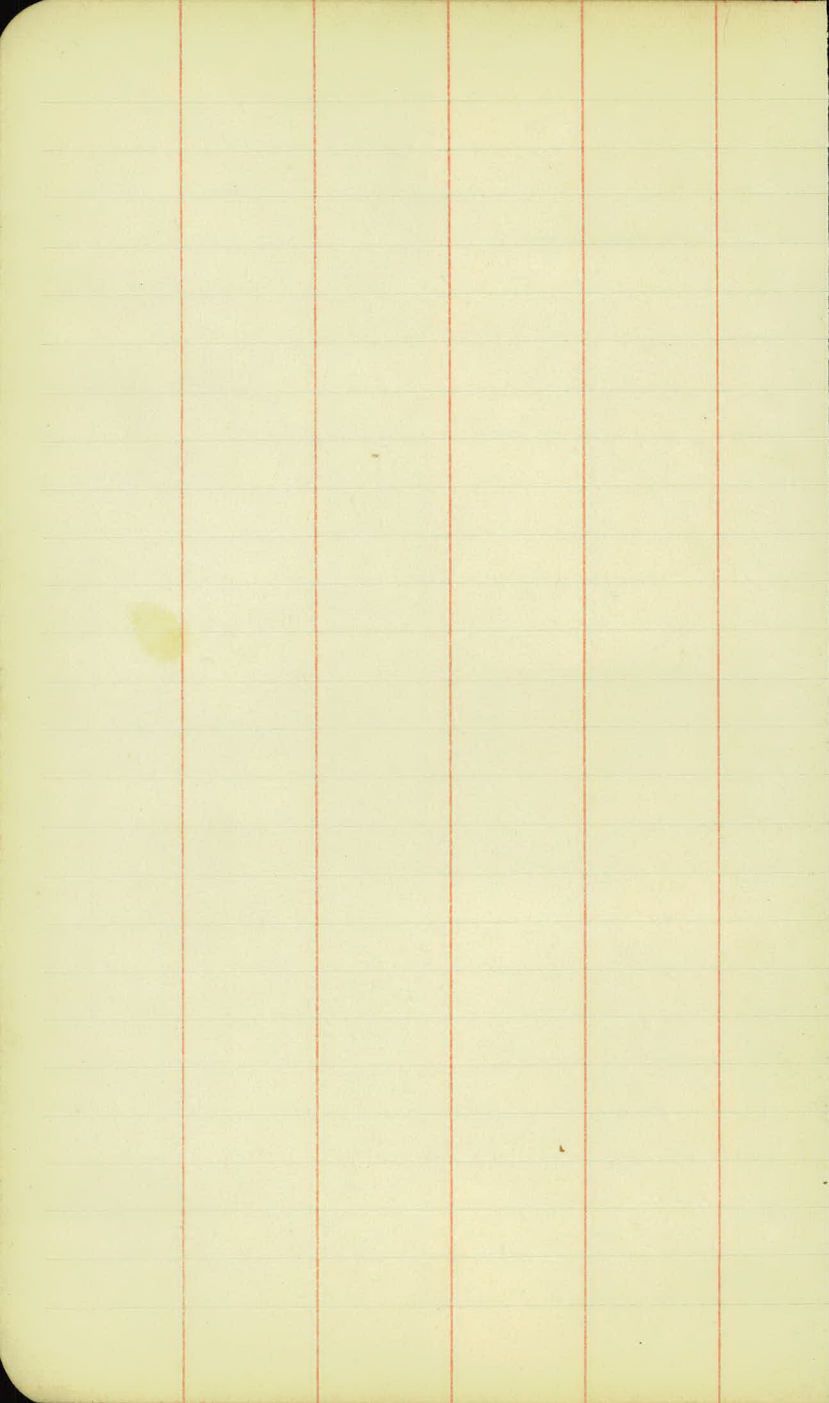
+25

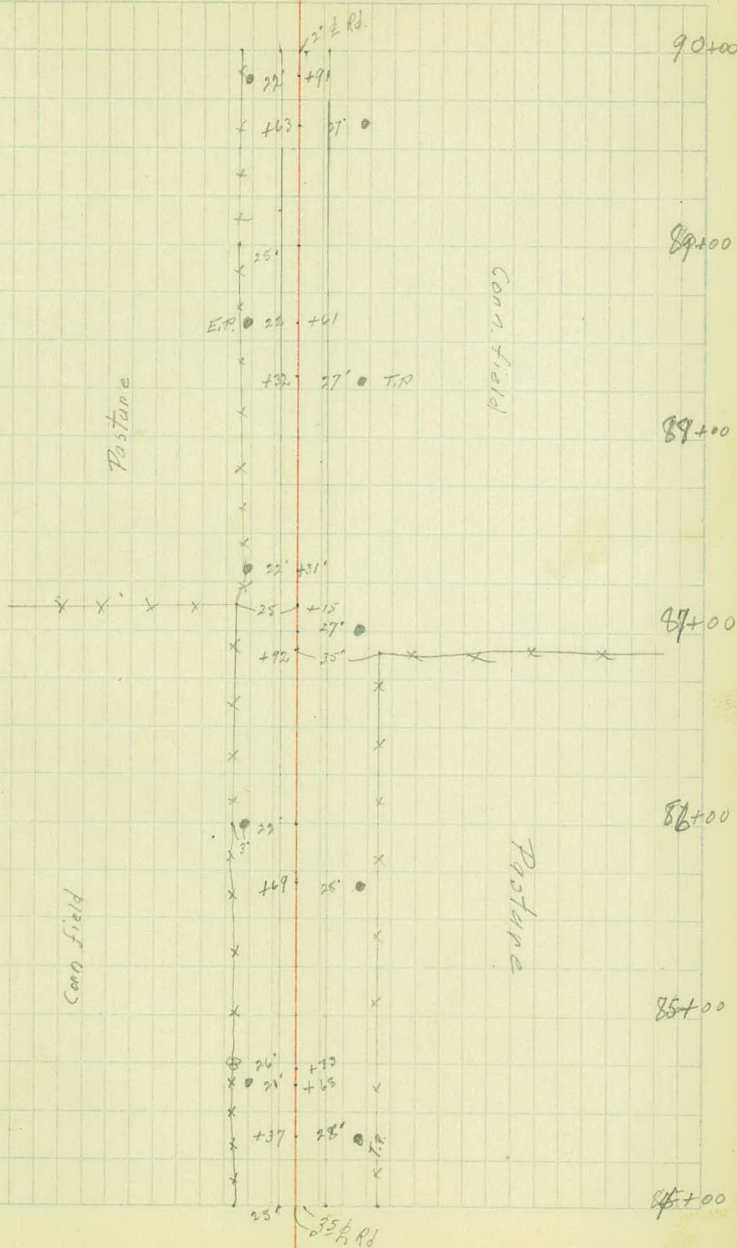
+22

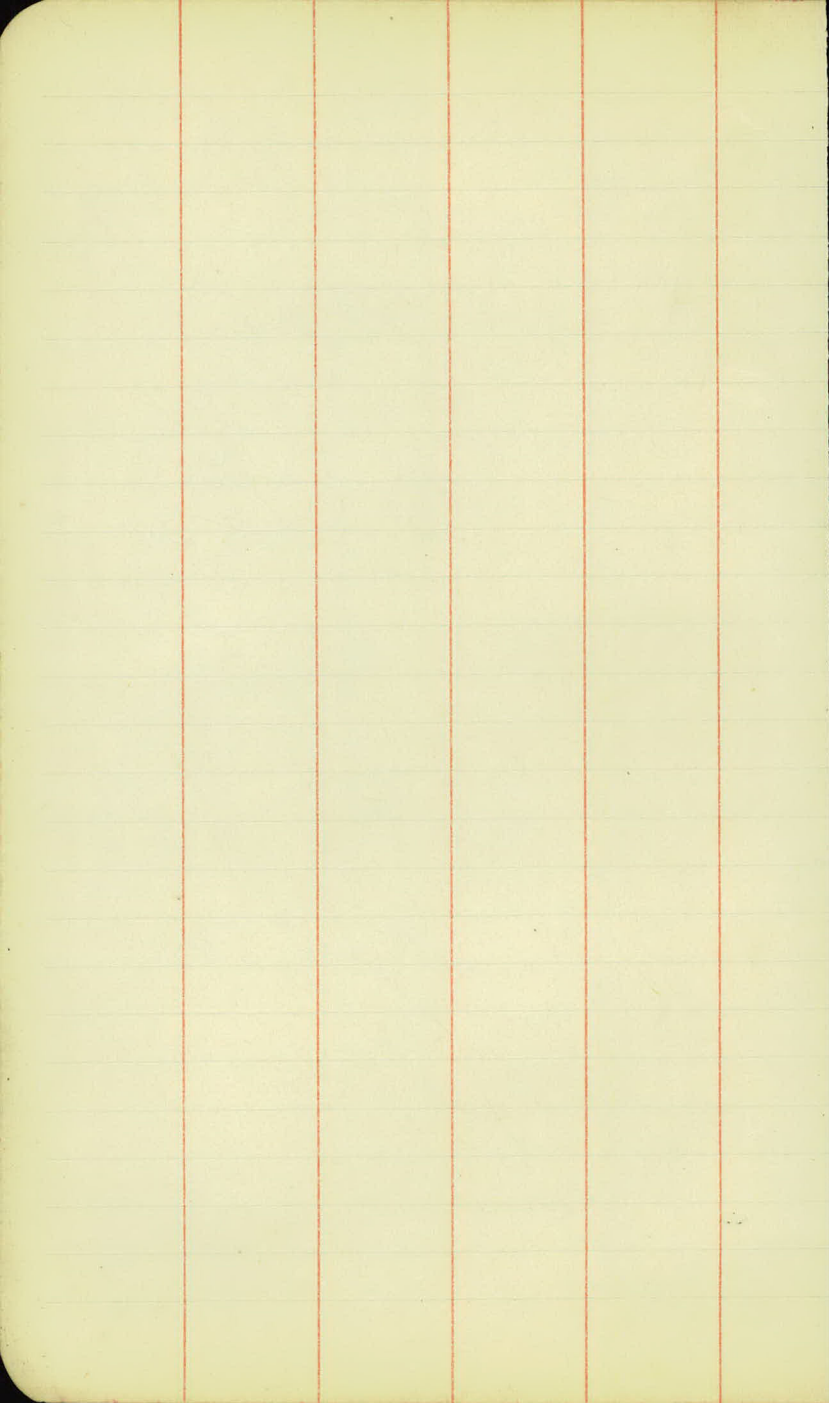
+27

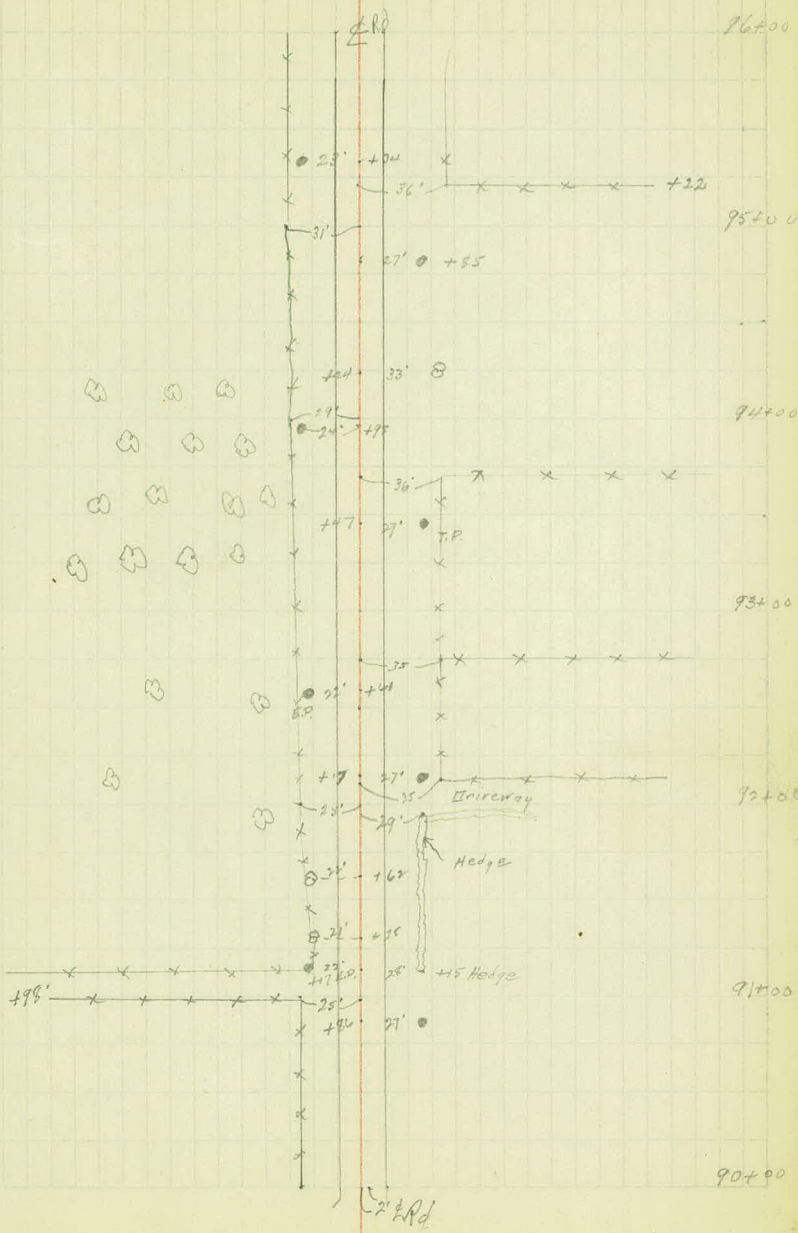
+13

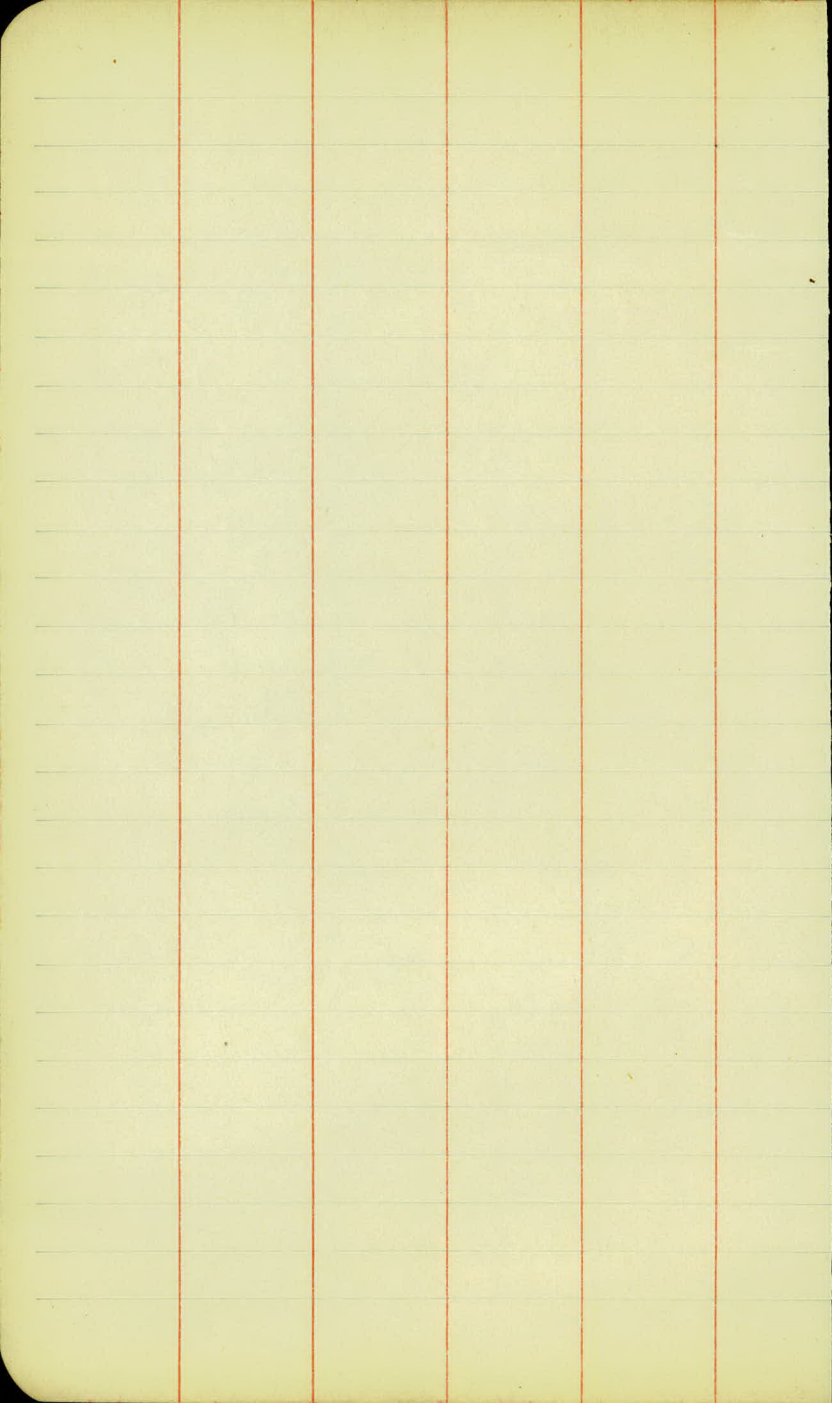
+97











103+00



101+00

13 26 T.P.

24



100+00

26 496 T.P.

23 +57

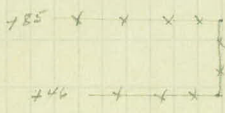
99+00

35°

43 26 T.P.

FR 23 +9

98+00



97+00

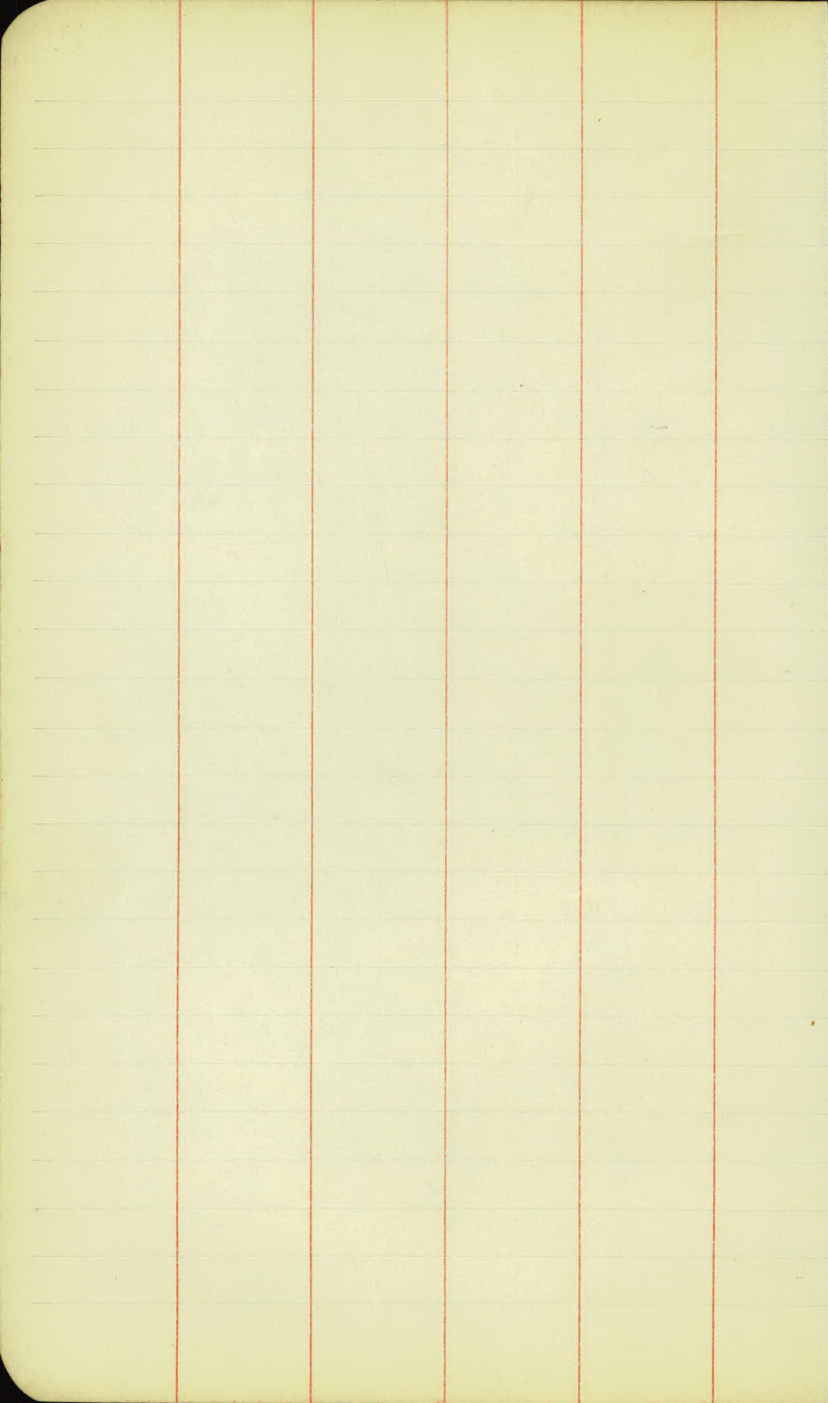
75 23 36

+51

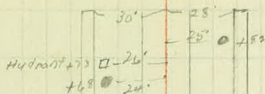
96+00

27

49



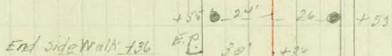
108+00



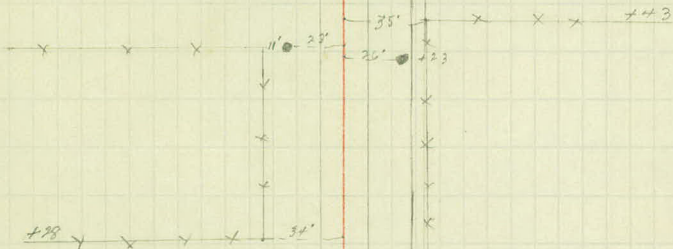
Concrete Walk

Concrete Side Walk 4.5 Wide

107+00

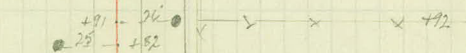


106+00



105+00

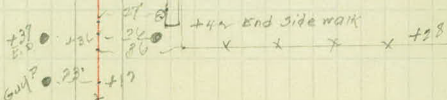
104+00



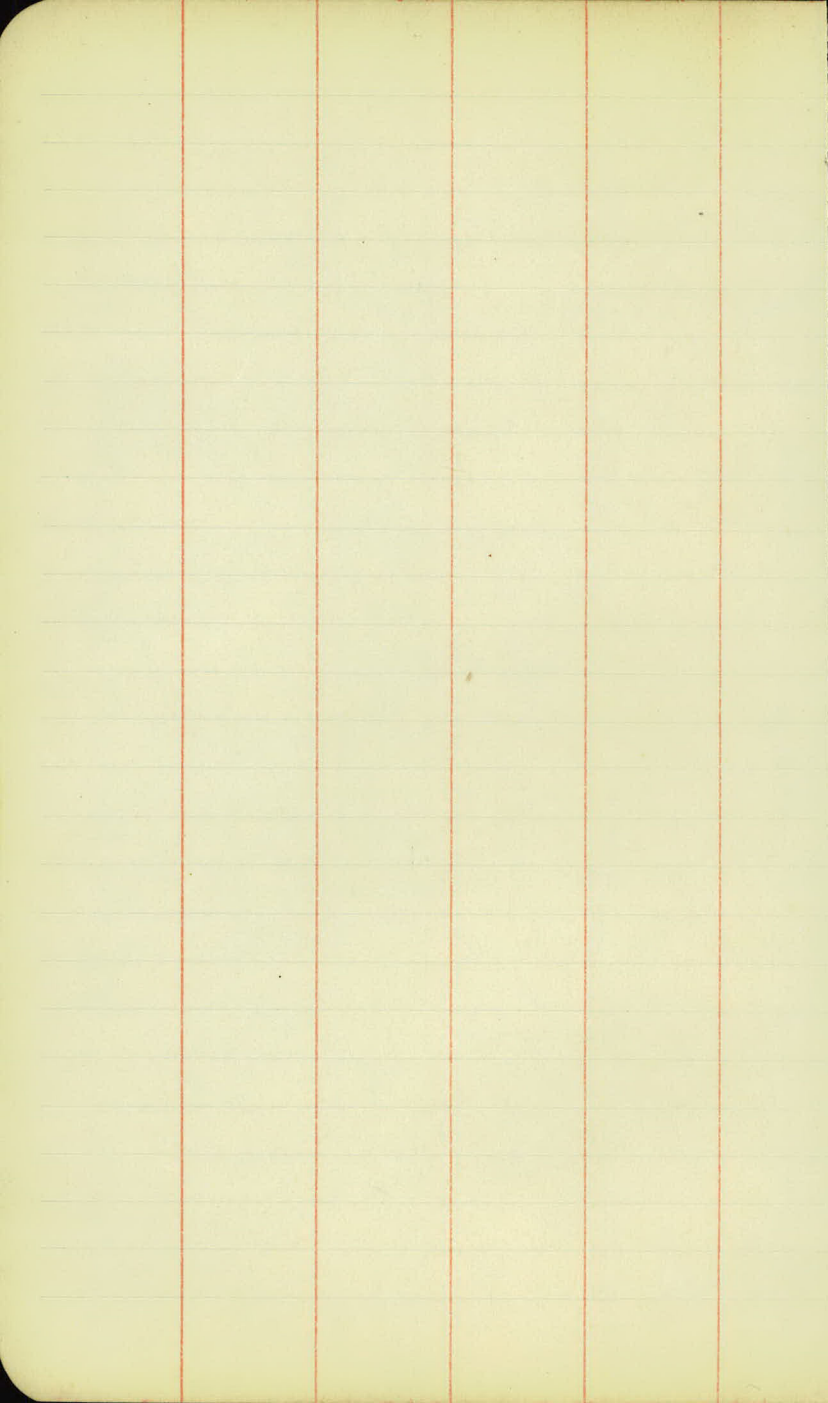
- +87 @ 21'
- +108 @ 21'
- +24 @ 27'

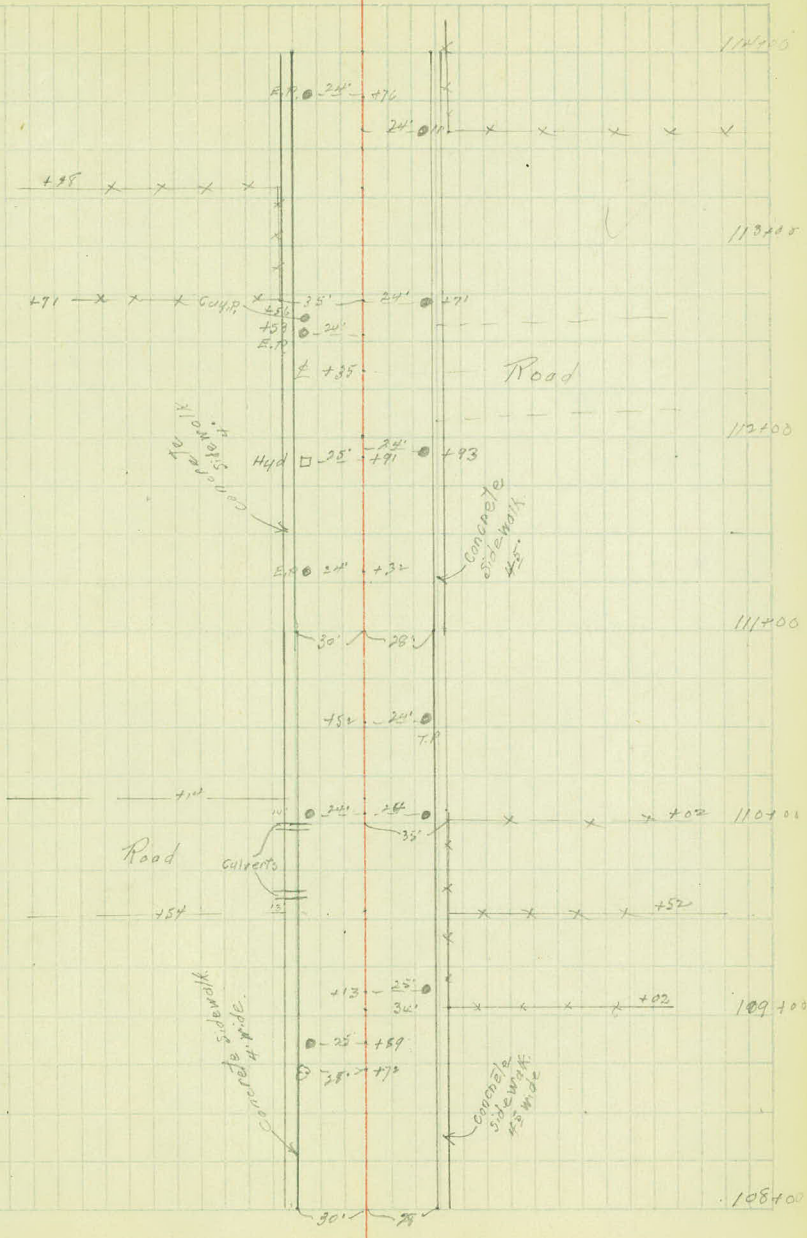
Concrete Side Walk 4.5 Wide

103+00



102+00

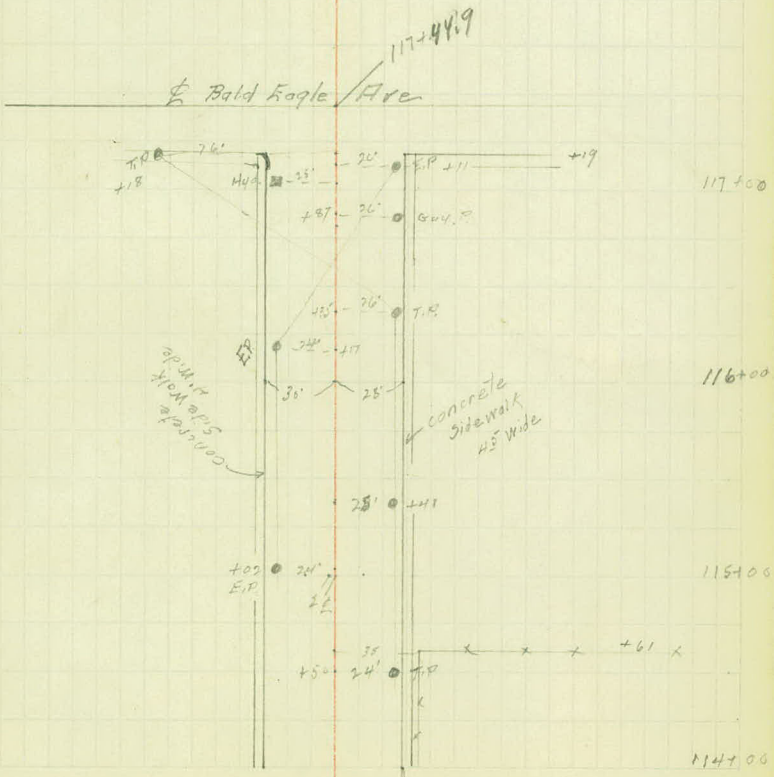




B.h. line - Artificial Topography.

2-27-23

R.B. Austin - Recorder
S. Skooglin } chain 28
R. Halsh. }



Culverts T.S. h. line

Sta

12 + 50

12" Vit. Pipe

Ext 17' R.

or 185 h.

34 + 00

12" Vit. Pipe

Extends 12' R - 18' height

60 + 42

10" Corrugated Pipe

Ext 14' R - 24' height

2-27-23

RK Austin
Skoglin
Walsh.

29

$$549.12 + 00 = 100.5$$

$$\begin{array}{r} 104.5 \\ 9. \end{array}$$

Inv. = 241.7

$$\frac{241.7}{16.0}$$

$$\frac{241.7}{80.0}$$

$$\frac{241.5}{50.0}$$

Remains Right

Inv. 226.0

$$\frac{225.0}{32}$$

$$\frac{224.9}{50}$$

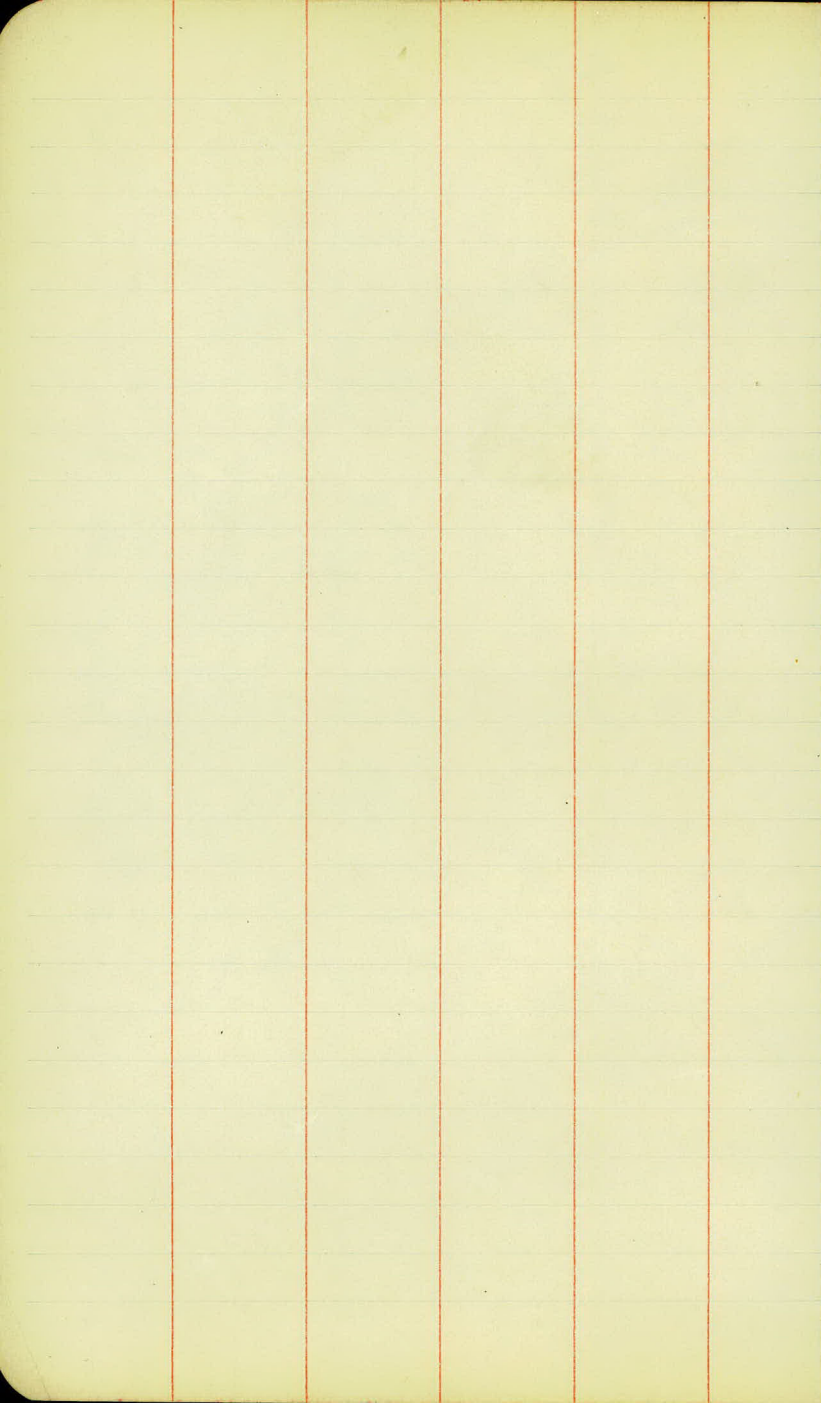
Remains left

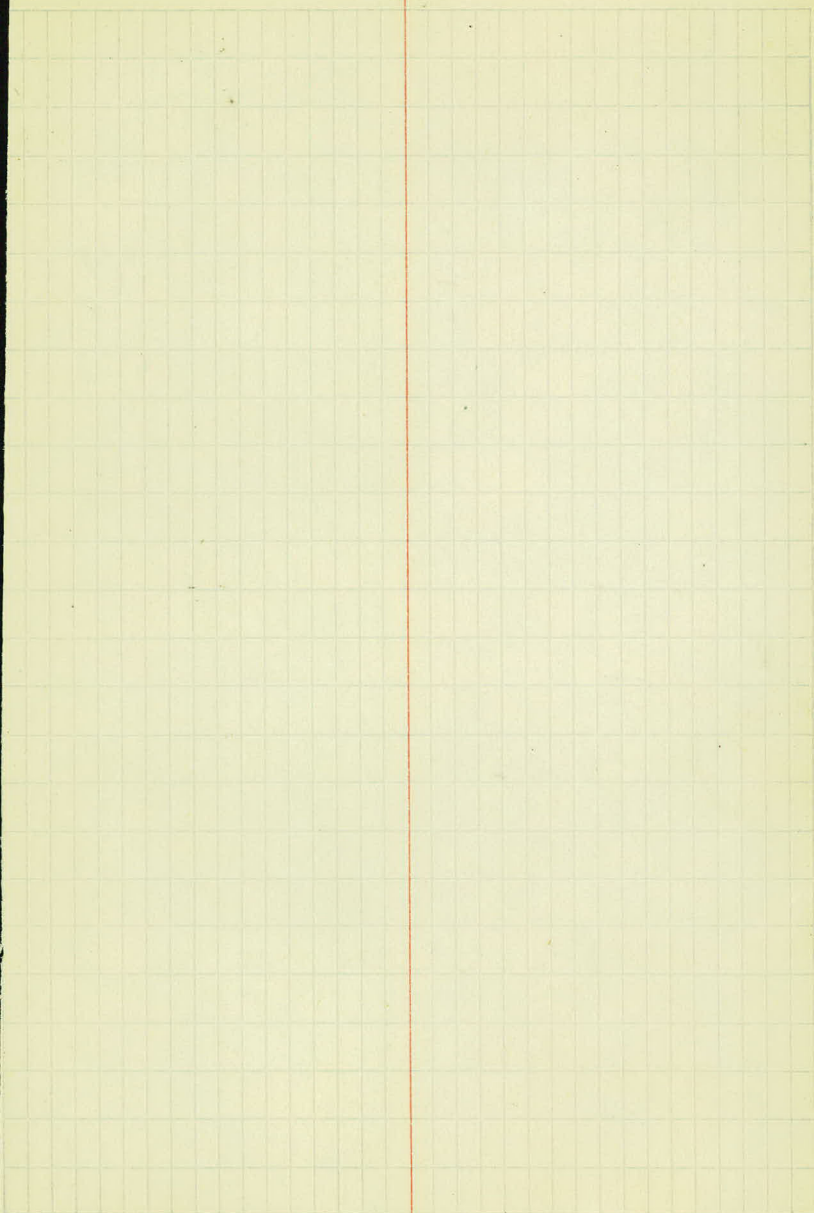
Inv. 226.1

$$\frac{225.7}{150}$$

$$\frac{225.6}{250}$$

Remains Right



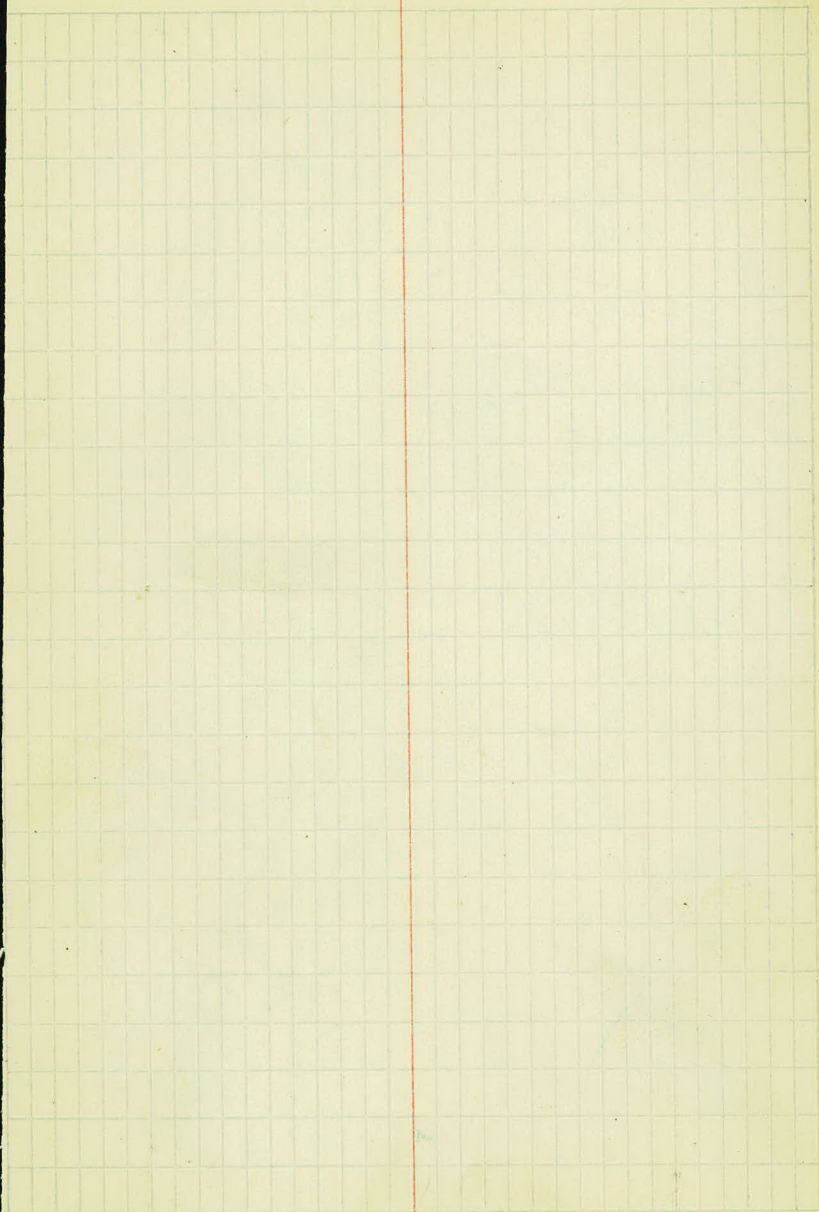


B.h. line Taarverse.

Road. $\frac{1}{2}$ Road.
Left. Right

Ang. h Ang. R.

Sta.	Left.	Right.	Ang. h	Ang. R.
37+11.7 = 0+00				
1+00	9.7			
2+00	0.0			
3+00		2.0		
4+00		4.0		
5+00		19.0		
L +15		21.0		31°00'
+57	0.0			
6+00	7.0			
7+00	23.5			
8+00	18.0			
+78	0.0			
9+00		6.5		
L +27				84°30'
+44	0.0			
10+00	40.0			
11+00	36.0			
12+00	16.0			
13+00		2.0		
14+00		12.0		
+78	0.0	0.0		
15+00	7.0			
+70E				40°30'
16+00	21.0			
+93	0.0	0.0		
17+00		1.0		



Sta.	Left	Right	Ang. L.	Ang. R.
0.4a.				
18+00		12.0		
19+00		10.0		
20+00		1.0		
+ 10.	0.0	0.0		
L + 472	8.0		20° 00'	
21+00	4.0			
22+00	0.0	0.0		
23+00		3.0		
24+00		22.0		
L + 25				58° 0'
25+00	2.0			
26+00	6.5			
27+00		9.0		
L + 072				29° 0'
28+00	0.0	0.0		
29+00	4.0			
30+00	3.0			
31+00	0.0	0.0		
32+00				
+ 10	Approx L Birch Arc			

Panty #2

- 1 Austin } Top. 1.2.5.
- 2 Laughlin } Xlet 6.7.3.4.
- 3 Bob Reeling }
- 4 Johnson }
- 5 Walsh }
- 6 R. J. Feuz }
- 7 McLeary }

$$\begin{array}{r} 16376 \\ 6373 \\ \hline 49128 \\ 114632 \\ 49128 \\ \hline 28256 \\ 1364248 \end{array}$$

$$\begin{array}{r} 575318 \\ 561502 \\ \hline 814 \end{array}$$

$$\begin{array}{r} 42+366 \\ 1+044 \\ \hline 471-322 = B.C. \\ 2+066 \\ \hline 434389 \end{array}$$

$$\begin{array}{r} 9/15.6 \quad 206.6 \\ 15 \\ \hline 60 \\ 34 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 37.2 \\ 287.8 \\ \hline 86.44 \end{array}$$

$$\begin{array}{r} 42-1023' \\ 43-5053' \\ \hline 10023' \end{array}$$

$$\begin{array}{r} 379 \\ 2501 \\ \hline 10813 \end{array}$$

$$\begin{array}{r} 1025 \\ 52 \\ \hline 8 \end{array}$$

$$\begin{array}{r} 42-3003' \\ 67843-7033' \\ \hline 6102+389-9018' \\ 188.06 \end{array}$$

$$\begin{array}{r} 1025 \\ 7033 \\ \hline 9018 \end{array}$$

90/8'

34 86
17043

131946
 4782
95834
 285569
 223624
 127784

 152.797716 2.7

12/354833 2.8521
24
 114
108
 63
44 60
 73 33
 92 24
 13 99

36+917
 1+52.8
35+38.9 = BC
 2+95.3
34+64.2 = F.C.

6.1
12
 1222
 611
733.2
 3
 219.96

32.2
12
 64.5
352.
 210.4
 123.12

36520 = 3040
 32+100 = 9040
 28. 15000
 24 = 17043

6-21-89

Steve Duff

city of white Bear

429-8526

VE CROSS
JUNE

RETROACTIVE Pay
1st HALF OF JUNE
Jim WAS TOLD

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 $\frac{1}{2}$ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

02451