

CONSTRUCTION NOTES  
NORTH ST. PAUL ROAD  
CO. PROJ. 23-54

FILE NO. 6

ENGINEERS'  
FIELD BOOK  
NO. 10403

*North St Paul*

*6 23-54*

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

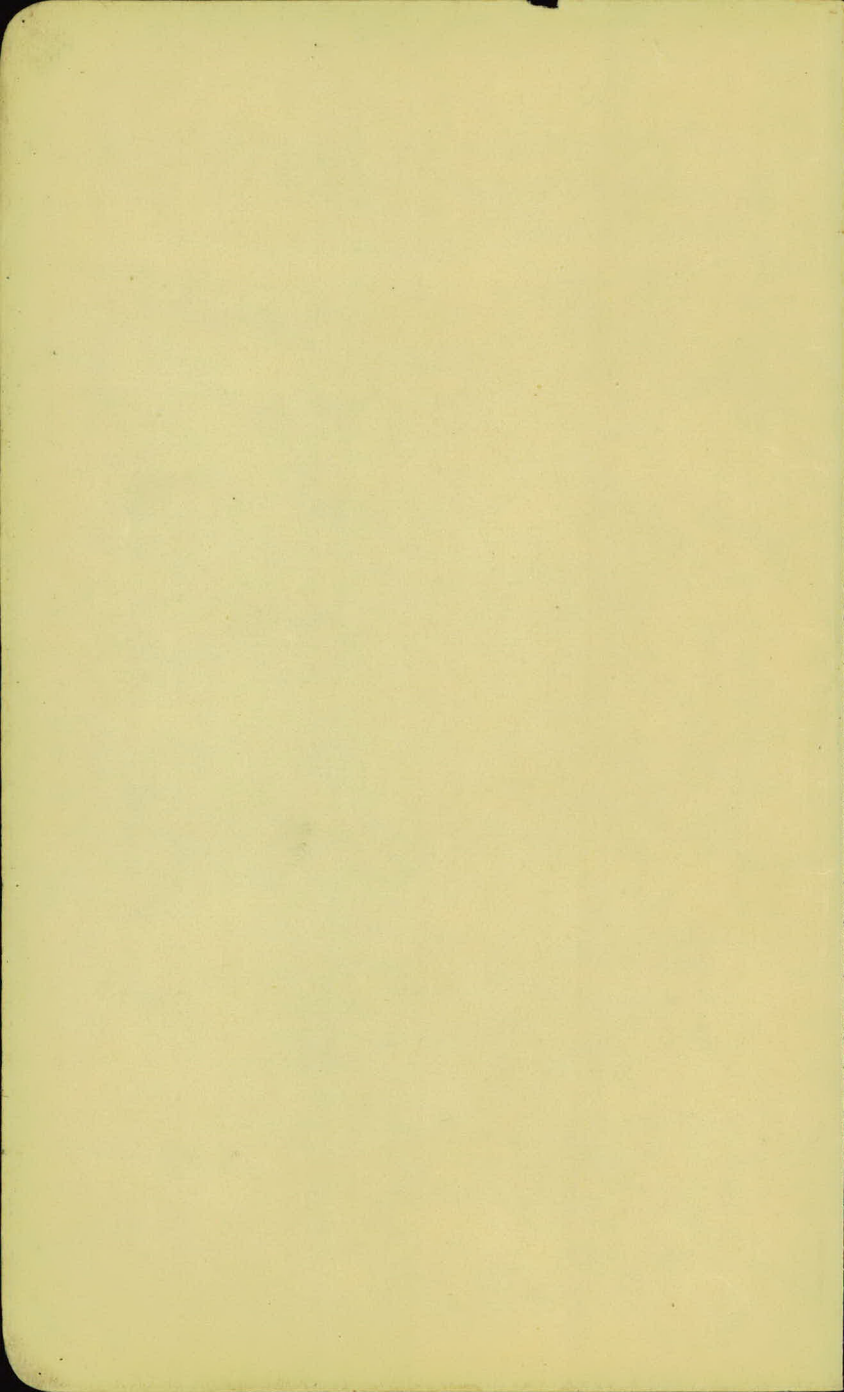
H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

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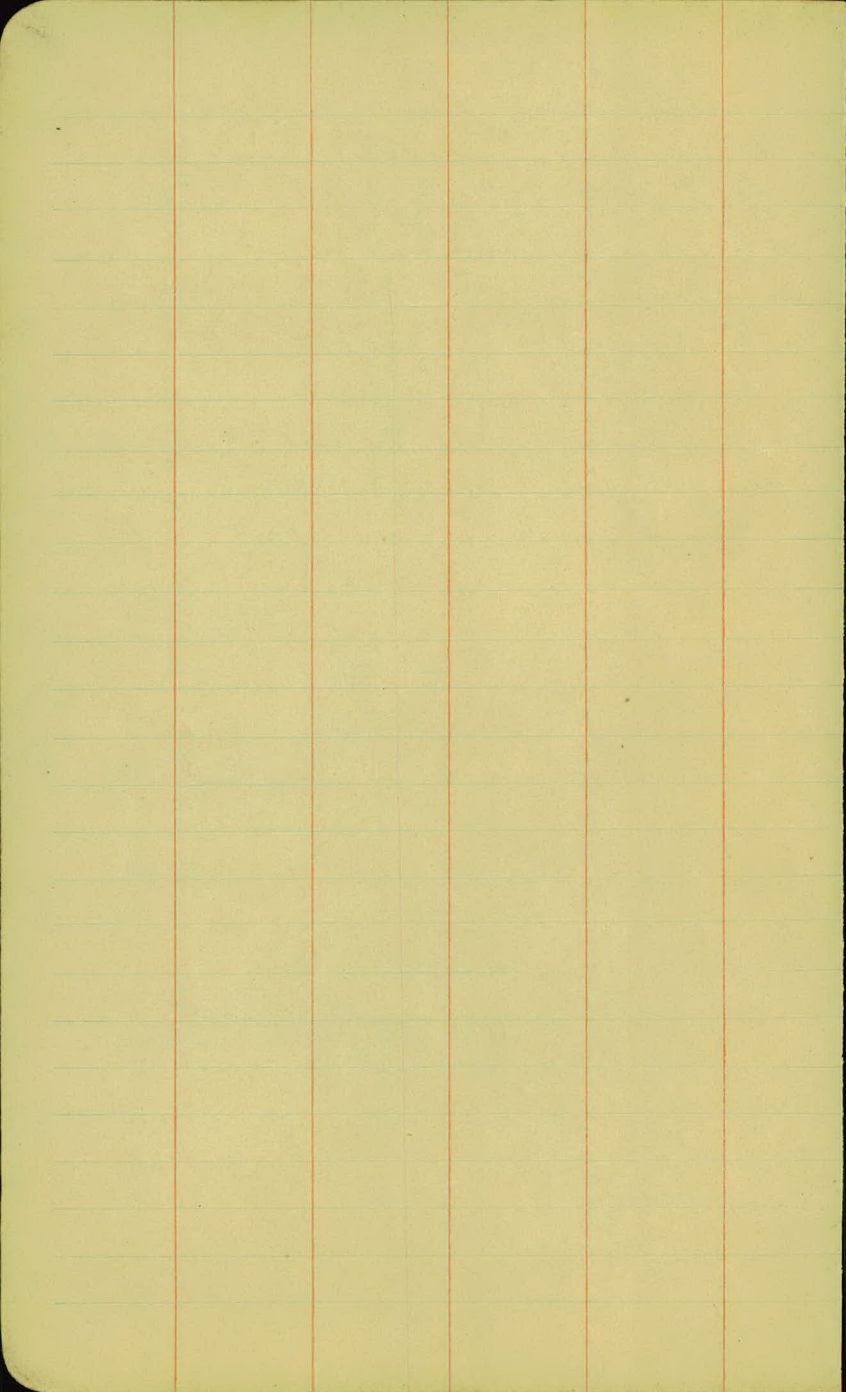
Binoh Lake - 25.56

1.1  
2.0  
3.9  
3.9

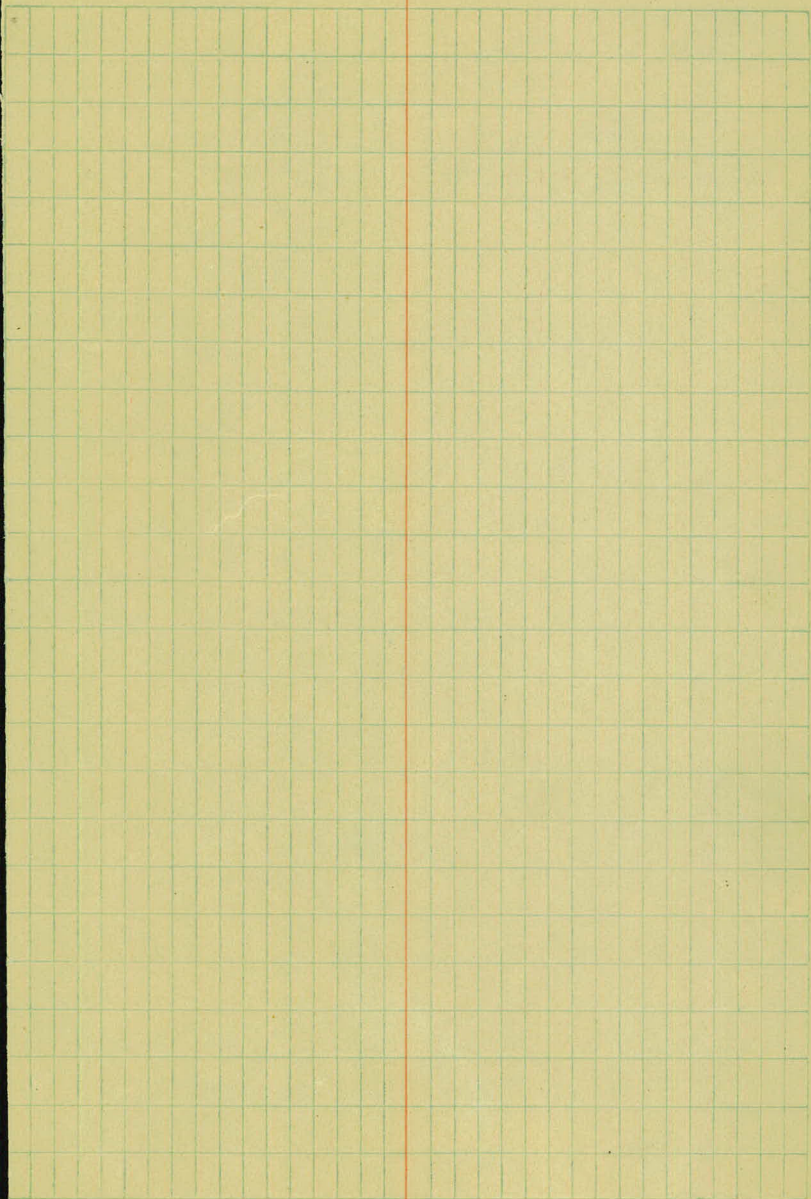


Page to Page	Description	Sta to Sta
5 - 8	Alignment	0 - 137
9	Curve Notes	136 -
11 - 14	Cross-Section	72 - 95 ✓
14 - 19	" "	0 - 71 ✓
20 - 21	" "	121 - 138 ✓
24	Grade Change	4 - 8+50 ✓

25-27	Final X-Sections (1924)	0+00 15+70
27-43	Final X-Sections (1923)	16 - 158
48-72	Final Topography (1923)	16 - 137
43 -	Final X-Sections (1924)	16 - 20
44	Final F.E. X-Sections (1924)	6+83
45-48	Final Topography (1924)	0+00 16+00



4



Anght.  $\frac{1}{2}$  Ang Rt.

5466.5 P.O.T

5402.3 F.C.

2468.9 P.I

50° 14'

0+00 B.C. = 1471.2 White Bear Rd.

Sta 50' 0 359 T/P 0

Sta.	Def.
0+00	0°00'
+50	2°30'
1+00	5°00'
+57	7°51'
2+00	10°06'
+50	12°30'
3+00	15°00'
+50	17°30'
4+00	20°00'
+50	22°30'
5+00	25°00'
+02.3	25°07'



10° Curve, P  
 $\Delta = 50^\circ 14'$   
 ST = 267.94 L  
 B.C. = 0+00  
 Length = 502.3'  
 E.C. = 5+02.3

Sta. Point Right Left

70 + 4 + 2 P.I.

53 + 66<sup>3</sup> P.O.T.  $\angle$  Elec. Ry.

$\left. \begin{array}{l} = 49 + 26^2 \\ 49 + 18^3 \end{array} \right\} \text{P.O.T.}$

36 + 91<sup>2</sup> P.I. 0° 02'

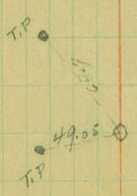
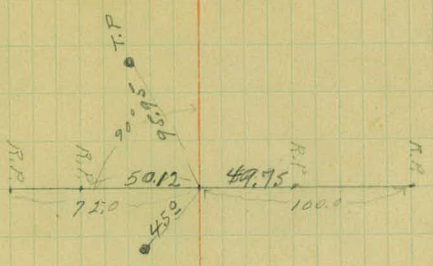
20 + 18<sup>3</sup> P.O.T.

15 + 94<sup>4</sup> P.O.T.

50.0  
 8.6  
 41.4

2945.0  
 20.9  
 231

7450.0  
 9.193  
 31.7

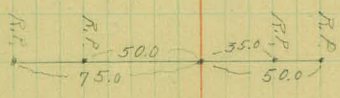


sta.	Point.	Right	Left
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76+013	P.O., T.		
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83+75.8	P.O., T.	= 83+74.8	
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8/8/23



Ang h  $\frac{1}{2}$  Ang R.

137+912 E.C.

137+098 P.I. 510 39'

137+912	25° 49' $\frac{1}{2}$
137+30	19-51
137+00	12° 36'
136+50	5° 21'
136+13.1	0° 00'

136+134 B.C.

$$\begin{array}{r} 115 \overline{) 1250} \\ 115 \phantom{0} \\ \hline 400 \\ 350 \\ \hline 500 \end{array}$$

$$\begin{array}{r} 2884 \\ 3696 \\ \hline 34844 \\ 560 \\ \hline 6-94- \\ 17-51 \\ \hline 1629 \end{array}$$

$$\begin{array}{r} 2583 \\ 2154 \\ \hline 37100 \\ 000 \\ \hline 2100 \\ 254- \\ \hline 1551 \\ 214 \\ \hline 2706 \end{array}$$

29° Curve Left

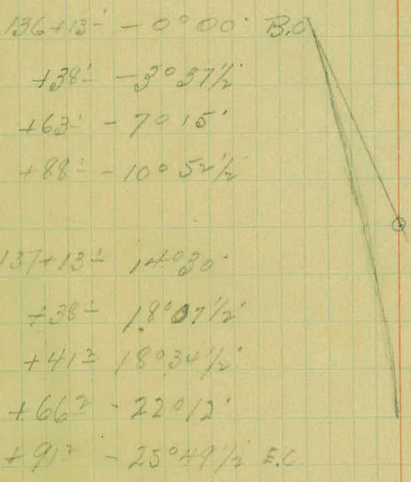
$\Delta = 51^{\circ}39'$

S.T. = 96.65

B.C. = 136+13'

Length = 178'

E.C. = 137+91'



136+13' - 0° 00' B.C.

+38' - 2° 37 1/2'

+63' - 7° 15'

+88' - 10° 52 1/2'

137+13' - 14° 30'

+38' - 18° 07 1/2'

+41' - 18° 34 1/2'

+66' - 22° 12'

+91' - 25° 49 1/2' E.C.

270 Curve heft. U37498

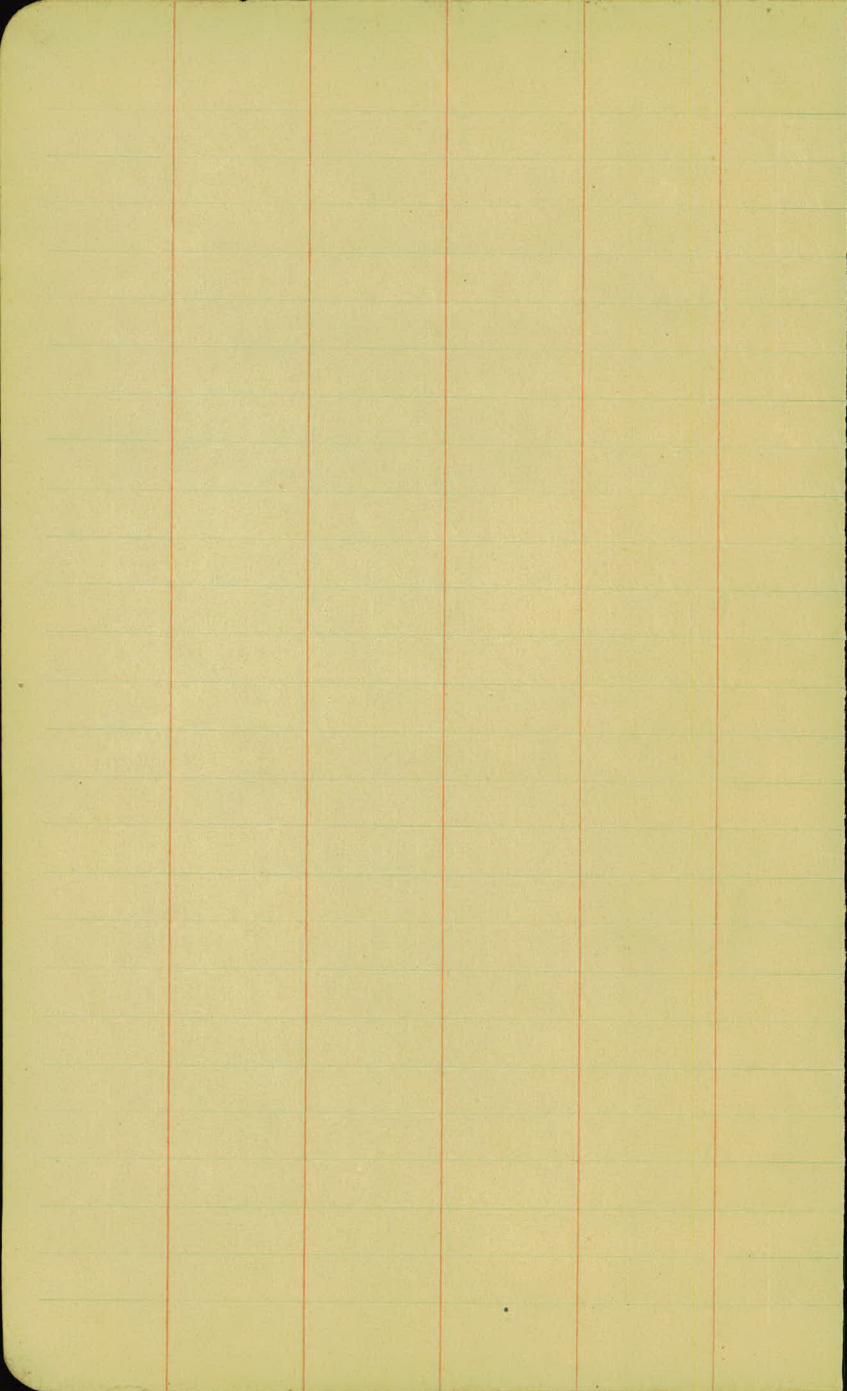
Station	Def	Point	Profile Grade	Super Per foot	Extra Width
134+63 <sup>+</sup>		B.S.T. 0	99.36	-009 -008	
134+88 <sup>+</sup>		25	98.86	+000 -008	
135+13 <sup>+</sup>		50	99.36	+008 -008	
135+38 <sup>+</sup>		75	99.86	+017 -017	
135+63 <sup>+</sup>		B.W.T 100	300.36	+026 -026	0.0
135+88 <sup>+</sup>		125	300.86	+035 -035	0.5
136+13 <sup>+</sup>	0°00'	B.C. 150	301.36	+044 -044	2.48
136+38 <sup>+</sup>		175	301.85	+053 -053	4.48
136+63 <sup>+</sup>		E.W.T E.S.T 200	302.30	+062 -062	5.00
+88 <sup>+</sup>			302.70	✓	5.00
137+13 <sup>+</sup>			303.05	✓	5.00
+38 <sup>+</sup>					
+41 <sup>±</sup>		E.S.T E.W.T 200			
+66 <sup>±</sup>		175			
+91 <sup>±</sup>	25°49 <sup>1</sup> / <sub>2</sub> '	E.C. 150			

Left

±

Right

Width	Elev.	Profile Grade	Elev	Width
10'	98.28 ✓	98.36	98.28 ✓	
10'	98.78 ✓	98.86	98.86 ✓	
10'	99.28 ✓	99.36	99.44 ✓	
10'	99.69 ✓	99.86	300.00 ✓	
10'	300.10 ✓	300.86	300.62 ✓	
10.5	300.49 ✓	300.86	301.21 ✓	
12.48	300.81 ✓	301.36	301.80 ✓	
14.48	301.08	301.85	302.38	
15.00	301.37	302.30	302.92	
✓	301.77	302.70	303.32	
✓	302.12	303.05	303.67	



The image shows a page of graph paper with a grid of small squares. A vertical red line runs down the left side of the page, creating a margin. The grid covers most of the page area.

Proj # 23-54

X. Sections & Slope Stakes  
 from Sta 95+00 to Sta. 81+00

Sta.	+	H.I.	-	Elev	Grade
B.M.	4.74	271.94 ✓		267.22 ✓	
95			4.3	267.7	267.3
94			2.4 ✓	269.6	269.6
T.P.	12.50	281.93	2.53	269.43 ✓	
93			10.1	271.3	272.3
92			6.8	275.1	275.7
91			2.7 ✓	279.2	279.5
T.P.	11.88	292.28	1.53	280.40 ✓	
90			7.1	283.2	283.3
B.M.			11.42	280.86	280.89
89			5.2	287.1	287.1

L

R

8/8/53

Spk. in Tel pole L. 579 100 + 10.

4.7 ✓ 2.04	F04	$\frac{5.1}{14.6}$	$\frac{4.1}{3.3}$	$\frac{4.6}{2.8}$	$\frac{5.2}{1.9}$	$\frac{4.7}{3.3}$	$\frac{4.0}{2.2}$	C.01
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2.4 ✓ 2.0	F11	$\frac{3.5}{17.4}$	$\frac{4.0}{3.3}$	$\frac{5.0}{3.1}$	$\frac{3.4}{1.9}$	$\frac{2.4}{5}$	$\frac{3.0}{1.5}$	$\frac{5.0}{2.1}$	$\frac{5.1}{3.3}$	$\frac{3.5}{17.4}$	F11
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2.6 ✓ 2.05	F23	$\frac{11.9}{19.6}$	$\frac{12.7}{2.3}$	$\frac{13.0}{2.9}$	$\frac{12.5}{2.5}$	$\frac{12.0}{2.3}$	$\frac{11.1}{1.5}$	$\frac{11.0}{1.7}$	$\frac{12.7}{3.3}$	$\frac{11.2}{18.4}$	F12
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2.2 ✓ 2.02	F21	$\frac{8.5}{19.3}$	$\frac{8.7}{3.3}$	$\frac{7.6}{3.1}$	$\frac{10.2}{2.7}$	$\frac{7.3}{2.5}$	$\frac{9.4}{2.2}$	$\frac{7.7}{1.4}$	$\frac{7.5}{1.7}$	$\frac{8.7}{2.8}$	$\frac{8.7}{3.3}$	$\frac{8.0}{18.7}$	F12
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2.4 ✓ 2.03	F18	$\frac{4.2}{18.7}$	$\frac{5.2}{3.3}$	$\frac{5.6}{3.0}$	$\frac{4.9}{2.3}$	$\frac{3.7}{1.7}$	$\frac{3.6}{1.5}$	$\frac{4.0}{2.4}$	$\frac{5.0}{2.8}$	$\frac{4.2}{2.4}$	$\frac{4.5}{3.3}$	$\frac{3.9}{18.7}$	F1.5
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2.0 ✓ 2.0	F11	$\frac{12.1}{17.7}$	$\frac{11.0}{2.3}$	$\frac{11.1}{2.8}$	$\frac{10.2}{1.8}$	$\frac{9.9}{1.8}$	$\frac{10.3}{2.7}$	$\frac{9.6}{2.8}$	$\frac{9.8}{3.3}$	$\frac{9.9}{2.1}$	F07
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Spk. in Tel pole R. 70 + 30

5.2 ✓ 2.0	F10	$\frac{6.2}{17.4}$	$\frac{9.1}{3.3}$	$\frac{7.0}{3.1}$	$\frac{6.6}{2.7}$	$\frac{6.1}{1.9}$	$\frac{5.7}{1.4}$	$\frac{5.7}{1.9}$	$\frac{5.3}{2.3}$	$\frac{5.4}{3.3}$	$\frac{5.5}{2.2}$	F00
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Sta.	+	H.I.	-	Elev.	Grade
		272.28			
88			1.4	290.9	290.8
T.P.	11.63	303.13 ✓	0.78	291.50 ✓	
87			8.3	<del>254.0</del> 94.8	293.8
+50			6.6	<del>285.7</del> 96.5	95.2
86			5.5	<del>286.8</del> 97.6	296.0
85			4.0	<del>288.3</del> 99.1	297.5
+25			4.1	<del>288.2</del> 99.0	97.7
T.P.	8147	307.51 ✓	4.09	299.04 ✓	
+45			8.3	90.2	98.0
+25			8.2		98.1
84			8.1	99.4	298.1
+70			8.1		98.2
+50			8.3	90.2	98.2
83			8.9	98.6	298.1
82			10.0	97.5	297.0
81			11.9	95.6	295.8

L

R 2/8/23

$\begin{matrix} 1.5 \\ 2.1 \end{matrix}$ 
 $\begin{matrix} 104.19 \\ 214 \end{matrix}$ 
 $\begin{matrix} 21 \\ 33 \end{matrix}$ 
 $\begin{matrix} 2.0 \\ 28 \end{matrix}$ 
 $\begin{matrix} 2.4 \\ 27 \end{matrix}$ 
 $\begin{matrix} 1.8 \\ 21 \end{matrix}$ 
 $\begin{matrix} 2.1 \\ 15 \end{matrix}$ 
 $\begin{matrix} 1.8 \\ 12 \end{matrix}$ 
 $\begin{matrix} 1.6 \\ 14 \end{matrix}$ 
 $\begin{matrix} 2.2 \\ 20 \end{matrix}$ 
 $\begin{matrix} 1.5 \\ 33 \end{matrix}$ 
 $\begin{matrix} 1.8 \\ 33 \end{matrix}$ 
 $\begin{matrix} 1.0 \\ 21.9 \end{matrix}$ 
 Fall

$\begin{matrix} 2.3 \\ 2.1 \\ 1.0 \\ 1.9 \end{matrix}$ 
 $\begin{matrix} 2.6 \\ 227.53 \\ 1.0 \\ 1.9 \end{matrix}$ 
 $\begin{matrix} 8.7 \\ 31 \\ 6.9 \\ 33 \end{matrix}$ 
 $\begin{matrix} 8.7 \\ 21 \\ 6.8 \\ 25 \end{matrix}$ 
 $\begin{matrix} 8.5 \\ 25 \\ 6.0 \\ 20 \end{matrix}$ 
 $\begin{matrix} 9.4 \\ 17 \\ 7.8 \\ 14 \end{matrix}$ 
 $\begin{matrix} 9.4 \\ 15 \\ 7.1 \\ 11 \end{matrix}$ 
 $\begin{matrix} 9.2 \\ 13 \\ 7.1 \\ 11 \end{matrix}$ 
 $\begin{matrix} 8.6 \\ 17 \\ 7.9 \\ 14 \end{matrix}$ 
 $\begin{matrix} 9.7 \\ 33 \\ 7.1 \\ 20 \end{matrix}$ 
 $\begin{matrix} 8.3 \\ 230 \\ 7.2 \\ 27 \end{matrix}$ 
 $\begin{matrix} 0.1 \\ 0.1 \\ 0.1 \\ 0.1 \end{matrix}$

$\begin{matrix} 2.1 \\ 1.0 \end{matrix}$ 
 $\begin{matrix} 150 \\ 241 \end{matrix}$ 
 $\begin{matrix} 5.0 \\ 33 \end{matrix}$ 
 $\begin{matrix} 5.5 \\ 31 \end{matrix}$ 
 $\begin{matrix} 5.0 \\ 23 \end{matrix}$ 
 $\begin{matrix} 4.0 \\ 19 \end{matrix}$ 
 $\begin{matrix} 4.3 \\ 13 \end{matrix}$ 
 $\begin{matrix} 4.7 \\ 15 \end{matrix}$ 
 $\begin{matrix} 4.7 \\ 33 \end{matrix}$ 
 $\begin{matrix} 5.6 \\ 235 \end{matrix}$ 
 $\begin{matrix} 0.1 \\ 0.1 \end{matrix}$

$\begin{matrix} 2.0 \\ 1.6 \\ 1.4 \end{matrix}$ 
 $\begin{matrix} 2.7 \\ 241 \\ 2.7 \end{matrix}$ 
 $\begin{matrix} 2.4 \\ 33 \\ 31 \end{matrix}$ 
 $\begin{matrix} 2.7 \\ 27 \\ 2.8 \\ 21 \end{matrix}$ 
 $\begin{matrix} 2.6 \\ 21 \\ 2.8 \\ 15 \end{matrix}$ 
 $\begin{matrix} 3.8 \\ 15 \\ 4.5 \\ 33 \end{matrix}$ 
 $\begin{matrix} 5.1 \\ 14 \\ 5.0 \\ 14 \end{matrix}$ 
 $\begin{matrix} 2.1 \\ 23 \\ 4.4 \\ 17 \end{matrix}$ 
 $\begin{matrix} 1.8 \\ 33 \\ 2.0 \\ 22 \end{matrix}$ 
 $\begin{matrix} 2.0 \\ 25.6 \\ 1.0 \\ 27 \end{matrix}$ 
 $\begin{matrix} 0.3 \\ 0.3 \\ 0.3 \\ 0.8 \end{matrix}$

$\begin{matrix} 5 \\ 4 \\ 4 \end{matrix}$ 
 $\begin{matrix} 8.5 \\ 33 \\ 5.7 \\ 33 \end{matrix}$ 
 $\begin{matrix} 8.5 \\ 33 \\ 6.0 \\ 31 \end{matrix}$ 
 $\begin{matrix} 9.4 \\ 22 \\ 6.0 \\ 18 \end{matrix}$ 
 $\begin{matrix} 8.9 \\ 10 \\ 6.0 \\ 12 \end{matrix}$ 
 $\begin{matrix} 9.2 \\ 15 \\ 7.2 \\ 16 \end{matrix}$ 
 $\begin{matrix} 8.5 \\ 18 \\ 8.3 \\ 23 \end{matrix}$ 
 $\begin{matrix} 6.1 \\ 24 \\ 6.2 \\ 28 \end{matrix}$ 
 $\begin{matrix} 5.7 \\ 33 \\ 5.7 \\ 33 \end{matrix}$ 
 $\begin{matrix} 7.4 \\ 7.4 \end{matrix}$ 
 $\begin{matrix} 0.2 \\ 0.2 \end{matrix}$

$\begin{matrix} 13 \\ 3 \\ 3 \\ 2 \end{matrix}$ 
 $\begin{matrix} 2.2 \\ 241 \\ 1.7 \\ 137 \end{matrix}$ 
 $\begin{matrix} 6.6 \\ 33 \\ 3.6 \\ 30 \end{matrix}$ 
 $\begin{matrix} 6.0 \\ 28 \\ 8.9 \\ 29 \end{matrix}$ 
 $\begin{matrix} 6.0 \\ 24 \\ 8.2 \\ 20 \end{matrix}$ 
 $\begin{matrix} 6.4 \\ 19 \end{matrix}$ 
 $\begin{matrix} 8.4 \\ 13 \end{matrix}$ 
 $\begin{matrix} 8.4 \\ 8.4 \\ 8.4 \\ 8.4 \end{matrix}$ 
 $\begin{matrix} 8.8 \\ 12 \end{matrix}$ 
 $\begin{matrix} 9.2 \\ 15 \end{matrix}$ 
 $\begin{matrix} 8.6 \\ 22 \end{matrix}$ 
 $\begin{matrix} 6.0 \\ 29 \end{matrix}$ 
 $\begin{matrix} 5.7 \\ 33 \end{matrix}$ 
 $\begin{matrix} 7.4 \\ 6.3 \\ 6.3 \\ 6.0 \end{matrix}$ 
 $\begin{matrix} 0.2 \\ 0.2 \\ 0.2 \\ 0.2 \end{matrix}$

$\begin{matrix} 1.5 \\ 1.5 \end{matrix}$ 
 $\begin{matrix} 1.4 \\ 251 \end{matrix}$ 
 $\begin{matrix} 8.4 \\ 33 \end{matrix}$ 
 $\begin{matrix} 10.4 \\ 27 \end{matrix}$ 
 $\begin{matrix} 9.2 \\ 24 \end{matrix}$ 
 $\begin{matrix} 9.3 \\ 21 \end{matrix}$ 
 $\begin{matrix} 10.6 \\ 17 \end{matrix}$ 
 $\begin{matrix} 10.8 \\ 14 \end{matrix}$ 
 $\begin{matrix} 7.6 \\ 24 \end{matrix}$ 
 $\begin{matrix} 6.8 \\ 33 \end{matrix}$ 
 $\begin{matrix} 7.4 \\ 23.1 \end{matrix}$ 
 $\begin{matrix} 0.3 \\ 0.3 \end{matrix}$

$\begin{matrix} 2.2 \\ 1.8 \end{matrix}$ 
 $\begin{matrix} 13.0 \\ 22.8 \end{matrix}$ 
 $\begin{matrix} 11.3 \\ 33 \end{matrix}$ 
 $\begin{matrix} 12.9 \\ 28 \end{matrix}$ 
 $\begin{matrix} 12.6 \\ 14 \end{matrix}$ 
 $\begin{matrix} 10.1 \\ 18 \end{matrix}$ 
 $\begin{matrix} 10.3 \\ 33 \end{matrix}$ 
 $\begin{matrix} 10.4 \\ 23.7 \end{matrix}$ 
 $\begin{matrix} 0.1 \\ 0.1 \end{matrix}$

10.1  
2.1

STA.	+	H.I.	-	Elev.	Grade
		307.51			
B.M.	1.48	298.55 ✓	10.42	297.09 ✓	297.09
80			5.8	92.8	292.8
79			9.0	99.6	289.6
78			12.2	86.4 ✓	286.4
T.P.	1.93	289.19 ✓	11.29	287.24	
77			4.2	83.0	283.0
+75			7.3		82.8
T.P.	3.79	283.00 ✓	9.98	279.21	
76			3.3	79.7	279.7
+70			5.1	77.9	77.9
75			4.5	76.5	276.4
+67			7.9	75.1	75.3
74			10.0	73.0 ✓	273.1
T.P.	5.55	276.80 ✓	11.75	271.25	



Sta.		H.I.		Elev.	Corr.
		276.80			
73			740.	269.8	270.1
72			74	267.2	267.5
T.P.			10.80	266.00	
B.M.	2.30	277.64 ✓		275.34	
T.P.	0.31	266.70 ✓	11.75	265.59 ✓	
T.P.	2.24	259.17 ✓	9.37	256.73 ✓	
0 + 50				49.54 ✓	
1 + 00				50.52 ✓	
+ 57				51.42 ✓	7.3
2 + 00				52.29 ✓	6.2 6.6
+ 50				54.95 ✓	3.7 4.4
3 + 00				57.0 ✓	1.2 2.2
T.P.	12.45	269.37 ✓	2.25	256.92 ✓	
+ 50				59.25 ✓	9.1 10.1
4 + 00				61.50 ✓	6.9 7.9
+ 50				63.6 ✓	4.7 5.0
5 + 00				65.4 ✓	3.3 4.0
+ 50					
B.M.	1.19	276.57 ✓			275.34
6 + 00				67.2 ✓	1.0 8.3
7 + 00				69.8 ✓	5.7
8 + 00				70.3 ✓	5.4
8 + 50				70.2 ✓	6.3



		276.52			
9+00				70.2 ✓	6.3
9+50				70.2 ✓	6.3
10+00				70.1 ✓	6.4
+64				70.0	6.5
B.M	1.00	276.34 ✓			275.34 ✓
T.P	5.94	271.18 ✓	11.10	(265.24)	
11+00			63.6	70.0	1.2 ✓
+50				70.1	1.1 ✓
12+00				70.3	0.9 ✓
+50				70.7	0.5 ✓
T.P.	11.10	274.83 ✓	7.45	(263.73)	
13+00				71.4	3.4 ✓
+50				71.9	2.9
+80				72.7	2.1
14+00				73.2	1.6 ✓
+50				74.4 ✓	0.4 ✓
T.P	6.72	280.45 ✓	1.10	(273.73)	
15+00				75.8	4.7 ✓
+50				77.3	3.2 ✓
T.P	7.47	286.64 ✓	1.25	(279.17)	
+70				77.9	8.7 ✓
16+00				79.8	7.8 ✓
+135				79.2	7.4
+230				79.5	7.1
+50				80.3	6.3

h	L			P				
✓ 7.1	6.2	6.2	(6.3)	5.5	2.5	x	1.9	71.8
33.0	24.0	24.0	4.7	20.0	26.0	29.0	33.0	
✓ 8.0	7.0	7.0	3.5	2.5	3.5	x		73.0
33.0	19.0	19.0	6.9	19.0	25.0	27.7	33.0	
✓ 8.2	7.5	7.5	11.2	10.3	9.7	5.7		70.1
33.0	28.0	28.0	11.2	25	20.5	33.0		65.3

40 At 1415 Nail in T.O

	x			10% Shrinkage				
✓ 8.5	8.5	8.2	7.5	7.0	6.0	5.7	5.0	63.7
33.0	28.0	17.0	7.5	8.0	16.0	22.7	33.0	
✓ 8.0	8.0	8.0	8.5	7.8	7.2			
33.0	24.7	13.0	8.5	16.0	32.0			
✓ 8.7	9.0	8.0	9.0	8.5	8.5			
33.0	27.0	15.0	9.0	15.0	32.0			
✓ 11.9	12.0	11.9	11.9	11.9	11.6	11.4		
33.0	29.9	15.0	11.9	10.0	29.3	33.0		
✓ 11.0	10.9	10.6	10.6	10.0	9.3	9.1		
33.0	27.0	17.0	10.6	9.5	22.0	33.0		
✓ 6.7	6.4	6.3	6.2	6.2	7.7	9.2		
33.0	26.0	16.0	6.2	13.0	21.0	33.0		
✓ 3.6	4.1	4.7	5.6	6.1	6.1	7.2	8.4	
33.0	19.9	21.5	10.5	9.5	17.5	25.4	33.0	
✓ 6.8	6.8	6.5	8.2	6.2	5.2	6.5		
33.0	14.0		8.2	10.5	18.0	33.0		
✓ 6.1	6.4	7.0	7.7	9.0	9.0	10.5	10% shrinkage	
33.0	16.7	11.0	7.7	12.5	24.5	33.0		
✓ 2.7	3.3	4.1	5.0	5.7	7.7	8.8		
33.0	26.0	14.5	11.5	12.0	22.0	33.0		

7.1	7.5	7.0	7.0	6.2	9.1	9.4	11.2	13.0
33.0	24.0	21.0	13.0	8.0	9.0	21.0	33.0	
6.1	6.0	5.7	6.0	4.1	3.6	4.5	5.9	4.7
33.0	22.5	15.5	7.0	6.5	3.6	7.5	15.0	22.0
6.7	5.0	5.4	5.6	3.4	3.3	2.5	3.1	4.7
33.0	21.0	9.5	3.5	3.4	10.0	18.0	7.0	20.0
5.0	5.9	5.9	5.1	5.7	5.2	3.5	1.9	2.2
33.0	31.0	27.0	12.0	11.0	5.2	14.5	20.0	25.0
0.9	4.1	4.3	4.1	4.4	4.2	3.6	2.7	2.6
33.0	25.5	21.5	9.0	4.4	6.5	9.5	12.0	24.0

Job - 23-54  
 X-Sections + Slope Stakes  
 Sta. - 17+00 -

Station	+	H.I. ✓	-	Grade	Rel.
20+15 B.M.	3.67	295.97			292.30
17+00				81.0	11.2 ✓
18+00				84.3	11.2
+50				86.2	9.8
19+00				87.4	8.6 ✓
+35				88.2	7.8
20+00				89.2	6.8 ✓
+50				89.9	6.1
21+00				90.3	5.7 ✓
22+00				90.6	5.4 ✓
+45				90.6 ✓	5.4 ✓
T.P.	5.74	296.38	5.30	(290.60)	
23+00				90.5	5.9 ✓
+50				90.4	6.0 ✓
24+00				90.4	6.0 ✓
+75				90.4	6.0 ✓
25+00				90.4	6.0 ✓
+18				90.4 ✓	6.0
T.P.	5.38	295.31	6.45	(289.93)	
26+00				90.4	4.9 ✓
+87				90.5	4.8
27+00				90.5	4.8 ✓
+50				90.6	4.7
28+00				90.6 ✓	4.7 ✓
T.P.	8.11	299.46	3.96	(291.50)	

h. £ P.

6.9	9.5	9.5	9.2	12.8	12.4	11.8	11.8	10.6	10.9	11.1	11.5
33.0	36.7	26.0	26.0	29.0	17.0	15.5	10.0	22.5	25.0	26.1	33.0
3.5	3.5	4.8	7.1	7.7	10.2	9.8	9.2	9.1	7.5	9.2	9.2
33.0	32.7	29.0	23.0	20.0	15.5	12.0	10.5	14.0	17.0	23.0	27.6
2.2	2.2	6.0	7.1	9.9	5.7	8.2	8.6	8.6	7.5	7.6	8.1
33.0	32.5	27.0	23.5	15.0	11.5	7.2	10.0	14.0	16.5	30.0	33.0
5.0	7.3	7.4	7.0	8.1	7.7	7.4	8.0	7.4	7.2	7.5	7.5
33.0	26.3	23.0	17.0	16.0	12.0	7.4	13.0	15.0	26.4	33.0	33.0
7.2	7.0	7.6	7.6	7.2	7.0	7.2	7.6	7.1	7.3	7.0	7.0
33.0	23.0	15.5	11.5	7.2	7.0	7.2	13.0	17.0	24.5	28.0	28.0
6.3	5.7	5.8	5.7	7.1	6.8	6.2	6.8	4.2	5.3	5.0	5.0
33.0	25.9	22.0	19.5	15.5	12.5	6.2	12.0	15.0	30.0	26.8	33.0
4.0	3.9	5.7	5.8	6.3	5.9	6.3	6.0	5.7	5.5	5.5	5.5
33.0	31.0	21.0	21.0	15.0	5.9	6.3	13.0	18.0	21.0	33.0	33.0
1.3	1.8	2.8	3.4	4.4	5.9	5.7	5.7	4.0	5.4	4.9	3.8
33.0	31.0	32.0	27.4	25.0	18.0	10.3	7.0	11.5	15.0	22.0	23.0
2.8	2.5	4.2	4.0	4.4	5.7	5.4	5.4	5.2	4.2	2.6	1.2
33.0	31.0	24.0	23.8	17.0	9.0	5.2	3.0	9.5	15.0	22.5	23.5
4.3	4.3	5.2	5.5	5.6	5.2	5.6	5.6	5.2	5.0	4.0	3.6
33.0	32.8	29.8	22.0	13.5	5.2	5.6	11.5	15.5	22.0	27.5	33.0
3.2	3.2	4.7	5.1	5.9	6.1	6.0	6.0	5.4	5.0	4.2	4.1
33.0	30.5	24.5	25.8	14.5	13.0	5.9	10.0	15.0	21.0	22.5	24.0
5.2	5.2	6.1	6.3	6.3	6.3	6.2	6.2	6.1	5.3	3.2	3.0
33.0	25.0	19.5	14.5	5.9	6.2	6.2	11.0	12.0	23.0	27.0	33.0
4.0	5.1	6.5	6.7	6.0	6.0	6.1	6.1	6.1	6.6	6.0	4.8
33.0	28.9	22.0	16.0	6.0	6.1	6.1	7.5	16.5	19.5	23.0	26.0
7.6	8.7	8.8	7.5	7.1	6.5	6.4	6.4	6.4	7.4	7.3	3.0
33.0	26.0	25.0	19.0	15.5	13.0	6.4	11.0	14.0	17.0	20.5	25.0
9.0	9.5	9.3	7.8	7.2	7.1	6.4	6.4	6.2	6.4	8.1	3.9
33.0	37.0	35.5	21.0	17.8	17.0	6.5	3.5	15.0	17.5	21.0	26.9
10.4	10.6	8.7	6.4	6.5	6.5	6.5	6.4	6.3	8.5	6.1	5.8
33.0	26.0	22.0	15.0	6.5	6.5	6.5	4.0	17.0	21.5	30.0	33.0
13.1	12.6	5.5	5.5	5.5	5.5	5.5	5.5	5.7	5.7	11.4	11.9
33.0	26.0	16.9	11.0	5.4	5.5	5.5	7.0	17.0	17.2	17.0	21.5
6.3	6.0	7.0	6.7	5.0	5.0	5.0	5.0	5.0	6.3	6.0	3.7
33.0	26.0	23.0	17.0	5.0	5.0	5.0	10.0	17.0	22.5	25.5	30.5
3.5	3.3	4.8	5.5	5.9	5.1	4.9	4.9	4.8	4.6	6.0	4.8
33.0	30.5	33.0	20.0	16.5	19.0	4.8	7.0	13.5	18.5	27.5	20.0
4.8	5.7	5.6	5.0	4.8	4.8	4.8	4.9	5.0	4.9	4.0	4.1
33.0	25.0	21.5	14.0	4.8	4.8	4.8	11.5	17.5	24.5	28.0	33.0
6.7	6.5	6.1	5.1	4.7	4.7	4.7	4.9	5.2	5.3	6.4	6.6
33.0	25.0	18.1	17.5	4.7	4.7	4.7	11.0	16.0	16.9	23.5	33.0

Station	+	H. I	-	Grade	Chase Rod.
		299.46			
28+70				90.7	8.8
29+00				90.7	8.8
+65				90.8	8.7
30+00				90.0	8.6
30+40					
B.M.	7.03	296.72		(299.69)	
31+00				91.2	5.5
32+00				91.6	5.1
33+00				92.0	4.7
34+00				92.4	4.3
T.P.	8.45	300.04	5.13	(291.59)	
35+00				92.6	7.4
+80				92.3	7.7
36+00				92.2	7.8
+91					
T.P.	2.04	295.46	6.62	(293.42)	
37+00				91.6	3.9
38+00				90.6	4.9
39+00				89.6	5.9
+24				89.4	6.1
T.P.	2.11	291.74	5.83	(299.63)	
40+00				88.6	3.1
41+00				87.6	4.1
42+00				87.2	4.5
43+00				88.0	3.7
T.P.	6.08	296.56	7.26	290.08	



Station	+	H. I	-	Grade Course	Grade Rod
		296.56			
44+00				90.2	6.4 ✓
+78				92.4	4.2
45+00				93.0	3.6
45+00				294.02 ✓	
B.M.	9.41	302.93 ✓			
46+00				95.7	8.1 ✓
47+00				97.9	5.9 ✓
+25				98.3 ✓	5.5
T.P.	9.01	308.99 ✓	4.45	299.38	
+62				98.7	9.7
48+00				99.0	9.4 ✓
+15				99.1	9.3
49+00				99.2	9.2 ✓
50+00				99.5	9.1 ✓
51+00				96.9 ✓	11.5 ✓
T.P.	5.18	302.11 ✓	11.46	296.93	
+75				95.1	7.0 -
52+00				94.4 ✓	7.7 -
53+00				91.4 ✓	10.7 ✓
T.P.	2.54	292.72 ✓	11.93	290.18 ✓	
+40				90.2	2.5
+66				90.1	2.6
54+00				88.6	4.1
55+00				85.5 ✓	7.2 ✓
T.P.	4.00	285.94 ✓	10.79	281.94 ✓	

h z R

14.2	13.7	19.3	18.3	7.5	7.0	6.7	6.9	7.0	7.3	11.2	12.1
33.0	28.0	27.4	21.0	11.5	7.0	6.8	8.0	15.0	17.0	15.0	25.5
		6.3	8.0	5.1	4.5	4.7	5.0	5.8	5.7		
		33.0	41.5	17.0	7.0	4.6	11.5	17.5	24.0	33.0	
5.3	4.1	4.7	4.9	4.0	3.7	4.1	4.5	5.2	4.8	4.1	
33.0	27.5	28.7	15.5	12.0	7.0	3.9	12.5	18.0	23.4	27.5	33.0

11.2	7.4	8.1	7.9	8.0	9.0	5.1	9.4	7.6	7.8	8.1
33.0	23.7	20.0	17.5	17.0	13.0	6.0	12.5	17.0	25.5	30.0
	8.7	6.6	6.4	6.3	5.6	5.9	5.6	5.3	5.4	5.2
	33.0	27.0	24.5	7.0	14.0	5.5	15.0	18.0	21.5	25.5
	7.0	6.1	5.4	4.7	4.7	4.9	5.1	4.8	4.1	
	33.0	23.5	18.0	13.0	5.1	15.5	19.0	27.0	33.0	

6.1	6.0	9.3	9.7	9.7	9.2	7.0	7.1	8.9	3.3
33.0	27.5	24.0	19.0	14.0	11.0	9.2	13.0	21.0	36.5
4.1	4.1	9.4	9.2	9.1	9.0	8.3	9.0	9.1	8.9
33.0	32.5	27.5	25.0	21.0	15.5	11.5	8.8	14.0	16.0
11.5	4.8	6.6	8.2	8.0	8.3	8.5	8.2	9.0	7.0
33.0	30.0	28.0	22.0	14.0	11.0	8.7	11.0	15.0	20.0
2.3	2.3	4.5	7.8	8.4	8.0	8.6	8.6	8.6	8.8
33.0	31.7	27.5	25.0	22.0	12.0	8.4	7.0	7.0	25.6
3.8	5.8	6.9	8.2	9.0	9.2	8.9	9.4	9.3	8.5
33.0	30.0	28.0	23.5	13.5	9.2	15.0	25.5	30.0	35.5
8.2	11.0	11.5	11.7	11.5	11.4	11.5	11.5	11.7	11.6
33.0	37.0	25.0	14.5	5.4	11.4	9.5	9.5	20.0	24.8

4.3	4.3	6.5	7.3	7.6	7.7	7.2	7.4	7.9	7.0
33.0	31.0	24.0	14.0	9.0	7.4	9.0	13.0	24.0	30.0
5.7	5.5	6.5	7.8	8.2	8.4	9.4	8.3	6.6	8.5
33.0	31.0	24.3	14.5	9.0	8.2	9.5	20.0	24.2	30.5
10.2	12.0	11.8	11.4	11.4	11.4	10.5	11.6	11.8	11.8
33.0	23.8	14.5	12.5	11.4	11.4	10.7	24.2	33.0	

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	3.9	3.4	2.6	2.0	3.0	3.6	2.3	2.1
	33.0	30.0	15.0	2.8	10.5	15.5	22.5	25.0
	4.7	4.6	4.0	2.7	2.5	2.6	6.6	7.3
	33.0	36.5	7.0	10.5	2.7	12.5	17.0	27.0
4.4	4.5	6.4	4.3	3.8	3.8	3.7	3.7	4.2
33.0	34.0	33.5	7.0	14.5	10.0	3.7	7.0	7.5
12.0	12.0	12.0	7.5	7.5	7.5	7.9	7.6	7.6
33.0	36.0	30.0	13.0	7.0	7.5	15.0	17.0	13.6

Station	+	H.I.	-	Profile Grade	Grade rod
		285.94			
56+00				82.2	3.7
57+00				78.9	7.0
58+00				75.6	10.3
T.P.	3.47	277.27	12.14	273.80	
59+00				77.3	5.0
60+00				69.0	6.3
T.P.	3.75	270.07	10.95	266.32	
61+00				66.3	3.2
62+00				64.7	5.4
63+00				63.7	6.4
B.M.	5.26	266.63		(261.37)	
64+00				62.7	3.9
65+00				62.0	4.6
66+00				61.7	4.9
67+00				61.7	4.9
68+00				61.9	4.7
T.P.	6.74	268.15	5.19	(261.44)	
69+00				62.6	5.6
70+00				63.8	4.4
+25				64.2	4.0
71+00				65.4	2.8

h.

L

P

1. 5. 400  
 2. 10. 1000  
 3. 15. 1500  
 4. 20. 2000  
 5. 25. 2500  
 6. 30. 3000  
 7. 35. 3500  
 8. 40. 4000  
 9. 45. 4500  
 10. 50. 5000  
 11. 55. 5500  
 12. 60. 6000  
 13. 65. 6500  
 14. 70. 7000  
 15. 75. 7500  
 16. 80. 8000  
 17. 85. 8500  
 18. 90. 9000  
 19. 95. 9500  
 20. 100. 10000

$\frac{7.6}{33.0} \frac{7.6}{23.0} \frac{4.2}{17.0} \frac{3.8}{15.0} \frac{3.7}{11.0} \frac{3.7}{12.5} \frac{4.1}{16.8} \frac{4.0}{17.5} \frac{3.7}{18.5} \frac{7.7}{26.0} \frac{7.9}{22.0} \frac{9.0}{20.0}$

$\frac{3.1}{33.0} \frac{8.1}{23.9} \frac{6.0}{19.0} \frac{6.9}{14.0} \frac{7.0}{10.5} \frac{7.1}{15.0} \frac{7.2}{16.5} \frac{7.3}{18.5} \frac{9.3}{22.0} \frac{9.1}{24.0} \frac{8.3}{26.0} \frac{7.9}{33.0}$

$\frac{11.2}{33.0} \frac{11.7}{25.0} \frac{11.7}{23.4} \frac{10.7}{19.0} \frac{11.0}{17.5} \frac{10.8}{15.0} \frac{10.6}{14.0} \frac{10.9}{14.0} \frac{11.0}{24.3} \frac{11.0}{33.0}$

$\frac{1.4}{33.0} \frac{1.2}{3.0} \frac{3.9}{27.0} \frac{3.9}{19.5} \frac{3.8}{12.0} \frac{3.5}{3.5} \frac{3.7}{12.5} \frac{3.3}{19.0} \frac{5.2}{22.0} \frac{4.5}{24.0} \frac{2.6}{28.0} \frac{2.8}{33.0}$

$\frac{3.1}{33.0} \frac{5.0}{30.5} \frac{6.2}{27.0} \frac{6.0}{24.0} \frac{5.7}{19.5} \frac{5.4}{17.0} \frac{5.1}{5.1} \frac{5.2}{15.0} \frac{5.0}{18.0} \frac{6.3}{23.5} \frac{6.3}{23.7} \frac{6.5}{26.0} \frac{5.5}{23.5} \frac{5.3}{32.0} \frac{3.2}{24.5}$

$\frac{10.1}{33.0} \frac{9.7}{28.5} \frac{8.2}{17.0} \frac{8.2}{12.0} \frac{8.5}{8.5} \frac{8.3}{16.0} \frac{8.4}{20.0} \frac{9.7}{23.6} \frac{10.2}{31.0} \frac{9.7}{33.0}$

$\frac{6.6}{33.0} \frac{6.1}{17.5} \frac{4.3}{16.0} \frac{3.8}{13.5} \frac{3.8}{3.8} \frac{2.9}{18.0} \frac{3.6}{18.0} \frac{4.7}{20.5} \frac{4.5}{24.0} \frac{4.8}{25.0} \frac{4.6}{33.0}$

$\frac{7.7}{33.0} \frac{7.1}{23.3} \frac{6.2}{18.0} \frac{6.0}{13.5} \frac{5.6}{5.6} \frac{5.4}{15.5} \frac{5.3}{16.7} \frac{6.4}{20.0} \frac{7.2}{23.2} \frac{7.4}{24.5} \frac{7.4}{33.0}$

$\frac{8.7}{33.0} \frac{8.7}{24.5} \frac{8.3}{21.0} \frac{6.5}{16.2} \frac{6.5}{14.0} \frac{6.7}{6.7} \frac{6.5}{15.0} \frac{6.5}{16.0} \frac{7.8}{20.0} \frac{8.0}{23.0} \frac{8.4}{33.0}$

$\frac{5.8}{33.0} \frac{6.9}{33.0} \frac{6.4}{25.0} \frac{5.7}{21.0} \frac{4.2}{17.0} \frac{4.2}{16.5} \frac{4.8}{11.5} \frac{4.2}{4.2} \frac{4.1}{12.0} \frac{4.1}{18.5} \frac{6.1}{19.8} \frac{6.5}{23.0} \frac{6.8}{33.0}$

$\frac{8.6}{33.0} \frac{7.7}{25.0} \frac{7.1}{23.0} \frac{5.2}{19.0} \frac{5.1}{16.8} \frac{5.1}{12.5} \frac{4.9}{4.9} \frac{5.0}{11.0} \frac{5.0}{14.0} \frac{6.1}{17.0} \frac{8.6}{21.0} \frac{8.6}{22.0} \frac{9.0}{33.0}$

$\frac{10.1}{33.0} \frac{9.1}{24.0} \frac{6.1}{19.0} \frac{5.6}{17.1} \frac{5.7}{11.0} \frac{5.5}{5.5} \frac{5.5}{11.0} \frac{5.4}{15.0} \frac{5.6}{17.4} \frac{7.9}{22.0} \frac{7.8}{33.0}$

$\frac{10.7}{33.0} \frac{10.2}{22.0} \frac{9.9}{23.8} \frac{5.9}{17.0} \frac{5.7}{12.5} \frac{5.6}{5.6} \frac{5.6}{12.0} \frac{5.7}{15.5} \frac{6.2}{19.0} \frac{7.4}{21.0} \frac{7.6}{33.0}$

$\frac{7.0}{33.0} \frac{7.7}{26.0} \frac{7.2}{20.0} \frac{6.8}{14.5} \frac{5.8}{13.0} \frac{5.4}{5.4} \frac{5.2}{11.0} \frac{4.9}{13.0} \frac{5.8}{17.7} \frac{6.3}{20.0} \frac{5.8}{33.0}$

$\frac{7.3}{33.0} \frac{7.6}{23.0} \frac{3.4}{22.5} \frac{6.4}{19.0} \frac{6.1}{16.8} \frac{6.1}{12.5} \frac{6.0}{6.0} \frac{6.0}{14.0} \frac{6.6}{14.5} \frac{9.2}{21.7} \frac{7.7}{33.0}$

$\frac{3.7}{33.0} \frac{4.9}{28.0} \frac{5.5}{25.0} \frac{5.2}{24.2} \frac{5.2}{19.0} \frac{4.7}{17.0} \frac{4.6}{4.6} \frac{4.7}{11.5} \frac{5.0}{12.0} \frac{5.7}{18.0} \frac{6.0}{20.0} \frac{7.5}{23.0} \frac{8.2}{33.0}$

$\frac{7.8}{33.0} \frac{9.0}{27.0} \frac{4.0}{22.5} \frac{4.4}{18.5} \frac{4.0}{15.0} \frac{4.0}{4.0} \frac{4.0}{10.0} \frac{4.2}{10.0} \frac{4.5}{11.0} \frac{4.5}{21.0} \frac{33.0}{33.0}$

$\frac{3.1}{33.0} \frac{5.1}{24.7} \frac{3.2}{16.0} \frac{2.8}{2.8} \frac{5.0}{17.0} \frac{3.5}{23.0} \frac{3.8}{24.0} \frac{4.1}{26.5} \frac{3.8}{26.5} \frac{1.1}{33.0}$

Station	+	H.I	-	Profile Grade	Grade Rod
B.M	4.24	295.32		291.08	
121+00				90.3	5.0
+50				90.7	4.6
122+00				91.1	4.2
123+00				91.9	3.4
124+00				92.7	2.6
T.P.	4.63	297.37	2.58	292.70	
+38				92.9	4.5
125+00				93.1	4.3
+62				93.0	4.4
126+00				92.8	4.6
127+00				92.1	5.3
128+00				91.4	6.0
T.P.	5.65	295.15	7.87	289.50	
+50				91.2	4.0
129+00				91.1	4.1
+50				91.2	4.0
130+00				91.5	3.7
131+00				92.3	2.9
132+00				93.4	1.8

E

P

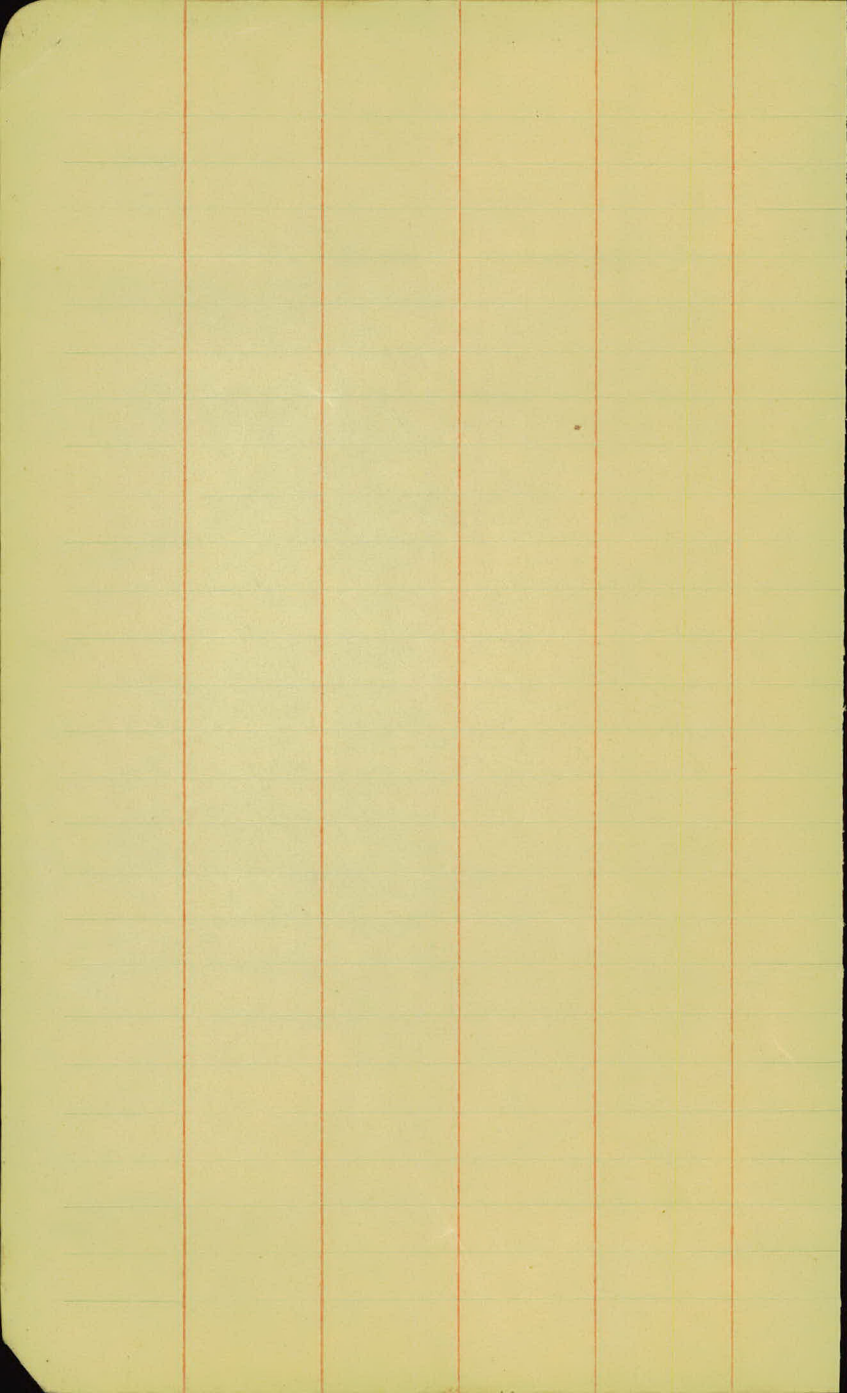
	5.3	5.6	5.6	5.1		5.1	5.5	5.6	5.8	
	33.0	39.0	14.5	7.0	3.1	10.5	21.5	27.0	33.0	
	5.3	5.6	5.6	4.8	4.7	5.5	5.7	4.8	4.7	
	33.0	34.2	22.0	14.0	7.0	4.9	11.5	75.0	24.8	33.0
	4.8	5.2	5.3	4.6		4.6	5.3	4.8	4.8	4.5
	33.0	34.0	15.5	12.0	4.6	6.0	14.0	23.0	20.7	30.0
	4.9	4.3	4.5	4.3	3.7	3.7	4.3	3.1	3.4	4.0
	33.0	24.2	22.0	16.5	12.0	3.7	7.8	75.0	22.5	25.0
	3.0	2.8	3.2	3.4	2.8	2.6	2.6	3.4	3.3	2.6
	33.0	28.5	24.4	16.5	12.0	2.6	4.0	12.0	13.5	16.0
	4.8	5.1	4.9	4.2		4.2	5.1	5.6	5.3	4.5
	33.0	31.0	16.0	11.5	4.3	11.0	15.0	18.0	23.5	7.0
	4.3	4.8	4.9	4.3	4.1	4.2	4.3	5.2	5.6	5.1
	33.0	28.5	24.2	15.7	3.0	4.1	12.0	12.5	15.0	23.9
	4.8	5.3	5.5	4.9	4.3	4.6	4.6	5.3	4.7	4.3
	33.0	25.0	30.0	11.0	12.0	4.2	6.0	12.0	14.5	7.0
	5.5	5.4	5.6	5.6	5.4	4.9	4.7	5.0	5.7	5.3
	33.0	28.0	24.0	12.0	14.5	4.6	5.0	13.0	14.5	17.5
	7.0	7.2	7.3	7.1	6.4	6.3	7.1	7.1	6.8	6.5
	33.0	27.5	23.0	13.5	13.0	6.0	12.5	15.0	21.5	23.5
	8.0	7.6	7.5	8.1	7.4	6.8	6.8	7.7	7.3	7.8
	33.0	23.4	22.0	16.0	13.0	6.6	7.0	15.0	23.4	27.0
	7.1	6.7	5.5	4.6	4.3	4.7	5.3	6.2	6.7	6.6
	33.0	30.0	13.5	11.4	8.5	4.5	11.0	13.0	18.0	34.0
	7.3	7.1	6.8	6.7	5.2	4.5	4.7	5.2	5.9	6.2
	33.0	24.5	20.0	7.0	12.0	4.4	12.5	14.0	12.9	27.0
	7.3	6.6	6.1	5.5	4.8	5.1	5.9	6.4	7.8	6.6
	33.0	24.0	14.0	10.0	8.0	4.8	12.0	15.0	18.0	19.5
	7.2	6.9	6.7	5.4	4.1	4.5	5.1	5.9	6.2	7.4
	33.0	21.0	17.5	13.0	14.5	4.5	8.0	74.0	7.0	12.0
	5.1	3.9	4.4	5.9	6.4	4.6	4.1	4.4	5.9	5.7
	33.0	24.0	21.5	20.5	15.0	3.5	12.0	18.0	17.0	20.5
	2.4	2.2	3.1	3.6	4.7	2.8	2.9	2.5	3.0	3.9
	33.0	24.3	21.5	7.5	12.0	1.9	13.0	15.0	76.0	19.0
	5.1	3.9	4.4	5.9	6.4	4.6	4.1	4.4	5.9	5.7
	33.0	24.0	21.5	20.5	15.0	3.5	12.0	18.0	17.0	20.5
	2.4	2.2	3.1	3.6	4.7	2.8	2.9	2.5	3.0	3.9
	33.0	24.3	21.5	7.5	12.0	1.9	13.0	15.0	76.0	19.0
	5.1	3.9	4.4	5.9	6.4	4.6	4.1	4.4	5.9	5.7
	33.0	24.0	21.5	20.5	15.0	3.5	12.0	18.0	17.0	20.5
	2.4	2.2	3.1	3.6	4.7	2.8	2.9	2.5	3.0	3.9
	33.0	24.3	21.5	7.5	12.0	1.9	13.0	15.0	76.0	19.0

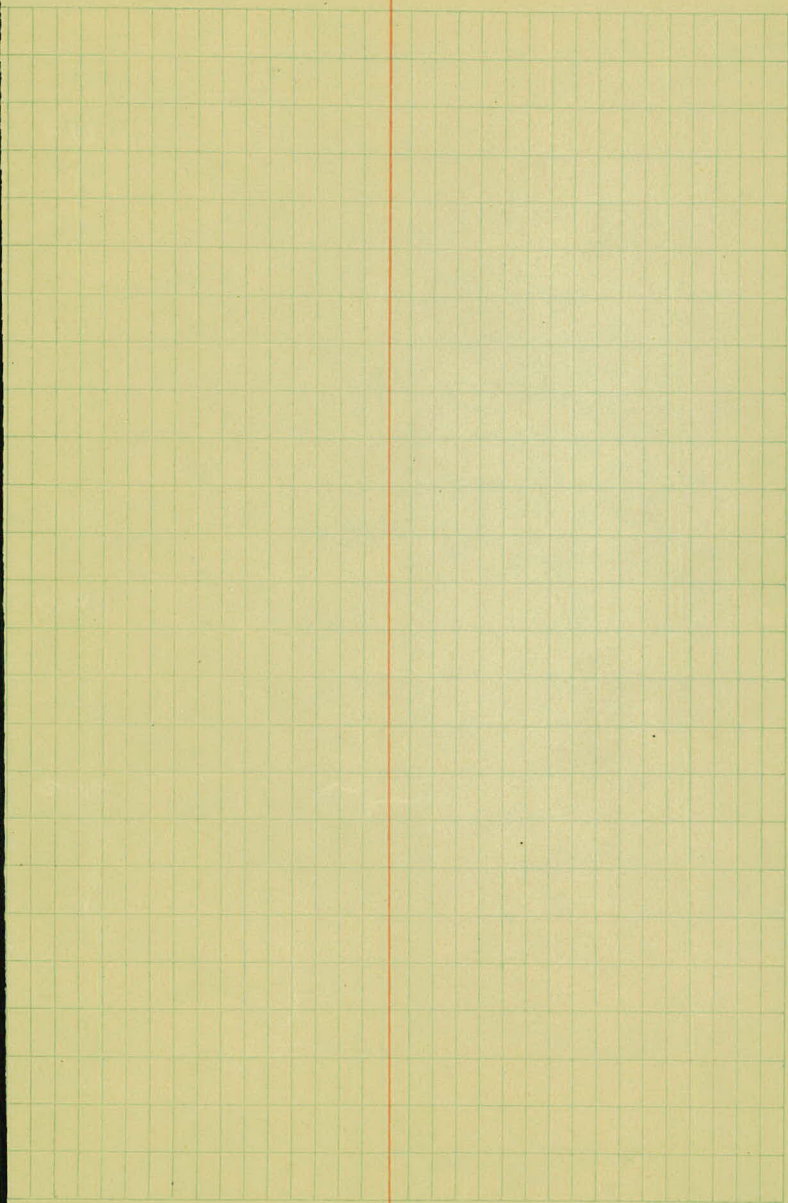
Station	+	H.I.	-	Profile Grade	Grade R.R.
182+					
B.M.	9.58	300.88		(292.80)	
133+00				95.1	5.8
+25				95.6	5.3
134+00				97.1	3.8
+63	B.S.T.			98.4	2.5
T.P.	6.10	305.57	1.41	(299.47)	
135+13		50		99.4	6.3 6.2-6
135+63	B.W.T.	100		300.4	5.6 5.2-4
136+13	B.C.	150		301.4	5.0 2.7 3
B.M.	4.59	306.57		301.98	
136+36		50		301.55	5.8 4.7
+63		50		302.30	5.6 4.7
+88				302.70	5.2 3.9
137+13				303.05	4.8 3.5
+42		50		303.40	4.5 3.2
+66		50		303.63	4.0 3.0
+91		50		303.83	3.5 2.8

E.W.T }  
E.S.T }

E.C.







Sta	+	H.S.	-	Elev	Grade
4					61.4
	+50				63.2
5					65.0
	+50				
6					67.6
	B.M.	0.30	275.64		<u>275.34</u>
	+50				69.0
7					69.4
	+50				70.2
8					70.1
	+50				
9					
	+50				
10					
	+50				
11					

LT

±

RT

24

9495

2112

$$\frac{5.4}{26.2}$$

$$\frac{6.8}{24.8}$$

102

2013

$$\frac{5.1}{25.3}$$

$$\frac{5.1}{25.3}$$

103

Final - X sections. Culverts. Guard Rail

Station	+	H.I.	-	Rod.	Profile Elev
B.M.	7.23	255.43	✓		248.20
0+00					
+50					
1+00					
+57					
2+00					
B.M.	9.98	264.60	✓	0.81	254.62 ✓
+50					
3+00					
+50			✓		
T.P.	10.19	271.79		3.00	261.60 ✓
4+00					
+50					
5+00					

fasting  
Kochian  
enthusiastic  
chirpitt

8-5-24

25

H. E. H.

Top. Hydrant White Bear Rd & Carpenter Ave

(6.0) 5.17  $\frac{5.30}{10.0}$   $\frac{4.7}{15.5}$   $\frac{8.3}{21.7}$   $\frac{9.6}{22.3}$   $\frac{9.2}{27.7}$   $\frac{8.1}{28.5}$   $\frac{7.4}{32.8}$   $\frac{7.4}{31.5}$

(5.1) 4.36  $\frac{4.48}{11.0}$   $\frac{4.26}{15.5}$   $\frac{4.4}{17.5}$   $\frac{6.9}{22.1}$   $\frac{7.0}{24.0}$   $\frac{6.6}{27.5}$   $\frac{6.3}{32.4}$

Edge Pond (3.9) 3.24  $\frac{3.49}{11.2}$   $\frac{3.24}{12.3}$   $\frac{3.1}{16.6}$   $\frac{5.1}{21.8}$   $\frac{5.5}{24.4}$   $\frac{5.3}{26.0}$   $\frac{4.7}{27.7}$   $\frac{4.7}{33.0}$

W. Spout (2.9) 2.0  $\frac{2.40}{11.1}$   $\frac{2.18}{12.3}$   $\frac{2.0}{14.5}$   $\frac{4.0}{23.2}$   $\frac{4.1}{25.9}$   $\frac{4.0}{28.0}$   $\frac{3.2}{29.8}$   $\frac{3.2}{38.0}$   
E. Div. 2.06  
24.4 E. Div. 1.72  
10.5

Drugs in Park H. 2-1-36

$\frac{12.3}{38.0}$   $\frac{12.6}{37.8}$   $\frac{12.2}{33.2}$   $\frac{7.4}{15.4}$   $\frac{8.0}{15.0}$  (9.0)  $\frac{9.75}{11.3}$   $\frac{9.52}{12.4}$   $\frac{9.6}{12.8}$   $\frac{10.8}{23.4}$   $\frac{12.0}{26.3}$   $\frac{11.4}{27.6}$   $\frac{10.6}{33.0}$

$\frac{9.1}{38.0}$   $\frac{9.1}{32.7}$   $\frac{10.4}{26.3}$   $\frac{10.2}{32.7}$   $\frac{6.4}{14.6}$  (7.6)  $\frac{6.25}{7.8}$   $\frac{7.68}{11.2}$   $\frac{7.53}{12.45}$   $\frac{7.5}{14.7}$   $\frac{9.8}{23.0}$   $\frac{10.1}{27.0}$   $\frac{6.8}{32.6}$   $\frac{4.8}{38.0}$

(5.3) 4.67  $\frac{5.03}{11.4}$   $\frac{5.26}{12.9}$   $\frac{5.2}{17.2}$   $\frac{6.9}{21.5}$   $\frac{6.7}{25.4}$   $\frac{2.6}{32.2}$   $\frac{2.4}{33.0}$

(10.7) 9.73  $\frac{10.5}{11.3}$   $\frac{10.32}{12.5}$   $\frac{10.7}{17.1}$   $\frac{12.2}{22.2}$   $\frac{12.6}{25.2}$   $\frac{12.0}{28.4}$   $\frac{11.5}{36.1}$   $\frac{5.8}{39.3}$

(8.2) 7.87  $\frac{8.65}{11.4}$   $\frac{8.43}{12.8}$   $\frac{8.7}{17.3}$   $\frac{10.8}{22.0}$   $\frac{10.5}{24.3}$   $\frac{9.6}{27.7}$   $\frac{5.0}{33.6}$

(6.4) 6.18  $\frac{6.64}{10.6}$   $\frac{6.03}{11.8}$   $\frac{6.5}{14.0}$   $\frac{8.5}{20.7}$   $\frac{8.5}{24.0}$   $\frac{8.0}{26.8}$   $\frac{5.7}{31.7}$   $\frac{4.8}{38.0}$

Station	+	H.I	-	Rod	Elev.
		271.79 ✓			
5+50					
6+00					
+50					
7+00					
8+00					
T.P.	5.05	276.04 ✓	0.80	270.99 ✓	
+50					
9+00					
+50					
B.M.			0.04	275.40 ✓	
10+00					
T.P.	4.79	275.42 ✓	5.20	270.64 ✓	
+64					
11+00					
+50					
12+00					

At.

±

At.

2.7	2.5	5.8	5.8	4.2	4.35	4.87	4.30	4.8	6.5	6.2	4.5	3.8
32.5	30.4	22.0	19.5	15.0	12.7	4.68	7.5	70.7	15.1	20.0	25.8	37.8

0.2	1.3	4.0	4.4	3.3	3.1	3.3	3.6	2.55	3.31	3.5	4.9	5.5	5.1	4.0	3.6	2.8
36.7	20.0	23.8	19.3	16.5	13.7	12.0	2.41	7.0	10.7	15.4	19.2	23.5	26.3	30.8	32.9	33.8

1.4	1.4	3.4	4.2	4.0	2.5	2.5	2.50	3.5	4.1	5.0	4.7	3.6	3.6
3.0	3.03	25.1	22.6	20.8	17.5	16.1	2.50	4.2	15.6	19.6	24.3	27.0	33.1

2.3	2.6	4.0	4.2	3.8	1.8	1.80	1.74	1.74	1.9	4.4	4.7	4.0	1.8
33.0	29.6	28.1	22.6	18.4	14.6	10.0	1.74	10.0	14.9	20.7	26.0	30.6	33.1

1.6	2.0	2.8	3.3	3.0	1.1	0.91	0.88	0.96	1.0	3.7	4.1	3.5	0.7
29.6	27.9	26.4	22.9	20.3	15.0	10.0	0.88	10.0	15.2	21.2	23.0	29.8	33.0

6.5	6.6	7.6	8.0	7.5	5.3	5.05	5.8	5.13	5.2	7.8	8.0	7.3	3.7	3.6
33.0	36.0	27.0	25.4	18.8	14.5	10.0	5.01	10.0	14.7	21.2	23.6	27.6	32.1	33.0

6.6	6.8	7.6	8.5	7.8	5.4	5.11	5.8	5.05	5.3	7.5	7.8	7.5	1.4	1.4
32.0	31.0	29.3	25.0	20.6	14.6	10.0	5.0	10.0	14.8	19.9	23.7	27.0	32.2	33.0

5.6	5.6	7.3	8.1	6.7	5.3	5.15	5.8	5.17	5.2	7.3	7.3	0.0
33.0	29.8	28.0	26.2	22.5	16.6	10.0	5.10	10.0	15.3	20.0	24.8	34.0

Galvin T.P. 35 At 9-25

8.7	8.7	10.0	10.4	9.4	5.5	5.28	5.9	5.25	5.3	6.5	8.4	8.0	7.2	2.8
33.0	32.3	30.9	27.4	25.1	15.4	10.0	5.18	10.0	14.8	17.9	20.5	25.0	26.0	33.0

2/49 270 11-00

12.1	11.9	9.3	5.9	5.1	4.7	5.4	4.75	4.8	9.5	9.9	9.4	8.6	7.8
33.0	29.5	25.4	18.0	14.7	10.0	4.73	10.0	15.8	21.4	24.6	30.5	32.2	33.5

12.6	11.6	6.1	5.1	5.00	5.4	4.88	4.88	5.0	8.7	9.5	4.5	7.8
33.0	27.2	18.1	15.4	10.0	4.55	4.88	10.0	15.2	22.2	26.3	30.7	33.0

12.9	12.7	5.2	4.88	5.3	4.81	4.81	4.81	4.8	11.0	11.6	11.4
33.0	20.6	16.0	10.0	4.82	4.81	4.81	10.0	15.0	25.1	31.8	33.0

12.8	12.5	5.0	4.73	5.1	4.73	4.73	4.73	5.0	11.4	12.0	12.1
33.0	29.6	16.3	10.0	4.73	4.73	4.73	10.0	15.4	24.4	28.8	33.0

Station	+	H.I.	-	Rod	Elev
		275.42	✓		
12+50					
13+00					
+55					
T.P.	6.59	280.73	✓	1.28	274.14 ✓
+80					
14+00					
+50					
15+00					
+50					
T.P.	8.37	287.84	✓	1.26	279.47 ✓
+70		See Page 43			
B.M.	2.45	294.75	✓		292.30
T.P.	1.50	285.26	✓	10.99	283.76 ✓
16+00	End of Pavement.				
+13.5					
+23					

St.

£

Rt.

12.4 12.0 4.8 4.20 (4.7) 4.05 4.0 11.8 12.4  
 33.0 30.0 16.4 10.0 4.06 10.0 15.7 27.0 33.0

11.8 11.1 3.8 3.45 (4.0) 3.27 3.30 11.1 11.7  
 33.0 27.0 16.2 12.0 3.30 10.0 15.3 37.0 33.0

10.4 10.0 4.3 5.1 2.85 (3.5) 2.65 2.5 8.7 9.7  
 33.0 26.0 17.8 14.5 10.0 2.70 10.0 15.4 26.2 33.0

11.4 11.4 12.2 12.9 12.3 7.2 7.13 (8.0) 7.08 7.1 12.4 14.5  
 33.0 32.5 31.0 26.7 25.8 15.5 12.0 7.01 10.0 15.0 24.3 33.0

9.5 11.0 11.4 11.0 6.9 6.61 (7.5) 6.64 6.6 13.0 14.0  
 33.6 30.6 28.3 24.4 15.5 10.0 6.59 10.0 14.8 26.0 33.0

8.3 9.2 8.8 7.0 5.8 5.3 5.33 (6.3) 5.37 5.5 10.9 12.2  
 31.0 28.6 25.7 21.7 17.8 14.7 10.0 5.77 10.0 14.9 23.3 33.0

6.4 7.9 7.7 6.8 4.2 4.01 (4.9) 4.06 4.3 7.0 7.6 12.7  
 34.0 30.4 25.7 23.0 14.8 10.0 3.96 10.0 14.7 23.0 26.0 33.0

5 2.7 4.9 6.2 3.4 2.9 2.73 (3.4) 2.81 3.0 7.4 9.0  
 0 31.4 27.4 26.4 16.6 14.0 10.0 2.70 10.0 15.3 23.7 33.0

6.2 8.8 9.6 7.6 9.3 9.32 (9.9) 9.32 9.6 13.3 14.4 500 19.23  
 33.0 31.0 21.0 16.8 14.0 12.0 9.05 10.0 14.6 26.7 33.0

Wail in T.P. Rt. Sta. 20 + 15

W.A.C.  
 P.H.C.  
 A.S.N.  
 M.S.A.

5.0 4.9 5.85 (6.3) 5.81 5.85 6.0 7.4 5.3 5.4 6.0 3.2  
 33 24 10.0 10.0 14 18 32 27 29 33

1.7 4.5 5.1 6.8 6.8 5.1 5.2 5.47 (6.1) 5.47 5.5 6.9 6.9 4.0 4.9  
 39 34 26 25 23 20 17 10.0 10.0 15 19 23 30 33

1.1 3.0 5.3 6.7 6.7 5.1 5.12 (5.8) 5.12 5.18 5.3 6.9 6.0 2.8 2.9  
 37 35 26 24 24 17 10.0 10.0 15 19 25 31 33

Station	+	H.I	-	Rod	Elev.
		285.76 ✓			
16+50					
T.P.	11.92	294.42 ✓	2.76	282.50 ✓	
17+00					
18+00					
+50					
19+00					
+35					
20+00					
B.M. for check			2.13		292.39
B.M.	5.01	297.31 ✓			292.30
+50					
21+00					
22+00					
+45					
23+00					

Flustin  
Kroglan  
Molloney  
Salvin

Part 1  
H.

W.H. Carlsons  
Hickerson  
Nelson  
Wilburg.

Dec 10, 23

28

£

Fl.

5.00

6.0	5.7	5.8	6.1	4.3	4.29	4.27	4.33	4.4	6.1	6.1	5.4	1.0
33	28.5	26	24	15	10.0	10.0	10.0	15	18	24	27	34

17.6

6.5	7.8	13.8	13.1	12.5	11.92	11.92	12.08	12.2	12.3	14.0	10.0
35	29	22.5	18	15	10.0	10.0	10.0	15	20	24	34

9.6

4.7	1.7	4.1	11.5	11.2	7.5	7.42	9.35	9.43	7.5	11.4	11.6	7.4	7.5
3	31	24	20	18	15	10.0	10.0	10.0	14	19	25	32	33

8.2

3.5	3.7	5.0	10.2	7.8	2.5	8.34	8.24	8.33	8.4	10.2	10.3	6.5	6.5
32	24.5	26	20.5	18	15	10.0	10.0	10.0	15	19	25	32	33

2.00

5.5	5.8	9.5	9.1	7.4	7.30	7.24	7.31	7.2	9.2	9.4	5.5	5.7
33	26	21.5	19	15	10.0	10.0	10.0	14	18.6	24.5	30.5	33

6.2

5.8	5.4	8.8	8.1	6.8	6.76	6.66	6.72	6.8	8.8	8.9	5.4	5.4
33	28.4	21	18	14	10.0	10.0	10.0	14.5	19	25	31.5	33

5.2

4.5	4.3	7.4	7.3	5.8	5.72	5.65	5.73	5.7	7.1	7.2	3.4	3.4
33	26	22	18.7	14.5	10.0	10.0	10.0	15	18.5	24	31.5	33

Nail to T.P. Pt. Sta 20+15

(Flustin)

5.3	6.5	7.1	8.5	8.6	8.1	8.0	8.05	8.2	9.2	4.8	6.5	7.0
30.0	25.6	25.5	22.3	18.2	14.2	10.0	10.0	15.2	18.1	22.0	27.6	33.0

12/15/23

7.00

2.6	4.1	4.7	8.5	8.5	7.5	7.4	7.5	7.6	9.0	8.0	5.6	5.5
30.5	27.6	24.5	22.0	17.5	14.6	10.0	10.0	14.5	19.4	22.5	30.0	33.0

6.7

2.0	3.9	5.6	8.5	8.5	7.0	6.55	6.86	7.1	8.3	8.9	2.2
30.0	30.7	27.5	22.7	18.5	14.0	10.0	10.0	14.8	17.5	25.0	33.5

6.7

5.4	6.5	6.7	8.5	8.3	6.8	6.72	6.75	7.1	8.2	8.5	5.2	4.7
30.4	30.0	27.4	23.5	18.5	14.2	10.0	10.0	15.5	18.0	21.5	26.7	33.0

6.8

4.1	5.5	6.4	8.2	8.2	6.8	6.73	6.75	6.9	8.2	8.4	4.3	4.7
30.2	27.4	26.5	23.3	19.8	14.4	10.0	10.0	15.0	17.7	21.5	26.0	33.0

Station	+	H.I.	-	Rod	Elev.
		297.31 ✓			
+50					
24+00					
+75					
25+00					
T.P.	7.62	294.99 ✓	9.94	287.37 ✓	
+19					
26+00					
+82					
27+00					
+50					
28+00					
+70					
29+00					

H.

E

H.

6.1	6.1	8.5	7.6	4.8	6.7	6.9	6.75	7.0	8.2	8.4	4.2	4.0
33.0	25.5	22.5	16.5	11.8	10.0	6.62	10.0	15.0	17.8	21.6	27.4	33.0

5.8	6.0	8.3	7.4	6.7	6.6	6.9	6.75	6.7	7.6	8.4	7.3	5.9	5.6
33.0	25.9	22.5	17.3	14.3	10.0	6.68	10.0	14.2	16.5	22.8	24.2	27.7	33.0

8.3	8.4	9.6	8.4	7.9	7.6	6.7	6.57	6.61	6.7	7.6	7.6	4.0	3.9	
33.0	30.5	28.0	24.8	21.0	17.4	14.3	10.0	6.52	10.0	14.5	17.0	23.0	31.0	33.0

9.8	10.5	10.2	8.6	6.8	6.55	6.9	6.58	6.7	8.6	8.9	5.0	5.0	
33.0	30.2	29.0	25.0	22.0	15.0	10.0	6.45	7.0	15.0	19.5	24.0	31.5	33.0

9.0	9.8	9.2	6.3	4.6	4.9	4.6	4.7	4.2	4.9	6.9	7.0	4.6	4.4
33.0	30.0	28.5	24.0	14.5	10.0	4.11	10.0	14.2	17.0	20.5	23.5	31.5	33.0

12.9	12.2	6.2	4.2	4.5	4.6	4.01	4.2	5.6	11.0	11.5
33.0	27.0	18.5	14.2	10.3	3.97	10.0	14.5	19.0	27.0	33.0

6.0	5.8	7.1	6.8	4.1	3.93	4.5	3.89	4.0	5.7	6.1	6.8	3.7
33.0	27.0	25.0	14.5	10.0	3.82	10.0	14.5	22.2	23.7	25.7	33.0	

19

3.4	3.4	6.7	6.3	4.1	3.93	4.5	3.89	4.0	4.9	6.3	2.2
33.0	30.5	30.0	21.5	14.5	10.0	3.78	10.0	15.0	23.0	28.9	33.0

4.5	4.5	6.1	5.9	4.1	3.83	4.4	3.82	4.0	5.1	6.0	3.7
33.0	31.7	29.0	20.0	14.1	10.0	3.73	10.0	15.5	18.0	25.5	33.0

6.2	6.1	6.3	4.0	3.82	4.4	3.79	3.9	5.9	6.3	6.1
33.0	15.0	20.0	14.3	10.0	3.72	10.0	14.2	19.4	26.0	33.0

295.7	1.6	5.9	5.7	4.0	3.71	4.3	3.73	4.0	5.6	5.9	4.9	3.6
33.0	31.4	24.5	18.5	11.5	10.0	3.68	10.0	14.7	19.0	26.0	31.0	33.0

295.3	0.0	2.6	5.8	5.1	3.9	4.3	3.7	3.8	5.2	5.8	3.6	0.5
33.0	32.5	30.0	24.5	17.0	14.8	10.0	3.6	10.0	14.6	18.5	26.0	33.0

Station	+	H.I.	—	rod	Elev.
		294.91	✓		
29+65					
B.M.	7.81	297.53	✓	5.27	289.72 ✓
30+00					
31+00					
32+00					
33+00					
34+00					
35+00					
+60					
36+00					
B.M.	2.21	295.65	✓	11.09	293.44 ✓
37+00					
38+00					
39+00					

H.

£

P.

2.4	3.5	4.5	5.3	4.5	3.9	3.60	(47)	2.23	3.7	4.1	5.5	4.1	3.6	0.8
33.0	28.5	24.7	25.9	14.5	14.0	10.0	5.53	10.0	15.5	18.1	25.5	29.5	33.0	25.5

Nail in T.P. 1004 20420

7.3	7.6	8.5	7.3	6.1	6.2		(46)	6.1	6.1	8.8	5.3	7.4		
38.0	37.8	26.2	18.7	14.0	10.0	6.0	11.0	15.7	20.1	24.0	33.0			

12/10/23

10.1	9.9	5.9	5.76				(43)	5.77	5.8	7.0	7.8	10.1	10.8	
38.0	21.6	14.5	10.0	5.49			10.0	14.1	17.6	21.2	24.8	30.0		

10.1	10.0	5.5	5.32				(54)	5.30	5.8	6.7	7.0	6.6		
38.0	29.7	14.6	10.0	5.32			7.0	15.1	19.0	25.5	33.0			

6.6	5.4	5.8	7.5	6.8	5.2	4.9	(55)	4.97	5.2	6.4	6.8	7.7	6.1	
31.0	31.2	26.4	20.8	18.4	10.0	4.87	7.0	15.0	18.5	23.8	30.5	33.0		

6.1	5.3	7.3	6.8	4.7	4.58		(51)	4.56	4.7	5.8	6.3	6.6	7.3	5.3	2.7
38.0	30.0	27.3	19.0	14.5	10.0	4.48	10.0	14.8	17.8	20.0	21.8	31.0	31.0		27.0

4.4	4.7	6.3	5.3	4.5	4.87		(49)	4.87	4.4	5.5	6.3	6.7	4.7	4.8	
31.0	27.0	22.5	18.4	15.0	10.0	4.3	10.0	15.5	18.5	24.5	31.3	34.8	37.5		

4.5	4.5	6.1	4.8	4.5			(57)	4.56	4.7	6.0	6.6	6.9	5.1	4.0	2.5
38.0	24.8	20.5	15.0	10.0	4.19		7.0	14.7	19.0	24.0	27.5	30.0	34.0	34.0	

4.8	3.5	6.6	6.2	4.8	4.63		(53)	4.63	4.8	6.1	6.7	7.3	6.8	6.0	5.5	4.0
38.5	31.0	24.5	19.1	14.5	10.0	4.54	10.0	14.5	17.0	22.0	27.5	29.5	31.5	34.5	36.0	

Nail in T.P. 1004 20420

3.7	3.5	5.3	4.1	4.5	3.6	3.49	(48)	3.52	3.7	5.3	7.8	9.0			
38.0	27.4	22.4	21.7	18.0	14.6	7.0	3.44	7.0	14.9	18.1	22.7	33.0			

11.5	11.4	6.8	6.2	4.6	4.48		(50)	4.51	4.6	5.9	10.0	9.8			
33.0	27.3	19.3	17.0	14.3	10.0	4.43	7.0	10.3	18.6	25.1	33.0				

7.7	7.4	9.4	7.1	5.5	5.46		(60)	5.47	5.5	6.0	6.7	10.5	10.8		
32.0	29.0	32.6	17.3	14.0	10.0	5.4	7.0	10.0	13.9	15.7	19.2	24.5	33.0		

Station	+	H.I	-	Rod	Elev.
		295.65	✓		
39+24					
40+00					
41+00					
T.P.	3.57	291.55	✓	7.67	297.95 ✓
42+00					
43+00					
T.P.	7.45	296.17	✓	2.93	288.70 ✓
44+00					
+78					
45+00					
B.M.	10.04	304.45	✓	1.76	291.41 ✓ (294.45)
46+00					
47+00					
+25					
+62					

left

E

Right

1.0	1.2	1.4	5.9	5.47	6.2	5.72	5.3	6.5	7.9	10.1	10.8
33.0	21.2	15.2	14.0	12.0	5.67	7.0	12.4	7.6	20.6	24.4	32.0

70

12.4	12.2	9.6	7.8	6.6	6.41	6.41	6.5	7.0	9.2	10.3	11.9	
33.0	25.9	20.8	16.5	14.3	11.0	6.35	10.0	14.4	16.8	20.0	24.1	33.0

80

17.2	14.6	13.1	9.8	8.2	7.5	7.43	7.44	7.5	9.4	9.7	13.1	16.1	16.4	
33.0	20.5	24.8	19.8	16.5	14.8	12.0	7.56	10.0	14.2	17.2	20.2	23.8	27.7	33.0

43

12.1	11.6	6.2	4.8	3.7	3.6	3.63	3.7	4.8	5.7	12.0	13.1	13.7	
33.0	24.3	17.7	16.3	14.2	12.0	8.53	10.0	11.2	16.5	19.2	20.8	20.3	20.3

35

15.3	13.0	10.2	4.8	3.7	2.9	2.85	2.85	2.9	4.1	9.0	13.1	13.4	
1.0	30.6	26.8	19.6	16.7	14.3	12.0	2.78	10.0	14.3	17.0	22.0	20.2	33.0

60

12.7	12.8	7.7	6.6	5.4	5.25	5.25	5.25	5.4	6.8	7.9	10.6	12.0
33.0	28.8	22.6	16.8	14.2	12.0	5.23	7.0	14.3	16.6	20.5	24.3	32.0

38

6.0	6.0	5.6	4.4	3.3	3.19	3.19	3.8	3.4	4.8	5.3	5.8	5.4
33.0	25.1	19.6	15.8	12.0	12.0	5.12	10.0	14.4	22.2	23.0	27.8	33.0

32

4.7	4.5	3.9	3.0	2.6	2.6	2.6	2.6	2.7	3.3	4.1	4.1
33.0	25.6	23.1	14.1	12.0	2.59	7.0	7.0	14.2	18.1	22.0	33.0

87

11.6	11.5	11.4	10.8	8.3	8.15	8.1	8.21	8.3	9.9	10.5	11.1	10.5	7.0
33.0	28.8	25.0	18.7	14.3	12.0	8.1	10.0	14.6	7.5	21.6	22.4	31.0	34.0

65

9.7	7.7	8.7	9.4	8.7	6.3	6.07	6.07	6.1	7.8	8.6	8.7	9.1	6.3	6.3	
33.0	27.7	26.2	24.3	19.7	4.3	10.0	6.01	10.0	7.0	17.7	20.7	26.0	27.8	32.2	33.0

61

7.8	7.2	9.0	8.5	7.4	5.9	5.71	5.69	5.7	8.2	8.4	7.0	5.3	5.2	
33.0	20.5	20.2	22.8	17.8	14.1	12.0	5.65	7.0	7.0	20.0	23.2	25.1	30.4	33.0

57

2.5	2.4	4.5	7.7	7.3	5.4	5.22	5.22	5.2	7.6	7.7	8.8	1.7	
33.0	39.6	25.7	22.8	18.1	14.6	12.0	5.17	7.0	14.9	20.1	23.1	29.8	33.0

Station	+	H.I.	-	Rod	Elev.	
		304.45	✓			
48+00						
+15						
49+00	} Short. station "91.4"					
T.P.		6.70	306.02	✓	5.13	299.32
49+18.3 =						
49+26.9						
50+00						
51+00						
+75						
T.P.	2.63	297.68	✓	10.97	295.05	
52+00						
53+00						
+20						
+66 <sup>3</sup>						
T.P.	2.54	291.81	✓	8.41	289.27	
54+00						
55+00						

H.

E

30  
99.2  
6.8

H

32

$\frac{6.1}{32.0}$	$\frac{3.5}{29.1}$	$\frac{6.7}{24.5}$	$\frac{7.4}{21.4}$	$\frac{7.0}{17.8}$	$\frac{5.0}{14.5}$	$\frac{4.9}{10.0}$	4.82	$\frac{4.88}{10.0}$	$\frac{4.9}{14.3}$	$\frac{6.5}{17.1}$	$\frac{7.5}{24.0}$	$\frac{5.0}{27.6}$	$\frac{1.0}{32.0}$	(54)			
$\frac{1.1}{33.0}$	$\frac{0.9}{30.5}$	$\frac{2.9}{27.0}$	$\frac{7.0}{21.5}$	$\frac{6.9}{18.2}$	$\frac{4.9}{14.5}$	$\frac{4.8}{10.0}$	4.71	$\frac{4.78}{13.0}$	$\frac{4.9}{14.5}$	$\frac{6.0}{18.0}$	$\frac{7.2}{23.7}$	$\frac{5.0}{27.5}$	$\frac{0.9}{29.1}$	(53)			
$\frac{3.0}{33.0}$	$\frac{0.0}{32.5}$	$\frac{5.2}{23.9}$	$\frac{7.0}{27.9}$	$\frac{6.6}{17.9}$	$\frac{4.9}{14.2}$	$\frac{4.0}{10.0}$	4.59	$\frac{4.58}{10.0}$	$\frac{4.7}{14.3}$	$\frac{6.7}{18.7}$	$\frac{7.0}{24.2}$	$\frac{4.8}{29.1}$	$\frac{3.6}{32.0}$	(52)			
$\frac{1.4}{30}$	$\frac{1.4}{32.3}$	$\frac{3.4}{31.0}$	$\frac{5.9}{24.7}$	$\frac{9.0}{22.0}$	$\frac{8.9}{19.5}$	$\frac{7.0}{14.9}$	$\frac{6.86}{10.0}$	6.76	$\frac{6.82}{10.0}$	$\frac{6.9}{15.6}$	$\frac{8.1}{17.8}$	$\frac{8.8}{21.6}$	$\frac{8.9}{26.8}$	$\frac{9.0}{29.0}$	$\frac{5.5}{32.0}$	$\frac{0.7}{37.0}$	(75)
$\frac{6.7}{31.6}$	$\frac{8.5}{25.2}$	$\frac{9.2}{24.5}$	$\frac{10.8}{22.6}$	$\frac{10.0}{17.6}$	$\frac{8.5}{14.9}$	$\frac{8.85}{10.0}$	8.32	$\frac{8.42}{10.0}$	$\frac{8.6}{15.2}$	$\frac{9.8}{18.4}$	$\frac{10.8}{27.4}$	$\frac{9.7}{29.2}$	$\frac{9.0}{31.6}$	$\frac{6.1}{34.0}$	(91)		
$\frac{9.1}{31.7}$	$\frac{10.1}{28.6}$	$\frac{11.3}{24.9}$	$\frac{12.9}{22.6}$	$\frac{12.7}{18.0}$	$\frac{10.5}{14.5}$	$\frac{10.99}{10.0}$	10.19	$\frac{10.23}{10.0}$	$\frac{10.4}{14.9}$	$\frac{11.7}{18.0}$	$\frac{13.0}{23.8}$	$\frac{13.1}{27.5}$	$\frac{11.3}{32.2}$	$\frac{9.0}{34.6}$	(109)		
$\frac{1.0}{33.0}$	$\frac{1.6}{27.8}$	$\frac{2.8}{25.3}$	$\frac{5.1}{22.6}$	$\frac{4.1}{17.4}$	$\frac{2.7}{14.3}$	$\frac{2.68}{10.0}$	2.59	$\frac{2.63}{10.0}$	$\frac{2.7}{15.0}$	$\frac{4.3}{18.9}$	$\frac{5.3}{25.1}$	$\frac{5.4}{24.8}$	$\frac{4.2}{27.7}$	$\frac{3.5}{32.4}$	$\frac{2.5}{32.5}$	(33)	
$\frac{7.7}{33.0}$	$\frac{7.4}{28.6}$	$\frac{9.0}{22.4}$	$\frac{7.5}{18.8}$	$\frac{5.9}{15.6}$	$\frac{5.66}{10.0}$	5.6	$\frac{5.66}{10.0}$	$\frac{5.8}{15.4}$	$\frac{6.8}{18.5}$	$\frac{7.6}{22.1}$	$\frac{7.4}{22.1}$	$\frac{7.2}{32.0}$	(63)				
$\frac{8.6}{33.0}$	$\frac{9.6}{23.4}$	$\frac{9.0}{22.7}$	$\frac{9.5}{18.2}$	$\frac{7.0}{15.5}$	$\frac{6.84}{10.0}$	6.75	$\frac{6.82}{10.0}$	$\frac{6.7}{15.0}$	$\frac{8.2}{20.0}$	$\frac{7.2}{24.8}$	$\frac{7.2}{24.8}$	$\frac{7.2}{55.0}$	(75)				
$\frac{9.0}{33.0}$	$\frac{8.7}{26.7}$	$\frac{7.9}{15.2}$	$\frac{7.9}{19.0}$	$\frac{7.78}{7.6}$	$\frac{7.35}{10.0}$	7.4	$\frac{7.4}{14.5}$	$\frac{8.1}{18.2}$	$\frac{11.3}{26.4}$	$\frac{12.0}{38.0}$	(19)						
$\frac{3.4}{33.0}$	$\frac{5.4}{27.5}$	$\frac{3.9}{20.3}$	$\frac{2.6}{14.8}$	$\frac{2.58}{10.0}$	2.5	$\frac{2.54}{10.0}$	$\frac{2.6}{18.6}$	$\frac{3.4}{18.5}$	$\frac{8.4}{25.6}$	$\frac{8.7}{33.0}$	(32)						
$\frac{11.4}{33.0}$	$\frac{11.0}{24.7}$	$\frac{11.3}{17.6}$	$\frac{5.78}{14.4}$	$\frac{5.62}{10.0}$	5.6	$\frac{5.71}{10.0}$	$\frac{5.7}{14.5}$	$\frac{7.6}{19.8}$	$\frac{12.1}{26.1}$	$\frac{12.4}{33.0}$	(63)						

Station	+	H.I.	-	Rod.	Elev
		291.91 ✓			
T.P.	2.69	285.52 ✓	8.99 ✓	282.82 ✓	
56+00					
57+00					
B.M.				6.91	278.60 ✓
58+00					
T.P.	1.57	274.50 ✓	12.58	272.94 ✓	
59+00					
60+00					
61+00					
62+00					
B.M.	5.91	267.25 ✓	13.07	261.40 ✓	
63+00					
64+00					
65+00					
66+00					
67+00					

H.

L

H.

$\frac{7.1}{33.0}$	$\frac{6.9}{22.0}$	$\frac{8.9}{16.8}$	$\frac{2.9}{14.4}$	$\frac{2.52}{10.0}$	$\frac{2.60}{2.60}$	$\frac{20.9}{10.0}$	$\frac{2.8}{14.8}$	$\frac{3.8}{15.9}$	$\frac{4.5}{20.2}$	$\frac{5.6}{25.5}$	$\frac{6.9}{27.1}$	$\frac{7.6}{33.0}$
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33

$\frac{7.7}{33.0}$	$\frac{8.4}{27.2}$	$\frac{8.0}{23.0}$	$\frac{7.2}{18.1}$	$\frac{6.1}{14.4}$	$\frac{5.96}{10.0}$	$\frac{5.94}{5.94}$	$\frac{6.89}{10.0}$	$\frac{6.2}{14.2}$	$\frac{7.7}{15.6}$	$\frac{8.5}{22.5}$	$\frac{7.5}{24.4}$	$\frac{7.5}{33.0}$
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6.6

$\frac{9.1}{33.0}$	$\frac{10.6}{30.9}$	$\frac{12.0}{24.2}$	$\frac{11.8}{19.9}$	$\frac{11.0}{17.2}$	$\frac{9.5}{14.2}$	$\frac{9.34}{10.0}$	$\frac{9.2}{9.2}$	$\frac{9.5}{10.0}$	$\frac{10.4}{14.5}$	$\frac{11.0}{16.2}$	$\frac{11.0}{21.8}$	$\frac{10.0}{23.6}$	$\frac{10.0}{25.1}$	$\frac{10.0}{33.0}$
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9.9

$\frac{0.2}{33.0}$	$\frac{0.2}{30.8}$	$\frac{2.0}{30.6}$	$\frac{2.6}{27.2}$	$\frac{4.2}{27.0}$	$\frac{3.8}{18.7}$	$\frac{1.6}{14.3}$	$\frac{1.57}{10.0}$	$\frac{1.45}{1.45}$	$\frac{1.5}{13.7}$	$\frac{3.2}{17.0}$	$\frac{3.3}{25.2}$	$\frac{2.4}{31.0}$	$\frac{0.5}{33.7}$
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2.7

$\frac{7.2}{33.0}$	$\frac{6.8}{30.1}$	$\frac{7.3}{28.1}$	$\frac{7.3}{22.9}$	$\frac{5.9}{18.4}$	$\frac{4.9}{14.5}$	$\frac{4.84}{10.0}$	$\frac{4.76}{4.76}$	$\frac{4.91}{10.0}$	$\frac{5.0}{14.6}$	$\frac{5.6}{16.6}$	$\frac{6.4}{18.4}$	$\frac{7.0}{27.8}$	$\frac{6.5}{33.0}$
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5.5

$\frac{10.8}{33.0}$	$\frac{10.5}{26.6}$	$\frac{9.1}{17.9}$	$\frac{7.7}{14.4}$	$\frac{7.56}{11.0}$	$\frac{7.46}{7.46}$	$\frac{7.57}{10.0}$	$\frac{7.7}{14.5}$	$\frac{8.3}{18.7}$	$\frac{9.6}{22.3}$	$\frac{9.9}{33.0}$
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8.2

$\frac{12.2}{33.0}$	$\frac{11.4}{22.2}$	$\frac{10.5}{18.5}$	$\frac{9.3}{14.4}$	$\frac{9.2}{10.0}$	$\frac{9.14}{9.14}$	$\frac{9.23}{10.0}$	$\frac{9.4}{14.4}$	$\frac{10.9}{19.5}$	$\frac{11.3}{26.6}$	$\frac{11.3}{33.0}$
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9.8

$\frac{5.2}{33.0}$	$\frac{6.9}{30.0}$	$\frac{5.7}{22.8}$	$\frac{4.7}{18.4}$	$\frac{2.9}{11.6}$	$\frac{2.94}{10.0}$	$\frac{2.87}{2.87}$	$\frac{3.0}{10.0}$	$\frac{3.0}{14.6}$	$\frac{4.5}{18.0}$	$\frac{5.1}{22.5}$	$\frac{5.5}{33.0}$
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3.5

$\frac{6.4}{33.0}$	$\frac{5.9}{31.8}$	$\frac{6.9}{27.4}$	$\frac{6.2}{19.5}$	$\frac{3.9}{14.2}$	$\frac{3.91}{10.0}$	$\frac{3.84}{3.84}$	$\frac{3.94}{10.0}$	$\frac{3.8}{14.8}$	$\frac{6.6}{22.0}$	$\frac{7.4}{33.0}$
--------------------	--------------------	--------------------	--------------------	--------------------	---------------------	---------------------	---------------------	--------------------	--------------------	--------------------

4.5

$\frac{8.5}{33.0}$	$\frac{7.9}{22.7}$	$\frac{6.3}{16.9}$	$\frac{4.8}{15.0}$	$\frac{4.65}{10.0}$	$\frac{4.6}{4.6}$	$\frac{4.68}{10.0}$	$\frac{4.7}{14.5}$	$\frac{5.5}{16.7}$	$\frac{7.9}{22.5}$	$\frac{9.3}{33.0}$
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5.5

$\frac{10.4}{33.0}$	$\frac{9.6}{24.2}$	$\frac{6.6}{19.7}$	$\frac{6.1}{16.8}$	$\frac{5.0}{14.6}$	$\frac{4.91}{10.0}$	$\frac{4.8}{4.8}$	$\frac{4.96}{10.0}$	$\frac{4.8}{14.4}$	$\frac{6.1}{17.0}$	$\frac{8.4}{21.9}$	$\frac{8.3}{33.0}$
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5.5

$\frac{11.3}{33.0}$	$\frac{10.6}{24.9}$	$\frac{7.1}{19.0}$	$\frac{5.0}{14.9}$	$\frac{4.86}{10.0}$	$\frac{4.8}{4.8}$	$\frac{4.88}{10.0}$	$\frac{4.8}{14.5}$	$\frac{6.2}{17.5}$	$\frac{7.9}{21.5}$	$\frac{7.9}{33.0}$
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5.5

Station	+	H.I	-	Rod	Elev
		267.25 <sup>5</sup> ✓			
68+00					
T.P.	5.67	270.20 <sup>6</sup> ✓	2.65	264.60 <sup>59</sup> ✓	
69+00					
70+00					
+25					
71+00					
B.M.				4.25	266.00 <sup>1</sup>
72+00					
T.P.	9.97	280.16 <sup>5</sup> ✓	0.08	270.18 <sup>8</sup> ✓	
73+00					
74+00					
+67					
75+00					
+40					
T.P.	9.81	289.74 <sup>3</sup> ✓	0.23	279.93 <sup>8</sup> ✓	
76+00					

H.

E

H.

(53)

7.7	7.7	8.0	8.7	6.7	4.7	4.81	4.76	4.8	6.4	7.0	6.5	6.3	
33.0	27.6	26.0	22.0	18.7	14.4	10.0	4.7	10.0	14.7	17.5	21.3	26.3	33.0

Ind. Vol. 100.1 74.4 65.2 50.0

(77)

9.5	8.8	11.0	14.6	7.1	7.0	6.87	7.0	10.0	11.3	11.7	11.7
33.0	25.9	24.6	23.5	14.3	12.0	6.93	12.0	14.8	19.9	23.2	33.0

(65)

6.2	7.7	8.7	7.9	5.8	5.83	5.8	5.8	7.4	9.6	10.4	10.4
33.0	25.2	23.4	18.6	14.2	10.0	5.75	10.0	15.0	17.6	22.0	33.0

(61)

6.3	5.1	6.1	7.7	7.1	5.0	5.07	5.0	5.0	6.2	6.7	6.7
33.0	27.2	24.7	23.0	18.0	14.8	10.0	5.39	10.0	14.8	25.6	33.0

(49)

5.2	5.1	6.0	5.8	4.0	4.37	4.3	4.3	5.0	6.8	7.0	5.2	4.6	3.1	
33.0	24.0	21.7	17.9	14.7	10.0	4.1	10.0	14.9	18.0	22.8	27.9	29.2	31.0	33.0

M. Vol. in T.P. 100.1 71.4 80.0

(78)

5.1	4.9	5.8	4.9	2.4	2.8	2.8	2.8	2.4	4.1	4.8	5.2	3.1	2.2
33.0	24.2	23.0	18.7	14.6	10.0	2.23	10.0	14.6	17.0	21.4	26.7	30.0	33.0

(100)

12.4	11.8	12.5	12.1	9.6	9.45	9.4	9.5	10.4	11.4	11.5	7.4	7.3	
33.0	25.0	23.0	19.0	14.6	10.0	9.37	10.0	14.5	17.6	20.4	25.1	29.5	33.0

(70)

8.0	8.1	8.9	9.5	6.4	6.40	6.4	6.4	7.4	8.4	7.6	5.7	5.6	
33.0	25.3	23.1	19.7	14.5	10.0	6.36	10.0	15.0	19.0	26.5	27.7	31.5	33.0

(48)

6.1	5.9	6.4	6.4	4.4	4.3	4.3	4.4	5.5	6.3	4.7	1.3	1.3	
33.0	24.6	23.9	19.5	15.0	10.0	4.2	10.0	14.7	17.6	25.0	28.2	30.0	33.0

(37)

4.0	4.4	5.4	5.2	3.2	3.2	3.2	3.2	3.4	4.6	5.0	4.4	4.1
33.0	24.4	23.0	20.5	15.0	10.0	3.15	10.0	14.7	17.7	22.0	29.5	33.0

(24)

7.9	7.4	6.0	3.8	2.9	1.88	1.94	2.0	5.5	5.7	5.7
33.0	27.2	25.0	15.0	14.5	10.0	1.84	10.0	14.4	17.0	33.0

(10.0)

12.7	12.5	11.9	9.6	9.52	9.5	9.3	11.8	12.3	13.0	13.0
33.0	24.6	19.5	14.3	15.0	9.43	10.0	15.0	21.5	27.5	33.0

Station	+	H.I	-	Rod	Elev.
		289.74			
76+75					
77+00					
78+00					
T.P.	11.83	301.57	0.14	289.60	
79+00					
80+00					
B.M.				4.31	297.07
81+00					297.07
82+00					
T.P.	6.33	304.97	2.77	298.60	
83+00					
+50					
+70					
T.P.	7.38	304.00	8.36	296.60	
84+00					
+25					

H.

L

R.

(69)

12.4	9.9	14.4	7.7	7.2	7.1	7.0	7.2	8.5	9.3	8.5	9.0	
33.0	29.5	37.0	19.3	14.2	10.0	6.76	15.0	15.0	18.3	26.3	28.1	33.0

(67)

7.5	7.7	7.7	7.5	6.3	6.24	6.17	6.7	7.4	8.8	7.3	6.4	6.4	
33.0	30.5	26.5	19.0	14.8	10.0	6.17	10.0	14.1	16.7	25.5	30.0	31.5	33.0

(34)

5.1	5.0	4.3	2.8	2.6	2.6	2.67	2.9	2.4	4.8	4.0	3.6	2.0
33.0	36.4	19.0	14.3	10.0	2.0	10.0	14.5	19.9	25.7	26.8	30.6	32.5

(11.8)

11.7	11.6	12.3	12.8	11.2	11.18	11.12	11.18	11.3	11.5	11.2
33.0	28.8	24.3	18.5	14.3	10.0	11.12	10.0	14.5	21.3	32.0

(86)

7.9	8.5	10.3	10.0	8.0	8.00	8.03	8.7	9.0	9.7	6.7	6.8	
33.0	32.5	35.5	19.9	14.7	10.0	7.98	10.0	14.3	17.0	20.6	23.5	33.0

61/10 T.P. R.H. 84-65

(61)

5.7	7.0	7.7	7.1	5.7	5.35	5.08	5.6	7.0	7.7	4.2	4.2	
33.0	28.3	23.6	19.0	14.2	10.0	5.46	10.0	14.2	14.8	19.5	24.0	33.0

(44)

2.3	4.8	6.1	5.1	3.8	3.93	3.81	3.8	4.7	4.9	1.8	6.7	
33.0	27.5	22.9	16.7	14.3	10.0	3.74	10.0	14.1	16.8	19.0	25.3	33.0

(69)

2.4	5.0	8.4	8.4	6.4	6.24	6.33	6.3	8.0	7.9	4.4	3.5	
33.0	29.0	23.0	18.5	14.6	10.0	6.24	10.0	14.3	17.3	19.1	24.3	33.0

(68)

1.8	2.8	5.3	5.7	8.1	6.4	6.24	6.25	6.3	7.5	7.5	3.8	8.0
33.0	30.1	26.0	20.3	18.5	14.8	6.19	10.0	14.3	16.3	18.9	25.0	33.0

(68)

5.3	5.4	5.0	5.0	6.7	6.24	6.24	6.3	7.3	7.3	3.7	3.3	
33.0	30.7	23.0	18.5	15.0	10.0	6.19	10.0	14.3	16.5	18.1	25.4	33.0

(59)

2.6	3.1	6.7	6.7	5.3	5.33	5.34	5.4	6.4	6.4	2.5	2.2	
33.0	25.7	22.0	18.4	14.7	10.0	5.07	10.0	14.3	17.1	20.6	27.0	33.0

(59)

2.5	3.0	7.0	6.8	5.0	5.04	5.87	5.3	6.7	6.7	2.7	2.2	
33.0	25.3	21.0	18.1	14.5	10.0	5.33	10.0	14.4	17.1	20.4	26.2	33.0

Station	+	HI	-	Red.	Black.
		304.00	✓		
84+25		0			
+85					
85+00					
86+00					
+85					
87+00					
T.P.	1.82	294.39	✓	11.44	292.59
88+00		8		6	
89+00					
90+00					
T.P.	1.00	283.28	✓	12.11	282.28
91+00		7		7	
B.M.				239	280.8
92+00					
T.P.	2.50	275.30	✓	10.24	272.80
93+00		3		3	

H.

L

A.

(6.0)

5.3	5.7	6.8	6.9	5.5	5.49	5.37	5.4	6.7	6.7	2.5	2.1	
33.0	23.4	21.1	18.9	15.5	10.0	5.36	10.2	14.7	10.9	19.5	25.8	33.0

(6.3)

5.9	5.7	7.3	7.1	5.7	5.76	5.73	5.8	6.8	6.8	2.7	2.5	
33.0	22.0	32.0	19.0	15.2	10.0	5.67	10.0	14.1	16.4	19.8	25.8	33.0

(6.5)

3.7	3.5	7.3	7.4	5.9	5.91	5.89	6.0	6.9	6.9	2.9	2.7	
33.0	25.0	22.0	18.0	14.9	10.0	5.93	10.0	14.7	16.9	19.5	25.4	33.0

(8.0)

6.1	5.9	8.9	8.9	7.5	7.39	7.37	7.3	8.8	8.9	6.4	5.6	
33.0	25.0	19.9	17.6	16.8	10.0	7.32	10.0	15.2	18.0	19.9	25.1	33.0

(8.8)

7.7	7.8	10.0	9.7	8.4	8.21	8.15	8.2	9.8	9.9	7.5	7.7	7.0	7.0	
33.0	28.6	22.4	17.5	14.5	10.0	8.12	10.0	14.9	18.3	20.4	24.3	27.3	28.5	33.0

(10.2)

9.3	9.5	11.2	11.2	9.6	9.53	9.56	9.2	10.0	11.9	9.9	8.4	
33.0	23.0	18.9	17.3	14.8	10.0	9.49	10.0	15.5	16.2	20.0	23.4	33.0

(3.6)

4.1	4.2	4.5	4.3	3.0	2.96	2.98	3.0	4.0	4.0	3.5	3.6	3.8	
33.0	27.0	20.9	18.5	14.1	10.0	2.9	10.0	14.4	17.0	18.8	21.0	26.0	33.0

(7.3)

8.2	8.8	8.2	6.7	6.65	6.69	6.6	7.8	7.7	7.5	7.8	
33.0	28.0	21.0	18.1	10.0	6.62	10.0	15.8	18.7	21.8	24.0	33.0

(11.1)

13.1	13.3	12.1	10.5	10.43	10.46	10.3	11.9	12.4	11.7	12.0	
33.0	27.0	19.0	14.8	10.0	10.38	10.0	15.4	21.1	24.5	28.4	33.0

(3.8)

6.6	6.3	5.5	3.3	2.21	3.1	3.1	3.2	5.0	5.3	6.2	5.5	5.9
33.0	27.0	19.7	14.5	10.0	3.1	10.0	14.4	17.6	22.9	27.4	27.0	33.0

(7.4)

10.9	11.3	10.8	10.4	7.1	6.97	6.97	7.1	9.2	9.9	10.1	
33.0	30.0	25.9	21.6	14.1	12.0	6.90	10.0	14.7	19.0	24.7	33.0

(3.0)

6.1	6.5	6.4	5.6	2.8	2.5	2.5	2.6	4.9	5.5	6.2	
33.0	30.3	26.8	21.0	14.8	10.0	2.42	10.0	14.8	17.6	25.0	33.0

275.34 ✓  
3

94+00

95+00

No. St. Paul City Limits

267.96

T.P.

4.73

272.58 ✓

7.49

267.05 ✓

96+00

7

266.98

97+00

98+00

99+00

100+00

B.M.

5.33

277.2

267.22

101+00

102+00

T.P.

6.33

274.82 ✓

4.04

268.54 ✓

103+00

6

3

+15 ✓

104+00

H.

E

H.

(57)

7.8	8.3	7.5	6.7	5.5	5.23	5.13	5.1	6.5	7.9	8.4
33.0	31.5	26.0	17.3	14.9	10.0	10.0	14.2	16.9	23.0	33.0

(8.0)

9.5	8.2	9.0	5.0	7.07	7.77	7.4	6.9
33.0	28.2	22.0	13.0	14.8	7.37	10.0	32.9

Sp. H. H. N.E. con Penn. Ave. + 7th. Ave

(63)

6.6	6.45	5.85	5.55	5.96	5.97	5.5	6.8
38.0	32.0	12.0	5.0	12.0	32.0	32.0	35.6

(6.0)

7.3	6.7	6.12	6.53	5.59	5.09	5.68	5.21	5.2	6.6
38.0	35.8	32.0	32.0	12.0	12.0	32.0	32.0	35.8	38.0

(57)

6.3	5.9	5.70	6.25	5.31	5.06	5.53	5.06	5.5	6.6
37.0	36.0	32.0	32.0	12.0	12.0	37.0	32.0	36.8	38.0

(54)

6.5	5.8	5.49	5.97	5.10	4.99	5.36	4.87	5.2	6.3
37.8	36.0	32.0	32.0	12.0	12.0	32.0	32.0	36.0	37.0

(51)

5.5	5.4	5.23	5.79	4.8	4.66	5.16	4.73	4.7	5.2
37.5	36.0	32.0	32.0	12.0	12.0	32.0	32.0	36.0	38.0

(48)

5.0	4.7	4.87	5.36	4.53	4.5	5.00	4.03	4.5	5.1
38.0	36.0	32.0	32.0	12.0	12.0	32.0	32.0	37.0	38.5

(4.5)

4.3	4.3	4.62	5.1	4.35	4.28	5.02	4.54	4.3	4.5
38.0	36.0	32.0	32.0	12.0	12.0	32.0	32.0	36.5	38.0

(6.0)

6.8	6.5	6.61	7.06	6.1	6.44	7.14	6.69	6.6	6.6
38.0	36.0	32.0	32.0	12.0	12.0	32.0	32.0	37.0	38.0

(58)

6.4	6.5	6.58	7.05	6.35	6.42	7.04	6.65	6.6	6.5
38.0	36.0	32.0	32.0	12.0	12.0	32.0	32.0	37.0	37.0

6.6	6.35	6.87	5.9	5.88	6.02	6.58	6.36	6.6	7.0
42.0	37.0	37.0	12.0	5.88	12.0	32.0	32.0	36.8	38.5

272.8⑦ ✓  
6

105+00

106+00

107+00

T.P. 794

281.5② ✓  
1

1.19

273.6③ ✓  
7

+51 ✓

+87 ✓

108+00

109+00

+87 ✓

110+00

+45 ✓

111+00

+78 ✓

T.P. 4.52

284.2⑤ ✓  
4

1.79

279.7⑥ ✓  
2

+78

(51)

$\frac{59}{31.0}$   $\frac{55}{36.5}$   $\frac{50.5}{32.0}$   $\frac{58.7}{32.0}$   $\frac{53.2}{12.0}$  4.9  $\frac{5.32}{12.0}$   $\frac{5.99}{32.0}$   $\frac{5.52}{32.0}$   $\frac{5.7}{36.0}$   $\frac{6.5}{38.0}$

(43)

$\frac{5.8}{38.0}$   $\frac{4.9}{36.4}$   $\frac{4.68}{32.0}$   $\frac{5.16}{32.0}$   $\frac{4.5}{12.0}$  4.2  $\frac{4.47}{12.0}$   $\frac{5.17}{32.0}$   $\frac{4.7}{32.0}$   $\frac{4.8}{36.0}$   $\frac{5.4}{37.5}$

(33)

$\frac{4.0}{37.5}$   $\frac{3.7}{36.5}$   $\frac{3.87}{32.0}$   $\frac{4.26}{32.0}$   $\frac{3.52}{12.0}$  3.0  $\frac{3.55}{12.0}$   $\frac{4.35}{32.0}$   $\frac{3.86}{32.0}$   $\frac{3.8}{37.0}$   $\frac{3.74}{40.0}$

1/16 4/16

$\frac{10.0}{37.5}$   $\frac{9.1}{36.4}$   $\frac{9.55}{32.0}$   $\frac{10.34}{32.0}$   $\frac{9.59}{12.0}$  7.3 ✓  $\frac{10.2}{12.0}$   $\frac{12.25}{32.0}$   $\frac{9.77}{32.0}$   $\frac{10.0}{46.0}$   $\frac{10.0}{44.0}$

12/16 53

$\frac{7.8}{38.0}$   $\frac{9.0}{37.0}$   $\frac{9.38}{32.0}$   $\frac{9.81}{32.0}$   $\frac{9.15}{12.0}$  8.7 ✓  $\frac{8.96}{12.0}$   $\frac{9.65}{32.0}$   $\frac{9.18}{32.0}$   $\frac{9.5}{39.0}$   $\frac{8.5}{44.0}$

(89)

$\frac{9.6}{38.0}$   $\frac{9.4}{36.0}$   $\frac{9.9}{32.0}$   $\frac{9.68}{32.0}$   $\frac{9.81}{12.0}$  5.5  $\frac{9.76}{12.0}$   $\frac{9.37}{32.0}$   $\frac{8.94}{32.0}$   $\frac{8.9}{39.0}$   $\frac{8.97}{44.0}$

(74)

$\frac{1.0}{89.0}$   $\frac{6.0}{87.0}$   $\frac{7.15}{32.0}$   $\frac{9.35}{32.0}$   $\frac{7.5}{12.0}$  7.3  $\frac{7.34}{12.0}$   $\frac{7.84}{32.0}$   $\frac{7.51}{32.0}$   $\frac{7.4}{36.0}$   $\frac{7.7}{37.5}$

$\frac{6.4}{41.0}$   $\frac{6.6}{38.0}$   $\frac{7.5}{38.0}$   $\frac{7.78}{32.0}$   $\frac{6.31}{12.0}$  5.9 ✓  $\frac{6.12}{18.7}$   $\frac{6.50}{32.0}$   $\frac{6.01}{32.0}$   $\frac{6.0}{38.0}$   $\frac{6.5}{35.5}$

(59)

$\frac{6.2}{42.0}$   $\frac{6.57}{32.0}$   $\frac{6.99}{32.0}$   $\frac{6.01}{12.0}$  5.7  $\frac{5.79}{12.0}$   $\frac{6.23}{32.0}$   $\frac{5.76}{32.0}$   $\frac{5.6}{39.0}$   $\frac{6.2}{41.0}$

$\frac{5.8}{42.0}$   $\frac{5.77}{32.0}$   $\frac{6.22}{32.0}$   $\frac{6.34}{12.0}$  5.1 ✓  $\frac{5.3}{12.0}$   $\frac{5.23}{32.0}$   $\frac{5.31}{32.0}$   $\frac{5.21}{36.5}$   $\frac{5.1}{42.7}$

(46)

$\frac{4.8}{32.0}$   $\frac{4.87}{32.0}$   $\frac{5.85}{32.0}$   $\frac{4.67}{12.0}$  4.4  $\frac{4.67}{12.0}$   $\frac{5.28}{32.0}$   $\frac{4.86}{32.0}$   $\frac{4.5}{32.0}$

$\frac{3.5}{42.0}$   $\frac{3.51}{32.0}$   $\frac{4.01}{32.0}$   $\frac{3.55}{12.0}$  3.4 ✓

✓  $\frac{6.42}{12.0}$   $\frac{7.03}{32.0}$   $\frac{7.1}{38.0}$   $\frac{6.9}{38.0}$   $\frac{6.75}{50.0}$

284.26 ✓  
4

112+00

+50 ✓

113+00

+12 ✓

114+00

115+00

116+00

T.P. 6.49 289.56 ✓ 1.18 283.7 ✓  
5 6

117+00

118+00

119+00

120+00

T.P. 7.30 296.67 ✓ 0.19 289.37 ✓  
6 6  
+45 ✓

$$\begin{array}{r} \frac{60}{420} \quad \frac{589}{320} \quad \frac{633}{320} \quad \frac{695}{120} \quad \frac{6.0}{6.0} \quad \frac{6.97}{120} \quad \frac{6.6}{320} \quad \frac{6.45}{30} \end{array}$$

(6.0)

$$\begin{array}{r} \frac{51}{500} \quad \frac{520}{440} \quad \frac{521}{440} \quad \frac{527}{320} \quad \frac{532}{120} \quad \frac{5.4}{5.4} \quad \frac{565}{180} \quad \frac{627}{320} \quad \frac{608}{320} \quad \frac{58}{420} \end{array}$$

(4.8)

$$\begin{array}{r} \frac{42}{500} \quad \frac{426}{430} \quad \frac{44}{430} \quad \frac{455}{320} \quad \frac{465}{120} \quad \frac{4.7}{4.7} \quad \frac{513}{120} \quad \frac{613}{320} \quad \frac{571}{320} \quad \frac{56}{420} \end{array}$$

$$\begin{array}{r} \frac{410}{410} \quad \frac{435}{320} \quad \frac{457}{320} \quad \frac{451}{120} \quad \frac{4.6}{4.6} \quad \frac{503}{120} \quad \frac{599}{320} \quad \frac{555}{320} \quad \frac{5.7}{379} \quad \frac{5.5}{420} \end{array}$$

(3.9)

$$\begin{array}{r} \frac{3.8}{410} \quad \frac{374}{320} \quad \frac{404}{320} \quad \frac{392}{120} \quad \frac{4.0}{4.0} \quad \frac{431}{120} \quad \frac{521}{320} \quad \frac{477}{320} \quad \frac{4.9}{420} \end{array}$$

(3.0)

$$\begin{array}{r} \frac{2.9}{410} \quad \frac{301}{320} \quad \frac{303}{320} \quad \frac{302}{120} \quad \frac{3.1}{3.1} \quad \frac{3.1}{120} \quad \frac{4.22}{320} \quad \frac{3.72}{320} \quad \frac{3.88}{370} \quad \frac{3.6}{420} \end{array}$$

(1.9)

$$\begin{array}{r} \frac{1.9}{410} \quad \frac{1.99}{320} \quad \frac{2.45}{320} \quad \frac{1.99}{120} \quad \frac{1.9}{1.9} \quad \frac{2.12}{120} \quad \frac{2.86}{320} \quad \frac{2.52}{320} \quad \frac{2.2}{370} \quad \frac{2.2}{420} \end{array}$$

(6.0)

$$\begin{array}{r} \frac{6.0}{410} \quad \frac{6.72}{320} \quad \frac{6.01}{120} \quad \frac{6.0}{6.0} \quad \frac{6.6}{120} \quad \frac{6.31}{320} \quad \frac{6.11}{420} \end{array}$$

(4.8)

$$\begin{array}{r} \frac{5.2}{410} \quad \frac{525}{320} \quad \frac{5.7}{320} \quad \frac{4.94}{120} \quad \frac{4.8}{4.8} \quad \frac{4.91}{120} \quad \frac{5.45}{320} \quad \frac{4.99}{320} \quad \frac{4.8}{360} \quad \frac{4.9}{420} \end{array}$$

(3.3)

$$\begin{array}{r} \frac{3.6}{420} \quad \frac{3.6}{380} \quad \frac{4.2}{320} \quad \frac{4.65}{320} \quad \frac{3.77}{120} \quad \frac{3.11}{3.11} \quad \frac{3.54}{120} \quad \frac{4.03}{320} \quad \frac{3.66}{320} \quad \frac{3.5}{380} \quad \frac{3.2}{420} \end{array}$$

(1.4)

$$\begin{array}{r} \frac{1.4}{420} \quad \frac{1.87}{320} \quad \frac{2.34}{320} \quad \frac{1.6}{120} \quad \frac{1.8}{1.8} \quad \frac{1.7}{120} \quad \frac{2.08}{320} \quad \frac{1.65}{320} \quad \frac{1.1}{420} \end{array}$$

$$\begin{array}{r} \frac{8.1}{420} \quad \frac{7.97}{320} \quad \frac{8.34}{320} \quad \frac{7.66}{120} \quad \frac{7.6}{7.6} \quad \frac{7.9}{120} \quad \frac{8.1}{320} \quad \frac{7.87}{320} \quad \frac{7.4}{420} \end{array}$$

296.07 ✓  
6

121+00

+50

122+00

B.M.

(291.08)  
291.11

123+00

124+00

+38

125+00

T.P.

2.19

297.70 ✓  
69

116

295.50 ✓  
0

+62

126+00

127+00

128+00

+50

T.P.

7.60

298.47 ✓  
6

6.73

290.97 ✓  
6

51

4

R1

6.7 6.57 6.77 6.47 6.4 6.47 6.48 5.7  
 41.0 32.0 32.0 32.0 6.4 32.0 32.0 50.0

64

6.86 6.02 5.5 5.46 5.6 6.8 7.1 6.0 5.5  
 50.3 32.0 10.0 5.46 12.0 15.0 17.1 22.3 22.5 33.3

6.0

6.2 6.0 6.4 6.0 5.1 4.98 4.99 5.1 6.7 6.8 5.8 5.3  
 33.0 22.0 21.0 17.0 15.0 12.0 4.9 10.0 15.0 17.0 23.7 26.8 33.0

5.6

Nail in T.R. - L. - 122730

5.3 5.2 5.6 5.8 4.4 4.2 4.8 4.5 5.4 5.9 5.1 5.3  
 33.0 32.0 22.0 16.4 14.4 10.0 4.12 10.0 15.1 17.8 23.0 25.4 33.0

4.8

4.8 4.1 4.6 4.8 3.5 3.4 3.45 3.4 4.8 5.0 4.1 4.2  
 33.0 21.8 24.8 16.2 15.0 10.0 3.34 10.0 15.1 17.2 24.1 26.6 33.0

4.0

4.0 4.0 4.4 3.9 3.2 3.15 3.19 3.3 4.6 5.0 3.7 3.9  
 33.0 22.0 21.0 17.0 15.1 10.0 3.1 10.0 15.5 18.0 23.9 26.0 33.0

3.8

3.7 3.8 4.3 3.9 3.2 2.99 3.01 3.1 4.7 4.4 3.3 3.3  
 33.0 21.6 20.9 16.3 15.0 12.0 2.91 10.0 15.0 17.3 24.9 27.3 33.0

3.6

Top Hyd Lt 510 125135

5.1 5.5 5.1 5.5 5.1 4.3 4.12 4.3 5.2 5.8 4.9 4.9  
 33.0 29.4 21.6 24.8 16.2 11.4 7.0 4.05 10.0 14.7 16.9 24.3 25.0 33.0

4.7

5.7 5.7 5.5 5.3 4.4 4.31 4.31 4.5 5.4 5.9 5.2 5.3  
 33.0 31.8 28.9 18.6 14.7 12.0 4.22 10.0 15.2 18.0 23.5 24.4 33.0

4.0

7.3 7.4 8.5 7.6 5.0 5.02 5.0 5.2 7.0 7.3 6.8 6.6  
 33.0 29.0 26.3 18.2 14.9 10.0 4.73 10.0 14.9 18.6 23.6 24.2 33.0

5.6

8.5 7.9 7.5 6.0 5.78 5.64 5.71 5.3 8.1 8.6 8.1 8.4 8.0  
 33.0 24.2 17.3 14.2 10.0 5.64 10.0 14.9 18.6 23.3 24.3 31.4 33.0

6.3

9.5 8.5 6.2 6.0 5.99 5.99 6.6 8.2 7.0 8.4  
 33.0 24.1 14.4 10.0 5.91 10.0 15.1 19.0 25.7 33.0

6.5

Top Hyd. Lt 510 129125

to here Austin.

298.40 ✓  
6

129

150

130

131

132

133

+25

134

T.R

11.03

309.06 ✓  
5

0.44

298.03 ✓  
2

+63

135+13

B.S.T.

+63

136+13

H. Carlson  
 C. Crane  
 S. Nelson  
 S. Ahlberg

Dec. 10, 23

K

R

41

(74)

$\frac{12.5}{33}$	$\frac{16.4}{23.1}$	$\frac{6.9}{4}$	$\frac{6.80}{10}$	$\frac{1.70}{-}$	$\frac{6.30}{10}$	$\frac{2.1}{17}$	$\frac{8.6}{29}$	$\frac{3.9}{35}$
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(73)

$\frac{8.6}{33}$	$\frac{6.1}{14}$	$\frac{6.71}{10}$	$\frac{6.38}{-}$	$\frac{6.71}{10}$	$\frac{6.9}{14}$	$\frac{10.5}{21}$	$\frac{10.7}{22.6}$	$\frac{8.8}{24}$	$\frac{10.4}{33}$
------------------	------------------	-------------------	------------------	-------------------	------------------	-------------------	---------------------	------------------	-------------------

(72)

$\frac{10.3}{33}$	$\frac{10.0}{20}$	$\frac{6.1}{14}$	$\frac{6.41}{10}$	$\frac{6.31}{31}$	$\frac{6.39}{10}$	$\frac{6.5}{10.4}$	$\frac{9.9}{21.7}$	$\frac{7.0}{33}$
-------------------	-------------------	------------------	-------------------	-------------------	-------------------	--------------------	--------------------	------------------

(62)

$\frac{10.3}{33}$	$\frac{10.3}{27}$	$\frac{9.3}{19.8}$	$\frac{5.1}{14.7}$	$\frac{5.59}{10}$	$\frac{5.52}{-}$	$\frac{5.58}{10}$	$\frac{5.7}{14.3}$	$\frac{8.6}{20.6}$	$\frac{3.1}{33}$
-------------------	-------------------	--------------------	--------------------	-------------------	------------------	-------------------	--------------------	--------------------	------------------

(51)

$\frac{7.1}{33}$	$\frac{8.4}{35}$	$\frac{8.1}{28}$	$\frac{7.7}{20.4}$	$\frac{4.6}{14}$	$\frac{4.06}{10}$	$\frac{4.39}{-}$	$\frac{4.48}{10}$	$\frac{4.6}{14.4}$	$\frac{7.2}{19.9}$	$\frac{7.0}{33}$
------------------	------------------	------------------	--------------------	------------------	-------------------	------------------	-------------------	--------------------	--------------------	------------------

(34)

$\frac{5.7}{36.3}$	$\frac{7.1}{37.3}$	$\frac{7.6}{36}$	$\frac{5.5}{19.7}$	$\frac{2.9}{14.3}$	$\frac{2.94}{10}$	$\frac{2.74}{-}$	$\frac{2.80}{10}$	$\frac{2.8}{10.4}$	$\frac{6.2}{20.7}$	$\frac{6.1}{20.7}$	$\frac{5.5}{22}$	$\frac{5.8}{22.2}$	$\frac{5.1}{31}$	$\frac{5.1}{33}$
--------------------	--------------------	------------------	--------------------	--------------------	-------------------	------------------	-------------------	--------------------	--------------------	--------------------	------------------	--------------------	------------------	------------------

(29)

$\frac{5.6}{37.9}$	$\frac{6.0}{26}$	$\frac{5.1}{18.7}$	$\frac{2.5}{14.5}$	$\frac{2.42}{10}$	$\frac{2.30}{-}$	$\frac{2.39}{10}$	$\frac{2.4}{14}$	$\frac{4.9}{19}$	$\frac{6.0}{19.5}$	$\frac{5.0}{22.2}$	$\frac{5.1}{31}$	$\frac{5.2}{33}$
--------------------	------------------	--------------------	--------------------	-------------------	------------------	-------------------	------------------	------------------	--------------------	--------------------	------------------	------------------

(14)

$\frac{4.7}{33}$	$\frac{4.9}{25.4}$	$\frac{3.5}{13.3}$	$\frac{1.0}{14}$	$\frac{0.87}{10}$	$\frac{0.83}{-}$	$\frac{0.90}{10}$	$\frac{0.9}{14.5}$	$\frac{4.0}{19.5}$	$\frac{4.4}{22}$
------------------	--------------------	--------------------	------------------	-------------------	------------------	-------------------	--------------------	--------------------	------------------

(10.7)

$\frac{14.2}{33}$	$\frac{14.4}{27}$	$\frac{12.3}{19}$	$\frac{10.2}{14.8}$	$\frac{10.20}{10}$	$\frac{10.09}{-}$	$\frac{10.12}{10}$	$\frac{10.1}{14}$	$\frac{12.7}{20}$	$\frac{13.0}{33}$
-------------------	-------------------	-------------------	---------------------	--------------------	-------------------	--------------------	-------------------	-------------------	-------------------

(9.7)

$\frac{12.2}{34}$	$\frac{12.7}{33}$	$\frac{12.3}{28.5}$	$\frac{10.8}{18.6}$	$\frac{9.1}{14.8}$	$\frac{9.14}{10}$	$\frac{8.97}{-}$	$\frac{8.99}{10}$	$\frac{8.9}{14.2}$	$\frac{12.6}{17.7}$	$\frac{11.5}{21.4}$	$\frac{11.9}{33}$
-------------------	-------------------	---------------------	---------------------	--------------------	-------------------	------------------	-------------------	--------------------	---------------------	---------------------	-------------------

(8.7)

$\frac{10.8}{33}$	$\frac{11.7}{26}$	$\frac{10.0}{19.4}$	$\frac{7.8}{14.9}$	$\frac{7.14}{10.1}$	$\frac{7.12}{10.8}$	$\frac{7.13}{-}$	$\frac{7.55}{10}$	$\frac{7.5}{15}$	$\frac{8.7}{20.2}$	$\frac{9.5}{33}$
-------------------	-------------------	---------------------	--------------------	---------------------	---------------------	------------------	-------------------	------------------	--------------------	------------------

(7.7)

$\frac{9.5}{33}$	$\frac{10.2}{27.5}$	$\frac{10.2}{21.6}$	$\frac{2.0}{16.3}$	$\frac{7.18}{12.2}$	$\frac{7.16}{11.9}$	$\frac{7.05}{-}$	$\frac{6.61}{10}$	$\frac{6.5}{14.7}$	$\frac{8.2}{19.5}$	$\frac{9.5}{33}$
------------------	---------------------	---------------------	--------------------	---------------------	---------------------	------------------	-------------------	--------------------	--------------------	------------------

309.06 ✓  
5

136+38.1

+63

136+28

137+55 ✓ End of Pavement.

+13

+42

+66

A.M.

7.00

302.06 ✓  
5

301.98

T.F.

0.33

298.30 ✓  
5

16.03

272.00 ✓  
5

B.M.

5.98

292.30 ✓  
5

292.30

P.M.

7.48

270.00 ✓  
5

(72)

28	7.8	8.6	2.1	6.29	7.08	6.55	6.09	6.0	6.6
29	2.5	2.27	1.87	1.43	1.40		$\frac{6.09}{10}$	$\frac{6.0}{19}$	$\frac{6.6}{33}$

(68)

3	8.5	4.0	2.1	6.5	4.75	6.12	5.51	5.4	5.13
2	2.2	2.57	2.5	1.9	1.47	1.43	$\frac{5.51}{10}$	$\frac{5.4}{20}$	$\frac{5.13}{33}$

(64)

8.7	8.2	8.4	6.2	6.21	6.55	5.68	5.09	4.8	4.7
3.3	2.5	2.2	1.7	1.49	1.46		$\frac{5.09}{10}$	$\frac{4.8}{25.5}$	$\frac{4.7}{33}$

2 to be corrected.

2.1	7.7	6.0	5.98	6.31	5.41	4.8	4.3	4.3
3.3	2.45	1.9	1.49	1.46		$\frac{4.8}{10}$	$\frac{4.3}{19}$	$\frac{4.3}{33}$

(60)

7.3	7.3	5.5	5.2	4.7	3.8
3.3	2.4	1.6		$\frac{4.7}{10}$	$\frac{3.8}{33}$

(57)

6.5	6.1	7.0	5.8	5.1	4.8	1.6
3.3	1.9	1.7	1.4		$\frac{4.8}{9}$	$\frac{1.6}{33}$

(55)

Same as original X-sec.

Spike in Pole R. 136+15.

Spike in Pole L. 132+

top of Hyd. L. 129+25

8-5-24

From Page 27

Final X-sections

Station	+	H.I		Red	Blue
		287.84	✓		

16 + 00

+ 13.5

+ 23.0

+ 50

17 + 00

T.P.	856	293.79	✓	2.61	285.23	✓
------	-----	--------	---	------	--------	---

18 + 00

+ 50

19 + 00

+ 35

20 + 00

B.M

1.52

292.27

H.

£

R1.

43

8-5-24

7.5	7.6	7.9	8.47	9.0
33.0	24.3	17.0	10.0	8.39

8.46	8.5	10.0	10.4	10.7	10.3	9.8
11.0	15.0	22.2	22.2	27.4	22.6	33.0

7.4	7.9	7.5	7.8	8.06	8.6
33.0	29.3	23.3	17.3	10.0	5.02

8.0	8.2	9.7	10.1	10.1	9.1	8.8	7.9
10.0	14.0	18.9	22.5	25.0	27.2	33.4	34.6

9.0	8.6	9.0	8.9	7.6	7.78	8.3
26.4	25.6	23.2	21.2	16.8	10.0	7.71

7.79	7.8	9.6	9.8	9.2	6.8	5.8
10.0	13.7	18.8	22.6	25.9	30.8	36.5

3.8  
4 57.6

5.6	6.4	8.3	9.3	7.1	6.90	7.0
52.6	26.3	23.8	19.6	15.0	70.6	6.87

6.98	7.3	8.8	9.2	3.6
10.0	13.8	12.4	24.8	34.8

4.0	1.2	7.2	7.4	5.5	5.35	6.0
36.5	28.7	22.6	18.8	13.6	10.0	5.86

5.50	5.7	5.0	8.0	6.9	3.3
10.0	13.8	20.2	24.2	26.1	33.0

4.0	5.5	10.7	10.9	9.2	8.78	9.0
31.6	26.2	21.0	18.0	14.9	10.0	8.73

8.82	8.9	10.2	11.2	8.2	6.9	7.0
10.0	13.2	19.7	23.8	28.6	31.8	33.0

3.9	4.5	9.3	9.6	7.7	7.70	7.0
25.7	26.3	22.9	18.4	13.8	10.0	7.62

7.68	7.9	9.4	10.4	9.8	5.8	5.9
10.0	13.5	16.3	20.7	25.6	31.2	33.0

5.1	7.0	8.4	9.1	6.9	6.69	6.4
32.3	26.3	23.7	21.3	17.4	13.9	10.0

6.69	6.7	8.4	8.7	8.2	5.0	5.9
10.0	13.7	18.0	20.7	25.2	30.8	33.0

4.8	6.3	7.9	7.8	6.3	6.16	6.0
25.1	23.4	21.4	17.4	13.7	10.0	6.05

6.10	6.2	7.8	8.1	7.7	4.8	4.8
10.0	13.5	17.5	22.6	25.4	31.9	33.0

4.0	3.7	6.8	6.6	5.3	5.10	4.6
33.0	25.7	21.8	18.1	14.4	10.0	5.03

5.12	5.1	6.2	6.6	5.9	2.9	2.0
10.0	13.9	17.2	21.5	25.1	31.1	33.0

11 Nail in T.P. R4 etc 20+10

Univeway Measurements.

Sta 6+830

Right

0+00 Shoulder line

+07.5

+18.5 a.g. line

Left

0+00 Shoulder line

+05

+14 a.g. line

Austin  
Hoaglan  
Bentbourne  
Schmidt.

8-6-24

$$\begin{array}{r} \frac{0.0}{12.0} \\ -2.6 \\ \hline 10.0 \end{array} \quad \begin{array}{r} 0.0 \\ 0.0 \\ \hline 0.0 \\ 0.0 \\ \hline 0.0 \end{array} \quad \begin{array}{r} 0.0 \\ 0.0 \\ \hline 0.0 \\ 0.0 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} \frac{0.0}{12.0} \\ \frac{0.0}{8.0} \\ \hline 8.0 \end{array} \quad \begin{array}{r} -2.6 \\ \hline 10.0 \end{array} \quad \begin{array}{r} \frac{0.0}{8.0} \\ \hline 8.0 \end{array}$$

$$\begin{array}{r} \frac{0.0}{10.0} \\ -2.0 \\ \hline 8.0 \end{array} \quad \begin{array}{r} \frac{0.0}{7.0} \\ \frac{0.0}{7.0} \\ \hline 0.0 \\ 0.0 \\ \hline 0.0 \end{array} \quad \begin{array}{r} 0.0 \\ 0.0 \\ \hline 0.0 \\ 0.0 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} \frac{0.0}{10.0} \\ \frac{0.0}{7.0} \\ \hline 7.0 \end{array} \quad \begin{array}{r} -2.0 \\ \hline 8.0 \end{array} \quad \begin{array}{r} \frac{0.0}{7.0} \\ \hline 7.0 \end{array}$$

6

4

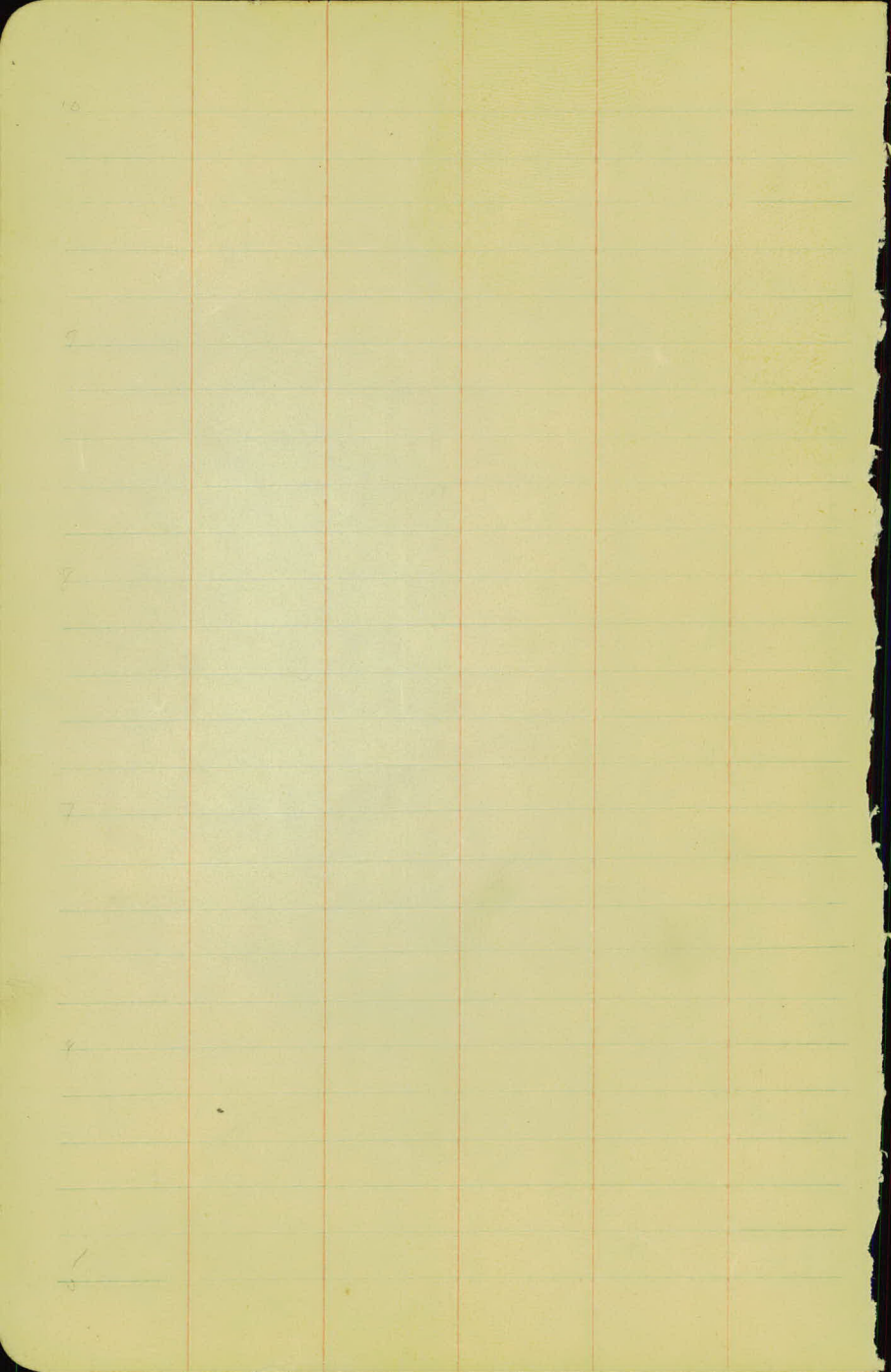
3

2

1

6+00





8-6-24

+94 Inrain Tile  
Outlet

+61 Bop. Gd. Rail

+95 P.P. 36.3

+79 Bop. Gd. Rail

+87 P.P. 36.5

+78 P.P. 36.4

Concrete Pavement

12" x 16.5 C.M.P.

+75

12" x 16.5 C.M.P.

+83 1/2 Unileway

+75

+76 P.P. 36.0

+47 End Int. Bur.

+62 P.P. 37.8 R.I.

10' x 10' +52.3 B.W.T

10' x 11.13' +62.3 P.T

10  
9  
8  
7  
6  
5

15

14

13

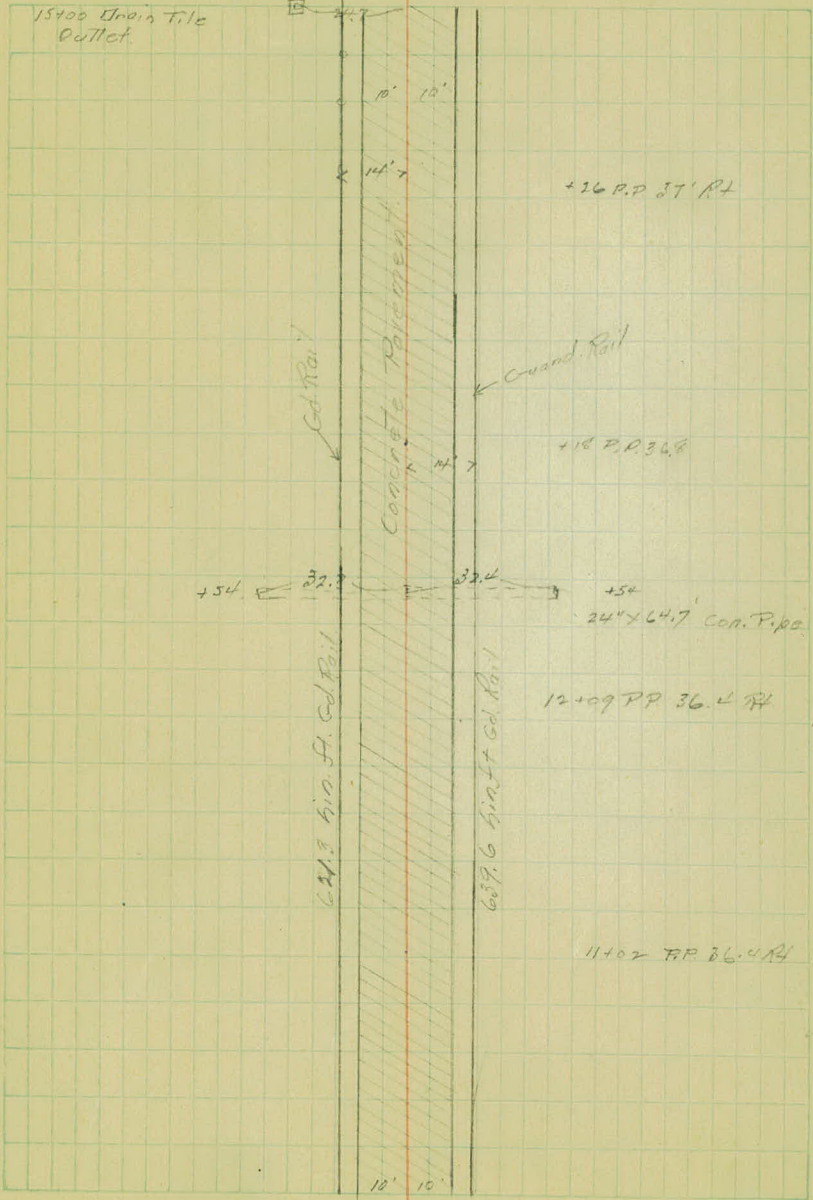
12

11

10

8-6-24

15400 Drain Tile  
Outlet



+36 P.P. 37' RT

+18 P.P. 36.8

+54 24" x 64.7' Con. Pipe. Coll

12+09 PP 36.4 RT

11+02 PP 36.4 RT

Gd. Rail

Guard Rail

Concrete Pavement

241.9 510. Ft. Gd. Rail

639.6 510. Ft. Gd. Rail

14

13

12

11

10

44.7

10' 10'

14.7

32.7

33.4

+54

10' 10'

20

19

18

17

16

End of Payment Dec. 11, 1973.

End of Cully

End of Cully  
or 11

15



25

156<sup>3</sup> Beg. of Gaurd Rail-L.

24

23

22

21

20



+72 Japin BR  
+56.3

⊕ +47 Po. Pole

Tel. Pole +13

⊕ +31 Po. Pole

Tel. Pole +74

Concrete Pavement

⊕ +32 Po. Pole

Subway Vile

Tel. Pole +43

⊕ +24 Po. Pole

Tel. Pole +14 33' →

37' ⊕ +16 Po. Pole

30

29

28

+06.0 Beg. of Fence R. 53'

27

+10.5 End of Guard Rail, L. & R.

+6.45 Log in G.R. L. & R.

26

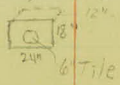
+52 End of 6" Drain Tile  
(24" R.)

Conc. Face Wall 24" X 12" X 12"

+15 End of Drain Tile (6" 27.5' L., Conc. Face Wall, 24" X 12" X 12"

+64.5 Beg. of G. Rail 15 R.

25



10' 10'

4

37'

55'

Tel. Pole +23

Wave Wire.

+13 Po. Pole

Burb Wire.

+79 Po. Pole

Tel. Pole +91

Entrance +79  
(16 Gate)

+93 Entrance 20' wide

+69 Po. Pole

Pavement

Concrete

55'

Tel. Pole +67

16'

4'

5'

16'

+62 Po. Pole

POST S.C.C.

POSTS S.C.C.

Tel. Pole +39

34.5'

+54 Po. Pole

+20.8 Top in G.R.

+04.5 Top G.R.

9'

10' 10'

35

34

33

+89.8 End of Gaurd Rail 15' Left

32

+77.5 End of Gaurd Rail 15' R.

31

+62 End of 6" Tile Drain 24' Left - Conc. Face Wall 24" X 18" X 12"

+26 End of 6" Tile Drain 26' R. Conc. Face Wall 24" X 18" X 12"

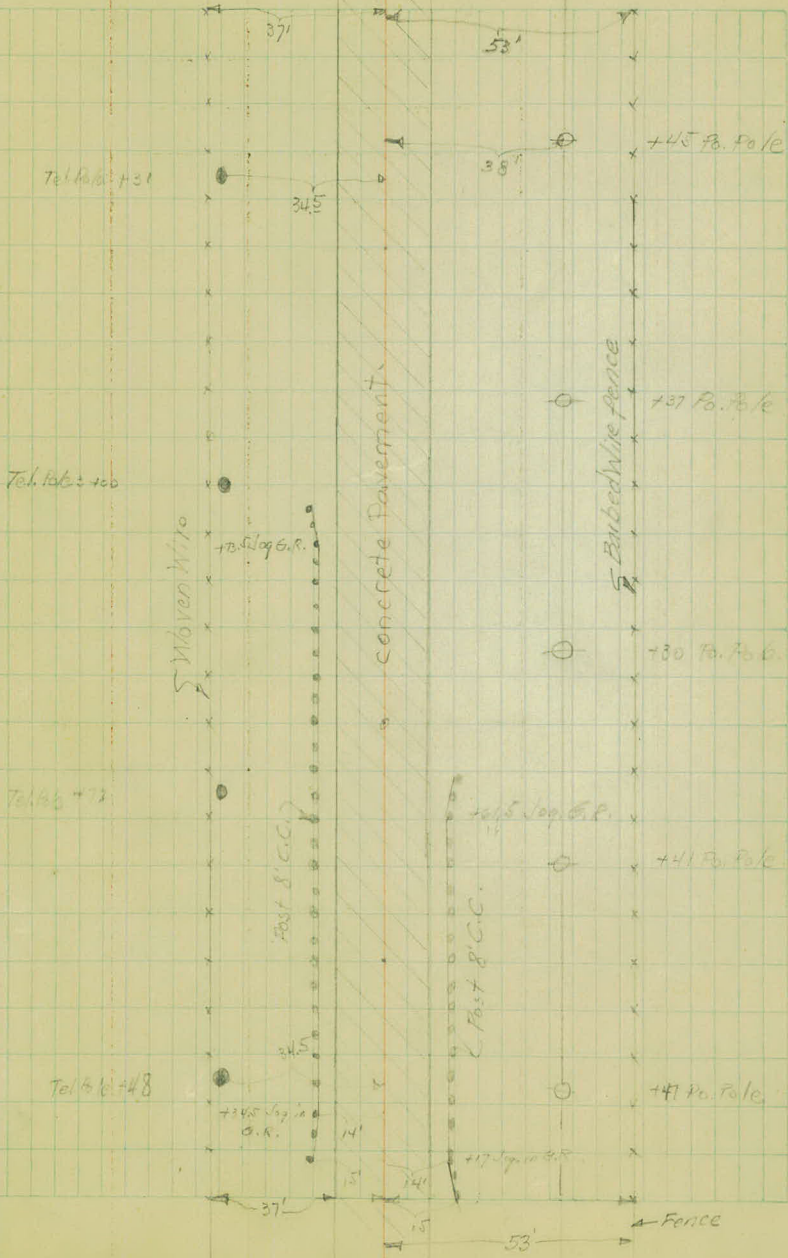
+12.5 Beg. Gaurd Rail 15' L.

-01 Beg. of Gaurd Rail, 15' R.

30

10 x 10

±



40

39

38

+43 End of 6" Drain Tile 26' L. Conc. Face Wall, 24" X 18" X 12"

+20.5 Beg of Guard Rail 15' Left

37 +08 End of 6" Drain Tile 34' R. Conc. Face Wall, 24" X 18" X 12"

+71.5 Beg of Guard Rail 15' R

36

35



45

+81 End of G.R. 14' L. 2 with Wings.

+80 End of G.R. 14' R.

+5.5 End of 6" Drain Tile 25' L. Conc. Face Wall 24" X 18" X 12"

+35 End of 6" Drain Tile 26' R. Conc. Face Wall 24" X 18" X 12"

44

43

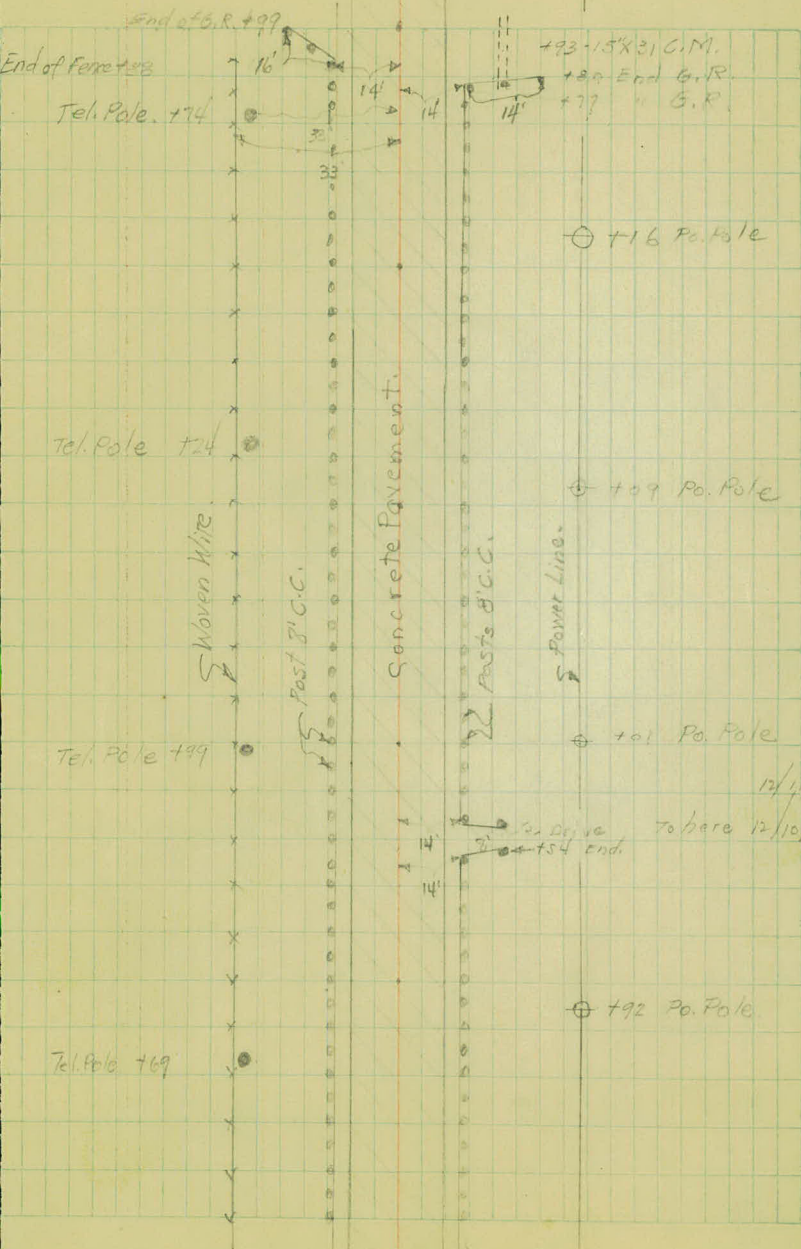
42

+67.5 Beg of Guard Rail 14' R.

+51.5 End of Guard Rail 14' R.

41

40



50

736 Drive R.

49

48

47

46

+14  $\notin$  Road

45



55

+10 End of 6" Drain Tile 27' L. Conc. Face Wall. 24" x 18" x 12"  
+05 Beg. G.R. 14' L.

54

+18 Beg. of G.R. 11' R.

+35 End of culvert 6" V. 23' L.

+34 End of <sup>6"</sup> Tile Drain 21' R. Conc. Face Wall 5. 24" x 18" x 12"

53

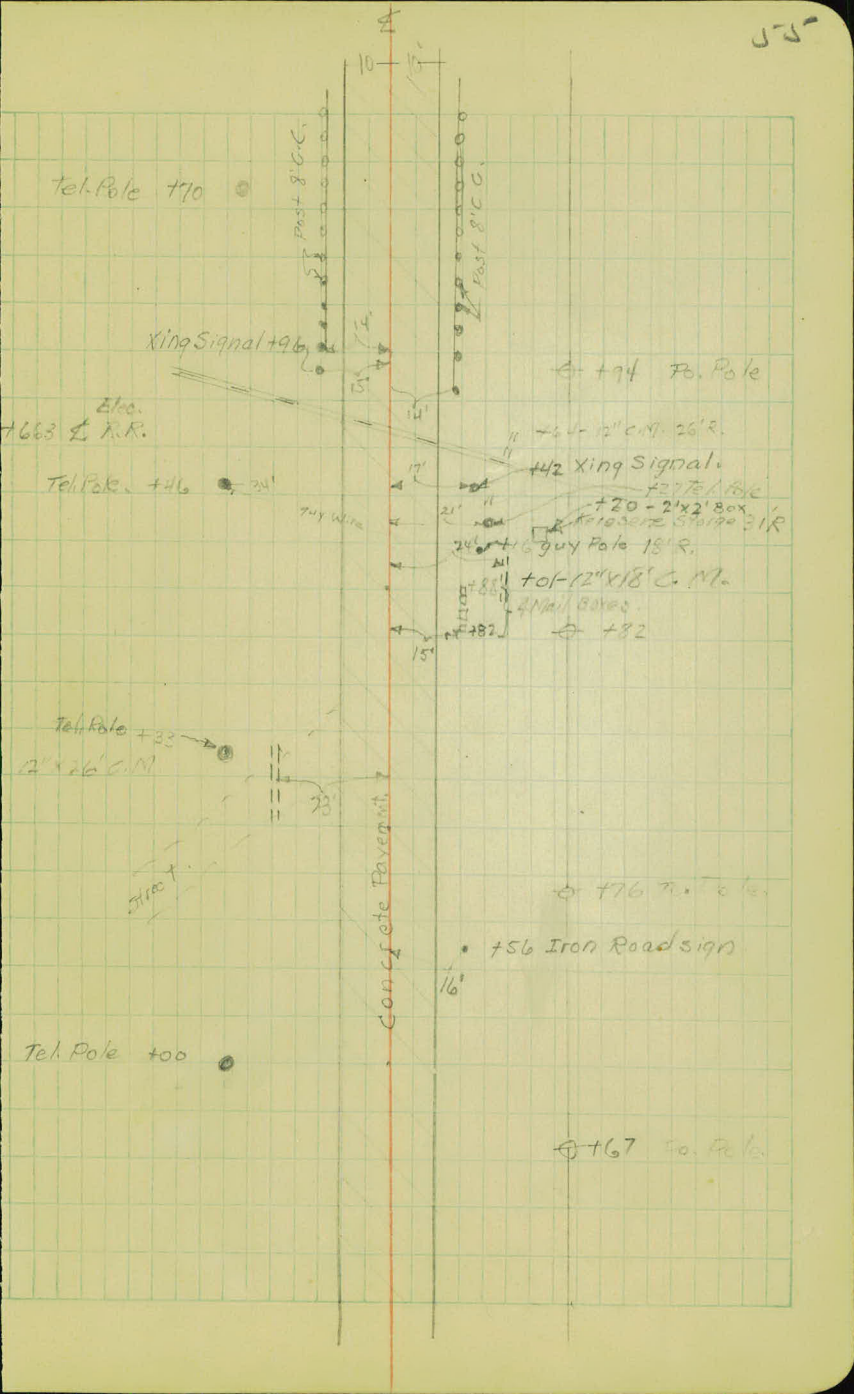
+18 Div. Drive L.

52

+18 Drive Drive.

51

50



60

59

704 Drive R.

58

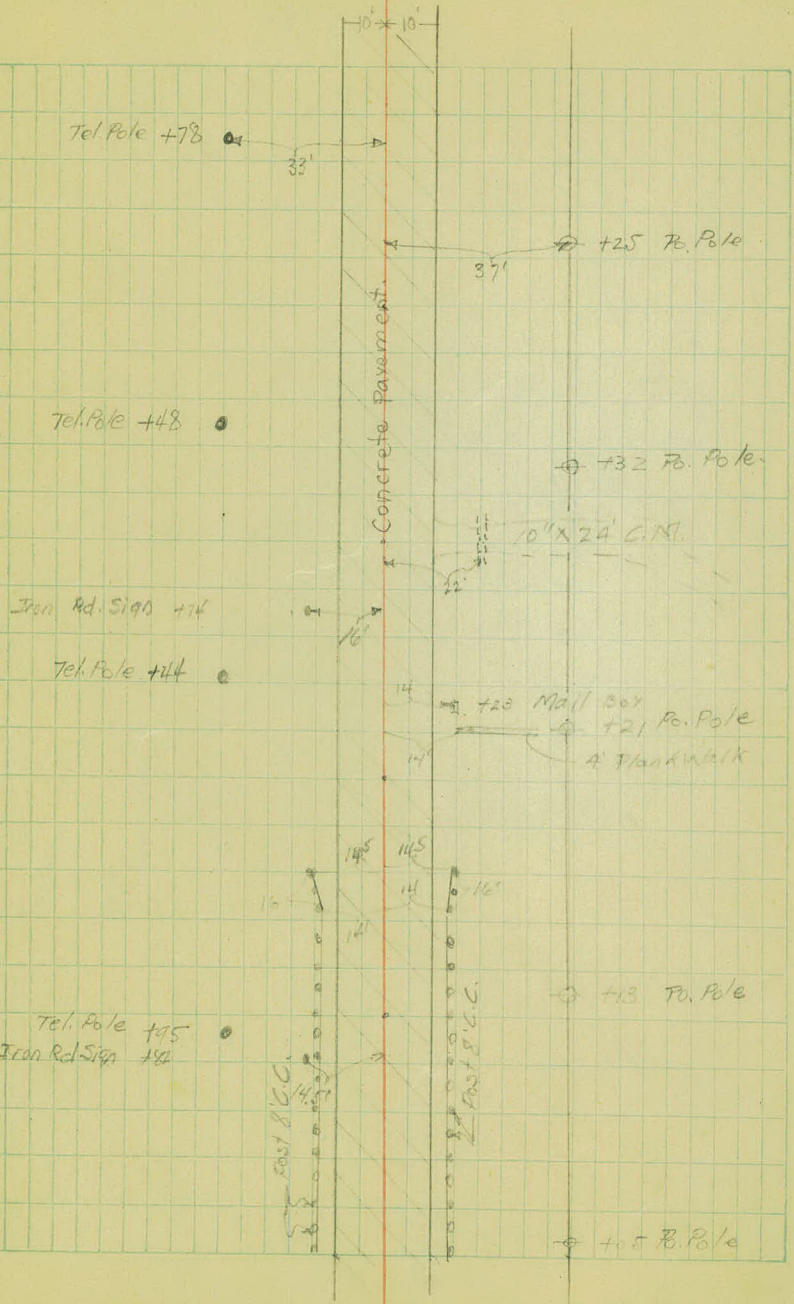
57

+62 End of G.R. L.  
760 End of G.R. R.

56

55

144



65

+ 61.5 End of G.R. 15' R

+ 59 End of G.R. 15' L

64

63

62

+ 96 E Street

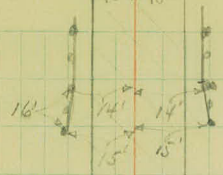
61

+ 755 End of 6" Drain Tile 21' L. Conc Face Wall 24" X 18" X 12"

60

E.

10' x 10'



Tel. Pole +82

⊖ +54 Tl. Pole

Tel. Pole +55

⊖ +58 Tl. Pole

Tel. Pole +51

⊖ +51 Tl. Pole

Concrete Pavement

Tel. Pole +15

⊖ +41 Tl. Pole

⊖ 733 Tl. Pole

70

69

+48 Beg. G.R. 14.5' R.

68 6 Street

+70 Pliv. Drive R

+62 End of G.R. 14' (R) L.

67

+84.5 End of G.R. 15' R.

66

+30.5 24" X 42.5 C.M. Drains L.

65



75

74

73

72 +00 End of 6" Di. T<sub>1</sub>/0 22' R. Conc Face Wall, 24" X 12" X 12"

71

+52 ± 4<sup>th</sup> St.

+07.5 End of C.R. 14' R.

70

E



⊕ +24 Po. Pole

Tel. Pole +71 ●

⊕ +15 Po. Pole

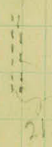
Tel. Pole +63 ● 31

⊕ +09 Po. Pole

Tel. Pole +51 ●

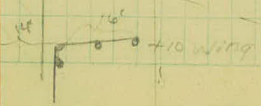
34' ● 71+00 Po. Pole

5" x 20  
S.M.  
+82  
+53



16' ● +75 Mail Box

Tel. Pole +13 ●



80

+52 Fire Hydr L.

+27 Priv. DIIVEL

79

+58 E Co. Road B

75 - Hand out

78

+09 End of G.R. 15' L.

77

+57 End of 6" Drain 24<sup>5</sup> L. CONC FIRE WALL 26" x 18 3/4"

76

75+00 Beg. of G.R. 15' L.



85

+68 £ Oak Hill Place NW

84

83

82

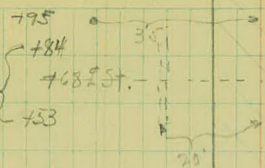
81

80

E

10' x 10'

Iron  
St. Sign



Tel. Pole +13


+95 Po. Pole


Tel. Pole +86

+87 Po. Pole

Concrete Pavement

Tel. Pole +58

15'  +92 - 2.5 x 10' Wood Work  
+87 Po. Pole

15'  +90 - 2.5 x 11' Wood Work

+67 Po. Pole

Tel. Pole +28

90

+67 End of 6" Drain Tile 25' L. Conc. Face Wall 21" x 18" x 12"

89

88

+81 Fire Hydrant 50' left.

+21 E 2<sup>nd</sup> St.

87

86

85

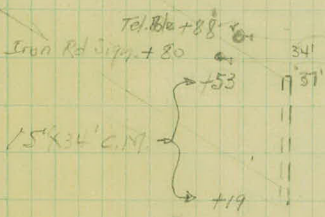
10' x 10'

Concrete Pavement

Tel. Pole +14

+26 P. Pole

+19 P. Pole



Tel. Pole +27

Gas Pole +69

+116 +19 P. Pole

15' x 37' C.M.

+179

+08 P. Pole

Tel. Pole +41

35'

+02 P. Pole

95

+68 Priv. Drive L.

94

+69 E Penn Place Left

93

92

+40 End of Tile Dia 10.275 Conc. Face Wall 24" x 18" x 12"

91

90

Z

56.2

199

774.5

789

July 18'

774.5

⊕ 765 P.O. Pole

12" x 14" c.M.

Tel. Pole +19



10" x 16" c.M.

789

Iron Rd Sign 753



⊕ 757 P.O. Pole

Tel. Pole +91



⊕ 749 P.O. Pole

Tel. Pole +63

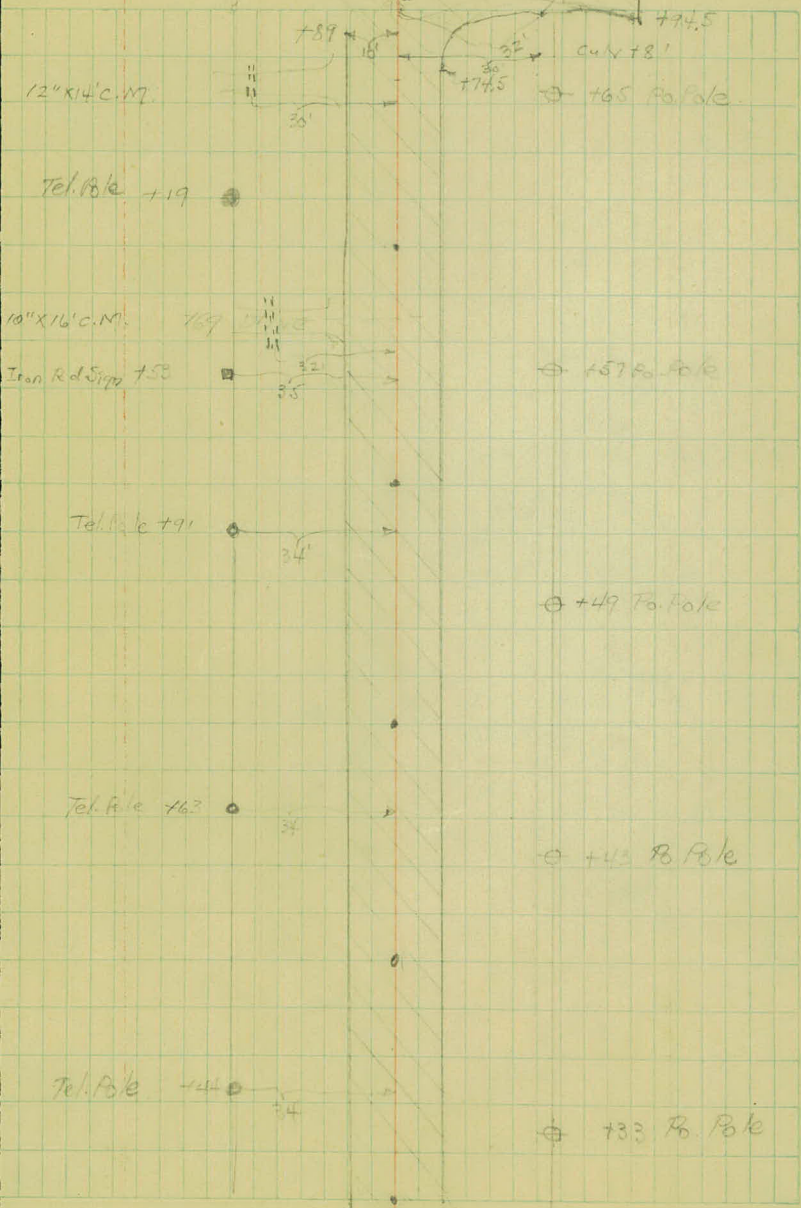


⊕ 743 P.O. Pole

Tel. Pole +44



⊕ 733 P.O. Pole



100

99

98

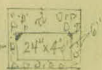
97

- +32 Mail Box (U.S.) 48" L.
- +24 Fire Hydrant 35" L.
- +22 Iron Sign Post 36" L.
- +17 Water Gate Valve.

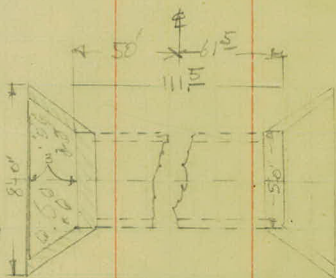
96

159  $\frac{1}{2}$  1st St.

- +55  $\frac{1}{2}$  Culv. Rd. Box
- +45 1st Culv. 66" R.



opening



95



105

+60 Iron Ref. Sign 34' L.

+30 Water Gate Valve 36' L.

+35 center of Arc of Paving.

104

+29 2 Helors St.

+44 center of Arc of Paving.

103

+66<sup>±</sup> E. PIN, DRIVE 10' DRIVE

102

101

100



110

+75.1  $\pm$  12' Priv. Drive

109

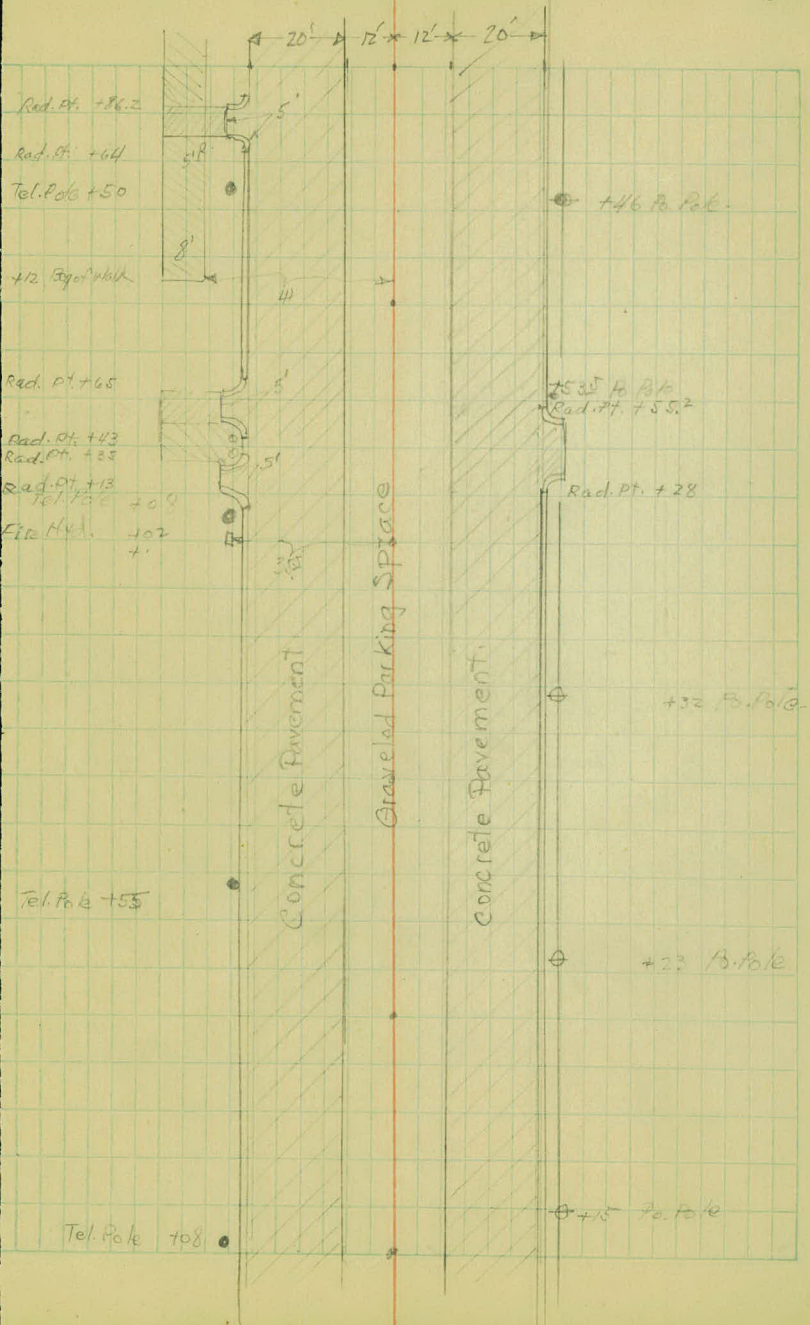
+54  $\pm$  12' Drive. Left.  
+41 Gas Pump 24' L.  
+36.5 Gas Pump 24' L.  
+25  $\pm$  12' Drive  
+28  $\pm$  24' Drive Right

108

107

106

105



Rad. Pt. +86.2  
 Rad. Pt. +64  
 Tel. Pole +50

1/2 Bay of Walk

Rad. Pt. +65

Rad. Pt. +43  
 Rad. Pt. +23

Rad. Pt. +13  
 Tel. Pole +08

Fire Hydr. +02  
 +1

Tel. Pole +55

Tel. Pole +08

Concrete Pavement

Graveled Parking Space

concrete Pavement

+46 B. Pole.

+55.2  
 Rad. Pt. +55.2

Rad. Pt. +28

+32 B. Pole.

+23 B. Pole

+15 B. Pole

115

+37.1 E 11' Drive.

114

+13 Iron Rd. Sign 40' L.


113

+76 Center of Arc of Paving.

+73 Mushroom Light.

+40' E Margaret St.

+26 Fire Hyd. 35' L.

+20 E of Tel. Booth. 36' Helogen 

+9.6 Mushroom light.

112

+95.5 center of Arc. of Paving.

+65 Pa. Rd 33' R.

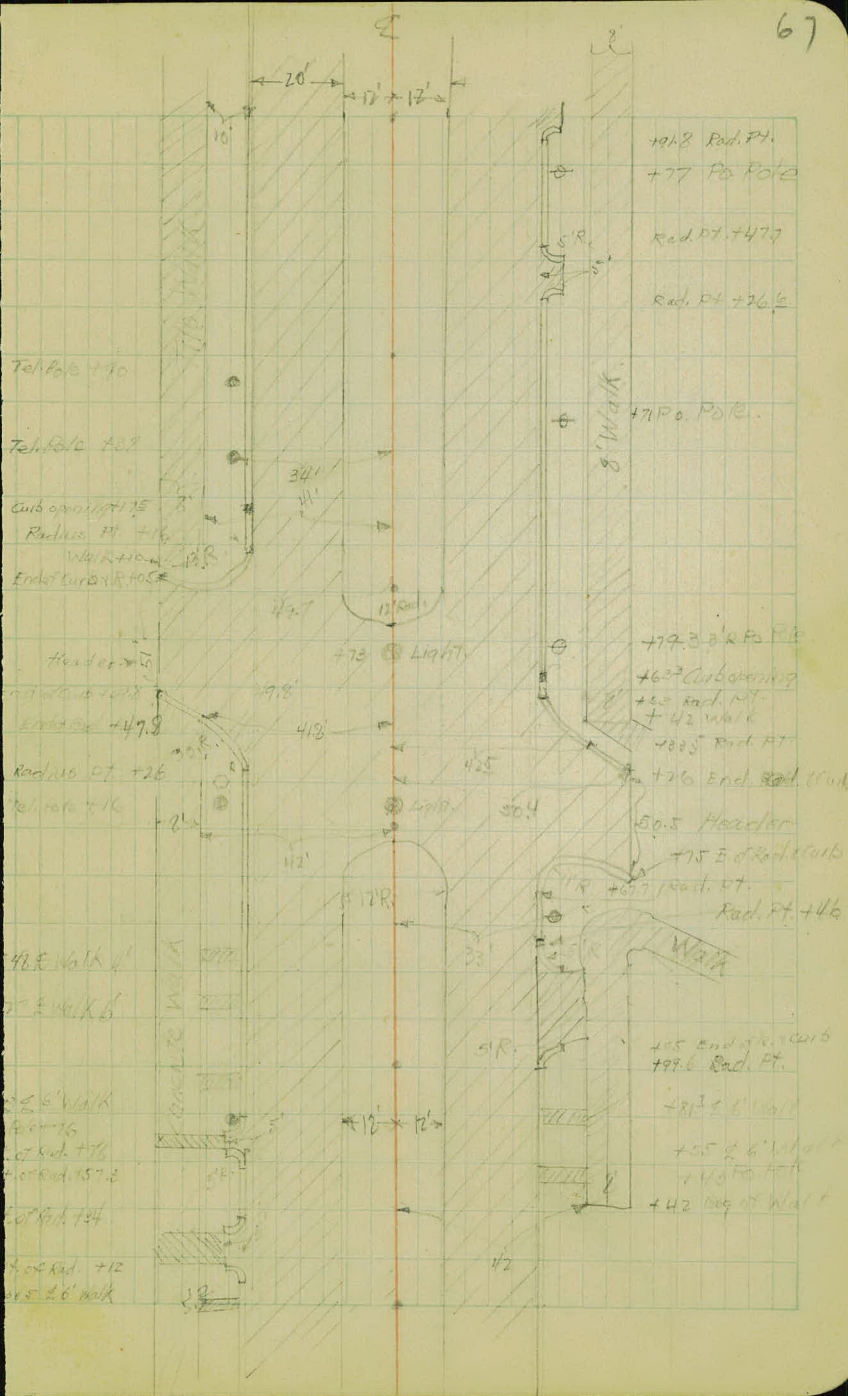
+22.8 E 32. Drive filling Sta.

111

+68 E Riv. Drive 10' wide.

+23 E Priv. Drive 12' wide.

110



120

119

+40  $\frac{5}{2}$  Gas Pump 34.5 L.  
+37 Gas Pump 34.5 L.

5x3' conc base

118 +06  $\frac{5}{2}$  DRIVE

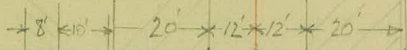
117

+23 Gas Pump 34.5 L.  
+18 " " 34.5 L.

conc base 2.5 x 2.5

116

115+02  $\frac{5}{2}$  DRIVE R.



+47 Tel. Pole

Concrete Walk

Rad. Pt. +16



Rad. Pt. +96.3

Tel. Pole +97  
33.5

+15 Fib. Hyd. 200

Rad. Pt. +07.5  
+023

11455?

Rad. Pt. +60.7  
Tel. Pole +34

5' 6" Curbing

8' Walk

Tel. Pole to 8  
344

Concrete Pavement

Graveled Parking Space

Concrete Pavement

6" Curbing

Walk

+14 Po. Pole 14' R.

+18 Po. Pole 20' R.

+53 Rad. Pt.  
+48.3

+75 Po. Pole  
+705 Air Stand

+41.0

+28.7 Rad. Pt.

+86 Po. Pole

+12 Rad. Pt.



125

124

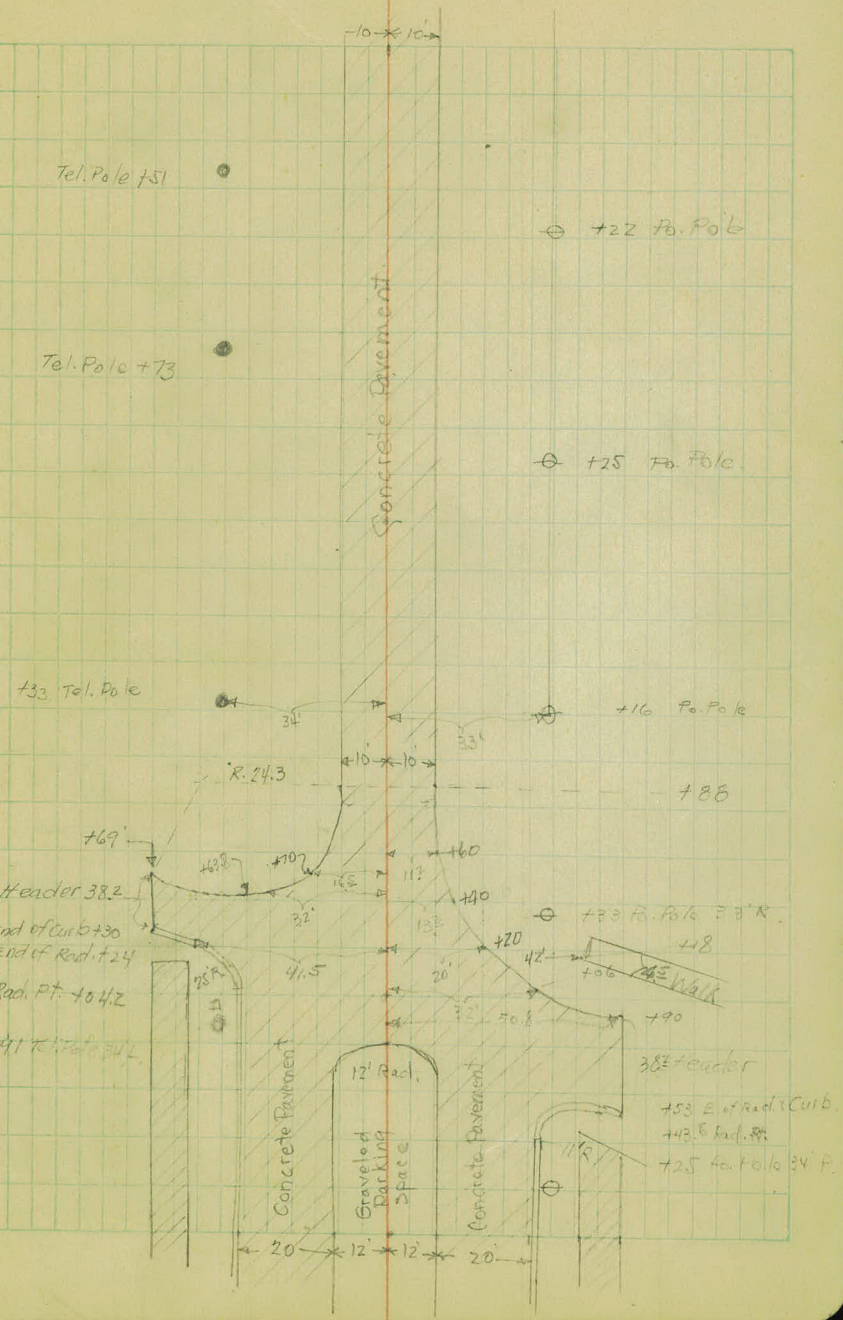
123

122

+11 E Charles St.  
+02 Iron Rd. Sign 39' L.  
121 +00  
+9.55 Fire Hydrant 34' L.  
+80.8 Center of Arc. of Paving

120

4



Tel. Pole +51

+22 Po. Pole

Tel. Pole +73

+25 Po. Pole

+33 Tel. Pole

+16 Po. Pole

R. 24.3

+88

+69

10' x 10'

Header 38.2

+33 Po. Pole E.B.N.

End of Curb +30

End of Rad. +24

Rad. Pt. +04.2

+41 Tel. Pole 34 F.

28'R

10' x 10'

+18

+06 Walk

11'

13'

20'

42'

50.6'

20'

12'

12'

20'

38" Header

+53 E of Rad. Curb

+43.6 Rad. Pt.

+25 Po. Pole 34 F.

Concrete Pavement

Gravelled Parking Space

Concrete Pavement

20' x 12' x 12' x 20'

130

128  $\frac{1}{2}$  Henry St.  
106 24" X 129 C.M.  
129

128

127

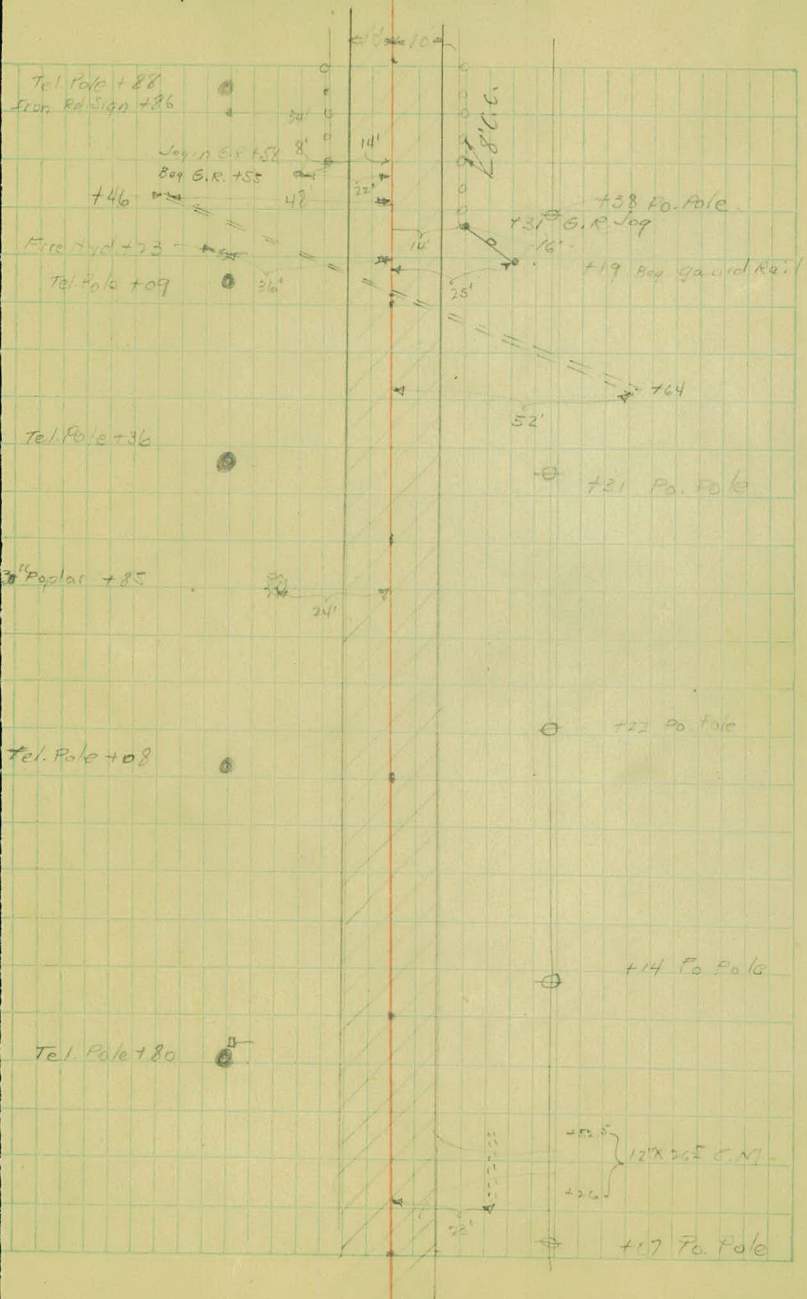
126

104 Fire Hyd. 34'L.

139  $\frac{1}{2}$  24' Drive R.

125

4



135

+20 Beg of G. Rail

134

133

+13 End of G. R. 14' L.

132

131

130

E

Pont 8' C.C.

Concrete Pavement

Po Pole +75-0

+21 Po Pole

+15 Po Pole

+0 Po Pole +35

+51 End of G.R.

+35 Jdg

904 Po Pole +07

+05 Po Pole

+00 Po Pole

130798 Po Pole

+16 Po Pole



	L	E	R
10+00	F 1.9	0.0	0.32
9+00	4.01	0.21	0.45
8+00	0.08	0.05	0.09

119 Iron Rd. Sign 32' R.

105.5 End of Pavement

137 195 Iron Rd. Sign 28' L.

111 Iron Rd. Sign 32' L.

165 Wood. sign post 32' L.

113.1 B.C.

136

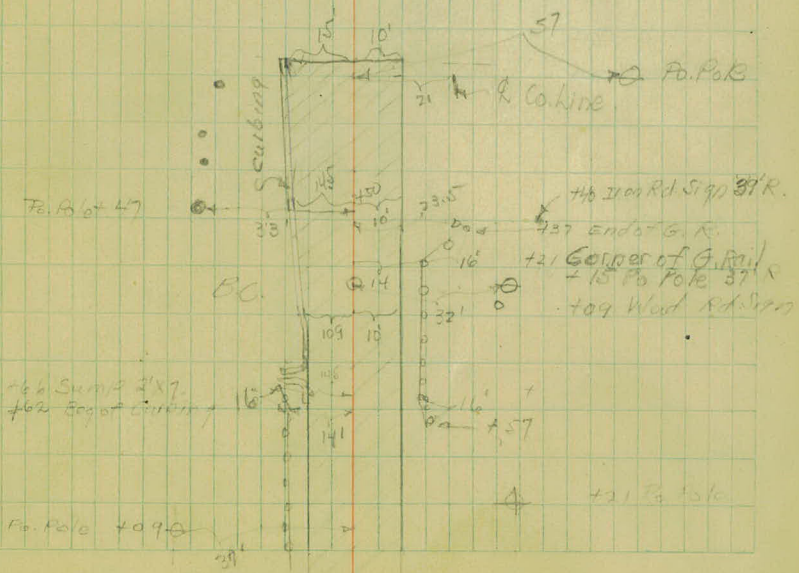
164.7 End of G.R. Left

157 Beg G.R. Right

135

W.H. Carlson  
P.C. Crane  
A. Nelson  
M. Ahlberg  
Dec 1273

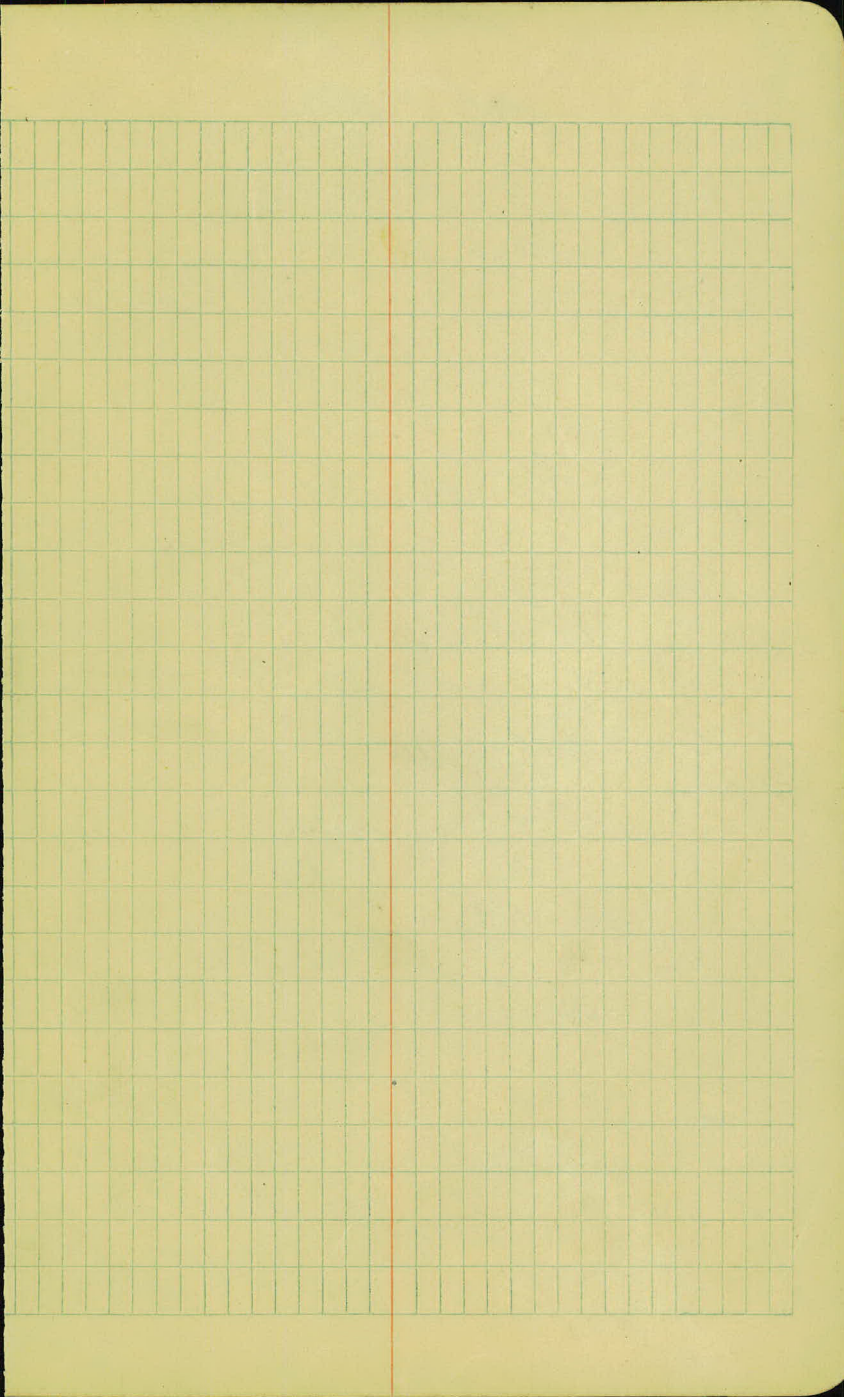
Z



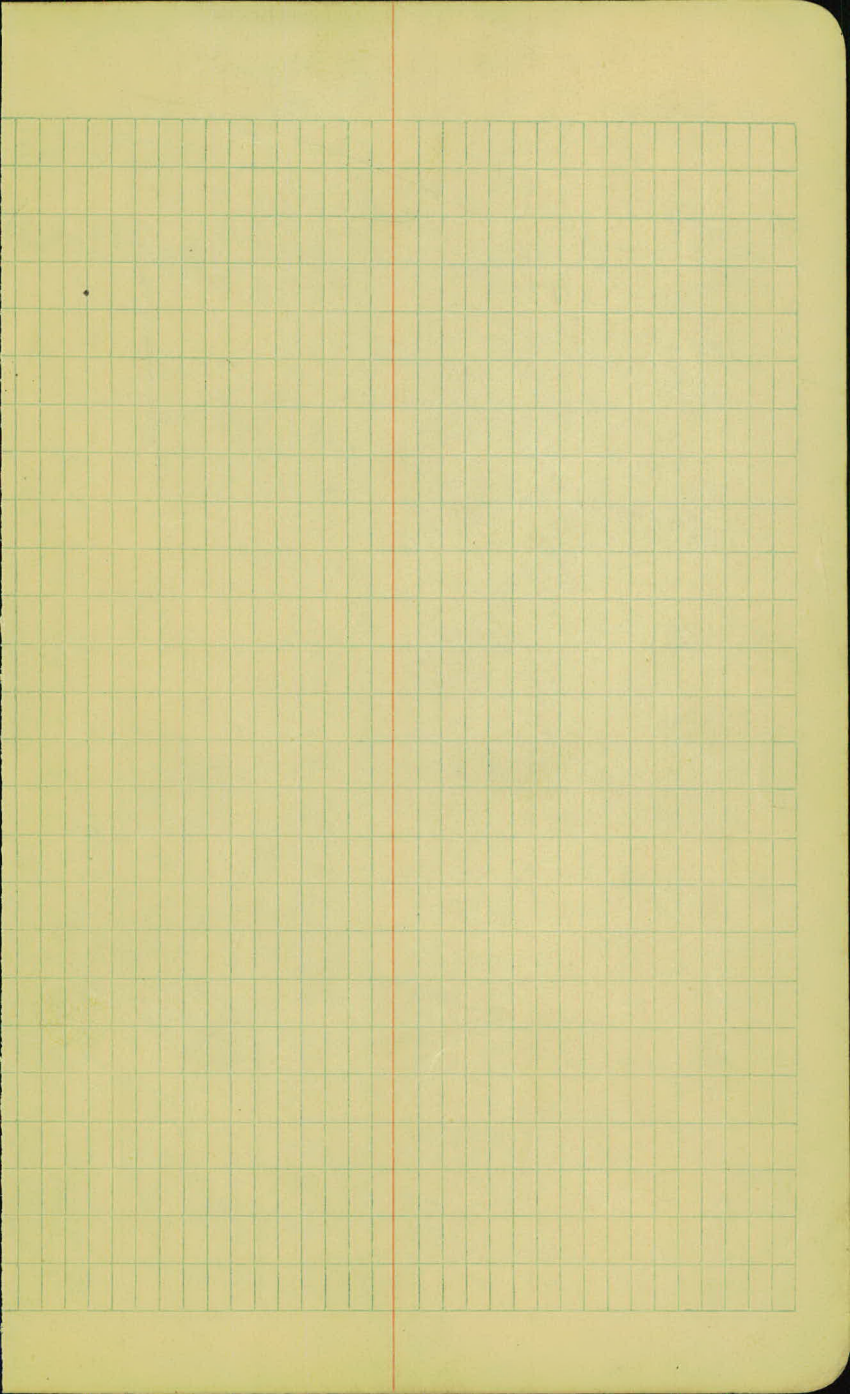
73

Profile  
Grade

0+00	B.C.	1.13			
+50		2.29			
1+00		}	50.42	+0.15	
+57			51.45	-0.15	
2+00			52.60	+0.30	
+50			54.75	-0.48	
+97				+0.48	
3+00			56.92	+0.62	
+50			58.92	-0.62	
4+00			60.76		
+52 <sup>3</sup>	E.S.T		2.29	+0.62	
5+02 <sup>3</sup>	E.C.		1.13	-0.62	
+52 <sup>3</sup>		0.0	+0.44		
6+02 <sup>3</sup>			-0.44		
+52 <sup>3</sup>	B.S.T		+0.26		
			-0.26		
			+0.08		
			-0.08		



Station.		700' v.c.			
B.C.	2+50	54.75	—	54.75 ✓	600' v.c.
	3+00	57.0	—	56.92 ✓	56.92
	+50	59.25	—	56.92 ✓	
	4+00	61.5	—	60.76 ✓	61.37
	+50	63.75	—	62.44 ✓	
	5+00	66.0	—	63.95 ✓	65.49
	+50	68.25	—	65.29 ✓	
P.I.	6+00	70.5	—	66.48 ✓	67.05
	+50	70.45	—	67.49 ✓	
	7+00	70.4	—	68.35 ✓	69.89
	+50	70.35	—	69.04 ✓	
	8+00	70.3	—	69.56 ✓	70.17
	+50	70.25	—	69.92 ✓	
	9+00	70.2	—	70.12 ✓	70.12
E.C.	+50	70.15	—	70.15	



10.Ht.

L

10.R

0+00

+50

1+00

50.42 ✓

50.29

1+57

51.40

51.45 ✓

51.30

51.18

+015

-015

+90

2+00

(52.60)

52.87 ✓

+03

-03

+23

+50

(54.75)

54.82 ✓

+048

-048

+87

E.S.T

56.40

+062

-062

3+00

57.0 ✓

+50

59.25

4+00

61.50

+50

62.60

2.3

5+02.3

E.C.

65.4

+045

-045

+50

0.0

6+00

+ 300 51.70

+ 26.5 51.62

3+23 = 51.54

14570

+ 71 = 50.49

2+67 = 50.4

} 1+00

9+290.0  
7+26.5  
3+23.0

14572

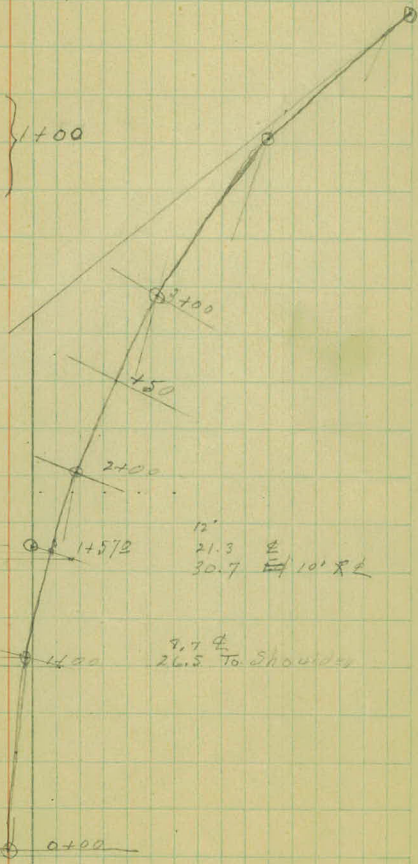
12'  
21.3 E  
30.7 E/10' R L

2+71  
2+67.0

1400

9.7 #  
26.5 To Shoulder

14762 0+00



B.M	0.35	292.65	(292.30)	
16 + 00			13.3	79.4
+ 50			12.7	80.0
17 + 00			11.5	81.2
+ 50			10.9	82.4
18 + 00			8.7	84.0
+ 50			7.7	85.0
19 + 00			6.3	86.4
+ 50			5.5	87.2
20 + 00			4.0	88.3
+ 50			3.7	89.0
21 + 00			3.2	89.5
+ 50			2.7	90.0
22 + 00			2.8	89.9
+ 50			2.5	90.2
23 + 00			2.9	89.5
+ 50			2.9	89.5
24 + 00			2.7	90.0

$\begin{array}{r} 21.8 \\ 1.0 \\ \hline 20.8 \\ 2.450 \\ \hline 2.450 \\ 100 \\ \hline 1.225 \end{array}$

$\begin{array}{r} 90.0 \\ 90.0 \\ \hline 180.0 \\ 400.0060 \\ \hline 580.0060 \end{array}$

$\begin{array}{r} 3.000 \\ .006 \\ \hline 2.994 \\ 1.7335 \end{array}$

$\begin{array}{r} 13 \\ 12 \\ \hline 25 \\ 12 \\ \hline 37 \end{array}$

$\begin{array}{r} 7335 \\ 15 \\ \hline 36675 \\ 22005 \\ \hline 58680 \end{array}$

- 16+00 - 78.8 - 78.8 ✓
- 16+50 - 80.3 - 80.3 ✓
- +73 - 80.7 - 80.7 ✓
- 17+00 - 81.8 - 81.78 ✓
- +50 - 83.3 - 83.15 ✓
- 18+00 - 84.8 - 84.4 ✓
- +50 - 86.3 - 85.52 ✓
- 19+00 - 87.8 - 86.51 ✓
- +50 - 89.3 - 87.38 ✓
- +73 - 90.0 - 87.75 ✓
- 20+00 - 90.0 - 88.14 ✓
- +50 - 90.0 - 88.76 ✓
- 21+00 - 90.0 - 89.25 ✓
- +50 90.0 - 89.62 ✓
- 22+00 - 90.0 - 89.87 ✓
- +50 - 90.0 - 89.98 ✓
- +73 - 90.0 - 90.0
- 23+00 - 90.0 ✓
- +50 - 90.0 ✓
- 24+00 - 90.0 ✓
- +50 - 90.0 ✓
- 25+00 - 90.0
- +50 - 90.0
- 26+00 - 90.0

MO = 2.58

L = 700

349	+	H.I	-	Red	5/100
B.M.	173	277.07			275.34
4 + 50				63.0	
5 + 00				65.4 ✓	
6 + 00				68.2 ✓	
7 + 00				69.8 ✓	F.I.U
8 + 00				70.3 ✓	
9 + 00				70.2 ✓	
10 + 00				70.1 ✓	
11 + 00				70.0	
12 + 00				-6.0 70.3	
13 + 00				-5.0 <sup>+5.0</sup> 71.4 ✓	65.8 Elev. -1.7
14 + 00				72.2 ✓	10.1
15 + 00				75.6 ✓	0.0

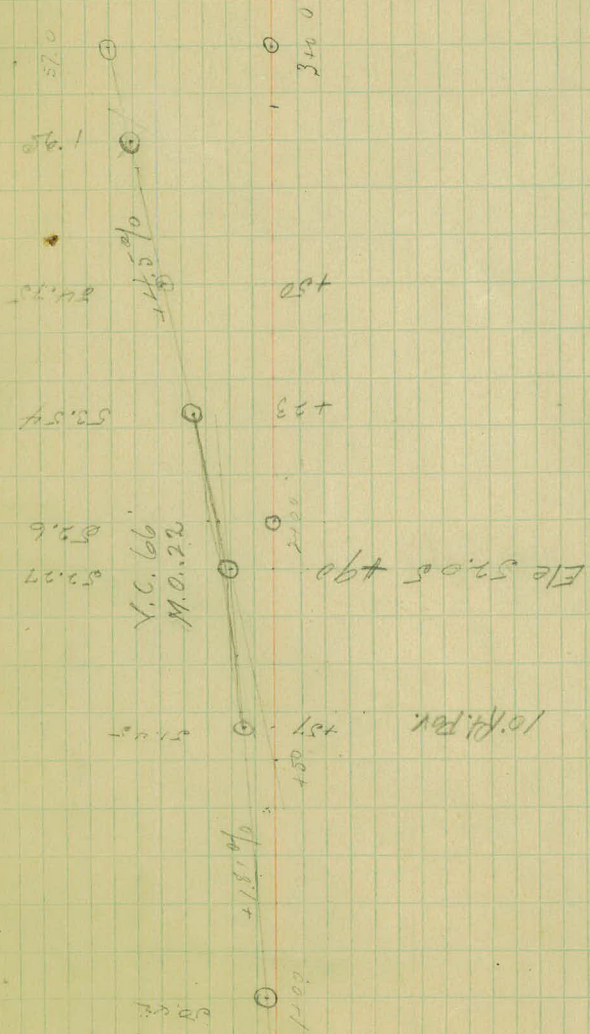
77.10	77.1	77.1	77.1	277.07	723.0
70.1	70.2	70.3	69.5	90.3	65.4
70	6.9	6.8	7.3	209.04	6.9
				330	
				272.34	
				68.2	
				0.1	

708

77.1	77.72		77.59	77.59	77.59
	.62				
	77.34		13.2	71.4	13.5
	0.25			4.2	6.5
	77.59		68.9		
	75.9				
	3.79				

57.0

4.5
13
13.5
0.5
5.5



-

HI

+

20+05

0.86

292,30

15+90

1203

✓278.5

+80

282.94

1.81

✓278.2

+70

✓277.9

+60

✓277.6

+50

✓277.3

+40

✓277.0

+30

✓276.70

+20

✓276.40

+10

✓276.10

15+00

B.M. 292.30 T.P. 35'R

5/ev

B.M 293.42 Nail in T.P. left 36+90

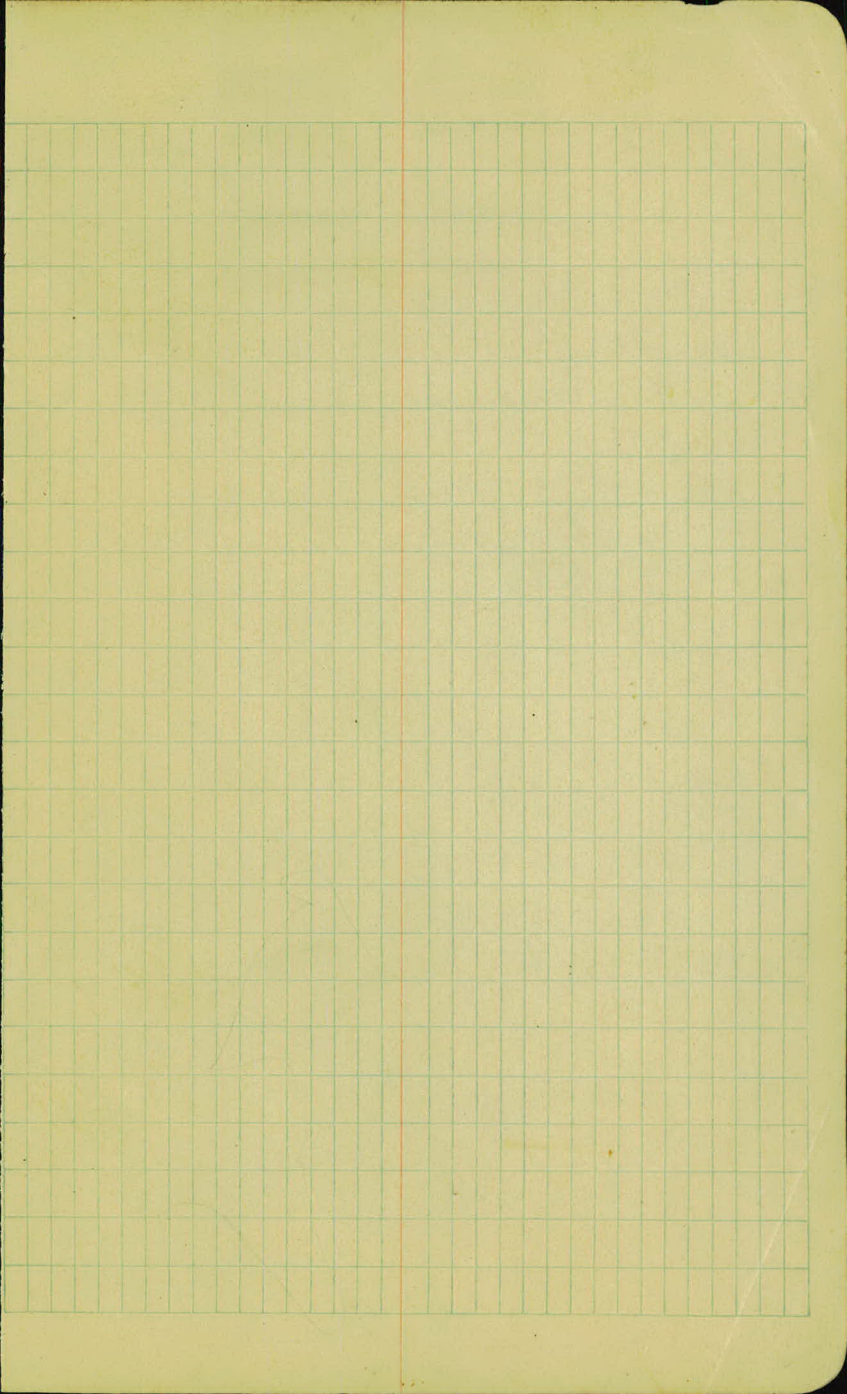
v/ 294.99 v/ v/ E.P. v/ 45+80

W. Rail 290.15

E v/ 290.04

B.M 278.55 Nail in T.P. Right Sta. 57+00

B.M 248.05 Top Hqd Kanpentoon + White Beant Ave



42 466  
30  
00  
50

95.7  
7  
00  
00  
00

25  
35  
120  
10625  
400  
2750  
2750  
2500  
0291750

179060  
 129048  
 ---  
 50° 12'

520  
 358'  
 ---  
 162

50.49  
 50.12  
 ---  
 6.16  
 00.6  
 69

179060  
 50014  
 ---  
 129046

48  
 36'  
 144  
 358 48

26.5  
 21.00  
 ---  
 21.3

520  
 358  
 ---  
 162

472  
 520  
 472  
 ---  
 48

213  
 008  
 ---  
 1702  
 383

57 | 1030  
 57  
 ---  
 460  
 466  
 ---  
 400

5162  
 31  
 ---  
 5120

275.27  
 1.28  
 ---  
 273.99  
 6.59  
 ---  
 280.58  
 1.26  
 ---  
 279.32  
 8.37  
 ---  
 287.69  
 2.61  
 ---  
 285.08  
 8.56  
 ---  
 293.64  
 1.52  
 ---  
 292.12

292.30 B.M.  
 + 1.10  
 ---  
 293.40 H I

- 10.71  
 282.69 17+00 T.P.  
 + 0.59  
 ---  
 283.28 H I

- 11.94  
 271.44 T.P.  
 + 4.61  
 ---  
 276.05 H

0.64  
 275.41 = B.M. 7+75  
 ---  
 276.05

5.28  
 270.77  
 0.29  
 ---  
 271.06  
 11.71  
 ---  
 282.77

25935  
 031  
 ---  
 25966  
 953  
 ---  
 25013  
 2.75  
 ---  
 25286  
 4.69  
 ---  
 248.19

5162  
 383  
 ---  
 51.237

5162  
 17  
 ---  
 51.25

59.66  
 5.04  
 ---  
 54.62

273 Sap Hyd 2arpt White Bear 24800

273  
819

73  
73  
219

1911  
506  
7.45 29  
370 45  
1440 56  
1663 225

3.00 1.75  
8.3  
375  
225  
2.625

53 29  
20  
266 45  
06 56  
33 225

9) 225  
18  
45  
25

9000  
686  
681 427  
157  
50  
9 29

127  
1.27  
889  
254  
177

227  
227  
1569  
45  
1211

3645  
1254  
018 225

1.61 29  
806 45  
322 58  
203 225

457  
5.16 59  
20  
299 29  
259295  
108719  
1.296475

123  
123  
369  
246  
133  
151 29

223  
223  
669  
446  
046

29929  
25  
149645  
598 58  
746 225  
29648  
118 58  
148 225

756 45  
302 58  
376 225

497 29  
25  
2486 45  
99 58

177  
177  
1239  
1739  
177  
3.13 29

277  
277  
1939  
1939  
550  
7.67 29

297.70  
683  
290.81

586 45  
26 58  
78 225  
3686 45  
153 45  
7.91 225

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \times 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.