

Book 94 Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

EAST CO. LINE RD.

From Carver Av. To Highwood Av

Road Acc't. No. 34

Date Filed 1-30-43

File

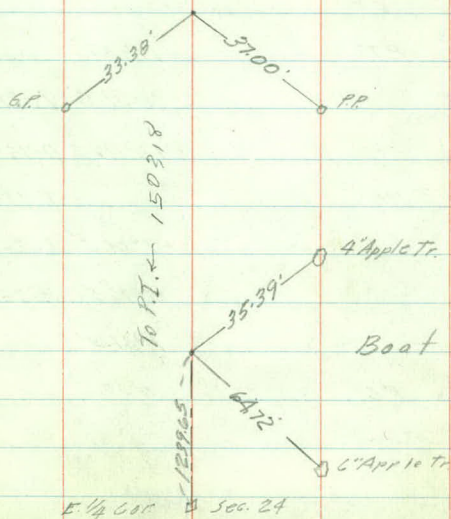
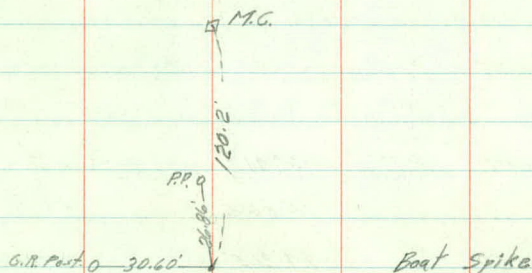
1

Alignment

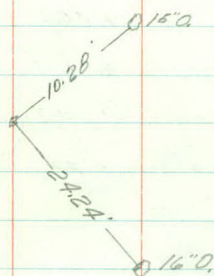
Sta	Point	ΔLt	ΔRt
12	+71.43 P.T.	11° 22.5'	
	+50	10° 37.5'	
12		8° 52.5'	$\Delta 22° 45'$
	+50	7° 07.5'	D-70-
11	+11.20 P.I.		T-164.77
11		5° 22.5'	L-325.00
	+50	3° 37.5'	R-819.02
10		1° 52.5'	
9	+46.43 P.G.	0° 00'	

4 +2872 P.O.T.

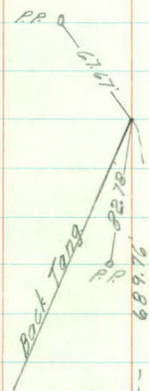
54+26.91
 0 +100 = P.T. 24+56.91 Carver Ave.



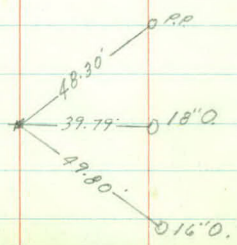
Sta	Point	Δ Lt	Δ Rt
+07.77	P.T.	18°41'	
22		18°06.5'	
+50		14°21.5'	Δ 37°22'
21		10°36.5'	D-15°-
+88.20	P.I.	37°22'	T-129.54
+50		6°51.5'	L-249.11'
20		3°06.5'	R-383.06
19 +58.66	P.C.	0°00'	
+41.22	P.T.		19°37'
17		16°21.5'	Δ 39°14'
+50		12°46.5'	D-15°-
16 +14.20	P.I.		T-136.53
16		9°01.5'	L-261.55
+50		5°16.5'	R-383.06
15		1°31.5'	
14 +79.67	P.C.	0°00'	



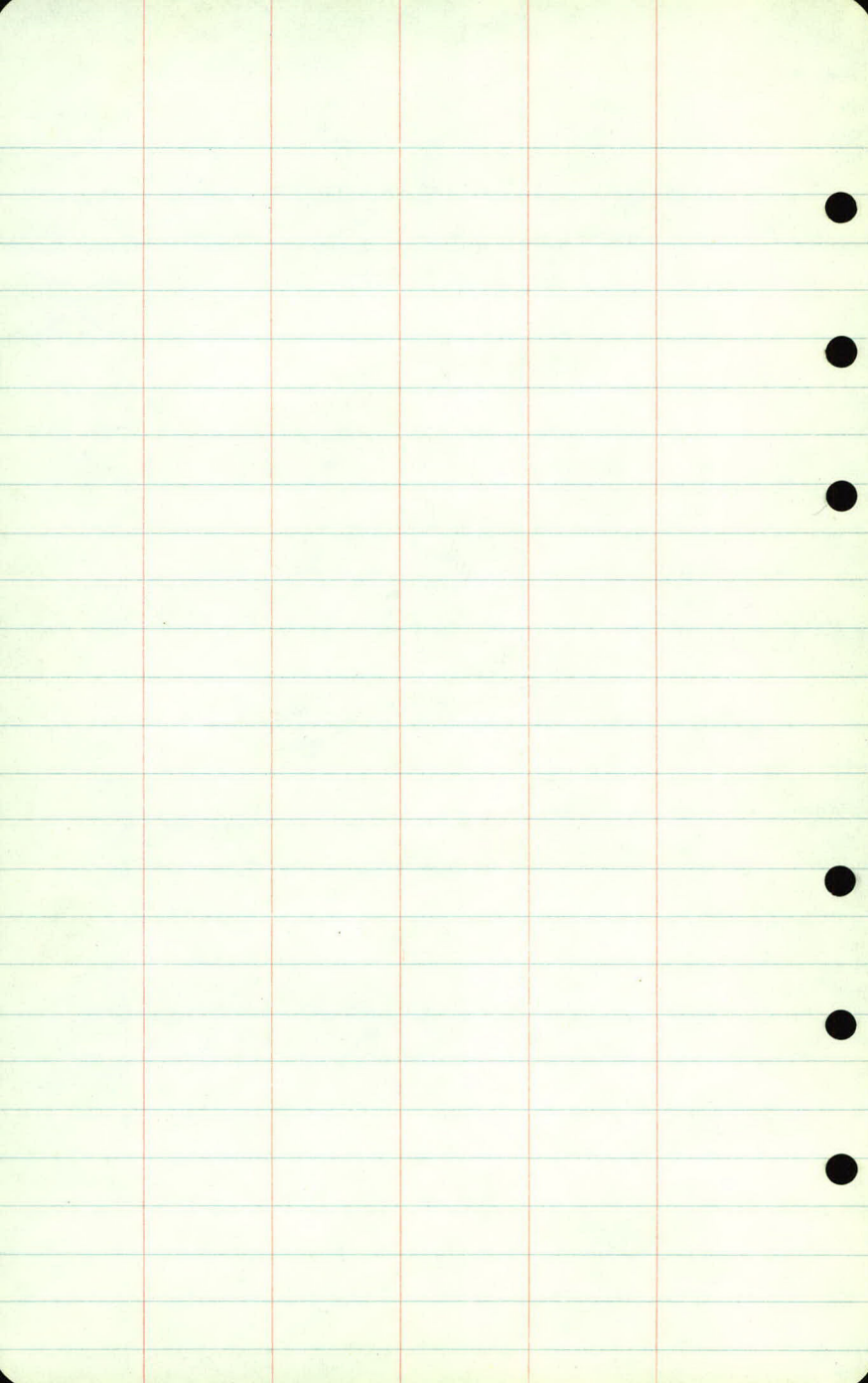
Sta	Point	ΔLt	ΔRt
42	+2772 = E. Highwood Ave.		
	+75.15 P.T.	11°41'	
	+50	10°40.7'	
32	P.T.	8°40.7'	$\Delta 23°22'$
	+50	6°40.7'	D. 8° —
31	+31.28 P.I.	23°22'	T. 148.22'
31		4°40.7'	L. 292.09'
	+50	2°40.7'	R. 716.78'
30		0°40.7'	
29	+83.06 P.C.	0°00'	
	+02.22 P.T.		22°12.5'
27			22°02.5'
	+50		18°17.5' $\Delta 44°25'$
26			14°32.5' D-15° —
	+62.5 P.I.		T-156.39'
	+50		10°47.5' L-296.11'
25			7°02.5' R-383.65'
	+50		3°17.5'
24	+06.11 P.C.		0°00'



M.C. #43 Sec. 13



289.58



Topography

+50-Fe-52'

Bea Plant Curb } 11.9'
+26-End Metal Curb }

5 Fe-47'

+72-Bea Metal Curb-12.4'

+54-~~Elm~~ Fe-58'

+49-1" Chinese Elm-58'

+32-

+24-1" Elm-

+16-1" Elm-

10' Fe-40'

+83- 199

+74-

+65-

+58-

+50-1" Chinese Elm-50

+53-Fe Cor-80'

4 +103-G.P.-22'
Fe-39'

10' 10' +99-P.P.-23'

+21-Ent-

3 Fe-35'

10' 9'

+49-Turn Sign-15'

+35-End Brush-50-18'

+50-Ent-

2 10' 9'

+63-Fe Cor-32'

+55-End Curb

+50-Bea Brush-23'-11'

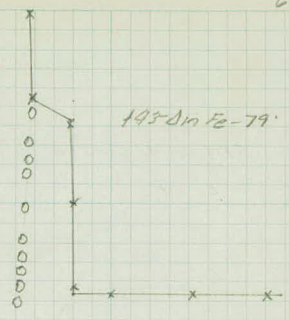
+36-4" Tr.-36' - Cor. Orchard

1 9' 11'

+50- 8' 10' +60-2" Apple Tr.-30'
+40-4" Apple Tr.-30'

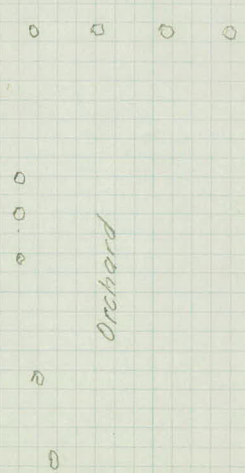
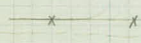
0+00 10' 10' +19-5" Apple Tr.-31'

193-0m Fe-79



Cult.

Orchard



G.R-13.4

+53-End 48" Conc. Culv-32.8'

+47-51/2 Ditch-51'

12 G.R-14' Ditch-62'

G.R-13.8'

11 G.R-13.8'

G.R-13.9

10 G.R-13.7'

+50-G.R-13.2'

+53-End Plank Spillway-36'

+46-Top Plank Spillway-13.2'

9 G.R-12'

+50-Fc-39'

8 G.R-11.9' Fc-36'

Plank Curb is in front of G.R.

+81-Fc G.R-11.9' to Fc

+74-End 24" C.M-17.8' 24" X 48" C.M

+68-End Metal Spillway-25'

+67-Top Metal Spillway-12'

+50-Fc-39'

+48-51/2-39' +42-51/2-35'

7 Curb-11.4' Fc-49'

+50-Fc-54'

6 Fc-56' Curb-11.6'

+89-8" Willow-35'

+75-8" Tree Willow-37'

G.R-12'

H.W-155' Wings-6' Long

+53-End 48" Conc. Culv-35'

+50-24" Elm-42'

9' G.R-12'

+43-Beg. G.R-13'

+37-PP-19'

+25-E. Edge Ditch

12'

+92-End G.R-13'

+60-Parking Area-37'

10' G.R-12.3'

9' G.R-12.5' Beg. Parking Area-40'

9' +50-G.R-12.5'

+35-PP-20'

11'

+90-Beg. G.R-13'

+88-End Wall-20.5'

Beg.
+46-Plank Retain Wall-19'
12'

+60-End 24" C.M-21.7'

+45-End Fc

+37-End 24" X 48" C.M

+24'

+01-PP-21.5'

12' End Fc-50'

Fc-53'

11 Fc-56'

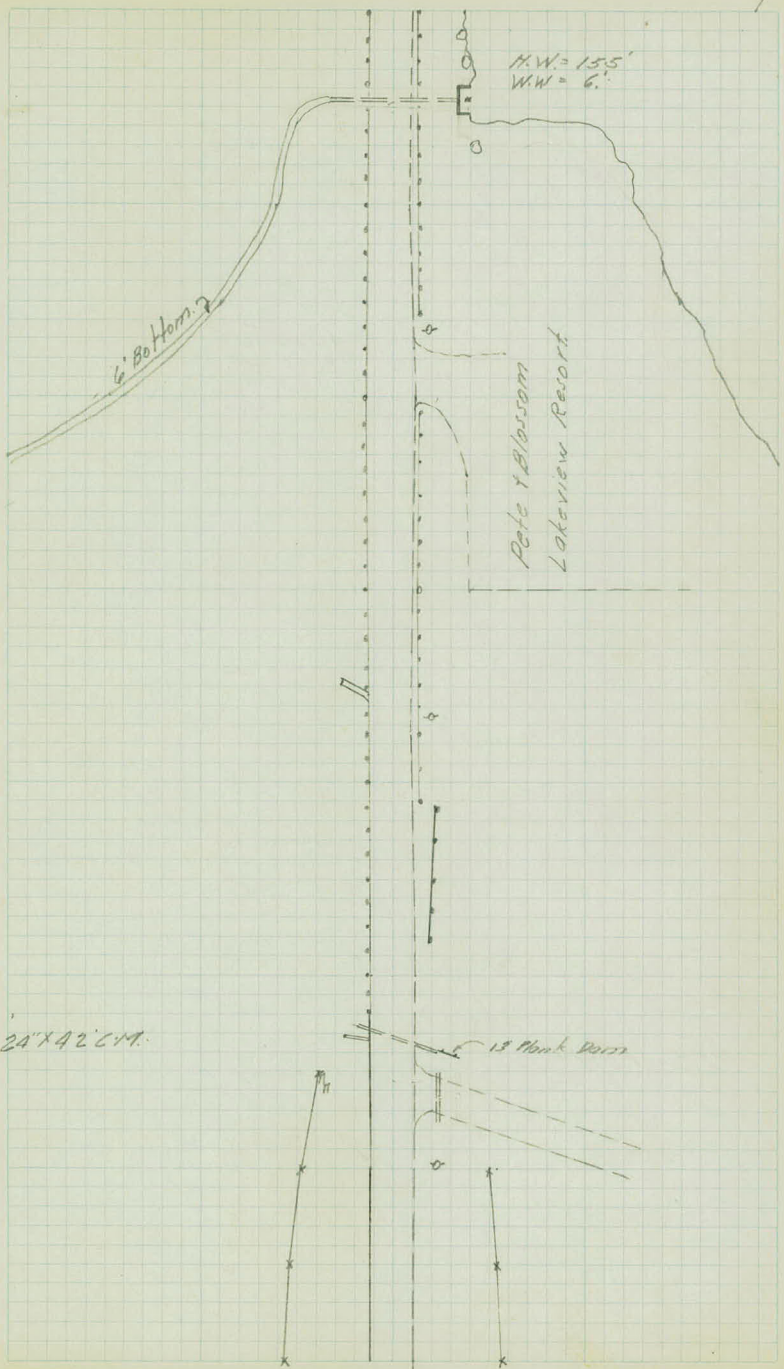
H.W. = 15.5'
W.W. = 6'

6' Bottom

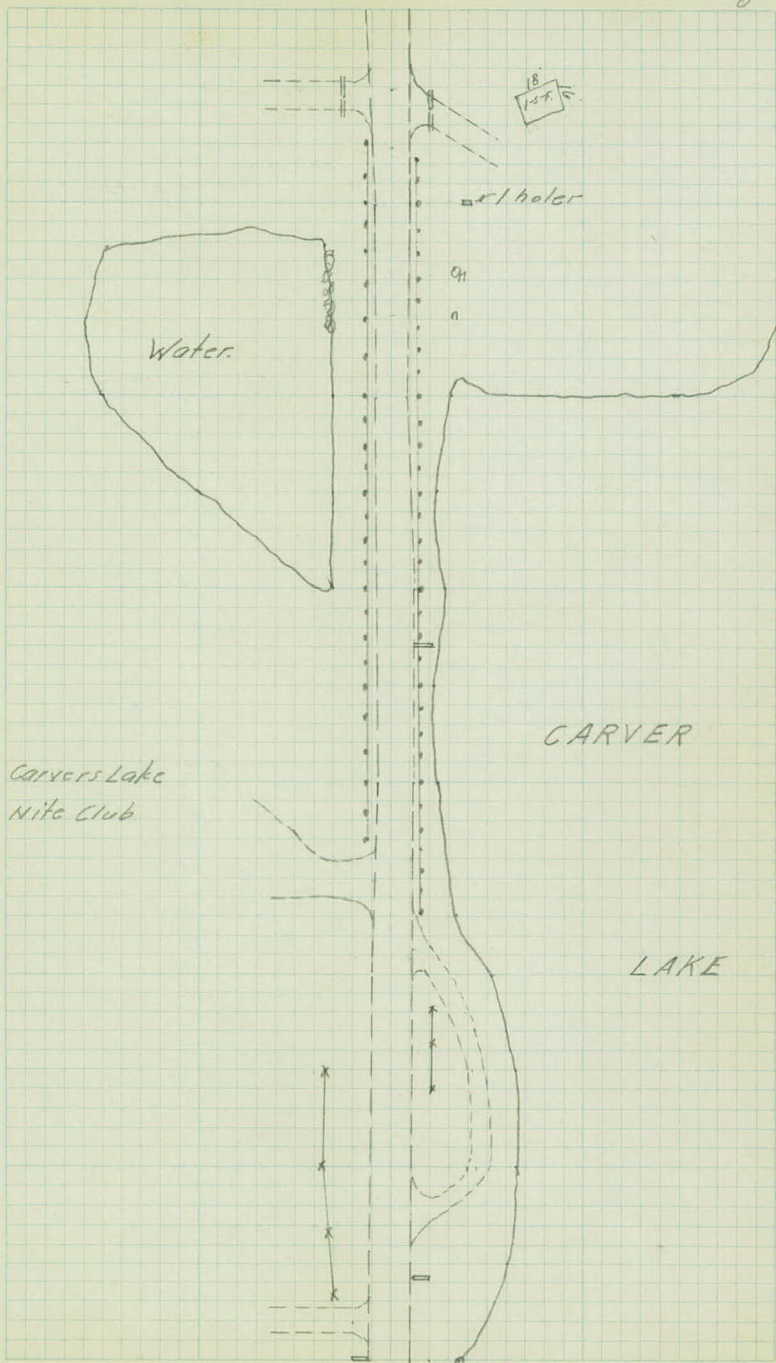
Pete & Blossom
Lakeview Resort

24" x 42" C.M.

18 Hank Dross



- 155-Ent. $\frac{12'' \times 22' \text{ G.R.}}{25'}$
 150-End G.R. 13'
 19 9' 10' 170-PP-24'
 158-Rampetic Locat.
 148-12' X 22' G.R. 20'
 159-Cor Ho-63'
 129-Large Ho-110
 125-End G.R. 125'
 Ctr 3' 13' Out Ho-38'
 178-End Pothole-35'
 179-End Willows-31'-35'
 135-Beg. Willows-31'-34'
 165-8' O-36'
 162-5' P-31'-37'
 142-5' P-33'
 145-PP-24'
 18 Pothole-31' G.R. 12.5 9' 9' G.R. 125' End Lake-31'
 Pothole-31' G.R. 12.5 8' 10' G.R. 13' Lake-24
 17 8' 11' 119-Beg. Pothole-30' G.R. 12.5 145 Lake-23
 111-Plank Spilling-143'-22'
 G.R. 12.5 9' 11' G.R. 145 Lake 22'
 16 G.R. 12' 8' 11' G.R. 145 Lake-25'
 170-Beg. G.R. 12.5
 148-Ent. 150 161-PP-22'
 133-G.R. 27' 11' 131-Beg. G.R. 14.5' Lake-33'
 15 10' 11' 112-Ent Lake 33'
 182-End Fc-22'
 150-End Fc-34' 150 Lake-65' Ent-42'
 150-Beg Fc-21'
 14 Fc-35' 11' 10' Lake-65' Ent-44'
 132-Beg Fc-30'
 120-Ent
 101-FW G.R. + Plank Curbs-12'
 115-Ent-
 150-Lake-60
 144-End 112' Top 12'
 142-5' Plank Bottom-20'
 124-PP-18
 8' Willows-35'
 13 Plank " } 12'
 Bottom " } 20'
 10' G.R. 13' Lake-35'



11'

Plank Curb - 13.8'

+55-Fc-32' End G.R.-12'

+02-10' Rep Fc-25

26 G.R.-11.5'

+79-G.P.-15'

G.R.-11.5'

+67-Fc Cor 49'

25 G.R.-11.5'

Masonry Wall

-H.W.-4' Wing - 7' H.W.-6' Wing

+52-End 36' Conc. Culv.-32'

+50-G.R.-12'

+47-G.P.-15'

24 G.R.-11.5'

+32-Box G.R.-12'

23

12' 9'

G.R.-12.5'

22

14' 8'

G.R.-18'

14' 7'

G.R.-12.5'

21

16' 7'

G.R.-12.5'

+50'

16' 6'

+02-Plank Spillway-14'-22.7'

Plank Curb-14.2'

+76-M.P.-31'

Plank Curb-14.5'

+49-Plank Spillway-14.5-19.5'

Plank Curb-19.4'-~~19.5'~~

+79-Plank Spillway-19.6'-22'

+50-Plank Curb-19.4'

+44-M.P.-32'

+31-End G.S.-14'

G.R.-13.5'

+72-18" O.-35'

+82-Box Gable G.R. to Plank Curb-13.2'

+78-End 36' Conc. Culv.-27.5'

+57-Retain Wall-33'

+51-G.R.-23' +50-15" O.-35'

+41-Retain Wall-45'

+38-Retain Wall-60' +50-Long Tie

+23-Box G.R.-31'

+07-End-11'-35'

Plank Spillway-13'-25'

+96-Box Gable G.R.-13'

+81-M.P.-23'

+23-M.P.-22'

+89-54p.-23'

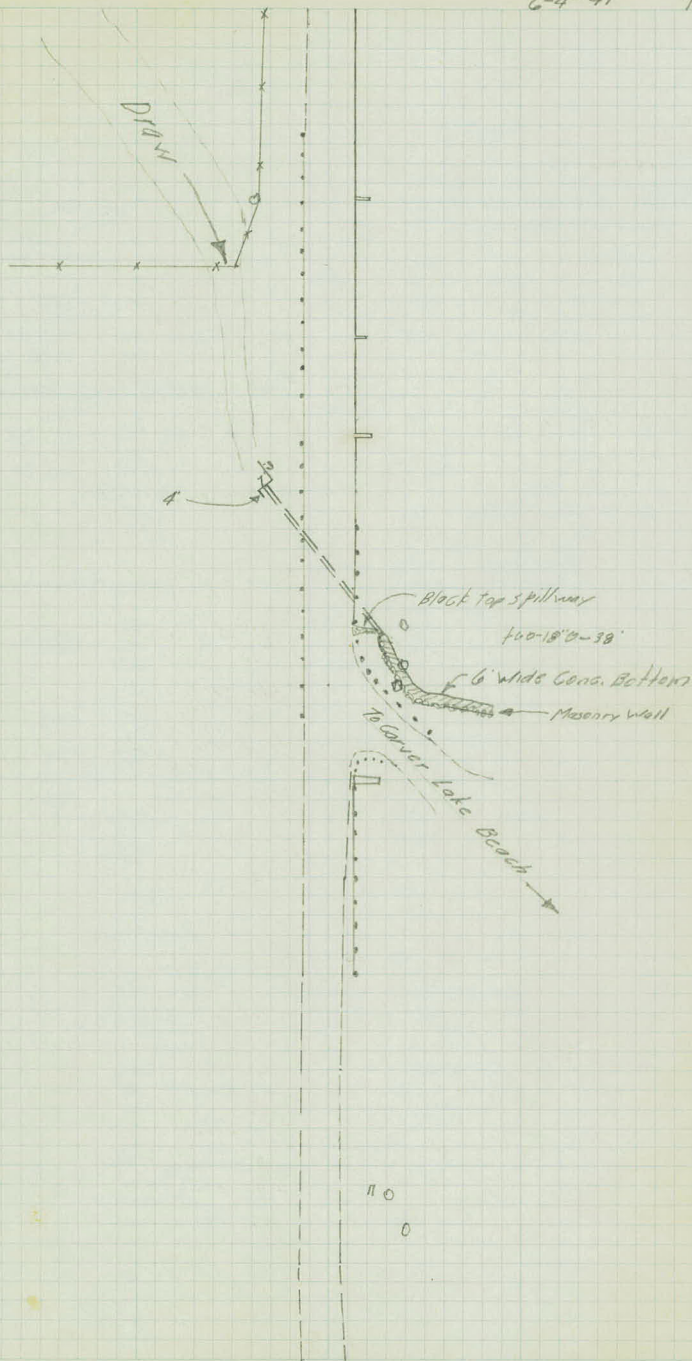
+86-15" O.-31'

+84-Box G.R.-12'

+68-16" O.-40'

20

14' 9'



+68-Kasec Tie to Fe
 +62-Bag Cattle S. R. + Plank Cur 6-116'
 +55-Bridge-23'
 +49-Fe-43'
 +57-8 Apple Tree 42' + Bag Brush

33 +18-PP-26' 9' 11'

+66-Winding Rd Signs -17' 10' 10'

32 +90-B Ent-46' 11' 12'
 +87-PP-19' +90-Ent
 +58-Ent.

11' 11' +54-End Fe-58'

31 +15-RR Ent
 FG-44 11' 12' Fe-35'

+72-Dim Fe-33' +73-Dim Fe-30'
 +70-Road Tie to Ent. 11' 10'
 +49-PP-24'

30 Ent G.R. 13.5' Fe-30' 10' 9' +10-Ent G.R. 12.5' Fe-57'

29 Fe-33' G.R.-11.5' 10' 11' G.R.-12.5'

+93-X Drive 24' X 34.8' Con. Curb. 22' 32.8'
 +75-PP-26'

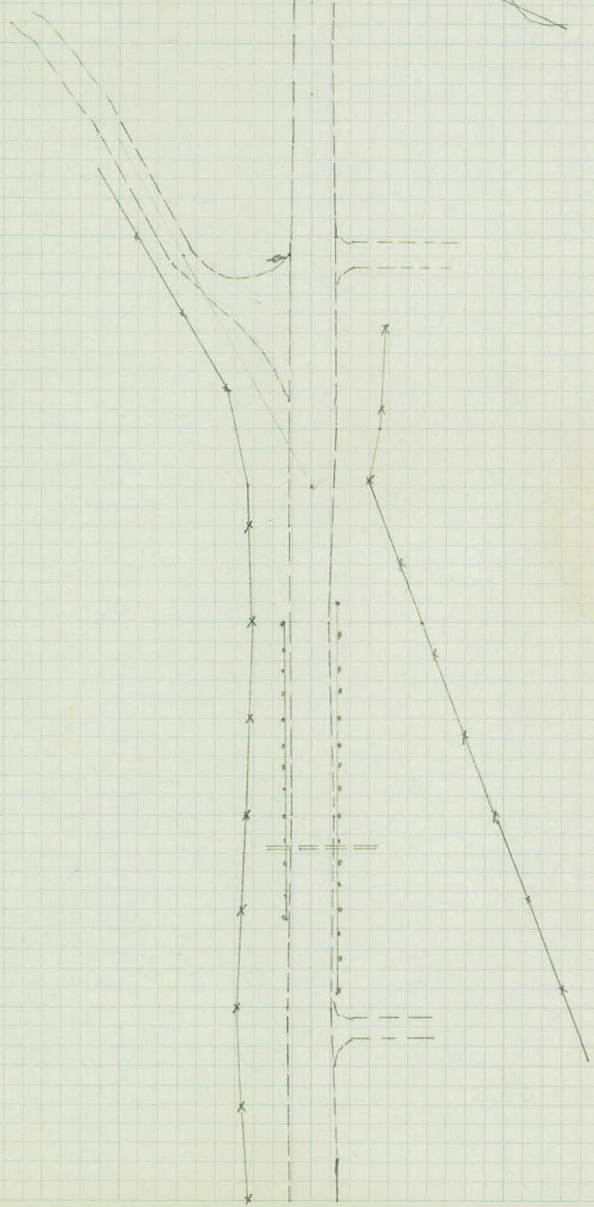
+45-Bag G.R. 12'

28 Fe-38' 12' 10' +107-Rd G.R. 13'

+87-End F.

27 +12-G.P.-23'
 Fe-33' 11' +121-End Plank Curb-132'
 +16-PP-20'

Hog Yard
Heavy Brush & Trees.



+59-PP-28'

40

11' 11'

G.R-12.5

+43-Ed. 5190-14'

39 +106-PP-28'

12'

G.R-12'

38

11' 11'

G.R-12.5'

+172-End G.R-12.5
+58-PP-27'

+32-X Drain 30" X 42.4' Conc.

20' 22.5'

37

12'

9' 10'

G.R-12'

36 +13-PP-27'

G.R-12'

8' 9'

+80-Beg. Cable G.R-13'

+65-Fc Cor-34'

+13-18" Pipe-41'

+12-18" Pipe-35'

+04-18" Pipe-42'

35

G.R-12'

9'

+33-G.R-27'

+32-Res. 12" x 36" - on G.R.

+25-Fmt G.R. + Mark Curb-11.9'

8 Fmt-46'

Beg. G.R-56'

+97-End Fc-38'

+67-PP-26'

+64-Plank Spillway-12'-30' Fc-35'

+26-14" Pipe-31'

+20-15" Pipe-36'

+02-Beg. G.R-12.5'

34

9'

Brush-34'

Fc-4.5'

PLAN SURVEY

E. CO. LINE

Carvers Ave. to Highwood Ave.

INDEX

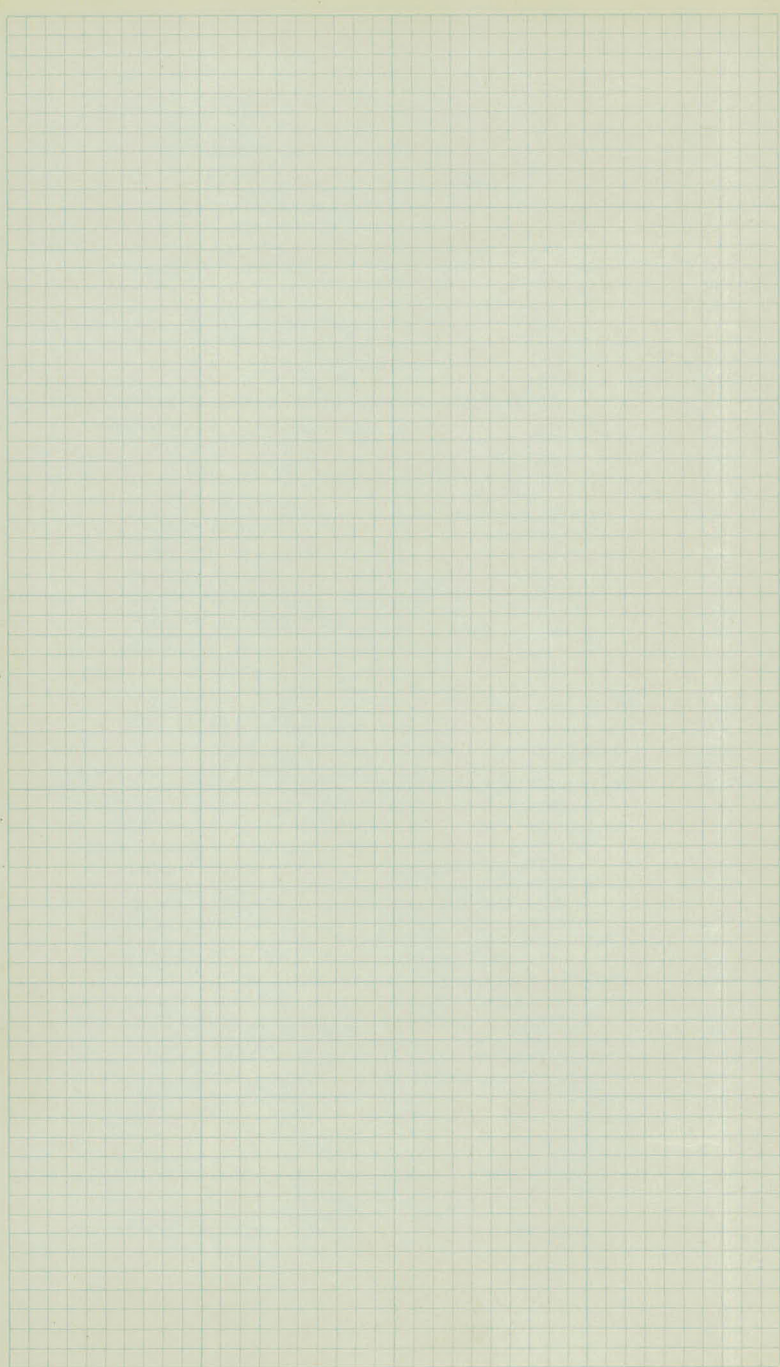
Align - 1-4

Topog - 5-12

Bench } - 13-14
Levels }

Sections - 15-24

Completed 6-21-41



Cult

Cult

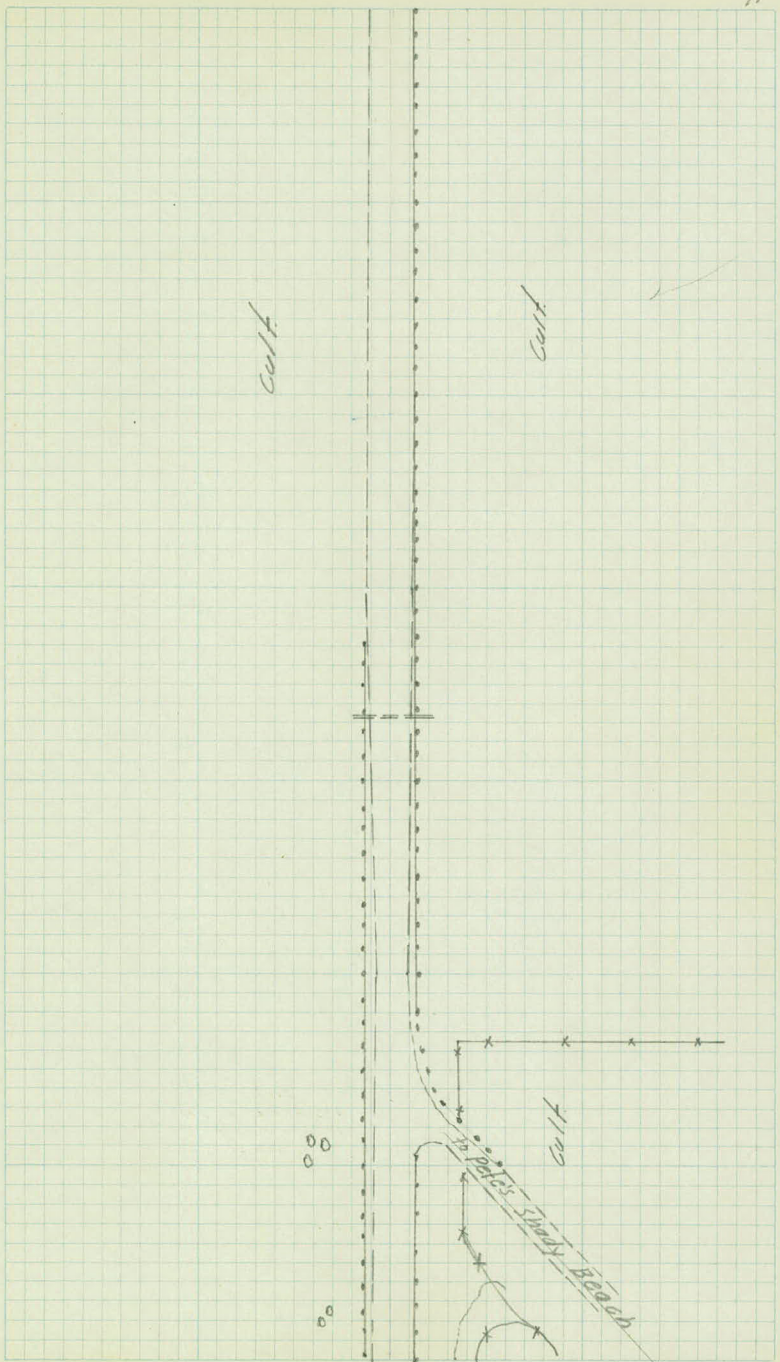
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X X X X X

Shark Beach

Cult



13' 12'

+75 Rod -13'

+57-Ent 55'

+15-Ent 46'

+85-Rod 12'

Broken Mono. Cuts N.G.)
+26-Rod Ent. Cut 19' 10' ex.
+66-Rod 105' 13'
+01-GR-27'

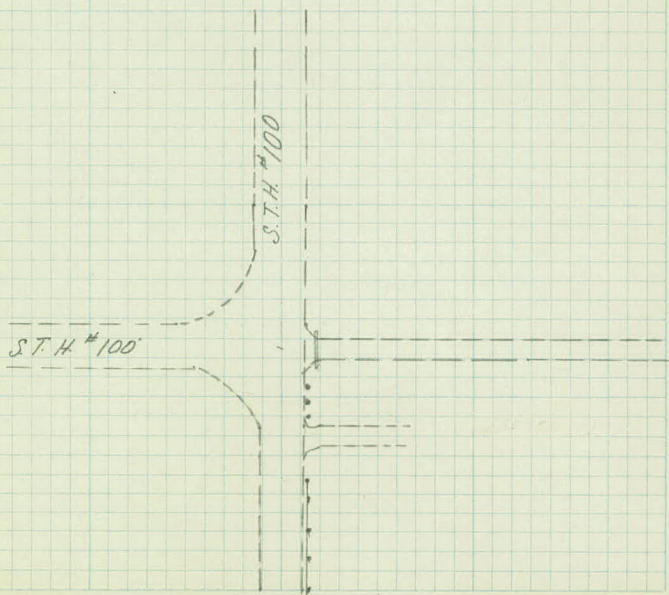
+90-
+30-GR 161-13'
+78-Ent.
+57-Ent 68-18.5'

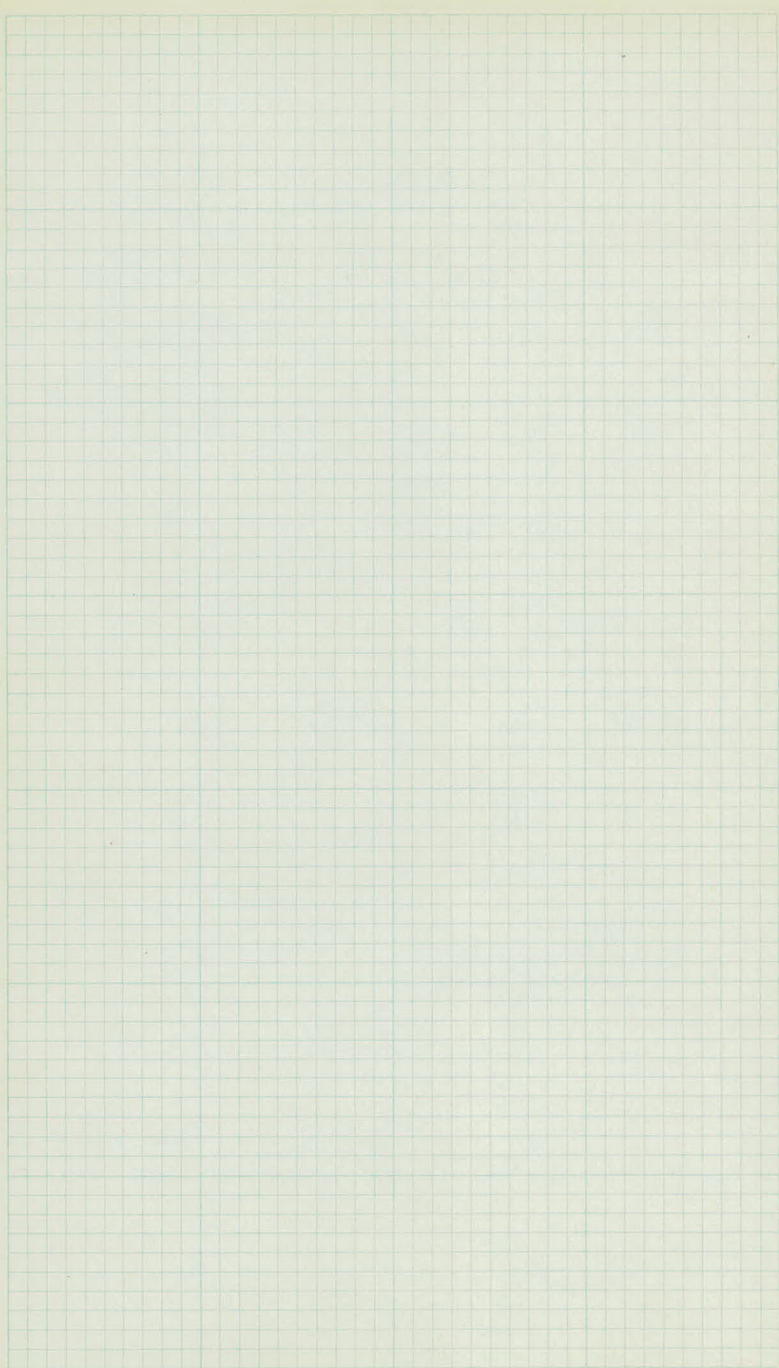
42 P.H. 30

41

11' 11'

G.R. -12.5'





Bench Levels.

Sta	+	π	-	E/cv
B.M.	10.44	990.82		(980.38)
T.P.	1.14	989.26	2.70	988.12
T.P.	0.15	976.42	12.99	976.27
B.M.	0.40	963.82	13.00	963.42
T.P.	0.38	950.62	13.58	950.24
T.P.	0.38	937.48	13.52	937.10
T.P.	1.00	924.98	13.50	923.98
B.M.			13.54	911.44
T.P.	5.31	919.51	10.78	914.20
T.P.	8.57	927.88	0.20	919.31
B.M.	13.46	935.76	5.58	922.30
T.P.	13.40	948.60	0.56	935.20
T.P.	13.77	962.04	0.33	948.27
B.M.	0.24	962.06	0.22	961.82
T.P.	0.80	949.18	13.68	948.38
T.P.	1.10	941.40	11.88	937.30
B.M.			2.67	938.73

5-27-41
K.H.
L.G.
M.B.
G.N.

14

Lt.

R.

Rt.

Top Conc Base at St. Sign Carver Ave + E. Co. Line

Top E. End X Drain. 22 Rt. sta. 7+60

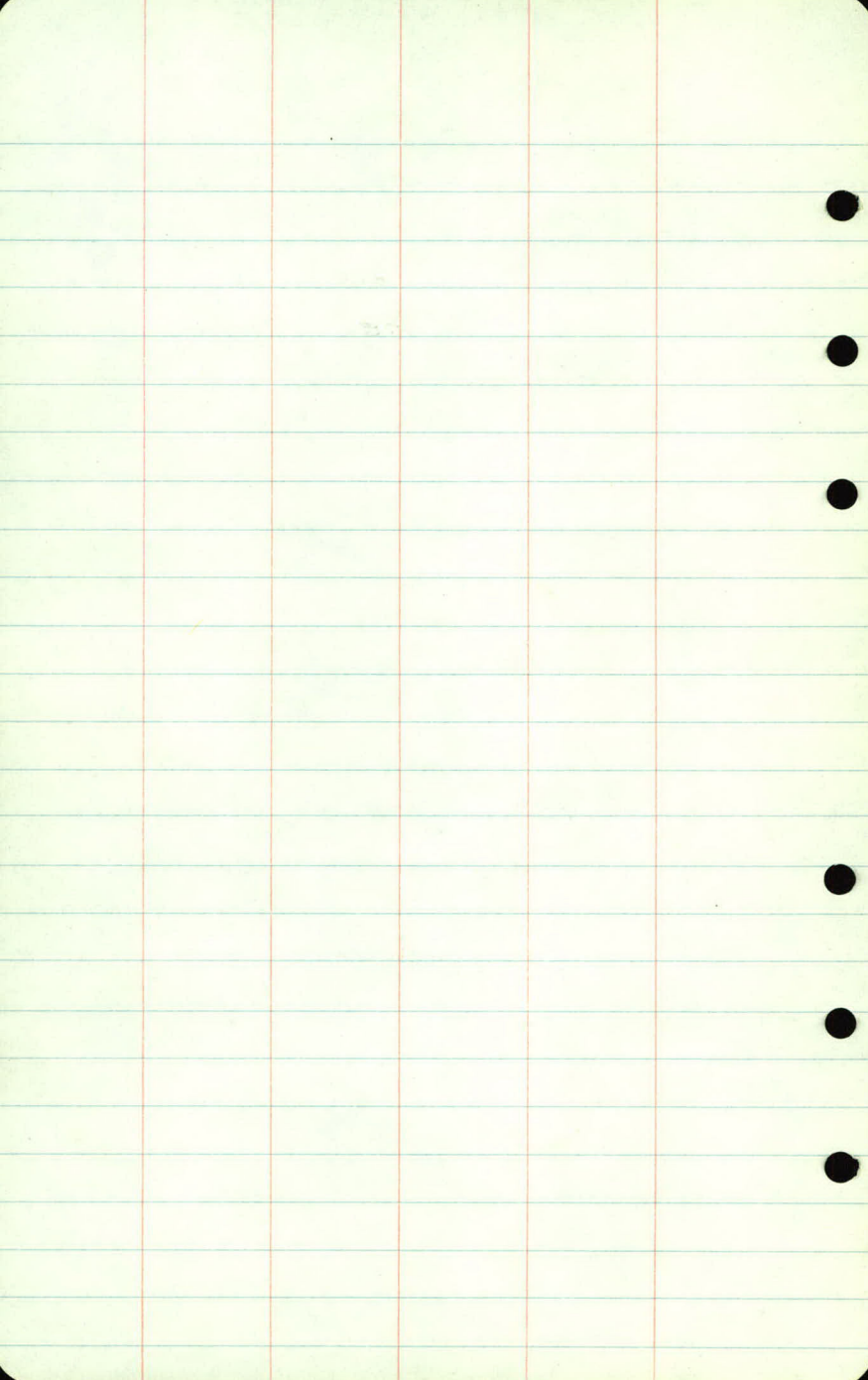
(of Spillway)

Top S.E. Cor Conc. H. W. of outlet of Carver Lake. 35 Rt. sta. 12+45

Spike in RR #638 1/3 23 Rt. sta. 22+81

Spike in RR 19 Lt. sta. 31+87

P.R. Spike in High Line Pdc. N.E. Cor. Highway Ave. & E. Co. Line.



X Sections

Width of X Sections from ϕ .

4+65 to 12+00 = 75' Rt.

4+65 to 9+00 = 75' Rt.

9+00 to 12+53 = 80' to 60' Rt.

20+00 to 24+52 = 100' Lt.

20+00 to 23+00 = 80' to 60' Rt.

25+00 to 26+00 = 75' Lt.

24+00 to 27+00 = 100' Rt.

32+00 to 33+62 = 60' Rt. & Lt.

all other sections are 50' from ϕ .

✓

Sta	+	π	-	Elev
B.M.	10.95	991.33.		980.38

0	+00			80.7
---	-----	--	--	------

	+50			82.2
--	-----	--	--	------

1				83.9
---	--	--	--	------

	+28			85.0
--	-----	--	--	------

	+54			85.8
--	-----	--	--	------

2				87.2
---	--	--	--	------

	+28			88.0
--	-----	--	--	------

T.P.	11.17	1000.67.	1.83	989.50.
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	+69			89.0
--	-----	--	--	------

3				89.5
---	--	--	--	------

	+36			89.8
--	-----	--	--	------

	+70			89.5
--	-----	--	--	------

LT

E

RT

Top Conc. Base of St. Sign Corner Ave. + E. Co. Line

143	138	130	114	106	107	115	113	84	70	6.9
50	33	18	14		13	16	25	29	42	50

142	125	117	97	91	95	103	101	53	31	
50	27	18	14		13	16	23	30	50	

130	98	96	80	74	79	94	93	25	0.8	
50	28	18	14		14	17	22	31	50	

118	89	68	67	83	82	70	63	67	83	80	07	10.3
50	24	31	28	22	17	14		13	17	21	33	50

115	59	56	77	77	62	55	60	77	78	10.2	11.6
50	32	25	20	16	13		14	17	21	33	50

140	116	91	81	46	41	45	60	63	25	1.0	
50	34	28	22	14		13	17	21	28	50	

108	94	81	61	53	35	33	35	42	43	20	0.3
50	44	36	29	18	14		14	15	23	28	50

step 3

128	99	88	134	137	122	117	118	120	72	72
50	36	29	20	17	14		14	24	32	50

106	80	70	119	127	118	112	115	124	117	35	35
50	38	29	22	18	14		12	17	23	36	50

71	78	80	121	124	113	109	114	124	115	21	1.4
50	37	32	22	16	13		14	17	23	38	50

32	41	57	122	128	116	112	118	127	123	115	4.2	3.0
50	39	53	23	17	14		15	18	21	25	36	50

Sta	+	π	-	Elev
		1000.67.		
4				89.1
I.P. 1			0.00	1000.67.
+30				88.4
T.P.	0.80	988.29.	13.18	987.49.
+65				87.3
5				85.8
+40				83.4
+55				82.4
+85				80.1
6				78.7
+20				77.0
I.P.	0.38	975.89.	12.78	975.51.
+50				74.4
+85				71.2

Lt

L

Rt

$\frac{1.7}{50}$ $\frac{30}{37}$ $\frac{116}{24}$ $\frac{130}{16}$ $\frac{118}{13}$ $\frac{116}{14}$ $\frac{119}{16}$ $\frac{125}{24}$ $\frac{118}{35}$ $\frac{49}{50}$ $\frac{36}{50}$

$\frac{0.8}{50}$ $\frac{24}{39}$ $\frac{133}{23}$ $\frac{189}{17}$ $\frac{125}{13}$ $\frac{123}{14}$ $\frac{124}{19}$ $\frac{135}{23}$ $\frac{131}{38}$ $\frac{37}{50}$ $\frac{3.1}{50}$

$\frac{16.2}{28}$ $\frac{28}{21}$ $\frac{3.0}{18}$ $\frac{1.2}{13}$ $\frac{10}{14}$ $\frac{14}{17}$ $\frac{28}{22}$

$\frac{0.0}{28}$ $\frac{4.2}{21}$ $\frac{9.3}{16}$ $\frac{27}{13}$ $\frac{25}{13}$ $\frac{3.0}{19}$ $\frac{4.2}{22}$ $\frac{37}{22}$

$\frac{0.0}{31}$ $\frac{3.2}{26}$ $\frac{6.3}{22}$ $\frac{6.4}{16}$ $\frac{5.1}{13}$ $\frac{4.9}{15}$ $\frac{5.0}{22}$ $\frac{6.4}{23}$ $\frac{6.4}{33}$ $\frac{0.0}{33}$

$\frac{6.3}{23}$ $\frac{7.6}{15}$ $\frac{6.1}{13}$ $\frac{6.2}{10}$ $\frac{5.9}{15}$ $\frac{6.0}{21}$ $\frac{7.5}{25}$ $\frac{4.6}{27}$

$\frac{9.0}{23}$ $\frac{9.1}{14}$ $\frac{8.3}{13}$ $\frac{8.5}{10}$ $\frac{8.2}{15}$ $\frac{8.8}{18}$ $\frac{9.5}{23}$ $\frac{9.3}{37}$ $\frac{0.0}{37}$

$\frac{3.8}{22}$ $\frac{9.1}{25}$ $\frac{11.2}{20}$ $\frac{11.2}{18}$ $\frac{9.6}{13}$ $\frac{9.8}{8}$ $\frac{9.6}{15}$ $\frac{9.9}{20}$ $\frac{11.0}{22}$ $\frac{11.0}{22}$

$\frac{7.9}{27}$ $\frac{12.3}{22}$ $\frac{13.3}{19}$ $\frac{12.9}{17}$ $\frac{11.6}{13}$ $\frac{11.6}{9}$ $\frac{11.3}{19}$ $\frac{11.9}{26}$ $\frac{13.9}{33}$ $\frac{6.4}{33}$

N4, 1 to Top Curb.

$\frac{3.0}{22}$ $\frac{3.0}{15}$ $\frac{1.6}{13}$ $\frac{1.7}{9}$ $\frac{1.5}{17}$ $\frac{1.9}{22}$ $\frac{3.2}{22}$

$\frac{1.7}{30}$ $\frac{7.1}{19}$ $\frac{7.1}{18}$ $\frac{4.7}{13}$ $\frac{4.9}{9}$ $\frac{4.7}{18}$ $\frac{5.3}{20}$ $\frac{7.1}{23}$ $\frac{7.4}{23}$

Sta	+	π	-	Elev	✓
				975.89.	
7				69.7	.
	+11			68.8	.
	+20			67.9	.
	+48			65.2	.
	+72			62.9	.
8				60.3	✓ ✓
	+15			58.9	✓ ✓
	+50			55.6	✓ ✓
B.M.			12.47	963.42.	963.42
I.P.	5.76	1006.43.		1000.67.	
4	+65			87.3	✓ ✓
5				85.8	✓ ✓
	+90			83.4	✓ ✓

Lt

R

Rt

$$\frac{00}{34} \frac{86}{21} \frac{86}{19} \frac{60}{19} \frac{64}{9} \frac{62}{15} \frac{68}{18} \frac{80}{28} \frac{84}{28}$$

$$\frac{94}{22} \frac{87}{18} \frac{71}{15} \frac{15}{8} \frac{71}{16} \frac{78}{21} \frac{92}{29}$$

$$\frac{40}{30} \frac{106}{23} \frac{83}{15} \frac{84}{9} \frac{80}{15} \frac{85}{22} \frac{104}{26} \frac{101}{27} \frac{91}{31} \frac{73}{75} \frac{2.8}{75}$$

$$\frac{41}{75} \frac{45}{50} \frac{55}{32} \frac{136}{19} \frac{136}{18} \frac{108}{74} \frac{108}{10} \frac{107}{18} \frac{109}{22} \frac{124}{27} \frac{126}{48} \frac{86}{60} \frac{51}{75} \frac{0.0}{75}$$

$$\frac{148}{50} \frac{170}{35} \frac{162}{20} \frac{131}{13} \frac{132}{9} \frac{130}{17} \frac{120}{22} \frac{154}{23} \frac{154}{26} \frac{134}{26} \frac{75}{43} \frac{1.5}{60} \frac{136}{75}$$

$$(15.6) \quad \frac{49}{41} \frac{111}{60} \frac{141}{75}$$

$$(17.0) \quad \frac{42}{42} \frac{101}{60} \frac{132}{75}$$

$$(20.3) \quad \frac{102}{40} \frac{70}{60} \frac{54}{75}$$

Top E. End X Drain 22 Rt sta 7+60

From T.P. #1

$$\frac{64}{75} \frac{69}{48} \frac{74}{47} \frac{77}{42} \quad (19.1) \quad \frac{51}{46} \frac{60}{54} \frac{70}{75}$$

$$\frac{76}{75} \frac{75}{60} \frac{69}{45} \quad (20.6) \quad \frac{25}{51} \frac{31}{60} \frac{39}{75}$$

$$\frac{76}{75} \frac{71}{60} \frac{65}{49} \quad (23.0) \quad \frac{38}{59} \frac{43}{63} \frac{45}{75}$$

Sta	+	π	-	Elev.		
		1006.43.				✓
5	+55			82.4	✓	✓
	+85			80.1	✓	✓
6				78.7	✓	✓
	+20			77.0	✓	✓
T.P.	0.96	993.76.	1363	992.80.		
	+50			74.4	✓	✓
	+85			71.2	✓	✓
7				69.7	✓	✓
	+11			68.8	✓	✓
	+20			67.9	✓	✓
T.P.	0.78	981.10.	1344	980.32.		
T.P.	1.03	973.21.	8.92	972.18.		
B.M.	0.90	964.32.	9.78	963.43.	963.42	
B				60.3		

Lt

R

Rt

$$\frac{7.0}{75} \quad \frac{6.7}{63} \quad \frac{5.8}{51} \quad (24.0) \quad \frac{3.1}{55} \quad \frac{4.2}{75}$$

$$\frac{6.1}{75} \quad \frac{5.7}{64} \quad \frac{5.0}{56} \quad (26.3) \quad \frac{4.5}{57} \quad \frac{5.0}{75}$$

$$\frac{6.4}{75} \quad \frac{6.3}{64} \quad \frac{5.9}{54} \quad (27.7) \quad \frac{6.2}{55} \quad \frac{6.6}{75}$$

$$\frac{8.6}{75} \quad \frac{8.8}{64} \quad \frac{8.4}{53} \quad (29.4) \quad \frac{10.5}{52} \quad \frac{10.6}{60} \quad \frac{10.5}{75}$$

$$\frac{1.2}{75} \quad \frac{1.9}{61} \quad \frac{2.0}{51} \quad (19.4) \quad \frac{2.7}{49} \quad \frac{2.5}{58} \quad \frac{1.9}{75}$$

$$\frac{6.9}{75} \quad \frac{6.9}{58} \quad \frac{6.6}{48} \quad (22.6) \quad \frac{7.0}{48} \quad \frac{7.9}{60} \quad \frac{9.0}{75}$$

$$\frac{7.5}{75} \quad \frac{8.0}{60} \quad \frac{8.6}{48} \quad (24.1) \quad \frac{11.0}{45} \quad \frac{12.7}{60} \quad \frac{14.6}{75}$$

$$\frac{9.2}{75} \quad \frac{8.7}{54} \quad \frac{9.4}{46} \quad (25.0) \quad \frac{13.2}{44} \quad \frac{14.8}{60} \quad \frac{17.8}{75}$$

$$\frac{12.1}{75} \quad \frac{11.6}{60} \quad \frac{11.7}{44} \quad (25.9)$$

Top E. End X Drain 22' Lt slo 1+60

$$\frac{13.3}{50} \quad \frac{15.3}{36} \quad \frac{12.3}{34} \quad \frac{14.8}{33} \quad \frac{4.8}{15} \quad \frac{4.0}{12} \quad \frac{4.3}{8} \quad \frac{4.0}{17} \quad \frac{4.3}{20} \quad \frac{6.6}{20} \quad \frac{7.0}{23}$$

✓

6

sta	+	π	-	Elev.
		964.32.		

8	+15			58.9
---	-----	--	--	------

	+50			55.6
--	-----	--	--	------

T.P.	0.28	954.90.	9.70	954.62.
------	------	---------	------	---------

8	+50			(55.6)	✓ ✓
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	+80			52.9
--	-----	--	--	------

9	+77			
---	-----	--	--	--

9	+09			50.3
---	-----	--	--	------

	+37			47.7
--	-----	--	--	------

	+76			44.0
--	-----	--	--	------

T.P.	3.00	944.33.	13.57	941.33.
------	------	---------	-------	---------

9	+09			(50.3)	✓ ✓
---	-----	--	--	--------	-----

	+37			(47.7)	✓ ✓
--	-----	--	--	--------	-----

	+76			(44.0)	✓ ✓
--	-----	--	--	--------	-----

Lt.

E

Rt.

$$\frac{181}{75} \quad \frac{194}{50} \quad \frac{200}{37} \quad \frac{129}{28} \quad \frac{66}{16} \quad \frac{56}{13} \quad \frac{59}{8} \quad \frac{54}{15} \quad \frac{58}{20} \quad \frac{83}{25}$$

$$\frac{139}{27} \quad \frac{109}{18} \quad \frac{88}{12} \quad \frac{90}{9} \quad \frac{87}{17} \quad \frac{86}{20.3} \quad \frac{10.0}{20.3} \quad \frac{111}{25}$$

Top Bolt G.C. Post Lt & +

$$S.S. \quad \frac{188}{75} \quad \frac{137}{56} \quad \frac{78}{38} \quad (+0.7)$$

$$S.S. \quad \frac{20.6}{75} \quad \frac{138}{53} \quad \frac{111}{42} \quad \frac{85}{28} \quad \frac{23}{13} \quad \frac{24}{9} \quad \frac{20}{11} \quad \frac{18}{14} \quad \frac{12}{15} \quad \frac{45}{20} \quad \frac{54}{20} \quad \frac{8.0}{24} \quad \frac{75}{34} \quad \frac{0.0}{35} \quad \frac{13.0}{35}$$

$$\frac{16.4}{75} \quad \frac{14.3}{50}$$

$$\frac{147}{32} \quad \frac{87}{20} \quad \frac{52}{13} \quad \frac{53}{10} \quad \frac{46}{9} \quad \frac{45}{13} \quad \frac{42}{19} \quad \frac{74}{23} \quad \frac{121}{28} \quad \frac{123}{29} \quad \frac{85}{34} \quad \frac{7.4}{50} \quad \frac{4129}{51} \quad \frac{08}{75}$$

$$\frac{138}{27} \quad \frac{92}{18} \quad \frac{77}{14} \quad \frac{79}{10} \quad \frac{72}{10} \quad \frac{68}{14} \quad \frac{68}{25} \quad \frac{127}{27} \quad \frac{170}{36} \quad \frac{170}{40} \quad \frac{124}{50} \quad \frac{111}{50} \quad \frac{83}{75}$$

$$\frac{17.8}{28} \quad \frac{130}{18} \quad \frac{118}{13} \quad \frac{118}{11} \quad \frac{10.9}{10} \quad \frac{10.3}{15} \quad \frac{10.1}{28}$$

$$\frac{17.0}{82} \quad \frac{13.0}{69} \quad \frac{9.0}{50} \quad (+6.0)$$

$$\frac{172}{60} \quad \frac{122}{43} \quad (+3.4)$$

$$\frac{172}{44} \quad (0.3) \quad \frac{106}{34} \quad \frac{114}{38} \quad \frac{114}{43} \quad \frac{103}{45} \quad \frac{89}{62} \quad \frac{79}{77}$$

Sta	+	T	-	Elev	
		944.33.			✓
10				41.7	.
	+50			36.8	.
	+78			34.1	.
11				32.1	.
I.R.	0.27	931.42.	13.18	931.15.	
9	+37			47.7	✓ ✓
	+76			44.0	✓ ✓
10				41.7	✓ ✓
11	+26			29.8	.
	+44			28.2	.
	+72			25.9	.
12				23.8	.
I.R.	1.70	921.94.	11.18	920.24.	

Lt

4

Rt

$$\frac{105}{30} \frac{53}{20} \frac{37}{15} \frac{36}{12} \frac{26}{11} \frac{21}{9} \frac{19}{14} \frac{52}{20} \frac{153}{38} \frac{145}{49} \frac{152}{75}$$

$$\frac{174}{35} \frac{116}{23} \frac{89}{17} \frac{82}{14} \frac{82}{11} \frac{75}{10} \frac{71}{13} \frac{66}{16} \frac{71}{16} \frac{140}{28} \frac{188}{35} \frac{19.2}{75}$$

$$\frac{184}{30} \frac{119}{17} \frac{110}{14} \frac{110}{11} \frac{102}{11} \frac{96}{13} \frac{92}{16} \frac{100}{16} \frac{189}{30} \frac{193}{75}$$

$$\frac{149}{20} \frac{131}{15} \frac{130}{11} \frac{122}{11} \frac{116}{11} \frac{122}{17} \frac{143}{25} \frac{173}{46} \frac{191}{75}$$

Tip eyeball on G.R. Rt 1142 B&G.R.

$$\frac{122}{100} \frac{7.7}{81} (+16.3)$$

$$\frac{188}{94} \frac{153}{82} \frac{118}{62} (+12.6)$$

$$\frac{198}{89} \frac{160}{62} (+10.3)$$

$$\frac{167}{42} \frac{83}{26} \frac{32}{18} \frac{24}{15} \frac{26}{12} \frac{16}{10} \frac{10}{20} \frac{07}{25} \frac{00}{40} \frac{20}{75} \frac{68}{75}$$

$$\frac{109}{28} \frac{44}{16} \frac{41}{14} \frac{41}{12} \frac{32}{11} \frac{26}{11} \frac{21}{12} \frac{26}{15} \frac{84}{24} \frac{93}{32} \frac{90}{45} \frac{78}{75}$$

$$\frac{148}{30} \frac{73}{16} \frac{63}{14} \frac{64}{11} \frac{5.5}{9} \frac{51}{12} \frac{48}{16} \frac{55}{25} \frac{108}{50} \frac{107}{50} \frac{97}{75}$$

$$\frac{144}{24} \frac{94}{17} \frac{84}{14} \frac{85}{12} \frac{76}{11} \frac{72}{13} \frac{68}{15} \frac{74}{25} \frac{131}{34} \frac{166}{41} \frac{160}{53} \frac{136}{75}$$

Sta	+	π	-	Elev	✓
		921.94.			
10	+50			36.8	✓ ✓
	+78			34.1	✓ ✓
11				32.1	✓ ✓
	+26			29.8	✓ ✓
	+44			28.2	✓ ✓
	+72			25.9	✓ ✓
12				23.8	✓ ✓
	+41			20.8	
	+53			20.0	

B. M. 11.81 923.25. 10.47 911.47 (911.44)

L.H.

L

R.H.

$$\frac{123}{90} \frac{93}{65} \frac{77}{59} (+14.9)$$

$$\frac{136}{90} \frac{119}{72} \frac{70}{54} (+12.2)$$

$$\frac{139}{90} \frac{122}{70} \frac{87}{52} (+10.2)$$

Top Bank
of Ditch

$$\frac{140}{82} \frac{112}{62} \frac{90}{50} (+7.9)$$

$$\frac{131}{76} \frac{109}{60} \frac{96}{45} (+6.3)$$

$$\frac{133}{72} \frac{117}{54} \frac{97}{39} (+4.0)$$

$$\frac{134}{70} \frac{127}{63} \frac{128}{62} \frac{146}{57} \frac{138}{55} \frac{115}{47} \frac{101}{35} (+1.9)$$

$$\frac{114}{75} \frac{128}{55} \frac{130}{54} \frac{137}{48} \frac{133}{47} \frac{101}{38} \frac{23}{28} \frac{16}{16} \frac{19}{12} \frac{11}{12} \frac{28}{9} \frac{02}{13} \frac{05}{15} \frac{39}{21} \frac{117}{33} \frac{128}{41} \frac{121}{37} \frac{124}{75}$$

Ground
↓
FL.
Cuts
↓Top
K.W.
↓
F.L.
Cuts
↓

920.49

$$\frac{141}{33} \frac{1570}{33} \frac{114}{28} \frac{98}{17} \frac{27}{15} \frac{23}{13} \frac{26}{11} \frac{19}{9} \frac{16}{12} \frac{13}{16} \frac{19}{30} \frac{105}{35} \frac{1051}{35} \frac{1566}{35} \frac{1392}{6-16-41}$$

$$\frac{140}{45} \frac{123}{46} \frac{116}{56} \frac{104}{70}$$

Top S.E. Cor. H.W. 35' R.H. Sta. 12+45

$$\begin{array}{r} 23.25 \\ 08.49 \\ \hline 14.76 \end{array}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

923.25.

12 + 6.5

19.4

13

17.6

+30

16.3

453

15.5

14

14.8

725

14.5

465

14.2

15

14.0

T.P.

5.20

9/9.27.

9.18

914.07.

431

13.9

470

13.7

16

13.8

Lt

C

Rt

Comp.
Lokk
Roa.

11.5	139	139	111	51	43	46	39	36	34	43	132	139	14.8	166	180
50	37	32	23	15	13	11	10	14	17	32	38	38	50	55	

82	100	105	98	66	61
50	35	28	19	13	11

57	55	61	13.4	14.8	162	181
11	16	27	34	47	75	

43	64	83	73	70	69	73	10.5	13.1	14.4	14.8	180
50	26	22	11	12	14	20	31	45	46	75	

25	34	57	82	8.8	7.9	78	78	84	10.1	12.1	14.1	14.8	174
50	30	28	23	17	11	10	14	19	30	54	56	75	

0.5	1.5	3.9	8.0	9.3	86
50	32	32	24	16	11

85	93	105	104	8.1	10.9	136	143	148	159
13	17	20	26	38	58	65	66	75	

00	1.5	3.5	9.2	96	87	88	96	111	112	95	120	137	148	156
50	33	31	21	15	12	12	17	22	27	37	56	64	75	

1.0	30	61	95	97	90	91	101	116	117	107	126	138	148	156
50	32	30	21	16	11	13	17	23	26	35	50	60	75	

34	61	99	102	93
50	28	23	15	11

9.3	101	118	132	146	148	173
12	18	36	50	52	75	

W.E.

22	28	45	64	64	59	53	54	61	64	83	96	108	128
50	42	26	22	20	17	11	10	14	18	25	36	75	

53	58	64	54	54	56	65	68	94	105	108	122	131
50	31	17	13	10	11	15	20	24	25	50	75	

57	82	84	51	51
50	28	24	14	9

55	66	69	98	108	123	121
11	15	21	25	50	75	

J

Sta	+	π	-	Elev
		919.27.		

16	+50			13.7
----	-----	--	--	------

17				13.9
----	--	--	--	------

	+50			14.5
--	-----	--	--	------

18				15.9
----	--	--	--	------

	+50			17.7
--	-----	--	--	------

19				19.3
----	--	--	--	------

T.P.	9.82	928.82.	0.27	919.00
	+33			20.6

	+58.6			21.5
--	-------	--	--	------

20				22.5
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	+38			23.1
--	-----	--	--	------

	+18			23.5
--	-----	--	--	------

LH

K

RH

$\frac{80}{50} \frac{95}{33} \frac{114}{31} \frac{116}{27} \frac{101}{25} \frac{98}{22} \frac{55}{15} \frac{51}{11} \frac{56}{11} \frac{66}{15} \frac{68}{15} \frac{94}{20} \frac{108}{24} \frac{125}{50} \frac{134}{75}$

$\frac{111}{50} \frac{117}{37} \frac{123}{36} \frac{123}{34} \frac{116}{32} \frac{115}{28} \frac{58}{17} \frac{50}{13} \frac{54}{13} \frac{62}{17} \frac{67}{17} \frac{100}{22} \frac{108}{28} \frac{130}{50} \frac{136}{75}$

(ET water)

$\frac{135}{50} \frac{124}{32} \frac{110}{29} \frac{48}{15} \frac{48}{13} \frac{55}{13} \frac{65}{16} \frac{108}{25} \frac{123}{30} \frac{128}{50} \frac{134}{75}$

$\frac{131}{50} \frac{124}{31} \frac{106}{27} \frac{35}{15} \frac{34}{13} \frac{38}{13} \frac{46}{16} \frac{101}{28} \frac{108}{31} \frac{114}{50} \frac{110}{66} \frac{110}{75}$

$\frac{134}{50} \frac{124}{36} \frac{102}{28} \frac{1.7}{13} \frac{1.7}{14} \frac{85}{27} \frac{87}{40} \frac{82}{50}$

$\frac{106}{50} \frac{86}{30} \frac{220}{13} \frac{10.3}{12} \frac{54}{25} \frac{54}{33} \frac{41}{50}$

Top Coll in G.R. Rd. Rt. 1940

$\frac{157}{50} \frac{153}{28} \frac{134}{22} \frac{93}{15} \frac{87}{12} \frac{82}{14} \frac{79}{20} \frac{105}{25} \frac{105}{39} \frac{91}{50} \frac{93}{50}$

$\frac{108}{50} \frac{89}{28} \frac{96}{21} \frac{96}{19} \frac{81}{13} \frac{73}{7} \frac{71}{17} \frac{72}{25} \frac{74}{28} \frac{50}{50} \frac{53}{50}$

$\frac{29}{15} \frac{14}{50} \frac{02}{38} \frac{83}{28} \frac{21}{22} \frac{81}{15} \frac{76}{14} \frac{63}{12} \frac{62}{17} \frac{69}{22} \frac{64}{22} \frac{105}{31} \frac{30}{34} \frac{88}{80}$

$\frac{81}{28} \frac{86}{23} \frac{77}{15} \frac{72}{14} \frac{57}{72} \frac{53}{17} \frac{66}{23} \frac{58}{31} \frac{102}{44} \frac{34}{44} \frac{65}{52} \frac{108}{60}$

$\frac{57}{29} \frac{80}{21} \frac{60}{8} \frac{53}{12} \frac{50}{17} \frac{65}{21} \frac{62}{25} \frac{49}{31} \frac{91}{41} \frac{164}{41} \frac{198}{60}$

Sta	+	π	-	Elev	
		928.82.			
21				23.6	
I.P.	3.97	927.16.	5.63	923.19.	
+50				23.2	
B.M.	4.84	927.14.	4.84	922.32.	922.30
22				22.5	
+50				22.2	
23				22.2	
+13				22.3	
+41				22.7	
+78				23.7	
24				24.6	
+25				25.8	
+52				27.6	✓ ✓

Lt

Z

Rt

$$\frac{5.0}{31} \frac{7.6}{21} \frac{6.7}{15} \frac{5.2}{11} \frac{4.9}{14} \frac{4.6}{16} \frac{5.1}{26} \frac{10.5}{40} \frac{18.0}{60} \frac{20.2}{60}$$

$$\frac{1.9}{34} \frac{5.3}{24} \frac{5.2}{15} \frac{4.6}{8} \frac{4.0}{11} \frac{3.9}{13} \frac{3.7}{16} \frac{4.1}{18} \frac{6.1}{48} \frac{16.1}{60} \frac{17.7}{60}$$

Spike in PR 23 Rt str. 22 + 81

$$\frac{3.4}{32} \frac{6.5}{19} \frac{5.1}{8} \frac{4.6}{11} \frac{4.4}{14} \frac{4.3}{18} \frac{5.8}{29} \frac{12.7}{43} \frac{16.4}{60} \frac{16.8}{60}$$

$$\frac{0.3}{34} \frac{4.2}{27} \frac{7.0}{20} \frac{7.0}{17} \frac{5.8}{13} \frac{4.9}{10} \frac{4.8}{13} \frac{4.9}{19} \frac{8.0}{36} \frac{15.2}{60} \frac{15.7}{60}$$

$$\frac{0.0}{34} \frac{2.6}{28} \frac{6.9}{23} \frac{6.8}{16} \frac{5.4}{12} \frac{4.9}{11} \frac{5.3}{15} \frac{5.3}{23} \frac{9.7}{29} \frac{11.4}{60} \frac{12.5}{60} \frac{12.9}{60}$$

$$\frac{0.0}{31} \frac{4.8}{22} \frac{6.9}{18} \frac{5.2}{14} \frac{4.8}{8} \frac{5.1}{13} \frac{5.4}{33} \frac{10.0}{50} \frac{11.3}{50} \frac{12.2}{50}$$

$$\frac{0.6}{32} \frac{4.2}{27} \frac{6.4}{23} \frac{6.4}{18} \frac{4.4}{12} \frac{4.4}{10} \frac{4.8}{10} \frac{6.8}{31} \frac{8.3}{34} \frac{10.8}{48} \frac{13.0}{50} \frac{14.4}{62} \frac{14.3}{75}$$

(FL
Calc)

$$\frac{0.0}{36} \frac{5.2}{29} \frac{6.3}{20} \frac{3.3}{13} \frac{3.4}{15} \frac{4.0}{15} \frac{7.0}{21} \frac{8.4}{26} \frac{11.95}{28} \frac{11.5}{34} \frac{9.9}{35} \frac{6.0}{50}$$

$$\frac{10.3}{40} \frac{5.6}{30} \frac{5.8}{21} \frac{2.3}{14} \frac{2.5}{12} \frac{3.2}{14} \frac{3.0}{21} \frac{7.1}{26} \frac{7.9}{26} \frac{9.1}{26} \frac{9.5}{30} \frac{8.4}{31} \frac{0.9}{50}$$

$$\frac{1.4}{41} \frac{6.7}{25} \frac{6.7}{26} \frac{1.1}{14} \frac{1.3}{12} \frac{2.1}{14} \frac{2.0}{22} \frac{5.5}{32} \frac{6.3}{32} \frac{1.3}{40} \frac{11.2}{43} \frac{7.4}{59} \frac{13.9}{75}$$

(FL
Calc)

$$\frac{1.2}{50} \frac{4.4}{46} \frac{9.7}{38} \frac{11.45}{32} \frac{6.0}{32} \frac{5.1}{23} \frac{1.0}{17} \quad +0.5 \quad \frac{0.6}{13} \frac{0.6}{16} \frac{4.6}{23} \frac{4.4}{28} \frac{0.1}{36}$$

Sta.	+	π	-	Elev.	
		927.14.			✓
25				30.9	✓ ✓
	+30			33.2	✓ ✓
	+50			34.8	✓ ✓
	+75			36.9	✓ ✓
26				39.1	✓ ✓
T.P.	13.81	940.90.	0.05	927.09.	
22	+50			22.2	✓ ✓
23				22.2	✓ ✓
	+13			22.3	✓ ✓
	+41			22.7	✓ ✓
	+78			23.7	✓ ✓
24				24.6	✓ ✓

L.A.

E

R.A.

$$\frac{29}{65} \frac{60}{58} \frac{72}{48} \frac{86}{45} \frac{85}{38} \frac{51}{33} (+3.8)$$

$$\frac{17}{75} \frac{54}{65} \frac{62}{50} \frac{79}{48} \frac{79}{41} (+6.1)$$

$$\frac{47}{75} \frac{58}{55} \frac{75}{52} \frac{73}{42} \frac{31}{35} (+7.7)$$

$$\frac{37}{75} \frac{56}{73} \frac{60}{51} \frac{24}{48} (+9.8)$$

$$\frac{44}{75} \frac{47}{50} (+12.0)$$

$$\frac{00}{64} \frac{53}{50} \frac{104}{37} \frac{123}{36} (18.7)$$

$$\frac{00}{63} \frac{59}{50} \frac{97}{42} (18.7)$$

$$\frac{00}{60} \frac{58}{47} \frac{115}{35} (18.6)$$

$$\frac{28}{50} \frac{46}{44} \frac{104}{38} (18.2)$$

$$\frac{39}{50} (17.2)$$

$$\frac{42}{53} (16.3)$$

Sto	t	T	-	Elev	✓
		940.90			
24	+25			25.8	✓ ✓
	+52			27.6	
25				30.9	
	+30			33.2	
	+50			34.8	
	+75			36.9	
26				39.1	
T.P.	10.36	951.27	+0.01	940.91	
20	+38			23.1	✓ ✓
	+78			23.5	✓ ✓
21				23.6	✓ ✓
	+50			23.2	✓ ✓

Lt

Z

Lt

$$\frac{134}{75} \quad (15.1)$$

$$\frac{134}{13} \quad \frac{13.3}{13}$$

$$\frac{126}{21} \quad \frac{97}{13} \quad \frac{100}{13} \quad \frac{113}{17} \quad \frac{114}{17} \quad \frac{148}{20} \quad \frac{144}{25} \quad \frac{37}{39}$$

$$\frac{137}{27} \quad \frac{74}{14} \quad \frac{77}{12} \quad \frac{87}{16} \quad \frac{88}{19} \quad \frac{118}{23} \quad \frac{118}{39}$$

$$\frac{130}{27} \quad \frac{57}{14} \quad \frac{58}{11} \quad \frac{61}{12} \quad \frac{71}{16} \quad \frac{73}{21} \quad \frac{100}{24} \quad \frac{100}{40} \quad \frac{0.5}{40}$$

$$\frac{120}{32} \quad \frac{35}{15} \quad \frac{35}{12} \quad \frac{40}{10} \quad \frac{49}{15} \quad \frac{52}{18} \quad \frac{68}{24} \quad \frac{69}{36} \quad \frac{0.2}{36}$$

$$\frac{97}{37} \quad \frac{44}{23} \quad \frac{10}{15} \quad \frac{13}{10} \quad \frac{18}{14} \quad \frac{27}{18} \quad \frac{35}{20} \quad \frac{52}{25} \quad \frac{54}{33} \quad \frac{0.9}{33}$$

$$\frac{194}{100} \quad \frac{174}{73} \quad \frac{169}{47} \quad (28.2)$$

$$\frac{113}{100} \quad \frac{113}{73} \quad \frac{109}{55} \quad (27.8)$$

$$\frac{86}{100} \quad \frac{91}{76} \quad \frac{97}{58} \quad (27.7)$$

$$\frac{100}{75} \quad \frac{64}{57} \quad \frac{97}{50} \quad \frac{138}{50} \quad (28.1)$$

✓

Sta + π - Elev

951.27.

22 (22.5) ✓ ✓

+50 (22.2) ✓ ✓

23 (22.2) ✓ ✓

+13 (22.3) ✓ ✓

+41 (22.7) ✓ ✓

+78 (23.7) ✓ ✓

24 (24.6) ✓ ✓

+25 (25.8) ✓ ✓

+52 (27.6) ✓ ✓

26 +34 42.0

+50 43.2

L.f.

Z

R.f.

$$\frac{20}{100} \quad \frac{35}{82} \quad \frac{87}{65} \quad \frac{135}{50} \quad (28.8)$$

$$\frac{+1.5}{100} \quad \frac{1.5}{90} \quad (29.1)$$

$$\frac{+3.5}{100} \quad \frac{07}{86} \quad \frac{70}{71} \quad (29.1)$$

$$\frac{+3.9}{100} \quad \frac{13}{82} \quad \frac{68}{68} \quad (29.0)$$

$$\frac{+5.9}{100} \quad \frac{18}{74} \quad \frac{60}{64} \quad (28.6)$$

$$\frac{+7.4}{100} \quad \frac{0.9}{76} \quad \frac{6.3}{64} \quad (27.6)$$

$$\frac{+5.7}{100} \quad \frac{11}{78} \quad \frac{7.2}{66} \quad (26.7)$$

$$\frac{+31}{100} \quad \frac{2.3}{85} \quad \frac{10.8}{70} \quad \frac{16.2}{56} \quad (25.5)$$

$$\frac{2.5}{100} \quad \frac{11.5}{80} \quad \frac{18.8}{65} \quad (23.7) \quad \frac{14.9}{50} \quad \frac{7.9}{79} \quad \frac{1.4}{100}$$

$$\frac{9.5}{50} \quad \frac{8.9}{24} \quad \frac{9.7}{22} \quad \frac{9.6}{17} \quad \frac{8.6}{14} \quad \frac{9.3}{11} \quad \frac{10.5}{15} \quad \frac{10.5}{20} \quad \frac{12.8}{25} \quad \frac{12.8}{29} \quad \frac{4.9}{36}$$

$$\frac{8.2}{30} \quad \frac{8.3}{40} \quad \frac{7.7}{23} \quad \frac{8.3}{21} \quad \frac{8.3}{15} \quad \frac{7.4}{12} \quad \frac{8.1}{12} \quad \frac{9.2}{17} \quad \frac{9.2}{20} \quad \frac{11.3}{29} \quad \frac{10.0}{29}$$

Sta. + π - Elev. ✓

951.27.

27 46.6

+24 48.0

T.P. 13.88 962.90. 2.25 949.02.

25 30.9 ✓ ✓

+30 33.2 ✓ ✓

+50 34.8 ✓ ✓

+75 36.9 ✓ ✓

26 39.1 ✓ ✓

+34 42.0 ✓ ✓

+50 43.2 ✓ ✓

27 46.6 ✓ ✓

T.P. 8.17 962.61. 8.46 954.44.

+61 50.2

Lt.

R

Rt.

$$\begin{array}{r} 135 \\ 50 \end{array} \quad \begin{array}{r} 122 \\ 30 \end{array} \quad \begin{array}{r} 59 \\ 19 \end{array} \quad \begin{array}{r} 56 \\ 16 \end{array} \quad \begin{array}{r} 43 \\ 13 \end{array} \quad \begin{array}{r} 41 \\ 13 \end{array} \quad \begin{array}{r} 58 \\ 13 \end{array} \quad \begin{array}{r} 65 \\ 16 \end{array} \quad \begin{array}{r} 20 \\ 21 \end{array} \quad \begin{array}{r} 90 \\ 24 \end{array} \quad \begin{array}{r} 35 \\ 31 \end{array}$$

$$\begin{array}{r} 157 \\ 50 \end{array} \quad \begin{array}{r} 147 \\ 32 \end{array} \quad \begin{array}{r} 30 \\ 22 \end{array} \quad \begin{array}{r} 49 \\ 16 \end{array} \quad \begin{array}{r} 33 \\ 14 \end{array} \quad \begin{array}{r} 33 \\ 10 \end{array} \quad \begin{array}{r} 38 \\ 15 \end{array} \quad \begin{array}{r} 45 \\ 19 \end{array} \quad \begin{array}{r} 65 \\ 22 \end{array} \quad \begin{array}{r} 63 \\ 22 \end{array} \quad \begin{array}{r} +0.3 \\ 32 \end{array} \quad \begin{array}{r} 00 \\ 37 \end{array} \quad \begin{array}{r} 01 \\ 50 \end{array}$$

$$\textcircled{32.0} \quad \begin{array}{r} 108 \\ 63 \end{array} \quad \begin{array}{r} 88 \\ 70 \end{array} \quad \begin{array}{r} 53 \\ 87 \end{array} \quad \begin{array}{r} 60 \\ 100 \end{array}$$

$$\textcircled{29.7} \quad \begin{array}{r} 43 \\ 66 \end{array} \quad \begin{array}{r} 32 \\ 70 \end{array} \quad \begin{array}{r} 24 \\ 82 \end{array} \quad \begin{array}{r} 41 \\ 100 \end{array}$$

$$\textcircled{28.1} \quad \begin{array}{r} 16 \\ 68 \end{array} \quad \begin{array}{r} 10 \\ 79 \end{array} \quad \begin{array}{r} 19 \\ 90 \end{array} \quad \begin{array}{r} 26 \\ 100 \end{array}$$

$$\textcircled{26.0} \quad \begin{array}{r} 1.8 \\ 65 \end{array} \quad \begin{array}{r} 0.5 \\ 79 \end{array} \quad \begin{array}{r} 0.8 \\ 100 \end{array}$$

$$\textcircled{23.8} \quad \begin{array}{r} 4.8 \\ 58 \end{array} \quad \begin{array}{r} 1.3 \\ 76 \end{array} \quad \begin{array}{r} +0.4 \\ 89 \end{array} \quad \begin{array}{r} +0.4 \\ 100 \end{array}$$

$$\textcircled{20.9} \quad \begin{array}{r} 63 \\ 53 \end{array} \quad \begin{array}{r} 53 \\ 60 \end{array} \quad \begin{array}{r} 3.3 \\ 71 \end{array} \quad \begin{array}{r} 0.8 \\ 86 \end{array} \quad \begin{array}{r} +1.1 \\ 100 \end{array}$$

$$\textcircled{19.7} \quad \begin{array}{r} 7.8 \\ 49 \end{array} \quad \begin{array}{r} 5.9 \\ 60 \end{array} \quad \begin{array}{r} 3.4 \\ 76 \end{array} \quad \begin{array}{r} 1.5 \\ 85 \end{array} \quad \begin{array}{r} +0.5 \\ 100 \end{array}$$

$$\textcircled{16.3} \quad \begin{array}{r} 104 \\ 37 \end{array} \quad \begin{array}{r} 97 \\ 46 \end{array} \quad \begin{array}{r} 81 \\ 64 \end{array} \quad \begin{array}{r} 60 \\ 75 \end{array}$$

$$\begin{array}{r} 52 \\ 50 \end{array} \quad \begin{array}{r} 69 \\ 32 \end{array} \quad \begin{array}{r} 128 \\ 23 \end{array} \quad \begin{array}{r} 133 \\ 16 \end{array} \quad \begin{array}{r} 125 \\ 13 \end{array} \quad \begin{array}{r} 124 \\ 14 \end{array} \quad \begin{array}{r} 128 \\ 17 \end{array} \quad \begin{array}{r} 141 \\ 27 \end{array} \quad \begin{array}{r} 141 \\ 27 \end{array} \quad \begin{array}{r} 119 \\ 27 \end{array} \quad \begin{array}{r} 118 \\ 34 \end{array} \quad \begin{array}{r} 13.9 \\ 50 \end{array}$$

✓

Sta	+	π	-	Elev.
		962.61		
28				52.3
	+50			54.7
	+83	X Drain		56.0
29				56.6
	+50			58.3
30				60.0
T.P.	13.79	975.08	1.32	961.29
	+50			61.3
31				61.9
	+50			62.1
	+71			62.0
	+81			61.8

Lt

A

Rt

$\frac{6.3}{50} \frac{7.0}{33} \frac{11.7}{25} \frac{11.6}{16} \frac{10.6}{13}$

$\frac{10.3}{11} \frac{10.7}{15} \frac{11.0}{21} \frac{13.6}{33} \frac{15.1}{33} \frac{15.8}{50}$

$\frac{8.2}{50} \frac{10.4}{30} \frac{11.9}{20} \frac{8.1}{13} \frac{8.3}{11} \frac{7.9}{12} \frac{8.0}{15} \frac{9.1}{31} \frac{16.1}{31} \frac{17.0}{50}$

(FL. CIV.)

(FL. CIV.)

$\frac{10.2}{50} \frac{11.2}{34} \frac{12.0}{22.4} \frac{12.8}{22.4} \frac{10.4}{21} \frac{7.2}{13} \frac{7.1}{11} \frac{6.6}{11} \frac{6.5}{15} \frac{6.5}{30} \frac{14.1}{32} \frac{16.5}{32} \frac{15.9}{32} \frac{17.1}{50}$

$\frac{10.5}{50} \frac{11.1}{34} \frac{10.1}{22} \frac{6.5}{13} \frac{6.5}{11}$

$\frac{6.0}{11}$

$\frac{6.0}{11}$

$\frac{6.2}{15} \frac{9.3}{21} \frac{15.1}{33} \frac{16.2}{50}$

$\frac{8.6}{50} \frac{9.6}{33} \frac{9.2}{27} \frac{8.0}{20} \frac{4.9}{13} \frac{4.7}{10} \frac{4.3}{11} \frac{4.0}{15} \frac{4.1}{19} \frac{6.3}{27} \frac{10.6}{34} \frac{11.8}{34} \frac{11.7}{50}$

$\frac{6.5}{50} \frac{6.7}{30} \frac{6.7}{22} \frac{3.5}{14} \frac{3.3}{10}$

$\frac{2.6}{10} \frac{2.3}{14} \frac{2.2}{19} \frac{4.9}{39} \frac{4.9}{39} \frac{3.6}{50}$

$\frac{15.3}{50} \frac{15.1}{28} \frac{14.4}{24} \frac{16.1}{19} \frac{15.1}{14} \frac{14.6}{11} \frac{13.8}{14} \frac{13.7}{17} \frac{14.7}{23} \frac{14.4}{23} \frac{12.7}{26} \frac{11.9}{40} \frac{11.2}{50}$

$\frac{11.2}{50} \frac{8.9}{35} \frac{13.7}{29} \frac{15.1}{19} \frac{14.1}{10} \frac{13.2}{12} \frac{13.4}{23} \frac{13.0}{35} \frac{4.8}{40} \frac{6.0}{40} \frac{7.0}{50}$

$\frac{7.7}{58} \frac{10.8}{35} \frac{13.1}{35} \frac{13.8}{21} \frac{13.8}{9}$

$\frac{13.0}{13}$

$\frac{12.8}{13}$

$\frac{13.2}{16}$

$\frac{12.5}{22}$

$\frac{4.0}{31} \frac{5.5}{50}$

$\frac{11.7}{50} \frac{13.0}{37} \frac{13.9}{10} \frac{13.1}{15} \frac{12.9}{30} \frac{11.3}{31} \frac{7.6}{37} \frac{4.6}{37} \frac{6.2}{50}$

$\frac{11.2}{50} \frac{13.5}{35} \frac{14.1}{25} \frac{15.4}{11} \frac{13.3}{11}$

$\frac{12.9}{19} \frac{11.3}{50}$

✓

Sta	+	π	-	Elev	
		97508.			
31	+91			61.6	
32	4 shot only		13.7		
	+15			(61.2)	✓ ✓
	+50			(60.4)	✓ ✓
	+87			(58.9)	✓ ✓
33	+11			(57.9)	✓ ✓
	+62			(55.2)	✓ ✓
B.M.	2.25	964.02.	13.27	961.81.	(961.82)
32	+15			61.2	
	+50			60.4	
	+87			58.9	
33	4 shot only			(58.4)	✓ ✓

Lt.

R.

Rt.

$$\frac{62}{50} \quad \frac{57}{45} \quad \frac{134}{35} \quad \frac{151}{20} \quad \frac{145}{9} \quad \frac{135}{25} \quad \frac{128}{50} \quad \frac{114}{50}$$
 ~~$\frac{75.8}{60.43}$~~

$$s.s. \frac{73}{60} \quad \frac{53}{43}$$

13.9

$$\frac{5.0}{40} \quad \frac{4.7}{50} \quad \frac{4.8}{60}$$

$$s.s. \frac{44}{60} \quad \frac{3.0}{47}$$

14.7

$$\frac{1.6}{45} \quad \frac{1.8}{50} \quad \frac{2.3}{60}$$

$$s.s. \frac{41.2}{60} \quad \frac{41.7}{52}$$

16.2

$$\frac{8.3}{50} \quad \frac{4.3}{60} \quad L.O.$$

$$s.s. \frac{404}{60} \quad \frac{406}{51}$$

17.2

$$\frac{6.7}{47} \quad \frac{7.3}{50} \quad \frac{7.9}{60}$$

$$\frac{66}{60} \quad \frac{76}{50} \quad \frac{81}{40}$$

19.9

Spk in PP. 19 Lt. 31+87

$$\frac{48}{24} \quad \frac{46}{16} \quad \frac{38}{10} \quad \frac{39}{13} \quad \frac{26}{16} \quad \frac{30}{23} \quad \frac{26}{29} \quad \frac{0.3}{29}$$

$$\frac{52}{24} \quad \frac{60}{17} \quad \frac{47}{13} \quad \frac{37}{12} \quad \frac{35}{16} \quad \frac{44}{24} \quad \frac{34}{24}$$

$$\frac{71}{20} \quad \frac{15}{16} \quad \frac{63}{13} \quad \frac{58}{9} \quad \frac{52}{13} \quad \frac{51}{17} \quad \frac{66}{23} \quad \frac{63}{31} \quad \frac{37}{42} \quad \frac{0.7}{42}$$

51

✓

Sta	+	π	-	Elev.
		964.07		
33	+11			57.9
	+62			55.2
T.P.	1.23	954.56	10.74	953.33
34				53.4
	+45			50.4
T.P.	1.80	949.15	7.21	947.35
	+85			48.0
35				47.1
	+37			44.8
	+70			42.9
T.P.	0.31	942.77	6.67	942.46
36				41.1
	+50			38.8
37				37.0

Lt

R

Rt

$$\frac{75}{22} \frac{84}{16} \frac{68}{11} \frac{62}{13} \frac{61}{17} \frac{76}{17} \frac{72}{22}$$

$$\frac{14}{36} \frac{40}{32} \frac{97}{21} \frac{100}{15} \frac{91}{13} \frac{99}{13} \frac{88}{17} \frac{97}{20} \frac{93}{24} \frac{86}{37} \frac{102}{50} \frac{132}{50}$$

$$\frac{139}{50} \frac{11}{37} \frac{24}{26} \frac{42}{22} \frac{40}{19} \frac{17}{12} \frac{12}{10} \frac{17}{14} \frac{21}{33} \frac{118}{50} \frac{150}{50}$$

$$\frac{39}{50} \frac{81}{32} \frac{78}{20} \frac{43}{13} \frac{42}{16} \frac{45}{12} \frac{43}{34} \frac{160}{50} \frac{201}{50}$$

Top Belt 6 & Pos 111

$$\frac{18}{50} \frac{43}{40} \frac{65}{30} \frac{65}{25} \frac{14}{13} \frac{12}{10} \frac{15}{13} \frac{13}{28} \frac{107}{38} \frac{133}{46} \frac{138}{50} \frac{128}{50}$$

$$\frac{24}{50} \frac{52}{39} \frac{76}{30} \frac{72}{24} \frac{25}{14} \frac{22}{12} \frac{21}{9} \frac{24}{13} \frac{20}{15} \frac{27}{27} \frac{100}{33} \frac{110}{37} \frac{96}{50} \frac{108}{50}$$

$$\frac{56}{50} \frac{66}{39} \frac{77}{33} \frac{84}{20} \frac{49}{14} \frac{44}{14} \frac{48}{14} \frac{52}{24} \frac{166}{45} \frac{174}{50}$$

$$\frac{51}{50} \frac{65}{38} \frac{103}{37} \frac{103}{20} \frac{68}{14} \frac{66}{12} \frac{63}{11} \frac{64}{14} \frac{66}{31} \frac{144}{40} \frac{149}{50} \frac{185}{50}$$

$$\frac{110}{50} \frac{105}{40} \frac{87}{37} \frac{53}{31} \frac{52}{20} \frac{17}{14} \frac{17}{14} \frac{19}{29} \frac{96}{35} \frac{108}{50} \frac{125}{50}$$

$$\frac{41}{50} \frac{58}{34} \frac{64}{19} \frac{46}{14} \frac{41}{11} \frac{40}{9} \frac{42}{12} \frac{38}{14} \frac{43}{26} \frac{113}{50} \frac{143}{50}$$

$$\frac{61}{50} \frac{83}{35} \frac{85}{18} \frac{59}{13} \frac{58}{12} \frac{59}{14} \frac{63}{24} \frac{117}{34} \frac{129}{50} \frac{138}{50}$$

Sta	+	π	-	Elev
		942.77.		
37	+32 X Drain			36.1
	+75			35.4
38				35.2
T.P.	6.83	942.04.	7.56	935.21.
	+50			35.1
39				35.6
	+50			36.3
40				36.8
	+50			37.5
41				38.1
T.P.	7.22	946.12. 946.16	3.14	938.90. 938.94
	+50			38.9
42				40.0

LH

K

PH

(FL)

(FL)

74	89	97	11.03	71	68	67	68	69	12.37	12.3	13.0
50	40	24	203	14	12		12	14	22.7	35	50

74	78	87	94	78	75	74	76	79	11.0	11.9	13.8
50	41	25	18	14	11		11	13	20	27	50

74	79	91	79	76	78	80	11.3	11.7	13.9
50	42	15	12		11	13	19	24	50

57	65	78	72	69	71	77	11.6	12.9	14.0
50	33	15	12		11	13	20	33	50

18	26	74	76	69	64	66	69	87	108	13.7
50	31	24	17	15		11	14	18	30	50

41.7	41.4	00	65	71	62	57	59	62	91	11.5	13.6
50	37	33	25	17	15		12	14	20	34	50

4.09	01	0.9	66	65	54	53	52	54	55	10.7	12.5	13.3
50	35	33	24	17	15	10		11	14	23	34	50

1.3	22	36	48	55	50	48	45	48	51	10.3	11.5	12.0
50	38	29	26	16	14	10		11	14	22	39	50

1.5	24	44	44	4.2	39	4.0	45	84	104
50	40	25	13	10		12	15	23	50

64	7.2	76	74	72	73	76	10.6	12.7
50	36	14	8		11	14	21	50

58	66	71	73	63	61	64	73	95	99	11.0
50	31	30	26	16		12	13	19	27	50

Sta	+	Σ	-	Elev.
		946.12 ✓ 946.16		
42	+13			40.3
	+20			40.5
	+27.72			40.6
	+50		5.5	40.6
43			6.3	39.8
	+50		6.2	39.9
44			5.1	41.0
B.M.			7.40	938.72 938.76 (938.73)

Lt.

C

Rt.

$\frac{53}{50}$	$\frac{62}{36}$	$\frac{50}{29}$	$\frac{54}{14}$	$\frac{58}{12}$	$\frac{62}{16}$	$\frac{69}{19}$	$\frac{99}{27}$	$\frac{98}{50}$	$\frac{123}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

$\frac{28}{50}$	$\frac{34}{43}$	$\frac{50}{17}$	$\frac{56}{11}$	$\frac{59}{11}$	$\frac{72}{29}$	$\frac{94}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{131}{150}$	$\frac{101}{100}$	$\frac{26}{50}$	$\frac{55}{13}$	$\frac{61}{32}$	$\frac{76}{32}$	$\frac{96}{50}$
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Spk. in P.P. N.E. Cor. Highwood Ave. & E. Co Line

Sta. + π - Elev.

Bench Levels

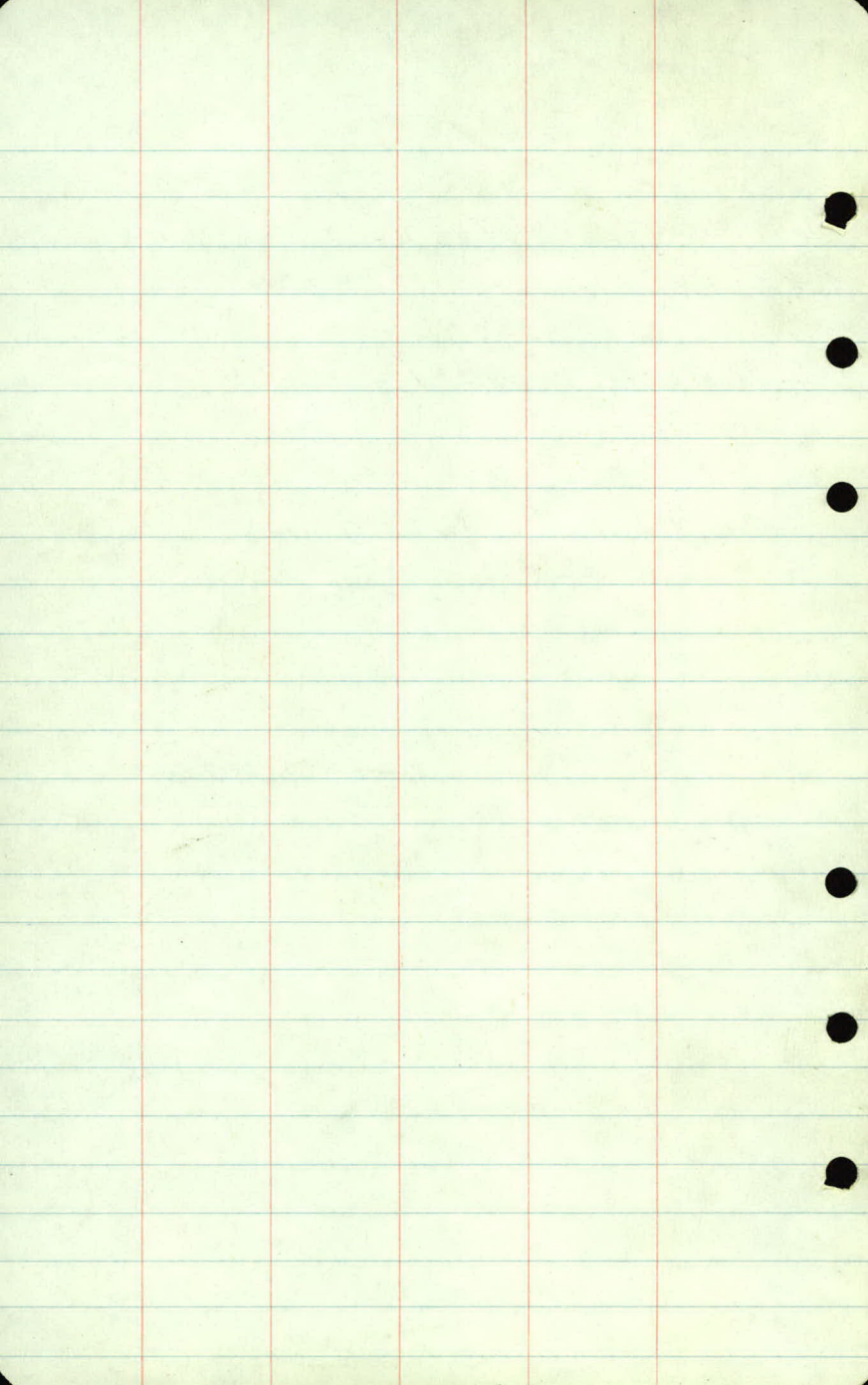
E. Co. Line

Highwood to Linwood Ave

Sta	+	π	-	Elev.
B.M.	13.52	952.25.		938.73
T.P.	13.37	965.38.	0.24	952.01.
T.P.	13.29	978.59.	0.13	965.25.
T.P.	13.49	991.82.	0.21	978.33.
B.M.	13.32	1005.14.	0.00	991.82.
T.P.	9.94	1015.07.	0.01	1005.13.
T.P.	12.24	1027.16.	0.15	1014.92.
B.M.			0.28	1026.88.

Spk in Hi-Line pole # 133

Top Mont. Linwood Ave + E. Co. line



FK
LG

9-23-1975

1

East County Line Rd.

Linwood to Lower Afton

Profile

Linwood = 26+31.4

BM	Assumed	107.45
35	9.90	
+50	9.65	
36	9.26	
+50	8.45	
37	7.44	
+50	6.57	
38	6.42	
+50	7.13	
Top Pipe West 905.33		
39	8.30	
+50	9.55	
40	10.76	
+50	12.07	

FX
LG

9-23-1975
Pizzol

2

Low spot on saddle 7.20

34 110.4

+50 110.3

West side 105.33

East side 104.94

Top Pipe East End 4.70

PG -1.73
 @ 20' Top Base
 ±

35	109.98			
+50	109.77			
36	109.56	7.83		
			(9.3)	
+50	109.35	7.62	9.02	
			(9.1)	
37	109.14	7.41	8.81	9.
			(9.0)	
+50	109.03	7.30	8.70	
			(9.18)	
38	109.12	7.40	8.79	
			(9.56)	
+50	109.41	7.68	9.08	
39	109.91	8.18	9.58	
+50	110.60		10.27	
40	111.50			
+50	112.60			

FK
4
Main

Oct 2, 1975

3

staked shoulder 18' R & L at
same as L Top Base

✓

✓

✓X

X

X ✓ 2.42

✓X

X

X ✓

X

X

X ✓

X

104.10 = Water 9-30-1975 X

✓X

X

X ✓

X

9.55
X

X

X

9.42

