

Book 83 Dr 16.

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

..... CLEVELAND AVE

From Larpenteur ^{or} To Co Rd "E"

Hoyt Ave. to Larpenteur Ave.

Road Acc't. No. 5

Date Filed 1-10-43

3-22-44

File

Plan Survey

Cleveland Ave

From Hoyt Ave To Larpenteur Ave

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Align	1 to 9	HAW
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Bench levels	21 to 24	L.G.
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Profile levels		
Grade List	At C ²	
Est Grades	Tile Line 36 to 38	
	at Co. Rd D	

Sta	Pt	ΔL	ΔR
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13+18.45	P.I.	0°21'	
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3+54.47	* Bridge		
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0+00	POT		
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Description

PP

53.72'

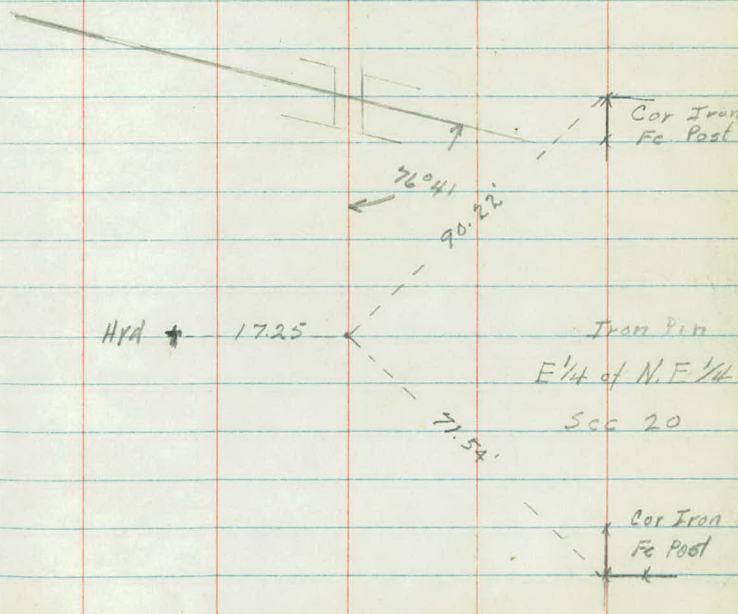
Stone Mark
N.E. Cor Sec 20

82.70'

45.44'

PP

Arch Pole



Sta

P/

Alt

Alt

50+1989

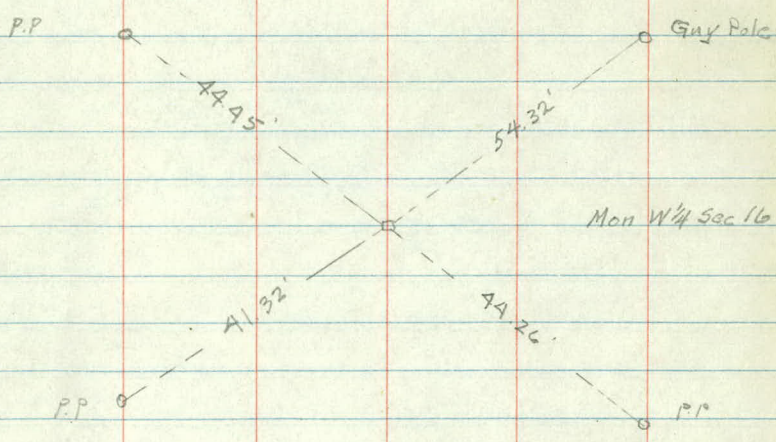
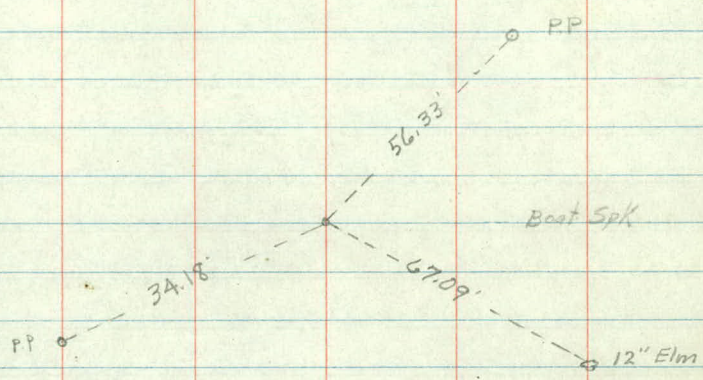
POT

39+5285

P.L.

0°07'

Description



Sta

Pt.

ALT

ΔRT

76+01³²

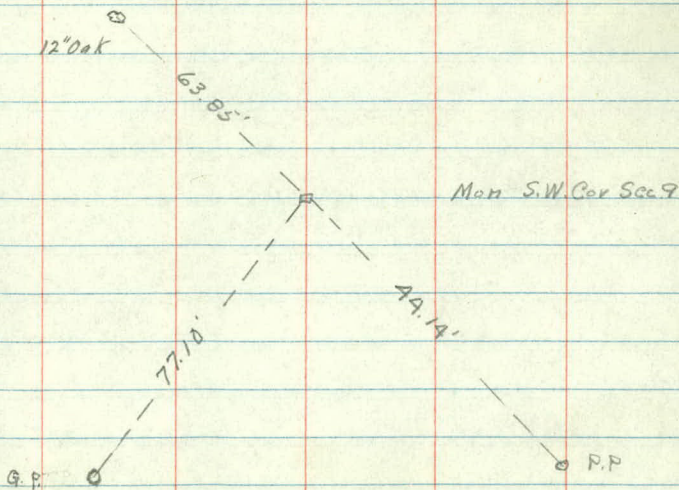
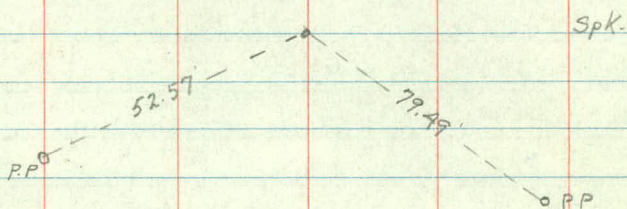
POT

65+79³⁹

P.1

0°10'

Description



Sta

Pt.

ΔL

ΔR

102+08.28

P.O.T.

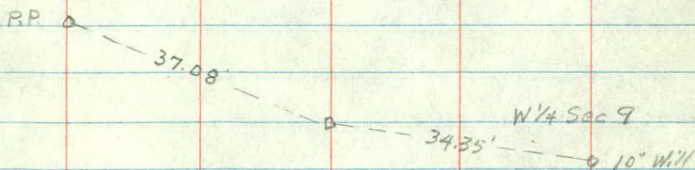
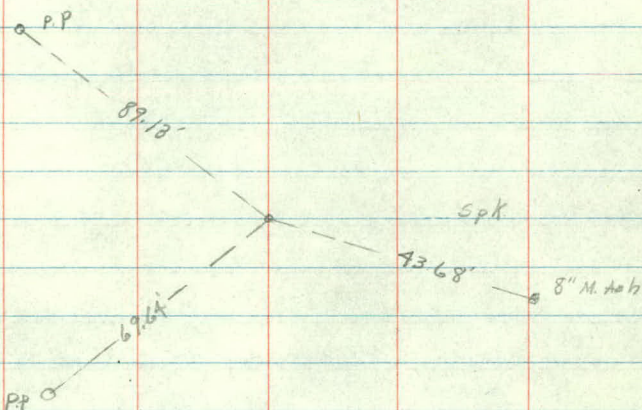
92+20.43

P.I.

$0^{\circ}54'$

5

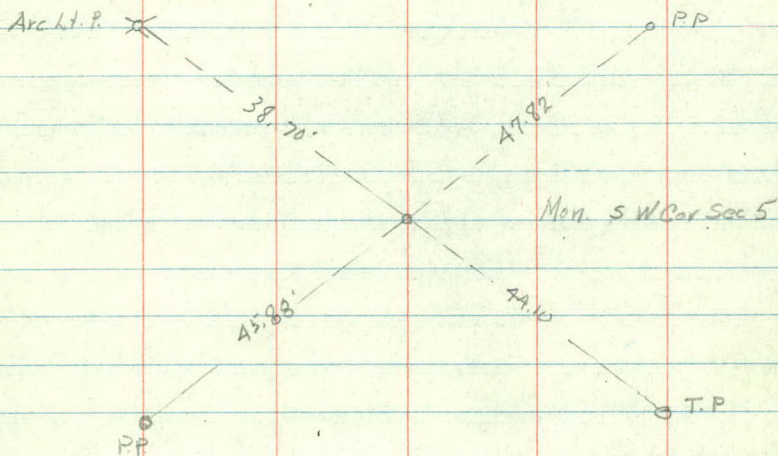
Description



Sta	Pt	ALT	ART
118+38 ²⁰	P1	0° 20'	± Co Rd "C"

116+3384	POT	± N.P. Tr.	
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Description

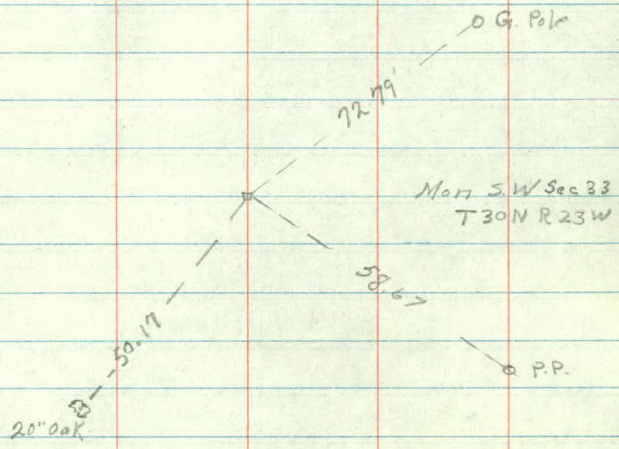


Sta	PI	ΔLT	ΔRT
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173+84.50	P.I	& Co Rd "D"	1°05'
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144+76.50	P.O.T.	& "C2"	
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Description



Sta

Pt

$\Delta L+$

$\Delta R+$

226+43.25

P.I

200+00.25

P.I

$0^{\circ}20'$

Description

Steel Plate
Sec Car underneath
Bridge

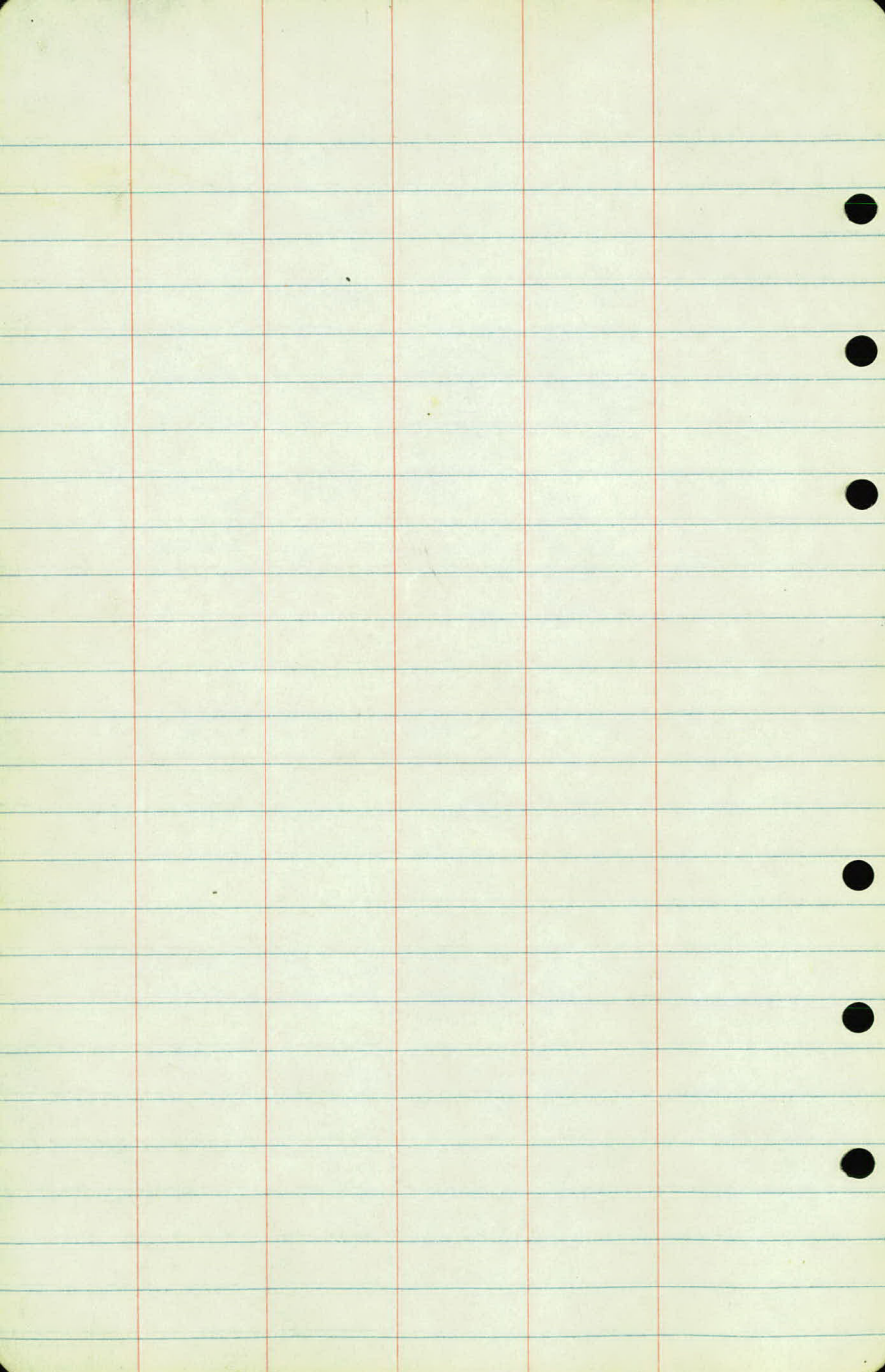
18" Oak

89.29'

T.P.O. — 27.42 —

Mon W. 1/4 Sec 33

T. 30 N. R. 23 W



Topography
Cleveland Ave

8-19-43

HAW
AM
LG

6 12 ^{Pave} 12

5 12 12

4 12 12

+85 End Tile Dr 79'

+61 Fe Cor 34'

+26 G R 13.
+21 Fe Cor 343.
+16 Rye tie Fe.

+34 ~~43~~ * Bridge over Inter Campus Line
see Page For Details
+34 12" Tile Dr 39.5'.
+21 G R 13.
12' 12'

3

+50 10' Path 58.
+56 Cor Nursery 39'

2 12' 12'

G R 16' Path 32'.
+54 Beg G R 16.8'.
93 20" Oak 38'.
+88 8" Oak 38'.
+86 End Curb 16.5'.

1 12' 12'

Curb 16.8 Hedge 38'.
+87 End Pop 45' & 50'.
+64 Beg Group 9 Pop 40' & 50'.

0 12' 12'

Lilac Hedge 50 Fence 53'.

G.R. 15.

+50 6" B.E. 30'.

G.R. 15'.

+61 G.R. 15'.

+54 Ryo Tie Fc.

+48 GE 13'.

+48.5 End Bridge.

+25 Bay Bridge 12'.

+15 G.R. 15'.

G.R. 15' End Woods 38'.

Woods 26'.

G.R. 15' Woods 21'.

+95 Bay G.R. 15'.

+90 Tel. M.H. 14'.

+42 12" B.E. 27'.

+00 12" Oak 31' Woods 31'.

+70 6" Oak 30'.

+02 Arch 16'.

0+00 Bay Woods 28'.

0-89 Pavc 15'.

0-89 Curb 15'.

Cultivated

Wood Post + Cable 2

7" I.C.C. Pavc

Wood Post + Cable 3

Cultivated

+718 Oak 39'.

+61 6" B.E. 27'.

+30 36" Oak 36'.

G.R. 16'.

+03 Twin 12" B.E. 35'.

G.R. 16'.

+63 G.R. 16'.

+44 Group 5 B.E. 44'.

+42 G.R. 13'.

+43.5 End Bridge 12'.

+20 Bay Bridge 12'.

+05 G.R. 16'.

G.R. 16'.

+99 Cor Nursery 46'.

+87 Nursery 100'.

+65 18" Oak 38'.

+47 18" Oak 39'.

+45 15" Oak 37'.

+36 18" Oak 37'.

+00 5" Oak 49'.

+86 End Walk 26.8 + 32.8

+84 8" Elm 22'.

+84 End Lawn.

+68 End Hedge 28'.

+38 6" Elm 22'.

Walk 26.8 + 32.8.

+94 8" Elm 22'.

+73 Fc Coy 54'.

+63 End Lila Hedge 30'.

+50 8" Elm 23'.

+03 8" Elm 22'.

+00 Hedge 38'.

Curb 16.8 Walk 26.8

32.8

0-95 Pavc 16.8.

Brush & Woods
Note Tel Cable Buried 14 ft

7" I.C.C. Pavc.

Lawn

Blacktop Tennis Court

C' Motion White 2

13

Pave
12' 12'

+59 Bes Rad 12' + 13'

+59 Bes Rad 12' + 13'

12

12 12

11

12' 12'

10

12' 12'

9

12' 12'

8

12' 12'

7

12' 12'

6

12' 12'

50' Rad

+90 End 12" CM 495' X

+84 Fc Cor. #1'

+77 2 in Fc 315'

+77 Bog 12' x 20' CM 27.5'

+63 24" Maple 40'
Fc 31'

+77 24" Maple 40'

+36 36" Maple 39'

+65 20" Maple 39'

Fc 31'

+65 48" Maple 50'

+53 End Cult. Bog School Yard

+53 Bog Fc 315'

School Yard

4' Woven Wire

4' Woven Wire

Cultivated
Buried Tel Cable 14'

7" I.C.C. Pipe

Cultivated

+06 Tel M.H. 14'

+94 End G.R. 15'

G.R. 15'

50' Rad

+87 Arc Lt Pole 34'

+85 Fc Cor 34'

+63 24" Maple

Fc 34'

Fc 34'

Fc 34'

Fc 34'

Fc 34'

+65 36" Oak 31'

+23 End G.R. 16'

+07 Bog Fc 34'

G.R. 16'

+80 24" Oak 32'

+56 18" Oak 32'

+46 15" Oak 32'

+25 24" Oak 32'

G.R. 16'

20

19

18

17

16

15

14

+18.45' $\frac{1}{2}$ Larpentenn

+08.45' Edge Parc

+09 End Rad 62'.

+07 End Rad 62'.

13

7" I.C.C. Pavr

50' Conc Rad.

50' Conc Rad

27

26

25

24

23

22

21

20

Bridge Detail

Sta 3+34.47

Over T.C. Lines

Inter Campus Line

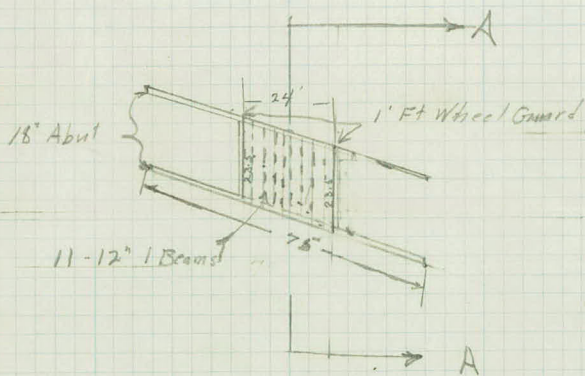
8-19-43

HAW

AM

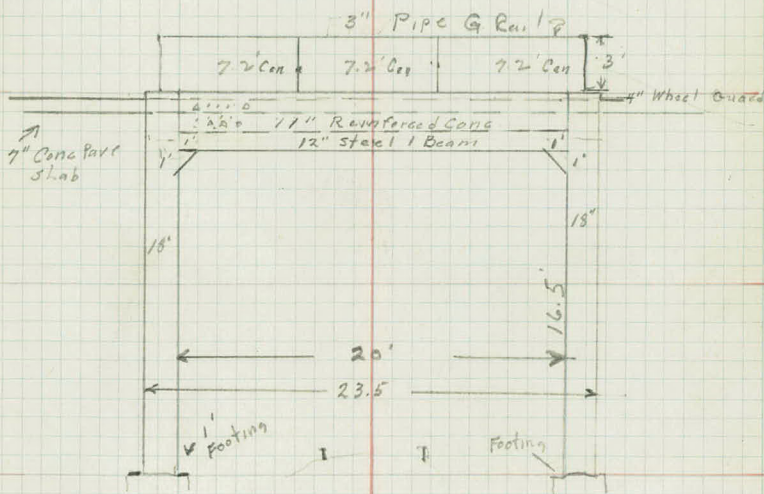
LG

Plan

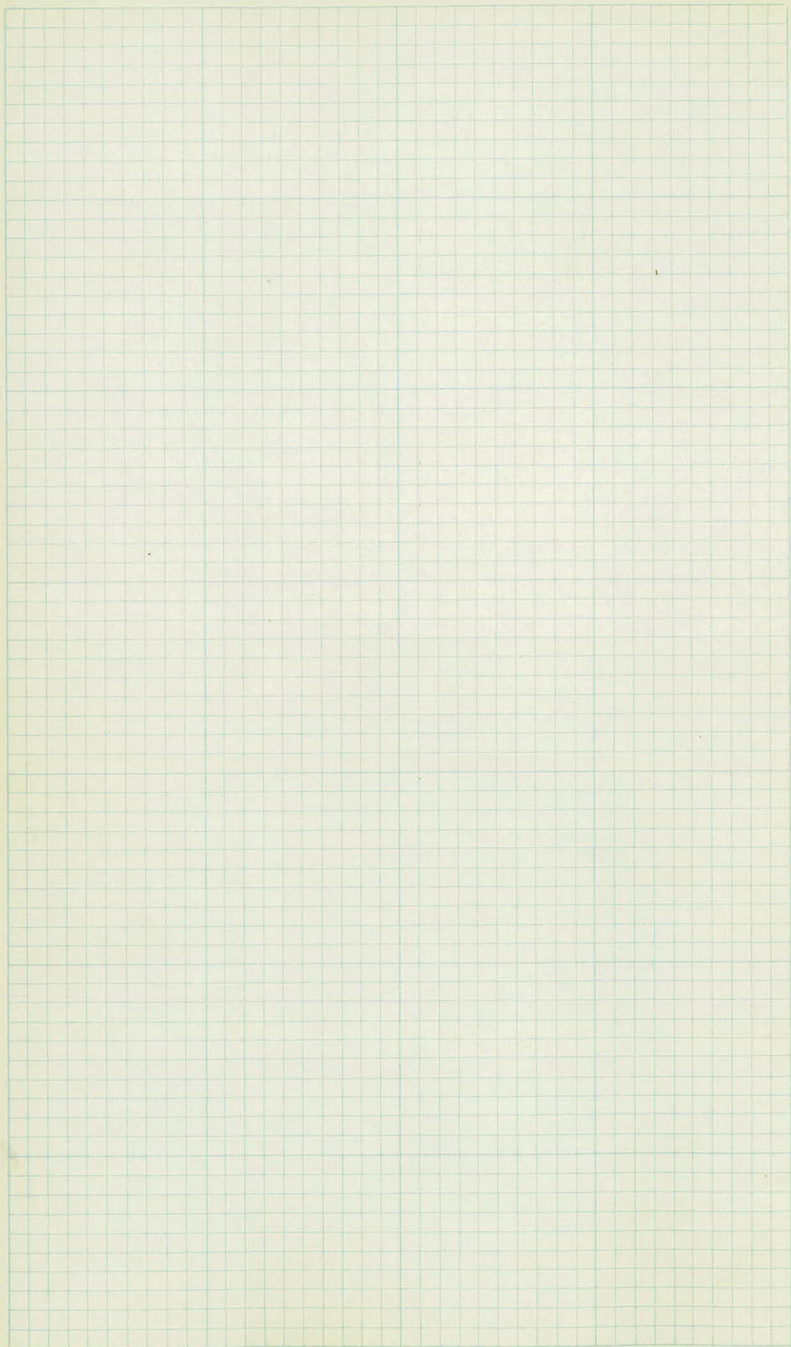


Scale 1" = 5'

Elev Sec A A



Scale 1" = 1'



Topography
Cleveland Ave

8-21-42

HAW
AM
LG.

Fe. 165 Rd 111

62

61

Rd 111

60

Rd 111

59

ROW Fe 165' Rd 113

58

ROW Fe 165'

57

56

55

x
 x
 x
 x
 x
 x
 x

+17 End Rad 14'
 +08 Beg Rad 30'
 ± Drive 80'

+90 & 28' Service Dr

+76 End Rad 29
 +66 Beg Rad 11

+88 Fe Cor 33

x x
 x
 x
 x

69

68

67

66

65

64

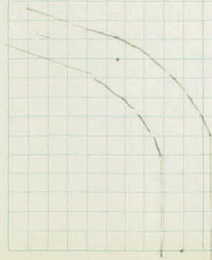
63

Rd 143

+ 50 Rge Tire Service Drive No West

62

+73 Edge Woods #8'



76

+80 End Drive

+66 * Drive

+52 Box Drive

Rd 63

75

74

Rd 71

73

72

71

70

69

+69 FeCoV 33-40

28' Service Drive

Fe 425

+02 R₉₀ TiFe

+84 FeCoV 40'

83

82

81

80

79

78

77

76

167

166

165

164

163

162

161

160

+98 End 4" + 6 Tile
20'

6' Conc Tile Line B
4' " " " " "

Elev Inv

Tile Line
+81 Cen M.H 21'
283 Ft East To CB

174

173

172

171

170

169

168

167

Bench Levels

Cleveland Ave

5-1-43

HAW

AM

L.G.

Sta	+	Δ	-	Elev
B.M	8.90	934.79.		925.89
	9.75	942.83	1.71	933.08
	12.31	954.86	0.28	942.55
B.M	9.88	964.19	0.55	954.31
	3.00	962.92	4.27	959.92
	1.73	954.80	9.85	953.07
	0.91	944.53	11.18	943.62
B.M	5.45	944.53	5.45	939.08
	9.92	952.10	2.35	942.18
	7.52	956.19	3.43	948.67
	10.34	966.38	0.15	956.04
B.M	2.20	966.38	2.20	964.18
	4.97	970.44	0.91	965.47
	7.39	973.44	4.39	966.05
B.M	4.15	977.05	0.54	972.90
	4.08	972.91	8.22	968.83
	12.47	984.32	1.06	971.85
B.M	9.11	988.27	5.16	979.16
	6.34	993.75	0.86	987.41
	1.60	987.08	8.27	985.48
B.M	4.63	987.08	4.63	982.45
	2.41	981.62	7.87	979.21
	9.72	986.00	5.34	976.28
B.M.	8.10	986.00	8.10	977.90
	5.62	987.36	4.26	981.74

Description

Top U.S.G.S # G.13 36' Rt Sta 115+05

Top Angle Iron Sta Marker 25 Lt Sta 104+77

Top Mon Sta 92+20.43

Spk in 15" Oak 45' Lt Sta 78+11

Top Mon Sta 65+79.29

Top of N.W Cor Btm Stop 70' Rt 53+50

Top Mon Sta 39+52.85

Top of Conc Fe Anchor 33' Lt Sta 26+40

Sta	+	Δ	-	Elev	
		987.36			
B.M	2.57	^{983.31} 982.95	6.98	980.38	plan sur. K.A. 980.74
	8.51	⁴² 986.06	5.40	977.91 977.55	
	9.06	^{995.26} 994.90	0.22	986.20 985.84	
B.M			1.50	993.76 993.40	
B.M	1.62	927.51		925.89	
	2.36	916.86	13.01	914.50	
	0.12	908.96	8.02	908.84	
B.M.	6.66	911.77	3.83	905.13	905.11
	3.47	909.54	6.70	905.07	
B.M	5.69	909.05	5.18	903.36	903.34
	6.37	910.76	4.66	904.39	
	6.67	914.06	3.37	907.39	
B.M	3.30	914.06	3.30	910.76	
	6.94	912.86	8.14	905.92	
	8.17	919.12	1.91	910.95	
B.M	3.24	920.14	2.22	916.90	917.00
	2.32	912.65	9.81	910.33	
	5.35	907.77	10.23	902.42	
B.M	7.18	907.77	7.18	900.59	
	9.45	916.06	1.16	906.61	
	10.33	926.21	0.18	915.88	
	7.27	933.19	0.29	925.92	
B.M	3.10	931.12	5.17	928.02	

Description

Top Mon Sta 13+18.45

Top Iron Pin 0+00.

Top U.S.G.S. *G13 36' Rt Sta 115+05 ✓
Co Rd

Top U.S.G.S. *G14 30' Lt Sta 1345 No Cord C

Spk in Arc Lt Pole SE Cor C² Y C leve

Top N.W Cor Btm. Step Rt Sta

Top Mon D & C leve.

Spk in T.P Lt Sta

Top Mon Sta
(D²)

Sta	+	π	-	Elev
		931.12		
	4.13	928.25	7.00	924.12
B.M.	4.56	928.64	4.17	924.08
	6.26	930.68	4.22	924.42
	7.92	936.73	1.87	928.81
	10.08	942.66	4.15	932.58
B.M.	2.18	934.67	10.18	932.48 932.491
	0.68	923.99	11.36	923.31
	1.14	912.08	13.05	910.94
	1.64	901.63	12.09	899.99
	3.88	893.90	11.61	890.02
	3.32	894.79	2.43	891.47
B.M.			10.46	884.33

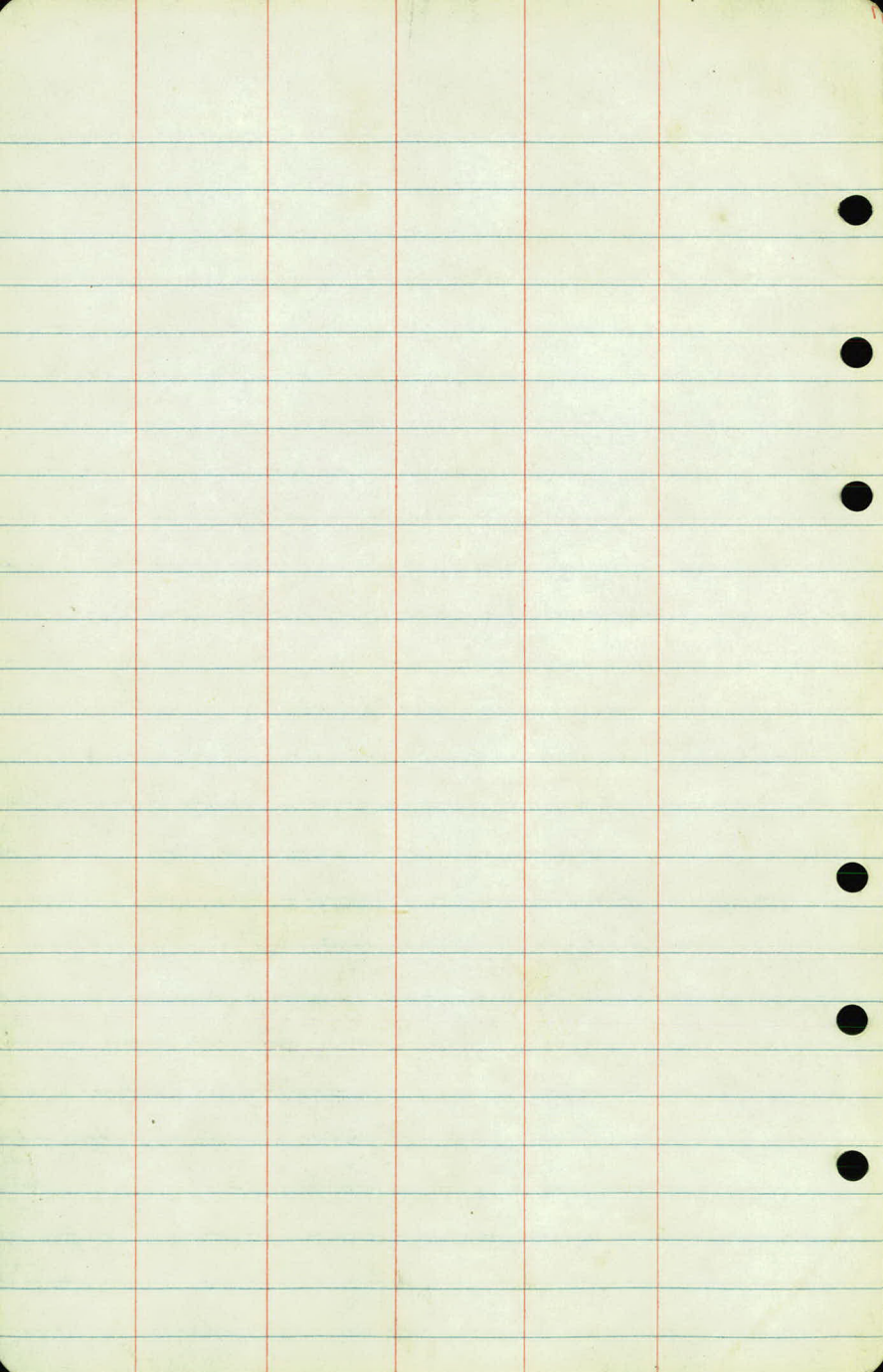
For B.M.s See Bk 83-Dr 16

Description

N.E. Cor Btm. Step Lt Sta

Top V.S.G.S # G15 N.W. Cor Co Rd E + Clev ✓

Spk in Top Sta East of line



X Sections
Cleveland Ave
From Hohlt to Larpentour

8-20-43

HAW

AM

L.G.

Sta	+	Σ	-	Elev
B.M.	5.47	999.23 998.87		993.76 997.76 95.97
0-1400				
0-0450				94.86
0400				93.76
0706				93.60
+32				92.94
+50				92.54
1400				91.35
+50				90.11
T.P.	4.98	993. ⁸⁸ 52	10.33	988.54 988.90
+85		End Curve 1 Walk Rt.		89.25
2400				88.90
+50				87.68
T.P.	3.27	989. ⁷⁵ 39	7.40	986.12 986.48
3400				86.48

Lt

X

Rt

Top Iron Plug Sta 0+00

3.26

4.37

$\frac{11.0}{54}$	$\frac{11.0}{44}$	$\frac{0.0}{38}$	$\frac{2.4}{73}$	$\frac{5.8}{22.9}$	$\frac{5.3}{15}$	$\frac{5.66}{12}$	5.47	$\frac{5.52}{12}$	$\frac{5.7}{14}$	$\frac{5.6}{16.8}$	$\frac{5.0}{16.8}$	$\frac{4.67}{26.8}$	$\frac{4.5}{32.8}$	$\frac{3.8}{50}$
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$\frac{+4.8}{50}$	$\frac{+4.9}{40}$	$\frac{0.0}{33}$	$\frac{6.2}{24.20}$	$\frac{5.6}{17}$	$\frac{5.83}{12}$	5.63	$\frac{5.68}{12}$	$\frac{5.4}{16.8}$	$\frac{5.13}{16.8}$	$\frac{4.78}{26.8}$	$\frac{4.6}{32.8}$	$\frac{3.9}{50}$
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$\frac{0.7}{50}$	$\frac{0.1}{33}$	$\frac{4.5}{24.20}$	$\frac{6.4}{17}$	$\frac{6.40}{12}$	6.29	$\frac{6.36}{12}$	$\frac{6.0}{16.8}$	$\frac{5.79}{16.8}$	$\frac{5.33}{26.8}$	$\frac{5.22}{32.8}$	$\frac{4.2}{50}$
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$\frac{1.9}{50}$	$\frac{1.3}{41}$	$\frac{1.4}{33}$	$\frac{4.3}{29}$	$\frac{8.2}{24.20}$	$\frac{7.0}{18}$	$\frac{6.82}{12}$	6.69	$\frac{6.82}{12}$	$\frac{6.4}{16.8}$	$\frac{6.25}{16.8}$	$\frac{5.81}{26.8}$	$\frac{5.70}{32.8}$	$\frac{4.3}{50}$
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$\frac{6.4}{50}$	$\frac{5.8}{29}$	$\frac{9.8}{24.20}$	$\frac{8.2}{17}$	$\frac{8.00}{12}$	7.88	$\frac{8.00}{12}$	$\frac{7.83}{16.8}$	$\frac{7.50}{16.8}$	$\frac{7.13}{26.8}$	$\frac{6.98}{32.8}$	$\frac{5.6}{50}$
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$\frac{5.8}{50}$	$\frac{7.2}{28}$	$\frac{11.0}{24.20}$	$\frac{9.4}{17}$	$\frac{9.23}{12}$	9.12	$\frac{9.22}{12}$	$\frac{9.0}{16.8}$	$\frac{8.74}{16.8}$	$\frac{8.48}{26.8}$	$\frac{8.36}{32.8}$	$\frac{7.6}{50}$
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$\frac{2.8}{50}$	$\frac{3.4}{26}$	$\frac{6.0}{24.20}$	$\frac{5.0}{17}$	$\frac{4.73}{12}$	4.63	$\frac{4.70}{12}$	$\frac{4.5}{16.8}$	$\frac{4.26}{16.8}$	$\frac{4.28}{26.8}$	$\frac{4.16}{32.8}$	$\frac{4.7}{50}$
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$\frac{5.6}{50}$	$\frac{6.8}{32}$	$\frac{7.0}{21}$	$\frac{5.2}{16}$	$\frac{5.08}{12}$	4.98	$\frac{5.16}{12}$	$\frac{5.3}{17}$	$\frac{6.6}{21}$	$\frac{6.1}{27}$	$\frac{6.2}{35}$	$\frac{7.3}{50}$
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$\frac{15.0}{50}$	$\frac{14.8}{30}$	$\frac{6.7}{17}$	$\frac{6.32}{12}$	6.20	$\frac{6.25}{12}$	$\frac{6.4}{18}$	$\frac{11.8}{28}$	$\frac{13.5}{32}$	$\frac{14.7}{50}$
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$\frac{14.0}{50}$	$\frac{14.0}{35}$	$\frac{3.4}{16}$	$\frac{3.45}{12}$	3.27	$\frac{3.46}{12}$	$\frac{4.0}{18}$	$\frac{13.5}{35}$	$\frac{15.4}{50}$
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Sta	+	Σ	-	Elev
		989. ⁷⁵ 39		
3+15				86.07
+20				85.97
+22				85.93
+28				85.81
+38				85.59
+44				85.47
+47				85.35
+50				85.25
+61				84.99
4+00				84.10
+50				82.93
T.P.	0.71	977. ⁸⁴ 48	12.62	976.47 977.13
3+28				85.81

L+

Z

R+

21

$$\frac{17.0}{50} \quad \frac{14.0}{33} \quad \frac{10.6}{28} \quad \frac{7.5}{21} \quad \frac{4.0}{15} \quad \frac{3.80}{12} \quad 3.68 \quad \frac{3.80}{12} \quad \frac{4.5}{16} \quad \frac{12.6}{29} \quad \frac{14.9}{37} \quad \frac{17.9}{50}$$

$$\frac{16.5}{50} \quad \frac{15.6}{35} \quad \frac{9.4}{20} \quad \frac{7.3}{14} \quad \frac{4.9}{12} \quad \frac{3.84}{12} \quad 3.78 \quad \frac{3.87}{12} \quad \frac{3.40}{12.13}$$

$$\frac{18.5}{50} \quad \frac{15.6}{35} \quad \frac{9.4}{20} \quad \frac{7.3}{14} \quad \frac{4.9}{12} \quad \frac{3.84}{12} \quad 3.82 \quad \frac{3.88}{12} \quad \frac{3.49}{12.13}$$

$$\frac{3.60}{13-12} \quad \frac{3.98}{12} \quad 3.94 \quad \frac{3.94}{12} \quad \frac{3.61}{12-13}$$

$$\frac{3.85}{13-12} \quad \frac{4.20}{12} \quad 4.16 \quad \frac{4.25}{12} \quad \frac{3.87}{12-13}$$

$$\frac{3.98}{13-12} \quad \frac{4.36}{12} \quad 4.28 \quad \frac{4.40}{12} \quad \frac{4.00}{12-13}$$

$$\frac{4.08}{13-12} \quad \frac{4.42}{12} \quad 4.40 \quad \frac{4.68}{12} \quad \frac{5.3}{14}$$

$$\frac{4.7}{14} \quad \frac{4.5}{12} \quad 4.50 \quad \frac{4.6}{12} \quad \frac{4.8}{15}$$

$$\frac{5.1}{15} \quad \frac{5.0}{12} \quad 4.71 \quad \frac{4.86}{12} \quad \frac{5.3}{16}$$

$$\frac{5.6}{15} \quad \frac{5.81}{12} \quad 5.65 \quad \frac{5.83}{12} \quad \frac{5.7}{17}$$

$$\frac{7.1}{15} \quad \frac{7.01}{12} \quad 6.82 \quad \frac{7.05}{12} \quad \frac{7.1}{17}$$

$$-18.3 \quad -18.3 \quad -18.5$$

$$\frac{10.3}{50} \quad \frac{10.3}{38} \quad \frac{10.5}{13} \quad + 7.97$$

Sta + π - E/cv

⁸⁴
977.48

3+38 85.59

+44 85.47

+47 85.35

+50 85.25

+61 84.99

4 84.10

+50 82.93

T.P. 6.72 ^{974.21}
~~973.85~~ 1035 967.13 967.49

3+20 85.97

+22 85.93

+28 85.81

+38 85.59

+44 85.47

Lt ✕ Ry

$$\begin{array}{r} -18.1 \\ 10.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -18.2 \\ 10.4 \\ \hline 73 \end{array}$$

$$+7.75$$

$$\begin{array}{r} -17.9 \\ 10.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -18.6 \\ 11.0 \\ \hline 13 \end{array}$$

$$+7.63$$

$$\begin{array}{r} -17.7 \\ 10.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -17.9 \\ 10.4 \\ \hline 37 \end{array}$$

$$+7.51$$

$$\begin{array}{r} -18.4 \\ 11.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -17.4 \\ 10.0 \\ \hline 44 \end{array}$$

$$\begin{array}{r} -15.2 \\ 9.8 \\ \hline 38 \end{array}$$

$$+7.41$$

$$\begin{array}{r} -12.3 \\ 5.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -14.9 \\ 7.2 \\ \hline 47.39 \end{array}$$

$$\begin{array}{r} -13.4 \\ 6.2 \\ \hline 39 \end{array}$$

$$\begin{array}{r} -12.6 \\ 5.4 \\ \hline 33 \end{array}$$

$$+7.15$$

$$\begin{array}{r} -11.1 \\ 4.8 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -10.9 \\ 4.6 \\ \hline 39 \end{array}$$

$$\begin{array}{r} -12.3 \\ 6.0 \\ \hline 38.37 \end{array}$$

$$\begin{array}{r} -10.6 \\ 4.3 \\ \hline 36 \end{array}$$

$$\begin{array}{r} -9.5 \\ 3.2 \\ \hline 32 \end{array}$$

$$+6.26$$

$$\begin{array}{r} -9.7 \\ 4.6 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -9.6 \\ 4.5 \\ \hline 29 \end{array}$$

$$\begin{array}{r} -10.5 \\ 5.4 \\ \hline 38.37 \end{array}$$

$$\begin{array}{r} -9.5 \\ 4.4 \\ \hline 35 \end{array}$$

$$\begin{array}{r} -8.8 \\ 3.7 \\ \hline 31 \end{array}$$

$$+5.09$$

$$\begin{array}{r} -16.2 \\ 4.4 \\ \hline 38 \end{array}$$

$$\begin{array}{r} -18.4 \\ 6.6 \\ \hline 50 \end{array}$$

$$+11.76$$

$$+11.72$$

$$\begin{array}{r} -18.1 \\ 6.4 \\ \hline 38 \end{array}$$

$$\begin{array}{r} -18.3 \\ 6.6 \\ \hline 50 \end{array}$$

$$+11.60$$

$$\begin{array}{r} -18.2 \\ 6.6 \\ \hline 13 \end{array}$$

$$\begin{array}{r} -18.2 \\ 6.6 \\ \hline 50 \end{array}$$

$$+11.38$$

$$\begin{array}{r} -18.6 \\ 4.2 \\ \hline 14 \end{array}$$

$$\begin{array}{r} -18.7 \\ 7.3 \\ \hline 38 \end{array}$$

$$\begin{array}{r} -16.3 \\ 4.9 \\ \hline 38 \end{array}$$

$$\begin{array}{r} -15.4 \\ 4.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} -16.4 \\ 5.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -17.0 \\ 6.2 \\ \hline 62 \end{array}$$

$$+11.26$$

$$\begin{array}{r} -14.6 \\ 3.3 \\ \hline 42 \end{array}$$

$$\begin{array}{r} -16.6 \\ 5.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -17.8 \\ 6.5 \\ \hline 62 \end{array}$$

Sta		+ T	-	Elev
		974.21 973.85		
3+47				85.35
+50				85.25
+61				84.99
4				84.10
+50				82.93
5				81.7
T.P.	1203	985.30 984.94	0.94	972.41 973.27.
5+00				81.7
+50				80.62
6+00				79.68
+50				78.95
T.P.	424	982.59 982.23	6.95	979.49 978.35
7				78.35
T.P.			6.95	977.99
+50				77.89

L+

K

R+

29

-14.9 -16.7 -17.7

+11.14

$$\begin{array}{r} 38 \\ 42 \\ \hline 50 \end{array} \quad \begin{array}{r} 56 \\ 50 \\ \hline 62 \end{array} \quad \begin{array}{r} 66 \\ 62 \\ \hline 62 \end{array}$$

-13.6 -15.9 -17.7

+11.04

$$\begin{array}{r} 26 \\ 40 \\ \hline 46 \end{array} \quad \begin{array}{r} 49 \\ 46 \\ \hline 62 \end{array} \quad \begin{array}{r} 67 \\ 62 \\ \hline 62 \end{array}$$

-14.8 -16.7 17.9

+10.78

$$\begin{array}{r} 40 \\ 42 \\ \hline 50 \end{array} \quad \begin{array}{r} 59 \\ 50 \\ \hline 62 \end{array} \quad \begin{array}{r} 71 \\ 62 \\ \hline 62 \end{array}$$

-15.3 -16.6 -17.7

+9.89

$$\begin{array}{r} 54 \\ 45 \\ \hline 50 \end{array} \quad \begin{array}{r} 67 \\ 50 \\ \hline 62 \end{array} \quad \begin{array}{r} 78 \\ 62 \\ \hline 62 \end{array}$$

-14.8 -16.7 -17.5

+8.72

$$\begin{array}{r} 61 \\ 40 \\ \hline 51 \end{array} \quad \begin{array}{r} 80 \\ 51 \\ \hline 60 \end{array} \quad \begin{array}{r} 88 \\ 60 \\ \hline 60 \end{array}$$

-14.3 -16.1

+7.49

$$\begin{array}{r} 68 \\ 40 \\ \hline 60 \end{array} \quad \begin{array}{r} 86 \\ 60 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 119 \\ 50 \\ \hline 32 \end{array} \quad \begin{array}{r} 115 \\ 32 \\ \hline 35-34 \end{array} \quad \begin{array}{r} 127 \\ 30 \\ \hline 30 \end{array} \quad \begin{array}{r} 112 \\ 30 \\ \hline 30 \end{array} \quad \begin{array}{r} 42 \\ 16 \\ \hline 12 \end{array} \quad \begin{array}{r} 382 \\ 12 \\ \hline 3.60 \end{array} \quad \begin{array}{r} 3.71 \\ 12 \\ \hline 40 \\ 16 \end{array}$$

$$\begin{array}{r} 116 \\ 50 \\ \hline 37 \end{array} \quad \begin{array}{r} 118 \\ 37 \\ \hline 32 \end{array} \quad \begin{array}{r} 114 \\ 32 \\ \hline 31-29 \end{array} \quad \begin{array}{r} 123 \\ 31-29 \\ \hline 29 \end{array} \quad \begin{array}{r} 113 \\ 29 \\ \hline 16 \end{array} \quad \begin{array}{r} 51 \\ 16 \\ \hline 12 \end{array} \quad \begin{array}{r} 497 \\ 12 \\ \hline 468 \end{array} \quad \begin{array}{r} 492 \\ 12 \\ \hline 5.3 \end{array} \quad \begin{array}{r} 5.3 \\ 16 \\ \hline 36 \end{array} \quad \begin{array}{r} 15.8 \\ 36 \\ \hline 50 \end{array} \quad \begin{array}{r} 16.2 \\ 50 \\ \hline 60 \end{array} \quad \begin{array}{r} 18.8 \\ 60 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 109 \\ 50 \\ \hline 36 \end{array} \quad \begin{array}{r} 114 \\ 36 \\ \hline 31 \end{array} \quad \begin{array}{r} 104 \\ 31 \\ \hline 30-29 \end{array} \quad \begin{array}{r} 119 \\ 30-29 \\ \hline 29 \end{array} \quad \begin{array}{r} 110 \\ 29 \\ \hline 16 \end{array} \quad \begin{array}{r} 59 \\ 16 \\ \hline 12 \end{array} \quad \begin{array}{r} 590 \\ 12 \\ \hline 5.62 \end{array} \quad \begin{array}{r} 580 \\ 12 \\ \hline 61 \end{array} \quad \begin{array}{r} 61 \\ 16 \\ \hline 30 \end{array} \quad \begin{array}{r} 126 \\ 30 \\ \hline 38 \end{array} \quad \begin{array}{r} 146 \\ 38 \\ \hline 60 \end{array} \quad \begin{array}{r} 162 \\ 60 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 103 \\ 30 \\ \hline 40 \end{array} \quad \begin{array}{r} 104 \\ 40 \\ \hline 35 \end{array} \quad \begin{array}{r} 105 \\ 35 \\ \hline 32 \end{array} \quad \begin{array}{r} 95 \\ 32 \\ \hline 29-28 \end{array} \quad \begin{array}{r} 115 \\ 29-28 \\ \hline 25 \end{array} \quad \begin{array}{r} 102 \\ 25 \\ \hline 17 \end{array} \quad \begin{array}{r} 66 \\ 17 \\ \hline 12 \end{array} \quad \begin{array}{r} 662 \\ 12 \\ \hline 635 \end{array} \quad \begin{array}{r} 648 \\ 12 \\ \hline 6.8 \end{array} \quad \begin{array}{r} 6.8 \\ 17 \\ \hline 29 \end{array} \quad \begin{array}{r} 125 \\ 29 \\ \hline 35 \end{array} \quad \begin{array}{r} 130 \\ 35 \\ \hline 40 \end{array} \quad \begin{array}{r} 165 \\ 40 \\ \hline 54 \end{array} \quad \begin{array}{r} 165 \\ 54 \\ \hline 54 \end{array}$$

$$\begin{array}{r} 84 \\ 69 \\ 30 \\ \hline 28 \end{array} \quad \begin{array}{r} 75 \\ 28 \\ 32 \\ \hline 26 \end{array} \quad \begin{array}{r} 73 \\ 26 \\ 32 \\ \hline 24 \end{array} \quad \begin{array}{r} 52 \\ 24 \\ 16 \\ \hline 12 \end{array} \quad \begin{array}{r} 42 \\ 12 \\ 16 \\ \hline 12 \end{array} \quad \begin{array}{r} 446 \\ 12 \\ \hline 4.24 \end{array} \quad \begin{array}{r} 4.34 \\ 12 \\ \hline 4.4 \end{array} \quad \begin{array}{r} 4.4 \\ 17 \\ \hline 29 \end{array} \quad \begin{array}{r} 8.9 \\ 29 \\ 32 \\ \hline 38 \end{array} \quad \begin{array}{r} 10.0 \\ 32 \\ 38 \\ \hline 50 \end{array} \quad \begin{array}{r} 10.7 \\ 38 \\ 50 \\ \hline 50 \end{array} \quad \begin{array}{r} 11.8 \\ 50 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 7.4 \\ 50 \\ \hline 29 \end{array} \quad \begin{array}{r} 65 \\ 29 \\ 27 \\ \hline 26.25 \end{array} \quad \begin{array}{r} 40 \\ 27 \\ 26.25 \\ \hline 24 \end{array} \quad \begin{array}{r} 82 \\ 26.25 \\ 24 \\ \hline 19 \end{array} \quad \begin{array}{r} 43 \\ 24 \\ 19 \\ \hline 19 \end{array} \quad \begin{array}{r} 5.0 \\ 19 \\ \hline 19 \end{array} \quad \begin{array}{r} 4.90 \\ 19 \\ \hline 19 \end{array} \quad \begin{array}{r} 4.70 \\ 19 \\ \hline 17 \end{array} \quad \begin{array}{r} 4.64 \\ 17 \\ \hline 17 \end{array} \quad \begin{array}{r} 4.9 \\ 17 \\ \hline 26 \end{array} \quad \begin{array}{r} 8.9 \\ 26 \\ 34 \\ \hline 40 \end{array} \quad \begin{array}{r} 9.3 \\ 34 \\ 40 \\ \hline 40 \end{array} \quad \begin{array}{r} 10.8 \\ 40 \\ 40 \\ \hline 38 \end{array} \quad \begin{array}{r} 10.6 \\ 38 \\ 40 \\ \hline 38 \end{array}$$

Sta	+	$\sum$	-	Elev
8+00		982.59		77.70
+50				77.54
9				77.74
+50				77.94
10				78.14
+50				78.35
T.P	6.48	985.00 984.64	4.07	978.16 978.52
11				78.52
+50				78.72
12				79.17
B.M	5.12	985.86 985.50	4.25	980.75 980.39 980.74 980.38
+50				79.99
+59				80.23
+77		Side Drain HI		

ht

Z

ct

30

$$\frac{7.1}{50} \frac{7.0}{28} \frac{8.6}{27.25} \frac{7.2}{24} \frac{5.4}{17} \frac{5.0}{12} 4.89 \frac{5.03}{12} \frac{5.4}{16} \frac{7.8}{22} \frac{8.4}{34} \frac{9.5}{37} \frac{9.0}{50}$$

$$\frac{7.5}{50} \frac{7.0}{33} \frac{7.4}{27} \frac{7.4}{23} \frac{5.5}{17} \frac{5.17}{12} 5.05 \frac{5.1}{12} \frac{5.4}{16} \frac{8.6}{23} \frac{8.1}{34} \frac{8.6}{37} \frac{8.3}{50}$$

$$\frac{6.8}{50} \frac{6.6}{34} \frac{7.4}{25} \frac{5.0}{17} \frac{4.97}{12} 4.85 \frac{4.97}{12} \frac{5.4}{16} \frac{8.0}{24} \frac{7.7}{34} \frac{8.0}{37} \frac{8.1}{50}$$

$$\frac{6.6}{50} \frac{6.7}{30} \frac{7.0}{24} \frac{5.1}{17} \frac{4.75}{12} 4.65 \frac{4.78}{12} \frac{4.9}{16} \frac{7.7}{23} \frac{7.5}{34} \frac{7.5}{50}$$

$$\frac{6.4}{50} \frac{6.6}{23} \frac{4.7}{17} \frac{4.54}{12} 4.45 \frac{4.55}{12} \frac{4.9}{16} \frac{7.3}{23} \frac{7.2}{34} \frac{7.2}{50}$$

$$\frac{6.1}{50} \frac{6.1}{32} \frac{6.0}{27} \frac{6.7}{24} \frac{4.6}{17} \frac{4.35}{12} 4.24 \frac{4.34}{12} \frac{4.7}{16} \frac{6.9}{23} \frac{7.0}{34} \frac{7.1}{50}$$

$$\frac{7.2}{50} \frac{7.7}{31} \frac{8.4}{25} \frac{8.3}{22} \frac{6.6}{16} \frac{6.58}{12} 6.48 \frac{6.58}{12} \frac{6.7}{16} \frac{8.6}{23} \frac{8.9}{34} \frac{8.7}{50}$$

$$\frac{8.2}{50} \frac{8.0}{34} \frac{8.0}{22} \frac{6.4}{17} \frac{6.38}{12} 6.28 \frac{6.38}{12} \frac{6.4}{16} \frac{7.8}{21} \frac{7.7}{25} \frac{6.7}{32} \frac{6.5}{50}$$

$$\frac{7.3}{50} \frac{6.9}{34} \frac{6.5}{25} \frac{7.6}{22} \frac{6.1}{17} \frac{5.93}{12} 5.83 \frac{5.93}{12} \frac{5.9}{16} \frac{6.9}{21} \frac{7.0}{25} \frac{5.6}{28} \frac{5.5}{32}$$

Top Man Larry Cleveland Sta 13+18.45

$$\frac{6.0}{50} \frac{6.1}{34} \frac{5.2}{31} \frac{6.1}{26} \frac{7.3}{24} \frac{6.9}{22} \frac{6.1}{17} \frac{5.97}{12} 5.87 \frac{5.97}{12} \frac{6.1}{18} \frac{7.3}{20} \frac{6.9}{25} \frac{7.1}{33} \frac{6.7}{38} \frac{5.8}{50}$$

$$\frac{6.0}{50} \frac{5.7}{26} \frac{7.0}{24-23} \frac{6.5}{22} \frac{5.8}{18} \frac{5.91}{13} \frac{5.68}{12} 5.63 \frac{5.80}{12} \frac{5.88}{13} \frac{6.1}{18} \frac{7.1}{22} \frac{6.8}{26} \frac{6.9}{34} \frac{6.8}{50}$$

$$(78.76)_{11V} \frac{7.10}{27}$$

Sta	7	7 86 985 50	-	Elev
12+90		Side Drain Lt		80.58
+97				80.68
13+0745		End Road		80.66
+0845		Edge Pav		80.68
+1845		E Lamp		80.74
		5.12	980.38	980.74
		use	(980.74)	

6.5
50

979.14

L+

2

R+

Inv

672 65 45 48 5.02 5.16 5.47 5.64 65 7.2 7.8
~~74~~ ~~44~~ ~~42~~ ~~36~~ ~~25~~ ~~13~~ ~~13~~ ~~25~~ ~~36~~ ~~40~~ ~~50~~

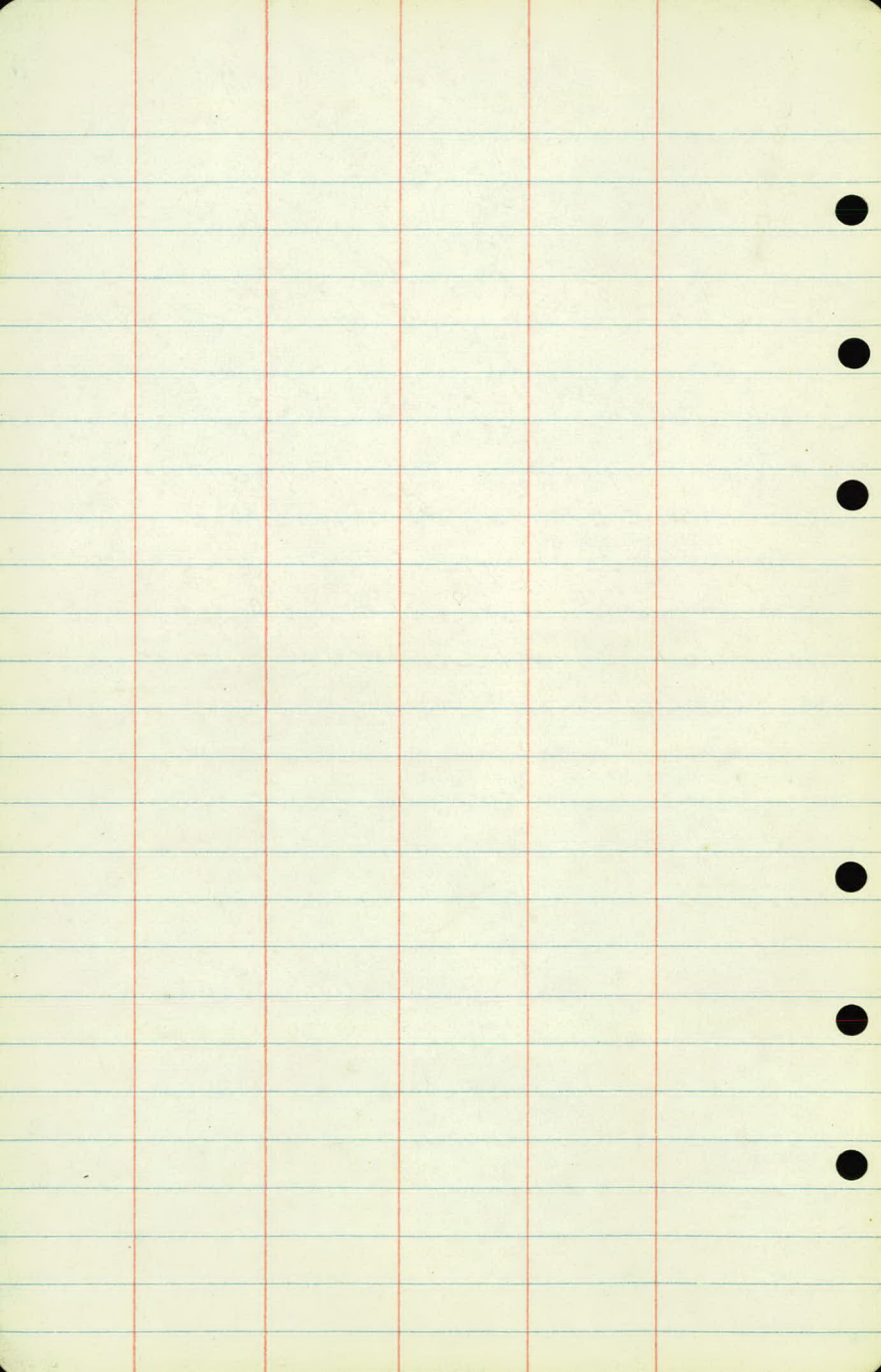
4.4 47 4.64 5.03 5.18 5.40 5.74 6.2 6.4
~~50~~ ~~41~~ ~~3~~ ~~12~~ ~~16~~ ~~31~~ ~~37~~ ~~50~~

4.45 4.80 5.00 6.44
~~62~~ ~~25~~ ~~25~~ ~~62~~

444 5.18 6.36
~~62~~ ~~62~~

4.47 6.00
~~50~~ ~~50~~

Top Mon Larp + Cleveland = 980.74



Profile

Grade Lift Cleveland Ave

8-21-43

37' Top $1\frac{1}{2} : 1$ Slope
per A.D.C.

Sta	+	π	-	Elev
B.M	5.08	908 ⁷⁸ 42		903.34 903.70
123				06.5

+50				06.2
-----	--	--	--	------

124				05.9 37' Top $\frac{1}{2}$ Slopes
-----	--	--	--	--------------------------------------

+50				05.6
-----	--	--	--	------

125				05.1
-----	--	--	--	------

+50				04.7
-----	--	--	--	------

126				04.4
-----	--	--	--	------

+50				04.3
-----	--	--	--	------

127				04.3
-----	--	--	--	------

+50				04.3
-----	--	--	--	------

128				04.3
-----	--	--	--	------

+50				04.2
-----	--	--	--	------

Lt.

L

Rt

SpK in Arc Lt Pole SECOV C² + Clevc.

2.3

2.6

2.9

3.2

3.7

4.1

4.4

4.5

4.5

4.5

4.5

4.6

Sta	+	Δ	-	Elev
-----	---	----------	---	------

908.78 ✓

129				04.2
-----	--	--	--	------

+50				04.3
-----	--	--	--	------

130				04.3
-----	--	--	--	------

+50				04.2
-----	--	--	--	------

131				04.0
-----	--	--	--	------

+50				04.0
-----	--	--	--	------

132				04.0
-----	--	--	--	------

+50				04.1
-----	--	--	--	------

133				04.4
-----	--	--	--	------

+50				04.6
-----	--	--	--	------

134				04.6
-----	--	--	--	------

+50				04.4
-----	--	--	--	------

2

4.6

4.5

4.5

4.6

4.8

4.8

4.8

4.7

4.4

4.2

4.2

4.4

Sta + π - Elev
908 ~~78~~

135 04.3

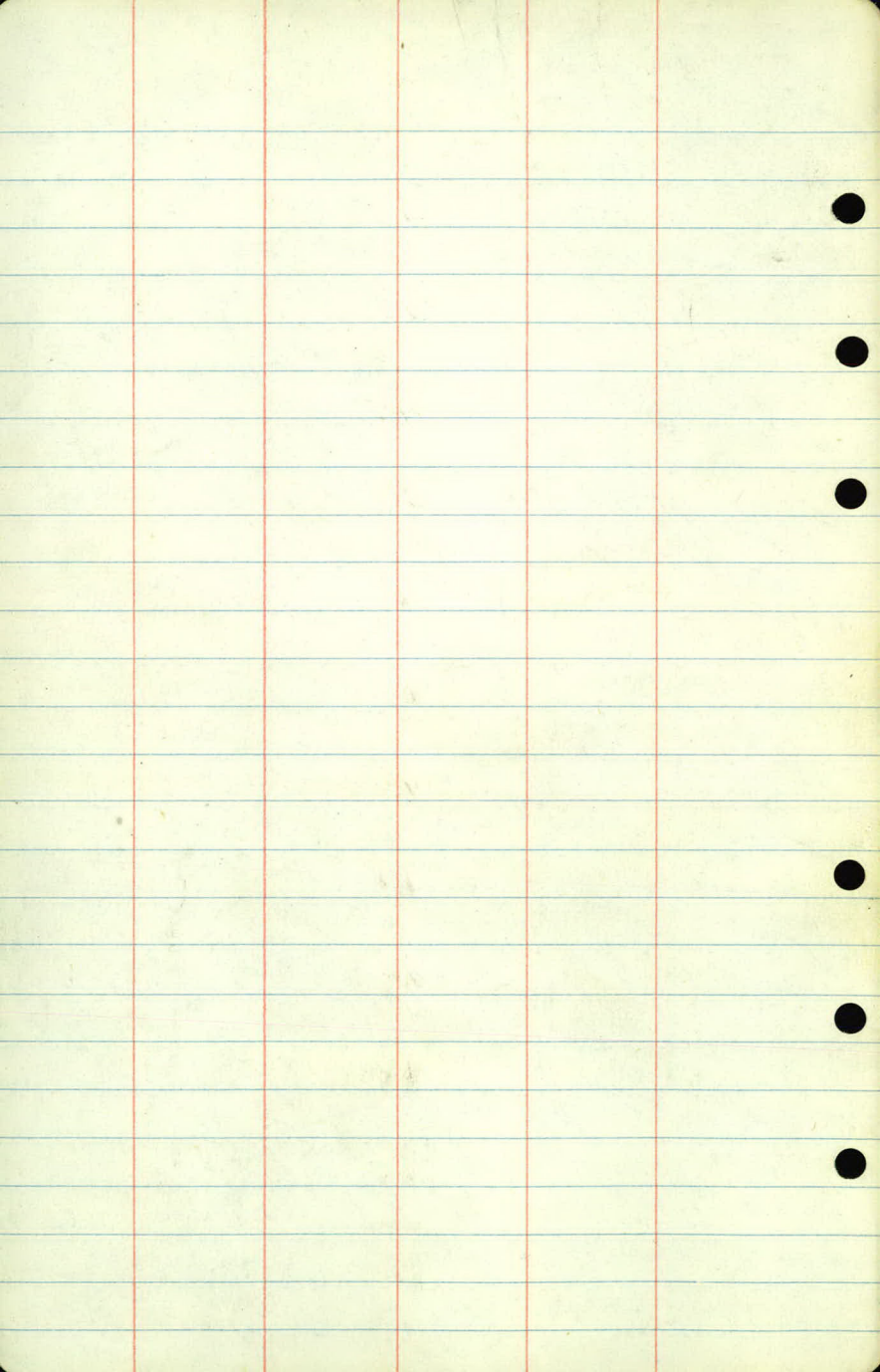
+50 04.3

~~4~~

45

45

45



Alignment
CLEVELAND AVE.

From Harpenteur Ave to Co. Rd. E

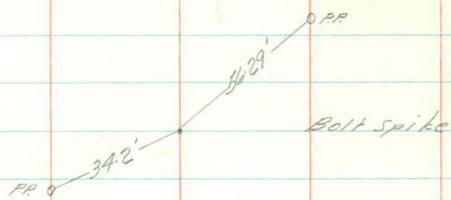
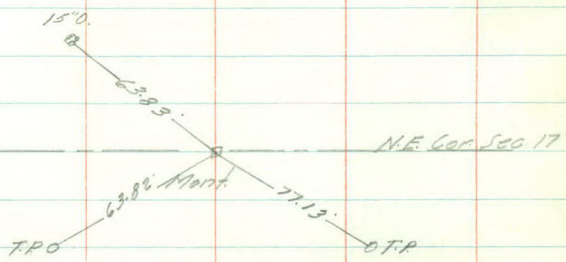
Sta	Point	ΔL	ΔR
-----	-------	------------	------------

52 +58.33	P.I.	0°10'	= & Co. Rd. "B"
-----------	------	-------	-----------------

37 +00.0	P.O.T.		
----------	--------	--	--

26 +33.62	P.I.	0°06'	= & Roselawn Ave.
-----------	------	-------	-------------------

0 +00	= & Carpentier Ave.		
-------	---------------------	--	--



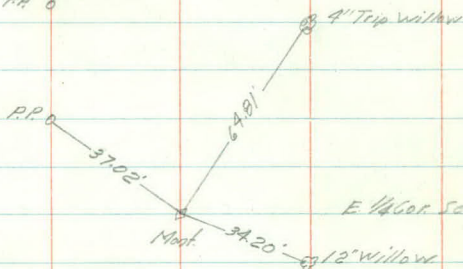
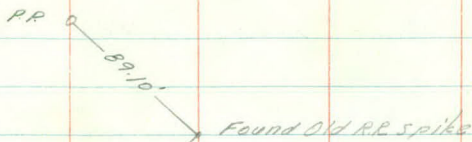
Sta.	Point	ΔL	ΔR
------	-------	------------	------------

88	+85.57	P.O.T.	
----	--------	--------	--

73	+97.90	P.I.	$0^{\circ}34'$
----	--------	------	----------------

66	+76.17	P.O.T. = E.S.T.H. 36	
----	--------	----------------------	--

62	+79.53	P.O.T.	
----	--------	--------	--



E. 1/4 Cor. Sec. 8

Mont.

34.20' 12" Willow



Found Nail & Disc



Sta	Point	ΔL	ΔR
-----	-------	------------	------------

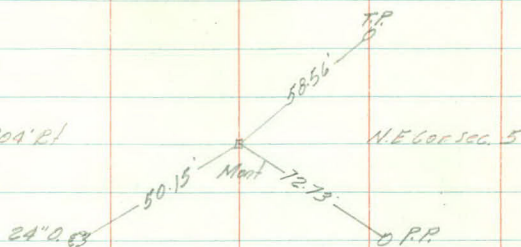
160 +58.18	P.I.		$1^{\circ}04'$
------------	------	--	----------------

131 +51.25	P.O.T.	= & Co. Rd. C"	
------------	--------	----------------	--

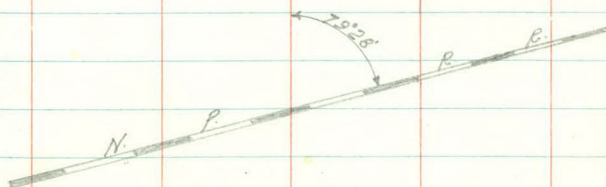
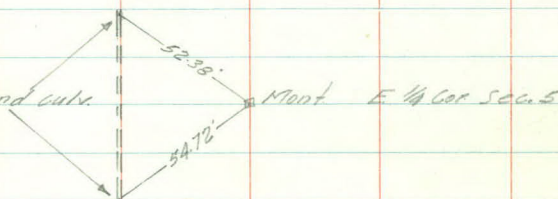
105 +14.14	P.I.	$0^{\circ}20'$	= & Co. Rd. C"
------------	------	----------------	----------------

103 +09.14	P.O.T.	= & R.R. Track	$\Delta 79^{\circ}28' NE$
------------	--------	----------------	---------------------------

160+5818 Δ 1004' R/L



Drill hole at end culv.



ΔR

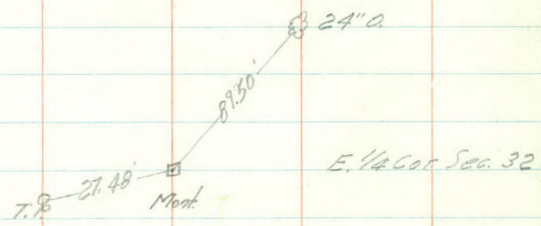
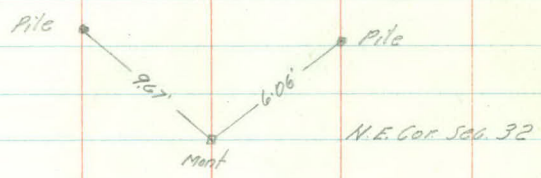
Sta Point ΔL

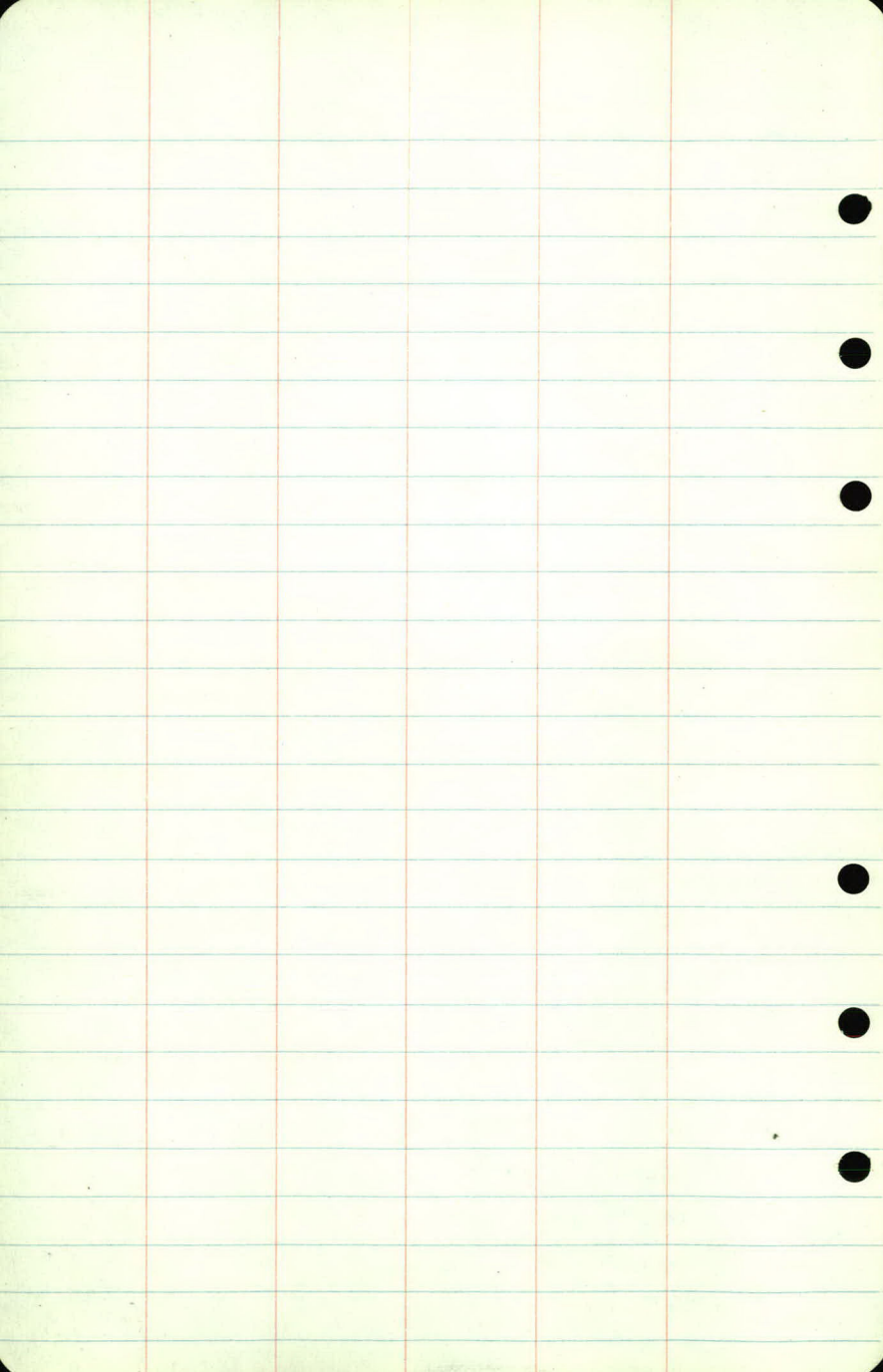
213 +14.75 P.I. 0°47'

186 +72.61 P.I. 0°20'

8-11-41
K.H.
L.C.
A.M.
C.F.
G.H.

Found Iron and assumed it o.k. For line





6

Topography

5 9' 13' Fe-33'

+90-Field Ent.

+73-PP-28'

+88-Rd. Sign-16'

4 Fe-30' 9' 13' Fe-33'

+86-18" Skate Cherry Tr.-30'

+22-PP-28'

3 +10-Fe. Cor.-31'
Fe-31' 10' 13' Fe-33'

+81-36" P.E.-35'

2 Fe-31' 11' 13' Fe-33'

+72-PP-28'

1 Fe-30' 11' 13' Fe-33'

+87-Rd. Sign-18' +58-Rd.-12' 16'-150'

+100-PP-31'

+33-Fe. Cor.-31'

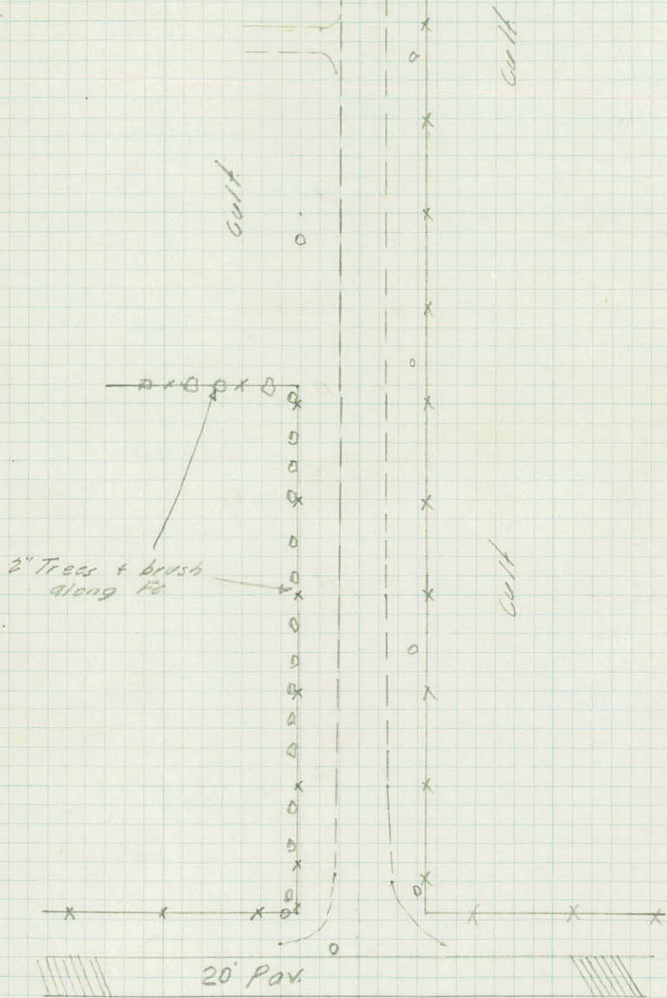
+34-Fe. Cor.-33'

+17-Rd.-40'

+17-Rd.-44'

+15-Tel. M.H.B.S. +10-Edge Pav.

0+00



+45-PP-28'

12

9' 12' Fe-33'

11

9' 13'
+90-PP-28'

+92-PP-36

+99-Cor Parking Area - 24'

10

9' 13'

+47-Cor Parking Area - 29'

+91-End Shrubs - 36'

+37-PP-29'

+54-Fe Cor - 33'

+34-PP-28'

9 Shrubs - 33'

9' 12'

+48-80g. Shrubs + Trees - 36'

+57-Ent - 12' x 17' CM - 26'

+50-Cor Willows - 33'

8

+14-Cor Willows - 33'

+98-Ent + 8' x 12' x 30' CM - 24'

+82-Range tie to ent

8' 12' Fe-33'

+71-PP-28'

+83-Ent Shrubs + Trees - 31'

+57-End Fe - 32' + 80g. Shrubs
+ Trees

7

8' 12'

6

Fe-31'

9' 13' Fe-33'

+21-PP-28'

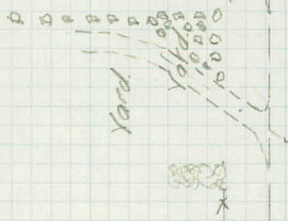
Green Ho.

Cult

Cult

Yard

Cult



+11-6" Pop-32'

+50-Fe Cor-33'

19

9' 11'

+79-15" Trip O-27'

+66-6" O-29'

+52-PP-28'

+49-15" O-30'

+19-15" O-29'

18 Fe-33'

10' 10' Fe-33'

+85-6" O-31'

+67-8" O-32'

+45-4" Water ^{M 95} 19015-45

+26-15" O-31'

+19-6" O-31'

+13-8" O-31'

17

10' 11' +06-PP-28'

+49-3" Water Pipe x 94 +49-5" Gate Valve-33'

+68-6" Cor. Box, S.F. Cor.-37'

+54-6" O-34'

16

Fe-33'

10' 12'

Fe-33'

+56-PP-28'

15

10' 12'

14

9'

+02-PP-28'

Fe Cor-33'

+85-Fe Cor-33'

+50-Telc. M.H. 1116'

+17-8" Fe-33'

+13-1" Edge. 48'

13

9' 12'

U of M.
Golf Course

x 4" water main

Postage

+83-X Drive 24"X70 CM 42 30.5
 +69-P+TP-27 +83-G.R.-20' 178-TP-28'
 +63-St Sign-39 +80-Road-10' +82-End -13'
 +51-M.H.-Tele-10' 148-End Cable G.R.-61'
 +98-End Cable G.R.-61' 143-End-54' 144-Road-50'
 +12-G.R.-43' End G.R.-91' 121-Road-50'
 +12-Beg Cable G.R.-55 120-50' 102-Pc Cor -23'
 26 PP-24 G.R.-22' 20' 22' 149-PP-28
 +95-Con Swamp-36 +90-11' 14'
 +92-End Cable G.R.-20.6'
 +45-Beg. G.R.-20.6'

25 Swamp-47 11' 13' Pathside -33

+63-24"X48 CM X Drive 2121'
 150-Swamp-50 151-PP-29'
 +25-Swamp-30
 24 Conduit-38' 12' 12' Pathside-23' Pc-33'
 +91-Pc Cor-23' 193-Pathside-33'
 +80-M. Con. Radio Tower-95' 167-Conduit-33'
 +53-PP-25' 158-Gate

23 11' 12' +01-PP-38'

22 Pc-33 11' 12' Pc-33'

+52-PP-28

+25-18'6" Ht-30'

21 24'6" Ht-30' 10' 11'

+60-Path through Pc Gate.

+01-Tele M.H.-12'
 20 Ht-18'6"-29' 9 11 106 PP-28
 Pc-33' 12-33'

No Cable on Road.

Black

Top

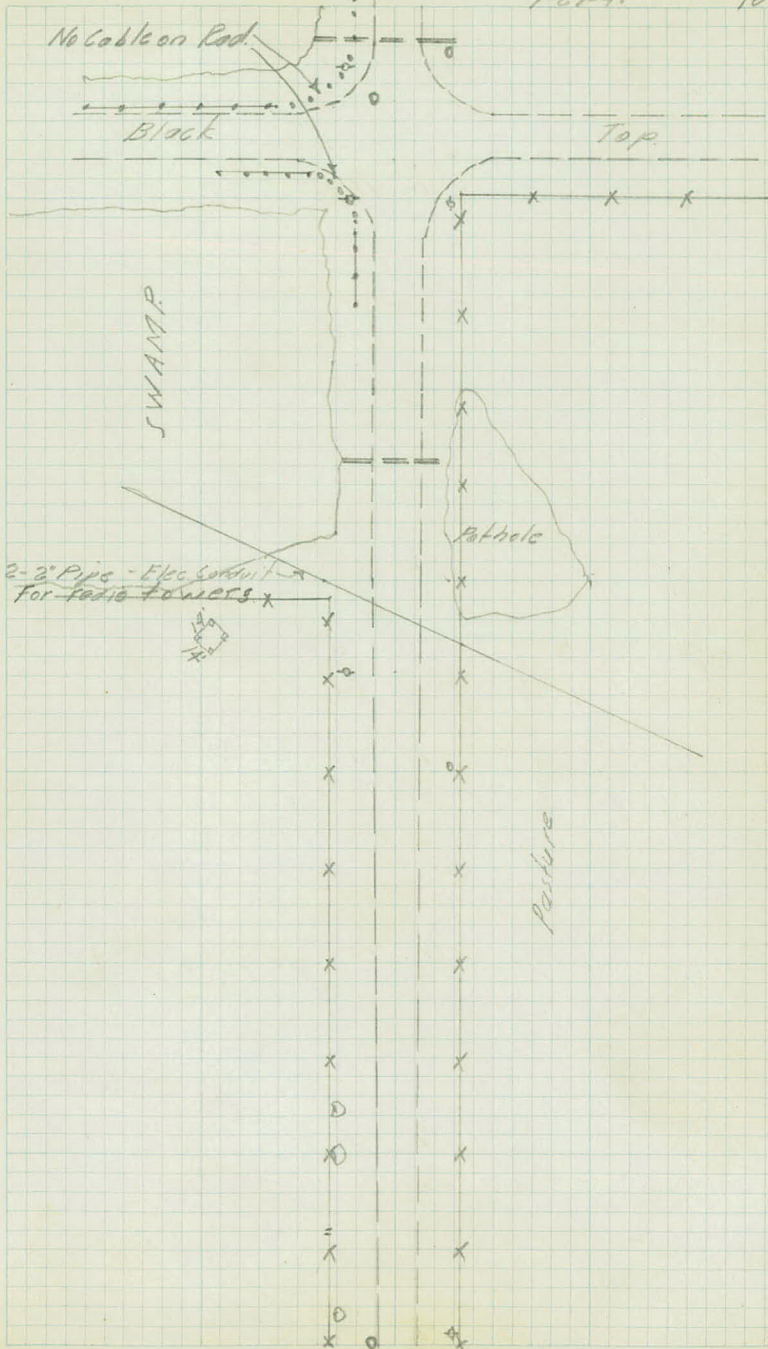
SWAMP

2-2" Pipe - Elec Conduit
for radio towers

1/2" x 1/2"

Bathole

Pasture



+54-P.P.-28

+53-Hedge-34

33

9' 12'

+20-P.P.-31

+36-Ent 15'x20' G.M.-26

+24-Hedge-37

+20-Cor Nursery-49

32

9' 12'

+82-78' M.R.-28

+24-Ent 15'x20' G.M.-20

31

9' 12'

~~+54-Ent~~

+10-T.P.P.-28

30

+40-Cor Nursery-50

+32-6' B.E.-39

+15-6'x5'x5' Rock-31 = 7

Moved to 45° Par. of Lot

9' 12'

+84-R.D. Sign-30

29

+94-Ent G.E.-19

9' 12'

+12-Ent 15'x24' G.M.-26

+93-18' Elm-50

+91-8'x10' Wide Hedge-50

+93-15' Elm-50

+60-Ent Hedge-41-50

+31-T.P.P.-

+21-Cor Swamp-37

28

G.R. 19

9' 12'

+39-18' Elm-52

+21-15' Elm-52

+19-Cor Hg-73

+65-Cor Hedge-44-50

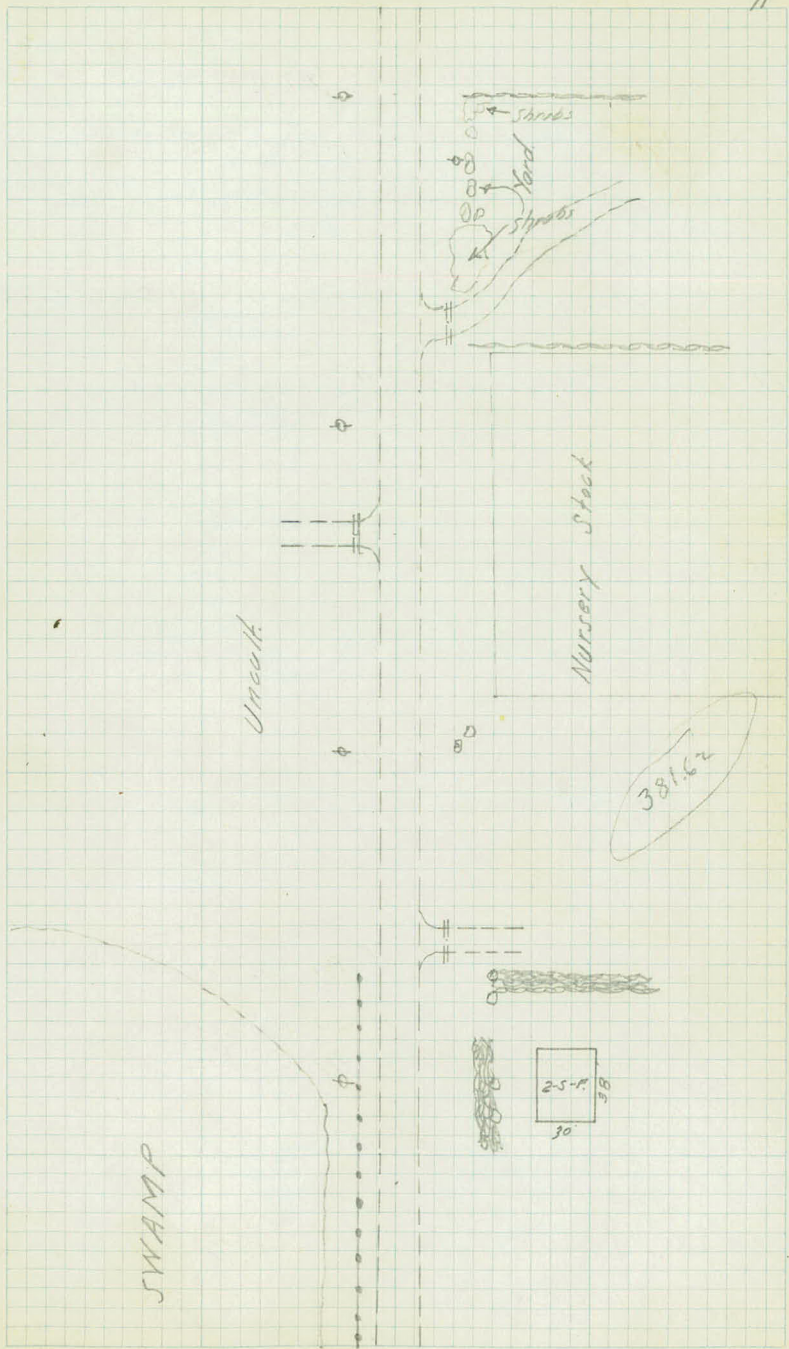
+85-Ridge to C to Swamp

+103-Beg Cable G.R.

27

Swamp-57

10' 13'



+98-Ent-15'X30'CM-25'
+94-PP-41'
+74-4' Elm-40'

+47-4' Elm-40'
+28-3' Elm-40'
+25-Cor Ho-74'
+06-2' Elm-40'

40 +90-PP-25'

9 12' +97-Row Raspberries Bushes-31'

39

9' 11'

+86-6' BE-41'

+35-PP-28'

+30-Ent-12'X20'CM-20'
+19-12' BE-40'

38

10' 11'

+59-15'X20'CM
23'

+66-Ent-12'X20'CM-22'
+57-Cor Flower Garden-36'
+52-15' CM-29'-65'
+50-PP-29'

37

10' 10'

+79-PP-28'

+89-Cor Flower Garden-39'
+79-6' Elm-43'
+64-18' Elm-57'
+40-18' PP-56'
+30-Ent-12'X18'CM-24'
+15-12-33'
+06-Willow Bush-33'

36

10' 11'

+97-Ent-12'X20'CM-22'

+89-Shrub-36'
+81-Shrub-36'
+72-Shrub-35'

+46-Cor Ho-108'
+97-Ent-15'X20'CM-24'
+25-PP-28'

35

9' 11'

+95-Ent-12'X18'CM-22'
+85-PP-30'
+78-Willow Bush-35' Cor Ho-81'

+51-8' PP-22'
+43-Ent-12'X2' CM-22'
+33-15' PP-35'

34

+14-Ent-15'X20'CM
24'

9' 11'

Uncult.

82
1-5-54
20

1-5-54
36
50

old

cult

Gardens
Orchard.

Shrubs

1-5F
34
24

Buried

197-Range tie to Fe.

162-PP-28

136-Ent.
125-Ent. Hedge-33

47

10' 12'

150 Cor. Swamp-29'

149-PP-32: Bog Hedge-32'

107-PP-28

46 Swamp-29

11' 12'

45 Swamp-29

12' 12'

180 & Road.

154-PP-28

155-Fe Cor-29: Embankment-31'

44 Swamp-29

12' 13'

Fe-30 Low land-32'

43 Swamp-35 PP 28' 11' 11' Fe-29 Low land-30

Feo Swamp 7 8"
160-Ent. Tile Drain-45

127-Feo 8" Drain Tile-13

42

11' 11'

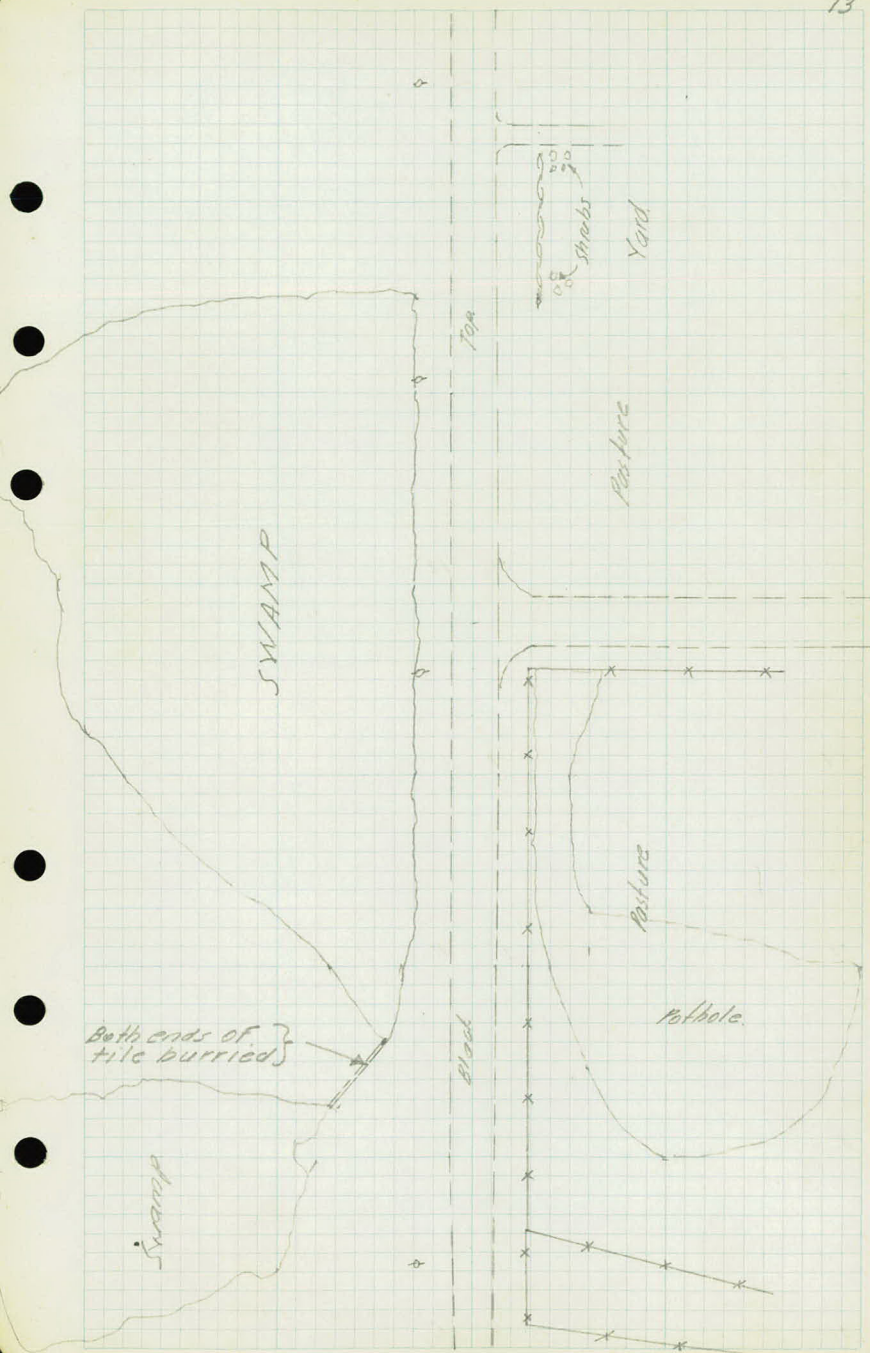
149-Range tie
162-Fe Cor-29

143-PP-28

113-Range tie
111-Fe Cor-29

41

9' 11'



144-PP-28'

+25-Rinditch

54 Fe-33

11' 12'

53
+91-Fe Cor-34'
+88-PP-28'

+10-Rd-10' +20-Rd-13'

+71-Rd-50' 62'

+45-Rd-57' 65'

+22-PP-28'

52

9' 14'-Rd

~~+71-PP-28'~~

51

+2-Fe Cor-38'
9' 12'

+71-PP-28'

50
~~+6-PP-28'~~

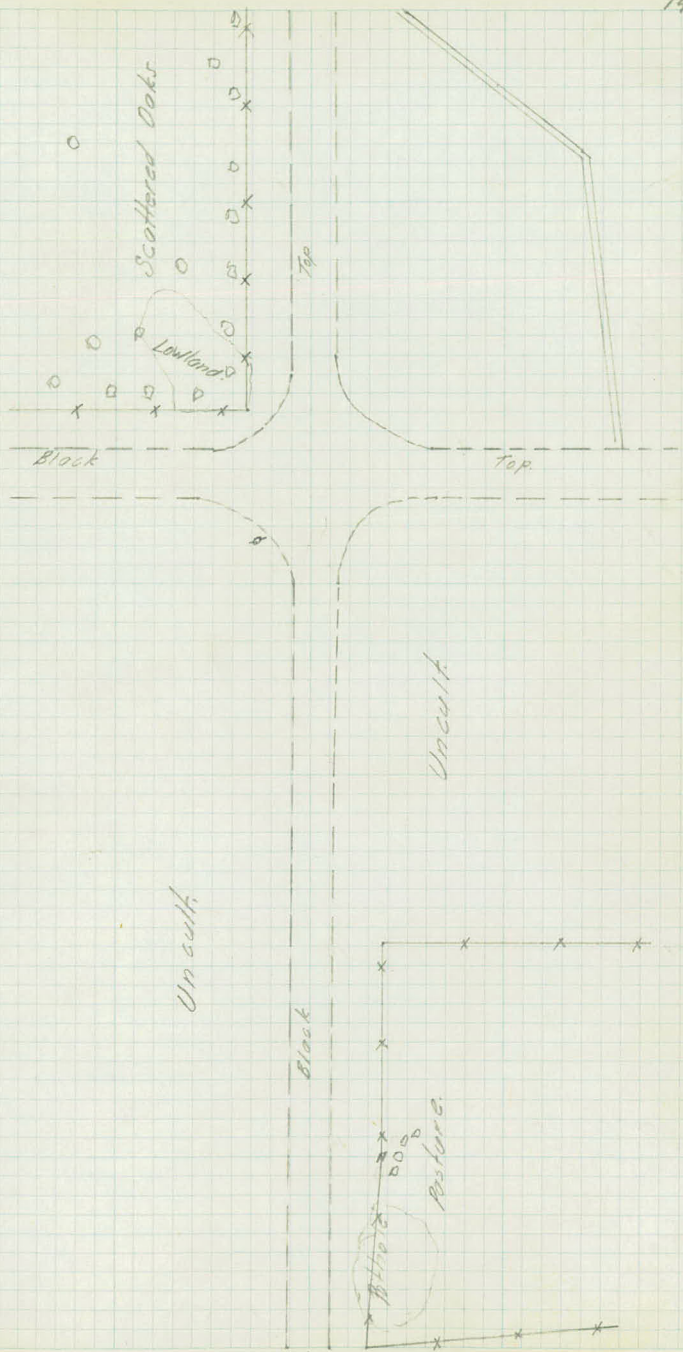
+12-Fe Cor-38'
~~+7-Rd-28'~~
10' 12'

49
+16-PP-28'

+17-Rd-30'
10' 11' step Fe-30'

48

+01-Fe Cor-30'
11' 11'



61 +98-Δ in ditch-65' 11' 11'

+77-T. + P.P.-29'

+73-Δ in ditch-40'

+59-XD.M. 24' X 68' C.M. 34' 34.5'

+46-Range tie to ditch

+89-Δ in ditch-36'

60 Lowland to FC-34 12' 11'

+20-P + T.P.-28'

+37-Rd Sign-20'

59 Lowland to FC-24 11' 11'

+30-Lowland-34'

58 FC-34 12' 11'

+61-PP-28'

57 FC-34 12' 11'

+65-PP-28'

56 FC-34 11' 12'

+91-End 24' C.M.-27' →
to Lowland

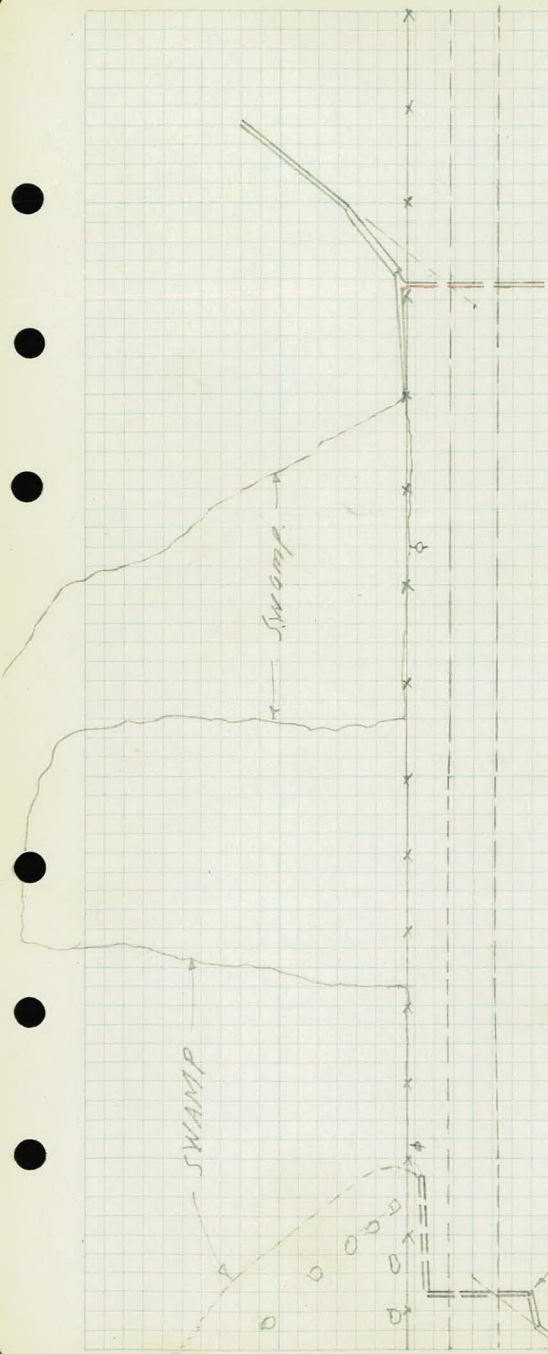
+54-Rd Sign-22'

+39-Range tie to ditch

+29-End 24' C.M.-29'

+13-Δ in ditch-52'

55 11' 12'



Uncult.

Uncult.

See Plan of pitch
for cult. layout & ditch

+97-P.P.-28'

+35-Pothole-44'

68

14' 12'

+34-End-15'
+32-End 490-22-P.P.-28'

~~+35-Pothole-44'~~
+36-End-14'
+30-End 24" Conc. Cul-48'

67

+93-End-60' 55'

+60-End-55' 60'

End. 15 Reg. Runkelle. +22-End-14'

+48-End 12" C.M.-34' for Spillway
+41-End 24" Conc.-48'
+20-End-15'
+23-End 150-21'

66

13' 14'

+78-Fc. Cor-34'
+71-End-15' X 20" C.M.-26'
+63-P.P.-28'

65

10' 12'

64

Fc-33'

12' 10'

+40-End-15' X 24" C.M.-24'

+99-T.P.P.-29'

+98-2" Pipe-91'
+87-2" Pipe-40'

63

12' 12'

+93-Cor 540-65-34'

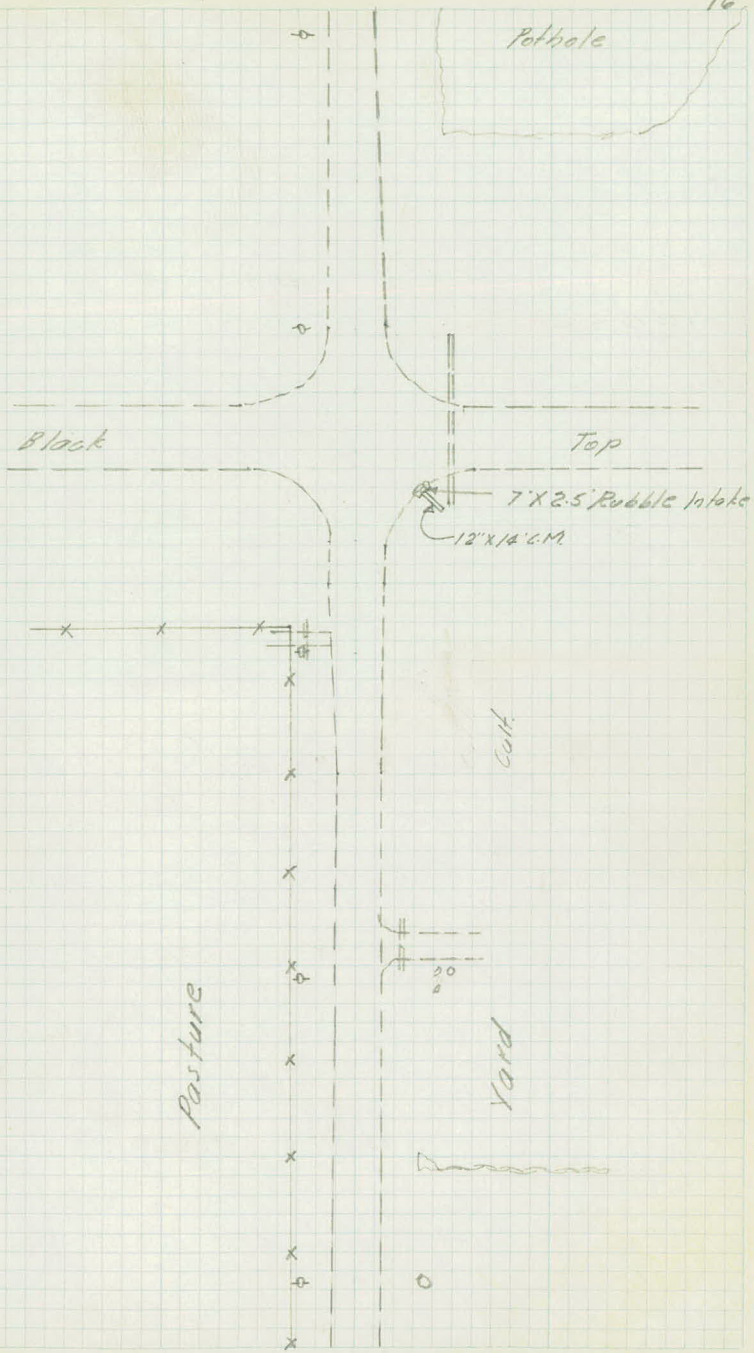
+34-T.P.P.-29'

+35-8" Pipe-34'

62

Fc-33'

12' 12'



+79-12" O-41'
 +50-24" O-36
 +39-18" O-49'
 +06-30" O-35'
 75 Swamp-50'

+85-End 15' C. M-22'
 +70-End
 +69-Fe Cor-33'
 +56-End
 +47-End 15' C. M-21'

12' 10' +17-End Fe-40'
 Fe-41'

+67-PP-28
 +52-15" O-44'
 +47-15" Tw O-44'
 +32-15" O-40'
 +26-15" O-40'

74 Swamp-51
 +87-18" O-37'

12' 11' Fe-42'

+42-18" O-41
 +07-End Sign-26'
 +05-PP-29
 73 Brush-30

12' 11'

+35-Reg Fe-43'

72 12' 10'

+72-24" O-40'

+96-PP-29'
 +26-24" O-35'
 +13-End-15' 20' C. 19-22'
 +04-8" O-45'

71 12' 10'

70 Brush-30'
 +97-PP-28

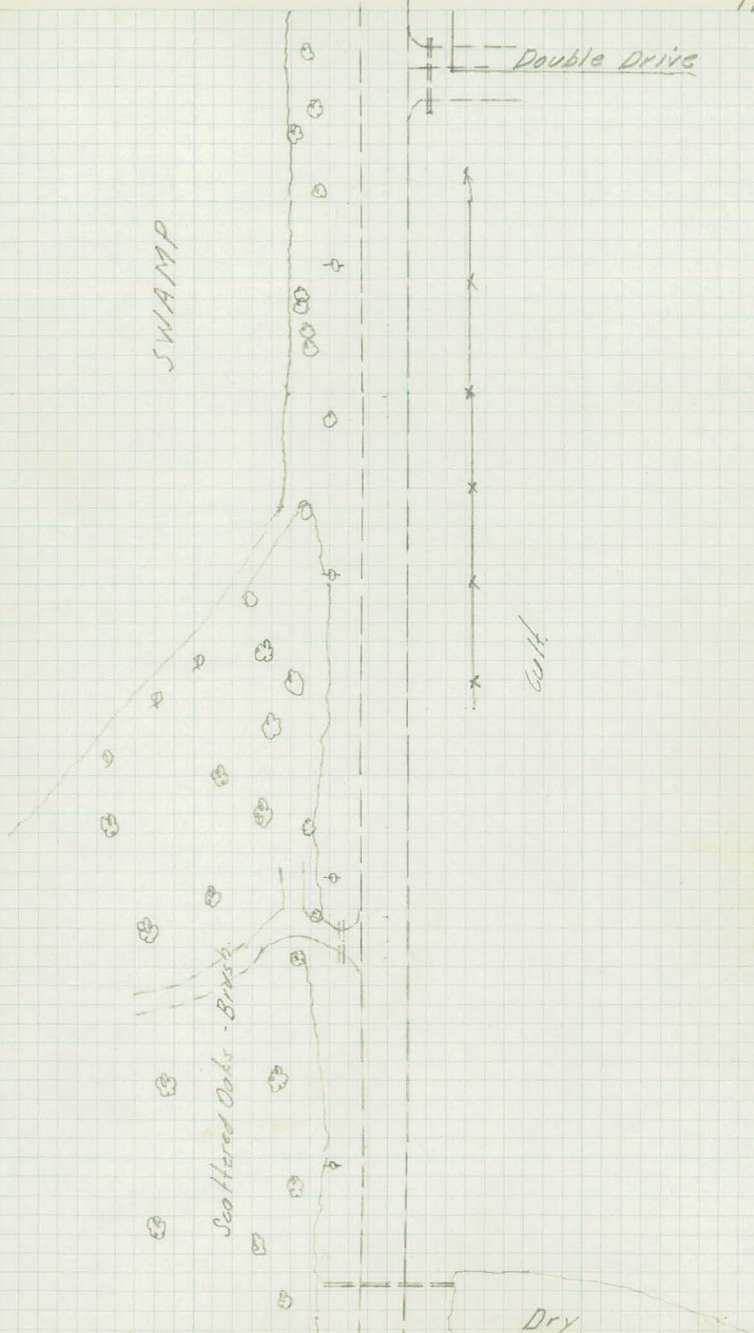
12' 10'

+33-X Drive 24" X 67' 214

32' 35' +40-Post hole-35'

69 +15-Reg Brush-8" O-37'

14' 9'



+41-Ent-15'x20'CM-24'

+50-FC-65'

+23-PP-27'

82

9' 11' FC-48'

+90-Swamp-50

+55-Δ₁₀ FC-33'

81 Swamp-41'

10' 10' FC-33'

+72-PP-28'

80 Swamp-35

11' 12' FC-33'

+55-5 Trip. Willow-29'

+22-PP-29'

+12-Pitch-39'

79

Swamp-40'

12' 11'

Willows

+90-12' Willow-33'
+81-FC Cor-34'

78 Swamp-33'

13' 11' FC-32'

+69-PP-29'

+62-XD1015-24'x62'CM

31' 31'

77

FC-32'

12' 10'

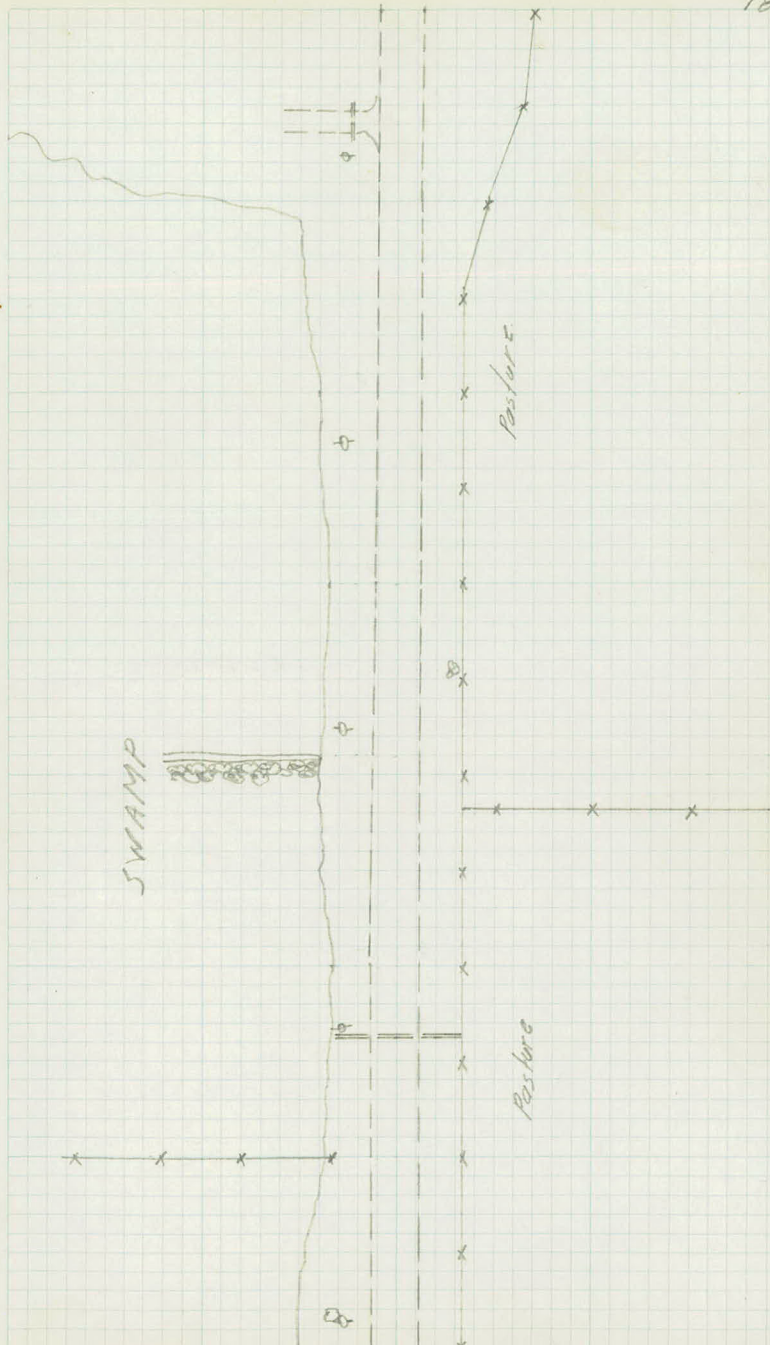
FC-33'

+19-30' O-33'

+14-PP-28'

76 Swamp-51'

13' 11'



178-Tele. Mt. H. - 9.
170-T. & P.R. - 28.

89

8' 14'

120-PP-28

88

9' 13'

132-6" Tric. E/W - 36'
130-Row Apple Trees - 40'
120-Ent. - 12" X 16' C.M. - 24'
114-Row Apple trees - 54'

87

9' 12'

172-PP-28

190-800 Lillies - 31'-38'
189-18' Tric. 35'
173-Ent. - 12" X 32' C.M. - 22'
158-Fc Cor. - 35'

86

9' 12'

166-Fc Cor. - 40'
162-PP-29
162-Long Tric to Fc

121-PP-28

85

9' 12'

84

9' 12'

171-PP-29

188-Fc Cor - 57'

133-Fc Cor - 67'

83

9' 12' Fc - 70'

Cult

Cult

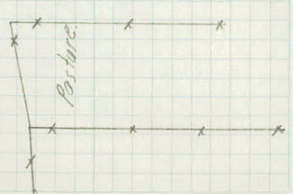
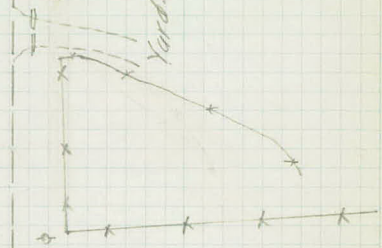
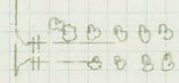
Yard

Cult

Yard

Cult

Pasture



199-30"E/m-17

149-12'0-34'

124-24"E/m-15'

96

8' 13' 110-12'0-34'
Fe-34'

180-PP-28'

95

8' 14' 108-Fe Cor-34'

196-12" R.E-38'
178-30" O-38'

132-PP-28'

165-24'0-36'
138-24'0-37'

94

8' 14' 110-18'0-39'
Fe-32'

181-24'0-39'
176-Fe Cor-32' 5"
174-Range Tie
160-24'0-38'
150-24'0-38'

93

7' 14' 113-Ent-12'42.8 CM
2.3'
109-15" Mon/G-44'

180-PP-27'

181-Cor-Base-34'
168-Cor Range Berms-34'

92

7' 14' 191-HI-Line 15.5

158-Brea. Pipe-24'
150-Brea. Pipe-26'

162-5m P
150-Brea.ther Pipe-33'

121-PP-27'

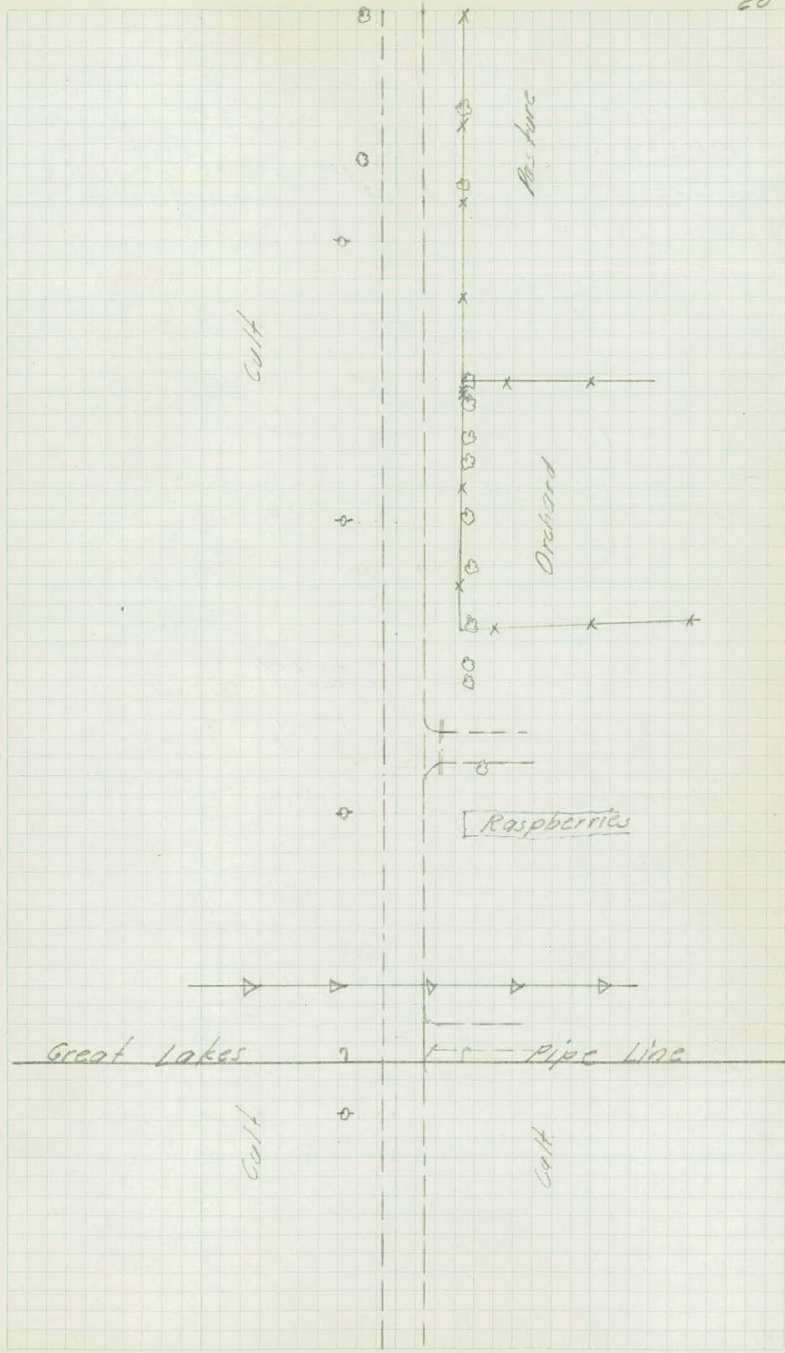
91

7' 15'

145-4" Pipe-35'

90

7' 15' 143-4" Pipe-30'



+16-15°O-36'
+62-PP-28'
+50-FC-30'
+43-Ent

+22-Xing Siso-19'

103

11'

+27-Ent 15° V.f. - 26'
+03-Ent 15° V.f. Culv - 28'

+56-PP-28'
+54-FC-40'
+45-Ent Siso-19'

+96-Xing Siso-18'
+65-FC Cor 45'

102

11'

10'

FC-39'

+93-6° Elm-36'
+72-10° Elm-39'
+61-6° Tw Elm-36'

+30-PP-28'

+31-FC-45'

101

10'

12'

FC-44'

+97-Ent 15° X20° M-26'

+77-N.E Cor Ho - 73'

+57-Ent
+45-24° O. + FC-37'

+32-24° O - 34'

100

9'

12'

FC-33'

+89-15° Elm-19.5'
+80-PP-28'
+75-30° Elm-20'

+31-N.E Cor Ho - 58'
+26-30° Elm-20'

99

9'

12'

FC-34'

+96-24° O-20'
+76-1° Pns-34' +79-1° Pns-29'
Found Black 1' (Holes)
+69-6° Tw Elm-26' N
+63-5° A-12° X20° M-24'
+53-24° O-31'
+45-PP-28'

98

9'

12'

FC-33'

+75-18° Elm-19' = Lt side

+59-10° Tw R.E-36'

+44-24° Elm-19'

+27-12° Elm-18'

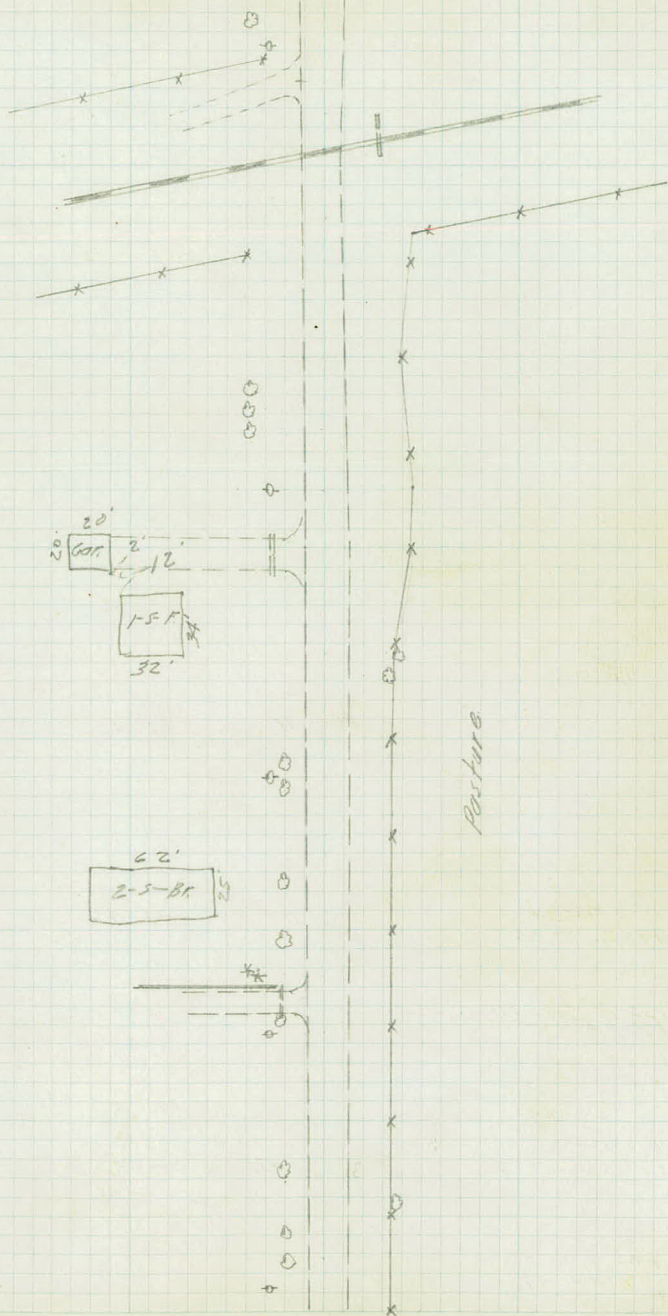
+12-PP-28'

97

7'

13'

FC-34'



110 FC-33 9' 11' FC-59

109 +18 Rod Sign-16' FC-33 9' 11' FC-54 Lowland 75

108 FC-33 10' 11' FC-51 Lowland-33

107 +05-Dir FC-38 FC-32 10' 11' FC-50

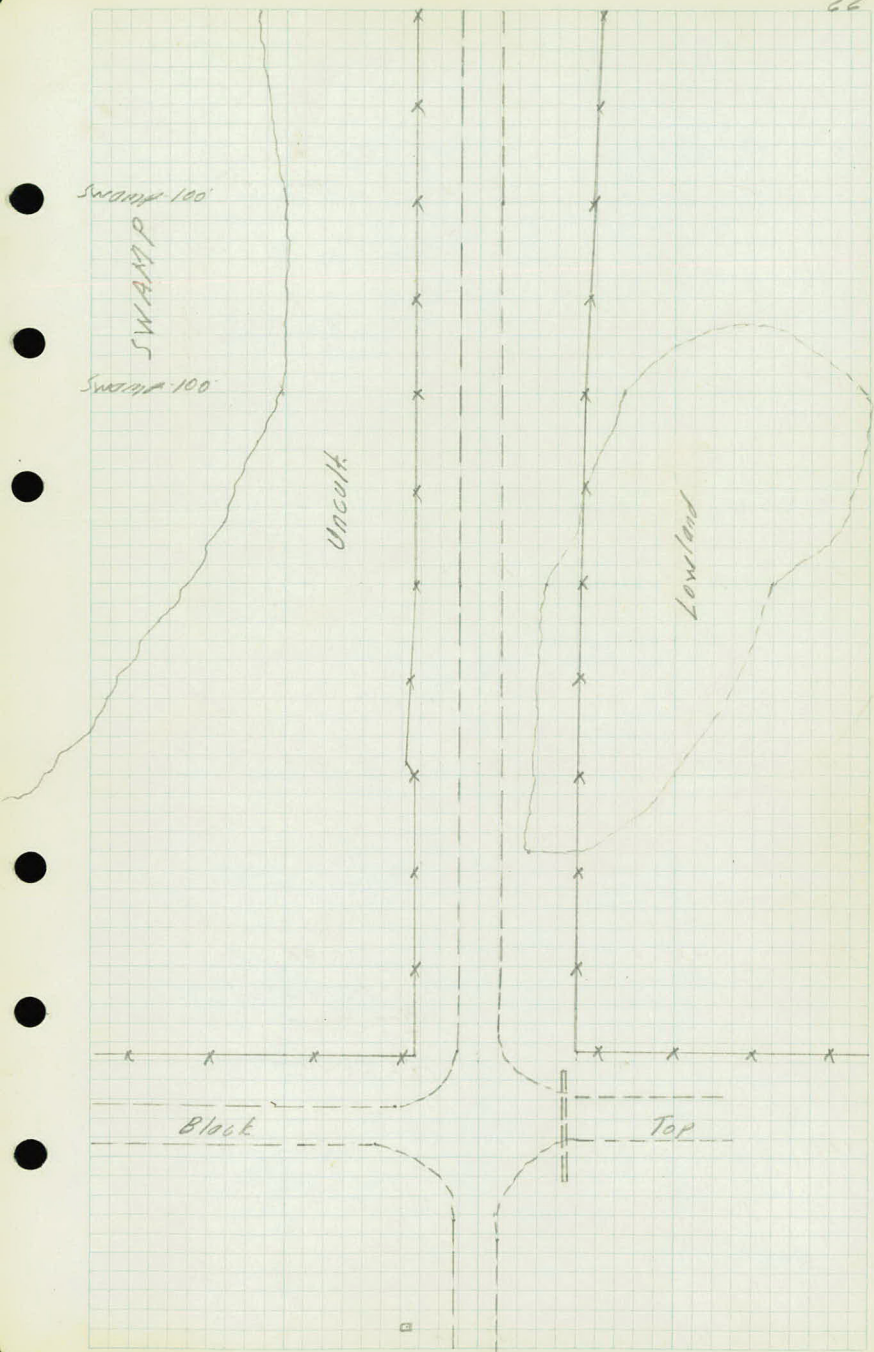
+00-Rod Lowland-24

106 FC-33 10' 11' FC-49
+90-G.P.-26
+55-Rod-10
+55-St Sign-26
+53-FC Cor-50
+45-Rod 18' CM-43
+41-RP-40
+32-Rod-50

+55-FC Cor-33 +55-Rod-11
+40-RP-28 +28-Rod-44
+07-Rod-53 +03-Rod-50

105
+77-RP-28
+72-Rod Sign-22
+67-Rod-12
+90-RP-30
+87-12' CM-44
+57-Rod-11

4' x 5' T 1/2 Box
+11-Pump-37
104 Shp-28 12' 10'



117 Fe-31' 9' 11' Fe-58'
+98-5" Pop-46'

+30-4" Pop-37'

116 Fe-29' Swamp 132' 9' 10' +03-Fe Cor-54'

+30-Swamp-35

115 Fe-30 9' 11' Fe-

+95-Low land-33'

+26-X Drain-24" X 42 CM 29' 15"

114 Fe-53' 8' 11' Low land-31' Fe-49'

113 Fe-33' 9' 11' Fe-49'

+80-Bog Low land-34'

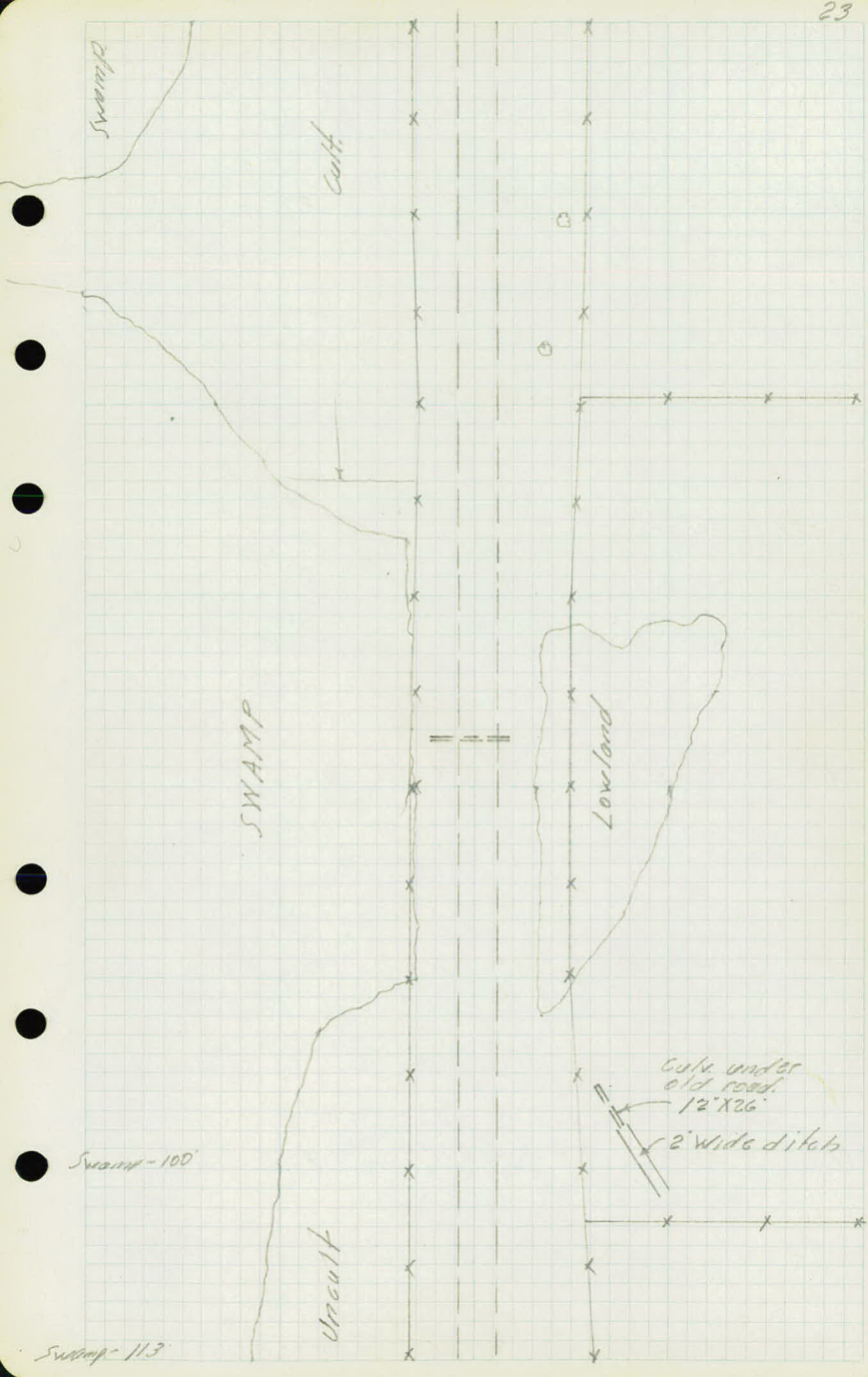
+42-Env 12' Vit Gully-63'

+23-Env 12' Vit Gully-76'

112 Fe-33 9' 10' Fe-55'

+72-Fe Gully-58'

111 Fe-33 9' 11' Fe-63'



Conc. Hwe-116
 +92-End 21 Vit. Cable-33'
 +88-Fc Cor-35' N
 +8-Range fig

+25-Ent-

124 Fc-35' 10' 11' Fc-57'

+59-Fc Cor-64' N
 +54-Range fig

123 Fc-36' 9' 10' Fc-62'

+40-Range fig 2
 +37-Fc Cor-34' 2

122 Fc-33' 10' 10' Fc-56'

+81-Tele. Cable Marker-32'
 Cable-20'E. of Marker

+54-Beg. 21 Vit. Cable-115'

121 Fc-33' 10' 10' Fc-50'

120 Fc-32' 9' 10' Fc-50'

119 Fc-32' Swamp-130 9' 10' Fc-51'

118 Fc-31' Swamp-145 9' 10' +88-4" Rd-25'
 Fc-57

Culv. Burned

Culv. Burned

pasture

~~5/4 mp. Pitch~~

~~11/24/18~~

60/4

172-End 24" Cor. Culv-47'
161-End-32' 31'

24" X 48" Cor. Culv.

125-End 24" Cor.-47' 138-End-34' 28'
125-Cor Swamp-20' 125-Bog Bl. Top 125-Cor Swamp-23'
117-Fe Cor.-34'

131 Swamp-20' 11' 12' Swamp-22'

130 Swamp-19' 12' 12' Swamp-20' Fe-

129 Swamp-18' 11' 13' Swamp-24' Fe-31'

128 Swamp-20' 11' 12' Swamp-25' Fe-33'

160-End Bl. Top.

127 Swamp-21' 11' 10' Swamp-25' Fe-34'

130 X Drains 24" 150 G.M. 26' 25'

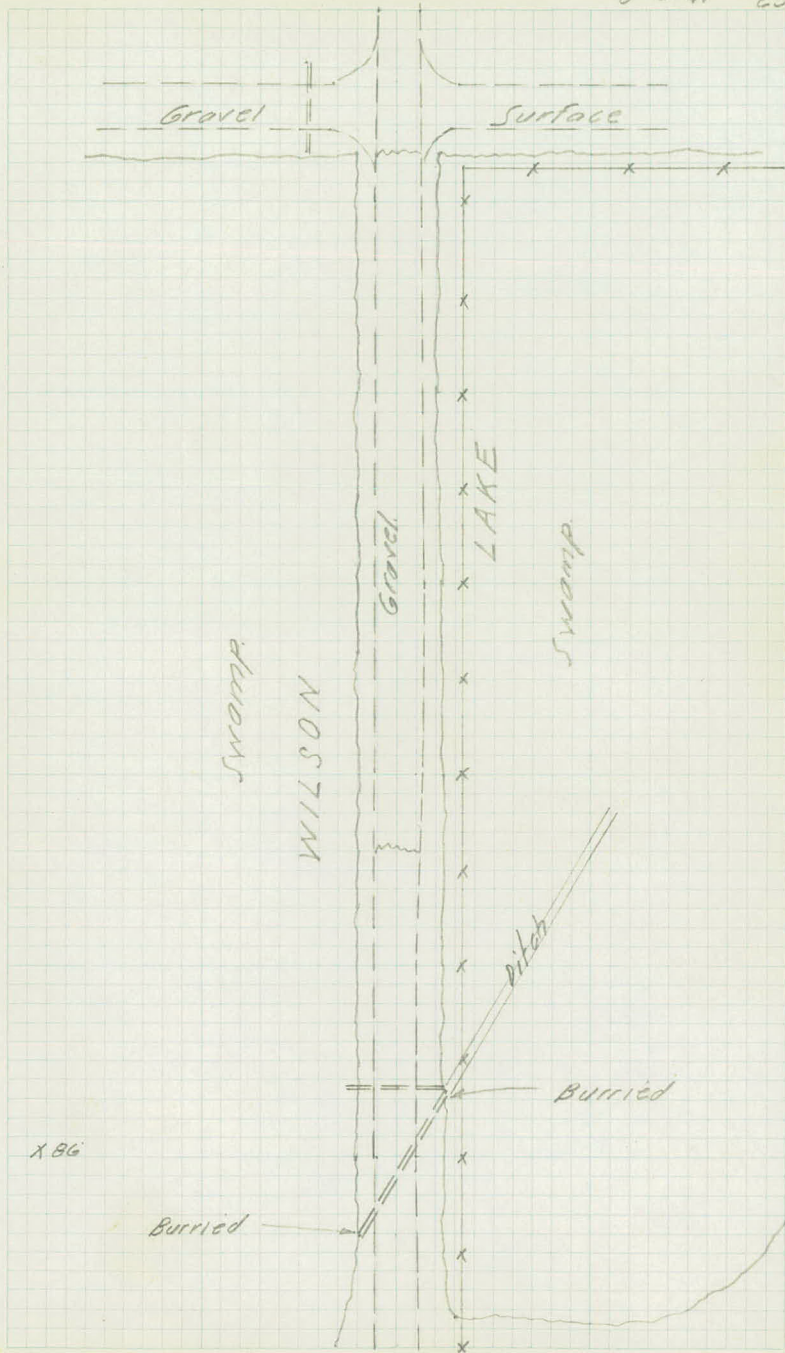
133-End X Drains-26'

126 Swamp-20' 10' 10' Swamp-28' Fe-33'

159-End X Drains-19'

125

11' 11' 115-Bog Swamp-30'
Fe-34'



+80-Fc-33'

138 9' 11'

+96-Telc Conduit Marker-31

+46-PP-27'

137 9' 11'

136 9' 11' Swamp-95

+60-PP-26'

148-Ent-LSA 20' G.M.A.
22'

+25-Swamp-85

135 9' 11'

134 9' 11'

133 9' 11'

132 9' 11'

x x x x

Uncont

Uncont

8



8

Swamp

Uncont

Uncont

+83-PP-28'
+91-6" Elm - 41'
+11-Ent - 15'x20' C.M. - 21'

145 FC-33' 11' 10'

+59-6" Chin. Elm - 41'
+50-PP-28'

+36-Ent - 15'

144 +16-Ent - 15'x20' C.M. - 21' 10' 11'
FC-33'

+17-Pine 2" - 38'

+30-SW Cor Ho - 33'

+16-2" Pine - 33'

+64-Ent - 15'x20' C.M. - 22'

+60-FC Cor - 33'

+12-Ent - 15'x20' C.M. - 22'

+29-4" Mt Ash - 40'

+26-N.E. Cor Ho - 100'

+21-Long C Tie

143 Mt Ash - 37' 10' 11'

+09-PP-23'

+69-Tree - 37'

+64-Beg Steel FC-33'

+12-Cross Pol - 51' Vent

+09-S.E. Cor Ho - 98'

142 +90-Ent - 15'x20' C.M. - 21' 9' 11'

+41-Ent - 15'x20' C.M. - 24'

+14-SW Cor Ho - 84'

+08-Chin Elm - 42'

+05-Shrub - 35'

+90-Ent - 10'x16' C.M. - 24' Burned

+72-PP-28'

+58-2" " " - 51'

+43-2" Chin Elm - 41'

+37-S.E. Cor Ho - 92'

+20-FC - 30' 15'x20' C.M.

+10-Ent - 21'

141 9' 11'

Chin. Elm - 43'

+73-S Chin Elm - 42'

+64-4" Chin Elm - 42'

+55-SW Cor Ho - 87'

+52-PP-28'

+23-Long Ho

+10-2-Ent - 60'

140 FC-33' 10' 11'

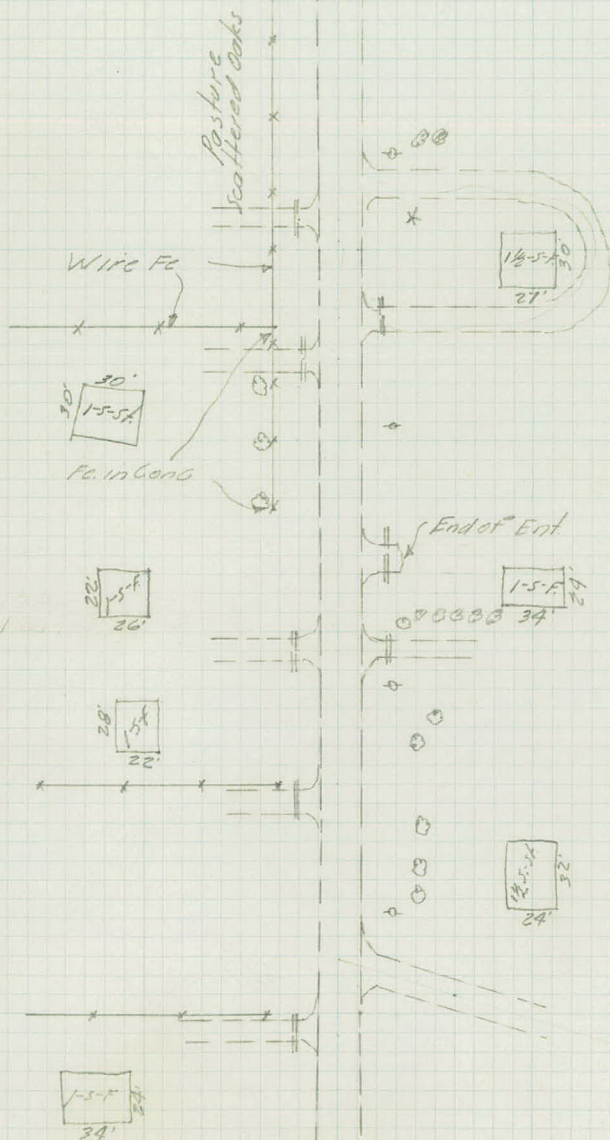
+89-Ent - 15'x20' C.M. - 22'

+

+43-S.E. Cor Ho - 107'

+30-PP-28'

139 11' 12'



152 11' 10'
+96-Fe. Cor-33' +95-PP-28'
+88-Ent.

+42-SE. Cor. Fored-91'

151 10' 10' Fe-30'
+178-Fe-35' +65-PP-28'
+170-Ent.

150 11' 10'
+89.35-Ditch #5 Sewer R.S. & Sec ditch #5 Survey for
Align + Grade.
+131-Ent. +55-PP-28'

149 11' 10' Fe-30'

+37-Fe Cor-34' +34-PP-28'

148 11' 10' +93-Fe. Cor-32'

147 Fe-24' 11' 10' +09-PP-28'

146 Fe-33' 11' 11' +32-6" Elm-41'
+16-6" Elm-41'
+14-SW Cor Ho-77'
5' Elm-42'

Posture



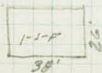
Posture



Posture

o

← Cult



159

+91-18" O-41'

+20-S.E. Cor Ho-96'

+11-15" O-34'

+106-Ent-12"X30 C.M.-22'

158

+89-P.P.-30'

+49-24" O-31'

+47-Cor Ho. S.E.-97'

+28-Ent-20"X15 C.M.-23'

157

+79-Fc-31'

156

+85-S.E. Cor Ho-95'

+74-Ent-12"X24 C.M.-22'

+42-Ent 18"X26 C.M.-21'

+33-N.E. Cor Ho-95'

155

+39-P.P.-43'

+38-Fc Cor-34'

154

+89-Tele. M.H.-13'

153

11' 11'

+95-P.P.-28'

+51-5" Elm-35'

+39-Ent

+18-10" Elm-35'

+15-Cor Hedge-29'

11'

+87-6" Elm-35'

+73-Plant Box 1/8" Wide 18-25'

+61-Ed. Sign-18'

+58-Beg. Hedge-28' 15" Elm-35'

+51-P.P.-28'

+50-Ent Rose Bush Hedge-26'

+22-10' Elm-35'

11' 11'

+92-Ent. Rood/Wall-25'

+86-Ent 15"X16 C.M.-23'

+76-15" B. Et-35'

+66-S.W. Cor Ho-61'

+41-Beg. Hedge-25' 12" Elm-34'

+39-Fc Dry. Rood/Wall-17-29'

+28-Ent 15"X24 C.M.-22'

+13-P.P.-28'

11' 10'

+89-Ent

+13-Fc Cor-30'

11' 10'

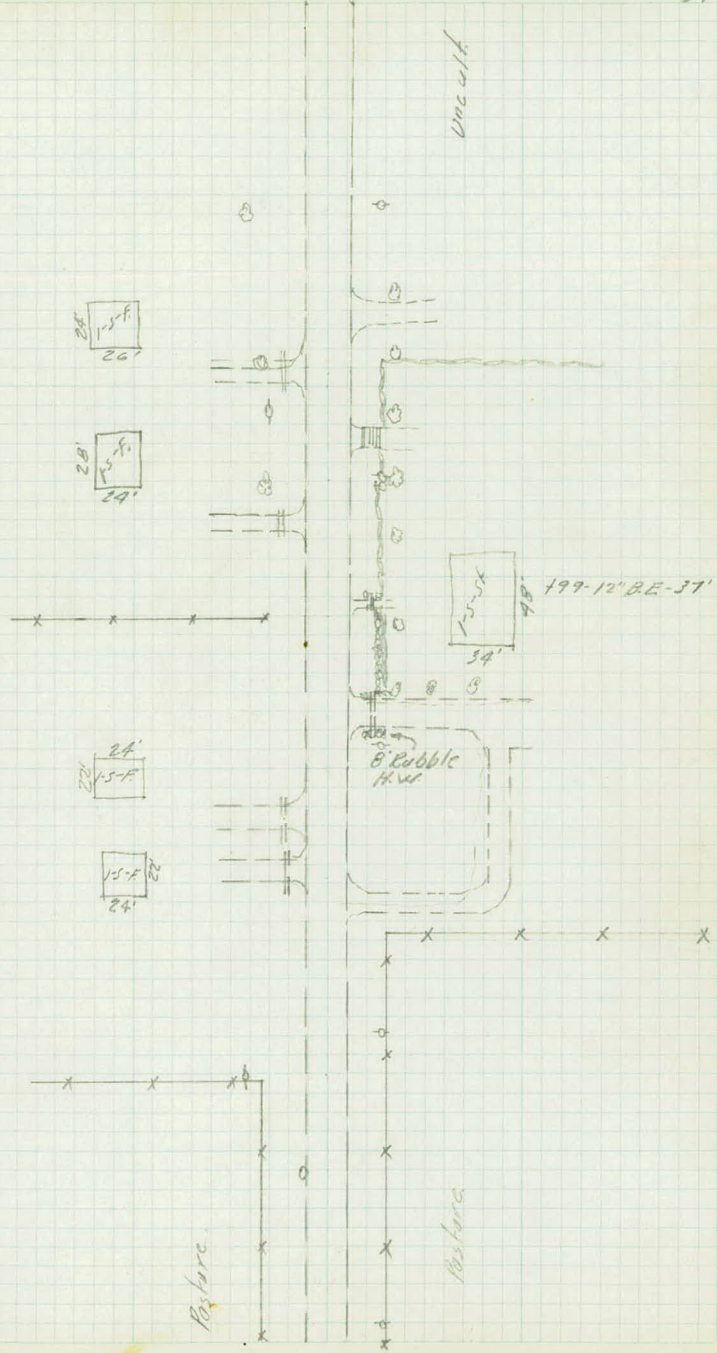
+61-P.P.-28'

11' 10'

+09-P.P.-28'

Fc-30'

11' 10'



166 11' 10'

+38-T.P.-22'

165 Fc-32'

12' 10'

+07-Leg of steel tower-29'
+01-Leg of steel tower-35.5'

+54-T.P.-23'

+85-Ctr. H' P-59.8' ctr. to ctr.
+75-T.P.-33'

+35-Ent.

164

12' 10'

+38-Rd. Sign-18'

163 Fc-30'

12' 10'

+97-T.P.-25'

+24-Ctr. H' P-100'

162

11' 10'

+78-T.P.-28'

161 +10-Dia Fc-39'

10'

+25-G.P.-27'
12-+10'

+88-Dia Fc-57'

+72-Tel. M.H.-13'

+49-Rd.-45' 50'

+37-24"-46'

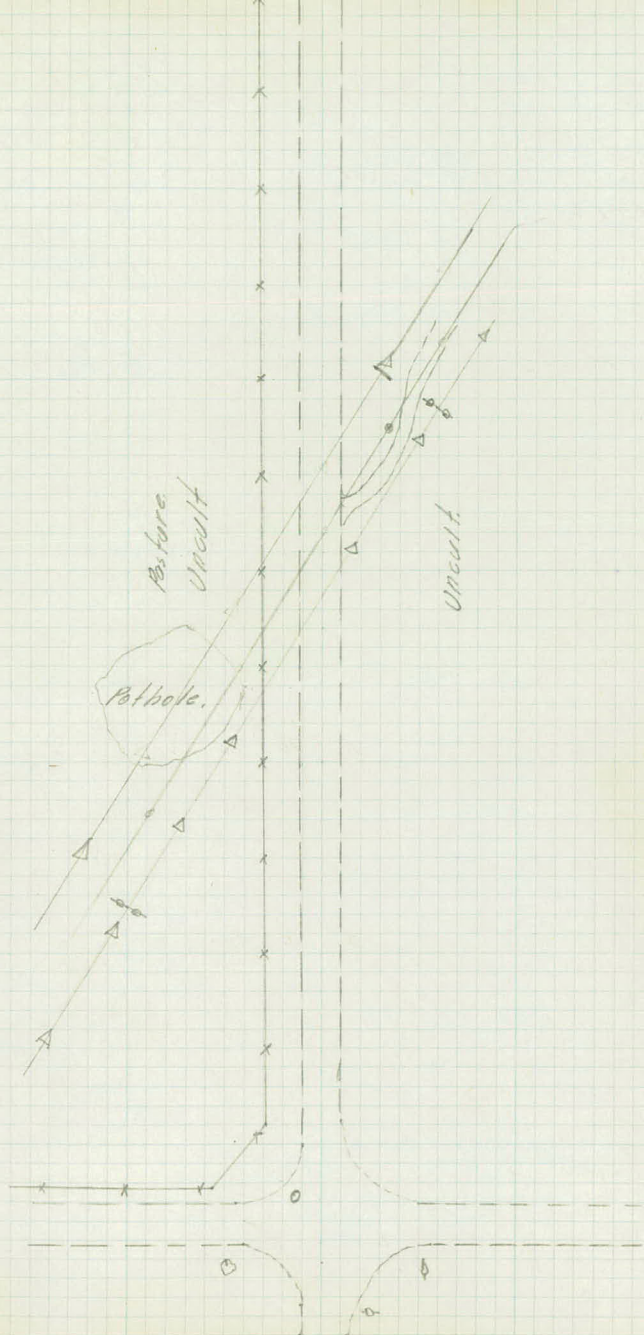
+48-Rd.-40' 56'

160

+16-Rd.-11'

11'

+39-P.P.-52'
+12-P.P.-26'



136-T.P.-24'

173 FC-34'

12' 10'

E.W.-21'

+80-EW-26'

+105-T.P.-23'

172 EW-30'

12' 10'

EW-20'

+74-X.Drain-24X52' G.M.

26' 26'

171 EW-26'

12' 10'

EW-21'

+52-T.P.-23'

+50-EW-29'

170

11' 10'

EW-23'

169 FC-33'

11' 10'

+70-T.P.-23'

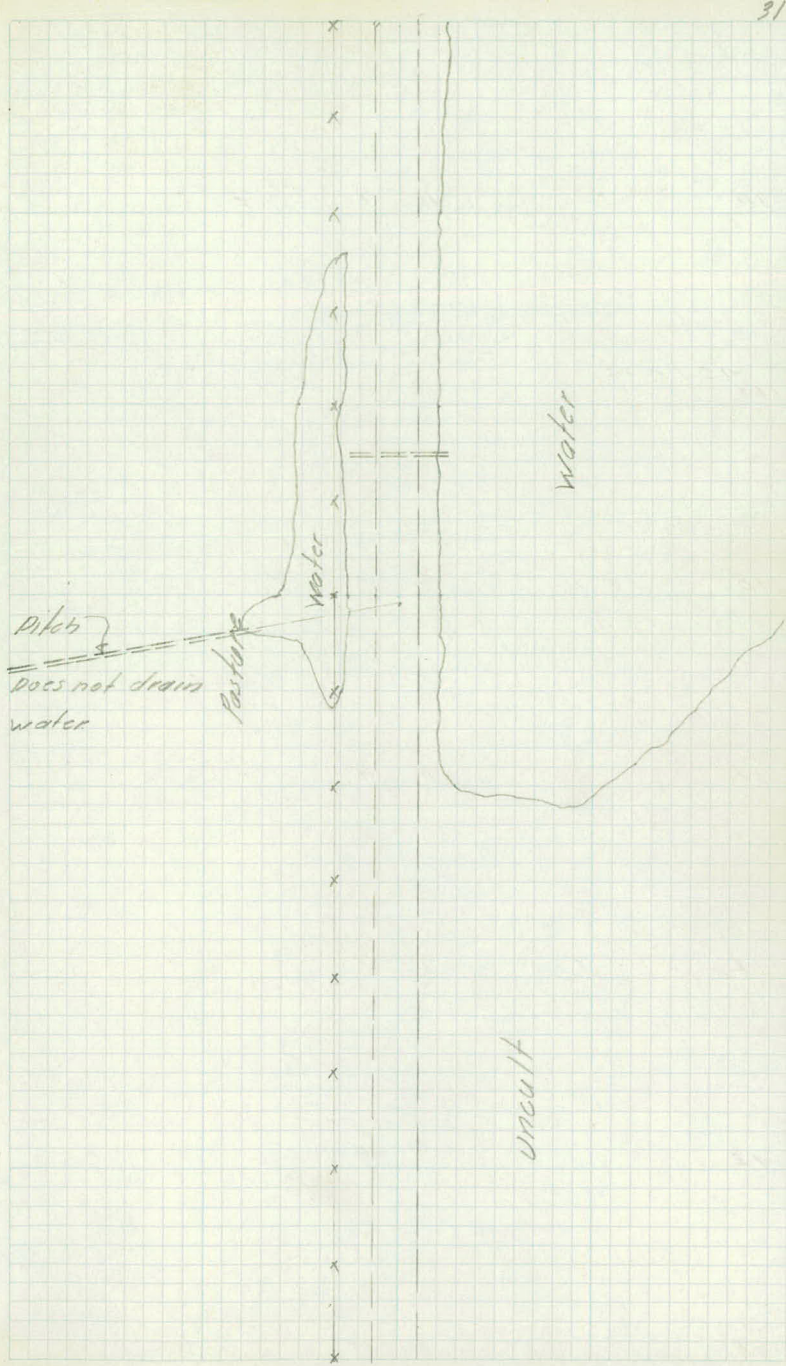
168

11' 10'

+32-T.P.-23'

167 FC-33'

12' 10'



+76-8" Pop-42'

+70-T.P.-25'

+80-8" Pop-42'

+45-12" Pop-42'

+78-8" Pop-30'

+72-4" Pop-28'

+63-8" Pop-29'

+31-5" Pop-21'

+89-End $\frac{15' \times 20' \times 11'}{25'}$

180

+98-End Fe-33'

+72-Fe Cor-34'

11' 9'

Fe-35'

+15-T.P.-24'

179

+22-Range tie

+18-Fe Cor-33'

11' 9'

178

Fe-33'

11' 9'

+84-T.P.-24'

177

11' 9'

+81-Fe Cor-36' →
+77-Range tie

+28-T.P.-24'

176

Fe-34'

11' 9'

+30-E.W.-35'

175

11' 9'

+82-T.P.-24'

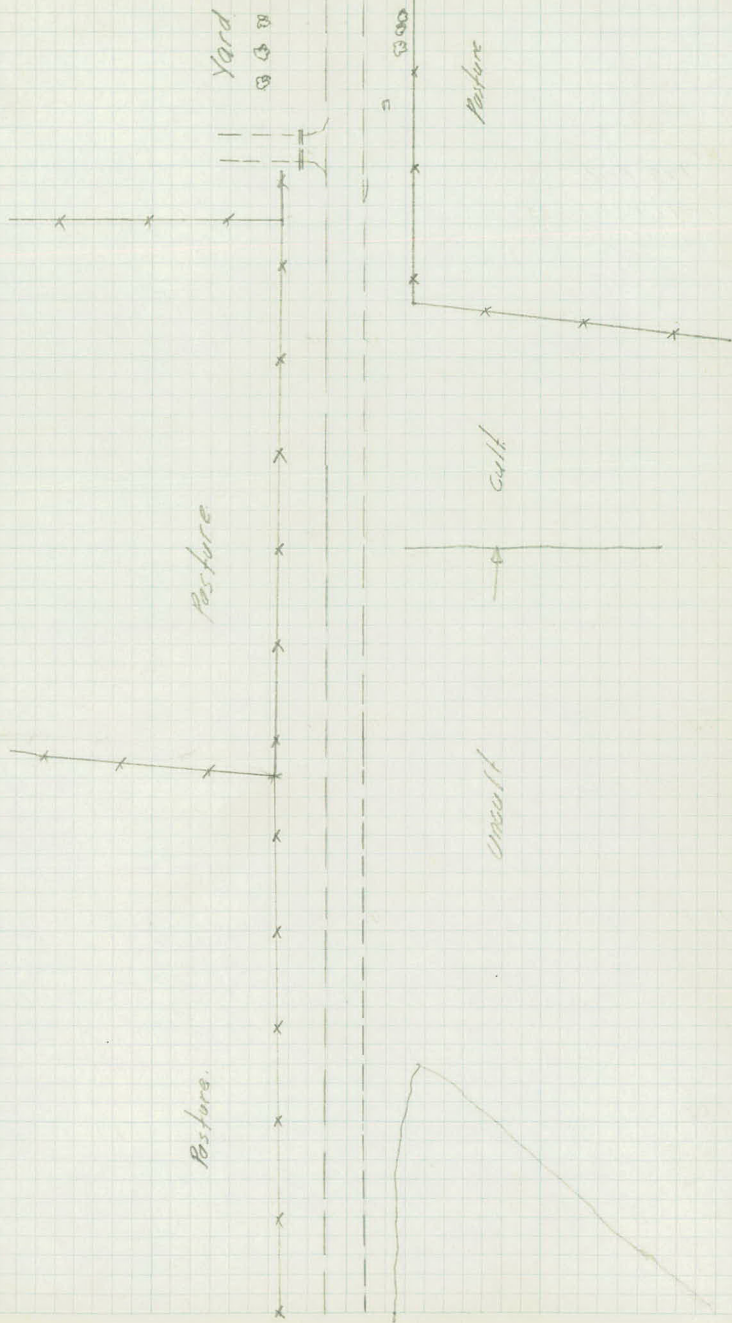
~~+30-E.W.-35'~~

174

Fe-35'

11' 10'

E.W.-25'



+5924'0-38

187
+94-Ent

10' 11'

+95-5 ft. + 809. Fc - 32'

+72-Fc Cor - 33'

+71-T.P - 27

+82-Ent

186

10' 10'

+20-T.P - 26'

185

10' 10'

+60-Fc Cor - 32'

184

Fc - 32'

10' 10'

Fc - 32'

+77-T.P - 26'

183

+03-809-Fc - 32'

11' 9'

+27-T.P - 26'

182

+12-Ent / 12' x 20' Dredge Pipe
21

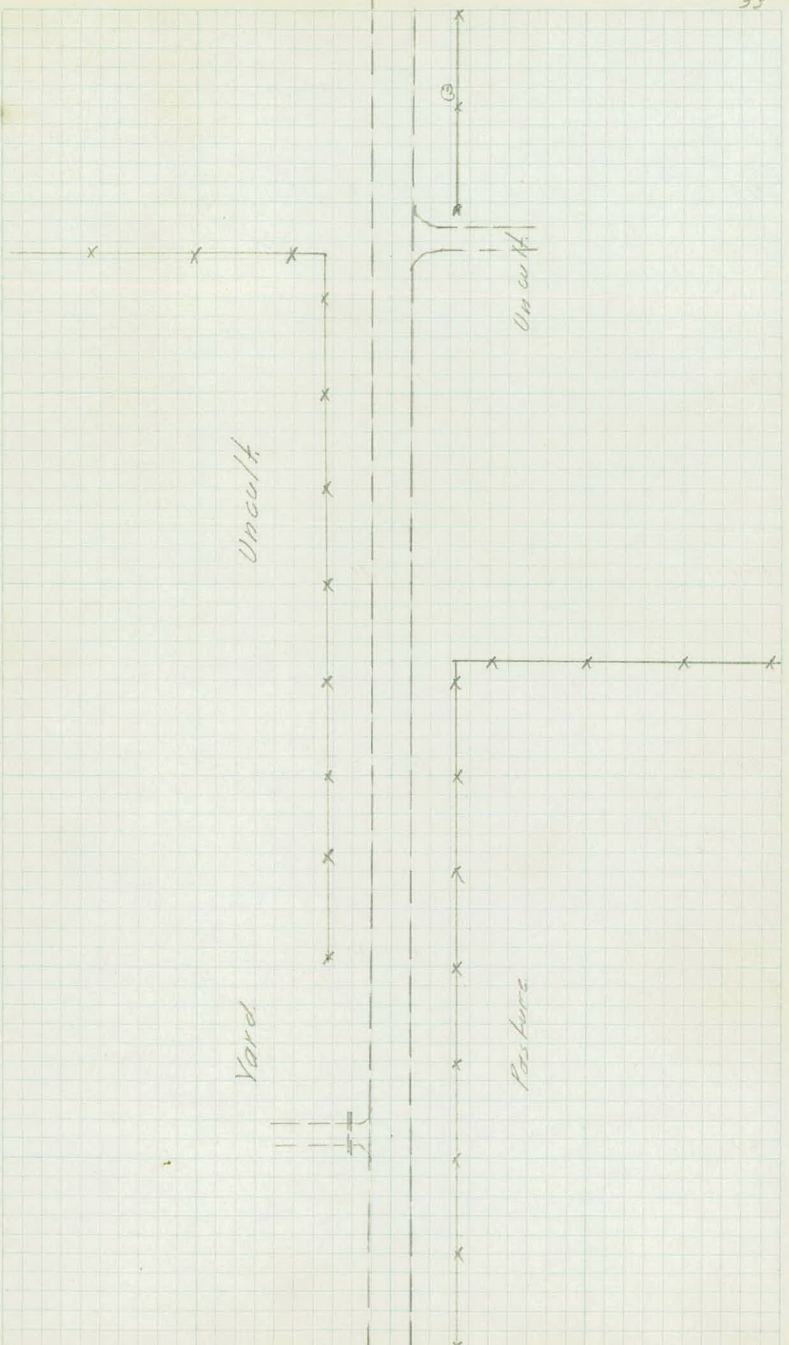
11' 10'

Fc - 34'

181

11' 10'

Fc - 34'



+88-56'-29'

+80-56'-24'

+23-T.P.-28'

+2815"0-26'

194

11' 11' Fe-26'

+80-24"0-27'

+67-8"0-32'

+57-12"0-27'

+57-Fe Cor-26'

+56-12"0-26'

193

+64-24"0-29'
11' 10' Fe-28'

+67-T.P.-28'

+95-26"0-30'

192

+61-24"0-27'
11' 10' Fe-30'

+50-56'-30'

+32-24"0-28'

191

+16-T.P.-28'

10' 11' Fe-30'

+97-18"0-31'

+70-6"0-32'

190

10' 11' Fe-28'

+33-T.P.-28'

189

10' 11' Fe-28'

+63-20"0-28'

188

T.P.-28'

+79-56'-30'
11' 11' 61-10" Fe 0-30'
Fe-31'

Vocult

postcard

Umsatz

Uncult.

+99-N.E. Cor. Ho.-90'

+98-4" Pns.-49'

+72-4" Pns.-49'

+107-T.P.-29'

+37-Ent.-

201

10' 10'

+77-5" Pns.-37'

+64-12" B.E.-37'

+51-S.W. Cor. Ho.-70'

+810' B.E.-36' 15" X 20' C.N.

+28-Ent.-20'

+109-T.P.-29'

202

11' 9'

8" B.E.-36'

+93-10' 0"-45'

+93-9' 0"-36'

+79-5' 0"-32'

+43-F.C. Cor.-27'

+29-9' 0"-26'

+14-8' 0"-33'

+12-8' 0"-32'

+103-12' 0"-31'

F.C.-26'

199

11' 9'

+89-10' 0"-26'

+86-12' 0"-32'

+82-12' 0"-26'

+49-30' 0"-33'

+26-8' 0"-28'

+17-9' 0"-34'

+11-9' 0"-42'

+1012' 0"-33'

F.C.-27'

198

12' 10'

+92-5' 0"-32'

+62-Ent.-15" X 20' C.N.
24'

+24-13' 0"-27'

+109-T.P.-28'

197

12' 10'

F.C.-28'

+94-20' 0"-29'

+53-15' 0"-29'

196

11' 11'

F.C.-28'

+84-20' 0"-27'

+66-T.P.-33'

+61-5' 0"-29'

+60-13' 0"-30'

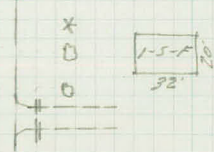
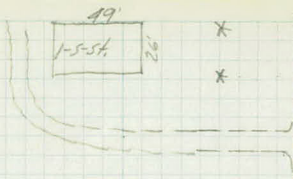
+24-15' 0"-28'

+17-10' 0"-34'

195

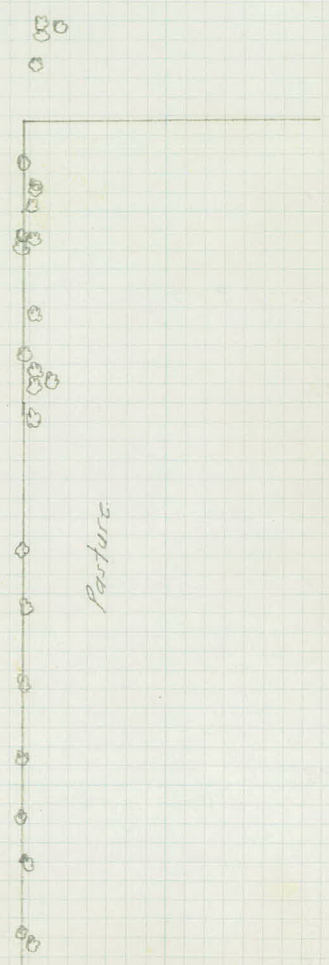
11' 10'

F.C.-27'



Uncult

Pasture



+54-T.P.-31'

+99-24'Ap-37'
+79-Ent
+66-P.P.-26'

208

11' 11' +75 W. Cor. Ho. - 80'

+91-15' E-32'

+67-T.P.-26'

+18-T.P.-31'
+17-S.E. Cor. Ho. - 67'
207 +108-6' E-43'

10' 11' +95-End-11'

+81-Row 18' Ap. - 53'
+57-Ent

+77-Ent 15' CM. 23' & Buried
57 = +66 End

+34-6' E/m-56
+32-Ent

36 = +46-Ent
+36-PP-25'
+33-Ent 15' CM. 22'
+18-Row-10'

206

11' 9'

+97-8' E-35'
+72-S.E. Cor. Ho. - 88'
+72-8' E-35' T.P. 29'
+61-8' E-35'

1

205

11' 10' +104 PP-27'

+30-T.P.-29'

204

11' 10'

+60-P.P.-26'

203

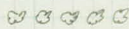
11' 10'

+87-T.P.-30'

+22-Ent-
+13-54/10-38
202

10' 10' +108-T.P.-26'

Cult.



Cult.



33



Road. Black Top.

Cult.

+88-P.P.-21'

+43-T.P.-27'

215 G.R.-14.5 10' 9' G.R.-15'

+45.00 Goff - 38' +61-Rd Sign - 16.5'
+43-T.P.-28' +39-G.R.-15.5'
+40-G.R.-13.5' +28-Pi Top - 8' 10' +36-P.P.-21'
Face Curb - 10' +28-N End Retain Wall Face Curb - 13'
6" X 15" - Plank

214

Curb Timber - 8" wide
6" Thick +73.3 - R Track
+59.0 - R Track
+45.35 - R Track

+14-T.P.-26' +67-P.P.-23'
213 6" X 15" Plank
Face Curb - 12' +90.3 - S End Retain Wall of Bridge Face Curb - 11'
+96-T.P.-29' +81-End G.R. - 14.5 14'

212 G.R.-15 11' 11' +64-P.P.-23'
G.R.-14'

+92-T.P.-30'

211 10' 10' G.R.-14'

+79-Beg. G.R.-15.5'

210 10' 10' +90-P.P.-24'
+91-T.P.-30' +92-Beg G.R.-13.5'

209 11' 11' +100-End of Ent



See Survey of Bridge
for Align. of Tracks.

218

16' 7'

150 14' 8'

+30-G.R.-25'

+20-Rad. 14'

217

21' 9'

+80-Rd.-60'

+95-RP-21

113-Sign-15'

+38-Ext

+46-End G.R.-42'

+57-Rad-57

+93-End G.R.-12.5'

+39-Rd. 550-13

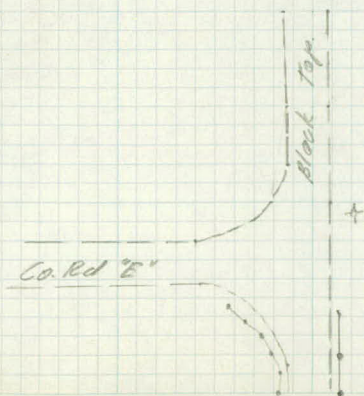
+38-G.R.-16'

+18-T.P.-26'

+15-Rad-12'

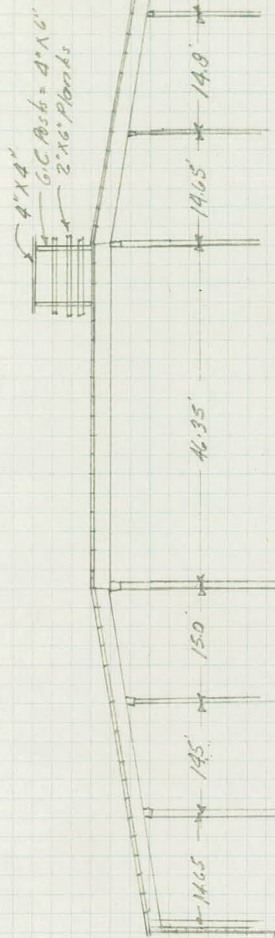
216 G.R.-16'

11' 9' G.R.-13.5



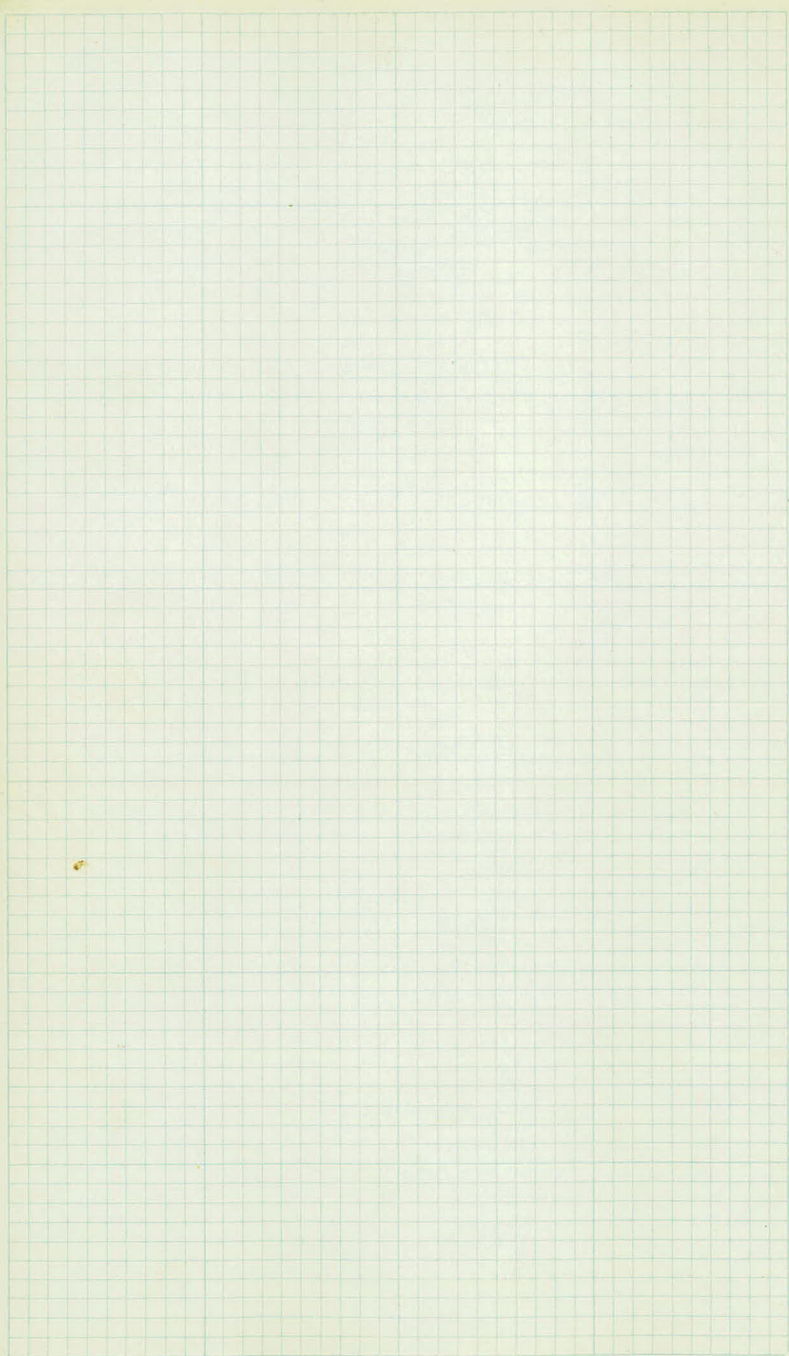
$$\begin{array}{r} 15/6 \\ 10/8 \\ 1/4 \end{array}$$

$$\begin{array}{r} 55 \\ 10/6 \\ 14/0 \\ 1/1 \end{array}$$



6 Piles in each Bent
 End Bent for Frame Bents
 Stringers 6" x 16" - 16 Stringers
 Caps = 12"
 Sway Braces 3" x 12"
 Flooring = 4" x 10" Planks

Ch. End Bent = 212' 7 1/2"



X sections

Sta	+	π	-	Elev
B.M.	564	986.38		980.74

0	+00		5.64	80.74.
---	-----	--	------	--------

	+10			80.7.
--	-----	--	--	-------

	+21			81.1
--	-----	--	--	------

	+26			81.1
--	-----	--	--	------

	+30			81.2
--	-----	--	--	------

	+33			81.2
--	-----	--	--	------

	+65			81.4.
--	-----	--	--	-------

1				81.5
---	--	--	--	------

	+50			81.6.
--	-----	--	--	-------

2				81.6.
---	--	--	--	-------

	+50			81.6-
--	-----	--	--	-------

Lt.

4

Rt.

Top Marsh Larpenteur Ave. + Cleveland.

$$\frac{5.09}{50} \quad \frac{5.70}{50} \quad \frac{6.56}{50}$$

$$\frac{54}{50} \quad \frac{59}{35} \quad \frac{53}{19} \quad \frac{53}{14} \quad \frac{55}{37} \quad \frac{64}{37} \quad \frac{6.6}{50}$$

on ground
N End. Xculx → $\frac{76}{72} \quad \frac{71}{51} \quad \frac{72}{32} \quad \frac{60}{28} \quad \frac{52}{12} \quad \frac{53}{19} \quad \frac{57}{30} \quad \frac{63}{39} \quad \frac{80}{39} \quad \frac{84}{50}$

$$\frac{71}{50} \quad \frac{72}{34} \quad \frac{60}{25} \quad \frac{52}{12} \quad \frac{52}{16} \quad \frac{56}{25} \quad \frac{61}{30} \quad \frac{79}{30} \quad \frac{84}{50}$$

$$\frac{52}{50} \quad \frac{52}{30} \quad \frac{62}{27} \quad \frac{53}{12} \quad \frac{52}{14} \quad \frac{59}{24} \quad \frac{60}{27} \quad \frac{75}{29} \quad \frac{78}{32} \quad \frac{66}{32} \quad \frac{72}{50}$$

$$\frac{52}{50} \quad \frac{51}{31} \quad \frac{61}{26} \quad \frac{62}{22} \quad \frac{54}{15} \quad \frac{53}{13} \quad \frac{50}{13} \quad \frac{53}{17} \quad \frac{55}{20} \quad \frac{60}{25} \quad \frac{64}{25} \quad \frac{63}{32} \quad \frac{71}{35} \quad \frac{74}{50}$$

$$\frac{48}{50} \quad \frac{48}{35} \quad \frac{50}{31} \quad \frac{62}{26} \quad \frac{60}{20} \quad \frac{52}{14} \quad \frac{49}{14} \quad \frac{52}{16} \quad \frac{60}{19} \quad \frac{63}{25} \quad \frac{60}{32} \quad \frac{68}{36} \quad \frac{70}{50}$$

$$\frac{48}{50} \quad \frac{46}{38} \quad \frac{52}{30} \quad \frac{60}{24} \quad \frac{60}{20} \quad \frac{50}{14} \quad \frac{48}{14} \quad \frac{51}{19} \quad \frac{58}{25} \quad \frac{63}{32} \quad \frac{60}{37} \quad \frac{67}{37} \quad \frac{72}{50}$$

$$\frac{51}{50} \quad \frac{53}{38} \quad \frac{57}{30} \quad \frac{60}{27} \quad \frac{61}{20} \quad \frac{51}{14} \quad \frac{48}{15} \quad \frac{52}{19} \quad \frac{59}{24} \quad \frac{64}{32} \quad \frac{63}{35} \quad \frac{69}{35} \quad \frac{74}{50}$$

$$\frac{64}{50} \quad \frac{64}{40} \quad \frac{64}{29} \quad \frac{63}{22} \quad \frac{53}{17} \quad \frac{51}{14} \quad \frac{48}{15} \quad \frac{53}{21} \quad \frac{67}{25} \quad \frac{71}{32} \quad \frac{72}{32} \quad \frac{75}{35} \quad \frac{71}{50}$$

Sta	+	π	-	Elev
		986.38		
3				81.7.
T.P.	5.77	987.42	4.73	981.65
+50				81.6.
4				81.9
+50				82.3
5				82.6.
+50				82.6.
6				82.6.
+27				82.6
+70				82.6.
7				82.6.
+35				82.5

1.

2

2.

64 61 63 53 49 47 52 69 74 74 79 79
50 30 21 17 11 14 21 27 33 35 50

69 83 73 70 64 59 58 61 79 83 87 89 90
50 35 30 21 17 11 14 21 25 32 34 50

64 70 64 83 73 71 62 57 55 58 62 77 80 82 84 85
50 35 30 35 30 21 17 10 13 17 23 27 33 35 50

61 63 64 63 56 53 51 53 62 68 69 74 74
50 36 30 20 16 10 14 20 25 32 35 50

55 58 56 60 59 51 50 48 52 60 64 59 61 62
50 38 30 26 19 14 10 14 20 25 32 35 50

47 52 49 58 59 55 50 48 53 60 58 52 54 55
50 39 30 23 21 18 10 15 23 27 32 35 50

41 44 37 56 57 51 50 48 53 60 58 49 51 52
50 37 30 23 18 14 10 16 22 26 32 35 50

37 40 36 58 60 52 50 48 51 54 57 58 49 50 50
50 38 30 23 20 15 9 11 17 19 24 32 35 50

30 30 31 25 60 60 50 48 50 52 57 56 47 46 50
50 42 36 31 23 19 13 12 17 20 26 32 35 50

21 27 19 57 59 50 48 51 53 58 55 46 47 51
50 38 31 23 19 13 12 17 22 27 32 35 50

30 34 23 60 60 51 49 52 53 59 59 48 47 52
50 38 31 23 20 13 12 16 21 25 32 35 50

Sta	+	π	-	Elev.
		987.42		
7	+56			82.4.
	+61			82.5.
8				82.4.
	+45			82.3.
	+78			82.1.
9				82.1.
	+36			82.2.
I.P.	3.48	985.33	5.57	981.85.
	+42			82.1.
	+75			82.0.
10				82.1.
	+33			82.2.

Lt

2

Lt

$$\frac{36}{50} \frac{50}{52} \frac{61}{23} \frac{61}{21} \frac{50}{15} \frac{50}{16} \frac{53}{20} \frac{60}{25} \frac{60}{32} \frac{49}{36} \frac{54}{50} \frac{56}{50}$$

$$\frac{50}{50} \frac{51}{28} \frac{61}{24} \frac{60}{20} \frac{51}{13} \frac{49}{11} \frac{52}{16} \frac{53}{20} \frac{58}{23} \frac{61}{32} \frac{50}{36} \frac{54}{50} \frac{56}{50}$$

$$\frac{60}{50} \frac{61}{29} \frac{66}{25} \frac{56}{19} \frac{51}{10} \frac{50}{16} \frac{52}{21} \frac{61}{27} \frac{64}{32} \frac{59}{36} \frac{66}{50} \frac{67}{50}$$

$$\frac{76}{50} \frac{75}{30} \frac{78}{26} \frac{57}{18} \frac{55}{10} \frac{51}{11} \frac{54}{17} \frac{58}{23} \frac{67}{27} \frac{70}{32} \frac{72}{37} \frac{78}{50} \frac{76}{50}$$

$$L.O. \frac{83}{36} \frac{82}{28} \frac{75}{23} \frac{68}{20} \frac{57}{9} \frac{53}{14} \frac{56}{18} \frac{61}{24} \frac{72}{29} \frac{76}{32} \frac{76}{39} \frac{76}{50}$$

$$L.O. \frac{87}{35} \frac{86}{30} \frac{82}{25} \frac{69}{20} \frac{57}{12} \frac{53}{17} \frac{58}{24} \frac{72}{32} \frac{74}{37} \frac{74}{50}$$

$$\frac{84}{50} \frac{84}{35} \frac{76}{27} \frac{58}{23} \frac{55}{10} \frac{52}{16} \frac{58}{22} \frac{67}{29} \frac{68}{32} \frac{66}{38} \frac{65}{50} \frac{65}{50}$$

$$\frac{37}{50} \frac{34}{25} \frac{35}{14} \frac{32}{12} \frac{36}{17} \frac{36}{22} \frac{47}{28} \frac{47}{32} \frac{45}{39} \frac{42}{50} \frac{44}{50}$$

$$\frac{36}{50} \frac{34}{22} \frac{33}{15} \frac{35}{22} \frac{46}{32} \frac{42}{42} \frac{42}{50} \frac{41}{50}$$

$$\frac{37}{50} \frac{34}{32} \frac{34}{11} \frac{32}{15} \frac{35}{25} \frac{46}{32} \frac{38}{42} \frac{38}{50}$$

$$\frac{36}{50} \frac{39}{20} \frac{32}{9} \frac{31}{15} \frac{36}{22} \frac{45}{27} \frac{44}{32} \frac{40}{50} \frac{38}{50}$$

Sta	+	π	-	Elev
		985.33		
10	+38			82.2.
	+70			82.1.
11				82.0.
	+30			81.7.
	+70			81.4.
12				81.0.
	+50			80.5.
	+88			80.0.
13	No X section			79.9.
	+14			79.8.
B.M.			7.08	978.25.
	+64			79.2.

Lt.

L

Rt.

34 33 41 37 33 31 36 45 45 37 39 38
50 29 26 20 8 16 22 27 32 41 50

3.2 36 39 40 36 34 32 35 47 41 37 40
50 26 24 20 17 10 15 23 32 41 50

29 38 39 38 35 33 36 47 48 44 45 4.6
50 25 21 17 12 15 23 28 32 42 50

27 39 38 36 40 50 51 53 54
50 28 14 15 22 32 42 50

35 48 51 46 44 39 43 52 52 49 50 57
50 28 21 18 15 14 21 27 32 36 50

47 53 56 51 46 43 47 55 54 47 47 50
50 30 21 18 11 15 22 27 32 42 50

60 63 61 53 50 48 51 59 57 43 38 49 4.4
50 37 22 17 11 15 19 24 32 41 44 50

61 64 68 65 57 54 53 56 66 6.8 6.8
50 45 37 20 16 10 14 21 32 50

SA

72 71 62 59 55 59 6.8 6.8 7.0
50 24 17 11 14 24 32 50

Top Conc. Base of Fe Post 33' Lt Sta 13+17

58 58 68 71 74 67 65 6.1 6.4 7.2 7.4 6.8 5.9 4.8
50 47 42 33 23 16 9 14 19 25 32 37 50

Sta	+	π	-	Elev
		985.83.		
14				78.8.
	+30			78.4.
	+85			77.6.
15				77.5.
T.P	3.85	981.36.	7.82	977.51.
	+50			77.1.
16				76.7.
	+50			76.6.
17				76.5.
	+45			76.5.
	+76			76.6.
18				76.7.

Lt

2

Pt.

6.5 7.5 8.6 8.2 7.2 6.8 6.5 6.8 7.0 7.9 7.8 7.2 6.2 5.8
 50 43 33 24 16 9 13 16 22 27 32 40 50

9.4 9.9 10.3 9.6 9.5 8.2 7.7 7.3 6.9 7.4 8.2 8.3 7.8 9.1 9.1
 50 46 38 36 32 23 17 11 15 21 32 37 43 50

14.0 13.6 10.6 10.5 10.0 8.3 7.7 8.0 8.5 11.7 12.0 11.5
 50 44 36 32 22 15 11 17 30 38 50

14.4 13.7 10.9 10.5 10.0 8.6 7.8 8.2 8.6 12.0 12.3 12.0 12.0
 50 42 36 32 22 16 11 15 30 33 42 50

L. Sta. - 15100

8.0 7.7 6.6 6.2 6.0 5.1 4.6 4.3 4.7 5.1 8.2 8.5 8.2
 50 45 35 33 24 19 9 13 17 28 32 50

5.7 6.7 6.9 6.7 6.2 5.4 5.0 4.7 5.0 5.2 8.2 8.5 8.2
 50 39 33 26 21 15 9 13 17 27 32 50

4.8 7.1 7.3 7.5 7.0 5.6 5.1 4.8 5.1 5.3 8.4 8.8 8.2
 50 38 33 25 21 15 10 13 17 28 32 50

8.0 8.6 8.1 7.7 7.1 5.7 5.2 4.9 5.2 5.4 7.8 8.0 8.0 7.4 6.6
 50 39 32 26 22 16 8 13 16 27 32 34 38 50

6.6 6.6 6.3 6.2 6.5 6.3 5.3 5.0 4.9 5.2 5.8 5.7 4.0 2.7 2.8
 50 36 34 33 28 22 16 7 13 21 25 32 40 50

3.5 4.0 4.8 4.8 5.4 5.8 5.4 5.0 4.8 4.9 5.7 5.6 1.4 0.3 0.4
 50 41 34 32 25 21 17 9 14 20 22 32 43 50

5.6 4.6 5.4 5.8 5.9 5.2 5.0 4.7 4.9 6.0 5.8 3.2 2.1 2.6
 50 40 32 25 19 17 9 13 20 24 32 43 50

Sto.	+	π	-	Elev
		981.36.		
18	+33			76.7.
	+65			76.8.
19				76.9.
	+50			76.9.
20				77.0.
T.P.	6.72	983.75.	4.33	977.03.
	+34			77.5.
	+66			77.9.
21				78.2.
	+19			78.4.
	+66			78.9.
22				79.2.

Lt

R

Lt

60 67 69 68 64 53 50 47 48 68 68 66 69
50 38 33 26 22 18 9 13 25 32 37 50

62 68 66 63 63 52 48 46 50 82 85 85 92
50 36 32 28 22 18 9 15 27 33 38 50

77 81 82 76 54 49 45 50 56 87 92 97 97
50 39 32 27 18 9 13 18 28 33 38 50

89 94 95 92 54 48 45 50 57 83 86 82 82
50 36 33 31 18 9 14 17 28 33 41 50

83 83 80 55 (47) 45 44 47 58 58 51 48 45
50 33 27 19 M.H. 9 14 21 21 33 38 50

88 86 87 87 86 71 68 63 67 77 75 66 60 54
50 37 33 27 24 17 9 15 23 28 33 37 50

77 77 76 79 66 64 59 64 73 75 69 68 66
50 38 33 24 16 9 14 22 29 33 38 50

59 64 72 70 71 61 60 56 61 67 74 82 78
50 37 33 27 21 15 10 20 27 33 38 50

57 59 58 65 68 58 56 54 57 75 80 85 84
50 37 33 26 22 15 9 14 21 33 37 50

41 47 51 61 61 55 52 49 52 64 64 62 59
50 38 33 27 22 17 10 14 23 33 37 50

31 26 37 39 41 56 57 53 49 46 49 61 67 75 75
50 39 37 33 29 24 20 16 9 14 23 33 42 50

Sta	+	π	-	Elev.
		983.75.		
22	+27			79.7.
T.P.	479	986.46.	2.08	981.67.
	+66			80.5.
23.				81.2.
	+50			81.6.
	+79			81.7.
B.M.			2.45	984.01. (984.04)
24				81.9.
	+50			82.1.
	+63 X Poin			82.0.
25				82.0.
	+30			82.1.
	+69			82.3.

44.

L

24

$\frac{43}{50} \quad \frac{44}{39} \quad \frac{46}{33} \quad \frac{51}{24} \quad \frac{52}{20} \quad \frac{46}{16} \quad \frac{44}{10} \quad \frac{41}{14} \quad \frac{43}{26} \quad \frac{58}{52} \quad \frac{56}{38} \quad \frac{57}{50}$

Spk. 10 P.P. 25.22 +

31 37 33 40 47 70 71 66 63 40 62 71 72 65 60 60
50 48 40 35 29 23 19 16 10 14 21 27 33 38 50

$\frac{26}{50} \frac{20}{47} \frac{26}{43} \frac{35}{30} \frac{64}{22} \frac{64}{19} \frac{58}{16} \frac{55}{9} \frac{53}{14} \frac{56}{19} \frac{64}{24} \frac{65}{33} \frac{40}{37} \frac{36}{50} \frac{41}{50}$

$\frac{22}{50} \frac{20}{43} \frac{29}{38} \frac{31}{30} \frac{59}{83} \frac{58}{19} \frac{52}{16} \frac{51}{9} \frac{49}{15} \frac{51}{20} \frac{60}{27} \frac{60}{33} \frac{56}{41} \frac{56}{50}$

53	50	49	58	57	52	49	48	50	62	81	89
50	37	31	25	20	17	9		16	22	33	50

Top of N. Conc Footing Radio Tower 95' Lt Sta 23+80

85	90	91	82	59	49	46	49	55	85	93	94	96	95
75	50	39	29	17	12		15	18	26	27	36	50	75

8.93
top water

112	111	97	84	53	47	44	48	51	87	94	96	95
75	63	49	32	21	12	12	19	28	36	46	50	

99
Top water

(Coke)

(Contd.)

115	105	101	99	95	93	54	47	45	40	50	8.85	84	82	93	90
75	61	58	39	28	37	21	10	12	18	21	21	29	39	50	

11.5 102 95 91 78 54 48 45 48 51 82 87 90 74
75 55 51 47 27 18 11 13 18 28 33 36 50

$\frac{11.2}{15} \quad \frac{11.1}{61} \quad \frac{9.1}{47} \quad \frac{6.9}{49} \quad \frac{6.2}{34} \quad \frac{7.5}{30} \quad \frac{7.5}{26} \quad \frac{5.2}{19} \quad \frac{4.7}{9} \quad \frac{4.4}{13} \quad \frac{4.7}{10} \quad \frac{4.8}{28} \quad \frac{7.3}{33} \quad \frac{8.1}{40} \quad \frac{8.1}{50} \quad \frac{6.5}{50}$

L.O. $\frac{111}{57} \frac{106}{40} \frac{96}{34} \frac{52}{21} \frac{47}{10} \frac{42}{13} \frac{44}{21} \frac{45}{29} \frac{58}{29} \frac{53}{33} \frac{45}{38} \frac{43}{50}$

Sta	+	π	-	Elev
		986.46.		
26				82.7.
+10				82.8.
+21				82.8.
+32.62 & X Road Profile				82.9.
+44				82.9.
+51				82.9.
+68				83.1.
+83 X Drain				83.3.
I.P.	5.55	989.16.	2.85	983.61.
27				83.6.
+50				84.1.
28				84.7.
I.P.	10.40	996.36.	3.20	985.96.

Lt.

L

Lt.

$$\begin{array}{cccccccccccccc} 95 & 92 & 85 & 57 & 50 & 44 & 38 & 39 & 43 & 49 & 47 & 42 \\ 75 & 50 & 42 & 33 & 21 & 70 & & 74 & 32 & 33 & 36 & 50 \end{array}$$

$$\begin{array}{cccccc} 54 & 51 & 41 & 37 & 37 & 46 & 42 & 36 \\ 50 & 29 & 9 & & 74 & 30 & 41 & 50 \end{array}$$

$$\begin{array}{cccccc} 51 & 45 & 41 & 37 & 36 & 40 & 41 \\ 50 & 26 & 70 & & 21 & 42 & 50 \end{array}$$

$$\begin{array}{cccccccccccccc} 73 & 69 & 64 & 58 & 52 & 47 & 42 & 36 & 36 & 35 & 29 & 24 \\ 300 & 250 & 200 & 150 & 100 & 50 & 25 & & 25 & 50 & 100 & 750 \end{array}$$

$$\begin{array}{cccccc} 51 & 47 & 40 & 36 & 36 & 38 & 37 \\ 50 & 27 & 11 & & 74 & 35 & 50 \end{array}$$
(Top
M.H.)
$$\begin{array}{cccccc} 54 & 51 & 45 & 40 & 36 & 36 & 42 & 43 & 40 \\ 50 & 30 & 18 & 10 & & 18 & 30 & 39 & 50 \end{array}$$

$$\begin{array}{cccccccccccccc} 100 & 81 & 77 & 55 & 46 & 48 & 39 & 34 & 36 & 41 & 43 & 51 & 49 \\ 75 & 50 & 46 & 34 & 19 & 15 & 9 & & 73 & 20 & 31 & 36 & 50 \end{array}$$
(10.0
topwater)

(Kulv)

75.76

(Kulv)

79.24

$$\begin{array}{cccccccccccccc} 110 & 110 & 105 & 1070 & 79 & 48 & 40 & 32 & 34 & 39 & 722 & 61 & 51 & 31 & 28 \\ 75 & 58 & 43 & 42 & 33 & 23 & 10 & & 13 & 22 & 31 & 38 & 50 & 65 & 75 \end{array}$$

$$\begin{array}{cccccccccccccccc} 143 & 138 & 130 & 121 & 94 & 70 & 64 & 57 & 56 & 57 & 61 & 91 & 91 & 78 & 69 & 54 & 48 \\ 75 & 50 & 39 & 37 & 27 & 19 & 9 & 6 & & 12 & 19 & 28 & 34 & 41 & 56 & 61 & 75 \end{array}$$

$$\begin{array}{cccccccccccccccc} 148 & 144 & 130 & 125 & 87 & 65 & 57 & 60 & 51 & 52 & 56 & 85 & 86 & 86 & 43 & 37 & 22 & 09 & 10 \\ 75 & 30 & 39 & 38 & 26 & 21 & 10 & 9 & & 12 & 18 & 24 & 31 & 36 & 43 & 53 & 59 & 63 & 10 \end{array}$$

$$\begin{array}{cccccccccccccccc} 147 & 138 & 130 & 122 & 89 & 56 & 53 & 52 & 45 & 46 & 49 & 75 & 75 & 24 & 08 & 20 & 120 & 126 \\ 50 & 32 & 40 & 38 & 26 & 19 & 11 & 9 & & 12 & 18 & 23 & 29 & 38 & 44 & 53 & 64 & 75 \end{array}$$

Sta	+	π	-	Elev
		996.36'		
28	+50			85.7,
	+90			86.4,
29				86.6,
	+35			87.1.
	+75			87.4.
30				87.7.
	+27			88.0.
	+67			88.5.
31				88.9.
	+50			89.1.
32				89.0.

LH

E

RH

L.O. $\frac{192}{60}$ $\frac{161}{38}$ $\frac{145}{29}$ $\frac{119}{18}$ $\frac{113}{11}$ $\frac{113}{9}$ $\frac{107}{14}$ $\frac{108}{18}$ $\frac{111}{23}$ $\frac{132}{28}$ $\frac{93}{35}$ $\frac{63}{42}$ $\frac{43}{56}$ $\frac{34}{70}$

$\frac{153}{75}$ $\frac{145}{61}$ $\frac{130}{45}$ $\frac{127}{31}$ $\frac{122}{28}$ $\frac{127}{22}$ $\frac{109}{19}$ $\frac{102}{9}$ $\frac{100}{11}$ $\frac{101}{19}$ $\frac{105}{23}$ $\frac{120}{27}$ $\frac{119}{34}$ $\frac{90}{40}$ $\frac{61}{75}$ $\frac{54}{75}$

$\frac{140}{75}$ $\frac{126}{50}$ $\frac{120}{36}$ $\frac{124}{27}$ $\frac{125}{23}$ $\frac{105}{18}$ $\frac{101}{9}$ $\frac{98}{11}$ $\frac{99}{21}$ $\frac{101}{24}$ $\frac{117}{27}$ $\frac{117}{31}$ $\frac{99}{51}$ $\frac{84}{75}$ $\frac{68}{75}$

$\frac{95}{75}$ $\frac{89}{50}$ $\frac{91}{36}$ $\frac{116}{28}$ $\frac{113}{21}$ $\frac{101}{18}$ $\frac{96}{9}$ $\frac{93}{12}$ $\frac{95}{18}$ $\frac{98}{23}$ $\frac{111}{27}$ $\frac{111}{31}$ $\frac{96}{51}$ $\frac{89}{75}$ $\frac{87}{75}$

$\frac{72}{75}$ $\frac{80}{56}$ $\frac{83}{42}$ $\frac{88}{36}$ $\frac{108}{28}$ $\frac{108}{21}$ $\frac{95}{17}$ $\frac{92}{8}$ $\frac{90}{13}$ $\frac{92}{17}$ $\frac{95}{23}$ $\frac{113}{28}$ $\frac{113}{29}$ $\frac{107}{30}$ $\frac{107}{75}$ $\frac{102}{75}$

$\frac{78}{75}$ $\frac{74}{55}$ $\frac{71}{37}$ $\frac{90}{32}$ $\frac{105}{26}$ $\frac{105}{22}$ $\frac{93}{18}$ $\frac{89}{9}$ $\frac{87}{12}$ $\frac{90}{18}$ $\frac{94}{23}$ $\frac{110}{29}$ $\frac{110}{32}$ $\frac{101}{50}$ $\frac{100}{75}$ $\frac{90}{75}$

$\frac{70}{75}$ $\frac{56}{65}$ $\frac{47}{32}$ $\frac{41}{40}$ $\frac{68}{35}$ $\frac{98}{27}$ $\frac{100}{22}$ $\frac{90}{18}$ $\frac{87}{9}$ $\frac{84}{12}$ $\frac{88}{19}$ $\frac{92}{24}$ $\frac{103}{27}$ $\frac{102}{37}$ $\frac{66}{50}$ $\frac{59}{75}$ $\frac{58}{75}$

$\frac{70}{75}$ $\frac{56}{62}$ $\frac{47}{52}$ $\frac{42}{38}$ $\frac{73}{33}$ $\frac{96}{27}$ $\frac{96}{22}$ $\frac{85}{18}$ $\frac{81}{9}$ $\frac{79}{12}$ $\frac{83}{17}$ $\frac{85}{22}$ $\frac{99}{25}$ $\frac{98}{30}$ $\frac{88}{38}$ $\frac{47}{55}$ $\frac{51}{75}$ $\frac{56}{75}$

$\frac{98}{75}$ $\frac{80}{61}$ $\frac{64}{30}$ $\frac{54}{37}$ $\frac{77}{33}$ $\frac{97}{27}$ $\frac{96}{22}$ $\frac{84}{18}$ $\frac{78}{9}$ $\frac{75}{13}$ $\frac{79}{18}$ $\frac{82}{23}$ $\frac{98}{25}$ $\frac{96}{30}$ $\frac{88}{39}$ $\frac{47}{50}$ $\frac{54}{75}$ $\frac{60}{75}$

$\frac{131}{75}$ $\frac{107}{58}$ $\frac{92}{45}$ $\frac{87}{34}$ $\frac{92}{31}$ $\frac{100}{26}$ $\frac{97}{21}$ $\frac{80}{16}$ $\frac{76}{8}$ $\frac{73}{12}$ $\frac{76}{18}$ $\frac{81}{22}$ $\frac{100}{26}$ $\frac{100}{30}$ $\frac{92}{38}$ $\frac{51}{44}$ $\frac{51}{47}$ $\frac{58}{75}$ $\frac{63}{75}$

$\frac{155}{75}$ $\frac{148}{62}$ $\frac{139}{57}$ $\frac{125}{43}$ $\frac{115}{33}$ $\frac{108}{26}$ $\frac{81}{16}$ $\frac{77}{8}$ $\frac{74}{12}$ $\frac{77}{18}$ $\frac{80}{23}$ $\frac{101}{27}$ $\frac{100}{29}$ $\frac{94}{37}$ $\frac{57}{54}$ $\frac{63}{75}$ $\frac{63}{75}$

Sta	+	π	-	Elev
		996.36		
32	+50			89.0
33				89.0
T.P.	4.17	993.19	7.34	989.02
	+35			89.0
	+55			89.0
	+70			89.2
34				89.2
	+50			89.1
35				89.1
	+50			89.0
36				88.5
	+50			88.0
B.M.			2.45	990.74

990.80

Lt.

K

Rt

$\frac{136}{75}$ $\frac{138}{50}$ $\frac{127}{35}$ $\frac{109}{27}$ $\frac{84}{19}$ $\frac{78}{9}$ $\frac{74}{11}$ $\frac{75}{16}$ $\frac{74}{22}$ $\frac{99}{28}$ $\frac{69}{36}$ $\frac{64}{40}$ $\frac{61}{56}$ $\frac{60}{75}$

$\frac{124}{75}$ $\frac{140}{55}$ $\frac{140}{44}$ $\frac{134}{36}$ $\frac{112}{28}$ $\frac{92}{23}$ $\frac{85}{17}$ $\frac{78}{9}$ $\frac{74}{11}$ $\frac{76}{16}$ $\frac{79}{23}$ $\frac{100}{28}$ $\frac{99}{37}$ $\frac{72}{42}$ $\frac{66}{60}$ $\frac{64}{75}$

$\frac{104}{75}$ $\frac{112}{65}$ $\frac{114}{47}$ $\frac{108}{37}$ $\frac{88}{28}$ $\frac{57}{21}$ $\frac{47}{9}$ $\frac{42}{11}$ $\frac{44}{16}$ $\frac{46}{24}$ $\frac{69}{28}$ $\frac{67}{33}$ $\frac{50}{38}$ $\frac{40}{35}$ $\frac{35}{L.O.}$

$\frac{104}{75}$ $\frac{112}{61}$ $\frac{113}{45}$ $\frac{105}{34}$ $\frac{87}{28}$ $\frac{54}{19}$ $\frac{46}{8}$ $\frac{42}{10}$ $\frac{44}{16}$ $\frac{46}{24}$ $\frac{68}{30}$ $\frac{67}{35}$ $\frac{38}{50}$ $\frac{37}{75}$

$\frac{56}{75}$ $\frac{61}{67}$ $\frac{63}{43}$ $\frac{61}{29}$ $\frac{53}{23}$ $\frac{48}{16}$ $\frac{44}{8}$ $\frac{40}{11}$ $\frac{44}{16}$ $\frac{46}{24}$ $\frac{67}{23}$ $\frac{67}{30}$ $\frac{37}{34}$ $\frac{35}{49}$ $\frac{32}{75}$

$\frac{83}{75}$ $\frac{89}{52}$ $\frac{80}{39}$ $\frac{73}{28}$ $\frac{62}{21}$ $\frac{47}{17}$ $\frac{43}{8}$ $\frac{40}{11}$ $\frac{44}{16}$ $\frac{41}{23}$ $\frac{65}{29}$ $\frac{63}{35}$ $\frac{36}{54}$ $\frac{33}{75}$

$\frac{72}{75}$ $\frac{56}{51}$ $\frac{49}{40}$ $\frac{41}{34}$ $\frac{56}{31}$ $\frac{75}{26}$ $\frac{72}{22}$ $\frac{44}{15}$ $\frac{43}{9}$ $\frac{41}{11}$ $\frac{43}{18}$ $\frac{45}{21}$ $\frac{62}{27}$ $\frac{60}{32}$ $\frac{33}{54}$ $\frac{27}{75}$

$\frac{63}{75}$ $\frac{56}{62}$ $\frac{49}{47}$ $\frac{58}{34}$ $\frac{56}{31}$ $\frac{73}{26}$ $\frac{70}{21}$ $\frac{45}{17}$ $\frac{43}{10}$ $\frac{41}{11}$ $\frac{43}{18}$ $\frac{43}{22}$ $\frac{63}{23}$ $\frac{63}{26}$ $\frac{53}{30}$ $\frac{34}{51}$ $\frac{29}{75}$

$\frac{36}{75}$ $\frac{38}{48}$ $\frac{44}{39}$ $\frac{59}{29}$ $\frac{70}{25}$ $\frac{67}{21}$ $\frac{48}{16}$ $\frac{45}{9}$ $\frac{42}{11}$ $\frac{46}{15}$ $\frac{47}{18}$ $\frac{55}{22}$ $\frac{68}{28}$ $\frac{63}{37}$ $\frac{30}{56}$ $\frac{29}{75}$

$\frac{47}{75}$ $\frac{39}{36}$ $\frac{48}{34}$ $\frac{73}{27}$ $\frac{74}{22}$ $\frac{52}{16}$ $\frac{47}{9}$ $\frac{41}{12}$ $\frac{50}{18}$ $\frac{52}{21}$ $\frac{68}{25}$ $\frac{67}{29}$ $\frac{58}{33}$ $\frac{44}{51}$ $\frac{38}{75}$

$\frac{49}{75}$ $\frac{49}{48}$ $\frac{44}{35}$ $\frac{78}{26}$ $\frac{76}{21}$ $\frac{57}{16}$ $\frac{54}{9}$ $\frac{52}{12}$ $\frac{56}{15}$ $\frac{57}{19}$ $\frac{81}{30}$ $\frac{82}{35}$ $\frac{54}{56}$ $\frac{53}{75}$

Top SW. Cor. Lower Cor. step at Ho. 100' Bl. sto 36+55

Sta	+	π	-	Elev
		993.19.		
37				87.3
T.P.	6.04	993.38.	5.05	987.34.
+50				86.6.
38				85.6.
+50				84.5.
39				83.3.
+42				81.8.
+52				81.5.
40				79.9.
T.P.	0.06	979.93.	13.51	979.87.
+38				78.5.
+70				77.6.
41				76.7.

LT

2

LT

$\frac{34}{75} \frac{38}{56} \frac{37}{36} \frac{81}{26} \frac{81}{22} \frac{65}{77} \frac{60}{8} \frac{57}{10} \frac{62}{15} \frac{64}{18} \frac{86}{30} \frac{87}{33} \frac{64}{51} \frac{66}{51} \text{ L.O.}$

Top Bellhop 2.56.37100

$\frac{12}{75} \frac{17}{65} \frac{25}{41} \frac{83}{27} \frac{86}{21} \frac{72}{15} \frac{69}{10} \frac{68}{11} \frac{71}{16} \frac{74}{20} \frac{97}{28} \frac{97}{33} \frac{76}{52} \frac{78}{75} \frac{91}{75}$

$\frac{0.2}{75} \frac{14}{58} \frac{29}{49} \frac{81}{32} \frac{98}{25} \frac{97}{21} \frac{84}{17} \frac{79}{9} \frac{78}{10} \frac{81}{15} \frac{84}{21} \frac{105}{30} \frac{106}{35} \frac{75}{75} \frac{90}{75}$

$\frac{27}{75} \frac{31}{57} \frac{34}{44} \frac{76}{35} \frac{107}{27} \frac{108}{21} \frac{97}{17} \frac{92}{14} \frac{71}{9} \frac{89}{17} \frac{92}{15} \frac{94}{21} \frac{115}{25} \frac{113}{30} \frac{103}{35} \frac{80}{60} \frac{90}{75} \frac{93}{75}$

$\frac{41}{75} \frac{47}{55} \frac{43}{43} \frac{81}{36} \frac{120}{28} \frac{120}{22} \frac{108}{19} \frac{104}{14} \frac{102}{9} \frac{101}{10} \frac{105}{16} \frac{109}{22} \frac{127}{27} \frac{124}{30} \frac{117}{37} \frac{84}{57} \frac{90}{75} \frac{97}{75}$

$\frac{49}{75} \frac{50}{65} \frac{48}{44} \frac{79}{39} \frac{133}{28} \frac{133}{22} \frac{120}{19} \frac{117}{9} \frac{116}{10} \frac{118}{15} \frac{121}{21} \frac{138}{25} \frac{138}{30} \frac{129}{36} \frac{103}{54} \frac{107}{75} \frac{116}{75}$

$\frac{52}{75} \frac{51}{64} \frac{52}{44} \frac{135}{27} \frac{136}{24} \frac{123}{20} \frac{120}{9} \frac{119}{11} \frac{123}{16} \frac{125}{21} \frac{141}{27} \frac{138}{32} \frac{141}{52} \frac{134}{75} \frac{132}{75}$

$\frac{87}{75} \frac{91}{55} \frac{99}{40} \frac{155}{27} \frac{154}{23} \frac{141}{18} \frac{136}{8} \frac{135}{11} \frac{138}{16} \frac{141}{21} \frac{151}{25} \frac{152}{30} \frac{142}{50} \frac{143}{75}$

$\frac{00}{75} \frac{09}{49} \frac{14}{33} \frac{36}{27} \frac{35}{22} \frac{19}{17} \frac{15}{10} \frac{14}{11} \frac{15}{15} \frac{18}{20} \frac{29}{27} \frac{28}{30} \frac{24}{30} \frac{29}{50} \frac{13}{75}$

$\frac{57}{75} \frac{42}{48} \frac{28}{30} \frac{48}{27} \frac{47}{21} \frac{29}{16} \frac{25}{9} \frac{23}{11} \frac{26}{15} \frac{28}{20} \frac{40}{28} \frac{39}{30} \frac{33}{60} \frac{30}{75} \frac{26}{75}$

$\frac{94}{75} \frac{74}{48} \frac{56}{29} \frac{56}{21} \frac{38}{15} \frac{35}{9} \frac{32}{11} \frac{34}{15} \frac{36}{26} \frac{37}{50} \frac{35}{75} \frac{25}{75}$ (Ent)

Sta	+	π	-	Elev
		979.93		
41	+50			751
42				73.6
T.P.	0.78	972.43	8.28	971.65
	+27			727
	+60			719
43				707
	+50			69.4
44				68.6
	+50			681
	+66			680
	+78	Profile Rd. Rk		68.0
	+90			68.0

Lt

R

Rt

126 102 89 77 54 50 48 53 59 81 78 86 78
75 50 37 25 17 10 11 20 28 31 50 75

150 131 120 105 79 73 67 63 67 76 106 124 128 135
75 52 40 29 22 18 10 10 19 29 39 50 75

(FL
716) 63.53

72 89 60 59 31 06 00 103 00 03 18 52 64 70 77
75 72 57 38 27 21 11 11 18 23 33 40 44 75

(R.T.K) 62.63

64 71 88 75 70 45 26 15 09 05 10 15 25 48 73 80 88
75 46 45 44 39 30 24 16 10 11 19 24 29 40 61 75

L.O. 81 71 40 29 22 17 20 27 56 6.2 81 84 83
35 53 25 19 17 10 18 28 30 39 55 75

L.O. 80 52 38 34 30 33 39 55 66 87 98 82 78 62
34 25 18 11 10 18 23 28 35 37 46 55 75

L.O. 82 65 51 43 38 43 46 59 79 86 95 83 73 61
29 26 20 11 12 19 24 30 33 37 46 59 75

82 72 80 58 47 43 47 57 64 81 85 104 89 80 70 62
52 42 30 21 11 17 21 24 29 31 35 39 59 64 75

L.O. 82 73 63 51 48 44 46 52 53
31 26 24 17 11 11 23 50

L.O. 82 74 57 49 44 46 48 50 48 49 53
30 26 18 11 11 23 50 80 100 150

L.O. 82 76 60 50 44 46 49 51
31 26 22 11 11 22 50

Sta	+	π	-	Elev
		972.431		
45				68.0
	+50			68.0
46				68.2
	+50			68.5
47				68.9
	+50			69.2
48				69.6
T.P.	7.70	977.431	2.78	969.651
	+34			70.0
	+64			70.3
49				70.8
	+26			71.2

Lt

E

Rt

$$L.O. \begin{array}{cccccccccccc} 82 & 76 & 55 & 49 & 44 & 46 & 54 & 73 & 82 & 83 & 77 \\ 31 & 27 & 20 & 11 & & 11 & 21 & 29 & 36 & 47 & 50 \end{array}$$

$$L.O. \begin{array}{cccccccccccc} 82 & 78 & 51 & 48 & 44 & 45 & 50 & 62 & 79 & 84 & 81 \\ 28 & 25 & 17 & 10 & & 11 & 18 & 25 & 31 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccc} 85 & 77 & 54 & 46 & 42 & 43 & 47 & 63 & 64 \\ 29 & 27 & 19 & 11 & & 11 & 18 & 28 & 50 \end{array}$$

$$\begin{array}{cccccccc} 84 & 81 & 78 & 71 & 48 & 42 & 39 & 41 & 49 & 46 & 48 \\ 50 & 37 & 30 & 26 & 17 & 10 & & 12 & 20 & 40 & 50 \end{array}$$

$$\begin{array}{cccccccc} 30 & 33 & 72 & 70 & 43 & 38 & 35 & 39 & 43 & 48 & 50 \\ 50 & 37 & 27 & 23 & 16 & 10 & & 10 & 18 & 24 & 50 \end{array}$$

$$\begin{array}{cccccccc} 20 & 24 & 64 & 63 & 38 & 35 & 32 & 36 & 43 & 45 \\ 50 & 37 & 27 & 23 & 15 & 10 & & 10 & 21 & 50 \end{array}$$

$$\begin{array}{cccccccc} 30 & 32 & 40 & 63 & 60 & 38 & 33 & 30 & 28 & 33 & 37 & 44 & 86 & 92 \\ 50 & 42 & 33 & 28 & 22 & 18 & 15 & 9 & & 11 & 15 & 20 & 31 & 50 \end{array}$$

$$\begin{array}{cccccccc} 75 & 83 & 106 & 104 & 85 & 82 & 77 & 74 & 80 & 84 & 100 & 145 & 149 & 199 \\ 50 & 35 & 28 & 23 & 19 & 16 & 9 & & 10 & 16 & 23 & 32 & 45 & 50 \end{array}$$

$$\begin{array}{cccccccc} 43 & 65 & 100 & 99 & 78 & 73 & 71 & 77 & 81 & 96 & 135 & 144 \\ 50 & 36 & 27 & 22 & 17 & 9 & & 11 & 16 & 21 & 29 & 50 \end{array}$$

$$\begin{array}{cccccccc} 20 & 33 & 93 & 93 & 74 & 69 & 66 & 70 & 74 & 81 & 101 & 111 & 97 & 106 & 112 \\ 50 & 39 & 26 & 23 & 18 & 10 & & 11 & 16 & 19 & 22 & 27 & 32 & 41 & 50 \end{array}$$

$$\begin{array}{cccccccc} 07 & 16 & 81 & 88 & 69 & 65 & 62 & 61 & 69 & 77 & 95 & 96 & 77 & 86 & 95 \\ 50 & 42 & 25 & 22 & 17 & 9 & & 11 & 15 & 20 & 22 & 28 & 32 & 42 & 50 \end{array}$$

Sta	+	π	-	Elev.
		977.43		
49	+60			71.6.
50				72.1.
	+35			72.5.
	+68			72.7.
51				72.8.
	+50			72.9.
52				73.3.
	+33			73.4.
	+41			73.5.
	+58.3 ³			73.3.
	Profile X Road.			
	+72			73.1.

LH

E

RH

25 44 87 87 64 59 58 63 65 72 87 89 89 62 77
 50 37 26 23 18 11 11 14 19 21 25 29 34 50

47 64 85 85 60 57 53 57 60 65 79 81 71 43 54
 50 32 26 22 16 9 10 15 19 22 25 30 35 50

61 75 85 85 71 57 52 49 53 56 61 72 75 70 33 33 38
 50 29 27 22 18 14 9 11 15 18 22 25 29 37 43 50

68 76 81 81 53 50 47 52 54 58 70 73 69 31 27 28
 50 29 27 22 14 9 12 15 19 22 24 29 37 42 50

74 73 78 77 52 50 46 52 56 68 69 65 34 37
 50 28 27 23 15 9 13 18 22 25 29 32 50

79 79 77 76 50 47 45 50 54 68 68 51 52
 50 26 27 22 15 10 13 17 22 28 33 50

71 67 47 44 41 46 50 52 35 46
 50 23 17 9 14 19 28 32 50

78 67 48 41 40 44 60 63
 50 37 28 10 16 29 50

43 46 41 39 44 64
 50 44 73 16 50

87 83 37 40 410 48 57 73 83 85 81 69
 150 100 50 25 25 50 100 150 200 250 300

42 46 43 43 50 61
 36 26 9 23 50

Sta	+	π	-	Elev
		977.43		
52	+90			72.7
53				72.4
B.M.	207	973.40	4.10	973.33 (973.29)
	+50			71.7
54				71.1
	+45			70.2
	+70			69.5
55				68.9
	+29 X Drain			68.4
	+59			67.9
56				67.3
T.P.	3.75	971.12	8.03	963.57
	+50			66.8

Lt.

L

Rt.

111 99 76 53 49 47 52 61 59 48 51
50 45 33 19 10 76 31 33 43 50

115 94 65 54 51 50 54 61 51 46 50
50 35 22 15 8 15 29 35 44 50

Top Mont. Co. Rd "B" + Cleveland Ave.

81 66 71 65 44 40 37 40 45 59 58 44 34 34
50 34 32 21 15 10 12 19 22 28 33 37 50

38 31 48 68 68 52 47 43 48 50 55 66 64 31 36
50 37 32 27 23 18 10 12 15 20 23 28 36 50

00 109 18 60 71 72 61 57 55 52 56 61 67 81 84 75 91
50 39 34 30 25 21 19 15 11 13 16 19 22 27 32 50

06 09 31 73 81 67 61 59 61 69 91 97 110
50 39 34 28 22 19 10 12 18 22 32 50

33 50 68 73 91 92 80 71 69 65 68 77 109 114 113 141 144 125
50 41 36 33 28 22 20 15 10 12 18 25 35 43 46 49 50

(FL. 6063
CULV

70 88 96 110 114 86 79 75 70 74 84 117 127 147 143 101 102
50 38 34 27 22 19 17 11 12 18 24 29 29 32 35 50

101 110 118 124 123 87 80 75 79 85 119 110 94 92
50 36 30 28 25 18 10 11 18 22 29 35 50

134 132 147 147 118 97 89 85 81 85 90 114 106 77 69
50 32 31 29 25 20 16 11 12 18 22 30 36 50

109 106 97 85 56 49 43 46 52 68 69 57 39 43 37
50 35 34 28 20 11 12 18 22 29 33 36 39 50

Sta	+	Σ	-	Elev
		971.12		
57				66.6
T.P	3.92	970.07	4.97	966.15
+23				66.6
+73				66.2
58				66.2
+50				66.0
59				65.9
+50				65.8
60				65.6
+50				65.6
+60 X Drain				65.5
61				65.6

Lt

R

Pt

96 95 87 80 44 56 50 45 47 55 66 65 49 27 33 2.5
50 35 34 30 23 18 11 11 19 23 28 34 37 39 50

9.56.58.100

68 69 65 58 42 41 35 37 44 59 51 17 23 1.5
50 31 30 25 14 11 11 17 21 29 36 39 50

53 58 42 46 45 39 41 46 66 63 48 45
50 34 26 16 11 12 16 23 27 36 50

68 68 64 61 48 46 39 44 48 68 66 58 5.8
50 36 33 26 17 11 12 15 23 32 41 50

97 93 88 83 60 50 47 41 45 51 68 67 61 62
50 35 31 30 21 15 11 12 16 22 29 33 50

105 103 102 94 72 53 46 42 44 48 65 63 48 50
50 37 36 34 26 18 12 11 17 23 28 37 50

106 103 89 72 57 46 43 46 59 75 74 69 74
50 36 35 24 20 12 11 17 24 32 35 50

101 103 93 78 59 48 45 49 57 88 90 90
50 35 34 23 18 12 11 17 23 33 50

102 107 97 80 58 50 45 48 56 97 100 101
50 35 33 25 17 11 12 17 25 35 50

(Culv) 57.00

(Culv) 57.67

103 109 116 130 101 92 78 58 50 46 49 55 96 101 124 115 106 102
50 41 33 33 32 29 24 17 11 12 11 26 34 35 35 38 50

100 100 80 58 50 45 48 56 96 102 105
50 32 25 18 11 12 18 26 30 50

Sta	+	π	-	Elev
		970.27		
61	+45			65.8
	+70			66.0
T.P.	822	974.30	3.99	966.08
62				66.1
	+36			66.0
	+50			66.0
63				65.7
	+33			65.3
	+66			64.9
64				64.4
	+26			63.8
	+65			62.7

Lt.

C

Pt.

68 90 92 88 67 54 45 43 46 51 81 85 80
50 39 35 28 23 18 11 12 19 28 40 50

57 71 69 62 55 45 43 41 45 50 68 70 59 62 52
50 41 35 24 21 16 12 12 18 23 29 31 44 50

63 60 66 69 98 98 87 84 82 85 88 100 94 98 37
50 37 35 34 27 23 15 11 12 16 23 29 38 50

30 28 59 63 87 93 87 84 83 86 90 94 84 23 23
50 49 37 34 29 22 19 11 19 12 23 31 39 50

26 26 62 64 87 96 96 85 84 83 85 90 83 54 49
50 42 35 29 24 22 17 12 13 18 29 36 50

28 34 71 71 76 97 92 87 86 91 96 94 83 62 54
50 42 35 34 33 23 19 13 12 18 26 32 35 50

30 35 68 68 85 99 96 91 90 94 99 92 65 59
50 42 34 33 31 23 20 13 12 20 30 35 50

58 55 70 72 99 105 96 94 97 99 108 108 94 70 63
50 39 35 33 28 21 14 11 17 23 26 31 35 50

138 115 106 106 115 117 104 103 99 100 100 106 113 113 104 77 68
50 36 34 32 30 23 17 14 10 18 22 24 25 29 35 50

159 140 123 123 111 105 104 105 110 120 120 110 80 84
50 36 23 22 15 11 17 22 23 26 30 38 50

128 106 104 113 134 134 124 119 116 117 121 129 129 116 77 78
50 38 35 33 27 24 17 12 12 19 23 26 32 39 50

Sta.	+	π	-	Elev.
		974.30		
65				61.6.
T.P.	521	966.83	12.68	961.62
+50				60.0.
66				59.0.
(+50)				(58.3.)
+76.17 Profile S.T.H. 36				57.9.
(67)				(57.3.)
T.P.	010	955.67.	11.26	955.57.
+50				55.6.
68				53.7.
+50				51.8.
69				50.1.
+33 X Drain				49.5.

Lt

L

Rt

$\frac{100}{50} \frac{100}{40} \frac{108}{35} \frac{136}{50} \frac{142}{26} \frac{142}{23} \frac{137}{19} \frac{129}{12} \frac{127}{19} \frac{128}{19} \frac{134}{19} \frac{137}{24} \frac{133}{30} \frac{79}{39} \frac{75}{50}$

$\frac{53}{50} \frac{46}{46} \frac{46}{37} \frac{53}{32} \frac{81}{28} \frac{78}{18} \frac{71}{14} \frac{68}{13} \frac{70}{20} \frac{76}{30} \frac{74}{37} \frac{38}{50} \frac{41}{50}$

$\frac{83}{50} \frac{72}{36} \frac{103}{28} \frac{103}{25} \frac{85}{16} \frac{83}{13} \frac{78}{15} \frac{81}{19} \frac{88}{23} \frac{100}{29} \frac{96}{35} \frac{78}{50} \frac{85}{50}$

85

$\frac{146}{200} \frac{129}{150} \frac{112}{700} \frac{100}{50} \frac{89}{50} \frac{82}{50} \frac{76}{100} \frac{73}{150} \frac{73}{200}$

95

$\frac{97}{50} \frac{85}{40} \frac{32}{28} \frac{08}{20} \frac{95}{13} \frac{01}{19} \frac{03}{21} \frac{06}{27} \frac{32}{36} \frac{76}{45} \frac{86}{50} \frac{89}{50}$

$\frac{86}{50} \frac{85}{31} \frac{67}{26} \frac{28}{18} \frac{25}{19} \frac{22}{12} \frac{21}{16} \frac{25}{24} \frac{63}{36} \frac{97}{36} \frac{108}{50}$

$\frac{105}{50} \frac{88}{28} \frac{70}{22} \frac{47}{18} \frac{42}{15} \frac{39}{12} \frac{41}{14} \frac{44}{18} \frac{52}{21} \frac{64}{31} \frac{107}{40} \frac{121}{50} \frac{128}{50}$

$\frac{78}{50} \frac{83}{36} \frac{84}{24} \frac{64}{17} \frac{60}{13} \frac{56}{12} \frac{60}{18} \frac{64}{23} \frac{118}{29} \frac{135}{38} \frac{180}{50}$

(FL. Cont.) 42.38

(FL. Cont.) 42.43

$\frac{120}{50} \frac{118}{34} \frac{129}{34} \frac{129}{32} \frac{132}{32} \frac{78}{21} \frac{70}{16} \frac{67}{13} \frac{62}{12} \frac{65}{18} \frac{72}{23} \frac{93}{29} \frac{113}{35} \frac{132}{36} \frac{129}{50} \frac{126}{50}$

Sta	+	π	-	Elev
		955.67		
69	+68			49.2.
70				48.9.
	+35			48.7.
B.M.	8.90	957.16	7.41	948.26. (948.23)
	+70			48.7.
71				48.9.
	+50			49.1.
72				49.2.
	+35			49.1.
	+70			49.0.
73				48.9.
	+30			48.5.

Lt

L

Pt

130	125	92	81	72	65	68	73	103	103	96
50	29	21	17	13	13	17	24	32	30	

144	131	80	77	74	68	70	74	91	89	71	60
50	32	21	15	12	11	17	22	27	32	50	

136	136	127	112	80	75	70	71	75	89	89	80	50	4.3
50	45	31	25	17	12	12	17	21	24	30	35	50	

spk in 24"0. 35.4/50. 71+25

132	123	107	93	88	85	87	92	105	100	93	71	6.3
50	27	22	16	10	12	18	22	27	31	35	50	

115	105	111	109	95	88	83	87	94	103	96	73	65
50	30	28	23	18	12	10	20	22	25	29	34	50

101	88	98	97	91	85	81	85	90	95	101	101	91	58	53
50	30	27	26	18	12	10	17	21	22	25	30	37	50	

92	81	93	96	88	84	80	82	84	94	94	85	55	58
50	31	28	23	17	13	10	16	24	24	30	38	50	

91	73	65	78	81	90	94	86	84	81	83	88	92	98	79	44	47
50	42	35	32	30	28	23	18	12	11	17	22	25	32	39	50	

114	80	70	90	88	85	82	85	88	95	98	85	29	40
60	38	33	28	20	18	10	17	22	25	32	39	50	

152	90	95	87	83	86	88	102	102	87	38	36
50	29	28	12	10	16	22	26	33	42	50	

170	137	101	91	87	90	93	99	99	91	24	20
50	34	24	13	11	18	24	27	31	43	50	

Sta	+	π	-	Elev
		957.16		
73	+70			47.8
74				47.3
T.P.	3.90	950.17	10.89	946.27
	+30			46.9
	+70			46.4
75				45.9
	+50			44.8
76				43.3
	+50			41.9
77				40.6
B.M.	4.54	943.71	10.97	939.20
	+27	944.74		40.0
	+27			
	+62	X Drain		39.3

939.17 ✓

8-6-41
F.A.
L.G.
A.M.
C.F.
C.N.

11

2

21

$\frac{20.8}{50} \quad \frac{16.7}{37} \quad \frac{128}{25} \quad \frac{108}{20} \quad \frac{101}{19} \quad \frac{94}{10} \quad \frac{96}{18} \quad \frac{99}{24} \quad \frac{104}{30} \quad \frac{96}{44} \quad \frac{27}{44} \quad \frac{27}{50}$

$\frac{20.1}{50} \quad \frac{184}{37} \quad \frac{157}{35} \quad \frac{113}{20} \quad \frac{105}{19} \quad \frac{99}{11} \quad \frac{101}{21} \quad \frac{110}{29} \quad \frac{104}{42} \quad \frac{55}{42} \quad \frac{46}{50}$

$\frac{148}{50} \quad \frac{14.0}{46} \quad \frac{83}{29} \quad \frac{52}{22} \quad \frac{43}{19} \quad \frac{38}{13} \quad \frac{33}{11} \quad \frac{36}{18} \quad \frac{41}{21} \quad \frac{50}{29} \quad \frac{44}{30} \quad \frac{2.8}{35} \quad \frac{26}{50}$

$\frac{14.4}{50} \quad \frac{111}{40} \quad \frac{72}{28} \quad \frac{50}{22} \quad \frac{42}{11} \quad \frac{38}{11} \quad \frac{4.0}{11} \quad \frac{4.3}{16} \quad \frac{6.0}{23} \quad \frac{56}{29} \quad \frac{48}{34} \quad \frac{45}{41} \quad \frac{44}{50}$

$\frac{148}{50} \quad \frac{11.0}{39} \quad \frac{68}{28} \quad \frac{5.7}{20} \quad \frac{50}{17} \quad \frac{47}{12} \quad \frac{4.3}{16} \quad \frac{46}{16} \quad \frac{51}{23} \quad \frac{6.5}{28} \quad \frac{61}{32} \quad \frac{50}{40} \quad \frac{5.3}{50}$

$\frac{132}{50} \quad \frac{125}{46} \quad \frac{70}{29} \quad \frac{60}{16} \quad \frac{58}{12} \quad \frac{54}{10} \quad \frac{57}{15} \quad \frac{61}{21} \quad \frac{7.7}{27} \quad \frac{76}{32} \quad \frac{52}{32} \quad \frac{6.8}{50}$

$\frac{135}{50} \quad \frac{105}{40} \quad \frac{87}{35} \quad \frac{79}{20} \quad \frac{72}{12} \quad \frac{6.9}{11} \quad \frac{72}{16} \quad \frac{76}{22} \quad \frac{87}{27} \quad \frac{8.7}{32} \quad \frac{6.3}{32} \quad \frac{6.5}{50}$

$\frac{17.0}{50} \quad \frac{15.2}{39} \quad \frac{137}{33} \quad \frac{100}{23} \quad \frac{92}{18} \quad \frac{88}{11} \quad \frac{86}{11} \quad \frac{91}{26} \quad \frac{102}{23} \quad \frac{95}{29} \quad \frac{85}{33} \quad \frac{85}{34} \quad \frac{90}{38} \quad \frac{8.9}{50}$

$\frac{173}{50} \quad \frac{155}{33} \quad \frac{116}{22} \quad \frac{105}{16} \quad \frac{101}{12} \quad \frac{96}{11} \quad \frac{99}{17} \quad \frac{102}{23} \quad \frac{109}{27} \quad \frac{125}{33} \quad \frac{133}{36} \quad \frac{137}{36} \quad \frac{136}{50}$

Top Mast sta 78+

$\frac{104}{50} \quad \frac{87}{31} \quad \frac{55}{24} \quad \frac{48}{16} \quad \frac{45}{12} \quad \frac{37}{10} \quad \frac{41}{16} \quad \frac{47}{21} \quad \frac{53}{29} \quad \frac{80}{29} \quad \frac{86}{33} \quad \frac{87}{50}$

(total) 3147

(total) 3279

$\frac{98}{50} \quad \frac{111}{32} \quad \frac{12.24}{32} \quad \frac{92}{30} \quad \frac{68}{25} \quad \frac{56}{19} \quad \frac{47}{12} \quad \frac{44}{10} \quad \frac{46}{18} \quad \frac{53}{28} \quad \frac{80}{31} \quad \frac{1872}{31} \quad \frac{98}{31} \quad \frac{85}{38} \quad \frac{7.2}{50}$

Sta	+	π	-	Elev
		943.74 944.74		
78				39.1
	+50			39.1
79				39.3
	+50			39.4
80				39.9
	+50			41.0
81				42.5
	+35			43.7
	+73			45.1
T.P.	12.16	955.42 956.45	0.45	943.26 944.29
	+73			45.1
82				46.2

8-7-91
K.P.
L.G.
A.M.
C.F.
C.N.

L1

2

R1

10.3 9.9 7.0 5.7 5.9 4.6 5.0 5.2 6.3 7.6 7.5 7.2 6.3
50 34 25 18 12 10 14 21 26 32 41 50

10.4 10.0 6.8 5.8 5.2 4.6 4.9 5.1 5.8 7.1 7.1 6.2 5.7
50 34 25 19 12 11 15 20 25 32 43 50

10.7 9.9 8.7 6.6 5.6 4.8 4.4 4.6 5.2 6.7 7.8 7.5 6.9 5.7
50 33 28 23 18 12 10 16 22 27 32 40 50

11.0 10.6 6.5 5.1 4.9 4.3 4.6 5.4 7.9 7.4 6.9 6.2
50 37 23 16 12 10 18 26 32 43 50

10.8 10.5 5.9 4.8 4.3 3.8 4.0 4.6 5.5 7.2 7.7 7.0
50 38 22 16 10 9 17 22 29 33 50

10.7 9.9 5.4 4.1 3.4 2.7 2.7 3.2 3.8 6.1 6.4 6.3
50 37 23 18 10 10 15 19 31 32 50

10.6 9.0 3.6 2.5 1.7 1.2 1.3 2.0 3.4 3.4 3.5 2.3
50 40 22 16 9 10 18 29 33 44 50

10.4 9.3 2.7 1.3 0.6 0.0 0.0 0.5 1.1 1.5 0.0 +1.7
50 44 21 16 9 10 17 29 34 43 50

34.8
37.4
41.2
89 6.3 2.5
50 38 24

+1.5

11.4 10.8 10.3 10.4 10.3 10.1 9.7 8.2 5.8 3.9
15 9 11 17 28 32 35 44 50

1.86 1.53 1.18 1.07 9.6 9.2 9.4 9.4 9.0 1.1 1.4.9
50 32 20 17 9 10 22 31 46 7.5

✓

Sta	+	π	-	Elev
		955.42 956.45		

82 +35

47.5

+70

48.7

83

49.9

+35

51.2

+70

52.3

84

53.2

T.P.

13.15

966.34
967.57

2.23

953.19
954.42

82 +35

47.5

+70

48.7

Lt

R

Rt

166 141 127 9.5 8.9 8.3 7.9 8.1 8.3 6.5 1.3
50 31 26 21 16 8 12 19 34 46

116 106 89 86 89 9.0 8.0 7.1 6.7 6.8 7.0 4.9 1.9
50 38 29 27 26 23 20 8 12 18 35 43

6.0 4.7 7.1 6.7 5.8 5.5 5.6 5.5 3.4 1.9
50 34 28 23 8 12 21 35 40

1.0 0.0 5.2 5.2 4.4 4.2 4.3 4.6 2.4 0.3
50 37 27 22 8 12 21 35 41

2.4 1.1 4.1 4.0 3.4 3.1 3.1 3.4 2.5 0.9
50 34 27 22 8 12 21 31 35

3.9 3.0 3.3 3.5 3.5 3.4 2.6 2.2 2.3 2.2 1.0
50 37 34 33 28 18 9 12 22 34

(18.8) 4.2 1.0
61 75

(17.6) +1.0 +2.4
67 75

Sta.	+	π	-	Elev.
		966.34		
		967.57		

83

49.9

+35

51.2

+70

52.3

84

53.2

+35

54.2

+50

54.9

85

55.9

+34

56.7

Lt

2

Rt

16.4

+30	+4.0	S.S.
69	75	

15.1

+1.8	+2.6	S.S.
66	75	

14.0

0.2	0.3	+0.3	S.S.
59	64	75	

13.1

1.7	1.0	S.S.
55	75	

139	141	140	130	127	121	124	126	132	117	2.5	1.1
50	41	24	16	9		12	19	26	33	50	75

124	129	126	117	114	117	123	123	110	38	25
50	29	18	9		13	22	28	33	47	60

93	109	125	115	107	104	106	108	121	118	73	64
50	30	27	19	9		12	18	23	29	39	50

112	114	123	120	113	107	109	96	97	99	117	113	84	82
50	31	27	22	20	17	9		12	17	23	27	34	50

Sta	+	Δ	-	Elev.
		966.34 967.57		
85	+79			57.6.
86				58.0.
	+30			58.6.
	+70			58.9.
87				59.3.
T.P.	9.65	968.92. 970.15	1.07	959.27. 960.50
	+50			59.9.
88				60.5.
	+40			60.9.

Lt

4

Rt

138 130 108 95 91 87 88 92 127 102 88 88
50 32 21 15 9 12 19 23 29 33 50

129 125 121 93 88 83 84 83 100 100 92 92 88
50 32 21 16 9 12 18 23 28 30 37 50

106 103 90 83 77 78 77 91 93 84 84 80
50 31 27 9 12 17 23 28 29 36 50

111 105 98 89 80 74 73 73 86 68 65
50 30 29 21 11 12 17 23 28 50

115 110 92 81 75 70 70 72 85 81 69 54
50 30 27 17 9 11 17 22 27 30 50

114 122 107 101 94 90 90 93 108 106 101
50 30 25 20 10 13 17 22 29 50

55 57 70 97 92 87 84 86 87 102 102 97
50 44 32 27 18 9 12 17 22 32 50

100 93 99 89 85 80 81 84 92 89 81
50 29 24 17 9 14 18 23 30 50

Sta	+	π	-	ELEV
		968.92 970.15		
88	+70			61.1.
89				61.2.
	+50			60.9.
90				60.1.
	+31			59.3.
	+70			57.9.
91				56.6.

(89 +79	Top M.H. L.H.	8.63	960.29)
	955.48		955.47
T.P.	0.01	956.71	13.45
			956.70

Lt

R

Rt

114 108 97 87 8.2 7.8 8.0 8.2 8.4 78 6.0
 50 45 27 17 8 14 19 25 30 50

9.5 7.8 9.2 8.5 8.0 7.7 7.8 8.1 8.5 8.5 6.8 4.7 3.5
 50 32 26 17 7 14 18 21 26 32 37 50

6.2 5.0 5.3 9.0 8.6 8.3 8.0 8.2 8.5 9.5 9.5 +1.7 +1.4
 50 43 35 28 16 9 15 18 24 28 48 75

6.9 5.8 5.8 8.9 10.0 9.6 9.2 8.8 9.0 9.5 10.7 10.3 5.2 +3.2 +3.5
 50 45 37 31 24 17 7 14 19 23 28 39 55 75

6.9 6.0 6.2 9.8 10.6 10.5 9.9 9.6 9.8 10.3 11.4 11.4 4.4 12.0 +2.6
 50 49 36 29 25 18 7 14 18 22 28 42 53 75

9.0 8.0 8.1 12.1 12.5 11.7 11.4 11.0 11.2 11.5 13.0 12.6 3.1 2.4
 50 43 36 28 24 16 7 15 18 23 29 46 60

12.4 10.5 13.5 13.8 13.0 12.8 12.3 12.2 12.4 12.6 14.1 13.0 7.7 6.8
 50 34 28 23 15 7 5 14 18 22 29 40 50

Sta	+	T	-	Elev.
		955.48 956.71		
91	+50			54.5
B.M.			0.83	954.65 955.88
				954.69
92				52.3
	+32			50.9
	+70			49.4
93				48.4
	+40			46.9
	+75			45.4
T.P.	0.13	944.49 945.72	11.12	944.36 945.59
93	+75			45.4

Lt

R

Rt

7.5 4.4 3.9 3.0 2.0 1.5 1.0 0.9 1.3 1.5 1.9 2.0 4.0 5 12.0
 50 33 31 25 15 7 5 14 19 21 25 30 50

Top Great Lakes Pipe Line sta. marker 25' Lt sta 94 54

141 13.6 11.4 9.4 4.0 3.6 3.2 3.0 3.4 3.6 4.3 2.9 3.5
 50 45 33 26 16 8 6 14 18 24 38 50

148 14.2 11.5 7.7 5.6 5.3 4.6 4.5 4.7 5.2 6.6 6.1 5.8
 50 45 32 22 16 8 6 15 20 28 37 50

116 12.1 11.7 10.5 6.8 6.7 6.1 6.0 6.4 6.7 7.5 7.4
 50 43 32 27 16 7 6 14 19 24 50

12.7 10.0 7.9 7.6 7.1 7.0 7.2 7.7 8.2 8.2 7.8 7.8
 50 29 18 7 6 14 20 22 24 27 50

19.2 16.2 12.5 9.7 9.1 8.6 8.5 8.7 8.8 10.5 10.8 10.5
 50 32 23 16 7 5 13 17 23 39 50

11.2 10.6 10.1 10.0 10.2 10.5 12.2 12.2
 16 8 4 13 18 23 50

Q sta 94 100

123 101 37
 50 34 26

+0.9

Sta	+		-	Elev
		944.49.		
		945.72		
94				44.4.
	+50			42.1.
95				40.0.
	+50			38.3.
96				37.0.
T.P.	2.02	938.21.	8.30	936.19.
		939.44		937.42
	+50			35.8.
97				34.5.
	+50			33.6.

L1

2

R1

134 112 115 11 04 01 0.0 04 06 2.3 3.4 39 36
50 34 29 15 8 6 13 18 24 32 40 50

156 133 9.7 37 28 24 23 26 30 56 6.7 8.2 7.7
50 34 27 17 8 6 14 18 26 32 40 50

166 156 103 7.3 57 49 45 44 48 52 84 10.3 10.5 10.5
50 34 25 20 14 7 6 14 18 26 32 40 50

17.1 158 131 7.9 71 67 62 61 63 70 10.2 11.8 12.2
50 33 28 19 14 7 6 13 18 26 33 50

159 142 9.0 8.3 78 7.5 7.5 7.8 8.2 10.8 12.2 13.2 13.3
50 30 19 14 8 5 13 17 24 32 38 50

87 67 3.3 26 24 24 27 31 5.7 6.8 8.2 84
50 30 18 8 6 13 19 26 32 41 50

106 90 44 4.0 37 36 38 41 62 74 80 9.2 97
50 28 16 8 4 12 16 25 30 34 45 50

112 101 55 50 46 43 48 54 85 10.9 11.4
50 27 17 8 5 13 19 27 36 50

Sta	+	T	-	Elev
		938.21 939.44		
98				32.9
+50				32.3
+75				31.8
99				31.4
+50				30.8
100				30.2
T.P.	6.31	936.56 937.79	7.96	930.25 931.48
+50				29.5
101				28.7

L.

Z

R.

10.9 10.9 7.8 6.1 5.7 5.3 5.2 5.5 6.2 9.2 10.6 11.5 11.7
 50 28 21 16 9 3 12 18 27 32 37 50

8.7 9.0 7.3 6.4 6.1 5.9 5.9 6.3 6.6 9.3 11.3 11.7 12.5
 50 25 20 14 8 3 11 16 24 32 35 50

6.1 6.5 7.1 6.7 6.5 6.4 6.4 6.7 7.2 10.1 11.5 12.3 12.8
 50 24 22 11 9 3 11 16 26 33 35 9

5.6 6.3 7.1 6.9 6.8 7.0 7.3 9.4 11.7 12.9 13.2
 50 23 21 9 11 14 23 32 38 50

6.1 6.7 7.3 7.8 7.6 7.4 7.7 8.1 8.5 10.5 12.2 13.0 13.1
 50 22 21 15 9 11 16 20 25 32 35 50

5.0 6.2 7.5 8.5 8.2 8.0 8.3 8.8 11.1 11.9 12.2 12.4
 50 33 23 21 9 11 18 26 33 40 50

4.6 4.6 5.9 7.9 7.3 7.1 7.3 7.6 8.2 7.1 6.5 7.1
 50 38 27 22 9 11 20 24 27 38 50

7.3 8.7 10.2 10.4 9.1 8.1 7.9 8.1 8.7 9.7 9.5 10.2 12.6
 50 37 27 23 17 9 11 19 21 28 33 43 50

Sta	+	π	-	Elev
		936.56 927.79		
101	+30			27.9'
	+70			26.6'
102				25.6'
T.P.	0.09	925.61 926.84	11.04	925.52' 926.75'
	+33			24.2'
	+60			23.2'
	+79			22.5'
103	Parallel to tracks			21.4'
+04	" " "			21.3'

Lt

L

Rt

8.7 7.9 7.5 10.8 11.0 9.4 9.0 8.7 9.1 9.5 11.0 10.2 8.6 3.2
 50 46 36 27 23 17 10 12 17 22 29 46 50

10.0 8.0 7.6 12.2 12.3 10.9 10.3 10.0 10.4 10.9 12.3 12.3 8.2 9.1 9.5
 50 44 38 28 22 18 10 10 17 21 28 36 43 50

11.8 10.1 9.2 10.0 13.4 13.4 12.1 11.5 11.0 11.4 11.8 13.7 14.0 13.8 14.6 15.2
 50 44 42 36 28 23 17 11 10 17 24 29 33 39 50

2.4 1.8 2.4 4.1 3.5 1.9 1.7 1.4 1.6 2.2 3.7 6.2 6.8 6.8
 50 46 31 26 20 16 11 10 18 22 33 42 50

4.8 3.6 4.2 4.2 2.9 2.5 2.4 2.7 3.3 6.7 8.3 8.4 8.6
 50 31 29 20 16 11 9 17 28 35 44 50

7.0 5.8 5.3 2.8 3.3 2.1 3.3 3.7 4.6 8.4 9.2
 50 38 24 18 11 8 14 19 31 50

(10let)

6.2 6.0 5.0 4.2 4.3 4.2 4.2 4.2 6.9 8.7 10.3 5.7 7.3
 50 39 28 18 11 7 15 24 27 30 34 50

5.3 5.2 4.3 4.3 4.2 4.7 5.1 5.1
 50 27 12 9 17 31 50

Sta	+	Σ	-	Elev	
		925.61			
		926.89			
103	+07.4	Top Rail		21.26	
	+12.4	" "		21.25	
	+17	Parallel to track		21.1	
	+26	" " "		20.9	
	+26	Outlet of Cul. Rt 1053			
	+60			19.9	
104				18.6	
	+50			17.1	
B.M.	2.37	61	10.45	915.16	915.24
		917.42		916.39	

Lt

R

Rt

4.44 4.35 4.36
15 15

4.48 4.36 4.37
15 15

5.5 5.5 4.5 4.5 4.8 5.6 5.1
50 29 12 8 16 29 50

9.5 7.5 5.3 4.8 4.7 4.9 5.4 10.0 9.3 10.9
50 26 19 11 9 18 26 29 50

11.3 9.3 6.3 5.9 5.7 5.9 6.2 6.6 9.5 11.0 11.5
50 28 17 11 8 12 19 26 33 50

14.5 13.0 11.5 10.0 7.9 7.2 7.0 7.2 7.8 11.0 12.4 12.4
50 45 30 24 18 11 9 17 26 38 50

13.1 11.4 10.8 9.5 9.0 8.5 8.8 9.3 12.8 13.4
50 35 22 16 11 10 17 29 50

Top Mont. Co. Rd. 6' x Cleveland

Sta + π - Elev.

917.42^{61'}

104 +89

16.0'

105

& only

1.9

15.7'

+04

15.7'

+14.14

See Cont'd C. Plan
Survey for Profile

15.4'

+32

14.8'

+41

14.5'

+72

13.8'

106

13.3'

Lt

L

Rt

5.3 42 31 19 16 17 24 28 50 59 Inlet
50 36 25 12 9 20 25 33 45 45 50

4.0 2.8 2.1 1.9 2.0 2.2 2.8 2.8
50 25 10 9 21 37 50

5.1 29 22 2.3 1.5
100 50 50 100

6.0 5.2 39 31 28 2.8 2.9 3.3 2.9
50 39 27 12 10 21 35 50

37 4.8 59 60 5.3 4.0 35 31 33 3.7 4.4 6.8 6.6
50 39 33 28 26 20 10 10 20 26 37 50

41 71 72 4.7 4.3 3.8 4.1 4.5 7.2 85 71
50 35 24 17 11 10 17 22 32 50

2.5 53 64 7.0 71 52 4.5 4.3 4.6 5.0 83 9.0 82
50 40 33 28 23 18 10 10 14 23 34 50

sta	+	T	-	Elev
		917.4 ⁶¹		
106	+50			12.9'
	+74			12.7'
107				12.6'
	+50			12.2'
108		914.82		12.0'
T.P.	3.27	914.63	6.06	11.55'
				11.36'
	+27			11.8'
	+54			11.6'
109				11.2'

Lt

R

Rt

12 47 7.8 8.1 5.4 4.9 4.7 5.2 5.8 10.2 10.5
50 39 29 23 18 9 11 16 23 50

0.0 5.6 7.8 8.0 5.5 5.2 4.9 5.4 6.2 9.8 11.1 11.1
50 34 28 24 19 9 11 17 23 38 50

11.0 10.8 3.5 7.8 8.0 5.7 5.3 5.0 5.5 6.2 10.2 11.2
50 47 38 28 24 17 9 10 17 25 50

8.2 3.5 3.6 8.6 8.5 6.2 5.6 5.7 5.8 6.3 9.9 10.8 11.5
50 41 39 28 24 18 9 11 15 25 36 50

12.7 11.9 9.0 9.6 9.5 6.4 5.9 5.6 5.9 6.4 8.4 10.4 10.6 11.2
50 43 30 28 25 17 9 11 19 24 35 46 50

11.2 9.6 8.7 3.9 3.3 3.0 3.2 3.6 4.0 3.2 6.1 7.7
50 37 31 18 9 10 17 22 29 37 50

11.4 9.5 4.0 3.5 3.2 3.4 4.0 3.2 3.3 6.6
50 35 18 9 10 21 33 42 50

11.9 10.9 8.9 4.6 4.0 3.6 3.7 4.1 3.5 3.2
50 40 31 17 9 11 21 32 50

5/4

+

T⁸²

-

Elev

914.62

109 +50

10.9'

110

10.4'

+50

09.7'

111

09.1'

+50

T.P.

1.00

56

908.37

7.26

08.5'

907.56

112

07.6'

+38

06.8'

+50

06.5'

8-1-41
K.H.
L.G.
A.M.
C.F.
C.N.

Lt.

K.

Rt.

121 108 76 47 43 39 42 44 3.5
50 38 26 17 9 11 26 50

119 103 54 48 44 4.8 4.9 4.4
50 36 22 9 11 29 50

112 96 88 62 55 51 54 5.0 47 3.2
50 35 30 22 9 11 30 45 50

112 96 91 74 65 61 57 60 5.8 54 45
50 37 32 26 18 9 12 31 45 50

119 110 100 84 71 66 6.3 6.6 6.5 6.1 5.0
50 40 30 24 17 9 11 31 46 50

9.50. 112

67 58 45 2.0 14 1.0 1.2 1.6 0.9 0.1
50 34 28 17 8 10 20 33 50

74 61 29 22 18 21 24 3.5 3.5 2.4 2.4 2.7
50 30 17 8 10 19 23 25 27 31 50

74 65 49 31 26 21 24 29 45 49 43
50 32 23 16 8 10 20 26 32 48

Sta	+	X 56	-	Elev
		908.37		

113				05.3
-----	--	--	--	------

	+50			04.5
--	-----	--	--	------

114				04.1
-----	--	--	--	------

	+26	X Drain		04.1
--	-----	---------	--	------

	+50			04.0
--	-----	--	--	------

115				04.3
-----	--	--	--	------

	+50			05.0
--	-----	--	--	------

116				05.4
-----	--	--	--	------

LT

2

RT

84 79 5.2 43 58 93 35 41 63 7.2 7.2
50 33 21 15 9 10 19 28 34 50

90 84 69 52 46 41 44 5.2 77 84 8.0
50 32 24 15 8 11 20 31 38 50

87 89 71 55 48 45 49 56 78 85 8.1
50 34 25 16 8 11 20 30 38 50

(outlet)

(inlet)

85 86 84 9 63 53 48 45 50 54 7.81 7.7 7.8 7.9
50 33 25 23 15 8 11 17 17 19 31 50

80 82 71 5.7 55 50 46 49 55 7.3 79 7.8
50 33 25 20 15 8 10 19 27 36 50

7.9 7.4 55 50 46 43 45 51 6.5 6.6 6.7
50 29 21 15 8 10 20 28 43 50

7.3 7.1 5.7 4.6 4.0 3.6 3.9 4.1 5.2 5.3 5.2
50 31 24 18 9 10 20 24 37 50

6.6 6.2 50 4.2 3.6 3.2 3.5 3.6 4.5 4.5 3.4 3.7
50 30 28 23 9 10 19 24 28 31 50

Sta	+	π 56	-	Elev
		908.37		

116	+50			05.8'
-----	-----	--	--	-------

117		911.81		06.1
T.P.	570	911.62	2.45	906.11 905.92

	+50			06.4'
--	-----	--	--	-------

118				06.7'
-----	--	--	--	-------

	+50			06.9'
--	-----	--	--	-------

119				07.1'
-----	--	--	--	-------

	+50			07.2'
--	-----	--	--	-------

120				07.2'
-----	--	--	--	-------

16

4

21

55 52 47 37 31 2.8 30 33 4.2 40 27 1.9
50 36 29 18 9 10 18 21 28 31 50

47 42 37 46 46 34 28 25 27 30 35 35 23 21 0.8
50 36 25 23 21 17 9 10 21 24 26 32 43 50

7.1 6.5 5.8 6.2 8.6 6.2 5.7 5.4 5.5 5.7 6.5 6.5 5.4 4.8
50 35 31 26 23 21 18 10 10 19 22 24 33 50

7.2 6.7 6.1 5.9 6.0 7.8 7.8 6.1 5.4 5.1 5.3 6.1 6.7 6.7 5.0 4.2
50 36 35 31 27 24 22 18 9 10 20 24 27 30 50

7.7 7.3 6.9 6.1 6.5 8.2 8.2 5.8 5.2 4.9 5.1 5.5 7.2 7.2 5.3 4.7
50 37 36 31 26 24 21 17 9 10 18 23 26 30 50

8.8 8.0 7.5 5.5 5.0 4.7 4.9 5.3 7.2 6.4 5.4 4.5
50 36 28 17 8 10 19 23 28 31 50

9.5 9.3 7.8 5.5 4.8 4.6 4.8 5.2 7.2 6.4 5.3
50 36 26 17 9 10 18 23 29 50

9.6 9.5 7.0 5.5 4.8 4.6 4.7 5.0 6.9 6.6 6.3 5.5
50 35 24 17 9 10 18 22 28 34 50

Sta + T - Elev
 911.82

120 +50

07.4

121

07.4

+50

07.2 ✓

+54

Ground = 13.1

E.L. = 1433 =

898.71

897.48

B.M.

3.07

908.74, 908.75

122

07.1 ✓

+50

06.9 ✓

123

06.5 ✓

+35

6.3

06.2

Lt

R

Rt

7.5 7.1 8.3 5.4 4.8 4.4 4.6 4.9 6.6 6.5 6.0 5.9
50 35 29 16 9 10 18 22 28 33 50

8.8 8.5 7.7 7.1 5.3 4.8 4.4 4.6 4.7 6.4 6.1 5.6 5.0
50 34 31 23 17 9 11 18 22 28 31 50

7.8 7.4 6.9 7.4 5.1 4.7 4.6 4.8 4.8 6.2 6.1 4.9 4.4
50 35 26 21 16 9 11 18 22 28 31 50

Inlet 18" Vit Drain 115' Lt.

12.5" = 100 Inside Pipe

1.75
14.32 assumed 21" Vit

Top Conc. Tele. Cable Marker 32' Lt. sta. 121+80

6.2 5.5 5.1 7.6 7.5 5.3 5.0 4.7 4.9 5.3 4.7 4.0
50 35 32 27 23 15 9 11 20 35 50

1.4 0.9 7.2 7.1 7.2 5.6 5.1 4.9 5.1 5.5 4.7 3.6
50 44 34 24 18 15 9 10 23 41 50

3.7 1.5 8.2 8.2 6.1 5.5 5.3 5.4 5.3 9.6 3.4
50 35 24 21 16 9 10 22 42 50

5.5

2.9 2.7 8.9 8.9 6.2 5.8 5.6 5.7 5.4 4.7 4.0
50 34 24 21 15 9 10 29 45 50

Sta + Δ - Elev

81
911.62

123 +70

06.1[✓]

124

T.P.

1.05

907.01[✓]

906.82

5.85

05.9[✓]

905.96[✓]

905.77

+50

05.6[✓]

+92 Lt. only

Top inside Pipe = $\frac{8.45}{1.75}$
+92 Lt. only assumed RL = 10.20

125

05.1
04.5.

+25

04.9
03.8.

+59

04.6
03.0.

14

2

Rt

34 21 26 90 90 6.9 6.05 7 61 6.1 4.5
50 44 34 25 20 15 10 11 24 50

5.8 5.2 5.0 9.4 9.4 6.6 6.1 5.9 6.2 6.5 5.6 5.2
50 46 33 25 24 16 9 11 30 35 50

2.7 3.3 3.4 5.3 5.0 2.0 1.7 1.4 1.6 1.9 3.0 3.4 2.7 1.5
50 42 32 26 19 14 10 11 18 26 31 36 50

(H.W.)

5.0 5.5 6.6 6.5 6.5 6.3 3.3 2.8 2.3
50 43 36 32 25 20 15 10

4.64
3.81
2.13

5.5 7.5 7.4 6.5
43 36 31 25

1.9

5.9 5.9 7.3 7.3 6.1 3.6 3.0 2.5 2.7 3.1 4.5 5.2 5.7 5.6 5.3
50 40 36 29 20 15 11 11 17 22 26 31 41 41

2.1

7.3 6.3 7.0 8.1 7.9 7.2 4.4 3.8 3.2 3.4 4.0 5.5 6.6 6.9 7.0 7.1
50 39 36 32 27 21 16 11 10 17 22 28 32 39 50

2.4

Inlet 9.66-Top Pipe 6.65 size 10 off file

9.66

19

8.6 8.0 8.9 7.5 7.0 5.4 4.9 4.4 4.1 4.4 7.5 8.0 8.0 7.9
50 31 30 24 19 16 11 10 16 27 33 42 50

Sta	+	π	-	Elev
		907.01		
		906.82		
126				04.4 02.4
				04.3
+33				02.3
+36				
				04.3
+65				02.4
				04.3
127				02.3
				04.2
+50				01.7
				04.3
128				01.5
				04.2
+50				01.6

lt

R

pt

2.6

88 86 93 86 61 54 46
50 33 31 21 16 11

47 52 70 82 84 82
11 16 24 29 35 50

2.7

Top Pipe 893 - outlet

89 88 87 91 94 80 66 55 47 49 54 86 86 86
50 35 31 29 23 19 16 11 10 16 26 38 50

26

9629

inlet

10.72
25

9629

outlet

10.72
25

2.7

88 91 94 96 91 83 60 53 46 48 51 78 82 92 98 98 88
50 42 39 29 27 20 16 11 10 17 26 35 38 40 48 50

2.7

L.O. 99 93 88 61 54 47 49 56 80 85 L.O.
42 30 20 16 11 10 17 25 34

2.8

L.O. 98 98 87 65 59 53 54 52 82 90 97 L.O.
40 30 20 16 11 10 17 24 29 32

2.7

L.O. 98 92 83 68 59 55 55 58 72 90 100 L.O.
35 27 20 16 11 10 19 23 27 34

2.8

L.O. 94 88 64 59 54 56 64 71 92 96 L.O.
33 20 16 12 11 18 22 28 33

Sta	+	^T	-	Elev
		907.01		
		906.82		
129				04.2
				01.4
				04.3
	+50			01.5
		908.38		901.97
T.P	6.41	908.19	5.04	901.78
				04.3
130				01.7
				04.2
	+50			02.1
				04.0
131				02.4
				04.0
	+28			02.9
				04.0
	+35			03.0
				04.0
				03.2
		909.03		903.02
P. Co Rd		908.99		902.83
B.M	5.96		5.36	
				903.07 ✓
				903.01

L.H.

L.

R.H.

(2.8)

L.O. 95 99 85 65 58 56 56 60 88 94 9.5 L.O.
35 28 18 16 12 12 19 26 29 33

(2.7)

L.O. 10.2 9.1 6.9 5.9 5.5 5.4 6.4 8.7 9.5 L.O.
33 20 16 13 11 17 23 33

(4.1)

L.O. 10.3 10.7 9.9 7.8 7.0 6.7 6.7 7.7 10.5 11.4 L.O.
33 30 19 16 12 11 16 22 31

(4.2)

L.O. 10.4 10.1 7.7 6.7 6.3 6.5 7.0 10.4 11.2 L.O.
31 20 16 12 12 15 23 33

(4.4)

L.O. 9.4 8.9 7.4 6.4 6.0 6.0 6.6 7.4 9.5 9.7 9.7
34 20 16 13 11 15 18 23 34 50

(4.4)

7.3 7.4 7.0 5.7 5.9 5.5 5.7 6.1 8.1 8.5
50 31 23 15 9 11 17 25 50

(4.4)

5.3 5.9 5.8 5.8 5.4 5.5 5.9 6.2 6.7
50 32 18 9 12 20 31 50

(4.4)

26 37 44 50 55 56 52 54 52 5.7 6.0 6.0 6.0
200 150 100 50 10 9 10 11 50 100 150 200

Top Mont. Co. Rd. 62 + Cleveland Ave

Sta	T	π	-	F/E/V
		909.03		
		908.99		

131	+69			04.0
				03.4

	+76			04.0
				03.6

132				04.0
				03.8

	+50			04.1
				04.0

133				04.4
				04.3

	+50			04.6
				04.4

134				04.6
				04.5

	+50			04.4
				04.2

Lt

A

Rt

(5.0)

6.0 5.8 5.9 5.6 6.0 6.1 6.6
50 25 8 15 25 50

(5.0)

9.4 9.0 7.4 6.0 5.8 5.8 5.4 5.1 4.1 7.9 8.3 8.7
50 37 29 21 18 9 10 17 23 32 50

(5.0)

7.7 7.8 8.5 8.6 6.2 5.6 5.2 5.5 5.9 7.7 7.7 7.0 8.0
50 29 27 23 17 9 10 15 22 28 30 50

(4.9)

6.3 6.3 8.2 8.4 6.1 5.1 5.0 5.1 5.5 7.3 7.4 6.9 4.8
50 32 27 22 17 8 11 17 24 28 32 50

(4.6)

6.0 6.1 8.2 8.0 5.7 5.0 4.7 4.8 5.0 6.0 7.1 7.3 6.6 6.3 5.6
50 31 27 21 17 9 11 15 20 25 28 32 38 50

(4.4)

6.4 6.1 7.5 7.6 5.6 4.8 4.6 4.7 5.1 7.7 7.7 6.9 5.6 5.0
50 31 28 21 17 8 10 17 26 29 32 39 50

(4.4)

5.4 5.6 7.0 7.0 5.0 4.6 4.5 4.7 5.2 7.3 7.7 6.5 5.7 4.8 5.1
50 32 28 21 17 9 11 15 23 28 32 36 42 50

(4.6)

3.7 4.7 6.1 7.3 7.2 5.3 4.7 4.8 4.9 5.3 7.8 7.8 6.8 7.0
50 33 29 26 19 15 9 11 17 24 27 30 50

Sta	T	T	-	Elev
		909.03		
		908.99		04.3
135				04.2.
+50				04.3.
T.P.	547	909.96	4.54	904.49.
		909.92		
136				04.5.
+50				04.7.
137				04.8.
+50				04.9.
138				05.2.
+50				05.5.

Lt

R

Rt

4.7

36 55 45 68 56 48 48 49 55 81 83 75 77
50 31 29 18 15 8 10 17 25 28 31 50

41 53 61 66 55 48 47 48 51 58 87 87 76 82
50 34 31 20 16 8 10 14 17 24 27 31 50

58 70 74 83 88 61 56 55 57 61 89 83 91
50 30 28 23 19 15 8 10 15 23 26 50

69 70 75 81 82 61 56 53 55 59 79 84 88
50 30 24 23 21 16 9 10 15 23 37 50

74 76 77 81 81 62 55 52 53 58 79 83 86
50 37 26 24 21 16 9 11 16 22 35 50

82 78 78 61 53 51 54 58 83 85 90
50 26 20 16 9 10 15 22 34 50

74 78 79 58 50 48 51 55 85 87 90
50 34 21 16 9 10 14 24 38 50

69 74 73 56 47 45 48 51 78 82 85
50 33 20 16 9 11 14 22 35 50

Sta.	T	π	-	Elev
		96 909.92		
139				06.0
+50				06.4
195				06.8
140				06.9
+40				07.2
+65				07.4
T.P.	6.38	.50 912.46	384	906.12 906.18
141				07.6
+33				07.6

8-8-41
K.F.
L.G.
A.M.
C.N.
C.F.

82

Lt

R

Pl.

6.0 5.8 6.4 6.3 5.0 4.3 4.0 4.4 4.8 7.0 7.0 7.2
50 25 23 21 16 9 11 16 22 34 50

3.4 3.5 6.0 5.9 4.3 3.8 3.6 3.9 4.2 5.7 5.7 4.8 4.8 4.9
50 29 24 20 15 9 11 15 20 23 26 38 50

2.5 3.0 4.9 5.0 3.2 3.4 3.2 3.4 3.8 4.6 4.4 2.8 2.3
50 27 24 21 17 9 10 16 21 24 27 50

0.5 0.4 4.9 5.0 3.2 3.4 3.1 3.4 3.9 4.1 3.4 2.1
50 30 24 21 17 9 10 18 25 29 50

10.9 10.9 5.0 5.0 3.2 3.0 2.8 2.9 3.1 3.2 2.5 1.5
50 31 23 20 16 9 10 15 24 30 50

11.1 11.0 4.3 4.3 2.8 2.7 2.6 2.8 2.8 3.8 3.8 1.6 1.9 0.7
50 30 22 20 14 9 11 16 22 24 29 36 50

Top N. End Ent. C. N. Lt 51.9 1.40+100

1.6 1.8 6.4 6.4 5.1 5.0 4.9 5.1 5.2 6.7 6.0 3.9 3.4 2.9
50 30 22 19 15 11 11 17 20 24 30 39 50

0.9 1.9 6.2 6.2 5.4 5.0 4.9 5.1 5.2 6.7 6.5 4.6 4.0 4.3
50 29 21 19 15 10 12 16 20 24 28 38 50

Sta + π 50 - Elev
912.46

141 +73 07.7 ✓

142 07.7

+50 07.9

+60 08.0

143 08.2

+27 08.3

+68 08.8

T.P. 8.89 918.02 3.37 909.13
~~917.98~~ ~~909.09~~

144 09.1

8-7-41
K.A.
L.C.
A.M.
C.F.
C.N.

83

Lt.

R.

Rt.

11 31 6.3 6.3 53 50 48
50 27 23 20 16 10

50 51 71 7.6 6.6 6.9
11 16 21 24 27 50

1.5 3.7 5.8 5.9 5.2 5.0 4.8 5.0 5.1 7.7 7.5 5.9 4.6
50 31 24 18 16 10 11 17 22 27 33 50

2.9 4.1 5.8 6.1 6.6 6.3 5.1 4.7 4.6 5.0 5.2 7.2 7.2 5.4 5.3
50 33 29 24 23 20 15 10 11 17 22 27 30 50

3.2 4.1 5.9 6.3 6.6 6.6 5.0 4.6 4.5 4.9 5.1 8.0 8.7 8.9
50 33 30 24 23 20 15 10 11 16 23 36 50

2.8 4.2 5.9 6.3 6.6 6.6 5.1 4.5 4.3 4.7 5.2 7.8 8.8 9.2
50 32 30 25 24 21 17 10 11 15 20 27 50

3.2 4.3 6.0 6.4 6.6 6.4 5.1 4.4 4.2 4.6 5.2 8.7 8.6 5.4 5.9
50 33 30 24 23 21 16 10 11 16 23 29 35 50

4.6 4.9 5.0 6.6 6.2 4.5 5.8 3.7 4.0 4.5 5.8 6.0 4.9 4.4
50 33 25 23 20 16 10 11 19 21 23 25 50

8.3 8.3 8.7 11.8 11.6 9.4 8.9 8.9 9.2 9.5 11.3 11.3 9.5 9.4
50 33 26 23 19 15 10 12 16 20 22 27 50

Sta	+	π	-	Elev
		918.02		
		917.98		
144	+50			09.4
145				09.4
	+50			09.4
146				09.6
B.M.		6.79		911.23 911.21
	+20			09.6
	+55			09.5
	+69			09.4
147		90		09.3
T.P.	4.10	912.86	9.22	80 908.76

Lt.

L

Rt.

6.5 6.7 11.5 11.5 9.7 9.0 8.6 9.0 9.1 10.8 10.8 8.5 8.7
 50 28 23 20 16 11 10 14 19 21 29 50

5.7 6.2 8.0 11.6 11.6 9.4 9.0 8.6 8.9 8.9 11.7 11.7 6.8 7.4 7.4
 50 29 27 23 20 15 11 10 13 19 22 28 37 50

4.7 5.1 5.1 11.8 11.8 9.1 8.9 8.6 8.8 8.8 11.2 11.2 7.8 7.3
 50 36 30 23 20 14 10 10 15 19 21 28 50

4.2 4.0 11.5 11.5 9.1 8.8 8.4 8.6 8.6 11.1 11.1 10.4 8.2 7.7 7.6
 50 32 22 19 14 11 10 14 17 19 22 30 39 50

Top SW Cor Lower Conc. Step Front of Ho. Rt sta 146t

4.7 5.2 11.4 11.4 8.8 8.7 8.4 8.6 8.7 11.3 11.3 10.4 8.2 7.8
 50 29 22 19 14 11 11 15 19 21 25 33 50

11.3 10.7 11.3 11.0 12.0 12.0 9.1 8.7 8.5 8.7 8.9 12.2 12.2 8.5 8.4
 50 39 34 24 22 19 14 10 10 14 20 23 30 50

11.6 11.8 11.2 12.0 12.0 9.4 8.8 8.6 8.8 9.2 12.0 12.5 12.8
 50 37 24 22 20 15 12 10 15 21 25 50

13.6 13.4 13.1 9.5 9.0 8.7 9.0 9.4 13.0 13.6
 50 31 21 15 11 10 15 22 50

Sta.	+	π_{90} 912.86	-	Elev
147	+50			09.11
148				08.81
	+50			08.61
149				08.41
	+50			08.21
150				08.11
	+50			08.41
151				08.51

Lt

R

Rt

95 94 87 51 42 38 41 45 85 95
50 30 31 15 10 10 14 22 50

100 99 94 54 46 41 45 52 91 108 108
50 33 23 15 10 10 16 23 33 50

100 98 93 55 47 43 46 53 92 101 102
50 32 23 15 9 10 16 23 28 50

101 102 96 85 60 50 45 49 57 98 100 98
50 35 26 20 16 12 10 16 27 31 50

102 101 91 60 51 47 50 54 98 102 106 96
50 31 23 15 10 10 16 25 31 43 50

101 96 88 60 50 48 50 53 90 99 92
50 32 22 16 10 9 15 23 30 50

95 90 83 56 48 45 47 53 85 90 90
50 35 21 15 10 10 15 23 31 50

97 93 84 55 47 44 46 52 82 85 79
50 32 22 16 10 10 15 22 31 50

Sta.	+	π	-	Elev
		90 912.86		
151	+50			08.5'
152				08.5'
	+50			08.8'
153				09.3'
	+50			09.9'
154		917.95		10.6'
T.P.	7.33	917.91	2.28	910.58 10.62'
	+50			11.4'
155				12.0'

Lt

E

Rt

74	76	73	55	47	44	45	50	72	74	72	64
50	34	20	16	12		10	15	21	32	44	50

94	90	82	53	48	44	43	45	70	69	71	58	
50	32	21	14	11			10	15	21	30	40	50

91	90	86	52	45	41	39	45	58	62	62	67	59	45	
50	35	23	16	11			10	16	19	25	27	31	38	50

88	82	72	46	40	36	35	36	56	60	47	47	34	28	
50	33	22	17	11			10	15	20	24	26	30	40	50

72	66	66	40	33	30	30	32	50	54	42	23	11	
50	34	22	17	11			9	16	20	23	28	30	50

36	28	63	41	30	26	23	24	27	46	46	32	16	12	
50	31	26	22	16	11			9	16	20	23	27	29	50

51	51	101	101	75	70	66	67	72	95	95	76	64	60	56	
50	34	26	22	16	11			9	15	20	23	27	30	37	50

47	53	93	93	65	64	60	60	63	85	85	62	66	60	
50	33	26	21	15	12			9	16	20	24	29	38	50

Sta. + $\pi_{.95}$ - Elev

917.91

155 +50

12.5'

156

13.2'

+50

13.9'

157

14.4'

+50

14.8'

158

T.P.

6.16

.36
921.32

2.75

15.2'
915.30
915.76

+50

15.7'

159

16.1'

Lt

L

Lt

39 5.4 7.5 7.6 5.6 5.6 5.5 5.7 6.5 8.0 8.1 6.4 5.6
 50 30 25 20 16 11 10 17 19 24 28 50

41 3.0 7.3 7.3 5.3 5.0 4.8 4.9 5.5 7.8 7.8 5.7 5.3
 50 29 25 20 16 11 9 16 20 23 28 50

45 4.6 6.4 6.5 4.5 4.2 4.1 4.4 4.9 7.0 7.0 5.0 4.6 4.6
 50 26 23 19 16 11 11 16 19 23.5 23.5 30 50

42 3.7 5.9 5.6 4.0 3.8 3.6 3.8 4.1 6.1 6.1 4.8 4.4
 50 27 24 21 16 10 10 16 19 23 27 50

35 3.8 5.0 5.0 4.0 3.4 3.2 3.5 3.7 6.0 6.0 4.8 4.8
 50 27 23 21 16 11 11 16 20 23 25 50

31 2.7 5.0 5.0 3.7 3.0 2.8 3.1 3.2 5.2 5.2 4.2 4.8
 50 28 24 20 18 11 11 16 21 24 26 50

58 5.6 7.5 7.6 6.4 5.9 5.7 6.1 6.1 7.8 7.9 6.2 6.5
 50 26 22 20 17 10 11 15 18 22 27 50

6.8 5.5 7.2 7.2 6.0 5.5 5.3 5.4 5.5 7.2 7.3 7.3 4.5 4.7
 20 26 22 19 16 10 11 15 20 22 23 28 50

Sta	+	π_{36} 921.72	-	Elev
159	+50			16.5'
160				16.9'
+24				17.2'
+36				17.4'
+41				17.4'
+53.18				17.4'
BM,	2.77	920.16	3.97	917.39 [✓] 917.39 [✓]
+72				17.4'
+82				17.2'

B-4-41
K.H.
L.C.
A.M.
C.F.
C.N.

88

Lt.

2

Rt.

80 63 71 70 56 51 49 51 52 71 71 41 36
50 24 22 19 15 10 11 15 19 23 30 50

82 67 60 63 55 48 45 49 55 63 63 43 36
50 30 26 21 17 11 12 16 20 22 27 50

69 64 58 47 42 43 49 54 34 26
50 37 21 13 10 20 25 31 50

50 58 57 47 40 41 47 50 34 31
50 36 27 20 11 32 38 43 50

55 54 48 40 41 47 48
50 34 27 11 42 50

56 51 50 48 42 40 41 43 47 48 52
200 150 100 50 25 25 50 100 150 200

Top Mont. Co. Rd. "D" & Cleveland Ave.

M.H.

42 39 306 30 28 29 32 33 33
50 35 13 10 10 28 42 50

35 53 33 38 31 30 31 52 30 30
50 39 23 20 10 9 26 36 50

Sta + π ¹⁶ - ELEV
920.12

161 17.1

+50 16.8

162 16.4

+50 15.9

163 15.6

+50 15.1

164 14.6

+50 13.8

Lt

L

Lt

41.33

4.6 4.1 3.8 3.4 3.1 3.3 3.7 4.5 3.2 3.5 3.8
50 33 16 11 10 15 20 28 36 50

5.7 5.3 6.1 5.9 4.2 3.8 3.4 3.8 4.4 5.5 5.0 3.5 4.1
50 25 22 20 16 11 11 17 20 24 27 50

6.7 6.7 6.2 6.8 6.9 4.5 4.3 3.8 4.1 5.0 6.2 5.4 5.5
50 37 26 23 20 16 11 10 17 19 23 50

8.5 8.0 7.1 7.5 5.1 4.8 4.3 4.6 5.1 6.4 6.4 5.8 5.9
50 36 26 21 17 11 10 16 19 21 22 50

9.8 8.4 8.1 5.5 5.1 4.6 4.8 5.2 4.5 6.5 5.7 5.2
50 32 22 17 12 10 15 18 20 22 50

10.8 9.7 8.8 8.0 5.9 5.5 5.1 5.4 6.0 7.2 7.2 6.0 4.8
50 32 26 21 16 12 10 16 18 20 23 50

9.0 8.1 7.6 8.0 6.7 6.3 5.6 6.0 6.4 7.5 7.5 5.2 4.6
50 32 25 20 17 12 10 14 17 19 24 50

7.0 6.0 6.4 8.7 8.7 7.7 6.9 6.4 6.7 10.8 8.0 5.5 4.8
50 32 28 22 20 17 12 10 15 19 23 27 50

Sta	+	π	-	Elev.
		920.16'		
165				13.0'
+50				12.1'
166				11.4'
I.P.	5.38	916.74'	8.80	911.36'
+50				10.5'
167				09.5'
+50				08.4'
168				07.5'
+30				06.8'

Lt

4

Rt

59 5.2 9.2 9.2 8.0 7.5 7.2 7.5 7.8 9.2 8.7 5.0 5.5
 50 28 23 20 18 12 10 15 18 22 28 50

6.3 5.6 10.0 10.0 9.1 8.5 8.1 8.3 8.5 10.0 9.9 5.0 5.5
 50 29 22 20 17 12 10 15 19 23 30 50

7.0 6.5 10.6 10.6 9.5 9.1 8.8 9.0 9.4 10.8 10.3 5.3 5.1
 50 29 23 20 17 11 10 15 19 23 31 50

4 sta. 166

9.3 3.3 3.1 8.1 8.1 6.9 6.6 6.2 6.6 7.1 8.4 8.4 7.2 2.7 2.3
 50 35 30 22 19 16 11 10 15 18 20 24 31 50

4.0 3.7 4.0 8.6 9.0 8.0 7.6 7.2 7.6 7.9 9.4 9.4 8.2 2.9 2.8
 50 35 29 24 20 17 12 10 16 19 21 24 32 50

5.2 4.8 4.8 8.1 10.0 10.0 8.9 8.5 8.3 8.6 9.0 10.3 10.3 9.3 3.9 3.6
 50 34 29 25 22 19 16 11 10 16 19 21 24 32 50

4.8 4.7 4.9 10.0 11.0 11.0 10.0 9.5 9.2 9.5 9.7 10.8 10.8 6.2 6.2
 50 35 31 25 22 20 17 11 10 16 19 24 30 50

4.2 4.1 10.7 11.6 10.5 10.1 9.9 10.0 10.3 11.4 10.3 7.0 7.4
 50 32 24 21 17 11 9 15 18 23 29 50

Sta	+	π	-	Elev
		916.74		
168	+64			06.1
169				05.5
T.P.	1.58	907.17	11.15	905.59
	+20			05.2
	+70			04.3
170				03.9
	+50			03.2
171				02.8
	+35			02.8

Lt

E

Rt

44 43 45 122 125 110 108 126 107 110 122 114 97 96
 50 37 32 23 19 16 11 10 15 18 23 25 50

88 9.8 101 132 132 119 115 112 115 119 137 134 140
 50 34 28 22 19 17 10 10 15 19 24 50

1.8 28 26 36 36 27 24 2.0 22 28 46 46 4.8 58
 50 39 24 21 19 16 10 9 15 21 23 30 50

6.1 56 6.0 56 3.8 3.2 29 3.1 3.5 7.0 7.4
 50 32 28 22 17 12 9 16 24 50

6.8 7.1 7.9 7.1 4.3 3.7 3.3 3.6 4.4 8.0 9.0 9.0
 50 26 25 21 17 11 9 14 22 31 50

9.0 9.2 8.7 8.0 5.0 4.5 4.0 4.6 5.1 9.5 11.3 L.O.
 50 38 27 22 16 11 10 16 23 35

10.6 10.0 9.0 5.4 4.8 4.4 4.9 5.5 9.4 12.1 L.O.
 50 34 25 17 11 9 15 20 33

9.15
 Top Water

9.15
 Top Water

10.2 11.0 10.0 9.1 5.3 4.8 4.4 5.0 5.5 9.4 11.6 L.O.
 50 39 34 25 17 11 10 15 21 32

Sta	t	π	-	Elev
		907. ^{.17} 13		

171	t74			02.7.
-----	-----	--	--	-------

172				02.7.
-----	--	--	--	-------

	t50			02.8.
--	-----	--	--	-------

173				03.2.
T.P	5.17	908. ^{.30} 26	4.04	703. ^{.13} 09

	t50			03.5.
--	-----	--	--	-------

174				04.0.
-----	--	--	--	-------

	t50			04.4.
--	-----	--	--	-------

175				05.1.
-----	--	--	--	-------

LK
76.46

K

RF
25.62
Al fell in and
got soaked
(Culv) K
FL

88 98 101 95 107 107 55 49 45 51 54 90 11.52 11.5 12.3
50 47 36 22 26 23 18 11 9 14 22 26 25 36

87 94 92 87 60 49 4.5 51 54 94 116 L.O.
50 44 30 25 18 12 9 14 22 30

91 93 96 90 54 48 44 50 53 96 115 L.O.
50 45 32 24 19 12 9 14 23 34

81 88 86 54 44 40 47 54 9.2 118 L.O.
50 35 25 18 11 9 16 23 36

82
91 91 94 82 60 52 48 55 63 80 99 108 119 L.O.
50 38 27 20 16 12 10 15 27 23 26 34

86 90 90 76 49 47 43 40 59 87 100 12.3 L.O.
50 38 27 20 16 11 9 15 20 27 37

86 88 86 76 59 47 4.2 39 46 49 87 101 119 L.O.
50 35 28 21 18 15 11 9 15 21 25 40

70 76 75 71 52 38 35 32 36 49 82 88 101 116
50 40 24 21 18 15 12 8 14 20 23 31 50

Sta	+	π	-	Elev.
		908.30		
175	+50			05.7.
176				06.2.
	+50			07.2.
T.P.	10.64	918.91	003	908.27
177				08.1.
B.M.			8.40	910.51
				910.52.
	+50			09.6.
178				10.9.
	+50			12.3.
T.P.	10.55	926.32	3.14	915.77.
179				13.9.

lt

R

Rt

6.7 70 48 60 45 30 29 26 30 31 85 97 104 101
50 38 26 21 18 19 11 9 15 25 34 36 50

5.9 61 5.7 39 26 24 21 25 28 7.8 86
50 35 22 17 15 11 8 19 25 50

L.O. 4.6 41 1.8 1.4 1.1 1.5 1.5 6.6 6.6
35 22 17 11 9 15 24 50

13.5 13.7 13.4 12.7 11.1 10.9 10.8 11.0 11.2 15.1 15.2
50 37 34 20 16 11 9 15 25 50

Spike in T.R. 24.44 177+89

11.8 11.3 11.5 10.9 11.7 11.5 9.6 9.6 9.3 9.6 9.7 12.5 12.4
50 35 33 25 23 20 16 11 8 15 23 50

9.5 9.5 8.9 8.2 8.4 9.9 9.9 8.1 8.2 8.0 8.2 8.4 10.2 9.7 9.2
50 36 32 29 25 21 19 15 10 8 15 20 47 50

6.6 6.1 6.9 8.2 8.0 6.7 6.8 6.6 6.8 7.0 7.7 7.1 6.0
50 33 26 23 19 16 10 8 15 17 32 50

No. 1 in T.R. 4.4 179+

11.2 10.8 10.2 10.7 14.0 13.7 12.8 12.8 12.4 12.8 12.5 11.9 8.4 8.3
50 46 30 29 22 20 16 10 9 15 25 47 50

Sta	+	π	-	Elev
		926.32		
179	+50			15.3.
180				16.8.
	+32			17.7.
	+15			18.8.
181				19.5.
	+50			20.9.
182				22.4.
T.P	9.92	932.34	390	922.42
	+50			23.9.

Lt

K

Rt

9.8 9.7 8.8 12.5 12.1 11.3 11.3 11.0 11.3 11.3 11.8 11.8 9.8 5.5 3.7 3.3
 50 34 30 24 20 17 10 9 17 19 21 28 34 41 50

7.1 7.2 10.1 9.8 9.5 9.8 9.8 10.1 9.9 8.0 2.8 0.7 L.O.
 50 33 25 9 9 17 18 23 28 39 44

6.5 6.7 10.0 10.0 9.0 9.0 8.6 8.9 9.0 10.8 1.3 10.3 L.O.
 50 32 23 21 17 10 9 19 25 35 42

3.3 3.6 8.2 8.5 8.0 7.8 7.5 7.8 7.8 5.7 1.2 10.4 10.5
 50 33 23 19 16 10 10 20 27 34 39 50

2.5 2.7 7.8 8.0 7.3 7.1 6.8 7.2 7.2 6.8 5.6 0.5 10.3
 50 32 24 20 17 10 10 21 23 27 34 50

1.9 1.4 6.9 7.0 5.8 5.6 5.4 5.7 5.1 6.2 5.7 4.6 0.4 0.0
 50 30 23 20 17 10 16 17 19 23 27 33 50

1.2 1.3 5.5 5.6 4.4 4.2 3.9 4.1 4.2 5.1 4.9 3.7 10.5 10.7
 50 30 23 20 17 10 10 16 20 25 26 32 50

5.7 5.5 10.7 10.7 8.9 8.7 8.4 8.6 8.8 10.3 10.3 8.5 5.0 5.1 5.2
 50 30 24 21 16 10 9 16 19 22 27 31 36 50

Sta	+	T.	-	Elev
		932.34		
183				25.1.
	+50			26.3.
184				27.2.
	+50			27.8.
185				28.4.
	+50			28.7.
186				28.7.
	+50			28.6.
B.M.	2.70	931.25	3.80	928.54 (928.55)

LT

Q

RT

46 42 95 93 77 75 72 74 75 92 93 85 49 5.2 48
50 29 23 19 16 10 9 16 20 21 24 31 35 50

3.7 40 83 81 66 63 60 64 66 81 84 42 43 46 4.4
50 28 23 20 17 10 10 15 19 23 29 34 36 50

3.3 26 30 73 72 58 54 51 54 57 74 73 64 37 38 38
50 31 28 23 20 17 11 10 16 19 22 25 29 33 50

36 28 27 36 67 64 52 49 45 49 50 68 69 37 37 33
50 34 31 27 23 20 17 11 10 16 20 22 27 32 50

3.5 37 61 61 46 41 39 42 46 65 65 29 2.2
50 27 23 20 17 10 10 15 20 22 29 50

3.4 2.5 24 60 57 48 40 36 40 43 59 59 43 17 1.3 1.3
50 37 29 23 20 16 10 10 16 20 22 26 30 40 50

28 21 16 55 55 41 38 36 39 42 56 56 26 21
50 37 28 23 21 17 10 10 16 20 24 29 50

17 1.7 27 55 59 41 38 37 40 43 55 55 21 2.0
50 33 28 23 20 17 10 10 15 19 22 29 50

Top Mont. & Sta. 186+72.61

Sta	T	π	-	Elev
		731.25		
187				28.4.
+50				27.9.
188				27.6.
+50				27.2.
189		Sta 189+00 to	26.3	26.8.
	Sta 204+00 Elev. Lowered 0.5' for spotting on cleve. Ave Final 1448 W.S.B.			
✓ +50			26.1	26.6.
190			25.9	26.4.
+50			25.6	26.1.

LT A Ct.

1.5 1.8 46 44 33 31 29 3.0 35 46 45 1.4 2.3 2.6
50 30 25 21 17 10 10 16 20 24 30 39 50

1.7 1.7 53 51 38 38 34 3.6 3.8 52 52 35 41
50 30 23 20 16 10 10 16 20 25 28 50

3.0 2.9 60 57 44 41 37 37 37 57 59 48 43 4.9
50 28 23 19 16 10 10 14 20 24 27 36 50

52 48 49 48 44 43 41 43 47 60 60 59 54
50 26 22 20 15 10 11 16 20 24 27 50

53 53 57 76 73 50 47 45 47 51 67 69 67 70
50 38 27 24 19 16 10 10 16 20 27 35 50

53 50 82 77 56 49 47 49 51 72 73 61 59 6.5
50 27 23 20 15 10 11 16 20 23 26 35 50

61 62 87 81 57 52 49 51 55 71 73 62 63
50 27 23 19 15 10 10 15 20 23 25 50

72 72 90 87 58 55 52 55 58 77 77 68 69 60 60 68 70
50 28 23 20 15 10 11 15 19 23 25 34 37 39 41 50

Sta	+	π	-	Elev
		931.25		
191			25.2	25.7.
T.P.	3.68	928.74	6.19	925.06.
+50			25.1	25.6.
			24.8	25.3.
192			24.3	24.8.
+50			24.0	24.5.
			23.8	24.3.
193			23.8	24.3.
+36			23.7	24.2.
+70			23.7	24.2.
			23.7	24.2.
194			23.7	24.2.

Lt

R

Lt

X

86 7.7 9.2 8.9 6.4 5.9 5.6 6.0 6.4 8.3 8.3 7.2 7.2 6.1 3.7 5
 50 27 23 20 16 10 11 15 19 23 26 34 37 41 50

Nail 10 T.R. 11 3/4 19 1/4

52 53 6.8 6.8 4.0 3.5 3.1 3.6 4.0 6.1 6.1 5.1 5.8
 50 27 24 21 16 11 10 15 19 22 26 50

X

55 55 7.1 7.1 4.2 3.7 3.4 4.0 4.3 6.1 6.1 5.3 5.0 4.8
 50 27 25 21 16 11 10 15 18 23 24 33 50

X

5.9 5.9 7.6 7.6 4.7 4.3 3.9 4.3 4.5 6.9 6.9 6.2 5.3 5.6 1
 50 27 25 21 16 11 10 14 19 22 26 38 50

7.1 7.0 7.5 7.5 5.3 4.5 4.2 4.6 5.1 7.1 6.9 6.6 7.1 7
 50 28 25 22 17 10 10 16 19 26 37 50

7.2 6.8 7.5 7.4 5.2 4.8 4.4 4.8 5.2 7.2 7.3 6.9 7.6 7.9
 50 28 26 22 16 10 10 16 19 22 24 29 50

X

6.9 6.0 7.6 7.4 5.3 4.8 4.4 4.9 5.2 7.4 7.4 5.5 6.0 5.5 6.2
 50 29 26 21 17 11 10 15 19 22 26 35 39 50

X

6.3 5.4 7.6 7.6 5.2 4.9 4.5 4.9 5.3 7.2 7.2 4.8 5.5
 50 29 25 21 15 11 10 15 19 22 26 50

Sta	+	π	-	Elev
		928.74		
194	+50	23.4		23.9.
195		23.0		23.5.
	+50	22.8		23.3.
196		22.7		23.2.
T.P.	5.26	928.14	5.86	922.88
	+50	22.6		23.1.
197		22.7		23.2.
	+50	23.0		23.5.
198		23.1		23.6.

Lt

Z

Lt

X

5.7 5.2 7.7 7.5 5.6 5.1 4.8 5.1 5.6 7.6 7.6 5.4 6.2
 50 28 25 21 16 11 10 15 19 22 26 50

6.2 5.7 8.1 7.9 5.6 5.4 5.2 5.6 6.0 8.1 8.1 7.0 7.4 7.0
 50 29 25 21 16 11 10 15 19 22 24 33 50

5.6 5.2 8.2 8.2 6.3 5.6 5.4 5.8 6.2 8.1 8.2 7.8 8.1 9.0
 50 29 24 21 17 11 9 15 19 22 23 29 50

5.9 5.9 8.7 8.7 6.3 5.8 5.5 5.9 6.3 8.4 8.4 7.9 8.3 9.3
 50 29 24 22 16 11 10 16 20 23 24 34 50

5.3 5.3 7.7 7.3 5.9 5.4 5.0 5.4 6.0 7.5 7.7 7.2 7.0 7.9
 50 28 23 20 17 11 10 16 19 23 24 33 50

5.6 5.1 7.9 7.9 5.9 5.2 4.9 5.3 6.1 8.0 8.4 8.8 8.3
 50 30 25 22 17 11 10 16 19 26 38 50

5.3 4.8 7.5 7.6 5.7 5.1 4.6 5.0 5.5 8.1 8.1 7.6 8.2 7.5
 50 30 25 21 17 11 9 15 20 24 25 32 50

6.3 5.5 7.9 7.9 5.4 4.8 4.5 4.8 5.6 8.0 8.0 7.1 7.3 6.2
 50 28 25 21 17 12 10 16 19 22 24 32 50

Sta	+	π	-	Elev
		928.14		
198 +50		23.1	23.6.	
199		23.1	23.6.	
+50		23.3	23.8.	
200		23.6	24.1.	
+50		23.8	24.3.	
201		24.1	24.6.	
+50		24.2	24.7.	
B.M.	2.52	930.16	0.49	927.65
				927.64
202		24.3	24.8.	

Lt.

4

Lt.

6.6 5.9 7.7 7.7 5.4 4.9 4.5 4.9 5.4 7.3 7.5 6.6 5.8
50 28 25 21 16 11 10 15 20 23 24 50

7.2 5.8 7.5 7.5 5.3 4.9 4.5 4.6 5.3 7.4 7.5 7.1 6.8 6.0
50 28 24 21 17 11 9 16 20 23 24 39 50

6.8 5.4 7.5 7.5 5.0 4.6 4.3 4.4 4.9 7.0 7.0 5.5 6.3 5.4
50 28 24 21 16 11 9 16 18 22 25 34 50

5.0 3.6 6.8 6.8 4.6 4.2 4.0 4.2 4.4 6.6 6.6 4.6 4.1
50 30 23 20 16 10 9 14 17 21 25 50

3.5 2.5 6.3 6.1 4.3 4.0 3.8 4.0 4.2 5.7 6.0 4.0 3.6
50 29 22 18 14 10 10 14 17 22 28 50

2.1 1.3 5.8 5.8 3.8 3.7 3.5 3.7 3.9 5.8 5.8 3.0 2.8
50 30 23 19 14 10 10 15 18 22 28 50

1.8 2.0 5.0 5.2 3.9 3.7 3.4 3.7 3.7 5.3 5.3 4.0 2.8 2.6
50 31 24 19 15 10 10 15 18 22 24 28 50

Sph. in T.R. Lt. sta 201+

4.7 5.5 7.6 7.5 6.0 5.7 5.4 5.6 5.9 7.4 7.4 5.1 5.3
50 29 23 19 15 10 10 15 19 22 27 50

Sta + π - Elev

930.16

202 +50

24.4

24.9.

203

24.7

25.2.

+50

25.0

25.5.

204

25.0

25.5.

+50

25.0

25.5.

205

25.9.

+50

25.9.

206 ✓

26.2.

Lt

R

Rt

66 52 73 73 60 56 53 57 59 72 72 55 50
50 30 24 20 16 10 10 15 18 23 26 50

X

65 48 54 68 68 56 59 50 53 55 49 69 55 47
50 29 26 22 19 15 11 10 16 19 23 27 50

X

64
68 53 64 57 51 47 50 54 64 69 57 50 47
50 28 18 15 11 10 17 19 21 23 32 50

X

69 57 49 68 68 51 50 47 50 54 64 69 56 50
50 39 29 22 19 15 11 10 17 19 22 30 50

X

72 60 68 72 72 53 50 47 50 54 61 60 52
50 32 24 23 20 16 11 9 17 19 25 50

X X

68 58 58 69 69 52 51 45 49 51 64 69 56 51
50 42 28 24 21 16 11 10 16 19 23 25 50

X

61 50 47 66 66 48 46 43 45 50 63 63 57 57
50 41 29 25 21 16 10 10 16 19 23 29 50

X

39 40 49 50 41 42 40 41 41 52 52 48 46
50 29 23 19 16 10 9 16 20 24 32 50

X

5to	+	π	-	Elcy
		930.16		

206 +32

26.6.

+56

27.0.

+14

27.2.

T.P.

9.98

937.47

2.67

927.49.

+19

27.3.

207

27.5.

+50

28.1.

208

28.6.

+50

29.2.

lt

x

rt

33. 32 36 37 36 36 40 40 48 48 41 39 X
50 39 19 9 9 16 19 21 24 27 50

25 30 34 32 32 30 29 29 31 31 X
50 24 10 9 31 50 100 150 200

1.4 2.8 3.8 33 30 31 37 38 34 X
50 26 20 10 9 23 31 50

81 96 117 117 107 105 102 104 111 120 120 93 94 X
50 30 23 19 16 10 10 19 21 23 30 50

7.3 7.6 11.8 121 106 103 100 102 10.4 121 121 8.7 8.5 X
50 32 24 19 16 10 11 16 20 23 29 50

6.0 7.6 10.9 10.9 9.9 9.7 9.4 9.6 9.9 11.3 11.3 9.7 7.1 6.5 X
50 31 21 18 16 11 11 16 19 22 27 31 50

5.7 6.2 9.4 9.5 9.2 8.9 9.1 9.3 10.8 10.8 8.6 5.5 5.0 X
50 30 21 17 11 10 16 18 22 29 40 50

4.7 3.7 9.3 8.8 8.6 8.3 8.5 8.6 10.5 10.5 7.3 5.7 5.6 X
50 31 19 17 11 10 15 19 22 30 40 50

Sta + π - Elev

937.47

209 30.0

+50 30.5

210 31.0

+50 31.8

211 33.0

+50 34.8

212 37.1

+50

39.6

Lt.

R

Rt

49 44 86 86 81 79 75 77 81 95 95 57 6.1 X
 50 29 21 18 16 11 11 17 20 22 29 50

54 50 86 86 73 73 70 72 75 100 100 77 76 X
 50 29 21 19 16 11 10 15 19 24 30 50

61 51 80 80 65 67 65 66 6.9 10.0 10.6 9.1 9.3 X
 50 30 22 19 16 11 10 14 20 27 32 50

75 69 66 53 59 57 59 65 11.5 11.4 10.8 10.7 X
 50 29 22 17 10 11 17 25 31 33 50

83 86 79 73 44 47 45 47 49 109 11.1 X
 50 33 32 25 17 10 11 16 29 50

88 85 80 78 35 29 27 30 34 110 11.5 X
 50 34 32 26 18 11 11 19 32 50

88 86 08 06 04 09 1.7 11.5 12.0 X
 50 33 18 10 11 21 38 50

89 76
 50 32

(42.1)

118 12.0
 39 50

Sta	+	Σ	-	Elev
		937.47		
212 +90.9				(41.53)
T.P.	8.21	945.28	0.40	937.07
212 +50				39.6
+90.9				41.53
B.M.			11.31	933.97
				(933.92)
213 +36			1.60	43.68
+82			1.70	43.58
214 +21.6			3.66	41.62
+28			3.66	41.62
+56			4.2	41.08

over this elev. as
bends

speaking
rec 62.66

Benches 62.66

LH.

A

RH.

90 83
50 36

(14.0)

9.7 11.1
34 50

6.6 6.1 5.7 6.1 6.6
18 10 11 19

33 375 3.6
14 14

Spike in P.P. Rt sta. 213406

Sta	T	X	-	Elev
		945.28		

215			5.2	40.1
-----	--	--	-----	------

+50			6.3	39.0
-----	--	--	-----	------

216			7.7	37.6
-----	--	--	-----	------

+50			9.5	35.8
-----	--	--	-----	------

217			11.4	33.9
-----	--	--	------	------

+50			13.2	32.1
-----	--	--	------	------

218			15.2	30.1
-----	--	--	------	------

Levels Under Bridge

Sta.	+	π	-	Elev.
B.M.	0.13	934.05		933.92

212	+91.4		+0.8	34.9
-----	-------	--	------	------

	+95.4		0.7	33.4
--	-------	--	-----	------

213	+08		83	25.8
-----	-----	--	----	------

	+14		10.3	23.8
--	-----	--	------	------

	+21		11.6	22.5
--	-----	--	------	------

	+31		12.6	21.5
--	-----	--	------	------

T.P.	6.59	928.96	11.68	922.37
------	------	--------	-------	--------

	+38		9.8	19.2
--	-----	--	-----	------

427	Top Nail			
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Lt

R

Rt

Spk. in P.P. Rt. sta. 213406

Sta	+	-	Elev
			928.96

213	+42.6	Top Rail	9.42	919.54
-----	-------	----------	------	--------

+86.5	"	"	9.33	919.63
-------	---	---	------	--------

+61.3	"	"	9.33	919.63
-------	---	---	------	--------

+70.7	"	"	9.10	919.86
-------	---	---	------	--------

+75.5			9.14	919.82
-------	--	--	------	--------

+80			9.3	919.7
-----	--	--	-----	-------

+85			80	21.0
-----	--	--	----	------

214			6.3	22.7
-----	--	--	-----	------

Lt

R

Rt

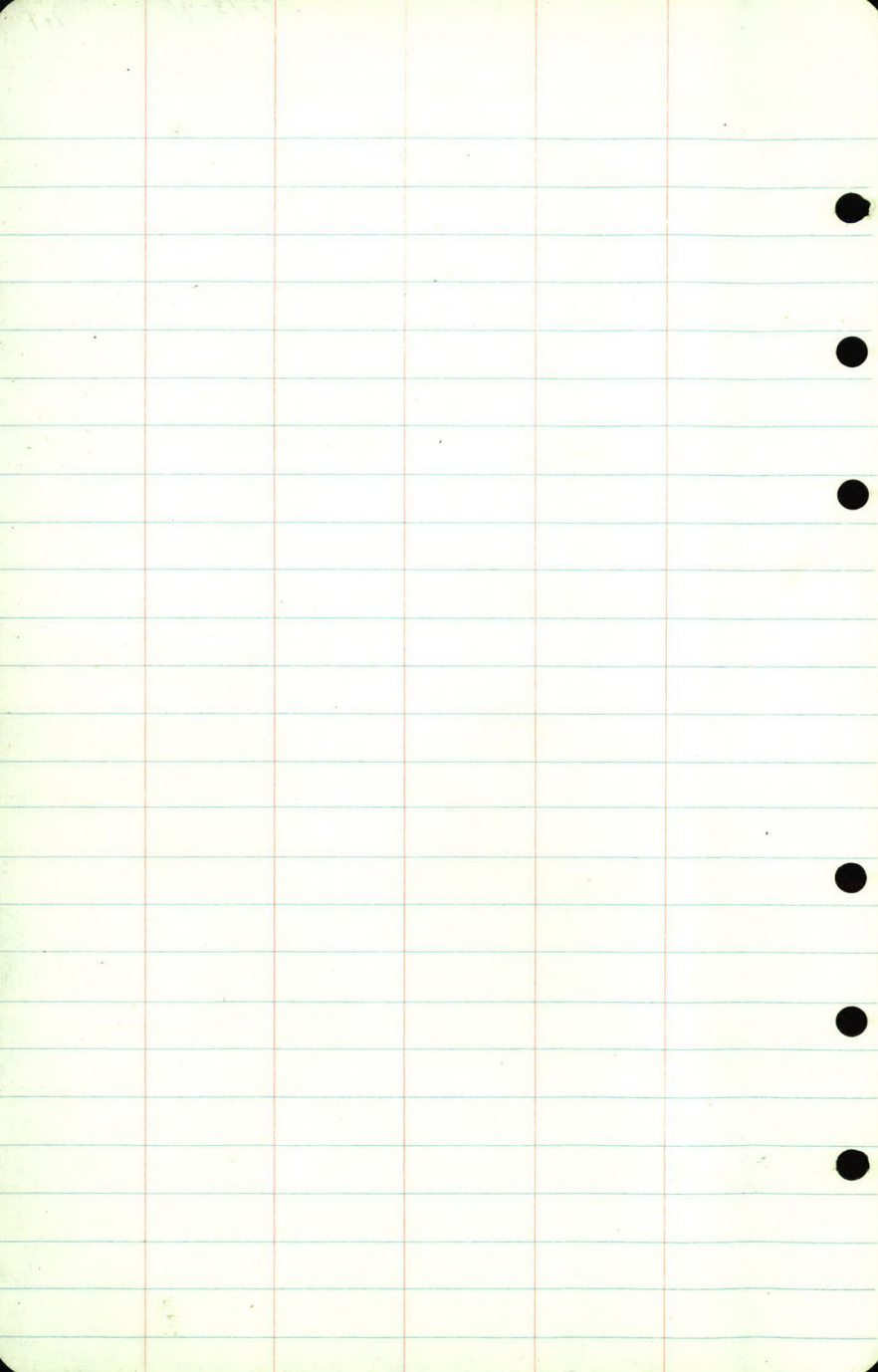
Sta.	+	π	-	Elev.
		728.96		
214 +05			5.8	23.2
T.P.	10.87	935.03	4.80	924.16
+24			2.2	32.8
+275			2.0	33.0
B.M.			1.11	933.92 (933.92)

Lt

R

Rt

Spk in PP Rt Sta 213 to 6



Bench Levels

Sta	+	π	-	Elev.
B.M.	4.45	952.68		948.23
T.P.	0.28	944.96	8.00	944.68
B.M.	9.82	948.99	5.79	939.17
T.P.	11.91	960.34	0.56	948.43
T.P.	7.03	965.67	1.70	958.64
B.M.	0.50	955.19	10.93	954.69
T.P.	0.59	944.79	10.99	944.20
T.P.	0.27	934.83	10.23	959.54
T.P.	1.34	922.92	13.25	921.58
B.M.	1.72	916.96	7.68	915.24
T.P.	0.24	909.70	7.50	909.46
T.P.	6.68	911.36	5.02	904.68
B.M.	1.27	910.02	2.61	908.75
T.P.	4.33	906.17	8.18	901.84
B.M.	6.38	909.45	3.10	903.07
T.P.	5.90	910.37	4.98	904.47
T.P.	6.60	914.12	2.85	907.52
B.M.	1.49	912.70	2.91	911.21
T.P.	5.89	914.25	4.34	908.36
T.P.	7.02	920.06	1.21	913.04
B.M.	2.55	919.94	2.67	917.39
T.P.	1.31	913.10	8.15	911.79
T.P.	2.05	906.92	8.23	904.87
T.P.	9.30	913.37	2.85	904.07
B.M.			2.85	910.52

Spk. 24" oak 35' Lt. Sta 71+25

Top Mast. Sta 78+

Top Great Lakes Sta. Marker Lt Sta 91+54

Top Mast. Co. Rd. G" + Cleveland Ave.

Top Conc. Tele. Cable Marker

Top Mast. Co. Rd. G" + Cleveland Ave.

Top S.E. Cor. Lower Conc. Sta Rt 146+

Top Mast. Co. Rd. D" + Cleveland Ave.

24'

177+84

Spk. in TP Lt. Sta (2017)

?

should be
Sta 177+84
Spk

Sta	+	π	-	Elev
		913.37		
T.P	12.18	925.20	0.35	913.02
T.P	8.47	933.26	0.41	924.79
B.M.	2.94	931.49	4.71	928.55
T.P	3.27	928.56	6.20	925.29
T.P	5.13	928.00	5.69	922.87
B.M.	2.40	930.04	0.36	927.64
T.P	8.30	936.07	2.27	927.77
T.P	11.22	945.86	1.93	934.64

10.87

934.99

11.94

933.92

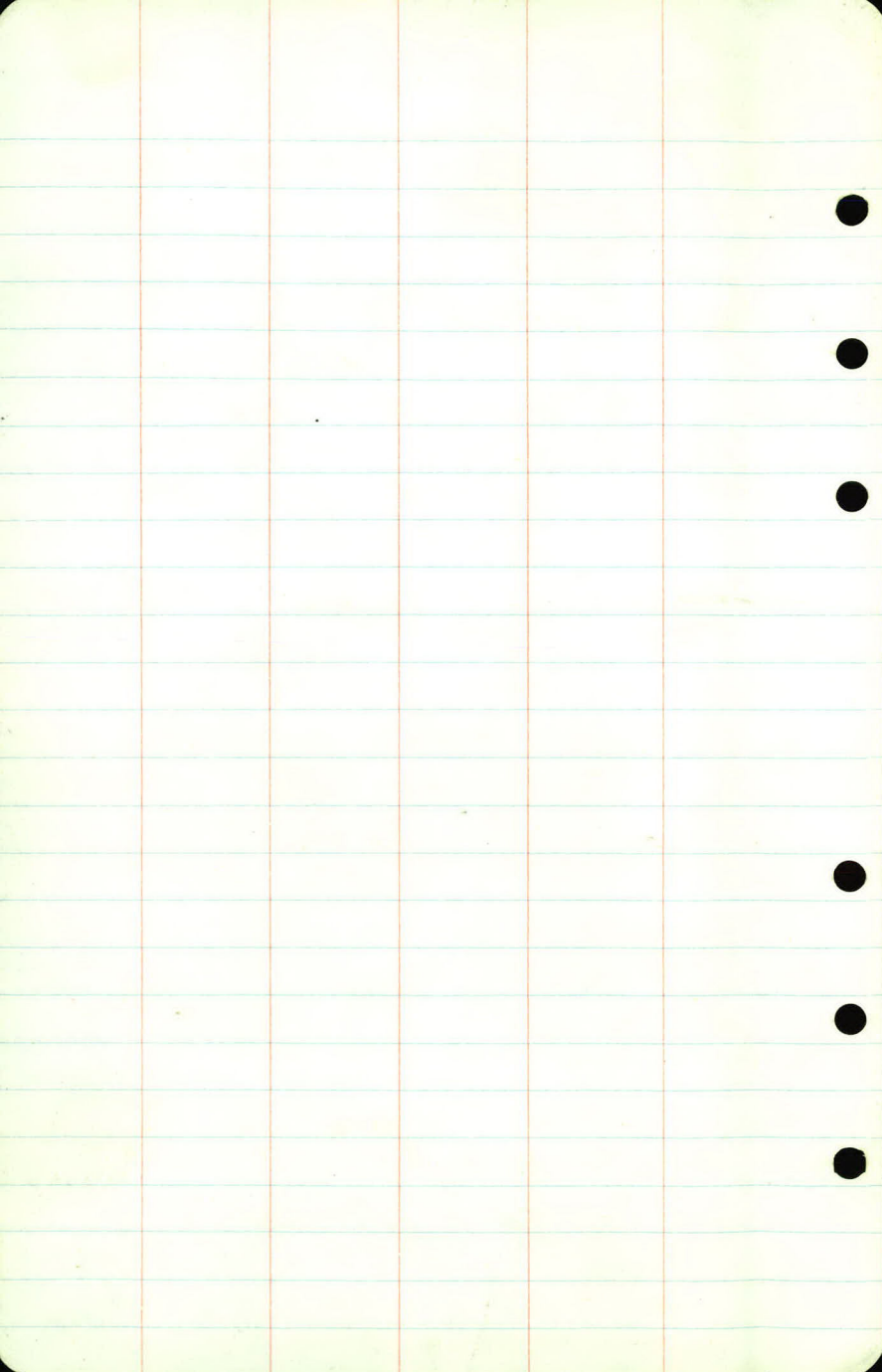


Description

Top Mont & sta. 186472.61

Spk. in T.P.L. sta. 201 + 47

Spk. in P.P.R. sta. 213 + 06



Ditch

Cleveland & "B"

	+	⌞	-	ELEV.	
B.M.	1.34	974.63		973.29	0.3.0
1				61.05	13.58
+50				60.98	0.1.0 13.65
T.P.	7.61	969.60	12.64	961.99	0.1.0
2				60.92	8.68
+50				60.85	0.1.0 8.75
3				60.79	0.1.0 8.81
+50				60.72	0.1.0 8.88
T.P.	7.55	977.00	0.15	969.45	
+70				60.71	Calc
B.M.			3.72	973.29	

Top Mon. Co. Rd. B. & Cleveland

$$\begin{array}{r} 10.58 \\ \underline{63.0} \end{array}$$

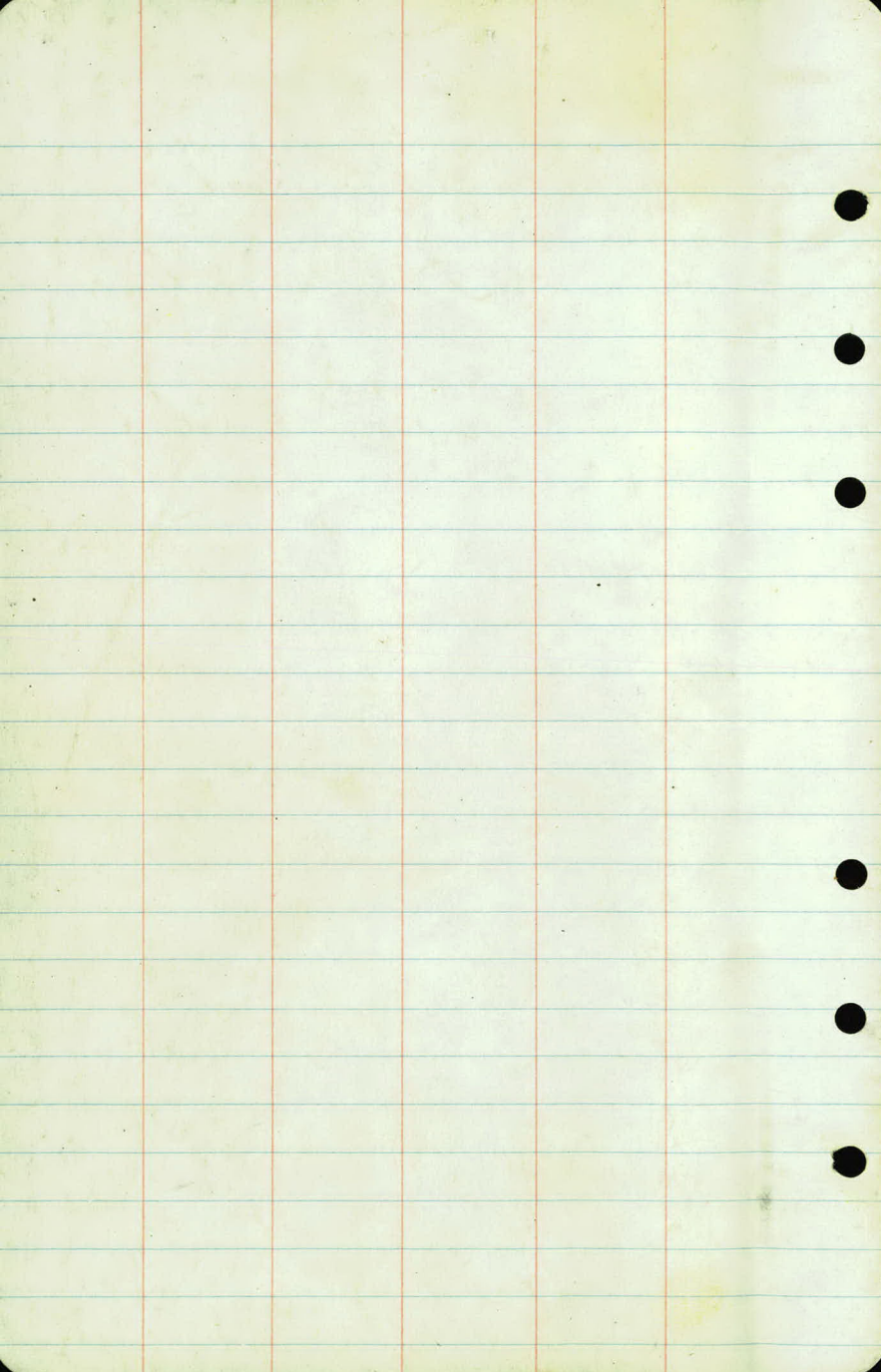
$$\begin{array}{r} 12.65 \\ \underline{61.0} \end{array}$$

$$\begin{array}{r} 7.68 \\ \underline{61.0} \end{array}$$

$$\begin{array}{r} 7.75 \\ \underline{61.0} \end{array}$$

$$\begin{array}{r} 7.81 \\ \underline{61.0} \end{array}$$

$$\begin{array}{r} 7.88 \\ \underline{61.0} \end{array}$$



Cleveland Ave. for fm

original X sections

0+00 to 189+00 Dr. 16 - Book 119

189+50 to 204+50 - Dr. 16 - Book 83

205+00 to 216+00 Dr. 15 Bk 18 - Brown Bk.

216+68

217+00 to 255+75 Dr. 15 Bk 18 - White

Final X sections

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2 Brown Books