22·00 22·05

2022
2022

HAMPTON - RICH VALLEY

DAKOTA COUNTY

JOB - 22-05

		PAGE
Final cross-section	0+00 - 18+00	1-3
Original - Book 80 - Page 25-26		
Final cross-section	33+00 - 50+00	4-8
Original - Book 80 - Page 23-24		
Final cross-section	75+67.8 - 131+19.5	9-16
Original - Book 80 - Page 19-20-21-22-31		

B.M.	3.39	96053			957.14
0+00			3.6	56.9	
01			4.2	56.3	
+99 ℄ E.C.			4.1	56.4	
02					
03			4.2	56.3	
04			4.6	55.9	
05			3.9	56.6	
06			2.9	57.6	
T.P.	6.86	964.08	3.31	957.77	
07			5.7	58.4	
08			4.8	59.3	
09			4.2	59.9	
10			3.7	60.4	
11			3.6	60.5	

L C R. 8/21/23

2

(4.9)

3.8 33 3.6 20 3.0 33

(5.0)

45 33 6.7 29 6.5 19 4.6 14 4.7 20 4.8 20 6.7 15 6.6 33 4.7 36

(4.8)

5.8 33 7.7 29 6.8 17 5.6 15 4.3 10 4.1 20 4.6 18 6.5 25 6.3 33 4.5 35

(5.3)

6.6 35 7.7 34 7.6 24 4.9 15 4.7 20 4.9 13 6.8 17 6.8 30 6.5 33

(5.2)

6.0 40 7.5 24 7.4 24 5.0 15 4.6 20 5.0 13 6.6 17 6.7 33

(4.3)

4.4 36 6.8 33 6.8 27 4.5 17 3.9 20 4.5 14 6.1 21 6.9 27 5.4 28 5.4 33

(3.5)

3.6 33 5.1 30 4.8 27 3.7 15 2.9 20 3.3 13 4.1 16 5.4 23 5.9 28 4.7 30 4.1 33

(6.5)

6.5 33 6.6 31 8.0 29 7.8 22 7.1 16 6.4 14 5.7 20 6.6 15 8.1 23 8.5 29 6.9 31 6.9 33

(5.7)

5.9 33 7.7 29 6.8 22 5.6 15 4.8 20 5.5 15 6.6 18 7.1 23 7.4 26 5.7 32 5.3 35

(4.9)

5.1 33 6.7 29 6.3 22 5.7 15 5.0 13 4.9 20 5.0 15 5.7 16 6.4 27 4.9 28 4.6 35

(4.0)

4.3 33 4.4 30 5.4 29 5.1 21 4.0 15 3.7 20 4.1 11 4.3 14 5.7 21 5.8 26 4.0 27 3.6 35

(4.3)

4.6 41 5.8 30 5.7 23 4.1 17 3.6 20 4.1 11 4.9 15 5.1 19 6.1 23 5.7 27 4.3 28 3.8 34

	+	964.08	-	Elev.
T.P.	6.10	966.42	3.76	960.32
12			5.8	60.6
13			4.3	62.1
			6.2	60.2
14			4.6	61.8
15			4.3	62.1
16			3.7	62.7
17			2.8	63.6
18			2.1	64.3
T.P.	8.00	972.04	2.38	964.04
	9.83	978.67	3.20	968.84
	5.49	983.92	0.24	978.43
B.M.			5.76	978.16 978.22

L. ± R. 8/2/23

3

(6.8)

7.1 8.9 8.8 8.3 7.4 7.1 6.1 5.8 6.1 6.3 7.3 7.2 6.7 6.6 7.3
35 33 28 22 20 16 13 10 14 15 17 20 23 28 33

(5.6)

6.2 6.0 6.0 6.7 5.8 6.8 4.3 4.6 6.1 7.1 6.8 6.6
33 27 24 21 18 13 10 13 17 20 30 34

6.2 top of pipe Lt. side (5.3) under R.R track upper end 18'11"?

6.0 7.9 7.9 6.7 4.8 4.6 5.3 6.8 7.0 7.9 8.0 7.3
36 34 27 20 15 10 13 17 20 23 30 33

(5.3)

5.8 7.6 6.7 6.2 6.0 4.3 4.9 5.5 6.2 6.6 7.7 6.1
33 31 23 18 15 10 11 14 16 20 27 33

(4.5)

5.0 7.0 6.0 5.5 4.4 3.7 3.9 5.0 5.8 6.6 6.6 5.4
33 32 23 16 15 10 10 14 16 24 28 33

(3.6)

3.7 5.6 4.8 4.6 3.0 2.8 3.4 4.7 6.2 4.6
33 31 21 17 14 10 13 16 26 33

(2.9)

2.1 3.8 3.7 2.9 2.1 2.5 2.8 3.8 4.0 3.1
36 35 18 16 10 10 13 15 21 33

Stg	+	H.I.	−	Elev.	
BM	6.68	1006.81 ✓			1000.13
+50				02.0	
45				02.5	
46				03.5	
47				05.0	
T.P.	5.51	1009.98 ✓	7.34	1004.47 ✓	
48			45	05.5	
49				05.6	
50				05.4	
	4.00	1008.84 ✓	5.14	1004.84 ✓	
B.M.			2.83	1006.01 ✓	1006.06

4/3/23

Fair Cloudy

5

(5.2)

Spike on tel. pole 27' of Sta 41+75

6.7/33 6.3/30 5.6/24 6.2/20 5.9/16 5.1/14 4.8/20 4.9/16 5.2/18 5.2/21 3.9/23 3.4/33

(4.8)

6.9/33 6.7/30 5.9/17 5.0/15 4.3/20 4.3/17 4.9/19 4.9/24 3.7/25 3.2/33

(3.4)

3.1/33 3.2/22 4.4/21 4.3/16 3.5/15 3.3/20 3.8/15 4.6/17 4.0/23 3.3/25 3.2/33

(1.3)

1.0/33 1.0/22 3.0/21 2.8/18 2.0/16 1.8/20 2.1/15 2.7/18 3.0/22 0.7/23 0.6/33

(4.3)

3.9/33 3.7/24 5.9/22 5.9/18 4.8/16 4.4/20 5.0/17 5.1/19 6.1/22 3.7/23 3.6/33

(4.4)

4.0/33 3.9/26 5.1/24 5.3/20 4.7/15 4.4/20 4.5/15 5.3/17 5.1/22 3.5/24 3.6/23

(4.8)

3.9/33 3.9/26 5.9/24 5.8/22 5.0/20 4.6/20 4.9/14 5.6/16 5.4/19 4.2/20 4.3/25 4.2/23

Spike on Tel. pole 20' Rt. of Sta 52+00

Stg	+	H.I.	−	
B.M.	443	1004.56 ✓		1000.13
44				01.4
43				01.0
42				00.6
41				99.8
40				99.1
+70				98.5
+50				97.9
39				95.6
+50				93.3
T.P.	156	993.84 ✓	1.54 ✓	99.30 ✓
38				91.2
+50				88.4
37				85.9
T.P.	1.79	985.09 ✓	10.54	983.30 ✓

L. 4 R. 7 8/21/23

Spike on Tel Pole Lt. of Stg 41+75

(5.5)

6.8 6.6 6.1 5.4 3.8 3.2 3.3 4.4 4.5 4.0 3.8 3.6
33 30 27 25 24 20 16 19 20 24 25 33

(6.6)

6.3 8.2 7.7 7.5 4.1 3.6 3.5 6.3 5.9 5.7
33 32 25 18 14 30 16 18 20 33

(4.5)

5.8 4.6 5.5 5.5 4.3 4.0 4.7 5.1 5.7 0.6 0.5
33 25 24 18 15 20 15 17 22 28 33

(5.1)

6.8 6.5 6.1 6.6 6.3 5.7 4.8 4.6 5.6 5.4 3.3 2.8 1.7 1.4
33 29 25 23 16 14 20 16 18 22 26 27 29 33

(5.9)

2.7 2.9 4.6 6.6 6.3 5.8 5.5 5.7 6.9 6.5 3.0 3.0
33 27 23 19 15 13 20 15 20 25 30 33

(5.4)

4.7 5.7 8.1 8.0 6.3 6.1 6.7 7.3 7.5 1.8 1.9
34 28 22 18 14 20 15 14 13 30 33

4.6 5.3 5.6 8.3 8.4 7.0 6.7 6.7 7.9 7.7 1.4 4.5
33 30 27 21 18 13 20 17 20 23 31 35

(9.5)

6.5 5.8 9.9 10.1 9.4 9.0 9.0 10.1 9.8 7.0 7.0
35 30 23 18 16 20 15 19 24 32 40

9.6 9.3 10.4 12.0 10.4 11.9 11.0 11.3 11.4 12.5 12.6 10.0 6.6 6.7
35 30 26 24 22 18 15 20 15 18 22 27 31 33

(2.9)

2.7 2.0 1.9 3.3 3.4 4.2 4.0 2.9 2.6 3.0 5.0 4.5 4.0 3.8 2.2 1.8
33 30 26 23 21 19 18 15 20 17 18 21 22 24 26 33

7.2 7.0 7.8 11.8 7.4 5.6 5.4 5.4 8.0 7.7 6.7 6.6
33 26 24 22 19 14 20 14 21 28 30 33

(8.9)

10.9 10.9 11.4 12.0 11.2 8.1 7.9 8.1 10.2 10.9 11.0 10.7
33 26 25 23 18 14 20 15 19 24 29 33

Sta	+	H.I.	-	Elev.
		985.09		
36			2.4	82.7
35			5.5	79.6
34			6.4	78.7
33				77.9
B.M.			6.60	978.49 978.49
T.P.	5.85	983.79	7.15	977.94
	3.47	986.26	0.93	982.86
B.M.			8.04	978.22 978.22

8/4/83

L. ≤ R. 8

(3.8)

3.9	5.5	6.3	6.8	5.5	2.9	2.6	2.7	4.5	5.1	5.1	4.7	4.4	3.3	3.0
33	29	28	26	19	13	00	10	17	24	24	25	28	31	33

(6.3)

7.6	7.5	8.6	8.5	6.7	5.5	5.9	7.1	7.0	4.6	3.7
33	30	28	21	16	20	13	19	24	27	33

(7.8)

7.7	9.5	9.4	7.1	6.4	6.4	7.9	8.5	7.9	5.9	5.1
33	29	29	16	00	10	15	20	24	28	33

(7.7)

8.0	8.1	8.1	8.8	8.5	7.6	7.7	7.5	8.9	8.4	8.8	7.3
33	30	26	25	18	14	00	13	19	24	29	33

Spike on tel. pole Lt. of Stg. 34+45

9

Final X Sections

Sta 0+00 to 131+19.4

Proj. 2-05

Road Acct #086

Hampton - Richvalley

Const. 192-

X Sect. 1923

	+	H.I	−	Elev
B.M	3.68	1002.22		998.54
131+19.5				999.0
131				999.1
130				998.2
129				97.7
128				98.4
127+53.3 EC				98.5
T.P.	2.46	1001.87	2.81	999.41
127				98.8
+50				99.0
126				98.8
+50				98.1
125				97.0
124+44.6 BC				95.9

Compass Whiskey Rotten bevy The Manic

L ∠ R. 6/1/23

10

2.0/33 2.5/27 2.9/24 3.1/17 3.2/20 3.3/12 3.7/18 3.7/33

(3.1)

2.7/33 2.3/29 3.3/26 3.7/21 4.2/19 3.6/17 3.7/20 3.5/15 4.1/18 4.6/23 4.6/33

(6.7)

4.8/33 4.3/30 5.0/26 5.3/19 5.8/17 4.6/15 4.0/20 4.8/17 6.2/19 6.7/33

(6.5)

4.3/33 4.5/29 4.9/25 5.3/19 5.9/17 4.8/15 4.0/20 5.2/15 6.0/18 6.4/20 6.4/27 6.8/33

(4.2)

2.0/33 1.7/29 2.5/26 3.4/33 4.3/22 4.7/19 3.7/17 3.8/20 4.6/19 3.5/22 4.6/24 4.8/33

+0.3/33 0.0/30 1.8/26 4.1/21 4.0/20 3.6/18 3.7/20 4.4/17 5.0/19 5.2/22 3.6/24 3.6/33

(2.7)

1.5/33 1.6/27 3.7/26 3.4/21 2.8/19 3.7/20 4.0/18 4.6/20 5.0/24 3.3/26 3.3/30

1.7/33 3.2/26 3.4/23 2.7/17 2.9/20 3.5/19 4.4/21 4.9/26 3.2/27 3.1/33

(2.2)

2.3/33 2.7/28 4.3/26 4.3/23 4.8/21 3.7/20 3.8/20 4.5/22 4.8/26 3.3/27 3.5/33

3.3/33 3.4/28 4.4/27 4.4/24 3.7/22 3.8/20 4.2/19 4.8/21 5.3/26 3.7/27 4.2/33

(3.9)

4.9/33 5.3/29 5.6/26 5.0/24 4.9/20 5.2/17 6.0/20 6.6/24 6.1/25 5.2/26 5.6/33

5.8/33 6.1/30 7.1/27 6.1/26 6.0/20 6.1/17 6.8/13 7.5/17 8.0/18 6.8/22 7.6/33

		1001.87		
124				995.2
123				92.7
T.P.	0.44	993.88	8.43	993.44
122				90.3
121				87.2
120				85.2
T.P.	2.92	987.44	9.36	984.52 984.51
119				83.7
118				80.6
117				78.7
116		988.35		78.9
T.P.	9.17	988.37	8.26	979.18
115				79.3
+50				80.6
114				82.3
		991.02		
T.P.	6.47	991.04	3.80	984.57 984.55

Cenaers
Pittsburgh
Ruth Bertha Bertus

6/1/73

L. ℄ R.

11

(7.3)

6.7 6.9 7.8 6.9 6.6 6.7 7.0 7.6 8.9 9.2 8.4 9.1
/33 /30 /26 /22 /07 /00 /07 /12 /16 /19 /20 /33

(9.0)

8.1 9.0 9.7 9.1 8.9 8.9 9.2 9.5 10.8 10.9 9.5 10.4
/33 /25 /22 /21 /15 /05 /00 /16 /18 /21 /22 /33

(3.7)

3.8 4.2 5.1 5.1 4.1 3.5 3.6 3.9 5.1 5.1 3.8 4.2
/33 /26 /25 /23 /22 /05 /00 /15 /17 /20 /22 /33

7.4

7.1 7.5 8.1 7.0 6.6 6.7 7.3 8.1 9.0 7.9 7.9
/33 /27 /24 /20 /04 /00 /15 /17 /20 /22 /33

(8.8)

8.5 8.7 10.4 10.1 9.8 8.1 9.3 10.7 10.6 9.5 9.5
/33 /26 /23 /20 /17 /00 /16 /18 /21 /22 /33

4.5

Top of S-End of gal. Culv. Rt. of Sta 12.0+00

3.7 4.1 5.9 5.9 4.7 4.5 4.7 4.8 6.4 6.2 5.0 5.0
/33 /25 /20 /18 /16 /11 /00 /15 /18 /21 /22 /33

(8.6)

6.7 7.3 8.5 8.4 7.3 6.8 7.7 8.4 9.4 8.5 8.6
/33 /25 /22 /18 /16 /00 /15 /18 /23 /34 /33

(10.6)

9.0 10.3 10.5 10.4 8.8 8.7 9.3 11.4 12.4 12.4 12.5 12.0
/33 /28 /27 /17 /15 /00 /14 /18 /21 /24 /30 /33

(11.7)

12.9 12.7 11.4 11.1 8.8 8.5 9.2 11.2 14.6 12.6
/33 /24 /21 /19 /15 /00 /14 /18 /25 /33

(12.0)

11.2 11.1 11.8 11.6 9.4 9.1 9.1 10.6 9.8 7.1 6.6
/33 /28 /24 /19 /14 /00 /16 /19 /27 /32 /36

7.5 7.6 9.9 9.8 8.2 7.8 7.6 8.2 7.3 3.8 3.2
/33 /30 /25 /18 /13 /00 /15 /19 /28 /31 /33

(5.5)

5.6 6.0 7.1 8.0 7.9 6.9 6.1 5.9 6.6 6.7 6.0 5.4 3.9 3.3 0.9
/33 /27 /26 /22 /19 /15 /00 /10 /15 /17 /19 /25 /29 /31 /33

Sta	+	H.I.	-	Elev	
		991.04			
		991.02			
+50				83.8	
01 ± E.C.				84.7	
113					
+50				84.7	
112				83.9	
+50				83.4	
111				83.1	
+71.9 E.T.S.				82.9	
+50				82.5	
+21.9				81.9	
110		983.25		81.5	
B.M.	1.18	983.27	8.95	982.09	982.07
109				79.7	
108				77.5	

L. Conners Wilkerson Rottenberg MS Hall & R.

12

7.3 7.3 9.3 9.4 9.7 7.7 7.2 7.0 7.3 7.6 6.7 5.7 4.5 2.9 2.6
3.3 2.8 2.6 2.3 2.3 2.0 1.7 1.0 1.1 1.7 1.7 2.0 2.4 2.7 3.0 3.3

(2.8)

6.8 6.3 4.3 7.9 8.0 6.7 6.3 6.3 5.6 5.4 3.8 2.4 2.3
3.3 3.0 2.8 2.5 2.0 1.7 1.0 1.6 1.9 2.3 2.6 2.9 3.3

7.3 7.1 7.5 7.7 8.5 8.3 7.0 6.3 6.7 6.5 5.9 5.3 3.8 3.9
3.3 2.7 2.6 2.5 2.4 1.9 1.4 1.0 1.6 2.0 2.1 2.6 2.8 3.3

(6.5)

8.6 8.1 8.2 9.2 9.0 7.4 7.1 6.6 7.6 7.9 6.5 6.5
3.3 2.6 1.9 1.7 1.4 0.5 1.0 2.2 2.4 2.6 3.0 3.3

8.9 8.5 8.4 9.5 9.4 8.2 7.6 7.6 8.6 8.8 7.6 7.7
3.3 2.4 1.9 1.7 1.4 1.0 1.0 2.3 2.6 2.8 3.0 3.3

(8.2)

9.0 8.5 8.9 10.0 9.9 8.8 7.9 7.5 7.0 6.7 Pain in tolerance on Rt.
3.3 3.1 1.7 1.6 1.4 1.1 1.0 1.6 2.4 3.3

9.0 8.6 9.3 9.4 10.4 10.1 9.3 8.1 7.8 8.4 8.2 6.5 6.7
3.3 2.5 2.3 1.9 1.8 1.4 1.2 1.0 2.1 2.3 2.5 2.8 3.3
8.9 8.8 9.3 9.5 10.6 10.6 9.6 9.5 6.6 9.2 8.8 7.0 7.0
3.3 3.0 2.9 2.3 2.1 1.9 1.6 1.0 1.7 1.8 2.0 2.3 3.3
9.5 9.7 9.6 10.1 11.1 11.0 9.8 9.1 9.7 9.6 9.5 7.5 7.4
3.3 2.6 2.5 2.1 1.9 1.7 1.3 1.0 1.9 2.1 2.4 2.6 3.3

(9.8)

10.1 9.7 10.1 10.4 11.6 11.6 10.4 9.5 10.0 10.6 10.5 8.6 8.0
3.3 2.6 2.4 2.1 2.0 1.7 1.4 1.0 1.9 2.1 2.4 2.6 3.3

Spike on Tel. pole Lt. of Sta 110+00

(9.0)

3.3 3.6 4.4 4.3 5.3 6.0 5.6 4.3 3.6 4.0 4.7 4.8 5.1 5.8
2.6 2.4 2.2 2.1 2.0 1.8 1.5 1.0 1.9 2.1 2.4 2.8 3.3

(6.6)

6.3 6.0 6.7 6.7 7.5 7.6 7.4 6.3 5.8 6.0 6.6 6.3 4.0 3.3
2.6 2.4 2.3 2.2 2.1 1.9 1.5 1.0 1.8 2.0 2.2 2.4 3.3

Sta	+	H.I.	−	Elev.	
		983.27	983.25		
107			7.9	75.4	
106			10.1	73.2	
T.P.	3.16	975.02 975.04	11.39	971.88	971.86
105			4.0	71.0	
104			4.6	70.4	
103			4.8	70.2	
102			4.3	70.7	
BM.		975.75	3.15	971.89	971.88
	3.88	975.76		971.88	971.87
101			4.7	71 ✓	
100			4.5	71 3/5 ✓	
99			5.5	70 3/5 ✓	
98			6.6	69 2/5 ✓	
97			7.5	68 3/5 ✓	
T.P	6.15	974.08 974.09	7.8 ✓	967.94	967.93
96			6.1	68 0 ✓	

Connors
Wilkinson
Rottenberg
McIlmoil

L. ± R.

8/2/23

13

(8.8)

8.3 7.0 9.4 9.9 9.8 8.9 7.9 8.1 8.9 8.7 7.0 6.4 6.0
33 29 26 25 33 20 20 16 18 21 23 25 33

(11.9)

13.5 12.2 12.3 12.1 10.7 10.1 10.6 11.3 11.3 8.6 8.4
33 22 21 19 15 20 16 19 22 24 33

(5.6)

7.4 6.7 6.6 4.2 4.0 4.4 5.5 5.9 5.7 2.7 3.2
33 25 20 15 20 16 18 20 22 25 33

(6.3)

6.5 7.1 6.8 4.6 4.6 4.8 6.8 7.5 7.6 7.7
33 30 20 16 20 15 18 21 23 33

(5.9)

5.0 5.7 5.4 5.2 4.7 4.5 5.5 7.1 7.2 7.5 8.3
33 25 23 18 16 20 16 19 21 24 33

(3.3)

1.8 1.0 1.4 5.0 5.0 4.3 4.3 4.6 5.6 5.6 3.7 4.2
33 28 25 23 18 16 20 17 19 23 25 33

V 8/3/23

(3.8)

Spike on E.P. Rt. of Stg 103 + 00

2.1 2.6 6.0 6.2 4.7 4.7 5.1 6.4 6.7 4.2 4.7 4.5
33 28 26 20 16 20 15 19 23 24 26 33

(3.1)

2.2 2.2 2.1 5.4 4.5 4.5 5.0 6.3 6.2 3.6 3.5
33 28 25 21 20 20 15 16 23 24 33

(4.1)

3.2 2.7 6.4 6.3 5.4 5.5 5.7 6.6 6.5 4.0
33 25 20 26 19 20 15 19 23 33

(5.6)

7.4 6.6 8.1 7.2 6.8 6.6 7.0 8.2 8.5 5.0 5.1
33 27 26 23 19 20 15 16 22 23 33

(8.5)

10.5 10.2 7.9 7.0 7.6 9.2 9.2 7.5 7.9
33 24 17 20 14 14 20 22 33

(8.9)

10.6 9.7 6.7 6.1 6.2 11.6 11.9
33 23 18 20 11 19 33

	+		−	Elev.	
95		974.09 974.08	4.6	695 ✓	
+74			4.7	699 ✓	
+15			4.3	695 ✓	
94			4.4	697 ✓	
93			3.9	707 ✓	
T.P.	11.19	983.68 983.69	1.59	977.50	972.49
92			10.1	736 ✓	
91		994.57	5.0	787 ✓	
T.P.	11.34	994.58	0.45	983.24	983.23
90			11.7	834 ✓	
89		998.68	5.3	893 ✓	
T.P.	7.78	998.69	3.17	991.4	991.40
+50			7.1	916 ✓	
+78			6.3	974 ✓	
88			5.5	937 ✓	
+50			5.1	936 ✓	
87			4.4	943 ✓	
+45			3.6	951 ✓	
B.M.			3.03	995.60 995.65	995.70
86					

8/3/23

L

(6.6)

13.1 12.0 4.7 4.6 4.8 8.9 13.7 13.5
33 20 10 00 10 15 18 33

R.

14

(4.3)

Water 12.7 6.1 4.4 4.2 4.4 6.5 13.5 Water
16 14 10 00 09 13 16

(4.4)

Water surface 14.7 6.6 4.5 4.3 4.6 7.0 12.9 Water
16 12 09 00 09 12 16

(5.1)

14.0 13.4 10.5 4.6 4.4 4.8 11.3 13.0 12.7
33 25 16 10 00 09 18 27 33

(4.2)

7.4 6.7 6.9 6.9 4.7 3.9 4.0 5.6 5.5 3.7
33 24 23 17 14 00 15 20 31 34

(11.1)

10.1 10.1 11.7 11.7 10.4 10.1 10.3 11.6 11.4 8.2
33 29 26 18 16 00 18 22 27 33

(7.0)

6.0 7.3 7.3 5.3 5.0 5.3 6.7 6.4 5.3 6.2
33 27 29 15 00 13 19 22 24 33

(12.5)

10.7 12.0 12.3 11.3 11.2 11.3 12.4 12.7 11.7 11.4
33 26 18 16 00 16 18 22 24 33

(5.9)

2.7 5.9 6.1 5.7 5.3 5.6 6.6 6.3 5.5
33 26 17 15 00 17 19 24 33

3.0 8.3 8.4 7.3 7.1 7.7 8.3 8.0 5.2
33 23 14 13 00 17 16 25 32

(4.0) 1.9 7.7 7.6 6.6 6.3 6.0 5.6 5.3
33 21 15 14 00 16 20 33

(2.5) 1.8 7.0 7.1 6.6 5.5 5.8 7.2 6.9 1.6
33 24 15 14 00 16 18 24 33

1.8 6.6 6.6 5.5 5.1 5.1 5.9 5.8 1.8
33 21 15 13 00 16 17 24 33

(0.9) 0.1 5.4 5.6 4.7 4.4 4.3 5.2 4.9 0.6
33 21 15 13 00 16 18 24 33

(1.1)

00 00 4.7 5.2 4.3 3.6 3.9 5.1 5.0 1.3 1.3
33 29 22 15 13 00 16 17 24 30 33

Spike on F.P. Rt. of Stg. 85+75

Sta.	+	H.I.	-	Elev.
B.M.	2.34	998.04		995.70
86			2.7	95.3
85			4.0	94.0
+50			4.8	93.2
84				93.2
83				95.7
T.P.	11.52	1009.02	0.54	997.50
+50				98.3
82				01.2
+75				02.4
+50				03.8
T.P.	8.16	1013.75	3.93	1005.09
81				05.4
+90				05.7
+50				06.1

8/2/23

L. ℄ R.

Spike on F.P. Rt of Sta. 85+75-2 15

(4.1)

1.7/33 1.1/30 1.9/31 4.4/24 4.6/18 3.1/15 7.7/10 3.2/15 4.0/16 4.0/23 2.7/25 3.0/33

(10.9)

10.6/33 10.5/25 4.7/15 4.0/10 4.7/16 11.0/27 11.1/33

(11.3)

13.5/33 12.3/30 11.8/27 5.7/15 4.8/10 5.3/15 11.5/25 11.9/33

(10.3)

13.2/33 12.7/28 12.2/25 5.0/13 4.8/10 5.3/16 11.1/26 11.4/30 11.6/33

(6.2)

6.8/33 6.1/26 2.7/26 2.3/10 2.3/14 7.0/22 7.3/28 7.2/31 7.1/33

(14.0)

14.6/33 14.4/30 13.3/24 11.1/16 10.7/10 11.2/17 11.1/14 13.3/18 12.5/21 13.7/32 14.0/33

(8.0)

6.7/33 6.0/29 6.4/24 9.0/21 9.1/16 8.0/15 7.8/10 6.4/14 9.3/18 9.3/21 8.9/27 9.6/31 9.2/33

(6.0)

0.9/33 1.1/28 3.4/25 7.8/21 7.7/15 6.7/14 6.6/10 7.0/15 8.3/19 8.2/22 7.1/24 6.8/29 6.2/32

(4.4)

0.9/33 1.1/29 2.7/26 1.1/24 5.3/21 5.8/16 5.3/14 5.2/10 5.7/15 7.0/18 7.1/21 5.2/26 4.8/33 4.6/36

E R

(5.0)

0.3/33 1.5/30 4.3/27 4.7/24 7.9/20 8.5/17 8.2/15 7.8/14 7.9/10 7.8/16 9.0/18 9.2/24 6.2/26 6.2/33

(0.6)

0.9/33 1.7/30 4.2/26 7.8/20 8.3/17 7.7/14 7.6/10 7.1/10 7.8/17 9.1/19 9.4/24 6.0/27 5.8/33

+1.0/33 3.5/25 7.9/19 7.9/15 7.4/11 7.2/10 7.5/16 8.9/19 9.2/21 9.9/23 6.1/26 5.8/29 5.2/31 5.1/33

Sta	+	H.I.	-	Elev
		1013.25		
80			7.6	05.7
+50			8.0	05.3
79			8.6	04.7
B.M.	5.35	1009.64	8.96	1004.29
+50				04.4
78				04.4
+50				04.5
77				04.9
+50				05.0
B.M.	5.58	1009.87	5.35	1004.29
76				
				05.3
B.C. & +67				05.2
T.P	4.35	1009.54	4.68	1005.19
"				1004.8
	5.70	1008.89	6.35	1003.19
			3.75	1005.14 1005.40

L. ℄ R.

16

(7.5)

3.3 3.7 6.8 9.7 8.7 7.6 8.1 9.9 9.7 7.7 7.0 7.3
33 30 21 15 13 00 16 19 23 26 29 33

6.4 6.7 6.9 8.9 8.9 8.3 8.0 9.4 9.4 9.3 8.5 8.7
33 30 27 23 19 15 00 15 17 28 29 33

(9.5)

8.0 9.3 9.7 9.5 8.8 8.6 8.9 9.9 10.2 9.7 9.3
33 31 21 17 15 00 16 23 28 30 33

Top of bottom Stop S-E. Cor. School house

5.8 6.3 6.6 6.5 6.4 5.2 5.3 6.3 6.5 5.7
33 32 26 21 16 00 19 22 31 33

(6.9) 6.77 bottom of C/L-School House

7.1 7.0 6.8 6.7 5.7 5.3 5.2 5.6 6.0 6.7 6.6 5.4 5.2
33 30 27 23 15 09 00 14 19 20 22 25 33

6.5 6.6 6.0 4.9 5.1 5.5 6.1 6.5 5.3 5.3
33 25 22 18 00 10 11 17 21 33

(5.2)

6.1 6.1 5.5 4.5 4.7 5.2 6.2 6.2 4.8 4.8
33 28 23 18 00 14 17 21 22 33

4.0 4.3 4.8 4.6 5.0 6.3 6.6 5.0 5.4
33 26 15 00 15 21 22 26 33

(5.5)

4.5 4.7 5.1 5.1 4.8 4.8 4.6 5.1 6.4 6.9 5.7 5.9
33 29 27 25 22 16 00 16 19 24 26 33

4.5 4.6 5.3 5.5 5.4 4.7 4.7 5.1 5.9 6.4 6.8 5.4 5.5
33 24 22 20 17 12 00 10 13 17 22 23 33

Spike on E.P. Rt. of Sta 63+90

HAMPTON - RICH VALLEY

DAKOTA COUNTY

JOB - 22-00

Road acct. No 86
Re X sectioning

Sta. 62+50 to Sta 66+00
Proj. 2200 - Dakota County
7/17/23

Original X sections
Dakota County book No 79
Page - 27

Unclassified Order
No 2 - Upton (C)

	+	H.I.	−	Elev.
B.M.	1.46	1060.30 ✓		1058.84 ✓
62+50 = Zero Excav. below profile Grade.			4.8	55 S
63			7.9	52 S
63+50			10.4	49 S
T. P.	2.43	1057.20 ✓	11.53	1048.77 ✓
64			3.2	48 S
64+50			5.4	45 S
65			7.7	43 S
65+50			10.0	41 S
66			12.0	39 S
T. P.	0.60	1040.12 ✓	11.68	1039.52 ✓

2 7/17/23

Cross Sections

Spike in Fence Post Rt. of Sta -61+70

2.6 6.5 6.5 6.3 4.8 5.6 6.7 6.7 2.6
27 22 18 14 00 17 19 21 25

H1 1060.30
3.6
29

9.0 9.0 7.8 7.9 8.0 9.4 9.4 4.4
24 18 16 00 16 19 24 28

(4.9)

10.60.30
3.6
31

11.7 11.4 10.4 10.4 10.1 11.4 11.6 4.3
24 18 16 00 15 18 24 30

H1 1060.30
2.8
35

4.7 4.2 3.1 3.2 3.3 4.2 4.3
24 18 15 00 15 17 22

(6.0)

H1 1060.30
2.6
34

H1 1060.30
2.5
37

+2.4

4.7 6.3 5.3 5.4 5.4 6.6 6.5
23 18 15 00 15 18 23

(4.2)

H1 1060.30
3.8
35

+1.1

H1 1060.30
5.3
37

8.6 8.5 7.4 7.7 7.7 8.9 9.1
24 18 15 00 15 18 24

(1.6)

H1 1060.30
11.0
31

37

6.7 10.4 10.2 9.9 10.0 9.8 11.2 11.5 10.4 13.3
29 26 20 19 00 16 18 23 35 35

(12.2)

7.2 12.3 12.9 11.8 12.0 12.2 13.6 13.6
31 26 18 16 00 15 18 22

Checked on Full Stake at Sta 67 - 0.1 - off.

Re X Sect. Notes
Sta. 71 to 83+50

To show material that was borrowed from side ditches in 1922
between Sta 72+25 to 77
Also to bal. yardage but
Sta 72+15 & 83+20

from Sta 77+50 to 84+00
Grade has been changed as indicated - and material
Taken from side ditches will be used for claying
These X sect. will also give check on material used for claying bet. Sta 104+50 back to approx. Sta 70- Sta to be determined later.

ORIGINAL X SECT. Notes
Book 79 - Page 28
Dakota Co Book.

Sta	+	HI	-	Elev.
		1017.40		
71			2.7	1014.4
72			6.1	11.3
T.P.			8.73	1008.67
72+25	2.43	1011.10	0.5	10.6
73			2.0	09.1
74			2.7	08.4
75			3.8	07.3
76			4.7	06.4
77			3.8	07.3
78			4.1	07.0
T.P.			2.73	1008.37
79	6.04	1014.41	6.7	07.71
80			4.2	10.2
81			1.4	13.0
T.P.	7.70	1020.95	1.16	1013.25
82			6.4	14.6

(6.8)

7.8	7.7	2.7	2.7	7.8	7.3	7.3
33	23	15	15	23	24	33

(8.1)

7.5	7.8	7.3	6.1	6.1	8.0	8.0
37	24	18	15	15	24	33

1.8	1.5	00	0.5	0.2	1.8	2.1	End of Bourbon Pit 1922
36	19	15	00	15	18	32	

(2.4)

2.0	4.0	3.7	3.2	1.6	2.0	2.7	3.3	4.3	4.1	2.6
35	33	26	16	14	00	15	17	29	32	33

(2.5)

2.2	4.3	3.9	2.1	2.6	2.7	3.2	3.8	4.4	4.3	2.5
34	32	26	18	15	00	15	17	25	32	34

(3.9)

2.9	4.9	4.6	4.2	3.8	3.8	3.7	4.3	5.1	5.3	3.1
33	31	26	17	14	00	15	19	26	33	34

(7.4)

7.7	7.8	8.0	4.6	4.7	4.8	6.8	8.0	7.9
34	29	22	17	00	14	17	23	33

(7.1)

7.9	8.1	7.9	4.1	3.8	3.9	8.0	8.3	7.9
37	28	22	14	00	13	24	32	35

(5.7)

7.0	7.3	7.1	4.3	4.1	4.2	7.3	7.3	6.7
37	29	21	16	00	15	20	29	34

(7.2)

6.1	6.5	6.9	6.4	6.7	7.0	6.4	6.6	6.3	6.7	5.9
33	24	20	5	00	3	9	18	27	29	33

(3.9)

3.4	3.3	3.6	4.2	4.3	4.0	3.6	3.7	3.8
33	27	23	00	3	8	17	27	33

(1.7)

0.6	0.8	1.7	1.4	1.8	2.0	1.5	1.1	1.1
33	24	12	00	4	10	19	27	33

(6.4)

5.6	5.7	6.3	6.2	6.4	6.6	6.1	6.6	6.1	6.2
33	24	23	16	00	9	16	23	27	33

Sta	+	HI	−	Elev.
82+50		1030.95	5.3	15.7
83			4.0	17.0
83+50			2.5	18.5
BM			2.28	1018.67

4.6	4.7	5.1	5.1	5.3	5.2	5.0	4.7
33	26	24	15	00	7	18	33

(4.4)

3.7	4.1	4.0	4.0	3.9	4.4	4.0
33	28	17	00	9	18	33

2.7	2.9	3.0	2.4	2.5	2.3	2.6	2.2	2.8	2.9
33	30	19	14	00	6	10	15	22	33

Mail in So. Gate Boat Lt. Sta 83

	Grade Elev.		Grade Elev.	
77		-0.295%	05.51	+0.295%
77+50	07.38		07.38	
78	07.23		07.39	
+50	07.20		07.72	
79	07.41	500' VC	08.37	200' VC
+50	07.82		09.35	
80	08.49		10.49	+2.28%
81	10.51		12.77	
82	13.45		15.04	
+50	15.28		16.31	
83	17.32	+4.333%	17.84	200' VC
+50	19.46		19.63	
84	21.66		21.66	

Profile Grades 1922

Grades Changed and Under Construction 1923

+4.333%

6

Road acct/ Nº 86

R & X Sections

S/G 121 - 136

Proj - 2200 Dakota Co.

7/17/23

Original X sections

Dakota Co. Book Nº 79

Pages - 31 - 32

B.M.	+	H.I.	-	Elev. 1071.81
Sta.	1.54	1073.35		
	2.30	1068.80	6.85	1066.50
121			3.2	1065.6
122			3.9	1064.9
123			4.5	1064 3/10
124			5.3	1063 5/10
125			6.7	1062 1/10
126			8.4	1060 4/10

Spike on 15" Oak 48' Lt. of Sta. 116+10

Cross Sections

7

(3.7)

40/26 5.6/24 3.9/18 3.7/00 3.7/17 4.9/20 4.9/22 4.1/23

(4.2)

4.7/26 6.2/24 4.4/18 3.9/00 4.4/16 6.1/21 4.6/22

(4.8)

5.0/24 6.5/23 6.3/19 4.9/16 4.5/00 5.0/16 6.2/19 6.0/22 4.8/23

(4.8)

5.5/26 6.7/24 6.4/18 5.2/16 5.3/00 5.5/17 6.6/19 6.2/24 5.2/25

(4.9)

5.1/27 8.1/22 8.0/17 7.2/15 6.8/00 7.2/16 8.1/19 7.6/24 5.1/28

(8.2)

6.2/28 9.3/24 10.0/20 8.8/17 8.4/00 8.8/17 10.0/21 10.0/23 9.1/26 5.3/31

Sta.	+	H.I.	−	Elev.
		1068.80	9.28	1059.52
	1.65	1061.17		
127			4.3	1056.9
+60			6.6	1054.6
128			7.8	1053.4
B.M.			8.66	1052.51
+40			8.8	1052.4
T.P.	0.48	1051.25	9.40	1051.77
129			1.2	1051.0
+50			1.5	1050.7
130			0.5	1051.7
T.P.	11.48	1063.25	0.48	1051.77
131			9.6	1053.6
132			6.1	1057.1
133			3.7	1059.5

(3.4)

6.7/28 6.3/24 6.4/23 5.9/18 4.6/16 4.3/20 4.3/18 5.5/24 0.6/32 5.3/30

(6.8)

3.8/36 9.8/29 9.8/20 7.1/16 6.6/20 6.8/17 7.8/20 7.7/25 2.8/32

(11.3)

12.5/20 12.5/23 8.1/16 11.8/20 8.3/17 11.2/22 11.2/32 8.9/37

Spike in FP 40' left 28+40

(12.4)

10.3/29 13.3/23 8.8/16 8.8/20 9.2/16 12.1/21 12.9/24 10.8/30 9.4/33

top stake at sta 43 29+00

(4.3)

11.5/24 2.5/14 1.2/20 1.6/14 11.8/29 13.7/35

(3.9)

0 15.9/33 1.9/10 1.5/20 2.2/15 12.1/30 13.0/35

(3.5)

13.6/34 1.2/15 0.5/20 0.8/14 10.7/27 10.4/33 old 7.11 stake

(11.2)

10.7/33 13.3/27 13.3/23 10.1/15 9.6/20 9.7/13 14.0/20 12.5/25 5.7/37

(5.7)

1.9/30 7.3/25 7.3/23 6.4/18 6.1/20 6.0/13 7.7/19 7.7/20 1.0/30

(2.9)

0.1/29 4.8/23 3.2/17 3.7/20 3.7/13 4.8/18 4.7/24 1.3/29 3.4/37

Barrows

Sfg	+	H.I.	-	E/eV
		1063.25		
	6.35	1069.05	0.55	1062.70
134			6.9	1062.2
135			5.2	1063.9
136			3.9	1065.2

5.9

$\frac{4.7}{29}$ $\frac{8.5}{24}$ $\frac{8.5}{22}$ $\frac{7.0}{17}$ $\frac{6.9}{20}$ $\frac{9.3}{15}$ $\frac{8.5}{18}$ $\frac{8.2}{26}$ $\frac{5.1}{28}$

4.3

$\frac{4.1}{29}$ $\frac{6.7}{23}$ $\frac{5.5}{18}$ $\frac{5.2}{20}$ $\frac{5.4}{14}$ $\frac{6.5}{16}$ $\frac{7.0}{20}$ $\frac{4.0}{28}$

3.8

$\frac{3.4}{28}$ $\frac{5.4}{24}$ $\frac{5.5}{19}$ $\frac{4.1}{17}$ $\frac{3.9}{20}$ $\frac{4.6}{15}$ $\frac{5.7}{18}$ $\frac{5.5}{23}$ $\frac{3.6}{26}$

Road Acct No. 86
RR X Sections
Sta 176 – 201
Proj 2200 7/18/23

Original X sections
Dakota County Book No. 79
Pages – 34 – 35

Sta	+	H.I.	−	Elev.	B.M.
	0.97	1067.35			1066.38
	3.81	1066.30	4.86	1062.49	
		1066.30			
176			3.7	62.6	
177			4.2	62.1	
+50			4.3	62.0	
178			4.6	61.7	
179			4.4	61.9	
180			4.6	61.7	
181			4.1	62.2	
T.P.	3.38	1067.86	3.82	1064.48	
182			5.5	62.4	
183			5.5	62.4	
184			5.0	62.9	
+75 BM.			1.47	1066.39	1066.38

Cross Sections

Spike on 7. P. 50 ft. Lt. of Sta. 184 +75

11

7-16-22
Stn-7C
C-S-Jr Mc

(5.3)

4.9 / 37 — 6.0 / 30 — 5.3 / 18 — 4.8 / 14 — 3.7 / 00 — 4.5 / 19 — 5.6 / 21 — 6.2 / 28 — 5.0 / 30

(6.6)

6.9 / 35 — 8.2 / 34 — 6.7 / 23 — 4.6 / 17 — 4.2 / 00 — 5.0 / 17 — 5.7 / 19 — 6.8 / 30 — 6.0 / 33

(7.1)

9.0 / 25 — 8.1 / 23 — 4.7 / 18 — 4.3 / 00 — 4.3 / 18 — 6.6 / 24 — 6.5 / 32

(6.9)

6.9 / 37 — 8.3 / 32 — 6.4 / 19 — 5.3 / 14 — 4.4 / 00 — 5.3 / 17 — 6.8 / 21 — 7.1 / 28 — 6.7 / 31

(5.6)

5.0 / 30 — 6.5 / 27 — 6.2 / 22 — 4.5 / 16 — 4.4 / 00 — 4.8 / 18 — 6.7 / 29 — 5.5 / 32

(5.9)

5.7 / 30 — 6.9 / 28 — 5.2 / 15 — 4.6 / 14 — 5.2 / 16 — 6.5 / 21 — 7.4 / 28 — 6.4 / 30

(6.4)

5.2 / 31 — 6.0 / 29 — 5.2 / 17 — 4.4 / 14 — 4.1 / 00 — 4.6 / 18 — 6.1 / 32 — 6.7 / 28 — 5.3 / 30

(7.5)

7.6 / 33 — 9.0 / 30 — 7.1 / 19 — 6.0 / 18 — 5.2 / 00 — 6.0 / 15 — 7.3 / 18 — 7.8 / 27 — 6.5 / 30

(7.9)

9.5 / 33 — 8.1 / 16 — 6.1 / 14 — 5.5 / 00 — 6.0 / 15 — 8.5 / 21 — 8.9 / 27 — 7.6 / 30

(6.2)

5.8 / 30 — 7.1 / 30 — 6.3 / 18 — 5.3 / 15 — 5.0 / 00 — 5.2 / 16 — 6.1 / 19 — 6.5 / 26 — 4.5 / 27

C-Stake
S-04

Spike on 7 Post. 50-ft. Lt of Sta - 184+75

Sta	+	H.I.	−	Elev	BM Elev
		1067.86			
185			4.0	63 9	
186			3.4	64 5	
187			3.0	64 9	
T.P.	3.81	1068.93	2.74	1065 19	
188			3.7	65 2	
189			3.9	65 0	
190			4.3	64 6	
191			4.1	64 8	
192			4.1	64 8	
193			4.4	64 5	
T.P.	5.20	1069.59	4.54	1064.39	
194			5.0	64 6	
195			4.7	64 9	
196			4.5	65 1	
197			4.6	65 0	

Cross Sections

12

7-18
4-23
5-15
20 mc

(3.3)

3.4/38 5.4/26 4.7/17 4.0/00 4.7/16 5.5/23 2.9/24

(2.7)

3.0/38 5.0/26 2.6/15 3.4/00 3.8/14 5.0/23 3.5/24

(2.8)

2.7/27 4.8/24 3.7/15 3.0/00 3.7/14 4.6/18 5.1/26 3.0/25

(4.3)

4.0/28 5.7/25 3.9/15 3.7/00 4.7/15 5.0/17 6.0/24 4.1/25

(5.1)

4.9/29 6.7/28 5.5/19 4.3/16 4.9/00 4.4/13 5.3/16 5.8/23 4.8/24

(5.7)

5.9/31 7.0/28 6.7/30 4.5/16 4.3/00 4.9/15 6.7/18 7.7/24 6.5/27 6.1/30

(5.2)

5.0/33 6.7/32 5.7/19 4.1/12 4.1/00 4.8/16 6.1/19 6.7/28 4.7/27

(3.4)

3.4/33 6.1/31 4.3/18 4.1/00 4.7/16 5.6/20 6.1/27 3.5/29

(4.3)

4.5/32 6.9/29 5.8/22 4.7/17 4.4/00 4.8/15 6.5/21 6.4/28 3.8/30

(5.4)

5.5/33 7.5/31 7.4/27 5.1/15 5.0/00 5.6/15 6.8/19 7.7/28 5.0/31

(5.0)

5.4/31 7.5/27 6.3/18 5.3/15 4.7/00 5.3/15 6.7/19 7.3/30 5.9/32

(4.6)

4.6/30 7.1/26 5.7/17 4.9/14 4.5/00 5.1/14 6.0/17 6.8/31 4.9/33

Top of S-Rail C.G. W Ry

5.0/30 6.7/28 6.1/18 4.8/15 4.6/00 (5.0) 5.2/14 6.3/16 6.5/20 6.1/25

Sta	+	H.I.	−	Elev	B.M.
		1069.59			
198			4.4	65	
+60	0.18	1065.55	4.22	1065.37	1065.05
199			1.1	64.5	
200			3.8	61.75	
201			6.3	59.25	
	7.61	1063.30	9.86	1055.69	
			1.05	1062.25	
	1.50	1063.75	2.40	1061.35	

Cross Sections 13

6.2

8.1/33 9.1/28 8.5/14 4.5/10 4.4/00 4.5/15 5.7/19

Top of S. Rail G. W. Rt. (1.3)

4.5/33 4.7/28 4.5/12 1.1/00 1.0/15 1.5/23 1.9/32

(9.0)

2.3/28 5.4/18 3.9/14 3.8/00 4.7/15 8.2/24 11.4/33

(10.2)

8.7/33 8.8/17 6.7/13 6.3/00 6.1/15 9.7/24 9.8/15 8.4/33

Foundation.

on top of Conc. Gas. pump Sta 207 Rt.

(106+46) on top of concrete gas intake Rt. Sta 207

Error 0.05

Road Acct. No 86

Re X Sections

Sta 281 - 309

Proj 2200

2/13/23

Conner
Wilshusen
Puttenberg
McManus

Original X sections
Dakota County Book No. 80
Pages 5-6-7
Hampton - Rich valley

+	H.I.	−	Elev
6.98	1026.15		1019.17
		0.16	1025.99
10.96	1036.95		
		0.80	1036.15
13.10	1049.25		
		0.12	1049.13
10.14	1059.27		
		0.76	1058.51
8.42	1066.93		
		7.11	1059.82

7-13-23
7.76
L+W
E-R
W mc

49.60 / 8.95

+ 8.95

40.65

+ 1019.17 ✓

1059.82

15

10" Oak - Rt. of Sta 293+10

On Top of 6" x 3" Rock Rt. of Sta 282+25

Sta	+	⌀	−	T.P. Elev.	Sta Elev.
				1018.79	
		1066.93			
281				(3.3)	63.6
282				(5.2)	61.7
283				(7.5)	59.4
+45				(9.2)	57.7
284				(11.4)	55.5
T.P.	0.20	1054.30	12.83	1054.10	
285				(3.0)	51.3
+40				(5.2)	49.1
+80				(7.1)	47.2
286				(8.1)	46.2
T.P.	0.23	1041.99	12.54	1041.76	
287				(2.0)	40.0
288				(8.1)	33.9
289				(12.8)	29.2
T.P.	1.07	1031.04	12.02	1029.97	
290				(5.6)	25.4

6 0/0

Lt & Rt 16

3.0

3.1/27 4.9/22 3.6/17 3.3/20 3.9/17 4.9/20 3.4/27

3.6

4.1/25 6.2/23 6.7/19 5.4/20 5.2/20 5.6/17 6.5/21 5.9/20 4.7/28 4.3/31

3.6

1.3/37 9.6/18 7.9/12 7.0/20 7.9/17 9.2/20 8.7/23 1.7/33

3.7

1.0/3.7 10.6/20 10.8/18 9.5/13 9.2/20 9.2/15 11.0/20 10.8/22 1.0/36

6.0

1.6/33 12.8/20 12.6/17 11.8/15 11.4/20 11.7/17 12.9/19 12.7/23 1.0/40

3.1

4.1/39 10.9/20 4.2/21 4.2/17 3.3/14 3.0/20 3.3/12 4.1/19

4.4

1.9/27 6.2/20 6.3/17 5.3/14 5.2/20 5.0/16 5.7/21

6.9

5.4/24 8.3/20 8.3/18 7.4/13 7.7/20 7.3/12 8.1/16

8.7

7.4/28 9.5/21 9.6/17 8.2/14 8.1/20 9.1/18 9.0/19

4.5

7.7/27 2.2/12 2.0/20 2.3/14 7.3/23

12.4

12.7/24 9.5/13 11/20 8.6/14 11.6/20 12.5/25

18.0

19.5/24 12.1/13 17.1/20 13.1/14 19.7/24 18.3/33

11.6

11.1/17 6.8/13 5.6/20 6.6/14 10.0/20 10.6/20

Sta	+	↑	—	TP Elev	Sta. Elev
		1031.04			
T.P. ✓			5.07	1025.97 ✓	
290+50				(6.9)	24.1 ✓
T.P.	0.15	1026.12 ✓			
291				(3.0)	23.1 ✓
292				(4.4)	21.7 ✓
BM			6.96	1019.16 ✓	
293				(4.1)	22.0 ✓
B.M.	7.34	1026.13 ✓	7.38	1018.79 ✓	
294				(2.2)	23.9 ✓
T.P.	8.30	1033.17 ✓	1.26	1024.87 ✓	
295				(6.1)	27.1 ✓
296				(2.7)	30.5 ✓
T.P.	9.79	1041.80 ✓	1.16	1032.01 ✓	
297				(7.1)	34.7 ✓
298				(3.4) ✓	38.4 ✓
	11.29	1050.85 ✓	2.24	1039.56 ✓	
299				(11.2)	39.6 ✓
T.P.	7.92	1046.92 ✓	11.85	1039.00 ✓	
300				(9.5)	37.4 ✓
T.P.	27.6	1036.86 ✓	12.82	1034.10 ✓	
301				(4.2)	32.7 ✓
302				(10.0)	26.9 ✓

17 9-13-23
2.C
H.W
E-R
W. Smc

TP 25.99 error .02 (12.2)

11.7 9.0 7.3 6.9 7.5 9.4 11.1
60 30 13 00 13 32 50

(8.6)

9.3 9.7 7.6 3.3 3.0 3.1 7.9 8.1 8.3
35 26 21 13 00 13 19 24 31

(9.2)

9.8 9.9 4.7 4.4 4.6 8.5 9.3 8.8
33 22 13 00 14 22 26 32

R.P. slu 29.3 +10 error (8.4) .01

9.5 9.3 8.2 4.7 4.2 4.2 8.6 8.8 8.2
32 22 19 14 00 14 21 24 30

R.P. 29.2 +65 B.M. (5.8)

6.8 7.1 6.5 2.4 2.2 2.0 5.8 6.3 6.1
34 26 20 13 00 13 19 23 28

(10.7)

12.4 11.0 6.4 6.1 6.2 9.2 9.7
31 20 14 00 14 19 27

(8.5)

10.3 9.6 3.1 2.7 3.0 5.1 5.1 4.6
25 21 12 00 13 19 26 28

R (8.7) L

10.4 9.8 7.4 7.1 7.0 8.6 7.2
23 18 14 00 16 22 26

(+1.1)

1.8 4.7 4.8 3.9 3.4 3.8 4.4 4.3 2.6
28 25 22 16 00 15 19 24 26

(1.8)

13 12.6 12.4 12.1 11.2 11.5 12.5 12.6 9.5
33 21 16 15 00 15 19 24 26

(4.8)

2.2 10.5 10.7 9.7 9.5 10.1 11.2 11.2 9.2
33 23 18 14 00 16 24 23 24

(2.4)

0.80 5.1 5.3 4.6 4.2 4.6 5.3 5.9
26 22 19 14 00 15 19 32

(9.0)

8.9 11.0 10.1 10.0 10.5 12.0 12.9 11.7
23 21 16 00 15 19 29 31

	+	H.I	−	TP Elev.	Sta Elev
		1036.86 ✓		✓	
T. P.	1.27	1025.67	12.46	1024.40	✓
303				(5.4)	20 3
304		✓		(10.9)	✓ 14 8
T. P.	1.84	1014.59	12.94	1012.73	✓
305				(5.1)	09 1
306		✓		✓ (7.9)	✓ 06 7
	3.16	1008.97	8.76	1005.81	✓
307				(3.7)	05 3
308				(4.3)	✓ 04 7
309				(4.3)	✓ 04 7
T. P.	3.21	1007.75	4.43	1004.54	✓
B.M.			4.90	1002.85	

18 3-23 T.C. HW. C-R

(7.8)

7.1/22 7.1/18 5.6/14 5.4/20 5.8/14 9.3/20 10.5/27 9.8/30

(16.3)

16.6/30 16.5/21 11.3/14 10.9/20 11.6/14 15.6/20 15.8/30

(9.6)

10.8/30 10.2/20 5.0/12 5.1/20 5.4/14 8.9/20 9.9/30

(10.8)

12.8/33 14.0/29 12.0/21 8.3/15 7.9/20 8.4/13 13.4/21 14.4/29 13.6/31

(15.9)

6.7/27 8.1/29 8.1/25 7.1/23 3.9/13 3.7/20 4.2/13 6.6/16 7.9/24

(4.9)

4.2/32 6.5/28 6.6/22 4.9/17 4.3/20 4.6/16 5.9/20 6.4/27 4.0/31

(4.9)

4.2/28 6.0/25 4.9/19 4.7/17 4.3/20 4.6/16 6.4/20 5.6/27 4.8/29

U.S.G.S. Mont. Left of Sta. 317+15
Elev. 1002.93 error. 0.08

2.7 3.2 3.4 4.0 7.1 7.6 7.7 7.2 5.6 4.9 3.5
00 06 10 17 20 30 40 41 43 47 48

Original X Sections
of
Borrow Pit

Sta 0+00 to 6+40
Dakota Co. Proj. 2200
Ramsey Co. Road acct No. 86
Hampton Richvalley
6/16/23

Unclassified Order
No 21-Item (6)

Sta	+	HI	−	Elev.	
BM1	1.08	1001.08		1000.00	
	5.60	999.28	7.40	993.68	
			9.72	989.56	
1+00					
1+30					991.5
1+75					97.3
2+00					97.2
2+50					96.7
3+00					97.3
3+35					97.3
3+40					
T.P.	7.26	998.82	7.72	991.56	
4+00					
4+50					96.2
5+00					96.7
5+50					96.8

· Elev. of water 6/16/23

(197.1) ✓	2.2	5.1	5.1	1.7	2.0
	6	17	30	40	66.4
	1.8	6.5	7.3	2.1	
	00	15	33	66.2	
	2.0	6.2		6.5	
	00	15		57.4	
	2.1	5.7		6.7	
	00	15		56	
	2.6	7.2	7.7	5.7	6.3
	00	15	23	40	57.8
	2.0	7.3	5.5	5.0	
	00	15	25	60.4	
	2.0	5.7	7.0	5.7	4.8	5.6
	00	15	18	20	25	59.2
(91.6)		7.7		7.7	
		25		59.2	
(91.6)		7.2	5.0	4.7	6.0
		17	22	45	57.4
	2.6	7.2	7.2	5.8	5.5
	00	15	23	30	58.4
	2.1	7.2	7.2	6.6	5.7	4.7	5.9
	00	16	23	28	32	47	59.6
	2.0	6.7	6.9	5.1		5.2
	00	15	23	38		59.0

Sta	+	HI	−	Elev.
		998.82		
6+00				95.8
6+40				93.1
6+45				

3.0 00 4.6 15 5.0 59.4

5.7 00 4.1 70

91.6 7.2 15 7.2 57

New Channel → 22

		+45	15	40	55
6			15	44	59
		+50	23	36	59
5			23	36	59
		+50	23	35.4	58.4
	40.7 × 15 =		610.5		
	38.7 × 50 =		1935.0		
4	36.3 × 50 =		1815.0	17	39.4	57.4
	36.0 × 50 =		1800.0		
	37.4 × 50 =		1870.0		
	38.7 × 5 =		193.5	15	41.2	59.2
	41.8 × 35 =		1463.0		
3	41.1 × 50 =		2053.0	15	42.4	60.4
	38.9 × 50 =		1945.0		
	38.7 × 25 =		967.5	+50 23	39.8	57.8
	43.7 × 45 =		1966.5		
	53 × 30 =		1590			
2			9180.5	10	38	54.0
			7231	+75 16	39.4	57.4
	Total ft =		16,411.5			
		+30	15	48	66.2
1	approx. 600 cu yds pr. ft Grading.		10	58	66

→ 18 ← R.O.W.

(← Shoulder Stakes 15 Ft. Rt. ℄)

593 cu yds — 6/16/22 Conner.

OLD CHANNEL

772 cu yds. — Art. Topog. of Borrow pit & Estimated yardage available

0+00

Re X sections
of
Borrow pit

Sta 0+00 to 6+40
Dakota County Proj. 22.00
Ramsey Co. Road acct No. 86
Hampton - Rich valley
7/19-23

	+	H.I.	−	Elev.
B.M.	0.98	1000.98 ✓		1000.00 ✓
01				
01+30				
01+55				
01+75				
02+00				
02+30				
02+50				
03				
03+35				
T.P	1.73	1000.45 ✓	2.26	998.72 ✓
03+40				
03+90				
04				

Rt.

7-19-23

24

T.C.
F.W.
E.W.Sns

Spike in 31" Maple-60 ft. Lt. of Sta 0+20
0+65 = Zero Excav.

(3.9)
2.7/60 3.7/06 3.4/10 6.0/17 7.1/20 7.6/30 7.7/40 7.7/61 5.8/68 4.9/67 3.5/68

(3.5)
2.1/60 7.1/10 8.6/15 8.9/28 8.4/33 7.2/62 3.9/65

Zero Excavation

Proj. 22+00 Pr. Cross Sections
Ft. Bottom Ext. on Right
Front Slo-
Extend to Sta. 24+47

No Excavation

Zero Excavation

(4.3)
3.1/60 8.6/13 8.8/15 9.0/23 9.1/40 8.1/58

(3.7)
3.2/60 6.4/07 8.3/15 9.0/24 8.7/50 8.3/67 6.7/71

(3.7)
3.1/60 6.3/08 7.6/15 8.3/20 8.9/25 9.5/58 9.7/50 7.7/70

Shoulder of Roadbed 15' Rt of Rt of Road

Zero Excavation

Zero Excavation

(8.9)
7.6/60 6.5/13 7.6/17 8.8/22 9.3/25 9.8/47 9.3/55 7.7/76

	+	#1.	−	
		1000.45		
04+50				
05+00				
05+50				
06+00				
06+40				
06+45				
		1002.89		998.21
T.P.	4.68	1002.89	2.24	998.19
B 177			2.88	999.97 1000.00 ✓
				1000.01

Rt.

25

4.3

3.8

3.7

4.7

7.4

15' Right of ℄ of Road

Zero Excavation

Spike in 30" Maple 60' Lt. of Sta 0+20
Error 0.01.

← Shoulder Line