

Book 84 Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN
(Drainage) Survey

DITCH # 4

From CO. RD. "C" To LYDIA STR.

Road Acc't. No.

Date Filed. 1-30-43

File

Align

Ditch #4
Co Rd "C" To Lydia Str.

6/1/42

HAW

AM

L-C

CF

LL

Completed 6/14/42

Sta

Pt

$\Delta L +$

$\Delta R +$

7 + 69.20 P. 1.

19° 35'

N 24° 48' E

4 + 34.10 P. 1.

12° 03'

0 + 76.85 P. D. /

N 5° 13' E

0 + 00 = sta P. 1.

sta 83 + 50

Description

□

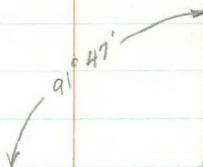
2"x2 Hub

□

2"x2 Hub

□

2"x2 Hub



2 Co Rd C

No. 1 Nail

Sta	Pt	Alt	Bkt
-----	----	-----	-----

17 + 09.10	P.I.	36° 57'	
------------	------	---------	--

14 + 60.30	P.I.		4° 32'
------------	------	--	--------

11 + 70.30	P.I.		57° 42'
------------	------	--	---------

10 + 24.60	P.I.		27° 13'
------------	------	--	---------

S 70° 17' E

N 52° 01' E

Description

□

2"x2 Hub

□

2"x2 Hub



□

1"x2 Hub

□

2"x2 Hub

St.	P.I.	ΔLT	ΔRt
-----	------	-------------	-------------

21 + 63.10	P.I.		29° 48'
------------	------	--	---------

20 + 90.70	P.I.		22° 00'
------------	------	--	---------

20 + 14.60	P.I.	31° 07'	
------------	------	---------	--

18 + 46.10	P.I.	28° 36'	
------------	------	---------	--

Description

□

2'x2 Hub

□

2'x2 Hub

□

2'x2 Hub

□

2'x2 Hub.

Sta

P.I.

ΔL

ΔR

25 + 84.00 P.I.

$9^{\circ}12'$

25 + 34.40 P.I.

$26^{\circ}27'$

23 + 24.70 P.I.

$44^{\circ}38'$

22 + 27.16 P.I.

$16^{\circ}20'$

Description

□

2' x 2 Hub

□

2' x 2 Hub

□

2' x 2 Hub

□

2' x 2 Hub

sta

Pt

ΔLt

ΔRt

33 + 38.7

P.I.

$8^{\circ} 07'$

32 + 31.80

P.I.

$52^{\circ} 34'$

31 + 43.0

P.I.

$27^{\circ} 59'$

27 + 33.0

P.I.

$18^{\circ} 30'$

Descriptor

□

2"x2 Hub

□

2"x2 Hub

□

2"x2 Hub

□

2"x2 Hub

Sta	Pt.	Δ Lt.	Δ Rt.
-----	-----	-------	-------

41+77.8	P. 1.	31° 10'	
---------	-------	---------	--

41+01.5	P. 1.	27° 11'	
---------	-------	---------	--

35+42.8	P. 1.	18° 45'	
---------	-------	---------	--

34+45.0	P. 1.	15° 34'	
---------	-------	---------	--

Description

□

2'x2 Hub

□

2'x2 Hub

□

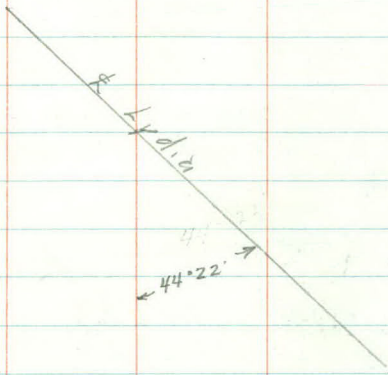
2'x2 Hub

□

2'x2 Hub

Sta	Pt.	Δ Lt.	Δ Rt.
51+11 ²⁰	P.O.T	£ Lydia	
50+36	P.O.T.	18" CM	
49+34 ⁵⁰	P.I.	16° 50'	
46+35 ⁹⁰	P.I		22° 58'
43+59 ⁶⁰	P.I	10° 00'	

Description



Na.

44°22'

Hub

2x2 Hub

549

P.T.

Δ LI

Δ RT

53+32

P.I

End 24" Conc

52+92⁰⁰

P.O.T

$\&$ Trail To

52+49⁷⁰

P.O.T

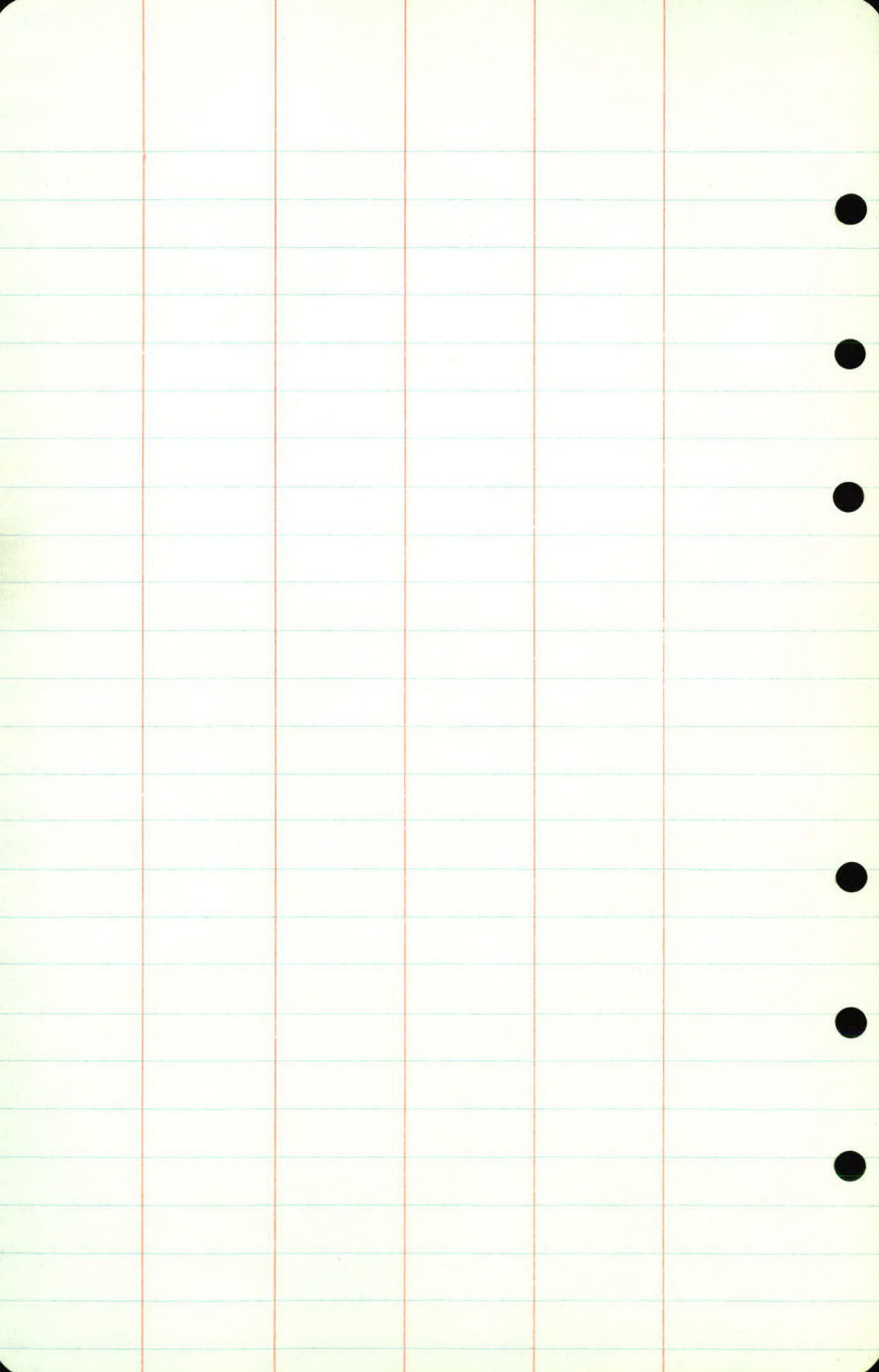
24" Conc.

52+04

P.I

$8^{\circ}18'$
N.W. End 18" CM

Description



Bench Levels

Sta	+	Δ	-	Elev
B.M.	0.40	925.15.		924.75
	5.34	918.53.	11.96	913.19.
	7.66	917.26.	8.93	909.60. 909.61.
	6.86	917.90.	6.22	911.04. 911.06
	3.51	917.90	3.51	914.39.
	3.79	913.30.	8.39	909.51. 909.53
	1.44	905.77.	8.97	904.33. 904.35.
	4.88	904.15.	6.50	899.27. 899.28
	5.28	902.95.	6.48	897.67.
	3.52	901.56.	4.91	898.04. 898.03
	7.05	901.02.	7.59	893.97.
	11.47	904.94.	7.55	893.47.
T.P.	6.17	911.07.	0.04	904.90.
	1.24	899.86.	12.45	898.62.
	2.58	892.28.	10.16	889.70.
	3.56	887.56.	8.28	884.00.
			5.60	881.96.

Spk in P.P.

N.W. Cor C" + New Brighton

Top Hub

Top Lath Sta 12+50

Top Hub " 14+60

Top " " 18+46 ¹⁰" " " 22+27 ¹⁰

Top " " 25+84

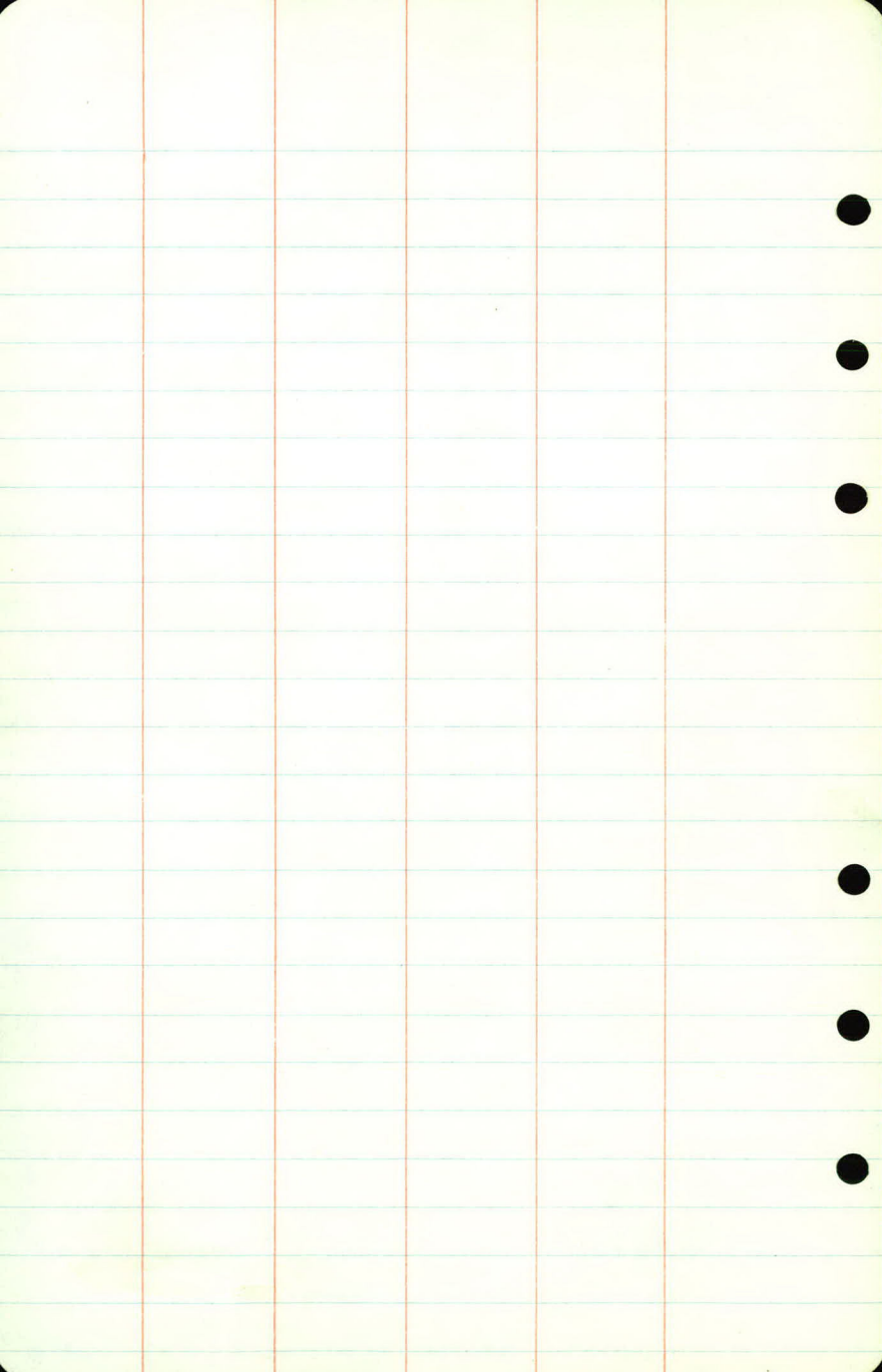
Spk in 18" Oak 100' Rt Sta 34+60

Top Hub Sta 41+77 ²⁰

Spk in 18" Pop 2' Rt Sta 48+

Spk in T.P. 175' Rt 18" Culv 50+00 31.

Spk in 10" B.E. Outlet of Ditch



TOPOGRAPHY

6

5

434.10 121

4

3

2

1

0

Fe 9 Ditch 16'

Fe 8 Ditch 15'

Fe 6' Ditch 15'

Fe 6' Ditch 16'

Fe 6 Ditch 19'

Hay Meadow

Baseline

Fe 7' Ditch 18'

Fe 7' ± 4' Ditch 18

Fe 8' Ditch 18'

13

12

+ 70 30 P.1

11

24 30 P.1

10

9

8

+ 69 20 P.1

7

6

Fc 17 Ditch 19'

12

Fc 15' Ditch 20'

+89 Fc Cor 6" Back Tangent

+70 Fc 3'

+89 Ditch 23'

Fc 1 Ditch 18'

Fc 9 Ditch 15'

Fc 6 Ditch 14'

Baseline

Fc 5 Ditch 13'

Fc 7 Ditch 13'

Fc 11 Ditch 15'

+22 Right Fc
+20 Fc Cor 10'

Fc 9 Ditch 15'

20

19

+46¹⁰

18

+09²⁰

17

+38 Rgetie Ditch

+28 OFFtake Ditch 24'

16

+53 4" W. 1125'

15 End Brush 14'-20'

+60³⁰ Brush 9'-18'

+45 Bay Poplar Brush 14'-20'

14

13

+95 Beg Ent Culv 17'

Fc 3' Pitch 14'

+46¹⁰ Fc 2' Ditch 20'

Fc 8' Ditch 16'

Fc 19' Ditch 20'

Fc 17' Ditch 20'

Baseline

Fc 13' Pitch 19'

+44 10" W.I. 17'

+36 Group 7-4" Pop 33' on 1st n

+26 2" Pop 15'

+65 Group 4-4" B.E 24'

Fc 12' Ditch 21'

Fc 9' Ditch 20'

+29 4" E/m 21'

+24 2" B.E 17'

+10 4" B.E 19'

Fc 8' Ditch 20'

+95 Group 5-5" B.E 10

+81 4" B.E 17'

27

26

25

24

23

22

+76 4" Oak 25'
+76 4" Oak 15'
+73 Twin 4" Oak 24'

21

+90 70

20

15" x 16' CM + 4' PLank End
20' End

14
Fe 12 Ditch 17'

Fe 13' Ditch 20'
+84²⁰ P.I. Fe 13 Ditch 20'

+70 Twin 3" Oak 17'

+58 4" Oak 28'

+34⁴⁰ P.I. Fe 13 Fe 20'

Fe 15' Ditch 20'

Fe 4' Ditch 9'

+25 4" Oak 29'

+24²⁰ Fe 16' Ditch 20'

+11 4" Oak 29'

+05 Group 2-4" Oak 24'

Fe 13' Ditch 16'

+89 6" Oak 22'

+42 4" Oak 28'

+30 Twin 4" Oak 30'

+27²⁰ P.I. Fe 12 Ditch 20'

Fe 3' Ditch 18'

+63 6" Oak 18'

+63²⁰ P.I. Ditch 20'

+59 3-4" Oak 6'

Fe 00 Ditch 20'

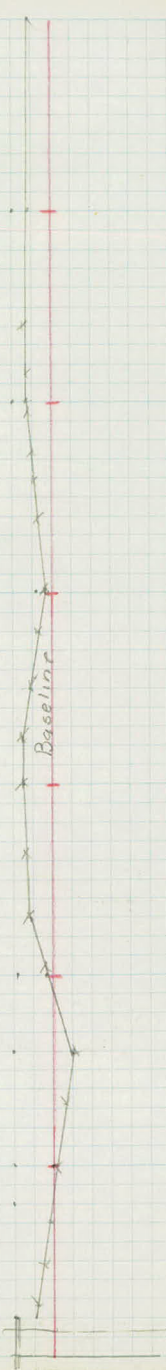
+97 Twin 2" Oak 8'

Fe 1' Ditch 20'

+146²⁰ End 15" CM 21'

+146²⁰ Fe 11 Ditch 20'

Fe 10' D



34

+78 Beg Oak Branch 12'-20'

33

32

+48 Fe 14 Ditch 20'

+43 30" Well 14'

31

30

29

28

27

+65 15" W. 11 30'
+38 Fe 14 Ditch 21'
+26 15" W. 11 26'
+15 15" W. 11 7'
+12 30" Pop 25'
+00 Fe 14 Ditch 18'

+36 Fe Cor 14 Ditch 20'
+20 Fe Cor 9 Angle Ditch 20'
Fe 10 Ditch 15'

+43 Bag Ditch, 20'
+43 Lake, 20'
+43 Fe 14'

+26 Fe X R
+00 Edge Lake

+33 End Ditch 20'
+33 Fe Cor 14
+00 Bag Lake 100'

+35 Fe X R

+00 Bag Lake 200'

41

40

39

38

37

36

+46' Fe X 2

35

+45 Brush 5'-50'

34 Brush 12-20

+82 Angle Fe. 18'

+50 End Swp 20'

Ditch 12 Fe 17 Swp 20-50'

+50 Swp 23' - 125'

Swp 200'
Ditch 12 Fe 16'

Swp 10'

+50 Swp 250'

+50 swp 50

Ditch 12 Fe 15'
Swp 220'

Swp 35'

+50 Swp 150'

+50 Swp 15'

Swp 110' Fe 14'
Ditch 12'

Swp 15'

+71 Swp 20'

Fe 14' Ditch 12'

Swp 50'

+4280 Fe Cor 12 Ditch 20'

+22 Fe 7' - 40'

+22 Oak 28'

+18 Oak 2'

+18 Oak 2'

+85 End. Brush 15-50

+98 15" Oak 10'

+45 Ditch 20'

+45 Fe 1

+29 36" Pop 31'

Fe 1 Ditch 24'

48

47

46

45

44

43

42

41

17
Ditch 1' Fe 19'

Ditch 6
Δ Fe 13'

+35 Ditch 7
Fe 33'

Ditch 5' Fe 30'

Ditch 7' Fe 21'

Ditch 7' Fe 14'

+60 Ditch 6'
Fe 10'

Fe 4 Ditch 7

+50 Ditch 5'

+50 Fe 6'

+18 End 24" CM 6'

+10 Field Ent 24" X 19' 9'

+00 End 24" CM 13

+78 Fe 27' Ditch 20'

Fe 21' Ditch 19'

Hay Field

+32 End 24" Con.

53

+92 & 10' Trail

+49²⁰ Beg 24

52

+04 N.W End 18" CM

+26 Edge Black Top

51

+11²⁰ & Lydia

+97 Edge Black Top

+67 Fox &

+36 S.E. End 18" CM

50

49

48

704 6" W. 1/1 4' 2 1/2

+ 6 8 6" Pop 15'

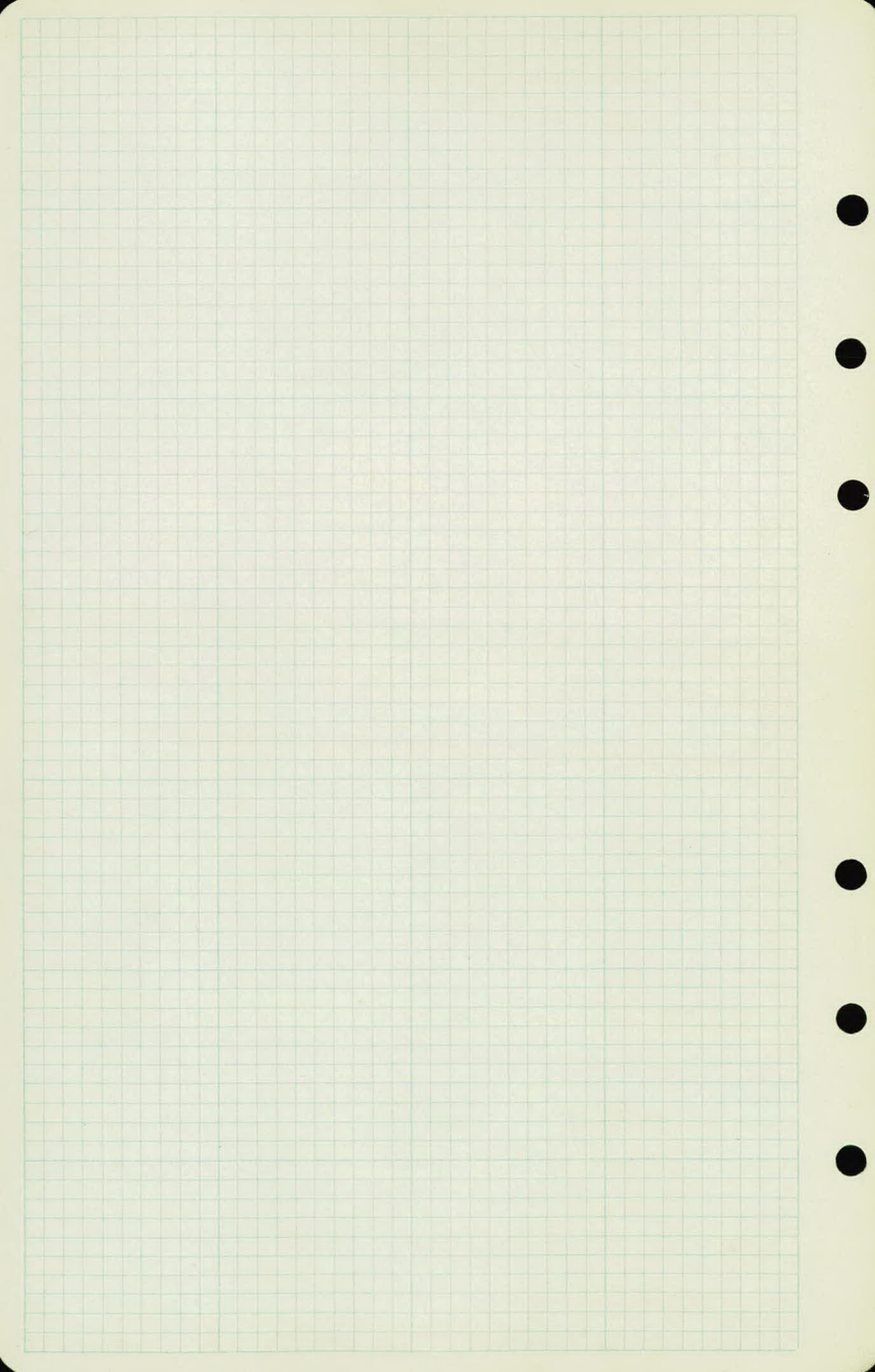
 $+3L \text{ Fe } 27'$

Ditch 3'
Fe Cor 60'

+34 Ditch 8' Fe 28'

Ditch 8' Fe 26'

740 24" Pop 1'



X Sections

Ditch #4

4/5/42

HAW

L^CM

L^L

CF

Sta	+	Σ	-	Elev	$\pm$ Ditch
B.M	1.72	926.47		924.75	
0+00 =				19.4	19.4
83+50					
+14				18.5	18.5
T.P.	5.63	918.86	1324	913.23	913.19
+28		Too slope		10.2	10.2
+50		18.9 10.5 7.4		10.1	08.9
+75				08.4	08.4
+100				08.1	08.1
2+50				07.5	07.5
250				08.2	07.3
+50				08.8	07.6
3				09.6	07.7
+50				09.4	07.7
4				07.3	07.0

Lt Rt
 Ditch

Spk. in P.P. N.W. Cor New Brighton Rd + Co Rd C"

7.1

8.0

$\frac{7.4}{25}$ $\frac{7.9}{16}$ 8.7 $\frac{8.4}{10}$ $\frac{8.4}{25}$

$\frac{8.2}{25}$ $\frac{8.2}{4}$ 8.8 $\frac{10.0}{13}$ $\frac{9.8}{25}$

$\frac{10.1}{25}$ $\frac{10.2}{10}$ 10.5 $\frac{9.4}{10}$ $\frac{10.0}{25}$

$\frac{10.1}{25}$ $\frac{10.0}{15}$ $\frac{9.7}{8}$ 10.8 $\frac{10.8}{5}$ $\frac{9.7}{8}$ $\frac{9.7}{25}$

$\frac{10.1}{25}$ $\frac{10.2}{15}$ $\frac{10.4}{8}$ $\frac{9.9}{2}$ 11.4 $\frac{10.7}{5}$ $\frac{9.7}{7}$ $\frac{9.7}{25}$

$\frac{10.3}{25}$ $\frac{10.5}{22}$ $\frac{10.3}{9}$ $\frac{10.1}{4}$ $\frac{10.6}{3}$ 10.7 $\frac{11.4}{2}$ $\frac{11.6}{5}$ $\frac{10.1}{7}$ $\frac{10.2}{25}$

$\frac{10.7}{25}$ $\frac{10.5}{18}$ $\frac{10.6}{7}$ 10.1 $\frac{11.3}{3}$ $\frac{11.0}{6}$ $\frac{10.3}{8}$ $\frac{10.0}{25}$

$\frac{9.7}{25}$ $\frac{9.6}{15}$ $\frac{9.3}{8}$ 9.3 $\frac{11.2}{4}$ $\frac{10.7}{7}$ $\frac{9.9}{8}$ $\frac{8.7}{11}$ $\frac{9.0}{25}$

$\frac{8.2}{25}$ $\frac{8.2}{15}$ $\frac{8.0}{1}$ 9.5 $\frac{11.2}{10}$ $\frac{11.2}{3}$ $\frac{10.8}{7}$ $\frac{8.0}{10}$ $\frac{7.6}{25}$ $\frac{7.8}{35}$

$\frac{8.3}{37}$ $\frac{8.7}{25}$ $\frac{8.5}{15}$ $\frac{8.3}{5}$ 11.6 $\frac{11.9}{1}$ $\frac{11.0}{3}$ $\frac{8.9}{5}$ $\frac{8.8}{25}$ $\frac{9.1}{35}$

Sta	+	π	-	Elev	$\pm$ Ditch
		918.82.			
4+3410	P.1			07.3.	07.3.
+70				07.5.	07.5.
5				07.6.	07.6.
+50				07.4.	07.4.
T.P.	5.69	915.30. 915.10	9.25	909.61 909.41	909.60
6				07.0.	07.0.
+50				06.7.	06.7.
7				06.8.	06.8.
+40				06.6.	06.6.
+69 ²⁰	P.1			06.4.	06.4.
8				06.7.	06.7.
+50				06.8.	06.2.
9				06.7.	06.2.

Lt

R
Ditch

Rt

$$\frac{8.5}{40} \quad \frac{8.2}{25} \quad \frac{8.7}{15} \quad \frac{9.5}{5} \quad \frac{11.3}{2} \quad 11.6 \quad \frac{11.5}{1} \quad \frac{10.8}{3} \quad \frac{10.1}{5} \quad \frac{9.5}{8} \quad \frac{9.8}{25} \quad \frac{9.8}{35}$$

$$\frac{9.8}{25} \quad \frac{10.0}{15} \quad \frac{9.8}{3} \quad \frac{11.2}{1} \quad 11.4 \quad \frac{10.9}{3} \quad \frac{10.3}{4} \quad \frac{10.3}{9} \quad \frac{10.5}{25}$$

$$\frac{10.2}{25} \quad \frac{10.2}{15} \quad \frac{10.2}{3} \quad \frac{11.0}{1} \quad 11.3 \quad \frac{11.1}{3} \quad \frac{10.7}{4} \quad \frac{11.0}{25}$$

$$\frac{10.2}{25} \quad \frac{10.2}{15} \quad \frac{10.6}{2} \quad \frac{11.2}{1} \quad 11.5 \quad \frac{11.5}{3} \quad \frac{11.1}{8} \quad \frac{10.9}{17} \quad \frac{11.1}{40}$$

$$\frac{6.7}{25} \quad \frac{7.1}{15} \quad \frac{7.4}{4} \quad 8.3 \quad \frac{7.8}{3} \quad \frac{7.4}{9} \quad \frac{7.6}{25}$$

$$\frac{7.4}{25} \quad \frac{7.7}{15} \quad \frac{7.3}{2} \quad \frac{7.8}{2} \quad 8.6 \quad \frac{8.1}{3} \quad \frac{7.7}{7} \quad \frac{7.5}{25}$$

$$\frac{7.5}{25} \quad \frac{7.5}{15} \quad \frac{7.6}{7} \quad \frac{7.7}{3} \quad \frac{8.5}{1} \quad 8.5 \quad \frac{8.1}{3} \quad \frac{7.9}{8} \quad \frac{7.8}{25}$$

$$\frac{7.8}{25} \quad \frac{7.7}{15} \quad \frac{7.6}{7} \quad \frac{7.8}{2} \quad \frac{8.7}{1} \quad 8.7 \quad \frac{8.7}{2} \quad \frac{8.3}{3} \quad \frac{7.7}{10} \quad \frac{7.8}{25}$$

$$\frac{7.9}{25} \quad \frac{8.0}{15} \quad \frac{8.1}{8} \quad \frac{7.6}{4} \quad \frac{8.9}{2} \quad 8.9 \quad \frac{8.9}{2} \quad \frac{8.2}{3} \quad \frac{7.8}{14} \quad \frac{7.9}{25}$$

$$\frac{7.8}{25} \quad \frac{8.0}{15} \quad \frac{7.8}{4} \quad \frac{8.6}{3} \quad 8.6 \quad \frac{8.0}{1} \quad \frac{7.8}{10} \quad \frac{7.9}{25}$$

$$\frac{8.0}{25} \quad \frac{8.3}{15} \quad \frac{8.0}{5} \quad \frac{9.1}{2} \quad \frac{9.1}{1} \quad 9.5 \quad \frac{7.8}{4} \quad \frac{8.1}{15} \quad \frac{8.4}{25}$$

$$\frac{8.2}{25} \quad \frac{8.1}{15} \quad \frac{8.1}{5} \quad \frac{9.1}{3} \quad \frac{9.1}{1} \quad 8.6 \quad \frac{8.2}{2} \quad \frac{7.9}{11} \quad \frac{8.1}{26}$$

Sta	+	Δ 915.30 915.10	-	Elev	Δ Ditch
9+50				06.3.	05.7.
10+00				05.7.	05.3.
+24 ⁶⁰	P. 1			05.2.	05.2.
+50				05.3.	05.3.
11				05.3.	05.3.
+50				04.7.	04.7.
+91	Δ in Ditch			05.0.	05.0.
12				05.0.	05.0.
+50				05.9.	04.9.
13				05.6.	05.6.
+50				06.0.	06.0.
T.P.	5.56	916.62 916.42	4.24	911.06 910.96	(911.04)
14				05.7.	05.7.

Lt.

£

Rt

24

Ditch

$$\frac{8.3}{25} \quad \frac{8.2}{15} \quad \frac{8.3}{5} \quad \frac{9.6}{3-1} \quad 9.0 \quad \frac{8.4}{1} \quad \frac{7.5}{10} \quad \frac{8.3}{25}$$

$$\frac{8.5}{25} \quad \frac{8.5}{15} \quad \frac{8.3}{5} \quad \frac{10.0}{3-1} \quad 9.6 \quad \frac{9.4}{2} \quad \frac{8.3}{3} \quad \frac{7.9}{15} \quad \frac{7.8}{25}$$

$$\frac{8.4}{25} \quad \frac{8.5}{15} \quad \frac{8.5}{7} \quad \frac{8.4}{3} \quad \frac{10.1}{2} \quad 10.1 \quad \frac{9.9}{2} \quad \frac{8.4}{4} \quad \frac{8.2}{15} \quad \frac{8.2}{25}$$

$$\frac{8.6}{25} \quad \frac{8.4}{15} \quad \frac{8.4}{4} \quad \frac{10.0}{3} \quad 10.0 \quad \frac{10.0}{1} \quad \frac{8.5}{2} \quad \frac{8.1}{15} \quad \frac{8.2}{25}$$

$$\frac{8.6}{25} \quad \frac{8.4}{15} \quad \frac{8.5}{8} \quad \frac{8.7}{4} \quad \frac{10.0}{2} \quad 10.0 \quad \frac{8.6}{1} \quad \frac{8.5}{15} \quad \frac{8.4}{25}$$

$$\frac{8.8}{25} \quad \frac{8.7}{15} \quad \frac{8.7}{4} \quad \frac{10.6}{2} \quad 10.6 \quad \frac{10.6}{1} \quad \frac{9.1}{2} \quad \frac{8.7}{9} \quad \frac{9.0}{25}$$

$$\frac{9.0}{25} \quad \frac{8.9}{15} \quad \frac{8.9}{2} \quad 10.3 \quad \frac{10.3}{11} \quad \frac{10.3}{25}$$

$$\frac{9.2}{25} \quad \frac{9.2}{18} \quad \frac{9.0}{5} \quad \frac{10.3}{2} \quad 10.3 \quad \frac{9.4}{12} \quad \frac{8.8}{25}$$

$$\frac{9.0}{25} \quad \frac{8.9}{16} \quad \frac{8.9}{4} \quad 9.4 \quad \frac{10.4}{1} \quad \frac{10.2}{3} \quad \frac{9.2}{5} \quad \frac{8.8}{12} \quad \frac{8.4}{25}$$

$$\frac{8.6}{25} \quad \frac{8.4}{14} \quad \frac{8.4}{4} \quad \frac{9.7}{2} \quad 9.7 \quad \frac{9.7}{2} \quad \frac{8.9}{3} \quad \frac{7.8}{10} \quad \frac{7.9}{25}$$

$$\frac{8.0}{25} \quad \frac{7.6}{13} \quad \frac{7.6}{4} \quad \frac{9.1}{2} \quad 9.3 \quad \frac{9.2}{3} \quad \frac{7.9}{4} \quad \frac{7.4}{12} \quad \frac{6.7}{25}$$

$$\frac{7.2}{35} \quad \frac{9.0}{26} \quad \frac{6.6}{17} \quad \frac{6.7}{7} \quad \frac{10.9}{1} \quad 10.9 \quad \frac{10.9}{2} \quad \frac{6.9}{8} \quad \frac{6.4}{14} \quad \frac{5.9}{27} \quad \frac{5.9}{44}$$

Sta	+	π	-	Elev	$\pm$ Ditch
		916.62			
		916.42			
14+60 ³⁰	P.1			05.8.	05.8.
T.P.	2.78	917.19	2.21	914.41	914.39
15		914.99		912.21	
				05.5.	05.5.
+50				05.9.	05.9.
16				05.7.	05.7.
+50				05.8.	05.3.
17				05.7.	05.7.
+09 ⁰⁰	P.1			05.9.	05.9.
+50				08.3.	05.7.
18				07.0.	04.9.
+46 ¹⁰	P.1			04.6.	04.6.
T.P.	4.84	914.37	7.66	909.53	909.51
19		913.68		908.76	
				07.8.	04.4.
+56				07.8.	04.3.

L1.

2
Ditch

R1

$$\frac{3.1}{43} \quad \frac{2.4}{24} \quad \frac{9.0}{10} \quad \frac{10.8}{1} \quad 10.8 \quad \frac{10.8}{1} \quad \frac{7.8}{3} \quad \frac{3.5}{10} \quad \frac{2.2}{25} \quad \frac{1.8}{50}$$

$$\frac{2.9}{46} \quad \frac{3.4}{29} \quad \frac{5.2}{10} \quad \frac{11.7}{2} \quad 11.7 \quad \frac{11.7}{3} \quad \frac{7.9}{5} \quad \frac{5.1}{11} \quad \frac{4.1}{18} \quad \frac{4.3}{30} \quad \frac{3.6}{50}$$

$$\frac{7.5}{50} \quad \frac{7.5}{30} \quad \frac{7.6}{11} \quad \frac{11.3}{4} \quad 11.3 \quad \frac{7.5}{6} \quad \frac{7.3}{20} \quad \frac{6.5}{27} \quad \frac{6.3}{46}$$

$$\frac{7.8}{30} \quad \frac{8.3}{15} \quad \frac{7.4}{6} \quad 11.5 \quad \frac{11.5}{3} \quad \frac{8.0}{9} \quad \frac{8.0}{26} \quad \frac{7.4}{50}$$

Ditch

$$\frac{7.9}{30} \quad \frac{8.6}{11} \quad \frac{7.6}{6} \quad \frac{9.0}{1} \quad 11.4 \quad \frac{11.9}{1} \quad \frac{11.9}{3} \quad \frac{9.4}{5} \quad \frac{8.2}{8} \quad \frac{9.1}{12} \quad \frac{9.4}{23} \quad \frac{8.4}{42}$$

Ditch

$$\frac{7.6}{30} \quad \frac{8.1}{23} \quad \frac{8.2}{11} \quad \frac{7.8}{8} \quad \frac{9.0}{4} \quad \frac{11.5}{1} \quad 11.5 \quad \frac{11.5}{1} \quad \frac{9.3}{2} \quad \frac{8.4}{5} \quad \frac{9.5}{7} \quad \frac{9.0}{27} \quad \frac{8.7}{45}$$

Ditch

$$\frac{7.7}{30} \quad \frac{8.3}{23} \quad \frac{8.2}{12} \quad \frac{7.6}{9} \quad \frac{11.3}{2} \quad 11.3 \quad \frac{11.3}{1} \quad \frac{9.4}{2} \quad \frac{9.2}{13} \quad \frac{8.4}{32}$$

Ditch

$$\frac{7.2}{30} \quad \frac{8.3}{14} \quad \frac{8.3}{3} \quad 8.9 \quad \frac{11.5}{5} \quad \frac{11.5}{7} \quad \frac{8.7}{10} \quad \frac{8.3}{28} \quad \frac{8.2}{50}$$

Ditch

$$\frac{7.5}{30} \quad \frac{8.0}{19} \quad \frac{9.2}{6} \quad \frac{18.9}{1} \quad 10.2 \quad \frac{11.2}{1} \quad \frac{12.3}{3.44} \quad \frac{10.5}{7} \quad \frac{8.6}{10} \quad \frac{8.6}{24} \quad \frac{8.2}{35}$$

Ditch

$$\frac{7.8}{30} \quad \frac{8.4}{17} \quad \frac{8.5}{6} \quad \frac{12.6}{1} \quad 12.6 \quad \frac{12.6}{2} \quad \frac{9.3}{4} \quad \frac{8.6}{6} \quad \frac{7.8}{28} \quad \frac{7.3}{35}$$

Ditch

$$\frac{4.8}{30} \quad \frac{6.0}{7} \quad 6.6 \quad \frac{10.0}{5} \quad \frac{10.0}{7} \quad \frac{6.4}{11} \quad \frac{5.7}{27} \quad \frac{5.0}{35}$$

Ditch

$$\frac{4.8}{30} \quad \frac{5.9}{9} \quad 6.6 \quad \frac{7.7}{4} \quad \frac{10.1}{6} \quad \frac{10.1}{8} \quad \frac{7.2}{11} \quad \frac{6.0}{26}$$

Sta	+	T	-	Elev	± Ditch
20		914.37 913.60		06.9. SEnd 15" CM	03.4.
+14 ⁶⁰	P.I.	NE N. End	15" CM	03.31.	03.3.
+50				03.1.	03.1.
+90 ²⁰				02.0.	02.0.
21				01.8.	01.8.
+50				00.7.	00.7.
+63 ¹⁰	P.I			901.0.	01.0.
22				899.8.	99.8.
T.P	5,23	909.58. 908.81	10.02	904.35. 903.58	904.33
27 ¹⁰	P.I			99.9.	99.9.
+50				898.6.	98.6.
23				902.1.	98.6.
24 ⁷⁰	P.I			897.9.	97.9.

L+

±

R+

Baseline

Ditch

$$\frac{6.7}{30} \quad \frac{7.1}{15} \quad 75 \quad \frac{10.4}{3-7} \quad \frac{11.00}{Inv} \quad \frac{7.5}{8} \quad \frac{5.6}{36}$$

$$\frac{7.4}{30} \quad \frac{7.5}{22} \quad \frac{7.2}{6} \quad \frac{11.4}{2} \quad \frac{11.06}{Inv} \quad \frac{11.4}{2} \quad \frac{7.4}{5} \quad \frac{6.1}{15} \quad \frac{5.4}{35}$$

Ditch

$$\frac{7.4}{30} \quad \frac{8.1}{20} \quad \frac{7.6}{11} \quad \frac{7.9}{7} \quad \frac{9.2}{2} \quad \frac{11.3}{1} \quad 11.3 \quad \frac{11.3}{1} \quad \frac{7.7}{5} \quad \frac{6.0}{11} \quad \frac{5.6}{34}$$

Ditch

$$\frac{7.8}{30} \quad \frac{8.8}{16} \quad \frac{8.6}{6} \quad \frac{9.3}{3} \quad \frac{12.4}{2} \quad 12.4 \quad \frac{12.4}{2} \quad \frac{9.0}{4} \quad \frac{8.3}{13} \quad \frac{5.8}{37}$$

Ditch

$$\frac{8.0}{30} \quad \frac{8.9}{18} \quad \frac{8.6}{7} \quad \frac{9.5}{4} \quad \frac{12.4}{3} \quad 12.6 \quad \frac{9.4}{4} \quad \frac{8.4}{13} \quad \frac{6.4}{20} \quad \frac{6.1}{32} \quad \frac{5.1}{50}$$

Ditch

$$\frac{8.2}{30} \quad \frac{9.0}{15} \quad \frac{9.6}{5} \quad \frac{13.7}{2} \quad 13.7 \quad \frac{13.7}{2} \quad \frac{10.1}{3} \quad \frac{9.7}{20} \quad \frac{6.8}{29}$$

Ditch

$$\frac{7.8}{30} \quad \frac{8.4}{20} \quad \frac{9.4}{5} \quad \frac{13.4}{4} \quad 13.4 \quad \frac{9.4}{5} \quad \frac{8.4}{10} \quad \frac{6.2}{30}$$

Ditch

$$\frac{8.0}{30} \quad \frac{9.2}{14} \quad \frac{10.0}{10} \quad \frac{11.0}{3} \quad \frac{14.6}{1} \quad 14.6 \quad \frac{14.6}{4} \quad \frac{10.3}{5} \quad \frac{10.0}{14} \quad \frac{8.8}{18} \quad \frac{7.8}{35}$$

Ditch

$$\frac{3.1}{30} \quad \frac{4.3}{16} \quad \frac{5.3}{12} \quad \frac{5.5}{5} \quad \frac{9.7}{3} \quad 9.7 \quad \frac{9.7}{2} \quad \frac{5.9}{4} \quad \frac{5.5}{9} \quad \frac{5.7}{30} \quad \frac{5.1}{40}$$

$$\frac{2.4}{30} \quad \frac{5.7}{10} \quad \frac{6.7}{2} \quad 11.0 \quad \frac{7.0}{4} \quad \frac{6.3}{7} \quad \frac{6.4}{20} \quad \frac{6.9}{40}$$

Ditch

$$\frac{5.1}{30} \quad \frac{5.4}{21} \quad \frac{5.9}{14} \quad 7.5 \quad \frac{11.0}{2} \quad \frac{11.0}{6} \quad \frac{7.3}{8} \quad \frac{4.5}{26} \quad \frac{7.5}{35}$$

Ditch

$$\frac{6.4}{30} \quad \frac{6.8}{16} \quad \frac{7.9}{5} \quad \frac{11.7}{2} \quad 11.7 \quad \frac{11.7}{1} \quad \frac{7.5}{4} \quad \frac{7.8}{35}$$

Sta	+	Σ	-	Elev	E Ditch
		909.58 908.81			

23+50				01.8.	97.3.
-------	--	--	--	-------	-------

24				00.7.	96.3.
----	--	--	--	-------	-------

+50				899.6.	97.9.
-----	--	--	--	--------	-------

25				98.5.	98.5.
----	--	--	--	-------	-------

+34 ⁴⁰				97.1.	97.1.
-------------------	--	--	--	-------	-------

+50				96.6.	96.6.
-----	--	--	--	-------	-------

T.P.	5.47	904.75. 903.98	10.30	899.28. 898.51	(899.27)
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+84 ⁰²				94.6.	94.6.
-------------------	--	--	--	-------	-------

26				96.3.	96.3.
----	--	--	--	-------	-------

+50				97.8.	94.3.
-----	--	--	--	-------	-------

T.P.	6.58	904.26. 903.49	7.07	897.68. 896.91	
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B.M			6.23	898.03. 897.26	(898.04)
-----	--	--	------	-------------------	----------

LH

Z

RT

Ditch

$\frac{66}{30}$ $\frac{71}{23}$ $\frac{75}{9}$ 7.8 $\frac{96}{8}$ $\frac{123}{7-12}$ $\frac{85}{13}$ $\frac{84}{22}$ $\frac{83}{35}$

Ditch

$\frac{83}{30}$ $\frac{89}{17}$ 8.9 $\frac{93}{8}$ $\frac{133}{10-13}$ $\frac{94}{13}$ $\frac{93}{35}$

Ditch

$\frac{102}{30}$ $\frac{10.3}{11}$ 10.0 $\frac{117}{1-3}$ $\frac{10.8}{7}$ $\frac{10.2}{12}$ $\frac{10.3}{35}$

Ditch

$\frac{103}{30}$ $\frac{10.3}{5}$ 11.1 $\frac{11.1}{2}$ $\frac{10.4}{3}$ $\frac{9.9}{6}$ $\frac{10.2}{11}$ $\frac{9.4}{16}$ $\frac{8.4}{35}$

Ditch

$\frac{107}{30}$ $\frac{110}{12}$ $\frac{104}{4}$ $\frac{125}{2}$ 125 $\frac{125}{1}$ $\frac{110}{2}$ $\frac{105}{7}$ $\frac{9.4}{18}$ $\frac{9.5}{35}$

Ditch

$\frac{110}{30}$ $\frac{110}{12}$ $\frac{10.6}{5}$ $\frac{13.0}{2}$ 13.0 $\frac{130}{1}$ $\frac{105}{2}$ $\frac{93}{5}$ $\frac{9.2}{20}$ $\frac{9.4}{35}$

Top Hub Stg 25 + 84 $\frac{00}{00}$ Ditch

$\frac{47}{30}$ $\frac{5.2}{15}$ $\frac{5.2}{5}$ $\frac{10.2}{2}$ 10.2 $\frac{10.2}{1}$ $\frac{5.8}{5}$ $\frac{5.9}{20}$ $\frac{5.7}{35}$

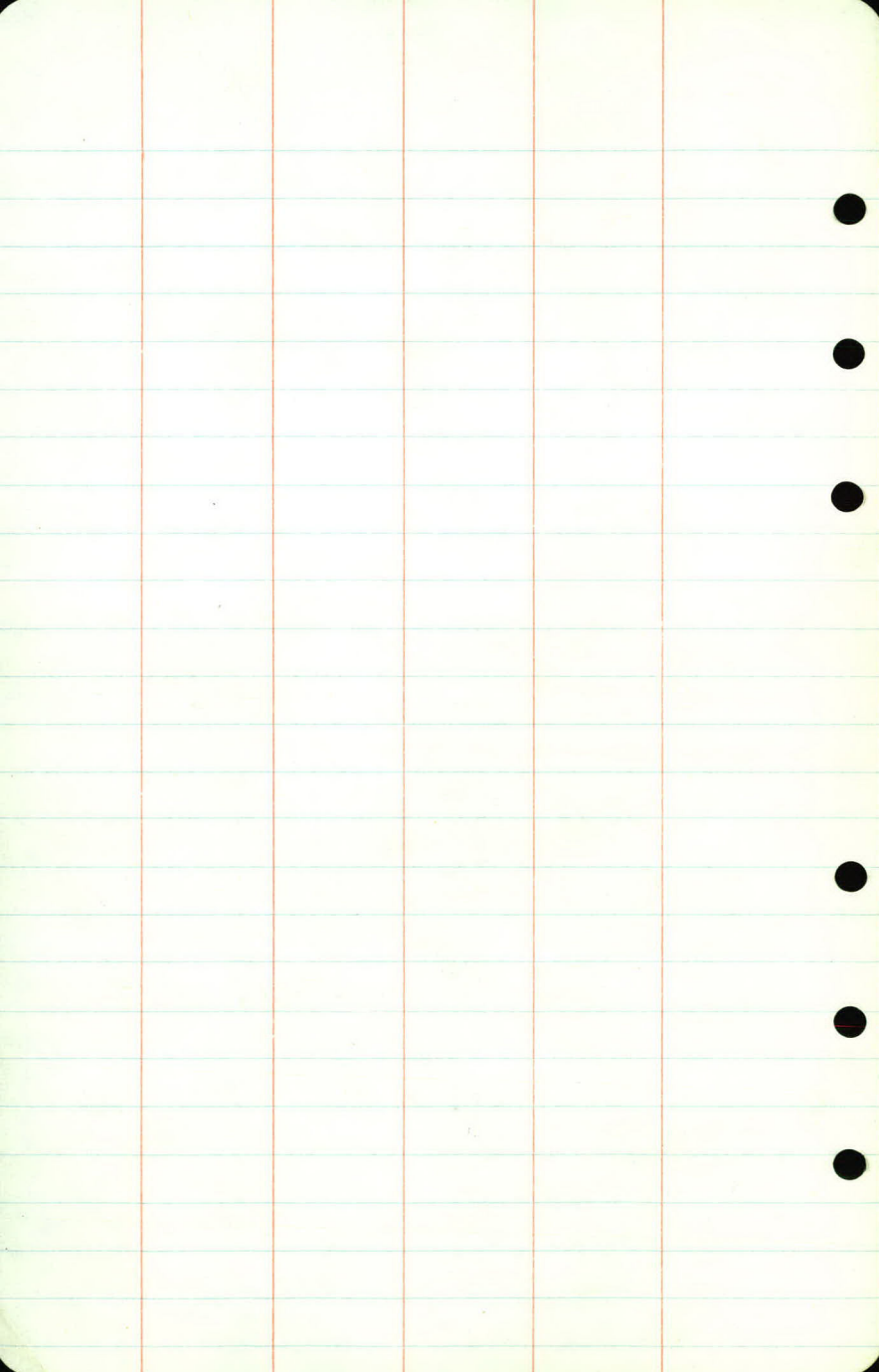
Ditch

$\frac{5.5}{30}$ $\frac{5.5}{14}$ $\frac{5.5}{5}$ $\frac{8.5}{2}$ 8.5 $\frac{8.5}{4}$ $\frac{6.2}{6}$ $\frac{6.5}{20}$ $\frac{6.4}{30}$

Ditch

$\frac{78}{30}$ $\frac{7.4}{8}$ $\frac{7.2}{5}$ 7.0 $\frac{10.5}{4-7}$ $\frac{7.0}{9}$ $\frac{7.5}{20}$ $\frac{7.6}{35}$

Spk in 18" Oak 80' RT Stg 94+60



X Sections

Sta	+	Σ	-	Elev	2 Ditch
B.M	2.10	901.37.		899.27	
27				964	95.8
+33.60		End Ditch		95.9	95.9
+50		Sand wash in Lake		96.5	
28				94.8	
		shots in Lake			
+50				(91.4)	
29				90.5	
+50				90.5	
30				90.2	
31				90.1	
B.M	3.06	901.10.		898.04	
31+43 ⁰⁰		Beg Ditch at outlet of Lake		93.9	93.7
32				96.1	93.4
+31.80	P.1			95.7	93.5

Lt. Rt

Top Hub Sta 25+84 Ditch

$$\frac{6.0}{25} \quad \frac{5.3}{7} \quad 5.0 \quad \frac{5.0}{1} \quad \frac{5.5}{3.5} \quad \frac{5.1}{6} \quad \frac{5.0}{14} \quad \frac{5.8}{35}$$

$$\frac{6.4}{25} \quad \frac{6.2}{12} \quad \frac{5.0}{2.3} \quad \frac{5.5}{5.5} \quad \frac{5.5}{2} \quad \frac{5.0}{3} \quad \frac{5.4}{11} \quad \frac{6.8}{23} \quad \frac{7.2}{30}$$

(94.6)

$$\frac{6.8}{25} \quad \frac{6.4}{11} \quad \frac{5.0}{10} \quad 4.9$$

$$\frac{4.9}{6} \quad \frac{6.4}{12} \quad \frac{6.8}{20} \quad \frac{7.3}{28}$$

(93.1)

$$\frac{7.8}{20} \quad \frac{7.4}{10} \quad \frac{6.5}{7} \quad 6.6 \quad \frac{7.0}{2} \quad \frac{7.7}{8} \quad \frac{8.3}{20} \quad \frac{8.3}{30}$$

10.0

10.9

10.9

11.2

11.3

Spk in 18" Oak 100 Rt Sta 34+60

$$\text{W.S. Lake } \frac{6.8}{25} \quad \frac{6.3}{13} \quad \frac{5.9}{11} \quad \frac{7.0}{7} \quad \frac{7.4}{2} \quad 7.2$$

$$\frac{6.2}{5} \quad \frac{5.9}{20}$$

6/8/01

$$\frac{3.9}{25}$$

$$\frac{4.4}{3}$$

$$5.0 \quad \frac{7.1}{3} \quad \frac{7.7}{4.7} \quad \frac{5.6}{10} \quad \frac{4.9}{25}$$

Ditch

Ditch

$$\frac{4.1}{25} \quad \frac{4.3}{13} \quad \frac{5.5}{7.4} \quad \frac{5.9}{2} \quad 5.9$$

$$\frac{6.8}{5} \quad \frac{7.2}{7} \quad \frac{6.7}{25}$$

Sta	+	Δ	-	Elev	* pitch
-----	---	----------	---	------	---------

901.10,

32+50

93.6

93.6

33

94.1

93.6

+38²⁰

93.5

93.5

B.M

3.77

901.81

3.06

898.04.

34

95.3

93.2

+45

P.1

92.9

92.9

35

92.8

92.8

+42⁸⁰

P.1

93.0

93.0

36

94.8

92.9

+50

94.6

93.0

37

92.9

92.4

38

92.7

91.9

T.P.

7.37

904.83

4.35

897.46

Low Shots in Water Hole Lt

Sta

38+00

91.5

Lt

K

Rt

$$\frac{3.9}{25} \quad \frac{4.9}{13} \quad \frac{4.5}{6} \quad \frac{7.5}{3} \quad \frac{7.5}{3} \quad \frac{6.0}{3} \quad \frac{5.1}{6} \quad \frac{6.4}{8} \quad \frac{6.7}{20-25}$$

Ditch

$$\frac{5.0}{25} \quad \frac{5.5}{11} \quad \frac{4.6}{8-5} \quad \frac{7.5}{7.0} \quad \frac{6.1}{1-3} \quad \frac{6.4}{6} \quad \frac{6.4}{25}$$

Ditch

$$\frac{4.8}{25} \quad \frac{6.0}{13} \quad \frac{5.1}{7} \quad \frac{7.6}{3} \quad \frac{7.6}{7.6} \quad \frac{7.2}{1} \quad \frac{5.0}{5-7} \quad \frac{5.5}{8} \quad \frac{5.7}{30}$$

Ditch

$$\frac{6.0}{25} \quad \frac{6.5}{16} \quad \frac{5.7}{10} \quad \frac{8.6}{6.2} \quad \frac{6.5}{6.5} \quad \frac{5.3}{5} \quad \frac{5.9}{9} \quad \frac{5.6}{30}$$

Ditch

$$\frac{6.7}{25} \quad \frac{6.7}{9} \quad \frac{6.0}{7} \quad \frac{8.9}{2} \quad \frac{8.9}{8.9} \quad \frac{5.1}{7-9} \quad \frac{6.0}{12} \quad \frac{5.6}{23} \quad \frac{4.8}{29}$$

Ditch

$$\frac{4.7}{25} \quad \frac{4.6}{2} \quad \frac{7.0}{9.0} \quad \frac{7.0}{4} \quad \frac{4.7}{8} \quad \frac{5.1}{30}$$

Ditch

$$\frac{5.1}{25} \quad \frac{6.0}{8} \quad \frac{8.8}{3} \quad \frac{8.8}{8.8} \quad \frac{8.8}{3} \quad \frac{6.7}{5} \quad \frac{6.7}{30}$$

Ditch

$$\frac{8.0}{25} \quad \frac{7.9}{8} \quad \frac{7.0}{7.0} \quad \frac{7.2}{2} \quad \frac{8.3}{4} \quad \frac{8.9}{4-8} \quad \frac{7.7}{11} \quad \frac{8.2}{30}$$

Ditch

$$\frac{7.4}{25} \quad \frac{7.5}{4} \quad \frac{7.2}{7.2} \quad \frac{8.4}{5} \quad \frac{8.8}{7} \quad \frac{8.9}{30}$$

Ditch

$$\frac{9.8}{25} \quad \frac{9.8}{10} \quad \frac{8.9}{8.9} \quad \frac{9.4}{2} \quad \frac{9.4}{1} \quad \frac{9.1}{20} \quad \frac{8.7}{30}$$

Ditch

$$\frac{10.2}{50} \quad \frac{9.4}{25} \quad \frac{9.2}{15} \quad \frac{9.1}{9.1} \quad \frac{9.3}{3} \quad \frac{9.9}{6-10} \quad \frac{9.1}{10} \quad \frac{9.0}{20} \quad \frac{8.6}{30}$$

$$\begin{array}{r} \text{Top} \quad \text{Fc} \quad \text{Post} \quad 37+95 \\ \hline 13.3 \quad 13.1 \quad 13.4 \quad 13.1 \end{array}$$

$$\begin{array}{r} 893.69 \\ 11.14 \\ \hline W.S \quad 6/8/42 \end{array}$$

$$91.4$$

Sta	+	Δ	-	Elev	
T.P	2.65	900.11.	7.37	897.46	
39+00				93.1	92.2

40				93.5	92.4
----	--	--	--	------	------

41				91.7	91.7
----	--	--	--	------	------

+50				91.7	91.7
-----	--	--	--	------	------

+77 ⁸²	P.I			92.0	92.0
-------------------	-----	--	--	------	------

42		S. End 24' CM		93.6	91.7
----	--	---------------	--	------	------

+18		N. End 24' CM		93.7	91.52
-----	--	---------------	--	------	-------

+50				94.5	92.1
-----	--	--	--	------	------

43				94.6	92.0
----	--	--	--	------	------

+59 ⁵²	P.I			94.7	92.0
-------------------	-----	--	--	------	------

44				94.8	91.6
----	--	--	--	------	------

45				94.5	91.4
----	--	--	--	------	------

Lt

K

Rt

Top Fe Pool Sta 37+95 (Ditch)

$$\frac{8.0}{25} \quad \frac{7.8}{7} \quad \frac{7.0}{7.05} \quad \frac{7.9}{7.9} \quad \frac{7.2}{12} \quad \frac{6.6}{30}$$

(Ditch)

$$\frac{6.9}{25} \quad \frac{7.6}{13} \quad \frac{7.0}{7} \quad 6.5 \quad \frac{6.07}{3.6} \quad \frac{7.7}{7.10} \quad \frac{7.2}{11} \quad \frac{6.7}{13} \quad \frac{6.1}{20} \quad \frac{5.6}{30}$$

Ditch

$$\frac{6.2}{25} \quad \frac{6.0}{6} \quad \frac{7.0}{3} \quad \frac{8.4}{2} \quad 8.4 \quad \frac{8.4}{1} \quad \frac{6.9}{3} \quad \frac{6.8}{20} \quad \frac{6.5}{30}$$

Ditch

$$\frac{5.3}{25} \quad \frac{6.4}{8} \quad \frac{5.5}{3} \quad 8.4 \quad \frac{8.2}{4} \quad \frac{6.6}{6} \quad \frac{6.3}{20} \quad \frac{6.3}{30}$$

Ditch

$$\frac{5.4}{25} \quad \frac{5.4}{8} \quad \frac{8.1}{2} \quad 8.1 \quad \frac{8.1}{2} \quad \frac{6.4}{3} \quad \frac{6.4}{20} \quad \frac{6.4}{30}$$

891.47
Inv (Ditch)

$$\frac{5.6}{25} \quad \frac{5.8}{17} \quad \frac{8.4}{12} \quad \frac{8.4}{14.11} \quad \frac{6.5}{10} \quad 6.5 \quad \frac{6.0}{15}$$

Inv Ditch

$$\frac{5.3}{25} \quad \frac{6.0}{10} \quad \left(\frac{8.4}{8} \quad \frac{8.59}{7} \quad \frac{8.4}{5} \right) \quad \frac{6.3}{4} \quad 6.4 \quad \frac{6.7}{6} \quad \frac{6.0}{25}$$

Ditch

$$\frac{5.0}{25} \quad \frac{6.0}{7} \quad \frac{5.1}{5} \quad 5.6 \quad \frac{8.0}{4.7} \quad \frac{6.9}{8} \quad \frac{6.2}{25}$$

Ditch

$$\frac{5.3}{25} \quad \frac{5.7}{5} \quad 5.5 \quad \frac{5.8}{4} \quad \frac{8.1}{6.9} \quad \frac{6.7}{11} \quad \frac{6.2}{30}$$

Ditch

$$\frac{4.8}{25} \quad \frac{5.4}{14} \quad 5.4 \quad \frac{5.4}{2} \quad \frac{8.1}{6.9} \quad \frac{6.0}{10} \quad \frac{6.0}{25}$$

$$\frac{4.4}{25} \quad \frac{5.1}{7} \quad 5.3 \quad \frac{5.3}{1} \quad \frac{8.5}{5.8} \quad \frac{6.2}{10} \quad \frac{6.1}{20}$$

Ditch

$$\frac{4.4}{25} \quad \frac{5.4}{13} \quad 5.6 \quad \frac{8.5}{5.8} \quad \frac{6.0}{11} \quad \frac{5.8}{25}$$

Sta	+	π	-	Elev	* Ditch
		900.11		93.7	91.5

46+00

93.7

91.5

+36

P.1

94.5

91.6

T.P.

9.47

904.23

5.35

894.76

47

94.4

91.8

+50

93.0

91.8

48

91.5

91.5

B.M.

9.50

902.97

10.76

893.47

893.47

+50

91.5

91.5

49

94.3

91.5

+34.50

P.1

95.1

91.8

50

91.6

90.2

+36

S.E. End 18" CM

90.2

+60

896.4

T.P.

6.63

909.60

0.00

902.97

+91

905.7

Lt

£

R4

Ditch

$\frac{4.3}{30}$ $\frac{5.2}{16}$ $\frac{5.3}{3}$ 6.4 $\frac{8.6}{3-7}$ $\frac{5.7}{11}$ $\frac{5.5}{25}$

Ditch

$\frac{4.3}{30}$ $\frac{5.0}{17}$ 5.6 $\frac{8.5}{4-8}$ $\frac{7.2}{10}$ $\frac{5.2}{14}$ $\frac{5.3}{30}$

Ditch

$\frac{8.1}{25}$ $\frac{7.2}{11}$ $\frac{8.7}{4}$ 9.8 $\frac{12.4}{3-7}$ $\frac{11.2}{8}$ $\frac{11.4}{11}$ $\frac{8.8}{13}$ $\frac{8.5}{25}$

Ditch

$\frac{8.9}{25}$ $\frac{9.3}{16}$ $\frac{9.8}{4}$ 11.2 $\frac{12.4}{2.6}$ $\frac{11.4}{5}$ $\frac{9.2}{14}$ $\frac{8.5}{25}$

Ditch

$\frac{8.8}{33}$ $\frac{9.6}{20}$ $\frac{10.5}{6}$ $\frac{11.9}{2}$ 12.7 $\frac{12.5}{3}$ $\frac{11.7}{5.7}$ $\frac{9.1}{15}$ $\frac{7.7}{25}$ $\frac{7.5}{35}$

Spk in 18" Pop 1' Lt Sta 48+40

$\frac{5.6}{25}$ $\frac{7.2}{18}$ $\frac{8.0}{8}$ $\frac{11.5}{3}$ 11.5 $\frac{11.5}{3}$ $\frac{8.8}{10}$ $\frac{5.5}{18}$ $\frac{4.4}{23}$ $\frac{4.0}{30}$

$\frac{4.7}{32}$ $\frac{5.7}{27}$ $\frac{6.0}{18}$ $\frac{5.5}{6}$ 8.7 $\frac{10.6}{3}$ $\frac{11.5}{6-10}$ $\frac{10.2}{12}$ $\frac{7.4}{18}$ $\frac{5.8}{23}$ $\frac{4.2}{31}$

$\frac{5.0}{30}$ $\frac{6.6}{22-17}$ $\frac{5.1}{10-8}$ 7.9 $\frac{10.4}{4}$ $\frac{11.2}{6-10}$ $\frac{10.6}{14}$ $\frac{9.4}{21}$ $\frac{6.6}{23}$ $\frac{5.9}{27}$ $\frac{4.5}{32}$

$\frac{4.0}{30}$ $\frac{6.5}{17}$ $\frac{6.5}{11}$ $\frac{7.6}{6}$ 11.4 $\frac{12.8}{2.5}$ $\frac{11.3}{7}$ $\frac{7.4}{13-16}$ $\frac{8.1}{18}$ $\frac{8.2}{32}$

90.17

$\frac{6.6}{25}$ $\frac{7.8}{10}$ $\frac{10.1}{5}$ $\frac{12.8}{1}$ 12.80 $\frac{12.7}{2}$ $\frac{10.2}{5}$ $\frac{7.0}{11}$ $\frac{7.0}{15}$ $\frac{4.0}{30}$

$\frac{5.5}{35}$ $\frac{7.6}{25}$ $\frac{7.6}{15}$ $\frac{7.2}{5}$ 6.6 $\frac{5.7}{6}$ $\frac{0.6}{19}$ $\frac{+4.0}{30}$

$\frac{10.8}{43}$ $\frac{11.3}{31}$ $\frac{7.3}{19}$ $\frac{4.3}{6}$ 3.9 $\frac{3.4}{9}$ $\frac{2.3}{30}$ $\frac{2.5}{47}$

Sta + X - Elev

90960

51 06.2

+11.2 2 Lydia St. 065

+37 05.6

+73 96.0

T.P. 1.89 900.40 11.09 898.51

52 90.2

+04 N.W. End 18" CM 887.99

+25 90.7 87.4

53+49²⁰ S.E. End 24" Conc 86.89

53+49²⁰ N.W. End 24" Conc

T.P. 8.22 904.94 3.68 902.90

53+49²⁰ N.W. End 24" Conc 85.64

T.P. 8.29 910.73 2.50 902.44

B.M 5.90 904.83 904.80

L1

2

R1

$$\frac{10.4}{41} \quad \frac{80}{35} \quad \frac{4.0}{13}$$

$$3.4 \quad \frac{2.7}{13} \quad \frac{2.9}{35} \quad \frac{2.5}{50}$$

3.1

$$\frac{41}{50} \quad \frac{3.1}{39} \quad 4.0 \quad \frac{4.7}{8} \quad \frac{9.4}{28}$$

$$\frac{46}{50} \quad \frac{48}{44} \quad \frac{11.8}{15} \quad 13.6 \quad \frac{15.0}{6} \quad \frac{15.0}{14} \quad \frac{12.4}{33}$$

$$\frac{3.5}{30} \quad \frac{5.5}{19} \quad \frac{9.3}{8} \quad 10.2 \quad \frac{9.8}{3} \quad \frac{6.8}{10} \quad \frac{4.7}{26}$$

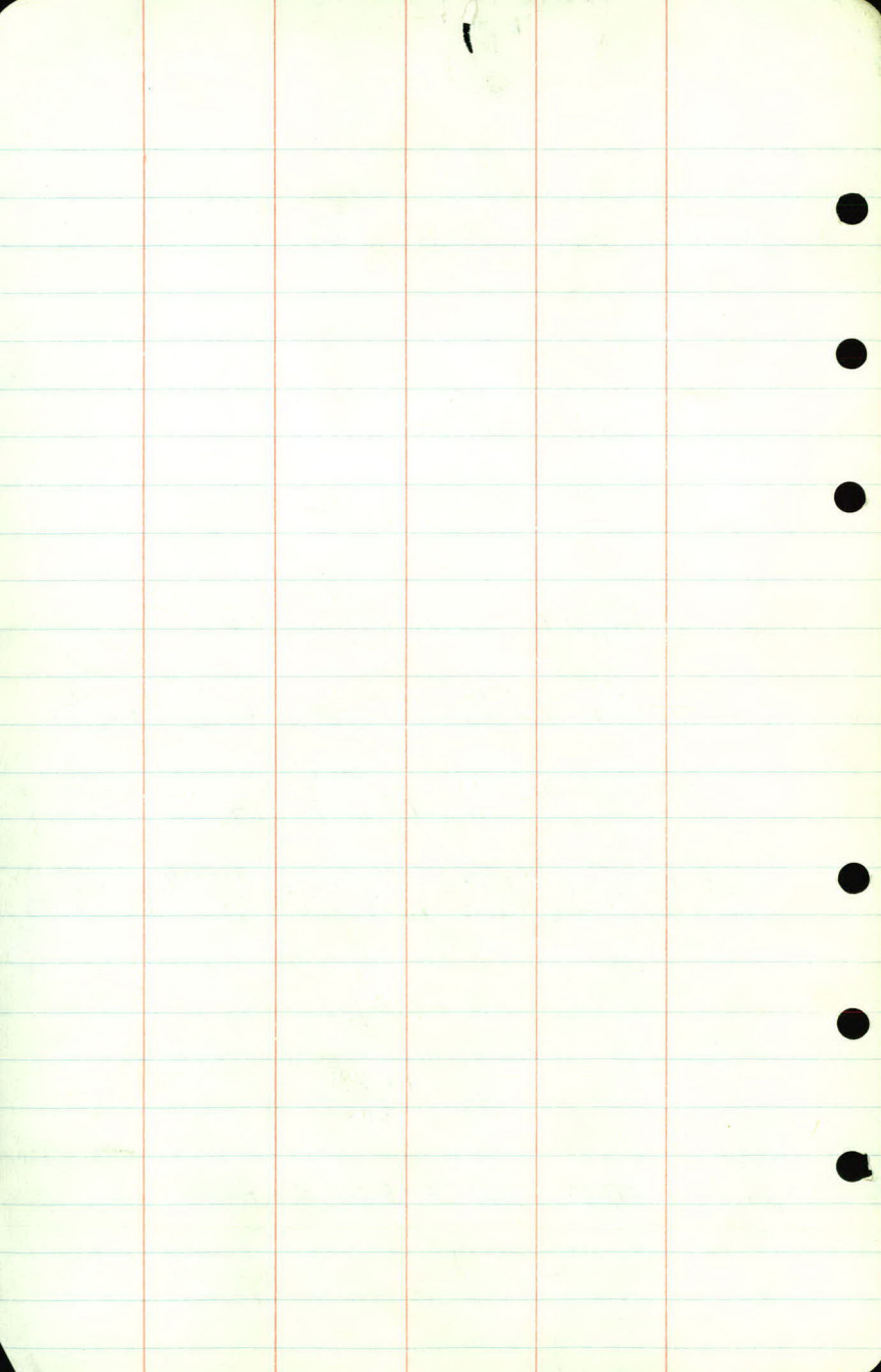
$$\frac{40}{31} \quad \frac{7.0}{18} \quad \frac{10.2}{4} \quad \frac{12.4}{2} \quad \overset{\text{Inv}}{12.4} \quad \frac{13.0}{0} \quad \frac{11.8}{4} \quad \frac{8.9}{6} \quad \frac{6.6}{12} \quad \frac{3.9}{31}$$

$$\frac{5.4}{32} \quad \frac{10.0}{11} \quad \frac{11.8}{6} \quad \frac{13.0}{5.3} \quad 9.7 \quad \frac{7.3}{8} \quad \frac{6.8}{17} \quad \frac{4.2}{32}$$

$$\frac{5.9}{32} \quad \frac{8.6}{12} \quad \frac{10.8}{8} \quad \frac{12.3}{2} \quad \overset{\text{Inv}}{13.51} \quad \frac{12.4}{2} \quad \frac{8.8}{7} \quad \frac{7.2}{19} \quad \frac{5.1}{32}$$

1930
Inv1930
Inv

Nail in T.P. 75' R1 Sta 50+00



9/17/42

L. C

C. F

A. M.

L. L

Elev. Ditch #4

From Co. Rd. "B" To New Brighton Rd.

Turned in 9/17/42

Plotted on X section sheet
to accompany New Brighton Rd.
drainage at Co. Rd. B.
9/21/42

Sta	+	Δ	-	Elev
B.M.	12.44	986.31		973.87
T.P.	0.44	974.58	12.17	974.14
T.P.	8.70	973.64	9.64	964.94
0 + 00 = S. End 18" C.M. Culv. at Co Rd "B"				60.17
+ 50				59.41
1				59.5
+ 50				59.0
2				58.40
+ 50				58.0
3				58.0
+ 50				58.8
T.P.	3.29	966.90	10.03	963.61
4				56.8
+ 50				56.2
5				56.1

LT. \$ RT
 Top Mont. Co. Rd. "B" + New Brighton Rd

13.47 F.I. So. End 18" CM X Drain

14.23 F.I. N.E. End 18" CM X Drain

14.1

14.6

15.2

15.4

15.6

14.8

10.1

10.7

10.8

Sta	+	T	-	Elev
		966.90		
5	+50			56.1
6				55.8
	+50			55.7
7				55.4
	+50			55.2
8				55.1
T.P.	3.65	963.25	7.30	959.60
	+50			55.0
9				54.9
	+50			54.5
10				54.1
	+50			53.6
11				53.3

Lt

±

Pt.

10.8

11.1

11.2

11.5

11.7

11.8

8.3

8.4

8.8

9.2

9.7

10.0

Sta	+	T	-	Elev
		963.25		
11	+50			53.2
12				52.6
	+50			52.7
13				52.6
	+50			51.5
14				50.9
	+50			50.9
15				50.8
	+50			50.0
+75	So. End 36" Conc. X Drain Xs Hwy #36			49.85
16 +79	No. End. 36" Conc. X Drain			48.90
T. P.	6.08	958.30	11.03	952.22
17				49.7

Lt.

±

Rt

55.9

7.40 Elev. Water in
Pot Hole

10.1

Swamp
Rt.

54.2

9.1 - Low spot in Swamp

10.7

10.6

10.7

11.8

12.4

12.4

12.5

13.3

13.40

14.35

8.6

Sta	+	π	-	Elev
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958.30

17 +50

49.0

18

48.4

+50

48.0

19

48.0

+50

47.6

20

47.5

+50

47.4

21

47.7

+50

47.9

22

47.7

+50

48.0

23

47.9

Lt.

£

Rt

9.3

9.9

10.3

10.3

10.7

10.8

10.9

10.6

10.4

10.6

10.3

10.4

Sta + π - Elev

958.30

23 +50

47.7

24

47.5

+50

47.7

25

47.6

+50

47.5

26

47.4

+17 W. End 36" x 36" Box CONC. X Drain Xs New Brighton Rd. 46.88

+63 E. End 36" x 36" Box CONC. X Drain 46.08

T.P. 8.35 961.39 5.26 953.04

T.P. 12.32 972.94 0.77 960.62

T.P. 6.44 977.99 1.39 971.55

B.M. 4.17 973.82 973.87

Lt.

£.

Rt.

10.6

10.8

10.6

10.7

10.8

10.9

11.42 F.I.

12.22 F.I.

Top Mont. Co. Rd. "B" + New Brighton Rd.

