

Book 80 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

COUNTY ROAD "I"

From U.S. #10 To Lexington

Road Acc't. No. 60

Date Filed. 1-30-43 File

Plan Survey

Co Rd "I"

From U.S.H #10 To Lexington Ave

9/19/41 H.A.W

11/4/41 AM

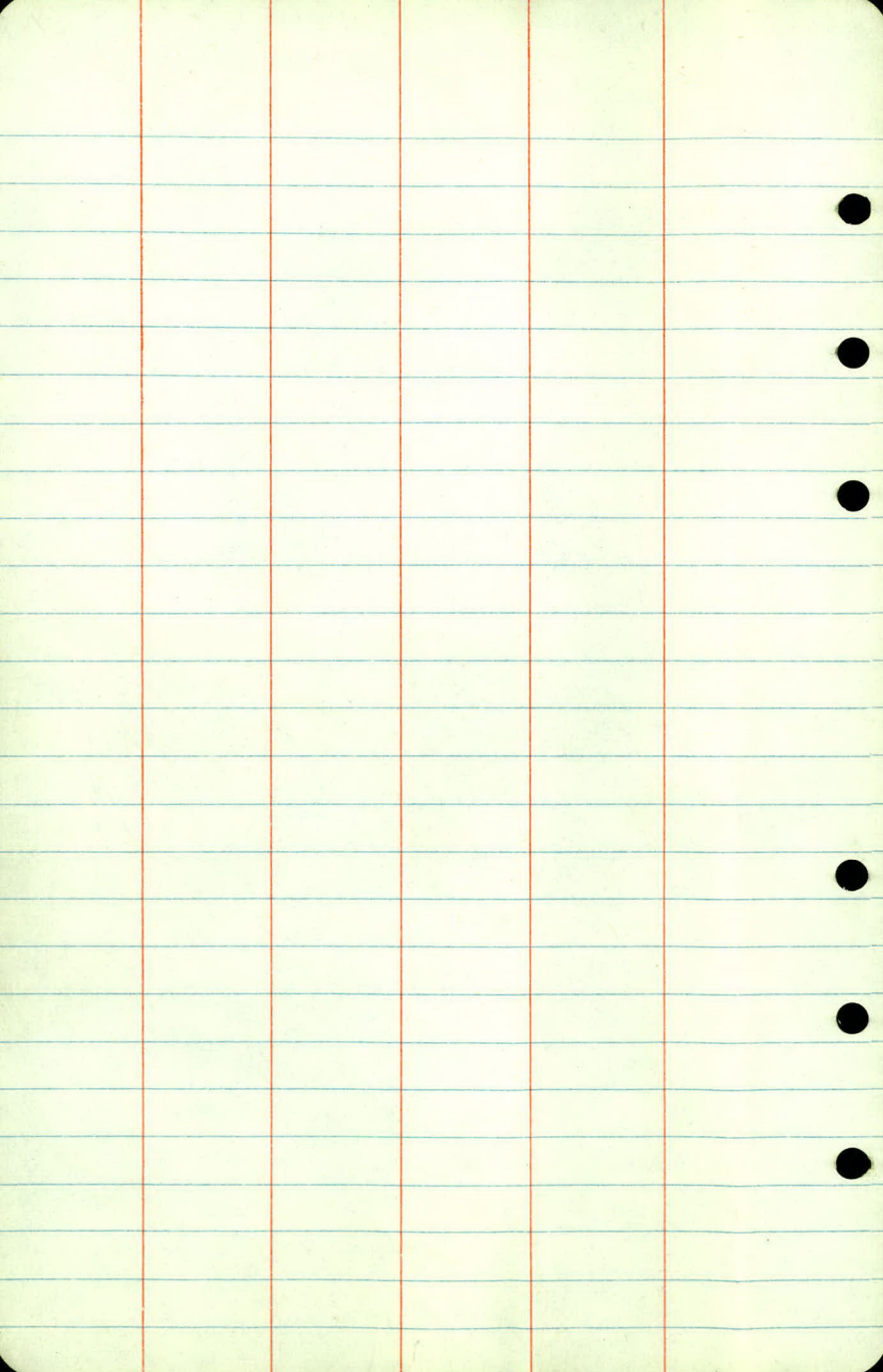
CN

LL

Index

Align	Pages 1 to 7
Topog.	" 48 to 74
Check Levels	" 43 to 46
X Sect.	" 8 to 43
Soundings	46 to 48
stading	74 to 77

Align - Line B. Revised - 7A to 7C
Topog. " " X " 74A to 74D
X sections " " " 42A to 42F
Push Soundings " " 47A to 47B

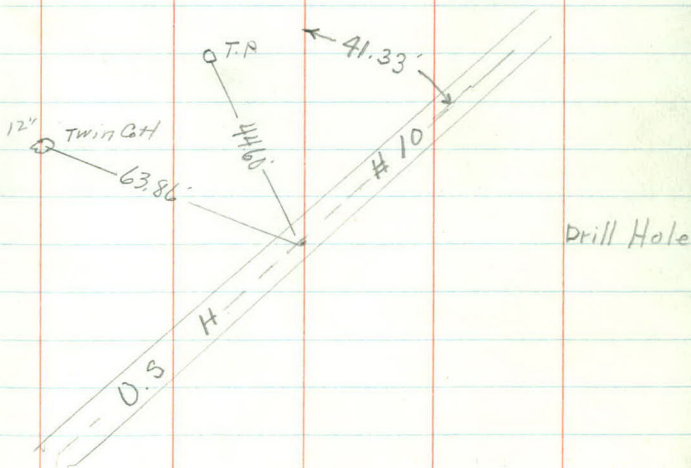
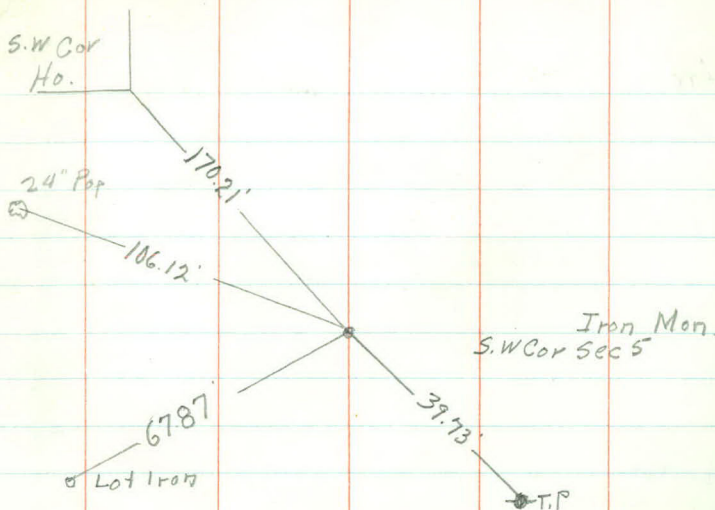


Align

Sta	Pt.	ΔL	ΔR
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12+93 ⁰⁶	P. 1.	Long Lake Rd	1° 29'
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0+00		U.S.H. # 10	
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Mon 5/4 6

Sta	Pt	Δ L	Δ R
-----	----	-----	-----

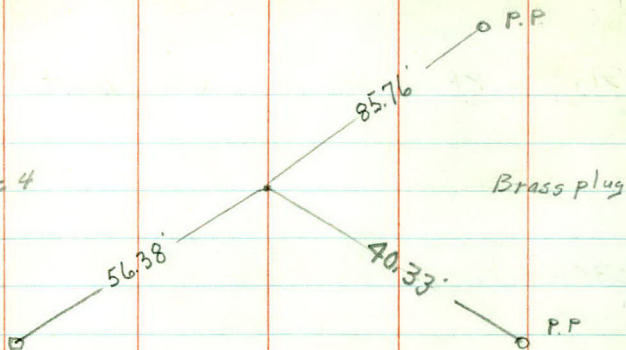
65+68.46	P. I.		0° 01'
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55+00	P. O. T.		
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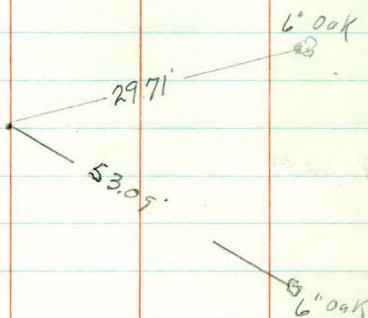
39+30.05	P. I.		0° 11'
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S.W. Cor Sec 4

Center
Conc. R.O.W.
Mon.



Boat spk



12" Pop

12" Pop

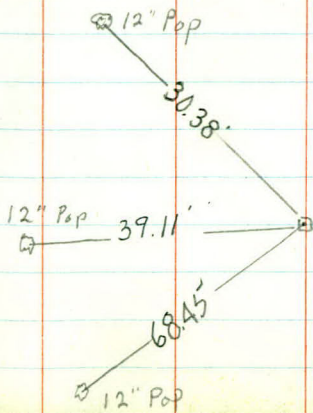
12" Pop

30.38'

39.11'

68.45'

S 1/4 Sec 5 Mon



Sta

Pt.

 ΔL ΔR

135+00

P.O.T

see Revised
(Line "B")
↓

Sta 130+51.93+

Sta 149+32.68

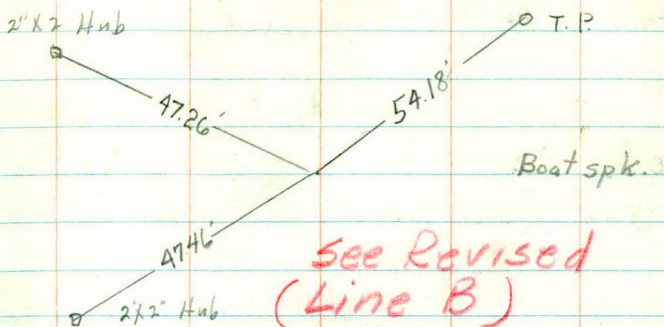
118+36.34

P.I

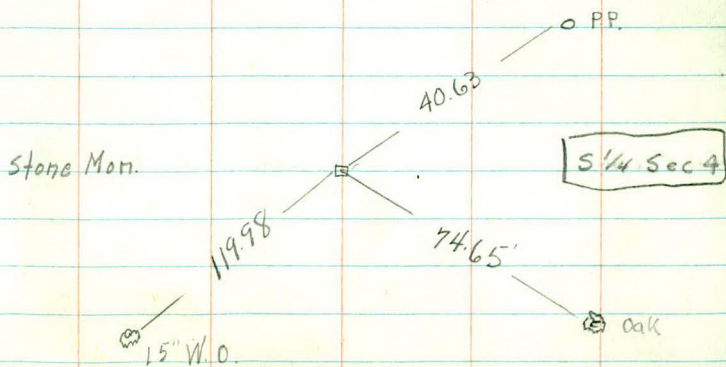
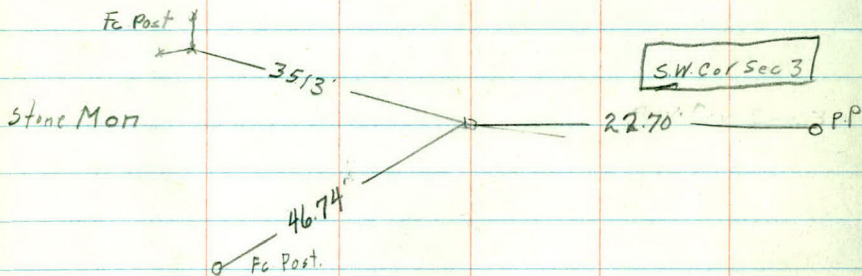
 $0^{\circ}43'$

92+02.00 P.I.

 $0^{\circ}03'$



See Revised
(Line B)



Sta

Pt.

ΔL

ΔR

144+72.44

P.I

118 36 5

1.27

300'

Exception

No on Hamline

see Revised
(Line "B")

144+72.44

P.I

19°00

C 13

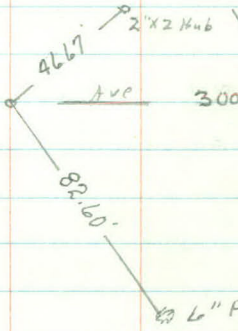
263610





Boat Spk.

Hamline



Mon
S 1/4 Cor. Sec 3

0°18'

Section Line

Bar

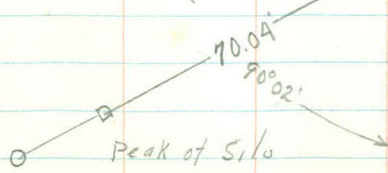
2" X 2" Hub

81.05'

Hamline

Ave

Stone Mark
S 1/4 Cor. Sec 3



See Revised
"B" (Line)



Sta

P.T.

Δ L+

Δ R+

171+19.62 = P.T.

214+01.50 Δ Lexington Ave

162+99.80 P.O.T.

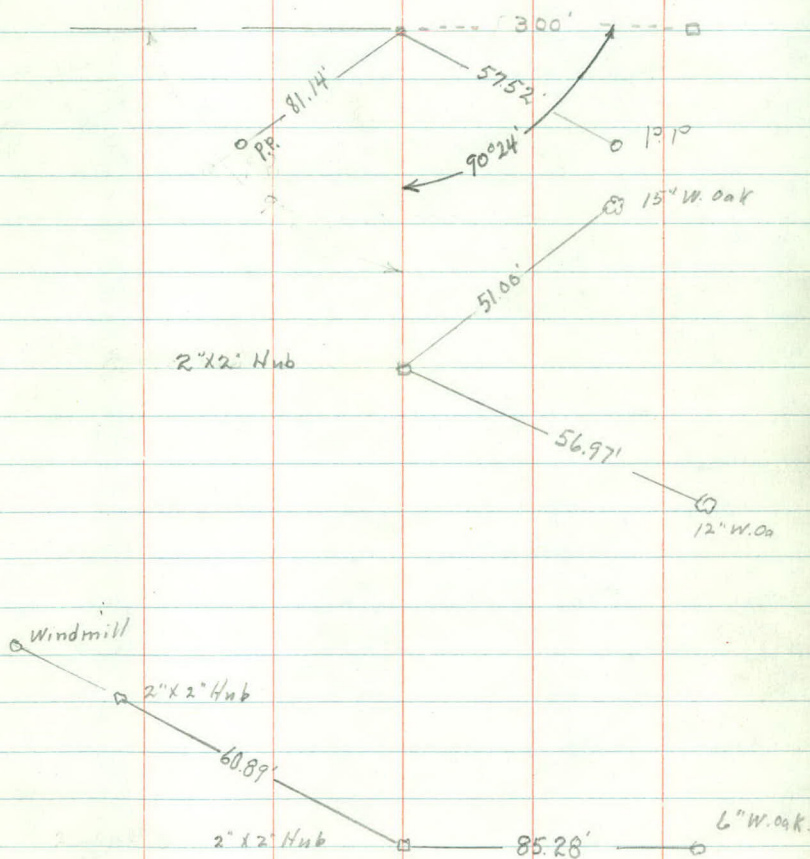
149+05.37 P.O.T.

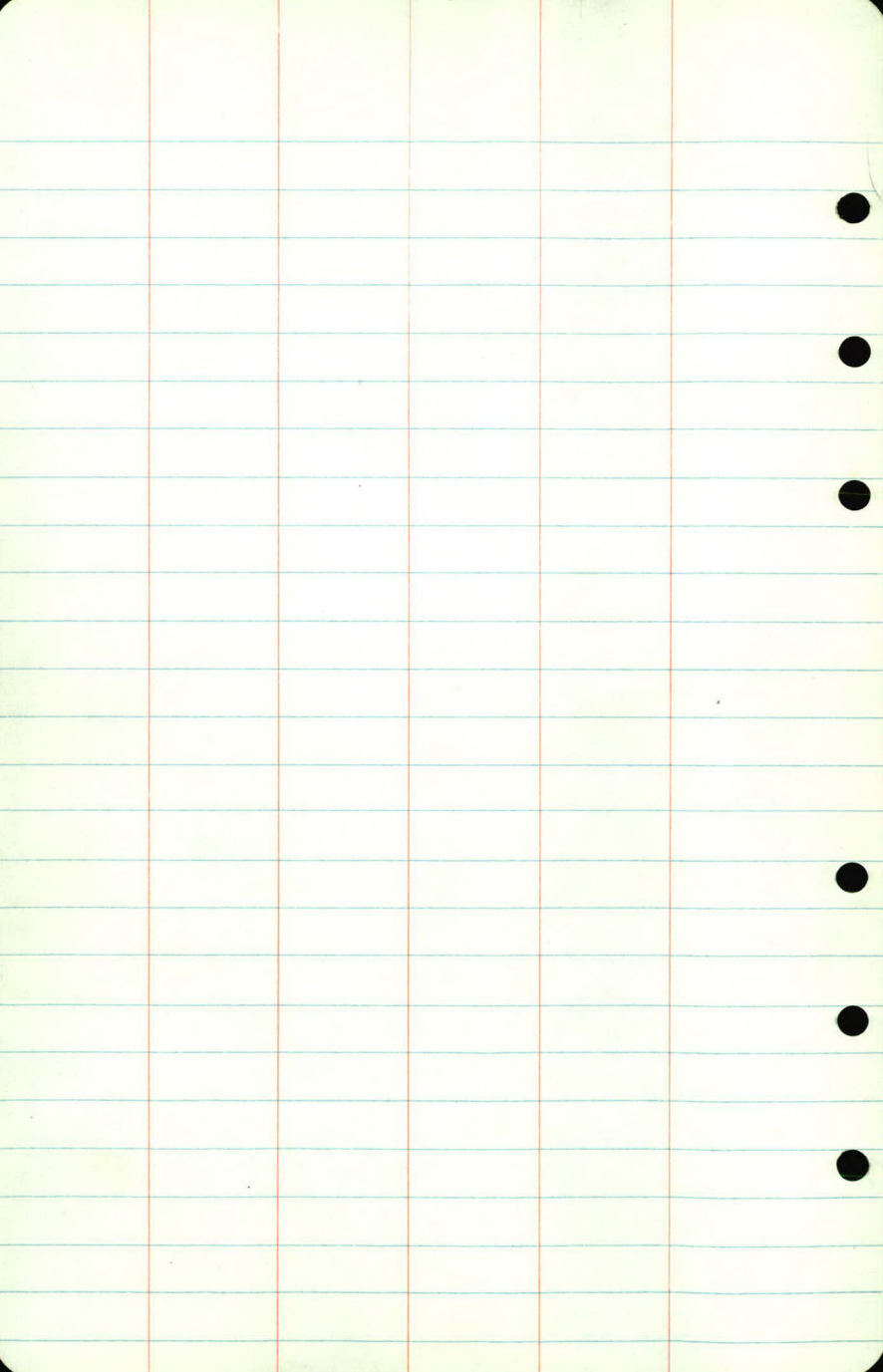
see Line Revision
Line B.

Sta 130+51.93 to 149+32.68

Description

SE Cor Sec 3





7A

+

Co. Rd. I

Line Revision

B Line

Sta 130+51.93 To Sta 149+32.68 =

149+00.60 A Line

11/10/41

NAW

AM

LF

C.V.

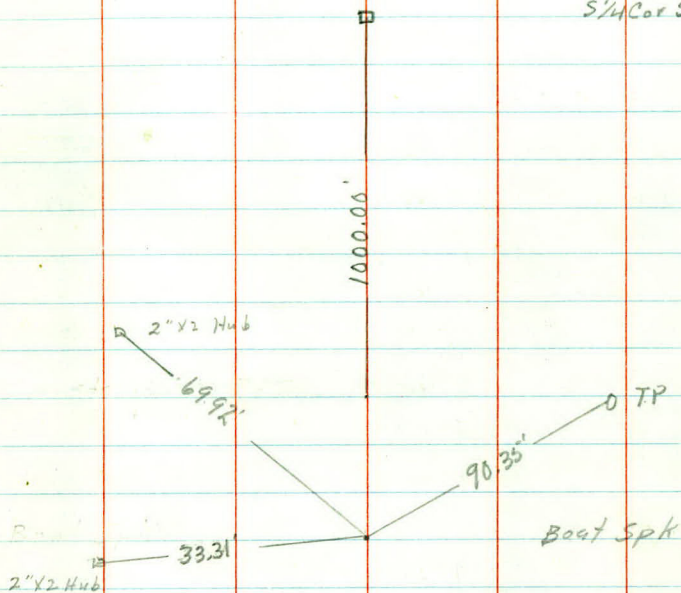
Finished 11/13/41

Sta	Point		ΔL	ΔR
+86.93	P.T	8° 21'		
+50		7° 59'		
138		7° 29'		
+50		6° 59'		
137		6° 29'		
+50		5° 59'		
136		5° 29'		
+50		4° 59'		
135		4° 29'		
134+72.44	P.I	16° 42'		
+50		3° 59'	D 2°	
134		3° 29'	T 420.51	
+50		2° 59'	L 835.00	
133		2° 29'	R 2864.93	
+50		1° 59'		
132		1° 29'		
+50		0° 59'		
131		0° 29'		
130+51.93	P.C	0° 00'		

Description

7B

Stone Mon

S $\frac{1}{4}$ Cor Sec 3

Note W. Main 45'
From & Cor'd I

Sta	Point	ΔL	ΔR
+32.68 = P.T. =	149 + 00.60	A Line	
149		8° 10'	
+50		7° 40'	
148		7° 10'	
+50		6° 40'	
147		6° 10'	
+50		5° 40'	
146		5° 10'	
+50		4° 40'	
145 + 10.84	P.I.		17° 00'
145		4° 10'	D 2°
+50		3° 40'	T 42816 .
144		3° 10'	L 850.00 .
+50		2° 40'	R 2864.93 .
143		2° 10'	
+50		1° 40'	
142		1° 10'	
+50		0° 40'	
141		0° 10'	
140 + 82.68	P.C.	0° 00'	

Description

2
7C

Note W.W. Pipeline

41' No at S $\frac{1}{4}$ Sec
3

2" x 2" Hub

46.67'

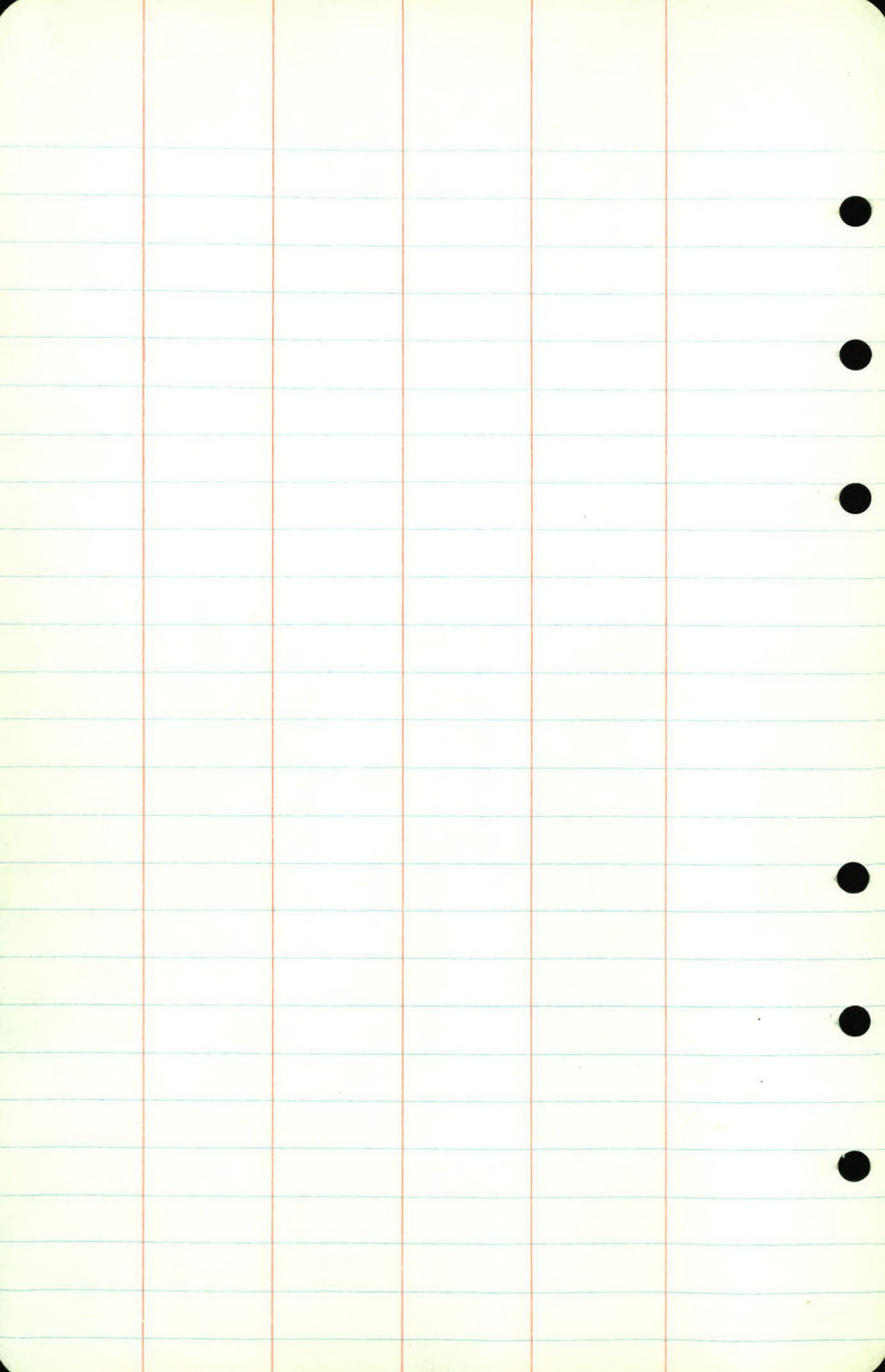
Boat Spk. E Hamline Ave

300'

S $\frac{1}{4}$ Sec 3
Mon

82.58'

6" Pop.



Cross sections

Sta	+	Δ	Elev
BM	3.95	914.14.	910.19
0+00			10.19
+ 20		Edge Pav	10.11
+ 25			09.9
+ 50			09.6
+ 77			09.5
1			09.4
+ 50			09.0
2			09.1
+ 50			09.0
3			08.7
+ 50			08.6
4			08.4

Lt

K

Rt

4

Drill hole 0400 K 12.5 #10 & G.R. 7"

$$\frac{4.19}{50}$$

395

$$\frac{3.73}{50}$$

✓

$$\frac{4.25}{50}$$

403

$$\frac{3.78}{50}$$

✓

$$\frac{5.2}{50}$$

$$\frac{5.7}{39}$$

$$\frac{5.4}{21}$$

$$\frac{4.3}{17}$$

42

$$\frac{4.03}{51}$$

Edge Pure ✓

$$\frac{5.6}{50}$$

$$\frac{5.2}{26}$$

$$\frac{6.0}{22}$$

$$\frac{5.9}{19}$$

$$\frac{4.7}{16}$$

45

$$\frac{3.80}{25}$$

Pure

✓

$$\frac{5.2}{50}$$

$$\frac{5.1}{26}$$

$$\frac{6.2}{22-19}$$

$$\frac{4.8}{15}$$

46

$$\frac{4.4}{16}$$

$$\frac{5.9}{24}$$

$$\frac{6.2}{30}$$

$$\frac{3.8}{42}$$

$$\frac{3.66}{50}$$

Pure ✓

$$\frac{5.1}{50}$$

$$\frac{5.1}{27}$$

$$\frac{6.3}{23-20}$$

$$\frac{5.0}{15}$$

47

$$\frac{4.7}{15}$$

$$\frac{6.5}{20}$$

$$\frac{6.8}{42}$$

$$\frac{6.2}{50}$$

✓

$$\frac{4.7}{50}$$

$$\frac{4.7}{27}$$

$$\frac{6.3}{23-19}$$

$$\frac{5.1}{15}$$

51

$$\frac{5.0}{15}$$

$$\frac{6.5}{18-23}$$

$$\frac{5.3}{26}$$

$$\frac{5.9}{50}$$

✓

$$\frac{4.7}{50}$$

$$\frac{4.3}{29}$$

$$\frac{6.7}{23-19}$$

$$\frac{5.0}{15}$$

50

$$\frac{4.9}{15}$$

$$\frac{6.8}{18-23}$$

$$\frac{4.4}{28}$$

$$\frac{5.5}{50}$$

✓

$$\frac{4.3}{50}$$

$$\frac{4.7}{28}$$

$$\frac{6.7}{23-19}$$

$$\frac{5.0}{15}$$

5.1

$$\frac{5.2}{15}$$

$$\frac{6.9}{18-23}$$

$$\frac{4.6}{27}$$

$$\frac{5.0}{50}$$

✓

$$\frac{3.7}{50}$$

$$\frac{4.4}{28}$$

$$\frac{4.1}{23-19}$$

$$\frac{5.6}{15}$$

5.4

$$\frac{5.5}{15}$$

$$\frac{7.2}{19-23}$$

$$\frac{5.0}{27}$$

$$\frac{5.4}{50}$$

✓

$$\frac{3.9}{50}$$

$$\frac{4.8}{40}$$

$$\frac{5.1}{28}$$

$$\frac{7.2}{23-19}$$

$$\frac{5.8}{15}$$

5.5

$$\frac{5.1}{15}$$

$$\frac{7.1}{19-23}$$

$$\frac{5.4}{27}$$

$$\frac{5.8}{50}$$

✓

$$\frac{4.5}{50}$$

$$\frac{6.3}{33}$$

$$\frac{6.7}{25}$$

$$\frac{7.3}{23-19}$$

$$\frac{5.7}{15}$$

5.7

$$\frac{5.8}{15}$$

$$\frac{7.4}{18-23}$$

$$\frac{6.7}{26}$$

$$\frac{6.7}{50}$$

✓

✓

Sta	+	π	-	Elev
		91414		
4				08.3
5				08.3
T.P.	5.70	91435	5.49	908.65
+50				08.7
6				08.9
+50				08.9
7				09.1
+50				09.3
8				09.3
+50				09.7
9				09.9
+50				09.9
10				10.2

Lt

±

Rt

10

$$\frac{5.5}{50} \frac{7.1}{33} \frac{7.1}{25} \frac{7.4}{22-20} \frac{6.0}{15} 5.8 \frac{5.8}{15} \frac{7.5}{18-22} \frac{6.8}{24} \frac{7.2}{50} \checkmark$$

$$\frac{5.5}{50} \frac{5.5}{44} \frac{7.3}{32} \frac{7.1}{25} \frac{7.6}{23} \frac{7.5}{20} \frac{6.0}{15} 5.8 \frac{6.0}{15} \frac{7.5}{19} \frac{7.7}{21} \frac{7.2}{23} \frac{7.5}{50} \checkmark$$

$$\frac{4.2}{50} \frac{7.0}{36} \frac{7.1}{34} \frac{6.9}{25} \frac{7.8}{24} \frac{7.8}{20} \frac{6.1}{15} 5.7 \frac{6.0}{15} \frac{7.9}{18} \frac{7.9}{22} \frac{7.1}{23} \frac{7.8}{50} \checkmark$$

$$\frac{5.3}{50} \frac{6.4}{35} \frac{6.3}{26} \frac{7.5}{23-20} \frac{5.7}{15} 5.5 \frac{5.8}{15} \frac{7.4}{19-22} \frac{6.7}{23} \frac{7.5}{50} \checkmark$$

$$\frac{5.3}{50} \frac{5.1}{27} \frac{6.0}{31} \frac{6.1}{26} \frac{7.4}{23} \frac{7.1}{19} \frac{5.6}{15} 5.5 \frac{5.5}{15} \frac{7.4}{19-22} \frac{6.4}{24} \frac{7.1}{50} \checkmark$$

$$\frac{5.3}{50} \frac{4.8}{42} \frac{6.6}{31} \frac{6.6}{24} \frac{7.0}{23} \frac{7.0}{19} \frac{5.4}{15} 5.3 \frac{5.3}{15} \frac{7.1}{19-22} \frac{6.3}{23} \frac{6.7}{50} \checkmark$$

$$\frac{5.4}{50} \frac{6.1}{35} \frac{6.9}{32} \frac{6.9}{19} \frac{5.3}{15} 5.1 \frac{5.0}{15} \frac{6.8}{19} \frac{6.8}{22} \frac{6.2}{23} \frac{6.2}{50} \checkmark$$

$$\frac{4.5}{50} \frac{4.4}{45} \frac{5.5}{34} \frac{5.6}{26} \frac{6.8}{24} \frac{6.8}{19} \frac{5.3}{15} 5.1 \frac{5.0}{15} \frac{6.8}{19-23} \frac{5.7}{24} \frac{5.7}{50} \checkmark$$

$$\frac{4.3}{50} \frac{4.4}{28} \frac{6.0}{25} \frac{6.5}{22} \frac{6.3}{19} \frac{4.8}{15} 4.7 \frac{4.8}{15} \frac{6.0}{18} \frac{6.5}{21} \frac{6.1}{23} \frac{4.4}{27} \frac{4.8}{50} \checkmark$$

$$\frac{4.9}{50} \frac{4.0}{38} \frac{3.8}{29} \frac{5.7}{25} \frac{6.1}{22} \frac{5.8}{19} \frac{4.7}{15} 4.5 \frac{4.6}{15} \frac{5.7}{18} \frac{6.1}{21} \frac{5.8}{24} \frac{3.2}{30} \frac{3.6}{50} \checkmark$$

$$\frac{4.8}{50} \frac{3.7}{28} \frac{5.5}{25} \frac{6.1}{22} \frac{5.7}{19} \frac{4.6}{15} 4.5 \frac{4.4}{13} \frac{6.0}{18-22} \frac{2.7}{31} \frac{3.0}{50} \checkmark$$

$$\frac{4.5}{50} \frac{3.2}{28} \frac{5.3}{24} \frac{5.8}{21} \frac{5.4}{18} \frac{4.2}{15} 4.2 \frac{4.1}{15} \frac{5.2}{18} \frac{5.7}{21} \frac{5.1}{25} \frac{2.4}{30} \frac{2.7}{50}$$

Sta	+	±	-	Elev
		914.35		
10+50				10.7
T.P.	6.80	917.40	3.75	910.60
11				11.0
+50				11.2
12				11.4
+50				11.8
B.M	5.47	917.40	5.47	911.93 911.94
+67				12.0
+71				12.1
+75				12.1
+78				12.1
+95				12.3
13+08				12.3
+13				12.2

Lt

Z

Rt

$\frac{4.0}{50} \frac{3.0}{29} \frac{4.6}{26} \frac{5.2}{23} \frac{5.0}{18} \frac{4.1}{15} 3.7 \frac{3.9}{11} \frac{4.4}{15} \frac{5.3}{22} \frac{4.8}{25} \frac{2.42.6}{30 50}$

$\frac{6.5}{50} \frac{5.6}{29} \frac{7.9}{25} \frac{8.4}{22} \frac{7.9}{19} \frac{6.6}{15} 6.4 \frac{6.5}{15} \frac{7.5}{17} \frac{8.0}{22} \frac{7.5}{25} \frac{5.4}{29} \frac{5.6}{50}$

$\frac{6.4}{50} \frac{5.8}{28} \frac{7.4}{25} \frac{7.9}{22} \frac{7.5}{19} \frac{6.3}{15} 6.2 \frac{6.0}{15} \frac{8.0}{19} \frac{8.2}{23} \frac{6.3}{28} \frac{6.2}{50}$

$\frac{7.1}{50} \frac{7.2}{26} \frac{7.6}{23} \frac{7.6}{19} \frac{6.2}{15} 6.0 \frac{6.0}{15} \frac{7.8}{19} \frac{8.0}{23} \frac{7.0}{25} \frac{6.6}{50}$

$\frac{7.0}{50} \frac{6.8}{25} \frac{7.5}{23} \frac{7.2}{19} \frac{5.9}{15} 5.6 \frac{5.7}{15} \frac{7.4}{19} \frac{7.5}{23} \frac{7.1}{25} \frac{6.4}{50}$

Spk 17 T.P S.W Con Co Rd J Long Lake Rd

$\frac{6.7}{50} \frac{6.4}{29} \frac{7.0}{24} \frac{6.9}{20} \frac{5.6}{16} 5.4 \frac{5.4}{15} \frac{6.9}{20} \frac{7.1}{24} \frac{6.7}{26} \frac{6.2}{50}$

$\frac{7.0}{50} \frac{6.6}{20} \frac{5.6}{16} 5.3 \frac{5.5}{16} \frac{6.9}{24} \frac{6.6}{50}$

$\frac{7.0}{50} \frac{6.8}{25} \frac{5.7}{18} 5.3 \frac{5.4}{18} \frac{6.3}{23} \frac{6.3}{50}$

$\frac{5.9}{50} 5.3 \frac{5.1}{23} \frac{4.8}{50}$

$\frac{5.6}{50} 5.1 \frac{4.4}{50}$

$\frac{5.9}{50} 5.1 \frac{4.7}{50}$

$\frac{7.4}{50} \frac{6.6}{39} \frac{5.8}{37} 5.2 \frac{4.8}{19} \frac{6.4}{25} \frac{6.2}{50}$

Sta + π - Elev

917.40.

13+16 12.2 .

+19 12.2 .

+50 12.3 .

14 12.6 .

+50 12.5 .

15- 12.2 .

+50 12.1 .

16 12.3 .

+50 12.3 .

T.P. 4.57 916.70. 5.27 912.13 .

17 12.1 .

+50 12.1 .

18 11.8 .

L+

L

R+

iv

$$\frac{7.4}{50} \frac{7.0}{42} \frac{5.5}{35} 5.2 \frac{4.9}{16} \frac{6.6}{20} \frac{6.3}{50}$$

$$\frac{5.7}{50} \frac{5.3}{25} \frac{6.4}{22} \frac{6.4}{18} \frac{5.2}{15} \frac{5.0}{15} \frac{6.6}{20} \frac{6.8}{24} \frac{5.9}{26} \frac{5.7}{50}$$

$$\frac{6.0}{50} \frac{5.6}{25} \frac{6.7}{23-19} \frac{5.0}{15} 5.1 \frac{5.0}{15} \frac{6.6}{19} \frac{6.7}{23} \frac{5.2}{27} \frac{5.9}{50}$$

$$\frac{6.0}{50} \frac{6.0}{25} \frac{6.8}{22-18} \frac{4.9}{15} 4.8 \frac{4.9}{15} \frac{6.5}{19} \frac{6.6}{23} \frac{5.3}{27} \frac{5.4}{50}$$

$$\frac{6.3}{50} \frac{6.8}{24} \frac{6.8}{19} \frac{5.3}{15} 4.9 \frac{4.8}{15} \frac{6.5}{19} \frac{6.5}{24} \frac{4.1}{31} \frac{4.4}{50}$$

$$\frac{6.1}{50} \frac{6.6}{24} \frac{7.2}{22-19} \frac{5.1}{15} 5.2 \frac{5.3}{15} \frac{7.0}{19-23} \frac{4.7}{29} \frac{3.3}{50}$$

$$\frac{5.2}{50} \frac{6.0}{25} \frac{7.1}{23-19} \frac{5.4}{15} 5.3 \frac{5.5}{14} \frac{6.9}{19} \frac{7.1}{21} \frac{6.5}{25} \frac{3.7}{31} \frac{3.1}{50}$$

$$\frac{5.2}{50} \frac{4.9}{26} \frac{6.8}{23-19} \frac{5.2}{15} 5.1 \frac{5.4}{14} \frac{6.3}{17} \frac{6.9}{21} \frac{6.4}{25} \frac{3.6}{31} \frac{3.2}{50}$$

$$\frac{4.5}{50} \frac{4.9}{27} \frac{6.6}{24} \frac{6.8}{21} \frac{6.4}{18} \frac{5.2}{15} 5.1 \frac{5.2}{14} \frac{6.3}{18} \frac{6.9}{21} \frac{6.7}{24} \frac{3.8}{30} \frac{3.2}{50}$$

$$\frac{3.9}{50} \frac{3.9}{28} \frac{5.7}{23-19} \frac{4.8}{15} 4.6 \frac{4.8}{15} \frac{5.7}{19} \frac{6.0}{23} \frac{2.5}{31} \frac{2.2}{50}$$

$$\frac{3.3}{50} \frac{3.5}{30} \frac{5.8}{24-19} \frac{4.6}{15} 4.6 \frac{4.6}{14} \frac{5.6}{18} \frac{6.0}{21} \frac{6.1}{23} \frac{2.0}{31} \frac{1.7}{50}$$

$$\frac{3.2}{50} \frac{4.0}{28} \frac{6.0}{23} \frac{6.2}{19} \frac{4.8}{15} 4.9 \frac{4.7}{15} \frac{6.0}{20-23} \frac{3.0}{30} \frac{2.6}{50}$$

Sta + π — Elev

916.70.

18+50

11.7 .

19

11.5 .

T.P.

0.90

915.13 . 247

914.23 .

+50

11.3 .

20

11.2 .

+50

11.1 .

21

10.8 .

+50

10.4 .

22

10.1 .

+50

09.9 .

23

09.7 .

+50

09.5 .

24

09.2 .

Lt

L

Rt

$$\frac{3.6}{50} \frac{3.8}{29} \frac{6.4}{24} \frac{6.4}{19} \frac{5.3}{15} 5.0 \frac{4.7}{14} \frac{6.2}{19} \frac{6.3}{24} \frac{3.6}{30} \frac{3.2}{50}$$

$$\frac{3.8}{50} \frac{4.0}{29} \frac{6.3}{24} \frac{6.6}{20} \frac{5.3}{15} 5.2 \frac{5.2}{15} \frac{6.2}{20} \frac{6.3}{24} \frac{3.4}{30} \frac{3.3}{50}$$

SpK in Fe Post 33 Rt SH₂ 19+47

$$\frac{2.9}{50} \frac{3.0}{29} \frac{4.8}{24} \frac{5.3}{19} \frac{3.7}{15} 3.8 \frac{3.9}{15} \frac{4.9}{19} \frac{5.1}{22} \frac{4.7}{25} \frac{1.6}{31} \frac{1.4}{50}$$

$$\frac{3.5}{50} \frac{3.9}{27} \frac{5.3}{24} \frac{5.6}{21} \frac{5.2}{18} \frac{3.8}{15} 3.9 \frac{4.1}{15} \frac{5.2}{19} \frac{5.6}{22} \frac{3.6}{28} \frac{4.2}{50}$$

$$\frac{4.3}{50} \frac{4.5}{27} \frac{5.5}{24} \frac{5.9}{21} \frac{5.6}{19} \frac{4.3}{15} 4.0 \frac{4.2}{15} \frac{5.4}{19} \frac{5.8}{21} \frac{5.6}{24} \frac{4.2}{27} \frac{5.1}{50}$$

$$\frac{3.8}{50} \frac{4.4}{27} \frac{5.7}{23} \frac{6.0}{21} \frac{5.8}{18} \frac{4.2}{15} 4.3 \frac{4.2}{15} \frac{6.1}{21} \frac{6.1}{24} \frac{4.4}{27} \frac{5.2}{50}$$

$$\frac{5.5}{50} \frac{5.7}{24} \frac{6.3}{22} \frac{6.1}{19} \frac{4.6}{15} 4.7 \frac{4.3}{15} \frac{5.9}{18} \frac{6.5}{23} \frac{5.3}{25} \frac{6.3}{50}$$

$$\frac{6.4}{50} \frac{6.7}{20} \frac{4.8}{15} 5.0 \frac{4.9}{15} \frac{7.0}{20} \frac{7.0}{24} \frac{6.5}{25} \frac{7.2}{50}$$

$$\frac{7.1}{50} \frac{8.3}{32} \frac{7.8}{22} \frac{5.2}{15} 5.2 \frac{5.4}{11} \frac{5.0}{16} \frac{7.8}{28} \frac{8.0}{50}$$

$$\frac{8.0}{50} \frac{8.0}{21} \frac{5.5}{15} 5.4 \frac{5.7}{11} \frac{5.4}{15} \frac{8.2}{24} \frac{8.6}{50}$$

$$\frac{7.4}{50} \frac{8.4}{27} \frac{8.9}{25} \frac{8.8}{22} \frac{5.6}{13} 5.6 \frac{5.7}{15} \frac{8.4}{22} \frac{8.5}{50}$$

$$\frac{7.8}{50} \frac{8.4}{27} \frac{8.8}{26} \frac{8.7}{22} \frac{5.8}{15} 5.9 \frac{5.8}{15} \frac{8.3}{21} \frac{8.3}{25} \frac{7.9}{26} \frac{8.2}{50}$$

Sta	+	π	-	Elev
		915.13.		
24+50				09.0.
25				08.9. ✓
T.P.	5.08	913.96.	6.25	908.88.
+50				08.9.
26				08.8.
B.M	290	913.96.	29.0	911.06. 911.08.
+50				08.6.
27				08.2.
+50				07.8.
28				07.4.
+50				07.1.
29				06.9.
+50				06.9.
30				06.8.

LH.

L

R.

174

$$\frac{7.7}{50} \quad \frac{8.1}{27} \quad \frac{9.1}{25-21} \quad \frac{6.1}{16} \quad 6.1 \quad \frac{5.8}{15} \quad \frac{8.4}{20-25} \quad \frac{7.5}{26} \quad \frac{7.7}{50}$$

$$\frac{6.8}{50} \quad \frac{7.9}{27} \quad \frac{9.2}{26-21} \quad \frac{6.3}{15} \quad 6.2 \quad \frac{5.9}{15} \quad \frac{8.2}{19} \quad \frac{8.6}{22} \quad \frac{8.4}{25} \quad \frac{7.3}{26} \quad \frac{7.6}{50}$$

$$\frac{5.4}{50} \quad \frac{6.3}{28} \quad \frac{7.9}{26} \quad \frac{7.9}{21} \quad \frac{5.2}{15} \quad 5.1 \quad \frac{4.8}{15} \quad \frac{6.9}{18} \quad \frac{7.3}{22} \quad \frac{7.0}{24} \quad \frac{5.3}{27} \quad \frac{5.9}{50}$$

$$\frac{5.2}{50} \quad \frac{6.2}{28} \quad \frac{7.8}{25-20} \quad \frac{5.1}{15} \quad 5.2 \quad \frac{5.1}{15} \quad \frac{7.1}{19} \quad \frac{7.5}{22} \quad \frac{7.0}{25} \quad \frac{5.2}{28} \quad \frac{5.7}{50}$$

SPH 14 8" Oak 75 Lt Sta 26 +40

$$\frac{5.2}{50} \quad \frac{6.1}{28} \quad \frac{7.8}{25} \quad \frac{8.1}{22} \quad \frac{7.9}{21} \quad \frac{5.5}{15} \quad 5.4 \quad \frac{5.3}{14} \quad \frac{7.4}{19} \quad \frac{7.8}{21} \quad \frac{7.5}{24} \quad \frac{5.1}{29} \quad \frac{5.5}{50}$$

$$\frac{4.4}{50} \quad \frac{5.2}{29} \quad \frac{7.7}{25} \quad \frac{8.1}{22} \quad \frac{7.8}{19} \quad \frac{5.8}{14} \quad 5.8 \quad \frac{5.7}{14} \quad \frac{7.5}{18} \quad \frac{7.9}{22} \quad \frac{7.6}{24} \quad \frac{5.0}{29} \quad \frac{5.3}{50}$$

$$\frac{3.2}{50} \quad \frac{4.2}{31} \quad \frac{7.5}{24} \quad \frac{8.0}{21} \quad \frac{7.6}{18} \quad \frac{6.2}{15} \quad 6.2 \quad \frac{6.1}{15} \quad \frac{7.7}{19} \quad \frac{8.1}{22} \quad \frac{7.8}{24} \quad \frac{4.4}{31} \quad \frac{4.9}{50}$$

$$\frac{3.1}{50} \quad \frac{3.5}{33} \quad \frac{8.3}{24} \quad \frac{8.3}{19} \quad \frac{6.7}{15} \quad 6.6 \quad \frac{6.3}{15} \quad \frac{8.1}{19} \quad \frac{8.5}{24} \quad \frac{4.1}{32} \quad \frac{4.4}{50}$$

$$\frac{3.1}{50} \quad \frac{3.2}{35} \quad \frac{7.5}{26} \quad \frac{8.3}{21} \quad \frac{7.0}{15} \quad 6.9 \quad \frac{6.6}{15} \quad \frac{8.1}{18} \quad \frac{8.6}{22} \quad \frac{8.3}{24} \quad \frac{4.0}{33} \quad \frac{4.6}{50}$$

$$\frac{2.3}{50} \quad \frac{2.4}{36} \quad \frac{8.0}{25} \quad \frac{8.0}{19} \quad \frac{7.3}{15} \quad 7.1 \quad \frac{7.0}{15} \quad \frac{8.5}{18} \quad \frac{8.8}{21} \quad \frac{7.9}{26} \quad \frac{4.2}{34} \quad \frac{4.6}{50}$$

$$\frac{1.2}{50} \quad \frac{1.5}{37} \quad \frac{8.5}{25} \quad \frac{8.5}{19} \quad \frac{7.1}{15} \quad 7.1 \quad \frac{7.3}{15} \quad \frac{8.4}{18} \quad \frac{8.8}{22} \quad \frac{8.0}{26} \quad \frac{4.0}{34} \quad \frac{4.6}{50}$$

$$\frac{1.6}{50} \quad \frac{1.7}{38} \quad \frac{6.3}{29} \quad \frac{8.6}{23} \quad \frac{8.6}{20} \quad \frac{8.0}{18} \quad \frac{7.3}{12} \quad 7.2 \quad \frac{7.3}{14} \quad \frac{8.5}{18} \quad \frac{8.9}{21} \quad \frac{8.1}{26} \quad \frac{4.2}{33} \quad \frac{5.0}{50}$$

Sta	+	+	-	Elev
		913.96		
30+50				06.4
31				06.4
T.P	5.11	912.16	6.91	907.05
+50				06.2
32				06.2
+06				06.2
+50				06.1
33				06.2
+50				06.1
34				06.1
+50				06.0
35				06.0
T.P	4.25	910.88	5.53	906.63
+50				06.2

L+

R

R+

15

$$\frac{1.0}{50} \frac{1.9}{39} \frac{5.3}{32} \frac{8.0}{26} \frac{8.9}{21} \frac{8.3}{18} \frac{7.4}{12} 7.6 \frac{7.5}{13} \frac{8.9}{17} \frac{9.3}{21} \frac{8.4}{26} \frac{4.3}{33} \frac{5.2}{50}$$

$$\frac{2.3}{50} \frac{2.7}{37} \frac{5.7}{31} \frac{8.9}{25} \frac{8.2}{21} \frac{7.6}{17} \frac{7.6}{12} 7.6 \frac{7.7}{13} \frac{9.3}{19} \frac{8.4}{22} \frac{5.4}{26} \frac{6.4}{31} \frac{6.4}{50}$$

$$\frac{1.4}{50} \frac{1.5}{36} \frac{6.9}{26} \frac{7.5}{22} \frac{7.3}{20} \frac{6.0}{15} 6.0 \frac{6.1}{15} \frac{7.6}{19} \frac{7.7}{22} \frac{7.0}{26} \frac{5.0}{30} \frac{5.2}{50}$$

$$\frac{2.1}{50} \frac{2.5}{37} \frac{3.7}{34} \frac{4.6}{29} \frac{7.2}{25} \frac{7.4}{21} \frac{5.7}{15} 6.0 \frac{5.8}{15} \frac{7.4}{19} \frac{7.8}{22} \frac{6.4}{27} \frac{7.7}{50}$$

$$\frac{2.4}{50} \frac{2.7}{37} \frac{4.4}{32} \frac{4.8}{30} \frac{7.5}{25} \frac{5.7}{20} 6.0 \frac{5.8}{15} \frac{7.6}{19} \frac{7.9}{50}$$

$$\frac{4.2}{50} \frac{4.3}{44} \frac{5.1}{41} \frac{6.7}{33} \frac{7.6}{31} \frac{7.7}{20} \frac{5.9}{15} 6.1 \frac{6.2}{15} \frac{8.2}{21} \frac{8.8}{50}$$

$$\frac{7.4}{50} \frac{7.5}{37} \frac{8.5}{28} \frac{8.0}{21} \frac{6.1}{15} 6.0 \frac{5.8}{15} \frac{9.0}{23} \frac{9.6}{50}$$

$$\frac{7.8}{50} \frac{8.9}{38} \frac{9.4}{25} \frac{6.4}{15} 6.1 \frac{6.2}{15} \frac{9.9}{24} \frac{10.5}{50}$$

$$\frac{8.6}{50} \frac{9.5}{35} \frac{9.5}{26} \frac{8.6}{22} \frac{6.1}{15} 6.1 \frac{6.2}{15} \frac{10.6}{25} \frac{11.4}{50}$$

$$\frac{9.3}{50} \frac{9.8}{41} \frac{10.1}{28} \frac{9.5}{24} \frac{6.4}{15} 6.2 \frac{6.2}{15} \frac{11.8}{26} \frac{12.1}{50}$$

$$\frac{10.1}{50} \frac{10.1}{41} \frac{10.9}{37} \frac{10.8}{29} \frac{10.0}{22} \frac{6.1}{15} 6.2 \frac{6.2}{15} \frac{11.1}{25} \frac{11.8}{28} \frac{12.6}{50}$$

$$\frac{8.2}{50} \frac{8.2}{45} \frac{9.8}{31} \frac{9.7}{24} \frac{4.8}{15} 4.7 \frac{4.7}{15} \frac{9.0}{24} \frac{10.8}{30} \frac{11.6}{50}$$

Sta	+	π	-	Elev
		910.88		
36	+00			06.2
	+50			06.1
37				06.0
	+50			06.0
38				06.1
	+50			06.1
39				06.1
B.M	5.48	911.10	5.28	905.60
	+50			06.0
40				06.1
	+50			06.1
41				06.0
	+50			06.1

905.62

Lt

K

Pt

16

$$\frac{9.1}{50} \quad \frac{10.0}{41} \quad \frac{10.0}{27} \quad \frac{8.8}{23} \quad \frac{4.9}{15} \quad 47 \quad \frac{5.0}{15} \quad \frac{9.2}{25} \quad \frac{9.9}{31} \quad \frac{11.4}{35} \quad \frac{12.0}{50}$$

$$\frac{9.2}{50} \quad \frac{10.0}{39} \quad \frac{10.0}{26} \quad \frac{7.6}{21} \quad \frac{4.9}{15} \quad 48 \quad \frac{4.9}{15} \quad \frac{9.5}{25} \quad \frac{11.6}{32} \quad \frac{11.8}{50}$$

$$\frac{9.1}{50} \quad \frac{9.1}{46} \quad \frac{10.6}{41} \quad \frac{10.2}{27} \quad \overset{Juv}{\frac{10.13}{27}} \quad \frac{4.8}{15} \quad 49 \quad \frac{5.0}{15} \quad \frac{11.62}{27} \quad \frac{11.3}{27} \quad \frac{11.7}{50}$$

$$\frac{8.6}{50} \quad \frac{8.6}{42} \quad \frac{10.3}{32} \quad \frac{10.3}{25} \quad \frac{5.0}{15} \quad 4.9 \quad \frac{4.8}{15} \quad \frac{11.0}{28} \quad \frac{11.6}{50}$$

$$\frac{8.7}{50} \quad \frac{9.8}{38} \quad \frac{9.5}{26} \quad \frac{4.7}{15} \quad 4.8 \quad \frac{5.0}{15} \quad \frac{9.8}{26} \quad \frac{11.0}{29} \quad \frac{11.6}{50}$$

$$\frac{8.7}{50} \quad \frac{8.7}{41} \quad \frac{9.8}{33} \quad \frac{9.5}{24} \quad \frac{4.9}{15} \quad 4.8 \quad \frac{4.8}{15} \quad \frac{9.4}{24} \quad \frac{10.8}{27} \quad \frac{11.4}{50}$$

$$\frac{8.5}{50} \quad \frac{8.5}{41} \quad \frac{9.5}{33} \quad \frac{9.9}{27} \quad \frac{5.0}{15} \quad 4.8 \quad \frac{4.9}{15} \quad \frac{9.2}{24} \quad \frac{10.6}{30} \quad \frac{11.0}{50}$$

$$\text{Top Mon Star } 39+30$$

$$\frac{8.2}{50} \quad \frac{9.8}{30} \quad \frac{10.8}{27} \quad \frac{9.3}{25} \quad \frac{9.1}{21} \quad \frac{5.3}{15} \quad 5.1 \quad \frac{5.0}{15} \quad \frac{9.6}{23} \quad \frac{10.3}{27} \quad \frac{10.8}{50}$$

$$\frac{8.3}{50} \quad \frac{8.3}{38} \quad \frac{9.9}{30} \quad \frac{9.7}{26} \quad \frac{8.1}{22} \quad \frac{7.8}{20} \quad \frac{5.1}{15} \quad 5.0 \quad \frac{5.2}{15} \quad \frac{8.4}{22} \quad \frac{9.1}{25} \quad \frac{9.5}{50}$$

$$\frac{7.8}{50} \quad \frac{7.2}{20} \quad \frac{5.2}{15} \quad 5.0 \quad \frac{5.0}{15} \quad \frac{7.2}{19} \quad \frac{7.6}{26} \quad \frac{8.6}{50}$$

$$\frac{6.5}{50} \quad \frac{6.1}{26} \quad \frac{6.8}{23} \quad \frac{6.9}{21} \quad \frac{6.7}{19} \quad \frac{5.1}{15} \quad 5.1 \quad \frac{5.0}{15} \quad \frac{6.7}{19} \quad \frac{6.7}{23} \quad \frac{7.3}{50}$$

$$\frac{5.1}{15} \quad \frac{4.9}{27} \quad \frac{6.9}{23} \quad \frac{5.0}{19} \quad \frac{5.0}{15} \quad 5.0 \quad \frac{4.9}{15} \quad \frac{6.8}{19-23} \quad \frac{5.7}{26} \quad \frac{6.7}{50}$$

50

Sta + π - Elev

911.10.

42

06.0.

+50

05.9.

43

06.3.

+50

06.4.

44

06.5.

+50

06.6.

T.P. 5.33 912.74 3.69 907.41.

45

06.9.

+50

07.0.

46

07.2.

+50

07.3.

47

07.5.

+50

07.9.

Lt

L

Rt

19

$$\frac{5.2}{50} \frac{4.8}{28} \frac{7.1}{24-19} \frac{5.1}{15} 5.1 \frac{5.1}{15} \frac{7.0}{18-22} \frac{5.8}{25} \frac{7.1}{50}$$

$$\frac{4.1}{50} \frac{5.2}{28} \frac{7.1}{24-19} \frac{5.2}{15} 5.2 \frac{5.2}{15} \frac{7.2}{18-22} \frac{6.1}{25} \frac{6.4}{50}$$

$$\frac{4.1}{50} \frac{5.0}{27} \frac{7.0}{24-19} \frac{5.0}{15} 4.8 \frac{4.9}{15} \frac{6.8}{18-22} \frac{5.5}{26} \frac{6.0}{50}$$

$$\frac{3.7}{50} \frac{4.4}{28} \frac{6.7}{24-18} \frac{4.7}{15} 4.7 \frac{4.8}{15} \frac{6.7}{19-24} \frac{4.6}{28} \frac{5.2}{50}$$

$$\frac{3.5}{50} \frac{3.8}{28} \frac{6.6}{24-19} \frac{4.7}{15} 4.6 \frac{4.6}{15} \frac{6.4}{18-23} \frac{4.2}{28} \frac{4.6}{50}$$

$$\frac{3.3}{50} \frac{3.4}{29} \frac{6.4}{24-19} \frac{4.5}{15} 4.5 \frac{4.3}{15} \frac{6.2}{18-24} \frac{3.4}{29} \frac{3.6}{50}$$

$$\frac{4.5}{50} \frac{4.5}{30} \frac{7.3}{24} \frac{7.3}{20} \frac{6.0}{15} 5.8 \frac{5.7}{14} \frac{7.1}{18} \frac{7.7}{21} \frac{7.2}{24} \frac{4.0}{31} \frac{4.2}{50}$$

$$\frac{3.9}{50} \frac{3.6}{31} \frac{7.3}{24-20} \frac{5.9}{15} 5.7 \frac{5.7}{14} \frac{6.8}{18} \frac{7.4}{21} \frac{7.0}{24} \frac{3.3}{31} \frac{3.9}{50}$$

$$\frac{3.8}{50} \frac{3.2}{31} \frac{7.2}{24-20} \frac{5.4}{15} 5.5 \frac{5.4}{14} \frac{6.8}{18} \frac{7.1}{21} \frac{6.8}{24} \frac{3.4}{31} \frac{3.8}{50}$$

$$\frac{3.0}{50} \frac{2.9}{31} \frac{7.0}{24-21} \frac{5.5}{15} 5.4 \frac{5.4}{15} \frac{6.9}{18-24} \frac{3.0}{32} \frac{3.2}{50}$$

$$\frac{3.0}{50} \frac{2.6}{32} \frac{6.9}{24-20} \frac{5.3}{15} 5.2 \frac{5.1}{15} \frac{6.7}{19-24} \frac{2.4}{32} \frac{2.5}{50}$$

$$\frac{3.1}{50} \frac{2.4}{32} \frac{6.5}{24-20} \frac{4.8}{15} 4.8 \frac{4.7}{15} \frac{6.1}{18} \frac{6.5}{22} \frac{6.3}{24} \frac{2.2}{33} \frac{2.1}{50}$$

Sta + π - Elev

912.74.

48 08.1.

1.

+50 08.3.

49 08.5.

+50 08.7.

50 08.9.

T.P 527 915.08 2.93 909.81.

+50 09.3.

51 09.5.

+50 09.6.

52 09.8.

+50 10.0.

53 10.3.

B.M 2.49 915.11. 2.49 912.59 912.62

+50 10.7. -

Lt

Z

Pt

18

$$\frac{3.4}{50} \quad \frac{2.9}{30} \quad \frac{6.5}{24-20} \quad \frac{4.7}{15} \quad 4.6 \quad \frac{4.6}{15} \quad \frac{6.2}{19-24} \quad \frac{2.2}{32} \quad \frac{2.2}{50}$$

$$\frac{4.0}{50} \quad \frac{3.4}{29} \quad \frac{6.1}{24-19} \quad \frac{4.4}{15} \quad 4.4 \quad \frac{4.3}{15} \quad \frac{5.7}{18} \quad \frac{6.2}{22} \quad \frac{5.8}{25} \quad \frac{3.0}{30} \quad \frac{3.1}{50}$$

$$\frac{3.7}{50} \quad \frac{3.7}{28} \quad \frac{6.1}{24-20} \quad \frac{4.2}{15} \quad 4.2 \quad \frac{4.2}{15} \quad \frac{5.7}{18} \quad \frac{6.2}{21} \quad \frac{5.8}{24} \quad \frac{3.7}{28} \quad \frac{4.3}{50}$$

$$\frac{3.6}{50} \quad \frac{3.4}{28} \quad \frac{6.1}{24-20} \quad \frac{4.1}{15} \quad 4.0 \quad \frac{4.0}{15} \quad \frac{5.5}{18} \quad \frac{6.0}{24} \quad \frac{4.1}{27} \quad \frac{4.6}{50}$$

$$\frac{3.6}{50} \quad \frac{3.4}{27} \quad \frac{5.6}{23-20} \quad \frac{3.8}{15} \quad 3.8 \quad \frac{3.8}{15} \quad \frac{5.3}{19} \quad \frac{5.8}{24} \quad \frac{3.7}{28} \quad \frac{4.3}{50}$$

$$\frac{6.2}{50} \quad \frac{6.2}{27} \quad \frac{7.6}{24-20} \quad \frac{5.8}{15} \quad 5.8 \quad \frac{5.7}{15} \quad \frac{7.4}{18} \quad \frac{7.9}{20} \quad \frac{7.6}{23} \quad \frac{6.0}{27} \quad \frac{6.1}{50}$$

$$\frac{6.2}{50} \quad \frac{6.6}{25} \quad \frac{7.6}{23-18} \quad \frac{7.2}{18} \quad \frac{5.9}{50} \quad 5.6 \quad \frac{5.6}{15} \quad \frac{7.1}{18} \quad \frac{7.6}{23} \quad \frac{6.4}{25} \quad \frac{6.3}{50}$$

$$\frac{6.9}{50} \quad \frac{6.6}{26} \quad \frac{7.4}{23-19} \quad \frac{5.5}{15} \quad 5.5 \quad \frac{5.6}{15} \quad \frac{7.1}{18} \quad \frac{7.6}{23} \quad \frac{6.5}{25} \quad \frac{6.6}{50}$$

$$\frac{6.3}{50} \quad \frac{6.3}{26} \quad \frac{7.3}{23} \quad \frac{6.8}{19} \quad \frac{5.4}{15} \quad 5.3 \quad \frac{5.3}{15} \quad \frac{6.8}{18} \quad \frac{7.4}{23} \quad \frac{6.3}{25} \quad \frac{6.3}{50}$$

$$\frac{5.0}{50} \quad \frac{5.1}{27} \quad \frac{6.8}{24} \quad \frac{6.8}{19} \quad \frac{5.0}{15} \quad 5.1 \quad \frac{5.1}{15} \quad \frac{6.8}{19} \quad \frac{6.8}{23} \quad \frac{5.6}{25} \quad \frac{5.4}{50}$$

$$\frac{3.5}{50} \quad \frac{3.9}{29} \quad \frac{6.7}{23-20} \quad \frac{4.8}{15} \quad 4.8 \quad \frac{4.8}{15} \quad \frac{6.8}{19} \quad \frac{6.8}{23} \quad \frac{5.2}{25} \quad \frac{5.0}{50}$$

Sph SW com. Wood M. H. Box 43' Lt Sta 53+15

$$\frac{3.9}{50} \quad \frac{3.7}{29} \quad \frac{5.9}{24} \quad \frac{6.6}{21} \quad \frac{6.1}{-18} \quad \frac{4.6}{15} \quad 4.4 \quad \frac{4.2}{15} \quad \frac{6.6}{19} \quad \frac{6.6}{24} \quad \frac{4.4}{28} \quad \frac{4.7}{50}$$

Sta	+	+	-	Elev
		915.11.		11.0.

54

+50

11.0.

55

T.P.	3.21	914.05	4.27	910.84
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+50

11.1.

56

11.0.

+50

10.8.

57

09.9.

+50

08.9.

58

07.4.

+33

06.4.

+62

05.4.

59

04.1.

T.P.	1.04	905.05	10.04	904.01
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LT

R

RT

19

$$\frac{4.0}{50} \frac{4.2}{28} \frac{5.7}{24} \frac{6.2}{22} \frac{5.8}{18} \frac{4.2}{15} \frac{4.1}{15} \frac{6.3}{19} \frac{6.3}{23} \frac{4.3}{27} \frac{4.3}{50}$$

$$\frac{4.3}{50} \frac{4.6}{27} \frac{6.2}{24-19} \frac{4.1}{15} \frac{4.1}{15} \frac{6.1}{19} \frac{6.1}{23} \frac{4.8}{26} \frac{4.7}{50}$$

$$\frac{4.2}{50} \frac{4.7}{26} \frac{6.0}{23-19} \frac{4.0}{15} \frac{4.0}{15} \frac{4.1}{15} \frac{5.9}{19} \frac{5.9}{23} \frac{5.1}{25} \frac{5.3}{50}$$

Nail in 6" Tree 33' RT Sta 54+50

$$\frac{3.2}{30} \frac{2.6}{28} \frac{4.2}{24} \frac{4.6}{21} \frac{4.2}{19} \frac{2.7}{15} \frac{3.0}{15} \frac{2.6}{19} \frac{4.7}{23} \frac{3.1}{26} \frac{3.4}{50}$$

$$\frac{3.4}{50} \frac{2.4}{28} \frac{4.7}{23-20} \frac{2.8}{15} \frac{3.1}{15} \frac{2.9}{15} \frac{4.8}{19-23} \frac{3.2}{27} \frac{3.9}{50}$$

$$\frac{3.4}{50} \frac{2.4}{29} \frac{5.0}{23-19} \frac{3.2}{15} \frac{3.3}{15} \frac{3.3}{15} \frac{5.2}{19-23} \frac{2.9}{27} \frac{3.3}{50}$$

$$\frac{4.0}{50} \frac{2.9}{29} \frac{5.8}{23-20} \frac{4.2}{15} \frac{4.2}{15} \frac{3.9}{15} \frac{5.9}{20-23} \frac{3.3}{29} \frac{3.8}{50}$$

$$\frac{4.5}{50} \frac{3.9}{29} \frac{6.9}{24-20} \frac{5.2}{15} \frac{5.2}{15} \frac{5.0}{15} \frac{6.9}{20-24} \frac{4.1}{29} \frac{4.0}{50}$$

$$\frac{5.4}{50} \frac{5.5}{29} \frac{7.3}{25} \frac{8.1}{21} \frac{7.5}{17} \frac{6.4}{15} \frac{6.7}{15} \frac{6.3}{15} \frac{8.1}{20-24} \frac{6.8}{28} \frac{7.0}{50}$$

$$\frac{6.3}{50} \frac{6.9}{29} \frac{8.6}{25} \frac{9.3}{21} \frac{8.8}{18} \frac{7.4}{15} \frac{7.7}{15} \frac{7.4}{15} \frac{9.6}{19-23} \frac{7.7}{27} \frac{8.2}{50}$$

$$\frac{7.2}{50} \frac{8.5}{28} \frac{10.6}{20-24} \frac{8.6}{15} \frac{8.7}{15} \frac{8.4}{15} \frac{10.3}{20} \frac{11.0}{32} \frac{12.4}{50}$$

$$\frac{7.2}{50} \frac{7.2}{45} \frac{10.2}{27} \frac{11.8}{23-20} \frac{10.2}{15} \frac{10.0}{15} \frac{9.9}{15} \frac{14.7}{25} \frac{16.4}{50}$$

Sta	+	π	-	Elev
		905.05		
59+50				02.5
60				00.9
+50				00.0
61				00.2
+50				00.3
62				01.0
T.P.	10.45	911.41	409	900.96
+50				01.9
63				02.8
+50				03.8
64				04.7
+50				05.6
65				06.5

Lt.

L

Rt

20

$$\frac{12.2}{50} \frac{11.6}{43} \frac{4.5}{34} \frac{4.7}{20} \frac{2.5}{15} 2.6 \frac{2.5}{15} \frac{10.4}{32} \frac{13.0}{50}$$

$$\frac{11.2}{50} 0.0 \frac{5.9}{42} \frac{6.2}{34} \frac{4.1}{20} \frac{4.5}{15} 4.2 \frac{15.2}{33} \frac{16.3}{50}$$

$$\frac{11.6}{50} \frac{10.7}{43} \frac{6.8}{33} \frac{7.2}{20} \frac{5.3}{15} 5.1 \frac{5.2}{14} \frac{16.3}{33} \frac{16.25}{33} \frac{16.2}{50}$$

$$\frac{12.0}{50} \frac{10.6}{43} \frac{6.9}{33} \frac{7.9}{21} \frac{8.14}{20} \frac{5.0}{15} 4.9 \frac{4.9}{15} \frac{11.23}{28} \frac{12.3}{29} \frac{13.0}{50}$$

$$\frac{12.0}{50} 0.0 \frac{6.5}{42} \frac{6.7}{32} \frac{4.8}{19} \frac{4.8}{15} 4.8 \frac{4.6}{15} \frac{9.3}{25} \frac{10.4}{50}$$

$$\frac{11.7}{50} 0.0 \frac{1.9}{42} \frac{2.7}{37} \frac{5.9}{30} \frac{4.2}{24} \frac{4.1}{19} \frac{4.0}{15} \frac{5.9}{19} \frac{6.9}{50}$$

$$\frac{4.2}{50} \frac{6.1}{34} \frac{10.6}{25} \frac{11.2}{21} \frac{10.7}{18} \frac{9.6}{15} 9.5 \frac{9.5}{15} \frac{11.1}{19-24} \frac{9.5}{27} \frac{10.3}{50}$$

$$\frac{3.3}{50} \frac{4.2}{35} \frac{9.8}{24} \frac{10.3}{21} \frac{8.7}{15} 8.6 \frac{8.6}{15} \frac{10.3}{19-24} \frac{7.9}{29} \frac{8.9}{50}$$

$$\frac{3.0}{50} \frac{4.0}{36} \frac{8.4}{25} \frac{9.2}{19} \frac{7.6}{14} 7.6 \frac{7.8}{15} \frac{9.2}{18} \frac{9.7}{21} \frac{9.4}{24} \frac{6.3}{30} \frac{7.1}{50}$$

$$\frac{2.2}{50} \frac{2.7}{35} \frac{7.6}{25} \frac{8.4}{21} \frac{6.7}{15} 6.7 \frac{6.9}{15} \frac{8.2}{18} \frac{8.6}{21} \frac{8.2}{25} \frac{4.2}{33} \frac{4.9}{50}$$

$$\frac{2.1}{50} \frac{2.3}{35} \frac{5.0}{29} \frac{6.9}{25} \frac{7.4}{20} \frac{5.9}{15} 5.8 \frac{6.0}{15} \frac{7.3}{18} \frac{7.9}{21} \frac{7.1}{25} \frac{2.8}{33} \frac{3.2}{50}$$

$$\frac{2.0}{50} \frac{2.2}{33} \frac{4.6}{28} \frac{6.2}{25} \frac{6.6}{21} \frac{6.1}{19} \frac{4.9}{15} 4.9 \frac{5.0}{15} \frac{6.4}{19} \frac{6.7}{22} \frac{6.1}{25} \frac{3.7}{30} \frac{4.3}{50}$$

Sta	+	π	-	Elev	
		911.41.		06.9.	
65+21					
+32				07.1.	
+47				07.4.	
+54		Top Curb		07.59.	
B.M.		3.95		907.46	907.40
+68.46		$\pm$ STH 8		07.46.	
+81.96		Top Curb		07.47.	-
+89				07.5.	
+95				07.4.	
66+05				07.0.	
+17				06.6.	
B.M	3.29	910.69	3.95	907.46	907.40
+50				05.5.	
67				04.1.	

Lt

K

Rt

24

$$\frac{1.4}{50} \frac{2.4}{34} \frac{5.2}{21} \frac{5.8}{21} \frac{5.1}{19} \frac{4.5}{15} 4.5 \frac{4.4}{14} \frac{5.5}{16} \frac{6.3}{21} \frac{5.8}{24} \frac{3.7}{30} \frac{4.2}{50}$$

$$\frac{1.9}{50} \frac{3.7}{38} \frac{4.8}{30} \frac{5.4}{22} \frac{3.7}{15} 4.3 \frac{4.2}{15} \frac{4.2}{22} \frac{3.8}{23} \frac{4.6}{50}$$

$$\frac{2.7}{50} \frac{3.7}{15} 4.0$$

$$\frac{4.1}{26} \frac{4.9}{50}$$

$$\frac{2.74}{50}$$

382

$$\frac{5.10}{50}$$

Top Brass Plug & U.S. #8 & Co. Rd. "I"

$$\frac{2.86}{50}$$

3.95

$$\frac{5.16}{50}$$

$$\frac{2.81}{50}$$

3.94

$$\frac{5.15}{50}$$

$$\frac{2.9}{50} \frac{3.3}{29} 3.9 \frac{4.3}{17} \frac{5.2}{29} \frac{5.0}{41} \frac{5.2}{50}$$

$$\frac{4.6}{50} \frac{4.9}{41} \frac{3.3}{32} \frac{4.0}{24} 4.0 \frac{4.4}{12} \frac{5.8}{26} \frac{6.7}{31} \frac{8.2}{50}$$

$$\frac{5.6}{50} \frac{5.8}{34} \frac{4.6}{21} 4.4 \frac{5.5}{20} \frac{6.9}{28} \frac{8.0}{50}$$

$$\frac{2.2}{50} \frac{5.7}{26} \frac{4.9}{16} 4.8 \frac{5.6}{16} \frac{6.4}{23} \frac{2.0}{38} \frac{2.9}{50}$$

Top Brass plug "I" Y U.S. #8

$$\frac{0.4}{50} \frac{4.2}{40} \frac{4.7}{32} \frac{6.6}{26} \frac{6.6}{20} \frac{5.7}{15} 5.2 \frac{5.5}{15} \frac{6.7}{19.22} \frac{6.4}{25} \frac{5.3}{28} \frac{1.4}{40}$$

$$\frac{1.9}{50} \frac{5.9}{41} \frac{6.4}{31} \frac{8.4}{26} \frac{8.4}{19} \frac{7.4}{16} 6.6 \frac{7.2}{15} \frac{8.4}{19} \frac{7.9}{24} \frac{5.8}{34} \frac{1.3}{45} \frac{1.3}{50}$$

Sta	+	π	-	Elev
		918.69.		02.2 .

67+50

68				99.6 .
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+50				97.3 .
-----	--	--	--	--------

T.P.	1.85	898.87	13.67	897.02.
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L9				94.8 .
----	--	--	--	--------

+50				92.4 .
-----	--	--	--	--------

70				90.0 .
----	--	--	--	--------

+50				87.6 .
-----	--	--	--	--------

T.P.	4.10	891.51	11.46	887.41 .
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71				85.3 .
----	--	--	--	--------

+50				83.4 .
-----	--	--	--	--------

72				82.3 .
----	--	--	--	--------

+50				81.8 .
-----	--	--	--	--------

73				81.3 .
----	--	--	--	--------

B.M	1.78	885.95	7.33	884.18	884.17 .
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Lt

L

Rt

22

$\frac{3.9}{50}$ $\frac{3.9}{47}$ $\frac{8.0}{40}$ $\frac{8.3}{31}$ $\frac{9.8}{26}$ $\frac{10.5}{22}$ $\frac{9.5}{16}$ 8.5 $\frac{9.0}{15}$ $\frac{10.1}{19}$ $\frac{9.4}{24}$ $\frac{8.6}{30}$ $\frac{6.4}{38}$ $\frac{1.8}{50}$

$\frac{6.3}{50}$ $\frac{6.3}{48}$ $\frac{9.8}{41}$ $\frac{10.8}{36}$ $\frac{10.7}{31}$ $\frac{12.5}{25}$ $\frac{13.1}{22}$ $\frac{11.6}{16}$ 11.1 $\frac{11.4}{15}$ $\frac{12.3}{19}$ $\frac{12.2}{21}$ $\frac{8.7}{36}$ $\frac{3.6}{50}$

$\frac{9.1}{50}$ $\frac{9.1}{47}$ $\frac{13.0}{39}$ $\frac{13.1}{32}$ $\frac{15.3}{25}$ $\frac{15.3}{21}$ $\frac{14.1}{16}$ 13.4 $\frac{13.9}{15}$ $\frac{14.6}{18}$ $\frac{14.6}{24}$ $\frac{10.1}{36}$ $\frac{7.4}{43}$ $\frac{2.5}{50}$

$\frac{1.7}{50}$ $\frac{1.4}{45}$ $\frac{3.8}{38}$ $\frac{4.0}{32}$ $\frac{5.3}{27}$ $\frac{5.3}{20}$ $\frac{4.5}{17}$ 4.1 $\frac{4.5}{15}$ $\frac{5.5}{19}$ $\frac{5.4}{24}$ $\frac{2.0}{35}$ $\frac{1.1}{50}$

$\frac{4.9}{50}$ $\frac{4.8}{43}$ $\frac{7.7}{31}$ $\frac{7.6}{23}$ $\frac{6.7}{16}$ 6.5 $\frac{6.9}{15}$ $\frac{8.0}{19}$ $\frac{8.4}{26}$ $\frac{7.0}{32}$ $\frac{7.7}{50}$

$\frac{4.2}{50}$ $\frac{7.8}{40}$ $\frac{10.4}{31}$ $\frac{10.5}{25}$ $\frac{9.5}{22}$ $\frac{9.2}{14}$ 8.9 $\frac{9.2}{15}$ $\frac{10.1}{18}$ $\frac{10.8}{28}$ $\frac{11.7}{36}$ $\frac{11.8}{50}$

$\frac{8.5}{50}$ $\frac{8.6}{45}$ $\frac{13.8}{33}$ $\frac{14.0}{28}$ $\frac{11.9}{23}$ $\frac{11.9}{16}$ 11.3 $\frac{11.5}{14}$ $\frac{13.8}{21}$ $\frac{14.8}{30}$ $\frac{16.3}{34}$ $\frac{17.5}{50}$

$\frac{1.7}{50}$ $\frac{2.3}{46}$ $\frac{8.6}{32}$ $\frac{8.6}{26}$ $\frac{6.7}{16}$ 6.2 $\frac{6.1}{15}$ $\frac{10.9}{28}$ $\frac{13.2}{50}$

$\frac{2.3}{50}$ $\frac{2.3}{45}$ $\frac{10.8}{31}$ $\frac{10.8}{27}$ $\frac{9.8}{22}$ $\frac{8.4}{15}$ 8.1 $\frac{8.1}{15}$ $\frac{12.0}{26}$ $\frac{14.6}{36}$ $\frac{14.3}{50}$

$\frac{2.2}{50}$ $\frac{2.8}{45}$ $\frac{11.7}{29}$ $\frac{9.3}{12}$ 9.2 $\frac{9.8}{18}$ $\frac{12.0}{25}$ $\frac{13.5}{32}$ $\frac{15.1}{50}$

$\frac{2.6}{50}$ $\frac{2.6}{47}$ $\frac{11.5}{29}$ $\frac{10.4}{23}$ $\frac{10.2}{13}$ 9.7 $\frac{10.2}{17}$ $\frac{13.9}{28}$ $\frac{14.9}{35}$ $\frac{14.6}{40}$ $\frac{14.1}{50}$

$\frac{2.5}{50}$ $\frac{2.6}{46}$ $\frac{11.5}{31}$ $\frac{11.7}{26}$ $\frac{10.5}{15}$ 10.2 $\frac{10.2}{17}$ $\frac{14.7}{31}$ $\frac{14.7}{42}$ $\frac{14.7}{50}$

Spk in Top End Guard Rail Post N.W. Cor Bridge

Sta	+	Δ	-	Elev
		885.95		
73	+50			81.2
	+80			81.2
	+86	West End Bridge		81.3
74				81.3
	+37	East End Bridge		81.3
	+43			81.2
	+66			81.1
75				80.9
	+50			80.8
76				81.4
	T.P.	8.36	892.46	1.85
	+50			884.70
				82.8
77				84.1

L.

Z

Rt.

$$\begin{array}{r} +3.3 \quad 6.0 \quad 7.4 \quad 7.1 \quad 5.8 \quad 5.3 \quad 4.7 \quad 5.2 \quad 9.8 \quad 9.8 \\ 50-47 \quad 32 \quad 25 \quad 21 \quad 17 \quad 13 \quad 48 \quad 15 \quad 22 \quad 36 \quad 50 \end{array}$$

$$\begin{array}{r} +2.6 \quad 3.9 \quad 5.8 \quad 10.2 \quad 4.8 \quad 4.8 \quad 9.0 \quad 9.3 \quad 6.6 \quad 9.2 \quad 9.5 \\ 50-46 \quad 35 \quad 29 \quad 23-21 \quad 11 \quad 48 \quad 11 \quad 19 \quad 22 \quad 27 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} +2.6 \quad 5.2 \quad 6.7 \quad 8.3 \quad 10.6 \quad 10.5 \quad 5.0 \quad 4.7 \quad 4.7 \quad 10.8 \quad 9.1 \quad 9.3 \\ 50 \quad 36 \quad 28 \quad 27 \quad 22 \quad 14 \quad 14 \quad 47 \quad 14 \quad 14 \quad 26 \quad 50 \end{array}$$

$$47 \quad \frac{12.54}{\text{Ever Water Rice Co.}}$$

$$\begin{array}{r} +2.5 \quad 7.6 \quad 10.0 \quad 10.8 \quad 4.9 \quad 4.9 \quad 10.7 \quad 9.8 \quad 6.8 \quad 6.8 \quad 8.2 \quad 8.5 \\ 50-48 \quad 34 \quad 25 \quad 13 \quad 13 \quad 47 \quad 14 \quad 14 \quad 24 \quad 30 \quad 32 \quad 36 \quad 50 \end{array}$$

$$\begin{array}{r} +2.5 \quad 4.3 \quad 5.2 \quad 9.5 \quad 9.7 \quad 4.7 \quad 4.9 \quad 8.8 \quad 7.5 \quad 7.1 \quad 8.5 \quad 8.8 \\ 50-45 \quad 36 \quad 33 \quad 26 \quad 22 \quad 13 \quad 4.8 \quad 11 \quad 21 \quad 27 \quad 30 \quad 34 \quad 50 \end{array}$$

$$\begin{array}{r} +2.9 \quad 8.4 \quad 5.7 \quad 5.2 \quad 5.0 \quad 4.7 \quad 8.7 \quad 9.1 \\ 50-46 \quad 30 \quad 23 \quad 11 \quad 4.9 \quad 15 \quad 24 \quad 33 \quad 50 \end{array}$$

$$\begin{array}{r} +2.6 \quad +2.4 \quad 6.4 \quad 6.6 \quad 5.1 \quad 5.0 \quad 5.6 \quad 8.4 \quad 8.6 \\ 50 \quad 45 \quad 31 \quad 18 \quad 16 \quad 5.1 \quad 16 \quad 24 \quad 33 \quad 50 \end{array}$$

$$\begin{array}{r} +2.7 \quad 6.5 \quad 5.5 \quad 5.2 \quad 5.2 \quad 5.6 \quad 9.1 \quad 10.4 \\ 50-46 \quad 28 \quad 12 \quad 5.2 \quad 15 \quad 20 \quad 30 \quad 50 \end{array}$$

$$\begin{array}{r} +3.0 \quad 5.1 \quad 4.7 \quad 4.6 \quad 4.6 \quad 4.9 \quad 7.4 \quad 7.1 \\ 50-45 \quad 30 \quad 11 \quad 4.6 \quad 16 \quad 28 \quad 33 \quad 50 \end{array}$$

$$\begin{array}{r} 2.6 \quad 2.6 \quad 10.2 \quad 10.8 \quad 10.8 \quad 9.9 \quad 10.1 \quad 9.9 \quad 10.2 \quad 11.0 \quad 11.0 \quad 9.8 \quad 10.1 \\ 50 \quad 46 \quad 31 \quad 28 \quad 23 \quad 17 \quad 13 \quad 9.7 \quad 17 \quad 21 \quad 28 \quad 33 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 3.2 \quad 3.2 \quad 8.7 \quad 9.7 \quad 9.7 \quad 8.8 \quad 8.4 \quad 8.8 \quad 9.2 \quad 10.3 \quad 10.4 \quad 5.9 \quad 6.0 \\ 50 \quad 45 \quad 31 \quad 26 \quad 24 \quad 15 \quad 8.4 \quad 18 \quad 20 \quad 25 \quad 34 \quad 40 \quad 50 \end{array}$$

Sta	+	π	-	Elev
		892.46		

77+50				85.3
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78				86.6
----	--	--	--	------

+22				87.2
-----	--	--	--	------

+50				87.8
-----	--	--	--	------

79				89.0
----	--	--	--	------

+50				90.3
-----	--	--	--	------

T.P	8.36	899.35	1.47	890.99
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80				91.7
----	--	--	--	------

+50				93.1
-----	--	--	--	------

81				94.4
----	--	--	--	------

+50				96.0
-----	--	--	--	------

T.P	7.67	904.64	2.38	896.97
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82				97.3
----	--	--	--	------

+50				98.2
-----	--	--	--	------

L+

2

R+ 24

$$\frac{46}{50} \frac{46}{45} \frac{8.5}{30} \frac{8.4}{20} \frac{7.1}{16} 7.2 \frac{5.4}{22} \frac{8.1}{26} \frac{8.3}{33} \frac{3.5}{41} \frac{3.4}{50}$$

$$\frac{6.0}{50} \frac{7.5}{27} \frac{7.2}{18} \frac{6.4}{14} 5.9 \frac{5.9}{17} \frac{6.2}{21} \frac{6.9}{25} \frac{7.2}{32} \frac{6.0}{36} \frac{2.4}{41} \frac{2.2}{50}$$

$$\frac{6.1}{50} \frac{6.1}{32} \frac{7.1}{27} \frac{7.1}{20} \frac{5.8}{14} 5.3 \frac{5.3}{17} \frac{5.9}{21} \frac{6.2}{29} \frac{2.8}{36} \frac{2.3}{50}$$

$$\frac{6.5}{50} \frac{6.1}{32} \frac{6.5}{25} \frac{6.2}{19} \frac{5.2}{12} 4.7 \frac{4.7}{17} \frac{5.4}{20} \frac{5.7}{29} \frac{4.1}{32} \frac{3.1}{50}$$

$$\frac{5.9}{50} \frac{5.4}{20} \frac{4.0}{15} 3.5 \frac{3.6}{16} \frac{4.7}{21} \frac{4.9}{30} \frac{4.0}{50}$$

$$\frac{4.1}{50} \frac{3.6}{31} \frac{4.1}{28} \frac{3.9}{19} \frac{2.6}{14} 2.2 \frac{2.3}{17} \frac{3.3}{20} \frac{3.2}{29} \frac{2.2}{32} \frac{2.3}{50}$$

$$\frac{9.7}{50} \frac{9.3}{32} \frac{9.7}{28} \frac{9.5}{20} \frac{8.0}{15} 7.7 \frac{7.9}{17} \frac{8.7}{21} \frac{8.7}{29} \frac{8.0}{31} \frac{6.9}{50}$$

$$\frac{8.9}{50} \frac{8.1}{20} \frac{7.9}{15} 6.3 \frac{6.4}{18} \frac{7.4}{21} \frac{7.3}{29} \frac{6.0}{32} \frac{5.5}{50}$$

$$\frac{7.5}{50} \frac{6.8}{31} \frac{6.7}{19} \frac{5.6}{14} 5.0 \frac{4.7}{17} \frac{5.5}{20} \frac{5.5}{29} \frac{4.3}{31} \frac{2.3}{37} \frac{3.8}{50}$$

$$\frac{5.9}{50} \frac{5.2}{32} \frac{5.6}{30} \frac{5.4}{19} \frac{4.1}{14} 3.4 \frac{3.2}{17} \frac{4.1}{21} \frac{4.2}{29} \frac{2.3}{31} \frac{1.4}{50}$$

$$\frac{9.2}{50} \frac{8.5}{31} \frac{9.6}{28} \frac{9.3}{19} \frac{7.9}{14} 7.3 \frac{7.2}{16} \frac{8.5}{21} \frac{8.5}{28} \frac{5.0}{32} \frac{4.4}{50}$$

$$\frac{7.3}{50} \frac{6.8}{82} \frac{8.3}{27} \frac{8.0}{18} \frac{6.9}{14} 6.4 \frac{6.4}{16} \frac{7.3}{21} \frac{7.5}{27} \frac{3.8}{34} \frac{3.3}{50}$$

Sta	+	π	-	Elev
		904.64.		

83				98.9
----	--	--	--	------

+50				99.4
-----	--	--	--	------

84				99.7
----	--	--	--	------

+50				99.6
-----	--	--	--	------

85				99.7
----	--	--	--	------

+50				99.9
-----	--	--	--	------

86				99.8
----	--	--	--	------

T.P.	5.57	905.46	4.75	899.89
------	------	--------	------	--------

+50				99.8
-----	--	--	--	------

87				00.0
----	--	--	--	------

+50				00.3
-----	--	--	--	------

88				00.6
----	--	--	--	------

+50				00.6
-----	--	--	--	------

Lt

R

Pt

$$\frac{6.3}{50} \frac{5.6}{33} \frac{7.4}{26} \frac{7.4}{20} \frac{6.1}{15} 5.7 \frac{6.0}{16} \frac{7.1}{21} \frac{6.6}{29} \frac{7.4}{39} \frac{3.8}{50}$$

$$\frac{6.2}{50} \frac{5.8}{30} \frac{6.6}{27} \frac{6.6}{19} \frac{5.8}{15} 5.2 \frac{5.5}{16} \frac{4.7}{20} \frac{6.8}{27} \frac{3.7}{32} \frac{4.7}{39} \frac{4.7}{50}$$

$$\frac{5.3}{50} \frac{4.7}{31} \frac{6.3}{27} \frac{6.2}{19} \frac{5.4}{16} 4.9 \frac{5.4}{17} \frac{6.2}{20} \frac{6.3}{27} \frac{3.3}{33} \frac{5.6}{39} \frac{5.9}{50}$$

$$\frac{4.5}{50} \frac{4.9}{30} \frac{6.2}{26} \frac{6.2}{21} \frac{5.0}{17} 5.0 \frac{5.3}{17} \frac{6.2}{20} \frac{6.6}{28} \frac{5.4}{31} \frac{6.0}{35} \frac{7.0}{50}$$

$$\frac{4.4}{50} \frac{4.0}{33} \frac{6.0}{27} \frac{6.1}{20} \frac{5.0}{17} 4.9 \frac{5.1}{16} \frac{6.3}{21} \frac{6.6}{27} \frac{5.6}{30} \frac{6.3}{34} \frac{6.9}{50}$$

$$\frac{4.9}{50} \frac{4.8}{32} \frac{6.2}{27} \frac{6.1}{19} \frac{5.0}{15} 4.7 \frac{5.1}{17} \frac{6.2}{20} \frac{6.4}{29} \frac{5.1}{31} \frac{5.5}{50}$$

$$\frac{5.6}{50} \frac{4.9}{32} \frac{6.4}{27} \frac{6.2}{19} \frac{5.0}{15} 4.8 \frac{5.0}{17} \frac{6.1}{21} \frac{6.3}{29} \frac{4.9}{31} \frac{5.0}{50}$$

$$\frac{7.5}{50} \frac{7.5}{44} \frac{6.5}{34} \frac{7.1}{29} \frac{6.9}{19} \frac{6.0}{16} 5.7 \frac{6.0}{17} \frac{7.1}{20} \frac{7.0}{28} \frac{5.2}{31} \frac{5.7}{50}$$

$$\frac{6.6}{50} \frac{7.0}{44} \frac{6.5}{33} \frac{7.1}{30} \frac{6.7}{19} \frac{6.0}{16} 5.5 \frac{5.9}{18} \frac{6.8}{21} \frac{6.9}{29} \frac{5.5}{31} \frac{5.6}{50}$$

$$\frac{6.4}{50} \frac{6.8}{41} \frac{6.3}{38} \frac{6.2}{32} \frac{7.0}{29} \frac{6.8}{20} \frac{5.6}{16} 5.2 \frac{5.4}{17} \frac{6.5}{20} \frac{6.6}{28} \frac{5.3}{31} \frac{6.0}{50}$$

$$\frac{5.7}{50} \frac{6.0}{39} \frac{5.1}{32} \frac{6.8}{27} \frac{6.5}{19} \frac{5.4}{15} 4.9 \frac{5.3}{17} \frac{6.3}{20} \frac{6.7}{29} \frac{5.2}{31} \frac{6.0}{50}$$

$$\frac{5.7}{50} \frac{5.4}{31} \frac{6.7}{28} \frac{6.6}{19} \frac{5.3}{15} 4.9 \frac{5.1}{16} \frac{6.4}{20} \frac{6.5}{29} \frac{4.9}{31} \frac{5.6}{34} \frac{6.0}{50}$$

Sta	+	π	-	Elev
		905.46		

89				00.7
----	--	--	--	------

+50				00.7
-----	--	--	--	------

90				00.6
----	--	--	--	------

+50				00.7
-----	--	--	--	------

91				00.7
----	--	--	--	------

+50				00.7
-----	--	--	--	------

B.M	5.18	905.57	5.07	900.39	900.39
-----	------	--------	------	--------	--------

92				00.8	£ Mounds View Rd
----	--	--	--	------	------------------

+16				01.0
-----	--	--	--	------

+21				00.9
-----	--	--	--	------

+50				00.9
-----	--	--	--	------

93				01.2
----	--	--	--	------

+50				01.4
-----	--	--	--	------

Lt

R

Pt

$$\frac{5.3}{50} \frac{5.4}{32} \frac{6.8}{27} \frac{6.6}{19} \frac{5.4}{15} 48 \frac{5.1}{17} \frac{6.1}{20} \frac{6.4}{29} \frac{5.2}{31} \frac{5.9}{50}$$

$$\frac{5.3}{50} \frac{5.0}{31} \frac{6.4}{29} \frac{6.7}{18} \frac{5.4}{15} 48 \frac{5.2}{16} \frac{6.2}{20} \frac{6.7}{28} \frac{4.9}{31} \frac{5.2}{50}$$

$$\frac{5.6}{50} \frac{5.5}{31} \frac{6.8}{29} \frac{6.7}{20} \frac{5.6}{16} 49 \frac{5.3}{15} \frac{6.5}{20} \frac{6.7}{29} \frac{4.6}{31} \frac{5.2}{34} \frac{5.3}{50}$$

$$\frac{5.0}{50} \frac{5.4}{32} \frac{6.3}{29} \frac{6.3}{19} \frac{5.1}{15} 48 \frac{5.2}{16} \frac{6.3}{19} \frac{6.7}{28} \frac{4.3}{31} \frac{4.9}{37} \frac{5.3}{50}$$

$$\frac{5.2}{50} \frac{5.6}{31} \frac{6.4}{28} \frac{6.3}{20} \frac{5.7}{18} \frac{5.2}{12} 48 \frac{5.3}{17} \frac{6.8}{28} \frac{5.0}{31} \frac{5.4}{50}$$

$$\frac{4.7}{50} \frac{4.7}{32} \frac{6.1}{27} \frac{6.2}{19} \frac{5.2}{16} 48 \frac{5.9}{16} \frac{5.1}{34} \frac{5.7}{50}$$

Top Men. Co Rd "I" & Mounds View Rd 92402

$$\frac{5.0}{50} 48 \frac{4.9}{50}$$

$$\frac{5.2}{50} \frac{5.5}{21} 4.6 \frac{5.2}{50}$$

$$\frac{4.7}{50} \frac{5.1}{33} \frac{6.5}{29} \frac{6.5}{22} \frac{5.4}{18} 47 \frac{5.0}{19} \frac{5.2}{50}$$

$$\frac{4.4}{50} \frac{4.5}{33} \frac{6.8}{28} \frac{6.7}{22} \frac{5.2}{16} 47 \frac{5.0}{15} \frac{4.7}{26} \frac{6.1}{50}$$

$$\frac{3.4}{50} \frac{3.7}{33} \frac{6.5}{28} \frac{6.5}{22} \frac{4.9}{16} 4.4 \frac{4.9}{26} \frac{6.3}{33} \frac{6.7}{15}$$

$$\frac{3.5}{50} \frac{3.2}{33} \frac{6.4}{28} \frac{6.4}{21} \frac{4.8}{15} 4.2 \frac{5.0}{25} \frac{5.9}{36} \frac{6.4}{50}$$

Sta	+	Δ	-	Elev
		905.57.		
94				01.5
+36				01.6
95				01.6
+50				01.5
96				01.4
+50				01.3
97				01.3
+50				01.4
T.P.	4.23	904.95	4.85	900.72
98				01.5
+50				01.6
99				01.7
+50				01.8

Lt.

2

Rt

$$\frac{4.1}{50} \frac{4.6}{35} \frac{6.1}{30} \frac{6.1}{21} \frac{4.6}{15} \quad 4.1 \quad \frac{4.8}{15} \frac{5.8}{18} \frac{6.3}{27} \frac{5.2}{30} \frac{5.9}{50}$$

$$\frac{3.9}{50} \frac{4.5}{36} \frac{6.0}{29} \frac{6.0}{22} \frac{4.5}{16} \quad 4.0 \quad \frac{4.7}{15} \frac{5.9}{20} \frac{6.0}{27} \frac{4.3}{31} \frac{4.3}{50}$$

$$\frac{4.8}{50} \frac{5.1}{36} \frac{6.1}{29} \frac{5.9}{20} \frac{4.5}{15} \quad 4.0 \quad \frac{4.6}{15} \frac{6.0}{21} \frac{6.1}{28} \frac{5.2}{31} \frac{5.5}{50}$$

$$\frac{4.7}{50} \frac{5.4}{35} \frac{6.0}{29} \frac{6.1}{21} \frac{4.7}{16} \quad 4.1 \quad \frac{4.7}{15} \frac{6.1}{21} \frac{6.7}{27} \frac{6.0}{30} \frac{6.2}{50}$$

$$\frac{5.6}{50} \frac{5.6}{33} \frac{6.2}{28} \frac{6.0}{21} \frac{4.8}{15} \quad 4.2 \quad \frac{4.9}{16} \frac{6.5}{22} \frac{6.7}{29} \frac{6.9}{50}$$

$$\frac{6.1}{50} \frac{6.0}{31} \frac{6.3}{30} \frac{6.1}{22} \frac{4.9}{16} \quad 4.3 \quad \frac{4.9}{15} \frac{6.6}{23} \frac{6.9}{50}$$

$$\frac{6.5}{50} \frac{5.9}{22} \frac{5.0}{15} \quad 4.3 \quad \frac{4.8}{15} \frac{6.4}{25} \frac{7.1}{50}$$

$$\frac{6.0}{50} \frac{5.6}{31} \frac{6.0}{26} \frac{4.9}{15} \quad 4.2 \quad \frac{4.6}{15} \frac{6.3}{22} \frac{6.9}{50}$$

$$\frac{5.3}{30} \frac{5.2}{23} \frac{4.0}{16} \quad 3.5 \quad \frac{3.9}{16} \frac{5.3}{22} \frac{5.9}{50}$$

$$\frac{5.2}{30} \frac{5.4}{30} \frac{4.0}{16} \quad 3.4 \quad \frac{3.9}{16} \frac{5.2}{23} \frac{5.9}{50}$$

$$\frac{5.4}{50} \frac{5.4}{34} \frac{4.9}{22} \frac{3.7}{16} \quad 3.3 \quad \frac{3.8}{15} \frac{5.4}{24} \frac{5.8}{50}$$

$$\frac{5.3}{50} \frac{5.1}{24} \frac{3.7}{16} \quad 3.2 \quad \frac{4.0}{15} \frac{6.2}{27} \frac{6.4}{50}$$

Sta + A - Elev
904.95 0

100 01.9

+50 02.0

101 02.2

+50 02.5

102 02.5

+50 02.7

103 02.7

T.P. 5.97 908.04 2.88 902.07

+50 02.6

104 02.8

+50 03.0

105 03.1

+50 03.2

T.P. 1.17 906.87

Lt.

R

Rt

$$\frac{4.9}{50} \quad \frac{5.2}{35} \quad \frac{5.1}{24} \quad \frac{3.7}{17} \quad 3.1 \quad \frac{3.7}{15} \quad \frac{6.2}{25} \quad \frac{6.5}{50}$$

$$\frac{4.7}{50} \quad \frac{4.8}{24} \quad \frac{3.5}{15} \quad 3.0 \quad \frac{3.6}{14} \quad \frac{6.0}{25} \quad \frac{5.9}{50}$$

$$\frac{4.2}{50} \quad \frac{4.6}{33} \quad \frac{4.8}{24} \quad \frac{3.4}{16} \quad 2.8 \quad \frac{3.3}{14} \quad \frac{4.6}{21} \quad \frac{5.4}{27} \quad \frac{5.2}{50}$$

$$\frac{3.6}{50} \quad \frac{3.7}{34} \quad \frac{4.4}{22} \quad \frac{3.2}{17} \quad 2.5 \quad \frac{2.9}{15} \quad \frac{4.7}{25} \quad \frac{4.4}{50}$$

$$\frac{3.5}{50} \quad \frac{3.6}{39} \quad \frac{4.5}{23} \quad \frac{3.0}{12} \quad 2.5 \quad \frac{2.9}{15} \quad \frac{4.5}{24} \quad \frac{3.8}{50}$$

$$\frac{3.5}{50} \quad \frac{3.6}{39} \quad \frac{4.3}{25} \quad \frac{3.8}{20} \quad \frac{2.8}{15} \quad 2.3 \quad \frac{2.6}{16} \quad \frac{4.2}{25} \quad \frac{3.8}{50}$$

$$\frac{4.0}{50} \quad \frac{4.4}{24} \quad \frac{2.9}{16} \quad 2.5 \quad \frac{2.8}{14} \quad \frac{4.9}{24} \quad \frac{4.8}{50}$$

$$\frac{7.4}{50} \quad \frac{7.1}{20} \quad \frac{6.1}{17} \quad 5.4 \quad \frac{5.9}{15} \quad \frac{8.4}{22} \quad \frac{9.2}{50}$$

$$\frac{6.6}{50} \quad \frac{6.4}{34} \quad \frac{7.1}{27} \quad \frac{7.2}{23} \quad \frac{5.8}{15} \quad 5.2 \quad \frac{5.9}{16} \quad \frac{7.5}{22} \quad \frac{8.5}{50}$$

$$\frac{5.6}{50} \quad \frac{6.2}{31} \quad \frac{7.3}{24} \quad \frac{6.9}{21} \quad \frac{5.5}{16} \quad 5.0 \quad \frac{5.3}{15} \quad \frac{7.2}{22} \quad \frac{6.9}{50}$$

$$\frac{4.8}{50} \quad \frac{5.2}{33} \quad \frac{6.8}{27} \quad \frac{6.9}{24} \quad \frac{5.3}{16} \quad 4.9 \quad \frac{5.1}{14} \quad \frac{6.7}{20} \quad \frac{6.9}{26} \quad \frac{5.7}{32} \quad \frac{6.0}{50}$$

$$\frac{4.8}{50} \quad \frac{4.4}{33} \quad \frac{6.8}{29} \quad \frac{6.4}{24} \quad \frac{5.2}{17} \quad 4.8 \quad \frac{5.4}{16} \quad \frac{6.6}{22} \quad \frac{6.8}{29} \quad \frac{4.4}{34} \quad \frac{3.7}{50}$$

Top Breather pipe 48' Lt. 105+35

Sta	+	X	-	Elev	
	1.10	907.97		906.87	
106				03.3	
+50				03.3	
107				03.2	
+50				03.0	
108				02.8	
+50				02.7	
109				02.7	
+50				02.4	
B.M			4.70	903.27	903.29
110				02.6	
+50				02.5	
111				02.6	
+50				02.5	
T.P	4.97	907.08	5.86	902.11	

Lt

Z

RT

$$\frac{5.1}{50} \frac{5.4}{32} \frac{7.0}{26} \frac{6.8}{22} \frac{5.2}{16} \frac{4.7}{15} \frac{5.5}{15} \frac{6.6}{21} \frac{7.0}{28} \frac{4.5}{34} \frac{3.8}{50}$$

$$\frac{5.6}{50} \frac{5.5}{34} \frac{7.3}{26} \frac{6.9}{22} \frac{5.3}{16} \frac{4.7}{16} \frac{5.4}{16} \frac{6.6}{22} \frac{6.6}{28} \frac{4.0}{36} \frac{3.9}{50}$$

$$\frac{6.4}{50} \frac{6.0}{33} \frac{7.1}{27} \frac{7.0}{22} \frac{5.8}{16} \frac{4.8}{15} \frac{5.4}{15} \frac{6.6}{21} \frac{7.0}{28} \frac{4.6}{33} \frac{4.0}{36} \frac{3.7}{50}$$

$$\frac{6.5}{50} \frac{6.0}{38} \frac{6.5}{31} \frac{7.6}{26} \frac{7.4}{22} \frac{5.6}{16} \frac{5.0}{15} \frac{5.7}{15} \frac{6.9}{20} \frac{7.2}{28} \frac{5.3}{33} \frac{4.8}{50}$$

$$\frac{6.6}{50} \frac{6.5}{32} \frac{7.6}{26} \frac{7.2}{22} \frac{5.8}{16} \frac{5.2}{16} \frac{5.9}{16} \frac{7.2}{21} \frac{7.6}{29} \frac{6.0}{33} \frac{5.6}{50}$$

$$\frac{6.0}{50} \frac{5.4}{33} \frac{7.1}{30} \frac{7.6}{28} \frac{7.4}{21} \frac{5.9}{15} \frac{5.3}{15} \frac{5.8}{15} \frac{7.4}{22} \frac{7.6}{29} \frac{5.4}{32} \frac{5.2}{50}$$

$$\frac{5.5}{50} \frac{5.2}{33} \frac{7.3}{28} \frac{7.2}{22} \frac{6.0}{16} \frac{5.3}{16} \frac{5.8}{14} \frac{7.5}{25} \frac{7.5}{37} \frac{6.8}{29} \frac{4.1}{33} \frac{3.8}{50}$$

$$\frac{5.3}{50} \frac{5.5}{33} \frac{7.6}{27} \frac{7.3}{21} \frac{5.8}{15} \frac{5.6}{15} \frac{5.9}{15} \frac{6.8}{19} \frac{7.3}{22} \frac{6.7}{27} \frac{3.3}{32} \frac{3.1}{50}$$

SPK 1N P.P. 30 25' RT STA 109+70

$$\frac{5.7}{50} \frac{6.5}{34} \frac{7.9}{28} \frac{7.6}{22} \frac{6.0}{15} \frac{5.4}{14} \frac{5.8}{14} \frac{7.0}{20} \frac{7.3}{26} \frac{6.8}{29} \frac{4.5}{33} \frac{4.4}{50}$$

$$\frac{6.8}{50} \frac{7.0}{33} \frac{7.9}{28} \frac{7.6}{23} \frac{6.0}{17} \frac{5.5}{16} \frac{6.0}{16} \frac{7.5}{21} \frac{7.8}{26} \frac{6.5}{30} \frac{7.1}{50}$$

$$\frac{7.8}{50} \frac{7.4}{32} \frac{8.1}{29} \frac{8.2}{26} \frac{6.1}{17} \frac{5.4}{16} \frac{6.3}{16} \frac{8.0}{23} \frac{8.7}{50}$$

$$\frac{9.6}{50} \frac{8.2}{27} \frac{6.1}{16} \frac{5.5}{17} \frac{6.2}{17} \frac{9.4}{30} \frac{10.3}{50}$$

STA	+	π	-	ELEV
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907.08.

112

02.3

+50

02.2

113

02.4

+50

02.4

114

02.4

+50

02.4

115

02.6

+50

02.8

116

03.1

T.P

4.57

907.53

4.07

903.01

+50

03.1

+70

03.2

117

03.2

L.T.

♀

R.T.

$$\frac{6.3}{50} \quad \frac{7.9}{34} \quad \frac{7.5}{33} \quad \frac{6.0}{20} \quad \frac{5.2}{16} \quad \frac{4.8}{16} \quad \frac{5.5}{16} \quad \frac{9.1}{30} \quad \frac{9.8}{50}$$

$$\frac{6.3}{50} \quad \frac{7.5}{41} \quad \frac{7.0}{23} \quad \frac{5.8}{19} \quad \frac{5.2}{16} \quad \frac{4.9}{17} \quad \frac{5.3}{17} \quad \frac{7.6}{23} \quad \frac{8.5}{31} \quad \frac{9.2}{50}$$

$$\frac{6.4}{50} \quad \frac{6.3}{45} \quad \frac{7.1}{39} \quad \frac{6.9}{24} \quad \frac{5.2}{17} \quad \frac{4.1}{16} \quad \frac{5.3}{16} \quad \frac{7.0}{27} \quad \frac{7.4}{31} \quad \frac{8.0}{50}$$

$$\frac{7.3}{50} \quad \frac{6.9}{24} \quad \frac{5.3}{19} \quad \frac{5.1}{16} \quad \frac{4.7}{16} \quad \frac{5.3}{16} \quad \frac{7.0}{27} \quad \frac{7.5}{30} \quad \frac{7.9}{50}$$

$$\frac{6.6}{50} \quad \frac{7.1}{24} \quad \frac{5.4}{19} \quad \frac{5.2}{16} \quad \frac{4.7}{16} \quad \frac{5.2}{16} \quad \frac{6.9}{23} \quad \frac{7.6}{31} \quad \frac{8.2}{50}$$

$$\frac{6.5}{50} \quad \frac{6.6}{32} \quad \frac{7.2}{27} \quad \frac{7.0}{24} \quad \frac{5.3}{16} \quad \frac{4.7}{15} \quad \frac{5.2}{15} \quad \frac{6.6}{24} \quad \frac{7.0}{50}$$

$$\frac{5.4}{50} \quad \frac{5.7}{33} \quad \frac{6.7}{30} \quad \frac{6.7}{22} \quad \frac{5.1}{16} \quad \frac{4.5}{15} \quad \frac{5.1}{15} \quad \frac{6.3}{21} \quad \frac{6.6}{28} \quad \frac{6.7}{32} \quad \frac{6.3}{50}$$

$$\frac{4.9}{50} \quad \frac{5.0}{34} \quad \frac{6.0}{31} \quad \frac{6.5}{28} \quad \frac{6.6}{22} \quad \frac{5.0}{17} \quad \frac{4.3}{15} \quad \frac{4.7}{15} \quad \frac{6.3}{22} \quad \frac{6.4}{28} \quad \frac{4.9}{33} \quad \frac{5.6}{50}$$

$$\frac{4.1}{50} \quad \frac{4.5}{32} \quad \frac{6.3}{29} \quad \frac{6.3}{22} \quad \frac{4.7}{16} \quad \frac{4.0}{15} \quad \frac{4.4}{15} \quad \frac{5.8}{22} \quad \frac{5.6}{29} \quad \frac{4.0}{33} \quad \frac{4.6}{50}$$

$$\frac{3.9}{50} \quad \frac{4.5}{34} \quad \frac{5.7}{31} \quad \frac{6.6}{27} \quad \frac{6.5}{23} \quad \frac{5.0}{16} \quad \frac{4.4}{16} \quad \frac{4.8}{16} \quad \frac{5.9}{21} \quad \frac{6.0}{26} \quad \frac{3.4}{33} \quad \frac{4.2}{50}$$

$$\frac{3.8}{50} \quad \frac{4.8}{34} \quad \frac{6.2}{30} \quad \frac{6.3}{22} \quad \frac{4.7}{15} \quad \frac{4.3}{15} \quad \frac{4.8}{15} \quad \frac{5.9}{20} \quad \frac{6.2}{27} \quad \frac{3.6}{33} \quad \frac{4.8}{50}$$

$$\frac{3.7}{50} \quad \frac{4.6}{33} \quad \frac{5.9}{31} \quad \frac{6.3}{28} \quad \frac{6.1}{21} \quad \frac{4.8}{16} \quad \frac{4.3}{15} \quad \frac{4.9}{15} \quad \frac{6.0}{21} \quad \frac{5.8}{29} \quad \frac{4.0}{33} \quad \frac{5.4}{50}$$

STA	+	π	-	ELEV
		907.53		
117	+50			03.2
118				03.3
	+50			03.4
B.M			4.21	903.32 (903.36)
119				03.1
B.M	3.53	906.89	4.21	903.32 903.36
	+50			02.9
120				02.7
	+50			02.5
121				02.5
	+50			02.6
122				02.4
	+50			02.3
123				02.1

LT

Q

RT

$$\frac{4.0}{50} \frac{5.9}{33} \frac{6.2}{30} \frac{6.8}{27} \frac{6.5}{21} \frac{4.8}{16} \frac{4.3}{15} \frac{4.9}{15} \frac{6.4}{23} \frac{6.6}{29} \frac{5.5}{33} \frac{7.2}{50}$$

$$\frac{3.9}{50} \frac{4.5}{33} \frac{5.8}{31} \frac{6.5}{28} \frac{6.5}{22} \frac{4.7}{16} \frac{4.2}{15} \frac{4.8}{15} \frac{6.3}{21} \frac{6.6}{28} \frac{6.2}{31} \frac{8.1}{50}$$

$$\frac{3.8}{50} \frac{4.9}{32} \frac{6.3}{30} \frac{6.2}{21} \frac{4.9}{15} \frac{4.1}{15} \frac{4.6}{15} \frac{5.4}{24} \frac{6.5}{33} \frac{7.0}{50}$$

Top MT STA 118 + 36.34

$$\frac{5.0}{50} \frac{5.6}{32} \frac{6.9}{30} \frac{6.9}{22} \frac{5.0}{14} \frac{4.4}{14} \frac{5.2}{14} \frac{6.5}{22} \frac{7.7}{50}$$

Top MT STA 118 + 36.34

$$\frac{5.1}{50} \frac{5.6}{32} \frac{6.4}{30} \frac{6.1}{22} \frac{4.4}{15} \frac{4.0}{15} \frac{4.7}{15} \frac{8.7}{28} \frac{9.1}{50}$$

$$\frac{4.8}{50} \frac{5.6}{32} \frac{6.2}{30} \frac{6.3}{22} \frac{4.6}{15} \frac{4.2}{15} \frac{4.8}{16} \frac{7.8}{28} \frac{7.9}{50}$$

$$\frac{4.0}{50} \frac{4.9}{32} \frac{6.2}{29} \frac{6.2}{22} \frac{4.8}{15} \frac{4.4}{17} \frac{5.0}{17} \frac{6.5}{23} \frac{6.8}{31} \frac{6.3}{33} \frac{6.6}{50}$$

$$\frac{3.4}{50} \frac{4.2}{33} \frac{5.8}{31} \frac{6.7}{27} \frac{6.4}{22} \frac{5.0}{15} \frac{4.4}{15} \frac{4.9}{15} \frac{6.7}{22} \frac{7.0}{30} \frac{5.6}{33} \frac{6.0}{50}$$

$$\frac{3.3}{50} \frac{4.2}{32} \frac{5.8}{30} \frac{6.5}{27} \frac{6.5}{21} \frac{5.2}{16} \frac{4.3}{16} \frac{5.0}{16} \frac{6.6}{22} \frac{7.0}{29} \frac{4.9}{33} \frac{5.6}{50}$$

$$\frac{3.5}{50} \frac{4.7}{34} \frac{5.8}{32} \frac{6.8}{27} \frac{6.6}{20} \frac{5.1}{15} \frac{4.5}{17} \frac{5.4}{17} \frac{6.8}{23} \frac{6.9}{28} \frac{4.7}{34} \frac{5.2}{50}$$

$$\frac{3.3}{50} \frac{4.3}{33} \frac{6.0}{31} \frac{6.7}{27} \frac{6.7}{21} \frac{5.3}{15} \frac{4.6}{17} \frac{5.4}{17} \frac{6.8}{21} \frac{7.0}{29} \frac{4.9}{33} \frac{5.7}{50}$$

$$\frac{4.2}{50} \frac{4.9}{33} \frac{6.2}{30} \frac{7.2}{26} \frac{6.9}{21} \frac{5.5}{15} \frac{4.8}{15} \frac{5.6}{15} \frac{7.1}{22} \frac{7.4}{29} \frac{5.4}{34} \frac{6.7}{50}$$

STA	+	π 906.89	-	ELEV
123+50				01.9.
124				01.8.
+50				01.6.
125				01.4.
T.P	3.43	905.80	4.52	902.37
+50				01.3.
126				01.3.
+50				01.3.
127				01.2.
+50				01.0.
128				00.9.
+50				00.9.
129				00.7.

L.T.

Q

R.T.

$$\frac{5.5}{50} \frac{5.8}{33} \frac{6.7}{21} \frac{7.2}{28} \frac{7.2}{22} \frac{5.6}{15} \underline{5.0} \frac{5.7}{15} \frac{6.9}{21} \frac{7.5}{29} \frac{6.0}{34} \frac{7.2}{50}$$

$$\frac{5.9}{50} \frac{5.9}{33} \frac{7.3}{29} \frac{7.5}{24-22} \frac{5.9}{15} \underline{5.1} \frac{5.7}{15} \frac{7.0}{22} \frac{7.5}{27} \frac{4.7}{34} \frac{6.0}{50}$$

$$\frac{7.2}{50} \frac{7.8}{36} \frac{7.4}{25} \frac{5.8}{15} \underline{5.3} \frac{6.2}{18} \frac{7.2}{20} \frac{7.6}{27} \frac{4.2}{34} \frac{5.0}{50}$$

$$\frac{8.8}{50} \frac{8.0}{46} \frac{7.0}{21} \frac{5.0}{15} \underline{5.5} \frac{6.5}{17} \frac{7.7}{22} \frac{8.0}{29} \frac{5.6}{35} \frac{4.0}{50}$$

$$\frac{6.5}{50} \frac{6.1}{31} \frac{6.5}{25} \frac{6.1}{22} \frac{5.4}{19} \frac{4.9}{16} \underline{4.5} \frac{5.0}{15} \frac{5.5}{19} \frac{6.9}{23} \frac{6.9}{28} \frac{6.2}{31} \frac{4.3}{35} \frac{3.5}{50}$$

$$\frac{5.8}{50} \frac{5.6}{33} \frac{6.8}{28} \frac{6.7}{23} \frac{5.4}{19} \frac{5.2}{16} \underline{4.5} \frac{5.0}{15} \frac{5.5}{19} \frac{6.6}{22} \frac{6.9}{27} \frac{6.0}{31} \frac{4.7}{34} \frac{3.8}{50}$$

$$\frac{5.4}{50} \frac{5.1}{33} \frac{6.4}{30} \frac{7.0}{27} \frac{6.4}{21} \frac{5.1}{16} \underline{4.5} \frac{5.0}{15} \frac{5.6}{19} \frac{6.7}{23} \frac{6.7}{30} \frac{5.5}{33} \frac{4.8}{50}$$

$$\frac{5.0}{50} \frac{5.2}{34} \frac{6.2}{31} \frac{6.8}{27} \frac{6.5}{22} \frac{5.3}{16} \underline{4.6} \frac{5.2}{14} \frac{6.3}{20} \frac{6.7}{22} \frac{6.9}{30} \frac{5.7}{32} \frac{5.7}{50}$$

$$\frac{5.5}{50} \frac{5.5}{33} \frac{6.2}{30} \frac{6.2}{20} \frac{5.4}{15} \underline{4.8} \frac{5.1}{14} \frac{6.7}{21} \frac{6.7}{30} \frac{5.6}{32} \frac{5.5}{50}$$

$$\frac{5.1}{50} \frac{5.1}{42} \frac{4.7}{38} \frac{5.0}{34} \frac{6.3}{30} \frac{6.9}{26} \frac{7.0}{22} \frac{5.3}{15} \underline{4.9} \frac{5.1}{15} \frac{6.8}{21} \frac{7.0}{29} \frac{5.3}{34} \frac{5.1}{50}$$

$$\frac{4.6}{50} \frac{4.5}{42} \frac{3.5}{38} \frac{6.0}{30} \frac{7.2}{25} \frac{6.8}{21} \frac{5.5}{16} \underline{4.9} \frac{5.4}{15} \frac{7.1}{25} \frac{7.1}{27} \frac{5.5}{34} \frac{5.6}{50}$$

$$\frac{5.5}{50} \frac{5.0}{41} \frac{4.4}{37} \frac{5.0}{33} \frac{6.6}{29} \frac{7.4}{26} \frac{7.5}{24} \frac{6.9}{21} \frac{5.7}{16} \underline{5.1} \frac{5.6}{14} \frac{6.9}{22} \frac{7.1}{29} \frac{6.1}{32} \frac{6.2}{50}$$

STA	+	π	-	ELEV
		905.80		
129+50				00.5.
130				00.5.
+50				00.3.
131				00.5.
B.M	4.88	905.68	5.00	900.80
+50				00.6.
132				00.6.
+50				00.8.
133				00.8.
+25				00.9.
+75				00.7.
134				00.7.
+50				00.8.

900.83

void here

LT.

¢

RT.

$$\frac{6.7}{50} \frac{6.6}{31} \frac{7.4}{28} \frac{7.0}{21} \frac{5.7}{15} \underline{5.3} \quad \frac{5.8}{16} \quad \frac{7.1}{23} \quad \frac{7.4}{50}$$

$$\frac{7.4}{50} \frac{7.0}{43} \frac{7.8}{39} \frac{7.3}{33} \frac{7.5}{26} \frac{7.2}{21} \frac{5.8}{15} \underline{5.3} \quad \frac{5.9}{15} \quad \frac{7.3}{23} \quad \frac{8.3}{50}$$

$$\frac{7.9}{50} \frac{6.7}{42} \frac{6.5}{31} \frac{7.7}{26} \frac{7.6}{23} \frac{5.7}{15} \underline{5.5} \quad \frac{5.8}{16} \quad \frac{7.6}{22} \quad \frac{8.4}{27} \quad \frac{8.4}{50}$$

$$\frac{8.2}{50} \frac{6.4}{44} \frac{6.0}{31} \frac{7.6}{28} \frac{7.8}{24} \frac{5.5}{14} \underline{5.3} \quad \frac{5.6}{16} \quad \frac{8.3}{26} \quad \frac{9.2}{50}$$

SPK IN T.P 26' RT STA 130+35

$$\frac{7.8}{50} \frac{6.2}{42} \frac{5.7}{32} \frac{7.2}{29} \frac{7.2}{21} \frac{5.3}{16} \underline{5.1} \quad \frac{5.5}{16} \quad \frac{7.2}{23} \quad \frac{8.2}{50}$$

$$\frac{5.7}{50} \frac{6.0}{32} \frac{7.5}{28} \frac{7.6}{23} \frac{5.7}{16} \underline{5.1} \quad \frac{5.4}{16} \quad \frac{7.9}{24} \quad \frac{8.6}{50}$$

$$\frac{5.2}{50} \frac{5.7}{32} \frac{7.2}{28} \frac{7.1}{22} \frac{5.4}{16} \underline{4.9} \quad \frac{5.5}{16} \quad \frac{7.5}{22} \quad \frac{7.2}{50}$$

$$\frac{5.2}{50} \frac{5.7}{32} \frac{7.1}{29} \frac{7.0}{22} \frac{5.4}{16} \underline{4.9} \quad \frac{5.4}{16} \quad \frac{6.7}{22} \quad \frac{7.1}{31} \quad \frac{6.2}{33} \quad \frac{6.0}{50}$$

$$\frac{5.9}{50} \frac{5.7}{32} \frac{7.3}{28} \frac{7.0}{22} \frac{5.2}{16} \underline{4.8} \quad \frac{5.1}{16} \quad \frac{6.5}{22} \quad \frac{6.6}{31} \quad \frac{5.3}{33} \quad \frac{4.8}{50}$$

$$\frac{5.2}{50} \frac{5.4}{33} \frac{6.7}{29} \frac{6.8}{21} \frac{5.0}{16} \underline{5.0} \quad \frac{5.1}{16} \quad \frac{6.9}{23} \quad \frac{6.7}{50}$$

$$\frac{5.5}{50} \frac{5.6}{32} \frac{7.0}{29} \frac{6.7}{21} \frac{5.2}{16} \underline{5.0} \quad \frac{5.2}{14} \quad \frac{5.6}{18} \quad \frac{7.6}{24} \quad \frac{7.5}{50}$$

$$\frac{6.3}{50} \frac{5.6}{32} \frac{7.0}{29} \frac{6.8}{21} \frac{5.1}{15} \underline{4.9} \quad \frac{5.1}{14} \quad \frac{5.9}{19} \quad \frac{8.4}{25} \quad \frac{8.1}{50}$$

STA + π - ELEV

905.68

135

00.9

+50

01.1

136

01.0

T.P.

3.79 901.89

? check
on Mon.
W.JB

BM

10.00

897.87

887.87

6.97

903.64

1.20

896.67

+50

00.8

137

00.5

+50

99.8

138

99.4

+50

98.9

139

98.7

+50

98.1

140

97.5

Void see Revised

L.T.

E

RT

$$\frac{5.2}{50} \frac{5.5}{33} \frac{7.0}{29} \frac{6.8}{22} \frac{5.3}{16} \underline{4.8} \frac{5.1}{14} \frac{5.3}{12} \frac{7.6}{23} \frac{7.0}{50}$$

$$\frac{5.0}{50} \frac{5.4}{32} \frac{6.6}{29} \frac{6.6}{22} \frac{5.1}{16} \underline{4.6} \frac{4.9}{15} \frac{6.9}{22} \frac{7.1}{30} \frac{5.2}{32} \frac{5.2}{50}$$

$$\frac{5.5}{50} \frac{5.5}{32} \frac{7.1}{29} \frac{7.0}{22} \frac{5.4}{16} \underline{4.7} \frac{5.1}{16} \frac{7.1}{21} \frac{7.1}{29} \frac{4.1}{33} \frac{4.5}{50}$$

T.P. 35' RT 135+50

Top Mon I & Hamline

$$\frac{3.7}{51} \frac{4.3}{37} \frac{4.1}{34} \frac{3.6}{33} \frac{5.2}{29} \frac{4.8}{21} \frac{3.6}{17} \underline{2.8} \frac{3.2}{15} \frac{5.2}{21} \frac{5.6}{29} \frac{2.3}{33} \frac{2.7}{50}$$

$$\frac{3.6}{50} \frac{3.6}{32} \frac{5.1}{29} \frac{5.2}{21} \frac{3.9}{17} \underline{3.1} \frac{3.7}{16} \frac{5.2}{21} \frac{6.0}{28} \frac{3.3}{34} \frac{3.2}{50}$$

$$\frac{4.0}{50} \frac{4.3}{33} \frac{6.0}{29} \frac{5.7}{21} \frac{4.1}{17} \underline{3.8} \frac{4.4}{17} \frac{6.3}{22} \frac{6.2}{29} \frac{4.4}{32} \frac{3.9}{50}$$

$$\frac{5.3}{50} \frac{4.5}{33} \frac{6.2}{29} \frac{6.1}{22} \frac{4.5}{17} \underline{4.2} \frac{4.7}{17} \frac{6.7}{22} \frac{7.0}{30} \frac{5.2}{32} \frac{5.1}{50}$$

$$\frac{4.5}{50} \frac{4.6}{33} \frac{6.7}{29} \frac{6.3}{22} \frac{4.8}{17} \underline{4.7} \frac{5.2}{17} \frac{7.0}{22} \frac{7.3}{30} \frac{5.9}{32} \frac{6.2}{50}$$

$$\frac{3.4}{50} \frac{3.0}{44} \frac{5.8}{36} \frac{5.1}{32} \frac{6.8}{29} \frac{6.6}{21} \frac{5.4}{17} \underline{4.9} \frac{5.6}{17} \frac{7.7}{24} \frac{7.9}{31} \frac{7.1}{32} \frac{7.5}{50}$$

$$\frac{4.7}{50} \frac{4.7}{40} \frac{6.2}{36} \frac{5.4}{32} \frac{7.5}{29} \frac{7.4}{23} \frac{6.1}{18} \underline{5.5} \frac{6.2}{18} \frac{8.1}{24} \frac{8.4}{31} \frac{8.4}{50}$$

$$\frac{5.2}{50} \frac{4.8}{39} \frac{6.2}{32} \frac{8.2}{29} \frac{8.1}{22} \frac{6.6}{17} \underline{6.1} \frac{6.6}{17} \frac{8.2}{21} \frac{8.5}{36} \frac{8.8}{50}$$

Sta	+	π	-	Elev
		903.64		
140+30				96.8
141				96.4
+50				95.7
+75				95.3
142				94.7
T.P.	2.73	897.10	9.27	894.37.
+50				93.4
143				92.1
+50				90.9
144				89.5
+41				88.7
+45				88.7
+50				88.6

Revised

500

Void

$$\frac{60}{50} \frac{56}{37} \frac{64}{31} \frac{88}{28} \frac{86}{21} \frac{71}{17} 68 \frac{71}{17} \frac{86}{22} \frac{90}{30} \frac{74}{32} \frac{78}{50}$$

$$\frac{78}{50} \frac{76}{37} \frac{83}{31} \frac{98}{28} \frac{94}{22} \frac{76}{17} 72 \frac{73}{17} \frac{94}{22} \frac{96}{29} \frac{67}{33} \frac{67}{50}$$

$$\frac{85}{50} \frac{83}{36} \frac{107}{29} \frac{102}{26} \frac{99}{21} \frac{84}{17} 79 \frac{83}{16} \frac{102}{21} \frac{99}{27} \frac{37}{33} \frac{36}{50}$$

$$\frac{87}{50} \frac{87}{36} \frac{110}{30} \frac{108}{22} \frac{90}{17} 83 \frac{87}{16} \frac{108}{22} \frac{112}{26} \frac{44}{33} \frac{36}{50}$$

$$\frac{93}{50} \frac{92}{36} \frac{115}{29} \frac{111}{22} \frac{96}{18} 89 \frac{93}{17} \frac{114}{22} \frac{115}{27} \frac{64}{33} \frac{60}{50}$$

$$\frac{43}{50} \frac{43}{36} \frac{62}{30} \frac{60}{23} \frac{44}{18} 37 \frac{43}{16} \frac{62}{21} \frac{62}{29} \frac{36}{33} \frac{35}{50}$$

$$\frac{56}{50} \frac{54}{35} \frac{72}{31} \frac{71}{22} \frac{54}{17} 50 \frac{55}{15} \frac{75}{21} \frac{76}{27} \frac{61}{32} \frac{57}{50}$$

$$\frac{61}{50} \frac{60}{35} \frac{82}{31} \frac{82}{23} \frac{67}{17} 62 \frac{70}{15} \frac{84}{23} \frac{81}{50}$$

$$\frac{77}{50} \frac{76}{33} \frac{96}{30} \frac{93}{21} \frac{80}{17} 76 \frac{79}{15} \frac{98}{21} \frac{101}{50}$$

$$\frac{90}{50} \frac{90}{47} \frac{102}{39} \frac{102}{30} \frac{92}{26} 84 \frac{93}{27} \frac{106}{28} \frac{108}{50}$$

$$\frac{108}{50} \frac{100}{33} \frac{94}{30} \frac{86}{15} 84 \frac{87}{12} \frac{95}{25} \frac{104}{28} \frac{109}{50}$$

$$\frac{108}{50} \frac{105}{42} \frac{97}{38} \frac{89}{23} 85 \frac{88}{13} \frac{98}{34} \frac{103}{39} \frac{107}{50}$$

Sta + π - Elev

89710

144+58 West Shl. Hamline 88.5

+72.44 $\pm$ Hamline 88.1

+87 East Shl Hamline 87.7

B.M. 5.78 893.65 921 887.89 887.87

300' Exception

144+58 West Shl Hamline 88.1

+72.44 $\pm$ Hamline 88.3

+87 East 88.5

+96 84.9

145+09 85.3

+12 83.2

+19 82.9

+21 85.2

Void See Back

Lt

K

Rt

36

$$\frac{9.5}{50} \quad \frac{9.0}{33} \quad \frac{8.7}{18} \quad 8.6 \quad \frac{8.8}{19} \quad \frac{9.5}{35} \quad \frac{9.6}{50}$$

$$\frac{9.2}{50} \quad 9.0 \quad \frac{9.0}{50}$$

$$\frac{9.8}{50} \quad \frac{9.6}{22} \quad 9.4 \quad \frac{9.2}{22} \quad \frac{9.4}{50}$$

Top Mon. 'I' + Hamline

$$\frac{5.3}{50} \quad 5.6 \quad \frac{6.0}{50}$$

$$\frac{5.0}{50} \quad 5.4 \quad \frac{5.9}{50}$$

$$\frac{5.4}{50} \quad 5.2 \quad \frac{6.2}{50}$$

$$\frac{8.4}{50} \quad 8.8 \quad \frac{9.1}{50}$$

$$\frac{7.7}{50} \quad \frac{8.3}{25} \quad \frac{9.1}{21} \quad \frac{11.0}{13} \quad \frac{10.2}{7} \quad \frac{8.8}{4} \quad 8.4 \quad \frac{9.1}{22} \quad \frac{9.3}{50}$$

$$\frac{7.8}{50} \quad \frac{8.5}{20} \quad \frac{9.4}{17} \quad \frac{10.5}{7} \quad 10.5 \quad \frac{10.1}{8} \quad \frac{8.5}{12} \quad \frac{9.2}{50}$$

$$\frac{7.7}{50} \quad \frac{7.6}{10} \quad 10.8 \quad \frac{10.9}{24} \quad \frac{9.0}{27} \quad \frac{9.1}{50}$$

$$\frac{7.7}{50} \quad \frac{7.6}{10} \quad 9.5 \quad \frac{8.6}{4} \quad \frac{11.3}{8} \quad \frac{10.5}{50}$$

Sta	+	Δ	-	Elev
		893.65		

145+30				85.5
--------	--	--	--	------

146				85.6
-----	--	--	--	------

+50				85.7
-----	--	--	--	------

147				85.5
-----	--	--	--	------

+50				85.7
-----	--	--	--	------

148				87.4
-----	--	--	--	------

+50				89.9
-----	--	--	--	------

+65				90.9
-----	--	--	--	------

T.P	5.64	899.21	0.08	893.57
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149				93.2
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+39				93.4
-----	--	--	--	------

+65				89.9
-----	--	--	--	------

+79				88.5
-----	--	--	--	------

See Revised

Lt

X

R+

$$\frac{7.7}{50}$$

$$\frac{8.0}{31}$$

8.2

$$\frac{8.1}{33}$$

$$\frac{8.2}{50}$$

$$\frac{7.8}{50}$$

8.1

$$\frac{8.1}{50}$$

$$\frac{7.7}{50}$$

8.0

$$\frac{8.2}{50}$$

$$\frac{7.8}{50}$$

8.2

$$\frac{8.2}{50}$$

$$\frac{8.0}{50}$$

8.0

$$\frac{8.2}{50}$$

$$\frac{7.1}{50}$$

6.3

$$\frac{5.6}{50}$$

$$\frac{2.7}{50}$$

$$\frac{3.2}{30}$$

3.8

$$\frac{4.8}{50}$$

$$\frac{2.5}{50}$$

$$\frac{2.8}{35}$$

2.8

$$\frac{3.1}{19}$$

$$\frac{3.5}{29}$$

$$\frac{4.4}{50}$$

$$\frac{3.3}{50}$$

$$\frac{3.8}{28}$$

6.0

$$\frac{7.5}{23}$$

$$\frac{8.5}{50}$$

$$\frac{4.8}{50}$$

5.8

$$\frac{6.5}{27}$$

$$\frac{6.9}{50}$$

$$\frac{8.5}{50}$$

9.3

$$\frac{9.0}{50}$$

10.4

10.7

$$\frac{10.6}{50}$$

Sta	+	Δ	—	Elev
		899.21		
150				87.8
+50				87.6
151				87.3
+50				86.8
152		-		86.9 -
T.P.	9.12	896.59	11.74	887.47
+50				87.3
153				87.3
+50				87.1
154				86.9
+47		Profile Ditch		86.9
		No Section		
+50				87.7
155				87.6

Lt

2

Rt

$$\frac{11.4}{50}$$

$$\frac{11.4}{25}$$

11.4

$$\frac{11.5}{50}$$

$$\frac{11.8}{50}$$

11.6

$$\frac{11.6}{50}$$

$$\frac{12.1}{50}$$

11.9

$$\frac{12.0}{50}$$

$$\frac{12.3}{50}$$

12.4

$$\frac{12.4}{50}$$

$$\frac{12.3}{50}$$

12.3

$$\frac{12.5}{50}$$

$$\frac{9.4}{50}$$

9.3

$$\frac{9.7}{50}$$

$$\frac{9.0}{50}$$

9.3

$$\frac{9.8}{50}$$

$$\frac{8.7}{50}$$

9.5

$$\frac{10.2}{50}$$

$$\frac{8.5}{50}$$

9.7

$$\frac{10.2}{50} \quad \frac{10.0}{58} \quad \frac{10.8}{60} \text{ pitch}$$

$$\frac{9.3}{100}$$

$$\frac{9.6}{85}$$

$$\frac{9.7}{50}$$

$$\frac{9.6}{27}$$

9.7

$$\frac{10.5}{28}$$

$$\frac{10.8}{50}$$

$$\frac{8.5}{50}$$

$$\frac{8.0}{9}$$

$$\frac{9.5}{5}$$

$$\frac{8.9}{3}$$

8.9

$$\frac{9.3}{50}$$

Ditch

$$\frac{7.4}{83}$$

$$\frac{9.3}{79}$$

$$\frac{8.1}{77}$$

$$\frac{8.3}{50}$$

9.0

$$\frac{9.3}{50}$$

Sta	+	π	-	Elev
		896.59		
155	150			87.6
156				87.7
+50				87.5
157				86.9
+50				86.6
TP	8.06	895.19	9.46	887.13
158				86.2
+50				85.9
159				85.7
+50				85.9
160				86.0
+50				88.1
161				90.3

Lt

L

Rt

$$\frac{8.3}{50} \quad \frac{8.3}{29} \quad 9.0 \quad \frac{9.8}{50}$$

$$\frac{8.9}{50} \quad 8.9 \quad \frac{9.7}{50}$$

$$\frac{9.3}{50} \quad 9.1 \quad \frac{9.8}{50}$$

$$\frac{9.7}{50} \quad 9.7 \quad \frac{9.9}{50}$$

$$\frac{9.9}{50} \quad 10.0 \quad \frac{10.2}{50}$$

$$\frac{8.9}{50} \quad 9.0 \quad \frac{9.3}{50}$$

$$\frac{9.3}{50} \quad 9.3 \quad \frac{9.6}{50}$$

$$\frac{9.2}{50} \quad 9.5 \quad \frac{9.7}{50}$$

$$\frac{9.2}{50} \quad 9.3 \quad \frac{9.5}{50}$$

$$\frac{9.6}{50} \quad 9.2 \quad \frac{9.4}{50}$$

$$\frac{7.1}{50} \quad 7.1 \quad \frac{7.3}{50}$$

$$\frac{4.7}{50} \quad 4.9 \quad \frac{5.3}{50}$$

Sta	+	Δ	-	Elev
		895.19		
161+25				92.1
+44				93.6
13. M	13.17	906.21	2.15	893.04
162				98.6
+50				03.3
+75				05.0
T.P.	4.84	909.84	1.21	905.00
163				06.0
+50				03.7
164				01.7
+50		Drain 50		00.4
165				00.6
+20				00.3 -
+50				01.7

Lt

Z

Rt

$$\frac{3.8}{50}$$

3.1

$$\frac{3.8}{50}$$

$$\frac{2.0}{50}$$

1.6

$$\frac{1.6}{50}$$

Spk in 12" Twin Oak 25' Lt sta 161+25

$$\frac{8.6}{50}$$

7.6

$$\frac{7.1}{50}$$

$$\frac{5.0}{50}$$

$$\frac{3.7}{25}$$

2.9

$$\frac{2.1}{50}$$

$$\frac{4.0}{50}$$

$$\frac{1.9}{17}$$

1.2

$$\frac{0.4}{50}$$

$$\frac{6.8}{50}$$

$$\frac{5.9}{20}$$

3.8

$$\frac{3.5}{21}$$

$$\frac{2.9}{50}$$

$$\frac{7.3}{50}$$

$$\frac{6.9}{9}$$

6.1

$$\frac{3.3}{50}$$

$$\frac{8.7}{50}$$

$$\frac{8.4}{25}$$

8.1

$$\frac{7.1}{25}$$

$$\frac{5.5}{50}$$

$$\frac{9.4}{50}$$

$$\frac{9.3}{34}$$

9.4

$$\frac{9.2}{31}$$

$$\frac{8.1}{50}$$

$$\frac{9.0}{50}$$

$$\frac{9.2}{28}$$

9.2

$$\frac{9.0}{26}$$

$$\frac{9.3}{50}$$

$$\frac{8.9}{50}$$

$$\frac{9.2}{26}$$

9.5

$$\frac{9.2}{28}$$

$$\frac{9.2}{50}$$

$$\frac{7.7}{50}$$

$$\frac{8.1}{32}$$

8.1

$$\frac{8.6}{35}$$

$$\frac{8.7}{50}$$

Sta	+	π	-	Elev
		909.84		

166				03.6
T.P.	6.72	911.03	5.53	904.31
+50				04.7

167				06.2
-----	--	--	--	------

+50				06.9
-----	--	--	--	------

168				06.1
-----	--	--	--	------

+50				04.9
-----	--	--	--	------

169				02.7
-----	--	--	--	------

+50				00.3
-----	--	--	--	------

+77				98.8
-----	--	--	--	------

T.P.	2.22	900.18	13.07	897.92
------	------	--------	-------	--------

170				96.3
-----	--	--	--	------

+50				93.8
-----	--	--	--	------

+88				92.9
-----	--	--	--	------

Lt

Z

Rt

41

$$\frac{6.3}{50}$$

$$\frac{6.3}{25}$$

$$6.2 \quad \frac{6.3}{19} \quad \frac{7.8}{50}$$

$$\frac{6.4}{50}$$

6.3

$$\frac{6.1}{50}$$

$$\frac{4.3}{50}$$

4.8

$$\frac{5.5}{50}$$

$$\frac{4.9}{50}$$

4.1

$$\frac{4.6}{50}$$

$$\frac{5.7}{50}$$

$$\frac{5.6}{22}$$

4.9

$$\frac{4.4}{50}$$

$$\frac{6.5}{50}$$

$$\frac{6.4}{24}$$

6.1

$$\frac{5.6}{30}$$

$$\frac{5.1}{50}$$

$$\frac{8.3}{50}$$

$$\frac{8.6}{23}$$

8.3

$$\frac{7.7}{27}$$

$$\frac{7.3}{50}$$

$$\frac{10.3}{50}$$

$$\frac{10.8}{28}$$

10.7

$$\frac{10.2}{27}$$

$$\frac{10.0}{50}$$

$$\frac{11.6}{50}$$

$$\frac{11.9}{27}$$

12.2

$$\frac{12.0}{26}$$

$$\frac{11.3}{50}$$

$$\frac{3.0}{50}$$

$$\frac{3.8}{40}$$

$$\frac{3.8}{25}$$

3.9

$$\frac{3.0}{24}$$

$$\frac{1.8}{50}$$

$$\frac{5.6}{50}$$

$$\frac{6.4}{39}$$

$$\frac{6.4}{25}$$

6.4

$$\frac{6.0}{23}$$

$$\frac{4.6}{50}$$

$$\frac{5.6}{50}$$

$$\frac{7.2}{23}$$

7.3

$$\frac{7.1}{26}$$

$$\frac{7.1}{50}$$

Sta	+	π 900.18	-	Elev
+91				91.4
+99				91.5
171+05				93.6
+1962				93.7
B.M.		7.84	892.34	892.36.

Lt

2

Rt

42

$$\frac{7.6}{30}$$

$$\frac{8.4}{26} \quad 8.8$$

$$\frac{9.1}{25}$$

$$\frac{8.9}{30}$$

$$\frac{7.8}{30}$$

$$\frac{8.5}{22}$$

$$8.7$$

$$\frac{8.9}{23}$$

$$\frac{8.9}{30}$$

$$\frac{6.1}{30}$$

$$\frac{6.4}{27}$$

$$6.6$$

$$\frac{6.8}{23}$$

$$\frac{7.3}{30}$$

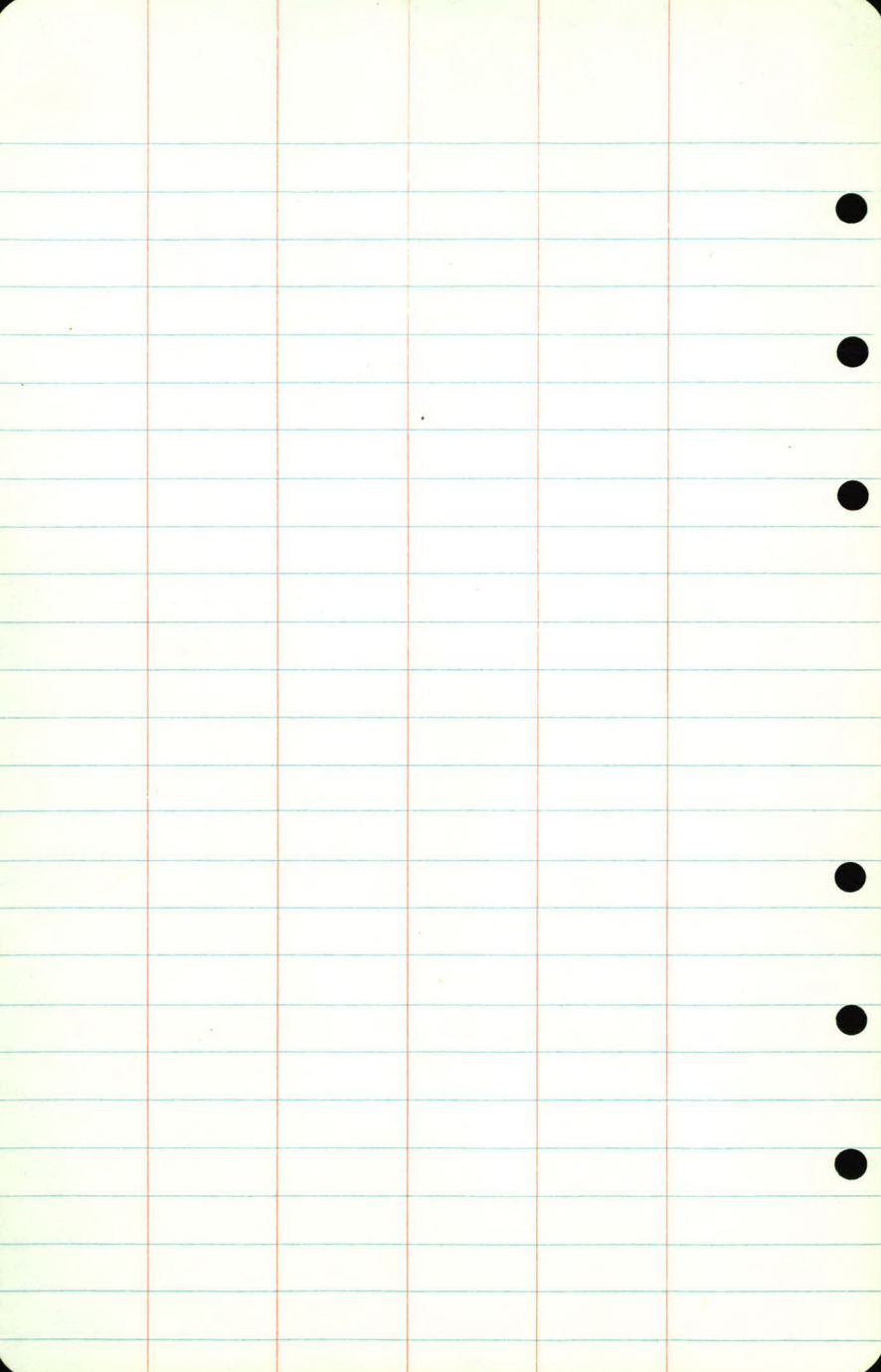
$$\frac{5.8}{30}$$

6

$$6.5$$

$$\frac{7.1}{30}$$

Spk in P.P. S.W. Cor I & Lexington



42 A

Revised

Sta 130 + 51.93 to 149 + 32.60

X Sections

Sta	+	Δ	-	Elev
B.M.	10.43	898.30.		887.87.
	760	904.94.	0.96	897.34.
	4.54	905.58.	3.90	901.04.

^{+51.93}
130 + 51.96 P.C. 00.4

131 00.6

+50 00.6

132 00.5

+50 00.4

133 00.5

B.M. 5.16 906.62. 4.12 901.46.

+50 00.5

134 899.0

+50 98.5

+68 98.9

+80 99.8

LH.

R

Rt.

9

42B

Top Morr Co Rd "I" + Hamline Ave

$$\frac{8.0}{50} \frac{6.3}{43} \frac{6.2}{31} \frac{7.4}{29} \frac{7.3}{22} \frac{5.7}{16} 5.2 \frac{5.5}{16} \frac{7.9}{25} \frac{8.2}{50}$$

$$\frac{8.4}{50} \frac{6.1}{41} \frac{5.7}{31} \frac{7.5}{28} \frac{7.3}{21} \frac{5.7}{16} 5.0 \frac{5.4}{17} \frac{7.9}{25} \frac{9.0}{50}$$

$$\frac{7.3}{50} \frac{6.0}{43} \frac{5.8}{30} \frac{7.3}{26} \frac{7.2}{20} \frac{5.5}{15} 5.0 \frac{5.4}{19} \frac{7.1}{26} \frac{8.0}{50}$$

$$\frac{6.4}{100} \frac{6.3}{70} \frac{6.6}{50} \frac{5.4}{43} \frac{5.9}{29} \frac{7.4}{25} \frac{7.3}{19} \frac{5.6}{13} 5.1 \frac{5.3}{20} \frac{7.8}{28} \frac{8.4}{50}$$

$$\frac{6.1}{100} \frac{5.7}{50} \frac{5.7}{26} \frac{7.1}{22} \frac{6.9}{14} \frac{5.6}{10} 5.2 \frac{4.8}{9} \frac{5.2}{23} \frac{7.3}{30} \frac{7.0}{50}$$

$$\frac{6.4}{100} \frac{5.3}{50} \frac{5.6}{22} \frac{7.1}{18} \frac{6.9}{12} \frac{5.3}{6.9} 5.1 \frac{5.2}{29} \frac{6.7}{34} \frac{6.8}{42} \frac{5.6}{45} \frac{5.4}{50}$$

SpK 177 Group 4-6" Pop 22' Lt 5' 9" 133+100

$$\frac{7.9}{100} \frac{6.9}{77} \frac{6.7}{42} \frac{6.5}{18} \frac{8.2}{13} \frac{7.6}{5} \frac{6.2}{1} 6.1 \frac{5.8}{17} \frac{6.2}{35} \frac{7.7}{39} \frac{7.9}{48} \frac{7.3}{51}$$

$$\frac{7.5}{100} \frac{6.2}{81} \frac{6.5}{41} \frac{6.4}{12} \frac{8.1}{3} 7.2 \frac{6.3}{4} \frac{5.9}{22} \frac{6.2}{41} \frac{8.3}{46} \frac{9.1}{50}$$

$$\frac{7.5}{100} \frac{7.4}{55} \frac{7.4}{25} \frac{6.4}{5} \frac{7.8}{3} 8.1 \frac{7.7}{7} \frac{6.2}{11} \frac{5.7}{25} \frac{6.3}{42} \frac{8.5}{51}$$

$$\frac{7.2}{100} \frac{7.6}{79} \frac{7.6}{45} \frac{7.2}{21} \frac{6.4}{2} 7.7 \frac{7.8}{10} \frac{6.1}{14} \frac{5.7}{30} \frac{6.1}{50} \frac{8.5}{55}$$

$$\frac{7.6}{100} \frac{7.7}{27} \frac{7.5}{33} 6.8 \frac{7.9}{2} \frac{7.8}{11} \frac{6.3}{15} \frac{5.6}{31} \frac{6.1}{50} \frac{8.6}{57}$$

Sta	+	π	-	Elev
		906.62		
135				00.0
+50				00.6
136				00.3
+50				00.0
137				00.3
+50				99.2
138				98.0
+50				97.8
139				98.0
T.P.	3.93	902.55	8.00	898.62
+50				97.8
140				96.7
+50				93.4

Elev Top W Cond.
7.72 898.90

L+

X

R+

42C

$$\frac{7.0}{100} \quad \frac{48}{60} \quad \frac{7.0}{28}$$

$$6.6 \quad \frac{63}{3} \quad \frac{7.8}{6} \quad \frac{7.7}{14} \quad \frac{6.2}{18} \quad \frac{5.6}{34} \quad \frac{6.0}{53} \quad \frac{8.0}{57}$$

$$\frac{5.1}{100} \quad \frac{44}{73} \quad \frac{48}{39} \quad 6.0 \quad \frac{6.2}{10} \quad \frac{7.5}{15} \quad \frac{7.4}{23} \quad \frac{6.1}{26} \quad \frac{5.5}{43} \quad \frac{5.9}{61} \quad \frac{7.5}{66}$$

$$\frac{5.5}{100} \quad \frac{5.3}{67} \quad \frac{5.7}{30} \quad \frac{5.2}{17} \quad 6.3 \quad \frac{6.6}{20} \quad \frac{7.9}{24} \quad \frac{7.7}{32} \quad \frac{6.4}{36} \quad \frac{5.6}{54} \quad \frac{6.0}{70} \quad \frac{7.8}{75}$$

$$\frac{6.9}{100} \quad \frac{6.7}{69} \quad \frac{6.6}{38} \quad 6.6 \quad \frac{6.7}{29} \quad \frac{8.2}{33} \quad \frac{7.8}{42} \quad \frac{6.7}{45} \quad \frac{5.8}{61} \quad \frac{6.3}{78} \quad \frac{7.9}{83}$$

$$\frac{7.6}{100} \quad \frac{6.9}{65} \quad \frac{6.9}{33} \quad 6.3 \quad \frac{6.6}{23} \quad \frac{6.4}{41} \quad \frac{8.0}{44} \quad \frac{8.2}{53} \quad \frac{7.0}{57} \quad \frac{6.2}{75} \quad \frac{6.9}{92} \quad \frac{9.0}{97}$$

$$\frac{8.0}{100} \quad \frac{7.6}{66} \quad \frac{7.6}{36} \quad 7.4 \quad \frac{7.2}{23} \quad \frac{7.3}{52} \quad \frac{8.9}{56} \quad \frac{8.7}{64} \quad \frac{7.2}{69} \quad \frac{6.9}{83} \quad \frac{7.2}{100}$$

$$\frac{8.7}{100} \quad \frac{8.1}{65} \quad \frac{8.2}{24} \quad 8.6 \quad \frac{7.9}{26} \quad \frac{8.0}{50} \quad \frac{7.9}{66} \quad \frac{9.3}{69} \quad \frac{9.2}{76} \quad \frac{7.7}{81} \quad \frac{7.4}{100}$$

$$\frac{10.2}{100} \quad \frac{10.0}{78} \quad \frac{9.7}{55} \quad \frac{9.1}{31} \quad 8.8 \quad \frac{7.9}{26} \quad \frac{7.7}{55} \quad \frac{7.8}{80} \quad \frac{9.7}{87} \quad \frac{9.4}{91} \quad \frac{8.0}{96} \quad \frac{7.8}{100}$$

$$\frac{13.0}{100} \quad \frac{11.9}{70} \quad \frac{10.5}{34} \quad 8.6 \quad \frac{7.2}{26} \quad \frac{6.9}{57} \quad \frac{6.8}{86} \quad \frac{8.2}{94} \quad \frac{9.7}{98}$$

$$\frac{11.2}{100} \quad \frac{9.5}{74} \quad \frac{8.8}{68} \quad \frac{8.2}{51} \quad \frac{7.0}{29} \quad 4.8 \quad \frac{2.9}{31} \quad \frac{2.4}{57} \quad \frac{3.6}{86} \quad \frac{3.6}{100}$$

$$\frac{12.6}{100} \quad \frac{10.2}{68} \quad \frac{8.9}{56} \quad \frac{7.7}{21} \quad 5.9 \quad \frac{3.9}{27} \quad \frac{4.2}{53} \quad \frac{5.6}{81} \quad \frac{5.1}{98} \quad \frac{4.0}{104}$$

$$\frac{13.0}{100} \quad \frac{12.1}{72} \quad \frac{10.6}{45} \quad \frac{9.9}{24} \quad 9.2 \quad \frac{8.9}{30} \quad \frac{7.7}{51} \quad \frac{7.4}{69} \quad \frac{8.7}{87} \quad \frac{8.6}{100}$$

Sta	+	Δ	-	Elev
		902.55.		
141				90.7
T.P.	5.59	896.90.	11.24	891.31.
+18				87.9
+50				86.5
142				86.8
+50				87.8
143				87.3
+50				86.5
144				84.8
B.M.	4.65	892.52.	9.03	887.87. 887.87.
+50				85.3.
+73				84.5.
+74				83.6.
+80				85.1.

Lt.

L

Rt

11

42 D

$$\frac{15.3}{100} \quad \frac{15.2}{66} \quad \frac{15.5}{43} \quad \frac{14.2}{22} \quad 11.9 \quad \frac{11.4}{9} \quad \frac{10.6}{39} \quad \frac{9.4}{68} \quad \frac{10.2}{81} \quad \frac{10.7}{100}$$

$$\frac{8.6}{100} \quad \frac{9.1}{78} \quad \frac{9.6}{77} \quad \frac{10.0}{39} \quad 9.0 \quad \frac{7.2}{15} \quad \frac{5.7}{21} \quad \frac{5.1}{41} \quad \frac{3.8}{68} \quad \frac{5.0}{100}$$

$$\frac{8.9}{100} \quad \frac{8.9}{89} \quad \frac{9.0}{56} \quad \frac{9.6}{55} \quad \frac{10.5}{27} \quad 10.4 \quad \frac{9.1}{34} \quad \frac{6.3}{48} \quad \frac{4.6}{89} \quad \frac{5.7}{100}$$

$$\frac{9.3}{100} \quad \frac{9.2}{53} \quad \frac{9.0}{18} \quad \frac{9.4}{17} \quad 10.1 \quad \frac{10.3}{35} \quad \frac{9.4}{62} \quad \frac{7.5}{78} \quad \frac{6.7}{100}$$

$$\frac{9.9}{100} \quad \frac{9.7}{60} \quad \frac{9.8}{24} \quad 9.1 \quad \frac{9.9}{43} \quad \frac{10.2}{81} \quad \frac{9.7}{100}$$

$$\frac{10.3}{100} \quad \frac{10.3}{79} \quad \frac{10.2}{38} \quad 9.6 \quad \frac{10.1}{30} \quad \frac{10.0}{69} \quad \frac{10.3}{100}$$

$$\frac{10.9}{100} \quad \frac{10.9}{61} \quad \frac{10.3}{30} \quad 10.4 \quad \frac{9.9}{34} \quad \frac{10.4}{64} \quad \frac{10.7}{100}$$

$$\frac{11.2}{100} \quad \frac{11.3}{60} \quad \frac{12.0}{36} \quad 12.1 \quad \frac{12.1}{25} \quad \frac{11.5}{27} \quad \frac{11.1}{62} \quad \frac{11.8}{100}$$

Top Mon Co Rd "I" + Hamline

$$\frac{8.2}{100} \quad \frac{8.3}{82} \quad \frac{8.5}{63} \quad \frac{7.6}{72} \quad \frac{7.9}{8} \quad \frac{7.2}{5} \quad 7.2 \quad \frac{7.3}{30} \quad \frac{7.2}{62} \quad \frac{7.0}{92} \quad \frac{7.0}{100}$$

$$\frac{7.7}{100} \quad \frac{8.8}{50} \quad 8.0 \quad \frac{7.5}{3} \quad \frac{7.3}{50} \quad \frac{7.0}{100}$$

$$\frac{8.4}{100} \quad \frac{8.7}{30} \quad 8.9 \quad \frac{8.8}{50} \quad \frac{8.3}{100}$$

$$\frac{6.5}{100} \quad \frac{6.6}{50} \quad 7.4 \quad \frac{7.7}{60} \quad \frac{7.4}{86} \quad \frac{7.0}{100}$$

Sta	+	$\bar{A}$	-	Elev
-----	---	-----------	---	------

		892.52.		
--	--	---------	--	--

+88				87.8.
-----	--	--	--	-------

145				88.0.
-----	--	--	--	-------

+17				87.7.
-----	--	--	--	-------

+23				86.0.
-----	--	--	--	-------

+30				84.7.
-----	--	--	--	-------

+44				84.1.
-----	--	--	--	-------

+50				84.7.
-----	--	--	--	-------

+61				82.7.
-----	--	--	--	-------

+62				85.1.
-----	--	--	--	-------

146				85.7.
-----	--	--	--	-------

+50				85.8.
-----	--	--	--	-------

147				85.8.
-----	--	--	--	-------

Lt

K

Rt

42E

$$\frac{3.9}{100} \quad \frac{4.3}{50} \quad 4.7 \quad \frac{5.0}{50} \quad \frac{5.0}{100}$$

$$\frac{3.7}{100} \quad \frac{4.0}{50} \quad 4.5 \quad \frac{4.9}{50} \quad \frac{5.0}{100}$$

$$\frac{4.1}{100} \quad \frac{4.3}{50} \quad 4.8 \quad \frac{5.4}{50} \quad \frac{5.5}{100}$$

$$\frac{7.3}{100} \quad \frac{6.8}{50} \quad 6.5 \quad \frac{7.3}{50} \quad \frac{7.6}{100}$$

$$\frac{9.2}{100} \quad \frac{10.0}{68} \quad \frac{9.0}{59} \quad \frac{7.5}{54} \quad 7.8 \quad \frac{8.1}{50} \quad \frac{8.3}{100}$$

$$\frac{6.5}{100} \quad \frac{7.6}{46} \quad \frac{9.5}{43} \quad \frac{9.4}{23} \quad \frac{7.7}{18} \quad 8.4 \quad \frac{8.3}{50} \quad \frac{8.4}{100}$$

$$\frac{6.8}{100} \quad \frac{6.9}{50} \quad \frac{7.2}{29} \quad \frac{9.6}{23} \quad \frac{9.9}{4} \quad 7.8 \quad \frac{8.3}{50} \quad \frac{8.4}{100}$$

$$\frac{6.6}{100} \quad \frac{6.5}{56} \quad \frac{6.6}{31} \quad \frac{7.6}{4} \quad 9.8 \quad \frac{10.1}{31} \quad \frac{8.5}{32} \quad \frac{8.4}{50} \quad \frac{8.4}{100}$$

$$\frac{6.6}{100} \quad \frac{6.5}{56} \quad \frac{6.6}{31} \quad 7.4 \quad \frac{7.4}{5} \quad \frac{10.0}{7} \quad \frac{10.0}{40} \quad \frac{8.4}{50} \quad \frac{8.4}{100}$$

$$\frac{6.4}{100} \quad \frac{6.6}{50} \quad 6.8 \quad \frac{7.4}{47} \quad \frac{7.4}{100}$$

$$\frac{6.3}{100} \quad \frac{6.6}{50} \quad 6.7 \quad \frac{6.9}{50} \quad \frac{7.0}{100}$$

$$\frac{6.3}{100} \quad \frac{6.6}{50} \quad 6.7 \quad \frac{7.2}{50} \quad \frac{7.3}{100}$$

Sta + π - Elev

892.52

147 + 50

85.6

148

85.8

T.P

9.49

898.58

3.43

887.09

+ 50

88.4

149

149

90.9

$P.T + 32^{60} = 149 + 50$

Use To match old

93.2

93.4

B.M.

10.71

887.87

L1

L2

R1

13

42F

$$\frac{6.4}{100}$$

$$\frac{6.8}{50}$$

$$6.9 \quad \frac{6.9}{50} \quad \frac{7.1}{100}$$

$$\frac{6.2}{100}$$

$$\frac{6.3}{50}$$

$$6.7$$

$$\frac{6.7}{50}$$

$$\frac{6.9}{100}$$

$$\frac{9.5}{100}$$

$$\frac{9.9}{50}$$

$$10.2$$

$$\frac{11.0}{50}$$

$$\frac{11.2}{100}$$

$$\frac{6.4}{100}$$

$$\frac{7.1}{50}$$

$$7.7$$

$$\frac{8.2}{37}$$

$$\frac{8.5}{41}$$

$$\frac{9.0}{50}$$

$$\frac{10.0}{100}$$

$$\frac{3.0}{100}$$

$$\frac{2.5}{50}$$

$$\frac{3.8}{18}$$

$$5.2$$

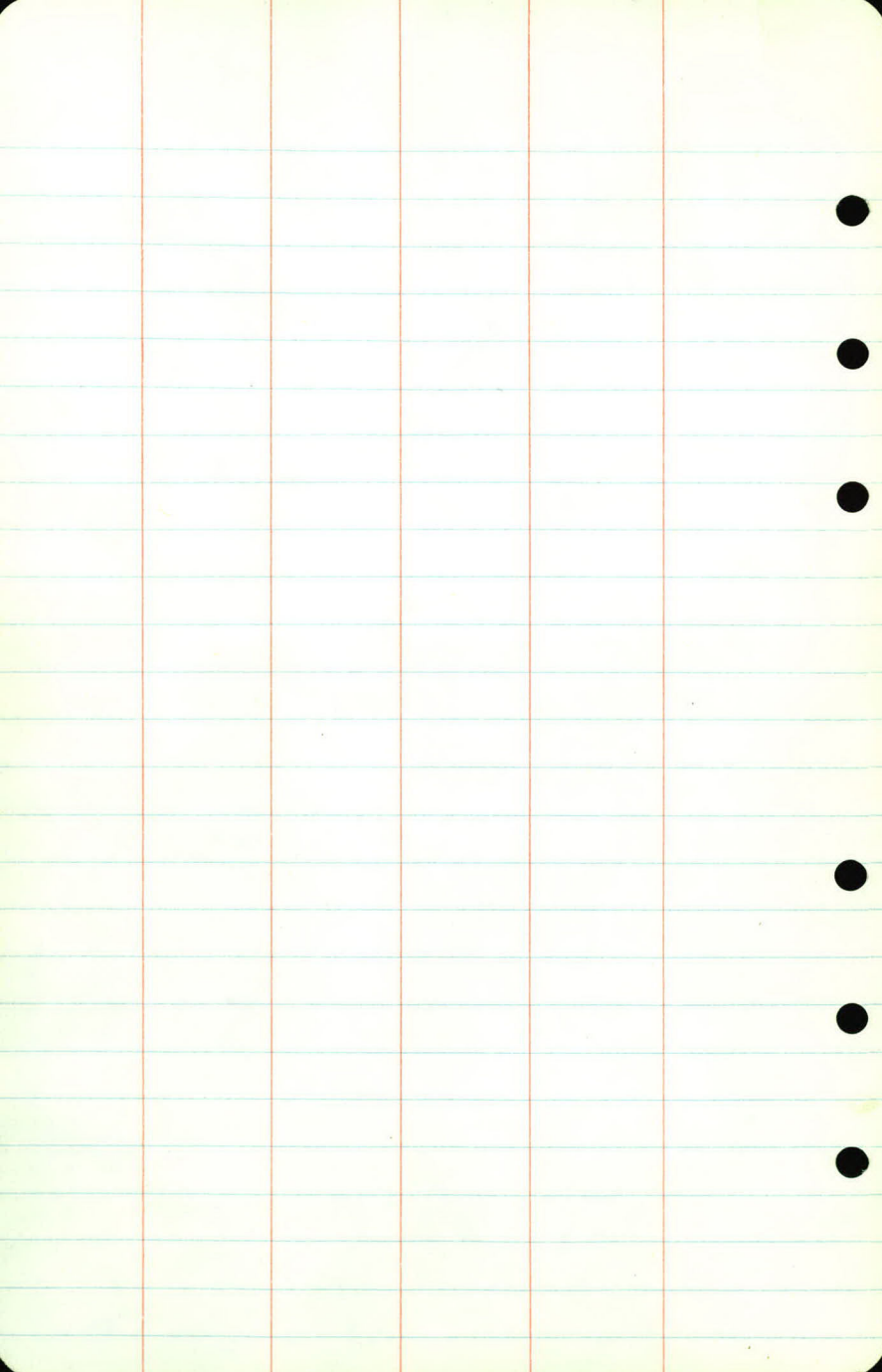
$$\frac{7.5}{31}$$

$$\frac{7.6}{50}$$

$$\frac{8.5}{80}$$

$$\frac{9.0}{100}$$

Top Mon "I" v Hamlin



Check Levels

Cloudy

9-24-41

HAW

A.M.

C.N.

L.L.

P.t.	+	π	-	Elev
B. M.	3.90	914.09.		910.19
	5.92	914.38.	5.63	908.46.
	6.45	917.37.	3.46	910.92.
B. M.	5.43	917.37.	5.43	911.94.
	4.39	916.64.	5.12	912.25.
	3.65	913.94.	6.35	910.29.
B. M.	2.86	913.94.	2.86	911.08.
	3.73	911.33	6.34	907.60.
	4.71	911.01.	5.03	906.30.
B. M.	5.51	911.13.	5.39	905.62.
	6.14	913.22.	4.05	907.08.
B. M.	3.55	916.17.	0.60	912.62.
	1.53	911.09.	6.61	909.56.
	9.23	909.43.	10.89	900.20.
	0.84	908.24.	2.03	907.40. (907.37)
	0.02	895.38.	12.88	895.36.
B. M.	3.53	887.70	11.21	884.17.
	13.02	900.23	0.49	887.21.
	5.47	905.06	0.64	899.59.
B. M.	6.32	906.71.	4.67	900.39.
	5.90	907.30.	5.31	901.40.
	5.35	907.88.	4.77	902.53.
B. M.	3.79	907.08.	4.59	903.29.
	6.01	908.45	4.64	902.44.
B. M.	4.30	907.66	5.09	903.36.

Description

Drill Hole. 0400 $\pm$ U.S.H. #10 & Co Rd "I."

Spk in P.P. S.W. Cor Co Rd "I" & Long Lake Rd

Spk. in 8" Oak 75' Lt Sta 26+40

Top Mon $\pm$ Sta 39+30.05

Spk. in S.W. Cor Wood M.H. Box 43' Lt Sta 53+15

Top Brass Plug $\pm$ U.S.H. #8 & Co. Rd "I"

Spk in Top End Guard Rail Post N.W. Cor Bridge

Top Mon & Co Rd "I" & Mounds View Rd.

Spk in PP #30 25' Rt. Sta 109+20

Top Mon. $\pm$ Sta 118+36.34

P.T.	+	Σ	-	Elev
		907.66		
	4.65	906.18	6.13	901.53
B.M	5.11	905.94	5.35	900.83
	3.04	903.86	5.12	900.82
	1.88	897.62	8.12	895.74
B.M.	6.72	894.59	9.75	887.87
	6.10	897.34	3.35	891.24
	5.18	896.20	6.32	891.02
T.P.	5.52	896.53	5.19	891.01
	8.16	901.47	3.22	893.31
	10.62	909.01	3.08	898.39
B.M	6.06	909.01	6.06	902.95
	0.34	905.51	3.84	905.17
			13.15	892.36

Description

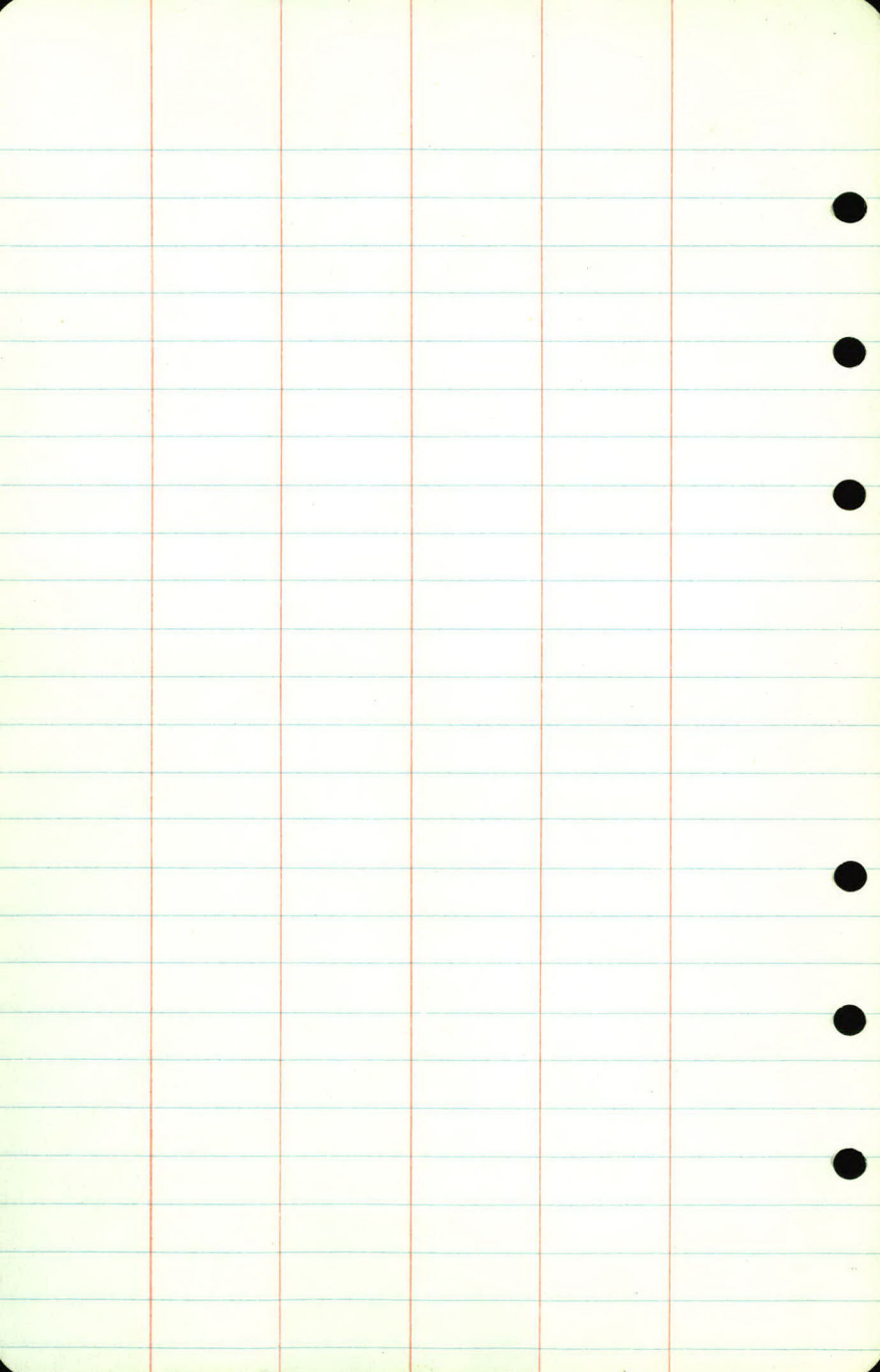
Spk. in T.P. 26' RI Sta 130735

Top Mon "I" + Hamline

S.E Cor Wooden Cover M.H.

Top M.H. East Side of Frame

Spk. in P.P. S.W Cor "I" & Lcy.



Push Soundings
Swamp

Sta 145 To Sta 148

Sta 150 To

Sta	Lt	100'	50'	$\frac{L}{0}$	Rt	50 = 100	Elev	$\frac{L}{0}$
-----	----	------	-----	---------------	----	----------	------	---------------

144+93

9'

145 7' 7' 6' 12' 16'

+50 6' 6' 8' 11' 16'

146 4' 5' 6' 7' 6'

+50 6' 7' 4' 6' 7'

147 4' 6' 7' 55' 8'

+50 8' 12' 11' 10' 10'

+75 8' 4' 8'

148 3' 3' 3'

+35 0'

149+80 0'

150 6' 4' 5'

R+

L4

±

Sta

100'

50'

50'

100'

150 + 50

12'

12'

10'

151

12'

13'

20'

+ 50

24'

152

17'

16'

18'

+ 50

10'

7'

8'

153

5'

4'

4'

+ 50

4'

6'

154

3'

11'

13'

+ 50

4'

155

2'

3'

4'

+ 50

3'

156

4.5'

8'

3'

A

±

R+

stg

100'

50

100'

156+30

4'

157

13'

6'

5'

+50

13'

158

14'

14.5'

21'

+50

29'

159

28'

34'

35'

+50

28'

160

16'

15'

22'

+28'

9'

+60

6'

Line. B.
Revised
Push Soundings

Marsh

Sta 140 To 145

	2+		50 RY
5+9	50	2	

141+16		0	
--------	--	---	--

+50		4'	
-----	--	----	--

142	14'	7'	2
-----	-----	----	---

+50		11'	
-----	--	-----	--

143	20'	15'	7'
-----	-----	-----	----

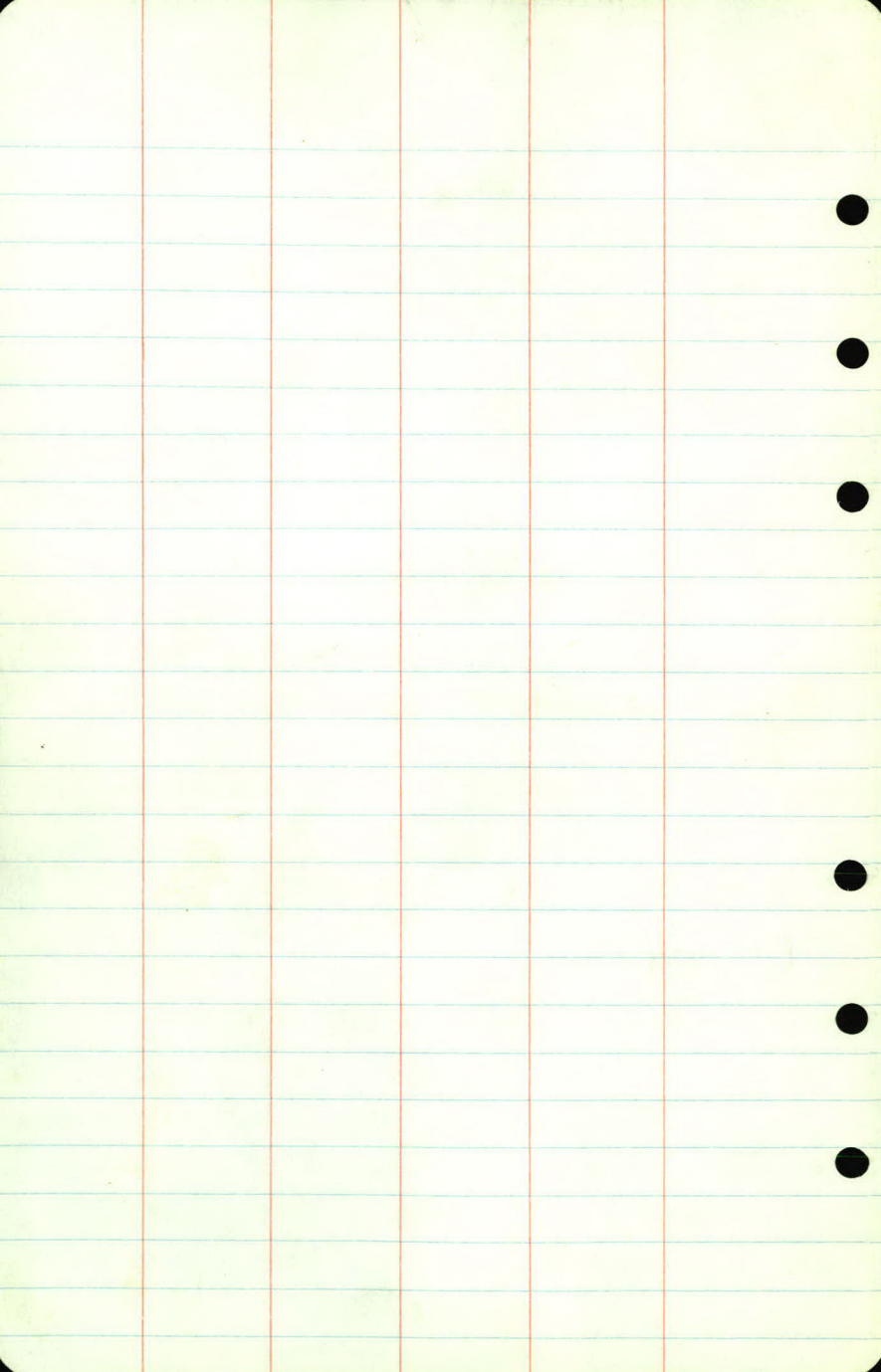
+50		16'	
-----	--	-----	--

144	21'	17'	21'
-----	-----	-----	-----

+50		19'	23'
-----	--	-----	-----

+80	17'	16'	22
-----	-----	-----	----

47 B



Topography

10-3-41

HAL
AM
CIV
LL

10d 15' 10d 15'

5 15' 15'

4 15' 15'

3 15' 15'

2 15' 15'

1 15' 15'

0 +20 Edge Para

+54 Beg Small Trees 33'-60'

+12 End Tree Line 62'

+33 Beg Trees 62'

+47 End Brush 60'

+63 Ent.

Cultivated

+62 Beg Brush 60'

+62 Vent 44 M.H 46' -

+38 20' Rd. -

End Brush 31' -

+24 Beg Lt. Brush 33' -

+06 C 5'x5 M.H 48' -

+39 End Rad 14' -

+35 T.P 33' -

+20 Beg Rad 19' -

+78 End Rad 16' -

+65 Beg Rad 31' -

10' shoulder
Pavement 4'

0.5 H 10.3
27' 1 c.c

13

Red

Red

12

15'

15'

11

15'

15'

10

15'

15'

9

15'

15'

8

15'

15'

7

15'

15'

6

15'

15'

+79 Rgo Tir Ent

+80 End Rad 24' .

+59 Beg Rad .

+80 End Rad 22'

+65 T.P. 28'

+60 End Cult

+59 Beg Rad 15'

Brush 60' .

+80 Brush 30' .

Brush

Brush 30' .

+47 Beg Brush 30' .

Planted Prop.

Cultivated

+66 $\frac{1}{2}$ 20' Rd. .

+50 End Trees 33'-50

20

Kd
15

Kd
15

19

15"

15"

18

15"

15"

17

15"

15"

16

15"

15"

15

15"

15"

14

15"

15"

13

15"

15"

+52 Vent 45 M.H 48'

+47 Fc Cor. 33'

Fc 33'

Fc 33'

Fc 33'

End Yd Beg Cult

Uncultivated

Fc 33'

+50 6" Plum 27'

Fc 33'

+69 Fc Cor 33'

Yard

+20 Ent 31'

+21 End Rad 15'

+06 Beg Rad 20'

27

Rd

Rd

26

15'

15'

25

15'

15'

24

15'

15'

23

15'

15'

22

15'

15'

21

15'

15'

20

15'

15'

+98 6" Tree 38'

+65 6" Oak 30'

+60 Group 7-6" Oak 34'

+31 6" Tree 36'

+24 Big Woods 87'

+20 End

+11 Ec Cor 60'

Woods

Uncultivated

End Cult

Uncultivated

Rel

Rel

33

15'

15'

32

15'

15'

31

15'

15'

30

15'

15'

29

15'

15'

28

15'

15'

27

15'

15'

Fc 60 Woods 200'

53

+55 Pothole 23'

+12 Fc Oak 65'

Fc 60 Woods 100'

Pothole 160'

+50 Pothole 200'

+08 8" Oak 37'

Fc 60 Woods 87'

Fc 60' Wood 87'

+54 Vent 45' M.H. 48'

← — — — — — too Bad Hayfield

Fc 60'

Uncultivated

Fc 60' Woods 87'

+23 6" Oak 35'

+11 6" Oak 35'

+06 6" Tree 35'

Fc 60' Woods 87'

41 Rd 15' Rd 15'

40 15' 15'

39 15' 15'

38 15' 15'

37 27' 100 L Drain 24" x 54 CM 27'

36 15' 15'

35 15' 15'

34 15' 15'

57
End Pothole 150'

+10 End Trees 26'

Uncultivated

Pothole 21-200'

+30 Fe Cor 60' * * *

+30 End Cult.

Fe 60' Trees 26-50'

Pothole 25-200'

Fe 60' Trees 26-60'

Fe 60' Trees 37-60'

Pothole 27-200'

+96 Stu 28'

+48 Trac line 38-60'

+475 Stu 25'

+44 Stu 30'

+36 Stu 31'

+30 Beg. Cult. 60'

+15 4 Will. 38'

Fe 60'

Pothole 26-200'

+90 15" Pop 39'

+80 10" Pop 40'

+77 12" Pop 39'

+04 Stu 28'

Fe 60'

Pothole 23-200'

Fe 60' Woods 200'

Pothole 23'-200'

Rd

Rd

47 15' 15'

46 15' 15'

45 15' 15'

44 15' 15'

43 15' 15'

42 15' 15'

41 15' 15'

Uncultivated

Uncultivated

55 R1 15' R1 15'

54 15' 15'

53 15' 15'

52 15' 15'

51 15' 15'

50 15' 15'

49 15' 15'

48 15' 15'

End Woods 28-70

Woods 28-150'

Woods

Woods 28'

+48 Beg Woods 28'

+45 X Fe 41

+37 Ent.

+14 Vent 48 MH 48'

+39 Ent

Uncultivated

Uncultivated

62

Rd

Rd

61

15'

15'

20

+98' Drain
18" x 48' CM

28'

+50' X DRAIN

P

33

60

15'

15'

59

15'

15'

58

15'

15'

57

15'

15'

56

15'

15'

55

15'

15'

Uncultivated

+ 30 Fe 33
+ 19 Retic Fe
Fe 33'

Pasture

Fe 33'

Fe 33'

+ 28 Fe Cor 33'
End Cult

+ 73 W.W. Drain Pipe 31'

Uncultivated

Cultivated.

+ 35 Field Ent

+ 00 Retic Cult

69 R9 R8
14 12

68 14

67 15' 14'

66 28' 408 x Drain
15' x 52' 24

+82 East Edge

+55 West Edge Pure

65 15' 15'

64 15' 15'

63 15' 15'

62 15' 15'

Fc 79'

Fc 65'

+85 Fc Cor 65'

+00 6" W. 11' 27'

+85 6" W. 11' 23'

+16 End Rad 15'

+90 Beg Rad 45'

US # 8

+48 End Rad 25'

+31 Beg Rad 15'

+24 End Cult

+40 Beg Cult

Cultivated

Scattered Oaks + Stumps

33'

+66 PP 20'

+40 PP 20'

+52 PP 20'

+16 End Rad 16'

+82 Beg Rad 53'

27' Pave

+34 T.P. 21'

+31 End 36'

+31 Beg Rad 15'

26'

+50 N.W. Cor Bldg 67

+26 Ent 30' Wid

Uncultivated

76

Rd

Rd

75

10'

14'

+29 T.P. 22'

74

+38 End Bridge

+79 Beg Wings Wall 19'

+85 Beg Bridge

73

10'

15'

72

10'

13'

71

13'

13'

70

13'

12'

69

Marsh 100' (57)

+85 Marsh 35'

+46 T.P 23'

Marsh 34'

+43 End Wing Wall 20'

+39 Cor Wing Wall 35'

Rice Creek

+94 Beg trestle 43'

+84 Beg Wing Wall 35'

+43 End Wing Wall 20'

+87 Beg Tie Creek

+79 Beg Wing Wall 19'

+66 End Walls 43'

+07 MH 50'

Fc 96'

Marsh 28'

+88 P.P 22'

+50 Beg Row Wills 100'

Fc 95'

+36 P.P 22'

Fc 95'

+00 Beg Marsh 33'

Uncultivated

Fc 93

+05 P.P 21'

+80 End Outlets

83

Red Red

82

10'

16'

81

10'

16'

80

10'

16'

79

10'

17'

78

10'

16'

77

10'

17'

76

10'

14'

+80 Beg Yard

+39 P.P. 27'

Woods 38'

Woods 41'
+100 P.P. 26'

Uncultivated

Woods 39'

+58 P.P. 26'

Woods 40'

+00 End Cult.

+18 P.P. 25'
Woods 41'

+00 Beg Cult
+90 Ent 15" x 16" CM 22'



+00 Beg Woods 41'

+80 TP 24'

+69 1/2" Oak 45'

+38 24" Oak 41'

90 RA RA

89 12' 16'

88 11' 15'

87 11 16'

86 11' 16'

85 11' 16'

84 11' 16'

83 11 16'

+90 Fc Cor 33'

+27 P.P. 33'
Woods 38'

Woods 86' Fc 33'
+87 Fc Cor 33'
+87 P.P. 44'
+67 Ent 15" x 20' CM 28'



Fc 33' Woods 80'

Woods 36'
+87 P.P. 32'

Woods 90' Fc 33'

Woods

+79 Fc Co 33'

+47 P.P. 31'

Woods 90' Fc 33'

Woods 35'

+37 Beg Woods 90'
+37 Fc Cor 34'



Fc 34'

+06 P.P. 29'
Woods 35'

+67 8" Apple Tree 33'

Scattered Fruit Trees
50'

+00 End Yard
+95 Beg Fc. 34'
+60 Ent 15" x 24' CM 22'

Woods 36'
+76 P.P. 28'

+48 P.P. 31'

+08 W.W.M.H. 48'

+04 S.W. Cor 31.5'



Woods 36'

97

Ra

Ra

96

13'

15'

95

14'

15'

94

13

15'

93

13

321

92

91

11'

16'

90

13'

15'

Airport

+69 P.P. 27'

End Cult Beg Airport

Cultivated
Defense Site

+96 P.P. 28'

+55 End Rad 16'

+06 M.H. 48'

+25 Beg Cult
+25 End Rad 14'
+12 Beg Rad 32'
+93 End Rad 40'
+72 Beg Rad 16'

+20 Beg Rad 84'
+00 Beg Cult
+80 End Rad 88'
+60 End Woods 60'

End Woods 92'

+00 Beg Rad 16'
Woods 40'

+52 Ent.
+43 End Fc 33'

+40 P.P. 34'

Woods 90 Fc 33'

Woods 38'

104

Kd

Kd

103

13'

12

102

13'

13'

101

13'

13'

100

13'

14'

99

13'

14'

98

13'

15'

97

13'

15'

+69 P.P. 26'

Cultivated

+50 Field Enl.

+98 P.P. 26'

Cultivated
Defense Site

+16 P.P. 27'

+60 End Airport
Beg Cult

+43 P.P. 27'

111

Red

Red

118

14'

12'

109

15'

12'

108

15'

12'

107

14'

13'

106

14'

12'

105

14'

12'

104

14'

12'

+00 End Garden

End Cult 64

+00 End Yard

+70 Ent.

+66 P.P. 24'

+87 S.E. Cor. No 685

+83 S.W. Cor. No 67

No 24
40

+40 End Cult Beg
Yard

+92 P.P. 23'

+83 Field Ent

Cultivated

Cultivated

+09 P.P. 24'

+31 M.H. 48 Ven 144'

+32 Ent

+43 P.P. 24'

118

Rd

Rd.

117

14'

13'

116

14'

13'

115

15'

12'

114

15'

15'

113

14'

13'

112

14'

13'

111

14'

13'

Fc 34'
+91 Ent.

+50 M.H 48 Vent 45'

Fc 34
+94 Fc Cor 34'

Fc 34

+24 Fc Cor 38'
+15 Fc Cor 25'
Fc 24'

Fc 23'

Fc 23

+59 Fc Cor 23'

Uncultivated

Pasture

+67 P.P. 22'

+90 P.P. 23'

+14 P.P. 23'

Uncultivated

+40 P.P. 24'

Rd

Rd

124

13'

14'

123

14'

15'

122

13

14'

121

13'

14'

120

14'

14'

119

14'

13'

118

15

13

+00 Ent 66

+50 Ent

Fc 33

+54 T.P. 29'

Fc 33

Fc. 33'

+87 P.P. 29'
+78 @ P.c 28'

Fc. 33'

+17 G.P. 24'
Fc 33'

+31 Ent

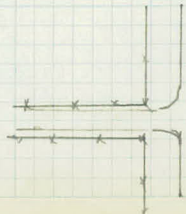
+18 P.P. 26'

Uncultivated

Fc 33'

Cultivated

+48 Fc Cor 33
+37 Ent
+31 Fc Cor 33
Fc 33



+40 Beg Cult
+36 P.P. 23'

132✓

Rd

R4

131

15'

14'

see

Revised



130

16'

14'

129

15'

12'

128

15'

13'

127

15'

13'

126

15'

13'

125

15'

13'

+91.6" Coll. 31

+44 Fe Cor 37'

+20 End Bthole 55-100'

Fe 37'

+85 Beg Bthole 55-110'

Fe 37'

+05 Fe Cor 38'

Fe 38

Fe 38'

+45 Water Pipe 33'

+27 Ent

Fe 33'

Fe 33'

+22 Fe Cor 33'

Fe 33

Pasture

Cultivated

Revised
See

+35 T.P. 30'

+35 End Cult

+65 T.P. 29'

+88 Ent

+27 Ent

+94 T.P. 29'

Cultivated

+25 T.P. 29'

Red

Red

138

15'

13'

137

15'

13'

136'

15'

14'

135'

15'

14

134

15'

13'

133

15'

13'

132

15'

13'

Revised
see

+85 Ent 15" x 20' CM 26'



68

+75 Ent.

+46 T.P. 29'

+80 End Pothole 20'

+35 Pothole 24.6'

+100 Pothole 20'

+74 T.P. 29'

Uncultivated

Pothole
Uncultivated

+99 8" Twin Coll 33'
+84 6" Coll 29'

+02 T.P. 29'

Rd

Rd.

145'

+88 East Edge Rd

144

16'

13'

143

16'

12'

142

16'

13'

141

16'

13'

140

15

13'

139

15

14

see Revised

Exception

+60 End Rad 55' ——— Hamlin Ave
 +25 Beg Rad 17' ——— +59 End Rad 45'
 +25 Beg Rad 15'

see revised

Uncultivated

Uncultivated

+78 Twin 6" C o H. 39
 +65 6" C o H. 34'

151

150

149

148

147

146

145

144

See Revised

+14 C. 8' Ditch

+96 Edge 5wp

+88 East Shl. Hamline

+58 West Shl. Hamline

SWP 250

SWP 250 70

+80 SWP 250

+79 Beg SWP

+100 SWP 100'

120 C of Brush 85'

+85 SWP 500'

+85 End SWP.

+85 SWP 240'

See Revised

+100 SWP 400'

+100 A in Ditch 39'

+100 SWP 250'

158

+84 Fence X 4

157

+50 Beg Brush

156

+50 Beg Swp

155

+49 Ditch X 4.
End Swp

154

153

152

151



Swp 300' Brush 110'

Swp 240' Brush 240'

+50 Brush 80'

+150 Beg Brush

+100 Swp 240'

+50 Swp 250'

+100 Ditch 65'

+100 Beg Swp 100'

+54 6" Elm 9'

Swp 25'

1" Elm Ditch

+100 Ditch 63'

End Swp End Brush

+150 Swp 50'

Swp 100'

Brush 100' Swp 250'

Swp 250'

+30 Brush 100'

Brush 150' Swp 240'

166

165 Cult 0

164 Cult 0

163 Cult 0'

164 Beg Cult 0'

162

+98 stu 14'
+85 15" Oak 16'
+82 stu 7'
161

160

159

+64 Fc x R
End Pasture

+35 Fc x R

+21 N.E. Cor Ho 166'
+26 Oak 75'
+12 N.E. Cor shed 103'
+02 Oak 96'
+72 24" Oak 35'
+60 N.E. Cor shed 92'
+62 18" Oak 2'
+93 24" Oak 35'
+30 N.W. Co. shed 89'
+35 Tree 81'
+15 stu 22'
+04 N.E. Cor. Crib 95'

+96 N.W. Co. Corn Crib 97'
+93 N.E. Cor Barn 101'
+78 N.W. Cor Barn 103'
+73 Fc Cor 70'
+70 N.E. Cor 131'
+46 N.W. Cor 130 138'
+24 Fc Oak 74'

+98 12" Tree 90'
+85 8" Oak 5'
+83 stu 51

+34 W. 11 68'
+33 W. 11 73'
+25 12" W. 11 63-82'

Cultivated

Uncultivated

Scattered oaks
45'
25'
No

14'
Shed
52'

+79 NW Cor Shed
101'

26'
Coop
9'

16'
12'

+97 Stn. 2'

Ba.
32'

+91 Oak 58'

+87 Oak 14'

+60 Stn 4'

+66 15" Oak 5'

+56 15" Oak 69'

+52 Stn 77'

+39 Stn 89' +76'

+39 Oak 57-81'

+35 15" Oak 109'

+26 12" Oak 89'

+08 12" Oak 41'

pasture

+35 Stn 35'

+31 Trn 12" 44'

+24 12" Will 47'

- +66 Stn. 5'
- +45 Oak 17'
- +21 Stn 26 Oak 26'
- +12 20' Oak 49'
- +00 15" Oak 30'
- +76 12" Oak 53'
- +64 Stn 43'
- +59 12" Oak 42'
- +52 12" Oak 19'
- +49 Stn. 18'
- +39 12" Oak 32'
- +31 24" Will 67'
- +29 12" Oak 21'

+78 12" Will 19'

+35 Triple Will 135'

+35 15" Will 7'

+35 End Swamp N14E

+00 End Brush

+50 End Brush

Brush 250 Swamp H00

Brush 200 Swamp H40

172

+36 Edge Rd

171

+10 Edge Rd

170

169

168

167

Cut D'

+99 Rd Sign 15' ϕ Lexington Ave 26' Black Top ϕ +93 P.P. 50'

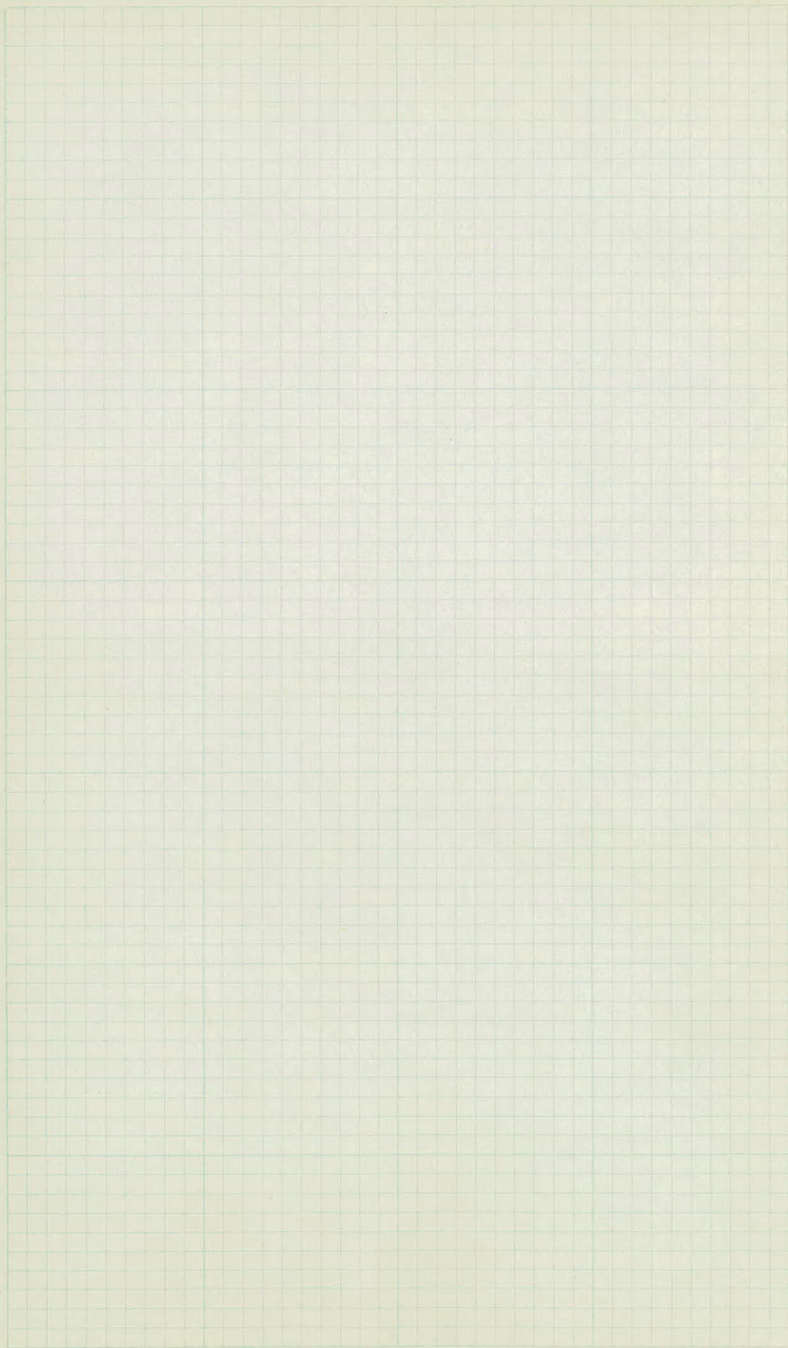
+93 P.P. 77'

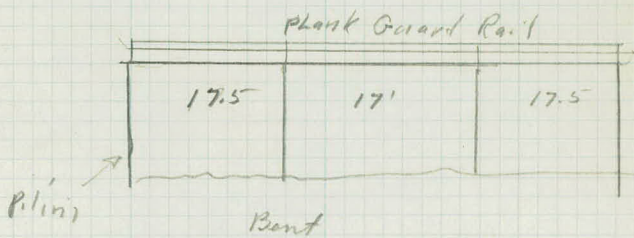
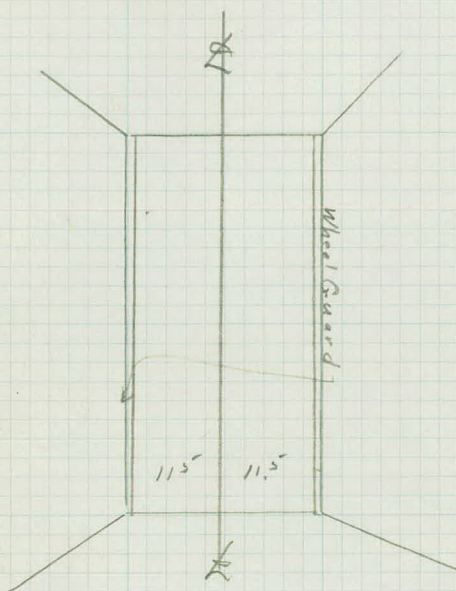
uncultivated

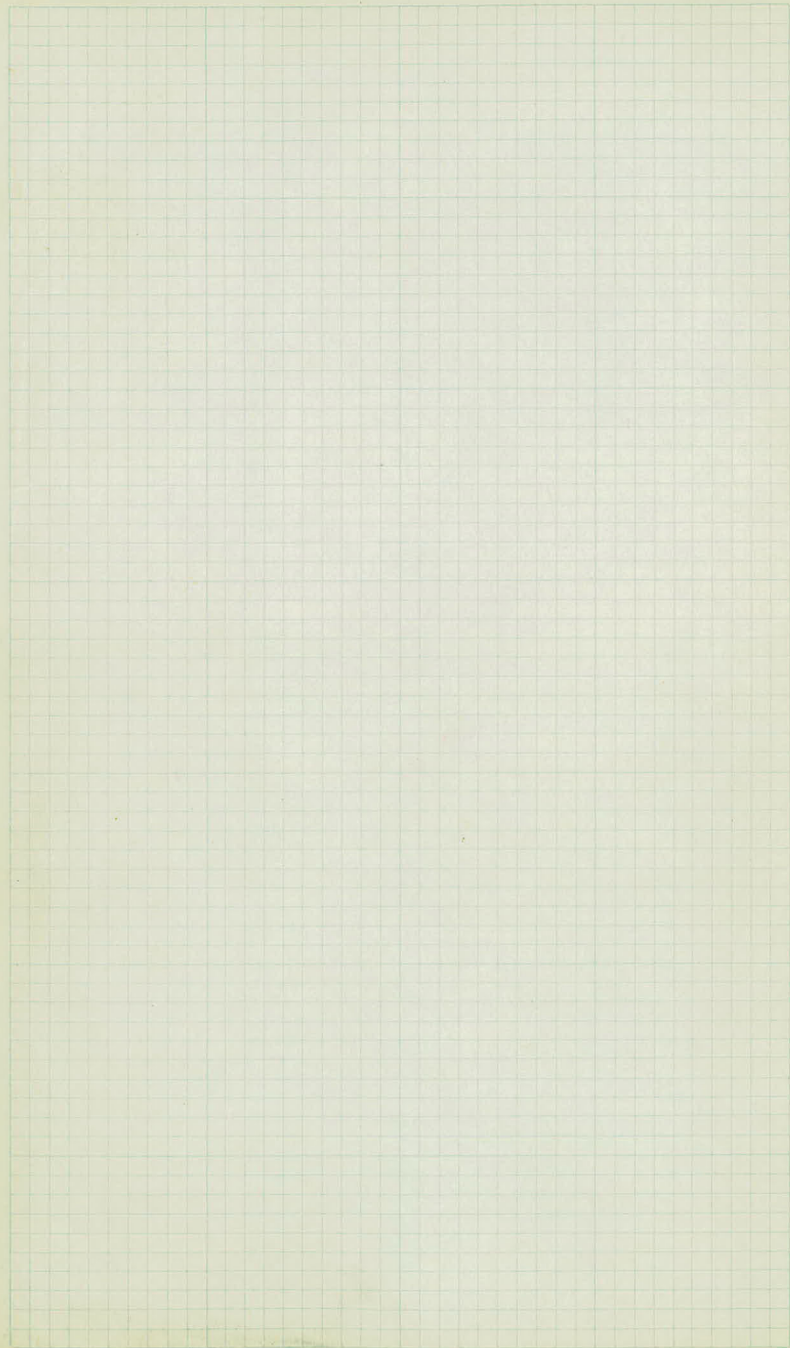
+00 End Cult

cultivated

Cult 200'







74A

Topography

B" Line

R1 R1
59' 94'

+50

47 81'

136

37' 71'

+50

28' 60'

135

19' - 52'

+50

12' 44'

134

4' 38'

+50

1

33'

133

6'

28'

+50

11'

23'

132

14'

20'

131

16'

16'

151.97 PC

16'

16'

130

74B

Cultivated

100 Beg Cult

+02 6" Triple Cot/24

+87 6" Cot/19'

+91 8" W. 11/28'

+74 W. 11/32'

+45 Fc Cor 34' 1'
End Pot Hole 55'

Fc 36' Pot Ho. 50'-100'

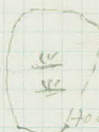
W. Main 45'

Fc 36

+50 Beg Pot/Hole 50'

Uncultivated

Pasture



+60 End Pot/Hole 60'
Pot Ho. 50'-75'

100 Beg Pot/Ho 46-75'

+67 T.P. 47'

Uncultivated



+30 End Pot/Hole 55'
+04 T.P. 28'
Pot Hole 26'-100'



+35 Beg Pot/Hole 26'-100'
+26 End Pot/Hole 29-100'
Pot Ho 26'-100'

+52 Pot/Ho 75'

143

142

141

140

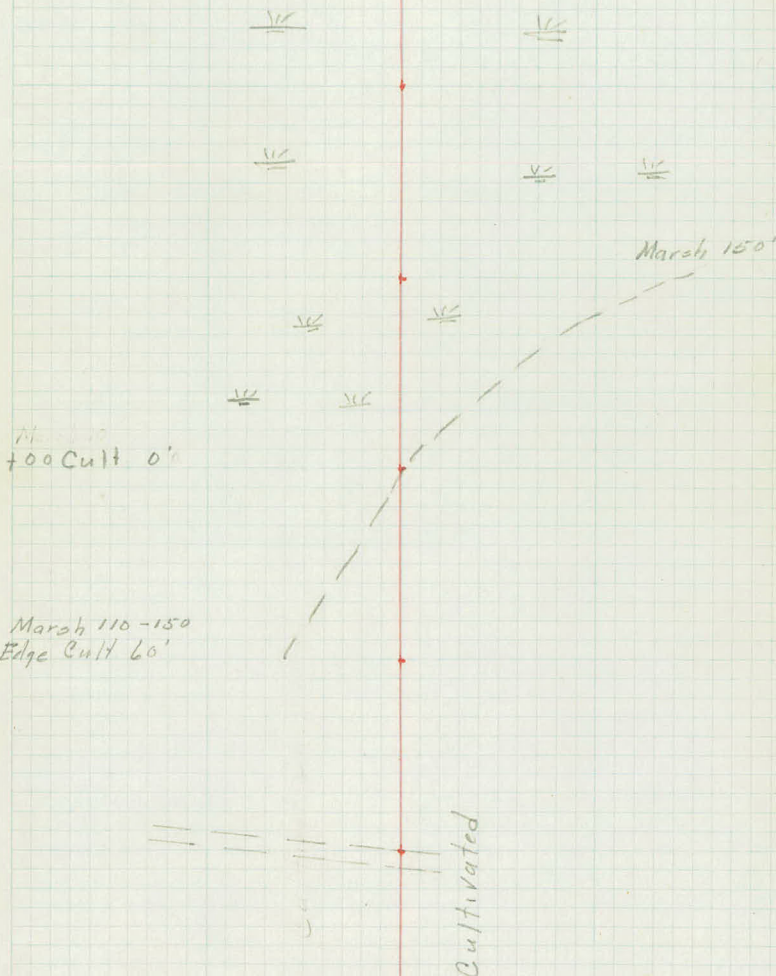
139

198 Field Rd X 2

138

137

74C



150

149

+25 End Swp

148

147

146

+55 Ditoh #1 X ♀

+27 Edge Swp

+16 Edge Rd

145

+90 Edge Rd

+80 Edge Swp

144

Uncultivated



8' Btm Ditch



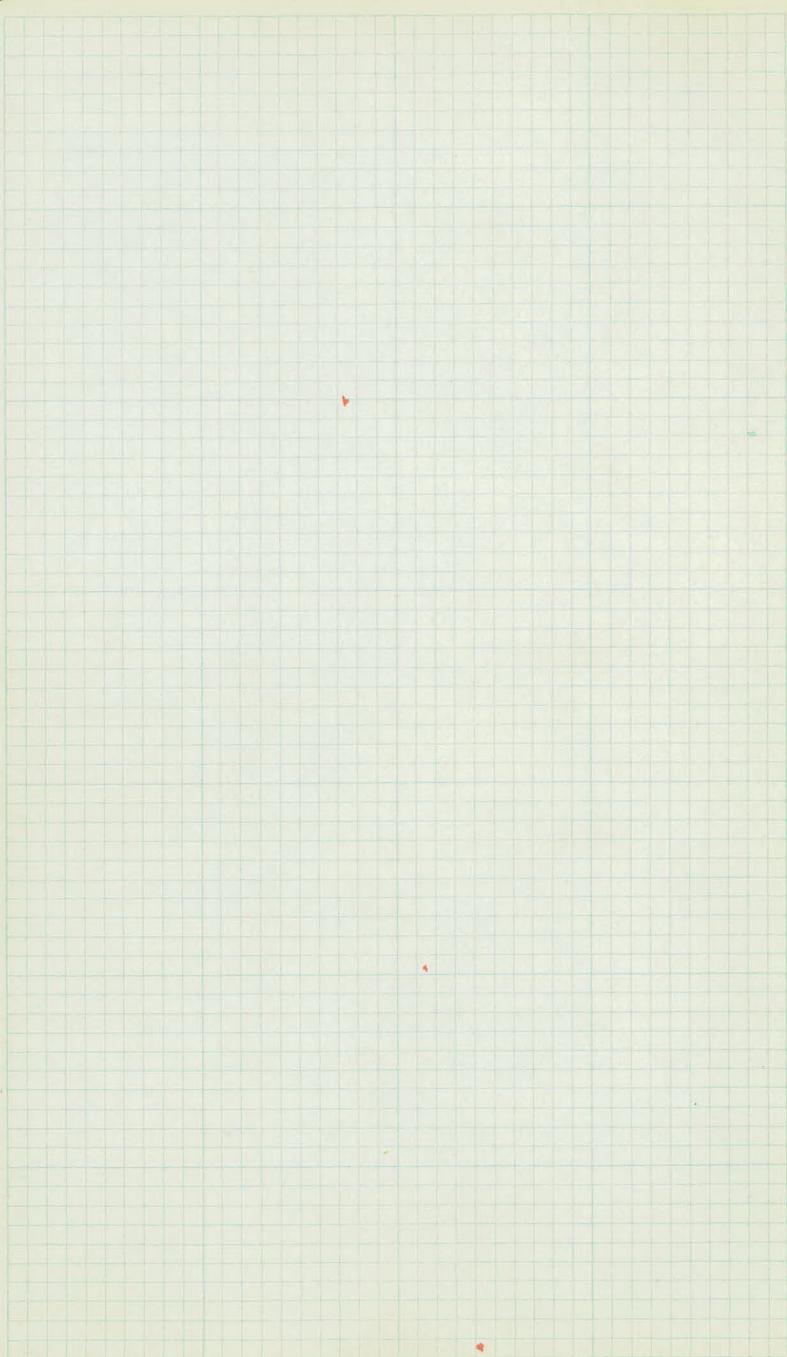
+30 A Ditch 24
+27 SWP 400

+27 SWP 200

Hamline Ave

Marsh +
Scattered Pop.





Stadia showing

Pothole

Line	Azimuth	Stadia Dist	Read on Rod	Vert Angle
At S ¹ / ₄ Sec 3	N = 0°00'		H. I = Elev 893.34	
	14°30	95'	9.0	
	5°55	220'	8.7	
	47°16	60'	5.4	
	42°45	70'	8.3	
	4°45	340'	11.0	
	73°50	144'	4.2	
	3°30	450'	10.3	
	67°25	145'	13.3	
	77°35	365'	8.1	
	2°45	715'	5.4	
	60°45	395'	7.6	

Description

Stone Murr

Edge Pothole

EDGE POTHOLE

Top CONDUIT

Top CONDUIT

ANGLE-IN-DITCH

X DITCH Top CONDUIT

EDGE POTHOLE

EDGE POTHOLE

" " "

" " "

" " "

LINE	STADIA AZIMUTH	READ DIST	ON ROD	VERT ANGLE
------	-------------------	--------------	--------	---------------

42° 05'	450'	7.2		
---------	------	-----	--	--

8° 20'	820'			
--------	------	--	--	--

30° 00'	542'	7.2		
---------	------	-----	--	--

16° 00'	880'	4.8		
---------	------	-----	--	--

25° 35'	650'	6.4		
---------	------	-----	--	--

23° 00'	745'	5.6		
---------	------	-----	--	--

DESCRIPTION

EDGE - POTHOLE

" " "

" " "

" " "

" " "

" " "

$$\begin{array}{r}
 171 + 196 \checkmark \\
 144 \quad 724 \checkmark \\
 \hline
 3018
 \end{array}$$

KP
JS
DS
WS
R. Boss

2 April 1963

Co. Rd I

Adams to Long Lake Rd.

culvert elevations

Sfa	+	π	-	Elev.	
BM	2.15	102.15			(100.00)
0+00			5.5	96.7	
0+51			6.1	96.1	
0+85			6.4	95.8	
1+12			6.6	95.6	
1+46			6.5	95.7	
2+00			6.3	95.9	
2+20			6.3	95.9	
2+92			7.0	95.2	
BM			2.16	99.99	(100.00)

2 APRIL 1963

Description

Top Hydrant S.W. Cor Co Rd 1 & Adams

Gutter at N.W. Cor. Adams & Co. Rd I.

FL. E. end 15" CM

FL W end 15" CM

FL E end 15" CM

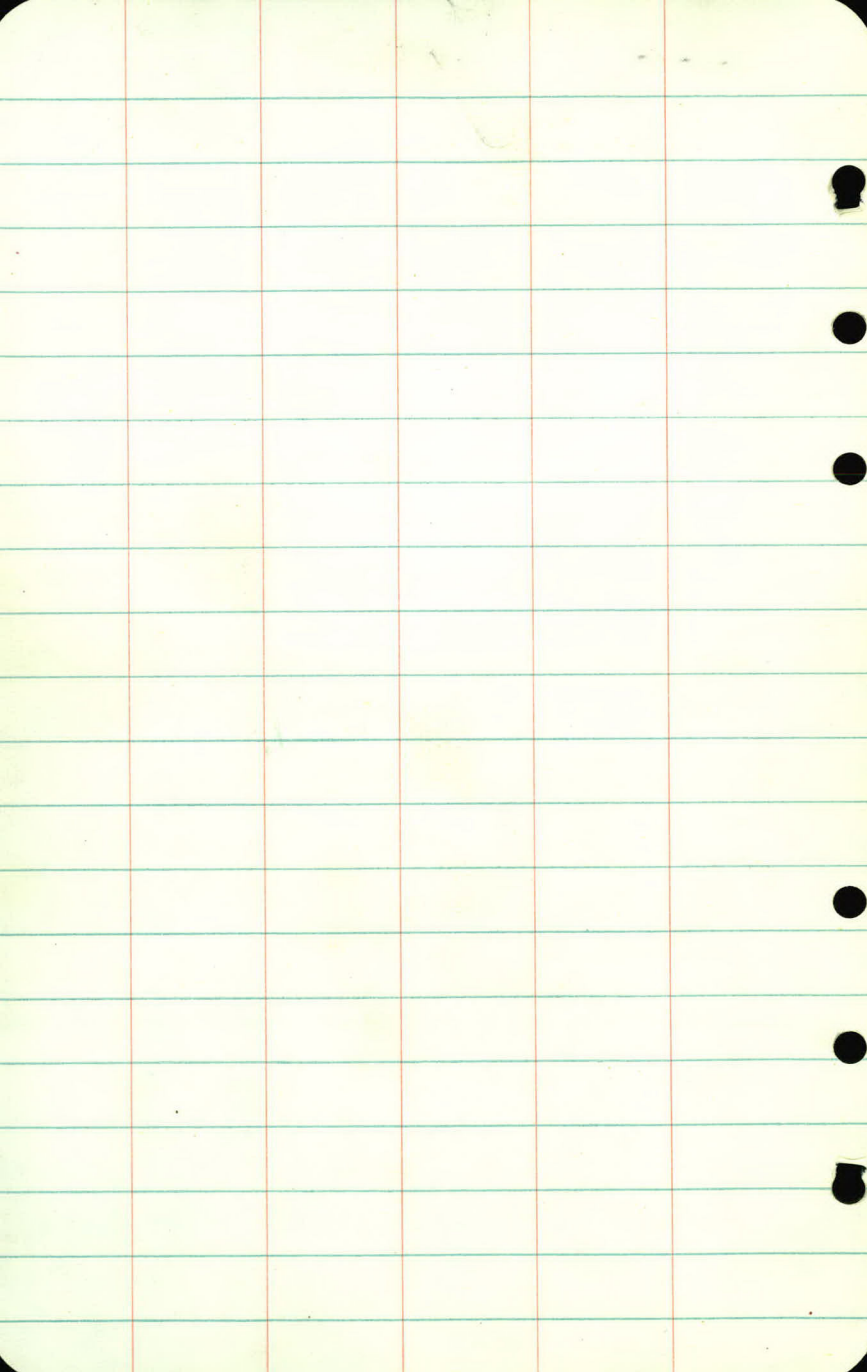
FL W. end 15" CM

FL. E end 15" CM

FL W. end 15" CM

DITCH

Top hydrant N.W. Cor Adams & Co. Rd I.



DITCH ELEVATIONS

ALONG T.H. # 10

LONG LAKE Rd To Co. Rd I

4 PAGES

Sta	INV GRADE	PCR	Rod	Cut	Elev
BM	3.89	918.82			914.93
TP	1.78	918.39	2.21	916.61	
TP	9.24	916.49	11.14	907.25	
1+00	904.95	11.54	5.98	5.56	
+50	5.00	11.49	6.24	5.25	
2+00	5.05	11.44	6.09	5.35	
+50	5.10	11.39	5.02	6.37	
3	5.15	11.34	5.27	6.07	
+50	5.20	11.29	5.40	5.89	
4	5.25	11.24	5.54	5.70	
4+30			8.36	908.13	906.95
TP	1.41	914.60	3.30	913.19	
			6.21	908.39	908.30
4+50	5.30				
5+00	5.35				
5+50	5.40	9.20	4.26	4.94	
6	5.45	9.15	4.97	4.18	

GA:WS
DS
BW

11-7-75

Description

2

TOP HYD

COR LONG LK Rd ; Co. Rd

TOP HYD

400'

N

of

LONG LK Rd ;

T.H. 10

Flow line

West end

Culvert @

Long LK

in

T.H. 10

EAST END F.L.

CULVERT

4+30

TOP HYD

ENT

AT

PENNYS

MARKET

WEST END F.L.

Culvert

5+00

Sta	INV GRADE	PGR	Rod.	Cut	Elev
		914.60			
6+50	5.50	9.10	5.09	4.01	
7	5.55	9.05	4.97	4.08	
+50	5.60	9.00	4.09	4.91	
8	5.65	8.95	3.15	5.80	
8+10			7.18	907.42	(902.45)
TP	2.82	914.63	2.79	911.81	
9+32			7.38	907.25	(907.17)
8+50	5.70				
9+00	5.75				
+50	5.80	8.83	4.26	4.57	
10	5.85	8.78	4.75	4.03	
+50	5.90	8.73	4.93	3.80	

WS
CA
DS
BW

11-7-75

Description

3

E END CULVERT

TOP SOUTH BOLT LIGHT STANDARD 8460 RT

W END CULVERT

Sta	INV Grade	PCR	Rod	Cut	Elev
		914.63			
11+00	5.95	8.68	4.49	4.19	
+50	6.00	8.63	4.19	4.44	
12	6.05	8.58	4.30	4.28	
+50	6.10	8.53	3.86	4.67	
13+00	6.15	8.48	4.07	4.41	
13+28			8.82	905.81	
BM			6.53	908.10	(908.15)

WS
CA
DS
BW

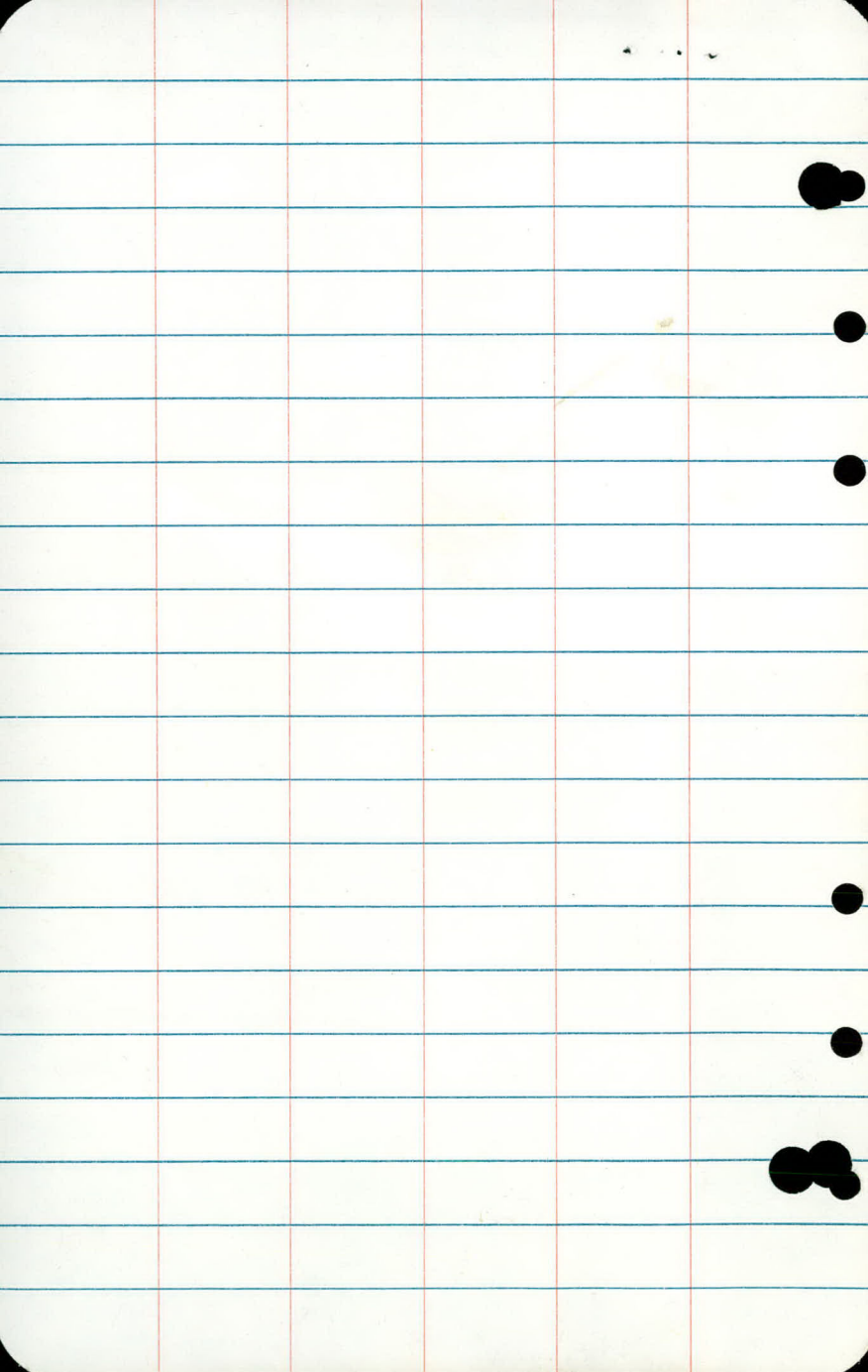
11-7-75

4

Description

F.L. CULVERT

Flow line Culvert 11/25



FK
RG
DS
HG

Nov 3, 1975

1

Co. Rd. "I"

Long Lake Road to TH #10

DRAINAGE

Sta	+	π	-	Elev.
BM	0.05	914.98		914.93
BM			1.30	913.68
BM	5.21	916.26	3.93	911.05
0+00	908.40		7.00	09.26 C 0.86
+50	08.25		7.51	08.75 C 0.50
1	08.10		7.46	08.80 C 0.70
+50	07.95		7.23	09.03 C 1.08
2	07.80		7.39	08.87 C 1.07
+50	07.65		7.52	08.74 C 1.09
3	07.20		6.18	10.08 C 2.88
+35	06.85		6.25	10.01 C 3.16

FH
RG
DS
HG

Nov. 3, 1975
Clear Calm 68°

2

Top Hyd S.W. Corner Long Lake Road

Top H 300' W of LL Rd. 4 Co Rd I

Top Hyd S - Corner I & Eastwood

8.8

7.5

8.8

7.5

8.8

7.5

8.9

7.4

9.0

7.3

9.2

7.6

7.1

9.4

6.9

9.2

7.1

Sta	π	π	-	Elev.	
		916.26			
3+70	06.50		6.46	09.86	C 3.30
+85	06.35		6.88	09.38	C 3.03
A	906.19		6.37	09.89	C 3.70
BM Check			8.10	910.16	(908.13)

FK
RG

Lt

Nov. 3, 1975

3

6.9

6.6

6.6

Inv. 18" RCP

