

WHITE BEAR RD.

Transit

FIELD BOOK

360

KEUFFEL & ESSER CO.

DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

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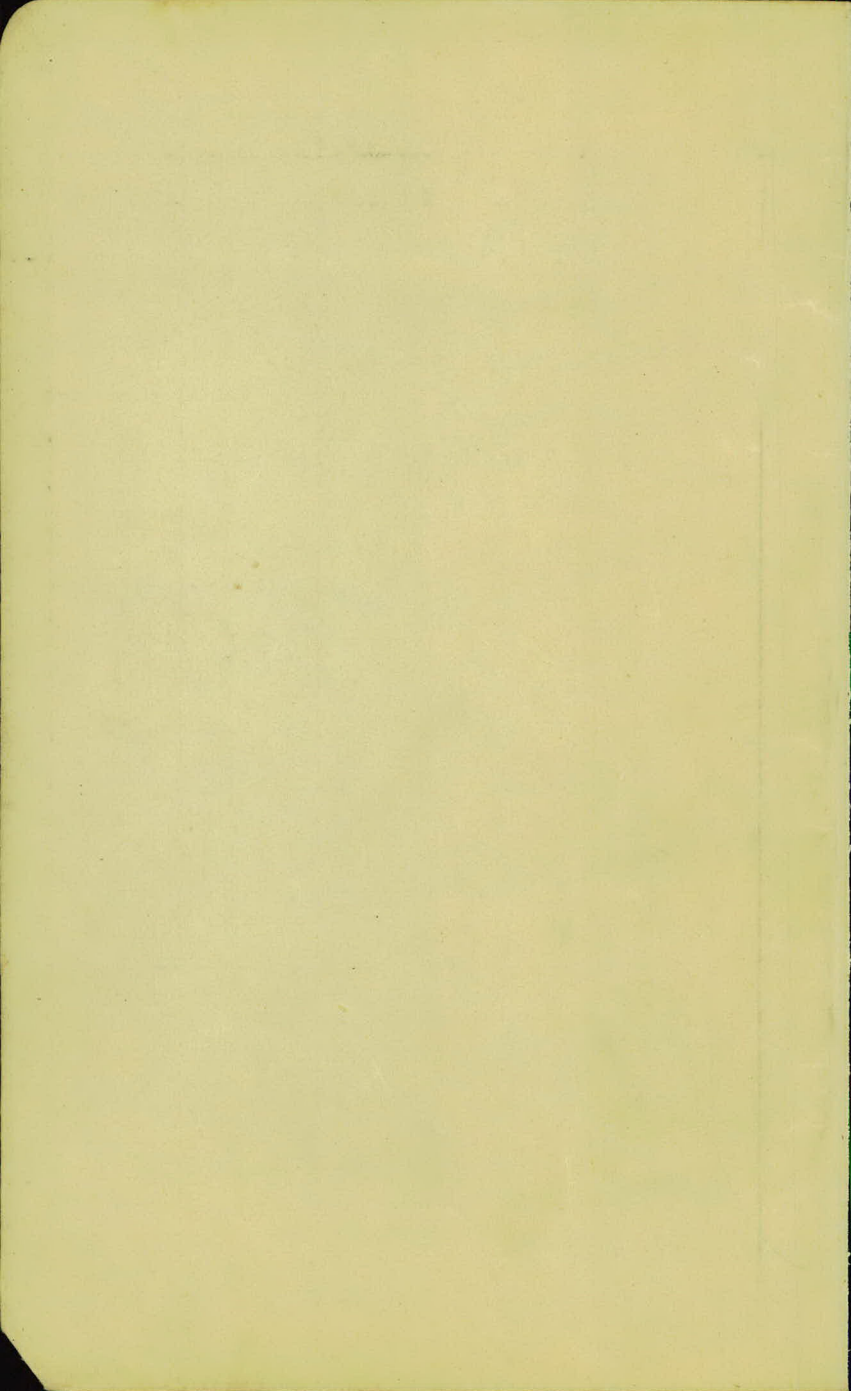
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0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

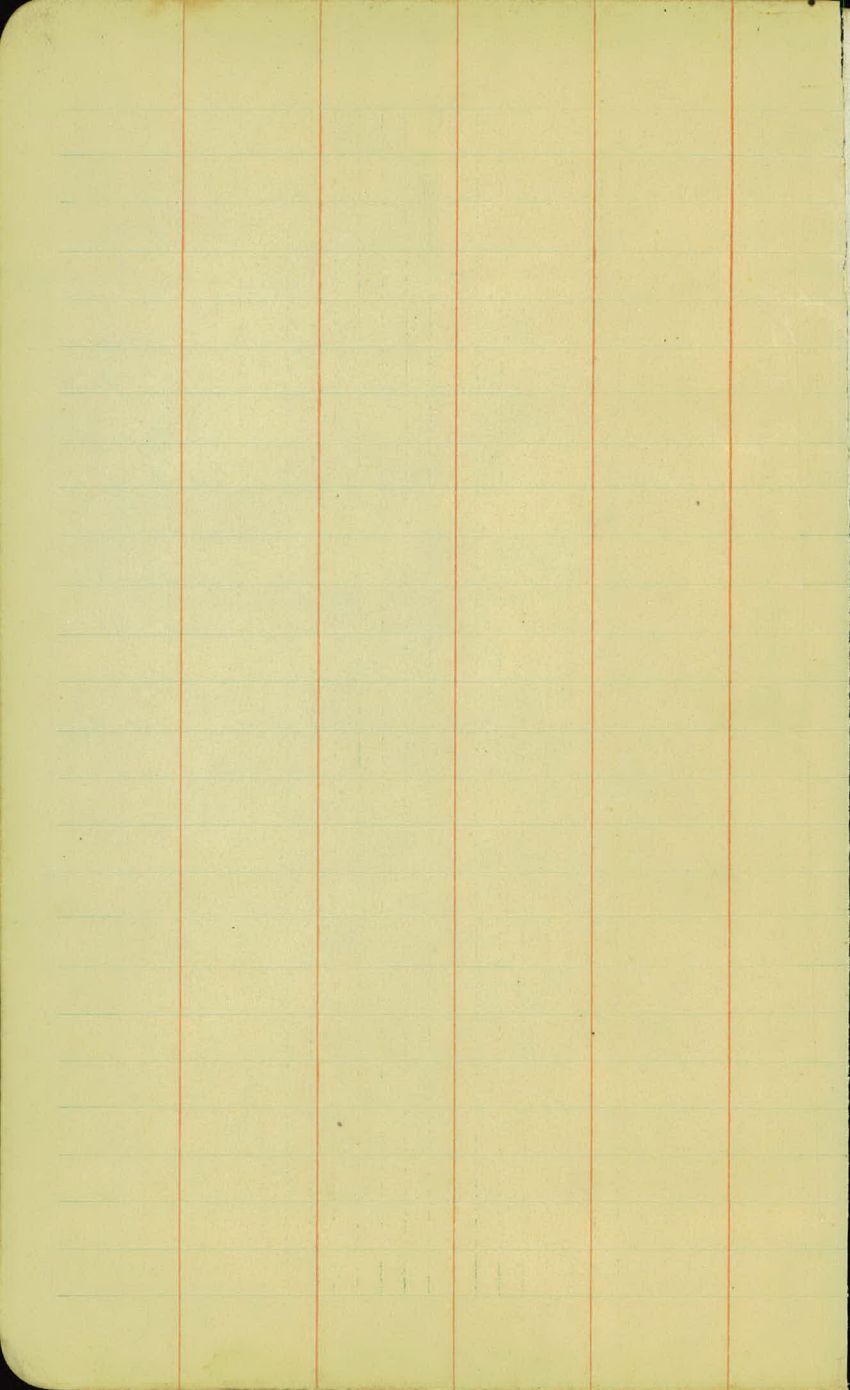
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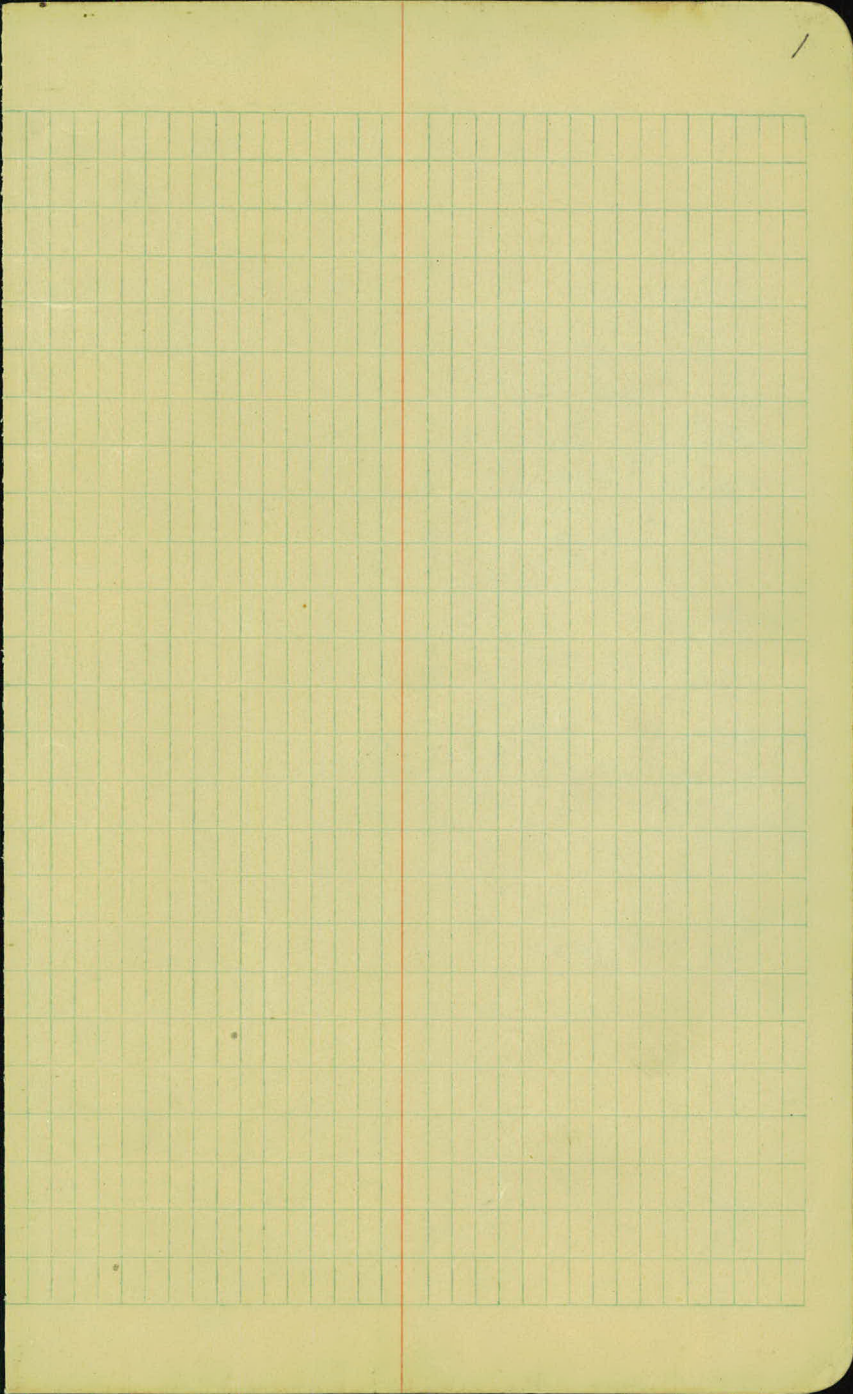
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Page to Page		Description				Sta. to Sta	
2	8	Cross Sections - Original				138	214
9	10	vv	vv	fine	Grading	90	101-174
11	13	vv	vv	vv	vv	77+18	89+67
14	21	vv	vv	vv	vv	165+50	209+75
22	32	vv	vv	vv	vv	27+75	277+68
33	40	Final Topography				277+68	222
42	54	"	"	"	"	208	110
54	61	"	"	"	"	110	0-33





Station	+	H I	-	F.lev	Prof Gaug
135 + 25 B.M.	3.68	249.11 ✓		245.43	4.6
138 + 00				44.7	241.5
+ 60				45.4	
139 + 00				45.5	3.9
140 + 00				46.3	245.7
T.P.	6.83	253.01 ✓	2.93	246.13 ✓	7.26.6 24
140 + 56.2				47.0	246.2
141 + 23.9				47.1	6.3 246.2 1
+ 65				47.3	246.3
142 + 00				47.5	5.7 47.3
143 + 00				48.6	5.0 48.0
T.P.	7.40	258.53 ✓	1.88	251.13 ✓	
+ 70				49.6	
144 + 00				49.9	9.8 49.7
145 + 00				50.1	9.0 49.3
146 + 20 B.M.	7.59	255.90 ✓	10.32 7	249.31	
146 + 00				50.4	6.0 49.7
147 + 00				50.8	5.8 50.1
148 + 00				51.9	4.0 48.8 0 51.1
+ 40				52.2	
+ 53				52.3	
+ 70				52.4	
149 + 00				53.0	3.4 3.6 3.7 52.8
T.P.	7.16	260.20 ✓	2.86	253.04 ✓	
+ 72				53.8	

L E R

2.7	3.6	6.6	7.1	4.6	5.1	4.6	4.4	4.6	5.2	7.5	11.8	12.7	13.4
33.0	30.0	24.5	19.8	15.0	12.0	9.0	4.4	5.0	12.0	19.0	25.0	29.1	33.0
3.0	2.0	4.0	5.2	4.2	4.2	4.2	3.7	4.3	5.1	5.9	7.9		
33.0	25.5	30.0	20.0	14.5	2.0			14.0	17.0	25.0	33.0		
6.2	5.0	3.0	3.0	3.0	3.0	3.0	3.0	3.8	4.7	4.2	2.7	2.6	
33.0	24.0	28.3	12.0	14.5	13.0	9.5	3.0	11.5	14.0	21.0	20.5	33.0	
13.2	9.0	8.0	3.8	3.6	3.8			3.2	3.8	3.7	3.3		
33.0	28.0	23.0	12.0	12.5	14.0			15.0	17.1	29.0	30.0		

12.9	12.1	10.8	6.9	6.0	4.1	7.1	7.7	7.2	6.7	3.8			
33.0	23.4	17.0	12.0	6.0	12.0	15.0	18.0	24.0	30.0	33.0			
6.9	7.7	7.7	7.2	9.2	6.3	6.5	9.0	8.5	8.3	3.2	6.7		
33.0	25.4	19.0	19.0	14.0	11.0	11.0	16.5	19.0	26.0	33.0	33.0		
11.6	6.0	8.6	8.4	6.3	6.2	8.5	8.8	9.4	9.4	9.4			
33.0	21.5	19.0	16.5	12.0	5.7	11.0	13.0	24.0	26.0	33.0			
5.6	5.3	6.5	2.8	6.0	5.7	5.1	5.9	6.5	8.7	9.1	10.7	10.9	
33.0	27.0	22.0	13.0	12.0	6.5	4.4	15.0	12.0	10.4	21.1	24.0	33.0	
4.8	4.7	5.4	5.6	5.6	5.0	4.7	5.0	5.2	6.2	5.7	5.3		
33.0	22.5	23.0	14.9	15.0	13.4	10.0	13.0	16.3	22.0	25.0	33.0		

7.1	6.2	9.2	7.8	9.5	7.1	8.7	11.0	8.7	3.7	3.5			
33.0	23.0	20.5	12.0	12.0	8.9	11.0	14.0	24.5	27.0	22.0	33.0		
7.0	8.4	8.3	8.2	9.4	3.2	8.8	9.1	8.8	8.5	6.0	4.3	3.5	
33.0	28.0	24.0	12.5	11.0	11.0	9.5	13.0	16.5	23.0	25.0	26.5	33.0	
10.5	8.0	9.3	11.0	10.2	3.2	8.4	9.6	8.4	8.1	6.7	6.5		
33.0	26.5	22.0	30.0	17.5	15.0	12.0	15.0	23.5	22.0	25.5	33.0		

9.1	8.5	7.9	6.6	6.2	5.9	6.2	7.8	7.7	7.5	2.0	2.4		
33.0	25.5	18.5	15.0	12.6	7.0	11.0	15.0	18.4	20.5	27.0	23.0		
5.0	4.9	7.3	7.1	7.2	5.5	5.5	5.8	7.0	7.0	6.9	8.5		
33.0	31.0	24.0	22.5	16.1	14.4	12.0	12.0	14.0	17.8	22.5	33.0		
4.3	6.6	6.2	6.2	6.6	4.5	6.9	9.2	9.2	9.2	11.6			
33.0	28.0	18.7	19.0	11.0	11.0	11.0	17.5	23.0	22.0	33.0			

3.9	6.1	6.2	6.2	4.1	4.5	5.7	10.2	10.5					
33.0	30.5	24.0	18.5	12.5	12.0	15.5	26.5	33.0					
4.2	6.4	6.6	6.0	4.2	4.3	5.5	5.5						
33.0	30.0	24.5	18.5	13.6	13.0	22.0	33.0						
4.1	6.7	6.5	4.1		4.0	4.8	5.5						
33.0	30.0	19.5	12.0		13.0	25.0	33.0						
3.2	3.1	5.8	6.1	3.7	3.6	4.9	5.7	5.7	7.9	8.4	8.5		
33.0	31.5	26.0	25.1	19.5	12.0	17.0	25.0	18.0	18.9	23.5	26.0	33.0	

8.0	7.8	8.7	8.4	4.3	7.0	8.3	8.6	7.0	7.2				
33.0	22.5	20.0	16.0	12.0	12.0	17.5	25.5	27.5	33.0				

Station	+	HI	-	Grade	Rod
		260.70			
150+00				54.1	456.7 53.5
+25				54.4	
+35				54.4	
151+00				55.1	528.5 54.7
T.P.	54.9	261.29 ✓	4.41	255.79 ✓	
152+00				56.1	528.9 55.5
153+00				56.2	528.8 55.5
154+00				56.1	6.2
155+00				55.2	55.1 6.4 54.4
B.M.	321	258.41 ✓	6.08	255.20 ✓	
156+00				55.6	3.1 55.3
157+00				56.5	2.4 56.0
T.P.	9.80	266.28 ✓	1.93	256.48 ✓	
+65				57.4	
158+00				57.6	9.8 9.2 57.1
159+00				58.8	8.6 9.0 56.3
160+00				59.7	7.8 7.2 59.1
T.P.	12.56	274.93 ✓	3.91	262.37 ✓	
160+00					158-15.0 59.1
155+25			19.73		
B.M.	6.95	267.15 ✓	?	255.20	
T.P.	8.10	267.60 ✓	2.65	259.50	
+65	8.			59.6	
161+00				59.7	8.5 59.1
+45				59.3	

Station	+	H.I.	-	Grade	Rod.
		267.60			
162+00				58.6	$\frac{9.3}{58.3}$
+60				57.7	
T.P.	2.65	259.61 ✓	10.64	256.96 ✓	
163+00				57.0	$\frac{5.1}{56.5}$
164+00				54.8	$\frac{5.3}{54.0}$
164+55					
B.M.	2.57	257.11 ✓	5.37 ?	254.24 ✓	
165+00				53.4	$\frac{4.3}{52.8}$
+35	± Rd			53.2	
166+00				52.3	$\frac{4.9}{52.2}$
+50				52.5	
167+00				52.7	$\frac{5.0}{52.1}$
+50				52.8	
168+00				52.8	$\frac{5.1}{52.0}$
169+00				52.4	$\frac{5.2}{51.9}$
+35					
T.P.	4.08	255.90 ✓	5.29	251.02 ✓	
170+00				52.1	$\frac{4.1}{51.8}$
171+00				51.4	$\frac{4.2}{51.7}$
172+00				51.3	$\frac{4.2 \ 4.3 \ 4.4}{51.6}$
T.P.	5.93	260.08 ✓	4.75	251.15 ✓	
+50				51.8	$\frac{8.0 \ 8.6 \ 9.2}{51.0}$
173+00				51.7	
+50				51.9	
174+00				52.0	$\frac{2.9 \ 3.7 \ 4.5}{51.0}$
+35				52.2	

A E R

6.3 33.0	6.7 28.0	7.2 25.2	7.7 21.0	8.5 14.0	9.4 13.0	9.9 7.5	9.4 7.5	8.8 11.5	7.6 13.5	8.0 16.0	2.2 28.0	2.1 28.0	X 30.7	1.3 32.0
				11.1 33.0	10.2 24.5	18.5 15.5	9.9 9.0	13.6 12.0	10.0 14.0	10.3 19.0	8.4 21.0	7.7 27.5	6.9 33.0	
5.8 33.0	4.3 29.5	4.0 22.5	X 16.3	8.3 11.4	3.1 2.6	3.1 9.2	3.9 13.0	2.9 17.5	X 20.5	2.6 23.7	2.3 27.0	2.0 27.0	1.0 33.0	
9.8 33.0	7.6 26.0	6.4 21.5	X 16.9	5.7 14.0	5.2 4.6	5.2 6.3	5.4 13.0	2.5 16.5	7.2 19.3	7.0 21.5	5.9 21.5	5.9 33.0		
9.2 33.0	8.7 30.0	7.2 24.0	X 17.6	6.6 16.0	4.3 14.3	4.1 9.5	3.7 15.0	X 17.1	5.0 20.0	5.6 24.8	5.0 24.8	4.2 33.0		
2.6 33.0	5.9 20.0	5.9 20.0	X 17.5	6.7 14.0	6.8 10.5	5.1 8.0	4.9 2.9	4.5 15.0	X 16.5	5.8 23.0	5.7 24.0	3.1 33.0		
4.7 33.0	4.6 28.0	4.5 23.0	X 20.0	5.6 16.5	5.5 12.0	6.1 6.0	5.1 4.1	4.5 3.0	5.1 15.0	5.4 18.5	2.5 21.5	4.9 27.5	3.0 33.0	
3.6 33.0	3.7 22.5	5.5 16.5	X 14.0	5.4 14.0	5.4 12.0	4.3 4.3	4.6 11.0	5.0 11.0	5.0 18.5	2.7 20.0	2.5 26.5	1.1 27.5	1.3 33.0	
2.9 33.0	X 24.9	3.3 22.0	3.3 18.5	4.7 14.0	5.5 10.2	5.1 4.3	5.1 13.5	5.5 17.0	3.9 20.0	3.9 23.5	3.2 24.9	2.9 26.0	3.1 33.0	
5.3 33.0	4.0 26.0	5.2 23.0	X 19.0	6.1 17.8	6.3 12.4	5.6 7.5	5.3 4.7	5.2 10.0	5.4 14.0	6.1 16.5	6.1 17.4	6.3 20.0	5.8 22.0	6.6 33.0
4.0 33.0	4.4 21.0	5.0 21.5	X 19.2	6.3 17.7	6.1 15.5	4.7 12.0	4.1 2.8	4.1 3.2	4.4 11.5	5.8 16.0	6.5 19.5	5.2 23.0	4.5 24.5	5.5 33.0
5.2 33.0	5.8 26.0	7.2 20.5	X 17.5	7.3 17.5	7.0 16.0	5.1 12.5	4.5 4.5	4.6 7.0	5.0 12.5	10.4 21.3	10.9 21.3	3.9 33.0		
3.9 33.0	4.9 28.0	X 20.0	5.0 23.0	6.2 17.0	4.6 13.0	4.6 4.6	4.9 11.0	9.5 16.0	11.3 27.3	12.0 39.0	6.2 18.7			
4.6 33.0	7.4 27.0	7.2 23.0	X 17.0	9.6 17.0	9.6 15.0	6.9 13.0	8.3 8.3	8.7 11.0	8.8 15.0	9.2 17.0	9.6 24.0	11.0 33.0		
3.5 33.0	4.0 29.0	6.6 24.4	X 22.0	8.6 22.0	9.4 18.0	9.5 16.0	9.0 16.5	5.9 11.0	9.7 13.0	8.6 15.5	8.1 24.5	6.1 24.1	7.9 32.0	
4.8 33.0	5.4 23.0	8.8 19.0	X 15.5	8.9 15.5	8.4 13.0	8.2 8.2	8.2 11.0	9.4 13.0	8.1 17.0	7.3 33.0				
4.8 33.0	4.9 26.0	9.2 22.0	X 17.0	9.1 17.0	8.6 13.0	8.1 8.1	8.1 15.0	8.5 24.0	7.8 23.0					
4.2 33.0	4.2 25.0	9.1 20.5	X 13.0	8.7 13.0	8.7 8.7	7.9 7.9	8.4 14.0	8.5 35.0	8.1 33.0					

Station	+	H.I.	-	Grade	Rod
		260.08			
174+48				52.3	4.0 9.8 4.0
175+00				52.4	51.3
T.P.	8.96	261.49 ✓	7.55	252.53 ✓	
+50				52.6	9.5 10.3 - 11.1
176+00				52.6	51.2
+12				52.6	
+50				52.0	8.7 10.5 11.3 51.0
177+00				51.3	10.1 10.9 11.7 50.6
T.P.	8.37	253.91 ✓	10.97	250.52 ✓	
+50				50.1	3.2 4.0 4.8 49.9
178+00				48.7	4.2 5.0 5.8 48.9
179+00				46.1	6.7 7.2 - 7.7 46.1
T.P.	4.16	249.56 ✓	9.21	244.70 ✓	
+45				45.1	
180+00				44.6	5.1 44.5
B.M.			8.32		
180+15	7.81	249.05 ✓	?	241.24 ✓	
181+00				42.9	6.3 42.9
+25				42.2	
182+00				41.3	7.3 41.7
T.P.	3.98	244.61 ✓	8.42	240.63 ✓	
183+00				41.2	3.2 41.4
				41.3	
184+00				41.2	3.7 3.3 41.9
T.P.	9.00	249.43 ✓	4.18	240.43 ✓	

x

L

P

	3.8	4.0	4.7	8.7		8.5	8.6	5.4	5.1
	33.0	21.5	20.0	13.0	7.8	17.0	23.0	27.5	33.0
2.1	1.7	2.5	2.7	8.2	8.6	8.3	8.8	8.8	8.0
33.0	27.1	24.5	19.3	13.0	14.5	17.0	20.0	23.0	21.6
									6.0
									27.5
									33.0

4.8	4.9	4.5	9.9	9.3		9.5	10.0	10.2	8.3
33.0	26.0	15.5	12.0	10.0	8.9	12.5	20.0	28.0	34.0

4.6	4.3	4.4	8.4	10.0		9.3	10.2	10.2	10.7
33.0	28.2	22.0	18.5	14.0	8.9	13.0	23.0	23.8	33.0

4.7	4.2	7.6	10.0	9.7		9.2	10.0	10.8	
33.0	23.0	20.0	16.0	12.5	8.9	12.0	21.0	33.0	

6.2	5.3	23.5	19.0	10.7		10.2	11.2	11.5	11.3
33.0	27.0	4.3	10.5	15.0	9.5	16.0	21.0	27.0	33.0

7.3	7.2	10.5	11.7	11.0		11.0	12.4	12.0	12.8
33.0	25.9	22.5	19.5	14.5	10.2	12.5	17.1	22.0	27.0
									19.6
									33.0

2.7	1.9	2.6	4.8	5.0	4.3	3.8	5.1	5.9	5.0	4.8	3.1
33.0	27.0	25.0	22.5	18.7	20.0	15.5	11.5	17.9	21.5	27.5	33.0

5.3	5.2	6.1	6.3	5.0		6.1	7.3	10.5	11.4	12.4	13.1	15.0
33.0	29.5	34.0	19.2	7.0	5.2	10.0	13.5	20.0	22.5	26.0	29.0	33.0

10.8	10.5	10.2	10.8	8.1		5.2	10.7	12.0	15	13.0	18.1
33.0	26.5	22.3	19.6	14.0	7.8	9.0	13.0	15.0	18.0	25.0	34.0

6.7	7.3	6.0	8.3	5.7	5.1	4.5	8.0	5.6	6.8	9.5	11.3
33.0	28.0	22.5	16.5	14.5	12.0		13.0	17.0	21.5	24.5	33.0

5.9	5.1	5.0	4.8	6.1	5.6	5.1	5.1	5.5	6.4	6.9	8.3
33.0	23.0	20.0	16.0	13.0	12.0	5.0	5.5	14.5	15.0	17.0	33.0

2.5	2.0	2.0	4.3	7.0	6.7	6.3	6.1	6.3	6.7	6.8	6.2	7.2
33.0	27.3	15.5	12.0	8.5	7.0	7.0	7.0	13.0	16.6	20.5	23.5	33.0

2.7	2.4	3.0	7.7	7.3		6.7	7.7	6.8	7.6
33.0	20.5	15.0	8.5	6.5	6.9	7.5	21.5	25.0	33.0

9.6	9.2	9.5	8.5	9.6	8.4		7.3	8.1	8.5	7.6	9.9
33.0	23.0	19.3	13.0	9.5	7.0	7.8	7.0	17.2	22.0	28.0	33.0

8.5	8.0	7.5	4.5		3.4	4.0	9.2	11.5	12.3
33.0	23.8	7.0	10.0	3.4	7.5	15.5	24.0	28.4	33.0

4.4	3.9	4.0	3.0	4.0		4.0	6.2	9.0	10.8	11.9
33.0	26.5	21.0	18.0	13.5	3.3	10.0	15.0	21.0	26.0	33.0

4.3	6.6	7.9	9.3	11.2		4.3	6.6	7.9	9.3	11.2
3.6	10.0	18.0	16.5	23.0	3.6	10.0	18.0	16.5	23.0	30.6



Station	+	H.I.	-	Grade	Rod.
		249.43 ✓			
184+00				41.2	$\frac{7.9 \ 7.5}{41.7}$
+30				41.2	
185+00				41.4	$\frac{7.2 \ 6.6 \ 6.0}{42.8}$
186+00				43.1	$\frac{6.3 \ 5.7 \ 5.1}{43.7}$
+50				44.0	
187+00				44.7	$\frac{5.4 \ 4.8 \ 4.2}{44.6}$
B.M.	10.04	250.26 ✓	9.21 ?	240.22 ✓	
+50				45.3	$\frac{5.4 \ 4.8 \ 4.2}{45.5}$
188+00				45.8	
T.P.	8.05	253.97 ✓	4.34	245.92 ✓	
+50				46.3	
189+00				46.6	$\frac{8.4 \ 7.8 \ 7.2}{46.7}$
+30				47.0	
+50				47.2	
190+00				47.8	$\frac{7.5 \ 6.9 \ 6.3}{47.1}$
+25				48.3	
T.P.	6.13	254.32 ✓	5.18	248.19 ✓	
+50				48.2	
191+00				48.6	$\frac{6.9 \ 6.3 \ 5.7}{48.0}$
+50				49.1	
192+00				49.2	$\frac{5.5 \ 5.4 \ 5.3}{48.9}$
193+00				50.1	$\frac{4.5}{48.8}$
193+15					
B.M.	6.33	256.23 ✓	4.42	249.90 ✓	
194+00				51.2	$\frac{5.7}{50.5}$

Station	+	H. I.	-	Grade	Grade To
		256.23			5.5
195+00				51.8	50.
196+00				51.6	5.
201+90			8.59		
B.M.	5.68	253.32 ✓	?	247.64 ✓	
197+00				51.0	2.4
198+00				50.2	50.4
199+00				49.5	3.0
200+00				48.2	50.3
201+00				47.4	3.9
202+00				46.9	4.5
B.M.	4.75	252.39 ✓	5.68	247.64 ✓	5.0
203+00				47.0	18.3
204+00				47.6	6.1
205+00				47.9	4.2
206+00				49.2	4.7
207+00				50.2	6.4
T.P.	9.37	260.02 ✓	1.74	250.65 ✓	26.7
208+00				51.6	5.6
209+00				53.5	46.3
+50				54.3	5.1
210+00				55.4	47.3
+30					4.6
B.M.	9.19	268.80 ✓	0.41	259.61 ✓	47.8
211+00				57.1	3.8
+50				57.8	50.0
212+00				58.8	2.4
					50.0
					12.3
					56.5
					10.6
					58.2

Station	+	H.I.	-	Grade	Red
		268.80			
212+30				59.3	
213+00				60.2	$\frac{9.2}{57.6}$
+50				60.3	
214+00				60.3	$\frac{1.6}{60.2}$

h E P

4.2	4.1	7.9	10.3	11.0	9.8		9.7	8.4	8.1	8.0	8.3
23.0	27.5	25.0	21.0	16.0	8.0	7.5	11.0	20.0	24.5	27.0	23.0
5.2	4.9	10.6	10.6	9.7	9.2	8.8	9.2	8.9	6.6	4.1	4.7
23.0	27.3	24.5	16.0	13.0	7.6	6.5	7.0	15.0	22.0	26.0	23.0
	5.8	6.1	7.9	9.1	8.6		8.9	7.9	5.9		
	33.0	24.5	19.0	13.5	8.0	8.5	12.5	17.0	23.0		
6.5	6.3	6.3	8.7	9.1	8.6		8.6	8.4	7.2	7.0	6.1
33.0	25.3	24.0	17.0	16.0	6.7	8.5	10.5	15.0	23.5	22.6	23.0

X sections for fine grading
 Station 90 - 101 + 74.3

Station					
B.M.	3.56	239.16			235.60
90+00				234.40	4.75
+25				34.35	4.80
+50				34.25	4.90
+75				34.20	4.95
91+00				34.10	5.05
+25				34.05	5.10
+50				33.95	5.20
+75				33.90	5.25
92+00				33.80	5.35
+25				33.70	5.45
+50				33.60	5.55
+75				33.45	5.70
93+00				33.30	5.85
+25				33.15	6.00
+50				32.95	6.20
+75				32.75	6.40
94+00				32.50	6.65
T.P.	3.00	235.50	6.66	237.50	
+25				32.25	3.25
+50				32.00	3.50
+75				31.75	3.75
95+00				31.50	4.00
+25				31.25	4.25
+50				31.05	4.45

h £ P

4.70 +0.15
 12.0
 4.55 +0.05
 4.85 +0.05
 12.00
 5.05 0.0
 12.0

5.00 +0.15
 12.0
 5.05 +0.15
 12.0

5.15 +0.15
 12.0

5.30 +0.05
 12.0

5.50 -0.05
 12.0

5.70 -0.15
 12.0

5.95 -0.3
 12.0

6.05 -0.25
 12.0

6.25 -0.3
 12.0

6.40 -0.3
 12.0

6.50 -0.2
 12.0

6.70 -0.2
 12.0

7.05 -0.3
 12.0

3.5 -0.15
 12.0

3.75 -0.15
 12.0

4.05 -0.2
 12.0

4.2 -0.1
 12.0

4.4 -0.05
 12.0

4.55 0.0
 12.0

4.65 +0.1
 12.0

4.70 +0.1
 12.0

4.80 +0.1
 12.0

5.05 +0.1
 12.0

4.95 +0.1
 12.0

4.95 +0.15
 12.0

5.05 +0.15
 12.0

5.20 +0.05
 12.0

5.30 +0.05
 12.0

5.45 -0.2
 12.0

5.90 -0.35
 12.0

6.05 -0.35
 12.0

6.00 -0.15
 12.0

6.15 -0.15
 12.0

6.25 -0.05
 12.0

2/00 6.25 +0.05
 12.0

6.25 0.0
 12.0

3.40 -0.15
 12.0

3.6 -0.1
 12.0

3.85 -0.1
 12.0

4.0 0.0
 12.0

4.2 +0.05
 12.0

4.4 +0.05
 12.0

4.6 +0.25
 12.0

4.6 +0.3
 12.0

4.65 +0.35
 12.0

4.80 +0.25
 12.0

4.85 +0.3
 12.0

4.75 +0.45
 12.0

5.15 +0.15
 12.0

5.25 +0.1
 12.0

5.40 +0.05
 12.0

5.60 -0.05
 12.0

5.70 -0.05
 12.0

5.80 0.0
 12.0

6.00
 12.0

6.20
 12.0

6.40
 12.0

6.60
 12.0

6.55
 12.0

8/00 +0.05 3.70
 12.0

-0.1 3.7
 12.0

-0.1 3.95
 12.0

-0.05 4.15
 12.0

0.0 4.35
 12.0

+0.2 4.35
 12.0

Station	+	H.I.	-	Grade
		235.50		
95+75				30.90 4.60
96+00				30.70 4.80
+25				30.60 4.90
+50				30.50 5.00
+75				30.50 5.00
97+00				30.40 5.10
+25				30.40 5.10
+50				30.35 5.15
+75				30.35 5.15
98+00				30.30 5.20
+25				30.30 5.20
+50				30.25 5.25
+75				30.25 5.25
98+96:				30.20 5.30
99+33.5				30.15 5.35
+71:				30.15 5.35
100+08.5				30.10 5.40
T.P.	4.39	234.59	5.30	230.20
+46.5				30.05 4.55
+75				30.05 4.55
101+00				30.00 4.60
+36.8				29.95 4.65
+74.8				29.95 4.65

h

L

R

	$\frac{4.20}{12.0} 0.0$		-0.1		$+0.25 \frac{4.25}{12.0}$	
	$\frac{5.00}{12.0} -0.1$		$\frac{4}{00} 4.7$	$\frac{3}{00} +0.95$	$+0.35 \frac{4.55}{12.0}$	
	$\frac{5.15}{12.0} -0.15$		$\frac{4}{00} 4.75$	$+0.15$	$+0.30 \frac{4.70}{12.0}$	
	$\frac{5.15}{12.0} -0.4$		$\frac{3}{00} 4.90$	$+0.1$	$+0.35 \frac{4.75}{12.0}$	
	$\frac{5.0}{12.0} +0.1$		$+0.05$		$+0.2 \frac{4.90}{12.0}$	
	$\frac{5.55}{12.0} +0.15$		4.95	$+0.05$	$+0.25 \frac{4.95}{12.0}$	
	$\frac{5.2}{12.0} 0.0$		5.05	-0.1	$+0.15 \frac{5.05}{12.0}$	
	$\frac{5.15}{12.0} +0.1$		5.20	$\frac{4}{00} -0.05$	$+0.15 \frac{5.1}{12.0}$	
	$\frac{5.30}{12.0} +0.05$	$\frac{4}{00}$	5.2	$\frac{3}{00} 0.0$	$+0.2 \frac{5.05}{12.0}$	
	$\frac{5.2}{12.0} +0.1$		5.15	0.0	$+0.25 \frac{5.05}{12.0}$	
	$\frac{5.25}{12.0} +0.05$		5.2	$+0.05$	$+0.15 \frac{5.15}{12.0}$	
	$\frac{5.25}{12.0} +0.1$		5.15	0.0	$+0.2 \frac{5.15}{12.0}$	
	$\frac{5.35}{12.0} 0.0$		5.25	-0.05	$-0.2 \frac{5.55}{12.0}$	
	$\frac{5.40}{12.0} 0.0$		5.30	-1.0	$+0.05 \frac{5.35}{12.0}$	
(5.30)	$\frac{5.3}{10.0} 0.0$		5.4	0.0	$\frac{7}{00} -0.05 \frac{5.5}{10.0}$	(5.45)
(5.15)	$\frac{5.4}{10.0} -0.25$		5.35	-0.05	$+0.05 \frac{5.5}{10.0}$	(5.55)
(5.10)	$\frac{5.15}{10.0} -0.05$		5.40	-0.05	$\frac{5}{00} -0.05 \frac{5.75}{10.0}$	(5.70)
(4.10)	$\frac{4.15}{10.0} -0.05$		5.45	-0.1	$+0.15 \frac{4.55}{10.0}$	(5.00)
(4.10)	$\frac{4.20}{10.0} -0.1$		4.65	$\frac{4}{00} -0.15$	$\frac{8}{00} +0.05 \frac{4.55}{10.0}$	(5.00)
(4.15)	$\frac{4.35}{10.0} -0.2$		4.70	0.0	$+0.12 \frac{4.85}{10.0}$	(5.05)
(4.20)	$\frac{4.45}{10.0} -0.25$		4.08	$+0.1$	$+0.25 \frac{4.85}{10.0}$	(5.10)
(4.35)	$\frac{4.80}{10.0} +0.05$	$\frac{3}{00}$	4.55	$+0.15$	$+0.15 \frac{4.80}{10.0}$	(4.95)
			4.50			

X sections - a fine gradient
 Sta. - 77+18.5 - 89+67.25

Station	+	H. I.	-	Elevation
B.M.	2.11	252.77		250.66
77+18.5				245.9
+43.6				46.5
+68.6				46.9
+93.6				47.35
78+25				47.70
+50				47.90
+75				48.00
79+00				48.00
+25				47.95
+50				47.90
+90				47.80
80+13				47.75
+43				47.70
+75				47.65
81+00				47.60
+25				47.55
+50				47.50
+75				47.45
82+00				47.40
T.P.	2.64	250.71	4.70	248.07
+25				47.35
+50				47.30
+75				47.25
83+00				47.20

h £ p

7.05	-0.2		+0.2		+0.15
6.35	7.25 10.0	$\frac{5}{00}$	6.65		6.50 10.0
5.95	6.30 10.0	+0.15	+0.05		-0.05
	5.90 10.0	+0.05	6.20 10.0	$\frac{5}{00}$	6.20 10.0
	5.70 10.0	-0.2	+0.05		5.70 10.0
	5.00 10.0	+0.15	$\frac{2}{00}$	$\frac{3}{00}$	5.60 10.0
	5.10 10.0	-0.15	5.35 10.0	$\frac{3}{00}$	5.30 10.0
	5.05 10.0	-0.2	4.90 10.0	$\frac{5}{00}$	5.15 10.0
	4.90 10.0	-0.05	-0.05		5.15 10.0
	5.0 10.0	-0.1	-0.2		5.2 10.0
	4.95 10.0	$\frac{0.0}{00}$	4.95		5.10 10.0
	5.05 10.0	-	4.90		4.95 10.0
	4.90 10.0	+0.2	5.10		5.25 10.0
5.15	5.10 10.0	+0.15	$\frac{3}{00}$	5.10 10.0	5.05 10.0
5.25	5.15 10.0	+0.1	$\frac{3}{00}$	5.15 10.0	5.05 10.0
5.35	5.05 10.0	+0.3	4.90 10.0	+0.2	5.00 10.0
5.40	5.15 10.0	-0.1	5.0 10.0	+0.15	5.00 10.0
5.45	5.20 10.0	+0.25	5.0 10.0	+0.2	5.00 10.0
5.50	5.30 10.0	+0.3	5.1 10.0	+0.15	5.00 10.0
5.55	5.30 10.0	+0.25	5.1 10.0	+0.2	5.00 10.0
			5.7	+0.05	5.00 10.0
3.55	3.55	0.0	5.35	0.0	5.00 10.0
3.60	3.7	-0.1	3.7	0.0	5.00 10.0
3.65	3.75	-0.1	3.7	+0.15	5.00 10.0
3.70	3.70	-0.1	3.8	+0.15	5.00 10.0
			3.35		5.00 10.0

6.65

6.15

5.85

5.05

4.95

4.95

5.00

5.10

5.15

5.05

5.05

4.95

4.95

5.00

5.05

5.10

5.15

3.15

3.20

3.25

3.30

Station	+	H.I.	-	Grade
		250.71		
83+25				47.10 3.60
+ 50				46.90 3.80
+ 75				46.65 4.05
84+00				46.30 4.40
+ 25				45.85 4.85
+ 50				45.30 5.40
+ 75				44.70 6.00
85+00				44.00 6.70
+ 25				43.25 7.45
+ 50				42.50 8.20
+ 75				41.75 8.95
86+00				41.00 9.70
+ 25				40.25 10.45
+ 50				39.50 11.20
+ 75				38.75 11.95
87+00				38.00 12.70
T.P	182	240.34	12.19	238.52
+ 25				37.30 3.05
+ 50				36.70 3.65
+ 75				36.00 4.35
88+00				35.80 4.55
+ 25				35.55 4.80
+ 50				35.35 5.00
+ 75				35.25 5.10

h c P

3.80/	$\frac{3.85}{10.0} - 0.05$	-0.05	-0.1	$\frac{3.3}{10.0}$	3.4
4.00/	$\frac{4.10}{10.0} - 0.1$	+0.05	+0.2	$\frac{3.4}{10.0}$	3.6
4.25/	$\frac{4.40}{10.0} - 0.15$	$\frac{3}{00}$ 3.75	+0.05	$\frac{3.8}{10.0}$	3.85
4.60/	$\frac{4.70}{10.0} - 0.1$	4.10	-0.05	$\frac{4.10}{10.0}$	4.20
5.05/	$\frac{5.2}{10.0} - 0.15$	$\frac{3}{00}$ 4.35	+0.05	$\frac{4.40}{10.0}$	4.65
5.60/	$\frac{5.80}{10.0} - 0.2$	4.9	-0.05	$\frac{4.65}{10.0}$	5.20
6.20/	$\frac{6.35}{10.0} - 0.15$	5.5	-0.1	$\frac{5.35}{10.0}$	5.80
6.90/	$\frac{6.95}{10.0} - 0.05$	6.2	-0.2	$\frac{6.10}{10.0}$	6.50
7.65/	$\frac{7.70}{10.0} - 0.05$	6.75	-0.05	$\frac{6.65}{10.0}$	7.25
8.40/	$\frac{8.35}{10.0} + 0.05$	7.1	-0.05	$\frac{7.35}{10.0}$	8.00
9.15/	$\frac{8.95}{10.0} + 0.2$	8.15	+0.05	$\frac{8.1}{10.0}$	8.75
9.90/	$\frac{9.75}{10.0} + 0.15$	8.9	+0.05	$\frac{8.9}{10.0}$	9.50
10.65/	$\frac{10.75}{10.0} - 0.1$	9.6	+0.1	$\frac{9.55}{10.0}$	10.25
11.40/	$\frac{11.0}{10.0} 0.0$	10.35	+0.1	$\frac{10.35}{10.0}$	11.00
12.15/	$\frac{12.05}{10.0} + 0.1$	11.2	0.0	$\frac{11.1}{10.0}$	11.75
13.90/	$\frac{12.65}{10.0} + 0.25$	11.95	0.0	$\frac{11.8}{10.0}$	12.50
		12.45	+0.25	$\frac{12.3}{10.0}$	
3.25/	$\frac{2.8}{10.0} + 0.45$	2.7	+0.35	$\frac{2.55}{10.0}$	2.85
3.85/	$\frac{3.6}{10.0} + 0.25$	3.1	+0.25	$\frac{3.25}{10.0}$	3.45
(4.55)	$\frac{4.4}{10.0} + 0.15$	4.1	+0.25	$\frac{4.0}{10.0}$	4.15
4.75/	$\frac{4.2}{10.0} - 0.15$	4.6	-0.5	$\frac{4.5}{10.0}$	4.35
(5.00)	$\frac{5.25}{10.0} - 0.25$	5.1	-0.3	$\frac{4.9}{10.0}$	4.60
(5.20)	$\frac{5.45}{10.0} - 0.25$	5.35	-0.35	$\frac{5.05}{10.0}$	4.80
(5.30)	$\frac{5.7}{10.0} - 0.40$	5.5	-0.40	$\frac{5.3}{10.0}$	4.90

Station	+	H.I.	-	Grade
		240.34		
88 + 9.2				35.30 5.05
89 + 11				34.65 5.70
+ 37.25				34.60 5.75
+ 67.25				34.50 5.85

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(5.25)

5.80/

5.85/

$\frac{5.85}{10.0} - 0.6$

$\frac{5.90}{75.0} - 0.1$
 $\frac{8}{00}$

$\frac{5.90}{70.0} - 0.05$
 $\frac{8}{00}$

$\frac{6.00}{70.0} - 0.05$
 $\frac{7}{00}$

-0.3
5.35

+0.2
5.5

+0.15
5.6

+0.1
5.75

-0.5
 $\frac{5.35}{10.0}$

+0.1
 $\frac{5.50}{70.0}$

+0.05
 $\frac{5.45}{10.0}$

$\frac{5.6}{10.0}$

(4.88)

5.60

5.70

+0.15

X sections for fine grading
 Sta. 165+50 — 209+75

Station	+	#I.	-	Elev.	
B.M.	267	256.83		254.16	
165+50				52.40	4.45
+75				52.20	4.65
166+00				52.20	4.65
+25				52.20	4.65
+50				52.15	4.70
+75				52.15	4.70
167+00				52.10	4.75
+25				52.10	4.75
+50				52.05	4.80
+75				52.05	4.80
168+00				52.00	4.85
+25				52.00	4.85
+50				51.95	4.90
+75				51.95	4.90
169+00				51.90	4.95
+25				51.90	4.95
+50				51.85	5.00
+75				51.85	5.00
170+00				51.80	5.05
T.P.	4.51	256.36	4.99	251.85	
+25				51.80	4.55
+50				51.75	4.60
+75				51.75	4.60
171+00				51.70	4.65

5
 24.62
 15.1
 9.52

h.

£

P

$\frac{4.75}{10.0}$	-0.2	-0.05	0.0
$\frac{4.75}{10.0}$	0.0	4.5	$\frac{4.55}{10.0}$
$\frac{4.75}{10.0}$	0.0	-0.2	-0.2 $\frac{4.95}{10.0}$
$\frac{4.9}{10.0}$	-0.15	-0.2	-0.1 $\frac{4.85}{10.0}$
$\frac{4.9}{10.0}$	-0.15	4.75	0.0 $\frac{4.75}{10.0}$
$\frac{5.1}{10.0}$	-0.3	-0.05	-0.05 $\frac{4.85}{10.0}$
$\frac{5.2}{10.0}$	-0.4	-0.15	-0.15 $\frac{4.95}{10.0}$
$\frac{5.0}{10.0}$	-0.15	-0.25	-0.05 $\frac{4.90}{10.0}$
$\frac{4.95}{10.0}$	-0.1	-0.1	+0.05 $\frac{4.85}{10.0}$
$\frac{4.9}{10.0}$	0.0	0.0	+0.1 $\frac{4.8}{10.0}$
$\frac{5.0}{10.0}$	-0.1	-0.05	+0.1 $\frac{4.8}{10.0}$
$\frac{5.0}{10.0}$	-0.05	-0.15	+0.05 $\frac{4.9}{10.0}$
$\frac{5.0}{10.0}$	-0.05	-0.15	-0.05 $\frac{5.0}{10.0}$
$\frac{5.1}{10.0}$	-0.1	-0.2	0.0 $\frac{5.0}{10.0}$
$\frac{5.2}{10.0}$	-0.5	-0.3	-0.2 $\frac{5.2}{10.0}$
$\frac{5.25}{10.0}$	-0.2	-0.3	-0.25 $\frac{5.3}{10.0}$
$\frac{5.35}{10.0}$	-0.3	-0.2	-0.2 $\frac{5.25}{10.0}$
$\frac{5.3}{10.0}$	-0.2	-0.1	-0.1 $\frac{5.30}{10.0}$
$\frac{5.25}{10.0}$	-0.15	0.0	+0.1 $\frac{5.10}{10.0}$
$\frac{5.25}{10.0}$	-0.1	-0.15	-0.05 $\frac{5.2}{10.0}$
$\frac{4.95}{10.0}$	-0.3	-0.3	-0.15 $\frac{4.8}{10.0}$
$\frac{4.95}{10.0}$	0.25	-0.1	-0.25 $\frac{4.95}{10.0}$
$\frac{4.95}{10.0}$	-0.25	-0.2	-0.25 $\frac{4.95}{10.0}$
$\frac{5.0}{10.0}$	-0.25	-0.15	-0.15 $\frac{4.9}{10.0}$

Station	+	H.I.	-	Elev.
		256.86		
171 + 35				51.65 4.70
+ 68 65				51.65 4.70
+ 93 65				51.60 4.75
172 + 18 65				51.60 4.75
+ 43 65				51.55 4.80
+ 68 65				51.55 4.80
+ 93 65				51.50 4.85
B.M.	3.91	256.14		252.29
172 + 18 65				51.50 4.65
+ 43 65				51.45 4.70
+ 70				51.45 4.70
174 + 00				51.40 4.75
+ 25				51.40 4.75
+ 50				51.35 4.80
+ 75				51.35 4.80
175 + 00				51.30 4.85
+ 25				51.30 4.85
+ 50				51.25 4.90
+ 75				51.25 4.90
176 + 00				51.20 4.95
+ 25				51.15 5.00
+ 50				51.00 5.15
+ 75				50.80 5.35
177 + 00				50.60 5.55

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	$\frac{5.10}{10.0} - 0.2$			-0.15		-0.15	$\frac{4.95}{10.0}$	
	$\frac{5.05}{10.0} - 0.25$			-0.35		-0.3	$\frac{5.1}{10.0}$	
4.70	$\frac{5.00}{10.0} - 0.3$			-0.15		-0.15	$\frac{5.0}{10.0}$	4.85
4.65	$\frac{4.9}{10.0} - 0.15$			-0.05		-0.1	$\frac{4.95}{10.0}$	4.65
4.60	$\frac{4.7}{10.0} - 0.1$			$+0.05$		-0.05	$\frac{5.05}{10.0}$	5.00
4.55	$\frac{4.6}{10.0} - 0.05$		$\frac{4}{00}$	0.00		-0.1	$\frac{5.10}{10.0}$	5.05
4.50	$\frac{4.6}{10.0} - 0.1$			-0.05		0.0	$\frac{5.2}{10.0}$	5.20
4.20	$\frac{4.35}{10.0} - 0.15$			-0.05		-0.05	$\frac{5.15}{10.0}$	5.10
4.15	$\frac{4.30}{10.0} - 0.05$			$+0.1$		$+0.1$	$\frac{5.15}{10.0}$	5.25
4.15	$\frac{4.25}{10.0} - 0.1$		$\frac{4}{00}$	$+0.05$		$+0.05$	$\frac{5.2}{10.0}$	5.25
4.20	$\frac{4.3}{10.0} - 0.1$			-0.1		0.0	$\frac{5.3}{10.0}$	5.30
4.20	$\frac{4.35}{10.0} - 0.15$		$\frac{4}{00}$	$+0.1$		0.0	$\frac{5.3}{10.0}$	5.30
4.25	$\frac{4.30}{10.0} + 0.05$			$+0.15$		$+0.1$	$\frac{5.35}{10.0}$	5.35
4.25	$\frac{4.30}{10.0} + 0.05$			$+0.15$		$+0.2$	$\frac{5.15}{10.0}$	5.35
4.30	$\frac{4.40}{10.0} - 0.1$		$\frac{7}{00}$	$+0.15$		$+0.1$	$\frac{5.3}{10.0}$	5.40
4.30	$\frac{4.5}{10.0} - 0.12$		$\frac{2}{00}$	$+0.05$		$+0.1$	$\frac{5.3}{10.0}$	5.40
4.35	$\frac{4.50}{10.0} - 0.15$			0.0		$+0.05$	$\frac{5.4}{10.0}$	5.45
4.35	$\frac{4.4}{10.0} - 0.05$		$\frac{9}{00}$	$+0.2$		$+0.05$	$\frac{5.4}{10.0}$	5.45
4.40	$\frac{4.5}{10.0} - 0.1$		$\frac{4}{00}$	$+0.05$		$+0.05$	$\frac{5.45}{10.0}$	5.50
4.45	$\frac{4.50}{10.0} - 0.05$		$\frac{5}{00}$	$+0.05$		0.0	$\frac{5.5}{10.0}$	5.55
4.60	$\frac{4.6}{10.0} 0.0$			$+0.1$		0.0	$\frac{5.7}{10.0}$	5.70
4.80	$\frac{4.95}{10.0} - 0.15$		$\frac{3}{00}$	$+0.05$		$+0.05$	$\frac{5.15}{10.0}$	5.90
5.00	$\frac{5.10}{10.0} - 0.1$		$\frac{4}{00}$	$+0.05$		$+0.2$	$\frac{5.90}{10.0}$	6.10

Station	+	H.I.	-	Grade
		256.14		
177+25				50.30 5.85
+50				49.85 6.30
+75				49.45 6.70
178+00				48.90 7.25
+37 ⁵⁵				48.05 8.10
+62 ⁵⁵				47.50 8.65
B.M	1.86	249.05		241.19
+97 ⁵⁵				46.95 2.10
179+12 ⁵⁵				46.40 2.65
+50				45.60 3.45
+75				45.05 4.00
180+00				44.50 4.55
B.M	7.62	248.81		241.19
+35				43.95 4.85
+50				43.50 5.30
+75				43.05 5.75
181+00				42.70 6.10
+25				42.35 6.45
+50				42.05 6.75
+75				41.85 6.95
182+00				41.65 7.15
+25				41.50 7.30
+50				41.40 7.40
+75				41.40 7.40

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5.30	$\frac{5.50}{10.0} - 0.2$	$\frac{2}{00}$	$\frac{10.05}{5.8}$	+0.2	$\frac{6.20}{10.0}$	6.40
5.75	$\frac{6.00}{10.0} - 0.25$		0.0	-0.1	$\frac{6.95}{10.0}$	6.85
6.15	$\frac{6.55}{10.0} - 0.4$		6.3	-0.15	$\frac{7.4}{10.0}$	7.25
6.70	$\frac{7.10}{10.0} - 0.4$		6.85	-0.35	$\frac{8.10}{10.0}$	7.80
7.55	$\frac{7.90}{10.0} - 0.35$		7.60	-0.45	$\frac{9.0}{10.0}$	8.65
8.20	$\frac{8.75}{10.0} - 0.55$		8.55	-0.55	$\frac{9.6}{10.0}$	9.10
1.75	$\frac{2.20}{10.0} - 0.45$			-0.4	$\frac{2.45}{10.0}$	2.45
2.40	$\frac{2.75}{12.0} - 0.35$		2.65	-0.4	$\frac{3.55}{12.0}$	2.90
3.30	$\frac{3.90}{13.0} - 0.6$		3.25	-0.6	$\frac{4.20}{12.0}$	3.60
3.95	$\frac{4.20}{13.0} - 0.25$		3.85	-0.15	$\frac{4.4}{12.0}$	4.10
4.60	$\frac{4.8}{12.0} - 0.2$		4.15	-0.15	$\frac{4.8}{12.0}$	4.65
	$\frac{4.95}{10.0} 0.0$		4.6	+0.1	$\frac{4.85}{10.0}$	
	5.3 +0.1		5.2	+0.1	$\frac{5.4}{10.0}$	
	5.65 +0.2		5.55	+0.2	$\frac{5.6}{10.0}$	
	6.05 +0.15		6.0	+0.1	$\frac{6.0}{10.0}$	
	6.5 +0.05		6.45	0.0	$\frac{6.5}{10.0}$	
	6.85 0.0		6.75	0.0	$\frac{6.85}{10.0}$	
	7.1 -0.05		7.05	-0.1	$\frac{7.1}{10.0}$	
	7.25 0.0		7.25	-0.1	$\frac{7.25}{10.0}$	
	7.3 +0.1		7.35	-0.05	$\frac{7.3}{10.0}$	
	7.5 0.0	$\frac{4}{00}$	7.45	-0.05	$\frac{7.55}{10.0}$	
	7.7 +0.1		7.35	+0.05	$\frac{7.25}{10.0}$	

Station	+	H.I.	-	Grade
		248.91		
183+06				41.40 7.40
+43 ⁵				41.55 7.25
+81.0				41.75 7.05
184+18 ⁵				42.05 6.75
B.M.	9.32	249.49		240.17
+56.0				42.40 7.10
+75				42.60 6.90
185+00				42.80 6.70
+25				43.05 6.45
+50				43.25 6.25
+75				43.50 6.00
186+00				43.70 5.80
+25				43.95 5.55
+50				44.15 5.35
+75				44.40 5.10
187+00				44.60 4.90
+25				44.85 4.65
+50				45.05 4.45
+75				45.30 4.20
188+00				45.50 4.00
+25				45.70 3.80
+50				45.85 3.65
+75				46.05 3.45
189+00				46.20 3.30

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	$\frac{7.5}{10.0} \quad 0.0$		0.0	$+0.3$	$\frac{7.2}{10.0}$	
7.35	$\frac{7.55}{10.1} \quad -0.2$		7.4	-0.1	$\frac{7.25}{10.0}$	7.20
7.25	$\frac{7.45}{10.0} \quad -0.2$		7.35	-0.2	$\frac{7.15}{10.0}$	6.85
7.05	$\frac{7.15}{10.0} \quad -0.1$		7.25	-0.1	$\frac{6.5}{10.0}$	6.45
			6.85			
7.55	$\frac{7.5}{10.0} \quad +0.05$		0.0	-0.2	$\frac{6.85}{10.0}$	6.65
7.35	$\frac{7.35}{10.0} \quad 0.0$		7.10	-0.15	$\frac{6.65}{10.0}$	6.45
7.15	$\frac{7.3}{10.0} \quad -0.15$		7.05	-0.15	$\frac{6.45}{10.0}$	6.25
6.90	$\frac{7.0}{10.0} \quad -0.1$		6.95	-0.2	$\frac{6.2}{10.0}$	6.00
6.70	$\frac{6.6}{10.0} \quad +0.1$		6.65	-0.2	$\frac{5.9}{10.0}$	5.80
6.45	$\frac{6.35}{10.0} \quad +0.1$		6.2	$+0.05$	$\frac{5.6}{10.0}$	5.55
6.25	$\frac{6.2}{10.0} \quad +0.05$		5.9	$+0.1$	$\frac{5.05}{10.0}$	5.35
6.00	$\frac{6.0}{10.0} \quad 0.0$		5.75	$+0.05$	$\frac{4.8}{10.0}$	5.10
5.80	$\frac{5.7}{10.0} \quad +0.1$		5.6	-0.05	$\frac{4.5}{10.0}$	4.90
5.55	$\frac{5.5}{10.0} \quad 0.0$		5.75	$+0.1$	$\frac{4.2}{10.0}$	4.65
5.35	$\frac{5.25}{10.0} \quad +0.1$		5.05	$+0.105$	$\frac{3.9}{10.0}$	4.45
5.10	$\frac{4.95}{10.0} \quad +0.25$		4.85	$+0.05$	$\frac{3.65}{10.0}$	4.20
4.90	$\frac{4.85}{10.0} \quad +0.05$	$\frac{5}{100}$	4.7	-0.05	$\frac{3.4}{10.0}$	4.00
4.65	$\frac{4.7}{10.0} \quad -0.05$	$\frac{5}{100}$	4.5	-0.05	$\frac{3.2}{10.0}$	3.75
4.45	$\frac{4.6}{10.0} \quad -0.15$		4.2	0.0	$\frac{2.95}{10.0}$	3.55
4.25	$\frac{4.4}{10.0} \quad -0.3$		4.1	-0.1	$\frac{2.75}{10.0}$	3.35
4.10	$\frac{4.55}{10.0} \quad -0.35$		3.9	-0.1	$\frac{2.55}{10.0}$	3.20
3.90	$\frac{4.45}{10.0} \quad -0.45$		3.8	-0.15	$\frac{2.35}{10.0}$	3.00
3.75	$\frac{4.35}{10.0} \quad -0.30$		3.75	-0.3	$\frac{2.2}{10.0}$	2.85
			3.5	-0.2	$\frac{2.05}{10.0}$	

Station	+	H.I.	-	Grade
		249.49		
TIP	5.26	252.23	2.57	246.97
189 + 25				46.45 5.80
+ 50				46.65 5.60
+ 75				46.90 5.35
190 + 00				47.10 5.25
+ 25				47.35 4.90
+ 50				47.55 4.70
+ 89.5 ^v				47.90 4.35
191 + 27.5				48.25 4.00
B.M.	4.71	254.56		249.85
+ 45				48.60 5.95
192 + 00				48.90 5.65
+ 37.5 ^v				49.25 5.30
+ 80				49.60 4.95
193 + 20				49.95 4.60
+ 50				50.20 4.35
+ 75				50.40 4.15
194 + 00				50.55 4.00
+ 25				50.65 3.90
+ 50				50.80 3.75
+ 75				50.90 3.65
195 + 00				50.95 3.60
+ 25				51.00 3.55
+ 50				51.05 3.50

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6.25	$\frac{6.35}{10.0} - 0.1$		-0.05	$\frac{-0.15}{10.0}$	5.35
6.05	$\frac{6.15}{10.0} - 0.1$	$\frac{5}{100}$	+0.1	$\frac{-0.05}{10.0}$	5.15
5.80	$\frac{5.9}{10.0} - 0.1$		0.0	$\frac{-0.05}{10.0}$	4.90
5.70	$\frac{5.85}{10.0} - 0.15$	$\frac{3}{100}$	+0.05	$\frac{+0.05}{10.0}$	4.80
5.35	$\frac{5.55}{10.0} - 0.2$	$\frac{5}{100}$	+0.15	$\frac{-0.1}{10.0}$	4.45
5.15	$\frac{5.2}{10.0} - 0.05$	$\frac{8}{100}$	+0.15	$\frac{-0.05}{10.0}$	4.25
4.80	$\frac{4.75}{10.0} + 0.05$		+0.1	$\frac{-0.1}{10.0}$	3.90
4.30	$\frac{4.50}{10.0} - 0.2$	$\frac{4}{100}$	+0.1	$\frac{-0.1}{10.0}$	3.70

6.15	$\frac{6.3}{10.0} - 0.15$		-0.05	$\frac{-0.25}{10.0}$	5.75
5.75	$\frac{6.0}{10.0} - 0.25$		-0.1	$\frac{-0.2}{10.0}$	5.60
	$\frac{5.6}{10.0} 0.0$		0.0	$\frac{+0.1}{10.0}$	
	$\frac{5.1}{10.0} - 0.05$		0.0	$\frac{+0.2}{10.0}$	
	$\frac{4.95}{10.0} - 0.25$		-0.2	$\frac{+0.05}{10.0}$	
	$\frac{4.35}{10.0} - 0.4$		-0.35	$\frac{-0.05}{10.0}$	
	$\frac{4.65}{10.0} - 0.4$		-0.4	$\frac{-0.2}{10.0}$	
	$\frac{4.35}{10.0} 0.35$		-0.25	$\frac{-0.25}{10.0}$	
	$\frac{4.35}{10.0} - 0.3$		-0.35	$\frac{-0.2}{10.0}$	
	$\frac{4.25}{10.0} - 0.7$		-0.55	$\frac{-0.45}{10.0}$	
	$\frac{4.05}{10.0} - 0.3$		-0.4	$\frac{-0.45}{10.0}$	
	$\frac{3.95}{10.0} - 0.25$		-0.2	$\frac{-0.3}{10.0}$	
	$\frac{3.8}{10.0} - 0.15$		-0.1	$\frac{-0.15}{10.0}$	
	$\frac{3.55}{10.0} - 0.25$		-0.2	$\frac{-0.25}{10.0}$	

Station	+	H.I.	-	Grade
		254.56		
195+75				51.05 3.50
196+00				51.05 3.50
T.P.	3.71	254.55		250.84
+25				51.00 3.55
+50				50.95 3.60
+75				50.90 3.65
197+00				50.80 3.75
+25				50.70 3.85
+50				50.55 4.00
+75				50.40 4.15
198+00				50.20 4.35
+25				50.05 4.50
+50				49.80 4.75
+75				49.60 4.95
199+00				49.30 5.25
+25				49.05 5.50
+50				48.80 5.75
+75				48.55 6.00
200+00				48.30 6.25
+25				48.05 6.50
+50				47.75 6.80
+75				47.50 7.05
201+00				47.20 7.35
T.P.	3.55	251.33	6.77	47.78

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$\frac{3.75}{10.0} - 0.15$			-0.35		-0.2
$\frac{3.6}{10.0} + 0.0$			3.5		$\frac{3.4}{10.0}$
			-0.05	$\frac{4}{00}$	$+0.1$
			3.55		$\frac{3.5}{10.0}$
$3.60 + 0.05$	$\frac{5}{00}$		-0.05		$+0.2$
$\frac{3.7}{10.0} + 0.0$			3.6	$\frac{3}{00}$	$\frac{2.45}{10.0}$
$3.65 + 0.1$	$\frac{5}{00}$		-0.1	$\frac{4}{00}$	$+0.2$
$3.40 + 0.05$			3.7		$\frac{3.5}{10.0}$
			3.75		0.0
			$+0.1$		$\frac{3.75}{10.0}$
			3.65		$+0.05$
			$+0.15$		$\frac{3.80}{10.0}$
$4.05 - 0.1$	$\frac{6}{00}$		3.7		$+0.1$
$4.05 + 0.05$			$+0.15$		$\frac{3.95}{10.0}$
			3.85		$+0.25$
			$+0.15$		$\frac{3.95}{10.0}$
$4.25 + 0.0$			4.0		$+0.25$
$4.25 + 0.0$			-0.05	$\frac{5}{00}$	$+0.05$
			4.6		0.0
$4.65 - 0.05$			-0.1		0.0
$4.9 - 0.05$			-0.15		$\frac{4.6}{10.0}$
$5.15 - 0.1$			-0.05		$\frac{4.95}{10.0}$
$5.4 - 0.05$			4.6		0.0
$5.7 - 0.15$			-0.15		-0.1
$6.10 - 0.25$			-0.2		-0.2
$6.40 - 0.12$			5.10		$\frac{5.25}{10.0}$
$6.6 - 0.25$			5.4		-0.05
$7.0 - 0.4$			5.75		-0.2
$7.2 - 0.3$			-0.2		0.0
$7.5 - 0.2$			-0.1		$\frac{5.85}{10.0}$
$7.5 - 0.05$	$\frac{5}{00}$		-0.15		-0.1
			6.10		$\frac{6.2}{10.0}$
			6.4		-0.1
			-0.25		$\frac{6.45}{10.0}$
			7.0		-0.3
			-0.2		$\frac{6.9}{10.0}$
			-0.1		-0.2
			$+0.05$		$\frac{7.1}{10.0}$
					-0.1
					$\frac{7.35}{10.0}$
					$+0.05$
					$\frac{7.40}{10.0}$

Station	+	H.I.	-	Grade
		257.33		
201+25				47.10 4.25
+ 50				46.95 4.40
+ 75				46.85 4.50
202+00				46.70 4.65
+ 25				46.65 4.70
+ 50				46.65 4.70
+ 75				46.70 4.65
203+00				46.80 4.55
+ 25				46.95 4.40
+ 50				47.05 4.30
+ 75				47.20 4.15
204+00				47.30 4.05
+ 25				47.45 3.90
+ 50				47.55 3.80
+ 75				47.70 3.65
205+00				47.80 3.55
+ 25				47.95 3.40
+ 50				48.05 3.30
T.P.	5.35	254.23	2.45	241.91
+ 75				48.35 5.90
206+00				48.60 5.65
+ 25				48.90 5.35
+ 50				49.25 5.00
+ 75				49.60 4.65

h

l

P

$\frac{4.4}{10.0} - 0.05$		$\frac{7}{00}$	$\frac{4.1}{10}$	$\frac{4.05}{10.0}$	$\frac{4.3}{10.0}$
$\frac{4.45}{10.0} + 0.05$			$\frac{4.3}{10}$	$\frac{4.1}{10.0}$	$\frac{4.4}{10.0}$
$\frac{4.45}{10.0} + 0.15$			$\frac{4.35}{10}$	$\frac{4.15}{10.0}$	$\frac{4.2}{10.0}$
$\frac{4.55}{10.0} + 0.2$			$\frac{4.5}{10}$	$\frac{4.15}{10.0}$	$\frac{4.55}{10.0}$
$\frac{4.65}{10.0} + 0.15$			$\frac{4.35}{10}$	$\frac{4.25}{10.0}$	$\frac{4.6}{10.0}$
$\frac{4.70}{10.0} + 0.1$			$\frac{4.4}{10}$	$\frac{4.3}{10.0}$	$\frac{4.60}{10.0}$
$\frac{4.75}{10.0} - 0.1$	$\frac{4}{00}$		$\frac{4.6}{10}$	$\frac{4.05}{10.0}$	$\frac{4.55}{10.0}$
$\frac{4.75}{10.0} - 0.05$		$\frac{8}{00}$	$\frac{4.4}{10}$	$\frac{4.15}{10.0}$	$\frac{4.4}{10.0}$
$\frac{4.65}{10.0} - 0.15$	$\frac{4}{00}$		$\frac{4.3}{10}$	$\frac{4.01}{10.0}$	$\frac{4.3}{10.0}$
$\frac{4.55}{10.0} - 0.15$	$\frac{4}{00}$		$\frac{4.2}{10}$	$\frac{4.1}{10.0}$	$\frac{4.4}{10.0}$
$\frac{4.30}{10.0} - 0.05$		$\frac{7}{00}$	$\frac{4.05}{10}$	$\frac{4.01}{10.0}$	$\frac{4.2}{10.0}$
$\frac{4.15}{10.0} 0.0$			$\frac{3.85}{10}$	$\frac{4.02}{10.0}$	$\frac{4.2}{10.0}$
$\frac{4.15}{10.0} - 0.15$	$\frac{4}{00}$		$\frac{3.8}{10}$	$\frac{4.01}{10.0}$	$\frac{4.0}{10.0}$
$\frac{4.1}{10.0} - 0.2$	$\frac{4}{00}$		$\frac{3.7}{10}$	$\frac{4.01}{10.0}$	$\frac{4.0}{10.0}$
$\frac{3.95}{10.0} - 0.2$			$\frac{3.65}{10}$	$\frac{4.0}{10.0}$	$\frac{3.8}{10.0}$
$\frac{3.75}{10.0} - 0.1$			$\frac{3.60}{10}$	$\frac{4.05}{10.0}$	$\frac{3.75}{10.0}$
$\frac{3.5}{10.0} 0.0$			$\frac{3.55}{10}$	$\frac{4.05}{10.0}$	$\frac{3.50}{10.0}$
$\frac{3.35}{10.0} + 0.05$			$\frac{3.30}{10}$	$\frac{4.00}{10.0}$	$\frac{3.25}{10.0}$
$\frac{5.75}{10.0} + 0.05$			$\frac{5.9}{10}$	$\frac{4.00}{10.0}$	$\frac{5.8}{10.0}$
$\frac{5.75}{10.0} 0.0$			$\frac{5.8}{10}$	$\frac{4.05}{10.0}$	$\frac{5.55}{10.0}$
$\frac{5.4}{10.0} + 0.05$		$\frac{8}{00}$	$\frac{5.5}{10}$	$\frac{4.05}{10.0}$	$\frac{5.30}{10.0}$
$\frac{5.25}{10.0} - 0.15$			$\frac{5.2}{10}$	$\frac{4.05}{10.0}$	$\frac{5.05}{10.0}$
$\frac{4.95}{10.0} - 0.2$			$\frac{4.9}{10}$	$\frac{4.05}{10.0}$	$\frac{4.75}{10.0}$

Station	+	H.I.	-	Grade
		254.20		
207+00				50.00 4.25
	+25			50.35 3.90
	+50			50.70 3.55
	+75			51.05 3.20
208+00				51.40 2.85
	+25			51.80 2.45
	+50			52.25 2.00
	+75			52.65 1.60
209+00				53.10 1.15
	+25			53.55 0.70
	+50			53.95 0.30
	+75			54.40 (-0.15)

No x-sections for fine grading
from Sta. 209+75 to 214+00.

This stretch was not finished
by Sub. Contractor. Owing to condition
of sub. grade and McCree + Co.
ordered same left unfinished for
hauling convenience.

L

E

R

$\frac{4.55}{10.0} - 0.2$
 $\frac{4.20}{10.0} - 0.2$
 $\frac{3.9}{10.0} - 0.25$
 $\frac{3.4}{10.0} - 0.1$
 $\frac{2.85}{10.0} + 0.1$
 $\frac{2.45}{10.0} + 0.1$
 $\frac{2.85}{10.0} + 0.05$
 $\frac{1.75}{10.0} - 0.05$
 $\frac{1.2}{10.0} + 0.05$
 $\frac{0.75}{10.0} + 0.05$
 $\frac{0.45}{10.0} - 0.05$
 $\frac{0.15}{10.0} + 0.1$

$\frac{5}{00}$
 $\frac{5}{00}$
 $\frac{5}{00}$

$\frac{4.4}{10.0} - 0.15$
 $\frac{4.0}{10.0} - 0.1$
 $\frac{3.7}{10.0} - 0.15$
 $\frac{3.2}{10.0} + 0.0$
 $\frac{2.55}{10.0} + 0.0$
 $\frac{2.45}{10.0} + 0.0$
 $\frac{2.05}{10.0} - 0.05$
 $\frac{1.55}{10.0} + 0.05$
 $\frac{1.20}{10.0} - 0.05$
 $\frac{0.85}{10.0} - 0.15$
 $\frac{0.5}{10.0} + 0.12$
 $\frac{0.15}{10.0} + 0.0$

$\frac{-0.2}{10.0} \frac{4.55}{10.0}$
 $\frac{-0.05}{10.0} \frac{4.05}{10.0}$
 $\frac{-0.1}{10.0} \frac{3.75}{10.0}$
 $\frac{+0.1}{10.0} \frac{3.2}{10.0}$
 $\frac{-0.05}{10.0} \frac{3.0}{10.0}$
 $\frac{-0.05}{10.0} \frac{2.6}{10.0}$
 $\frac{-0.05}{10.0} \frac{2.15}{10.0}$
 $\frac{+0.1}{10.0} \frac{1.6}{10.0}$
 $\frac{+0.1}{10.0} \frac{1.15}{10.0}$
 $\frac{0.0}{10.0} \frac{0.8}{10.0}$
 $\frac{-0.1}{10.0} \frac{0.5}{10.0}$
 $\frac{+0.25}{10.0} \frac{0.0}{10.0}$

X-sections for Fine Grading.

Station 277+68 —

Station	+	H.I.	-	Grade
B.M.	3.93	252.76		248.73
277+68				48.05 4.70
+30				48.05 4.70
277+00				48.1 4.65
+75				48.10 4.65
+50				48.10 4.65
+25				48.10 4.65
276+00				48.10 4.65
+75				48.05 4.70
+50				47.95 4.80
+25				47.90 4.85
275+00				47.8 4.95
+75				47.7 5.05
+50				47.6 5.15
+25				47.5 5.25
274+00				47.4 5.35
+75				47.3 5.45
+50				47.2 5.55
+25				47.1 5.65
273+00				47.0 5.75
+75				46.9 5.85
+50				46.8 5.95
+25				46.7 6.05
T.P.I.	3.85	250.57		246.72
272+00				46.6 3.95

h. L R

$\frac{4.75}{10.0} - 0.15$		-0.3	-0.1	$\frac{4.9}{10.0}$
$\frac{5.0}{10.0} - 0.12$		-0.25	$+\frac{0.05}{0.00}$	$\frac{5.75}{10.0}$
$\frac{4.5}{10.0} - 0.1$		-0.15	0.0	$\frac{4.75}{10.0}$
$\frac{4.8}{10.0} - 0.15$		-0.05	$+\frac{0.1}{0.00}$	$\frac{4.65}{10.0}$
$\frac{4.7}{10.0} + 0.05$		$+0.1$	$+0.1$	$\frac{4.65}{10.0}$
$\frac{4.6}{10.0} - 0.05$	$\frac{5}{0.00}$	$+0.05$	$+0.05$	$\frac{4.7}{10.0}$
$\frac{4.75}{10.0} 0.0$		0.0	0.0	$\frac{4.75}{10.0}$
$\frac{4.9}{10.0} - 0.1$		0.0	-0.05	$\frac{4.65}{10.0}$
$\frac{4.95}{10.0} - 0.05$		-0.1	-0.05	$\frac{4.95}{10.0}$
$\frac{5.25}{10.0} - 0.3$		-0.25	-0.05	$\frac{5.0}{10.0}$
$\frac{5.05}{10.0} 0.0$		-0.15	-0.1	$\frac{5.15}{10.0}$
$\frac{5.35}{10.0} - 0.2$		0.0	$+0.1$	$\frac{5.05}{10.0}$
$\frac{5.35}{10.0} - 0.1$		0.0	$+0.1$	$\frac{5.15}{10.0}$
$\frac{5.35}{10.0} 0.0$		-0.05	$+0.1$	$\frac{5.25}{10.0}$
$\frac{5.30}{10.0} + 0.15$	$\frac{4}{0.00}$	-0.05	-0.05	$\frac{5.5}{10.0}$
$\frac{5.6}{10.0} - 0.05$		-0.05	$+0.1$	$\frac{5.45}{10.0}$
$\frac{5.7}{10.0} - 0.05$	$\frac{5}{0.00}$	$+0.05$	$+0.15$	$\frac{5.5}{10.0}$
$\frac{5.65}{10.0} + 0.1$		$+0.1$	$+0.05$	$\frac{5.7}{10.0}$
$\frac{5.9}{10.0} - 0.05$	$\frac{7}{0.00}$	$+0.1$	$+0.25$	$\frac{5.6}{10.0}$
$\frac{5.9}{10.0} + 0.05$		$+0.1$	$+0.1$	$\frac{5.85}{10.0}$
$\frac{6.05}{10.0} 0.0$		$+0.1$	$+0.05$	$\frac{6.00}{10.0}$
$\frac{6.00}{10.0} + 0.15$		$+0.05$	$+0.2$	$\frac{5.95}{10.0}$
$\frac{6.05}{10.0} 0.0$		$+0.05$	$+0.15$	$\frac{6.0}{10.0}$
$\frac{6.05}{10.0} 0.0$		$+0.05$	$+0.15$	$\frac{6.0}{10.0}$

Station	+	H.I.	-	Elev
		250.57		
271	+ 75			46.50 4.05
	+ 50			46.40 4.15
	+ 25			46.30 4.25
271	+ 00			46.20 4.35
	+ 75			46.10 4.45
	+ 50			46.00 4.55
	+ 25			45.90 4.65
270	+ 00			45.80 4.75
	+ 75			45.70 4.85
	+ 50			45.60 4.95
	+ 25			45.50 5.05
269	+ 00			45.40 5.15
	+ 75			45.30 5.25
	+ 50			45.20 5.35
	+ 25			45.10 5.45
268	+ 00			45.00 5.55
	+ 75			44.90 5.65
	+ 50			44.80 5.75
	+ 25			44.70 5.85
267	+ 00			44.60 5.95
T.P	3.96	248.48		244.52
	+ 75			44.50 4.00
	+ 50			44.40 4.10
	+ 25			44.30 4.20

L

E

R

4.15 0.0
10.0
 4.15 +0.1
10.0
 4.5 -0.15
10.0
 4.5 -0.05
10.0
 4.4 +0.15
10.0
 4.5 +0.15
10.0
 4.7 +0.05
10.0
 4.8 +0.05 $\frac{7}{00}$
10.0
 5.05 -0.1
10.0
 5.05 0.0
10.0
 5.2 -0.05
10.0
 5.35 -0.1
10.0
 5.5 -0.15
10.0
 5.6 -0.15
10.0
 5.7 -0.15
10.0
 5.85 -0.2
10.0
 5.95 -0.2
10.0
 6.1 -0.15
10.0
 6.1 -0.15
10.0
 6.25 -0.2
10.0
 4.15 -0.05
10.0
 4.25 -0.05
10.0
 4.35 -0.05
10.0

$\frac{4}{00}$

-0.15
 4.2
 -0.05
 4.2
 -0.05
 4.3
 -0.05
 4.4 $\frac{4}{00}$
 0.0
 4.45
 0.0
 4.55
 +0.05
 4.6
 -0.1
 4.85 $\frac{7}{00}$
 -0.15
 5.0
 -0.15
 5.1
 -0.05
 5.1
 -0.1
 5.25
 0.0
 5.25
 -0.1
 5.45 $\frac{7}{00}$
 -0.05
 5.5
 -0.05
 5.6
 -0.15
 5.8
 -0.1
 5.85
 -0.2
 6.05
 -0.2
 6.05
 -0.2
 6.15
 -0.2
 4.7 -0.2
 4.1 0.0
 4.25 -0.05

$\frac{9}{00}$

$\frac{4}{00}$

$\frac{7}{00}$

+0.05 4.1
10.0
 -0.05 4.3
10.0
 0.0 4.35
10.0
 +0.1 4.35
10.0
 +0.25 4.3
10.0
 +0.15 4.5
10.0
 +0.05 4.7
10.0
 +0.05 4.8
10.0
 -0.05 5.0
10.0
 -0.25 5.3
10.0
 -0.2 5.35
10.0
 0.0 5.25
10.0
 +0.05 5.3
10.0
 +0.05 5.4
10.0
 -0.05 5.6
10.0
 0.0 5.65
10.0
 -0.05 5.8
10.0
 -0.2 6.05
10.0
 -0.25 6.2
10.0
 -0.25 6.3
10.0
 -0.25 4.35
10.0
 -0.2 4.1
10.0
 -0.05 4.35
10.0

Station	+	H.I.	-	Elev.
		248.48		
266+00				44.20 4.30
+75				44.10 4.40
+50				44.00 4.50
+25				43.90 4.60
265+00				43.80 4.70
+75				43.70 4.80
+50				43.60 4.90
+25				43.50 5.00
264+00				43.40 5.10
B.M.	2.31	249.18		246.87
+75				43.35 5.85
+50				43.30 5.90
+25				43.30 5.90
263+00				43.30 5.90
+75				43.40 5.80
+50				43.55 5.65
+25				43.70 5.50
262+00				43.95 5.25
+75				44.20 5.00
+50				44.50 4.70
+25				44.80 4.40
261+00				45.20 4.00
+75				45.55 3.65
+50				45.95 3.25

h

L

R

$\frac{4.4}{10.0} + 0.0$
 $\frac{4.7}{10.0} - 0.2$
 $\frac{4.75}{10.0} - 0.15$
 $\frac{4.85}{10.0} - 0.15$
 $\frac{4.85}{10.0} - 0.05$
 $\frac{4.95}{10.0} - 0.05$
 $\frac{5.15}{10.0} - 0.15$
 $\frac{5.15}{10.0} - 0.05$
 $\frac{5.3}{10.0} - 0.1$

$\frac{4}{00}$

4.8
 4.45
 4.6
 4.75
 4.95
 4.9
 4.9
 5.15
 5.05

$\frac{3}{00}$

$+0.05 \frac{4.35}{10.0}$
 $0.0 \frac{4.5}{10.0}$
 $0.0 \frac{4.6}{10.0}$
 $-0.05 \frac{4.75}{10.0}$
 $-0.1 \frac{4.9}{10.0}$
 $0.0 \frac{4.9}{10.0}$
 $+0.05 \frac{4.95}{10.0}$
 $-0.15 \frac{5.75}{10.0}$
 $-0.15 \frac{5.35}{10.0}$

$\frac{5.6}{10.0} + 0.15$
 $\frac{5.7}{10.0} + 0.3$
 $\frac{5.95}{10.0} + 0.05$
 $\frac{5.8}{10.0} + 0.2$
 $\frac{5.65}{10.0} + 0.25$
 $\frac{5.75}{10.0} 0.0$
 $\frac{5.45}{10.0} + 0.15$
 $\frac{5.25}{10.0} + 0.1$
 $\frac{5.05}{10.0} + 0.05$
 $\frac{4.9}{10.0} - 0.1$
 $\frac{4.4}{10.0} + 0.1$
 $\frac{4.1}{10.0} 0.0$
 $\frac{3.65}{10.0} + 0.1$
 $\frac{3.1}{10.0} - 0.05$

$\frac{5}{00}$

$\frac{7}{00}$

5.65
 5.7
 5.85
 5.65
 5.45
 5.45
 5.3
 5.95
 5.1
 4.9
 4.6
 4.75
 3.95
 3.65
 3.15

0.0
 $+0.2$
 $+0.05$
 -0.25
 $+0.35$
 $+0.35$
 $+0.25$
 $+0.15$
 $+0.25$
 $+0.15$
 $+0.1$
 $+0.1$
 $+0.15$
 $+0.05$
 $+0.15$
 $+0.1$
 7
 5

$\frac{7}{00}$

$\frac{5}{00}$

$-0.1 \frac{6.05}{10.0}$
 $+0.05 \frac{5.95}{10.0}$
 $0.0 \frac{6.0}{10.0}$
 $+0.2 \frac{5.8}{10.0}$
 $+0.3 \frac{5.6}{10.0}$
 $+0.15 \frac{5.6}{10.0}$
 $+0.3 \frac{5.2}{10.0}$
 $+0.4 \frac{4.95}{10.0}$
 $+0.35 \frac{4.75}{10.0}$
 $+0.3 \frac{4.55}{10.0}$
 $+0.2 \frac{4.3}{10.0}$
 $0.0 \frac{4.1}{10.0}$
 $-0.1 \frac{3.85}{10.0}$
 $-0.1 \frac{3.45}{10.0}$

Station	+	H.I.	-	Elev.
		249.18		
260+25				46.30 2.90
260+00				46.65 2.55
B.M.	8.17	254.31		(245.44)
+75				47.05 7.25
+50				47.40 6.90
+25				47.75 6.55
259+00				48.10 6.20
+75				48.50 5.80
+50				48.85 5.45
+25				49.20 5.10
258+00				49.60 4.70
+75				49.95 4.35
+50				50.25 4.05
+25				50.55 3.75
257+00				50.80 3.50
+75				51.00 3.30
+50				51.20 3.10
+25				51.40 2.90
256+00				51.50 2.80
T.P.	+2.47	255.62	2.10	252.15
+75				51.65 3.95
+50				51.70 3.90
+25				51.75 3.85
255+00				51.75 3.85

h.

L

P.

$$\frac{2.95}{10.0} + 0.05$$

$$\frac{2.6}{10.0} + 0.05$$

$$\frac{7.25}{10.0} 0.0$$

$$\frac{6.95}{10.0} + 0.05$$

$$\frac{6.55}{10.0} + 0.1$$

$$\frac{6.2}{10.0} + 0.1$$

$$\frac{5.75}{10.0} + 0.15$$

$$\frac{5.4}{10.0} + 0.15$$

$$\frac{5.05}{10.0} + 0.15$$

$$\frac{4.8}{10.0} 0.0$$

$$\frac{4.45}{10.0} 0.0$$

$$\frac{4.1}{10.0} + 0.05 \quad \frac{1}{0.0}$$

$$\frac{3.95}{10.0} - 0.1$$

$$\frac{3.85}{10.0} - 0.25$$

$$\frac{3.6}{10.0} - 0.2$$

$$\frac{3.3}{10.0} - 0.1$$

$$\frac{3.15}{10.0} - 0.15$$

$$\frac{2.9}{10.0} 0.0$$

$$\frac{4.05}{10.0} 0.0$$

$$\frac{4.05}{10.0} - 0.05$$

$$\frac{3.75}{10.0} + 0.1$$

$$\frac{3.6}{10.0} + 0.35$$

$$2.9 0.0$$

$$2.55 0.0$$

$$7.25 0.0$$

$$6.85 + 0.05$$

$$6.45 + 0.1$$

$$6.2 0.0$$

$$5.75 + 0.05$$

$$5.35 + 0.1$$

$$4.95 + 0.15$$

$$4.6 + 0.1$$

$$4.45 - 0.1$$

$$4.15 - 0.1$$

$$3.85 - 0.1$$

$$3.75 - 0.25$$

$$3.65 - 0.35$$

$$3.3 - 0.2$$

$$3.0 - 0.1$$

$$2.85 - 0.05$$

$$3.95 0.0$$

$$3.9 0.0$$

$$3.65 + 0.2$$

$$3.6 + 0.25$$

$$-0.05 \frac{3.85}{10.0}$$

$$-0.05 \frac{2.7}{10.0}$$

$$0.0 \frac{7.35}{10.0}$$

$$+0.15 \frac{6.85}{10.0}$$

$$+0.1 \frac{6.55}{10.0}$$

$$+0.2 \frac{6.1}{10.0}$$

$$+0.2 \frac{5.7}{10.0}$$

$$+0.25 \frac{5.3}{10.0}$$

$$+0.2 \frac{5.0}{10.0}$$

$$+0.2 \frac{4.6}{10.0}$$

$$-0.05 \frac{4.5}{10.0}$$

$$-0.05 \frac{4.2}{10.0}$$

$$0.0 \frac{3.85}{10.0}$$

$$-0.15 \frac{3.75}{10.0}$$

$$-0.15 \frac{3.55}{10.0}$$

$$-0.15 \frac{3.35}{10.0}$$

$$-0.15 \frac{3.15}{10.0}$$

$$0.0 \frac{2.9}{10.0}$$

$$-0.05 \frac{4.15}{10.0}$$

$$0.0 \frac{4.0}{10.0}$$

$$+0.25 \frac{3.7}{10.0}$$

$$+0.2 \frac{3.75}{10.0}$$

Station	+	H.I.	-	Elev
		255.62		
254	+ 75			51.75 3.85
	+ 50			51.70 3.90
	+ 25			51.65 3.95
254	+ 00			51.50 4.10
	+ 75			51.40 4.20
	+ 50			51.25 4.35
	+ 25			51.15 4.45
253	+ 00			51.00 4.60
	+ 75			50.90 4.70
	+ 50			50.75 4.85
	+ 25			50.65 4.95
252	+ 00			50.50 5.10
	+ 75			50.40 5.20
	+ 50			50.25 5.35
	+ 25			50.15 5.45
251	+ 00			50.00 5.60
	+ 75			50.15 5.45
	+ 50			50.35 5.35
	+ 25			50.40 5.20
250	+ 00			50.70 4.90
B.M.	6.38	256.43		250.08
	+ 75			51.25 5.20
	+ 50			51.75 4.70
	+ 25			52.20 4.25

L.

E

P

$\frac{3.7}{10.0} + 0.25$	$\frac{3.6}{10.0} + 0.25$	$\frac{3.65}{10.0} + 0.2$
$\frac{3.7}{10.0} + 0.3$	$\frac{3.65}{10.0} + 0.25$	$\frac{3.6}{10.0} + 0.25$
$\frac{3.8}{10.0} + 0.25$	$\frac{3.75}{10.0} + 0.2$	$\frac{3.7}{10.0} + 0.2$
$\frac{4.05}{10.0} + 0.15$	$\frac{4.05}{10.0} + 0.05$	$\frac{4.1}{10.0} + 0.1$
$\frac{4.3}{10.0} 0.0$	$\frac{4.3}{10.0} - 0.1$	$\frac{4.35}{10.0} - 0.05$
$\frac{4.4}{10.0} + 0.05$	$\frac{4.35}{10.0} 0.0$	$\frac{4.55}{10.0} - 0.1$
$\frac{4.55}{10.0} 0.0$	$\frac{4.6}{10.0} - 0.15$	$\frac{4.65}{10.0} - 0.1$
$\frac{4.75}{10.0} - 0.05$	$\frac{4.75}{10.0} - 0.15$	$\frac{4.75}{10.0} - 0.05$
$\frac{4.75}{10.0} - 0.15$	$\frac{5.00}{10.0} - 0.3$	$\frac{4.95}{10.0} - 0.15$
$\frac{5.15}{10.0} - 0.2$	$\frac{5.2}{10.0} - 0.45$	$\frac{5.1}{10.0} - 0.15$
$\frac{5.2}{10.0} - 0.15$	$\frac{5.3}{10.0} - 0.35$	$\frac{5.2}{10.0} - 0.15$
$\frac{5.2}{10.0} 0.0$	$\frac{5.2}{10.0} - 0.1$	$\frac{5.2}{10.0} 0.0$
$\frac{5.3}{10.0} 0.0$	$\frac{5.3}{10.0} - 0.1$	$\frac{5.3}{10.0} 0.0$
$\frac{5.45}{10.0} 0.0$	$\frac{5.55}{10.0} - 0.2$	$\frac{5.45}{10.0} 0.0$
$\frac{5.5}{10.0} + 0.05$	$\frac{5.6}{10.0} - 0.15$	$\frac{5.6}{10.0} - 0.05$
$\frac{5.5}{10.0} + 0.2$	$\frac{5.55}{10.0} + 0.05$	$\frac{5.6}{10.0} + 0.1$
$\frac{5.45}{10.0} + 0.1$	$\frac{5.5}{10.0} 0.0$	$\frac{5.5}{10.0} + 0.05$
$\frac{5.35}{10.0} 0.0$	$\frac{5.25}{10.0} 0.0$	$\frac{5.45}{10.0} - 0.1$
$\frac{5.10}{10.0} + 0.2$	$\frac{5.00}{10.0} + 0.2$	$\frac{5.3}{10.0} 0.0$
$\frac{4.9}{10.0} + 0.1$	$\frac{4.85}{10.0} + 0.15$	$\frac{5.0}{10.0} 0.0$
$\frac{5.35}{10.0} - 0.05$	$\frac{5.3}{10.0} - 0.1$	$\frac{5.5}{10.0} - 0.2$
$\frac{4.95}{10.0} - 0.15$	$\frac{5.0}{10.0} - 0.3$	$\frac{5.05}{10.0} - 0.25$
$\frac{4.4}{10.0} - 0.05$	$\frac{4.4}{10.0} - 0.15$	$\frac{4.3}{10.0} + 0.05$

Station	+	H.I	-	Elev.	
		256.43			
249+00				52.65	3.80
+75				53.05	3.40
+50				53.35	3.10
+25				53.70	2.75
248+00				54.00	2.45
+75				54.35	2.10
+50				54.65	1.80
+25				55.00	1.45
247+00				55.30	1.15
+75				55.65	0.80
T.P	7.40	262.67	1.16	255.27	
+50				55.95	6.70
+25				56.25	6.40
246+00				56.55	6.10
B.M.	4.64	263.34		258.70	
+75				56.85	6.50
+50				57.10	6.25
+25				57.35	6.00
245+00				57.60	5.75
+75				57.80	5.55
+50				58.00	5.35
+25				58.20	5.15
244+00				58.40	4.95

h

E

P

$\frac{3.40}{10.0} + 0.05$
 $\frac{3.0}{10.0} + 0.1 \quad \frac{7}{100}$
 $\frac{3.10}{10.0} + 0.1$
 $\frac{2.65}{10.0} + 0.2$
 $\frac{2.3}{10.0} + 0.25$
 $\frac{2.00}{10.0} + 0.2$
 $\frac{1.8}{10.0} + 0.1$
 $\frac{1.4}{10.0} + 0.15$
 $\frac{1.3}{10.0} - 0.05$
 $\frac{1.0}{10.0} - 0.1$

0.0
 3.4
 -0.15
 3.55
 3.05
 $+0.05$
 $+0.05$
 2.7
 2.45
 2.10
 1.9
 1.45
 -0.1
 1.25
 -0.4
 1.20

$+0.05 \quad \frac{3.85}{10.0}$
 $+0.1 \quad \frac{3.4}{10.0}$
 $+0.2 \quad \frac{3.0}{10.0}$
 $+0.1 \quad \frac{2.75}{10.0}$
 $+0.05 \quad \frac{2.5}{10.0}$
 $0.0 \quad \frac{2.2}{10.0}$
 $+0.05 \quad \frac{1.85}{10.0}$
 $+0.15 \quad \frac{1.4}{10.0}$
 $+0.2 \quad \frac{1.05}{10.0}$
 $+0.1 \quad \frac{0.8}{10.0}$

$\frac{6.6}{10.0} + 0.2$
 $\frac{6.35}{10.0} + 0.15$
 $\frac{5.95}{10.0} + 0.25$

$\frac{2}{100} \quad -0.05$
 6.75
 6.3
 5.95
 $+0.1$
 $+0.15$

$+0.2 \quad \frac{6.6}{10.0}$
 $+0.3 \quad \frac{6.2}{10.0}$
 $+0.3 \quad \frac{5.9}{10.0}$

$\frac{6.35}{10.0} + 0.25$
 $\frac{6.25}{10.0} + 0.1$
 $\frac{6.0}{10.0} + 0.1$
 $\frac{5.6}{10.0} + 0.05 \quad \frac{5}{100}$
 $\frac{5.6}{10.0} + 0.05$
 $\frac{5.35}{10.0} + 0.1$
 $\frac{5.0}{10.0} + 0.25$
 $\frac{4.75}{10.0} + 0.1$

6.35
 6.2
 5.95
 5.8
 5.55
 5.3
 5.0
 4.9
 $+0.15$
 $+0.05$
 $+0.05$
 -0.05
 0.0
 $+0.05$
 $+0.15$
 $+0.05$

$+0.2 \quad \frac{6.4}{10.0}$
 $+0.3 \quad \frac{6.05}{10.0}$
 $+0.4 \quad \frac{5.7}{10.0}$
 $+0.15 \quad \frac{5.7}{10.0}$
 $+0.25 \quad \frac{5.4}{10.0}$
 $-0.05 \quad \frac{5.10}{10.0}$
 $+0.25 \quad \frac{5.00}{10.0}$
 $+0.2 \quad \frac{4.85}{10.0}$

Station	+	H.I.	-	Elev.
		263.34		
243+75				58.55 4.80
+ 50				58.70 4.65
+ 25				58.90 4.45
243+00				59.00 4.35
+ 75				59.15 4.20
+ 50				59.25 4.10
+ 25				59.40 3.95
242+00				59.50 3.85
T.P.	4.83	263.26	4.91	258.43
+ 75				59.60 3.65
+ 50				59.75 3.50
+ 25				59.85 3.40
241+00				59.95 3.30
+ 75				60.00 3.25
+ 50				60.10 3.15
+ 25				60.15 3.10
240+00				60.20 3.05
+ 75				60.25 3.00
+ 50				60.30 2.95
+ 25				60.35 2.90
239+00				60.40 2.85
+ 75				60.45 2.80
+ 50				60.45 2.80
+ 25				60.45 2.80

h

L

R

$$\frac{4.7}{10.0} + 0.2$$

$$\frac{4.75}{10.0} + 0.05$$

$$\frac{4.7}{10.0} + 0.2$$

$$\frac{4.6}{10.0} + 0.15$$

$$\frac{4.6}{10.0} + 0.05$$

$$\frac{4.6}{10.0} + 0.15$$

$$\frac{4.5}{10.0} + 0.05$$

$$\frac{4.3}{10.0} + 0.15$$

$$\frac{4.45}{10.0} + 0.1$$

$$\frac{4.4}{10.0} + 0.05$$

$$\frac{4.3}{10.0} + 0.05$$

$$\frac{4.35}{10.0} + 0.1$$

$$\frac{4.30}{10.0} - 0.05$$

$$\frac{5}{100} \frac{4.15}{10.0} + 0.05$$

$$\frac{4.3}{10.0} + 0.0$$

$$\frac{4.30}{10.0} - 0.1$$

$$\frac{4.10}{10.0} + 0.0$$

$$\frac{4.2}{10.0} + 0.0$$

$$\frac{4.10}{10.0} - 0.05$$

$$\frac{4.0}{10.0} - 0.05$$

$$\frac{4.10}{10.0} - 0.1$$

$$\frac{4.0}{10.0} - 0.05$$

$$\frac{5}{100} \frac{3.8}{10.0} + 0.05$$

$$\frac{4.0}{10.0} - 0.05$$

$$\frac{3.65}{10.0} + 0.1$$

$$\frac{3.6}{10.0} + 0.05$$

$$\frac{3.85}{10.0} - 0.1$$

$$\frac{3.55}{10.0} + 0.05$$

$$\frac{3.4}{10.0} + 0.05$$

$$\frac{3.4}{10.0} + 0.0$$

$$\frac{3.4}{10.0} + 0.1$$

$$\frac{3.32}{10.0} + 0.05$$

$$\frac{3.4}{10.0} + 0.1$$

$$\frac{3.25}{10.0} + 0.15$$

$$\frac{3.10}{10.0} + 0.2$$

$$\frac{3.25}{10.0} + 0.15$$

$$\frac{3.05}{10.0} + 0.3$$

$$\frac{3.0}{10.0} + 0.25$$

$$\frac{3.0}{10.0} + 0.35$$

$$\frac{3.0}{10.0} + 0.25$$

$$\frac{3.05}{10.0} + 0.1$$

$$\frac{2.85}{10.0} + 0.4$$

$$\frac{3.0}{10.0} + 0.2$$

$$\frac{2.95}{10.0} + 0.15$$

$$\frac{2.85}{10.0} + 0.15$$

$$\frac{2.9}{10.0} + 0.25$$

$$\frac{2.9}{10.0} + 0.15$$

$$\frac{3.05}{10.0} + 0.1$$

$$\frac{2.85}{10.0} + 0.05$$

$$\frac{2.95}{10.0} + 0.05$$

$$\frac{2.95}{10.0} + 0.25$$

$$\frac{2.8}{10.0} + 0.05$$

$$\frac{2.9}{10.0} + 0.05$$

$$\frac{2.95}{10.0} + 0.1$$

$$\frac{2.8}{10.0} + 0.1$$

$$\frac{3.0}{10.0} - 0.1$$

$$\frac{2.8}{10.0} + 0.2$$

$$\frac{2.8}{10.0} + 0.05$$

$$\frac{2.9}{10.0} - 0.05$$

$$\frac{2.85}{10.0} + 0.1$$

$$\frac{2.8}{10.0} + 0.05$$

$$\frac{3.05}{10.0} - 0.25$$

$$\frac{2.95}{10.0} - 0.05$$

$$\frac{2.8}{10.0} - 0.1$$

$$\frac{3.05}{10.0} - 0.25$$

$$\frac{3.1}{10.0} - 0.2$$

$$\frac{2.85}{10.0} - 0.15$$

$$\frac{3.1}{10.0} - 0.3$$

$$\frac{3.05}{10.0} - 0.15$$

Station	+	H.I.	-	Elev.
		263.26		
239+00				60.40 2.85
+ 75				60.35 2.90
+ 50				60.25 3.00
+ 25				60.15 3.10
237+00				60.00 3.25
+ 75				59.85 3.40
+ 50				59.70 3.55
+ 25				59.55 3.70
236+00				59.40 3.85
+ 75				59.25 4.00
+ 50				59.10 4.15
+ 25				58.95 4.30
235+00				58.80 4.45
T.P.	2.89	261.85		258.96
+ 75				58.65 3.20
+ 50				58.50 3.35
+ 25				58.35 3.50
234+00				58.20 3.65
+ 75				58.10 3.75
+ 50				57.95 3.90
+ 25				57.85 4.00
233+00				57.70 4.15
+ 75				57.60 4.25
+ 50				57.45 4.40

h. ϕ P

$\frac{3.0}{10.0}$	-0.05		-0.2	-0.25	$\frac{3.2}{10.0}$
$\frac{2.9}{10.0}$	+0.1		3.05	0.0	$\frac{3.0}{10.0}$
$\frac{2.9}{10.0}$	+0.2	$\frac{4}{100}$	3.1	0.0	$\frac{3.1}{10.0}$
$\frac{3.15}{10.0}$	-0.3		3.3	-0.2	$\frac{3.0}{10.0}$
$\frac{3.3}{10.0}$	+0.05	$\frac{8}{100}$	3.2	-0.15	$\frac{3.45}{10.0}$
$\frac{3.3}{10.0}$	+0.2		3.45	+0.05	$\frac{3.45}{10.0}$
$\frac{3.4}{10.0}$	+0.25	$\frac{3}{100}$	3.55	0.0	$\frac{3.5}{10.0}$
$\frac{3.6}{10.0}$	+0.2		3.7	0.0	$\frac{3.6}{10.0}$
$\frac{3.9}{10.0}$	+0.05		3.85	0.0	$\frac{3.9}{10.0}$
$\frac{4.05}{10.0}$	+0.05	$\frac{8}{100}$	4.15	-0.15	$\frac{3.95}{10.0}$
$\frac{4.15}{10.0}$	+0.1	$\frac{5}{100}$	4.25	-0.1	$\frac{4.2}{10.0}$
$\frac{4.4}{10.0}$	0.0		4.75	-0.05	$\frac{4.3}{10.0}$
$\frac{4.5}{10.0}$	+0.05		4.45	0.0	$\frac{4.4}{10.0}$
$\frac{3.35}{10.0}$	-0.05		3.3	-0.1	$\frac{3.2}{10.0}$
$\frac{3.6}{10.0}$	+0.05	$\frac{5}{100}$	3.4	-0.05	$\frac{3.55}{10.0}$
$\frac{3.65}{10.0}$	-0.05		3.75	-0.25	$\frac{3.6}{10.0}$
$\frac{3.7}{10.0}$	+0.05	$\frac{5}{100}$	3.7	-0.05	$\frac{3.8}{10.0}$
$\frac{3.85}{10.0}$	0.0		3.9	-0.15	$\frac{3.95}{10.0}$
$\frac{4.1}{10.0}$	-0.1		4.05	-0.15	$\frac{4.15}{10.0}$
$\frac{4.1}{10.0}$	0.0		4.15	-0.15	$\frac{4.2}{10.0}$
$\frac{4.2}{10.0}$	+0.25	$\frac{3}{100}$	4.2	-0.05	$\frac{4.2}{10.0}$
$\frac{4.35}{10.0}$	+0.1		4.4	+0.05	$\frac{4.3}{10.0}$
$\frac{4.3}{10.0}$	+0.2	$\frac{4}{100}$	4.5	-0.1	$\frac{4.25}{10.0}$

Station	+	H. I.	-	Elev.
		261.85		
232	+ 25			57.35 4.50
232	+ 00			57.20 4.65
	+ 75			57.10 4.75
	+ 50			56.95 4.90
	+ 25			56.85 5.00
231	+ 00			56.70 5.15
	+ 75			56.55 5.30
	+ 50			56.45 5.40
	+ 25			56.30 5.55
230	+ 00			56.15 5.70
	+ 75			56.00 5.85
	+ 50			55.85 6.00
	+ 25			55.70 6.15
229	+ 00			55.50 6.35
	+ 75			55.35 6.50
	+ 50			55.15 6.70
	+ 25			55.00 6.85
228	+ 00			54.80 7.05
	T. P.	4.53	257.15	252.62
	+ 75			54.65 2.50
	+ 50			54.45 2.70
	+ 25			54.30 2.85
227	+ 00			54.10 3.05
	+ 75			53.95 3.20

4

E

P

$\frac{4.05}{10.0} + 0.15$		$+0.05$	$+0.3$	$\frac{4.3}{10.0}$
$\frac{4.0}{10.0} + 0.15$		$+0.15$	$+0.25$	$\frac{4.5}{10.0}$
$\frac{4.75}{10.0} + 0.1$		$+0.05$	$+0.25$	$\frac{4.4}{10.0}$
$\frac{4.85}{10.0} + 0.15$		$+0.1$	$+0.3$	$\frac{4.7}{10.0}$
$\frac{5.85}{10.0} + 0.05$	$\frac{7}{100}$	-0.1	$\frac{5}{100} + 0.1$	$\frac{5.0}{10.0}$
$\frac{5.0}{10.0} + 0.25$	$\frac{2}{100}$	-0.05	$+0.25$	$\frac{5.0}{10.0}$
$\frac{5.15}{10.0} + 0.25$	$\frac{3}{100}$	-0.1	$+0.05$	$\frac{5.35}{10.0}$
$\frac{5.5}{10.0} 0.0$		0.0	$+0.1$	$\frac{5.4}{10.0}$
$\frac{5.4}{10.0} + 0.25$		$+0.15$	0.0	$\frac{5.65}{10.0}$
$\frac{5.7}{10.0} + 0.1$		0.0	$+0.15$	$\frac{5.65}{10.0}$
$\frac{5.85}{10.0} + 0.1$	$\frac{5}{100}$	-0.1	$+0.15$	$\frac{5.9}{10.0}$
$\frac{6.05}{10.0} + 0.05$	$\frac{5}{100}$	-0.05	$+0.15$	$\frac{5.95}{10.0}$
$\frac{6.3}{10.0} - 0.05$		-0.15	0.0	$\frac{6.25}{10.0}$
$\frac{6.35}{10.0} + 0.1$		$+0.05$	$+0.3$	$\frac{6.15}{10.0}$
$\frac{6.45}{10.0} + 0.15$		$+0.1$	$+0.25$	$\frac{6.35}{10.0}$
$\frac{6.8}{10.0} 0.0$		$+0.15$	$+0.05$	$\frac{6.75}{10.0}$
$\frac{6.85}{10.0} + 0.1$		$+0.15$	0.0	$\frac{6.95}{10.0}$
$\frac{7.1}{10.0} + 0.05$		$+0.15$	$+0.05$	$\frac{7.1}{10.0}$
$\frac{2.5}{10.0} + 0.1$		$+0.05$	-0.1	$\frac{2.7}{10.0}$
$\frac{2.85}{10.0} - 0.05$	$\frac{7}{100}$	$+0.1$	$+0.05$	$\frac{2.75}{10.0}$
$\frac{3.10}{10.0} - 0.15$		-0.1	$+0.15$	$\frac{2.9}{10.0}$
$\frac{3.4}{10.0} - 0.25$		-0.05	-0.05	$\frac{3.2}{10.0}$
$\frac{3.55}{10.0} - 0.25$		-0.2	-0.1	$\frac{3.4}{10.0}$

Station	+	H. I.	-	Elev.
		257.15		
226+50				53.75 3.40
+25				53.60 3.55
226+00				53.40 3.75
+75				53.25 3.90
+50				53.05 4.10
+25				52.90 4.25
225+00				52.70 4.45
+75				52.55 4.60
+50				52.40 4.75
+25				52.30 4.85
224+00				52.20 4.95
T.P.	5.09	257.23	5.01	(257.14)
+75				52.20 5.05
+50				52.15 5.10
+25				52.15 5.10
223+00				52.20 5.05
+75				52.25 5.00
+50				52.30 4.95
+25				52.35 4.90
222+00				52.40 4.85
+75				52.50 4.75
+50				52.60 4.65
+25				52.75 4.50
221+00				52.90 4.35

L R

37 10.0	-0.2		-0.2		0.0	3.5 10.0
37.5 10.0	-0.1		-0.2		-0.15	3.8 10.0
39.0 10.0	-0.05		-0.1		+0.5	3.8 10.0
4.0 10.0	-0.1		-0.1		7/100	4.2 10.0
4.4 10.0	-0.2		-0.2		-0.1	4.3 10.0
4.55 10.0	-0.2		-0.05		-0.2	4.55 10.0
4.6 10.0	-0.05		-0.05		+0.1	4.45 10.0
4.75 10.0	-0.05		0.0		4/100	4.55 10.0
4.7 10.0	+0.15		0.0		+0.15	4.75 10.0
4.7 10.0	+0.25		+0.05		+0.1	4.85 10.0
4.8 10.0	+0.25		+0.05		0.0	5.05 10.0
5.0 10.0	+0.15		+0.05		0.0	5.15 10.0
5.15 10.0	+0.05		0.0		+0.15	5.25 10.0
5.2 10.0	0.0		+0.15		+0.15	5.05 10.0
5.2 10.0	-0.05	5/100	+0.05		+0.05	5.1 10.0
5.2 10.0	-0.1	4/100	+0.05		-0.05	5.15 10.0
5.3 10.0	-0.25	2/100	+0.05		-0.05	5.10 10.0
5.0 10.0	0.0		+0.05		+0.1	4.9 10.0
4.85 10.0	+0.1		+0.15		+0.15	4.8 10.0
4.75 10.0	+0.1		+0.2		+0.2	4.65 10.0
4.7 10.0	+0.05		+0.2		+0.15	4.6 10.0
4.85 10.0	+0.05		+0.2		+0.1	4.5 10.0
4.3 10.0	+0.15		+0.15		+0.05	4.6 10.0

Station	+	H.I.	-	Elev.
		25723		
220 + 75				53.25 4.00
+ 50				53.45 3.80
+ 25				53.75 3.50
220 + 00				54.10 3.15
219 + 75				254.50 2.75

4

4

P

$$\begin{array}{r} 4.15 \\ \hline 10.0 \end{array} - 0.05$$

$$\begin{array}{r} 3.95 \\ \hline 10.0 \end{array} + 0.05$$

$$\begin{array}{r} 3.6 \\ \hline 10.0 \end{array} 0.0$$

$$\begin{array}{r} 3.3 \\ \hline 10.0 \end{array} - 0.05$$

$$\begin{array}{r} 2.70 \\ \hline 10.0 \end{array} + 0.15$$

$$\begin{array}{r} -0.05 \\ 4.05 \end{array}$$

$$\begin{array}{r} 0.0 \\ 3.80 \end{array}$$

$$\begin{array}{r} +0.05 \\ 3.25 \end{array}$$

$$\begin{array}{r} 0.0 \\ 3.15 \end{array}$$

$$\begin{array}{r} +0.05 \\ 2.70 \end{array}$$

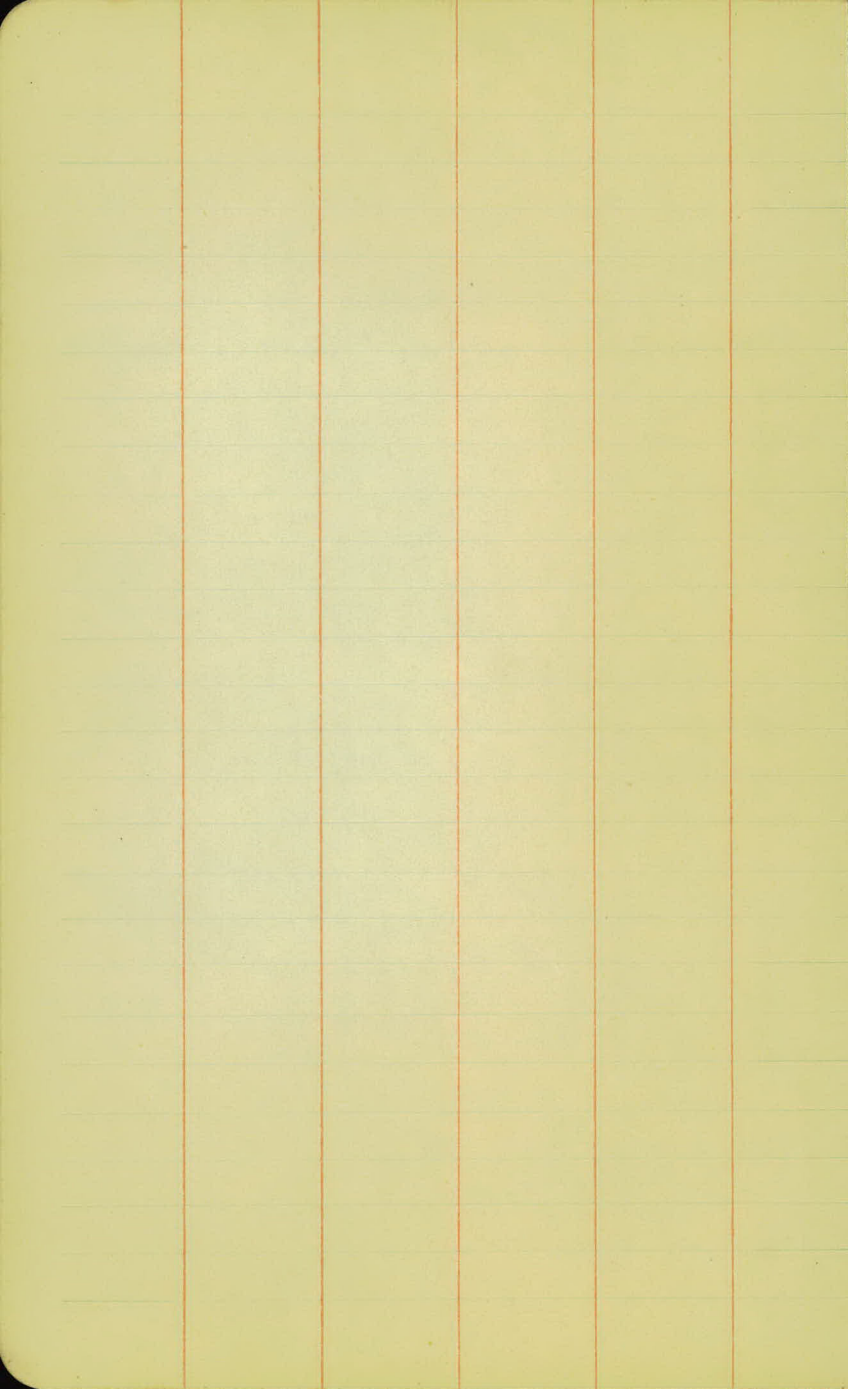
$$\begin{array}{r} -0.1 \\ 4.2 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} -0.05 \\ 3.95 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ 3.4 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} +0.2 \\ 3.05 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} +0.1 \\ 2.75 \\ \hline 10.0 \end{array}$$



Final - Topography

23-52

Carley
PERSONS
B11995
ECK.

Date	- sta	to	sta
11-16-23	-277	"	221

540

277

276

275

274

273

272

271

270

LT # RT

Tr 77+35

277+45 Tr 30'

70+38 Tr 31'

276+62 T.P. 23' P.P.

73+33 Tr. 30'

76+18. P.P. 26'

74+39 Tr. 23'

275+19 T.P. 23'

74+19 Tr. 24'

77+10 P.P. 28'

273+88 T.P. 23'

73+40 Tr 25

72+75 Tr. 23'

72+48

272+50 T.P. 23'

72+21 P.P.

272+23 C.M.P. 30'x15'
23' P.P. + V-rod

70+38 start fence

70+37 Tr. 26'

272+04 Tr. 23'

70+98 Tr. 32'

5th

269

268

267

266

265

264

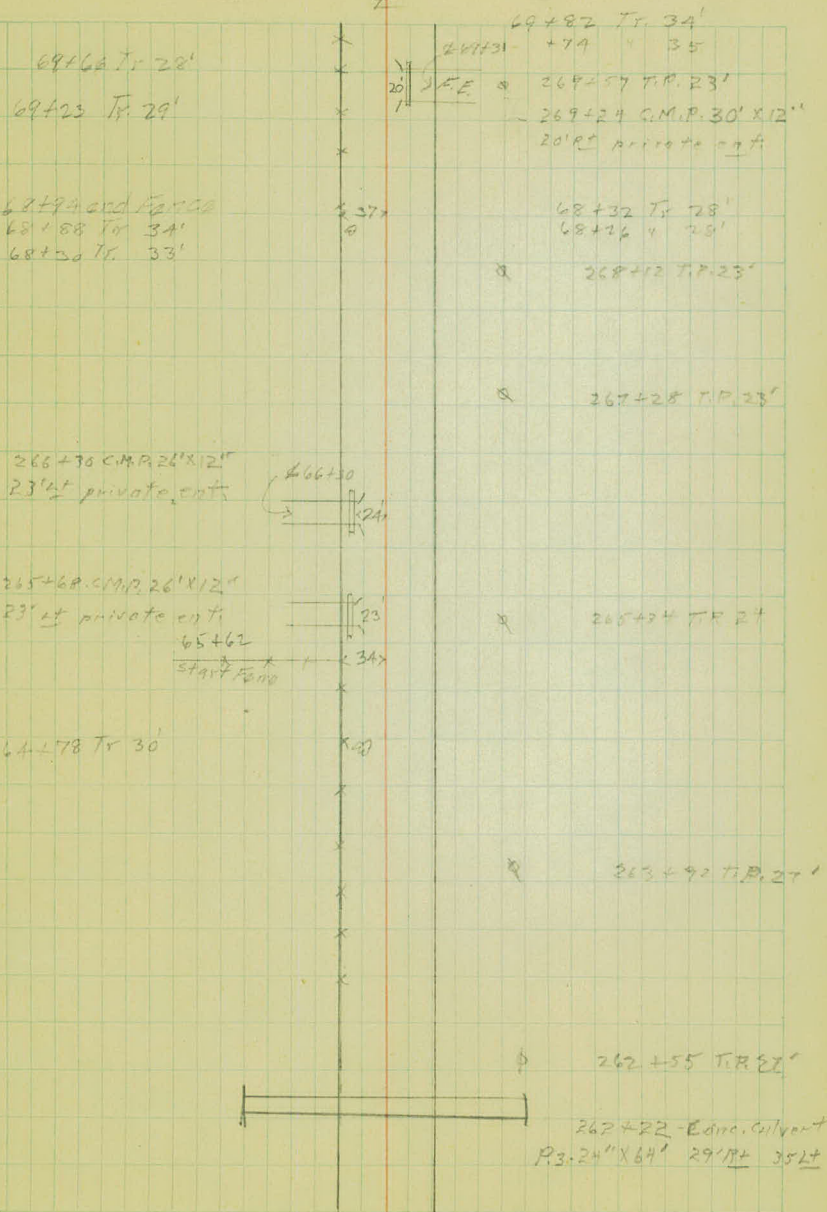
263

262

LT

±

RT



54a

261

260

259

258

257

256

255

254

LT & RT

	X		
60+84 Tr. 34	X 36' X	X	261+12 Tr. 28'
427 Tr. 32'	X		
	X		
	X		
59+64 Tr. 35'	X	X	259+69 Tr. 28'
	X		
	X		
58+66 Tr. 30'	X 36' X	X	258+25 Tr. 28'
57+45 Tr. 27'	X		
		X	256+86 Tr. 28'
		X	255+45 Tr. 28'
		X	254+08 Tr. 28'

24' FE. & ← 260+52 C.M.P. 26" x 12"
24' Field. Ent.

54d

253

252

251

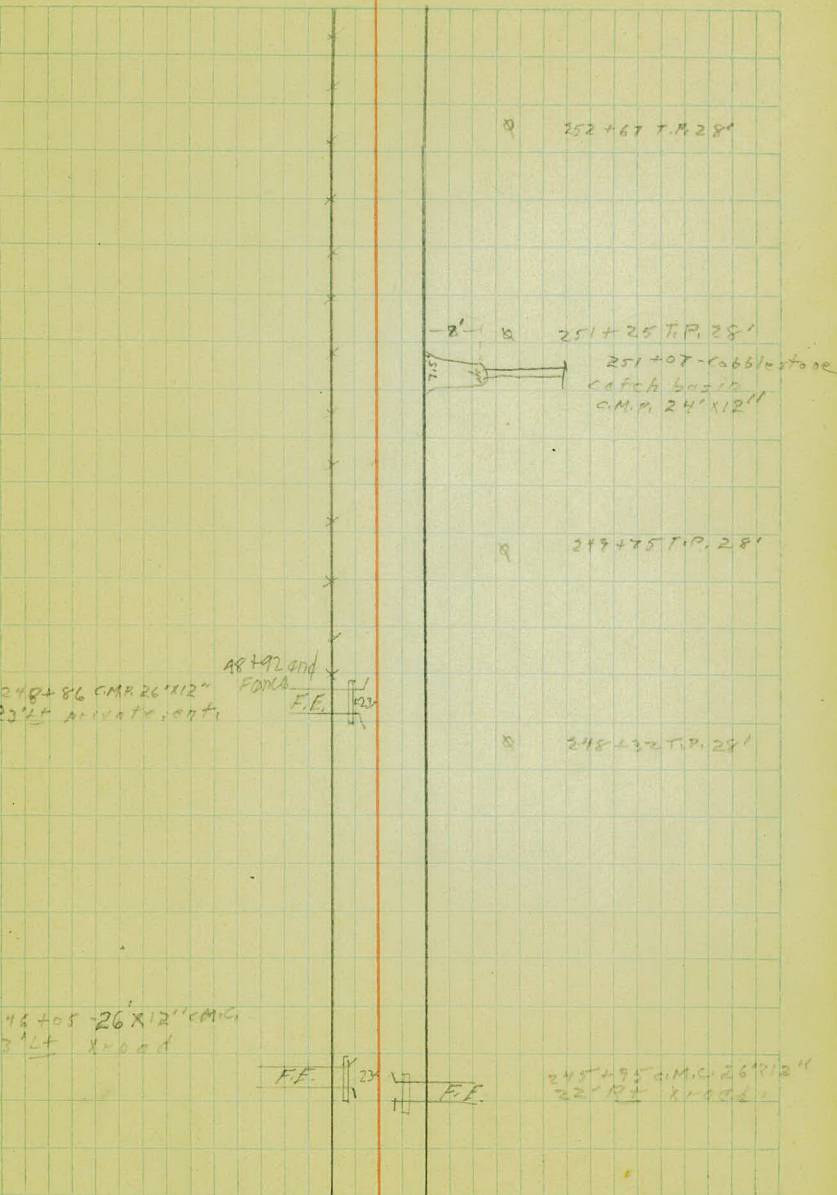
250

249

248

247

246



252+67 T.P. 28'

251+25 T.P. 28'
251+07 - Cobblestone
catch basin
C.M.C. 24" x 12"

249+75 T.P. 28'

248+86 C.M.C. 26" x 12"
23" LT x road
AR 192 and FDNCA
F.F.

248+32 T.P. 28'

245+95 C.M.C. 26" x 12"
22" RT x 12" C.M.C.

F.F.

245+95 C.M.C. 26" x 12"
22" RT x 12" C.M.C.

34a

245

244

243

242

241

240

239

238

Lt

±

Rt

45+75 Start new
Tracs 32

0
10
20
30
40
50
60
70
80
90
100
110
120
130
140
150
160
170
180
190
200
210
220
230
240
250
260
270
280
290
300
310
320
330
340
350

244+33 T.P. 28'

243+03 T.P. 28'

241+79 T.P. 28'

no cut-off



F.E.

241+50 C.M.P. 26+12"
23' Rt field cut.

240+43 T.P. 28'

239+15 T.P. 28'

and Tracs 35'

5th

237

236

235

234

233

231

230

229

237+85 T.P. 28'

236+52 T.P. 28'

235+25 T.P. 28'

234+00 T.P. 28'

232+63 T.P. 28'

32+10 F.M.C.O.

231+53 T.P. 28'

30+92

30+02

230+23 T.P. 25'

231+57 C.M.P. 26'x12"

20' LT private cut

F.E.

227

225

225

30+17

x

x

x

x

x

no cut

F.E.

229+56 C.M.P. 26'x12"

21' RT private cut

229+47 T.P. 26'

29+00 old F.M.C.O.

5 to

228

227

226

225

224

223

222

221

LT ♀ RT

26+70 School 15' LT
caution sign

⊙

⊙ 227+45 T.P. 27'

⊙ 226+18 T.P. 28'



ZE

225+14 C.M.P. 26" x 12"
22' RT field cut

⊙ 224+92 T.P.

✓

✗

✗

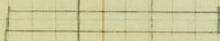
✓

✗

✗

⊙ 223+67 T.P. 28'

⊙ 222+42 T.P. 28'



222+17 conc. culvert
24" x 48' 25' LT 23' RT

⊙ 221+16 T.P. 28'

54a

220

219

218

217

216

215

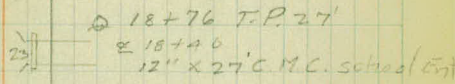
214

213

Lt Rt

19+47 C

131 County Rd sign P 23' ~~X~~
27 T.P. 34'



18+76 T.P. 27'

18+46
12'' x 28' C.M.C.



0015+96 T.P. 25' x 31'

14+50 T.P. 22'

13+32 school equation
sign 17'

5 Feb

212

211

210

209

208

207

206

205

0 12+97 T.P. 28'

0 11+55 T.P. 28'

0 10+32 T.P. 28'

0 8+92 T.P. 28'

2+76 Mail Box 0

8+50 & FE.	FE.	21
12" X 20.5" C.M.C.	FE.	22
	FE.	21

8+30 start Fane x
x 35'

Φ 207+54 T.P. 28'

x
x
x
x

Φ 206+10 T.P. 28'

5+85 start Fane 30' x
x 30'

0
0
0

Φ 204+73 T.P. 28'

5th

204

203

202

201

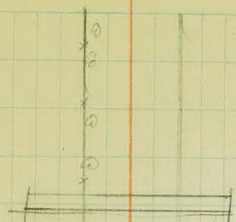
200

199

198

197

L E RT



x 203+27 T.P. 28'
 203+05 CONC. CH/VISIT
 24'x40' 19' RT 31' LT
 ORIGIN LT

x 201+92 T.P. 28'

x 200+47 T.P. 28'

x 199+05 T.P. 28'

48+80 end Trees 28'

x 241

x 197+65 T.P. 28'

x 196+25 T.P. 28'

540

196

195

194

193

192

191

190

189

574

188

187

186

185

184

183

182

181

LT & RT

2 in. Ft. curb. 75.5.9'

Q 187+85 T.P. 28'

Q 186+52 T.P. 28'

Q 185+19 T.P. 28'

Q 183+75 T.P.

183+68 Conc. spillway
8' X 3'
183+63 Beg. curb.



182+70 Conc culvert
24" X 48" - 22' Lt 26' Rt
Drains RT.

Q 182+48 T.P. 28'

81+78 Start
Form CQ



Q 181+16 T.P. 28'

570

180

179

178

177

176

175

174

173

LT & RT

180+16 Vit pipe, 17'x10"
25' Field ent. FE.

20'x

20+19
2nd Face
180+02 T.P. 30'

179+68 End curb.
179+61 Conc. spillway
8'x3' Rubble gutter 7'x3'

178+20 T.P. 30'

177+63 Vit. pipe.
18'x12" Field ent. II

177+63 T.P. 30'

Curb Lin. Ht. 58.18

176+42 T.P. 33'

175+25 T.P. 28'

173+90 T.P. 25'

173+90 T.P. 25'

173+61 C.M.P. 27'x12"
Field ent. FE.

173+80 End Curb.
173+56 C.M.P. 37'x12"
Field ent. FE.

old pipe

old pipe

370

172

171

170

169

168

167

166

165

LT RT

not placed
 172+19 C.M.P. 12'x15' II
 Field ent. $\frac{72+37}{549}$ start Field 33'

Q 172+79 T.P. 28'

171+84 conc culvert
 24" x 48" - 20' L - 28' RT,
 Drains RT.

Q 171+76 T.P. 28'

x
 x
 x
 x
 x

Q 170+56 T.P. 28'

Q 169+34 T.P. 28'

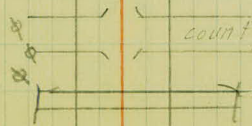
Q 168+12 T.P. 28'

Q 166+84 T.P. 28'

165+67 T.P. 16'
 165+59 T.P. 12'
 165+32 T.P. 16'

country Rd D.

165+03 conc. culvert
 24" x 40" - 21' L - 19' RT
 Drains RT



570

164

163

162

161

160

159

158

157

LT RT

164+65 T.P. 28'	φ	5	64+81 start trees 34
		8	
163+65 T.P. 28'	φ	6	163+77 T.P. 25'
		13	
162+62 T.P. 28'	φ	0	
		0	62+06 end trees 34
		0	162+56 T.P. 25'
161+63 T.P. 28'	φ		
			161+48 T.P. 23'
160+74 T.P. 28'	φ		
			160+25 T.P. 23'
159+75 T.P. 28'	φ		
			159+18 T.P. 26'
158+72 T.P. 28'	φ		
157+69 T.P. 28'	φ		

58+50
X X

130' 157+31 Fence
F.E.
157+87 T.P. 25'
157+78 C.M.P. 26'x12'
23' RT field entrance

374

156

155

154

153

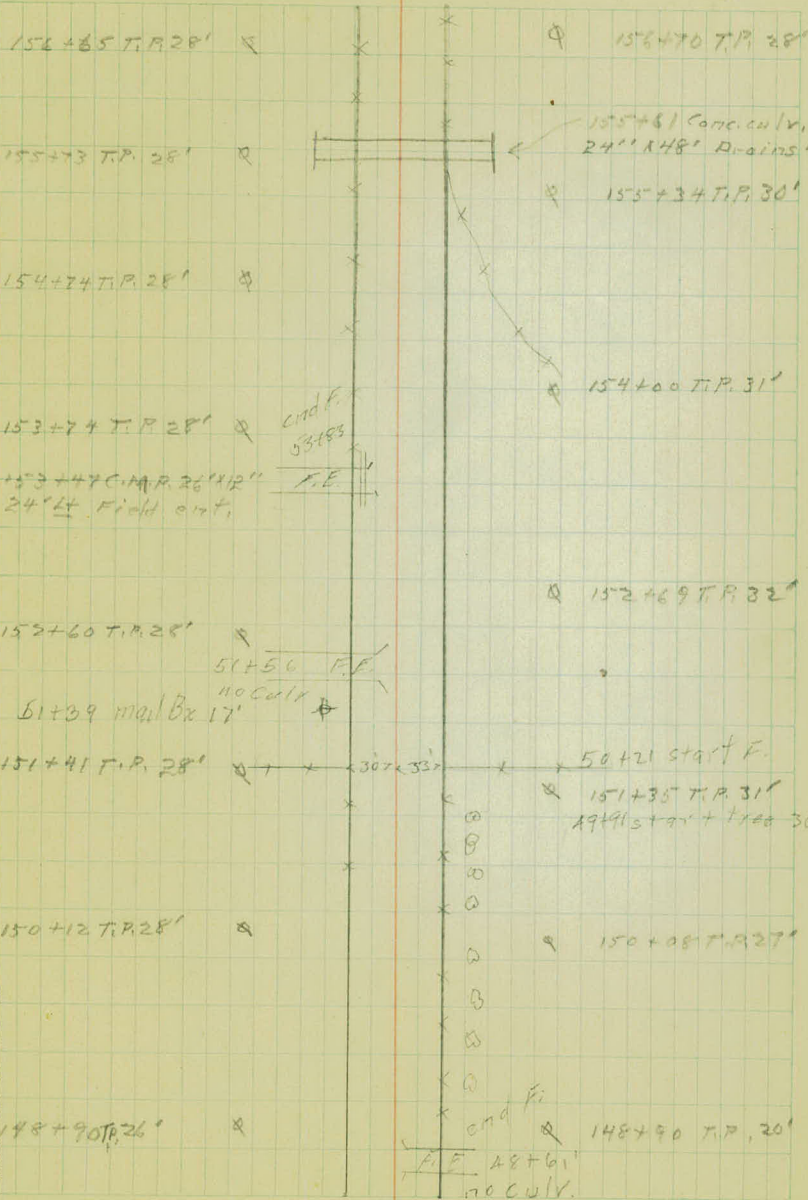
152

151

150

149

1st of RT



155+85 T.P. 28'

156+70 T.P. 28'

155+73 T.P. 28'

155+81 Correc. culv.,
24" x 48" Drains Left.

155+34 T.P. 30'

154+74 T.P. 28'

154+00 T.P. 31'

153+74 T.P. 28'

cmd. F.
53183

153+47 C.M.R. 26 1/2"
24" x 48" Field out.

F.E.

152+69 T.P. 32'

155+60 T.P. 28'

51+56 F.E.
110 Culv.

51+39 mail Bx 17'

151+41 T.P. 28'

307 x 337

50+21 start F.

151+35 T.P. 31'
19191 start + 1900 30'

150+12 T.P. 28'

150+08 T.P. 27'

148+90 T.P. 26'

cmd. Fi

148+90 T.P. 20'

F.E. 48+61
no culv.

Sta

148

1

147

146

145

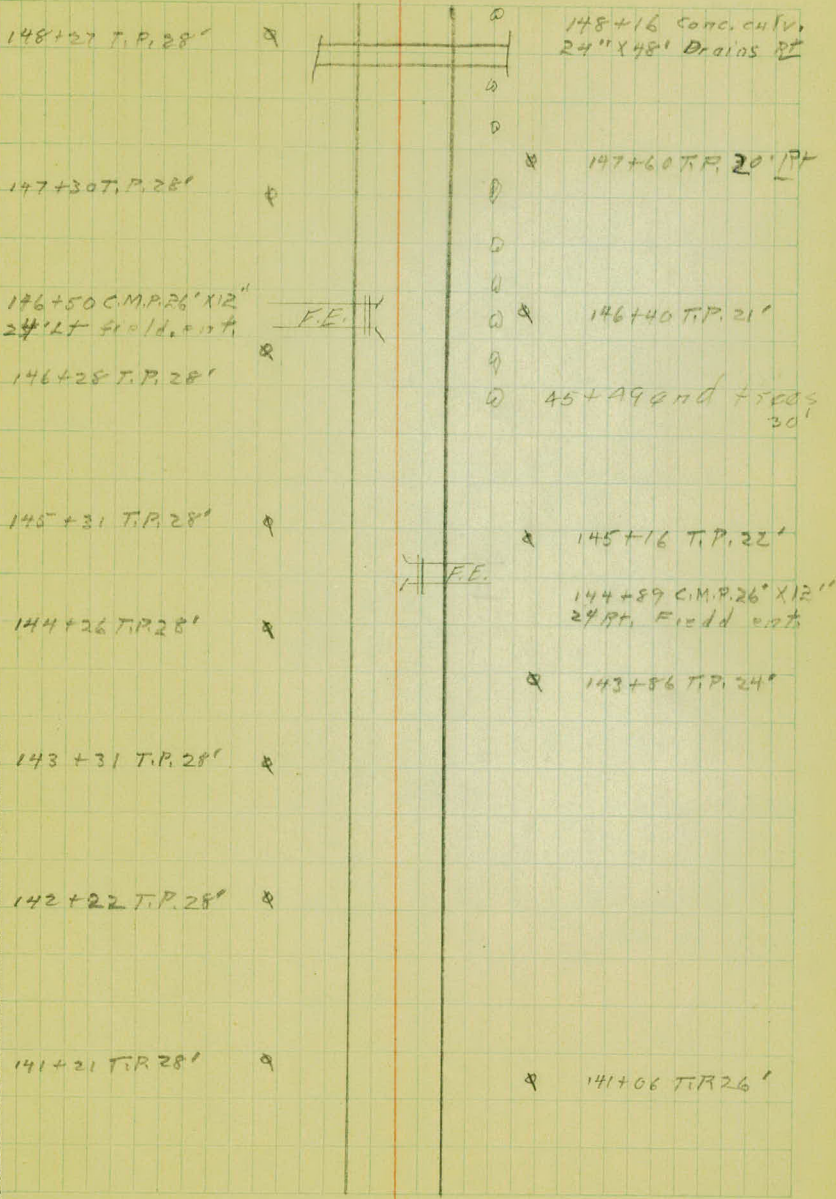
144

143

142

141

LT & RT



148+37 T.P. 28'

148+16 Conc. curv.
24" X 48' Drains RT

147+30 T.P. 28'

147+60 T.P. 20' RT

146+50 C.M.P. 26' X 12"
24' LT Field, end

FE.

146+40 T.P. 21'

146+28 T.P. 28'

45+49 end of road
30'

145+31 T.P. 28'

145+16 T.P. 22'

FE.

144+26 T.P. 28'

144+89 C.M.P. 26' X 12"
24' RT Field end

143+31 T.P. 28'

143+86 T.P. 24'

142+22 T.P. 28'

141+21 T.P. 28'

141+06 T.P. 26'

570

140

139

138

137

136

135

134

133

sta

132

131

130

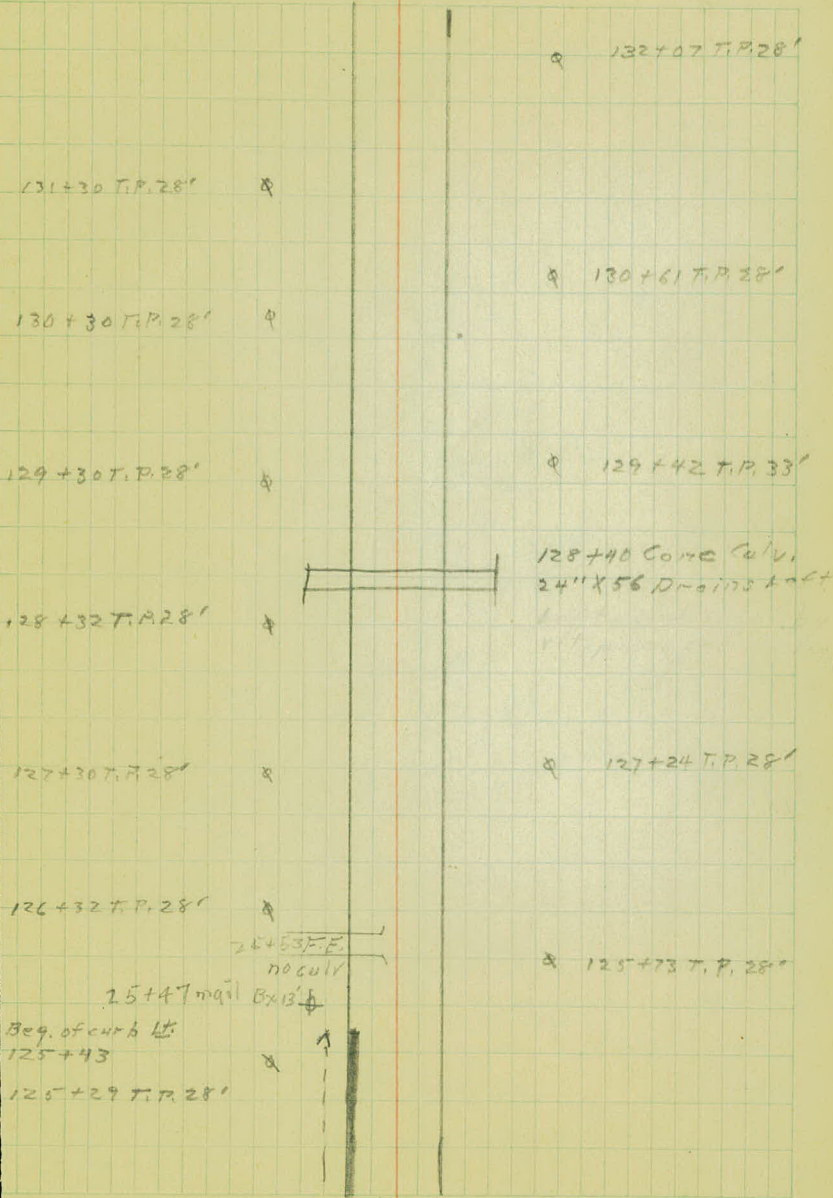
129

128

127

126

125



57a

124

123

122

121

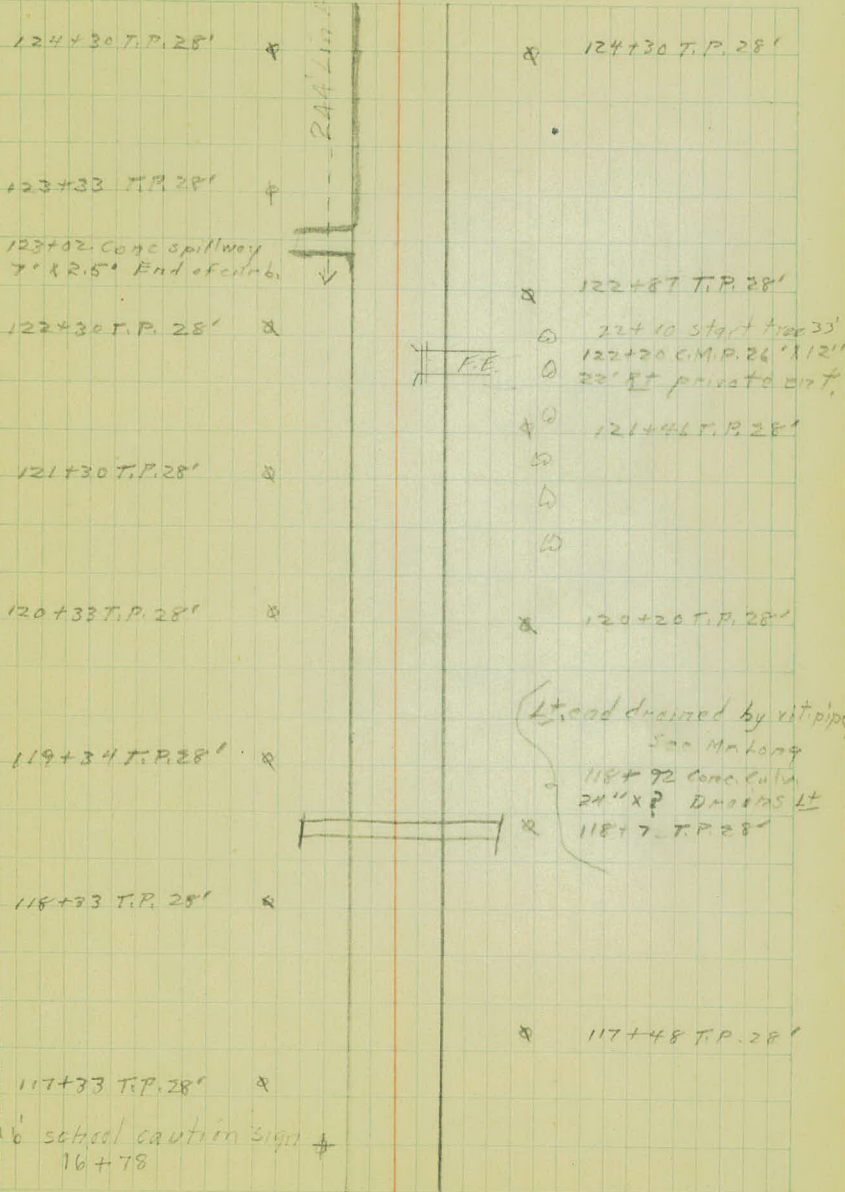
120

119

118

117

LT E RT



124+30 T.P. 28' x

x 124+30 T.P. 28'

123+33 T.P. 28' x

123+02 Conc spillway
7' x 2.5' End of curb

x 122+87 T.P. 28'

122+30 T.P. 28' x

o 22+10 start tree 33'

o 122+20 C.M.P. 26' x 12"

o 22' x 8' private dirt

121+30 T.P. 28' x

x 121+44 T.P. 28'

120+33 T.P. 28' x

x 120+20 T.P. 28'

119+34 T.P. 28' x

118+92 Conc. Culv.
24" x 8" D.M. 1/15 LT

118+7 T.P. 28'

118+33 T.P. 28' x

x 117+48 T.P. 28'

117+33 T.P. 28' x

6' school caution sign +
16+78

54d

116

115

114

113

112

111

110

109

LT & RT

116+34 T.P. 28' Q

Q 116+17 T.P. 30'

115+35 T.P. 28' Q

Q 114+78 T.P. 29'

114+33 T.P. 28' Q

Q 113+43 T.P. 29'

113+34 T.P. 28' Q

112+34 T.P. 28' Q

111+64 T.P. 28' Q

Q 111+88 T.P. 28'

111+64 C.M.P. 26' X 12'
21' RT school entry

111+01 T.P. 28' Q

Q 110+01 T.P. 28'

± 10+62 noculr.

Co. Rd. C 10+42 T.P. 27'

10+30 P.P. 27' Q

9+75 Guy P. 28' O

19' F.E. 9+68

12' X 26' C.M.C.

O 9+51 T.P. 28'

374

108

107

106

105

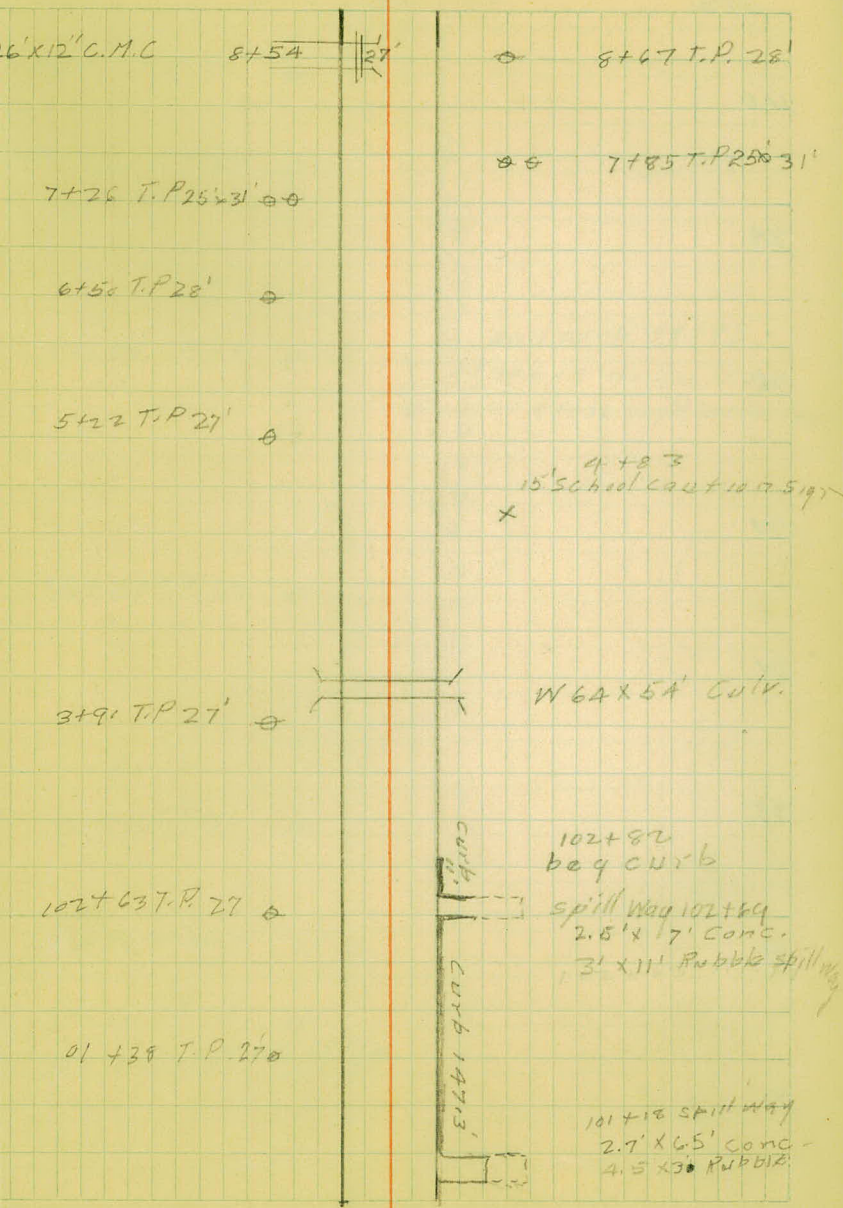
104

103

102

101

Lt & Rt



6'x12' C.M.C

8+54

27'

8+67 T.P. 28'

7+26 T.P. 25x31

7+85 T.P. 25x31

6+50 T.P. 28'

5+22 T.P. 27'

4+83
15' School Caut 107.519'
x

3+9 T.P. 27'

W 6 X 5' CULV.

102+63 T.P. 27

Curb

102+82
bag CURB

spill way 102+69
2.5' x 17' CONC.

3' x 11' Rubble spill way

01+38 T.P. 27

Curb 14713

101+18 spill way
2.7' x 6.5' CONC. -
4.5' x 3' Rubble.

61

60

59

8

7

6

5

4

3

2

1

50

49

8

7

6

5

4

3

2

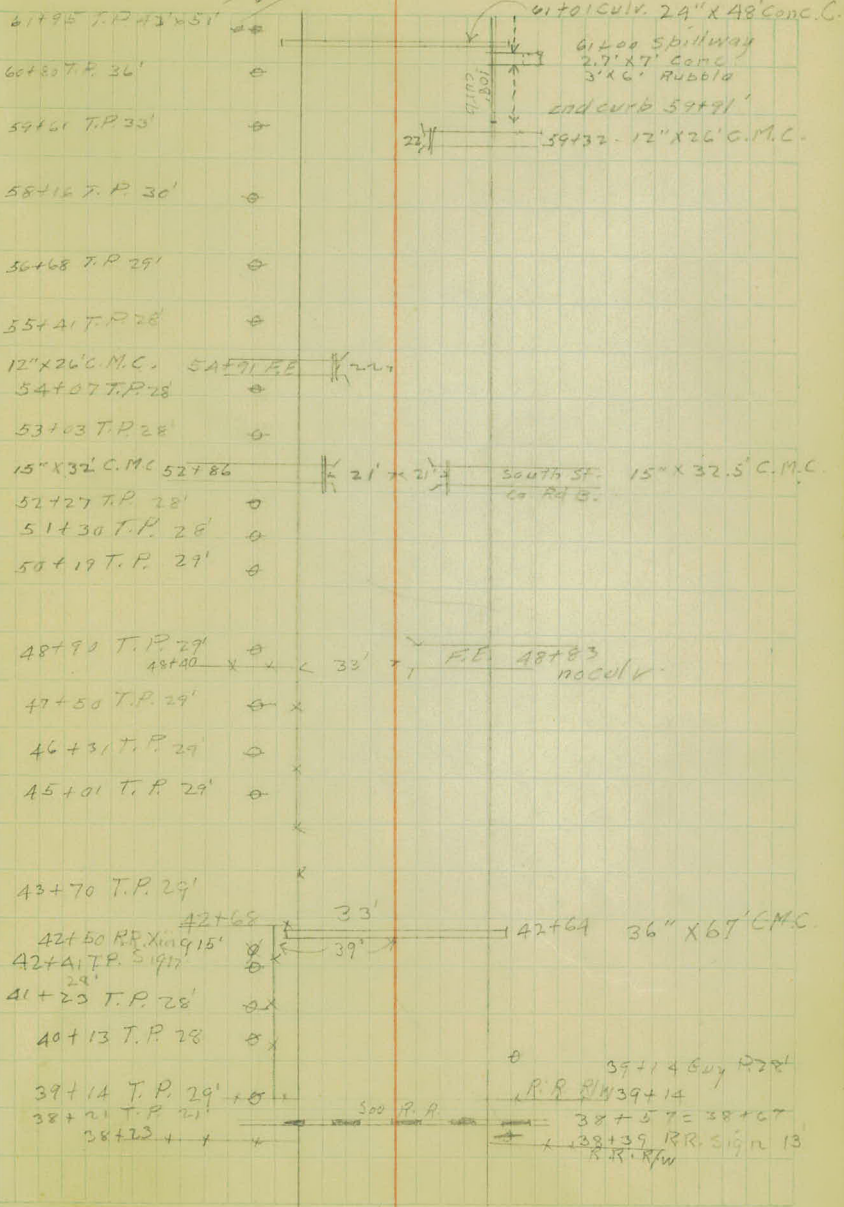
1

40

39

8

White Bear Ave
62+00



37

6

5

4

3

2

1

30

29

28

27

6

5

4

3

2

1

20

19

8

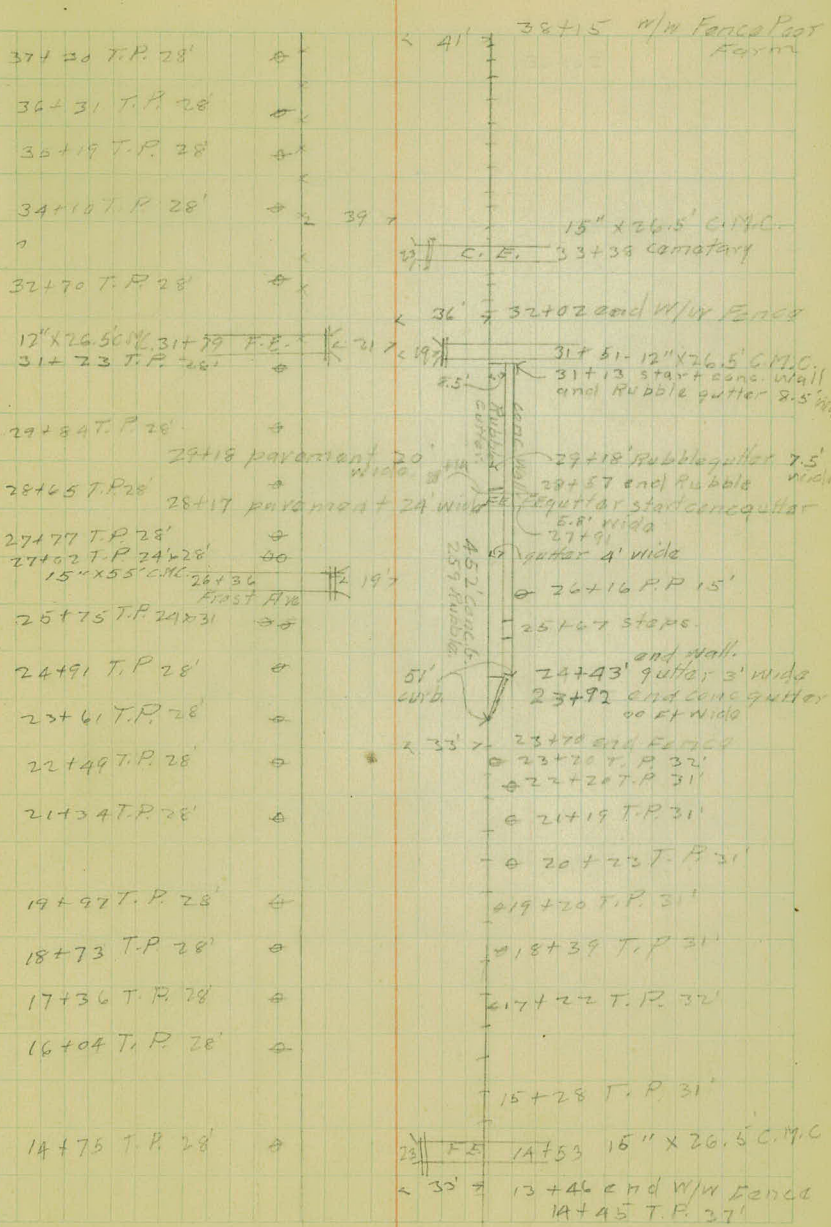
7

6

5

4

3



37+20 T.P. 28'

36+31 T.P. 28'

35+19 T.P. 28'

34+10 T.P. 28'

32+70 T.P. 28'

12" x 26.5' C.M.C. 31+79 F.E.

31+23 T.P. 28'

29+84 T.P. 28'

28+65 T.P. 28'

27+77 T.P. 28'

27+02 T.P. 24' x 28'

25+75 T.P. 24 x 31

24+91 T.P. 28'

23+61 T.P. 28'

22+49 T.P. 28'

21+34 T.P. 28'

19+97 T.P. 28'

18+73 T.P. 28'

17+36 T.P. 28'

16+04 T.P. 28'

14+75 T.P. 28'

38+15 w/w Fence Post Farm

39'

15" x 26.5' C.M.C.

C.E. 33+39 cemetery

36' 32+02 end w/w Fence

31' x 19'

31+51- 12" x 26.5' C.M.C.

31+13 start conc. wall and Rubble gutter 8.5' wide

29+18 pavement 20' wide

29+18' Rubble gutter 7.5' wide

28+17 pavement 24' wide

29+57 end Rubble gutter start conc gutter 5.8' wide

28+36 Frost Ave

27+91 gutter 4' wide

19'

26+16 P.P. 15'

25+67 steps and Hall

24+43' gutter 3' wide

23+92 end conc gutter 00 ft wide

23+78 end F.E. 28'

23+70 T.P. 32'

22+20 T.P. 31'

21+19 T.P. 31'

20+23 T.P. 31'

19+20 T.P. 31'

18+39 T.P. 31'

17+22 T.P. 32'

15+28 T.P. 31'

23' F.E.

14+53 15" x 26.5' C.M.C.

13+46 end w/w Fence

14+45 T.P. 37'

13

12

11

10

9

8

7

6

5

4

3

2

1

0

-33 end Pavement.

13+30 T.P. 25x31' 0+

old.
N.S.F. Rd ← 13+24

12+80 T.P. 28' 0

10+60 T.P. 28' 0

9+22 T.P. 28' 0

7+96 T.P. 28' 0

6+61 T.P. 28' 0

5+35 T.P. 28' 0

3+18 Gup.P. 20' 0

2+68 T.P. 28' 0
2+16 Gup.P. 21' 0

1+23 T.P. 28' 0

0+58 T.P. 21-28 0+

0+44 T.P. 28' 0

0-23 T.P. 28' Latpore Ave

NEW N.S.F. Rd.

4+33 Gup.P.

3+25

0 2+18 P.P. 27'

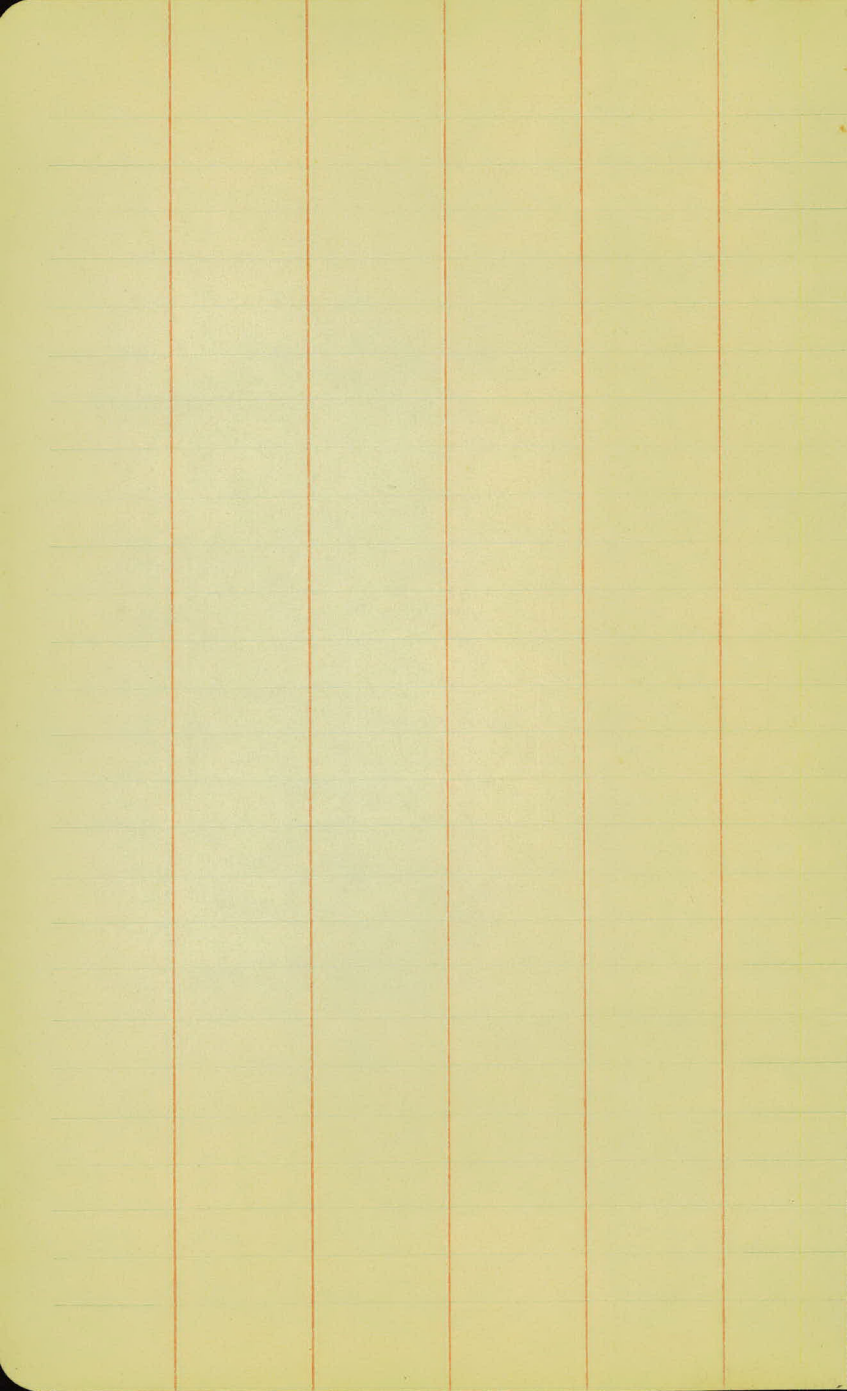
1+19 P.P. 27'

0+22 P.P. 27'

24" X 48' CONC. CURB

4 0+00

0-23 T.P. 27'



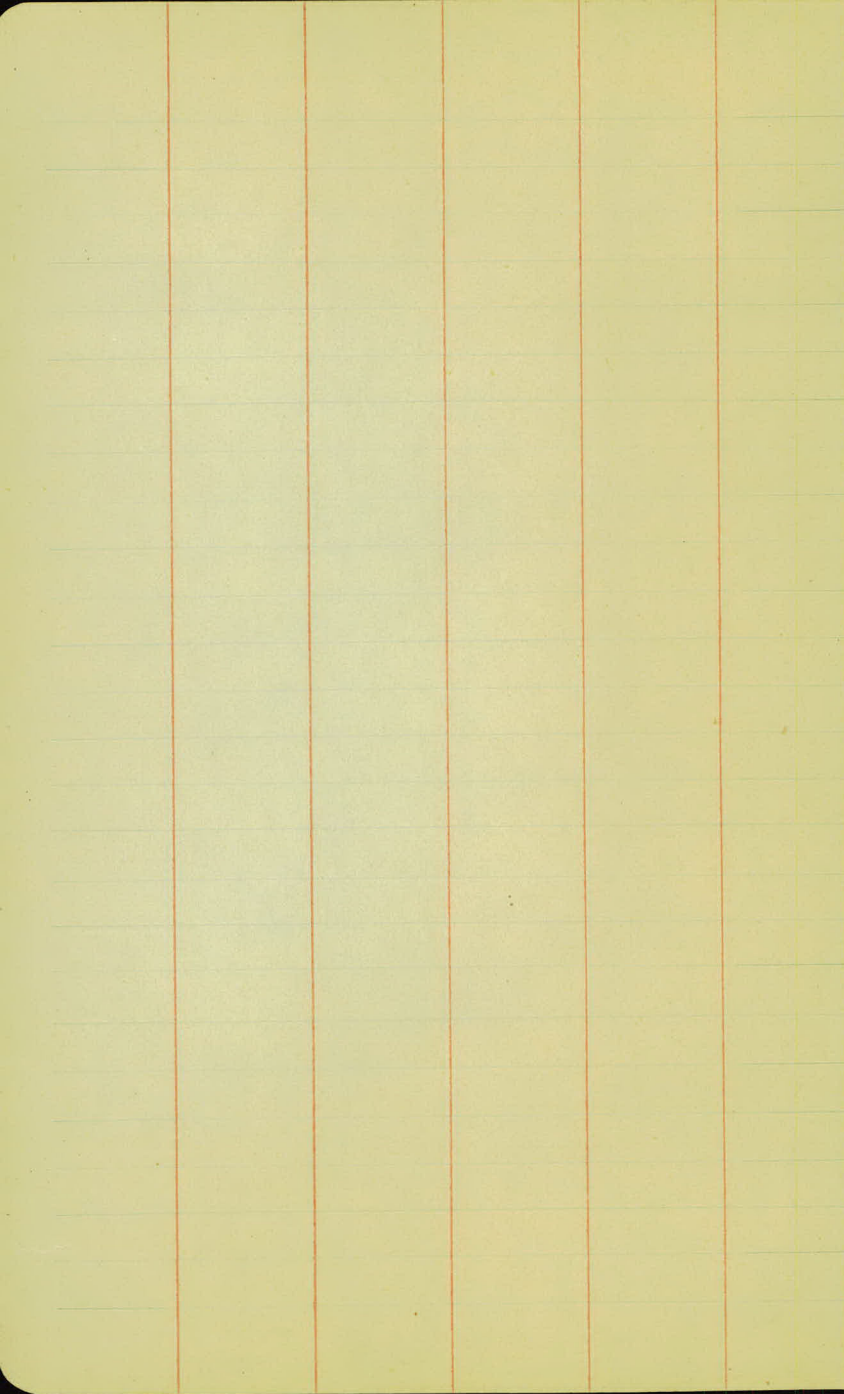
31413

23492

7121

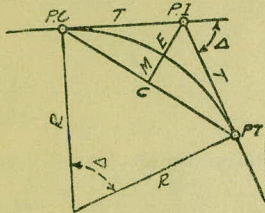
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DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

Radius= $R = \frac{50}{\sin. \frac{D}{2}}$ (1) Degree of Curve= D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos. \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos. \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin. \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C.=Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.=Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158—Sta. P. C. = 54.50, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 91.27$ and from Table V correction = .10 or $E = 91.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

TABLE I.—MINUTES IN DECIMALS OF A DEGREE.

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

TABLE II.—INCHES IN DECIMALS OF A FOOT.

1-16	3-32	1/8	3-16	1/4	5-16	3/8	1/2	5/8	3/4	7/8
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III.—RADI, ORDINATES AND DEFLECTIONS.

Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Offset	Def. for 1 Foot
0° 10'	34377.5	.036	.145	0.05'	7°	819.02	1.528	6.105	2.10'
20	17188.8	.073	.291	0.10	20'	781.84	1.600	6.395	2.20
30	11459.2	.109	.436	0.15	30	764.49	1.637	6.540	2.25
40	8594.42	.145	.582	0.20	40	747.89	1.673	6.685	2.30
50	6875.55	.182	.727	0.25					
1					8	716.78	1.746	6.976	2.40
10	5729.65	.218	.873	0.30	20	688.16	1.819	7.266	2.50
20	4911.15	.255	1.018	0.35	30	674.69	1.855	7.411	2.55
30	4297.28	.291	1.164	0.40	40	661.74	1.892	7.556	2.60
40	3819.83	.327	1.309	0.45					
50	3437.87	.364	1.454	0.50	9	637.28	1.965	7.846	2.70
	3125.36	.400	1.600	0.55	20	614.56	2.037	8.136	2.80
2					30	603.80	2.074	8.281	2.85
10	2864.93	.436	1.745	0.60	40	593.42	2.110	8.426	2.90
20	2644.58	.473	1.891	0.65					
30	2455.70	.509	2.036	0.70	10	573.69	2.183	8.716	3.00
40	2292.01	.545	2.181	0.75	30	546.44	2.292	9.150	3.15
50	2148.79	.582	2.327	0.80	11	521.67	2.402	9.585	3.30
	2022.41	.618	2.472	0.85	30	499.06	2.511	10.02	3.45
3					12	478.34	2.620	10.45	3.60
10	1910.08	.655	2.618	0.90	30	459.28	2.730	10.89	3.75
20	1809.57	.691	2.763	0.95	13	441.68	2.839	11.32	3.90
30	1719.12	.727	2.908	1.00	30	425.40	2.949	11.75	4.05
40	1637.28	.764	3.054	1.05	14	410.28	3.058	12.18	4.20
50	1562.88	.800	3.199	1.10	30	396.20	3.168	12.62	4.35
	1494.95	.836	3.345	1.15					
4					15	383.07	3.277	13.05	4.50
10	1432.69	.873	3.490	1.20	30	370.78	3.387	13.49	4.65
20	1375.40	.909	3.635	1.25	16	359.27	3.496	13.92	4.80
30	1322.53	.945	3.718	1.30	30	348.45	3.606	14.35	4.95
40	1273.57	.982	3.926	1.35	17	338.27	3.716	14.78	5.10
50	1228.11	1.018	4.071	1.40	18	319.62	3.935	15.64	5.40
	1185.78	1.055	4.217	1.45	19	302.94	4.155	16.51	5.70
5					20	287.94	4.374	17.37	6.00
10	1146.28	1.091	4.362	1.50	21	274.37	4.594	18.22	6.30
20	1109.33	1.127	4.507	1.55	22	262.04	4.814	19.08	6.60
30	1074.68	1.164	4.653	1.60	23	250.79	5.035	19.94	6.90
40	1042.14	1.200	4.798	1.65	24	240.49	5.255	20.79	7.20
50	1011.51	1.237	4.943	1.70					
	982.64	1.273	5.088	1.75	25	231.01	5.476	21.64	7.50
6					26	222.27	5.697	22.50	7.80
10	955.37	1.309	5.234	1.80	27	214.18	5.918	23.35	8.10
20	929.57	1.346	5.379	1.85	28	206.68	6.139	24.19	8.40
30	905.13	1.382	5.524	1.90	29	199.70	6.360	25.04	8.70
40	881.95	1.418	5.669	1.95	30	193.18	6.583	25.88	9.00
	859.92	1.455	5.814	2.00					

Note. Chord Deflection=2 times tangent deflection.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
1°	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
2	100.01	.87	12	602.21	31.56	22	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3	150.04	1.96	13	652.81	37.07	23	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4	200.08	3.49	14	703.51	43.03	24	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5	250.16	5.46	15	754.32	49.44	25	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6	300.28	7.86	16	805.25	56.31	26	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7	350.44	10.71	17	856.30	63.63	27	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8	400.66	13.99	18	907.49	71.42	28	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9	450.93	17.72	19	958.81	79.67	29	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10	501.28	21.89	20	1010.3	88.39	30	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
31°	1589.0	216.3	41°	2142.2	387.4	51°	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
32	1643.0	230.9	42	2199.4	407.6	52	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
33	1697.2	246.1	43	2257.0	428.5	53	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
34	1751.7	261.8	44	2314.9	450.0	54	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
35	1806.6	278.1	45	2373.3	472.1	55	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.8	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
36	1861.7	294.9	46	2432.1	494.8	56	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
37	1917.1	312.2	47	2491.3	518.2	57	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
38	1972.9	330.2	48	2551.0	542.2	58	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
39	2029.0	348.6	49	2611.2	566.9	59	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
40	2085.4	367.7	50	2671.8	592.3	60	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
61°	3375.0	920.2	71°	4086.9	1308.2	81°	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
62	3442.7	954.8	72	4162.8	1352.6	82	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
63	3511.1	990.2	73	4239.7	1398.0	83	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
64	3580.3	1026.6	74	4317.6	1444.6	84	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
65	3650.2	1063.9	75	4396.5	1492.4	85	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
66	3720.9	1102.2	76	4476.5	1541.4	86	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
67	3792.4	1141.4	77	4557.6	1591.6	87	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
68	3864.7	1181.6	78	4639.8	1643.0	88	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
69	3937.9	1222.7	79	4723.2	1695.8	89	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
70	4011.9	1265.0	80	4807.7	1749.9	90	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
91°	5830.5	2444.9	101°	6950.6	3278.1	111°	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.2	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
92	5933.2	2518.5	102	7075.5	3374.9	112	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
93	6037.8	2594.0	103	7203.2	3474.4	113	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.5	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
94	6144.3	2671.6	104	7333.6	3576.8	114	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
95	6252.8	2751.3	105	7467.0	3682.3	115	8993.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.8
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
96	6363.4	2833.2	106	7603.5	3791.0	116	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
97	6476.2	2917.3	107	7743.2	3902.9	117	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
98	6591.2	3003.8	108	7886.2	4018.2	118	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
99	6708.6	3092.7	109	8032.7	4137.1	119	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	5808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
100	6828.3	3184.1	110	8182.8	4259.7	120	9924.0	5729.7
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

TABLE V.—CORRECTIONS FOR TANGENTS AND EXTERNALS.

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table IV) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.297	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.891	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

TABLE VI.--CORRECTIONS FOR SUB-CHORDS AND LONG CHORDS.

FOR SUB-CHORDS ADD										Excess of arc per 100 ft.	LONG CHORDS				
D	10	20	30	40	50	60	70	80	90		D	200	300	400	500
4°	.00	.00	.01	.01	.01	.01	.01	.01	.06	.02	1	199.99	299.97	399.92	499.85
6	.00	.01	.01	.02	.02	.02	.02	.01	.01	.05	2	199.97	299.88	399.70	499.39
8	.01	.02	.02	.03	.03	.03	.03	.02	.01	.08	3	199.93	299.73	399.32	498.63
10	.01	.02	.03	.04	.05	.05	.05	.04	.02	.13	4	199.88	299.51	398.78	497.57
12	.02	.04	.05	.06	.07	.07	.07	.05	.03	.18	5	199.81	299.24	398.10	496.20
14	.02	.05	.07	.08	.09	.10	.09	.07	.04	.25	6	199.73	298.90	397.26	494.53
16	.03	.06	.09	.11	.12	.12	.12	.09	.05	.33	7	199.63	298.51	396.28	492.57
18	.04	.08	.11	.14	.15	.16	.15	.12	.07	.41	8	199.51	298.05	395.14	490.31
20	.05	.10	.14	.17	.19	.20	.18	.15	.09	.51	9	199.38	297.54	393.86	487.75
22	.06	.12	.17	.21	.23	.24	.22	.18	.10	.62	10	199.24	296.96	392.42	484.90
24	.07	.14	.20	.25	.28	.28	.26	.21	.12	.74	12	198.90	295.63	389.12	478.34
26	.09	.17	.24	.29	.32	.33	.31	.25	.15	.86	14	198.51	294.06	385.22	470.65
28	.10	.19	.27	.34	.37	.38	.36	.29	.17	1.00	16	198.05	292.25	380.76	461.86
30	.11	.22	.31	.39	.43	.44	.41	.33	.19	1.15	18	197.54	290.21	375.74	452.02
32	.13	.25	.36	.44	.49	.50	.47	.38	.22	1.31	20	196.96	287.94	370.17	441.15
34	.15	.28	.40	.50	.55	.57	.53	.43	.25	1.48	22	196.32	285.44	364.06	429.30
36	.17	.32	.45	.56	.62	.64	.59	.48	.28	1.66	24	195.63	282.71	357.43	416.53
38	.18	.36	.51	.62	.70	.71	.66	.53	.31	1.86	26	194.87	279.76	350.30	402.89
40	.21	.40	.56	.69	.77	.79	.73	.59	.35	2.06	28	194.06	276.59	342.69	388.43
42	.23	.44	.62	.76	.85	.87	.81	.65	.38	2.28	30	193.18	273.20	334.61	373.20
44	.25	.48	.68	.84	.94	.96	.89	.72	.42	2.50	32	192.25	269.61	326.08	357.28
46	.27	.52	.75	.92	1.02	1.05	.98	.78	.46	2.74	34	191.26	265.81	317.12	340.73
48	.30	.57	.81	1.00	1.12	1.14	1.06	.86	.50	2.99	36	190.21	261.80	307.77	323.61
50	.32	.62	.89	1.09	1.21	1.24	1.15	.93	.55	3.24	38	189.10	257.60	298.03	305.99
52	.35	.67	.96	1.18	1.31	1.35	1.25	1.01	.59	3.52	40	187.94	253.21	287.94	287.94
54	.38	.73	1.04	1.28	1.42	1.46	1.35	1.09	.64	3.80	42	186.72	248.63	277.51	269.54
56	.41	.78	1.12	1.38	1.53	1.57	1.46	1.17	.69	4.09	44	185.44	243.87	266.78	250.85
58	.44	.84	1.20	1.48	1.65	1.69	1.57	1.26	.74	4.40	46	184.10	239.93	255.78	231.95
60	.47	.91	1.29	1.59	1.76	1.81	1.68	1.35	.80	4.72	48	182.71	233.83	244.51	212.92

NOTE.—When a chord of less than 100 ft. is used the corrections given in the above table should be added to the nominal length of chord to get the length which should be used in order that the 100 ft. points will check with those obtained by using the standard 100 ft. chord. Thus in locating a 14° curve by 25 ft. chords measure 25'06 for each chord. Long chords are useful in passing obstacles.

TABLE VII.--MIDDLE ORDINATES FOR RAILS IN FEET.

Deg. of Curve	LENGTH OF RAILS						Deg. of Curve	LENGTH OF RAILS.							
	32	30	28	26	24	22		32	30	28	26	24	22	20	
1°	.022	.020	.016	.013	.011	.009	.008	16°	.356	.313	.273	.236	.200	.170	.139
2	.045	.038	.034	.029	.025	.021	.017	17	.378	.333	.290	.252	.213	.180	.148
3	.037	.058	.051	.044	.037	.031	.026	18	.400	.351	.306	.265	.225	.190	.156
4	.089	.079	.069	.060	.050	.042	.035	19	.423	.371	.324	.280	.238	.201	.165
5	.112	.099	.086	.074	.063	.053	.044	20	.445	.392	.341	.296	.250	.212	.174
6	.134	.117	.102	.088	.076	.064	.052	21	.466	.410	.357	.309	.262	.222	.182
7	.156	.137	.120	.104	.088	.074	.061	22	.487	.430	.375	.325	.275	.233	.191
8	.179	.158	.137	.119	.100	.085	.070	23	.509	.450	.390	.338	.287	.243	.199
9	.201	.175	.153	.133	.112	.095	.078	24	.531	.469	.408	.354	.299	.253	.208
10	.223	.196	.171	.148	.125	.106	.087	25	.552	.486	.424	.367	.311	.263	.216
11	.245	.216	.188	.163	.139	.117	.096	26	.573	.506	.441	.382	.323	.274	.225
12	.268	.236	.206	.179	.151	.128	.105	27	.594	.524	.457	.396	.335	.284	.233
13	.290	.254	.222	.192	.163	.138	.113	28	.618	.545	.475	.411	.348	.294	.242
14	.312	.275	.239	.207	.175	.148	.122	29	.638	.564	.491	.424	.361	.303	.250
15	.334	.295	.257	.223	.188	.159	.131	30	.660	.583	.508	.438	.374	.313	.259

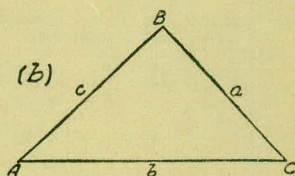
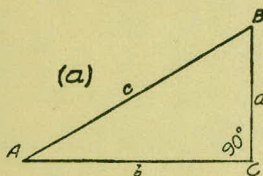
SLOPE REDUCTIONS.

When distances are measured on a slope they may be reduced to the equivalent horizontal distance by the following approximate rule:—subtract from the slope distance the square of the rise divided by twice the slope distance. Thus for a slope distance of 250.3 ft. and a rise of 15 ft. correction= $15^2 \div 2 \times 250.3 = .45$ (by slide rule) or horizontal distance= $250.3 - .45 = 249.85$. When vertical angle= $V. A.$ is measured horizontal distance= $\text{slope distance} - \text{slope distance} (1 - \text{Cos. } V. A.)$. Thus for slope distance of 248.7 ft. and $V. A.$ of $4^\circ 20'$ from Table VIII $\text{Cos.} = .99714$ and correction= $1 - .99714 = .00286$ per foot or total of $.286 \times 2\frac{1}{2}$ (near enough) = .57 and horizontal distance= $248.7 - .57 = 248.13$ ft.

See fig. (a).

TRIGONOMETRICAL FORMULAS.

$$\begin{aligned} \sin. & A = \frac{a}{c} \\ \cos. & A = \frac{b}{c} \\ \tan. & A = \frac{a}{b} \\ \cot. & A = \frac{b}{a} \\ \sec. & A = \frac{c}{b} \\ \text{cosec.} & A = \frac{c}{a} \end{aligned}$$



FORMULA FOR SOLVING TRIANGLES.

Given	Sought.	Right triangles. See fig. (a).
a, c	A, B, b	$\sin. A = \frac{a}{c}, \cos. B = \frac{a}{c}, b = \sqrt{(c+a)(c-a)}$
a, b	A, B, c	$\tan. A = \frac{a}{b}, \cot. B = \frac{a}{b}, c = \sqrt{a^2 + b^2}$
A, a	B, b, c	$B = 90^\circ - A, b = a \cot. A, c = \frac{a}{\sin. A}$
A, b	B, a, c	$B = 90^\circ - A, a = b \tan. A, c = \frac{b}{\cos. A}$
A, c	B, a, b	$B = 90^\circ - A, a = c \sin. A, b = c \cos. A$

Given	Sought.	Oblique triangles. See fig. (b).
A, B, a	b	$b = \frac{a \sin. B}{\sin. A}$
A, a, b	B	$\sin. B = \frac{b \sin. A}{a}$
a, b, C	$A - B$	$\tan. \frac{1}{2}(A - B) = \frac{(a - b) \tan. \frac{1}{2}(A + B)}{a + b}$
a, b, c	A	$\left\{ \begin{aligned} \text{If } s = \frac{1}{2}(a + b + c), \sin. \frac{1}{2} A &= \sqrt{\frac{(s-b)(s-c)}{bc}} \\ \cos. \frac{1}{2} A &= \sqrt{\frac{s(s-a)}{bc}}, \tan. \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}} \\ \sin. A &= \frac{2\sqrt{s(s-a)(s-b)(s-c)}}{bc} \end{aligned} \right.$
A, B, C, a	area	$\text{area} = \frac{a^2 \sin. B \sin. C}{2 \sin. A}$
A, b, c	area	$\text{area} = \frac{1}{2} b c \sin. A$
a, b, c	area	$s = \frac{1}{2}(a + b + c), \text{area} = \sqrt{s(s-a)(s-b)(s-c)}$

TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.		Angle	Sine.	Tan.	Cotg.	Cosin.	
0	0	0	∞	1	90	8	.1392	.1405	7.115	.99027	82
10	.0029	.0029	343.8	1	50	10	.1421	.1435	6.968	.98986	50
20	.0058	.0058	171.9	.99998	40	20	.1449	.1465	6.827	.98944	40
30	.0087	.0087	114.6	.99996	30	30	.1478	.1495	6.691	.98902	30
40	.0116	.0116	85.94	.99993	20	40	.1507	.1524	6.561	.98858	20
50	.0145	.0145	68.75	.99989	10	50	.1536	.1554	6.435	.98814	10
1	.0175	.0175	57.29	.99985	89	9	.1564	.1584	6.314	.98769	81
10	.0204	.0204	49.10	.99979	50	10	.1593	.1614	6.197	.98723	50
20	.0233	.0233	42.96	.99973	40	20	.1622	.1644	6.084	.98676	40
30	.0262	.0262	38.19	.99966	30	30	.1650	.1673	5.976	.98629	30
40	.0291	.0291	34.37	.99958	20	40	.1679	.1703	5.871	.98580	20
50	.0320	.0320	31.24	.99949	10	50	.1708	.1733	5.769	.98531	10
2	.0349	.0349	28.64	.99939	88	10	.1736	.1763	5.671	.98481	80
10	.0378	.0378	26.43	.99929	50	10	.1765	.1793	5.576	.98430	50
20	.0407	.0407	24.54	.99917	40	20	.1794	.1823	5.485	.98378	40
30	.0436	.0437	22.90	.99905	30	30	.1822	.1853	5.396	.98325	30
40	.0465	.0466	21.47	.99892	20	40	.1851	.1883	5.309	.98272	20
50	.0494	.0495	20.21	.99878	10	50	.1880	.1914	5.226	.98218	10
3	.0523	.0524	19.08	.99863	87	11	.1908	.1944	5.145	.98163	79
10	.0552	.0553	18.07	.99847	50	10	.1937	.1974	5.066	.98107	50
20	.0581	.0582	17.17	.99831	40	20	.1965	.2004	4.989	.98050	40
30	.0610	.0612	16.35	.99813	30	30	.1994	.2035	4.915	.97992	30
40	.0640	.0641	15.60	.99795	20	40	.2022	.2065	4.843	.97934	20
50	.0669	.0670	14.92	.99776	10	50	.2051	.2095	4.773	.97875	10
4	.0698	.0699	14.30	.99756	86	12	.2079	.2126	4.705	.97815	78
10	.0727	.0729	13.73	.99736	50	10	.2108	.2156	4.638	.97754	50
20	.0756	.0758	13.20	.99714	40	20	.2136	.2186	4.574	.97692	40
30	.0785	.0787	12.71	.99692	30	30	.2164	.2217	4.511	.97630	30
40	.0814	.0816	12.25	.99668	20	40	.2193	.2247	4.449	.97566	20
50	.0843	.0846	11.83	.99644	10	50	.2221	.2278	4.390	.97502	10
5	.0872	.0875	11.43	.99619	85	13	.2250	.2309	4.331	.97437	77
10	.0901	.0904	11.06	.99594	50	10	.2278	.2339	4.275	.97371	50
20	.0929	.0934	10.71	.99567	40	20	.2306	.2370	4.219	.97304	40
30	.0958	.0963	10.39	.99540	30	30	.2334	.2401	4.165	.97237	30
40	.0987	.0992	10.08	.99511	20	40	.2363	.2432	4.113	.97169	20
50	.1016	.1022	9.788	.99482	10	50	.2391	.2462	4.061	.97100	10
6	.1045	.1051	9.514	.99452	84	14	.2419	.2493	4.011	.97030	76
10	.1074	.1080	9.255	.99421	50	10	.2447	.2524	3.962	.96959	50
20	.1103	.1110	9.010	.99390	40	20	.2476	.2555	3.914	.96887	40
30	.1132	.1139	8.777	.99357	30	30	.2504	.2586	3.867	.96815	30
40	.1161	.1169	8.556	.99324	20	40	.2532	.2617	3.821	.96742	20
50	.1190	.1198	8.345	.99290	10	50	.2560	.2648	3.776	.96667	10
7	.1219	.1228	8.144	.99255	83	15	.2588	.2679	3.732	.96593	75
10	.1248	.1257	7.953	.99219	50	10	.2616	.2711	3.689	.96517	50
20	.1276	.1287	7.770	.99182	40	20	.2644	.2742	3.647	.96440	40
30	.1305	.1317	7.596	.99144	30	30	.2672	.2773	3.606	.96363	30
40	.1334	.1346	7.429	.99106	20	40	.2700	.2805	3.566	.96285	20
50	.1363	.1376	7.269	.99067	10	50	.2728	.2836	3.526	.96206	10
					82						74
	Cosin.	Cotg.	Tan.	Sine.	Angle.		Cosin.	Cotg.	Tan.	Sine.	Angle.

TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.	Angle	Sine.	Tan.	Cotg.	Cosin.	
16	.2756	.2867	3.487	.96126	74	.4067	.4452	2.246	.91355	
10	.2784	.2899	3.450	.96046	10	.4094	.4487	2.229	.91236	
20	.2812	.2931	3.412	.95964	20	.4120	.4522	2.211	.91116	
30	.2840	.2962	3.376	.95882	30	.4147	.4557	2.194	.90996	
40	.2868	.2994	3.340	.95799	40	.4173	.4592	2.177	.90875	
50	.2896	.3026	3.305	.95715	50	.4200	.4628	2.161	.90753	
17	.2924	.3057	3.271	.95615	73	.4226	.4663	2.145	.90631	
10	.2952	.3089	3.237	.95545	10	.4253	.4699	2.128	.90507	
20	.2979	.3121	3.204	.95459	20	.4279	.4734	2.112	.90383	
30	.3007	.3153	3.172	.95372	30	.4305	.4770	2.097	.90259	
40	.3035	.3185	3.140	.95284	40	.4331	.4806	2.081	.90133	
50	.3062	.3217	3.108	.95195	50	.4358	.4841	2.066	.90007	
18	.3090	.3249	3.078	.95106	72	.4384	.4877	2.050	.89879	
10	.3118	.3281	3.048	.95015	10	.4410	.4913	2.035	.89752	
20	.3145	.3314	3.018	.94924	20	.4436	.4950	2.020	.89623	
30	.3173	.3346	2.989	.94832	30	.4462	.4986	2.006	.89493	
40	.3201	.3378	2.960	.94740	40	.4488	.5022	1.991	.89363	
50	.3228	.3411	2.932	.94646	50	.4514	.5059	1.977	.89232	
19	.3256	.3443	2.904	.94552	71	.4540	.5095	1.963	.89101	
10	.3283	.3476	2.877	.94457	10	.4566	.5132	1.949	.88968	
20	.3311	.3508	2.850	.94361	20	.4592	.5169	1.935	.88835	
30	.3338	.3541	2.824	.94264	30	.4617	.5206	1.921	.88701	
40	.3365	.3574	2.798	.94167	40	.4643	.5243	1.907	.88566	
50	.3393	.3607	2.773	.94068	50	.4669	.5280	1.894	.88431	
20	.3420	.3640	2.747	.93969	70	.4695	.5317	1.881	.88295	
10	.3448	.3673	2.723	.93869	10	.4720	.5354	1.868	.88158	
20	.3475	.3706	2.669	.93769	20	.4746	.5392	1.855	.88020	
30	.3502	.3739	2.675	.93667	30	.4772	.5430	1.842	.87882	
40	.3529	.3772	2.651	.93565	40	.4797	.5467	1.829	.87743	
50	.3557	.3805	2.628	.93462	50	.4823	.5505	1.816	.87603	
21	.3584	.3839	2.605	.93358	69	.4848	.5543	1.804	.87462	
10	.3611	.3872	2.583	.93253	10	.4874	.5581	1.792	.87321	
20	.3638	.3906	2.560	.93148	20	.4899	.5619	1.780	.87178	
30	.3665	.3939	2.539	.93042	30	.4924	.5658	1.767	.87036	
40	.3692	.3973	2.517	.92935	40	.4950	.5696	1.756	.86892	
50	.3719	.4006	2.496	.92827	50	.4975	.5735	1.744	.86748	
22	.3746	.4040	2.475	.92718	68	.4999	.5774	1.732	.86603	
10	.3773	.4074	2.455	.92609	10	.5025	.5812	1.720	.86457	
20	.3800	.4108	2.434	.92499	20	.5050	.5851	1.709	.86310	
30	.3827	.4142	2.414	.92388	30	.5075	.5890	1.698	.86163	
40	.3854	.4176	2.394	.92276	40	.5100	.5930	1.686	.86015	
50	.3881	.4210	2.375	.92164	50	.5125	.5969	1.675	.85866	
23	.3907	.4245	2.356	.92050	67	.5150	.6009	1.664	.85717	
10	.3934	.4279	2.337	.91936	10	.5175	.6048	1.653	.85567	
20	.3961	.4314	2.318	.91822	20	.5200	.6088	1.643	.85416	
30	.3987	.4348	2.300	.91706	30	.5225	.6128	1.632	.85264	
40	.4014	.4383	2.282	.91590	40	.5250	.6168	1.621	.85112	
50	.4041	.4417	2.264	.91472	50	.5275	.6208	1.611	.84959	
				66					58	
	Cosin.	Cotg.	Tan.	Sine.	Angle.	Cosin.	Cotg.	Tan.	Sine.	Angle.

TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.		Angle	Sine.	Tan.	Cotg.	Cosin.	
°						°					
32	.5299	.6249	1.600	.84805	58	30	.6225	.7954	1.257	.78261	
10	.5324	.6289	1.590	.84650	50	40	.6248	.8002	1.250	.78079	
20	.5348	.6330	1.580	.84495	40	50	.6271	.8050	1.242	.77897	
30	.5373	.6371	1.570	.84339	30						
40	.5398	.6412	1.560	.84182	20	39	.6293	.8098	1.235	.77715	
50	.5422	.6453	1.550	.84025	10	10	.6316	.8146	1.228	.77531	
						20	.6338	.8195	1.220	.77347	
33	.5446	.6494	1.540	.83867	57	30	.6361	.8243	1.213	.77162	
10	.5471	.6536	1.530	.83708	50	40	.6383	.8292	1.206	.76977	
20	.5495	.6577	1.520	.83549	40	50	.6406	.8342	1.199	.76791	
30	.5519	.6619	1.511	.83389	30						
40	.5544	.6661	1.501	.83228	20	40	.6428	.8391	1.192	.76604	
50	.5568	.6703	1.492	.83066	10	10	.6450	.8441	1.185	.76417	
						20	.6472	.8491	1.178	.76229	
34	.5592	.6745	1.483	.82904	56	30	.6494	.8541	1.171	.76041	
10	.5616	.6787	1.473	.82741	50	40	.6517	.8591	1.164	.75851	
20	.5640	.6830	1.464	.82577	40	50	.6539	.8642	1.157	.75661	
30	.5664	.6873	1.455	.82413	30						
40	.5688	.6916	1.446	.82248	20	41	.6561	.8693	1.150	.75471	
50	.5712	.6959	1.437	.82082	10	10	.6583	.8744	1.144	.75280	
						20	.6604	.8796	1.137	.75088	
35	.5736	.7002	1.428	.81915	55	30	.6626	.8847	1.130	.74896	
10	.5760	.7046	1.419	.81748	50	40	.6648	.8899	1.124	.74703	
20	.5783	.7089	1.411	.81580	40	50	.6670	.8952	1.117	.74509	
30	.5807	.7133	1.402	.81412	30						
40	.5831	.7177	1.393	.81242	20	42	.6691	.9004	1.111	.74314	
50	.5854	.7221	1.385	.81072	10	10	.6713	.9057	1.104	.74120	
						20	.6734	.9110	1.098	.73924	
36	.5878	.7265	1.376	.80902	54	30	.6756	.9163	1.091	.73728	
10	.5901	.7310	1.368	.80730	50	40	.6777	.9217	1.085	.73531	
20	.5925	.7355	1.360	.80558	40	50	.6799	.9271	1.079	.73333	
30	.5948	.7400	1.351	.80386	30						
40	.5972	.7445	1.343	.80212	20	43	.6820	.9325	1.072	.73135	
50	.5995	.7490	1.335	.80038	10	10	.6841	.9380	1.066	.72937	
						20	.6862	.9435	1.060	.72737	
37	.6018	.7536	1.327	.79864	53	30	.6884	.9490	1.054	.72537	
10	.6041	.7581	1.319	.79688	50	40	.6905	.9545	1.048	.72337	
20	.6065	.7627	1.311	.79512	40	50	.6926	.9601	1.042	.72136	
30	.6088	.7673	1.303	.79335	30						
40	.6111	.7720	1.295	.79158	20	44	.6947	.9657	1.036	.71934	
50	.6134	.7766	1.288	.78980	10	10	.6967	.9713	1.030	.71732	
						20	.6988	.9770	1.024	.71529	
38	.6157	.7813	1.280	.78801	52	30	.7009	.9827	1.018	.71325	
10	.6180	.7860	1.272	.78622	50	40	.7030	.9884	1.012	.71121	
20	.6202	.7907	1.265	.78442	40	50	.7050	.9942	1.006	.70916	
							.7071	1.	1.	.70711	
										°	
	Cosin.	Cotg.	Tan.	Sine.	Angle.		Cosin.	Cotg.	Tan.	Sine.	Angle.

TABLE IX.—CALCULATION OF EARTHWORK.

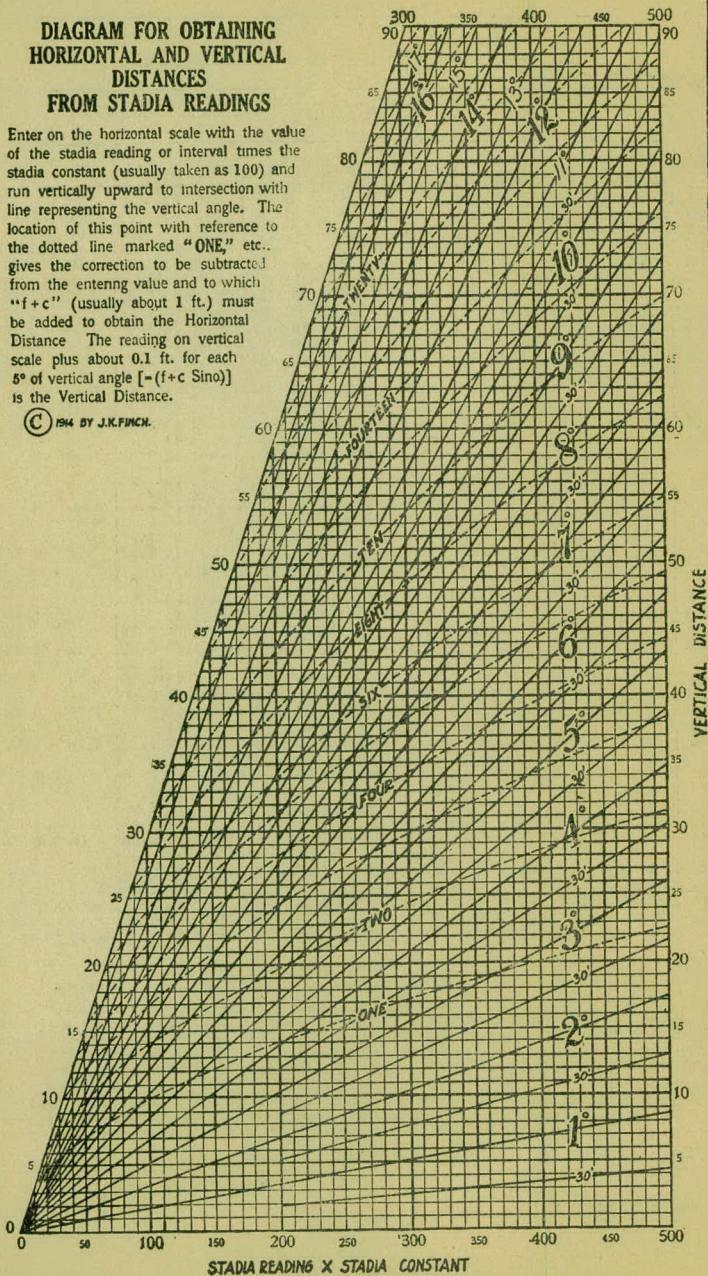
Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

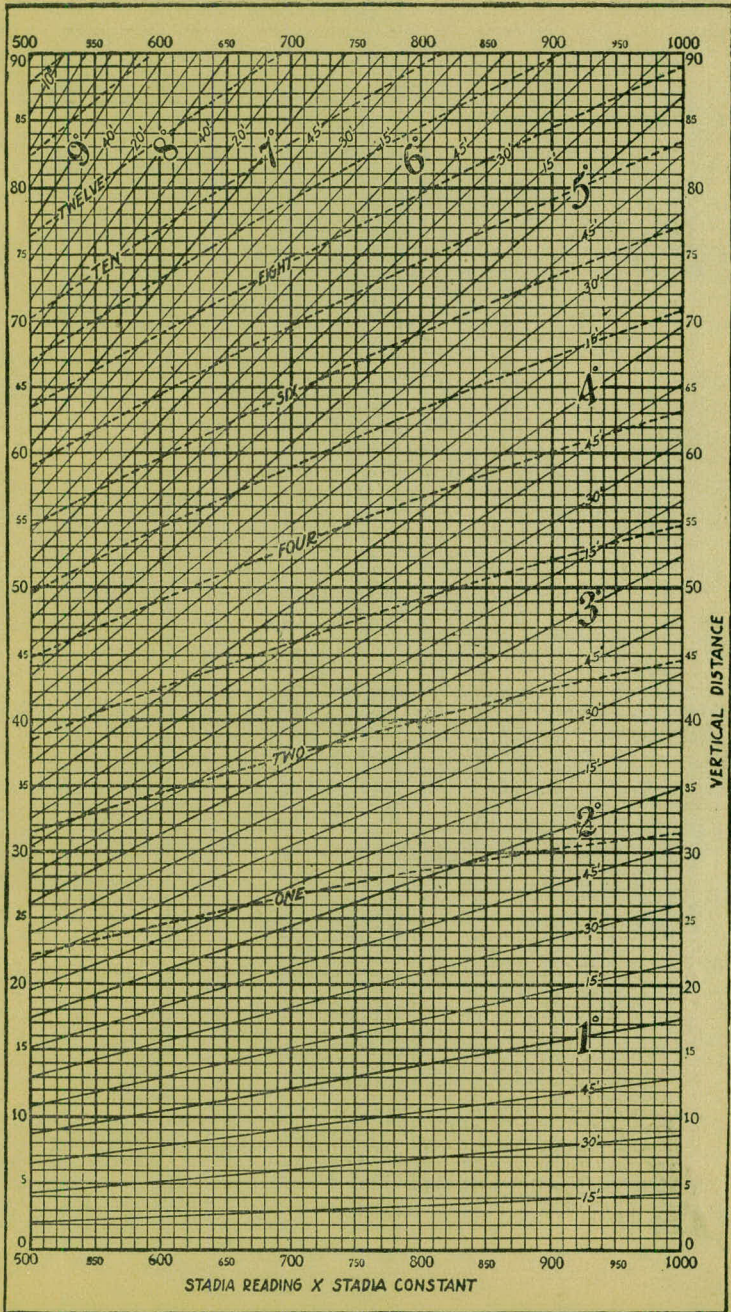
Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w = 16.2$ and $h = 5.3$, cu. yds. $= 1.48 + .028 + .089 = 1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) $= h$, and $\frac{1}{2}$ the roadbed $= w$, add the triangles formed by taking the distance out to each break in turn ($= w$'s) by the difference between the cuts (or fills) on each side of it ($= h$'s) always subtracting the outer from the inner.

DIAGRAM FOR OBTAINING HORIZONTAL AND VERTICAL DISTANCES FROM STADIA READINGS

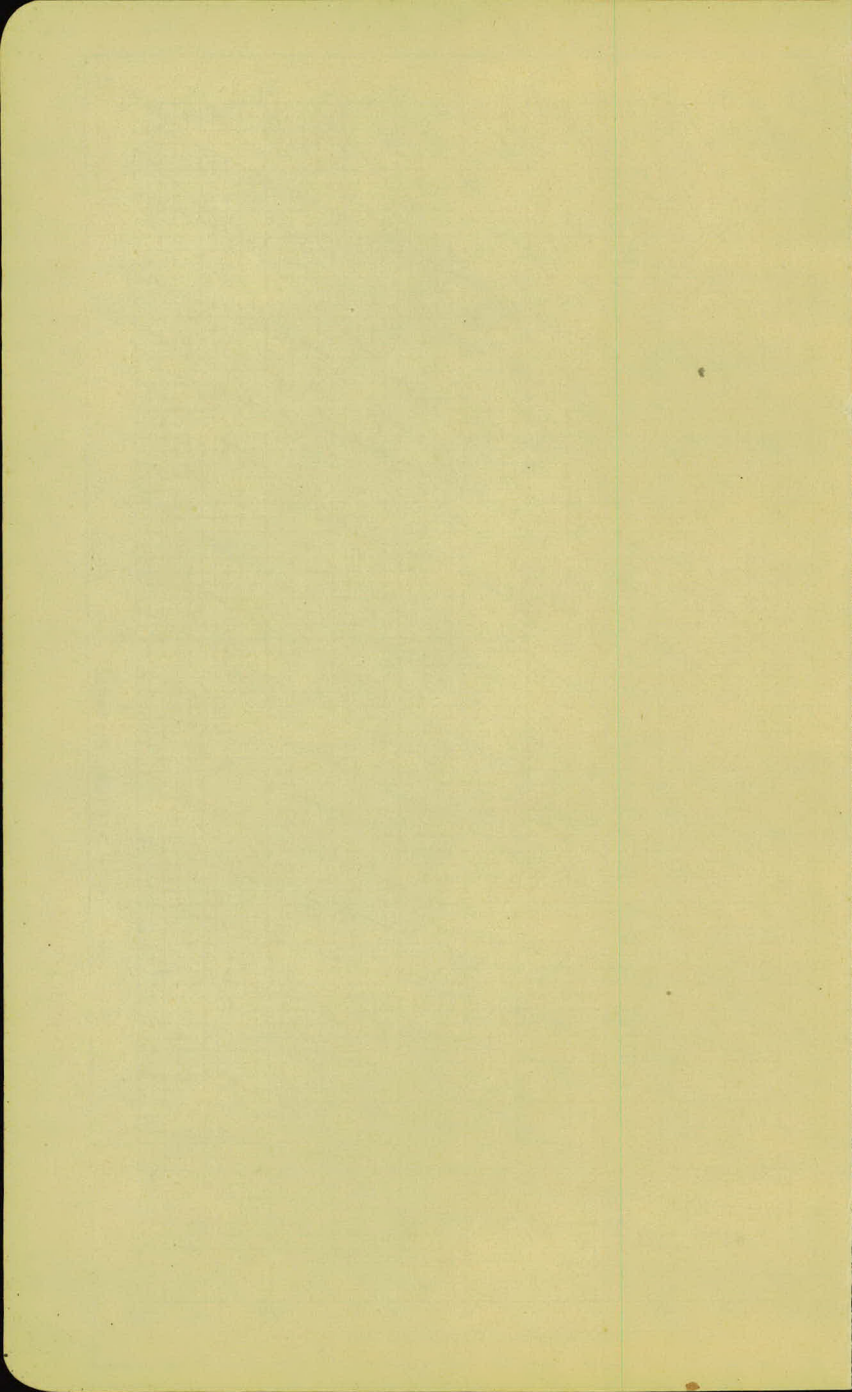
Enter on the horizontal scale with the value of the stadia reading or interval times the stadia constant (usually taken as 100) and run vertically upward to intersection with line representing the vertical angle. The location of this point with reference to the dotted line marked "ONE," etc., gives the correction to be subtracted from the entering value and to which "f+c" (usually about 1 ft.) must be added to obtain the Horizontal Distance. The reading on vertical scale plus about 0.1 ft. for each 5° of vertical angle [- (f+c Sino)] is the Vertical Distance.

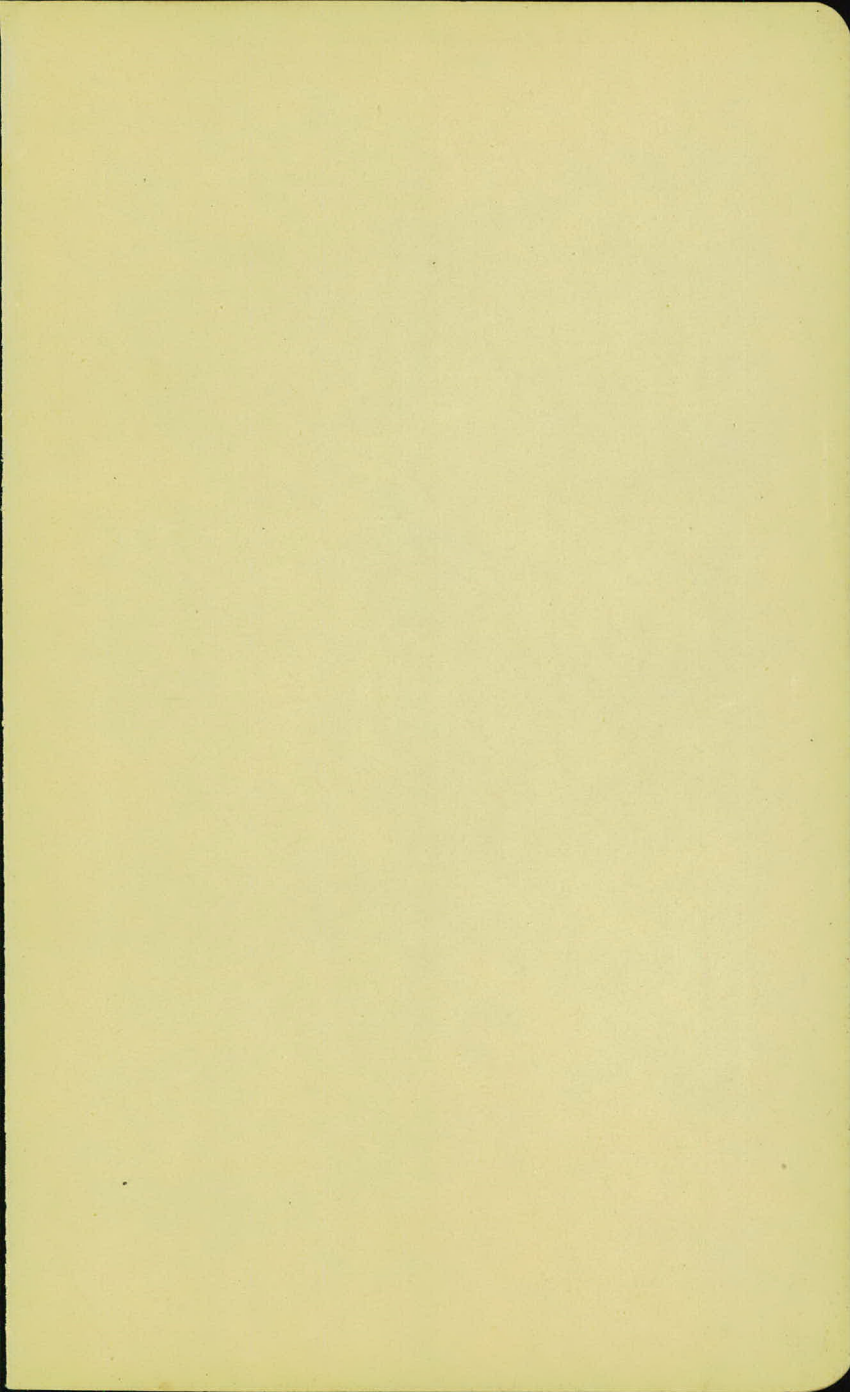
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STADIA READING X STADIA CONSTANT





577
4.8

581.8

U 2449

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

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