

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

VICTORIA ST.

From Lorpenaue To Lexington

Road Acc't. No. 21

DE-16

Date Filed 1-30-43

File BK-89

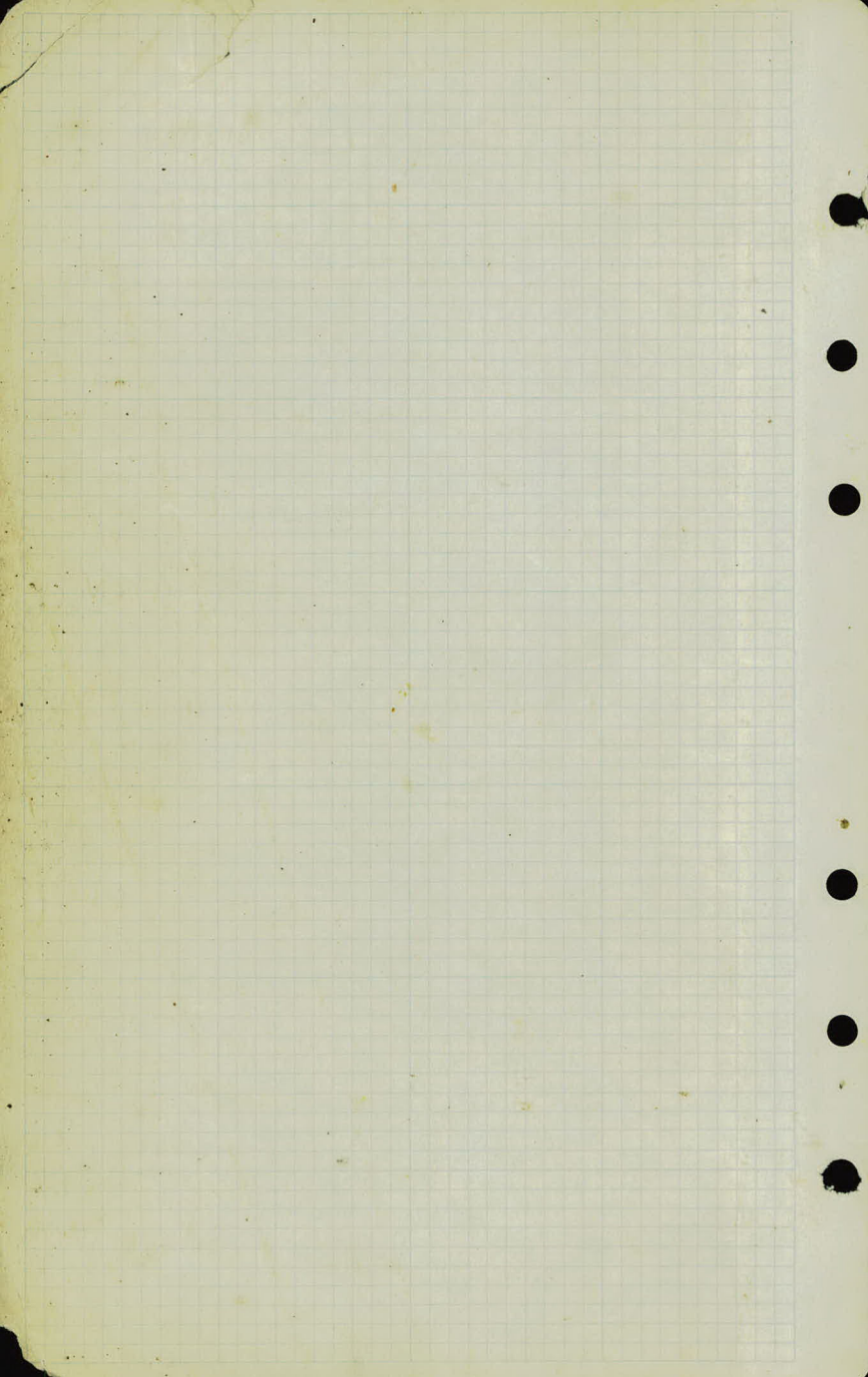
PLAN SURVEY

VICTORIA STR.

FROM LARPELLEUR TO LEXINGTON

INDEX

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Align	1 to 29
TOPOG	30 to 79
BENCH LEVELS	80 to 84
X Sections	87 to 162



Align

Victoria Str

10/21/41

HAW

AM

L. L.

C. N.

Completed 2/3/42

Sta. Point

ΔL ΔR

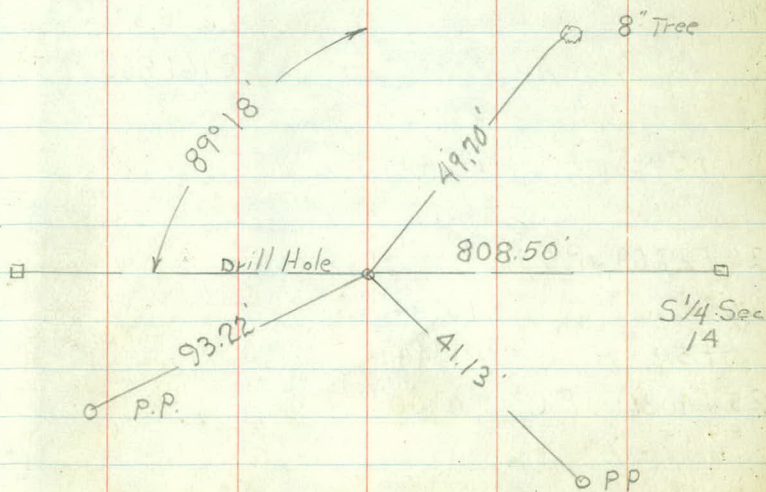
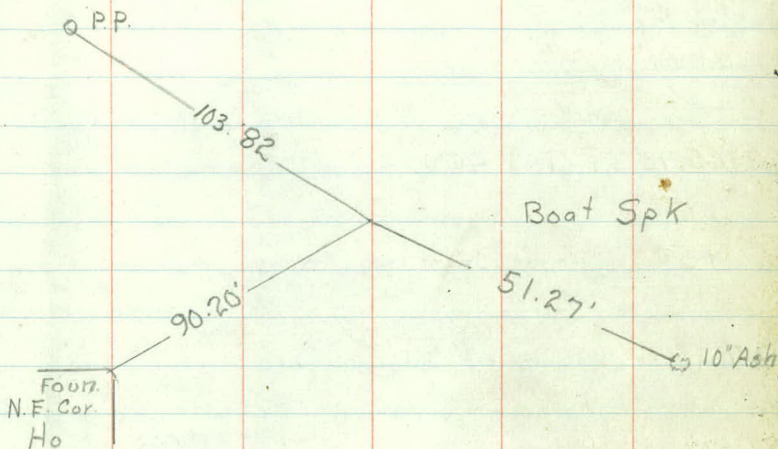
22+01.35 P.O.T

0+00

P.I.

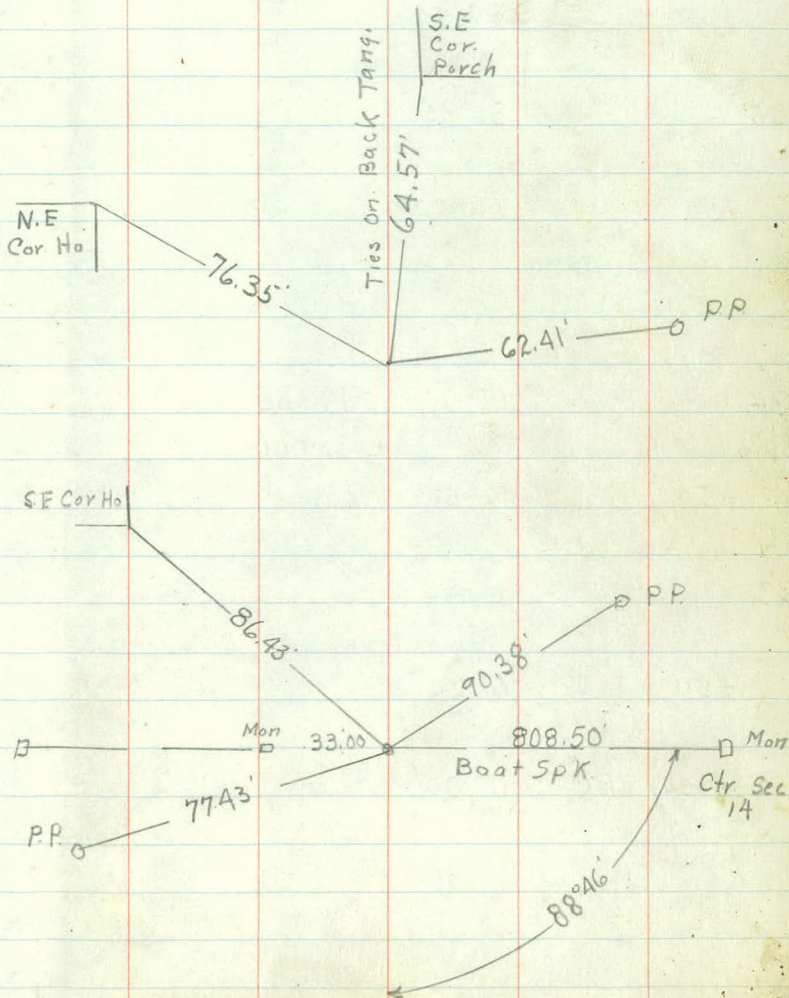
E. Larpenieur Ave.

Description



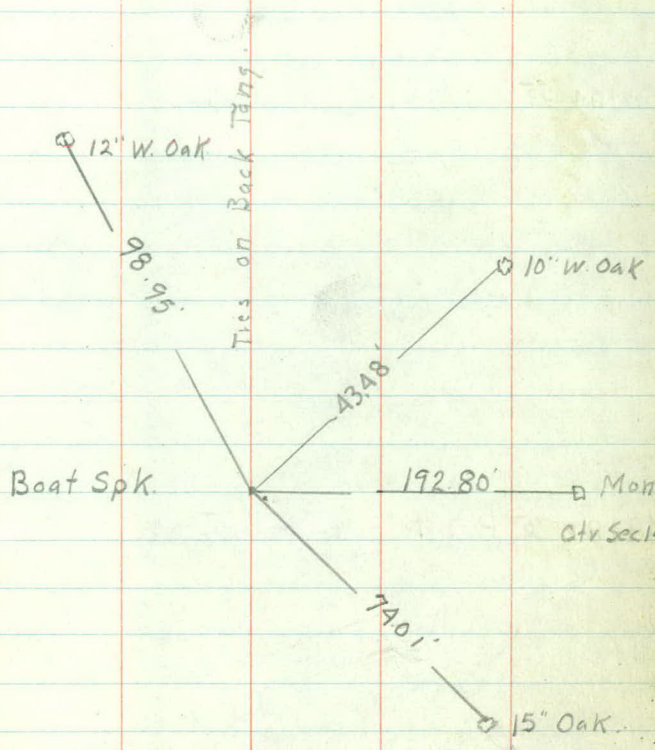
Sta	Point	Alt	ARt
27+65.73	P.T.	40°04'	
+50		37°44'	
27		28°44'	
26+78.90	P.I.		81°08'
			D 36°
			T 138.58
			L 225.37'
			R 161.803
+50		19°44'	
26+27.68	P.O.S.T		
26		10°44'	
+50		1°44'	
25+40.36	P.C.	0°00'	

Description



Sta	Point	ΔL	ΔR
+71.94		$40^{\circ}34'30''$	
+50		$37^{\circ}50'$	
35		$31^{\circ}35'$	
+50		$25^{\circ}20'$	
+45.17	P.I.	$81^{\circ}09'$	
		$D 25^{\circ}$	
34		$19^{\circ}05'$	T 197.83
			L 324.60
+50		$12^{\circ}50'$	R 231.011
33		$6^{\circ}35'$	
+50		$0^{\circ}20'$	
32+47.34	P.C.	$0^{\circ}00'$	

Description



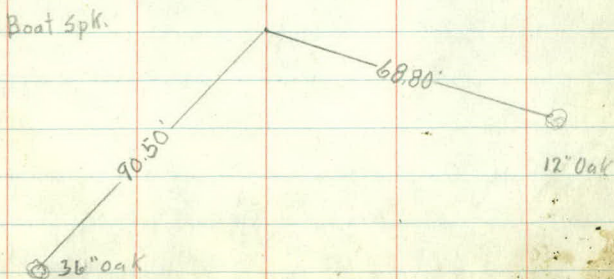
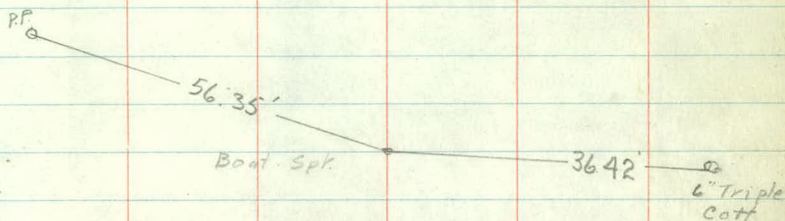
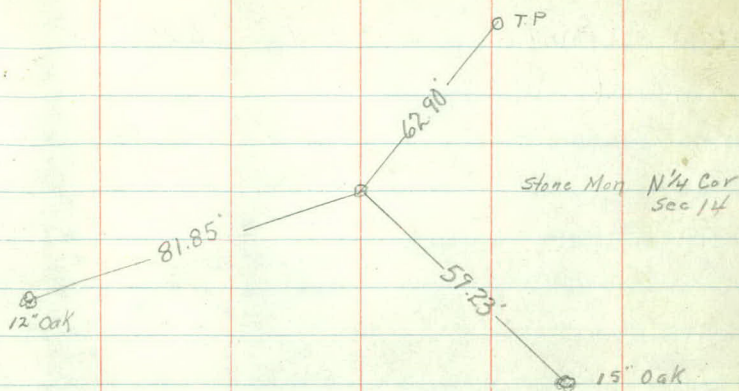
Sta	Point	ΔL	ΔR
58+04.55	P.I.	0°33'	± Co. Rd "B"

49+87.75	P.O.T	± Parker Ave.
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45+50.03	P.O.T
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Description

5

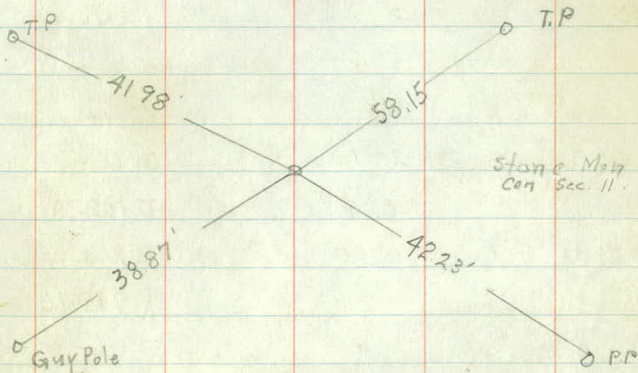
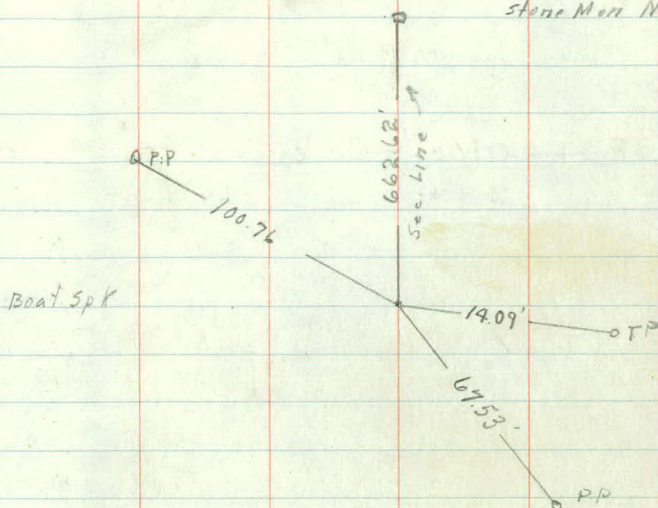


Sta	Point	ΔL	ΔR
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19734	P.T	24° 01' 50	
+50		18° 45'	
102		13° 19'	
103+9573	P1	48° 03'	
+50		7 49'	D 22°
103		2° 19'	T 11680
102+7893	P.C	0° 00'	L 218.41
			R 262.04

84+35.40	P.O.T.	(Co.Rd. B-2)	
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Stone Mon N¹/₄ Sec 11



Sta	Point	ALT	APV
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110+43.18 = P.O.T = 0+00 & Co Rd "C"

+77.12	PT	6° 07'	
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+50		5° 18'	
-----	--	--------	--

108		3° 48'	
-----	--	--------	--

107+75.61	PI		12° 14'
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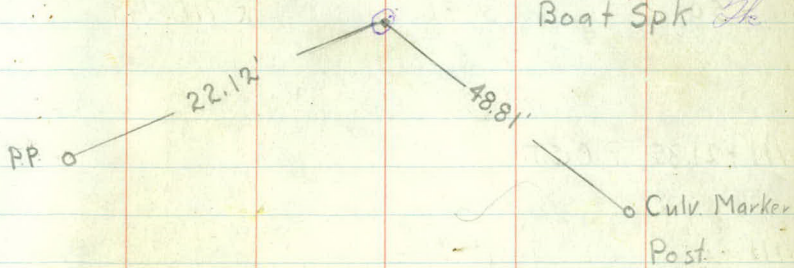
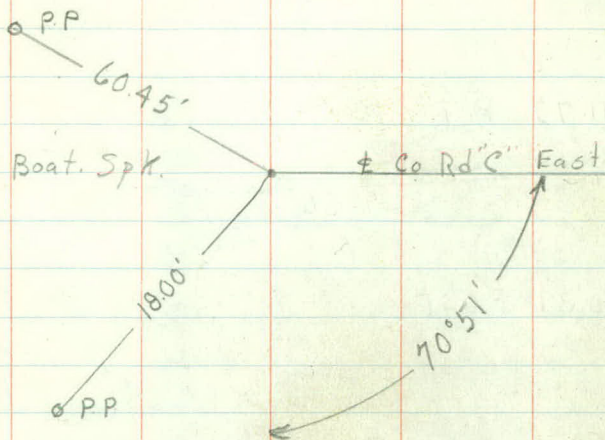
+50		2° 18'	D 6°
-----	--	--------	------

107		0° 48'	T 102.38
-----	--	--------	----------

106+73.23	PC	0° 00'	L 203.89
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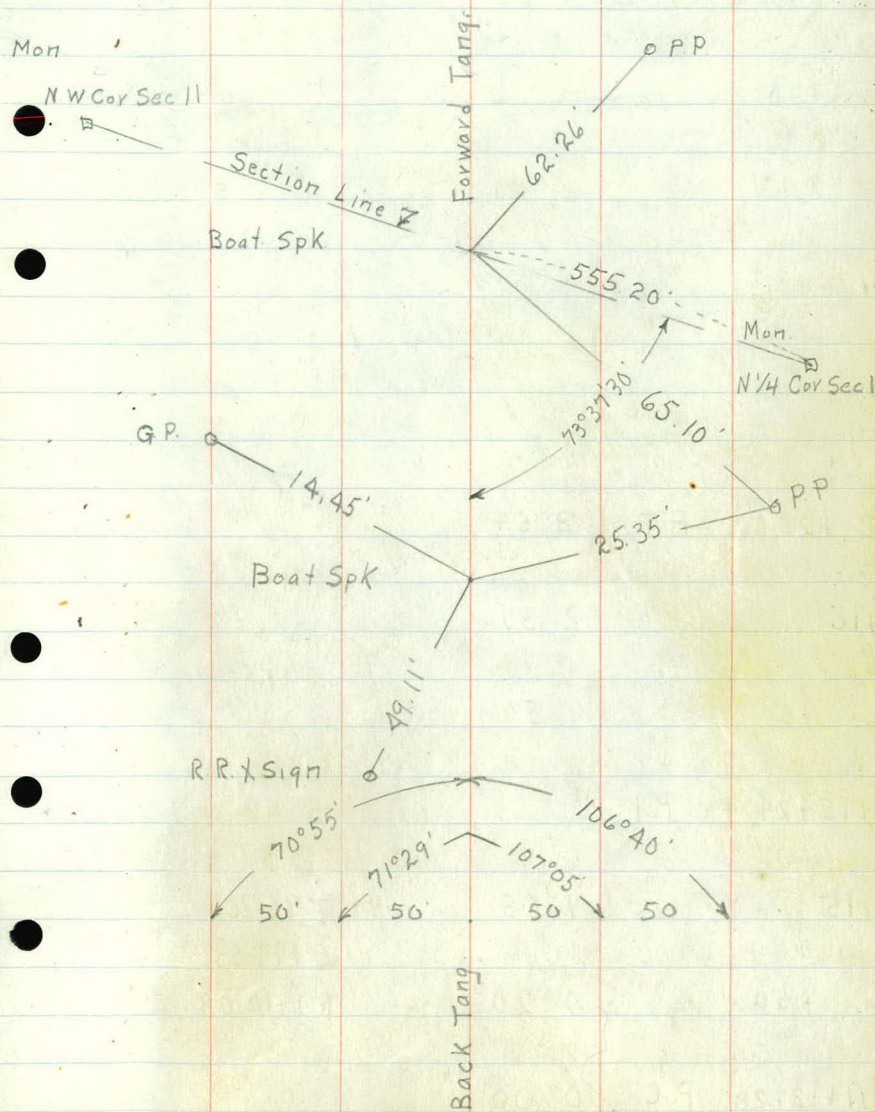
			R 955.366
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Description



Sta	Point	Alt	Δ Rt
+11.73	P.T	10°04'	
113		9°36'	
+60.89	POST		
+50		7°36'	
112		5°36'	
111+87.30	P.I		20°08'
			D 8°
			T 127.25
			L 251.68
+50		3°36'	R 716.779
111+21.35	P.O.S.T.		
111		1°36'	
110+60.05	P.C.	0°00'	

Description



Sta	Point	Alt	ARt.
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+20.61	PT	2°54'	
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116		2°35'	
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		2°12.5'	
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+50		1°50'	
-----	--	-------	--

		1°27.5'	
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115+2404	P.I		
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			5°48'
--	--	--	-------

			D 3°
--	--	--	------

115		1°05'	
-----	--	-------	--

		0°42.5'	
--	--	---------	--

			T 96.76
--	--	--	---------

			L 193.33
--	--	--	----------

+50		0°20'	
-----	--	-------	--

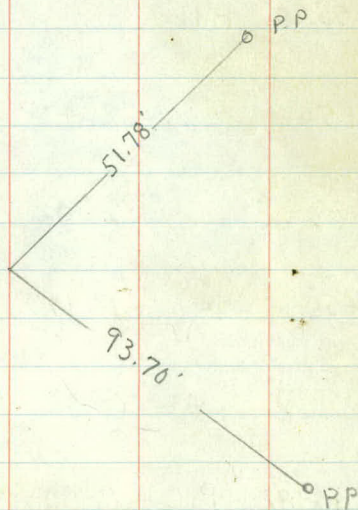
			R 1910.08
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114+27.28	P.C.	0°00'	
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Description

Boat Spk.



Sta	Point	ΔL	ΔR
+46.70	P.T.	$5^{\circ}44'30''$	
		$5^{\circ}24\frac{1}{2}'$	
121		$5^{\circ}02'$	
		$4^{\circ}39\frac{1}{2}'$	
+50		$4^{\circ}17'$	
120+01.17	P.O.S.T.	$\pm$ Co Rd 'C'	
		$3^{\circ}54\frac{1}{2}'$	
120		$3^{\circ}32'$	
+55.97	P.I.		$11^{\circ}29'$
		$3^{\circ}09\frac{1}{2}'$	$D 3^{\circ}$
+50		$2^{\circ}47'$	T 192.05
		$2^{\circ}24\frac{1}{2}'$	L 382.78
119		$2^{\circ}02'$	R 1910.08
		$1^{\circ}39\frac{1}{2}'$	
+50		$1^{\circ}17'$	
		$54\frac{1}{2}'$	
118		$0^{\circ}32'$	
117+63.92	P.C.	$0^{\circ}00'$	

Description

Forward Tang

Ca Rd "C" West

T.P.

89° 07'

Face
Corner Fe
Post

34.86

104° 35'

46.66'

Boat Spk
Found 4-27-1976
7k

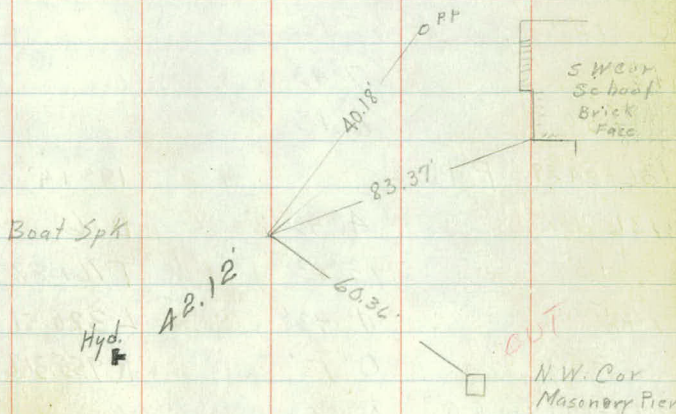
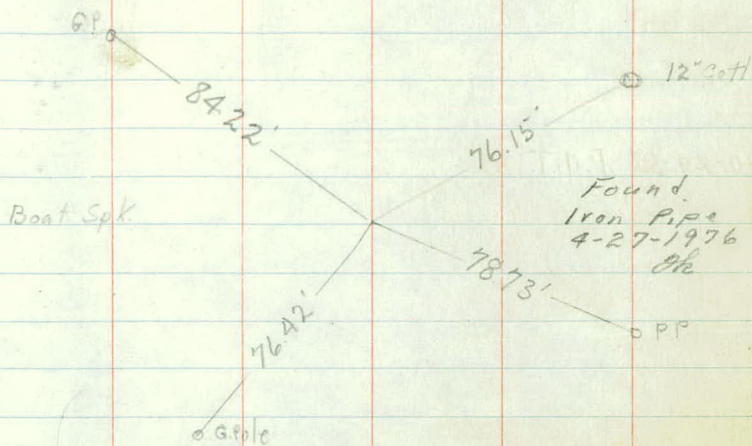
68.21'

Face
PPKnot in
Arc Light
Pole

O T P

Sta	Point	ΔL	ΔR
+25.46	P.T.	$13^{\circ} 43'$	
131		$12^{\circ} 11'$	
+50		$9^{\circ} 11'$	$27^{\circ} 26'$
130+13.60	P.I.		$D 12^{\circ}$
130		$6^{\circ} 11'$	$T 116.75$
+50		$3^{\circ} 11'$	$L 228.61$
			$R 478.339$
129		$0^{\circ} 11'$	
128+96.85	P.C.	$0^{\circ} 00'$	
+38.48	P.T.	$3^{\circ} 26' 30''$	
125		$2^{\circ} 39'$	
124+69.75	P.I.	$6^{\circ} 53'$ ✓	
		$D 5^{\circ}$ ✓	
+50		$1^{\circ} 24'$	$T 68.94$
			$L 137.67$ ✓
124+00.81	P.C.	$0^{\circ} 00'$	$R 1146.279$

Description



Sta	Point	ΔL	ΔR
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140+24.55	P.O.T.		
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		1° 21'	
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+63.25	P.T.	9° 37'	
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+50		9° 13'	
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137		7° 43'	
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+50		6° 13'	
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136+04.57	P.I.		
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		19° 14'	
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136		4° 43'	
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		D 6°	
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+50		3° 13'	
-----	--	--------	--

		T 161.88	✓
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135		1° 43'	
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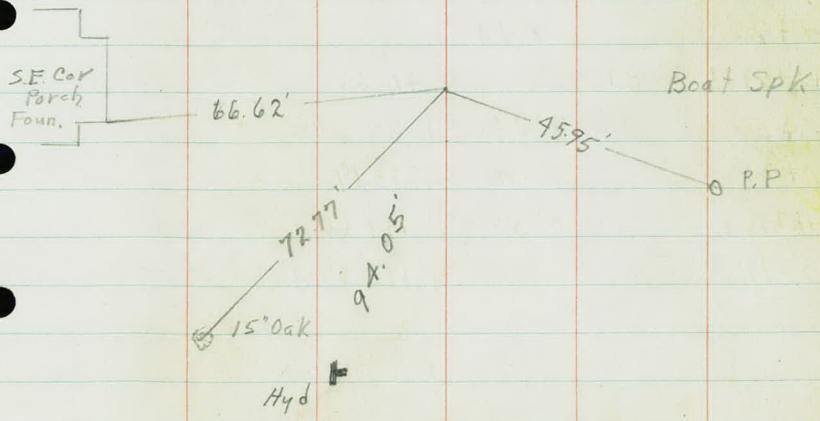
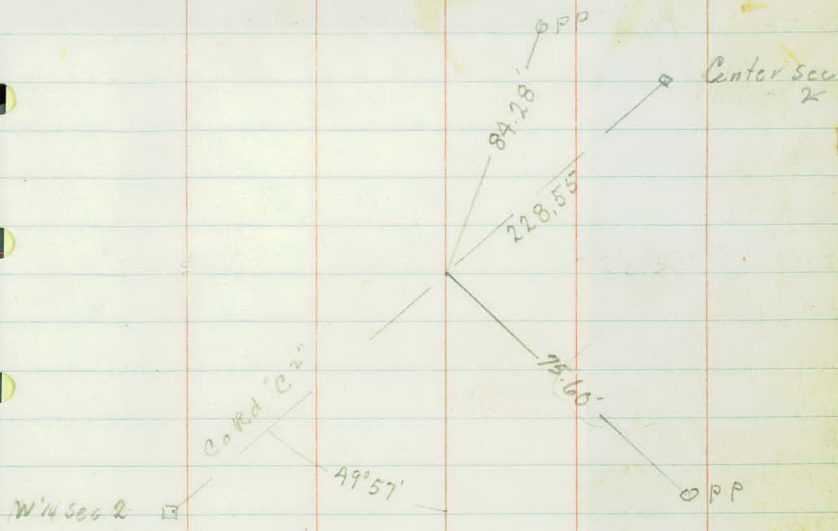
		L 320.56	
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+50		0° 13'	
-----	--	--------	--

		R 955.366	
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134+42.69	P.C.	0° 00'	
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Description



Sta Point Alt APT

154+29.45 P.O.T.

S: 129 | 23 | 2 |

Victoria Street | Victoria 1943

Alignment. dwg

13452	P.T	20°45'	
+25		19°19'	
144		15°34'	
+75		11°49'	
143+69.37	P.I	41°30'	
+50		8°04'	D 30°
+25		4°19'	T 73.19
143		0°34'	L 138.34
142+96.18	P.C	0°00'	R 193.185

Boat Spk.

65.66' O.T.P.

80.39'

O.T.P.

Hyd

50.41'

G. Pole

3369'

3300'

Arc Lt. Pole

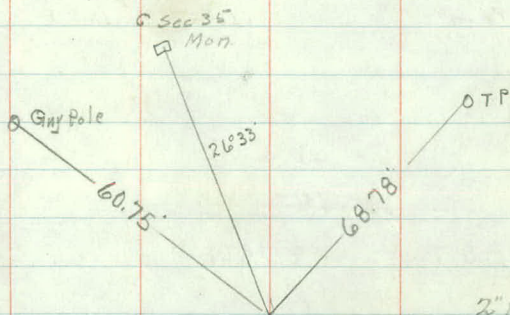
Boat Spk.

Section 263-92
L 1111

Con/Sec 2

Sta	Point	ΔLT	ΔRT
+9114	P.T.	13°16'30"	
+50		10°17'	
177+01.52	PI		26°33'
177		6°40'	D14°30'
+50		3°0.3'	T9348
176+0804	PC	0°00'	L183.10
			R396.20
170+15.00	PI		0°29'

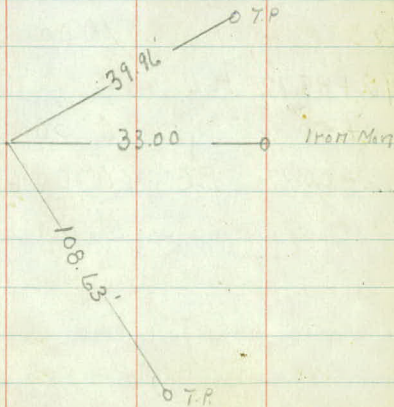
Description



2" 12 Hub

Section Line

Boulder Mon.
N 1/4 Sec 2



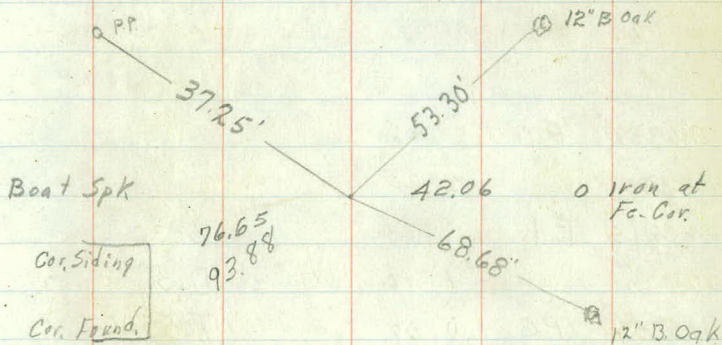
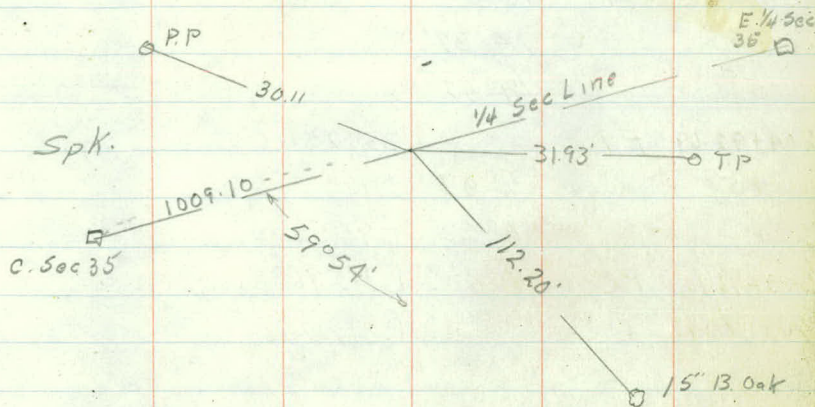
Sta	Point	ΔL	ΔR
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198+84.24	P.O.T	$\pm$ Arbogast Rd	
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+71.10	P.T	$1^{\circ} 42' 30''$	
+50		$1^{\circ} 30'$	
193		$1^{\circ} 00'$	

192+85.72	P.I.		$3^{\circ} 25'$
+50		$0^{\circ} 30'$	$D 2^{\circ}$
192+00.27	P.C	$0^{\circ} 00'$	$T 85.45'$
			$L 170.83$
			$R 286.93$

Description



Sta	Point	ΔL	ΔR
+82.06	P.T.	17°40'	
+50		14°37"	
205		9°52'	
204+92.69	P.I.	35°20'	
+50		5°07'	D 19°
204		0°22'	T 96.59
203+96.10	P.C.	0°00'	L 185.96
			R 302.943

+63.59	P.T.	2°45'	
+50		2°25'	
202+08.65	P.I.		5°30'
202		1°10'	D 5°
201+53.59	P.C.	0°00'	T 55.06
			L 110.00
			R 114.628

Description

Iron pin

15.27' O.T.P.

99.90'

O.T.P.

O.T.P.

76.35'

R.R. Spk

22.18'

Punch Hole
W. End 24" CM

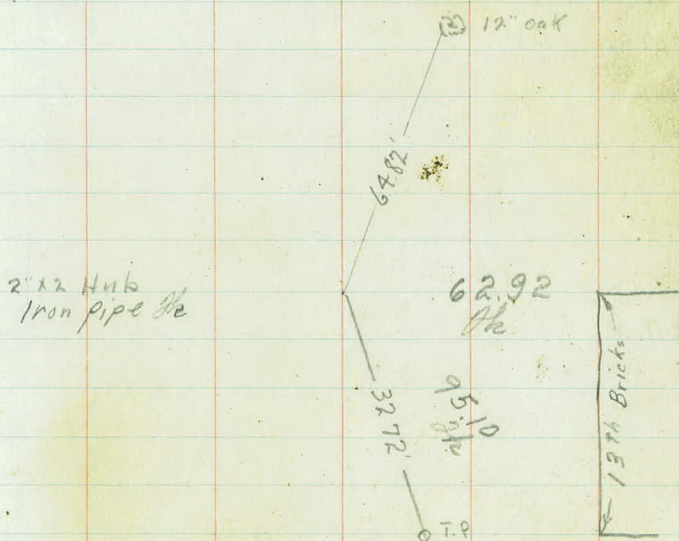
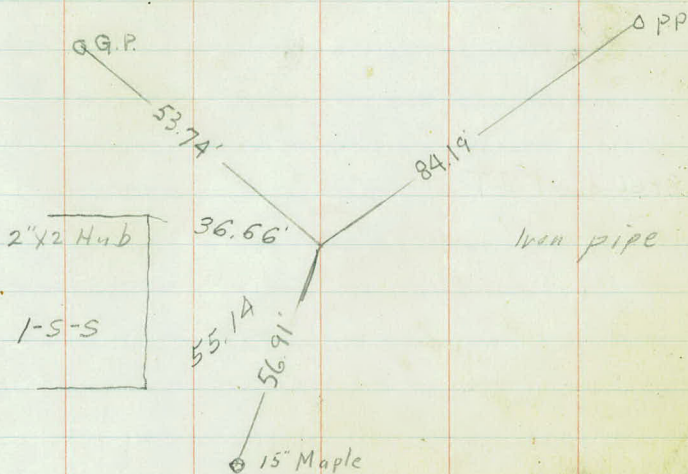
66.34'

O.T.P.

Sta	Point		$\Delta L+$	$\Delta R+$
+61.28	P.T.	31° 07'		
+50		29° 52'		
222		24° 22'		
+50		18° 52'		
221+36.58	P.I.			62° 14'
221		13° 22'		D 22°
+50		7° 52'		T 158.18
220		2° 22'		L 282.88
219+78.40	P.C.	0° 00'		R 262.042

+35.22	P.T.	25° 10'		
215		20° 56'		
+50		14° 56'		
214+38.50	P.I.		50° 20'	
214		8° 56'	D 24°	
+50		2° 56'	T 113.00	
213+25.50	P.C.	0° 00'	L 209.72	
			R 240.487	

Description



Sta Point

ΔL ΔH

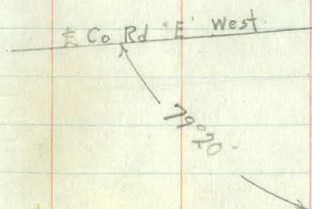
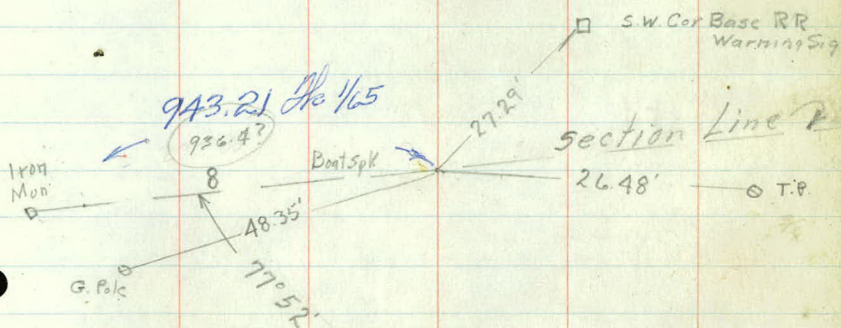
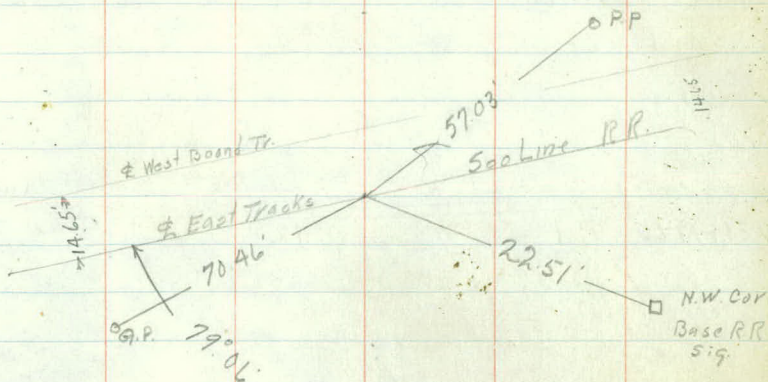
228+66.89 P.O.T

228+32.49 P.O.T

✓

227+98.40 P.O.T

Description



Sta

Point

ΔL

ΔR

231+17.65

P.I

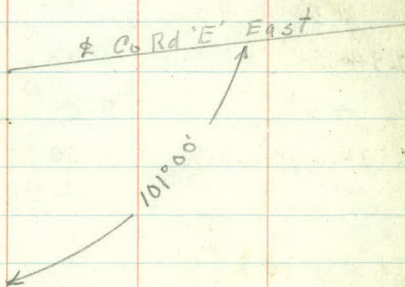
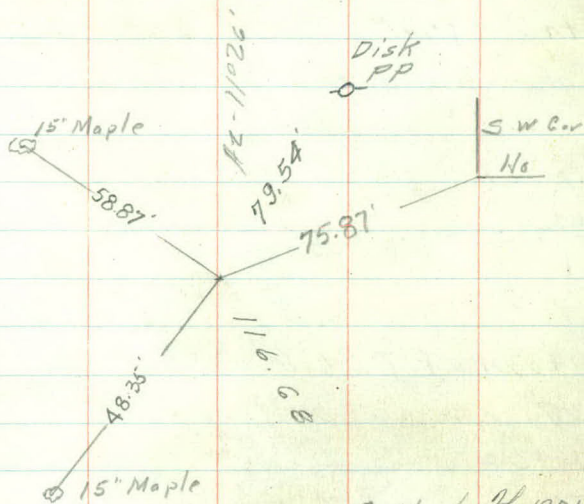
$0^{\circ}42'$

229+48.85

P.O.T

Description

19



Sta	Point	Alt	ARt
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+33.01	P.T	6° 14' 30"	
257		5° 45'	
+50		5° 00'	
256		4° 15'	
+50		3° 30'	

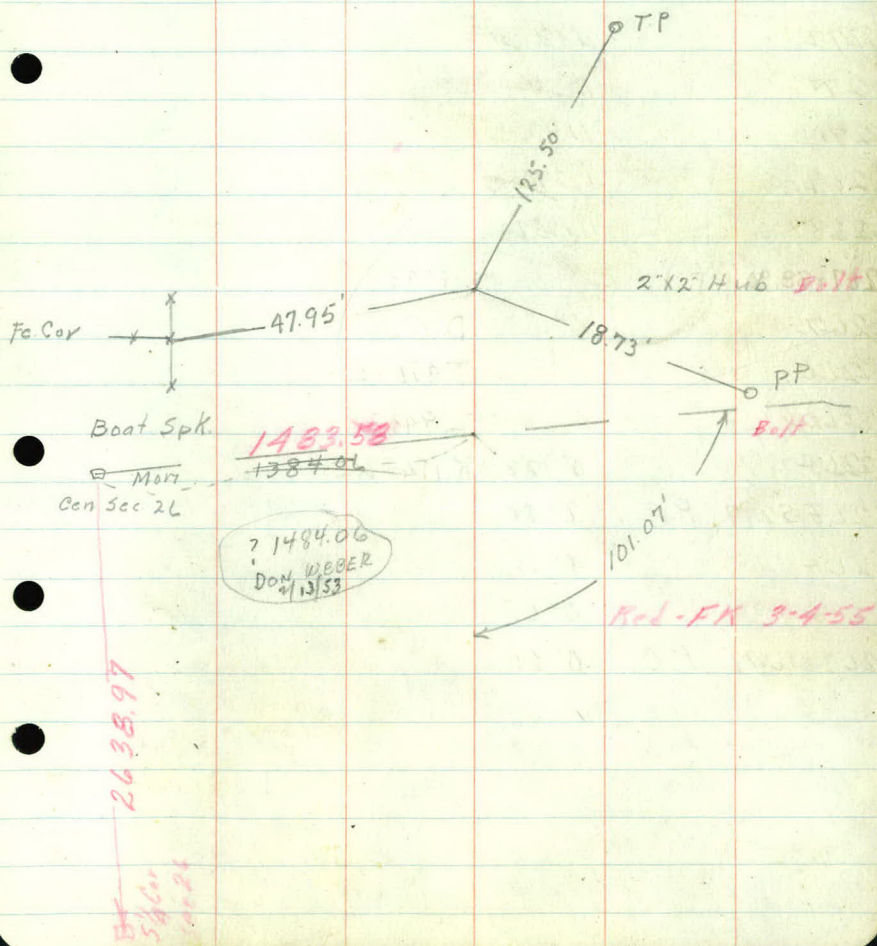
255+25.81	P.I	12° 29'	
		D 3°	
		T 208.91	

255+16.51	P.O.S.T.	L 416.11	
255+00		R 1910.08	

+50		2° 00'	
254		1° 15'	
+50		0° 30'	

253+16.90	P.C	0° 00'	
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Description



Sta	Point	ΔL	ΔR
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+60.30	P.T	2° 21' 30"	
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272		2° 12' 30"	
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271		1° 57' 30"	
-----	--	------------	--

270		1° 42' 30"	
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269+00		1° 27' 30"	
--------	--	------------	--

268+00		1° 12' 30"	
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267+88.90	P.I	4° 43'	
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267		0° 57' 30"	D 0° 30'
-----	--	------------	----------

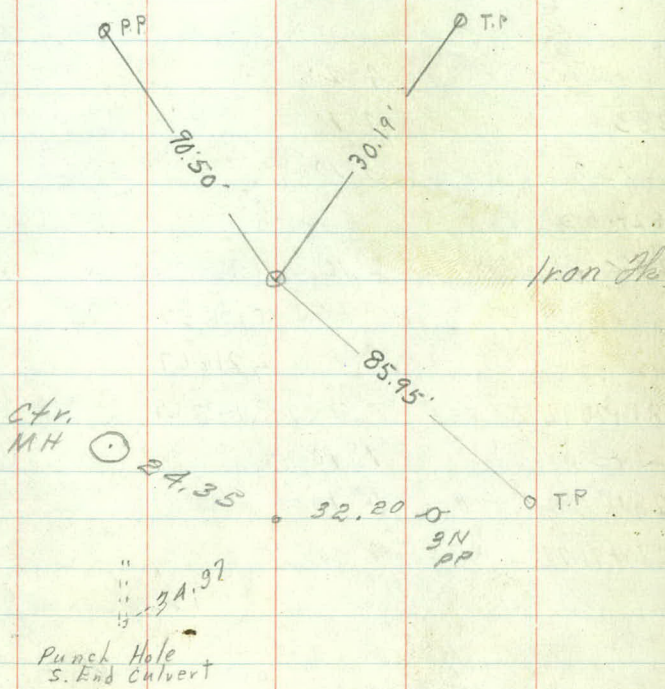
266		0° 42' 30"	T 471.93
-----	--	------------	----------

265		0° 27' 30"	L 943.33
-----	--	------------	----------

264		0° 12' 30"	R 11459.2
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263+16.97	P.C	0° 00'	
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Description



Sta	Point	ΔL	ΔR
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+108.45	P.T.	$4^{\circ}20'$	
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283		$4^{\circ}10'$	
-----	--	----------------	--

+50		$3^{\circ}10'$	
-----	--	----------------	--

282+00.35	P.I.	$8^{\circ}40'$	
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282		$2^{\circ}10'$	$D 4^{\circ}$
-----	--	----------------	---------------

			T 108.57
--	--	--	----------

			L 216.67
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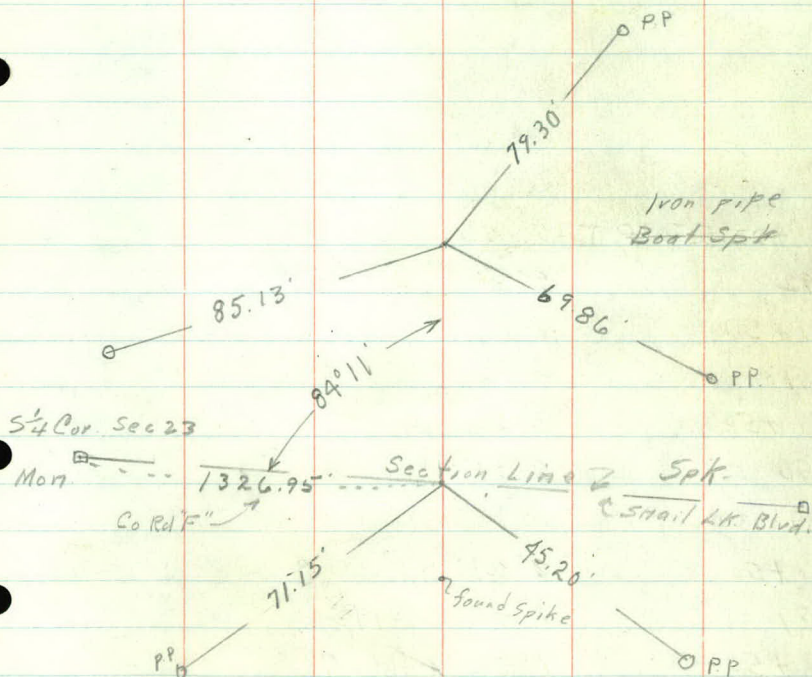
281+70.12	POST		R 1432.69
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+50		$1^{\circ}10'$	
-----	--	----------------	--

281		$0^{\circ}10'$	
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280+91.78	P.C.	$0^{\circ}00'$	
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Description

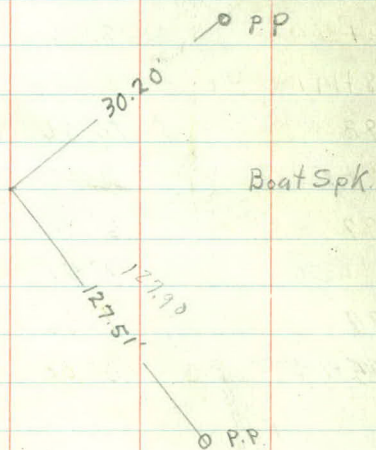
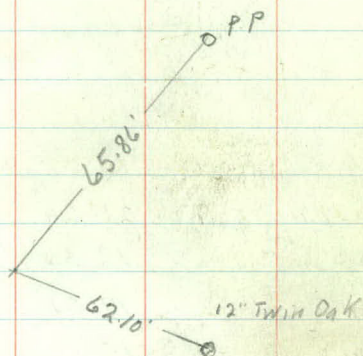


Sta	Point	ΔL+	ΔR+
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+22.55	P.T	5° 45' 30"	
292		5° 28'	
+50		4° 51'	
291		4° 13'	
+50		3° 36'	
290		2° 58'	
289+93.00	P.I	11° 31'	
+50		2° 21'	D 2° 30'
289		1° 43'	T 231.12
+50		1° 06'	L 460.67
288		0° 28'	R. 2292.01
287+61.88	P.C.	0° 00'	

Description

Nail



Sta	Point	ΔL	ΔR
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+39.91	P.T.	21° 24'	
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300		19° 36'	
-----	--	---------	--

+50		17° 21'	
-----	--	---------	--

299		15° 06'	
-----	--	---------	--

+50		12° 51'	
-----	--	---------	--

298+14.10	P.I.	42° 48'	
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298		10° 36'	D 9°
-----	--	---------	------

+50		8° 21'	T. 249.75'
-----	--	--------	------------

297		6° 06'	L. 475.56
-----	--	--------	-----------

+50		3° 51'	R. 637.275
-----	--	--------	------------

296		1° 36'	
-----	--	--------	--

295+64.35	P.C.	0° 00'	
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Don C.
42° 45'

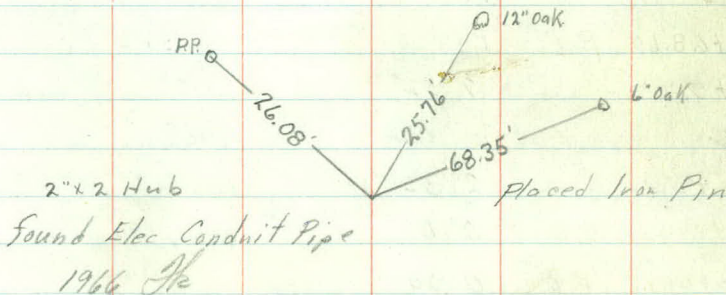
Rm Meyer
42° 44' 57"

3-17-75

42° 45' 30"

Description

20 31' 20" 4" 10" c

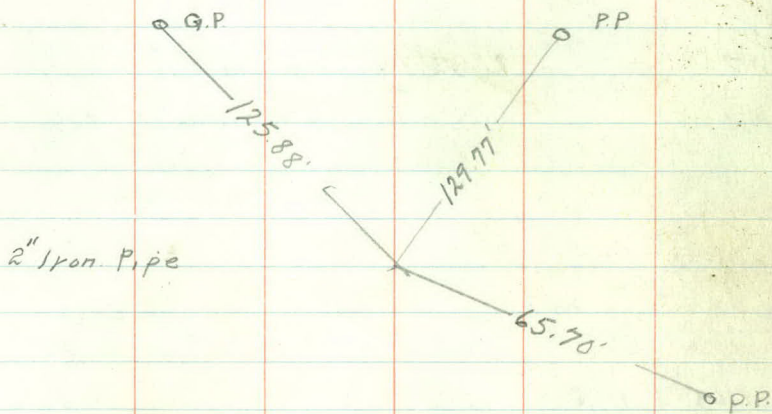


Found Spike
Placed iron pipe

Sta	Point	Alt	Δ Rt
-----	-------	-----	------

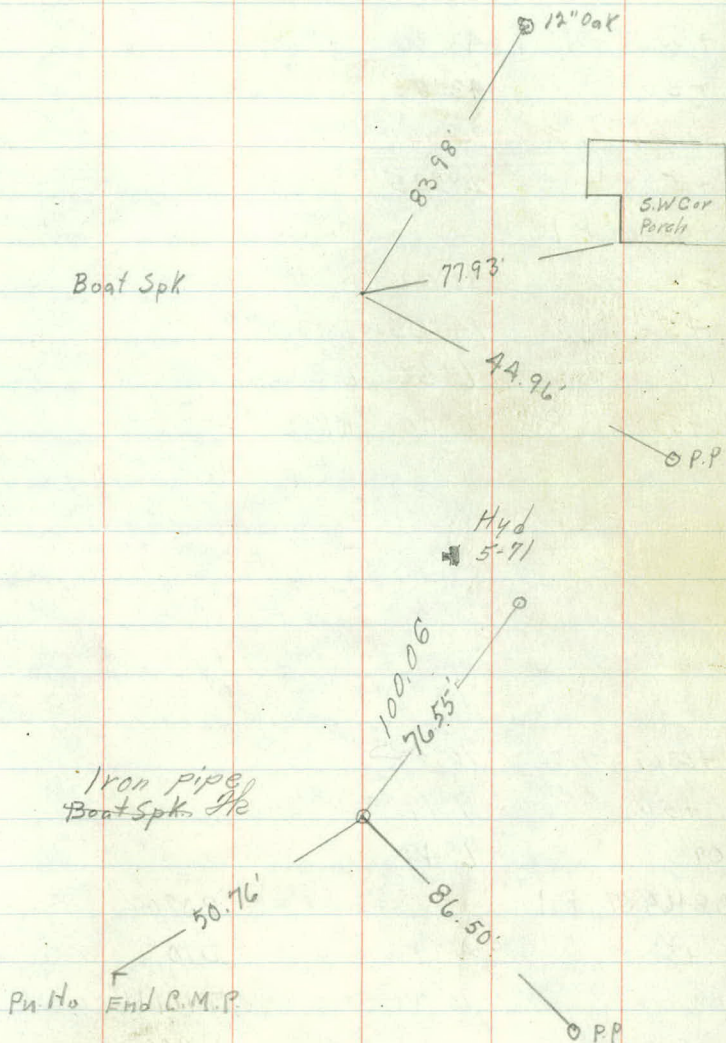
+28.21		16° 27'	
304		15° 02'	Ben Meyer 32° 53' 47"
+50		12° 32'	
303		10° 02'	OK Δ 3-17-75
302+68.60	P1		32° 54' ✓
+50		7° 32'	D10°
302		5° 02'	T169.39
+50		2° 32'	L329.00
301		0° 02'	R.573.686
300+99.21	P.C	0° 00'	

Description



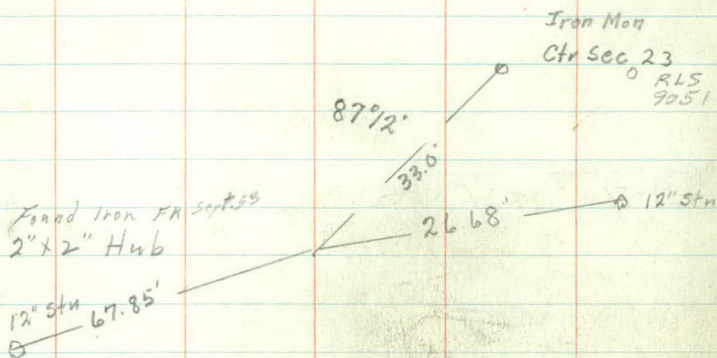
Sta	Point	ΔL	ΔR
307+63.69	P.C.C.	$7^{\circ}00'$	
+50		$6^{\circ}02'30''$	
307+14.06	P.I		$14^{\circ}00'$
			D 14°
307		$2^{\circ}32'30''$	T 50.37
			L 100.00
			R.
+63.69	P.C.C.	$1^{\circ}00'$	
+50		$0^{\circ}52'$	
306+13.71	P.I		$2^{\circ}00'$
306		$0^{\circ}22'$	D 2°
305+63.69	P.C	$0^{\circ}00'$	T 50.02
			L 100.00
			R 2864.93

Description



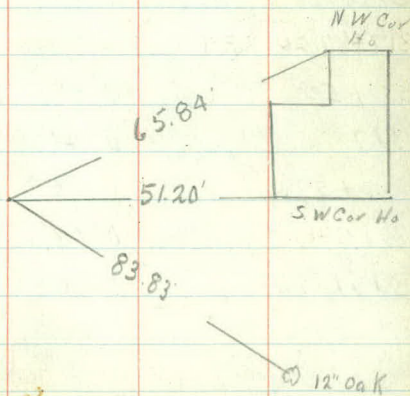
Sta	Point	ΔL	ΔR
+53.58	P.T	43°36'	
+50		43°05'	
313		35°50'	/
+50		28°35'	
312+43.06	P.I	87°12'	
312		21°20' D 29°	
+50		14°05' T.19017	
311		6°50' L.300.69	
310+52.89	P.C	0°00'	R199.696
+63.69	P.T	10°00'	
+50		9°19'	
309		6°49'	
308+64.87	P.I		20°00'
+50		4°19'	D10°
308		1°49'	T101.16
			L 200.00
307+63.69	P.C.C.	0°00'	R.573.686

Description



Section Line

Boat Spk
(Found)
Placed Iron Pipe
and Iron Pin etc
5-28-71



Sta Point

$\Delta L + \Delta R +$

331+76.00 P.O.T.

+14.69 P.T. $1^{\circ} 31'$

320 $1^{\circ} 28'$

+50 $1^{\circ} 18'$

319 $1^{\circ} 08'$

+50 $0^{\circ} 58'$

318 $0^{\circ} 48'$

317+87.24 P.I. $3^{\circ} 02'$

+50 $0^{\circ} 38'$ D $0^{\circ} 40'$

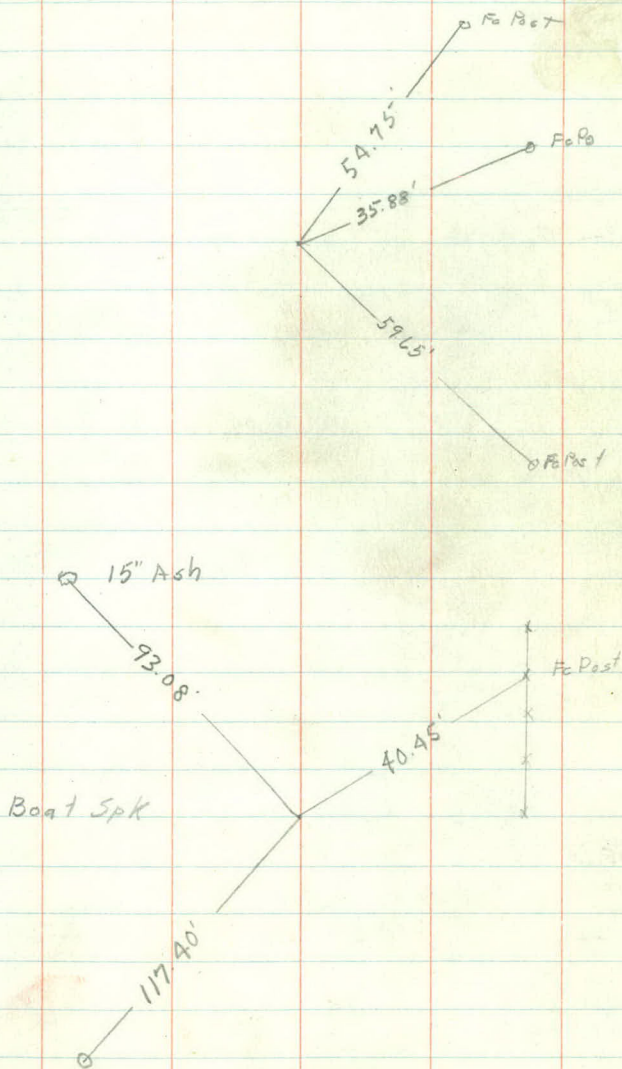
317 $0^{\circ} 28'$ T 22755

+50 $0^{\circ} 18'$ L 45500

316 $0^{\circ} 08'$ R 859442

315+59.69 P.C. $0^{\circ} 00'$

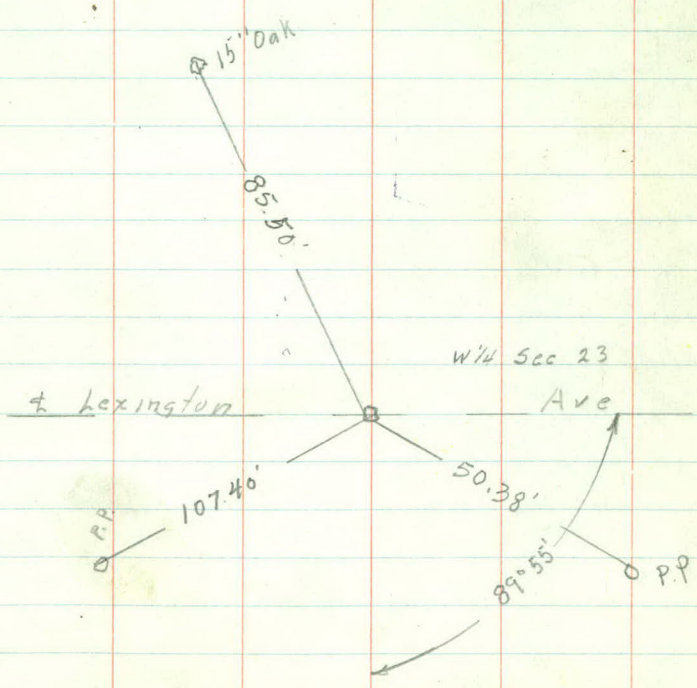
Description

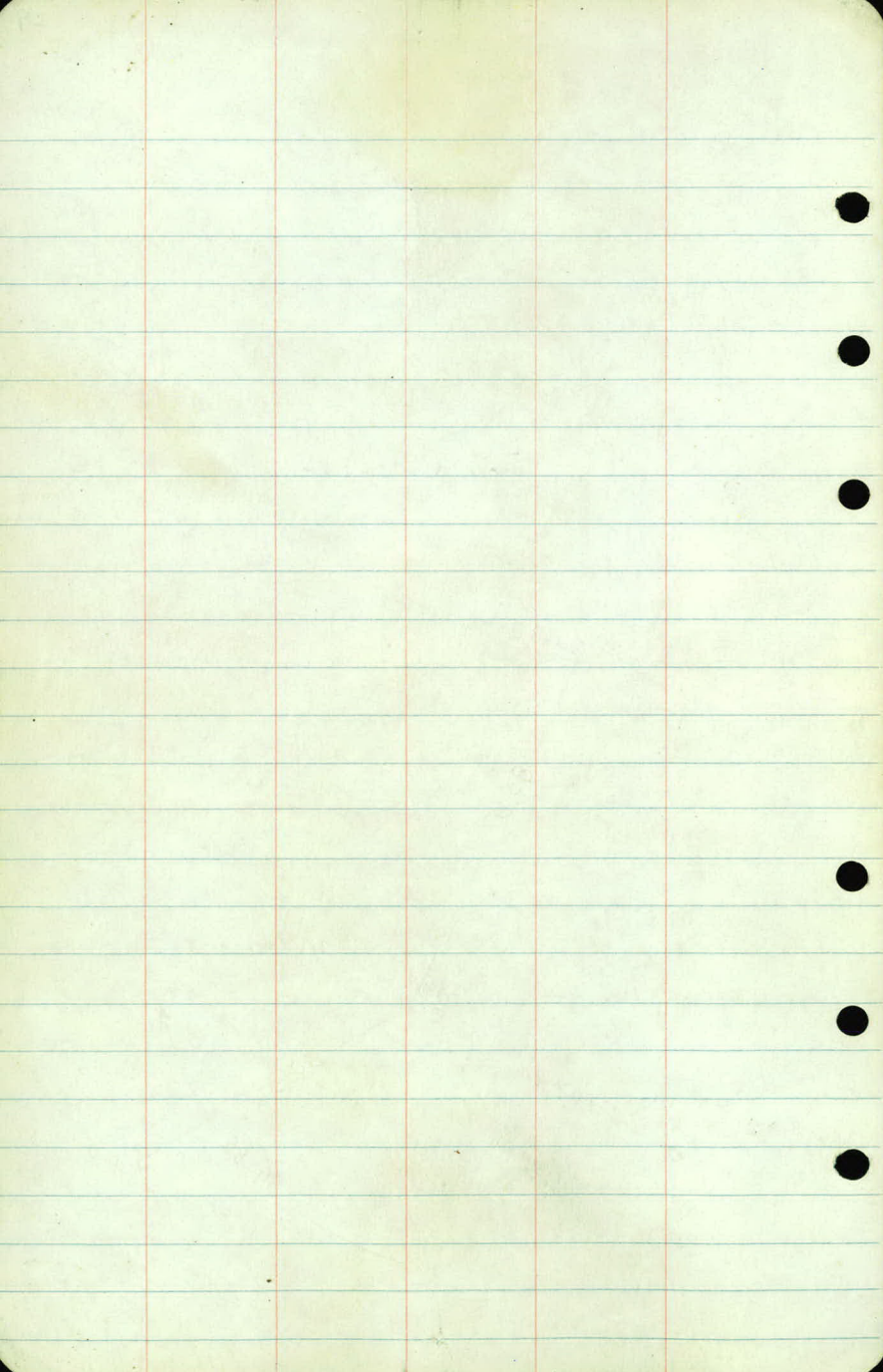


Sta	Point	$\Delta L +$	$\Delta R +$
-----	-------	--------------	--------------

338+05.35			
-----------	--	--	--

Description





Topography
Victoria Str
Larpentour To Lexington Ave's.

Rel Rel

5 9 8
+ 89 x Drain
15' x 34' CM 17'

4 15' 7

3 10 7

2 10' 8'

1 10' 10

0

+37 12" Elm 38'
+05 24" Will 36'
Hodge 33+46

+78 12" Tree 38'

+38 12" Ash 38'
Hodge 34-47

+55 15" Ash 38'
Hodge 34-47

Hodge 33-46

Hodge 32-46

+58 End Rad 13

+33 Cor Hodge 34

+14 Beg Rad 60'
Arc

Cultivated

Buckhorn & Lilac
Rose lawn Cemetery

+49 End Rad 19'
+14 Beg Rad 41'

Larytentens 20' 100' Part

13

R4

E4

12

10'

8'

11

9'

9'

10

10

9'

9

9

9

8

8

9

7

9'

8'

6

9

8

+

+96 12" Ash 42'

+27 12" Ash 38'

Hodge 33-46'

+37 12" Twin W/14'

Hodge 33-46'

+62 12" Elm 41'

+65 12" Ash 39'

Hodge 35-46'

Cemetery

+49 24" BE 39'

Hodge 33-46'

Rose lawn

+25 18" Elm 41'

Hodge 33-46'

+59 18" Elm 40'

+28 24" W/11 44'

Hodge 34-47'

+97 12" Ash 39'

Hodge 33 & 46'

Uncultivated

Cultivated

100 End Cult

Rd

R11

19 10' 9'

18 10' 7'

17 10' 8

16 11' 8

15 10' 8'

14 10 9

13 10' 8

+99 6" Ash 38'
+75 6" Ash 42'

Hedge 33-40'

+40 6" Twin Ash 47'

+05 6" Twin Ash 41'
Hedge 34-40'

+76 Triple 6" Ash 36'

+50 8" Ash 46'

+22 6" Ash 37'

Hedge 34-46'

+95 6" Ash 46'

+67 6" Ash 37'

Rose Lawn Cemetery

+25 Twin B.E. 27'

+84 Trip B.E. 25'

+65 Twin B.E. 29'

+28 Twin B.E. 30'

+00 6" Tree 36'

Uncultivated

Hedge 38-46'

+67 6" Ash 45'

+63 Twin 6" Ash 36'

+17 8" Ash 46'

Hedge 36'-46'

+90 6" Ash 40'

Hedge 34-46'

+78 8" Will 40'

+47 6" Twin Ash 44'

+18 12" Will 38'

Hedge 32-46'

27

RA

RA

+75

15'

10'

+50

28'

11

+50

26

50'

8'

+19 6" Ash 22'

+75

+50

13'

8'

25

14'

8'

•

24

11'

7

•

+94 Twin B.E 25'

23

10'

8'

•

•

22

11

7

21

11'

8'

•

•

20

9

9

+95 P.P. 23'

+11 Beg Rad 76'

+95 End Cult.

+72 Beg Rad 19'

+47 P.P. 33'

+48 Beg Cult.

+48 P.P. 32'

+38 Ent 12" x 20' CM. 20'

+45 Beg Yard

+00 P.P. 30'

+10 Beg Cult.

+00 Spruce 38'

+93 Spruce 46'

+91 " 35'

+70 P.P. 23'

+62 4' Conc Walk 32'

+32 End 15" CM. 20'

+22 * Ent

+00 * Ent

+92 End 15" CM. 20'

+48 Beg Yard

+06 P.P. 22'

+00 End Pines 36'

+95 P.P. 31'

+84 Rge Tie Ent

+50 Trees 41'

+28 Beg Evergreens 31'

+00 End Hedge 23'

+00 10' Ash 33'

+96 Stn 33'

+53-12" Ash 53'

+50 Hedge 31'-40'

+02 24" Elm 48'

Hedge 31'-40'

+44 15" Ash 41'

+21 P.P. 44'

+12 12" B.E. 44'

+01 12" B.E. 39'

Hedge 32'-40'

+92 10" B.E. 45'

+84 12" B.E. 38'

+81 6" B.E. 42'

+71 10" Twine 42'

+69 12" Elm 38'

+15 6" Ash 39'

Hedge 33-40'

+89 6" Ash 42'

Rosclawn Cemetery

+34 12" Ash 42'

Hedge 32-40'

+72 10" Ash 43'

+43 8" Ash 36'

Hedge 31-40'

+56 6" Ash 37'

+27 12" Ash 43'

Hedge 33-40'

+50

14-38

33

6'

19'

32

10'

11'

31

10

11'

30

10'

10

29

10'

10'

27' +16 X Drain 15" X 44' CM.

17'

28

8'

10'

+50

6'

16'

+97 stu 37'

+93 6" Tree 46'

+90 6" Tree 56'

+86 Tree 38'

+78 2" Pine 50'

27

7'

13'

+70 20" Oak 19

Scattered oaks

+50 Fc 61-71

+48 6" oak 62

End Woods 33'

Fc 38-47

+79 stu 45'

+40 Fc 34-43

+40 6" oak 35'

Woods 40'

+85 Ent 50'

+74 Rgc Tie

Fc 34-43

+63 Fc 34-43

+03 stu 38'

+00 stu 50'

Fc 33-81

Woods 44'

Woods

+64 stu 40'

+45 stu 33'

+38 stu 40'

+32 stu 31'

+15 6" oak 40'

Fc 33-71

+47 Bay Wood 40'

+47 X Fc 32

+42 Ent

+30 15" Oak 32'

+63 stu 47'

+46 stu 44'

+43 P.P. 41

+10 End GR 13'

+09 24" Oak 44'

Fc 32-62

+29 G.P. 32'

+16 stu 30'

G. Rail 14'

+84 X Fc 38'

+29 Fc 32-55

+26 P.P. 29'

+18 Tree 36'

+18 stu 46'

+13 6" Tree 52'

+00 12" Oak 62'

+73 6" Pine 38'

+68 6" Birch 45'

+59 6" Pine 42'

+37 24" Oak 55'

+19 stu 45'

+17 20" Oak 58'

+14 stu 45'

+12 Ent 12' X 34 OH

+20 Bay G. Rail 12'

No Oak

39'

41 Ra Ra

40 8' 15'

39 8' 10'

38 8' 10'

37 8' 12'

36 7' 14'

+50 4' 16'

35 8' 28'

+50 28' - 50'

34 36' 62'

+90 End Swp + Brush 23'

Swp + Brush 23'

Swp + Brush 28'

Swp + Brush 29'

+50 Swp + Brush 34'

+00 End Plum trees 34'

+94 Stn 34'

+83 Stn 36'

+65 Stn 41'

+53 Stn 33'

+50 Beg Swp 150'

+45 Beg Plum Trees 40'

+21 Ent

+00 10" Oak 58'

+80 10" Oak 34'

+64 10" Oak 34'

+00 8" Oak 28'

Swp + Brush

Scattered Oaks
Uncultivated

+79 Fe Cor 32' 36

+90 End Swp 23'

+50 Swp 150'

Swp 20 Fe 32'

Swp 20 - 400 Fe 33'

100 Swp 23-91' Fe-33

+75 Beg Swp 50'

+60 Tree line 75'

+00 Woods 33
Fc 33'

Fc 33'

Woods

+50 Fc 35'

Fc 46'

+60 Fc 70

Beg Woods

+12 Fe Cor 115'

+00 Fe Cor 120'

Fc 107

48

Rd Rq

47

8'

10'

46

9'

10'

45

9'

11'

44

8'

11'

43

7

12'

42

7

12'

41

8'

11'

+72 Ent.

+53 Oak 40'

+11 Ent.
+00 Beg Yard+12 Oak 44'
Fc 40'

Uncultivated

Fc 46'

Pasture
Scattered
Oaks

+22 End Oaks 45'

+03 Beg Oaks 45'

+75 24" Oak 51'

+70 10" Oak 48'

Fc 37'
+98 Oak 50'
+93 12" Oak 37'
+70 Ent.

+98 20" Oak 24'

Pasture
Scattered oaks

Fc 33'

+50 End Brush

Scattered Oaks
Oak Brush

+75 Group 5 Will 50'

+32 Oak 35'

Fc 33'

+51 10" Oak 25'

+14 Beg Oak Brush 23'

+00 Beg Pasture
Fc 32'

56 Rd Rd

54 9' 9'

53 9' 10'

52 8' 10'

51 8' 10'

50 10'

+87 & Parker

49 8' 11'

48 8' 11'

+90 End Pot Hole 40-10

+41 Pot Ho 36-100

+00 End Cult.

+00 Beg Cult.

+16 20' CoH 29'

Uncultivated

Uncultivated

+25 End Rad 9'

+12 PP 50

+00 Beg Rad 46'

+87 & Rad 15" x 56' CM 23'

+76 End Rad 46'

+47 Beg Rad 9'

+47 End Uncult.

+81 PP 54'

+78 Twin CoH 36'

+00 End Yard

+89 Ent 15" x 20' CM 23'

Uncultivated

+20 Fc 33' Beg Yard

Fc 35' End Pasture

+00 End Yard

62 Rd Rd

61 12 11'

60 12' 11'

59 11' 10'

58 13' 10'

#71 End Rubble Gutter
32'

57 12' 8'

56 10' 8'

55 10' 8'

+66 12" x 20' CM 18'

+72 PP. 22'

+10 Ent.

+52 Ent

+45 4" Tree 28'

+16 3" Ash 26'

+05 Ent.

Yards

Cultivated

+43 Ent

+20 Beg. Yard

+00 PP 22'

+54 PP 21'

Bag Cult.

+38 End Rad 11'

+20 End CM 33'

+17 Beg Rad 44'

+94 End Rad 65'

+78 PP 59'

+71 End 15" CM 32'

+59 End Hedge 36'

+54 Beg Rad 10'

+62 End Rad 16'

Uncult

+17 Beg Rad 60'

Co Rd

+93 End Rad 53'

+69 End Woods 65'

+57 Beg Rad 14'

Oaks 50'

+90 Stn 38'

+80 Beg Oaks 60'

Scattered Trees

Yard

+76 Cor Hedge 30'

+75 Beg 3" Rubble Gutter

+60 Ent 15" x 30" CM 23'

+38 10" Twin Oak 38'

+23 End Tree 26-30'

Trees 27-30'

+50 Ent

+27 Beg trees 27-30'

+00 Beg Cult

Uncultivated

67 Rel Rel

68 10 11'

67 10' 11

66 9' 12'

65 8' 12'

64 7' 13'

63 8 12'

62 9 11

+95 6" Elm 37'
 +75 10" Elm 37'
 +59 6" Tree 37'
 +43 10" Elm 37'
 +22 8" Elm 37'
 +14 Ent.

+06 10" Elm 36'
 +00 X Hedge 36'

+94 Ent
 +85 6" BE 34'
 +67 10" BE 33'
 +58 15" Cotl 27'
 +47 Ent

+35 10" BE 33'
 +28 End Berry Patch 40' ---

+05 10" BE 33'

+88 2" Tree 33'
 +66 10" Tree 33'
 +47 Beg Berry Patch 46'
 +47 10" Pop 33'
 +40 X Hedge 34'

+34 Ent.
 +25 6" Tree 33'

+99 4" Tree 33'

+71 6" Ash 33'

+59 Ent 12' x 20' CM 18' ---

+47 8" BE 23'
 +47 End Cult + Beg Yard
 +10 10" Ash 23'

+00 PP 24'



+67 12' Wood Plank Ent
 --- 23'

Sand Pit

+50 6" Oak 24'
 +45 PP 24'
 +37 10" Oak 23'
 +30 6" Oak 21'

+54 Ent To Sand Pit

+90 Beg Sand Pit 50'
 +90 End Cult
 +86 PP 23'

Cultivated

+30 PP 22'

Cultivated

+75 End Berry Patch 29
 X Beg Cult

+45 Beg Berry Patch 29
 +30 End Yards

76

75

10'

10'

74

10'

9

73

9'

10

72

+70 & 5TH #26

71

10'

11

70

10'

10'

69

10

10'

+61 Ent
 +42 30" B.E 32'
 +27 24" B.E 31'
 +02 15" B.E 32'
 Fc 34'
 +88 12" B.E 33'
 +52 Fc Cor 34'

Yard.

+75 P.P. 26'

+52 Beg Cult.

----- +25 End Seedlings

R.O.W. Highway Dept
Grass

Highway Dept has
Seedlings Planted

+66 P.P. 26'

+56 P.P. 26'

+25 End Rad 13'

+40 End Rad 10'

+90 Beg Rad 72'

+55 End Rad 50'

+86 Beg Rad 58'

+51 End Rad 71'

+10 Beg Rad. 11'

+07 Ent

+00 End Yards

+98 6" Ash 34'

+72 12" B.E 32'

+45 6" Ash 34'

+35 Ent

+25 4" Ash 34'

+10 Ent

+06 Beg Rad 12'

+06 P.P. 26'

+25 End Sand Pit

+87 P.P. 25'

+73 2" Conc Slab 50'

+70 End Conc Slab 93'

+59 Range Tie

+54 Beg Conc Slab 90'

+67 12" B.E 31'

+42 Ent

+30 10" Elm 37'

+21 Ent

+13 8" Elm 37'

Yards

3' wide

83

Rd 8 Rd 12

+94 15" Co H 19'

82

8'

12'

81

8'

13'

80

8'

12'

79

8

12'

78

8'

11

77

10'

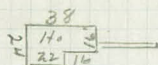
10'

76

10'

10'

+75 15' CoH 20'
 +66 Ent
 +56 12' CoH 20'
 +38 15' CoH 20'
 +21 E2 Walk + Step 15'
 +28 S.E. Cor Porch
 +19 15' CoH 20'
 +00 15' CoH 20'
 +00 Bag Yard
 +91 Ent
 +82 18' CoH 20'
 +65 20' CoH 20'
 +46 15' CoH 20'
 +25 18' CoH 20'
 +02 12' CoH 23'



0223300

42
 + End Yard
 +88 L1/20 Hedge 31'

+57 P.P. 21'

+52 8' Oak 43'

+32 Bag Yard
 +32 Ent 12' x 28' CM 28'
 +02 Rq. Tic Ent
 +05 P.P. 23'
 +95 End Cult.

+68 P.P. 24'

Uncultivated

+80 End Yard
 +72 Ent

+60 12' B.E. 30'
 +50 12' B.E. 30'
 +36 20' B.E. 30'
 +20 24' B.E. 30'

+05 Ent

+93 24' B.E. 33'

+66 Row Fc Posts #6'

+52 24' B.E. 30'

+23 P.P. 34'

+15 P.P. 32'

+11 Ent

+05 End Fc 34'

Yards

Cultivated

+06 P.P. 23'

+38 P.P. 26'

90

R4

R4

89

7'

12'

88

9'

11'

87

9'

13'

86

9

12'

85

9'

12'

84

135 ± B²

9

83

8

12

Uncultivated

Oak Brush

+90 End Brush 35'

+50 Brush 31-50'

+03 PP 28'

Brush 40-50'

+94 Bag Brush 4'

+80 End Kgd

+73 TP 31'

+61 Ent

+98 4" Oak 44'

+65 End Cult Bag Yard - - -

+37 TP 29'

+64 4" Oak 45'

+24 4" Oak 35'

+10 3 1/4 31'

+05 PP 28'

+46 Twin 6" Pop 19'

+03 TP 28'

+01 4" Oak 24'

+54 PP 28'

Cultivated

Cultivated

+18 TP 27'

+41 Ent

+30 8" B.E. 20'

+06 GP 28'

+04 12" B.E. 23'

+84 12" B.E. 23'

+61 10" B.E. 22'

+40 8" Ash 21'

+17 8" Ash 21'

+09 6" Oak 23'

+81 End Rad 14'

+65 PP 50'

+51 Bag Rad 46'

+35 18" X 44" CM 33'

+22 End Rad 52'

+08 PP 32'

+80 Bag Rad 12'

+75 PP 21'

97

Rd

Rd
9

96

11'

10'

95

11'

10'

94

11

10

93

10'

11

92

11'

10'

91

10

10'

90

9

11

+25 Field Ent.

Fc 30

+63 T.P. 28'

Cultivated

+15 PP 28'

Fc 31'

+21 T.P. 28'

+10 Ent

Fc 32'

+92 6" BE 26'

Celery Patch

+28 PP 28'

Fc 34'

+78 T.P. 28'

Hay Field

Fc 35'

+86 Beg Celery Patch

+45 T.P. 29'

+14 PP 28'

Fc. 36'

+80 Beg Hay Field
+77 End Brush 32'

+91 Beg Fc. 36'

+30 Beg Willow Brush 27

+09 T.P. 29'

Cultivated

104

+50

15' 7'

103

13' 5'

+79

13' 6'

102

11' 8'

101

10' 10' 10'

100

9' 10'

99

9' 10'

98

10' 9'

+47 X Drain
24" X 38' CM.

18'

20'

97

11' 9'

+68 T.P. 27'

+47 T.P. 29'
+31 Ent.

+00 6" Triple CoH 31'

+90 4" BE. 32'

+53 6" CoH 33'
+50 6" " 32'

+97 T.P. 29'
+76 Cor Hedge 34'
+96 Fe Cor 27'

Fe 29 Hedge 35'
+86 Beg Hedge 36'
+80 Beg Fe 29'
+70 Ent

+60 Row Trees 42' 0 0 0 0

+47 T.P. 29' End Cult

Great Lakes Pipe Lines
+70 Vent Pipe 38'

+03 T.P. 29'

Cultivated

Orchard
Vinyard

Pasture

+95 Fe Cor 29'
+81 PP 34' Δ Fe 34'
+50 Fe 25' Ditch 50'
+30 PP 33'
Fe 19' Ditch 41'

+79 Fe 18'
Ditch 41'
+52 Fe Cor 20'

Ditch 40'

+15 PP 28'
Ditch 56'

+00 Ditch 54'

+00 Ditch 42'
+98 PP 29'

+00 Ditch 40'
+70 Beg Hay Field
+70 Vent Pipe 40'
+63 Vent Pipe 39'
+47 Beg Ditch 38'

+38 Fe Cor 28' 6"
End Colony

+02 PP 28'

3' B+M Ditch
Hay Field

111 Rd Rd

+56 N.S.P.H. Line

110 10' 32'

109 9' 10'

+50 9' 10'

108 9' 11'

+50 9' 11'

17' +30 X Drain 24' X 36 C.M. 19'

107 8' 11'

106 10' 10'

105 11' 11'

+50 11' 9'

104 11' 7'

+78 P.P. 44'
 +66 N.E. Cor Tower 56'
 +59 End G.R. 17'
 +46 S.E. Cor Tower 56'
 +40 End Cult
 +36 Arc Lt. P. 18'
 +28 Beg. Q. Rail 17'



Plank. G.R.



+95 End Rad 11'
 +60 Rad 24'
 +47 Beg Rad. 45'

+12 End Rad. 68'

+55 Beg Rad 10 to
 End Hay Field

+27 P.P. 3'

Cultivated

Hay Field

+64 P.P. 26'

+21 P.P. 24'

+00 Beg Hay Field
 +97 Fa Cor. 24'

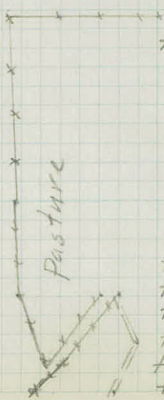
Cultivated

Pasture

Fc. 27'

+75 P.P. 26'

+50 Fc 71'
 +50 A Ditch 77'
 +50 Fc 80'
 +25 A Ditch 89'
 +15 Fa Cor 41'
 +15 Fc. 47'



118 Rd Rd

+64 14' 14'

117 14' 14'

116 13' 16'

+50 14' 16'

115 14' 14'

+50 15' 14'

114 15' 14'

113 13' 13'

+50 11' 12'

112 12' 10'

19' +62 x Drain 24' x 40' CM 21'

+50 9' 9'

111 9 11'

+86 PP 26'

+64 PP 32'

+38 PP 31'

+15 PP 27'

+70 Field Ent.

+50 Ent 10" x 20' Dredge Pipe 18'

+95 G.P. 22'

+75 Bag Cult.

+73 RR ROW Fe 72'

3' Rubble Wing Wall

+95 PP 14'

+70 Bag Cult.

+67 Fe Cor 32'

+56 Bag Fe 32'

+37 RR X Sign 16'
 +24 X Plank 16'
 +19 X " 16'

+21 N.P. RR.

+24 X Plank 16'
 +19 X Plank 16'
 +04 RR X Sign 15'

Cultivated

125

Rd Rd

+50

15'

13'

+73 End Conc. Walk 29'

+67 Beg Conc Walk 29'

+14 Beg School Yard

+196 Grond 3 Small Pines 26'

+10 End Playground

124

15'

15'

123

15'

15'

122

14'

17'

+46

13'

17'

121

16'

19'

+75

21'

41' +53 X Drain 12"X100 CM 59'

+50

34'

18'

+25

62'

120

18'

+75

38'

+50

24'

14'

30' +14 X Drain 15"X60 CM 30'

119

18'

15'

+50

15'

14'

118

14'

15'

Wall 30' 48'
 +87 15' Oak 43'
 +73 Beg Wall 29'
 +67 Wall 29'
 +50 Face Wall 29'
 +23 End G.Rail 16'
 +14 Beg Rubble Wall 20'
 +10 X Fc 26'
 G.R. 16'
 +84 PP 20'

Cultivated

G.Rail 17'

+65 PP 24

+00 Beg Playground
 +00 End Cult
 +98 Beg G.Rail 20'
 +78 Ent

+67 End G.R. 21'

+36 PP 27'

G.R. 23'

+50 G.Rail 23'

+27 PP 28'

G.Rail 22'

+87 T.P. 26'

+50 G.Rail 21'

+08 Beg G.Rail 20'

+80 Field End.
 +55 PP 24'

+00 Beg Cult

+82 Ent

+73 Fc Cor 32'

Fc 38

+83 End Rad 17'

+75 Fc 41

+54 Δ Fc 46'

+41 Δ Fc 58'

+33 Fc Cor 75'

+30 PP 90'

+20 Beg Rad 100'

+95 Ent Rad 85'

+87 T.P. 67

+67 End Cult

+51 G.P. 24'

Cultivated

132

Rd Rd

+25

14'

15'

131

15'

17'

+50

17'

18'

28' + 14' X Drain 24' X 73' Conc. 45'

130

17'

18'

+50

17'

18'

129

17'

17'

128

15'

15'

127

15'

14'

126

15'

14'

+38

15'

12'

+79

+73 12" Oak 47'

+67 8" Oak 55'

+58 Beg Curb 33'

+52 Rgc Tie Ent.

+44 Beg Conc Curb 33'

125

15'

13'

#91 GP 32'

+63 Ent 30
+47 6"Oak 45'
+25 Rgs Tr Ent
+10 12"Oak 35'
Lake 152'
+88 PP 26'
+77 24"CoH 52'
61 8"CoH 44'-12"CoH 5
+41 24"CoH 52'

Lake 157

139 G.P. 33'

443 PP 25'

Lake 156

105 P.P. 23
L9Kc 165

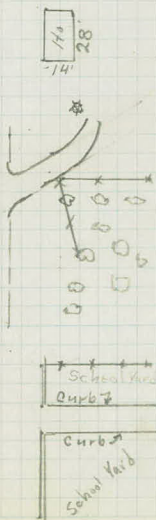
#66 N.W. Cor Ho 32'

+38.5 W Cor H_o 32'
+31 PP 18'
+15 8" Evergreen 50
+80 Ent 33'
+77 Fc Cov 40'
+65 End Trees 40
+60 Rge Tie Ent
+35 Beg Fc 48'
+27 PP 19'
+04 Beg Grove Cnt 49'

+79 X Fe. 35.5'
+79 End Wall 34'
+58 Beg Wall 31'
+53 Ent 12'x16' CM.
+44 End Wall 31'
+06 P.R. 22'
Wall 30'

Hay Meadows

Cultivated



+09 8' W. 11. 32'

139

Rd. 15' Rd. 15'

138

15' 17'

+50

15' 16'

137

14' 12'

19' +68 X Drain 24" X 52 CM 31'

+50

16'

136

+95 12" Oak 37'
+84 8" Elm 45'

14' 15'

+50

14' 14'

23 +10 X Drain 24" X 52' Conc. 29'

135

14' 13'

+50

14' 17'

134

15' 16'

133

14' 14'

132

15' 13'

100 End Oaks 35-45'

840
840
840
840

50

+72 Beg Grove Small Oaks 35-45'

+35 P.P. 30'

+00 Beg Cult

+13 B.P. 27'

+13 P.P. 30'

+00 Beg Cult

+74 20' Elm 32'

+56 Ent.

+45 End Yard

+42 10' Elm 44'

+37 Tree 40'

+25 4' Oak 34'

+21 End Hedge 34'

Hedge 38'

+58 P.P. 29'

+76 Beg Hedge 38'

+70 End Woods 30'

Beg. Yard

+50 Woods 31'

Yard

Small Oaks

+26 Cor Wood 32'

+10 End Cult

+85 G.P. 27'

+88 P.P. 29'

+37 4' Oak 34'

+27 4' Oak 36'

+09 8' Oak 40'

+05 4' Oak 36'

+94 4' Oak 42'

+45 P.P. 29'

+28 P.P. 27'

+05 6' Oak 37'

Lake 150'

146

Kd
10Kd
10

145

9'

12'

+34

11'

13'

144

12'

17'

+75

12'

117'

+82 End 12' CM 25'

+50

13'

48'

+25

15'

27'

143

17'

19'

142

15'

14'

141

16'

15'

21' +50 X Drain 24' X 44' Conc 23'

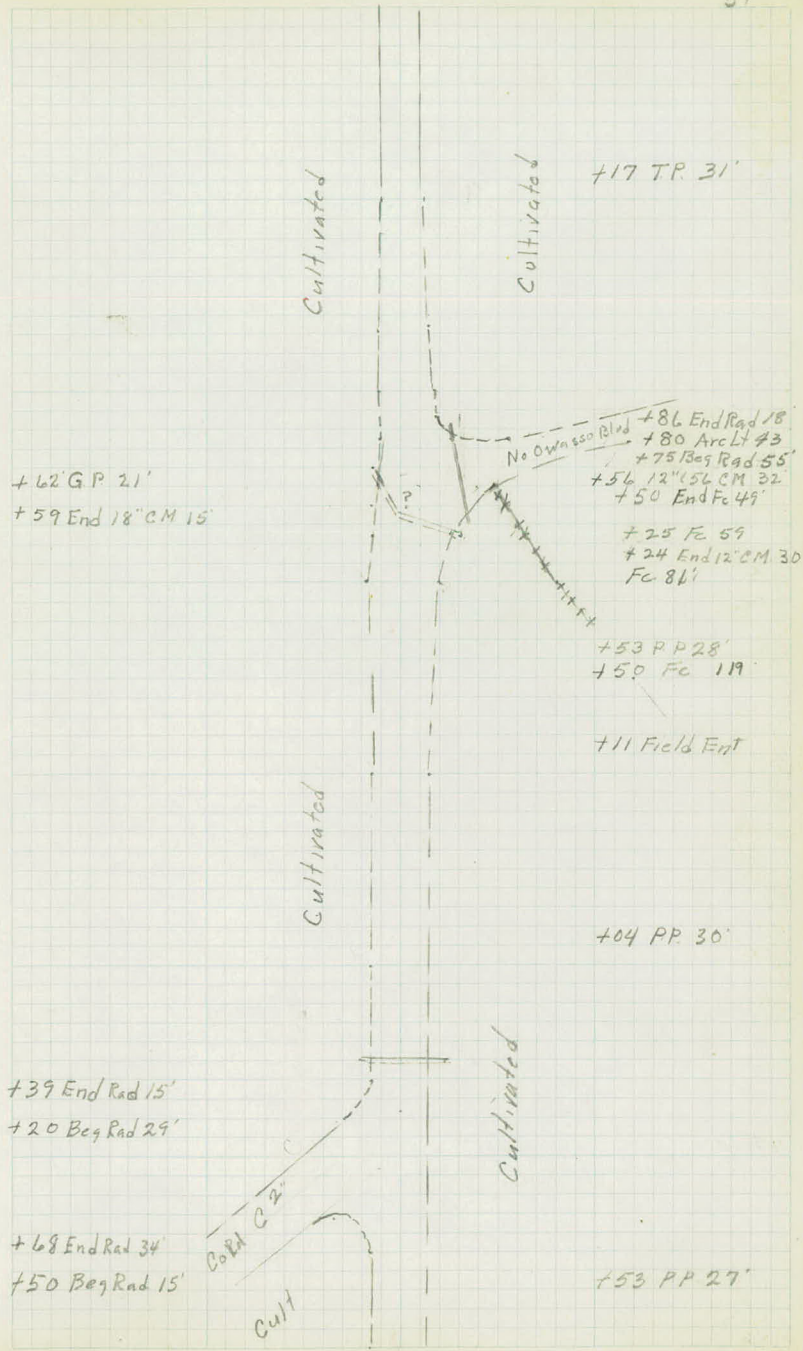
140

15'

139

15'

15'



Cultivated

Cultivated

+17 TP 31'

+62 G.P. 21'
+59 End 18" CM 15'

No Overpass Blvd
+86 End Rad 18'
+80 Arc Lt 43
+75 Beg Rad 55'
+56 12" 154 CM 32'
+50 End Fc 49'
+25 Fc 59
+24 End 12" CM 30'
Fc 86'

+53 PP 28'
+50 Fc 19'

+11 Field Ent

Cultivated

+04 PP 30'

+39 End Rad 15'
+20 Beg Rad 29'

Cultivated

+68 End Rad 34'
+50 Beg Rad 15'

Cont C 2"

Cult

+53 PP 27'

153

10^d
1010^d
10

152

10^d10^d

151

10^d10^d

150

10^d10^d

149

10^d10^d

148

10

10^d

147

10

10^d

146

10

10

+24 T.P. 32'

+97 T.P. 32'

+60 T.P. 32'

Cultivated

Cultivated

+19 T.P. 32'

+07 Field Ent

+69 T.P. 32'

160

Rd. Rd.
11' 10'

159

10'

10'

158

10'

10'

157

10

10'

156

11'

11'

155

11'

12

154

11'

10

153

10'

10'

Fc 34'

Hop Yard

Scattered
Stu. & Trees

+17 Fc Cor 34'
Fc 33'

+90 T.P. 32'

Fc 33'

Scattered Trees
Pasture + Stu.

+50 T.P. 32'

Fc 34'

Cultivated

+21 T.P. 32'

Fc 34'

+85 12' Oak 32'

+55 15' Co. H. 36'

+46 Beg. Fc 34'

+37 Ent

+30 Fc Cor 34'

+30 End Cult.

+27 Field Ent

+23 Rgative Fc

+85 Ent 15' x 20' CM 25'

+88 T.P. 32'

Cultivated

Cultivated

+56 T.P. 32'

167

Rel
10Rel
10

166

10

10

165

10

10

164

10

10

163

11

11

162

11

10

161

10

10

160

11

10

Fc 34'

+23 6" Tree 21'

Fc 34'

+50 T.P. 32'

+44 2-4" Trees 44

+25 T.P. 32'

Fc 34'

Stn. + Trees

Fc 34'

+01 T.P. 32'

Fc 35'

+75 T.P. 32'

+35 Ent.

+28 Fc Cor 35'

+23 Rgc Tis Fc.

Fc 34'

Scattered Trees + Stn.

Pasture

Cultivated

+48 T.P. 32'

Fc 34'

+10 Field Ent

+76 Fc Cor 34'

Fc 34'

+19 T.P. 32'

174 28' + 95' X Drain 24' X 56' CM 28'

173 11' 11'

172 10' 10'

+87 4" Plum 41'

+87 18" Co H 27'

+73 4" Cedar 28'

+66 4" Cedar 45'

171 9' 11'

170 10' 10'

169 10' 10'

168 10' 10'

167 10' 10'

+90 Beg Cult

+75 Beg Cult

+65 End Orchard 30'

+10 Beg Orchard 30'

+04 12" Cott 27'

+96 Ent 12"x26" CM 22'

+50 Ent.

+36 4" Cedar 29'

+31 Fe + Lilac Hedge 31'

+28 Evergreen 43'

+12 End Berry

+03 Beg Berry Patch 37'

End Cult

Cultivated

Uncultivated

Cultivated

+10 End Pot Ho 50-10

+96 T.P. 33

2' Btm Ditch
Trn Center Pot Ho

Pothole 100'

+65 T.P. 33'

+39 T.P. 33'

+15 End Cult

+11 T.P. 32'

+24 Ent 12"x26'

Dredge Pipe 23'

+46 Beg Cult

+40 Fe Cor 34'

Fe 34'

+81 T.P. 32'

+53 6" Tree 23'

181 10 10

180 10' 10'

179 10' 10'

178 26 +51 X Drain 24" X 52' CM 26'
12 12

+50 8' 13'

177 8' 15'

+50 8' 15'

176 11 13'

175 10 10

174 11 11

145 TP 33'

Uncultivated

Cu^{+}

VmCult 26'-100

+28 Ent 15" x 26" CM 24

405 T.P. 32'

Cult.

+ 68 End Pot hole 34

+ 50 Pot/Holz 200'

 $+18 \text{ Be}, \text{Pot}/\text{H}_2 \text{ } 34$

+ 75 Beg Un Cult. 33'

+ 55GP

454 T.P. 31

Cult.

+98 G.P. 33'

+92 T.P 33'

7/14/5

Cult

+45 TP 32'

188

Rd Rd
10' 10'

187

10 10

186

10' 10'

185

10' 10'

184

10' 10'

183

10 10

182

10' 10'

181

10 10'

+75 T.P. 32'

+60 Pot No. 33'

+10 Beg. Pot hole 53

+92 Fo. Cor 33' 4"
End Cult

+40 T.P. 33'

Uncultivated

Cult.

+93 T.P. 32'

+37 End Yard
+27 Ent 15" x 20" CM 25'

+70 Ent 15" x 20" CM 25'

+46 Beg. Yard

+41 T.P. 33'

Uncultivated

Cult

+90 T.P. 33'

195

10 11

29' 7/16" X Drain 24" X 58' CM 29'

194

10' 11'

193

10' 11'

192

10' 11'

191

10' 10'

190

10' 10'

189

10 10

188

10 10

400 PP 28'

Fc 34'

58

+45 TP 33'

Fc 35'

+20 Beg Yard

Waste land

+11 PP 29'

End Yard

Fc 35'
+98 TP 31

Scattered Oaks

Fc 34'
+98 TP 32'

+74 Ent 15' x 20' CM 26'

+64 PP 30'

+50 Beg Yard

Scattered Oaks

Woods
+ Pasture

Fc 34'

+93 Ent 15' x 20' CM 26'

+80 End Brush

+50 End Pot Hole 75
+38 TP 32'

Small Brush

Uncult

Fc 33'
Pot Holes 40-150

+16 Ent 15' x 20' CM 25'
Rip Rap Ends.

+105 TP 32'
Fc 33'
Pot Hole 60-100

Pot Hole 50-75'

202

Rd. Rd.
6 3

20 + 98 X Drain 24" X 54" CM 34'

150

8' 13'

201

9 11'

200

10' 10'

199

11'

27 + 57 X Drain 24" X 54" 27'

198

11' 11'

197

11 11

196

11' 11'

195

10' 11

+50 T.P. 37'

March 32-150'

+70 Marsh 33'

+20 T.P. 32'

+00 Beg Marsh 100'

+73 End Rod 10'

+37 Beg Rod 67'

+85 T.P. 33'

+60 Fe Cor 33'

Fe 33'

+44 T.P. 32'

Fe 33'

Fe 33'

+97 T.P. 32'

Fe 34'

Hayfield

+00 P.P. 27'

+36 12" X 28' CM 75'

+20 Ditch 63'

+85 Beg 1' Btm Ditch 33' Brush
Uncult

+40 End Yard

+81 Ent 15" X 20' CM 27'

+66 P.P. 28'

+74 Ent

+33 Ent 15" X 20' CM 26'

Yards

Stu + Scattered Oaks
Pasture

209

Rd Rd

208

11'

11'

207

11'

11'

206

13'

9'

+50

16'

7

205

17'

7

+50

16'

7

204

12'

9'

203

8'

13'

+63

8'

13'

202

7'

13'

+86 T.P. 31'

+49 T.P. 31'

+17 T.P. 31'

Hay Field

+95 T.P. 31'

Hay Field

+10 Ent 15" x 20' C.M. 27

+93 T.P. 31'

+00 End Marsh 37-73

+75 T.P. 37

Marsh 24' - 150'

216 Rd Rd
10' 10'

+35 14' 9'

215 16' 8'

+80 End Hay Field

+50 16' 5'

214 17' 6'

+50 15' 9'

+25 13' 8'

213 12' 11'

212 12' 11'

211 11' 10'

210 10' 10'

209 10' 10'

Fe 36 61

Cultivated

Pasture

+35 Fe 34

+00 Fe 36

+85 TP 28

+79 Fe Cor 42

+67 Ent

+62 Rqctie Fe

+00 End Hay Field
Beg Cult.

+00 TP 28

+82 T.P 32

Hay Field

Hay Field

+52 T.P. 31

+24 End Pot Hole 31-
+24 T.P 31

+70 Pot hole 24-90

+33 Beg Pot Ho 100

223

Kd. Kd.
12' 12'

+50

9' 13'

222

9' 13'

+50

9' 13'

221

8' 14'

+50

13'

220

9' 11'

219

11' 11'

26' + 32' X Drain 24" (60 CM. 34'

218

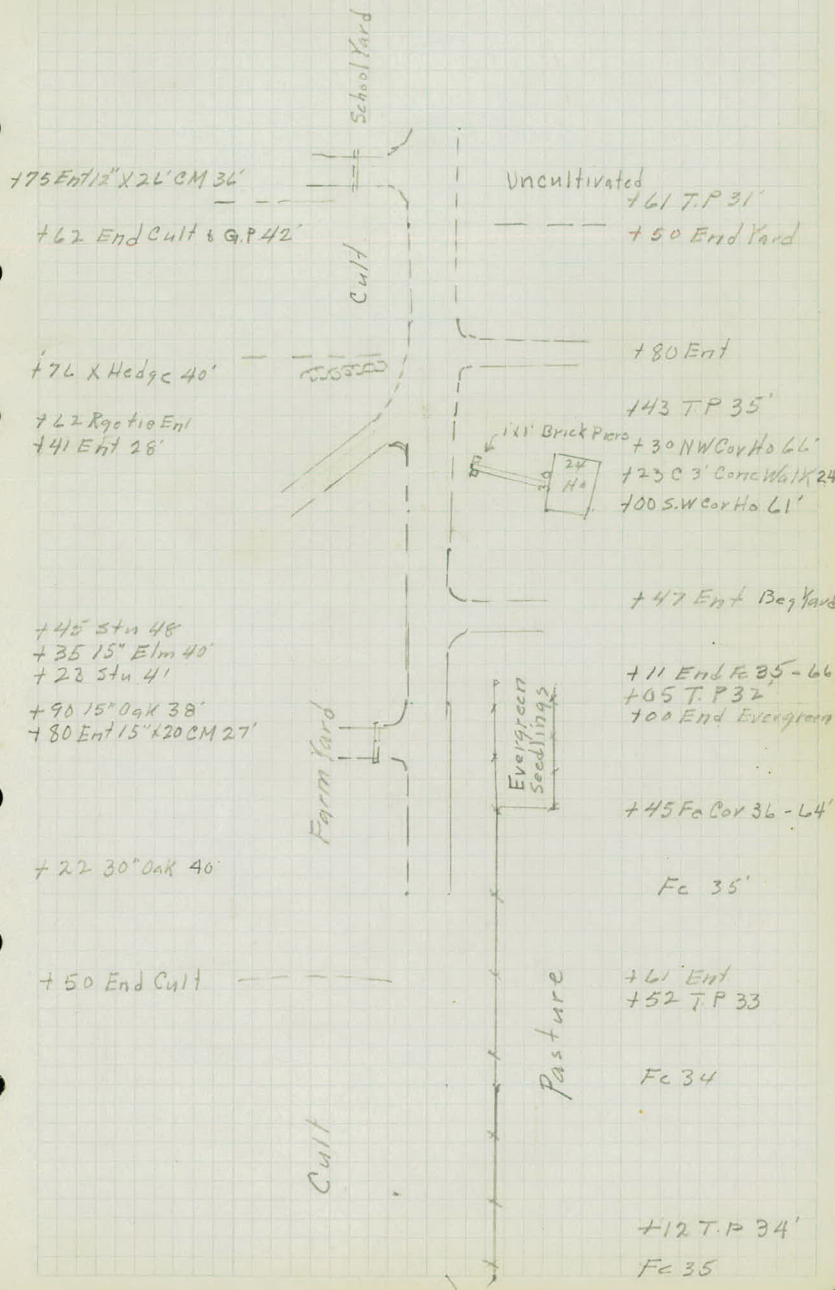
11' 11'

217

10' 10'

216

10' 10'



230

Rd Rd
9

105 RR ROW Fc 54'

229

9'

22' + 95' X Drain 18' X 43' CM 21'

228

13'

227

11'

9'

160 Beg Orchard 60'

226

20' + 12' X Drain 24' X 50' CM 30

11'

13'

225

10'

12'

224

10'

12'

223

12'

12'

+76 PP 78'
+72 Beg Rad 75'

+146 End Rad 75'
+13 TP 32'

X Sing Plank 12'
+93 Beg Rad 11'

+52 Battery Well 24
+52 X Sing 20

+30 TP 27'
+20 PP 32'
+14 PP 32'
+89 Ent
+80 Fc Cor 46'

Fc 35'

+79 T.P 33'

Fc 33'

+47 T.P 32'

Fc. 36'

+20 T.P 33'

Fc 34'

Fc 33

+15 Beg Cult.
+12 G.P. 32'
+04 RR Sign 25'

R.R. X Sing Plank 12'

+55 End Rad 9'

+16 G. Pole 44'
+08 Beg Rad 50'

+81 End Rad 71'

+30 Beg Rad 10'
+10 End Orchard 65'

+72 6" Maple 32'
+60 Twin Maple 28'
+41 10" Maple 28'
+35 End Woods
+34 Birch 30'

+05 24" B.E 32'
+70 8" B.E 30'
+75 12" B.E 31'

+50 24" Maple 31
+65 12" Maple 28'
Woods 28'

+88 26" Maple 27'
+75 Ent

+63 15" Maple 25'
+45 15" Maple 25'
+26 Maple 26'
+05 24" Maple 26'
Woods 30'

+84 Beg Woods 30'

+57 End Yard

Woods

Uncultivated

237

13' 13'

236

13' 13'

235

13' 13'

+92 15" Oak 50

234

13' 13'

233

12' 12'

232

10' 10'

+85 Row. Elms 32'

231

9' 13'

230

9'

FC 33'

Fc 34'
+87 T.P. 32'

FL 33'
+ 92 Retic Fe
+ 87 Fe Cor 33'
+ 77 Ent 15" x 20" CM 25'

$F_c 34'$

+47 PP 30'

+45° T.P 32' + Beg Fc

109 12" Oak 42

+19 Ent. 15" x 20' CM 25

Fc 34

+96 Sta. 31'

Pasture

+26 Fc Cor 34'

Cult

+96 Ent+

+ 80 15" Maple 42'

#17 2-15' Maples 35-52'

102 2-15" Maples 32-52'

+ 89 12" Maple 50'

477 T.P.32

+ 64 15' Maple 35'

+37 12" Maple 35'

+15 10" Apple 48'

Yard

+ 84 12" Maple 35'
+ End Cult Bcg Yard

Yard

+00 End Yard

192 T.P. 32

471 6' B E 50'

+64 4" Tree 33

+ 37 2" Cedar 34

+ 35 4" Ash 42

+ 29 4° Cedar 28

177 FM 7 12" X 20 CM - 23

104 3- Pop 30-42.63

+41 T. P. 32'

+20 End Rad 15°

244

13

13

243

13

13

32" x 61" x Drain 24" x 60" CM

28

242

18

13

241

13

13

240

13

13

239

13

13

238

13

13

237

13

13

Fc 34 Ditch 44'

+75 Ditch 58'

+42 Beg. Ditch 87'
End Pothole

Fc 34' Beg. Pothole 85'

Fc 32

65

+22 T.P. 31

Fc 31'

Fc 34'

Fc 31

+72 T.P. 31

Fc 34'

Fc 33'

Fc 34

+22 T.P. 32'

Fc 33'

+90 Ent

Fc 34'

+25 End Pothole 60-100'

Fc 33 Pothole 50'

+71 T.P. 32'

+60 Beg Pothole 60-100'

Fc 33'

Fc 33'

Fc 34

+30 T.P. 32'

Fc 33'

Pasture

Cultivated

251

Rd
13Rd
13'

250

13'

13'

249

13'

13'

248

13

13'

247

13'

13'

246

13

13'

245

13'

13'

244

13'

13'

Fc 35

Fc 35

Fc 36

Fc 34

Fc 34

+84 End Pothole 70-150

+50 Pothole 52

Fc 34 Pothole 60

+50 Pothole 94-155

+35 End Ditch 88' Bag
Pothole

Fc 34 Ditch 5L

+70 Δ Ditch 38

Fc 34 Ditch 44

2' Btm

Fc 32

66

+67 T.P 32

Fc 32

+22 T.P. 31

Fc 32

Fc 32

+69 T.P 31

+05 Ent 15" x 20 CM 2
Fc 32

+21 T.P 31

Fc 32

Fc 32

+71 T.P 31

Fc 32

Cultivated

258

14' 15'

+50

15' 14'

257

15' 15'

+50

14' 15'

256

14' 15'

+50

15' 15'

255

15' 15'

+50

15' 15'

254

13' 13'

+50

13' 13'

253

13' 13'

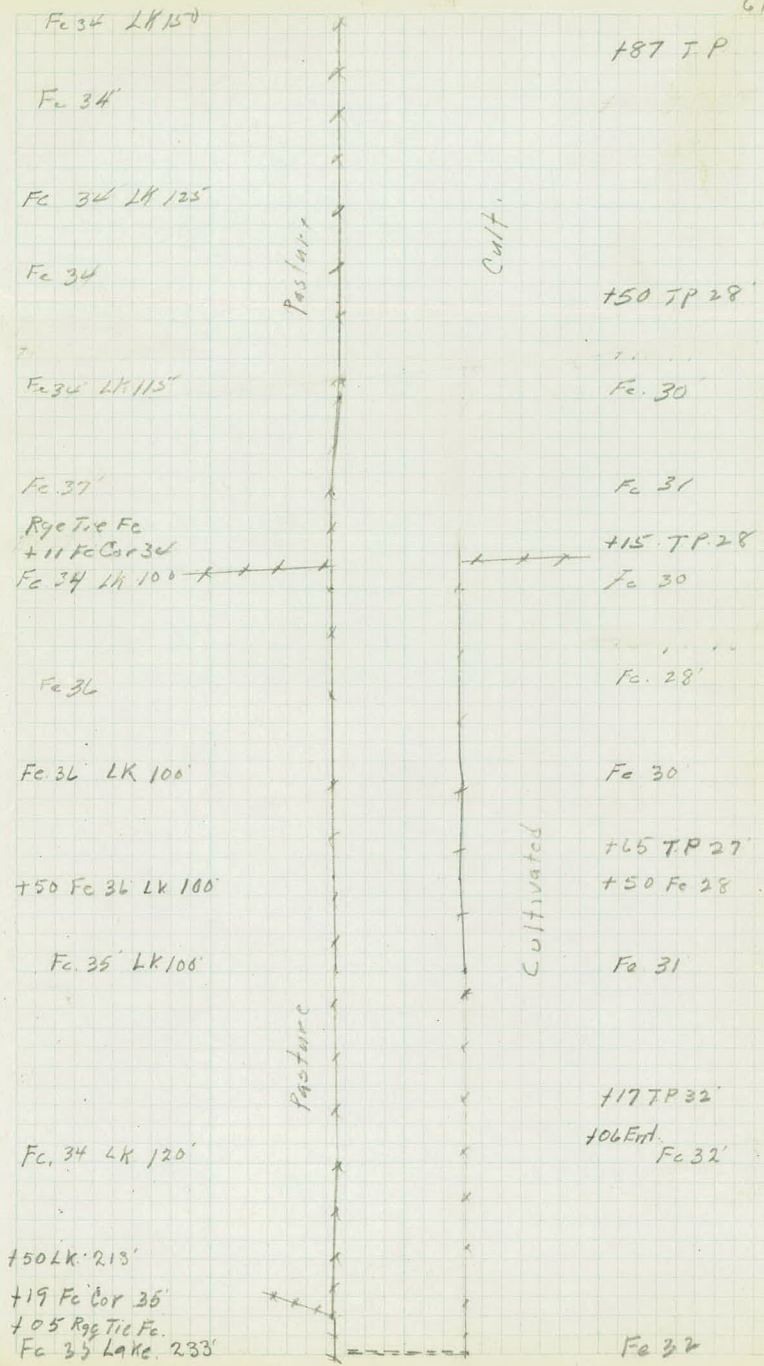
252

13' 13'

251

29' +02 X Drain 24" X 62 CM 33'

13 13



265

Rd Rd
16' 16'

264

16' 16'

263

16' 16'

262

16' 16'

261

16' 16'

260

15' 15'

259

15' 15'

258

14' 15'

Fe 35

68

+48 Beg Fe. 36

Evergreen
Seedlings

Nursery 38

+75 Beg Nursery 38

+10 End Yard

+100 Ent 15" X 20' CM 27

Yard.

+27 4" Ash 5

+69 Row Tr. 40

+09 Beg Yd.

+92 X Fe 32' X Hedge

+82 Row Apple Tr. 38

+67 Row Apple Tr. 38

+24 Ent 15" X 20' CM 28

+06 3" Elm 36

+78 3" Elm 37

+46 2" Elm 38

+29 X Hedge 33 Beg Yard

+26 Fe Cor 33

+26 P P 50

+20 Ent 15" X 20' CM 30

LK 300 Fe 3V

Yard

Fe 34 LK 15V

+60 End Orchard 47
Beg Cult.

+42 T P 31

+92 Beg Orchard 47

+70 Cor Row Tr. 43

Beg Yard.

+14 Beg Row Small Tr 45

+11 T P 32

+100 Ent 15" X 20' CM 26

+90 End Row Tr.

Yard

+42 Beg Row 2" Tr. 4

+94 Pgc Tr.
+89 Fe Cor 33

+60 T P 32

+90 Fe Cor 34

+30 T P 31

+22 Ent 15" X 20' CM 26

+24 T P 31

Pasture

Cult.

272

15' 15'

61' + 26 X Drain 24" X 100' CM: 39'

271

15' 15'

270

16' 16'

269

16' 16'

268

15' 15'

267

15' 15'

266

16' 16'

265

16' 16'

+90 Bay Lilac Brush 51'-61'

+72 Ent 15"X20"CM-28'

+47 24"BE 51'

+84 Δ in Ditch 130' 3' Btm Brush

+80 Rubble Ditch Check 19'-31'

+67 Stn 43'

+70 P.P. 27'
+56 2 Gramsie Rd 15"X28"
CM-24'

+40 Fe Cor 34'

Fe 34'

Fe 36 End Nursery

Fe 35'

Fe 36'

Evergreen
Seedlings

Cult.

Planted

Pasture

Cultivated

Yard

Yard

Yard

Uncultivated

Fe. 35 Ditch 84'

+75 Δ in Ditch 78'

+46 Fe Cor 34'

+41 End 1 Drain 35'

+97 Ent
+92 TP 36
End Yard

+50 Ent
+42 Row Tree 42
+38 Hedge 36'

+75 4 Elm 42'
+68 TP 33'

+46 3 Elm 42'

+28 Ent 15"X20 CM-26'

+44 2 Gramsie Rd 15"X32"
CM-27'

+10 T.P. 33'

+66 T.P. 33'

+62 Ent 15"X20 CM-27'

+75 T.P. 33'

+50 End Cult

279

Rd Rd
15' 15'

278

15' 15'

277

15' 15'

34' + 86' X Drain 24" x 72" CM 38'

276

16' 16'

275

15' 15'

274

15' 15'

273

15' 15'

272

15' 15'

+62 T.P. 33'

+23 Field Ent

Cultivated

Cultivated

+72 Field Ent

+36 T.P. 33'

Beg Cult

+09 Fe Cor 36

Fc 36'

+80 End Pot/hole 100

+68 End X Drain 32'

+20 Beg Pot/hole 70-100

+12 Ent

+08 Fe Cor 35

+06 T.P. 33

Fc 35'

Beg Cult.

+06 End Orchard

Orchard

+37 Beg Orchard 41

+14 20" Maple 41

+50 Ent 15" x 20" CM 27'

+48 Stu 47'

+48 End Hedge 32'

+30 End Maple 41

+92 Beg Maple 47'

+90 Beg Hedge 32'

+76 Ent

+65 End Sm. Tr. 35'

4-12" Maple

0 0 0 0

0 0 0 0 0 0 0 0

Fc 35

+79 T.P. 33'

+68 Ent

Fc 35

+50 T.P. 33

+40 Rge Tie

+37 Fe Cor 35'

Fc 35'

+00 End Pot/hole 50-150

Row Tr. 35'

Planted

11-2" Tr.

0 0 0 0 0 0 0 0

0 0 0 0 0 0 0 0

+24 End Lilac Brush 51-61

+11 stu 53

+11 Beg Row 2" Tr. 34

0 0 0 0 0 0 0 0

0 0 0 0 0 0 0 0

0 0 0 0 0 0 0 0

0 0 0 0 0 0 0 0

0 0 0 0 0 0 0 0

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0 0 0 0 0 0 0 0

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0 0 0 0 0 0 0 0

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0 0 0 0 0 0 0 0

0 0 0 0 0 0 0 0

+31 T.P. 31

+30 Beg Pot/hole 50-150

Fc 35 Ditch 84'

286

16Rd 12Rd

285

15[°] 15[°]

284

15[°] 15[°]

283

15[°] 15[°]

282

15[°] 15[°]+70 * G.R. 17[°]

281

15[°] 15[°]

280

15[°] 15[°]

279

15[°] 15[°]

+72 T.P. 32'

+22 T.P. 32'

Hay Field

Cultivated

+74 T.P. 30'

+00 End Rad 15'

+87 Beg Rad 29'

Co

Rd

F

+00 End Rad 15'

+84 Beg Rad 34'

+59 End Rad 31'

+39 Beg Rad 15'

+55 End Rad 39'

+41 T.P. 33'

+40 Beg Rad 16'

Cultivated

Cultivated

+90 T.P. 33'

293

16
1716
17

292

16

16

+91 Twin Oak 62'
+90 5th 45'

291

16

16

290

16'

16'

289

16'

16'

288

16'

16'

287

16'

16'

286

16'

16'

+81 T.P. 32'

Hayfield

Hayfield

+97 54 36'
 +92 54 35'
 +76 15" x 20' CM 26'

+52 T.P. 31'

+16 T.P. 32'

+75 Field End

Hayfield

Cultivated

+27 T.P. 30'

+19 T.P. 32'

300

17' 17'

+50

17' 17'

299

17' 17'

+50

16' 17'

298

15' 17'

+50

15' 17'

297

17' 17'

+50

18' 15'

296

19' 16'

+64

17' 17'

295

17' 17'

294

17' 17'

293

17' 17'

Cultivated

+40 End Brush line

Brush line 64'

+50 Brush line 95'

Hayfield

1 Stand Fe
Pasture
Brush

+51 TP 32'
+50 Fe 35'

Fe 35

+50 Fe 35' - 71'

+22 TP 32'
+17 Fe Cor 39

+90 Rge Tie Fe.

+85 TP 33'

Hayfield

+46 TP 33'

+11 TP 32'

307

Rd 17 Rd 17

+50

16 18

306

17 17

35 +82 X Drain 24" X 60' CM 25'

+63

17 18'

305

18 18'

304

16 18'

+50

15' 18'

303

16 19'

+50

17' 20'

302

16 19'

+50

15 20

301

17 19'

300

17 17

Fe 34-68

+86 3" Apple 41
+85 T.P. 33' 74

+50 Fe 34'-105'

+47-2" Apple 47'
381m Ditch

Fe 35'

+18 Ent

+63 Fe 33'

+88 End 24" CM 25'
+83 Fe Cor 30
+73 Rgetic Fe
+63 Fe 32'

Fe 33

+34 T.P. 33'

Fe 34

Fe 32'

+84 G.P. 31

+50 Fe 28'

+14 Rgetic Fe.

+85 Fe Cor 35'

+85 Rgetic Ent

+57 Ent 26'

Cultivated

1 Strand Barb Wire

Pasture

Fe 35'

+81 T.P. 33

+50 Fe 35'

Fe 36
+97 Ent 27'

+69 Rgetic Ent
+50 Fe 38

+29 T.P. 32'

Fe 37'

Pasture

+50 Fe 37
+32 Fe Cor 34

+16 Rgetic Fe

Fe 35

+84 T.P. 34'

Cultivated

1 Strand Barb Wire

Pasture

Fe 34

314 Kd 16 Kd 16

+50 18' 18'

313 17 17'

+50 18' 16

312 16' 19

+50 15' 20'

311 19' 17'

+50 21' 15'

310 18' 16

+50 16' 16'

309 15' 17'

+96 Oak 49

+50 15' 15'

308 15' 15'

+89 Oak 38'
+87 Oak 46'
+86 4" Oak 57'
+81 Oak 49'
+56 4" Apple 38'

+50 15' 15'

307 17 17

Barnford

321

Kd 16 Kd 16

320

17 17

36' + 05' x Drain 24' x 90' CM 54'

319

17 17

318

16 16

317

17' 17'

316

16 16

315

17' 17'

29' + 32' x Drain 24' x 58' 29'

314

16 16

+37 Stn 37'
+34 Oak 41'
+20 Oak 48'
+17 Oak 42'

+100 Ent 15'x20'CM 27'

+85 Fe Cor 22

+80 P.P. 32

+76 Rqctic Fe

Fe 26

+90 Ent 24'CM 32'
Rubble End

+40 Rqctic Fe

+37 Fe Cor. 29

+100 Rqctic Ent

+85 Ent 31

+67 End. Fe 32

Fe 33

+87 P.P. 55

Fe 34

Fe 33

Fe 32

Cult.

Post Only

Hay Field

Cult.

Fe 31

Brush

4' Btm Ditch

Fe 34

Fe 34

Fe 33

Fe 32

+44 Ent

+31 Fe Cor 32

+26 Rqctic Fe

Fe 33

Fe 33

328

16
1716
17

327

16

16

326

17

17

325

17

17

324

25' + 05' X Drain 24" X 56' CM 31'

17

17

323

17

17

322

16

16

+ 92 Oak 45'
 + 81 Oak 41'
 + 77 Sfr 44'

321

16

16

Fe 34

Fe 34 77

Fe 44

+42 Ent

Fe 34'

Fe 34

Cultivated

Cultivated

Fe 34

Fe 34

+84 Fe Cor 34'

+77 Oak 40'

Fe 36'

+84 Fe Cor 36'

Fe 34

Fe 38'

Fe 34

Turkey
Pasture

Cultivated

Fe 33

+64 Field Ent.

Fe 34

+83 Fe Cor 34'

+62 15' x 20' CM 24

+46 Stn 39'

+39 Stn 39'

+37 Stn 53

Yard.

Fe 34

335

Rd
17Rd
17

334

17

17'

333

17

17

332

15"

17

331

15

17'

330

15

17'

329

16

17

328

25 + 15 x Drain 24" x 54" CM 29'

17

17

197 Rgc + 17 Fe
+ 80 Fe Cor 36'

Pasture

Fe 35' 78

Fe 35'

+ 54 Ent 15' x 20' CM
Fe 34²⁵

Fe 36

Fe 34

Fe 36'

Fe 34

Fe 38

Cultivated

Cultivated

Fe 34

Fe 45 End Brush

Fe 34'

+ 50 Fe 50' Brush 31

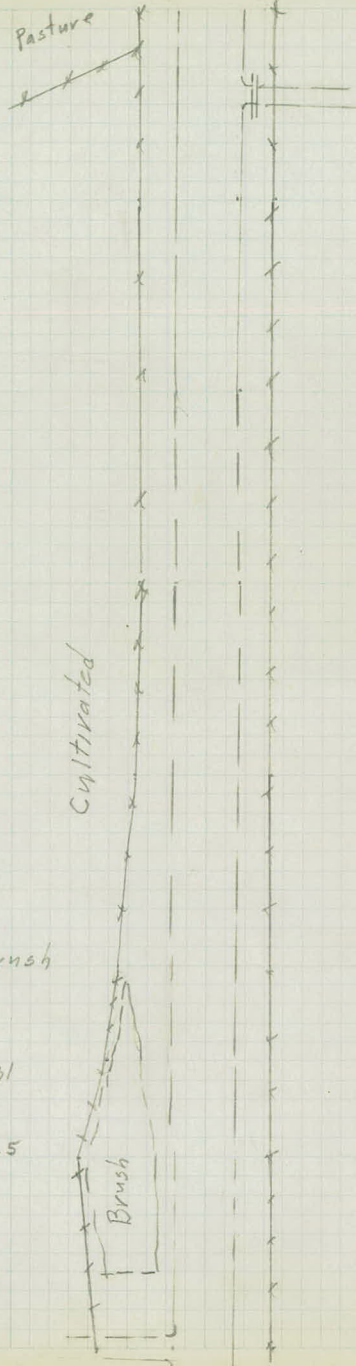
Brush 26 Fe 65

Fe 34

+ 40 Beg Brush 26'

+ 02 Ent
Fe 36

Fe 34



Rd Rd

339

+19 G Rail
+14 Edge Black top

338

+75

33'

30'

+50

18

18

337

17

17

336

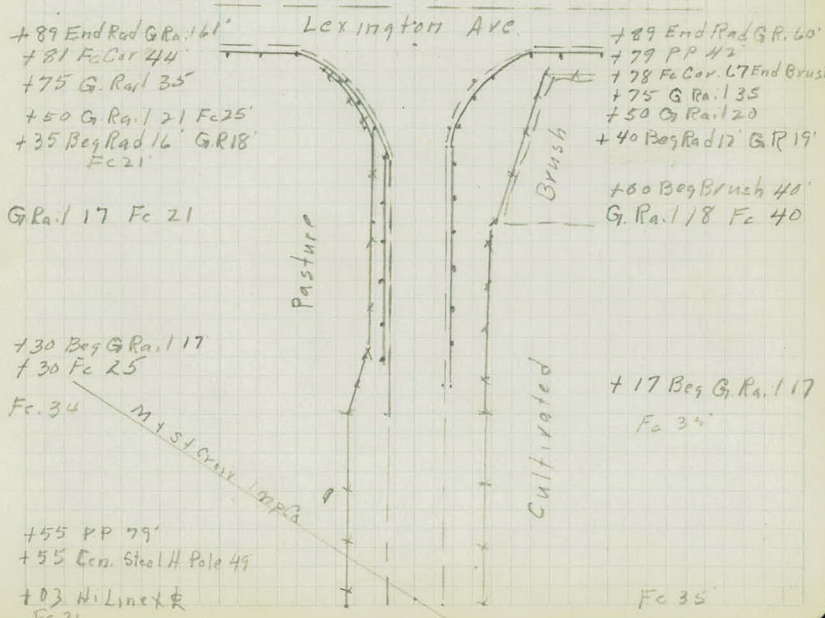
17

17

335

17

17



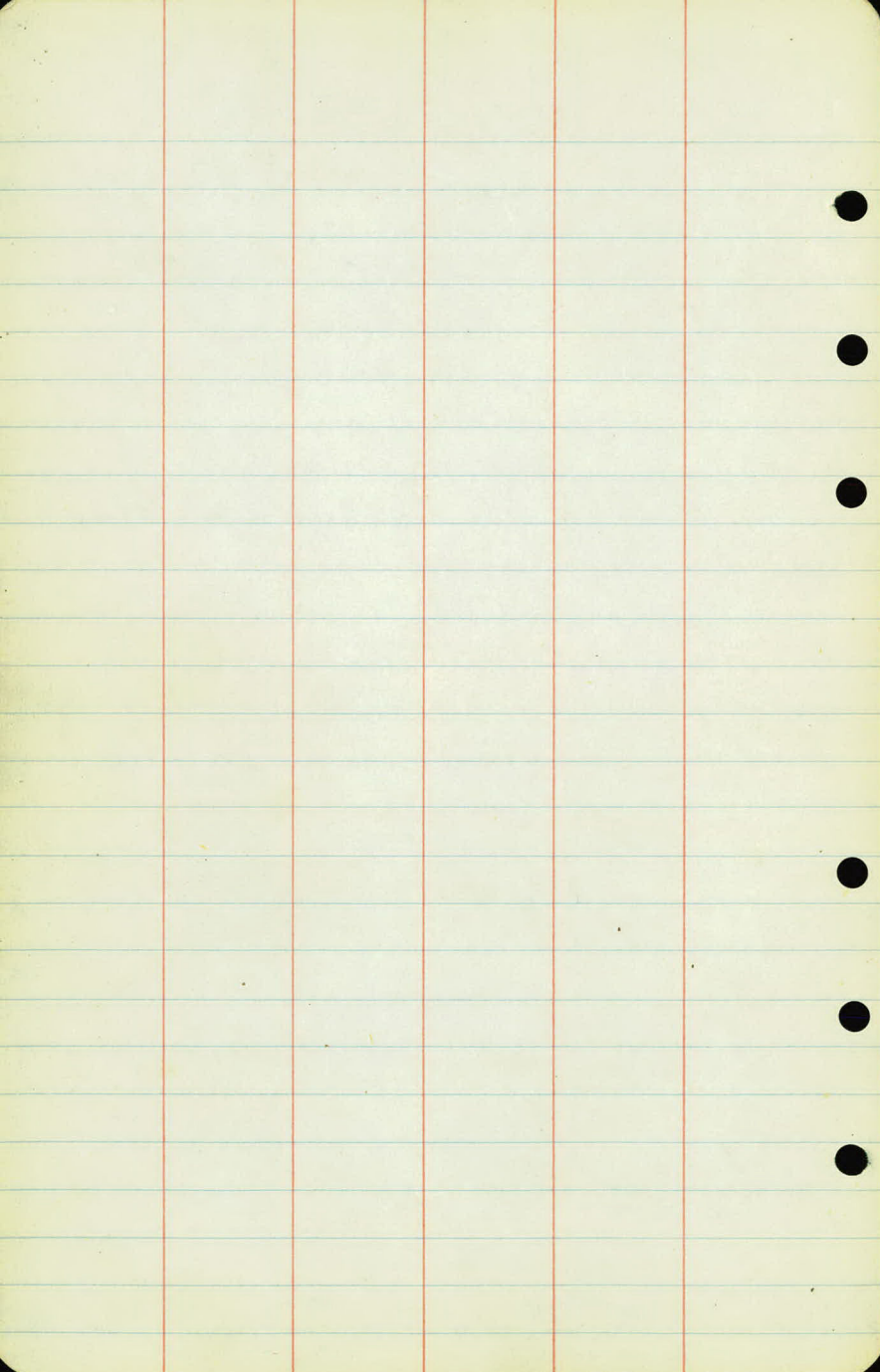


Victoria St. Levels raised
11-5-48 to conform with
other county datums:

X Sections should be fixed
to agree with bench level
datum. ?

K.A.

(Victoria St. Notes)



Bench Levels
Victoria Str.

Sta	+	Δ	-	Elev
B.M.	3.63	917.17		913.54
	2.74	908.26	11.65	905.52
	2.70	907.73	3.23	905.03
	1.71	903.09	6.35	901.38
	9.76	904.98	7.87	895.22
	13.44	917.91	0.51	904.47
	9.87	926.43	1.35	916.56
	7.24	929.07	4.60	921.83
	6.63	931.48	4.22	924.85
	12.20	943.39	0.29	931.19
	5.98	948.81	0.56	942.83
B.M.	12.29	959.40	1.70	947.11 ✓
	11.73	970.19	0.34	959.06
	11.12	980.46	0.85	969.34
	9.57	989.63	0.40	980.06
	2.75	989.84	2.54	987.09
	2.12	982.68	9.28	980.56
	1.85	974.19	10.34	972.34
	2.00	966.16	10.03	964.16
	1.74	958.01	9.89	956.27
	11.06	968.16	0.91	957.10
	9.76	977.20	0.72	967.44
	1.59	971.84	6.95	970.25
	2.17	964.86	9.15	962.69
	3.03	957.74	10.15	954.71

U.S.G.S Bench Mark NE. Cor. STH 96 & USH 48

Top Man Snelling & Co Rd G.

Sta	+	Σ	-	Elev
		957.74 ✓		
	2.20	950.06	9.88	947.86 ✓
	8.37	953.04	5.39	944.67
B.M.	2.37	953.04	2.37	950.67 ✓
	5.79	956.02	2.81	950.23
	7.86	959.82	4.06	951.96
	6.18	965.38	0.62	959.20
	6.09	966.54	4.93	960.45
	5.13	966.44	5.23	961.31
	6.45	965.03	7.86	958.58
B.M.	6.71	968.14	3.60	961.43 (961.98)
	9.46	976.82	0.78	967.36
	0.86	970.50	7.18	969.64
	1.21	960.49	11.23	959.27 ✓
B.M.	7.45	960.48	7.45	953.03 (953.58) ✓
	1.78	953.35	8.91	951.57 ✓
	2.46	946.41	9.40	943.95 ✓
	9.26	948.98	6.69	939.92 ✓
B.M.	6.32	948.98	6.32	942.66 (943.21)
	9.62	956.62	1.98	947.00
	9.44	965.36	0.70	955.92
T.B.M.	10.97	975.55	0.78	964.58 (965.13) K.A.
	11.65	986.53	0.67	974.88
	12.96	998.84	0.65	985.88
	3.93	1001.65	1.12	997.72

Top Man Co Rd G + Lexington Ave

Top Man Lexington + Victory St

Spk in 8" Oak 40' Rt Sta 324+80

Top Iron Mt. Ctr Sec 23 (33' No P. 1 Sta 312+43.00)

Spk in T.P. 28' Rt Sta 305+30

Sta	+	π ✓ -	Elev	
		1001.65		
B.M	5.52	1001.65	5.52	996.13 (996.68) K.R.
	1.76	994.16	9.25	992.40
	1.36	987.06	8.46	985.70
B.M	8.25	988.61	6.70	980.36 (980.91)
	4.75	989.23	4.13	984.48
	3.44	985.82	6.85	982.38
B.M	4.85	985.82	4.85	980.97 (981.52)
	2.98	980.75	8.05	977.77
	2.30	974.45	8.60	972.15
	1.50	966.74	9.21	965.24
	2.97	958.52	11.19	955.55
B.M	10.70	958.52	10.70	947.82 (948.37)
	5.78	959.07	5.23	953.29
	7.74	962.70	4.11	954.96
	5.64	964.74	3.60	959.10
	2.43	961.98	5.19	959.55
B.M	5.46	959.45	7.99	953.99 (954.55)
	10.98	969.14	1.29	958.16
	4.37	971.55	1.96	967.18
B.M	3.88	967.23	8.20	963.35 (963.96) ✓
	1.59	961.78	7.04	960.19
	0.22	950.58	11.42	950.36
	5.24	947.58	8.24	942.34
	5.61	947.58	5.61	941.97 (942.57) K.R.

Spk in Twin Oak 50' Rt Sta 291+90

Spk in P.P. S.W. Cor. Co Rd "F" & Victoria

S.W. Cor 4th Platform at Ho 100' Rt Sta 269+50

Spk in cluster 5 Will 75' Lt Sta 252+00

Top. S.W. Bolt X Signal 10' Rt Sta 228+50
(954.65 = EL. used for Island Lake) k.H.

Spk in 15" W. Oak 50' Rt Sta 214+90

Spk in 15" Oak 50' Rt Sta 197+90

Sta	+	Δ	-	Elev	
		947.58			
	6.43	950.09	3.92	943.66	
	6.38	952.19	4.28	945.81	
B.M.	7.08	953.72	7.55	944.64	(945.24) K.A.
	7.46	957.70	1.48	952.24	
	6.54	961.32	4.92	954.78	
B.M.	2.68	957.31	6.69	954.63	(955.23)
	5.39	957.19	5.51	951.80	
	6.81	959.77	4.23	952.96	
B.M.	2.76	959.77	2.76	957.01	(957.61)
	0.13	949.79	10.11	949.66	
	0.52	938.68	11.63	938.16	
	0.55	927.80	11.43	927.25	
	1.95	917.90	11.85	915.95	
B.M.	2.00	910.26	9.64	908.26	(909.27)
	4.54	904.17	10.63	899.63	
	7.96	907.49	4.64	899.53	
	9.07	914.98	1.58	905.91	
B.M.	5.17	914.98	5.17	909.81	(910.42)
	6.81	918.30	3.49	911.49	
	2.24	914.30	6.24	912.06	
	1.84	902.96	13.18	901.12	
B.M.	0.77	897.30	6.43	896.53	(897.21) K.A.
	6.73	900.83	3.20	894.16	
	1.69	895.75	6.77	894.06	

Description

84

SpK in 15" W Oak 90' Rt Sta 187+05

Top Boulder Mon 170+15

SpK in 12" Oak 35' Lt Sta 155+95

SpK in PP. 28' Rt Sta 141+06

Top S.W. Cor Gona Platform at School Rt 124+75

Top High Anchor Nut N.E. Leg Steel Hi. Tension.
Lt Sta 111+00

Sta	+	Δ	-	Elev	
		895.75			
B.M	8.54	899.74	4.55	891.20	(891.90) K.A.
	11.95	911.26	0.43	899.31	
	12.86	923.90	0.22	911.84	
	13.46	936.29	1.07	922.83	
	7.12	942.99	0.42	935.87	
B.M	5.58	942.99	5.58	937.41	(938.12)
	5.53	942.81	5.71	937.28	
	5.59	942.74	5.66	937.15	
B.M	4.35	942.74	4.35	938.39	
	2.86	940.11	5.49	937.25	
	6.94	938.79	8.26	931.85	
B.M	1.35	934.63	5.51	933.28	(934.01)
	4.77	926.34	13.06	921.57	
	13.33	939.47	0.20	926.14	
	12.67	951.92	0.22	939.25	
B.M	1.51	951.92	1.51	950.41	(951.13)
	2.82	949.53	5.21	946.71	
	10.73	952.91	7.35	942.18	
	13.05	965.22	0.74	952.17	
	10.38	975.19	0.41	964.81	
B.M	2.92	975.19	2.92	972.27	(973.28)
	4.72	976.35	3.56	971.63	
	3.93	978.69	1.59	974.76	
B.M	1.66	976.21	4.14	974.55	(975.25) T.A.

Description

Spk in P.P. 28' Rt Sta 95+05

Top Mon Sta 84+35.40 Cor Scall

~~Spk in P.P. 25' Rt. Sta 71+05~~

Top Mon $\pm$ Cor R. B + Victoria

B 95421
22.25
73

Spk in 15" Oak 50' Lt Sta 44+00

Spk in 12" Oak S.E. Cor Sta 34+50

Top S.E. Cor Conc Walk 32' Lt Sta 21+60

Sta + π - Elev

976.21

0.26 963.96 12.51 963.70

0.21 951.62 12.55 951.41

1.78 943.23 10.17 941.45

B.M 5.01 943.23 5.01 938.22

(938.92)

3.91 937.50 9.64 933.59

6.01 937.66 5.85 931.65

B.M. 4.02 933.64

(934.33)

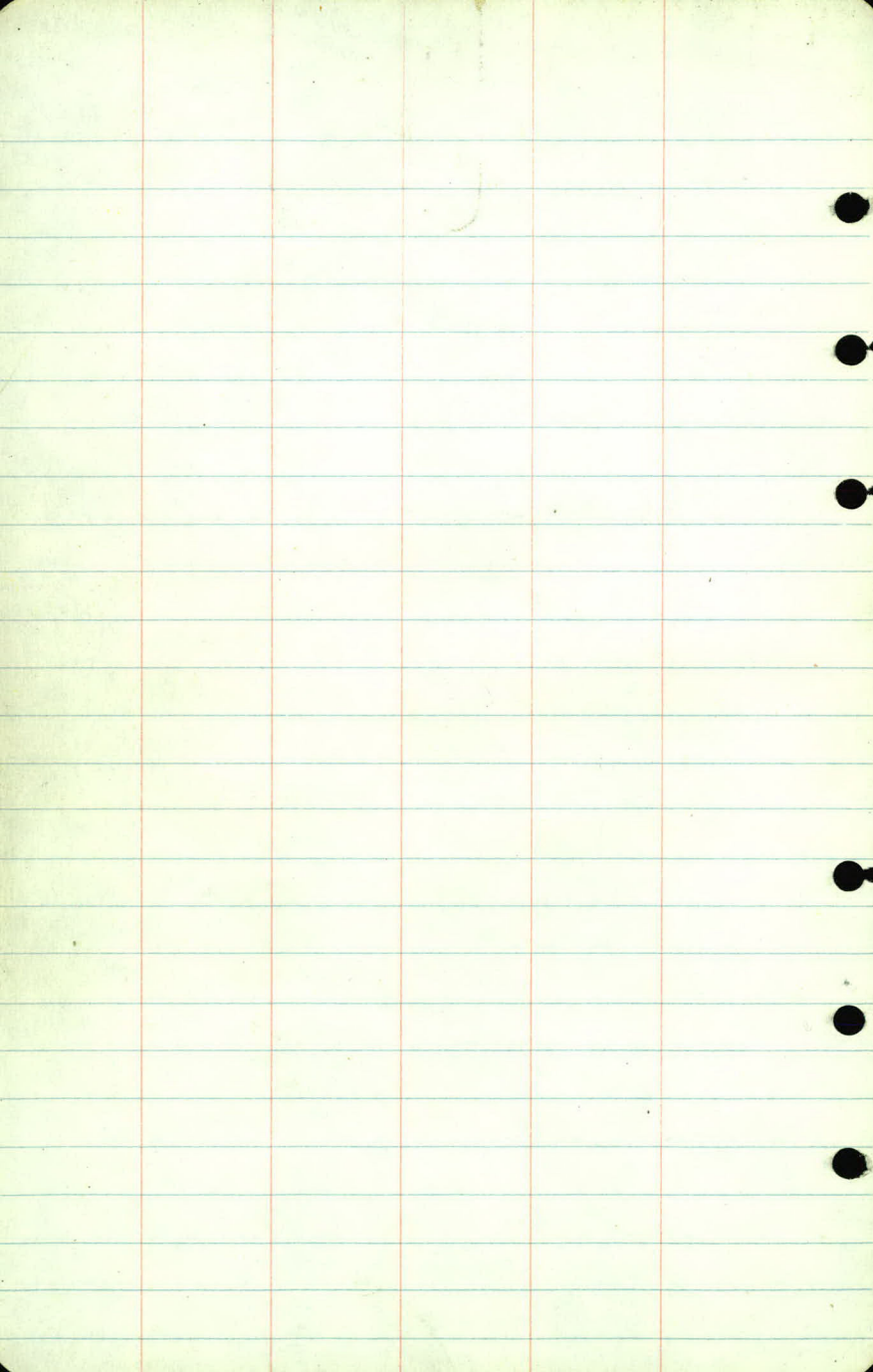
K.A.

Description

SpK in 12" Ash, 39' Rt Sta 10+05

Top Drill Sta 0+00 & Victoria & Carpentier Av

1



X. sections

Victoria Str

1-19-42

Sta	+	Δ	-	Elev
B.M	4.45	938.09		933.64

0+00

+10

+20

+25

+33

+50

1+00

+50

2

+50

3

+50

Lt

L

Rt.

Top Drill Hole & Victoria & Larpenbourg Ave.

$$\frac{3.32}{50}$$

$$4.45$$

$$\frac{5.25}{50}$$

$$\frac{3.49}{50}$$

$$4.68$$

$$\frac{5.98}{50}$$

$$\frac{3.8}{50}$$

$$\frac{4.2}{20}$$

$$4.3$$

$$\frac{5.2}{25}$$

$$\frac{6.2}{50}$$

$$\frac{4.8}{50}$$

$$\frac{5.1}{28}$$

$$\frac{4.4}{25}$$

$$4.4$$

$$\frac{5.7}{30}$$

$$\frac{6.5}{50}$$

$$\frac{4.8}{50}$$

$$\frac{5.4}{22}$$

$$\frac{4.5}{17}$$

$$4.4$$

$$\frac{4.9}{14}$$

$$\frac{6.0}{28}$$

$$\frac{5.5}{33}$$

$$\frac{5.4}{50}$$

$$\frac{4.7}{50}$$

$$\frac{5.7}{19}$$

$$\frac{4.7}{14}$$

$$4.6$$

$$\frac{5.2}{15}$$

$$\frac{6.0}{19}$$

$$\frac{5.7}{32}$$

$$\frac{5.3}{50}$$

$$\frac{4.6}{50}$$

$$\frac{5.1}{33}$$

$$\frac{6.2}{19}$$

$$\frac{5.2}{14}$$

$$5.0$$

$$\frac{5.2}{12}$$

$$\frac{6.2}{17}$$

$$\frac{6.2}{31}$$

$$\frac{5.9}{50}$$

$$\frac{4.1}{50}$$

$$\frac{4.7}{32}$$

$$\frac{6.2}{17}$$

$$\frac{5.2}{12}$$

$$5.0$$

$$\frac{5.3}{13}$$

$$\frac{6.4}{17}$$

$$\frac{6.2}{31}$$

$$\frac{5.7}{50}$$

$$\frac{4.4}{50}$$

$$\frac{4.6}{32}$$

$$\frac{6.3}{20-17}$$

$$\frac{5.7}{15}$$

$$\frac{5.4}{10}$$

$$5.1$$

$$\frac{5.3}{12}$$

$$\frac{6.6}{17}$$

$$\frac{6.6}{21}$$

$$\frac{5.6}{32}$$

$$\frac{5.5}{50}$$

$$\frac{5.4}{50}$$

$$\frac{5.6}{31}$$

$$21-17$$

$$\frac{6.7}{14}$$

$$\frac{5.9}{10}$$

$$5.5$$

$$\frac{5.7}{11}$$

$$\frac{6.7}{17}$$

$$\frac{6.7}{21}$$

$$\frac{4.7}{33}$$

$$\frac{4.0}{50}$$

$$\frac{7.1}{50}$$

$$\frac{7.3}{31}$$

$$\frac{7.2}{21-18}$$

$$\frac{6.6}{15}$$

$$\frac{6.1}{10}$$

$$5.8$$

$$\frac{6.1}{10}$$

$$\frac{6.3}{13}$$

$$\frac{7.1}{17-19}$$

$$\frac{4.7}{32}$$

$$\frac{3.6}{50}$$

$$\frac{7.2}{50}$$

$$\frac{7.1}{31}$$

$$\frac{7.5}{21-18}$$

$$\frac{7.0}{15}$$

$$\frac{6.5}{10}$$

$$6.3$$

$$\frac{6.4}{9}$$

$$\frac{6.6}{13}$$

$$\frac{7.4}{17-20}$$

$$\frac{4.9}{33}$$

$$\frac{3.6}{50}$$

Sta	+	π	-	Elev
		938.09		

4+00

T.P.	6.37	937.16	730	930.79
------	------	--------	-----	--------

+50

+89

15" X Drain

5

+50

6

+50

7

+50

8

+50

9

Lt

Z

Rt

$$\frac{7.1}{50} \frac{7.3}{32} \frac{7.7}{21-18} \frac{7.0}{13} \frac{6.8}{10} 6.6 \frac{6.7}{9} \frac{6.9}{13} \frac{7.8}{18-20} \frac{5.8}{33} \frac{4.8}{50}$$

$$\frac{6.3}{50} \frac{6.3}{31} \frac{6.8}{21-17} \frac{6.2}{14} \frac{5.8}{10} 5.8 \frac{6.0}{8} \frac{6.1}{11} \frac{7.2}{17-20} \frac{6.4}{30} \frac{4.6}{50}$$

$$\frac{6.2}{50} \frac{6.5}{33} \frac{6.6}{23-} \overset{\text{Inv.}}{\frac{7.1}{18} \frac{7.35}{18} \frac{6.0}{14} 5.7} \frac{5.9}{9} \frac{6.2}{14} \overset{\text{Inv.}}{\frac{7.3}{16} \frac{7.75}{16}} \frac{7.4}{26} \frac{6.4}{50}$$

$$\frac{6.1}{50} \frac{6.4}{13} \frac{6.8}{19} \frac{6.0}{14} \frac{5.7}{10} 5.7 \frac{5.8}{8} \frac{6.0}{14} \frac{7.0}{17-21} \frac{6.3}{33} \frac{6.8}{50}$$

$$\frac{5.9}{50} \frac{6.7}{41} \frac{6.2}{32} \frac{6.6}{18} \frac{5.8}{14} \frac{5.6}{9} 5.5 \frac{5.7}{8} \frac{6.0}{13} \frac{6.8}{16-19} \frac{4.7}{32} \frac{5.2}{50}$$

$$\frac{5.8}{50} \frac{6.1}{31} \frac{6.5}{18} \frac{5.7}{14} \frac{5.3}{10} 5.3 \frac{5.5}{8} \frac{5.7}{13} \frac{6.2}{17-21} \frac{3.7}{33} \frac{3.3}{50}$$

$$\frac{5.7}{50} \frac{6.0}{33} \frac{6.3}{17} \frac{5.4}{14} \frac{5.2}{18} 5.0 \frac{5.2}{8} \frac{5.3}{13} \frac{6.3}{17-21} \frac{3.8}{32} \frac{3.1}{50}$$

$$\frac{5.5}{50} \frac{5.9}{34} \frac{6.2}{18} \frac{5.1}{13} \frac{4.9}{9} 4.8 \frac{5.0}{9} \frac{5.2}{14} \frac{6.0}{17-21} \frac{4.3}{32} \frac{4.1}{50}$$

$$\frac{5.5}{50} \frac{5.9}{35} \frac{5.7}{17} \frac{4.6}{13} \frac{4.4}{9} 4.3 \frac{4.5}{9} \frac{4.8}{13} \frac{5.7}{18} \frac{5.5}{32} \frac{5.0}{50}$$

$$\frac{5.0}{50} \frac{5.1}{34} \frac{5.3}{18} \frac{4.3}{14} \frac{4.1}{9} 3.9 \frac{4.0}{9} \frac{4.1}{12} \frac{5.6}{18} \frac{5.5}{32} \frac{5.5}{50}$$

$$\frac{4.5}{50} \frac{4.7}{34} \frac{4.6}{18} \frac{3.6}{14} \frac{3.4}{9} 3.4 \frac{3.5}{9} \frac{3.7}{14} \frac{5.0}{18} \frac{5.2}{31} \frac{5.2}{50}$$

$$\frac{2.6}{50} \frac{3.0}{27} \frac{3.1}{21} \frac{3.6}{18} \frac{2.7}{13} \frac{2.5}{9} 2.3 \frac{2.6}{9} \frac{2.7}{13} \frac{4.1}{19} \frac{3.6}{33} \frac{3.3}{39} \frac{3.3}{50}$$

Sta	+	Δ	-	Elev
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937.16

9+50

T.P.	10.16	946.61	0.71	936.45
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10+00

B.M.	8.45	946.67	8.45	938.16	938.22
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+50

11

+50

12

+50

13

+50

T.P.	8.96	954.25	1.38	945.29
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14

+50

15

Lt

L

Rt

$\frac{1.4}{50}$ $\frac{1.7}{26}$ $\frac{2.5}{22-18}$ $\frac{1.6}{13}$ $\frac{1.4}{9}$ 1.2 $\frac{1.3}{9}$ $\frac{1.5}{13}$ $\frac{2.5}{17-20}$ $\frac{1.6}{29}$ $\frac{2.1}{50}$

$\frac{8.9}{50}$ $\frac{9.5}{28}$ $\frac{10.8}{19-17}$ $\frac{9.9}{14}$ $\frac{9.6}{10}$ 9.4 $\frac{9.5}{9}$ $\frac{9.8}{12}$ $\frac{10.7}{17-20}$ $\frac{9.6}{29}$ $\frac{10.6}{50}$

SPK 12" Ash 39' Rt Stg 10 + 05

$\frac{7.0}{50}$ $\frac{7.5}{29}$ $\frac{9.7}{20-17}$ $\frac{8.7}{13}$ $\frac{8.5}{10}$ 8.1 $\frac{8.3}{9}$ $\frac{8.6}{12}$ $\frac{9.5}{17-20}$ $\frac{8.6}{30}$ $\frac{9.6}{50}$

$\frac{5.6}{50}$ $\frac{6.2}{30}$ $\frac{8.4}{20-17}$ $\frac{7.5}{14}$ $\frac{7.2}{10}$ 7.0 $\frac{7.2}{9}$ $\frac{7.6}{13}$ $\frac{8.5}{17-20}$ $\frac{8.0}{30}$ $\frac{8.3}{50}$

$\frac{4.8}{50}$ $\frac{5.2}{31}$ $\frac{7.5}{19-17}$ $\frac{6.3}{13}$ $\frac{6.2}{10}$ 6.0 $\frac{6.2}{9}$ $\frac{6.4}{12}$ $\frac{7.3}{16-19}$ $\frac{7.0}{31}$ $\frac{7.0}{50}$

$\frac{4.0}{50}$ $\frac{4.4}{32}$ $\frac{6.4}{21-18}$ $\frac{5.7}{15}$ $\frac{5.4}{10}$ 5.2 $\frac{5.4}{9}$ $\frac{5.4}{12}$ $\frac{6.4}{17-20}$ $\frac{5.5}{32}$ $\frac{5.5}{50}$

$\frac{3.8}{50}$ $\frac{3.7}{32}$ $\frac{5.5}{21}$ $\frac{5.5}{18}$ $\frac{4.7}{15}$ $\frac{4.3}{10}$ 4.1 $\frac{4.3}{9}$ $\frac{4.6}{13}$ $\frac{5.3}{16-20}$ $\frac{4.2}{30}$ $\frac{3.7}{50}$

$\frac{3.2}{50}$ $\frac{3.2}{31}$ $\frac{4.4}{21}$ $\frac{4.4}{18}$ $\frac{3.5}{15}$ $\frac{3.2}{10}$ 3.0 $\frac{3.2}{9}$ $\frac{3.4}{13}$ $\frac{4.0}{17-20}$ $\frac{2.2}{32}$ $\frac{2.2}{50}$

$\frac{2.4}{50}$ $\frac{2.2}{30}$ $\frac{3.4}{21}$ $\frac{3.4}{18}$ $\frac{2.6}{15}$ $\frac{2.1}{10}$ 1.9 $\frac{2.0}{9}$ $\frac{2.2}{13}$ $\frac{3.1}{16-19}$ $\frac{0.6}{33}$ $\frac{0.0}{50}$

$\frac{9.1}{50}$ $\frac{8.5}{29}$ $\frac{9.8}{21}$ $\frac{7.8}{18}$ $\frac{8.8}{14}$ $\frac{8.7}{10}$ 8.5 $\frac{8.6}{9}$ $\frac{8.9}{12}$ $\frac{9.6}{15-18}$ $\frac{8.7}{22}$ $\frac{5.5}{32}$ $\frac{4.8}{50}$

$\frac{10.7}{50}$ $\frac{9.4}{28}$ $\frac{9.2}{19}$ $\frac{8.0}{14}$ $\frac{7.7}{10}$ 7.6 $\frac{7.6}{9}$ $\frac{7.7}{12}$ $\frac{8.7}{16-19}$ $\frac{7.0}{24}$ $\frac{4.3}{33}$ $\frac{3.8}{50}$

$\frac{10.6}{50}$ $\frac{10.1}{39}$ $\frac{10.6}{33}$ $\frac{10.3}{28}$ $\frac{7.4}{15}$ $\frac{6.7}{10}$ 6.8 $\frac{7.0}{9}$ $\frac{7.2}{12}$ $\frac{7.8}{16-20}$ $\frac{6.2}{33}$ $\frac{4.1}{50}$

Sta + Δ - Elev

~~954.25~~

15+50

16

+50

17

T.P. 12.52 965.99 0.78 953.47

+50

18

+50

19

T.P. 12.10 976.21 1.88 964.11

+50

20

+50

21

B.M. 6.02 980.57 1.63 974.57 974.55

Lt

L

Rt

$$\frac{10.1}{50} \quad \frac{9.8}{29} \quad \frac{6.3}{15} \quad \frac{5.9}{10} \quad 5.7 \quad \frac{5.9}{8} \quad \frac{6.2}{12} \quad \frac{7.0}{16-19} \quad \frac{6.4}{29} \quad \frac{5.5}{34} \quad \frac{4.1}{50}$$

$$\frac{9.4}{50} \quad \frac{8.7}{28} \quad \frac{5.1}{15} \quad \frac{4.6}{10} \quad 4.3 \quad \frac{4.4}{8} \quad \frac{4.7}{11} \quad \frac{5.6}{16} \quad \frac{5.1}{22} \quad \frac{4.1}{34} \quad \frac{3.4}{50}$$

$$\frac{8.4}{50} \quad \frac{7.7}{32} \quad \frac{3.3}{16} \quad \frac{2.8}{11} \quad 2.5 \quad \frac{2.6}{9} \quad \frac{3.0}{13} \quad \frac{4.0}{17-20} \quad \frac{2.9}{33} \quad \frac{1.1}{50}$$

$$\frac{6.5}{50} \quad \frac{5.3}{29} \quad \frac{1.5}{15} \quad \frac{1.2}{11} \quad 0.8 \quad \frac{1.2}{12} \quad \frac{2.0}{16} \quad \frac{1.9}{26} \quad \frac{1.1}{32} \quad \frac{0.0}{50}$$

$$\frac{16.2}{50} \quad \frac{15.0}{30} \quad \frac{11.5}{14} \quad \frac{11.1}{10} \quad 10.8 \quad \frac{11.0}{9} \quad \frac{11.3}{13} \quad \frac{12.1}{18-21} \quad \frac{10.8}{36} \quad \frac{10.4}{50}$$

$$\frac{13.7}{50} \quad \frac{13.4}{34} \quad \frac{12.1}{26} \quad \frac{9.7}{16} \quad \frac{9.2}{10} \quad 9.0 \quad \frac{9.2}{9} \quad \frac{9.4}{13} \quad \frac{9.7}{17} \quad \frac{9.8}{26} \quad \frac{9.2}{34} \quad \frac{8.7}{50}$$

$$\frac{10.8}{50} \quad \frac{10.1}{36} \quad \frac{9.1}{25} \quad \frac{7.5}{16} \quad \frac{7.1}{10} \quad 7.0 \quad \frac{7.1}{9} \quad \frac{7.3}{13} \quad \frac{8.3}{17-20} \quad \frac{5.6}{32} \quad \frac{4.0}{50}$$

$$\frac{8.5}{50} \quad \frac{8.3}{39} \quad \frac{6.4}{23} \quad \frac{5.3}{15} \quad \frac{4.9}{10} \quad 4.6 \quad \frac{4.7}{9} \quad \frac{4.9}{14} \quad \frac{5.2}{16-19} \quad \frac{5.1}{21} \quad \frac{2.0}{32} \quad \frac{0.0}{50}$$

$$\frac{14.8}{50} \quad \frac{14.0}{31} \quad \frac{13.2}{18} \quad \frac{12.4}{14} \quad \frac{12.1}{10} \quad 11.8 \quad \frac{12.0}{9} \quad \frac{12.2}{13} \quad \frac{13.0}{16-21} \quad \frac{10.7}{27} \quad \frac{8.6}{32} \quad \frac{6.4}{50}$$

$$\frac{9.6}{50} \quad \frac{9.3}{28} \quad \frac{9.9}{21-17} \quad \frac{9.1}{14} \quad \frac{8.9}{10} \quad 8.6 \quad \frac{8.8}{9} \quad \frac{9.2}{13} \quad \frac{9.7}{16-19} \quad \frac{6.2}{33} \quad \frac{5.0}{50}$$

$$\frac{4.6}{50} \quad \frac{4.9}{33} \quad \frac{7.3}{20-18} \quad \frac{6.4}{14} \quad \frac{5.9}{10} \quad 5.8 \quad \frac{6.0}{9} \quad \frac{6.3}{11} \quad \frac{6.9}{15-19} \quad \frac{3.7}{27} \quad \frac{2.5}{32} \quad \frac{2.2}{50}$$

$$\frac{3.5}{50} \quad \frac{4.3}{27} \quad \frac{4.8}{21-18} \quad \frac{3.6}{10} \quad 3.3 \quad \frac{3.5}{9} \quad \frac{4.2}{15-18} \quad \frac{+0.8}{32} \quad \frac{+0.8}{50}$$

Top S.E. Cor Conc. Walk 32' Lt Sta 21+60

Sta + Δ - Elev

980.57

21+50

22

+50

23

+50

24

+50

25

+50

T.P. 4.49 976.02 7.04 971.53

26

+50

27

L+

A

R+

$$\frac{5.8}{50} \frac{6.4}{33} \frac{7.1}{27} \frac{7.3}{20} \frac{7.0}{15} \frac{6.3}{10} 6.1 \frac{6.3}{9} \frac{6.7}{12} \frac{6.9}{15-17} \frac{6.5}{19} \frac{4.2}{25} \frac{1.4}{33} \frac{1.4}{50}$$

$$\frac{5.7}{50} \frac{6.6}{32} \frac{6.7}{24} \frac{6.6}{19} \frac{5.7}{15} \frac{5.3}{10} 5.1 \frac{5.1}{9} \frac{5.4}{13} \frac{5.6}{16-18} \frac{4.0}{22} \frac{0.0}{33} \frac{+0.5}{50}$$

$$\frac{7.7}{50} \frac{6.2}{27} \frac{6.2}{20} \frac{5.2}{14} \frac{4.9}{10} 4.6 \frac{4.5}{9} \frac{4.7}{12} \frac{5.4}{16-19} \frac{2.8}{26} \frac{0.0}{33} \frac{+2.7}{50}$$

$$\frac{8.2}{50} \frac{7.8}{33} \frac{7.0}{29} \frac{6.7}{22} \frac{5.1}{13} \frac{5.0}{10} 4.8 \frac{4.9}{9} \frac{5.0}{11} \frac{6.1}{15-18} \frac{1.0}{32} \frac{+1.5}{50}$$

$$\frac{6.7}{50} \frac{6.6}{22} \frac{5.5}{15} \frac{5.3}{10} 5.0 \frac{5.2}{9} \frac{5.3}{12} \frac{6.4}{15-18} \frac{1.5}{32} \frac{10.7}{50}$$

$$\frac{5.7}{50} \frac{6.0}{34} \frac{7.0}{25} \frac{7.1}{20} \frac{6.0}{15} \frac{5.8}{10} 5.6 \frac{5.7}{9} \frac{6.0}{12} \frac{6.7}{15-18} \frac{2.8}{32} \frac{1.0}{50}$$

$$\frac{7.2}{50} \frac{7.1}{31} \frac{7.5}{21} \frac{7.5}{17} \frac{6.7}{15} \frac{6.4}{12} 6.2 \frac{6.3}{8} \frac{6.5}{12} \frac{7.4}{15-18} \frac{3.8}{32} \frac{2.4}{50}$$

$$\frac{7.6}{50} \frac{7.5}{32} \frac{8.0}{23-20} \frac{7.3}{17} \frac{7.0}{14} 6.7 \frac{6.8}{9} \frac{7.0}{12} \frac{8.0}{15-19} \frac{4.8}{31} \frac{3.3}{50}$$

$$\frac{8.8}{50} \frac{8.3}{27} \frac{8.6}{23-20} \frac{8.1}{18} \frac{7.9}{15} 7.5 \frac{7.9}{9} \frac{8.0}{12} \frac{8.9}{16-19} \frac{5.4}{31} \frac{4.9}{50}$$

2 Roselawm

$$\frac{8.2}{100} \frac{3.7}{50} \frac{3.7}{20} 4.4 \frac{5.1}{8} \frac{5.2}{11} \frac{5.8}{14-16} \frac{3.6}{25} \frac{2.6}{50}$$

$$\frac{4.9}{50} \frac{4.1}{31} \frac{4.2}{8} 4.7 \frac{5.1}{11} \frac{5.3}{14} \frac{6.8}{19-24} \frac{5.5}{28} \frac{4.6}{50}$$

$$\frac{6.6}{46} \frac{7.4}{42} \frac{7.4}{34} \frac{5.2}{27} \frac{5.0}{21} \frac{3.8}{15} \frac{3.9}{8} 4.3 \frac{4.8}{10} \frac{4.9}{22} \frac{6.3}{27-30} \frac{4.7}{32} \frac{5.0}{50}$$

Sta	+	π	-	Elev
		976.02		

27+50

28

+16 15" X Drain

+50

29

T.P.	1332	984.35	5.00	971.02
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+50

30

+50

31

T.P.	16.54	987.56	1332	971.02
------	-------	--------	------	--------

+50

32

+56

Lt

2

Rt

$$\frac{12.1}{50} \quad \frac{10.0}{38} \quad \frac{7.8}{26} \quad \frac{4.5}{17} \quad \frac{4.1}{7} \quad 4.7 \quad \frac{5.6}{17} \quad \frac{6.9}{22-27} \quad \frac{3.4}{35} \quad \frac{3.5}{44} \quad \frac{4.1}{45} \quad \frac{4.1}{50}$$

$$\frac{19.4}{50} \quad \frac{14.3}{32} \quad \frac{6.2}{18} \quad \frac{5.4}{8} \quad 5.4 \quad \frac{6.0}{11} \quad \frac{7.3}{15} \quad \frac{7.4}{24} \quad \frac{6.0}{30} \quad \frac{3.8}{50}$$

$$\begin{array}{c} \text{Inv} \\ \frac{19.4}{50} \quad \frac{16.1}{36} \quad \frac{15.2}{30} \quad \frac{14.5}{29} \quad \frac{6.6}{18} \quad \frac{5.7}{13} \quad 5.7 \end{array} \quad \begin{array}{c} \text{Inv} \\ \frac{6.0}{10} \quad \frac{8.2}{15} \quad \frac{8.2}{16} \quad \frac{7.6}{21} \quad \frac{5.7}{34} \quad \frac{4.0}{50} \end{array}$$

$$\frac{18.7}{50} \quad \frac{13.2}{30} \quad \frac{6.0}{12} \quad \frac{5.8}{9} \quad 5.5 \quad \frac{5.8}{10} \quad \frac{6.0}{13} \quad \frac{7.3}{16-21} \quad \frac{3.7}{30} \quad \frac{2.6}{50}$$

$$\frac{13.4}{50} \quad \frac{10.7}{35} \quad \frac{9.5}{24} \quad \frac{8.7}{19} \quad \frac{5.6}{12} \quad \frac{5.4}{8} \quad 5.1 \quad \frac{5.5}{10} \quad \frac{5.7}{13} \quad \frac{6.5}{17-22} \quad \frac{5.0}{25} \quad \frac{0.7}{31} \quad \frac{2.4}{50}$$

$$\frac{18.8}{50} \quad \frac{15.9}{20} \quad \frac{14.2}{15} \quad \frac{13.6}{10} \quad 13.1 \quad \frac{13.2}{12} \quad \frac{13.3}{14} \quad \frac{14.3}{17-21} \quad \frac{7.3}{33} \quad \frac{3.8}{50}$$

$$\frac{19.2}{50} \quad \frac{16.1}{21} \quad \frac{14.0}{15} \quad \frac{13.6}{11} \quad 12.9 \quad \frac{13.0}{10} \quad \frac{13.2}{14} \quad \frac{14.1}{18-21} \quad \frac{5.7}{33} \quad \frac{2.3}{50}$$

$$\frac{18.9}{50} \quad \frac{15.4}{19} \quad \frac{13.6}{13} \quad \frac{13.2}{10} \quad 12.7 \quad \frac{12.9}{10} \quad \frac{13.3}{15} \quad \frac{14.2}{18-22} \quad \frac{7.1}{32} \quad \frac{3.8}{50}$$

$$\frac{18.4}{50} \quad \frac{16.1}{21} \quad \frac{13.6}{14} \quad \frac{13.1}{11} \quad 12.6 \quad \frac{13.0}{11} \quad \frac{13.4}{15} \quad \frac{14.0}{19-23} \quad \frac{7.8}{32} \quad \frac{4.6}{31}$$

$$15.6 \quad \frac{16.1}{12} \quad \frac{16.2}{16} \quad \frac{16.3}{19-23} \quad \frac{10.1}{33} \quad \frac{8.0}{50}$$

$$\frac{6.7}{34} \quad \frac{4.7}{43} \quad \frac{3.5}{50}$$

$$\frac{6.2}{32} \quad \frac{4.4}{43} \quad \frac{3.4}{50}$$

Sta + Δ - Elev

987.56

33

+50

T.P 5.75 976.76 16.54 971.02

31+50

32

+50

33

+50

+64

B.M 5.73 978.00 4.50 976.26 972.27

34

+32

+50

+71

Lt

E

Rt

$$\frac{10.2}{37} \quad \frac{8.2}{47} \quad \frac{8.0}{50}$$

$$\frac{11.7}{60} \quad \frac{10.5}{70}$$

$$\frac{10.0}{50} \quad \frac{7.4}{21} \quad \frac{5.7}{14} \quad \frac{5.4}{10}$$

$$\frac{7.2}{50} \quad \frac{5.3}{31} \quad \frac{6.1}{28} \quad \frac{5.8}{17} \quad \frac{5.3}{11} \quad 4.7 \quad \frac{5.0}{12} \quad \frac{5.2}{16} \quad \frac{5.4}{18.2}$$

$$\frac{5.4}{50} \quad \frac{2.8}{26} \quad \frac{5.1}{23} \quad \frac{5.6}{18} \quad \frac{5.3}{11} \quad 4.8 \quad \frac{5.1}{12} \quad \frac{5.2}{15} \quad \frac{5.1}{18.2}$$

$$\frac{7.8}{50} \quad \frac{5.5}{36} \quad \frac{4.5}{23} \quad \frac{5.1}{21} \quad \frac{6.2}{14} \quad \frac{5.7}{6} \quad 5.3 \quad \frac{5.3}{20} \quad \frac{5.7}{24-28}$$

$$\frac{9.1}{50} \quad \frac{6.9}{25} \quad \frac{5.7}{7} \quad 7.6 \quad \frac{7.0}{15} \quad \frac{6.5}{28} \quad \frac{6.7}{39} \quad \frac{6.9}{42} \quad \frac{7.4}{51-53}$$

$$\frac{9.4}{50} \quad \frac{6.8}{20} \quad 5.4 \quad \frac{8.0}{5-8} \quad \frac{7.8}{9} \quad \frac{7.6}{22} \quad \frac{7.1}{36} \quad \frac{7.3}{50} \quad \frac{7.8}{60}$$

SpK in 12" Oak 5.E Cur Rt Sta 34+50

$$\frac{7.6}{50} \quad \frac{7.6}{23} \quad 6.3 \quad \frac{5.8}{6} \quad \frac{12.6}{17} \quad \frac{11.6}{25} \quad \frac{11.9}{35} \quad \frac{10.3}{50} \quad \frac{10.1}{73}$$

$$\frac{7.6}{50} \quad \frac{5.6}{26} \quad 4.1 \quad \frac{13.3}{19} \quad \frac{13.5}{37} \quad \frac{12.5}{50} \quad \frac{12.8}{72}$$

$$\frac{6.1}{50} \quad \frac{4.8}{29} \quad \frac{4.1}{9} \quad 9.4 \quad \frac{14.6}{8} \quad \frac{14.4}{28} \quad \frac{13.6}{41} \quad \frac{13.9}{50} \quad \frac{14.2}{57-59} \quad \frac{13.4}{61}$$

$$\frac{5.6}{50} \quad \frac{4.9}{15} \quad 16.1 \quad \frac{15.7}{13} \quad \frac{15.4}{20} \quad \frac{15.0}{30} \quad \frac{15.7}{42} \quad \frac{16.0}{50}$$

$$\frac{7.3}{79}$$

Sta	+	π	-	Elev
		978.03		
35				
+50				
B.M.	0.43	972.70	5.73	972.27
35				
	4.96	966.41	11.25	961.45
+50				
36				
+12				
+21				
T.P.	3.27	956.84	12.84	953.57
+37				
+42				
+50				
37				
T.P.	3.07	948.88	11.03	945.81
+50				

Lt

L

Rt

95

$$\frac{48}{63} \quad \frac{5.6}{50} \quad \frac{7.1}{37} \quad \frac{73}{26}$$

$$\frac{13.5}{70} \quad \frac{11.9}{60} \quad \frac{11.6}{50} \quad \frac{11.7}{34}$$

$$\frac{11.9}{11} \quad 120$$

$$\frac{11.6}{8}$$

L Rd

$$\frac{11.3}{18}$$

$$\frac{11.7}{29}$$

$$\frac{12.2}{36-39}$$

$$\frac{7.5}{47}$$

$$\frac{3.9}{56}$$

$$\frac{9.3}{22}$$

$$\frac{8.6}{13}$$

$$\frac{8.9}{11-9}$$

$$\frac{8.5}{4}$$

$$82$$

$$\frac{8.3}{17}$$

$$\frac{8.3}{21}$$

$$\frac{9.1}{24-26}$$

$$\frac{3.8}{39}$$

$$\frac{3.8}{50}$$

$$\frac{7.1}{50} \quad \frac{6.4}{32}$$

$$\frac{12.2}{24}$$

$$\frac{12.0}{11}$$

$$\frac{11.8}{6}$$

$$113$$

$$\frac{11.6}{12}$$

$$\frac{12.2}{20}$$

$$\frac{12.8}{22-25}$$

$$\frac{6.2}{36}$$

$$\frac{6.1}{50}$$

$$\frac{10.9}{50} \quad \frac{9.6}{32}$$

$$\frac{13.1}{28}$$

$$\frac{12.8}{14}$$

$$\frac{12.6}{6}$$

$$120$$

$$\frac{12.2}{13}$$

$$\frac{12.8}{20}$$

$$\frac{13.5}{22-24}$$

$$\frac{7.6}{34}$$

$$\frac{7.6}{50}$$

$$\frac{14.1}{50} \quad \frac{13.6}{45}$$

$$\frac{15.4}{43}$$

$$\frac{14.4}{29}$$

$$\frac{13.2}{7}$$

$$12.6$$

$$\frac{12.9}{13}$$

$$\frac{13.4}{20}$$

$$\frac{13.9}{22-24}$$

$$\frac{8.6}{33}$$

$$\frac{8.4}{50}$$

$$\frac{7.3}{50}$$

$$\frac{6.1}{40}$$

$$\frac{5.0}{19}$$

$$\frac{4.5}{7}$$

$$40$$

$$\frac{4.4}{12}$$

$$\frac{4.6}{20}$$

$$\frac{5.1}{22-25}$$

$$\frac{2.5}{30}$$

$$\frac{1.7}{50}$$

$$\frac{9.9}{50}$$

$$\frac{8.3}{34}$$

$$\frac{6.5}{23}$$

$$\frac{5.4}{19}$$

$$\frac{4.8}{10}$$

$$43$$

$$\frac{4.7}{13}$$

$$\frac{4.9}{20}$$

$$\frac{5.3}{22-26}$$

$$\frac{3.7}{28}$$

$$\frac{3.4}{33}$$

$$\frac{3.2}{41}$$

$$\frac{11.9}{50}$$

$$\frac{8.7}{26}$$

$$\frac{6.6}{20}$$

$$\frac{5.3}{14}$$

$$\frac{5.2}{7}$$

$$47$$

$$\frac{5.1}{12}$$

$$\frac{5.1}{21}$$

$$\frac{5.8}{22-25}$$

$$\frac{5.1}{26}$$

$$\frac{4.9}{36}$$

$$\frac{3.7}{50}$$

$$\frac{17.2}{50}$$

$$\frac{15.5}{34}$$

$$\frac{13.1}{26}$$

$$\frac{9.7}{19}$$

$$\frac{8.5}{13}$$

$$77$$

$$\frac{8.0}{12}$$

$$\frac{8.5}{19}$$

$$\frac{10.0}{23}$$

$$\frac{10.5}{37}$$

$$\frac{11.6}{37}$$

$$\frac{12.2}{50}$$

$$\frac{12.0}{50}$$

$$\frac{11.0}{34}$$

$$\frac{6.7}{23}$$

$$\frac{3.4}{14}$$

$$\frac{2.8}{9}$$

$$2.2$$

$$\frac{2.5}{11}$$

$$\frac{2.7}{15}$$

$$\frac{8.1}{28}$$

$$\frac{8.2}{50}$$

Sta	+	Δ	-	Elev
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		948.88		
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38				
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+50				
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39				
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+50				
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40				
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+50				
-----	--	--	--	--

+92				
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41				
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T.P.	632	950.02	5.22	943.66
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+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

42				
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+50				
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LT

Z

RT

$$\frac{13.2}{50} \quad \frac{13.2}{31} \quad \frac{6.0}{17} \quad \frac{4.7}{9}$$

$$42 \quad \frac{4.5}{11} \quad \frac{5.3}{17} \quad \frac{11.6}{26} \quad \frac{12.1}{50}$$

$$\frac{13.3}{50} \quad \frac{12.7}{24} \quad \frac{6.4}{13} \quad \frac{6.0}{9} \quad 5.4 \quad \frac{5.8}{11} \quad \frac{6.4}{16} \quad \frac{11.8}{24} \quad \frac{12.4}{33} \quad \frac{11.2}{43} \quad \frac{10.6}{50}$$

$$\frac{13.2}{50} \quad \frac{13.1}{24} \quad \frac{7.5}{14} \quad \frac{6.6}{9} \quad 6.1 \quad \frac{6.4}{11} \quad \frac{7.0}{16} \quad \frac{11.8}{22} \quad \frac{12.2}{28} \quad \frac{10.7}{33} \quad \frac{10.4}{50}$$

$$\frac{13.2}{50} \quad \frac{13.3}{24} \quad \frac{7.4}{12} \quad \frac{6.7}{9} \quad 6.4 \quad \frac{7.0}{10} \quad \frac{7.1}{14} \quad \frac{11.6}{22} \quad \frac{10.4}{33} \quad \frac{10.4}{50}$$

$$\frac{13.3}{50} \quad \frac{13.0}{24} \quad \frac{7.4}{13} \quad \frac{7.1}{9} \quad 6.5 \quad \frac{7.0}{10} \quad \frac{7.2}{15} \quad \frac{10.8}{22} \quad \frac{12.2}{31} \quad \frac{10.6}{50}$$

$$\frac{13.3}{50} \quad \frac{13.0}{23} \quad \frac{7.1}{13} \quad \frac{6.7}{9} \quad 5.9 \quad \frac{6.4}{10} \quad \frac{7.9}{14} \quad \frac{11.6}{21} \quad \frac{12.7}{32} \quad \frac{10.5}{50}$$

$$\frac{11.4}{50} \quad \frac{11.2}{24} \quad \frac{6.4}{13} \quad \frac{5.8}{9} \quad 5.3 \quad \frac{5.6}{11} \quad \frac{6.5}{20} \quad \frac{9.7}{26} \quad \frac{10.2}{34} \quad \frac{10.2}{50}$$

$$\frac{10.8}{50} \quad \frac{9.8}{23} \quad \frac{6.4}{15} \quad \frac{5.7}{9} \quad 5.2 \quad \frac{5.4}{10} \quad \frac{6.1}{20} \quad \frac{8.2}{24} \quad \frac{8.4}{33} \quad \frac{6.6}{50}$$

$$\frac{2.9}{50} \quad \frac{3.8}{31} \quad \frac{7.6}{22} \quad \frac{6.7}{16} \quad \frac{6.3}{8} \quad 5.8 \quad \frac{6.2}{11} \quad \frac{6.4}{21} \quad \frac{7.8}{23} \quad \frac{7.3}{28} \quad \frac{1.8}{37} \quad \frac{2.3}{50}$$

$$\frac{0.7}{50} \quad \frac{0.6}{35} \quad \frac{7.1}{25} \quad \frac{7.2}{20} \quad \frac{6.3}{13} \quad \frac{6.0}{8} \quad 5.6 \quad \frac{6.0}{12} \quad \frac{6.4}{20} \quad \frac{7.0}{22-25} \quad \frac{0.3}{38} \quad \frac{0.3}{50}$$

$$\frac{4.0}{50} \quad \frac{3.0}{31} \quad \frac{6.9}{23} \quad \frac{6.7}{18} \quad \frac{6.0}{11} \quad \frac{5.7}{7} \quad 5.5 \quad \frac{6.0}{12} \quad \frac{6.2}{20} \quad \frac{6.8}{22-25} \quad \frac{2.1}{33} \quad \frac{2.5}{50}$$

$$\frac{10.8}{50} \quad \frac{11.0}{31} \quad \frac{6.7}{17} \quad \frac{6.2}{7} \quad 5.8 \quad \frac{6.2}{11} \quad \frac{6.7}{19} \quad \frac{10.4}{29} \quad \frac{10.9}{37} \quad \frac{9.7}{50}$$

Sta	+	Δ	-	Elev
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		950.02		
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42+80				
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43				
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+25				
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+50				
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+75				
-----	--	--	--	--

44				
----	--	--	--	--

+25				
-----	--	--	--	--

+60				
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45				
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T.P	2.78	952.12	0.68	949.34
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B.M	1.71	952.12	1.71	950.41	950.41
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	10.56	959.90	2.78	949.34
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+25				
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+50				
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Lt

Z

Rt

97

$$\frac{13.4}{50} \quad \frac{11.3}{31} \quad \frac{7.1}{17} \quad \frac{6.3}{7}$$

$$5.9 \quad \frac{6.0}{12} \quad \frac{6.5}{19} \quad \frac{11.3}{31} \quad \frac{11.5}{50}$$

$$\frac{12.8}{50} \quad \frac{11.5}{30} \quad \frac{7.0}{20} \quad \frac{6.4}{17} \quad \frac{6.1}{6}$$

$$5.8 \quad \frac{5.9}{12} \quad \frac{6.8}{20} \quad \frac{9.4}{27} \quad \frac{9.4}{33} \quad \frac{10.0}{50}$$

$$\frac{9.7}{50} \quad \frac{8.3}{35} \quad \frac{7.0}{27} \quad \frac{6.1}{18} \quad \frac{5.6}{7}$$

$$5.2 \quad \frac{5.4}{12} \quad \frac{5.9}{20} \quad \frac{6.9}{23} \quad \frac{7.0}{31} \quad \frac{6.3}{32} \quad \frac{6.4}{50}$$

$$\frac{3.0}{50} \quad \frac{2.1}{31} \quad \frac{5.3}{23} \quad \frac{4.9}{8}$$

$$4.5 \quad \frac{4.8}{12} \quad \frac{5.2}{20} \quad \frac{6.1}{23} \quad \frac{6.4}{28} \quad \frac{3.9}{33} \quad \frac{4.4}{50}$$

$$\frac{10.7}{50} \quad \frac{10.7}{35} \quad \frac{4.4}{25} \quad \frac{4.2}{8}$$

$$3.8 \quad \frac{4.1}{12} \quad \frac{4.5}{21} \quad \frac{5.7}{25} \quad \frac{4.1}{28} \quad \frac{4.6}{31} \quad \frac{5.3}{45} \quad \frac{5.3}{50}$$

$$\frac{1.5}{50} \quad \frac{2.0}{29} \quad \frac{4.5}{23} \quad \frac{3.6}{8}$$

$$3.2 \quad \frac{3.5}{12} \quad \frac{3.8}{20} \quad \frac{4.6}{23} \quad \frac{4.6}{29} \quad \frac{6.8}{37} \quad \frac{6.9}{50}$$

$$\frac{4.7}{50} \quad \frac{4.6}{33} \quad \frac{3.6}{21} \quad \frac{3.1}{11}$$

$$2.7 \quad \frac{3.0}{12} \quad \frac{3.1}{19} \quad \frac{3.7}{25} \quad \frac{6.9}{38} \quad \frac{6.9}{50}$$

$$\frac{5.5}{50} \quad \frac{5.3}{38} \quad \frac{3.1}{25} \quad \frac{2.3}{19} \quad \frac{2.2}{9}$$

$$1.7 \quad \frac{2.2}{19} \quad \frac{2.7}{22} \quad \frac{2.2}{28} \quad \frac{4.0}{35} \quad \frac{4.6}{50}$$

$$\frac{10.2}{50} \quad \frac{11.0}{39} \quad \frac{8.0}{32} \quad \frac{1.3}{28} \quad \frac{1.5}{20} \quad \frac{0.8}{8}$$

$$0.6 \quad \frac{1.2}{11} \quad \frac{1.6}{25} \quad \frac{12.0}{32} \quad \frac{12.0}{50}$$

Sp4 in 15" Oak 50' Lt Stg 44+00

$$\frac{2.7}{50} \quad \frac{3.0}{44} \quad \frac{6.4}{41} \quad \frac{11.5}{32} \quad \frac{11.1}{19} \quad \frac{10.7}{9}$$

$$10.2 \quad \frac{10.6}{11} \quad \frac{11.1}{23} \quad \frac{3.4}{41} \quad \frac{3.6}{50}$$

$$\frac{2.1}{60} \quad \frac{2.1}{55} \quad \frac{11.0}{45} \quad \frac{13.1}{34} \quad \frac{12.9}{23} \quad \frac{11.2}{20} \quad \frac{10.7}{9}$$

$$10.4 \quad \frac{10.5}{11} \quad \frac{11.1}{23} \quad \frac{8.3}{31} \quad \frac{1.3}{45} \quad \frac{1.8}{50}$$

Sta	+	Δ	-	Elev
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959.90

45+90

46

+50

47

T.P.	4.01	953.35	10.5L	949.34
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+40

+42

48

+11

+16

+50

T.P.	2.77	943.10	13.02	940.33
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49

+22

L+

X

R+

$\frac{6.8}{55}$	$\frac{10.3}{48}$	$\frac{12.4}{46}$	$\frac{12.8}{25}$	$\frac{11.7}{19}$	$\frac{11.5}{10}$	11.1	$\frac{11.5}{11}$	$\frac{11.5}{22}$	$\frac{9.7}{30}$	$\frac{1.6}{45}$	$\frac{2.0}{50}$
$\frac{1.6}{5.9}$											
$\frac{2.0}{9.4}$	$\frac{13.7}{32}$	$\frac{14.2}{27}$	$\frac{12.0}{25}$	$\frac{11.8}{9}$	11.4	$\frac{11.7}{11}$	$\frac{11.7}{23}$	$\frac{7.9}{33}$	$\frac{1.9}{45}$	$\frac{2.0}{50}$	
$\frac{4.4}{50}$	$\frac{4.7}{42}$	$\frac{13.9}{32}$	$\frac{12.5}{26}$	$\frac{13.2}{22}$	$\frac{13.0}{9}$	12.7	$\frac{13.0}{10}$	$\frac{13.1}{21}$	$\frac{12.1}{27}$	$\frac{5.7}{41}$	$\frac{6.0}{50}$
$\frac{9.3}{50}$	$\frac{8.9}{35}$	$\frac{14.7}{25}$	$\frac{14.8}{21}$	$\frac{14.2}{9}$	13.9	$\frac{14.5}{11}$	$\frac{14.7}{22}$	$\frac{13.8}{26}$	$\frac{9.0}{37}$	$\frac{9.1}{50}$	
$\frac{2.4}{50}$	$\frac{2.8}{40}$	$\frac{6.5}{34}$	$\frac{6.6}{30}$	$\frac{9.0}{23}$	$\frac{8.4}{9}$	8.3	$\frac{8.9}{10}$	$\frac{8.9}{23}$	$\frac{3.5}{36}$	$\frac{3.5}{50}$	
$\frac{5.3}{50}$	$\frac{6.7}{29}$	$\frac{8.7}{24}$	$\frac{8.6}{10}$			8.4	$\frac{8.9}{10}$	$\frac{9.2}{23}$	$\frac{3.6}{36}$	$\frac{3.3}{50}$	
$\frac{6.2}{50}$	$\frac{6.9}{39}$	$\frac{8.6}{28}$	$\frac{10.6}{15}$	$\frac{10.6}{8}$	10.3	$\frac{10.7}{10}$	$\frac{10.8}{22}$	$\frac{9.0}{29}$	$\frac{5.6}{35}$	$\frac{5.7}{50}$	
$\frac{6.8}{50}$	$\frac{7.2}{36}$	$\frac{9.0}{27}$	$\frac{10.2}{23}$	$\frac{10.5}{8}$	10.7	$\frac{11.1}{11}$	$\frac{11.2}{23}$	$\frac{9.5}{28}$	$\frac{6.1}{33}$	$\frac{6.5}{50}$	
$\frac{2.3}{50}$	$\frac{2.4}{43}$	$\frac{9.9}{33}$	$\frac{11.1}{8}$		10.9	$\frac{11.3}{10}$	$\frac{11.3}{18}$	$\frac{11.2}{25}$	$\frac{6.6}{33}$	$\frac{7.0}{50}$	
$\frac{7.3}{50}$	$\frac{7.4}{37}$	$\frac{12.5}{24-21}$	$\frac{12.2}{18}$	$\frac{12.3}{8}$	12.0	$\frac{12.4}{11}$	$\frac{12.5}{17}$	$\frac{12.9}{21-24}$	$\frac{9.3}{32}$	$\frac{11.1}{50}$	
$\frac{4.2}{50}$	$\frac{4.2}{27}$	$\frac{5.2}{22}$	$\frac{4.7}{18}$	$\frac{4.5}{7}$	4.1	$\frac{4.3}{10}$	$\frac{4.6}{20}$	$\frac{5.1}{21-24}$	$\frac{2.2}{31}$	$\frac{2.2}{50}$	
$\frac{5.7}{50}$	$\frac{5.2}{26}$	$\frac{6.1}{24-21}$	$\frac{5.7}{19}$	$\frac{5.6}{8}$	5.1	$\frac{5.4}{11}$	$\frac{5.7}{19}$	$\frac{6.3}{21-25}$	$\frac{1.4}{34}$	$\frac{1.1}{50}$	

Sta	+	π	-	Elev
		94310		

49+36

+60

+68

+75

+87.75 $\pm$ Parker

50

+07

+17

+50

51

T.P.	1.60	931.30	13.40	929.70
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+50

52

Lt.

Z

Rt

$$\frac{6.5}{50} \quad \frac{5.5}{28} \quad \frac{7.6}{24.21} \quad \frac{6.4}{19} \quad \frac{6.1}{8} \quad 57 \quad \frac{6.0}{10} \quad \frac{6.2}{16} \quad \frac{6.8}{24} \quad \frac{8.1}{50}$$

$$\frac{4.3}{50} \quad \frac{4.5}{32} \quad \frac{8.7}{26.22} \quad \frac{9.3}{20} \quad \frac{7.4}{16} \quad \frac{6.9}{4} \quad 6.9 \quad \frac{7.3}{10} \quad \frac{7.1}{18} \quad \frac{7.5}{21} \quad \frac{8.4}{25} \quad \frac{9.1}{50}$$

$$\frac{8.7}{50} \quad \frac{8.5}{33} \quad \frac{7.8}{26} \quad 7.2 \quad \frac{7.6}{11} \quad \frac{7.4}{19} \quad \frac{8.6}{27} \quad \frac{9.0}{50}$$

$$\frac{8.1}{50} \quad \frac{7.9}{38} \quad \frac{7.6}{16} \quad 7.5 \quad \frac{8.0}{12} \quad \frac{8.0}{30} \quad \frac{2.8}{37} \quad \frac{2.8}{50}$$

$$\frac{7.1}{100} \quad \frac{7.8}{50} \quad 8.0 \quad \frac{8.4}{10} \quad \frac{8.4}{24} \quad \frac{4.7}{34} \quad \frac{3.3}{50}$$

$$\frac{8.4}{50} \quad \frac{8.1}{27} \quad \frac{34.5}{8.6} \quad \frac{8.8}{10} \quad \frac{9.1}{23} \quad \frac{4.2}{37} \quad \frac{4.8}{50}$$

$$\frac{9.3}{50} \quad \frac{10.2}{33} \quad \frac{9.5}{25} \quad \frac{9.0}{8} \quad \frac{34.3}{8.8} \quad \frac{9.1}{10} \quad \frac{9.3}{24} \quad \frac{3.9}{37} \quad \frac{5.2}{50}$$

$$\frac{5.2}{50} \quad \frac{5.1}{36} \quad \frac{10.2}{24} \quad \frac{11.5}{22} \quad \frac{10.0}{19} \quad \frac{33.9}{9.2} \quad \frac{9.5}{10} \quad \frac{9.9}{24} \quad \frac{6.2}{34} \quad \frac{6.0}{50}$$

$$\frac{6.0}{50} \quad \frac{5.6}{40} \quad \frac{10.3}{28} \quad \frac{12.0}{22} \quad \frac{11.2}{8} \quad \frac{32.2}{10.9} \quad \frac{11.3}{10} \quad \frac{11.4}{19} \quad \frac{11.8}{21-25} \quad \frac{6.9}{36} \quad \frac{6.9}{50}$$

$$\frac{6.5}{50} \quad \frac{7.0}{36} \quad \frac{13.7}{19} \quad \frac{13.7}{8} \quad \frac{27.8}{13.3} \quad \frac{13.7}{10} \quad \frac{13.7}{17} \quad \frac{14.2}{20-26} \quad \frac{8.5}{36} \quad \frac{9.4}{50}$$

$$\frac{1.6}{50} \quad \frac{3.6}{36} \quad \frac{4.8}{21} \quad \frac{3.7}{10} \quad \frac{27.8}{3.6} \quad \frac{3.8}{9} \quad \frac{4.6}{19} \quad \frac{6.6}{26} \quad \frac{7.4}{50}$$

$$\frac{10.2}{50} \quad \frac{9.1}{32} \quad \frac{9.2}{21} \quad \frac{6.5}{14} \quad \frac{25.3}{6.0} \quad \frac{6.9}{17} \quad \frac{10.2}{26} \quad \frac{11.2}{50}$$

Sta	+	π	-	Elev
		931.30		
52+50				
TP				
53				
+50				
T.P.	3.58	923.56	11.32	919.98
54				
+50				
55				
+50				
56				
+20				
+35				
+50				
T.P.	9.93	933.28	0.21	923.35
56+35				

Lt

Z

Rt

$$\frac{140}{50} \quad \frac{138}{21} \quad \frac{88}{13} \quad \frac{23.3}{80} \quad \frac{89}{16} \quad \frac{12.7}{31} \quad \frac{12.6}{50}$$

$$\frac{186}{50} \quad \frac{123}{31} \quad \frac{151}{19} \quad \frac{107}{11} \quad \frac{21.4}{9.9} \quad \frac{110}{17} \quad \frac{13.4}{30} \quad \frac{15.8}{50}$$

$$\frac{211}{50} \quad \frac{207}{28} \quad \frac{190}{23} \quad \frac{121}{11} \quad \frac{17.7}{11.4} \quad \frac{12.5}{19} \quad \frac{19.4}{34} \quad \frac{19.5}{50}$$

$$\frac{136}{50} \quad \frac{127}{26} \quad \frac{64}{15} \quad \frac{53}{9} \quad \frac{19.0}{46} \quad \frac{50}{9} \quad \frac{5.7}{78} \quad \frac{12.0}{31} \quad \frac{12.8}{34} \quad \frac{13.3}{50}$$

$$\frac{140}{50} \quad \frac{132}{28} \quad \frac{117}{23} \quad \frac{6.0}{14} \quad \frac{5.4}{9} \quad \frac{18.7}{49} \quad \frac{5.3}{10} \quad \frac{5.9}{18} \quad \frac{11.7}{30} \quad \frac{14.0}{39} \quad \frac{14.1}{50}$$

$$\frac{140}{50} \quad \frac{132}{28} \quad \frac{5.7}{14} \quad \frac{5.0}{9} \quad \frac{19.0}{46} \quad \frac{50}{8} \quad \frac{5.5}{18} \quad \frac{12.4}{29} \quad \frac{13.9}{39} \quad \frac{13.8}{50}$$

$$\frac{13.4}{50} \quad \frac{12.1}{29} \quad \frac{4.5}{14} \quad \frac{3.9}{10} \quad \frac{20.4}{3.2} \quad \frac{3.4}{9} \quad \frac{3.6}{18} \quad \frac{6.4}{26} \quad \frac{7.8}{50}$$

$$\frac{11.2}{50} \quad \frac{10.3}{30} \quad \frac{1.8}{14} \quad \frac{1.5}{10} \quad \frac{22.7}{0.9} \quad \frac{6.3}{8} \quad \frac{1.5}{20} \quad \frac{5.1}{24} \quad \frac{5.8}{50}$$

$$\frac{9.1}{50} \quad \frac{7.6}{27} \quad \frac{6.1}{22} \quad \frac{0.6}{14} \quad \frac{0.5}{10} + 0.1 \quad \frac{0.2}{8} \quad \frac{1.2}{17} \quad \frac{3.7}{21} \quad \frac{4.8}{50}$$

$$\frac{8.4}{50} \quad \frac{5.9}{23}$$

$$\frac{5.9}{50} \quad \frac{3.2}{22}$$

$$\frac{9.6}{13} \quad \frac{9.4}{11} \quad 8.8 \quad \frac{9.2}{8} \quad \frac{9.4}{17} \quad \frac{12.2}{20} \quad \frac{7.5}{26} \quad \frac{7.7}{50}$$

Sta	+	∇	-	Elev	
		933.28			
56+50					
+68					
+80					
BM	4.50	937.58	0.03	933.25	933.28
57					
+21					
+50					
+72					
+81					
+89					
BM	5.52	938.80	4.56	933.28	
58+04.55					
+17					
+25					

Lt

2

Pt

$$\frac{8.9}{14} \quad \frac{8.7}{11} \quad \frac{25.2}{81} \quad \frac{8.5}{8} \quad \frac{8.4}{15} \quad \frac{11.2}{21} \quad \frac{7.6}{26} \quad \frac{7.6}{50}$$

$$\frac{11.5}{50} \quad \frac{9.2}{24} \quad \frac{9.5}{21} \quad \frac{8.0}{14} \quad \frac{7.8}{11} \quad \frac{21.0}{7.3} \quad \frac{7.7}{8} \quad \frac{7.9}{15} \quad \frac{8.3}{19-21} \quad \frac{7.4}{37}$$

$$\frac{9.4}{58} \quad \frac{8.2}{28} \quad \frac{7.4}{14} \quad 6.7 \quad \frac{7.3}{8} \quad \frac{6.9}{17} \quad \frac{7.8}{19-21} \quad \frac{2.2}{32} \quad \frac{0.9}{50}$$

Top Mon B + Victoria

$$\frac{10.5}{50} \quad \frac{9.4}{40} \quad \frac{11.3}{34} \quad \frac{11.0}{21} \quad \frac{10.8}{12} \quad \frac{27.5}{10.1} \quad \frac{10.5}{8} \quad \frac{10.1}{17} \quad \frac{10.7}{19-21} \quad \frac{2.7}{33} \quad \frac{1.5}{50}$$

$$\frac{8.0}{50} \quad \frac{6.7}{38} \quad \frac{11.9}{28} \quad \frac{11.4}{24} \quad \frac{10.2}{19} \quad \frac{9.8}{12} \quad 9.1 \quad \frac{9.4}{8} \quad \frac{9.1}{18} \quad \frac{9.7}{19-21} \quad \frac{0.8}{33} \quad \frac{0.5}{50}$$

$$\frac{6.4}{50} \quad \frac{8.0}{31} \quad \frac{9.6}{27-23} \quad \frac{8.3}{19} \quad \frac{8.0}{13} \quad 7.3 \quad \frac{7.6}{8} \quad \frac{7.7}{19} \quad \frac{8.4}{20-23} \quad \frac{1.2}{33} \quad \frac{1.4}{50}$$

$$\frac{6.1}{50} \quad \frac{6.7}{38} \quad \frac{8.3}{35} \quad \frac{8.3}{31} \quad \frac{7.1}{25} \quad \frac{6.6}{16} \quad 6.0 \quad \frac{6.0}{24} \quad \frac{7.3}{30-33} \quad \frac{1.5}{45} \quad \frac{1.4}{50}$$

$$\frac{6.3}{50} \quad \frac{6.7}{34} \quad \frac{5.8}{10} \quad 5.5 \quad \frac{5.6}{36} \quad \frac{6.0}{41} \quad \frac{5.7}{50}$$

$$\frac{6.5}{50} \quad \frac{5.8}{24} \quad 5.0 \quad \frac{4.9}{27} \quad \frac{4.9}{50}$$

Top Mon. B + Victoria

$$\frac{7.9}{100} \quad \frac{6.6}{50} \quad 5.5 \quad \frac{5.4}{50} \quad \frac{4.8}{100}$$

$$\frac{7.1}{50} \quad \frac{5.7}{15} \quad 5.5 \quad \frac{6.0}{28} \quad \frac{5.6}{50}$$

$$\frac{7.3}{50} \quad \frac{7.3}{38} \quad \frac{5.9}{14} \quad 5.6 \quad \frac{6.1}{18} \quad \frac{5.7}{25} \quad \frac{5.8}{50}$$

Sta	+	π	-	Elev
		938.80		

58 + 40

59

+50

60

+50

+77

+83

61

+60

62

+32

+43

L

X

R

$$\frac{5.0}{50} \quad \frac{4.8}{34} \quad \frac{7.0}{26} \quad \frac{7.0}{22} \quad \frac{6.0}{12} \quad \frac{5.9}{10} \quad \frac{5.7}{17} \quad \frac{4.2}{21} \quad \frac{3.5}{50}$$

$$\frac{3.3}{50} \quad \frac{3.7}{21} \quad \frac{5.8}{15-13} \quad \frac{5.2}{11} \quad \frac{5.4}{11} \quad \frac{4.0}{19} \quad \frac{3.1}{50}$$

$$\frac{3.3}{50} \quad \frac{3.8}{25} \quad \frac{5.2}{15} \quad 5.1 \quad \frac{5.2}{12} \quad \frac{3.6}{19} \quad \frac{2.8}{50}$$

$$\frac{3.0}{50} \quad \frac{3.9}{25} \quad \frac{5.1}{17} \quad 5.2 \quad \frac{5.3}{10} \quad \frac{5.2}{13} \quad \frac{3.6}{19} \quad \frac{2.6}{50}$$

$$\frac{3.7}{50} \quad \frac{4.0}{22} \quad \frac{5.0}{12} \quad \frac{5.2}{11} \quad 5.1 \quad \frac{5.3}{12} \quad \frac{3.5}{22} \quad \frac{2.6}{50}$$

$$\frac{3.8}{50} \quad \frac{3.9}{22} \quad \frac{5.4}{15} \quad 5.1 \quad \frac{5.4}{12} \quad \frac{3.7}{19} \quad \frac{2.4}{50}$$

$$\frac{4.4}{50} \quad \frac{5.1}{21} \quad \frac{5.4}{15} \quad 5.1 \quad \frac{5.4}{13} \quad \frac{4.1}{18} \quad \frac{2.7}{50}$$

$$\frac{4.7}{50} \quad \frac{5.5}{21} \quad \frac{5.6}{12} \quad 5.3 \quad \frac{5.6}{12} \quad \frac{4.0}{17} \quad \frac{2.5}{50}$$

$$\frac{5.5}{50} \quad \frac{5.4}{28} \quad \frac{7.0}{20-18} \quad \frac{6.2}{14} \quad 5.8 \quad \frac{6.0}{13} \quad \frac{4.2}{19} \quad \frac{2.9}{50}$$

$$\frac{4.3}{50} \quad \frac{4.6}{17} \quad \frac{6.7}{14} \quad 6.3 \quad \frac{6.6}{13} \quad \frac{5.4}{20} \quad \frac{4.0}{29} \quad \frac{3.2}{50}$$

$$\frac{8.7}{50} \quad \frac{8.0}{25} \quad \frac{8.2}{18} \quad \frac{7.1}{14} \quad \frac{6.9}{9} \quad 6.5 \quad \frac{7.0}{14} \quad \frac{6.0}{22} \quad \frac{4.4}{50}$$

$$\frac{11.0}{50} \quad \frac{9.9}{30} \quad \frac{8.6}{23} \quad \frac{8.7}{18} \quad \frac{7.2}{14} \quad 6.6 \quad \frac{7.0}{14} \quad \frac{6.1}{21} \quad \frac{4.5}{50}$$

Sta	+	π	-	Elev
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		938.80		
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63				
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	+50			
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T.P.	784	939.68	6.96	931.84
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64				
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	+50			
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65				
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	+43			
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	+54			
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66				
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	+50			
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67				
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	+50			
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68				
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L1

R

RT

$$\frac{13.6}{50} \quad \frac{12.3}{21} \quad \frac{7.4}{10} \quad 6.9 \quad \frac{7.2}{13} \quad \frac{8.2}{19} \quad \frac{7.1}{24} \quad \frac{6.2}{50}$$

$$\frac{13.4}{50} \quad \frac{12.7}{28} \quad \frac{11.6}{17} \quad \frac{7.6}{10} \quad 7.0 \quad \frac{7.2}{14} \quad \frac{8.5}{20-24} \quad \frac{7.0}{50}$$

$$\frac{13.8}{50} \quad \frac{12.5}{28} \quad \frac{11.2}{16} \quad \frac{8.0}{10} \quad 7.4 \quad \frac{7.8}{15} \quad \frac{8.7}{21} \quad \frac{8.0}{28} \quad \frac{7.3}{50}$$

$$\frac{12.5}{50} \quad \frac{11.3}{29} \quad \frac{9.8}{22} \quad \frac{9.6}{16} \quad \frac{7.6}{11} \quad 7.1 \quad \frac{7.3}{15} \quad \frac{7.7}{23} \quad \frac{6.7}{50}$$

$$\frac{10.3}{50} \quad \frac{8.8}{29} \quad \frac{8.2}{25} \quad \frac{8.4}{19-17} \quad \frac{6.7}{11} \quad 6.3 \quad \frac{6.6}{13} \quad \frac{6.5}{29} \quad \frac{6.3}{50}$$

$$\frac{8.3}{50} \quad \frac{7.2}{20} \quad \frac{7.8}{19-17} \quad \frac{5.9}{14} \quad 5.5 \quad \frac{5.6}{12} \quad \frac{6.0}{28} \quad \frac{7.0}{50}$$

$$\frac{5.8}{50} \quad \frac{5.6}{29} \quad \frac{7.8}{19-17} \quad \frac{5.6}{9} \quad 5.3 \quad \frac{5.5}{12} \quad \frac{5.7}{26} \quad \frac{7.2}{50}$$

$$\frac{5.0}{50} \quad \frac{4.9}{18} \quad \frac{5.2}{17-16} \quad \frac{5.0}{14} \quad \frac{4.8}{9} \quad 4.5 \quad \frac{4.6}{12} \quad \frac{4.9}{35} \quad \frac{5.5}{50}$$

$$\frac{4.1}{50} \quad \frac{3.7}{34} \quad \frac{3.0}{30} \quad \frac{3.2}{18} \quad \frac{4.2}{14} \quad 3.7 \quad \frac{3.9}{17} \quad \frac{2.7}{25} \quad \frac{2.7}{50}$$

$$\frac{3.9}{50} \quad \frac{3.3}{37} \quad \frac{2.6}{31} \quad \frac{2.6}{23} \quad \frac{3.5}{14} \quad 3.1 \quad \frac{3.3}{14} \quad \frac{2.2}{21} \quad \frac{2.2}{50}$$

$$\frac{1.7}{50} \quad \frac{2.0}{35} \quad \frac{3.0}{17} \quad 2.6 \quad \frac{2.9}{11} \quad \frac{3.1}{26} \quad \frac{3.8}{50}$$

$$\frac{2.1}{50} \quad \frac{2.5}{31} \quad \frac{2.6}{9} \quad 2.4 \quad \frac{2.8}{15} \quad \frac{2.7}{26} \quad \frac{3.8}{50}$$

Sta	+	π	-	Elev
		939.68		

68+50

T.P.	5.26	942.69	2.25	937.43
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69

2.7

+50

+62

70

+50

71

B.M	4.29	942.68	4.29	942.40	938.39
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+50

42.9

+70

Φ

STH. #36

72

+32

+50

Lt Rt

$\frac{2.2}{50}$ $\frac{2.3}{35}$ $\frac{3.0}{31}$ $\frac{3.1}{16}$ $\frac{2.4}{10}$ 20 $\frac{2.4}{19}$ $\frac{1.8}{26}$ $\frac{0.0}{31}$ $\frac{1.9}{36}$ $\frac{2.1}{43}$ $\frac{2.1}{50}$

$\frac{5.1}{50}$ $\frac{5.1}{36}$ $\frac{5.7}{30}$ $\frac{5.6}{14}$ 51 $\frac{5.4}{13}$ $\frac{4.8}{21}$ $\frac{2.2}{32}$ $\frac{2.4}{43}$ $\frac{4.0}{50}$

$\frac{4.9}{50}$ $\frac{5.4}{32}$ $\frac{5.5}{10}$ 5.1 $\frac{5.5}{14}$ $\frac{5.2}{18}$ $\frac{5.6}{26}$ $\frac{2.0}{35}$ $\frac{4.0}{50}$

Edge conc slab

$\frac{4.9}{50}$ $\frac{5.4}{32}$ $\frac{5.5}{10}$ 5.1 $\frac{5.4}{10}$ $\frac{5.9}{28}$ $\frac{7.9}{50}$

$\frac{4.9}{50}$ $\frac{5.4}{25}$ 4.9 $\frac{5.5}{14}$ $\frac{5.7}{30}$ $\frac{6.4}{50}$

$\frac{6.3}{50}$ $\frac{6.3}{36}$ $\frac{5.3}{26}$ $\frac{5.4}{10}$ 5.0 $\frac{5.2}{9}$ $\frac{5.6}{27}$ $\frac{6.6}{50}$

$\frac{6.6}{50}$ $\frac{6.1}{25}$ $\frac{5.6}{11}$ 5.2 $\frac{5.4}{12}$ $\frac{5.6}{23}$ $\frac{7.3}{50}$

Spk in P.P. 25' Rt. Sta 71+05

$\frac{5.2}{50}$ $\frac{4.8}{39}$ $\frac{5.9}{34}$ 5.1 $\frac{5.3}{50}$

$\frac{5.5}{100}$ $\frac{5.4}{50}$ 5.1 $\frac{4.9}{50}$ $\frac{4.8}{100}$

$\frac{5.7}{50}$ 5.3 $\frac{5.6}{22}$ $\frac{6.9}{50}$

$\frac{9.3}{50}$ $\frac{9.2}{28}$ $\frac{8.1}{19}$ $\frac{6.1}{12}$ 5.7 $\frac{5.9}{15}$ $\frac{7.2}{21}$ $\frac{8.0}{50}$

$\frac{9.5}{50}$ $\frac{8.7}{20}$ $\frac{6.0}{9}$ 5.8 $\frac{6.0}{15}$ $\frac{7.1}{20}$ $\frac{8.1}{50}$

Sta + π - Elev

942.68
42.7

73

+50

74

T.P. 3.62 942.17 413 938.55

+50

42.2

75

+50

76

+50

77

+50

78

+50

L1

R

R+

$$\frac{7.4}{50} \quad \frac{7.1}{16} \quad \frac{6.1}{11} \quad 5.5 \quad \frac{5.9}{14} \quad \frac{7.0}{20} \quad \frac{7.8}{50}$$

$$\frac{6.9}{50} \quad \frac{6.7}{22} \quad \frac{5.8}{12} \quad 5.5 \quad \frac{5.9}{11} \quad \frac{6.2}{23} \quad \frac{6.5}{50}$$

$$\frac{7.3}{50} \quad \frac{7.1}{17} \quad \frac{5.9}{12} \quad 5.5 \quad \frac{5.7}{13} \quad \frac{6.4}{27} \quad \frac{6.7}{50}$$

Top Row Marker

$$\frac{4.6}{50} \quad \frac{4.3}{31} \quad \frac{4.9}{21} \quad \frac{5.8}{16} \quad \frac{5.6}{10} \quad 5.1 \quad \frac{5.3}{10} \quad \frac{6.4}{19} \quad \frac{6.7}{50}$$

$$\frac{4.5}{50} \quad \frac{4.3}{26} \quad \frac{4.7}{21} \quad \frac{5.6}{17} \quad \frac{5.0}{9} \quad 4.9 \quad \frac{5.3}{10} \quad \frac{5.5}{14} \quad \frac{6.2}{19} \quad \frac{6.4}{50}$$

$$\frac{4.4}{50} \quad \frac{4.4}{34} \quad \frac{5.0}{21} \quad \frac{5.4}{17} \quad \frac{5.0}{9} \quad 4.7 \quad \frac{5.0}{10} \quad \frac{5.2}{14} \quad \frac{6.4}{21} \quad \frac{6.4}{50}$$

$$\frac{4.6}{50} \quad \frac{4.4}{33} \quad \frac{4.7}{11} \quad 4.6 \quad \frac{5.0}{12} \quad \frac{6.0}{19} \quad \frac{6.0}{50}$$

$$\frac{4.9}{50} \quad \frac{4.7}{29} \quad \frac{5.3}{20} \quad \frac{5.7}{17-15} \quad \frac{5.0}{11} \quad 4.6 \quad \frac{4.9}{11} \quad \frac{6.4}{20} \quad \frac{6.3}{50}$$

$$\frac{5.3}{50} \quad \frac{5.1}{24} \quad \frac{5.1}{10} \quad 4.9 \quad \frac{5.0}{12} \quad \frac{6.1}{19} \quad \frac{6.2}{50}$$

$$\frac{5.6}{50} \quad \frac{5.7}{19} \quad \frac{4.9}{12} \quad 4.8 \quad \frac{5.1}{12} \quad \frac{6.3}{20} \quad \frac{6.4}{50}$$

$$\frac{5.7}{50} \quad \frac{6.2}{17} \quad \frac{5.4}{12} \quad 5.0 \quad \frac{5.3}{13} \quad \frac{5.9}{21} \quad \frac{6.3}{50}$$

$$\frac{6.2}{50} \quad \frac{6.2}{17} \quad \frac{5.4}{12} \quad 4.9 \quad \frac{5.4}{15} \quad \frac{5.6}{26} \quad \frac{6.3}{50}$$

Sta	+	π	-	Elev
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		942.17		
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		42.2		
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79				
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+50				
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80				
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T.P.	5.27	942.66	4.78	937.39
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+50		42.7		
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81				
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+50				
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82				
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+50				
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83				
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+50				
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84				
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+10				
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	Lt			*	Rt			
$\frac{6.2}{30}$	$\frac{6.2}{16}$	$\frac{5.9}{12}$		37.4 4.8	$\frac{5.4}{15}$	$\frac{5.5}{27}$	$\frac{6.0}{30}$	$\frac{6.2}{50}$
	$\frac{5.9}{30}$	$\frac{5.8}{15}$	$\frac{5.0}{12}$	37.5 4.7	$\frac{5.1}{13}$	$\frac{5.3}{26}$	$\frac{5.9}{30}$	$\frac{6.1}{50}$
	$\frac{5.9}{50}$	$\frac{5.8}{16}$	$\frac{5.0}{12}$	37.5 4.7	$\frac{5.1}{19}$	$\frac{6.2}{30}$	$\frac{6.3}{50}$	
		$\frac{6.5}{50}$	$\frac{6.4}{15}$	$\frac{5.6}{12}$	37.5 5.2	$\frac{5.6}{14}$	$\frac{6.3}{26}$	$\frac{6.8}{30}$
	$\frac{5.5}{50}$	$\frac{5.8}{28}$	$\frac{5.6}{10}$	37.5 5.2	$\frac{5.4}{15}$	$\frac{5.9}{22}$	$\frac{6.7}{27}$	$\frac{6.2}{50}$
	$\frac{5.5}{50}$	$\frac{5.3}{27}$	$\frac{5.5}{14}$	37.6 5.1		$\frac{5.5}{28}$		$\frac{5.5}{50}$
	$\frac{4.6}{50}$	$\frac{4.7}{19}$	$\frac{5.3}{18}$	37.6 4.9	$\frac{5.3}{13}$	$\frac{5.5}{29}$	$\frac{5.3}{50}$	
	$\frac{3.3}{50}$	$\frac{4.1}{19}$	$\frac{5.1}{13}$	37.9 4.8	$\frac{5.1}{13}$	$\frac{4.9}{35}$	$\frac{5.1}{50}$	
	$\frac{4.0}{50}$	$\frac{3.4}{27}$	$\frac{3.5}{28}$	$\frac{5.2}{15}$	38.0 4.7	$\frac{5.1}{13}$	$\frac{4.6}{24}$	$\frac{4.3}{50}$
	$\frac{3.3}{50}$	$\frac{3.0}{33}$	$\frac{2.3}{20}$	$\frac{5.0}{14}$	37.9 4.8	$\frac{5.0}{16}$	$\frac{3.7}{31}$	$\frac{4.0}{50}$
	$\frac{3.2}{50}$	$\frac{2.3}{29}$	$\frac{2.2}{22}$	$\frac{5.1}{15}$	37.7 5.0	$\frac{5.3}{25}$	$\frac{4.1}{30}$	$\frac{3.5}{50}$
	$\frac{3.1}{50}$	$\frac{2.3}{29}$	$\frac{2.4}{22}$	$\frac{5.5}{14}$	37.7 5.0	$\frac{4.8}{14}$	$\frac{5.4}{29}$	$\frac{6.0}{31}$
								$\frac{5.6}{50}$

Sta + π - Elev

942.66

42.7

84+18

+35⁴⁰~~£ "B 2"~~

+50

+57

+64

+75

85

BM

430

941.71

5.27

937.39

937.41

+50

41.7

86

+56

87

+35

Lt

X

Rt

$$\frac{3.0}{50} \quad \frac{2.3}{29} \quad \frac{2.3}{22} \quad \frac{5.5}{15} \quad 5.1 \quad \frac{4.7}{18} \quad \frac{5.2}{38} \quad \frac{4.9}{50}$$

$$\frac{1.8}{50} \quad \frac{1.7}{31} \quad \frac{2.1}{23} \quad \frac{5.6}{15} \quad 5.3 \quad \frac{4.3}{50} \quad \frac{4.0}{50}$$

$$\frac{2.6}{30} \quad \frac{2.4}{29} \quad \frac{3.3}{21} \quad \frac{5.7}{15} \quad 5.6 \quad \frac{5.1}{24} \quad \frac{4.8}{50}$$

$$\frac{3.6}{50} \quad \frac{2.5}{25} \quad \frac{3.0}{21} \quad \frac{5.8}{16} \quad 5.8 \quad \frac{5.7}{30} \quad \frac{7.0}{32} \quad \frac{6.7}{50}$$

$$\frac{3.6}{50} \quad \frac{2.7}{24} \quad \frac{6.2}{14} \quad 6.0 \quad \frac{6.3}{23} \quad \frac{7.2}{25} \quad \frac{4.1}{28} \quad \frac{4.5}{34} \quad \frac{4.5}{50}$$

$$\frac{4.0}{50} \quad \frac{3.3}{38} \quad \frac{2.9}{23} \quad \frac{6.6}{12} \quad 6.3 \quad \frac{6.9}{17} \quad \frac{7.4}{18-20} \quad \frac{4.2}{25} \quad \frac{3.3}{34} \quad \frac{4.6}{50}$$

$$\frac{4.6}{50} \quad \frac{3.7}{23} \quad \frac{3.6}{23} \quad \frac{7.4}{12} \quad 7.1 \quad \frac{7.5}{16} \quad \frac{7.7}{18} \quad \frac{5.1}{23} \quad \frac{3.8}{31} \quad \frac{4.4}{50}$$

$$\frac{4.3}{50} \quad \frac{3.5}{23} \quad \frac{7.9}{13} \quad \frac{8.1}{9} \quad 7.8 \quad \frac{8.1}{17} \quad \frac{3.9}{22} \quad \frac{2.5}{28} \quad \frac{3.2}{50}$$

$$\frac{5.4}{50} \quad \frac{5.0}{40} \quad \frac{4.1}{24} \quad \frac{8.8}{18-14} \quad \frac{9.9}{11} \quad 9.5 \quad \frac{10.1}{18} \quad \frac{4.5}{24} \quad \frac{4.2}{31} \quad \frac{4.1}{50}$$

$$\frac{5.8}{50} \quad \frac{5.9}{23} \quad \frac{11.9}{15} \quad 11.5 \quad \frac{12.2}{19} \quad \frac{6.1}{26} \quad \frac{5.4}{33} \quad \frac{5.9}{50}$$

$$\frac{7.5}{50} \quad \frac{4.1}{23} \quad \frac{13.9}{15} \quad 13.6 \quad \frac{14.4}{20} \quad \frac{8.1}{29} \quad \frac{7.8}{43} \quad \frac{8.6}{50}$$

$$\frac{7.7}{50} \quad \frac{7.2}{27}$$

$$\frac{9.5}{32} \quad \frac{10.0}{50}$$

Sta	+	$\uparrow$	-	Elev
		941.71		
87+40		41.7		
+50				
88				
+50				
T.P.	3.44	931.37	13.78	927.93
87+35		31.4		
+40				
+50				
88				
+50				
89				
T.P.	0.63	918.95	13.05	918.32
89		19.0		
+50				

Lt

L

Rt

$$\frac{9.5}{34} \quad \frac{9.8}{50}$$

$$\frac{9.4}{37} \quad \frac{9.9}{50} \quad \frac{11.7}{75}$$

$$\frac{7.1}{50} \quad \frac{7.0}{55} \quad \frac{9.2}{75}$$

$$\frac{10.6}{56} \quad \frac{12.6}{75}$$

$$\frac{5.7}{14} \quad \frac{5.3}{9} \quad \frac{6.0}{12} \quad \frac{6.3}{20} \quad \frac{5.2}{24}$$

$$\frac{13.5}{44} \quad \frac{1.3}{40} \quad \frac{1.3}{29} \quad \frac{1.2}{21} \quad \frac{6.0}{16} \quad \frac{5.5}{8} \quad \frac{6.1}{11} \quad \frac{6.5}{19} \quad \frac{5.7}{24}$$

$$+ \frac{3.5}{50} \quad \frac{3.8}{50} \quad \frac{3.8}{42} \quad \frac{3.5}{22} \quad \frac{6.4}{15} \quad \frac{6.2}{8} \quad \frac{7.3}{17-20} \quad \frac{6.5}{26}$$

$$\frac{4.1}{50} \quad \frac{5.2}{37} \quad \frac{8.7}{20} \quad \frac{10.1}{16} \quad \frac{10.1}{9} \quad \frac{9.7}{11} \quad \frac{10.3}{15} \quad \frac{10.1}{32}$$

$$\frac{6.6}{50} \quad \frac{10.2}{40} \quad \frac{12.6}{18} \quad \frac{13.4}{9} \quad \frac{13.1}{14} \quad \frac{13.8}{35}$$

$$\frac{11.2}{44} \quad \frac{10.3}{50} \quad \frac{11.3}{75}$$

$$\frac{3.0}{50} \quad \frac{2.4}{34} \quad \frac{4.1}{16} \quad \frac{4.1}{8} \quad \frac{4.1}{12} \quad \frac{4.4}{33}$$

$$\frac{10.7}{50} \quad \frac{7.8}{20} \quad \frac{7.5}{12} \quad \frac{7.2}{11} \quad \frac{7.7}{23} \quad \frac{6.5}{29} \quad \frac{6.4}{50}$$

Sta	+	π	-	Elev
		918.95		
		19.0		
89+80				
T.P.	1.44	910.42	9.97	908.98
90		10.9		
+50				
91				
T.P.	1.37	900.19	11.60	898.82
91		00.2		
+50				
92				
+50				
93				
T.P.	1.96	894.68	7.47	892.72
+50		94.7		
94				

Lt.

K

Rt.

$$\frac{149}{50} \quad \frac{134}{32} \quad \frac{116}{19} \quad \frac{98}{13} \quad 92 \quad \frac{96}{10} \quad \frac{100}{16} \quad \frac{99}{29} \quad \frac{149}{50}$$

$$\frac{82}{58} \quad \frac{64}{25} \quad \frac{53}{20} \quad \frac{27}{13} \quad 21 \quad \frac{24}{9} \quad \frac{32}{19} \quad \frac{64}{27} \quad \frac{76}{32} \quad \frac{116}{42} \quad \frac{123}{50}$$

$$\frac{119}{50} \quad \frac{98}{19} \quad \frac{56}{11} \quad 53 \quad \frac{58}{16} \quad \frac{142}{29} \quad \frac{173}{50}$$

$$\frac{87}{12} \quad 8.2 \quad \frac{90}{14}$$

$$\frac{62}{50} \quad \frac{44}{23} \quad \frac{75}{30} \quad \frac{114}{50}$$

$$\frac{113}{50} \quad \frac{104}{27} \quad \frac{15}{13} \quad 09 \quad \frac{19}{14} \quad \frac{117}{30} \quad \frac{133}{50}$$

$$\frac{124}{50} \quad \frac{113}{27} \quad \frac{40}{13} \quad 34 \quad \frac{46}{16} \quad \frac{126}{31} \quad \frac{140}{50}$$

$$\frac{122}{50} \quad \frac{121}{24} \quad \frac{57}{11} \quad 53 \quad \frac{62}{15} \quad \frac{133}{27} \quad \frac{139}{50}$$

$$\frac{126}{50} \quad \frac{125}{22} \quad \frac{73}{11} \quad 69 \quad \frac{99}{15} \quad \frac{136}{26} \quad \frac{144}{50}$$

$$\frac{67}{50} \quad \frac{67}{20} \quad \frac{37}{15} \quad \frac{28}{10} \quad 24 \quad \frac{28}{9} \quad \frac{39}{16} \quad \frac{84}{25} \quad \frac{87}{50}$$

$$\frac{63}{50} \quad \frac{64}{30} \quad \frac{57}{28} \quad \frac{38}{11} \quad 3.4 \quad \frac{38}{10} \quad \frac{53}{17} \quad \frac{88}{24} \quad \frac{88}{50}$$

Sta	+	Δ	-	Elev
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894.68

94+50

94.7

95

B.M

3.48

894.68

3.48

891.20

891.20

+50

96

+50

97

T.P.

8.21

897.90

4.99

889.69

+47

24" x Drain

98

+50

99

+50

100

Lt.

L

Rt.

$$\frac{7.2}{50} \quad \frac{8.2}{21} \quad \frac{5.7}{15} \quad \frac{4.9}{11} \quad 43 \quad \frac{4.8}{11} \quad \frac{8.5}{21} \quad \frac{9.2}{50}$$

$$\frac{8.2}{50} \quad \frac{8.4}{23} \quad \frac{5.8}{15} \quad 48 \quad \frac{5.1}{11} \quad \frac{5.8}{15} \quad \frac{8.9}{22} \quad \frac{9.6}{50}$$

Spk in P.P 28 Rt 50 95+05

$$\frac{8.5}{50} \quad \frac{9.3}{23} \quad \frac{5.4}{11} \quad 48 \quad \frac{5.1}{11} \quad \frac{6.5}{16} \quad \frac{9.0}{22} \quad \frac{9.7}{50}$$

$$\frac{8.1}{50} \quad \frac{8.8}{23} \quad \frac{6.5}{17} \quad \frac{5.4}{11} \quad 47 \quad \frac{5.0}{10} \quad \frac{6.1}{16} \quad \frac{9.2}{23} \quad \frac{9.5}{50}$$

$$\frac{8.3}{50} \quad \frac{8.7}{23} \quad \frac{6.4}{17} \quad \frac{5.4}{7} \quad 5.1 \quad \frac{5.3}{10} \quad \frac{7.0}{17} \quad \frac{9.3}{22} \quad \frac{9.7}{50}$$

$$\frac{8.8}{50} \quad \frac{8.5}{19} \quad \frac{5.5}{13} \quad 5.2 \quad \frac{5.5}{10} \quad \frac{6.5}{16} \quad \frac{9.2}{22} \quad \frac{9.2}{50}$$

$$\frac{11.0}{50} \quad \frac{11.3}{27} \quad \frac{12.8}{18} \quad \frac{13.6}{18} \quad \frac{9.4}{15} \quad \frac{8.4}{12} \quad 78 \quad \frac{8.2}{9} \quad \frac{9.0}{14} \quad \frac{12.9}{19} \quad \frac{12.8}{9} \quad \frac{13.2}{50}$$

INV

Ditch

$$\frac{9.7}{50} \quad \frac{9.5}{26} \quad \frac{8.9}{19} \quad \frac{4.7}{13} \quad 7.6 \quad \frac{7.8}{11} \quad \frac{8.7}{14} \quad \frac{12.0}{20} \quad \frac{11.8}{34} \quad \frac{13.0}{39} \quad \frac{12.5}{41} \quad \frac{12.5}{43}$$

$$\frac{5.3}{50} \quad \frac{6.3}{28} \quad \frac{7.0}{11} \quad 6.8 \quad \frac{4.4}{10} \quad \frac{8.5}{14} \quad \frac{11.3}{20} \quad \frac{12.0}{39} \quad \frac{13.1}{40} \quad \frac{12.5}{42} \quad \frac{12.1}{43} \quad \frac{12.5}{50}$$

Ditch

Ditch

$$\frac{0.3}{50} \quad \frac{2.6}{30} \quad \frac{3.5}{26} \quad \frac{6.2}{21} \quad \frac{6.1}{10} \quad 6.1 \quad \frac{6.6}{9} \quad \frac{7.1}{14} \quad \frac{10.0}{21} \quad \frac{10.7}{37} \quad \frac{12.4}{41} \quad \frac{11.5}{43} \quad \frac{11.5}{45} \quad \frac{11.5}{50}$$

$$\frac{1.0}{34} \quad \frac{1.2}{27} \quad \frac{5.3}{23} \quad \frac{5.2}{9} \quad 5.1 \quad \frac{5.5}{10} \quad \frac{6.4}{17} \quad \frac{9.4}{24} \quad \frac{10.7}{44} \quad \frac{12.0}{47} \quad \frac{11.3}{49} \quad \frac{11.3}{50} \quad \frac{11.3}{55}$$

Ditch

Ditch

$$\frac{1.4}{31} \quad \frac{4.8}{24} \quad \frac{4.3}{10} \quad 4.3 \quad \frac{4.6}{10} \quad \frac{5.6}{23} \quad \frac{7.3}{30} \quad \frac{10.1}{50} \quad \frac{11.1}{52} \quad \frac{10.4}{55} \quad \frac{10.4}{56}$$

Sta + Δ - Elev

897.90

100+50

101

+18

+25

+40

+45

T.P. 1214 907.02 3.02 894.88

99+50

100

+50

101

+18

+45

Lt.

X

Rt

Ditch

$$\frac{1.0}{29} \quad \frac{3.3}{23} \quad \frac{3.5}{9} \quad 7.5 \quad \frac{4.0}{10} \quad \frac{4.2}{23} \quad \frac{6.1}{29} \quad \frac{9.0}{51} \quad \frac{10.9}{54.56} \quad \frac{10.0}{58}$$

$$\frac{1.0}{29} \quad \frac{2.3}{26} \quad \frac{2.8}{12} \quad 2.9 \quad \frac{3.3}{10} \quad \frac{4.0}{21} \quad \frac{5.6}{29} \quad \frac{8.8}{50} \quad \frac{11.1}{54.56} \quad \frac{9.9}{58}$$

$$\frac{2.0}{27} \quad \frac{2.7}{9} \quad 2.6 \quad \frac{3.5}{16} \quad \frac{5.8}{24} \quad \frac{7.6}{34} \quad \frac{8.6}{48} \quad \frac{10.8}{51.53} \quad \frac{9.7}{55}$$

$$\frac{0.0}{50} \quad \frac{1.4}{31} \quad \frac{2.6}{10} \quad 2.6 \quad \frac{3.1}{10} \quad \frac{3.5}{16} \quad \frac{5.8}{24} \quad \frac{8.2}{35} \quad \frac{10.8}{49.51} \quad \frac{9.7}{53}$$

$$\frac{0.2}{50} \quad \frac{1.2}{36} \quad \frac{2.0}{27} \quad \frac{2.5}{9} \quad 2.5 \quad \frac{3.0}{9} \quad \frac{3.3}{17} \quad \frac{5.4}{24} \quad \frac{7.5}{42} \quad \frac{10.3}{49.51} \quad \frac{9.5}{53}$$

$$\frac{0.9}{27} \quad \frac{2.2}{21} \quad \frac{2.5}{9} \quad 2.5 \quad \frac{3.0}{10} \quad \frac{3.4}{19} \quad \frac{5.0}{24} \quad \frac{6.8}{40} \quad \frac{10.2}{46.48} \quad \frac{9.3}{50}$$

$$\frac{5.7}{50} \quad \frac{8.2}{35}$$

$$\frac{2.5}{50} \quad \frac{3.7}{39}$$

$$\frac{2.8}{50} \quad \frac{3.6}{38}$$

$$\frac{4.0}{50} \quad \frac{4.1}{38}$$

$$\frac{3.7}{50} \quad \frac{5.3}{38}$$

$$\frac{4.3}{50} \quad \frac{5.0}{34}$$

Sta	+	π	-	Elev
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907.02

102

+50

T.P	5.99	900.87	12.14	894.88
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102

00.9

+50

103

+60

T.P.	4.94	900.40	5.41	895.42
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104

+50

105

94.3

+50

106

92.7

+22

92.3

T.P	12.76	909.65	3.51	896.89
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Lt. Z Rt

$$\frac{3.9}{50} \quad \frac{5.4}{33}$$

$$\frac{5.5}{50} \quad \frac{6.3}{32}$$

$$\frac{5.4}{23} \quad \frac{5.4}{10} \quad 5.4 \quad \frac{5.9}{12} \quad \frac{9.8}{22} \quad \frac{11.0}{33} \quad \frac{13.5}{38.42} \quad \frac{12.8}{44.50}$$

$$\frac{5.2}{23} \quad \frac{5.5}{13} \quad 5.2 \quad \frac{5.7}{8} \quad \frac{6.4}{12} \quad \frac{11.3}{21} \quad \frac{12.4}{34} \quad \frac{14.2}{38.41} \quad \frac{13.2}{44}$$

$$\frac{1.2}{50} \quad \frac{1.7}{34} \quad \frac{5.5}{26} \quad \frac{5.5}{13} \quad 5.3 \quad \frac{5.4}{5} \quad \frac{6.3}{13} \quad \frac{10.4}{21} \quad \frac{12.2}{34} \quad \frac{14.7}{40.42} \quad \frac{13.6}{45} \quad \frac{13.5}{50}$$

$$\frac{1.8}{50} \quad \frac{1.3}{31} \quad \frac{5.3}{21} \quad \frac{5.6}{14} \quad 5.0 \quad \frac{5.2}{13} \quad \frac{10.5}{27} \quad \frac{12.0}{42} \quad \frac{14.0}{47.50} \quad \frac{13.3}{50}$$

Spk in T.P. Rt Stg 103.475

$$\frac{0.0}{50} \quad \frac{0.3}{28} \quad \frac{5.4}{19} \quad \frac{5.6}{11} \quad 4.8 \quad \frac{4.7}{15} \quad \frac{5.1}{24} \quad \frac{6.2}{35} \quad \frac{10.1}{50}$$

$$\frac{5.2}{20} \quad \frac{6.3}{16} \quad \frac{6.3}{11} \quad 5.4 \quad \frac{5.3}{10} \quad \frac{5.4}{25} \quad \frac{10.3}{36} \quad \frac{12.7}{50}$$

$$\frac{4.3}{20} \quad \frac{6.7}{10} \quad 6.1 \quad \frac{6.4}{11} \quad \frac{6.6}{21} \quad \frac{10.7}{26} \quad \frac{12.5}{34} \quad \frac{13.3}{50}$$

$$\frac{7.2}{19} \quad \frac{7.5}{9} \quad 7.0 \quad \frac{7.5}{11} \quad \frac{7.7}{20} \quad \frac{11.2}{25} \quad \frac{12.5}{31} \quad \frac{13.3}{50}$$

$$\frac{8.0}{19} \quad \frac{8.2}{13} \quad 7.7 \quad \frac{8.5}{10} \quad \frac{8.8}{14} \quad \frac{12.4}{23} \quad \frac{13.7}{50}$$

$$\frac{6.6}{25} \quad \frac{7.8}{18} \quad \frac{8.4}{14} \quad 8.1 \quad \frac{9.1}{10} \quad \frac{9.9}{15} \quad \frac{11.1}{19} \quad \frac{12.1}{27} \quad \frac{13.7}{50}$$

Sta	+	π	-	Elev
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104+50		909.65 91.6		
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105				
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+50				
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106				
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+22				
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T.P	0.03	896.92	12.76	896.89
+73		96.9		91.6

107				91.5
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+29	24" x Drain			
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+50				
-----	--	--	--	--

108				91.8
B.M	2.90	899.43	0.40	896.52
+50				92.1

109				92.5
-----	--	--	--	------

Lt

L

Rt

$$\frac{5.3}{75} \quad \frac{6.1}{50} \quad \frac{7.3}{41} \quad \frac{7.7}{28}$$

$$\frac{3.2}{75} \quad \frac{4.8}{50} \quad \frac{4.8}{33}$$

$$\frac{0.0}{75} \quad \frac{1.8}{50} \quad \frac{2.0}{39}$$

$$\frac{4.4}{75} \quad \frac{8.0}{50} \quad \frac{9.8}{29}$$

$$\frac{7.5}{75} \quad \frac{12.0}{50} \quad \frac{13.2}{33}$$

$$\frac{2.0}{50} \quad \frac{3.4}{35} \quad \frac{5.6}{18} \quad \frac{5.4}{11} \quad 5.3 \quad \frac{6.2}{10} \quad \frac{6.5}{15} \quad \frac{8.9}{22} \quad \frac{10.5}{50}$$

$$\frac{2.6}{50} \quad \frac{5.9}{21} \quad \frac{6.2}{15} \quad \frac{5.5}{11} \quad 5.4 \quad \frac{6.4}{10} \quad \frac{6.6}{16} \quad \frac{9.1}{22} \quad \frac{10.5}{50}$$

$$\begin{array}{c} \text{Inv} \\ \frac{10.3}{50} \quad \frac{9.1}{19} \quad \frac{9.4}{19} \quad \frac{6.3}{11} \end{array} \quad 5.3 \quad \begin{array}{c} \text{Inv} \\ \frac{5.5}{9} \quad \frac{7.9}{17} \quad \frac{8.1}{17} \quad \frac{8.1}{20} \quad \frac{6.3}{21} \quad \frac{4.1}{50} \end{array}$$

$$\frac{4.4}{50} \quad \frac{5.8}{29} \quad \frac{5.6}{21} \quad \frac{6.2}{18} \quad \frac{5.4}{9} \quad 5.3 \quad \frac{6.2}{11} \quad \frac{6.3}{15} \quad \frac{9.6}{23} \quad \frac{10.2}{50}$$

$$\frac{4.5}{50} \quad \frac{5.4}{13} \quad \frac{5.3}{10} \quad 5.1 \quad \frac{5.8}{10} \quad \frac{6.4}{14} \quad \frac{9.4}{21} \quad \frac{9.7}{50}$$

H: Nut N.E Leg Steel 11 Tension Tower Lt 111+00

$$\frac{5.5}{15} \quad \frac{7.5}{25} \quad \frac{7.3}{16} \quad \frac{7.6}{9} \quad 7.3 \quad \frac{8.0}{10} \quad \frac{8.4}{15} \quad \frac{11.0}{29} \quad \frac{12.5}{50}$$

$$\frac{4.3}{50} \quad \frac{6.1}{26} \quad \frac{6.3}{16} \quad \frac{7.3}{12} \quad 6.9 \quad \frac{7.4}{11} \quad \frac{7.4}{17} \quad \frac{9.4}{27} \quad \frac{11.6}{36} \quad \frac{12.4}{50}$$

Sta	+	π	-	Elev
		899.43		
109+50				93.0
110				93.8
+40	$\pm$	Co Rd C (East)		94.3
+20				
111				94.9
+06				
+19		South Rail		95.26
+24		North Rail		95.23
+27				
+50				95.8
+63		24" x Drain		
112				97.3

LT. ~~R~~ RT

$$\frac{3.3}{50} \quad \frac{4.0}{41} \quad \frac{5.8}{33} \quad \frac{6.5}{29} \quad \frac{6.6}{11} \quad 6.4 \quad \frac{6.9}{10} \quad \frac{7.4}{25} \quad \frac{9.8}{41} \quad \frac{12.2}{51} \quad \frac{12.7}{57}$$

$$\frac{3.6}{50} \quad \frac{4.1}{42} \quad \frac{5.9}{32} \quad \frac{6.0}{14} \quad 5.6 \quad \frac{5.8}{22} \quad \frac{6.5}{36} \quad \frac{8.4}{50}$$

$$\frac{4.1}{50} \quad \frac{5.5}{30} \quad \frac{6.7}{26} \quad \frac{6.6}{21} \quad \frac{5.2}{16} \quad \frac{5.4}{10} \quad 5.1 \quad \frac{5.2}{25} \quad \frac{5.8}{50}$$

$$\frac{4.6}{50} \quad \frac{5.1}{25} \quad \frac{5.3}{10} \quad 4.9 \quad \frac{5.3}{14} \quad \frac{5.9}{28} \quad \frac{10.5}{45} \quad \frac{10.7}{50}$$

$$\frac{5.3}{30} \quad \frac{4.5}{38} \quad \frac{4.9}{29} \quad \frac{5.8}{16} \quad \frac{4.6}{10} \quad 4.5 \quad \frac{4.8}{9} \quad \frac{4.9}{17} \quad \frac{9.5}{30} \quad \frac{11.0}{50}$$

$$\frac{5.3}{50} \quad \frac{4.9}{30} \quad \frac{5.3}{16} \quad \frac{4.4}{10} \quad 4.4 \quad \frac{4.7}{9} \quad \frac{4.3}{14} \quad \frac{5.4}{20} \quad \frac{6.0}{50}$$

4.17

4.20

$$\frac{4.4}{50} \quad \frac{4.7}{34} \quad \frac{4.1}{14} \quad 4.1 \quad \frac{4.3}{11} \quad \frac{5.5}{39} \quad \frac{6.4}{50}$$

$$\frac{4.4}{50} \quad \frac{3.4}{23} \quad \frac{3.4}{9} \quad 3.6 \quad \frac{3.8}{11} \quad \frac{4.6}{17} \quad \frac{6.9}{23} \quad \frac{8.0}{50}$$

$$\frac{4.3}{50} \quad \frac{3.0}{23} \quad \frac{5.6}{22} \quad \frac{5.6}{19} \quad \frac{3.0}{15} \quad 3.2 \quad \frac{3.6}{9} \quad \frac{4.1}{14} \quad \frac{6.6}{22} \quad \frac{7.9}{22} \quad \frac{7.9}{50}$$

$$\frac{2.1}{50} \quad \frac{2.2}{22} \quad \frac{3.7}{20-17} \quad \frac{1.8}{13} \quad 2.1 \quad \frac{2.7}{10} \quad \frac{3.3}{19} \quad \frac{6.6}{29} \quad \frac{6.8}{50}$$

Sta	+	Δ	-	Elev
		899.43		

112+50

T.P.	13.29	912.55	0.17	899.26
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113		12.6		901.2
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+50

114				05.3
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+50

T.P.	11.94	921.04	3.45	909.10
------	-------	--------	------	--------

+50		21.0		
-----	--	------	--	--

115				09.0
-----	--	--	--	------

+50

116				11.3
-----	--	--	--	------

+50

117				12.3
-----	--	--	--	------

T.P.	5.81	918.54	8.31	912.73
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+50		18.5		
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Lt.

K

Rt.

$$\frac{0.0}{50} \quad \frac{0.7}{23} \quad \frac{2.4}{21-17} \quad \frac{0.2}{1.3} \quad 0.2 \quad \frac{0.2}{9} \quad \frac{1.0}{15} \quad \frac{3.0}{30} \quad \frac{3.7}{50}$$

$$\frac{10.0}{50} \quad \frac{10.6}{25} \quad \frac{12.8}{22-18} \quad \frac{11.5}{14} \quad 11.4 \quad \frac{11.8}{17} \quad \frac{12.6}{19} \quad \frac{12.4}{24} \quad \frac{10.9}{28} \quad \frac{12.0}{50}$$

$$\frac{6.5}{50} \quad \frac{7.3}{21} \quad \frac{10.8}{23-20} \quad \frac{9.7}{18} \quad \frac{9.5}{15} \quad \frac{9.3}{15} \quad \frac{9.6}{20} \quad \frac{11.4}{21} \quad \frac{5.6}{31} \quad \frac{6.6}{50}$$

$$\frac{1.7}{50} \quad \frac{2.2}{40} \quad \frac{9.7}{25-22} \quad \frac{7.3}{17} \quad 7.3 \quad \frac{8.1}{15} \quad \frac{9.0}{19} \quad \frac{3.4}{33} \quad \frac{3.5}{50}$$

$$\frac{7.6}{24-21} \quad \frac{5.1}{17} \quad 5.4 \quad \frac{5.9}{15} \quad \frac{6.9}{19} \quad \frac{5.7}{24} \quad \frac{0.7}{35} \quad \frac{0.9}{50}$$

$$\frac{5.6}{50} \quad \frac{6.0}{42} \quad \frac{7.0}{36}$$

$$\frac{1.5}{50} \quad \frac{1.5}{38} \quad \frac{1.8}{32} \quad \frac{14.2}{22-20} \quad \frac{12.0}{15} \quad 12.0 \quad \frac{12.5}{14} \quad \frac{12.6}{17} \quad \frac{13.4}{20} \quad \frac{12.3}{24} \quad \frac{6.5}{36} \quad \frac{6.9}{50}$$

$$\frac{0.0}{50} \quad \frac{0.2}{38} \quad \frac{0.8}{33} \quad \frac{12.3}{21-19} \quad \frac{10.7}{15} \quad 10.6 \quad \frac{11.1}{17} \quad \frac{12.0}{19} \quad \frac{10.9}{26} \quad \frac{4.9}{38} \quad \frac{4.8}{50}$$

$$\frac{1.8}{50} \quad \frac{2.0}{37} \quad \frac{3.0}{31} \quad \frac{11.4}{21-18} \quad \frac{9.8}{15} \quad 9.7 \quad \frac{10.1}{16} \quad \frac{10.8}{19} \quad \frac{9.4}{27} \quad \frac{2.0}{40} \quad \frac{2.1}{50}$$

$$\frac{3.6}{50} \quad \frac{5.1}{31} \quad \frac{7.9}{25} \quad \frac{10.6}{21-18} \quad \frac{9.2}{15} \quad 9.2 \quad \frac{9.5}{15} \quad \frac{10.6}{20} \quad \frac{7.8}{25} \quad \frac{3.9}{37} \quad \frac{3.6}{50}$$

$$\frac{5.1}{50} \quad \frac{5.1}{35} \quad \frac{6.2}{27} \quad \frac{9.1}{24-17} \quad \frac{8.8}{15} \quad 8.7 \quad \frac{9.3}{16} \quad \frac{10.4}{19-22} \quad \frac{8.7}{27} \quad \frac{8.1}{50}$$

$$\frac{1.2}{50} \quad \frac{2.0}{32} \quad \frac{2.5}{28} \quad \frac{7.6}{23-19} \quad \frac{6.2}{15} \quad 6.1 \quad \frac{6.8}{16} \quad \frac{7.9}{19-23} \quad \frac{7.4}{25} \quad \frac{8.1}{31} \quad \frac{9.8}{50}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

		918.54		
--	--	--------	--	--

		18.5		
--	--	------	--	--

118				
-----	--	--	--	--

+50				
-----	--	--	--	--

119				
-----	--	--	--	--

+14	15" X Drain			
-----	-------------	--	--	--

+50				
-----	--	--	--	--

120				
-----	--	--	--	--

+50				
-----	--	--	--	--

121				
-----	--	--	--	--

+50				
-----	--	--	--	--

122				
-----	--	--	--	--

+50				
-----	--	--	--	--

T.P.	3.87	914.79	7.62	910.92
------	------	--------	------	--------

123				
-----	--	--	--	--

		14.8		
--	--	------	--	--

L1

R

R+

$$\frac{+1.0}{50} \quad \frac{0.4}{30} \quad \frac{7.3}{25-19} \quad \frac{6.1}{15} \quad 6.2 \quad \frac{6.7}{18} \quad \frac{7.7}{20-23} \quad \frac{7.2}{25} \quad \frac{10.5}{50}$$

$$\frac{3.7}{50} \quad \frac{4.4}{29} \quad \frac{7.1}{25-20} \quad \frac{6.5}{18} \quad \frac{6.2}{15} \quad 6.1 \quad \frac{6.6}{18} \quad \frac{8.4}{23} \quad \frac{9.1}{50}$$

$$\frac{5.1}{50} \quad \frac{5.4}{30} \quad \frac{7.1}{29-23} \quad \frac{6.1}{21} \quad 5.6 \quad \frac{6.1}{15} \quad \frac{6.5}{21} \quad \frac{9.7}{29} \quad \frac{8.6}{50}$$

Inv

$$\frac{5.2}{50} \quad \frac{5.4}{33} \quad \frac{8.05}{30} \quad \frac{7.9}{20} \quad \frac{7.1}{25} \quad \frac{5.9}{21} \quad 5.7 \quad \frac{6.1}{20} \quad \frac{10.75}{29} \quad \frac{10.3}{29} \quad \frac{9.9}{50}$$

Inv

$$\frac{5.5}{50} \quad \frac{5.3}{40} \quad \frac{6.5}{37} \quad \frac{6.3}{30} \quad \frac{5.7}{28} \quad 5.6 \quad \frac{6.0}{14} \quad \frac{6.4}{12} \quad \frac{12.8}{37} \quad \frac{14.0}{50}$$

$$\frac{4.6}{50} \quad \frac{5.0}{18} \quad 5.2 \quad \frac{6.0}{14} \quad \frac{6.3}{21} \quad \frac{20.6}{57}$$

$$\frac{5.9}{52} \quad \frac{7.8}{51-50} \quad \frac{7.8}{45-17} \quad \frac{5.4}{17} \quad \frac{5.1}{5.5} \quad \frac{6.2}{15} \quad \frac{7.1}{23} \quad \frac{20.3}{59} \quad \frac{22.8}{66}$$

$$\frac{5.8}{50} \quad \frac{6.8}{38} \quad \frac{8.1}{35} \quad \frac{8.0}{23} \quad \frac{6.1}{17} \quad 6.2 \quad \frac{6.5}{15} \quad \frac{6.8}{22} \quad \frac{19.3}{50}$$

$$\frac{6.7}{50} \quad \frac{7.4}{33} \quad \frac{8.0}{31} \quad \frac{8.1}{22} \quad \frac{6.6}{15} \quad 6.7 \quad \frac{7.2}{15} \quad \frac{7.5}{22} \quad \frac{12.2}{34} \quad \frac{14.9}{50}$$

$$\frac{3.6}{50} \quad \frac{5.9}{31} \quad \frac{9.0}{27} \quad \frac{9.0}{20} \quad \frac{7.0}{15} \quad 6.9 \quad \frac{7.4}{20} \quad \frac{14.3}{37} \quad \frac{14.8}{50}$$

$$\frac{0.4}{50} \quad \frac{3.8}{30} \quad \frac{8.8}{26} \quad \frac{9.3}{23-21} \quad \frac{7.3}{16} \quad 7.2 \quad \frac{7.6}{18} \quad \frac{14.3}{34} \quad \frac{14.7}{50}$$

$$\frac{5.1}{25} \quad \frac{5.5}{23} \quad \frac{6.0}{22-20} \quad \frac{3.8}{16} \quad 3.7 \quad \frac{3.8}{17} \quad \frac{10.8}{32} \quad \frac{10.9}{50}$$

Sta + π - Elev

123+50 914.79
14.8

124

+10

+23

+50

B.M 5.00 914.81 5.00 909.79 909.81

125

+38

+63

+80

126

T.P 18.76 925.04 8.53 906.28

123

+50

Lt.

R

Rt.

$$\begin{array}{r} 5.9 \\ 25 \end{array} \quad \begin{array}{r} 6.5 \\ 23-21 \end{array} \quad \begin{array}{r} 4.8 \\ 17 \end{array} \quad 4.1 \quad \begin{array}{r} 4.1 \\ 16 \end{array} \quad \begin{array}{r} 10.7 \\ 29 \end{array} \quad \begin{array}{r} 10.8 \\ 50 \end{array}$$

$$\begin{array}{r} 6.2 \\ 24 \end{array} \quad \begin{array}{r} 6.8 \\ 21-19 \end{array} \quad \begin{array}{r} 5.1 \\ 16 \end{array} \quad 4.7 \quad \begin{array}{r} 4.4 \\ 16 \end{array} \quad \begin{array}{r} 10.8 \\ 27 \end{array} \quad \begin{array}{r} 10.9 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 22 \end{array} \quad \begin{array}{r} 6.8 \\ 21-19 \end{array} \quad \begin{array}{r} 5.2 \\ 16 \end{array} \quad 4.9 \quad \begin{array}{r} 4.5 \\ 16 \end{array} \quad \begin{array}{r} 10.8 \\ 26 \end{array} \quad \begin{array}{r} 10.9 \\ 50 \end{array}$$

$$\begin{array}{r} 6.0 \\ 23 \end{array} \quad \begin{array}{r} 4.0 \\ 21-19 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad 5.1 \quad \begin{array}{r} 4.7 \\ 16 \end{array} \quad \begin{array}{r} 6.7 \\ 24 \end{array} \quad \begin{array}{r} 6.1 \\ 30 \end{array} \quad \begin{array}{r} 5.9 \\ 50 \end{array}$$

$$\begin{array}{r} 4.4 \\ 24 \end{array} \quad \begin{array}{r} 5.7 \\ 21 \end{array} \quad \begin{array}{r} 6.9 \\ 20-18 \end{array} \quad \begin{array}{r} 5.8 \\ 17 \end{array} \quad 5.4 \quad \begin{array}{r} 5.3 \\ 16 \end{array} \quad \begin{array}{r} 6.4 \\ 23 \end{array} \quad \begin{array}{r} 6.0 \\ 28 \end{array} \quad \begin{array}{r} 5.8 \\ 50 \end{array}$$

Top S.W. Cor Conc Step Platform School Ho^{Top Wall}

$$\begin{array}{r} 4.3 \\ 26 \end{array} \quad \begin{array}{r} 6.5 \\ 22 \end{array} \quad \begin{array}{r} 7.3 \\ 21-19 \end{array} \quad \begin{array}{r} 6.5 \\ 16 \end{array} \quad 6.2 \quad \begin{array}{r} 6.0 \\ 17 \end{array} \quad \begin{array}{r} 6.5 \\ 24 \end{array} \quad \begin{array}{r} 6.3 \\ 30 \end{array} \quad \begin{array}{r} 5.6 \\ 31 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 7.3 \\ 24 \end{array} \quad \begin{array}{r} 8.9 \\ 21-19 \end{array} \quad \begin{array}{r} 7.1 \\ 16 \end{array} \quad 6.8 \quad \begin{array}{r} 6.6 \\ 18 \end{array} \quad \begin{array}{r} 7.2 \\ 25 \end{array} \quad \begin{array}{r} 6.4 \\ 32 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array}$$

$$\begin{array}{r} 7.3 \\ 26 \end{array} \quad \begin{array}{r} 9.2 \\ 23-20 \end{array} \quad \begin{array}{r} 7.6 \\ 16 \end{array} \quad 7.2 \quad \begin{array}{r} 7.1 \\ 17 \end{array} \quad \begin{array}{r} 8.2 \\ 23 \end{array} \quad \begin{array}{r} 8.8 \\ 29 \end{array} \quad \begin{array}{r} 7.1 \\ 33 \end{array} \quad \begin{array}{r} 6.4 \\ 35 \end{array} \quad \begin{array}{r} 6.5 \\ 50 \end{array}$$

$$\begin{array}{r} 8.5 \\ 25 \end{array} \quad \begin{array}{r} 10.0 \\ 23-20 \end{array} \quad \begin{array}{r} 7.8 \\ 16 \end{array} \quad 7.4 \quad \begin{array}{r} 7.7 \\ 17 \end{array} \quad \begin{array}{r} 10.1 \\ 30 \end{array} \quad \begin{array}{r} 12.6 \\ 35 \end{array} \quad \begin{array}{r} 13.7 \\ 50 \end{array}$$

$$\begin{array}{r} 8.7 \\ 25 \end{array} \quad \begin{array}{r} 10.4 \\ 23-20 \end{array} \quad \begin{array}{r} 8.3 \\ 17 \end{array} \quad 7.7 \quad \begin{array}{r} 8.3 \\ 17 \end{array} \quad \begin{array}{r} 9.7 \\ 25 \end{array} \quad \begin{array}{r} 15.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.4 \\ 50 \end{array} \quad \begin{array}{r} 8.9 \\ 30 \end{array}$$

$$\begin{array}{r} 5.5 \\ 50 \end{array} \quad \begin{array}{r} 10.5 \\ 30 \end{array}$$

Sta	+	π	-	Elev
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925.04

124

+10

+23

+50

125

+38

+63

+80

126

+50

127

T.P

3.89

910.17

18.76

906.28

126+50

10.2

L1

X

R1

$$\frac{48}{50} \quad \frac{9.1}{30}$$

$$\frac{38}{50} \quad \frac{8.6}{30}$$

$$\frac{2.8}{50} \quad \frac{7.6}{30}$$

$$\frac{1.6}{50} \quad \frac{5.4}{31}$$

$$\frac{4.2}{50} \quad \frac{7.1}{32}$$

$$\frac{3.9}{50} \quad \frac{7.8}{32}$$

$$\frac{5.9}{50} \quad \frac{9.9}{32}$$

$$\frac{6.2}{50} \quad \frac{10.5}{40}$$

$$\frac{8.1}{50} \quad \frac{11.7}{32}$$

$$\frac{9.1}{50} \quad \frac{12.6}{32}$$

$$\frac{7.3}{50} \quad \frac{10.7}{32}$$

$$\frac{6.4}{24.21} \quad \frac{4.3}{17} \quad 3.9 \quad \frac{43}{16} \quad \frac{5.0}{20} \quad \frac{133}{44} \quad \frac{13.8}{5.0}$$

06.3

Sta	+	π	-	Elev
-----	---	-------	---	------

127		910.17 10.2		
-----	--	----------------	--	--

+50

128

+50

T.P	18.92	919.98	9.11	901.06
-----	-------	--------	------	--------

127+50

128

+50

129

T.P	11.58	912.64	18.92	901.06
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129

+50

130

+15 24" x Drain

L1 ~~2~~ R4

$$\frac{67}{23-20} \quad \frac{46}{15} \quad \frac{05.7}{45} \quad \frac{5.1}{16} \quad \frac{8.1}{33} \quad \frac{14.0}{50}$$

$$\frac{5.7}{24} \quad \frac{6.9}{22-20} \quad \frac{5.1}{15} \quad \frac{05.1}{5.1} \quad \frac{5.3}{16} \quad \frac{7.4}{29} \quad \frac{7.4}{31} \quad H_0$$

$$\frac{7.8}{24-21} \quad \frac{6.0}{17} \quad \frac{03.3}{5.9} \quad \frac{6.5}{18} \quad \frac{10.9}{31} \quad \frac{15.6}{50}$$

$$\frac{7.0}{27} \quad \frac{8.1}{26} \quad \frac{8.0}{21} \quad \frac{6.7}{17} \quad \frac{03.3}{6.9} \quad \frac{7.3}{14} \quad \frac{7.7}{19} \quad \frac{12.1}{31} \quad \frac{17.2}{50}$$

Nail in P.P R4 Stg 129+

$$\frac{+40}{75} \quad \frac{0.1}{50} \quad \frac{3.7}{34}$$

$$\frac{+23}{75} \quad \frac{+10.0}{60} \quad \frac{1.9}{50} \quad \frac{46}{35}$$

$$\frac{1.7}{70} \quad \frac{3.8}{60} \quad \frac{7.2}{45} \quad \frac{8.1}{37}$$

$$\frac{8.9}{70} \quad \frac{12.8}{50}$$

$$\frac{7.0}{36} \quad \frac{11.1}{30} \quad \frac{11.4}{22} \quad \frac{9.7}{78} \quad \frac{9.02.6}{10.0}$$

$$\frac{7.2}{50} \quad \frac{8.7}{34} \quad \frac{11.9}{31} \quad \frac{12.2}{23} \quad \frac{10.3}{18} \quad \frac{9.01.9}{10.7}$$

$$\frac{5.2}{50} \quad \frac{6.8}{39}$$

$$\frac{2.4}{60} \quad \frac{4.5}{50} \quad \frac{6.2}{39}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

912.64

130+50

131

+50

132

+50

133

+36

T.P	3.43	904.49	11.58	901.06
-----	------	--------	-------	--------

129

04.5

+50

138

+15

x Drain

+50

Lt.

Z

Rt.

$$\begin{array}{r} 1.4 \\ 60 \end{array} \quad \begin{array}{r} 3.6 \\ 58 \end{array} \quad \begin{array}{r} 6.5 \\ 36 \end{array}$$

$$\begin{array}{r} 1.6 \\ 60 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array} \quad \begin{array}{r} 8.5 \\ 36 \end{array}$$

$$\begin{array}{r} 2.9 \\ 60 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 8.1 \\ 35 \end{array}$$

$$\begin{array}{r} 3.0 \\ 60 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 34 \end{array}$$

$$\begin{array}{r} 3.2 \\ 60 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array} \quad \begin{array}{r} 4.8 \\ 34 \end{array}$$

$$\begin{array}{r} 5.7 \\ 60 \end{array} \quad \begin{array}{r} 6.5 \\ 50 \end{array} \quad \begin{array}{r} 7.1 \\ 34 \end{array}$$

$$\begin{array}{r} 9.7 \\ 50 \end{array} \quad \begin{array}{r} 12.0 \\ 33 \end{array}$$

$$\begin{array}{r} 2.8 \\ 15 \end{array} \quad \begin{array}{r} 3.4 \\ 20 \end{array} \quad \begin{array}{r} 12.5 \\ 47 \end{array} \quad \begin{array}{r} 12.7 \\ 50 \end{array}$$

$$\begin{array}{r} 3.9 \\ 17 \end{array} \quad \begin{array}{r} 4.1 \\ 19 \end{array} \quad \begin{array}{r} 5.4 \\ 25 \end{array} \quad \begin{array}{r} 15.7 \\ 65 \end{array} \quad \begin{array}{r} 13.9 \\ 50 \end{array}$$

$$\begin{array}{r} 6.8 \\ 31 \end{array} \quad \begin{array}{r} 4.8 \\ 29 \end{array} \quad \begin{array}{r} 4.8 \\ 28 \end{array} \quad \begin{array}{r} 2.5 \\ 21 \end{array} \quad \begin{array}{r} 0.1 \\ 31 \end{array}$$

$$\begin{array}{r} 4.5 \\ 14 \end{array} \quad \begin{array}{r} 4.8 \\ 20 \end{array} \quad \begin{array}{r} 6.1 \\ 25 \end{array} \quad \begin{array}{r} 14.7 \\ 50 \end{array} \quad \begin{array}{r} 15.6 \\ 65 \end{array}$$

$$\begin{array}{r} 7.3 \\ 32 \end{array} \quad \begin{array}{r} 7.6 \\ 29 \end{array} \quad \begin{array}{r} 7.7 \\ 28 \end{array} \quad \begin{array}{r} 2.7 \\ 21 \end{array} \quad \begin{array}{r} 0.2 \\ 33 \end{array}$$

$$\begin{array}{r} 5.0 \\ 19 \end{array} \quad \begin{array}{r} 6.1 \\ 25 \end{array} \quad \begin{array}{r} 14.4 \\ 46 \end{array} \quad \begin{array}{r} 14.6 \\ 46 \end{array} \quad \begin{array}{r} 14.6 \\ 50 \end{array} \quad \begin{array}{r} 15.4 \\ 65 \end{array}$$

$$\begin{array}{r} 5.3 \\ 30 \end{array} \quad \begin{array}{r} 5.7 \\ 24 \end{array} \quad \begin{array}{r} 3.0 \\ 19 \end{array} \quad \begin{array}{r} 0.8 \\ 37 \end{array}$$

$$\begin{array}{r} 4.8 \\ 13 \end{array} \quad \begin{array}{r} 5.0 \\ 29 \end{array} \quad \begin{array}{r} 6.8 \\ 25 \end{array} \quad \begin{array}{r} 14.1 \\ 46 \end{array} \quad \begin{array}{r} 15.9 \\ 60 \end{array}$$

Sta + π - Eled

904.49

131

04.5

+50

132

+50

133

+36

T.P

4.91

902.96

6.44

898.05

134

903.0

+50

135

+10

+50

136

L1.

2

R1.

$$\frac{5.9}{31} \quad \frac{6.2}{23} \quad \frac{38}{17}$$

$$\frac{5.1}{19} \quad \frac{9.1}{30} \quad \frac{138}{45} \quad \frac{15.2}{53} \quad \frac{16.1}{65}$$

$$\frac{6.2}{30} \quad \frac{6.6}{22} \quad \frac{45}{17}$$

$$\frac{5.1}{17} \quad \frac{6.4}{25} \quad \frac{8.7}{32} \quad \frac{16.0}{54} \quad \frac{17.8}{68}$$

$$\frac{5.8}{28} \quad \frac{6.8}{22} \quad \frac{4.7}{17}$$

$$\frac{5.4}{15} \quad \frac{6.6}{18} \quad \frac{11.6}{45} \quad \frac{16.2}{68} \quad \frac{17.3}{70}$$

$$\frac{6.7}{27} \quad \frac{7.2}{20} \quad \frac{5.4}{17}$$

$$\frac{5.8}{50} \quad \frac{7.4}{19} \quad \frac{15.3}{49} \quad \frac{16.6}{65}$$

$$\frac{7.1}{26} \quad \frac{7.4}{21} \quad \frac{5.4}{17}$$

$$\frac{6.1}{15} \quad \frac{8.2}{22} \quad \frac{16.2}{46} \quad \frac{17.3}{65}$$

$$\frac{7.2}{28} \quad \frac{7.6}{22} \quad \frac{5.5}{16}$$

$$\frac{6.3}{16} \quad \frac{8.7}{22} \quad \frac{15.7}{44} \quad \frac{16.5}{50}$$

$$\frac{3.4}{50} \quad \frac{5.4}{32} \quad \frac{6.6}{30} \quad \frac{6.5}{22} \quad \frac{3.9}{16}$$

$$\frac{5.2}{17} \quad \frac{10.1}{32} \quad \frac{12.6}{50}$$

$$\frac{5.4}{50} \quad \frac{6.6}{23} \quad \frac{3.9}{16}$$

$$\frac{5.5}{15} \quad \frac{5.9}{19} \quad \frac{11.4}{34} \quad \frac{12.7}{50}$$

$$\frac{3.8}{50} \quad \frac{5.5}{32} \quad \frac{6.6}{30} \quad \frac{7.0}{24} \quad \frac{4.2}{16} \quad 44$$

$$\frac{5.7}{15} \quad \frac{6.3}{20} \quad \frac{10.6}{29} \quad \frac{12.0}{50}$$

$$\frac{11.0}{29} \text{ Inv}$$

$$\frac{8.2}{24} \text{ Inv}$$

$$\frac{2.1}{50} \quad \frac{5.2}{28} \quad \frac{6.2}{26} \quad \frac{6.3}{22} \quad \frac{4.0}{17}$$

$$\frac{5.8}{18} \quad \frac{11.1}{32} \quad \frac{12.0}{50}$$

$$\frac{1.2}{50} \quad \frac{4.1}{27} \quad \frac{6.0}{23} \quad \frac{6.0}{20} \quad \frac{3.9}{16}$$

$$\frac{5.2}{17} \quad \frac{9.7}{28} \quad \frac{11.4}{50}$$

Sta. + π — Elev

902.96 903.0

136+68 24" X Drain

137

+50

138

T.P. 10.12 911.61 1.47 901.49

+50

11.6

139

+47

+55

+65

+68

140

11.62"

+25

Lt.

L

Rt.

Inv

Inv

$$\frac{3.3}{50} \quad \frac{4.8}{25} \quad \frac{6.0}{22} \quad \frac{6.8}{19} \quad \frac{3.4}{15} \quad 39 \quad \frac{4.5}{17} \quad \frac{11.2}{33} \quad \frac{11.8}{36} \quad \frac{11.9}{50}$$

$$\frac{3.2}{50} \quad \frac{4.1}{26} \quad \frac{5.1}{24} \quad \frac{5.7}{21} \quad \frac{4.9}{18} \quad \frac{3.1}{15} \quad 34 \quad \frac{4.2}{19} \quad \frac{10.5}{21} \quad \frac{12.0}{42} \quad \frac{12.5}{50}$$

$$\frac{3.5}{50} \quad \frac{3.3}{28} \quad \frac{4.7}{25} \quad \frac{4.4}{24} \quad \frac{4.3}{21} \quad \frac{2.5}{17} \quad 2.4 \quad \frac{3.5}{19} \quad \frac{10.0}{33} \quad \frac{11.0}{50}$$

$$\frac{3.0}{50} \quad \frac{3.0}{29} \quad \frac{3.4}{21} \quad \frac{1.6}{17} \quad 1.5 \quad \frac{1.9}{17} \quad \frac{5.6}{26} \quad \frac{7.2}{35} \quad \frac{7.4}{50}$$

$$\frac{9.7}{50} \quad \frac{9.6}{34} \quad \frac{11.2}{31} \quad \frac{11.1}{21} \quad \frac{9.1}{17} \quad 9.0 \quad \frac{9.4}{17} \quad \frac{11.2}{24} \quad \frac{11.7}{29} \quad \frac{11.0}{36} \quad \frac{11.5}{50}$$

$$\frac{5.7}{50} \quad \frac{4.4}{33} \quad \frac{9.9}{26} \quad \frac{10.0}{21} \quad \frac{7.9}{16} \quad 7.8 \quad \frac{8.0}{16} \quad \frac{10.1}{22} \quad \frac{10.5}{28} \quad \frac{6.2}{34} \quad \frac{7.9}{50}$$

$$\frac{3.2}{50} \quad \frac{2.0}{33} \quad \frac{8.1}{21} \quad \frac{8.1}{20} \quad \frac{6.4}{17} \quad 6.7 \quad \frac{6.9}{15} \quad \frac{9.3}{21} \quad \frac{9.0}{27} \quad \frac{3.6}{34} \quad \frac{4.2}{39} \quad \frac{4.6}{50}$$

$$\frac{6.3}{50} \quad \frac{7.7}{28} \quad \frac{8.0}{21} \quad \frac{6.3}{17} \quad 6.6 \quad \frac{6.8}{16} \quad \frac{9.2}{21-26} \quad \frac{3.3}{33} \quad \frac{4.4}{50}$$

$$\frac{4.4}{50} \quad \frac{4.8}{41} \quad \frac{7.0}{32} \quad \frac{7.2}{24} \quad \frac{5.8}{20} \quad 6.4 \quad \frac{6.6}{16} \quad \frac{8.9}{21-26} \quad \frac{2.4}{34} \quad \frac{3.6}{50}$$

$$\frac{4.2}{50} \quad \frac{5.7}{22} \quad 6.3 \quad \frac{6.5}{16} \quad \frac{8.9}{21-26} \quad \frac{2.3}{34} \quad \frac{3.3}{50}$$

$$\frac{4.6}{50} \quad \frac{5.4}{12} \quad 5.6 \quad \frac{5.8}{16} \quad \frac{8.6}{23} \quad \frac{7.9}{26} \quad \frac{2.0}{34} \quad \frac{2.5}{50}$$

$$\frac{0.0}{56} \quad \frac{6.0}{43} \quad \frac{6.7}{38-33} \quad \frac{5.1}{28} \quad 5.0 \quad \frac{5.2}{16} \quad \frac{8.4}{23} \quad \frac{7.5}{27} \quad \frac{2.6}{34} \quad \frac{2.6}{50}$$

Sta	+	π	-	Elev
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		911.61		
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140+40				
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+50	24" X	Drain		
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B.M	10.12	918.38	3.36	908.25 908.26
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141		18.4		
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+50				
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142				
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+50				
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143				
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+25				
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+50				
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+75				
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+83				
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144				
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L-1

2

Rt.

$$\frac{10.3}{50} \quad \frac{0.0}{34} \quad \frac{6.2}{26} \quad \frac{70}{24.2} \quad \frac{43}{16} \quad 4.6 \quad \frac{4.7}{16} \quad \frac{7.8}{22} \quad \frac{78}{26} \quad \frac{70}{28} \quad \frac{27}{33} \quad \frac{2.7}{50}$$

$$\frac{10.3}{50} \quad \frac{0.3}{32} \quad \frac{7.4}{24} \quad \frac{74}{21} \quad \frac{76}{21} \quad \frac{41}{15} \quad 4.6 \quad \frac{4.6}{16} \quad \frac{86}{24} \quad \frac{7.6}{28} \quad \frac{25}{34} \quad \frac{2.5}{50}$$

SPK 17 PP 28' Rt Sta 141+06

$$\frac{6.8}{50} \quad \frac{7.9}{32} \quad \frac{11.9}{27} \quad \frac{12.2}{23} \quad \frac{11.9}{28} \quad \frac{10.2}{16} \quad 10.3 \quad \frac{10.4}{17} \quad \frac{12.1}{21} \quad \frac{12.5}{24} \quad \frac{11.8}{29} \quad \frac{7.9}{33} \quad \frac{8.2}{50}$$

$$\frac{9.7}{50} \quad \frac{9.3}{34} \quad \frac{10.7}{27.22} \quad \frac{9.3}{17} \quad 9.3 \quad \frac{9.4}{16} \quad \frac{11.2}{20} \quad \frac{10.7}{28} \quad \frac{7.2}{33} \quad \frac{6.9}{50}$$

$$\frac{11.2}{50} \quad \frac{100}{22} \quad \frac{83}{16} \quad 8.6 \quad \frac{8.8}{15} \quad \frac{106}{19} \quad \frac{10.7}{28} \quad \frac{9.7}{32} \quad \frac{9.4}{50}$$

$$\frac{11.0}{50} \quad \frac{10.2}{22} \quad \frac{7.8}{17} \quad 8.9 \quad \frac{8.4}{17} \quad \frac{10.8}{22} \quad \frac{12.0}{50}$$

$$\frac{10.5}{50} \quad \frac{9.2}{23} \quad \frac{6.9}{18} \quad 7.0 \quad \frac{7.7}{20} \quad \frac{10.8}{27} \quad \frac{11.2}{50}$$

$$\frac{9.9}{50} \quad \frac{9.3}{30} \quad \frac{8.7}{23} \quad \frac{6.4}{17} \quad 6.4 \quad \frac{7.1}{27} \quad \frac{9.1}{34} \quad \frac{9.9}{50}$$

$$\frac{9.1}{50} \quad \frac{7.6}{22} \quad \frac{6.5}{17} \quad \frac{6.0}{12} \quad 5.7 \quad \frac{5.5}{23} \quad \frac{6.1}{47} \quad \frac{7.8}{53}$$

$$\frac{8.2}{50} \quad \frac{6.2}{24} \quad \frac{7.0}{21} \quad \frac{6.7}{15} \quad \frac{5.5}{12} \quad 5.1 \quad \frac{5.2}{25} \quad \frac{5.2}{41} \quad \frac{4.9}{50}$$

$$\frac{7.6}{50} \quad \frac{6.1}{25} \quad \frac{6.7}{21} \quad \frac{6.5}{16} \quad \frac{5.3}{12} \quad 4.9 \quad \frac{5.2}{22} \quad \frac{6.2}{24.29} \quad \frac{2.0}{41} \quad \frac{2.3}{50}$$

$$\frac{7.1}{50} \quad \frac{5.3}{27} \quad \frac{6.0}{25} \quad \frac{6.0}{17} \quad \frac{4.9}{13} \quad 4.4 \quad \frac{4.8}{19} \quad \frac{5.8}{23} \quad \frac{5.3}{30} \quad \frac{1.6}{37} \quad \frac{2.0}{50}$$

Sta	+	Δ	-	Elev
		918.38		
144+50				
T.P.	10.41	927.67	1.12	917.26
145		27.7		
+50				
146				
+50				
147				
+50				
148				
T.P.	12.21	939.50	0.38	927.29
+50		39.5		
149				
+50				
150				
T.P.	11.41	949.48	1.43	938.07

Lt

A

Rt

$$\frac{2.2}{50} \quad \frac{1.8}{32} \quad \frac{4.1}{28} \quad \frac{4.1}{20} \quad \frac{3.1}{10} \quad 2.9 \quad \frac{3.1}{14} \quad \frac{4.0}{22} \quad \frac{3.8}{26} \quad \frac{1.8}{30} \quad \frac{3.3}{50}$$

$$\frac{9.0}{50} \quad \frac{8.6}{33} \quad \frac{11.7}{26} \quad \frac{11.7}{20} \quad \frac{11.2}{18} \quad \frac{10.7}{9} \quad 10.5 \quad \frac{10.8}{14} \quad \frac{12.0}{26} \quad \frac{14.9}{44} \quad \frac{14.9}{50}$$

$$\frac{7.7}{50} \quad \frac{7.3}{33} \quad \frac{10.1}{27} \quad \frac{10.0}{21} \quad \frac{9.5}{19} \quad \frac{9.1}{9} \quad 8.9 \quad \frac{9.1}{10} \quad \frac{9.6}{17} \quad \frac{14.3}{34} \quad \frac{15.0}{50}$$

$$\frac{6.3}{50} \quad \frac{6.3}{33} \quad \frac{8.8}{28} \quad \frac{8.9}{21} \quad \frac{7.8}{18} \quad \frac{7.3}{9} \quad 7.3 \quad \frac{7.4}{10} \quad \frac{8.3}{18} \quad \frac{13.5}{33} \quad \frac{14.0}{50}$$

$$\frac{6.9}{50} \quad \frac{6.6}{33} \quad \frac{7.2}{28} \quad \frac{7.0}{21} \quad \frac{6.5}{19} \quad \frac{5.8}{9} \quad 5.8 \quad \frac{5.9}{10} \quad \frac{6.8}{17} \quad \frac{11.1}{34} \quad \frac{12.0}{50}$$

$$\frac{7.4}{50} \quad \frac{6.0}{37} \quad \frac{5.6}{21} \quad \frac{5.0}{19} \quad \frac{4.6}{15} \quad 4.2 \quad \frac{4.4}{11} \quad \frac{5.1}{18} \quad \frac{7.5}{26} \quad \frac{8.4}{50}$$

$$\frac{8.1}{50} \quad \frac{4.7}{24} \quad \frac{3.2}{18} \quad \frac{2.5}{10} \quad 2.3 \quad \frac{2.4}{11} \quad \frac{2.7}{17} \quad \frac{4.0}{22} \quad \frac{4.2}{29} \quad \frac{3.5}{32} \quad \frac{3.3}{50}$$

$$\frac{6.8}{50} \quad \frac{3.5}{23} \quad \frac{1.5}{19} \quad \frac{0.8}{11} \quad 0.5 \quad \frac{0.6}{10} \quad \frac{1.1}{17} \quad \frac{3.8}{24} \quad \frac{3.7}{50}$$

$$\frac{15.0}{50} \quad \frac{13.6}{24} \quad \frac{11.2}{18} \quad \frac{10.5}{9} \quad 10.3 \quad \frac{10.5}{7} \quad \frac{11.1}{17} \quad \frac{14.0}{26} \quad \frac{14.3}{50}$$

$$\frac{10.6}{50} \quad \frac{10.5}{26} \quad \frac{10.4}{22} \quad \frac{9.0}{17} \quad \frac{8.4}{9} \quad 8.2 \quad \frac{8.4}{12} \quad \frac{9.1}{18} \quad \frac{10.7}{23} \quad \frac{11.0}{50}$$

$$\frac{6.0}{50} \quad \frac{6.1}{42} \quad \frac{7.5}{27} \quad \frac{7.6}{20} \quad \frac{6.9}{18} \quad \frac{6.1}{9} \quad 5.9 \quad \frac{6.5}{18} \quad \frac{7.9}{22} \quad \frac{7.8}{31} \quad \frac{7.6}{33} \quad \frac{7.3}{50}$$

$$\frac{2.5}{50} \quad \frac{4.0}{32} \quad \frac{5.1}{28} \quad \frac{5.1}{19} \quad \frac{4.4}{17} \quad \frac{3.7}{9} \quad 3.5 \quad \frac{3.6}{10} \quad \frac{4.3}{18} \quad \frac{5.1}{21} \quad \frac{5.1}{31} \quad \frac{4.8}{33} \quad \frac{4.9}{50}$$

Sta	+	π	-	Elev
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		949.48		
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		49.5		
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150+50				
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151				
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+50				
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152				
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T.P.	10.81	959.66	0.63	948.85
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+50				
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		59.7		
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153				
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+50				
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154				
-----	--	--	--	--

+50				
-----	--	--	--	--

155				
-----	--	--	--	--

+50				
-----	--	--	--	--

156				
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B.M	2.64	959.65	2.64	957.02 957.01
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LT

2

RT

95	103	127	126	117	111	109	110	117	126	129	125	127
50	33	28	21	18	9	109	10	18	22	29	31	50

64	73	97	96	88	84	82	84	89	99	102	89	91
50	32	28	20	18	8	82	11	18	22	29	32	50

45	48	70	69	63	57	55	56	61	72	72	49	52
50	33	29	20	18	9	55	10	18	22	27	32	50

01	08	44	46	35	30	27	28	33	47	47	08	07
50	33	26	21	18	9	27	10	17	20	25	33	50

60	64	124	114	108		107	108	112	126	119	67	68
50	33	24-21	18	9		107	9	17	20	24	32	50

38	46	101	101	92	89	87	87	91	107	99	37	24
50	32	25	21	18	9	87	10	16	21	25	33	50

30	33	84	87	78	71	71	72	79	90	83	13	06
50	33	25	20	18	9	71	10	18	20	24	33	50

25	27	73	78	64	62	60	62	66	75	71	27	14
50	33	26	20	17	10	60	10	17	20	26	33	50

42	35	71	70	57	54	52	53	58	67	61	0.4	+0.2
50	33	27	21	19	9	52	10	17	20	25	33	50

43	37	66	65	52	50	48	48	51	64	64	0.9	0.0
50	33	28	20	16	9	48	10	17	20	26	33	50

55	40	28	66	64	54	50	50	53	61	58	12	12
50	43	33	25	20	17	8	49	8	17	20	25	33

55	32	68	67	54	52	51	51	55	66	56	0.5	0.3
50	33	26	20	16	10	51	10	16	20	25	33	50

Spk in 12" Oak 35' LT Sta 155+95

Sta	+	Δ	-	Elev
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		959.65		
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		69.7		
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156+50				
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157				
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T.P.	424	958.05	5.84	953.81
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+50		58.0		
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158				
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+50				
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159				
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+50				
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160				
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+50				
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+71				
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161				
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+50				
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Lt

A

Rt

$$\frac{6.9}{50} \frac{4.3}{33} \frac{7.2}{26} \frac{7.2}{20} \frac{5.9}{17} \frac{5.5}{9} \frac{5.4}{10} \frac{6.1}{17} \frac{7.2}{20} \frac{6.8}{26} \frac{3.1}{33} \frac{1.8}{50}$$

$$\frac{11.0}{50} \frac{10.1}{33} \frac{9.5}{26} \frac{6.3}{17} \frac{5.7}{9} \frac{5.6}{9} \frac{5.7}{9} \frac{6.2}{17} \frac{8.7}{25} \frac{9.5}{34} \frac{7.6}{50}$$

$$\frac{12.7}{50} \frac{12.3}{33} \frac{4.9}{16} \frac{4.4}{9} \frac{4.2}{10} \frac{4.4}{10} \frac{5.0}{17} \frac{9.3}{30} \frac{8.8}{50}$$

$$\frac{13.0}{50} \frac{11.7}{32} \frac{5.4}{16} \frac{4.8}{9} \frac{4.5}{9} \frac{4.8}{9} \frac{5.4}{16} \frac{10.5}{31} \frac{10.3}{50}$$

$$\frac{8.5}{50} \frac{9.4}{37} \frac{9.8}{27} \frac{5.4}{16} \frac{5.0}{10} \frac{4.7}{10} \frac{5.1}{10} \frac{5.5}{17} \frac{12.7}{33} \frac{13.6}{50}$$

$$\frac{4.3}{50} \frac{5.8}{32} \frac{7.4}{29} \frac{7.2}{21} \frac{5.6}{17} \frac{5.1}{9} \frac{4.8}{10} \frac{5.1}{10} \frac{5.7}{17} \frac{12.4}{35} \frac{14.2}{50}$$

$$\frac{4.1}{50} \frac{3.8}{32} \frac{7.3}{27} \frac{7.2}{21} \frac{5.7}{17} \frac{5.3}{9} \frac{5.1}{9} \frac{5.2}{9} \frac{5.6}{16} \frac{7.1}{21} \frac{8.2}{31} \frac{11.3}{50}$$

$$\frac{3.4}{50} \frac{3.9}{32} \frac{7.4}{25} \frac{7.0}{21} \frac{6.1}{17} \frac{5.5}{10} \frac{5.3}{10} \frac{5.4}{10} \frac{6.0}{17} \frac{7.1}{20} \frac{7.2}{29} \frac{6.9}{31} \frac{9.6}{50}$$

$$\frac{11.5}{50} \frac{1.9}{32} \frac{6.7}{26} \frac{7.3}{23-20} \frac{5.9}{16} \frac{5.6}{9} \frac{5.6}{10} \frac{5.7}{10} \frac{6.0}{17} \frac{7.1}{20} \frac{7.1}{29} \frac{6.1}{31} \frac{7.8}{50}$$

$$\frac{0.6}{50} \frac{0.9}{33} \frac{6.4}{26} \frac{7.3}{23-20} \frac{6.1}{17} \frac{5.4}{9} \frac{5.6}{9} \frac{5.8}{9} \frac{6.0}{17} \frac{7.3}{21} \frac{7.3}{27} \frac{6.6}{31} \frac{7.9}{50}$$

$$\frac{1.7}{50} \frac{2.7}{32} \frac{6.8}{26} \frac{7.3}{23-20} \frac{6.2}{17} \frac{5.9}{9} \frac{5.7}{9} \frac{5.7}{9} \frac{6.2}{17} \frac{7.4}{22} \frac{7.5}{30} \frac{8.4}{50}$$

$$\frac{5.8}{50} \frac{5.5}{32} \frac{7.6}{28} \frac{7.5}{21} \frac{6.5}{18} \frac{6.1}{10} \frac{5.9}{9} \frac{6.1}{9} \frac{6.5}{17} \frac{9.5}{28} \frac{10.8}{50}$$

Sta	+	π	-	Elev
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958.05

58.0

162

+50

T.P.

4.72

956.70

6.07

951.98

163

+50

+65

164

+10

+50

165

+50

166

+50

Lt

K

Rt

$$\frac{8.4}{50} \frac{8.4}{36} \frac{8.0}{20} \frac{6.2}{16} \frac{6.2}{9} \frac{51.9}{61} \frac{6.1}{9} \frac{6.4}{16} \frac{7.5}{21} \frac{8.8}{32} \frac{9.7}{50}$$

$$\frac{11.0}{50} \frac{10.1}{30} \frac{6.6}{18} \frac{6.3}{9} \frac{51.9}{61} \frac{6.1}{9} \frac{6.6}{17} \frac{7.7}{19} \frac{8.6}{24} \frac{9.4}{50}$$

$$\frac{11.4}{50} \frac{10.8}{32} \frac{7.8}{22} \frac{5.5}{16} \frac{4.8}{9} \frac{52.1}{46} \frac{4.8}{9} \frac{5.2}{17} \frac{8.8}{29} \frac{9.7}{50}$$

$$\frac{7.9}{50} \frac{9.3}{35} \frac{8.5}{25} \frac{6.8}{20} \frac{5.4}{17} \frac{4.9}{9} \frac{4.9}{10} \frac{5.4}{17} \frac{9.9}{30} \frac{10.1}{50}$$

$$\frac{5.6}{50} \frac{6.2}{41} \frac{8.2}{29} \frac{7.3}{22} \frac{5.5}{18} \frac{5.0}{10} \frac{4.9}{9} \frac{5.5}{17} \frac{10.1}{32} \frac{10.3}{50}$$

$$\frac{3.8}{50} \frac{3.4}{33} \frac{6.4}{29} \frac{7.0}{26} \frac{6.7}{20} \frac{5.7}{17} \frac{5.1}{9} \frac{5.0}{9} \frac{5.5}{17} \frac{7.0}{22} \frac{8.1}{33} \frac{9.1}{50}$$

$$\frac{3.9}{50} \frac{3.1}{33} \frac{6.3}{28} \frac{7.0}{26} \frac{6.7}{20} \frac{5.7}{17} \frac{5.1}{10} \frac{5.0}{10} \frac{5.4}{17} \frac{7.0}{22} \frac{7.2}{32} \frac{8.3}{50}$$

$$\frac{2.8}{50} \frac{2.1}{33} \frac{6.1}{27} \frac{6.7}{24} \frac{6.7}{21} \frac{5.8}{18} \frac{5.0}{9} \frac{5.0}{9} \frac{5.1}{17} \frac{6.6}{21} \frac{6.3}{24} \frac{5.7}{27} \frac{2.0}{33} \frac{2.2}{50}$$

$$\frac{1.1}{50} \frac{1.3}{33} \frac{6.0}{27} \frac{6.6}{23-20} \frac{5.8}{17} \frac{5.0}{9} \frac{5.0}{10} \frac{5.6}{18} \frac{6.7}{21} \frac{6.7}{24} \frac{6.0}{28} \frac{3.0}{33} \frac{3.2}{50}$$

$$\frac{1.8}{50} \frac{2.0}{33} \frac{6.4}{27} \frac{6.9}{23-20} \frac{5.9}{17} \frac{5.3}{9} \frac{5.1}{10} \frac{5.6}{18} \frac{6.6}{21-23} \frac{5.7}{27} \frac{1.2}{33} \frac{1.2}{50}$$

$$\frac{7.6}{50} \frac{7.6}{36} \frac{7.1}{31} \frac{7.5}{28} \frac{7.2}{21} \frac{5.7}{17} \frac{5.2}{9} \frac{5.3}{10} \frac{5.7}{17} \frac{7.0}{20} \frac{7.1}{26} \frac{6.5}{29} \frac{4.6}{32} \frac{5.1}{50}$$

$$\frac{10.6}{50} \frac{9.7}{34} \frac{9.5}{28} \frac{6.9}{20} \frac{5.7}{17} \frac{5.1}{8} \frac{5.0}{10} \frac{5.5}{18} \frac{7.7}{24} \frac{7.8}{34} \frac{8.3}{50}$$

Sta	+	π	-	Elev
		956.70		

167

+40

168

+50

T.R	7.55	961.11	3.14	953.56
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169

+50

170

B.M	6.49	961.12	6.49	954.62	954.63
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+50

171

+50

172

+50

Lt

X

Rt

$$\frac{12.6}{50} \quad \frac{12.3}{40} \quad \frac{11.4}{30} \quad \frac{5.6}{17} \quad \frac{4.9}{8} \quad \frac{4.6}{10} \quad \frac{5.4}{18} \quad \frac{6.6}{21} \quad \frac{9.3}{29} \quad \frac{10.0}{35} \quad \frac{10.1}{50}$$

$$\frac{12.5}{50} \quad \frac{12.0}{36} \quad \frac{11.0}{29} \quad \frac{5.3}{17} \quad \frac{4.5}{8} \quad \frac{4.4}{10} \quad \frac{4.5}{10} \quad \frac{5.0}{18} \quad \frac{9.1}{32} \quad \frac{8.7}{50}$$

$$\frac{7.2}{50} \quad \frac{6.0}{21} \quad \frac{4.5}{17} \quad \frac{4.0}{8} \quad \frac{3.9}{0} \quad \frac{3.9}{9} \quad \frac{4.2}{18} \quad \frac{5.4}{21} \quad \frac{5.1}{30} \quad \frac{4.0}{33} \quad \frac{3.2}{50}$$

$$\frac{4.0}{50} \quad \frac{2.8}{31} \quad \frac{5.2}{27} \quad \frac{5.2}{20} \quad \frac{4.0}{18} \quad \frac{3.5}{8} \quad \frac{3.4}{10} \quad \frac{4.0}{18} \quad \frac{5.2}{21} \quad \frac{5.3}{29} \quad \frac{3.4}{32} \quad \frac{2.8}{50}$$

$$\frac{5.8}{50} \quad \frac{5.2}{33} \quad \frac{8.1}{28} \quad \frac{9.1}{25} \quad \frac{8.9}{20} \quad \frac{7.9}{17} \quad \frac{7.5}{9} \quad \frac{7.3}{10} \quad \frac{7.4}{18} \quad \frac{7.9}{18} \quad \frac{8.9}{20} \quad \frac{8.3}{26} \quad \frac{6.5}{30} \quad \frac{6.9}{33} \quad \frac{6.9}{50}$$

$$\frac{4.3}{50} \quad \frac{4.5}{32} \quad \frac{8.0}{27} \quad \frac{8.6}{25} \quad \frac{8.5}{20} \quad \frac{7.4}{17} \quad \frac{6.9}{9} \quad \frac{6.7}{10} \quad \frac{7.5}{18} \quad \frac{8.5}{21} \quad \frac{8.0}{27} \quad \frac{6.7}{29} \quad \frac{7.4}{32} \quad \frac{7.4}{50}$$

$$\frac{3.9}{50} \quad \frac{4.4}{32} \quad \frac{8.2}{27} \quad \frac{8.0}{20} \quad \frac{7.0}{17} \quad \frac{6.4}{8} \quad \frac{6.2}{9} \quad \frac{6.4}{18} \quad \frac{7.8}{21} \quad \frac{8.0}{28} \quad \frac{5.7}{32} \quad \frac{6.7}{50}$$

Top Mort Sta 170 + 4.5

$$\frac{4.2}{50} \quad \frac{4.6}{31} \quad \frac{7.3}{26} \quad \frac{7.3}{20} \quad \frac{6.2}{17} \quad \frac{6.0}{8} \quad \frac{5.8}{10} \quad \frac{6.3}{18} \quad \frac{7.6}{21} \quad \frac{7.8}{32} \quad \frac{7.3}{33} \quad \frac{8.7}{50}$$

$$\frac{4.1}{50} \quad \frac{4.5}{30} \quad \frac{6.7}{25} \quad \frac{7.0}{20} \quad \frac{5.7}{17} \quad \frac{5.5}{8} \quad \frac{5.4}{10} \quad \frac{5.5}{10} \quad \frac{6.1}{18} \quad \frac{7.0}{21} \quad \frac{7.0}{30} \quad \frac{5.6}{33} \quad \frac{7.2}{50}$$

$$\frac{4.8}{50} \quad \frac{4.9}{26} \quad \frac{4.2}{18} \quad \frac{5.0}{24} \quad \frac{5.0}{15} \quad \frac{5.0}{7} \quad \frac{5.0}{11} \quad \frac{5.3}{18} \quad \frac{5.8}{22} \quad \frac{6.9}{29} \quad \frac{6.9}{32} \quad \frac{5.5}{32} \quad \frac{6.3}{50}$$

$$\frac{3.6}{50} \quad \frac{4.1}{26} \quad \frac{6.4}{23} \quad \frac{5.1}{20} \quad \frac{5.1}{16} \quad \frac{5.1}{8} \quad \frac{5.1}{10} \quad \frac{5.6}{18} \quad \frac{7.6}{23} \quad \frac{9.1}{50}$$

$$\frac{2.6}{50} \quad \frac{3.4}{36} \quad \frac{5.4}{26} \quad \frac{6.9}{22} \quad \frac{5.5}{20} \quad \frac{5.1}{16} \quad \frac{4.8}{8} \quad \frac{5.1}{10} \quad \frac{5.8}{18} \quad \frac{11.0}{33} \quad \frac{11.5}{50}$$

Sta	+	π	-	Elev
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		961.12		
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173				
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+50				
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+96	24" X Drain			
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174				
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+50				
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175				
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T.P.	447	960.07	5.52	955.60
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+50				
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176				
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+50				
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177				
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+50				
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178				
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+51	24" X Drain			
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L+

2

R+

$\frac{5.5}{50}$	$\frac{7.0}{27}$	$\frac{7.2}{20}$	$\frac{5.6}{17}$	$\frac{5.0}{9}$	48	$\frac{5.1}{10}$	$\frac{5.7}{17}$	$\frac{11.0}{32}$	$\frac{11.8}{50}$
$\frac{9.1}{50}$	$\frac{8.7}{26}$	$\frac{5.8}{17}$	$\frac{5.3}{10}$	5.0	5.0	$\frac{5.4}{10}$	$\frac{6.0}{18}$	$\frac{11.1}{32}$	$\frac{12.0}{50}$
		$\frac{10.3}{Inv}$					$\frac{10.6}{Inv}$		
$\frac{9.7}{50}$	$\frac{9.8}{29}$	$\frac{6.3}{18}$	$\frac{5.5}{10}$	5.1	5.1	$\frac{5.4}{10}$	$\frac{5.9}{18}$	$\frac{9.4}{27}$	$\frac{9.6}{31}$
								$\frac{9.0}{35}$	$\frac{9.1}{50}$
$\frac{8.9}{50}$	$\frac{8.8}{27}$	$\frac{6.3}{19}$	$\frac{5.6}{10}$	5.1	5.1	$\frac{5.4}{10}$	$\frac{5.8}{17}$	$\frac{7.8}{21}$	$\frac{8.2}{28}$
								$\frac{6.2}{31}$	$\frac{6.0}{50}$
$\frac{8.0}{50}$	$\frac{7.5}{22}$	$\frac{6.2}{18}$	$\frac{5.4}{10}$	5.3	5.3	$\frac{5.7}{9}$	$\frac{6.3}{17}$	$\frac{7.4}{20-23}$	$\frac{6.8}{27}$
								$\frac{3.0}{33}$	$\frac{3.1}{50}$
$\frac{5.4}{50}$	$\frac{6.0}{25}$	$\frac{6.0}{21}$	$\frac{4.7}{18}$	$\frac{4.2}{10}$	4.2	$\frac{4.7}{11}$	$\frac{5.3}{17}$	$\frac{6.1}{20}$	$\frac{6.3}{25}$
								$\frac{5.9}{28}$	$\frac{2.8}{33}$
								$\frac{2.6}{50}$	
$\frac{2.2}{50}$	$\frac{2.9}{33}$	$\frac{5.5}{28}$	$\frac{5.5}{23}$	$\frac{5.1}{20}$	$\frac{4.3}{18}$	$\frac{4.0}{10}$	$\frac{4.3}{43}$	$\frac{4.9}{12}$	$\frac{5.7}{19}$
								$\frac{6.5}{22}$	$\frac{6.4}{29}$
								$\frac{3.9}{33}$	$\frac{4.1}{50}$
$\frac{0.8}{50}$	$\frac{0.9}{31}$	$\frac{4.9}{24}$	$\frac{5.1}{20}$	$\frac{4.3}{16}$	4.3	$\frac{5.2}{12}$	$\frac{5.8}{19}$	$\frac{6.5}{21}$	$\frac{6.9}{29}$
								$\frac{4.1}{34}$	$\frac{4.6}{50}$
$\frac{1.9}{50}$	$\frac{2.6}{32}$	$\frac{5.7}{26}$	$\frac{5.6}{20}$	$\frac{4.3}{16}$	$\frac{4.4}{9}$	4.7	$\frac{5.5}{13}$	$\frac{6.9}{23-26}$	$\frac{6.2}{29}$
								$\frac{4.1}{33}$	$\frac{4.9}{50}$
$\frac{5.7}{50}$	$\frac{5.9}{32}$	$\frac{6.6}{36}$	$\frac{6.5}{24}$	$\frac{6.0}{20}$	$\frac{4.7}{14}$	5.0	$\frac{6.0}{13}$	$\frac{7.0}{20}$	$\frac{7.2}{27}$
								$\frac{4.6}{33}$	$\frac{6.0}{50}$
$\frac{9.1}{50}$	$\frac{8.6}{26}$	$\frac{5.2}{17}$				5.1	$\frac{6.0}{11}$	$\frac{6.7}{18}$	$\frac{7.9}{22}$
								$\frac{8.2}{50}$	
$\frac{10.3}{50}$	$\frac{11.7}{Inv}$	$\frac{10.1}{30}$	$\frac{6.0}{17}$	$\frac{5.4}{10}$	5.3	$\frac{5.8}{9}$	$\frac{6.4}{17}$	$\frac{9.9}{27}$	$\frac{11.8}{Inv}$
								$\frac{10.0}{50}$	

Sta	+	Δ	-	Elev
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		960.07		
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179				
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+50				
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180				
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+50				
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181				
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+50				
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T.P.	2.11	954.81	737	952.70
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182				
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+50				
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183				
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+50				
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184				
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+50				
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Lt

Z

Rt

$$\begin{array}{cccccccccccc} 10.5 & 9.8 & 9.1 & 6.4 & 5.7 & 5.5 & 5.6 & 5.9 & 7.8 & 8.3 & 7.3 & 7.7 \\ 50 & 31 & 25 & 18 & 10 & 5.5 & 10 & 17 & 23 & 31 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 10.6 & 10.5 & 9.7 & 6.6 & 6.1 & 5.6 & 5.8 & 6.1 & 7.4 & 7.3 & 4.8 & 4.6 \\ 50 & 31 & 25 & 17 & 10 & 5.6 & 9 & 17 & 21 & 28 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 10.3 & 9.9 & 9.3 & 7.6 & 6.4 & 6.0 & 5.9 & 6.2 & 7.6 & 6.7 & 2.3 & 2.1 \\ 50 & 30 & 25 & 20 & 17 & 10 & 9 & 17 & 20 & 27 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 9.8 & 8.1 & 7.9 & 6.5 & 6.3 & 5.9 & 6.1 & 6.4 & 7.9 & 7.9 & 7.0 & 3.2 & 3.1 \\ 50 & 31 & 21 & 17 & 10 & 5.9 & 9 & 17 & 21 & 23 & 27 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 8.2 & 7.6 & 8.7 & 8.5 & 7.0 & 6.6 & 6.4 & 6.9 & 8.2 & 7.4 & 3.4 & 3.0 \\ 50 & 32 & 29 & 20 & 16 & 10 & 6.4 & 9 & 18 & 21 & 23 & 28 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 8.7 & 8.1 & 9.3 & 9.0 & 8.0 & 7.2 & 7.0 & 7.5 & 8.8 & 8.8 & 8.3 & 5.1 & 5.5 \\ 50 & 33 & 29 & 21 & 18 & 10 & 6.9 & 9 & 19 & 21 & 24 & 28 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 3.3 & 3.1 & 4.5 & 4.1 & 3.5 & 2.7 & 2.3 & 2.4 & 3.0 & 4.1 & 4.1 & 3.5 & 1.0 & 0.9 \\ 50 & 32 & 28 & 20 & 17 & 10 & 2.3 & 9 & 18 & 21 & 24 & 30 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 2.9 & 2.9 & 5.1 & 4.7 & 3.8 & 3.3 & 3.1 & 3.1 & 3.9 & 5.0 & 4.4 & 1.3 & 1.1 \\ 50 & 32 & 28 & 20 & 17 & 10 & 3.1 & 9 & 19 & 22 & 29 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 3.3 & 3.8 & 5.4 & 5.4 & 4.6 & 4.0 & 3.8 & 4.0 & 4.7 & 5.4 & 5.3 & 2.9 & 2.8 \\ 50 & 32 & 27 & 19 & 19 & 9 & 3.8 & 10 & 19 & 21 & 29 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 5.5 & 5.5 & 6.0 & 5.1 & 4.5 & 4.3 & 4.6 & 5.1 & 6.0 & 6.0 & 4.6 & 4.9 \\ 50 & 31 & 21 & 16 & 9 & 4.3 & 10 & 19 & 22 & 30 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 7.4 & 7.3 & 5.5 & 5.2 & 5.3 & 5.7 & 6.7 & 6.9 & 6.4 & 6.3 \\ 50 & 21 & 13 & 9 & 5.3 & 9 & 18 & 21 & 30 & 32 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 11.0 & 9.8 & 6.3 & 5.7 & 5.4 & 5.5 & 6.1 & 7.4 & 7.3 & 6.8 & 6.1 \\ 50 & 25 & 18 & 9 & 5.4 & 11 & 18 & 22 & 31 & 35 & 50 \end{array}$$

Sta + π - Elev

954.81

185

+50

186

+50

187

B.M

6.50

951.14

10.16

944.65

944.64

+50

51.1

188

+50

189

+50

190

+50

Lt

Z

Rt

$\frac{11.7}{50}$ $\frac{10.8}{27}$ $\frac{7.1}{16}$ $\frac{6.3}{9}$ 59 $\frac{6.0}{11}$ $\frac{6.6}{17}$ $\frac{8.0}{22}$ $\frac{8.1}{30}$ $\frac{7.7}{33}$ $\frac{7.8}{50}$

$\frac{11.5}{50}$ $\frac{11.0}{27}$ $\frac{7.6}{16}$ $\frac{7.0}{9}$ 64 $\frac{6.4}{11}$ $\frac{6.7}{17}$ $\frac{8.4}{22-29}$ $\frac{7.8}{34}$ $\frac{8.0}{50}$

$\frac{9.5}{50}$ $\frac{10.0}{44}$ $\frac{9.9}{24}$ $\frac{7.8}{17}$ $\frac{7.2}{7}$ 69 $\frac{6.9}{11}$ $\frac{7.5}{18}$ $\frac{8.6}{21}$ $\frac{8.7}{31}$ $\frac{7.8}{34}$ $\frac{7.8}{50}$

$\frac{8.6}{50}$ $\frac{8.6}{21}$ $\frac{7.8}{17}$ $\frac{7.4}{10}$ 73 $\frac{7.4}{11}$ $\frac{7.9}{18}$ $\frac{9.0}{21}$ $\frac{8.9}{30}$ $\frac{7.0}{33}$ $\frac{8.0}{50}$

$\frac{10.0}{50}$ $\frac{9.5}{21}$ $\frac{8.4}{17}$ $\frac{7.8}{11}$ 75 $\frac{7.6}{17}$ $\frac{7.6}{22}$ $\frac{9.8}{31}$ $\frac{9.4}{32}$ $\frac{10.0}{50}$

Spk 14 15" W. Oak 90' Rt Sta 187 to 5
 $\frac{6.9}{50}$ $\frac{6.1}{21}$ $\frac{4.7}{17}$ $\frac{4.1}{10}$ 40 $\frac{4.3}{11}$ $\frac{5.1}{19}$ $\frac{6.1}{22}$ $\frac{7.1}{26}$ $\frac{8.1}{33}$ $\frac{8.6}{50}$

$\frac{5.1}{50}$ $\frac{4.3}{33}$ $\frac{6.8}{28}$ $\frac{6.5}{22}$ $\frac{4.6}{17}$ $\frac{4.2}{8}$ 41 $\frac{4.2}{10}$ $\frac{5.1}{19}$ $\frac{7.5}{26}$ $\frac{8.7}{34}$ $\frac{9.0}{50}$

$\frac{2.9}{50}$ $\frac{2.5}{33}$ $\frac{6.9}{27}$ $\frac{6.6}{21}$ $\frac{4.9}{17}$ $\frac{4.5}{9}$ 42 $\frac{4.3}{10}$ $\frac{4.7}{18}$ $\frac{7.0}{24}$ $\frac{6.9}{33}$ $\frac{7.9}{35}$ $\frac{8.3}{50}$

$\frac{3.7}{50}$ $\frac{3.0}{33}$ $\frac{7.2}{26}$ $\frac{6.9}{21}$ $\frac{5.3}{14}$ $\frac{4.7}{9}$ 44 $\frac{4.4}{10}$ $\frac{4.7}{18}$ $\frac{6.9}{22}$ $\frac{7.0}{26}$ $\frac{6.4}{29}$ $\frac{3.7}{33}$ $\frac{6.9}{50}$

$\frac{4.6}{50}$ $\frac{3.3}{33}$ $\frac{7.3}{27}$ $\frac{7.1}{22}$ $\frac{5.2}{17}$ $\frac{4.8}{10}$ 46 $\frac{4.7}{9}$ $\frac{5.2}{17}$ $\frac{6.7}{21}$ $\frac{7.2}{25}$ $\frac{6.5}{28}$ $\frac{2.3}{33}$ $\frac{6.6}{50}$

$\frac{5.2}{50}$ $\frac{4.3}{33}$ $\frac{7.5}{27}$ $\frac{7.3}{21}$ $\frac{5.5}{16}$ $\frac{5.1}{9}$ 50 $\frac{5.1}{10}$ $\frac{5.5}{18}$ $\frac{7.4}{23}$ $\frac{7.5}{28}$ $\frac{6.7}{31}$ $\frac{4.7}{33}$ $\frac{7.6}{50}$

$\frac{6.1}{50}$ $\frac{5.1}{33}$ $\frac{8.0}{29}$ $\frac{7.7}{22}$ $\frac{5.8}{16}$ $\frac{5.4}{9}$ 53 $\frac{5.4}{10}$ $\frac{6.0}{18}$ $\frac{7.6}{23}$ $\frac{8.0}{28}$ $\frac{7.5}{29}$ $\frac{5.6}{33}$ $\frac{7.2}{50}$

Sta	+	π	-	Elev
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		951.14		
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191				
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		51.1		
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+50				
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192				
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+50				
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T.P	3.72	948.83	603	945.11
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193				
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		48.8		
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+50				
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194				
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+15	24" L Drain			
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+50				
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195				
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+50				
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196				
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Lt

K

R+

$$\begin{array}{cccccccccccccccc} \frac{5.7}{50} & \frac{5.4}{34} & \frac{8.2}{29} & \frac{7.9}{23} & \frac{5.7}{16} & \frac{5.6}{9} & 5.4 & \frac{5.5}{9} & \frac{6.0}{17} & \frac{8.0}{22} & \frac{8.2}{26} & \frac{7.6}{29} & \frac{4.1}{33} & \frac{5.5}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{4.1}{50} & \frac{4.8}{35} & \frac{8.6}{30} & \frac{8.3}{23} & \frac{6.3}{16} & \frac{5.8}{9} & 5.6 & \frac{5.7}{9} & \frac{6.4}{18} & \frac{8.4}{23} & \frac{8.6}{30} & \frac{6.5}{33} & \frac{7.5}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{3.4}{50} & \frac{4.6}{34} & \frac{8.5}{28} & \frac{8.3}{23} & \frac{6.3}{17} & \frac{5.9}{9} & 5.8 & \frac{5.9}{10} & \frac{6.7}{18} & \frac{8.6}{23} & \frac{8.8}{29} & & \frac{7.9}{33} & \frac{9.2}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{4.3}{50} & \frac{5.3}{33} & \frac{8.5}{29} & \frac{8.3}{23} & \frac{6.4}{17} & \frac{6.0}{9} & 5.9 & \frac{6.2}{11} & \frac{6.7}{18} & \frac{9.0}{24} & \frac{9.0}{30} & \frac{7.9}{32} & \frac{8.7}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{4.1}{50} & \frac{5.8}{34} & \frac{7.0}{31} & \frac{6.9}{24} & \frac{4.5}{17} & \frac{4.0}{9} & 3.9 & \frac{3.9}{10} & \frac{4.7}{17} & \frac{7.0}{23} & \frac{7.4}{30} & \frac{7.0}{32} & \frac{9.5}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{8.2}{50} & \frac{8.0}{28} & \frac{4.7}{17} & \frac{4.2}{9} & & & 4.0 & \frac{4.4}{10} & \frac{5.0}{17} & \frac{8.8}{28} & & & \frac{9.3}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{8.0}{50.47} & \frac{9.0}{42} & \frac{8.7}{29} & \frac{5.2}{18} & \frac{4.4}{9} & 4.3 & \frac{4.5}{9} & \frac{5.2}{17} & \frac{9.5}{28} & & & & \frac{10.0}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{8.2}{50} & \frac{9.2}{45} & \frac{9.7}{30} & \frac{5.4}{19} & \frac{4.5}{10} & 4.4 & \frac{4.7}{9} & \frac{5.2}{17} & \frac{10.4}{29} & \frac{9.8}{30} & \frac{10.0}{36} & \frac{9.5}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{8.0}{50} & \frac{8.0}{46} & \frac{9.4}{42} & \frac{8.1}{26} & \frac{5.3}{18} & \frac{4.7}{11} & 4.5 & \frac{4.8}{9} & \frac{5.4}{17} & \frac{9.6}{29} & \frac{9.6}{31} & \frac{8.6}{34} & \frac{8.6}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{8.0}{50} & \frac{8.5}{33} & \frac{7.8}{25} & \frac{5.1}{17} & \frac{4.7}{18} & 4.7 & \frac{5.0}{10} & \frac{5.5}{17} & \frac{9.7}{30-32} & & & & \frac{8.6}{33} & \frac{9.6}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{5.2}{50} & \frac{5.5}{34} & \frac{7.7}{30} & \frac{7.5}{23} & \frac{5.5}{18} & \frac{4.9}{10} & 4.9 & \frac{5.2}{10} & \frac{5.7}{17} & \frac{8.7}{25} & & & \frac{8.9}{33} & \frac{9.3}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{5.0}{50} & \frac{5.7}{34} & \frac{8.0}{30} & \frac{8.0}{23} & \frac{5.4}{16} & \frac{5.3}{10} & 5.1 & \frac{5.5}{10} & \frac{5.9}{17} & \frac{8.0}{22} & \frac{8.1}{30} & \frac{6.8}{33} & \frac{8.5}{50} \end{array}$$

Sta	+	Δ	-	Elev
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948.83

196+50

48.8

197

+50

+78

BM	6.90	948.87	6.90	941.93	941.97
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48.9

198

+50

+72

T.P.	4.95	947.44	6.38	942.49
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199 Approx $\pm$ Arbogast Rd

47.4

+50

200

+50

201

Lt.

2

Rt.

$$\frac{61}{50} \frac{67}{33} \frac{79}{31} \frac{80}{22} \frac{59}{16} \frac{55}{10} 54 \frac{56}{9} \frac{61}{17} \frac{82}{22} \frac{84}{29} \frac{21}{32} \frac{79}{50}$$

$$\frac{51}{50} \frac{53}{33} \frac{80}{29-22} \frac{60}{17} \frac{57}{10} 56 \frac{57}{10} \frac{61}{17} \frac{83}{23} \frac{83}{30} \frac{64}{32} \frac{80}{50}$$

$$\frac{70}{50} \frac{71}{33} \frac{83}{30} \frac{82}{22} \frac{63}{17} \frac{57}{9} 57 \frac{58}{9} \frac{63}{17} \frac{85}{22} \frac{87}{30} \frac{67}{32} \frac{80}{50}$$

$$\frac{81}{50} \frac{78}{33} \frac{88}{30} \frac{87}{22} \frac{61}{16} \frac{59}{9} 58 \frac{60}{10} \frac{63}{17} \frac{88}{23} \frac{89}{30} \frac{76}{33} \frac{85}{50}$$

$$\frac{82}{50} \frac{80}{33} \frac{89}{31} \frac{87}{23} \frac{65}{17} \frac{60}{10} 60 \frac{62}{10} \frac{66}{17} \frac{86}{22} \frac{88}{29} \frac{61}{33} \frac{69}{50}$$

$$\frac{78}{50} \frac{73}{34} \frac{88}{29} \frac{88}{24} \frac{65}{21} \frac{62}{11} 61 \frac{65}{10} \frac{67}{17} \frac{90}{22} \frac{92}{30} \frac{80}{33} \frac{83}{50}$$

$$\frac{83}{50} \frac{77}{37} \frac{69}{32} \frac{65}{14} 63 \frac{67}{10} \frac{71}{19} \frac{92}{24} \frac{94}{29} \frac{85}{33} \frac{88}{50}$$

$$\frac{57}{50} \frac{57}{34} \frac{77}{30} \frac{77}{24} \frac{56}{18} \frac{52}{12} 51 \frac{59}{22} \frac{69}{50} \frac{85}{100}$$

$$\frac{60}{50} \frac{62}{24} \frac{79}{30} \frac{77}{23} \frac{56}{17} \frac{51}{10} 52 \frac{58}{12} \frac{69}{24} \frac{75}{50}$$

$$\frac{45}{50} \frac{50}{34} \frac{80}{30} \frac{77}{24} \frac{55}{18} \frac{52}{11} 53 \frac{55}{8} \frac{58}{16} \frac{90}{24} \frac{88}{27} \frac{77}{31} \frac{80}{50}$$

$$\frac{13}{50} \frac{30}{35} \frac{78}{30} \frac{78}{22} \frac{53}{18} \frac{52}{10} 52 \frac{55}{8} \frac{63}{16} \frac{112}{28} \frac{97}{32} \frac{97}{50}$$

$$\frac{14}{50} \frac{32}{34} \frac{81}{29} \frac{81}{23} \frac{54}{19} \frac{51}{10} 52 \frac{55}{8} \frac{65}{18} \frac{123}{32} \frac{135}{50}$$

Sta + π - Elev

947.44

47.4

201750

202 24 X Drain

T.P. 6.18 949.11 45' 942.93

+50

49.1

"

203

+50

204

+50

205

T.P. 11.77 960.64 0.24 948.87

+50

60.6

206

+50

207

L1

K

R+

$$\frac{4.4}{50} \frac{4.9}{32} \frac{8.3}{28} \frac{8.0}{22} \frac{5.7}{16} \frac{5.2}{8} \frac{5.1}{11} \frac{5.6}{21} \frac{6.1}{21} \frac{12.5}{36} \frac{13.2}{50}$$

$$\frac{5.4}{50} \frac{6.1}{32} \frac{8.4}{29} \frac{8.3}{21} \frac{8.4}{21} \frac{5.4}{17} \frac{5.1}{10} \frac{4.9}{13} \frac{5.2}{21} \frac{5.8}{21} \frac{11.3}{34} \frac{11.0}{34} \frac{12.4}{50}$$

$$\frac{6.5}{60} \frac{7.7}{32} \frac{8.1}{29} \frac{8.7}{22} \frac{6.8}{16} \frac{6.3}{7} \frac{6.1}{12} \frac{7.2}{21} \frac{11.7}{33} \frac{13.4}{50}$$

$$\frac{7.5}{50} \frac{8.0}{33} \frac{8.4}{32} \frac{8.2}{24} \frac{6.1}{18} \frac{5.6}{9} \frac{5.4}{11} \frac{5.4}{18} \frac{6.0}{18} \frac{11.9}{33} \frac{13.4}{50}$$

$$\frac{6.4}{50} \frac{7.3}{38} \frac{7.2}{23} \frac{5.3}{18} \frac{4.7}{9} \frac{4.4}{9} \frac{4.3}{9} \frac{4.9}{18} \frac{8.9}{30} \frac{9.0}{50}$$

$$\frac{6.3}{50} \frac{6.1}{24} \frac{4.6}{21} \frac{4.0}{12} \frac{2.9}{6} \frac{3.4}{17} \frac{5.1}{22} \frac{5.5}{31} \frac{4.7}{32} \frac{3.5}{50}$$

$$\frac{5.1}{50} \frac{4.4}{24} \frac{3.6}{22} \frac{2.8}{15} \frac{1.7}{4} \frac{1.8}{17} \frac{4.3}{24} \frac{4.5}{38} \frac{4.3}{50}$$

$$\frac{2.4}{50} \frac{2.4}{36} \frac{3.1}{35} \frac{2.9}{24} \frac{1.5}{17} \frac{0.2}{4} \frac{0.1}{16} \frac{2.4}{22} \frac{2.6}{30} \frac{1.2}{32} \frac{1.1}{50}$$

$$\frac{10.0}{50} \frac{10.2}{37} \frac{12.5}{34} \frac{12.7}{27} \frac{12.2}{23} \frac{11.1}{15} \frac{10.0}{5} \frac{10.1}{16} \frac{12.4}{23} \frac{12.4}{30} \frac{11.0}{33} \frac{10.7}{50}$$

$$\frac{4.3}{50} \frac{4.5}{35} \frac{11.5}{28} \frac{11.1}{23} \frac{9.7}{16} \frac{9.4}{12} \frac{8.7}{7} \frac{9.0}{16} \frac{10.8}{21} \frac{10.1}{26} \frac{6.1}{32} \frac{6.6}{50}$$

$$\frac{3.6}{50} \frac{4.1}{34} \frac{9.8}{27} \frac{10.0}{24} \frac{8.6}{26} \frac{8.3}{17} \frac{7.8}{11} \frac{7.6}{8} \frac{7.8}{17} \frac{9.4}{21} \frac{8.2}{26} \frac{3.3}{32} \frac{3.0}{50}$$

$$\frac{3.3}{50} \frac{3.3}{34} \frac{7.8}{28} \frac{8.4}{26} \frac{8.3}{23} \frac{6.9}{18} \frac{6.3}{10} \frac{6.1}{9} \frac{6.7}{17} \frac{8.0}{20} \frac{7.0}{26} \frac{2.7}{32} \frac{4.1}{50}$$

Sta	+	π	-	Elev
		960.64		
207+50		60.6		

208

+50

209

+29

+50

+70

210

T.P.	8.05	968.50	0.19	960.45
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+50

211

+50

212

L

R

Rt

$$\frac{1.9}{50} \quad \frac{1.5}{35} \quad \frac{7.1}{27-24} \quad \frac{6.0}{21} \quad \frac{4.9}{12} \quad \frac{55.9}{4.7} \quad \frac{49.54}{9} \quad \frac{6.7}{17} \quad \frac{5.9}{26} \quad \frac{2.2}{26} \quad \frac{4.4}{32} \quad \frac{4.4}{50}$$

$$\frac{4.3}{50} \quad \frac{3.8}{34} \quad \frac{6.0}{31} \quad \frac{5.7}{23} \quad \frac{4.5}{20} \quad \frac{3.7}{10} \quad \frac{3.5}{35} \quad \frac{3.7}{9} \quad \frac{4.1}{17} \quad \frac{5.8}{21} \quad \frac{5.9}{28} \quad \frac{4.2}{32} \quad \frac{5.0}{50}$$

$$\frac{4.9}{50} \quad \frac{5.0}{40} \quad \frac{4.8}{24} \quad \frac{3.5}{19} \quad \frac{2.7}{12} \quad \frac{2.5}{25} \quad \frac{2.7}{8} \quad \frac{3.3}{16} \quad \frac{5.5}{21} \quad \frac{5.9}{27} \quad \frac{6.7}{35} \quad \frac{6.8}{50}$$

$$\frac{4.1}{50} \quad \frac{4.5}{32} \quad \frac{4.2}{24} \quad \frac{2.7}{19} \quad \frac{1.9}{11} \quad \frac{1.7}{1.7} \quad \frac{1.9}{9} \quad \frac{2.4}{16} \quad \frac{4.1}{21} \quad \frac{4.3}{30} \quad \frac{2.6}{33} \quad \frac{3.3}{50}$$

$$\frac{3.8}{50} \quad \frac{4.1}{34} \quad \frac{3.5}{23} \quad \frac{2.2}{19} \quad \frac{1.6}{11} \quad \frac{1.4}{1.4} \quad \frac{1.6}{8} \quad \frac{2.1}{16} \quad \frac{3.4}{20} \quad \frac{3.6}{28} \quad \frac{1.7}{33} \quad \frac{2.3}{50}$$

$$\frac{3.4}{50} \quad \frac{3.8}{33} \quad \frac{3.4}{24} \quad \frac{2.1}{20} \quad \frac{1.3}{11} \quad \frac{1.1}{1.1} \quad \frac{1.3}{8} \quad \frac{2.0}{16} \quad \frac{3.3}{20} \quad \frac{3.4}{29} \quad \frac{2.1}{33} \quad \frac{2.1}{50}$$

$$\frac{3.3}{50} \quad \frac{3.5}{33} \quad \frac{3.1}{23} \quad \frac{1.5}{18} \quad \frac{1.1}{11} \quad \frac{1.0}{1.0} \quad \frac{1.1}{8} \quad \frac{1.6}{16} \quad \frac{3.4}{21-29} \quad \frac{3.7}{50}$$

$$\frac{2.9}{50} \quad \frac{2.4}{34} \quad \frac{3.2}{33} \quad \frac{3.0}{23} \quad \frac{1.5}{19} \quad \frac{0.9}{11} \quad \frac{0.6}{0.6} \quad \frac{0.8}{8} \quad \frac{1.1}{16} \quad \frac{3.6}{25} \quad \frac{4.8}{31} \quad \frac{4.8}{50}$$

$$\frac{8.7}{50} \quad \frac{8.0}{35} \quad \frac{10.4}{31} \quad \frac{10.1}{24} \quad \frac{8.9}{19} \quad \frac{8.1}{14} \quad \frac{8.0}{8.0} \quad \frac{8.1}{7} \quad \frac{8.6}{17} \quad \frac{10.2}{21} \quad \frac{10.4}{28} \quad \frac{9.2}{32} \quad \frac{9.5}{50}$$

$$\frac{8.4}{50} \quad \frac{7.8}{34} \quad \frac{9.9}{29} \quad \frac{9.4}{21} \quad \frac{8.4}{19} \quad \frac{7.8}{14} \quad \frac{7.4}{7.4} \quad \frac{7.5}{9} \quad \frac{8.1}{16} \quad \frac{9.8}{21-27} \quad \frac{9.2}{30} \quad \frac{7.3}{33} \quad \frac{8.1}{50}$$

$$\frac{9.7}{50} \quad \frac{9.7}{33} \quad \frac{9.2}{23} \quad \frac{8.1}{19} \quad \frac{7.4}{13} \quad \frac{6.9}{6.9} \quad \frac{7.3}{10} \quad \frac{8.0}{17} \quad \frac{9.3}{20} \quad \frac{9.7}{29} \quad \frac{8.0}{31} \quad \frac{8.0}{50}$$

$$\frac{8.4}{50} \quad \frac{8.8}{34} \quad \frac{9.4}{33} \quad \frac{9.0}{22} \quad \frac{7.8}{19} \quad \frac{7.1}{14} \quad \frac{6.6}{6.6} \quad \frac{6.9}{12} \quad \frac{7.6}{17} \quad \frac{9.0}{20-26} \quad \frac{8.4}{29} \quad \frac{5.9}{32} \quad \frac{5.6}{50}$$

Sta	+	Δ	-	Elev	
		96850			
212+50					
213					
+50					
214					
+50					
B.M	5.14	96849	5.14	963.36	963.35
215					
+50					
216					
+50					
217					
+50					
T.P.	5.92	972.56	1.85	966.64	
218		72.6			

Lt.

★

Rt.

$$\frac{31}{50} \frac{42}{34} \frac{81}{29} \frac{96}{26} \frac{86}{21} \frac{75}{18} \frac{68}{11} \frac{64}{12} \frac{65}{12} \frac{72}{17} \frac{85}{20} \frac{85}{23} \frac{77}{26} \frac{40}{32} \frac{51}{50}$$

$$\frac{10.5}{50} \frac{20}{33} \frac{79}{28} \frac{85}{26-20} \frac{74}{18} \frac{68}{11} \frac{61}{9} \frac{5.8}{9} \frac{62}{17} \frac{79}{20-22} \frac{69}{26} \frac{1.1}{33} \frac{16}{46} \frac{20}{50}$$

$$\frac{1.2}{50} \frac{35}{33} \frac{81}{28-24} \frac{72}{20} \frac{68}{15} \frac{5.8}{18} \frac{5.5}{18} \frac{60}{19} \frac{77}{22} \frac{80}{30} \frac{74}{32} \frac{8.3}{50}$$

$$\frac{1.1}{50} \frac{29}{32} \frac{77}{26} \frac{77}{23} \frac{71}{21} \frac{67}{15} \frac{54}{6} \frac{5.1}{6} \frac{5.4}{16} \frac{74}{22} \frac{76}{31} \frac{71}{33} \frac{8.6}{50}$$

$$\frac{1.2}{50} \frac{21}{32} \frac{72}{26-24} \frac{68}{21} \frac{50}{4} \frac{47}{4} \frac{48}{17} \frac{69}{22} \frac{71}{32} \frac{64}{34} \frac{7.0}{50}$$

Sp K. in 15" W. Oak 50 Rt 50 214 + 90

$$\frac{2.6}{50} \frac{27}{34} \frac{70}{27-23} \frac{62}{20} \frac{47}{10} \frac{46}{18} \frac{44}{23} \frac{67}{32} \frac{68}{34} \frac{5.8}{34} \frac{7.0}{50}$$

$$\frac{46}{50} \frac{5.2}{32} \frac{67}{28} \frac{67}{20} \frac{60}{18} \frac{5.3}{12} \frac{46}{7} \frac{44}{19} \frac{46}{27} \frac{81}{33} \frac{8.7}{34} \frac{84}{34} \frac{9.4}{50}$$

$$\frac{34}{50} \frac{46}{33} \frac{64}{30} \frac{63}{21} \frac{49}{19} \frac{43}{9} \frac{39}{9} \frac{3.9}{9} \frac{44}{17} \frac{12.9}{35} \frac{14.4}{50}$$

$$\frac{1.3}{50} \frac{3.0}{34} \frac{5.8}{30} \frac{5.7}{21} \frac{3.8}{17} \frac{3.4}{8} \frac{3.1}{9} \frac{3.4}{9} \frac{41}{17} \frac{118}{34} \frac{133}{50}$$

$$\frac{10.3}{50} \frac{1.6}{33} \frac{5.5}{29} \frac{5.4}{21} \frac{34}{17} \frac{28}{9} \frac{24}{9} \frac{2.8}{9} \frac{3.4}{17} \frac{10.2}{34} \frac{12.0}{50}$$

$$\frac{2.3}{50} \frac{48}{34} \frac{60}{31} \frac{5.5}{22} \frac{26}{16} \frac{20}{9} \frac{1.8}{9} \frac{2.1}{9} \frac{2.7}{16} \frac{8.2}{30} \frac{108}{50}$$

$$\frac{8.0}{50} \frac{10.2}{36} \frac{10.0}{24} \frac{68}{16} \frac{5.9}{10} \frac{5.7}{9} \frac{6.1}{9} \frac{6.9}{17} \frac{161}{35} \frac{173}{50}$$

Sta	+	X	-	Elev
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218+33		972.56 72.6		
	24"	X Drain		

+50

+68

219

+13

+20

+50

220

T.P.	217	970.83 70.8	3.88	968.66
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+50

221

+50

222

L1

X

R+

Inv

Inv

$$\frac{7.7}{50} \frac{10.6}{36} \frac{10.9}{27} \frac{11.2}{26} \frac{6.5}{16} \frac{5.8}{10} \frac{5.6}{5.6} \frac{6.1}{8} \frac{7.3}{17} \frac{16.6}{35} \frac{17.9}{35} \frac{18.8}{50}$$

$$\frac{8.1}{50} \frac{10.1}{39} \frac{9.1}{23} \frac{6.3}{17} \frac{5.7}{10} \frac{5.5}{5.5} \frac{6.0}{8} \frac{6.7}{16} \frac{17.7}{36} \frac{18.7}{50}$$

$$\frac{8.5}{50} \frac{8.7}{27} \frac{6.1}{17} \frac{5.6}{9} \frac{5.4}{5.4} \frac{5.9}{9} \frac{6.8}{17} \frac{15.8}{36} \frac{16.7}{50}$$

$$\frac{7.4}{50} \frac{7.2}{32} \frac{7.7}{31} \frac{7.4}{20} \frac{5.8}{16} \frac{5.3}{9} \frac{5.3}{5.3} \frac{5.7}{9} \frac{6.4}{18} \frac{11.5}{28} \frac{13.6}{50}$$

$$\frac{6.3}{50} \frac{6.7}{32} \frac{7.6}{31} \frac{7.3}{20} \frac{5.5}{15} \frac{5.1}{10} \frac{5.2}{5.2} \frac{5.7}{10} \frac{6.2}{17} \frac{9.0}{23} \frac{12.2}{50}$$

$$\frac{5.7}{50} \frac{6.4}{33} \frac{7.6}{30} \frac{7.4}{20} \frac{5.4}{16} \frac{5.1}{9} \frac{5.2}{5.2} \frac{5.7}{10} \frac{6.2}{17} \frac{6.4}{26} \frac{6.8}{50}$$

$$\frac{2.5}{50} \frac{2.7}{33} \frac{7.0}{28} \frac{6.8}{20} \frac{5.4}{16} \frac{5.1}{9} \frac{5.2}{5.2} \frac{5.7}{9} \frac{6.3}{16} \frac{6.2}{50}$$

$$\frac{0.3}{50} \frac{0.8}{32} \frac{6.0}{25} \frac{6.5}{23} \frac{6.5}{18} \frac{5.3}{16} \frac{5.1}{9} \frac{5.4}{5.4} \frac{6.2}{12} \frac{6.5}{20} \frac{5.4}{23} \frac{5.5}{50}$$

Top N.E. Cor of North Brick Pier

$$\frac{11.7}{50} \frac{11.7}{40} \frac{5.6}{27.20} \frac{3.6}{16} \frac{3.8}{8} \frac{4.2}{4.2} \frac{5.0}{11} \frac{5.9}{20} \frac{4.1}{24} \frac{3.8}{50}$$

$$\frac{0.5}{50} \frac{3.3}{31} \frac{6.5}{26} \frac{6.3}{20} \frac{4.6}{16} \frac{4.6}{8} \frac{4.7}{4.7} \frac{6.0}{14} \frac{6.5}{18} \frac{7.1}{20} \frac{7.3}{26} \frac{5.2}{31} \frac{4.7}{50}$$

$$\frac{5.4}{50} \frac{6.3}{34} \frac{7.7}{32} \frac{7.4}{23} \frac{5.5}{18} \frac{5.6}{9} \frac{5.8}{5.8} \frac{7.0}{13} \frac{7.3}{18} \frac{9.5}{23} \frac{9.6}{29} \frac{7.2}{35} \frac{7.4}{50}$$

$$\frac{3.1}{50} \frac{3.5}{44} \frac{9.0}{33} \frac{8.5}{23} \frac{6.6}{18} \frac{6.6}{7} \frac{7.0}{7.0} \frac{7.9}{13} \frac{8.7}{18} \frac{11.4}{24} \frac{13.4}{50}$$

Sta	+	Δ	-	Elev
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970.83

222+50

223

+42

T.P.

1.98

963.31

950

961.33

222+50

223

+42

+65

224

+50

225

+50

T.P.

3.49

957.73

9.07

954.24

226

L1

E

R1

$$\frac{2.7}{60} \quad \frac{2.8}{53} \quad \frac{10.9}{35} \quad \frac{10.6}{22} \quad \frac{8.1}{17} \quad \frac{7.7}{9} \quad \frac{62.8}{80} \quad \frac{9.1}{11} \quad \frac{10.1}{18}$$

$$\frac{3.3}{65} \quad \frac{3.6}{58}$$

$$\frac{4.3}{70} \quad \frac{4.2}{62}$$

$$\frac{10.0}{34} \quad \frac{11.1}{50}$$

$$\frac{4.9}{38} \quad \frac{4.8}{23} \quad \frac{2.1}{17} \quad \frac{1.7}{9} \quad 20 \quad \frac{30}{10} \quad \frac{4.1}{17} \quad \frac{13.5}{35} \quad \frac{15.4}{50}$$

$$\frac{6.3}{41} \quad \frac{6.4}{23} \quad \frac{3.4}{16} \quad \frac{3.2}{9} \quad 33 \quad \frac{3.8}{10} \quad \frac{4.6}{17} \quad \frac{13.5}{39} \quad \frac{15.2}{50}$$

$$\frac{8.3}{51} \quad \frac{7.5}{24} \quad \frac{4.4}{16} \quad \frac{4.0}{9} \quad 39 \quad \frac{4.3}{10} \quad \frac{4.9}{18} \quad \frac{10.2}{29} \quad \frac{13.7}{41} \quad \frac{15.2}{50}$$

$$\frac{10.5}{50} \quad \frac{9.7}{28} \quad \frac{7.3}{24} \quad \frac{5.4}{16} \quad \frac{5.0}{9} \quad 50 \quad \frac{5.5}{11} \quad \frac{6.3}{17} \quad \frac{11.7}{30} \quad \frac{15.4}{50}$$

$$\frac{11.9}{50} \quad \frac{10.5}{25} \quad \frac{7.0}{16} \quad \frac{6.5}{7} \quad 63 \quad \frac{6.6}{11} \quad \frac{7.1}{16} \quad \frac{10.7}{26} \quad \frac{15.6}{50}$$

$$\frac{8.8}{50} \quad \frac{8.6}{27} \quad \frac{10.2}{25} \quad \frac{7.9}{19} \quad \frac{8.2}{15} \quad \frac{7.7}{8} \quad 74 \quad \frac{7.7}{10} \quad \frac{8.4}{18} \quad \frac{11.2}{25} \quad \frac{15.5}{50}$$

$$\frac{7.4}{50} \quad \frac{7.8}{29} \quad \frac{11.2}{24} \quad \frac{11.2}{20} \quad \frac{9.2}{16} \quad \frac{8.5}{7} \quad 83 \quad \frac{8.7}{9} \quad \frac{9.6}{17} \quad \frac{14.0}{27} \quad \frac{15.9}{50}$$

$$\frac{3.8}{50} \quad \frac{5.5}{28} \quad \frac{6.3}{25-20} \quad \frac{4.0}{15} \quad \frac{3.6}{7} \quad 35 \quad \frac{4.1}{9} \quad \frac{5.1}{18} \quad \frac{9.9}{29} \quad \frac{11.2}{50}$$

Sta + Δ - Elev

957.73

57.7

226+12

+50

227

+43

+60

+70

228 $\pm$ "E" West ✓

B.M. 3.74 957.73 3.74 953.99 953.99

+50

+66

+64.50 East Rail So Tracks

+75

+84.70 No Rail No Tracks

LT

F

RT

Inv

Inv

$$\frac{45}{15} \frac{56}{27} \frac{6.7}{25} \frac{6.9}{21} \frac{7.0}{20} \frac{4.3}{15} \frac{3.8}{7}$$

$$\frac{43}{10} \frac{5.2}{19} \frac{10.2}{30} \frac{10.0}{31} \frac{11.1}{50}$$

$$\frac{4.9}{50} \frac{5.4}{25} \frac{6.8}{24-20} \frac{5.0}{16} \frac{4.4}{8}$$

$$\frac{4.5}{10} \frac{5.1}{18} \frac{7.9}{24} \frac{10.3}{50}$$

$$\frac{4.3}{50} \frac{4.7}{26} \frac{6.7}{23-19} \frac{5.6}{15} \frac{4.8}{7}$$

$$\frac{4.6}{10} \frac{5.1}{17} \frac{7.4}{22} \frac{7.6}{29} \frac{4.7}{33} \frac{5.7}{50}$$

$$\frac{3.3}{50} \frac{3.0}{26} \frac{6.6}{22-19} \frac{5.3}{16}$$

$$\frac{5.0}{9} \frac{5.4}{17} \frac{6.7}{21} \frac{6.7}{25} \frac{6.2}{29} \frac{2.8}{33} \frac{4.6}{50}$$

$$\frac{3.9}{50} \frac{3.5}{38} \frac{6.3}{32-28} \frac{5.2}{27}$$

$$\frac{5.2}{9} \frac{5.4}{17} \frac{6.6}{21-25} \frac{5.7}{29} \frac{2.6}{32} \frac{3.4}{40} \frac{5.3}{50}$$

$$\frac{6.9}{50} \frac{6.7}{37} \frac{5.5}{33} \frac{5.1}{17}$$

$$\frac{5.1}{17} \frac{6.6}{21-25} \frac{5.6}{29} \frac{2.6}{32} \frac{4.5}{50}$$

$$\frac{5.7}{50} \frac{5.1}{50}$$

$$\frac{5.3}{14} \frac{5.2}{27} \frac{3.4}{33} \frac{4.5}{50}$$

Top. S.W. Bolt X Signal 16' Rt Stg 228 + 50

$$\frac{6.6}{50} \frac{5.8}{14} \frac{5.0}{37} \frac{5.7}{16} \frac{6.1}{28} \frac{3.7}{33} \frac{4.0}{41} \frac{5.4}{50}$$

$$\frac{6.4}{50} \frac{6.4}{20} \frac{5.9}{10} \frac{5.8}{5.9} \frac{5.8}{8} \frac{6.3}{13} \frac{6.9}{50}$$

51.95

5.98

$$\frac{4.7}{50} \frac{6.3}{13} \frac{6.0}{9} \frac{5.9}{5.9} \frac{6.5}{18} \frac{6.8}{50}$$

5.84

Sta + Δ - Elev

957.73

228+87

15" X Drain

+95

229

+10

+30

+50 $\pm$ E East

T.P. 10.93 96463 4.03 953.70

+83

230

+50

231

+50

+75

Lt.

Z

Rt

$$\frac{8.3}{50} \quad \frac{7.4}{41} \quad \frac{6.5}{19} \quad \frac{5.8}{11} \quad 5.7 \quad \frac{5.9}{12} \quad \frac{6.8}{50}$$

$$\frac{4.5}{50} \quad \frac{5.3}{30} \quad \frac{7.9}{27} \quad \frac{7.8}{20} \quad \frac{5.8}{15} \quad \frac{5.5}{8} \quad 5.5 \quad \frac{6.4}{18} \quad \frac{9.0}{22} \quad \frac{7.5}{31} \quad \frac{7.1}{50}$$

$$\frac{4.4}{50} \quad \frac{4.7}{32} \quad \frac{7.5}{27} \quad \frac{7.6}{20} \quad \frac{5.7}{16} \quad \frac{5.5}{11} \quad 5.4 \quad \frac{6.3}{14} \quad \frac{6.2}{21} \quad \frac{8.0}{24} \quad \frac{5.9}{27} \quad \frac{5.1}{50}$$

$$\frac{4.1}{50} \quad \frac{4.2}{31} \quad \frac{7.5}{26-20} \quad \frac{5.6}{15} \quad \frac{5.3}{9} \quad 5.2 \quad \frac{5.5}{7} \quad \frac{6.2}{21} \quad \frac{7.5}{26-29} \quad \frac{5.1}{35} \quad \frac{5.6}{50}$$

$$\frac{3.9}{50} \quad \frac{3.5}{30} \quad \frac{7.3}{26} \quad \frac{7.3}{21} \quad \frac{5.3}{16} \quad \frac{5.1}{8} \quad 4.8 \quad \frac{5.5}{20} \quad \frac{6.6}{22} \quad \frac{7.6}{50}$$

$$\frac{3.7}{50} \quad \frac{2.7}{30} \quad \frac{6.8}{25-19} \quad \frac{5.2}{15} \quad \frac{4.8}{8} \quad 4.5 \quad \frac{5.3}{29} \quad \frac{5.9}{50} \quad \frac{6.6}{100}$$

$$\frac{7.3}{50} \quad \frac{7.4}{30} \quad \frac{12.5}{26} \quad \frac{13.0}{22-19} \quad \frac{11.7}{15} \quad \frac{11.0}{8} \quad 10.8 \quad \frac{11.0}{11} \quad \frac{12.6}{36} \quad \frac{13.3}{45} \quad \frac{13.3}{50}$$

$$\frac{8.4}{50} \quad \frac{7.3}{30} \quad \frac{11.8}{24} \quad \frac{12.8}{22-19} \quad \frac{11.4}{15} \quad \frac{10.7}{7} \quad 10.5 \quad \frac{10.5}{17} \quad \frac{11.6}{22} \quad \frac{12.8}{27-29} \quad \frac{8.9}{37} \quad \frac{9.5}{50}$$

$$\frac{8.2}{50} \quad \frac{6.0}{30} \quad \frac{11.2}{25} \quad \frac{11.6}{22-19} \quad \frac{10.0}{15} \quad \frac{9.4}{8} \quad 9.2 \quad \frac{9.4}{9} \quad \frac{9.8}{18} \quad \frac{11.5}{22-25} \quad \frac{10.6}{29} \quad \frac{6.9}{32} \quad \frac{7.3}{50}$$

$$\frac{5.7}{50} \quad \frac{5.7}{30} \quad \frac{9.3}{27} \quad \frac{10.3}{24-21} \quad \frac{8.3}{16} \quad \frac{7.9}{8} \quad 7.8 \quad \frac{7.9}{9} \quad \frac{8.0}{17} \quad \frac{9.4}{21-24} \quad \frac{8.8}{28} \quad \frac{5.9}{32} \quad \frac{6.3}{50}$$

$$\frac{5.5}{50} \quad \frac{6.1}{32} \quad \frac{8.8}{28} \quad \frac{8.6}{21} \quad \frac{6.9}{15} \quad \frac{6.5}{8} \quad 6.4 \quad \frac{6.5}{9} \quad \frac{6.8}{18} \quad \frac{8.3}{21-23} \quad \frac{6.5}{28} \quad \frac{6.5}{50}$$

$$\frac{5.5}{50} \quad \frac{5.9}{31} \quad \frac{8.4}{28} \quad \frac{8.1}{20} \quad \frac{6.3}{15} \quad \frac{5.9}{8} \quad 5.8 \quad \frac{5.9}{9} \quad \frac{6.0}{17} \quad \frac{7.7}{21} \quad \frac{7.9}{24} \quad \frac{6.7}{29} \quad \frac{6.7}{50}$$

Sta	+	Δ	-	Elev
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		964.63		
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232				
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	+50			
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233				
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	+50			
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234				
-----	--	--	--	--

	+45			
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	+76			
--	-----	--	--	--

235				
-----	--	--	--	--

	+50			
--	-----	--	--	--

236				
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T.P	476	964.22	5.17	959.46
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	+50			
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237				
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Lt

±

Rt

$\frac{5.5}{50} \frac{6.0}{31} \frac{7.7}{28} \frac{7.5}{21} \frac{5.8}{15} \frac{5.5}{8} \frac{5.2}{5.4} \frac{5.4}{9} \frac{5.6}{17} \frac{7.4}{24} \frac{9.5}{50}$

$\frac{5.5}{50} \frac{6.1}{31} \frac{7.1}{30} \frac{6.6}{19} \frac{5.4}{15} \frac{5.1}{4.9} \frac{5.0}{10} \frac{5.2}{18} \frac{7.3}{23} \frac{8.0}{26} \frac{9.4}{50}$

$\frac{6.7}{50} \frac{6.9}{22} \frac{5.4}{17} 48 \frac{4.9}{8} \frac{5.1}{17} \frac{7.1}{23} \frac{6.1}{50}$

$\frac{8.4}{50} \frac{8.6}{30} \frac{8.9}{23} \frac{5.4}{16} \frac{5.2}{8} 50 \frac{5.1}{9} \frac{5.4}{18} \frac{7.4}{20} \frac{7.3}{36} \frac{6.7}{50}$

$\frac{7.3}{50} \frac{7.0}{30} \frac{7.6}{28} \frac{7.7}{22} \frac{5.3}{16} \frac{5.0}{9} 49 \frac{5.1}{8} \frac{5.4}{18} \frac{6.8}{23} \frac{7.4}{27} \frac{7.2}{50}$

$\frac{5.0}{50} \frac{3.7}{33} \frac{7.0}{29} \frac{6.7}{22} \frac{5.4}{17} \frac{5.1}{9} 50 \frac{5.1}{8} \frac{5.4}{17} \frac{6.5}{21} \frac{6.7}{30} \frac{5.0}{33} \frac{6.5}{50}$

$\frac{6.0}{50} \frac{5.3}{32} \frac{7.0}{29} \frac{6.6}{22} \frac{5.2}{17} \frac{5.1}{10} 49 \frac{5.1}{8} \frac{5.6}{18} \frac{6.5}{22} \frac{6.6}{29} \frac{3.8}{34} \frac{5.3}{50}$

$\frac{5.0}{50} \frac{4.4}{32} \frac{6.9}{29} \frac{6.6}{21} \frac{5.3}{18} \frac{5.0}{10} 49 \frac{5.2}{9} \frac{5.4}{17} \frac{6.7}{21-27} \frac{6.1}{30} \frac{3.1}{33} \frac{4.6}{50}$

$\frac{2.6}{50} \frac{2.6}{33} \frac{6.1}{29} \frac{6.4}{25-20} \frac{5.4}{17} \frac{5.1}{10} 49 \frac{5.3}{17} \frac{6.8}{21-23} \frac{6.4}{24} \frac{5.3}{29} \frac{0.8}{33} \frac{1.7}{50}$

$\frac{2.2}{50} \frac{1.5}{33} \frac{6.1}{28} \frac{7.0}{26-22} \frac{5.5}{18} \frac{5.1}{9} 50 \frac{5.2}{9} \frac{5.5}{17} \frac{6.7}{21-24} \frac{5.6}{29} \frac{0.8}{33} \frac{2.7}{50}$

$\frac{2.3}{50} \frac{2.1}{32} \frac{6.5}{27} \frac{6.2}{20} \frac{5.1}{18} 46 \frac{4.8}{9} \frac{5.2}{18} \frac{6.4}{20} \frac{6.5}{30} \frac{3.9}{34} \frac{5.5}{50}$

$\frac{5.7}{50} \frac{4.5}{33} \frac{6.7}{30} \frac{6.2}{20} \frac{5.3}{17} 47 \frac{5.1}{15} \frac{6.4}{20} \frac{6.5}{29} \frac{5.2}{32} \frac{5.6}{50}$

Sta + Δ - Elev

964.22

237 +50

238

+50

239

+25

+55

240

+50

241

+31

T.P.

3.33

961.02

6.53

957.69

242

+60

24" X Drain

Lt.

R

Rt.

$$\frac{7.1}{50} \quad \frac{5.5}{33} \quad \frac{6.7}{31} \quad \frac{6.5}{21} \quad \frac{5.2}{17} \quad 4.8 \quad \frac{5.3}{17} \quad \frac{6.5}{20} \quad \frac{6.7}{26} \quad \frac{6.0}{29} \quad \frac{3.0}{33} \quad \frac{2.7}{50}$$

$$\frac{7.9}{50} \quad \frac{6.2}{33} \quad \frac{6.9}{32} \quad \frac{6.5}{21} \quad \frac{5.4}{17} \quad 4.9 \quad \frac{5.3}{17} \quad \frac{6.6}{20-29} \quad \frac{4.2}{33} \quad \frac{4.0}{50}$$

$$\frac{7.1}{50} \quad \frac{5.0}{33} \quad \frac{6.7}{30} \quad \frac{6.4}{21} \quad \frac{5.3}{18} \quad 5.0 \quad \frac{5.3}{16} \quad \frac{7.6}{22} \quad \frac{7.4}{29} \quad \frac{6.5}{31} \quad \frac{7.6}{50}$$

$$\frac{6.7}{50} \quad \frac{5.1}{33} \quad \frac{6.8}{31} \quad \frac{6.5}{21} \quad \frac{5.3}{17} \quad 5.1 \quad \frac{5.5}{16} \quad \frac{11.5}{30} \quad \frac{14.4}{50}$$

$$\frac{7.6}{50} \quad \frac{6.2}{33} \quad \frac{6.9}{31} \quad \frac{6.6}{22} \quad \frac{5.3}{17} \quad 5.1 \quad \frac{5.8}{16} \quad \frac{12.5}{31} \quad \frac{13.6}{50}$$

$$\frac{8.5}{50} \quad \frac{6.9}{33} \quad \frac{7.1}{32} \quad \frac{6.7}{22} \quad \frac{5.5}{17} \quad 5.3 \quad \frac{5.6}{16} \quad \frac{9.0}{26} \quad \frac{10.5}{50}$$

$$\frac{6.8}{50} \quad \frac{4.7}{33} \quad \frac{7.4}{30} \quad \frac{7.2}{21} \quad \frac{5.9}{18} \quad 5.5 \quad \frac{5.9}{16} \quad \frac{7.0}{21} \quad \frac{6.8}{28} \quad \frac{4.8}{32} \quad \frac{5.1}{50}$$

$$\frac{4.8}{50} \quad \frac{3.3}{33} \quad \frac{7.4}{30} \quad \frac{7.2}{21} \quad \frac{6.0}{17} \quad 5.8 \quad \frac{6.1}{17} \quad \frac{7.0}{20} \quad \frac{7.6}{24} \quad \frac{6.4}{28} \quad \frac{1.7}{32} \quad \frac{2.5}{50}$$

$$\frac{3.4}{50} \quad \frac{3.0}{33} \quad \frac{7.8}{28} \quad \frac{7.4}{20} \quad \frac{6.3}{17} \quad 6.0 \quad \frac{6.6}{17} \quad \frac{7.7}{20-23} \quad \frac{6.7}{29} \quad \frac{1.5}{31} \quad \frac{2.7}{50}$$

$$\frac{3.1}{50} \quad \frac{2.9}{32} \quad \frac{8.0}{28} \quad \frac{7.6}{21} \quad \frac{6.6}{17} \quad 6.3 \quad \frac{6.7}{17} \quad \frac{8.0}{19-24} \quad \frac{7.2}{29} \quad \frac{2.6}{31} \quad \frac{3.6}{50}$$

$$\frac{6.1}{50} \quad \frac{7.3}{34} \quad \frac{7.3}{30} \quad \frac{4.2}{17} \quad 3.6 \quad \frac{4.2}{17} \quad \frac{6.8}{25} \quad \frac{7.2}{32} \quad \frac{7.2}{50}$$

$$\frac{11.4}{50} \quad \frac{11.4}{33} \quad \frac{11.6}{32} \quad \frac{4.7}{17} \quad 4.2 \quad \frac{4.7}{16} \quad \frac{10.6}{Inv} \quad \frac{10.1}{29} \quad \frac{9.4}{50}$$

28

Sfg + Δ - Elev

961.02

243

+50

244

+50

245

+50

246

+50

247

+50

248

+50

L1

L

R1

$$\frac{11.6}{50} \quad \frac{10.3}{34} \quad \frac{4.7}{17} \quad 4.6 \quad \frac{5.1}{16} \quad \frac{8.6}{27} \quad \frac{9.0}{31} \quad \frac{9.0}{50}$$

$$\frac{11.0}{50} \quad \frac{8.9}{30} \quad \frac{5.3}{17} \quad 5.1 \quad \frac{5.3}{16} \quad \frac{7.0}{22} \quad \frac{7.1}{26} \quad \frac{6.7}{29} \quad \frac{5.3}{34} \quad \frac{4.4}{50}$$

$$\frac{11.4}{50} \quad \frac{12.6}{43} \quad \frac{11.0}{38} \quad \frac{10.2}{30} \quad \frac{6.1}{17} \quad 5.5 \quad \frac{5.9}{16} \quad \frac{8.1}{21-26} \quad \frac{7.5}{29} \quad \frac{5.6}{33} \quad \frac{5.2}{50}$$

$$\frac{12.0}{50} \quad \frac{12.7}{40} \quad \frac{11.8}{33} \quad \frac{8.5}{21} \quad \frac{6.9}{17} \quad 6.2 \quad \frac{6.5}{16} \quad \frac{8.2}{21} \quad \frac{8.5}{32} \quad \frac{7.1}{50}$$

$$\frac{12.3}{50} \quad \frac{12.1}{39} \quad \frac{11.4}{32} \quad \frac{7.2}{18} \quad 6.5 \quad \frac{6.8}{16} \quad \frac{8.9}{22} \quad \frac{8.3}{32} \quad \frac{7.0}{50}$$

$$\frac{10.8}{50} \quad \frac{9.5}{33} \quad \frac{9.4}{26} \quad \frac{8.7}{24} \quad \frac{7.2}{17} \quad 6.7 \quad \frac{7.1}{15} \quad \frac{8.8}{20} \quad \frac{9.2}{27} \quad \frac{8.5}{30} \quad \frac{5.8}{34} \quad \frac{3.5}{50}$$

$$\frac{12.0}{50} \quad \frac{10.5}{35} \quad \frac{9.6}{26} \quad \frac{7.3}{17} \quad 6.8 \quad \frac{7.2}{16} \quad \frac{9.0}{21-24} \quad \frac{7.9}{29} \quad \frac{4.6}{33} \quad \frac{1.8}{50}$$

$$\frac{12.3}{50} \quad \frac{11.1}{35} \quad \frac{10.4}{27} \quad \frac{7.5}{18} \quad 7.0 \quad \frac{7.2}{16} \quad \frac{9.0}{21-24} \quad \frac{7.9}{29} \quad \frac{4.2}{32} \quad \frac{1.8}{50}$$

$$\frac{9.4}{50} \quad \frac{9.5}{33} \quad \frac{9.9}{30} \quad \frac{9.6}{25} \quad \frac{7.4}{17} \quad 6.9 \quad \frac{7.2}{16} \quad \frac{9.6}{22-26} \quad \frac{8.6}{30} \quad \frac{6.4}{32} \quad \frac{5.1}{50}$$

$$\frac{3.5}{50} \quad \frac{5.3}{33}$$

$$\frac{0.3}{50} \quad \frac{2.4}{33}$$

$$\frac{0.2}{50} \quad \frac{2.4}{33}$$

Sta	+	Σ	-	Elev
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961.02

249

T.P.	4.46	958.36	712	953.90
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247+50

248

+50

249

+50

250

B.M	11.45	959.27	1052	947.84	947.82
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+50

251

+04 24" X Drain

+50

252

L1

2

R1

$$\frac{1.0}{50} \quad \frac{2.8}{33}$$

$$\frac{6.1}{30} \quad \frac{7.2}{28} \quad \frac{6.6}{22} \quad \frac{4.8}{16} \quad 4.3 \quad \frac{4.7}{16} \quad \frac{6.8}{21-29} \quad \frac{5.4}{31} \quad \frac{4.2}{50}$$

$$\frac{5.6}{29} \quad \frac{6.5}{24} \quad \frac{6.5}{21} \quad \frac{4.9}{16} \quad 4.6 \quad \frac{5.0}{15} \quad \frac{7.0}{21-26} \quad \frac{6.2}{30} \quad \frac{3.9}{32} \quad \frac{3.0}{50}$$

$$\frac{5.5}{29} \quad \frac{4.4}{23} \quad \frac{6.1}{20} \quad \frac{5.1}{16} \quad 4.9 \quad \frac{5.1}{15} \quad \frac{6.7}{21} \quad \frac{7.1}{26} \quad \frac{6.4}{29} \quad \frac{3.0}{33} \quad \frac{1.7}{50}$$

$$\frac{6.1}{29} \quad \frac{6.1}{24} \quad \frac{6.7}{24} \quad \frac{6.7}{22} \quad \frac{5.2}{16} \quad 5.0 \quad \frac{5.4}{16} \quad \frac{7.3}{21} \quad \frac{7.6}{29} \quad \frac{5.2}{31} \quad \frac{4.7}{50}$$

$$\frac{0.0}{50} \quad \frac{2.9}{33} \quad \frac{6.8}{30} \quad \frac{7.0}{22} \quad \frac{5.4}{16} \quad 5.1 \quad \frac{5.4}{16} \quad \frac{7.7}{22} \quad \frac{8.4}{26} \quad \frac{8.0}{29} \quad \frac{6.5}{31} \quad \frac{6.7}{50}$$

$$\frac{4.0}{50} \quad \frac{5.5}{33} \quad \frac{7.5}{31} \quad \frac{7.2}{22} \quad \frac{5.5}{15} \quad 5.1 \quad \frac{5.6}{16} \quad \frac{8.5}{24} \quad \frac{9.0}{31} \quad \frac{9.6}{50}$$

$$\frac{6.7}{50} \quad \frac{8.0}{33} \quad \frac{8.8}{32} \quad \frac{8.6}{24} \quad \frac{6.6}{16} \quad 6.2 \quad \frac{6.8}{16} \quad \frac{11.1}{27} \quad \frac{12.4}{50}$$

$$\frac{8.0}{50} \quad \frac{10.1}{35} \quad \frac{12.0}{33} \quad \frac{12.0}{27} \quad \frac{6.5}{16} \quad 6.1 \quad \frac{6.6}{14} \quad \frac{12.1}{31} \quad \frac{12.4}{50}$$

$$\frac{11.05}{29} \text{ Inv}$$

$$\frac{12.5}{33} \text{ Inv}$$

$$\frac{11.6}{50} \quad \frac{11.1}{44} \quad \frac{10.1}{36} \quad \frac{13.2}{34-31} \quad \frac{9.5}{27} \quad \frac{6.1}{15} \quad 5.6 \quad \frac{6.0}{16} \quad \frac{8.9}{25} \quad \frac{8.6}{50}$$

$$\frac{11.6}{50} \quad \frac{9.3}{32} \quad \frac{5.4}{16} \quad 5.1 \quad \frac{5.2}{15} \quad \frac{7.5}{20} \quad \frac{7.5}{29} \quad \frac{6.2}{32} \quad \frac{6.8}{50}$$

Sta	+	λ	-	Elev
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959.27

252 + 50

253

+50

254

T.P.	10.54	968.40	1.41	957.84
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+50

255

+50

256

+50

257

T.P.	9.00	974.81	2.59	965.81
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+50

258

L1.

2

R1

$$\frac{113}{50} \quad \frac{10.6}{46} \quad \frac{8.7}{35} \quad \frac{4.8}{16} \quad 46 \quad \frac{4.8}{16} \quad \frac{7.0}{20} \quad \frac{7.5}{23} \quad \frac{7.6}{30} \quad \frac{7.4}{31} \quad \frac{8.1}{50}$$

$$\frac{10.7}{50} \quad \frac{8.9}{32} \quad \frac{4.5}{16} \quad 3.9 \quad \frac{4.2}{15} \quad \frac{7.0}{23} \quad \frac{7.4}{50}$$

$$\frac{11.3}{50} \quad \frac{9.5}{40} \quad \frac{8.6}{31} \quad \frac{4.0}{16} \quad 3.1 \quad \frac{3.3}{16} \quad \frac{5.3}{22} \quad \frac{5.4}{28} \quad \frac{4.9}{30} \quad \frac{4.6}{50}$$

$$\frac{11.8}{50} \quad \frac{8.7}{36} \quad \frac{3.5}{16} \quad 2.3 \quad \frac{2.0}{15} \quad \frac{4.1}{20} \quad \frac{4.3}{27} \quad \frac{1.9}{30} \quad \frac{1.3}{50}$$

$$\frac{21.4}{50} \quad \frac{18.2}{39} \quad \frac{16.0}{31} \quad \frac{11.7}{15} \quad 10.5 \quad \frac{10.1}{15} \quad \frac{12.4}{20-28} \quad \frac{8.7}{31} \quad \frac{6.4}{50}$$

$$\frac{18.7}{50} \quad \frac{13.9}{33} \quad \frac{11.9}{26} \quad \frac{11.6}{22} \quad \frac{10.5}{16} \quad 9.4 \quad \frac{9.2}{17} \quad \frac{11.4}{20-24} \quad \frac{10.4}{28} \quad \frac{4.9}{32} \quad \frac{2.7}{50}$$

$$\frac{14.9}{50} \quad \frac{9.9}{31} \quad \frac{11.0}{29} \quad \frac{10.4}{22} \quad \frac{9.2}{19} \quad 8.2 \quad \frac{7.8}{15} \quad \frac{10.0}{21-24} \quad \frac{8.5}{28} \quad \frac{2.2}{34} \quad \frac{1.1}{50}$$

$$\frac{11.6}{50} \quad \frac{8.5}{33} \quad \frac{9.9}{31} \quad \frac{9.5}{23} \quad \frac{7.7}{19} \quad 6.5 \quad \frac{6.3}{15} \quad \frac{8.9}{21} \quad \frac{8.5}{27} \quad \frac{3.2}{33} \quad \frac{3.2}{50}$$

$$\frac{10.1}{50} \quad \frac{8.4}{34} \quad \frac{8.8}{31} \quad \frac{8.8}{24} \quad \frac{6.0}{19} \quad 5.0 \quad \frac{4.9}{15} \quad \frac{7.4}{22} \quad \frac{7.4}{26} \quad \frac{6.4}{29} \quad \frac{2.0}{32} \quad \frac{0.8}{50}$$

$$\frac{9.8}{50} \quad \frac{6.5}{33} \quad \frac{7.7}{32} \quad \frac{7.3}{23} \quad \frac{4.8}{19} \quad 3.8 \quad \frac{3.5}{16} \quad \frac{6.2}{23} \quad \frac{5.0}{28} \quad \frac{10.4}{33} \quad \frac{10.7}{50}$$

$$\frac{14.0}{50} \quad \frac{10.7}{34} \quad \frac{12.3}{20} \quad \frac{12.3}{24} \quad \frac{9.8}{19} \quad 9.0 \quad \frac{8.7}{16} \quad \frac{11.4}{22-27} \quad \frac{5.6}{34} \quad \frac{5.9}{50}$$

$$\frac{14.8}{50} \quad \frac{10.5}{31} \quad \frac{12.4}{29-25} \quad \frac{8.6}{16} \quad 8.1 \quad \frac{8.1}{15} \quad \frac{10.1}{22} \quad \frac{10.0}{26} \quad \frac{9.1}{29} \quad \frac{5.1}{32} \quad \frac{5.5}{50}$$

Sta	+	Δ	-	Elev
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		974.81		
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258+50				
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259				
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+50				
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260				
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+50				
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261				
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+50				
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262				
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+50				
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T.P.	8.59	982.05	1.35	973.46
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263				
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+50				
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264				
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Jake Sandheim
Anoka County Engineer

Victoria	800'
<u>Co. Rd. E</u>	<u>179 -</u>

338-4706

Erickson

L1

L2

R1

$$\frac{11.7}{50} \quad \frac{9.6}{32} \quad \frac{11.7}{30-26} \quad \frac{10.4}{23} \quad \frac{7.3}{17} \quad 10 \quad \frac{7.3}{17} \quad \frac{9.5}{23} \quad \frac{9.3}{28} \quad \frac{6.4}{32} \quad \frac{6.5}{50}$$

$$\frac{11.9}{50} \quad \frac{10.4}{32} \quad \frac{11.2}{30-27} \quad \frac{9.4}{24} \quad \frac{6.5}{16} \quad 6.1 \quad \frac{6.5}{16} \quad \frac{8.9}{24} \quad \frac{8.9}{29} \quad \frac{7.5}{32} \quad \frac{7.4}{50}$$

$$\frac{9.3}{50} \quad \frac{8.7}{32} \quad \frac{9.5}{31-27} \quad \frac{6.0}{16} \quad 5.4 \quad \frac{5.9}{17} \quad \frac{8.1}{24} \quad \frac{8.5}{32} \quad \frac{7.7}{50}$$

$$\frac{8.1}{50} \quad \frac{7.7}{31} \quad \frac{8.6}{29-27} \quad \frac{5.4}{16} \quad 4.8 \quad \frac{4.9}{16} \quad \frac{7.5}{23} \quad \frac{7.6}{50}$$

$$\frac{8.1}{50} \quad \frac{7.2}{30} \quad \frac{7.9}{28-26} \quad \frac{7.2}{24} \quad \frac{4.5}{16} \quad 4.2 \quad \frac{4.3}{17} \quad \frac{6.0}{23} \quad \frac{6.3}{50}$$

$$\frac{6.9}{50} \quad \frac{6.1}{30} \quad \frac{6.8}{29} \quad \frac{6.7}{24} \quad \frac{3.9}{16} \quad 3.6 \quad \frac{3.7}{17} \quad \frac{5.5}{23} \quad \frac{5.8}{32} \quad \frac{4.3}{34} \quad \frac{4.7}{50}$$

$$\frac{5.0}{50} \quad \frac{4.6}{33} \quad \frac{5.9}{30} \quad \frac{5.2}{22} \quad \frac{3.2}{17} \quad 2.8 \quad \frac{3.3}{17} \quad \frac{4.9}{22} \quad \frac{5.0}{32} \quad \frac{4.2}{33} \quad \frac{4.7}{50}$$

$$\frac{3.7}{50} \quad \frac{3.8}{34} \quad \frac{4.9}{31} \quad \frac{4.2}{21} \quad \frac{2.7}{16} \quad 2.2 \quad \frac{2.6}{16} \quad \frac{4.6}{22} \quad \frac{4.9}{30} \quad \frac{4.0}{33} \quad \frac{5.4}{40} \quad \frac{5.7}{50}$$

$$\frac{2.6}{50} \quad \frac{2.5}{33} \quad \frac{3.8}{31} \quad \frac{3.8}{21} \quad \frac{2.1}{17} \quad 1.7 \quad \frac{1.8}{17} \quad \frac{3.9}{22} \quad \frac{4.1}{31} \quad \frac{2.4}{34} \quad \frac{3.4}{50}$$

$$\frac{7.9}{50} \quad \frac{8.0}{32} \quad \frac{9.8}{30} \quad \frac{9.5}{20} \quad \frac{8.5}{17} \quad 8.4 \quad \frac{8.2}{16} \quad \frac{9.5}{21} \quad \frac{9.6}{29} \quad \frac{6.5}{34} \quad \frac{6.3}{50}$$

$$\frac{7.8}{50} \quad \frac{6.9}{32} \quad \frac{9.8}{29} \quad \frac{9.4}{19} \quad \frac{8.2}{16} \quad 7.9 \quad \frac{8.1}{17} \quad \frac{9.2}{21} \quad \frac{9.7}{29} \quad \frac{6.1}{35} \quad \frac{5.4}{50}$$

$$\frac{7.6}{50} \quad \frac{6.3}{32} \quad \frac{9.5}{29} \quad \frac{9.3}{21} \quad \frac{7.7}{17} \quad 7.2 \quad \frac{7.5}{18} \quad \frac{9.0}{21} \quad \frac{9.0}{26} \quad \frac{8.0}{31} \quad \frac{4.0}{34} \quad \frac{7.3}{50}$$

Sta	+	π	-	Elev
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982.05

264+50

265

+50

266

+50

267

+50

268

+25

+29

BM

7.41

988.38

1.07

980.98

980.97

2+50

+57

Lt

R

Rt

$$\frac{6.9}{50} \frac{5.5}{32} \frac{8.8}{29} \frac{8.3}{19} \frac{6.9}{16} \quad 6.5 \quad \frac{6.8}{17} \frac{8.4}{22} \frac{8.7}{25} \frac{8.1}{31} \frac{3.4}{34} \frac{2.5}{50}$$

$$\frac{5.7}{50} \frac{4.6}{33} \frac{8.2}{29} \frac{7.8}{20} \frac{6.2}{17} \quad 5.8 \quad \frac{6.2}{17} \frac{8.0}{23} \frac{8.0}{31} \frac{6.2}{34} \frac{5.7}{50}$$

$$\frac{6.8}{50} \frac{6.2}{33} \frac{7.9}{31} \frac{7.5}{22} \frac{5.6}{17} \quad 5.0 \quad \frac{5.5}{17} \frac{7.6}{22} \frac{7.7}{31} \frac{6.2}{34} \frac{6.2}{50}$$

$$\frac{6.5}{50} \frac{5.4}{32} \frac{7.2}{30} \frac{6.9}{20} \frac{5.1}{17} \quad 4.8 \quad \frac{4.9}{17} \frac{6.8}{22} \frac{7.0}{26} \frac{6.8}{31} \frac{4.2}{35} \frac{4.1}{50}$$

$$\frac{6.1}{50} \frac{4.9}{33} \frac{6.7}{36} \frac{6.3}{21} \frac{4.6}{16} \quad 4.2 \quad \frac{4.4}{17} \frac{6.1}{23} \frac{6.4}{33} \frac{5.2}{35} \frac{6.0}{50}$$

$$\frac{5.4}{50} \frac{4.3}{32} \frac{6.0}{30} \frac{5.9}{25} \frac{5.5}{19} \frac{3.9}{16} \quad 3.5 \quad \frac{3.7}{17} \frac{5.7}{23} \frac{6.2}{32} \frac{5.0}{35} \frac{5.5}{50}$$

$$\frac{5.4}{50} \frac{4.1}{32} \frac{5.2}{31} \frac{4.8}{20} \frac{3.4}{16} \quad 2.9 \quad \frac{3.1}{17} \frac{5.2}{24} \frac{5.6}{33} \frac{4.7}{35} \frac{4.6}{50}$$

$$\frac{4.6}{50} \frac{3.9}{33} \frac{4.8}{31} \frac{4.4}{20} \frac{2.7}{16} \quad 2.3 \quad \frac{2.7}{17} \frac{4.5}{23} \frac{5.2}{33} \frac{4.3}{35} \frac{4.5}{50}$$

$$\frac{4.5}{50} \frac{3.5}{32} \frac{4.5}{31} \frac{4.3}{20} \frac{2.3}{15} \quad 2.2 \quad \frac{2.5}{20} \frac{4.1}{24} \frac{4.7}{50}$$

$$\frac{4.5}{50} \frac{3.5}{32} \frac{4.5}{31} \frac{4.1}{20} \frac{2.3}{16} \quad 2.2 \quad \frac{2.7}{25} \frac{3.3}{50}$$

Top 4x6 Conc Plat Form 100 Rt Sta 269+50

$$\frac{10.2}{50} \frac{8.3}{16} \quad 8.3 \quad \frac{8.7}{25} \frac{9.1}{50}$$

$$\frac{10.2}{50} \frac{8.3}{16} \quad 8.3 \quad \frac{8.7}{25} \frac{9.1}{50}$$

Sta + Δ - Elev

98838

268+59

+76

269

+50

270

+50

271

271+50

272

+50

273

+50

L

Z

R+

$$\frac{11.4}{50} \quad \frac{10.0}{31} \quad \frac{10.3}{29} \quad \frac{9.6}{20} \quad \frac{8.3}{16}$$

8.2

$$\frac{8.6}{22} \quad \frac{10.1}{25} \quad \frac{10.6}{50}$$

$$\frac{10.6}{50} \quad \frac{9.0}{32} \quad \frac{10.2}{30} \quad \frac{9.6}{21} \quad \frac{8.3}{15}$$

$$8.0 \quad \frac{8.2}{17} \quad \frac{10.1}{22} \quad \frac{10.4}{31} \quad \frac{9.3}{37} \quad \frac{8.8}{50}$$

$$\frac{11.8}{50} \quad \frac{10.4}{32} \quad \frac{10.1}{31} \quad \frac{9.6}{21} \quad \frac{8.1}{16}$$

7.7

$$\frac{8.0}{17} \quad \frac{9.6}{22} \quad \frac{10.0}{31} \quad \frac{8.1}{26} \quad \frac{8.5}{50}$$

$$\frac{11.5}{50} \quad \frac{9.4}{32} \quad \frac{9.8}{30} \quad \frac{9.2}{22} \quad \frac{7.8}{16}$$

$$7.3 \quad \frac{7.3}{17} \quad \frac{8.9}{20} \quad \frac{9.2}{31} \quad \frac{7.8}{34} \quad \frac{7.9}{50}$$

$$\frac{9.0}{50} \quad \frac{5.4}{33} \quad \frac{8.9}{28} \quad \frac{8.5}{20} \quad \frac{7.2}{16}$$

$$6.8 \quad \frac{7.4}{18} \quad \frac{8.8}{21} \quad \frac{8.5}{29} \quad \frac{7.4}{37} \quad \frac{7.3}{50}$$

$$\frac{8.7}{50} \quad \frac{5.7}{33} \quad \frac{8.5}{29} \quad \frac{8.2}{20} \quad \frac{6.9}{16}$$

$$6.3 \quad \frac{6.5}{16} \quad \frac{7.2}{22} \quad \frac{7.8}{34} \quad \frac{7.4}{40} \quad \frac{7.3}{50}$$

$$\frac{9.8}{50} \quad \frac{7.8}{33} \quad \frac{8.2}{31} \quad \frac{8.1}{22} \quad \frac{6.3}{16}$$

6.0

$$\frac{6.2}{17} \quad \frac{7.7}{27} \quad \frac{9.0}{36} \quad \frac{10.4}{50}$$

$$\frac{6.8}{50} \quad \frac{6.9}{33} \quad \frac{7.7}{31} \quad \frac{7.4}{21} \quad \frac{6.1}{16}$$

$$5.8 \quad \frac{6.5}{18} \quad \frac{13.0}{34} \quad \frac{14.8}{50}$$

$$\frac{2.0}{50} \quad \frac{5.1}{39} \quad \frac{5.4}{33} \quad \frac{7.3}{28} \quad \frac{6.9}{20} \quad \frac{5.6}{16}$$

5.3

$$\frac{6.0}{17} \quad \frac{14.3}{36} \quad \frac{15.7}{50}$$

$$\frac{2.3}{50} \quad \frac{4.7}{40} \quad \frac{4.7}{34} \quad \frac{6.8}{30} \quad \frac{6.5}{20} \quad \frac{5.1}{16}$$

$$5.0 \quad \frac{5.8}{16} \quad \frac{15.4}{36} \quad \frac{16.9}{50}$$

$$\frac{5.5}{50} \quad \frac{5.1}{34} \quad \frac{6.8}{30} \quad \frac{6.0}{21} \quad \frac{5.0}{15}$$

4.6

$$\frac{5.2}{17} \quad \frac{12.5}{34} \quad \frac{14.1}{50}$$

$$\frac{4.6}{50} \quad \frac{5.0}{33} \quad \frac{6.5}{30} \quad \frac{6.0}{21} \quad \frac{4.6}{15}$$

4.2

$$\frac{4.6}{16} \quad \frac{7.5}{27} \quad \frac{8.1}{36} \quad \frac{8.6}{50}$$

Sta	+	Δ	-	Elev
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988.38

274

+50

275

+50

276

T.P	4.12	988.70	3.80	984.58
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+50

277

24" X Drain

+50

278

+50

279

+50

Lt.

Z

Rt

$$\frac{49}{50} \quad \frac{47}{32} \quad \frac{65}{30} \quad \frac{62}{20} \quad \frac{44}{16} \quad 41 \quad \frac{42}{16} \quad \frac{61}{23} \quad \frac{65}{32} \quad \frac{60}{34} \quad \frac{72}{50}$$

$$\frac{35}{50} \quad \frac{36}{38} \quad \frac{45}{33} \quad \frac{59}{31} \quad \frac{57}{21} \quad \frac{41}{15} \quad 39 \quad \frac{40}{17} \quad \frac{58}{22} \quad \frac{63}{32} \quad \frac{52}{34} \quad \frac{64}{50}$$

$$\frac{48}{50} \quad \frac{50}{33} \quad \frac{55}{30} \quad \frac{54}{21} \quad \frac{39}{15} \quad 38 \quad \frac{40}{17} \quad \frac{60}{22} \quad \frac{65}{31} \quad \frac{49}{33} \quad \frac{47}{50}$$

$$\frac{45}{50} \quad \frac{51}{33} \quad \frac{57}{31} \quad \frac{58}{21} \quad \frac{36}{15} \quad 3.8 \quad \frac{40}{17} \quad \frac{60}{23} \quad \frac{64}{31} \quad \frac{59}{32} \quad \frac{55}{50}$$

$$\frac{56}{50} \quad \frac{62}{34} \quad \frac{66}{30} \quad \frac{58}{23} \quad \frac{38}{15} \quad 3.7 \quad \frac{42}{18} \quad \frac{77}{27} \quad \frac{86}{50}$$

$$\frac{96}{50} \quad \frac{94}{43} \quad \frac{87}{26} \quad \frac{43}{15} \quad 41 \quad \frac{50}{18} \quad \frac{98}{32} \quad \frac{107}{50} \quad \frac{11.91}{Inv}$$

$$\frac{1094}{Inv} \quad \frac{95}{50} \quad \frac{95}{36} \quad \frac{87}{29} \quad \frac{47}{14} \quad 3.9 \quad \frac{46}{17} \quad \frac{86}{28} \quad \frac{10.19}{50}$$

$$\frac{94}{50} \quad \frac{82}{27} \quad \frac{45}{16} \quad 39 \quad \frac{44}{17} \quad \frac{68}{26} \quad \frac{81}{50}$$

$$\frac{77}{50} \quad \frac{67}{28} \quad \frac{62}{21} \quad \frac{45}{14} \quad 41 \quad \frac{45}{16} \quad \frac{65}{22} \quad \frac{66}{29} \quad \frac{58}{35} \quad \frac{63}{15}$$

$$\frac{75}{50} \quad \frac{60}{32} \quad \frac{70}{28} \quad \frac{66}{21} \quad \frac{51}{15} \quad 46 \quad \frac{49}{17} \quad \frac{69}{22} \quad \frac{72}{30} \quad \frac{58}{33} \quad \frac{65}{50}$$

$$\frac{57}{50} \quad \frac{57}{33} \quad \frac{77}{28} \quad \frac{75}{21} \quad \frac{58}{16} \quad 5.5 \quad \frac{57}{16} \quad \frac{64}{23} \quad \frac{76}{30} \quad \frac{57}{34} \quad \frac{56}{50}$$

$$\frac{66}{50} \quad \frac{77}{27} \quad \frac{84}{24} \quad \frac{82}{21} \quad \frac{66}{16} \quad 62 \quad \frac{67}{16} \quad \frac{80}{21} \quad \frac{83}{29} \quad \frac{62}{35} \quad \frac{59}{50}$$

Sta	+	Δ	-	Elev
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988.70

280

+50

281

B.M	7.28	988.14	8.36	980.34	980.36
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+44

+50

+57

+71

Δ "F"

+88

+95

282

+50

283

Lt.

R

Rt

$$\frac{7.4}{50} \quad \frac{7.5}{26} \quad \frac{8.7}{24} \quad \frac{8.5}{18} \quad \frac{7.5}{16} \quad 7.0 \quad \frac{7.5}{16} \quad \frac{8.2}{19} \quad \frac{8.8}{22} \quad \frac{8.6}{31} \quad \frac{6.8}{34} \quad \frac{6.1}{50}$$

$$\frac{7.3}{50} \quad \frac{7.8}{33} \quad \frac{8.4}{27} \quad \frac{9.5}{24} \quad \frac{9.5}{20} \quad \frac{8.1}{16} \quad 7.7 \quad \frac{8.2}{16} \quad \frac{9.3}{20} \quad \frac{9.2}{25-28} \quad \frac{9.3}{30} \quad \frac{7.6}{34} \quad \frac{7.4}{50}$$

$$\frac{7.9}{50} \quad \frac{8.4}{32} \quad \frac{10.2}{28-22} \quad \frac{9.8}{19} \quad \frac{8.5}{16} \quad 8.3 \quad \frac{8.6}{16} \quad \frac{10.4}{21} \quad \frac{10.5}{30} \quad \frac{8.8}{34} \quad \frac{9.3}{50}$$

Spk in R.P.S.W Cor "F" & Victoria

$$\frac{8.3}{50} \quad \frac{8.3}{33} \quad \frac{9.8}{29} \quad \frac{9.5}{20} \quad \frac{8.2}{17} \quad 8.0 \quad \frac{8.5}{18} \quad \frac{10.1}{24} \quad \frac{10.5}{31} \quad \frac{9.9}{33} \quad \frac{10.3}{50}$$

$$\frac{9.8}{50} \quad \frac{9.6}{25} \quad \frac{8.5}{22} \quad \frac{8.1}{9} \quad 8.0 \quad \frac{8.5}{15} \quad \frac{9.0}{23} \quad \frac{10.4}{29} \quad \frac{11.3}{31} \quad \frac{11.9}{40} \quad \frac{12.5}{50}$$

$$\frac{8.5}{50} \quad 8.0 \quad \frac{10.2}{50}$$

$$\frac{8.0}{100} \quad \frac{8.0}{50} \quad 8.2 \quad \frac{10.0}{50} \quad \frac{12.0}{100}$$

$$\frac{8.5}{50} \quad 8.1 \quad \frac{10.1}{50}$$

$$\frac{10.2}{50} \quad \frac{9.8}{20} \quad \frac{8.5}{17} \quad 8.1 \quad \frac{8.7}{20} \quad \frac{10.4}{30} \quad \frac{11.2}{50}$$

$$\frac{8.4}{50} \quad \frac{8.2}{33} \quad \frac{10.2}{30} \quad \frac{10.1}{21} \quad \frac{8.5}{16} \quad 8.0 \quad \frac{8.8}{19} \quad \frac{10.2}{23} \quad \frac{10.5}{33} \quad \frac{10.8}{50}$$

$$\frac{7.7}{50} \quad \frac{7.3}{34} \quad \frac{10.1}{31} \quad \frac{9.7}{20} \quad \frac{8.4}{16} \quad 7.8 \quad \frac{8.3}{17} \quad \frac{10.1}{23} \quad \frac{10.3}{31} \quad \frac{9.3}{33} \quad \frac{10.0}{50}$$

$$\frac{9.4}{50} \quad \frac{8.6}{34} \quad \frac{9.9}{33} \quad \frac{9.8}{24} \quad \frac{9.4}{20} \quad \frac{7.8}{16} \quad 7.2 \quad \frac{7.9}{17} \quad \frac{9.8}{22} \quad \frac{9.8}{28} \quad \frac{9.4}{32} \quad \frac{8.0}{34} \quad \frac{8.3}{50}$$

Sta	+	Δ	-	Elev
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283	+50			
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284				
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+50				
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285				
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+50				
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286				
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+50				
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T.P.	936	995.58	1.92	986.22
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287				
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+50				
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288				
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+50				
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289				
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Lt.

Z

Rt.

$$\frac{11.8}{50} \quad \frac{10.0}{33} \quad \frac{9.3}{21} \quad \frac{7.3}{16} \quad 6.8 \quad \frac{7.5}{16} \quad \frac{9.0}{21} \quad \frac{9.0}{32} \quad \frac{7.2}{35} \quad \frac{7.0}{50}$$

$$\frac{11.9}{50} \quad \frac{10.2}{33} \quad \frac{9.0}{22} \quad \frac{7.0}{17} \quad 6.2 \quad \frac{6.9}{17} \quad \frac{8.6}{22} \quad \frac{8.6}{31} \quad \frac{6.3}{33} \quad \frac{6.1}{50}$$

$$\frac{12.2}{50} \quad \frac{9.9}{33} \quad \frac{9.0}{25} \quad \frac{5.9}{16} \quad 5.6 \quad \frac{6.1}{17} \quad \frac{7.5}{21} \quad \frac{7.7}{30} \quad \frac{4.4}{33} \quad \frac{4.1}{50}$$

$$\frac{11.1}{50} \quad \frac{8.7}{34} \quad \frac{7.3}{24} \quad \frac{5.0}{16} \quad 4.8 \quad \frac{5.2}{18} \quad \frac{6.4}{21} \quad \frac{6.4}{30} \quad \frac{2.6}{33} \quad \frac{2.5}{50}$$

$$\frac{10.1}{50} \quad \frac{7.9}{28} \quad \frac{4.2}{16} \quad 4.0 \quad \frac{4.4}{16} \quad \frac{5.6}{21} \quad \frac{5.9}{27} \quad \frac{5.3}{30} \quad \frac{1.8}{34} \quad \frac{1.9}{50}$$

$$\frac{9.4}{50} \quad \frac{8.2}{34} \quad \frac{7.2}{27} \quad \frac{5.0}{20} \quad \frac{4.0}{17} \quad 3.4 \quad \frac{3.6}{17} \quad \frac{5.1}{21} \quad \frac{5.1}{28} \quad \frac{4.7}{30} \quad \frac{1.1}{34} \quad \frac{1.2}{50}$$

$$\frac{8.3}{50} \quad \frac{6.7}{29} \quad \frac{4.5}{21} \quad \frac{2.9}{16} \quad 2.5 \quad \frac{2.8}{17} \quad \frac{4.5}{20-27} \quad \frac{3.9}{30} \quad \frac{0.0}{34} \quad \frac{0.4}{50}$$

$$\frac{15.0}{50} \quad \frac{13.3}{29} \quad \frac{9.7}{16} \quad 9.3 \quad \frac{9.6}{17} \quad \frac{11.1}{21-28} \quad \frac{10.7}{30} \quad \frac{7.2}{34} \quad \frac{7.3}{50}$$

$$\frac{14.4}{50} \quad \frac{12.3}{29} \quad \frac{9.0}{16} \quad 8.6 \quad \frac{8.9}{18} \quad \frac{10.1}{21} \quad \frac{10.4}{31} \quad \frac{7.5}{33} \quad \frac{7.4}{50}$$

$$\frac{14.7}{50} \quad \frac{12.3}{30} \quad \frac{8.4}{16} \quad 7.8 \quad \frac{8.2}{17} \quad \frac{9.4}{21} \quad \frac{9.8}{30} \quad \frac{7.3}{33} \quad \frac{7.6}{50}$$

$$\frac{14.2}{50} \quad \frac{13.0}{33} \quad \frac{7.7}{16} \quad 7.1 \quad \frac{7.3}{18} \quad \frac{8.6}{21} \quad \frac{9.2}{31} \quad \frac{7.9}{33} \quad \frac{7.9}{50}$$

$$\frac{12.6}{50} \quad \frac{11.6}{31} \quad \frac{7.1}{17} \quad 6.4 \quad \frac{6.4}{17} \quad \frac{8.1}{20} \quad \frac{8.2}{33} \quad \frac{7.9}{34} \quad \frac{7.9}{50}$$

Sta	+	Δ	-	Elev
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995.58

289+50

290

+50

T.P.	7.91	1001.08	2.41	993.17
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291

+50

292

B.M	6.81	1002.94	4.94	996.14	996.13
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+50

293

+50

294

+40

295

LT * RT

$\frac{10.3}{50}$ $\frac{9.3}{27}$ $\frac{6.5}{17}$ 5.6 $\frac{5.4}{16}$ $\frac{7.0}{20}$ $\frac{7.2}{32}$ $\frac{6.2}{34}$ $\frac{6.2}{50}$

$\frac{8.9}{50}$ $\frac{8.2}{28}$ $\frac{5.5}{18}$ 4.6 $\frac{4.3}{17}$ $\frac{5.8}{22}$ $\frac{5.8}{28}$ $\frac{3.4}{33}$ $\frac{3.3}{50}$

$\frac{9.3}{50}$ $\frac{8.4}{33}$ $\frac{6.6}{22}$ $\frac{4.1}{16}$ 3.4 $\frac{3.0}{17}$ $\frac{4.4}{21}$ $\frac{4.3}{29}$ $\frac{0.3}{34}$ $\frac{0.0}{50}$

$\frac{12.2}{50}$ $\frac{9.6}{28}$ $\frac{9.3}{22}$ $\frac{8.1}{17}$ 7.4 $\frac{7.1}{17}$ $\frac{8.9}{22-27}$ $\frac{7.9}{29}$ $\frac{4.0}{33}$ $\frac{4.4}{50}$

$\frac{8.9}{50}$ $\frac{7.0}{32}$ $\frac{8.5}{30}$ $\frac{8.4}{23}$ $\frac{6.9}{17}$ 6.1 $\frac{6.0}{16}$ $\frac{7.6}{22}$ $\frac{7.6}{28}$ $\frac{4.9}{34}$ $\frac{6.0}{50}$

$\frac{2.3}{50}$ $\frac{2.3}{33}$ $\frac{6.3}{30}$ $\frac{7.2}{27-22}$ $\frac{6.1}{18}$ $\frac{5.8}{14}$ 5.2 $\frac{5.3}{16}$ $\frac{6.8}{20}$ $\frac{7.1}{30}$ $\frac{5.3}{32}$ $\frac{6.3}{50}$

SPK, 17 12" Twin Oak 50' RT Sta 291+90

$\frac{1.6}{50}$ $\frac{2.5}{34}$ $\frac{7.5}{29}$ $\frac{8.6}{25}$ $\frac{8.3}{21}$ $\frac{7.0}{16}$ 6.4 $\frac{6.6}{17}$ $\frac{8.2}{21}$ $\frac{8.4}{32}$ $\frac{7.5}{33}$ $\frac{8.6}{50}$

$\frac{1.6}{50}$ $\frac{1.8}{34}$ $\frac{7.1}{29}$ $\frac{7.8}{25}$ $\frac{7.6}{22}$ $\frac{6.0}{17}$ 5.6 $\frac{6.0}{18}$ $\frac{7.4}{21}$ $\frac{7.4}{29}$ $\frac{5.7}{35}$ $\frac{6.5}{50}$

$\frac{4.8}{50}$ $\frac{5.0}{34}$ $\frac{7.4}{29}$ $\frac{7.2}{22}$ $\frac{5.4}{17}$ 5.1 $\frac{5.6}{17}$ $\frac{7.2}{22}$ $\frac{7.5}{29}$ $\frac{6.8}{34}$ $\frac{7.5}{50}$

$\frac{2.5}{50}$ $\frac{2.1}{33}$ $\frac{6.3}{28}$ $\frac{7.2}{26}$ $\frac{6.9}{21}$ $\frac{5.5}{17}$ 5.1 $\frac{5.2}{18}$ $\frac{6.5}{21-28}$ $\frac{6.3}{31}$ $\frac{4.8}{35}$ $\frac{5.7}{50}$

$\frac{10.8}{50}$ $\frac{11.2}{33}$ $\frac{7.0}{25}$ $\frac{6.6}{20}$ $\frac{5.5}{16}$ 5.2 $\frac{5.2}{17}$ $\frac{6.8}{21-26}$ $\frac{5.9}{31}$ $\frac{3.5}{34}$ $\frac{4.4}{50}$

$\frac{4.7}{50}$ $\frac{3.5}{34}$ $\frac{7.4}{27}$ $\frac{7.0}{21}$ $\frac{5.7}{16}$ 5.3 $\frac{5.6}{18}$ $\frac{7.3}{22}$ $\frac{7.6}{31}$ $\frac{5.8}{34}$ $\frac{6.7}{50}$

Sta + Δ - Elev

1002.94

295+50

296

+50

T.P. 0.39 993.74 9.59 993.35

297

+50

298

+50

299

+50

300

T.P. 1.58 984.69 10.63 983.11

+50

301

Lt

Z

T

Rt

$$\frac{82}{50} \frac{64}{33} \frac{8.3}{28} \frac{77}{21} \frac{65}{18} 5.8 \quad \frac{6.3}{17} \frac{7.8}{22} \frac{8.2}{33} \frac{7.2}{39} \frac{8.0}{50}$$

$$\frac{11.2}{50} \frac{9.0}{34} \frac{9.6}{33} \frac{9.3}{24} \frac{7.5}{18} 6.8 \quad \frac{7.0}{16} \frac{8.5}{22} \frac{8.8}{31} \frac{7.8}{35} \frac{8.3}{50}$$

$$\frac{12.8}{50} \frac{10.0}{33} \frac{10.8}{31} \frac{10.1}{23} \frac{9.2}{19} 8.0 \quad \frac{8.1}{17} \frac{9.7}{20} \frac{9.7}{30} \frac{8.3}{33} \frac{7.9}{50}$$

$$\frac{12.2}{50} \frac{7.2}{50} \frac{6.5}{41} \frac{3.4}{26} \frac{1.8}{17} 0.6 \quad \frac{0.2}{17} \frac{1.8}{22} \frac{1.8}{28} \frac{1.1}{31} \frac{1.3}{34} \frac{1.2}{50}$$

$$\frac{9.2}{50} \frac{5.9}{30} \frac{4.1}{18} \frac{3.7}{13} 2.7 \quad \frac{2.0}{18} \frac{3.7}{23} \frac{3.8}{29} \frac{1.2}{34} \frac{1.0}{50}$$

$$\frac{12.9}{50} \frac{10.5}{33} \frac{5.9}{17} \quad 4.4 \frac{4.2}{18} \frac{5.8}{22} \frac{5.6}{30} \frac{3.1}{35} \frac{2.8}{50}$$

$$\frac{15.2}{50} \frac{12.5}{30} \frac{4.9}{18} \frac{7.2}{14} 5.9 \quad \frac{5.8}{18} \frac{7.2}{24} \frac{7.8}{30} \frac{4.7}{34} \frac{3.0}{50}$$

$$\frac{13.6}{50} \frac{12.0}{28} \frac{9.5}{18} \frac{8.6}{13} 7.6 \quad \frac{7.2}{18} \frac{9.3}{23} \frac{8.1}{34} \frac{7.6}{35} \frac{7.6}{50}$$

$$\frac{11.6}{50} \frac{12.3}{42} \frac{12.1}{24} \frac{11.1}{20} \frac{10.3}{14} 9.3 \quad \frac{9.0}{18} \frac{10.8}{24} \frac{9.3}{32} \frac{9.4}{35} \frac{9.4}{50}$$

$$\frac{13.3}{50} \frac{12.2}{22} \frac{11.6}{16} \quad 11.0 \frac{10.9}{17} \frac{12.6}{23} \frac{13.3}{30} \frac{10.9}{34} \frac{11.2}{50}$$

$$\frac{6.0}{50} \frac{6.5}{41} \frac{5.8}{26} \frac{5.0}{21} \frac{3.8}{17} 3.7 \quad \frac{4.0}{17} \frac{5.8}{22} \frac{6.4}{30} \frac{4.8}{34} \frac{5.7}{50}$$

$$\frac{8.7}{50} \frac{7.7}{25} \frac{6.9}{21} \frac{5.4}{17} 5.3 \quad \frac{6.6}{18} \frac{8.3}{24} \frac{8.3}{28} \frac{7.2}{33} \frac{8.5}{50}$$

Sta	+	Δ	-	Elev
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98469

301+50

302

T.B.M.	449	977.45	11.73	972.96
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+50

303

+50

304

+50

305

-	3.67	968.25	12.87	964.58
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+50

+82 24" X Drain

306

+50

Lt.

Z

Rt

$$\frac{11.1}{50} \quad \frac{10.3}{28} \quad \frac{9.3}{23} \quad \frac{6.8}{16} \quad 6.8$$

$$\frac{8.2}{19} \quad \frac{12.0}{32} \quad \frac{13.4}{50}$$

$$\frac{12.5}{50} \quad \frac{10.9}{24} \quad \frac{8.1}{17} \quad 8.6 \quad \frac{10.6}{20} \quad \frac{15.2}{36} \quad \frac{16.4}{43} \quad \frac{16.3}{50}$$

$$\frac{6.9}{50} \quad \frac{5.6}{42} \quad \frac{3.9}{21} \quad \frac{2.3}{17} \quad 2.9 \quad \frac{4.6}{20} \quad \frac{8.4}{31} \quad \frac{9.8}{50}$$

$$\frac{9.3}{50} \quad \frac{6.2}{32} \quad \frac{5.3}{19} \quad \frac{4.2}{16} \quad 4.5 \quad \frac{5.6}{20} \quad \frac{9.1}{50}$$

$$\frac{11.6}{50} \quad \frac{8.2}{28} \quad \frac{7.2}{19} \quad \frac{5.5}{14} \quad 5.9 \quad \frac{7.2}{19} \quad \frac{7.4}{24} \quad \frac{8.7}{32} \quad \frac{7.5}{33} \quad \frac{8.9}{50}$$

$$\frac{9.7}{50} \quad \frac{7.7}{32} \quad \frac{9.2}{30} \quad \frac{8.9}{21} \quad \frac{7.2}{15} \quad 7.5 \quad \frac{8.8}{19} \quad \frac{9.7}{23} \quad \frac{10.1}{31} \quad \frac{9.5}{33} \quad \frac{8.4}{34} \quad \frac{9.4}{50}$$

$$\frac{12.7}{50} \quad \frac{10.1}{32} \quad \frac{11.0}{30} \quad \frac{10.9}{22} \quad \frac{8.9}{17} \quad 9.2 \quad \frac{10.6}{18} \quad \frac{11.6}{22} \quad \frac{12.1}{32} \quad \frac{10.4}{34} \quad \frac{10.9}{50}$$

$$\frac{15.1}{50} \quad \frac{13.2}{31} \quad \frac{13.2}{25} \quad \frac{10.8}{17} \quad 11.0 \quad \frac{12.2}{18} \quad \frac{13.3}{22} \quad \frac{14.1}{50}$$

$$\frac{10.1}{50} \quad \frac{8.3}{30} \quad \frac{3.4}{17} \quad 3.4 \quad - \quad \frac{4.4}{17} \quad \frac{5.9}{23} \quad \frac{6.4}{50}$$

$$\frac{10.8}{\text{Inv}}$$

$$\frac{11.3}{\text{Inv}}$$

$$\frac{10.6}{17} \text{ Ditch}$$

$$\frac{11.1}{50} \quad \frac{10.5}{35} \quad \frac{4.7}{18} \quad 4.8 \quad \frac{5.6}{17} \quad \frac{6.8}{22} \quad \frac{8.6}{50}$$

$$\frac{8.3}{50} \quad \frac{7.9}{33} \quad \frac{8.5}{30} \quad \frac{8.3}{24} \quad \frac{5.7}{17} \quad 6.2 \quad \frac{7.1}{18} \quad \frac{8.2}{21} \quad \frac{8.2}{30} \quad \frac{6.4}{32} \quad \frac{8.8}{50}$$

Sta	+	Δ	-	Elev
		968.25		

307

+50

308

+50

309

+50

T.P.	6.43	961.50	1318	955.07
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309

+50

310

+50

311

+19

222	952.05	11.67	949.83
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Lt

R

Rt

$$\frac{4.2}{50} \quad \frac{4.9}{32} \quad \frac{7.8}{27-21} \quad \frac{7.5}{16} \quad 7.5 \quad \frac{8.7}{17} \quad \frac{10.1}{24-28} \quad \frac{9.3}{31} \quad \frac{7.3}{35} \quad \frac{8.5}{50}$$

$$\frac{5.6}{50} \quad \frac{6.3}{32} \quad \frac{11.2}{26-21} \quad \frac{9.1}{17} \quad 8.9 \quad \frac{10.0}{17} \quad \frac{11.5}{21-28} \quad \frac{10.0}{31} \quad \frac{7.6}{35} \quad \frac{7.3}{50}$$

$$\frac{9.9}{50} \quad \frac{9.4}{34} \quad \frac{12.9}{29-23} \quad \frac{10.5}{18} \quad 10.3 \quad \frac{10.6}{14} \quad \frac{12.1}{19-25} \quad \frac{7.0}{32} \quad \frac{7.0}{50}$$

$$\frac{10.9}{50} \quad \frac{10.7}{34} \quad \frac{14.0}{29-22} \quad \frac{11.7}{17} \quad 11.6 \quad \frac{12.3}{15} \quad \frac{13.0}{19-23} \quad \frac{11.8}{27} \quad \frac{6.4}{34} \quad \frac{5.1}{50}$$

$$\frac{13.3}{50} \quad \frac{13.1}{32}$$

$$\frac{6.6}{35} \quad \frac{5.3}{50}$$

$$\frac{10.1}{35} \quad \frac{9.4}{40} \quad \frac{8.4}{43} \quad \frac{8.4}{50}$$

$$\frac{9.0}{28-22} \quad \frac{6.6}{15} \quad 6.5 \quad \frac{7.4}{18} \quad \frac{8.2}{21-24} \quad \frac{7.0}{28}$$

$$\frac{11.1}{50} \quad \frac{10.6}{30} \quad \frac{10.9}{28-22} \quad \frac{8.8}{16} \quad 8.3 \quad \frac{9.2}{18} \quad \frac{10.2}{20-25} \quad \frac{9.5}{28}$$

$$\frac{14.1}{50} \quad \frac{13.1}{26} \quad \frac{10.9}{20} \quad 10.0 \quad \frac{10.6}{16} \quad \frac{11.7}{19-24} \quad \frac{10.5}{26} \quad \frac{5.5}{34} \quad \frac{4.0}{41} \quad \frac{3.9}{50}$$

$$\frac{3.5}{36} \quad \frac{2.3}{41} \quad \frac{2.3}{50}$$

$$\frac{6.2}{36} \quad \frac{6.7}{50}$$

$$\frac{9.8}{36} \quad \frac{11.6}{50}$$

Sta + Δ - Elev

952.05

310+50

311

+19

+50

312

B.M. 9.36 952.02 942.69 942.66

+50

313

+50

T.P. 2.80 944.65 10.20 941.85

314

+33 24" x drain

315

+60

L+ £ R+

<u>6.0</u>	<u>4.9</u>	<u>3.5</u>	<u>3.1</u>	2.1	<u>2.5</u>	<u>3.8</u>	<u>3.8</u>	2.9
50	29	25	21		13	17	20	23

5.6	5.9	4.2	4.2	4.4	3.5	3.8	5.2	3.9
50	32	31	27	23	16		20	22

5.6	5.4	6.6	6.6	4.9	4.0	4.2	5.7	5.7
50	32	30	25	20		18	22	25

5.0	5.3	8.2	6.9	5.2	4.6	6.9	6.7	4.8
50	27	22	17		21	28	40	50

6.4	6.9	9.5	9.5	8.0	6.5	5.8	9.2	9.7
50	35	27	22	18		19	31	50

9.8	10.2	10.4	10.4	9.3	7.5		7.3	10.5	11.4
50	32	30	23	18			17	30	50
A1.4	A1.3	40.7	40.7	A1.4	A2.2	A3.0	A3.0	40.6	41.5
10.6	10.7	11.3	11.3	10.6	9.8	9.0	11.1	11.4	10.5
50	33	31	25	22	15	18	26	31	33
	39.2		38.9	40.7	41.8		41.6	39.6	39.5
	12.8		13.1	11.3	10.2		10.4	12.4	12.5
	50		23	18			19	25	32

37.6	37.5		40.2		40.9	40.5	38.5	37.1
7.1	7.2		9.5		3.8	4.2	6.2	7.6
50	26		16			18	25	50
36.9	35.8	35.6	37.8	40.2	40.5	39.8	34.9	35.1
7.8	8.9	8.5	4.9	9.5	4.2	4.9	8.6	9.3
50	30	29	19	11		18	29	31

39.8	38.3	36.7	36.7	39.5	40.1	39.1	34.3	32.8
4.9	6.9	8.0	8.0	5.2	4.6	5.6	10.4	11.9
50	33	31	26	17		17	30	50

38.1	37.0	36.3	36.3	39.1	39.6	38.9	36.6	36.9
6.6	7.7	8.9	8.9	5.6	5.1	5.8	8.1	7.8
50	32	31	29	17		17	23	32

Sta + Δ - Elev

944.65

316 +00

+50

317

+50

318

T.P. 7.85 948.19 4.31 940.34

+27

+50

* 319

+12

+37

+50

320

Lt.

E

Rt

38. A	37.3	36.8	39.0	39.7	38.7	35.6	35. A	35.0
6.3	7.1	7.9	5.7	5.0	6.0	9.1	9.3	8.7
50	40	23	17		17	24	36	50
39.6	38. A	37.9	39.2	39.9	38.8	37.1	36.8	36.35
5.1	6.3	6.8	5.5	4.8	5.9	2.6	2.9	8.3
50	38	22	18		17	22	36	50
39.9	38.8	38.6	39.7	40.3	39. A	38.0		
4.8	5.9	6.1	5.0	4.9	5.3	6.7	7.0	4.8
50	32	21	16		18	22	30	33

9.3	1.6	5.2	4.1	3.8	4.8	4.2	6.6	2.7	3.6
50	35	21	17		18	21	28	33	50

A

3.5	5.7	5.7	4.9	4.5	3.3	3.3	4.0	5.7	5.7	6.0	1.7
55	57	46	43	21	16		16	21	26	33	50
Naif in Cor. F.P. Lt 54 318+40											
104	86	81	69			74	9.1	8.5	2.3	2.9	
50.44	40	21	16			66	17	21-25	27	33	50

13.8	13.3	9.1	8.1	6.5	6.6	7.3	9.3	8.3	4.0	4.1
50	45	38	20	16		16	21-25	28	33	50

A.5

15.82	13.7	12.9	8.4	8.0	6.9	7.1	9.9	9.5	
Inv.	50	41	31	21	16	67	17	27-32	50

13.2	11.9	8.2	7.6	6.5	6.5	7.2	10.6	10.8	10.7
50	37	31	20	17		19	27	34	50

10.8	9.9	8.2	7.8	6.1	7.4	18.4	22.8	22.8	
<u>50</u>	<u>33</u>	<u>28</u>	<u>22</u>	<u>17</u>	5.9	<u>18</u>	<u>42</u>	<u>47</u> _{Inv.}	<u>50</u>

7.6	8.2	8.3	7.5	5.9		6.6	12.5	13.3
50	35	28	21	17	5.6	17	34	50

A3.5

6.1	6.6	5.0	5.4	7.1	9.6	11.4
50	21	17	47	17	22	33

Sta	+	π	-	Elev
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948.19

320+50

T.P.	979	955.09	289	945.30
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321

+50

322

+50

323

+20

+60

324

+05 24" x Drain

+50

+82

B.M	2.06	955.09	2.06	955.03	953.03
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Lt.

Z

Rt

$$\frac{0.3}{50} \quad \frac{0.0}{34} \quad \frac{5.0}{28-21} \quad \frac{4.2}{17}$$

$$3.8 \quad \frac{4.3}{16} \quad \frac{5.8}{20-25} \quad \frac{5.2}{27} \quad \frac{2.0}{32} \quad \frac{4.2}{50}$$

$$\frac{1.5}{50} \quad \frac{3.9}{33} \quad \frac{11.4}{25} \quad \frac{11.4}{21} \quad \frac{10.1}{16}$$

A3.5

$$9.6 \quad \frac{10.3}{16} \quad \frac{11.8}{20-27} \quad \frac{11.4}{29} \quad \frac{7.6}{33} \quad \frac{9.1}{50}$$

$$\frac{4.8}{50} \quad \frac{5.3}{33} \quad \frac{10.9}{28-21} \quad \frac{9.0}{16} \quad \frac{8.2}{17}$$

$$8.7 \quad \frac{9.4}{17} \quad \frac{10.8}{21} \quad \frac{11.1}{29} \quad \frac{8.1}{33} \quad \frac{8.7}{50}$$

$$\frac{3.6}{50} \quad \frac{3.7}{33} \quad \frac{9.1}{27} \quad \frac{9.1}{19} \quad \frac{7.9}{16} \quad 7.6$$

$$\frac{8.4}{17} \quad \frac{9.9}{21-28} \quad \frac{4.9}{33} \quad \frac{6.7}{50}$$

$$\frac{1.8}{50} \quad \frac{1.1}{33} \quad \frac{8.1}{27-21} \quad \frac{6.8}{16}$$

$$6.5 \quad \frac{7.0}{17} \quad \frac{8.7}{22} \quad \frac{8.7}{28} \quad \frac{7.1}{33} \quad \frac{10.1}{50}$$

$$\frac{2.2}{50} \quad \frac{5.5}{33} \quad \frac{7.7}{32} \quad \frac{7.4}{22} \quad \frac{5.6}{16} \quad 5.5$$

$$\frac{6.2}{18} \quad \frac{9.8}{28} \quad \frac{12.6}{50}$$

$$\frac{3.4}{50} \quad \frac{6.8}{33} \quad \frac{7.4}{32} \quad \frac{7.0}{21} \quad \frac{5.6}{16} \quad 5.0$$

$$\frac{6.0}{17} \quad \frac{9.1}{27} \quad \frac{11.1}{38} \quad \frac{12.2}{50}$$

$$\frac{2.8}{50} \quad \frac{4.1}{34} \quad \frac{6.9}{32} \quad \frac{6.7}{22} \quad \frac{4.7}{16} \quad 4.3$$

$$\frac{5.3}{18} \quad \frac{8.2}{26} \quad \frac{10.9}{50}$$

$$\frac{6.5}{50} \quad \frac{6.6}{33} \quad \frac{7.0}{29} \quad \frac{7.0}{26} \quad \frac{4.0}{16}$$

$$3.5 \quad \frac{4.7}{20} \quad \frac{11.8}{32} \quad \frac{13.7}{43} \quad \frac{14.1}{50}$$

7.62
Inv.12.28
Inv.

$$\frac{4.3}{50} \quad \frac{5.7}{41} \quad \frac{5.5}{26} \quad \frac{3.2}{16}$$

$$2.7 \quad \frac{4.0}{17} \quad \frac{13.3}{34} \quad \frac{14.9}{50}$$

$$\frac{1.5}{50} \quad \frac{2.5}{33} \quad \frac{4.2}{32} \quad \frac{4.2}{22} \quad \frac{2.4}{16}$$

$$2.2 \quad \frac{2.8}{17} \quad \frac{10.3}{33} \quad \frac{12.1}{50}$$

Spk 14 8" Oak 40' Lt Stg 324+80

Sta + λ - Elev

955.09

325

+50

+80

T. P. 11.09 965 85 0.33 954 76

325

+50

+80

326

+50

327

+50

328

+17

24" x Drain

Lt.

Rt.

Rt.

$$\frac{3.7}{29} \quad \frac{4.0}{22} \quad \frac{2.3}{16} \quad 1.8 \quad \frac{2.5}{18} \quad \frac{4.4}{24} \quad \frac{4.5}{29} \quad \frac{4.2}{33} \quad \frac{5.9}{50}$$

$$\frac{1.3}{26} \quad \frac{2.5}{23} \quad \frac{2.5}{20} \quad \frac{1.3}{16} \quad 0.8 \quad \frac{1.3}{17} \quad \frac{3.0}{22} \quad \frac{2.2}{28}$$

$$\frac{0.8}{25} \quad \frac{1.8}{22-20} \quad \frac{0.6}{16} \quad 0.3 \quad \frac{0.8}{16} \quad \frac{2.4}{22} \quad \frac{1.4}{27}$$

$$\frac{8.9}{50} \quad \frac{10.6}{34}$$

$$\frac{4.2}{50} \quad \frac{4.7}{33}$$

$$\frac{8.1}{33} \quad \frac{8.5}{50}$$

$$\frac{1.2}{50} \quad \frac{0.5}{33}$$

$$\frac{4.9}{33} \quad \frac{4.7}{50}$$

$$\frac{1.3}{50} \quad \frac{0.5}{33} \quad \frac{11.1}{25} \quad \frac{12.3}{22-20} \quad \frac{10.9}{16} \quad 10.7 \quad \frac{11.3}{18} \quad \frac{12.7}{22} \quad \frac{11.7}{27} \quad \frac{5.0}{34} \quad \frac{4.3}{50}$$

$$\frac{6.7}{50} \quad \frac{6.6}{39} \quad \frac{7.1}{33} \quad \frac{11.6}{27} \quad \frac{11.4}{22} \quad \frac{9.8}{17} \quad 9.6 \quad \frac{10.4}{17} \quad \frac{11.8}{22-26} \quad \frac{10.9}{30} \quad \frac{6.8}{33} \quad \frac{5.6}{50}$$

$$\frac{7.6}{50} \quad \frac{8.6}{33} \quad \frac{10.8}{28} \quad \frac{9.7}{22} \quad \frac{8.5}{16} \quad 8.1 \quad \frac{8.8}{17} \quad \frac{10.4}{23} \quad \frac{10.4}{29} \quad \frac{8.0}{33} \quad \frac{8.6}{50}$$

$$\frac{8.0}{50} \quad \frac{8.9}{23} \quad \frac{6.8}{17} \quad 6.5 \quad \frac{6.8}{17} \quad \frac{9.7}{29} \quad \frac{10.0}{50}$$

$$\frac{8.1}{50} \quad \frac{7.5}{24} \quad \frac{5.4}{16} \quad 5.0 \quad \frac{5.9}{18} \quad \frac{10.1}{30} \quad \frac{11.0}{36} \quad \frac{12.1}{50}$$

$$\frac{8.1}{50} \quad \frac{8.5}{25} \quad \overset{\text{Inv}}{\frac{8.67}{25}} \quad \frac{5.0}{18} \quad 4.4 \quad \frac{5.4}{19} \quad \overset{\text{Inv}}{\frac{10.48}{29}} \quad \frac{10.6}{30} \quad \frac{11.9}{50}$$

Sta + A - Elev

965.85

328+50

329

+50

330

T.P. 12.41 977.72 0.54 965.31

330

+50

331

+50

332

+50

333

T.P. 12.52 989.04 1.20 976.52

330

Lt.

Z

Rt

$$\frac{8.0}{50} \quad \frac{8.1}{33} \quad \frac{5.5}{25} \quad \frac{5.1}{21} \quad \frac{4.0}{17} \quad 33 \quad \frac{4.1}{19} \quad \frac{9.5}{33} \quad \frac{10.5}{50}$$

$$\frac{5.2}{50} \quad \frac{4.8}{36} \quad \frac{3.3}{26} \quad \frac{3.1}{21} \quad \frac{1.8}{17} \quad 17 \quad \frac{2.7}{19} \quad \frac{9.4}{31} \quad \frac{10.3}{37} \quad \frac{11.2}{50}$$

$$\frac{14.0}{50} \quad \frac{0.4}{37} \quad \frac{0.1}{34} \quad \frac{1.0}{31} \quad \frac{1.0}{21} \quad \frac{0.0}{17} \quad 0.0 \quad \frac{0.7}{18} \quad \frac{6.8}{29} \quad \frac{8.6}{34} \quad \frac{10.2}{50}$$

$$\frac{1.3}{30} \quad \frac{4.4}{50}$$

$$\frac{10.3}{26} \quad \frac{11.0}{19} \quad 9.5 \quad \frac{10.0}{19} \quad \frac{11.5}{32}$$

$$\frac{8.2}{22} \quad \frac{8.7}{18} \quad \frac{8.0}{16} \quad 7.6 \quad \frac{8.2}{16} \quad \frac{9.9}{22} \quad \frac{9.9}{26} \quad \frac{9.3}{29} \quad \frac{5.3}{32} \quad \frac{7.7}{50}$$

$$\frac{6.4}{24} \quad \frac{7.3}{18} \quad \frac{6.7}{13} \quad 6.4 \quad \frac{7.1}{17} \quad \frac{8.6}{23} \quad \frac{7.7}{27} \quad \frac{1.8}{33} \quad \frac{3.4}{50}$$

$$\frac{5.8}{25} \quad \frac{6.8}{22-18} \quad \frac{5.8}{15} \quad 5.4 \quad \frac{6.1}{16} \quad \frac{7.3}{20-24} \quad \frac{6.6}{27} \quad \frac{0.8}{33} \quad \frac{1.7}{50}$$

$$\frac{5.3}{25} \quad \frac{6.5}{21} \quad \frac{6.5}{18} \quad \frac{5.6}{15} \quad 5.2 \quad \frac{5.8}{17} \quad \frac{7.2}{20} \quad \frac{7.2}{23} \quad \frac{6.0}{28} \quad \frac{0.5}{33} \quad \frac{1.8}{50}$$

$$\frac{6.2}{26} \quad \frac{7.1}{23-20} \quad \frac{6.0}{16} \quad 5.5 \quad \frac{6.1}{16} \quad \frac{7.4}{20} \quad \frac{7.4}{25} \quad \frac{6.6}{28} \quad \frac{1.2}{33} \quad \frac{2.5}{50}$$

$$\frac{7.2}{50} \quad \frac{6.8}{34} \quad \frac{8.4}{31} \quad \frac{8.3}{22} \quad \frac{7.0}{17} \quad 6.4 \quad \frac{7.1}{18} \quad \frac{8.6}{22} \quad \frac{8.6}{25} \quad \frac{7.6}{28} \quad \frac{1.9}{33} \quad \frac{0.9}{50}$$

$$\frac{5.0}{75} \quad \frac{7.9}{43} \quad \frac{11.9}{32}$$

Sta + Δ - Elev

989.04

330+50

331

+50

332

+50

T.P. 0.55 977 07 12.52 976.52

333+50

334

+50

+81

335

+50

T.P. 3.06 967 01 13.12 963.95

335+50

Lt

2

Rt

$$\frac{21}{75} \quad \frac{34}{50} \quad \frac{31}{40} \quad \frac{45}{37} \quad \frac{56}{33}$$

$$\frac{38}{75} \quad \frac{44}{50} \quad \frac{47}{37} \quad \frac{60}{33}$$

$$\frac{44}{75} \quad \frac{58}{50} \quad \frac{71}{33}$$

$$\frac{70}{75} \quad \frac{66}{50} \quad \frac{72}{33}$$

$$\frac{117}{75} \quad \frac{103}{50} \quad \frac{95}{33}$$

$$\frac{82}{50} \quad \frac{83}{34} \quad \frac{94}{32} \quad \frac{91}{22} \quad \frac{76}{18} \quad 7.2 \quad \frac{7.9}{18} \quad \frac{9.5}{22} \quad \frac{9.5}{30} \quad \frac{6.5}{33} \quad \frac{61}{50}$$

$$\frac{9.0}{50} \quad \frac{93}{34} \quad \frac{106}{31} \quad \frac{107}{22} \quad \frac{85}{17} \quad 8.7 \quad \frac{95}{18} \quad \frac{112}{22-29} \quad \frac{97}{32} \quad \frac{78}{33} \quad \frac{65}{50}$$

$$\frac{71}{50} \quad \frac{72}{34} \quad \frac{11.2}{29} \quad \frac{12.2}{22} \quad \frac{10.3}{17} \quad 10.3 \quad \frac{10.6}{17} \quad \frac{11.9}{21-28} \quad \frac{11.3}{31} \quad \frac{7.4}{34} \quad \frac{61}{50}$$

$$\frac{6.6}{50} \quad \frac{5.2}{34} \quad \frac{12.9}{25} \quad \frac{12.9}{22} \quad \frac{111}{17} \quad 11.2 \quad \frac{11.8}{16} \quad \frac{13.3}{21-26} \quad \frac{12.3}{28} \quad \frac{5.7}{34} \quad \frac{4.9}{50}$$

$$\frac{6.8}{50} \quad \frac{63}{34} \quad \frac{13.2}{27} \quad \frac{13.2}{22} \quad \frac{11.8}{17} \quad 11.8 \quad \frac{12.6}{18} \quad \frac{141}{23} \quad \frac{12.9}{27} \quad \frac{5.9}{34} \quad \frac{4.8}{50}$$

$$\frac{96}{50} \quad \frac{12.0}{33}$$

$$\frac{9.5}{33} \quad \frac{91}{50}$$

$$\frac{4.9}{30} \quad \frac{4.9}{22} \quad \frac{33}{17} \quad 3.1 \quad \frac{3.7}{16} \quad \frac{41}{19} \quad \frac{5.7}{25} \quad \frac{5.2}{28}$$

Sta	+	Δ	-	Elev
-----	---	----------	---	------

967.01

336

+50

337

+50

+62

+85

338

+

$\pm$ Lexington

B.M

5.57 961.44 961.43

Lt

£

Rt

$$\frac{60}{50} \quad \frac{50}{33} \quad \frac{6.2}{31} \quad \frac{6.2}{23} \quad \frac{4.5}{17} \quad 40 \quad \frac{49}{17} \quad \frac{5.5}{20} \quad \frac{6.4}{24} \quad \frac{6.4}{28} \quad \frac{5.8}{30} \quad \frac{2.5}{34} \quad \frac{1.9}{50}$$

$$\frac{129}{50} \quad \frac{12.6}{35} \quad \frac{5.8}{21} \quad \frac{5.1}{17} \quad 45 \quad \frac{5.2}{17} \quad \frac{8.9}{29} \quad \frac{8.7}{35} \quad \frac{86}{50}$$

$$\frac{203}{71} \quad \frac{21.6}{54} \quad \frac{20.4}{50} \quad \frac{6.4}{20} \quad \frac{5.4}{16} \quad \frac{5.4}{11} \quad 5.1 \quad \frac{6.1}{16} \quad \frac{6.2}{18} \quad \frac{15.0}{39} \quad \frac{14.6}{50}$$

$$\frac{236}{66} \quad \frac{18.2}{50} \quad \frac{6.2}{25} \quad \frac{6.3}{21} \quad \frac{5.5}{11} \quad 5.5 \quad \frac{5.9}{11} \quad \frac{6.5}{20} \quad \frac{7.1}{24} \quad \frac{19.8}{50} \quad \frac{21.8}{65}$$

$$\frac{214}{75} \quad \frac{18.3}{65} \quad \frac{15.3}{51} \quad \frac{6.1}{31} \quad \frac{5.4}{27} \quad \frac{5.5}{14} \quad 5.6 \quad \frac{6.2}{15} \quad \frac{6.8}{24} \quad \frac{7.1}{28} \quad \frac{19.8}{50} \quad \frac{21.8}{65}$$

$$\frac{4.5}{50} \quad \frac{5.0}{39} \quad \frac{5.2}{22} \quad 5.9 \quad \frac{6.7}{23} \quad \frac{7.7}{40} \quad \frac{7.7}{50}$$

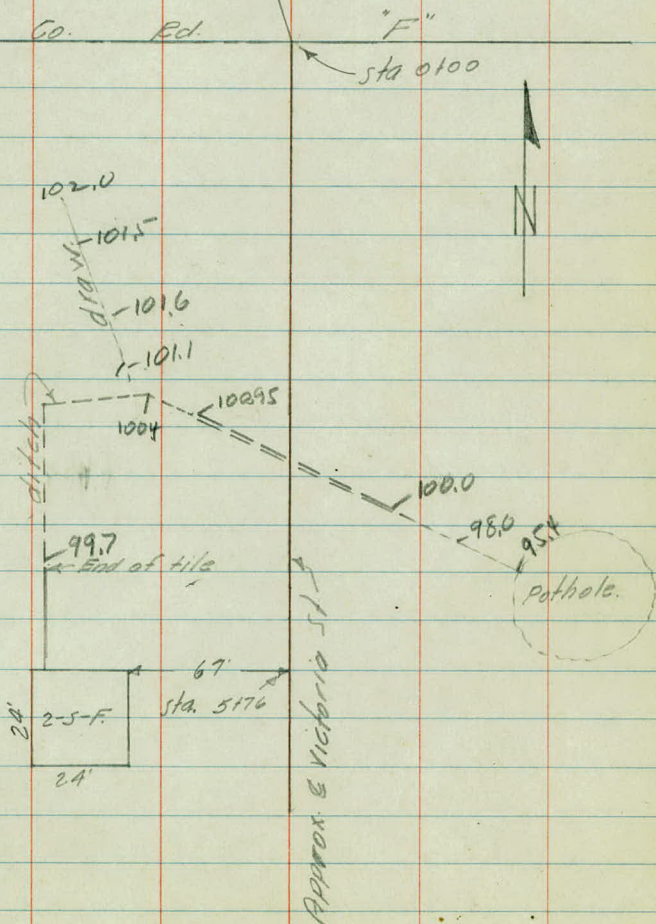
$$\frac{3.9}{50} \quad 5.6 \quad \frac{7.5}{50}$$

$$\frac{1.8}{100} \quad \frac{3.8}{50} \quad 5.4 \quad \frac{7.4}{50} \quad \frac{8.7}{100}$$

Top Mon. Lex + Victoria

Sta + π - Elev

Victoria st Levels at X Drain south of Co Rd "F"



Sta.	+	π	-	Elev.
B.M.	13.0	113.0		100.0

3 +00

+50

4

+50

+54 Δ in ditch rt.

+60 Δ in ditch rt.

+69 End 24" G.M. Rt.

5

ditch from tank 51 = G. road

11-9-44

K.A.
L.C.
G.F.

Lt.

E

Rt.

FL East End of Gully

102.0
110
110

101.5
115
100

101.6
114
85

119
67

124
60

126
86

1205
30

133
93

Low land

ditch from
Septic tank

FL

Sta	+	π	-	Elev
-----	---	-------	---	------

5	102			
---	-----	--	--	--

136	End of Tile from tank			
-----	-----------------------	--	--	--

Lt.

E

Rt.

West edge
of path hole

F.L.

100.00

176

150

130

96

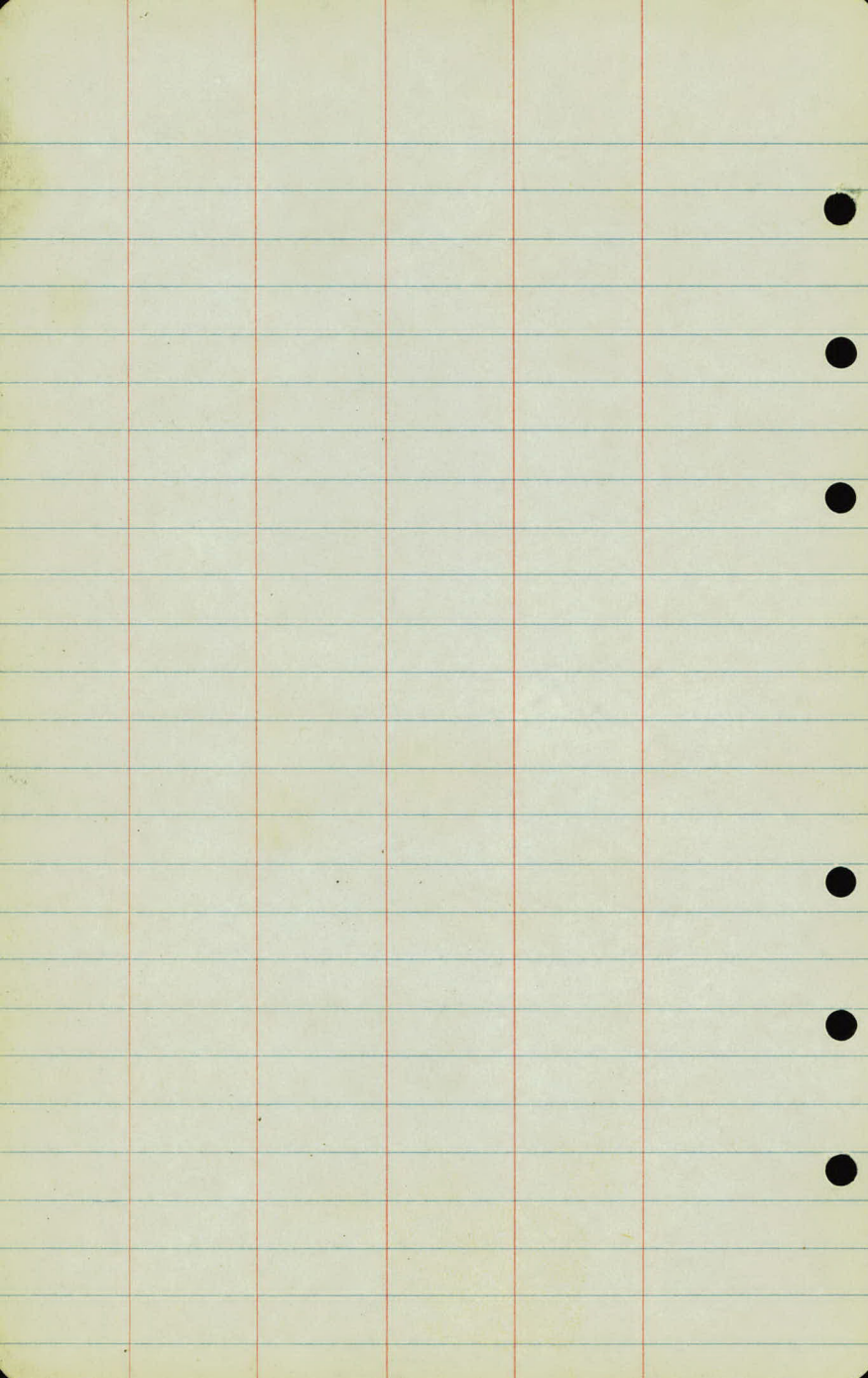
81

32

FL. 4" Tile

124

97



Victoria St
& Levels
from Co. Rd "F" South

Sta	+	π	-	Elev
B.M.	9.27	990.50		981.23 990.50

0 +00	=E.C. rd "E"		9.6	80.9
-------	--------------	--	-----	------

1			9.0	81.5
---	--	--	-----	------

2			7.6	82.9
---	--	--	-----	------

3			6.1	84.4
---	--	--	-----	------

4			5.0	85.5
---	--	--	-----	------

+	^{X.DRAIN} FL. Culv rt.		12.00	78.5
---	------------------------------------	--	-------	------

5			5.1	85.4
---	--	--	-----	------

6			5.0	85.5
---	--	--	-----	------

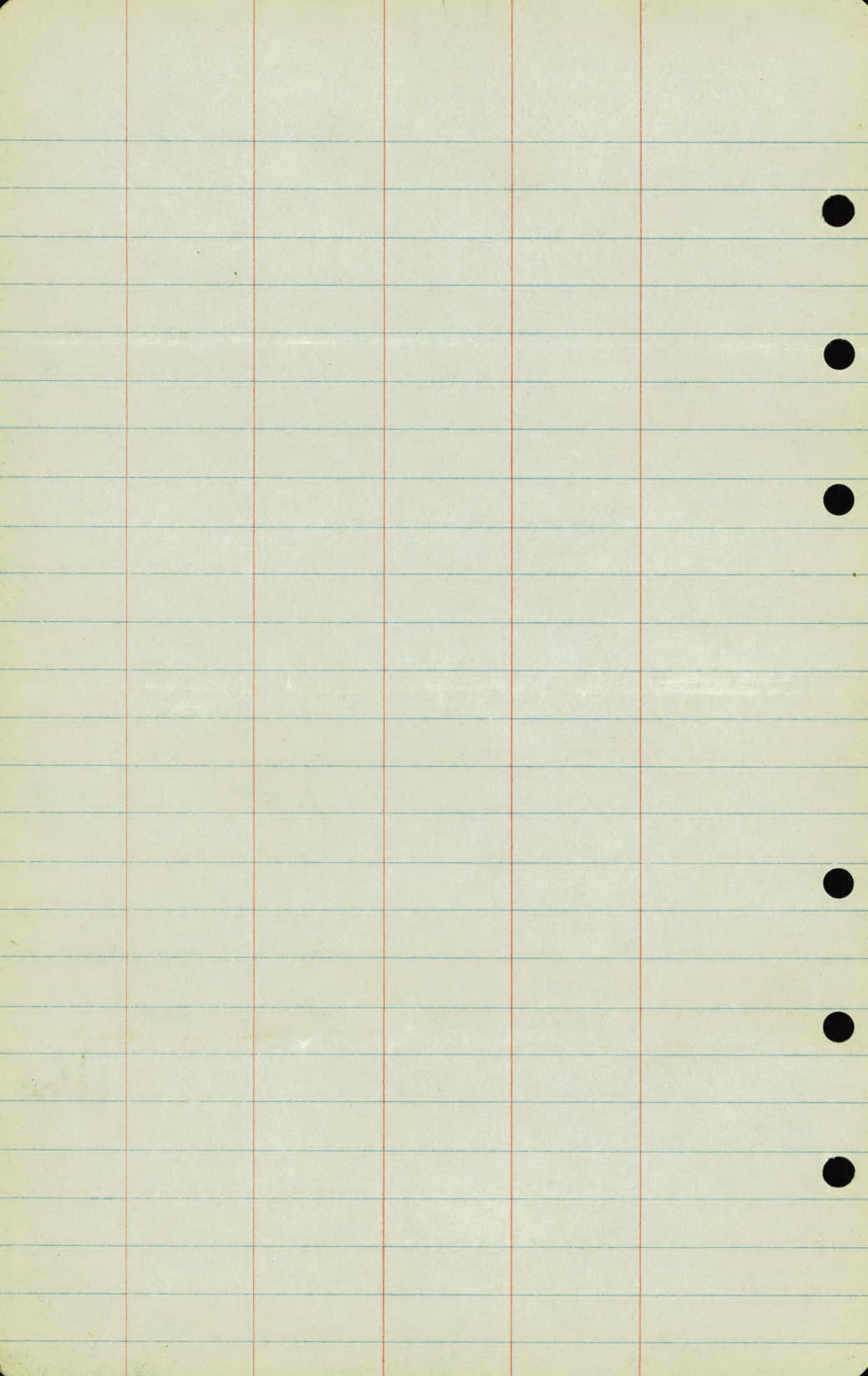
11-13-44

lt

e

pt.

Spk in PP SW Cor. Cord R. & Victoria St.



Victoria St.

Check Levels @ "F"

B.M.	2.90	996.88			993.98
------	------	--------	--	--	--------

T.P.	7.97	1003.84	1.01	995.87	
------	------	---------	------	--------	--

✓	2.25	999.77	6.32	997.52	
---	------	--------	------	--------	--

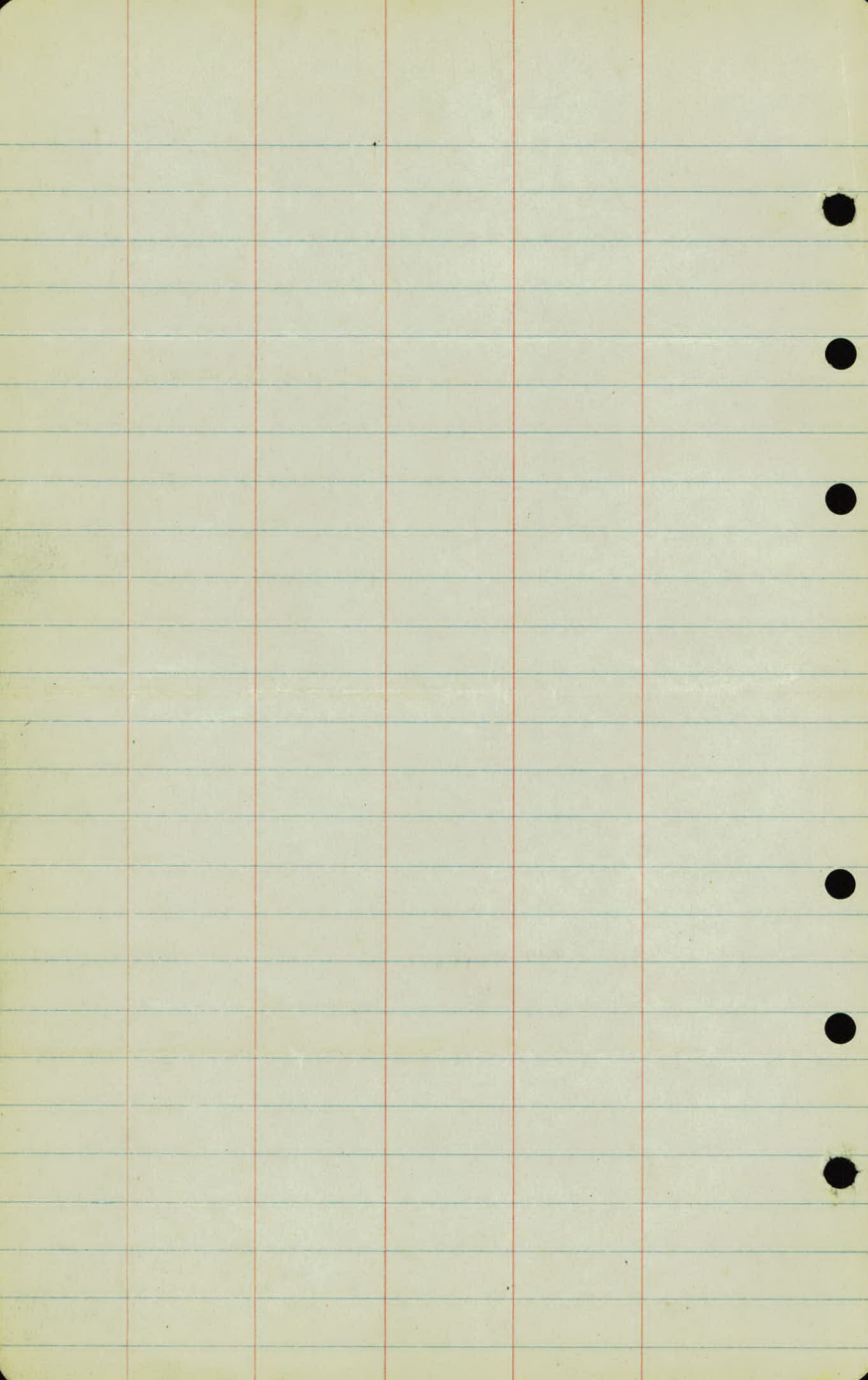
✓	1.68	993.03	8.42	991.35	
---	------	--------	------	--------	--

✓	1.73	987.60	7.20	985.87	
---	------	--------	------	--------	--

B.M.			6.38	981.22	981.23
------	--	--	------	--------	--------

R.R. Spk. In 12" Oak 50' Rt. Sta. 157+40

Spk. In P.P. S.W. Cor. Co. Rd. "F" + Victoria St.



5-28-48

BENSH - LEVELS

VICTORIA - ST

Co. RD. B - TO - LEXINGTON

5.09

STA	+	∇	-	ELEV
B.M.	4.80	938.81		934.01
	8.85	941.72	5.94	932.87
	4.26	942.46	3.52	938.20
	4.77	942.70	4.53	937.93
B.M.	0.05	938.12	4.63	938.07
	0.39	924.88	13.63	924.49
	0.10	911.86	13.12	911.76
	0.10	900.06	11.90	899.96
	6.33	896.36	10.03	890.03
	6.00	901.60	0.76	895.60
	6.33	898.48	9.45	892.15
B.M.			3.46	895.02
	13.31	911.20	0.59	897.89
	6.61	917.47	0.34	910.86
B.M.	4.24	914.64	7.07	910.40
	1.78	907.51	8.91	905.73
	5.10	904.71	7.90	899.61
	9.33	913.90	0.14	904.57
B.M.	11.36	920.00	5.26	908.64
	11.48	930.68	0.80	919.20
	12.27	942.34	0.61	930.07
B.M.			2.33	940.01
	12.71	954.62	0.43	941.91

Top. MONT. AT VICTORIA + Co. RD. B

Top MONT. AT VICTORIA + Co. RD. B. 2

Top BREATHER PIPE N.E COR VICTORIA + C

Top S.W. Cor Conc. Platform of School "C" & Victoria

SPIKE IN P. POLE N.E COR. VICTORIA + Co. RD C-2

Top S.E COR LOWER STEP 2963 VICTORIA

STA	+	Δ	-	ELEV
-----	---	----------	---	------

954.62

5.85	959.46	1.01	953.61
------	--------	------	--------

3.88	957.27	6.07	953.39
------	--------	------	--------

5.30	957.46	5.11	952.16
------	--------	------	--------

5.19	960.98	1.67	955.79
------	--------	------	--------

B.M

4.21	956.77
------	--------

4.53	959.14	6.37	954.61
------	--------	------	--------

2.29	952.68	8.75	950.39
------	--------	------	--------

3.91	950.45	6.14	946.54
------	--------	------	--------

3.94	948.24	6.15	944.30
------	--------	------	--------

B.M.

5.34	947.93	5.65	942.59
------	--------	------	--------

942.90

12.17	956.77	3.33	944.60
-------	--------	------	--------

9.55	965.88	0.44	956.33
------	--------	------	--------

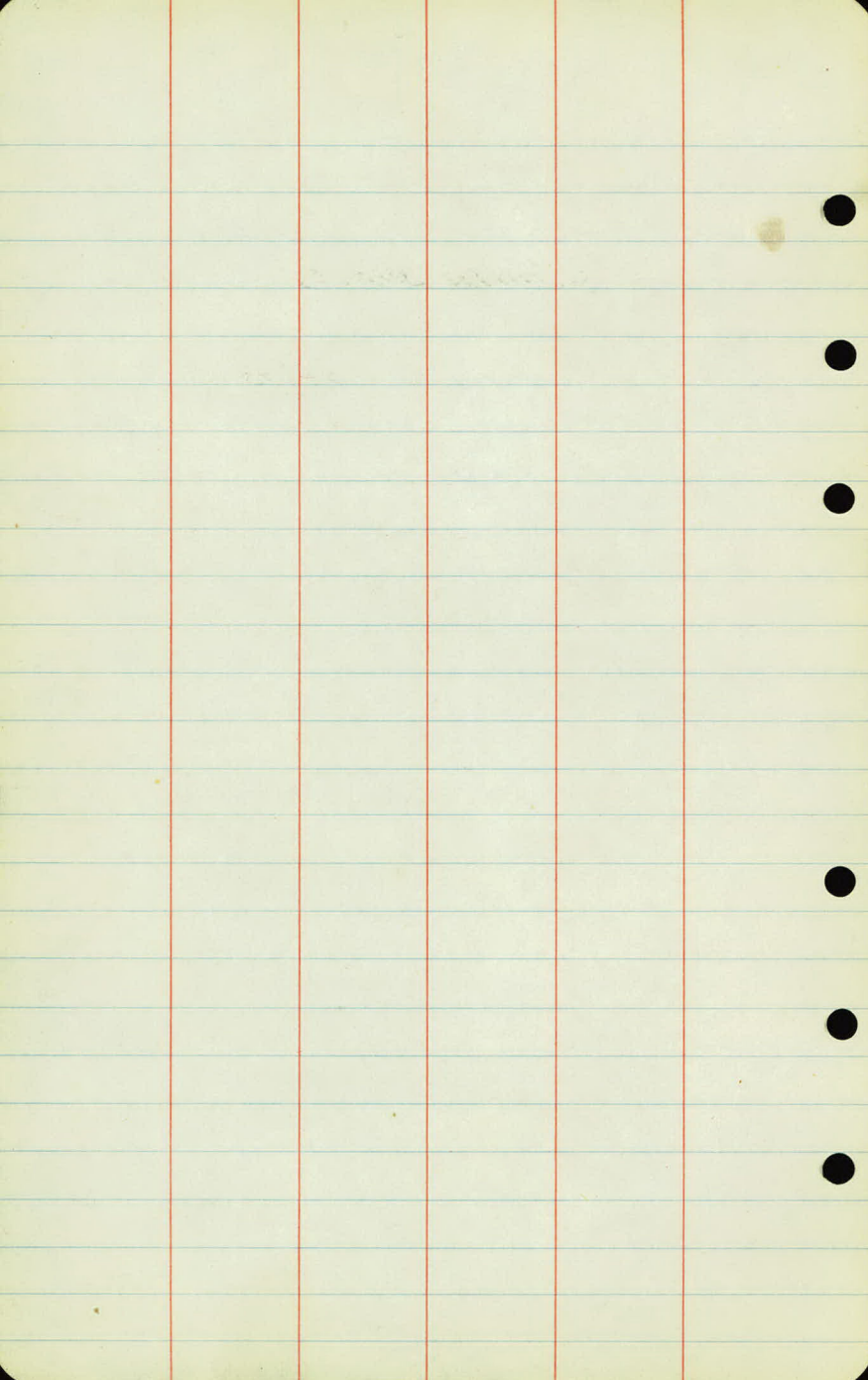
1.97	963.91
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964.28

SPIKE IN P. POLE LEFT SEC CON

SPIKE IN 15" OAK S.E. ABROGAST 700' S.E.

SPIKE IN 15" OAK 700' N.W. of HARRIET-AU



Bench Levels

Co. Rd. "C"

Hamline Ave to

Sta.	+	π	-	Elev.
B.M.	4.67	927.35		(922.68)
B.M.			4.38	922.97 (923.21)

Lowered 0.24 to conform to Handing Avg Data

B.M.	1.25	940.08		938.83 (939.07)
T.P.	0.43	927.36	13.15	926.93
T.P.	12.63	929.65	0.34	927.02
T.P.	0.79	934.12	6.32	933.33
T.P.	0.32	920.78	13.66	920.46
T.P.	4.83	916.70	8.91	911.81
B.M.			6.47	910.23

check of 1941 Survey Cor'd. "C" ↓

B.M.	5.64	916.94		911.30
B.M.			6.29	910.65 (910.42)
B.M.	6.87	929.55		(922.68)
B.M.			2.57	926.98 (922.19)

3-31-46

(1945 Data)
R.R. spk. in 18" O. N.W. Cor. "C" & Hamline Ave.

Spk. in G.P. N.E. Cor. "C" & Hamline Ave.

$$\begin{array}{r} 923.21 \\ 2297 \\ \hline 0.24 \end{array}$$

Spk. in stump N.W. Cor. "C" & Lexington Ave.

$$\begin{array}{r} 939.07 \\ - 0.24 \\ \hline 938.83 \end{array}$$

Top S.W. Cor. Conc. Platform at School ("C" & Victoria)

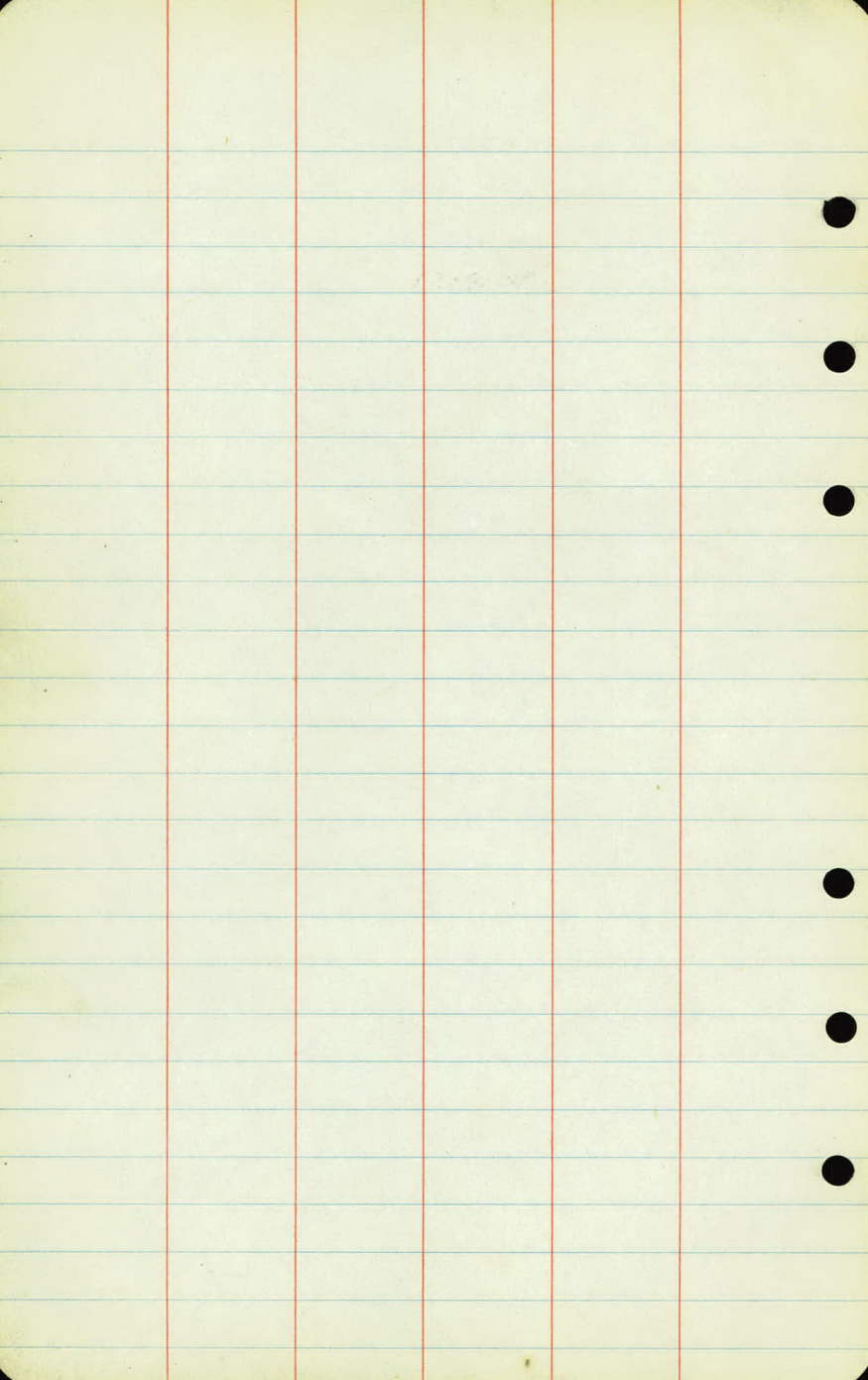
Spk. in P.P. E. of Victoria & "C"

(Lowered 0.25' to conform with Hamline Ave)

Top S.W. Cor. Conc. Platform Lake Oswego School

(Hamline Data)
Spk. in 18" O N.W. Cor. C & Hamline Ave.

Top Mont. at Hamline & "C"

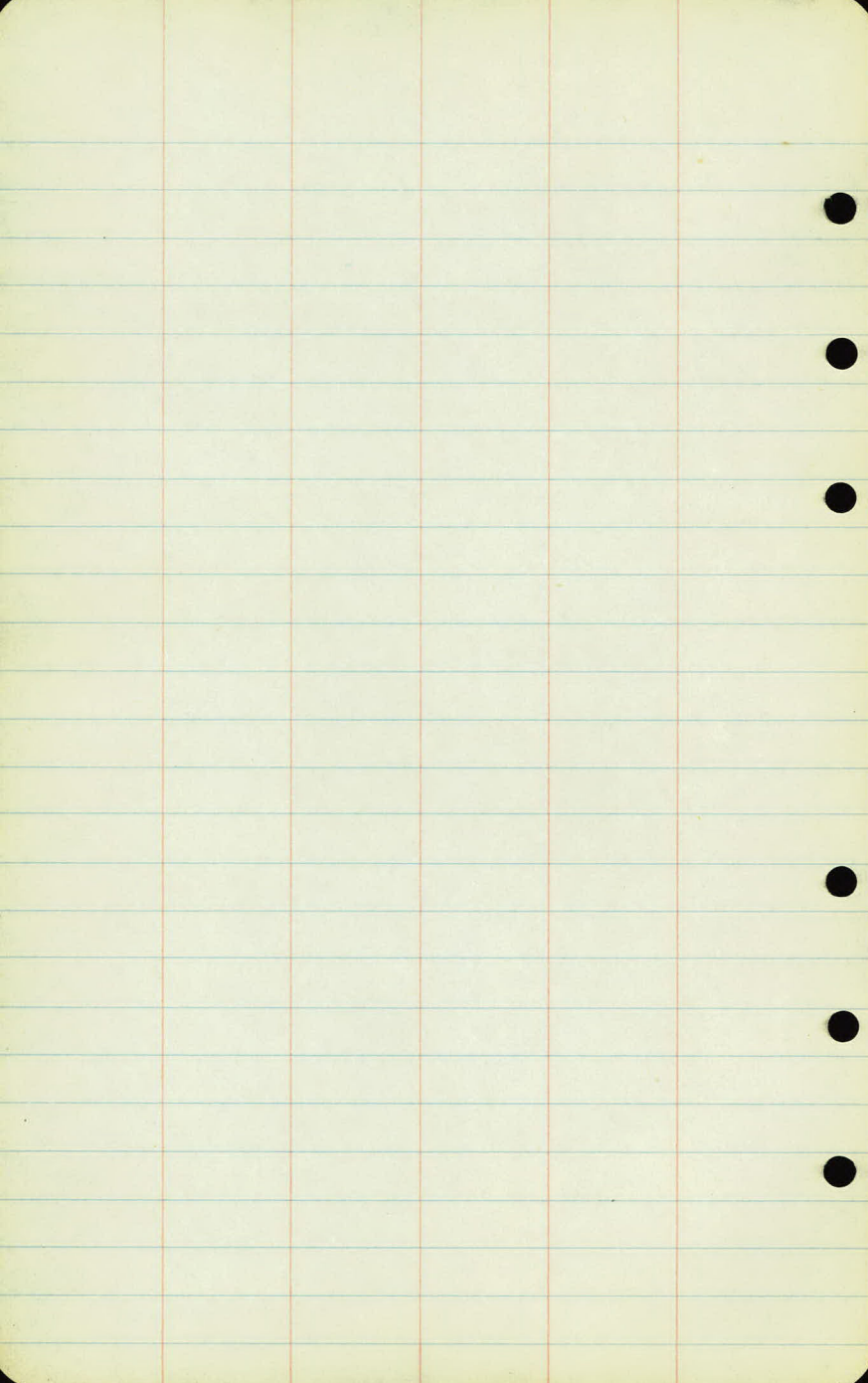


$\frac{1}{2}$ π - E/ev.

Lexington Ave.

B.M. =	2.14	1009.32		(1007.18)
T.P.	1.08	997.82	12.58	996.74
T.P.	0.06	984.24	13.64	984.18
B.M.	0.25	974.17	10.32	973.92 (373.98)
B.M.			12.38	961.79 ←

Top Mont. at Victoria St.



BENCH - LEVELS

Co. RD-E-

STW #51 To VICTORIA

STA + π - ELEV.

B.M. 13.58 930.23 916.65

12.56 942.36 0.43 929.80

3.83 945.27 0.92 941.44

3.60 936.47 12.40 932.87

11.18 937.22 10.43 926.04

7.30 944.06 0.46 936.76

4.29 943.43 4.92 939.14

9.39 950.16 2.66 940.77

B.M. 7.71 953.32 4.55 945.61

9.25 951.22 11.35 941.97

12.15 962.67 0.70 950.52

0.71 957.17 6.21 956.46

7.32 955.88 8.61 948.56

B.M. 11.29 965.82 1.35 954.53

B.M. 1.92 963.90

B.M. 4.75 950.39 (945.61) 96

B.M. 4.12 946.27

Top + E of S. END. CONC. PUMP BASE ^{N.W. COR} CORD. E & STH. S

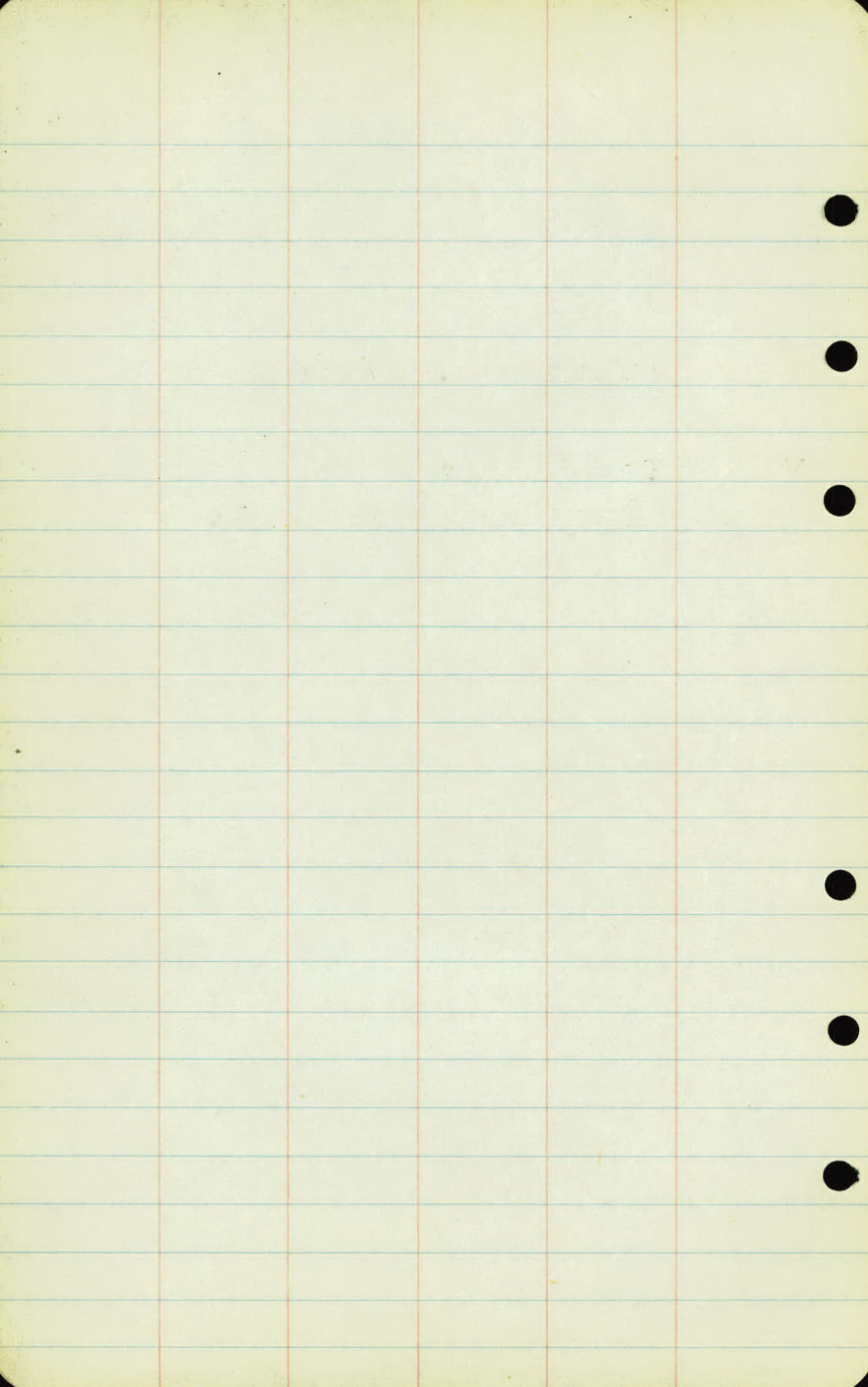
Top S. E & RAD. WALL OIL-TANKS LEXINGTON + COR. E

Top S.W. BOLT of SIGNAL XING S.E. COR S 00-LINE ^{+ VICTOR}
SPIKE 15" OAK 200' N & W of HARRIET AVE

Top S.E. & Rad Wall Oil Tanks

Top Mont at "E" & Lex.

.64



BENCH - LEVELS

STH. #8 + 96

TO LEXINGTON + VICTORIA

STA	+	⌵	-	ELEV
B.M	2.75	916.29		913.54
	3.83	911.03	9.09	907.20
	3.27	907.09	7.21	903.82
	7.54	905.27	9.36	897.73
	13.42	918.69	0.00	905.27
B.M	7.80	925.71	0.78	917.91
	8.78	932.04	2.45	923.26
	12.55	942.85	1.74	930.30
	13.76	956.46	0.15	942.70
B.M			4.11	952.35
	12.88	969.20	0.14	956.32
	13.71	982.86	0.05	969.15
	9.91	992.64	0.13	982.73
	1.10	984.93	8.81	983.83
	0.15	972.21	12.87	972.06
	2.11	960.98	13.34	958.87
B.M	11.99	966.43	6.54	954.44
	8.81	975.21	0.03	966.40
	0.75	966.52	9.44	965.77
	0.06	953.11	13.47	953.05
	6.83	954.89	5.05	948.06
B.M			6.31	948.58
	7.85	959.49	3.25	951.64

U.S.G.S N.E. COR. STH #8 + STH #96

No. COR. CONC BASE CONTROL BOX
S.W. COR STH #96 + #10

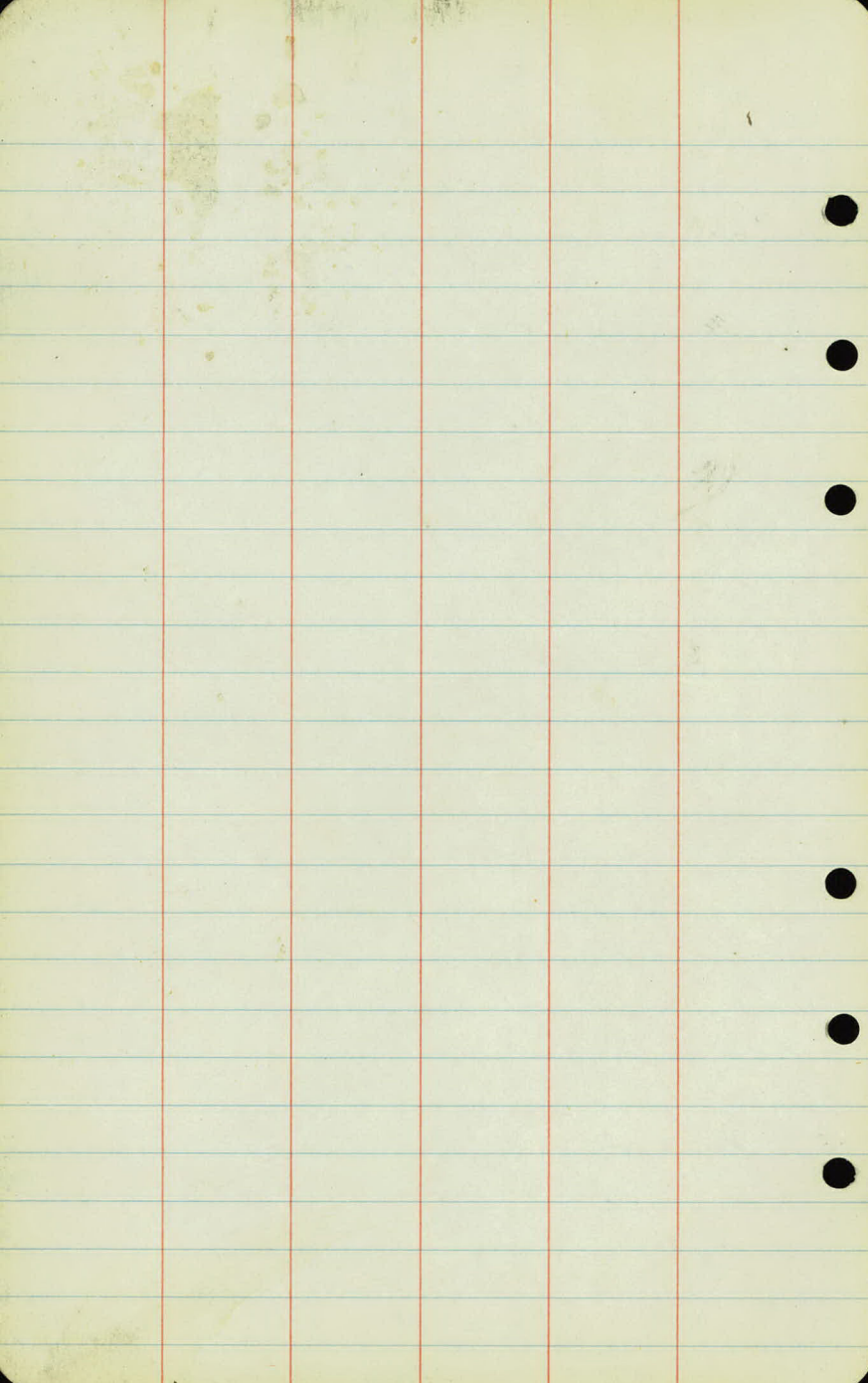
P. POLE & STH #96 50' EAST SNELLING - AVE

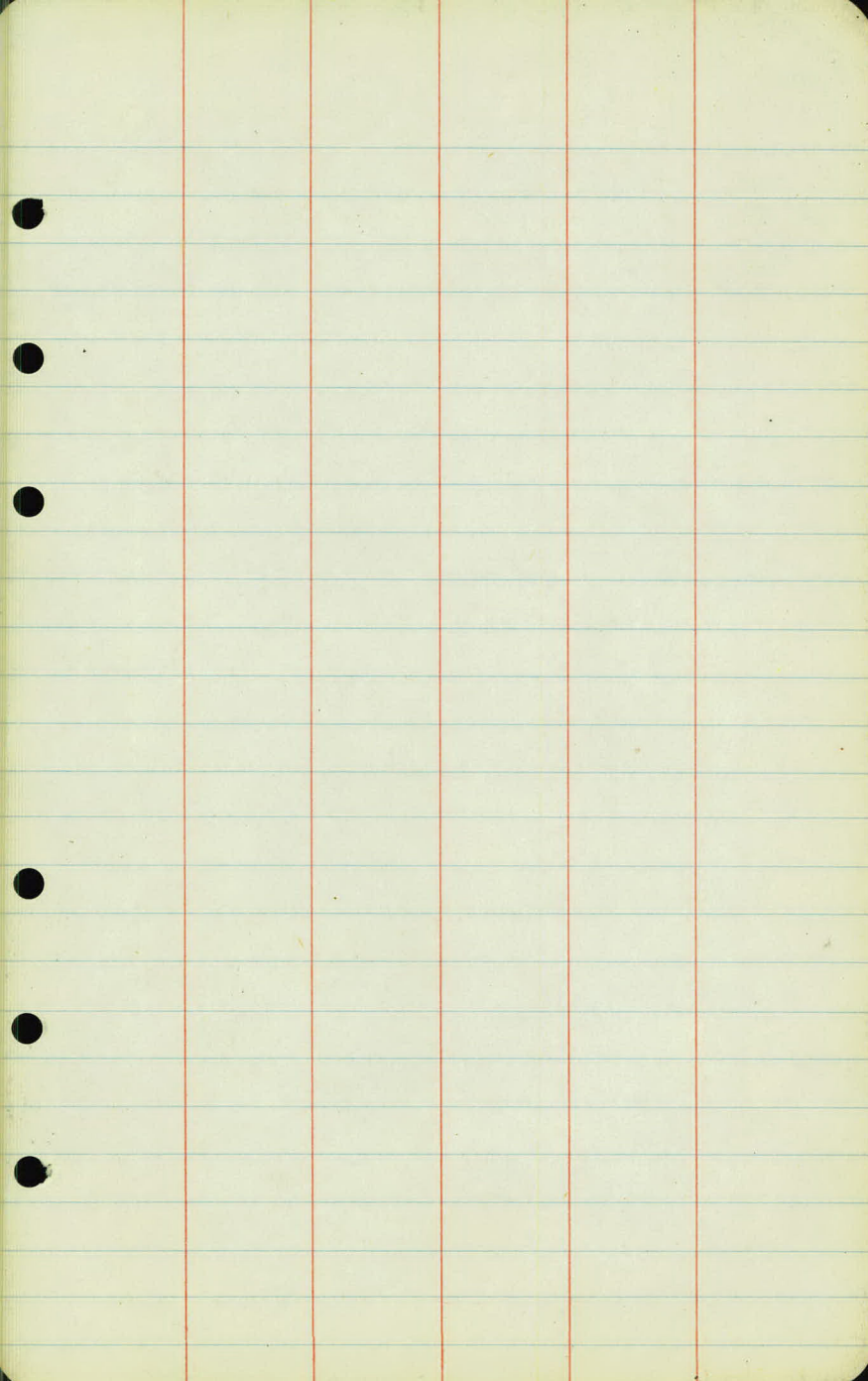
P. POLE S.W. COR STH #96 + HAMLINE AVE

TOP MONT LEXINGTON + STH #96

STA	+	π	-	ELEV
		959.49		
	6.54	965.90	0.13	959.36
	5.26	966.86	4.30	961.60
B.M.			555	961.31 (961.43)

Top Mount. at Lex. & Victoria





Larp Ave

Top Mast at Len. & Victoria

Spt. in 15" oak 200' N.W. of Harriet Ave

1

Top s.w. cor. conc. platform at School (Co. Rd. "C")

Top Mast at Co. Rd. "B"

Drill Hole at Larpentour Ave.

93433

Elev. from Various Surveys

Hamline

Gold B Lex. Gold E Gold C Victoria Rice St

961.75

(.32)

961.43

963.90

.55

963.35

964.23

(.93)

(.61)

910.42 909.81

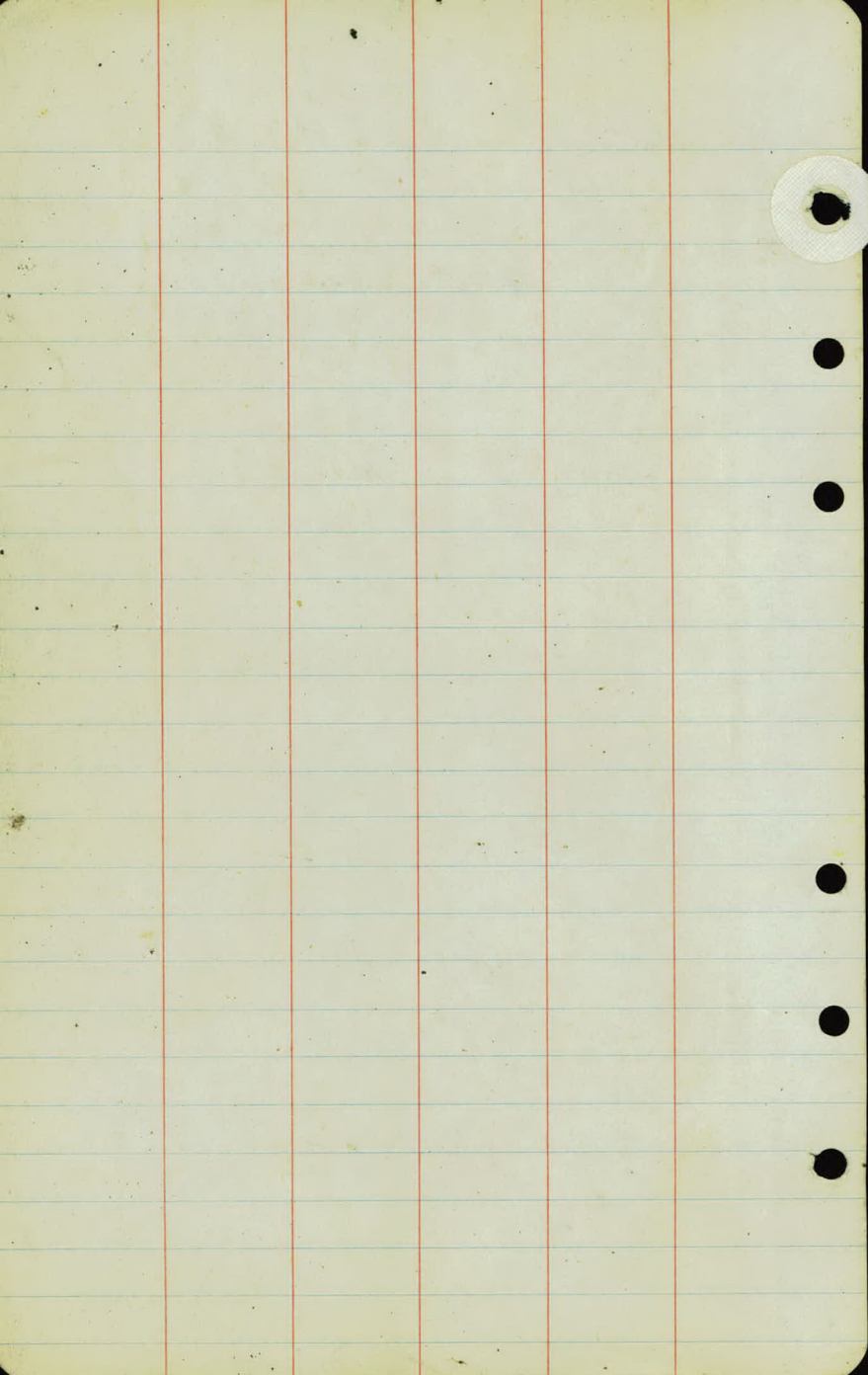
934.01

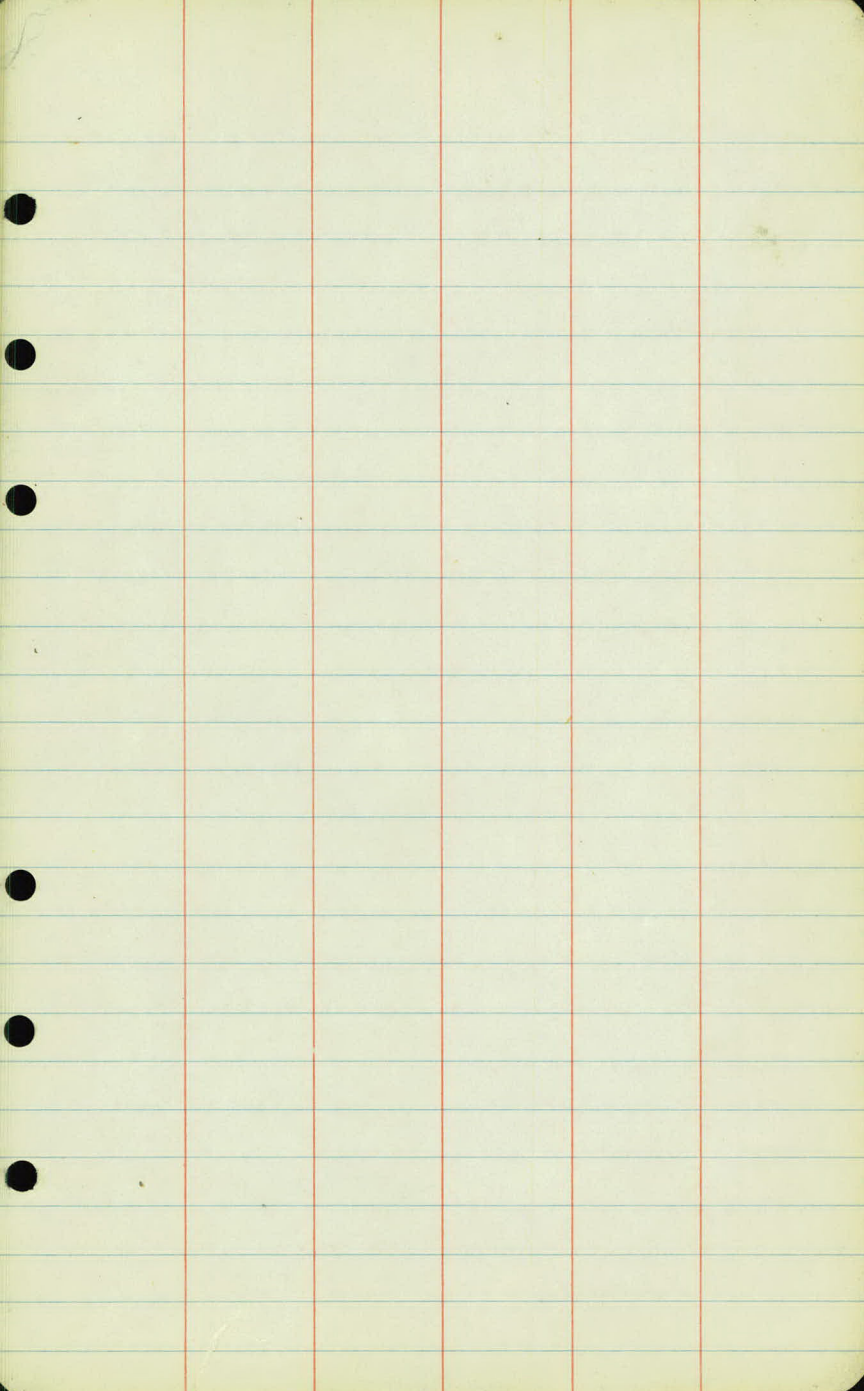
(.73)

933.28

(.69)

933.64





+40 Post Rtie Ho 73.8

+08 Post Rtie 63.6

220

+78 PC 61.5

+44 Rtie

+33 Cor Ga 46.7

+07 Rtie S. side

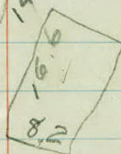
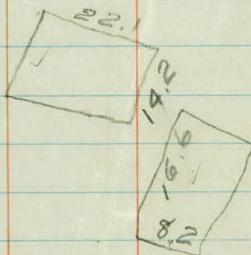
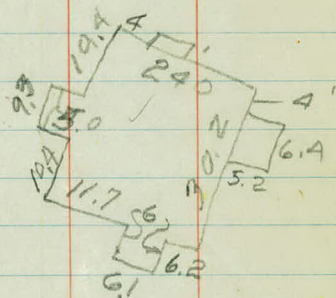
217

218+98 S.W. Cor Horse barn 56.0

211+11.8 S.E. Cor. Ho, 69'

209+11 S.E. Cor Ho 64.4

Jan, 10, 1965



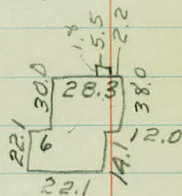
R/6

66.6

R/5

108.10

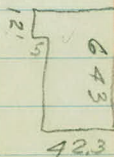
88.9



P.I.

62.92

95.10

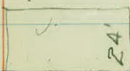
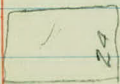


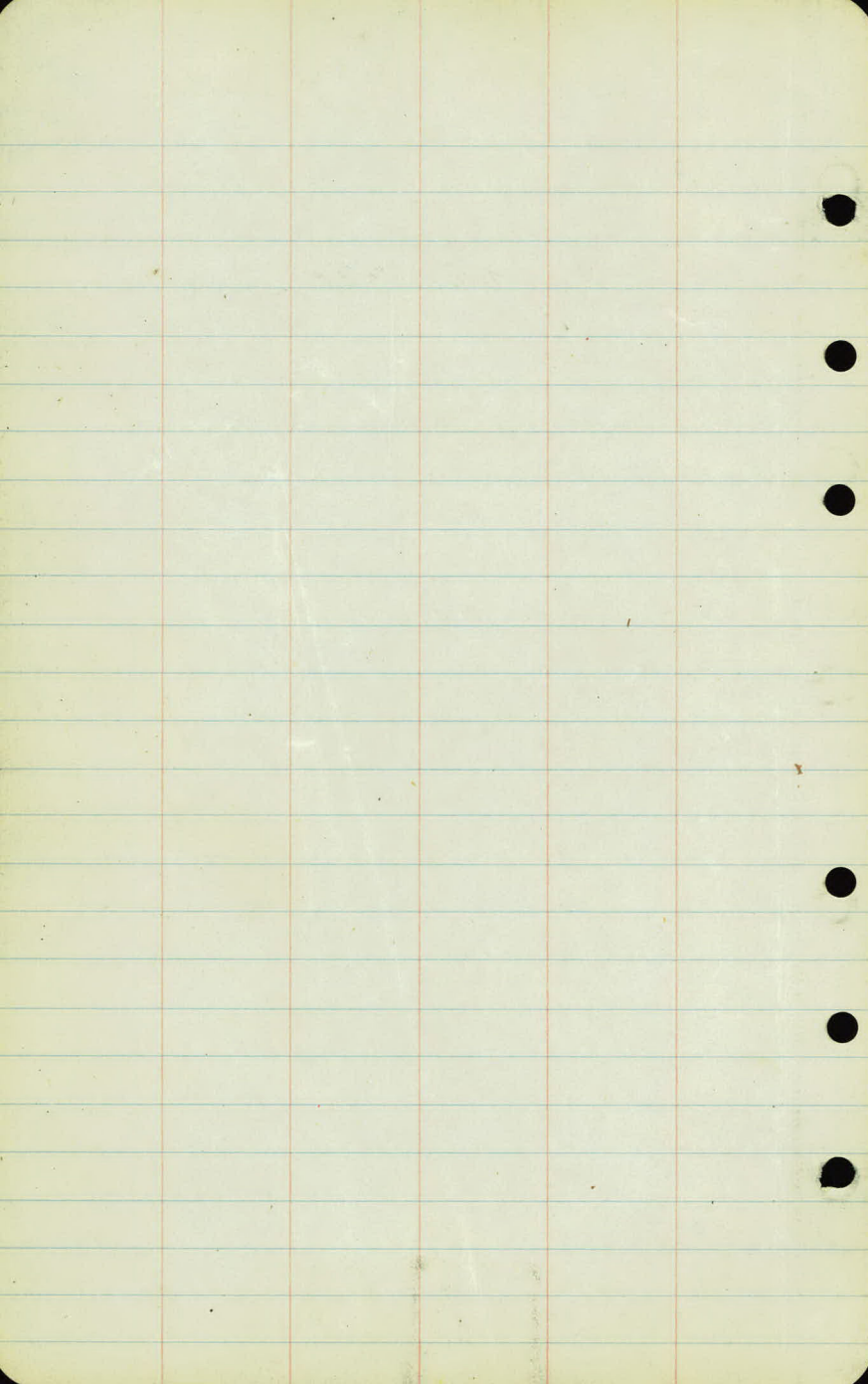
R/34

P.C.

88.5

42.3





FK
HL
PA

Sept. 9, 1966

1

Victoria St. House Locations

Rec. 9-12-66

plotted 9-13-66

Tot P.T. Sta 298+14.10
to P.T. Sta 302+68.60 0°00'

N.W. Cor Ho 153°25' 77

Cor Ho + Ga. 147°30 91

NW Cor, Ga 138°25' 84

NE " " 134°- 103

S.W. Cor. Ho 172°40' 111

SE, Cor Garage 325°10' 167

NE " " 331° 158

NW Cor Ga. 334°50' 182

NW. Cor House 339°30' 215

Tot Ct. Sec 23

150

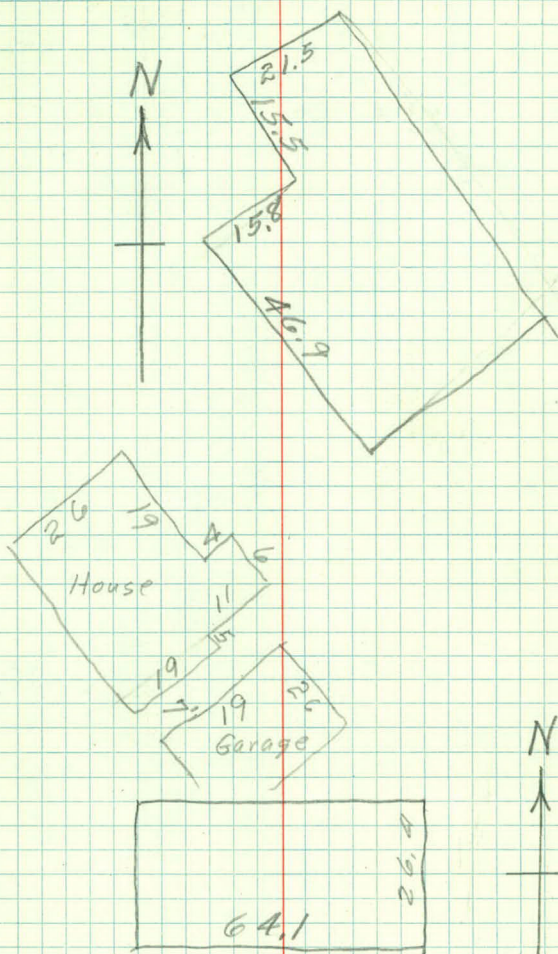
N.E. Cor. Ho 301°15' 150'

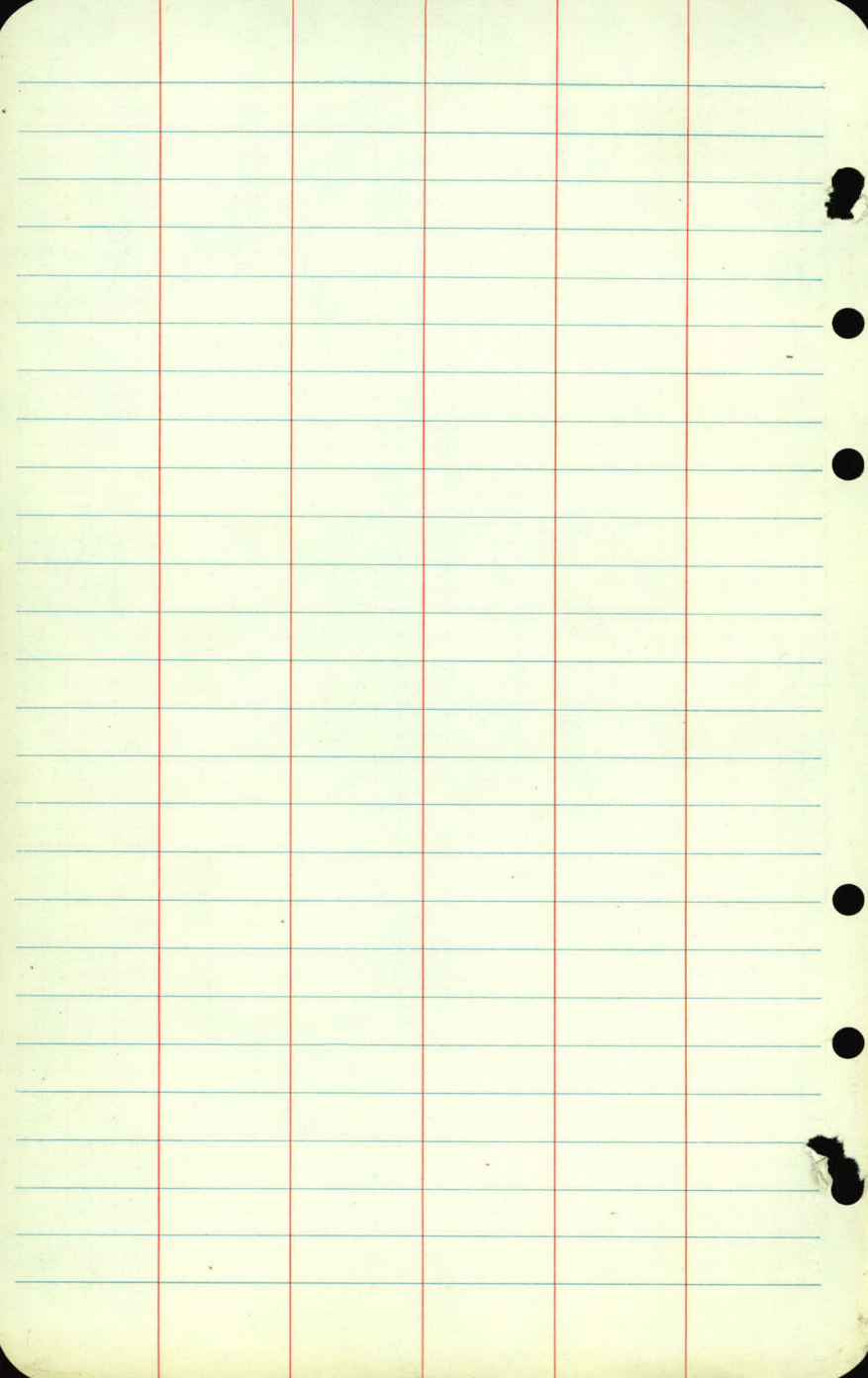
S.E. Cor Ho 291°38' 140

S.W. " " 285°53' 202

Sept. 9, 1966

2





1
Victoria & Arbogast

Ditch stakes

5
pages

Sta	PG	DG	DGR	Elev
	6.02	948.39		942.57

194+16	450	38.95	9.64
--------	-----	-------	------

6136.3

+50		38.85	9.74
-----	--	-------	------

195		38.75	9.84
-----	--	-------	------

+50		38.65	9.94
-----	--	-------	------

196		38.55	10.04
-----	--	-------	-------

+50		38.45	10.14
-----	--	-------	-------

197		38.35	10.24
-----	--	-------	-------

+45		38.25	10.34
-----	--	-------	-------

11 June 1953

80° Clear Hot

2

FA
AM
PM

F

RT

Spk in 15" Oak SE Cor Victoria & Arbogast

3.55

$$\left(\begin{array}{c} 7.5 \\ 2.1 \\ 40.5 \end{array} \right)$$

3.6

$$\left(\begin{array}{c} 6.6 \\ 3.1 \\ 42.3 \end{array} \right)$$

3.8

$$\left(\begin{array}{c} 7.5 \\ 2.3 \\ 40.6 \end{array} \right)$$

4.0

$$\left(\begin{array}{c} 7.7 \\ 2.2 \\ 39.9 \end{array} \right)$$

4.2

$$\left(\begin{array}{c} 7.0 \\ 3.0 \\ 42.0 \end{array} \right)$$

43 R/W

33 R/W

944.4

4.5

$$\left(\begin{array}{c} 6.1 \\ 4.0 \\ 33 \end{array} \right)$$

4.7

$$\left(\begin{array}{c} 5.7 \\ 4.5 \\ 33 \end{array} \right)$$

4.9

$$\left(\begin{array}{c} 5.8 \\ 4.5 \\ 33 \end{array} \right)$$

Sta + DG DGR
948.59

197 + 70 38.15 10.44

198 38.15 10.47

+ 43 38.05 10.54

+ 70 37.95 10.64

Arbogast St

0 + 50 37.80 10.8

1 37.30 11.3

BM 6.020 942.37

TD 3.87 942.91 9.55 939.04

+ 50 36.80 6.1

6.5

1.6

18.5
75
23.5
15. 21.9

24
102
132
152

25
25
155

3

2

R.

50

(8.3
R21
33)

51

(5.6
R4.8
33)

54

(6.6
R3.9
33)

56

(7.8
R2.9
33)

74

(7.8
R3.0
33)

939.8

31

31

88

(5.9
R5.4
33)

998

4.8

(6.1
R00
21.9)

Re-Staking

Sta	PG	PGK	DG	DGR	Elev
BM	5.93	948.50			942.57
196+50		38.45	10.05	3.8 6.4	
197		38.35	10.15	3.3	
+45		38.25	10.25	6.4	
+70		38.15	10.35		
198		38.15	10.35	4.9 5.4	15.6 4.7 10.9
+43		38.05	10.45		5.1 2.6 12.8 1.8 3.4
+70		17.95	10.55		9
	2.39	944.28	6.61		941.89
0+50		37.80	6.48		

18 June 1953

FK
LO
PM

4

18
141
321

5.0 15.
19.
33

4.4

(3.8
DC 6.2
45.4)

5.5 23

4.6

(5.3
DC 4.8
42.6)

32.7

4.8

(6.2
DC 4.0
40.7)

32.4

5.0

(6.0
DC 4.3
41.0)

32.1

5.1

(4.9
DC 5.4
42.9)

31.9

5.3

(6.05
DC 4.4
40.6)

31.5

5.5

(7.55
DC 3.0
36.5)

31.9
29.
8.7
18.7
26.7

6.2

3.1

(3.5
DC 3.0
36.7)

Sta	DG	DGR	Elev
-----	----	-----	------

	994.28		
--	--------	--	--

1100			
------	--	--	--

	37.30		
--	-------	--	--

		6.98	
--	--	------	--

		1.7	
--	--	-----	--

		2.45	
--	--	------	--

130			
-----	--	--	--

	36.80		
--	-------	--	--

		5	
		7.48	

			1.3
--	--	--	-----

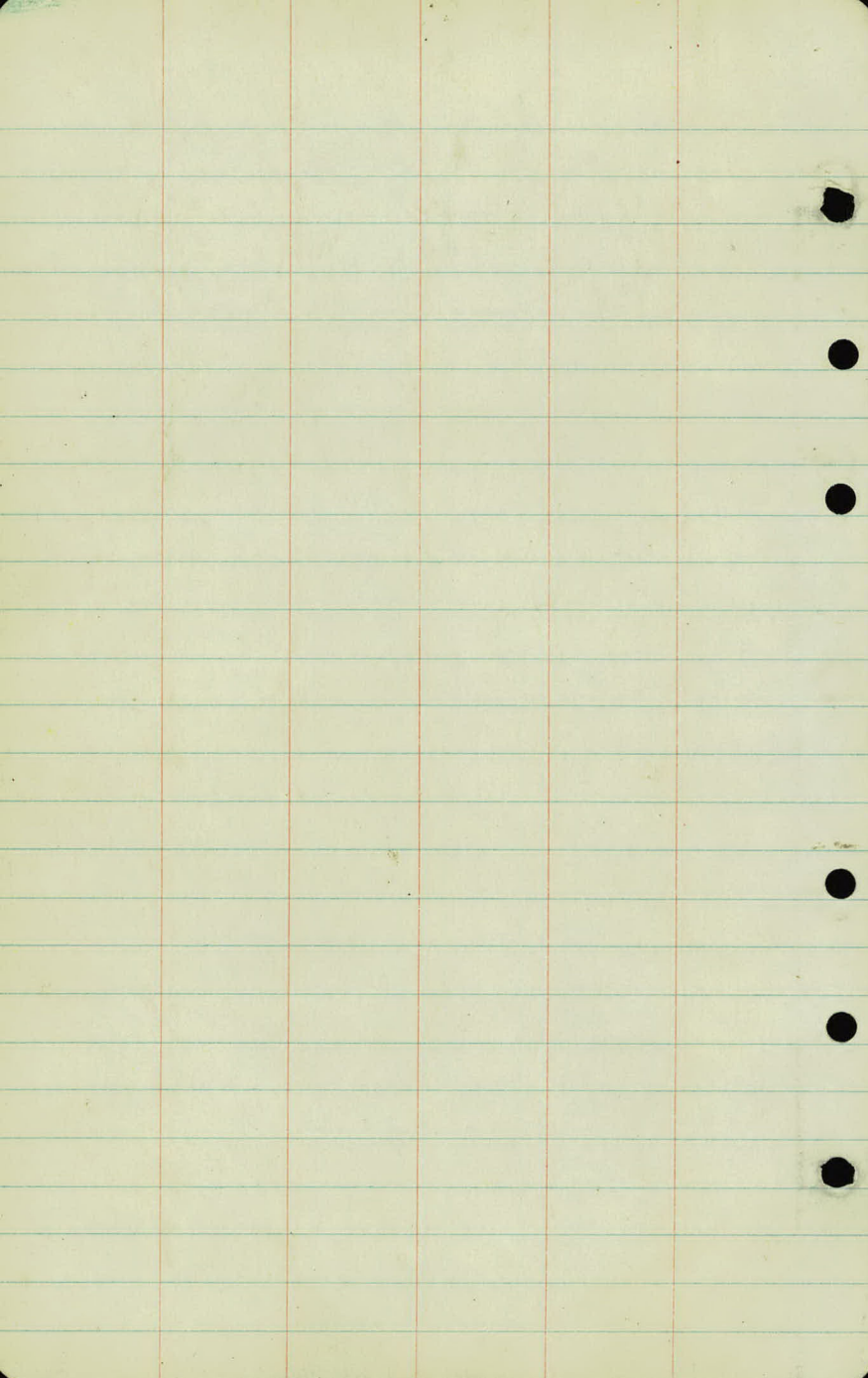
			0.6
--	--	--	-----

2.6
 6.3
 1.8
 2.4 3
 1.1 2
 22.8
 2.4
 18
 20.4

4.4

1.66
 10.5.3
 34.9

6.2



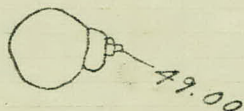
FK
NM
DM
WF

July 19, 1968

Victoria & F

Boat Spike

Tell Post



○ Disk
P.P.

108.77

○

46.05
49.06

○ 3N
PP

○ Iron by Fe Post