

BK. 76 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Drainage Survey

_____ Ditch # 1

From Rice Creek To Marsden Lake

Road Acc't. No. _____

Date Filed. 6-11-41

File _____

PLAN SURVEY

Ditch #1-

Rice Creek to Marsden Lake
to Lexington Av.

Completed - 10-9-'40

INDEX

Alignment - 1 thru 7

Topog 8 thru 16

Bench Levels 17 thru 19

X Sects. 20 thru 28, 29 thru 32

PARTY

R. Pense
L. Goldberg
C. Fewer
M. Benson

Plan Completed
11/9/40

Sta.	Pt.	Angle		Bearing	
		Lt.	Rt.	Mag.	Calc.

8 + 48.10	P.I.				
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175.90

S 54° 50'

S 58° 50' E

6 + 72.20	P.I.				
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7° 18' Lt.

171.30

S 46° 30' E

S 46° 32' E

5 + 00.90	P.I.				
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15° 06' Lt.

32.7

S 31° 15' E

S 31° 26' E

4 + 68.20	P.I.				
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19° 20' Lt.

42.2

S 11° 45' E

S 12° 06' E

0 + 47.00	P.I.				
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S 1° 38' R.

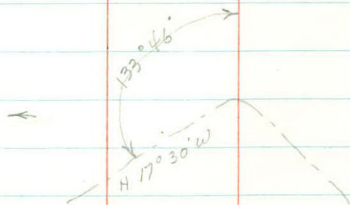
4.7

S 64° E

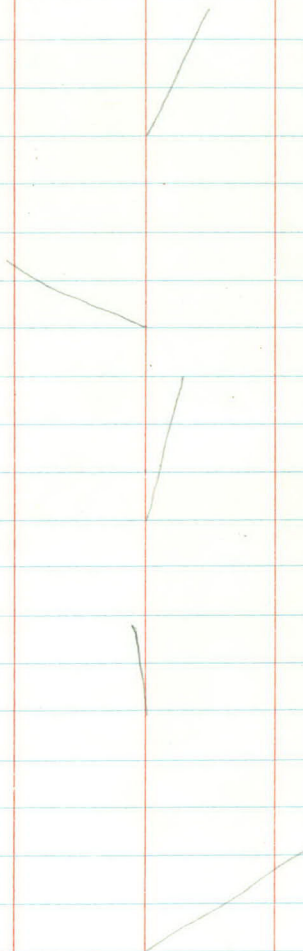
S 63° 44' E

0100	Intersection of Rice Creek & Ditch #1				
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N 17° 30' W.



Sta	Pl.	Angle		Bearing	
		Lt.	Rt.	Mag.	Calc.
917.00	P.I.			553° E	552° 47' E
26 + 99.80	P.I.		19° 16' Rt.		
533.00				572° 15' E	573° 03' E
26 + 46.50	P.I.	68° 36' Lt.			
684.00				53° 45' E	54° 27' E
19 + 62.00	P.I.		2° 35' Rt.		
1078.00				56° 30' E	570° E
7 + 33.95	P.I.	0° 19' Lt.			
558.5	P.O.T. -	Lexington		58° 50' E	56° 43' E
8 + 48.10	P.I.		47° 07' Rt.		
				554° 50' E	553° 50' E



Sta	Pt	Angle Lt Rt	Bearing Mag Calc
50+87.3	P.I.	21°38' Lt.	56°15'E 512°15'E
10465			
49+82.65	P.I.	63°09' Rt	571°15'E 575°24'E
4940			
49+33.25	P.I.	40°33' Lt.	532°15'E 534°51'E
49.5			
45+78.50	P.I.	6°59' Rt.	536°15'E 541°56'E
46			
45+32.50	P.I.	16°17' Rt.	552°30'E 558°07'E
905 W			
36+26.80	P.I.	0°40'	553° E 558°47'E
31+83.20	P.O.T.		

1

2

3

4

5

6

Sta.	Pt.	Angle Lt. Rt.	Bearing Mag Calc
------	-----	------------------	---------------------

62+79.80	P.I.		
----------	------	--	--

860
Stadia

(over Conduit)
S 23° E

S 36° 32' E

54+19.80	P.I.		
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65° 48' R.I.

(Over Conduit)
N 72° 15' E

N 77° 40' E

15.30

54+04.50	P.I.		
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68° 27' L.I.

S 28° 15' E

S 33° 53' E

31 7.20

50+87.30	P.I.		
----------	------	--	--

21° 38' L.I.

S 6° 15' E

S 12° 15' E

Traverse from

Sta. 54+19.80 to Lexington,
to Culvert - into swamp

Bearing

△ B.S F S Inc. Angle Dist. Mag Calc.

Mon
(Lex- I)

C

599.66

N 85° E

179° 45' 30"

N 79° 29' 30" E

B

273.21

N 84° 30' E

177° 11' 30"

N 79° 15' E

C

A

751.07

N 80° 45' E

179° 54'

N 76° 26' 30" E

B

54+19.8

435.11

N 80° 45' E

180° 23' 30"

N 76° 26' 30" E

A

62+79.8

444.00

589° 30' E

66° 44'

N 76° 24' E

54+19.80

62+79.8

536.50

536.50



62+798

86° 0' 0"
66° 44' 1"
36° 03' 2"
5

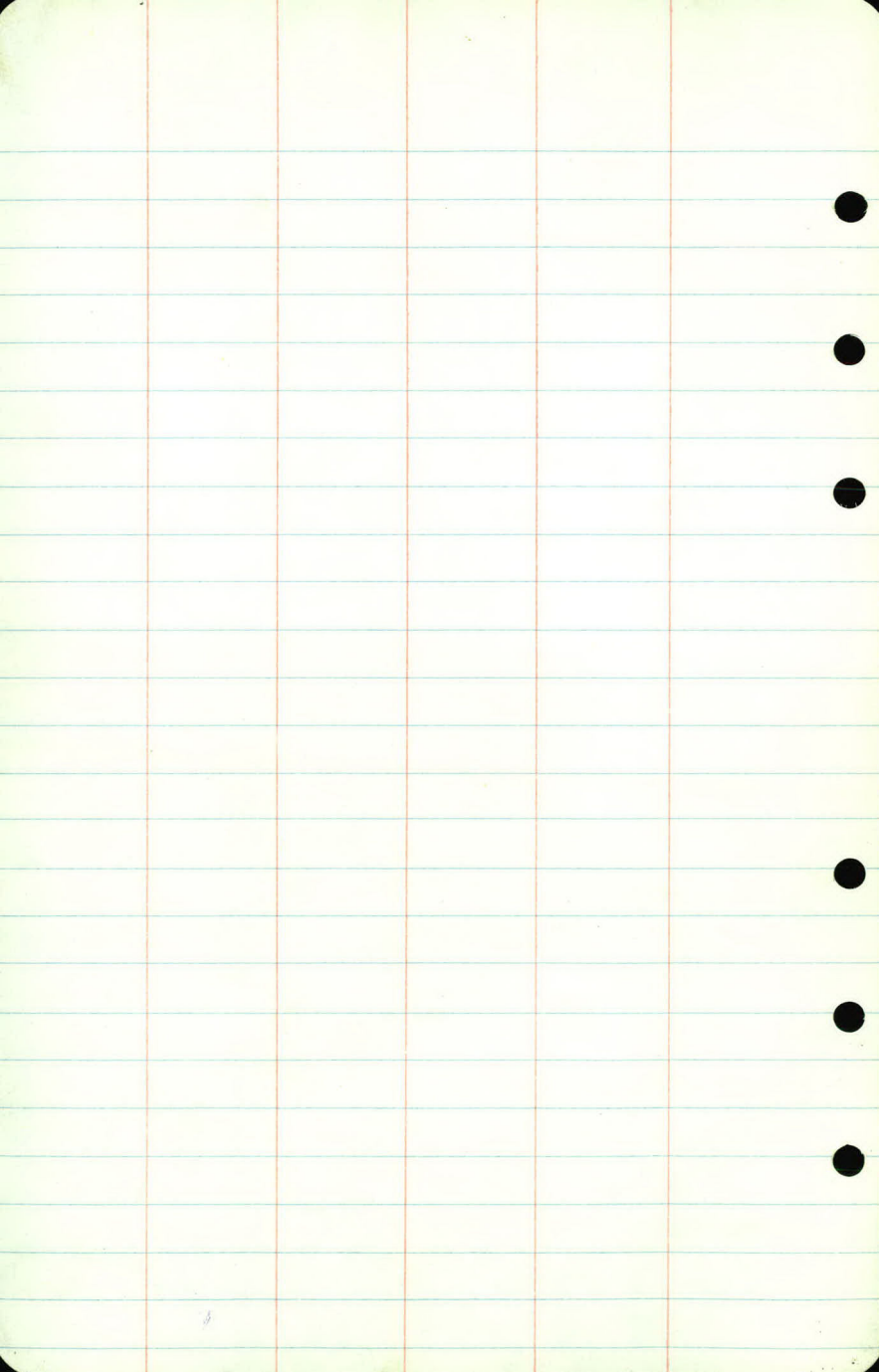
Δ	B. S	F. S	Inc Angle	Dist	Bearing Mag Calc.
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		62+79.8			
E	Mon-Lex I		83°55'30"		58°W
					582°17'W
		E (rail over culvert on sec. line)			
D	Mon-Lex I		93°17'	955.70	58°36'E
					513°27'30"E

855555

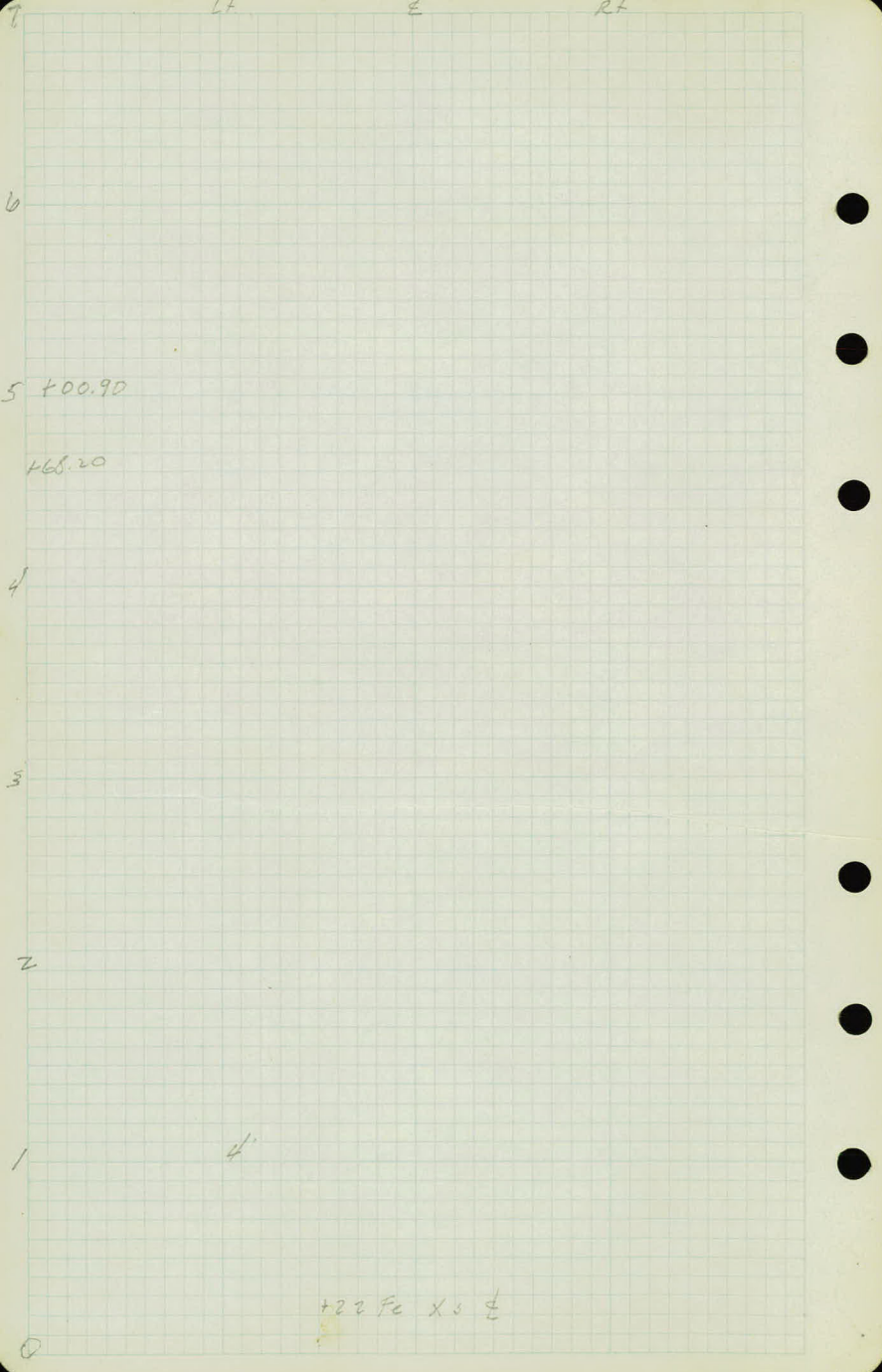
Rec Line - Lex.
E

93° 17'



TOPOGRAPHY

DITCH # 1



+ 88.3 End 30° x 160M-1.5'
172.3 End 30° x 160M3

3

3

3

5

6

5

4'



+ 15.4' Will 05'

104 L 5 E Rt.

13 5

2 6

11 6

10 7

124 5

9 5

+ 75 shldr xs d
+ 50 shldr xs d
+ 36 Fo xs d

8 3

7 0

178 End 41" C.M. 4

LEXINGTON AVE

+ 48 End 41" C.M. 3

+ 13 End 41" C.M. 3



21 12

20 7

+62 6

19 5

18 5

17 6

16 5

15 5

14 5

+60 Bush 3

+20 Bush 3

172 Twin Birch 5

+73 Ditch Rd.

129 Ditch Rd.

28		9
27	146.50	7
	35	
26	34	
25	29	
24	24	
23	20	
22	16	
21	12	

100 3 Pops 4
180 Twin Pop 4

+50 5 Pops 5
+30 2 Pops 5
+20 3 Pops 5

+99 4" Pop 5

+15 4 Pops 5

+87 2 Pops 5

+71 3 Pops 5
+64 Pop 4

+45 Pop 3
+23 8 Pops 4
+06 4 Birch 4
+00 3 Birch 4
+90 3 Pops 5
+75 4 Pops 4
+70 Pop 4

+00 2 Birch 4

+70 2 Pops 5

+55 3 Pop 5
+40 2 Pops 4

+20 3 Birch 4

+100 4 Pops 4

+45 Pop 4

+50 Pop 4

+20 Triple 7
+10 Triple 5

+12 2 Pops -6
+00 Pop 5

+88 Triple 5

+85 Triple 4
+70 Pop 3

+05 3 Pops 7

+35 3" Pop 5
+25 3" Pop 6

+02 Stamp 2

35

6

34

6

33

6

32

102 End 24" x 28" 7
 + 88, Abandoned Ed Xs 2
 + 74 End 24" x 28" 7
8

+ 74

31

7

30

8

29

7

+ 85 Fe Lin. Xs 2

28

8

Abandoned

Roadway

+00 End 24" x 26" 1/4 3'

+74 End 24" x 26" 7/16 3'

x x x x

+50 2 Stumps 5'

20

42

4

41

3

40

2

39

0

38

 $+36Fe \times 5 \frac{1}{2} +$

2

37

4

+26.80

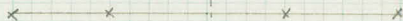
6

36

6

35

6



+28 4 Birch 10'

+10	3 Birch	10
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478	Pop	10'
479	42.5	5'

+70 4 Pops 5

+ 50 clump with 10

+30 6 Amps with
+40 5 Pops 8.0

415	Elop	7
406	Birch	8

Feb	Birch	Q
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49

1

48

1

47

3

46

4

+78.5 ± 6'

+79 End 30" x 20' C.M.
 +70 ± Field Est. XS ±
 +59 End 30" x 20' C.M.

+32.5 6'

45

9

44

7

43

6

42

4

Field

Ent.

+22 2 Pops 6"

+15 - 4 Pops 6

+94 - 8 Pops 8

+83 - 2 Pops 7

+75 - 6 Pops 7

+50 - 4 Pops 8

+40 - 6 pops - 8

56

55

+34 FL. 48" x 28" C.M. 7' + 34
(Siphon)

54 +93.
+84

8'
8'

+93 FL. 48" x 28" C.M.
(Siphon)

53

7'

52

7'

51

+87.30

7'

9'

50

+82.65 ± 7'

7'

+87 End 30" C.M.
+75 Shldr x 3 E
Narrow line

+43 Shldr x 3 d
+33.25 End 30" C.M. +33.25 - ± 4'

49

1'

HAMLIN

AVE.

7' + 19.80

62

61

60

59

58

57

56

COUNTY DITCH #1

Bench Levels

P.I.	+	π	-	Elev.
B.M.	5.10	897.68		892.58
T.P.	9.02	904.59	2.11	895.57
	3.37	904.41	3.55	901.04
	1.92	900.23	6.10	898.31
	6.81	900.96	6.08	894.15
	9.81	905.83	4.94	896.02
	3.58	901.61	7.80	898.03
T.P.	4.48	904.36	1.73	899.88
	7.15	911.13	0.38	903.98
	4.68	910.63	5.18	905.95
	0.41	900.38	10.66	899.97
	3.34	893.52	10.20	890.18
	3.50	893.36	3.66	889.86
	5.55	891.47	7.44	885.92
	5.17	891.13	5.51	885.96
B.M.			5.90	885.23

Top Mon. Lexington & I.

Spk. Fc. B.

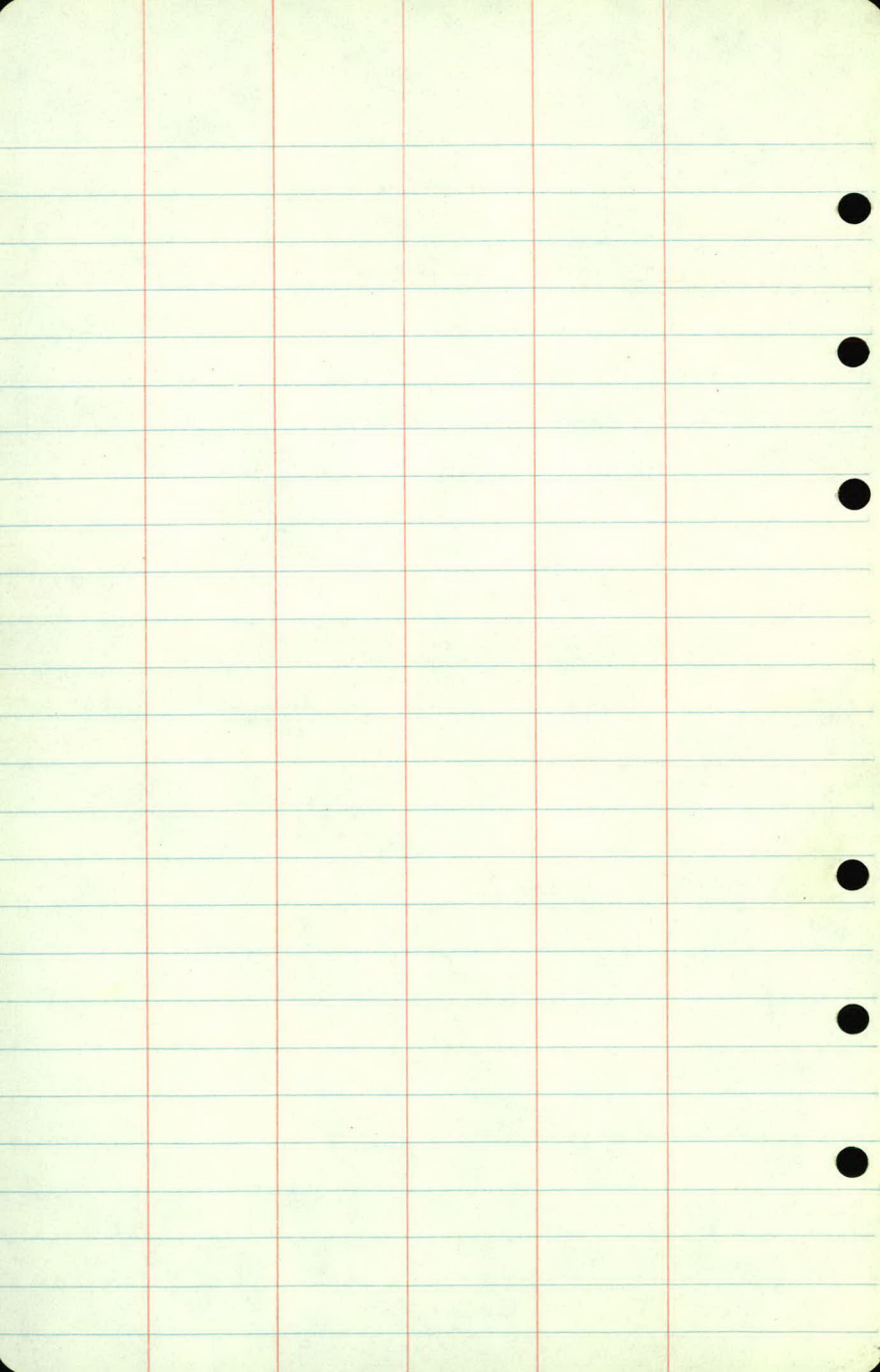
Spk in Cap. S.E. Cor Bridge

Sta	+	π	-	Elev
B.M	5.90	891.13		885.23
	5.23	891.26	5.10	886.03
	7.99	893.84	5.41	885.85
	4.00	893.71	4.13	889.71
	10.52	900.69	3.54	890.17
	10.08	910.37	0.40	900.29
	5.20	911.00	4.57	905.80
	1.70	904.30	8.40	902.60
T.P	4.42	904.30	4.42	899.88
	4.03	902.18	6.15	898.15
	9.89	906.12	5.95	896.23
	4.69	901.00	9.81	896.31
	5.85	900.27	6.58	894.42
	6.45	904.97	1.75	898.52
	1.60	902.86	3.71	901.26
B.M.			10.27	892.59
				892.58

Spk. in. Cap S.E. Cor Bridge

Spk in Fe. Post.

Top of Mont Lexx Co Pd⁺I⁺



CROSS SECTIONS

Ditch #1

Sta.	+	π	-	Elev.
B.M.	3.02	888.25		885.23
Highwater Mark on Bridge Under Lexington				
0+00			11.8	76.5
+47			11.0	77.3
1			10.8	77.5
2			10.1	78.2
T.P.	5.51	887.81	5.95	882.30
3			9.0	78.8
4			8.8	79.0
+68.20			8.6	79.2
5+00.90			8.5	79.3
6			7.9	79.9
+72.3			8.10	79.71
7			7.3	80.5
T.P.	7.62	889.83	5.60	882.21

Spike Cap S.E. Cor Bridge
(10-4-1940)- 7.84 (880.41)

$$\frac{11.8}{10} \quad 11.8 \quad \frac{11.8}{10}$$

$$\frac{56}{26} \quad \frac{5.9}{14} \quad \frac{7.2}{10} \quad \frac{9.6}{7} \quad 11.0 \quad \frac{10.9}{2} \quad \frac{7.2}{6} \quad \frac{7.7}{18}$$

$$\frac{7.1}{23} \quad \frac{6.8}{10} \quad \frac{8.1}{5} \quad \frac{10.8}{2} \quad 10.8 \quad \frac{10.5}{2} \quad \frac{6.3}{4} \quad \frac{6.4}{12} \quad \frac{6.1}{22}$$

$$\frac{7.2}{19} \quad \frac{7.4}{6} \quad \frac{8.6}{2} \quad \frac{9.9}{1} \quad 10.1 \quad \frac{10.2}{1} \quad \frac{8.1}{5} \quad \frac{7.2}{6} \quad \frac{7.2}{13} \quad \frac{7.1}{20}$$

$$\frac{6.4}{23} \quad \frac{6.4}{8} \quad \frac{7.3}{2} \quad 9.0 \quad \frac{8.6}{2} \quad \frac{7.3}{6} \quad \frac{6.6}{10} \quad \frac{6.5}{20}$$

$$\frac{6.7}{20} \quad \frac{7.0}{10} \quad \frac{7.7}{2} \quad \frac{8.6}{1} \quad 8.8 \quad \frac{8.6}{1} \quad \frac{7.7}{2} \quad \frac{6.7}{5} \quad \frac{6.3}{15} \quad \frac{6.3}{20}$$

$$\frac{6.9}{20} \quad \frac{6.6}{14} \quad \frac{7.2}{2} \quad \frac{8.5}{1} \quad 8.6 \quad \frac{8.5}{1} \quad \frac{7.7}{3} \quad \frac{5.5}{9} \quad \frac{5.4}{20}$$

$$\frac{5.7}{26} \quad \frac{6.5}{14} \quad \frac{6.8}{9} \quad \frac{7.0}{2} \quad \frac{8.5}{1} \quad 8.5 \quad \frac{8.3}{1} \quad \frac{7.0}{2} \quad \frac{5.7}{13} \quad \frac{6.3}{21}$$

$$\frac{6.6}{20} \quad \frac{6.6}{7} \quad \frac{6.6}{2} \quad \frac{7.7}{1} \quad 7.9 \quad \frac{7.8}{1} \quad \frac{6.7}{2} \quad \frac{5.7}{20}$$

$$\frac{5.3}{23} \quad \frac{5.0}{7} \quad \frac{6.3}{1} \quad \frac{6.6}{8} \quad \frac{6.7}{10} \quad \frac{5.9}{2} \quad \frac{4.4}{10} \quad \frac{4.1}{20}$$

$$5. FL \\ 9.06 \quad 78.75$$

$$\frac{5.9}{20} \quad \frac{7.3}{9} \quad 7.3 \quad \frac{6.7}{12} \quad \frac{4.9}{14} \quad \frac{3.4}{18} \quad \frac{3.4}{20}$$

Sta.		π	-	Elev.
		889.83		
8			9.1	80.4
	+48		10.66	79.17
	+60	$\pm$ Lex.	3.9	85.9
	+78		10.39	79.44
9			9.3	80.5
	+54		9.4	80.4
10			9.5	80.3
11			9.3	80.5
12			9.2	80.6
T.P.	7.55	891.75	5.63	884.20
13			10.9	80.9
14			11.1	80.7

$$\begin{array}{r} 6.9 \\ 20 \end{array} \quad \begin{array}{r} 7.1 \\ 11 \end{array} \quad \begin{array}{r} 8.3 \\ 4 \end{array} \quad \begin{array}{r} 9.2 \\ 2 \end{array} \quad 9.4 \quad \begin{array}{r} 9.5 \\ 2 \end{array} \quad \begin{array}{r} 6.8 \\ 3 \end{array} \quad \begin{array}{r} 8.2 \\ 5 \end{array} \quad \begin{array}{r} 7.3 \\ 8 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array}$$

84.66

$$\begin{array}{r} 6.9 \\ 20 \end{array} \quad \begin{array}{r} 7.0 \\ 6 \end{array} \quad \begin{array}{r} 8.0 \\ 4 \end{array} \quad \begin{array}{r} 9.3 \\ 2 \end{array} \quad \begin{array}{r} 9.8 \\ 00 \end{array} \quad (F.L.) \quad \begin{array}{r} 5.17 \\ 10.66 \end{array} \quad \text{Handwall} \quad \begin{array}{r} 5.0 \\ 3 \end{array} \quad \begin{array}{r} 5.2 \\ 5 \end{array} \quad \begin{array}{r} 4.0 \\ 17 \end{array} \quad \begin{array}{r} 3.8 \\ 25 \end{array}$$

3.9

$$\begin{array}{r} 6.2 \\ 18 \end{array} \quad \begin{array}{r} 6.9 \\ 4 \end{array} \quad \begin{array}{r} 9.0 \\ 1 \end{array} \quad \begin{array}{r} 9.2 \\ 00 \end{array} \quad F.L. \quad \begin{array}{r} 9.0 \\ 10.39 \end{array} \quad \begin{array}{r} 7.2 \\ 2 \end{array} \quad \begin{array}{r} 6.4 \\ 4 \end{array} \quad \begin{array}{r} 5.6 \\ 9 \end{array} \quad \begin{array}{r} 5.8 \\ 16 \end{array} \quad \begin{array}{r} 5.8 \\ 20 \end{array}$$

$$\begin{array}{r} 7.1 \\ 20 \end{array} \quad \begin{array}{r} 6.6 \\ 6 \end{array} \quad \begin{array}{r} 8.2 \\ 3 \end{array} \quad \begin{array}{r} 9.4 \\ 2 \end{array} \quad 9.3 \quad \begin{array}{r} 8.9 \\ 7 \end{array} \quad \begin{array}{r} 6.8 \\ 5 \end{array} \quad \begin{array}{r} 6.4 \\ 23 \end{array}$$

$$\begin{array}{r} 7.4 \\ 20 \end{array} \quad \begin{array}{r} 7.1 \\ 6 \end{array} \quad \begin{array}{r} 8.2 \\ 3 \end{array} \quad \begin{array}{r} 9.6 \\ 2 \end{array} \quad 9.4 \quad \begin{array}{r} 9.2 \\ 4 \end{array} \quad \begin{array}{r} 6.9 \\ 5 \end{array} \quad \begin{array}{r} 6.7 \\ 20 \end{array}$$

$$\begin{array}{r} 7.4 \\ 20 \end{array} \quad \begin{array}{r} 7.4 \\ 3 \end{array} \quad \begin{array}{r} 9.3 \\ 1 \end{array} \quad 9.5 \quad \begin{array}{r} 9.1 \\ 4 \end{array} \quad \begin{array}{r} 7.5 \\ 6 \end{array} \quad \begin{array}{r} 7.0 \\ 7 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array}$$

$$\begin{array}{r} 7.7 \\ 20 \end{array} \quad \begin{array}{r} 7.7 \\ 3 \end{array} \quad \begin{array}{r} 9.3 \\ 2 \end{array} \quad 9.3 \quad \begin{array}{r} 9.1 \\ 3 \end{array} \quad \begin{array}{r} 7.6 \\ 5 \end{array} \quad \begin{array}{r} 7.2 \\ 7 \end{array} \quad \begin{array}{r} 7.2 \\ 20 \end{array}$$

$$\begin{array}{r} 7.5 \\ 20 \end{array} \quad \begin{array}{r} 7.2 \\ 4 \end{array} \quad \begin{array}{r} 9.1 \\ 2 \end{array} \quad 9.2 \quad \begin{array}{r} 9.1 \\ 3 \end{array} \quad \begin{array}{r} 7.5 \\ 4 \end{array} \quad \begin{array}{r} 7.0 \\ 20 \end{array}$$

$$\begin{array}{r} 9.3 \\ 20 \end{array} \quad \begin{array}{r} 9.5 \\ 4 \end{array} \quad \begin{array}{r} 11.3 \\ 3 \end{array} \quad 10.7 \quad \begin{array}{r} 11.2 \\ 2 \end{array} \quad \begin{array}{r} 9.3 \\ 4 \end{array} \quad \begin{array}{r} 9.0 \\ 20 \end{array}$$

$$\begin{array}{r} 8.9 \\ 20 \end{array} \quad \begin{array}{r} 8.6 \\ 6 \end{array} \quad \begin{array}{r} 10.9 \\ 3 \end{array} \quad 11.1 \quad \begin{array}{r} 11.2 \\ 2 \end{array} \quad \begin{array}{r} 9.8 \\ 3 \end{array} \quad \begin{array}{r} 8.5 \\ 4 \end{array} \quad \begin{array}{r} 8.4 \\ 20 \end{array}$$

Sta	+	π	-	Elev
		891.75		
15			11.1	80.7
+29	Profile	Ditch Rt.	11.4	80.4
16			10.8	81.0
17			10.8	81.0
18			10.8	81.0
T.P.	7.30	893.53	5.52	886.23
+73	Profile	Ditch Rt.	12.3	81.2
19			12.2	81.3
+62			12.4	81.1
20			12.3	81.2
21			11.7	81.8
T.P.	3.42	889.49	7.46	886.07
22			8.0	81.5
23			7.8	81.7
T.P.	6.32	892.94	2.87	886.62

$$\begin{array}{r} 9.9 \\ 20 \end{array} \quad \begin{array}{r} 9.0 \\ 5 \end{array} \quad \begin{array}{r} 10.8 \\ 3 \end{array} \quad 11.1 \quad \begin{array}{r} 10.8 \\ 2 \end{array} \quad \begin{array}{r} 8.3 \\ 4 \end{array} \quad \begin{array}{r} 8.6 \\ 20 \end{array}$$

$$\begin{array}{r} 10.5 \\ 114 \end{array} \quad \begin{array}{r} 10.2 \\ 2 \end{array} \quad \begin{array}{r} 10.4 \\ 5 \end{array} \quad \begin{array}{r} 9.8 \\ 14 \end{array} \quad \begin{array}{r} 9.4 \\ 29 \end{array} \quad \begin{array}{r} 9.2 \\ 50 \end{array} \quad \begin{array}{r} 8.7 \\ 100 \end{array} \quad \begin{array}{r} 7.3 \\ 150 \end{array} \quad \begin{array}{r} 7.2 \\ 190 \end{array}$$

$$\begin{array}{r} 9.4 \\ 20 \end{array} \quad \begin{array}{r} 8.9 \\ 5 \end{array} \quad \begin{array}{r} 10.5 \\ 2 \end{array} \quad 10.8 \quad \begin{array}{r} 10.3 \\ 3 \end{array} \quad \begin{array}{r} 8.5 \\ 5 \end{array} \quad \begin{array}{r} 8.4 \\ 26 \end{array}$$

$$\begin{array}{r} 8.8 \\ 20 \end{array} \quad \begin{array}{r} 9.2 \\ 3 \end{array} \quad \begin{array}{r} 10.5 \\ 2 \end{array} \quad 10.8 \quad \begin{array}{r} 10.4 \\ 2 \end{array} \quad \begin{array}{r} 9.0 \\ 4 \end{array} \quad \begin{array}{r} 8.9 \\ 20 \end{array}$$

$$\begin{array}{r} 8.5 \\ 20 \end{array} \quad \begin{array}{r} 7.9 \\ 7 \end{array} \quad \begin{array}{r} 10.5 \\ 2 \end{array} \quad 10.8 \quad \begin{array}{r} 10.7 \\ 2 \end{array} \quad \begin{array}{r} 8.5 \\ 4 \end{array} \quad \begin{array}{r} 9.4 \\ 20 \end{array}$$

$$\begin{array}{r} 11.7 \\ 123 \end{array} \quad \begin{array}{r} 10.9 \\ 4 \end{array} \quad \begin{array}{r} 9.7 \\ 50 \end{array} \quad \begin{array}{r} 9.0 \\ 100 \end{array} \quad \begin{array}{r} 7.2 \\ 150 \end{array} \quad \begin{array}{r} 7.2 \\ 200 \end{array}$$

$$\begin{array}{r} 9.8 \\ 20 \end{array} \quad \begin{array}{r} 9.9 \\ 6 \end{array} \quad \begin{array}{r} 12.0 \\ 2 \end{array} \quad 12.2 \quad \begin{array}{r} 12.6 \\ 2 \end{array} \quad \begin{array}{r} 10.3 \\ 4 \end{array} \quad \begin{array}{r} 10.5 \\ 20 \end{array}$$

$$\begin{array}{r} 9.6 \\ 20 \end{array} \quad \begin{array}{r} 9.3 \\ 5 \end{array} \quad \begin{array}{r} 11.9 \\ 1 \end{array} \quad 12.4 \quad \begin{array}{r} 11.8 \\ 3 \end{array} \quad \begin{array}{r} 10.1 \\ 6 \end{array} \quad \begin{array}{r} 10.7 \\ 20 \end{array}$$

$$\begin{array}{r} 9.6 \\ 20 \end{array} \quad \begin{array}{r} 9.2 \\ 6 \end{array} \quad \begin{array}{r} 11.7 \\ 3 \end{array} \quad 12.3 \quad \begin{array}{r} 11.9 \\ 2 \end{array} \quad \begin{array}{r} 10.1 \\ 4 \end{array} \quad \begin{array}{r} 10.7 \\ 20 \end{array}$$

$$\begin{array}{r} 9.6 \\ 20 \end{array} \quad \begin{array}{r} 10.3 \\ 4 \end{array} \quad \begin{array}{r} 11.9 \\ 3 \end{array} \quad 11.7 \quad \begin{array}{r} 11.4 \\ 3 \end{array} \quad \begin{array}{r} 10.0 \\ 6 \end{array} \quad \begin{array}{r} 9.6 \\ 20 \end{array}$$

$$\begin{array}{r} 5.4 \\ 20 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 4.5 \\ 10 \end{array} \quad \begin{array}{r} 5.6 \\ 5 \end{array} \quad \begin{array}{r} 7.5 \\ 2 \end{array} \quad 8.0 \quad \begin{array}{r} 7.5 \\ 3 \end{array} \quad \begin{array}{r} 5.3 \\ 6 \end{array} \quad \begin{array}{r} 4.6 \\ 11 \end{array} \quad \begin{array}{r} 5.4 \\ 20 \end{array}$$

$$\begin{array}{r} 4.4 \\ 20 \end{array} \quad \begin{array}{r} 4.7 \\ 8 \end{array} \quad \begin{array}{r} 5.7 \\ 5 \end{array} \quad \begin{array}{r} 7.5 \\ 3 \end{array} \quad 7.8 \quad \begin{array}{r} 6.7 \\ 4 \end{array} \quad \begin{array}{r} 4.2 \\ 10 \end{array} \quad \begin{array}{r} 5.0 \\ 14 \end{array} \quad \begin{array}{r} 5.7 \\ 20 \end{array}$$

Top Fc Post Lt St 24

Sta		Δ	-	Elev.
		892.94		
24			11.0	81.9
25			11.1	81.8
26			11.5	81.4
+46.50			10.9	82.0
26+99.80			11.1	81.80
28			10.2	82.7
29			10.7	82.2
30			10.1	82.8
T.P.	541	893.35	5.00	887.94
31			10.3	83.1
+74			12.42	80.93
+83			6.5	86.9
+94			6.6	86.8

8

$$\begin{array}{r} 7.5 \\ 2.5 \end{array} \quad \begin{array}{r} 7.5 \\ 11 \end{array} \quad \begin{array}{r} 8.0 \\ 6 \end{array} \quad \begin{array}{r} 10.6 \\ 3 \end{array} \quad \begin{array}{r} 10.4 \\ 11.0 \end{array} \quad \begin{array}{r} 8.2 \\ 3 \end{array} \quad \begin{array}{r} 8.7 \\ 6 \end{array} \quad \begin{array}{r} 2.5 \end{array}$$

$$\begin{array}{r} 8.8 \\ 2.5 \end{array} \quad \begin{array}{r} 8.0 \\ 8 \end{array} \quad \begin{array}{r} 8.4 \\ 5 \end{array} \quad \begin{array}{r} 10.5 \\ 3 \end{array} \quad \begin{array}{r} 10.4 \\ 11.1 \end{array} \quad \begin{array}{r} 8.8 \\ 3 \end{array} \quad \begin{array}{r} 8.7 \\ 6 \end{array} \quad \begin{array}{r} 2.5 \end{array}$$

$$\begin{array}{r} 8.9 \\ 2.5 \end{array} \quad \begin{array}{r} 7.6 \\ 9 \end{array} \quad \begin{array}{r} 8.0 \\ 5 \end{array} \quad \begin{array}{r} 10.5 \\ 2 \end{array} \quad \begin{array}{r} 10.1 \\ 11.5 \end{array} \quad \begin{array}{r} 8.1 \\ 4 \end{array} \quad \begin{array}{r} 8.5 \\ 8 \end{array} \quad \begin{array}{r} 9.6 \\ 14 \end{array} \quad \begin{array}{r} 2.0 \end{array}$$

$$\begin{array}{r} 9.2 \\ 2.5 \end{array} \quad \begin{array}{r} 9.0 \\ 5 \end{array} \quad \begin{array}{r} 10.0 \\ 3 \end{array} \quad \begin{array}{r} 10.9 \\ 10.9 \end{array} \quad \begin{array}{r} 11.0 \\ 3 \end{array} \quad \begin{array}{r} 8.4 \\ 6 \end{array} \quad \begin{array}{r} 9.0 \\ 13 \end{array} \quad \begin{array}{r} 9.0 \\ 2.5 \end{array}$$

$$\begin{array}{r} 9.0 \\ 2.5 \end{array} \quad \begin{array}{r} 9.2 \\ 6 \end{array} \quad \begin{array}{r} 10.2 \\ 4 \end{array} \quad \begin{array}{r} 10.3 \\ 11.1 \end{array} \quad \begin{array}{r} 8.4 \\ 3 \end{array} \quad \begin{array}{r} 9.5 \\ 6 \end{array} \quad \begin{array}{r} 2.5 \end{array}$$

$$\begin{array}{r} 8.6 \\ 2.5 \end{array} \quad \begin{array}{r} 8.7 \\ 5 \end{array} \quad \begin{array}{r} 9.8 \\ 3 \end{array} \quad \begin{array}{r} 9.8 \\ 10.2 \end{array} \quad \begin{array}{r} 7.7 \\ 4 \end{array} \quad \begin{array}{r} 8.2 \\ 9 \end{array} \quad \begin{array}{r} 8.8 \\ 16 \end{array} \quad \begin{array}{r} 2.5 \end{array}$$

$$\begin{array}{r} 8.5 \\ 2.5 \end{array} \quad \begin{array}{r} 8.9 \\ 4 \end{array} \quad \begin{array}{r} 10.1 \\ 2 \end{array} \quad \begin{array}{r} 10.7 \\ 10.7 \end{array} \quad \begin{array}{r} 10.0 \\ 6 \end{array} \quad \begin{array}{r} 8.6 \\ 7 \end{array} \quad \begin{array}{r} 9.0 \\ 2.5 \end{array}$$

$$\begin{array}{r} 7.9 \\ 2.5 \end{array} \quad \begin{array}{r} 8.2 \\ 8 \end{array} \quad \begin{array}{r} 9.1 \\ 4 \end{array} \quad \begin{array}{r} 9.7 \\ 2 \end{array} \quad \begin{array}{r} 10.1 \\ 10.1 \end{array} \quad \begin{array}{r} 9.6 \\ 3 \end{array} \quad \begin{array}{r} 7.7 \\ 8 \end{array} \quad \begin{array}{r} 8.2 \\ 15 \end{array} \quad \begin{array}{r} 8.6 \\ 2.5 \end{array}$$

$$\begin{array}{r} 7.3 \\ 2.5 \end{array} \quad \begin{array}{r} 7.4 \\ 11 \end{array} \quad \begin{array}{r} 8.7 \\ 7 \end{array} \quad \begin{array}{r} 10.1 \\ 2 \end{array} \quad \begin{array}{r} 10.3 \\ 10.3 \end{array} \quad \begin{array}{r} 9.6 \\ 1 \end{array} \quad \begin{array}{r} 8.1 \\ 2 \end{array} \quad \begin{array}{r} 8.7 \\ 6 \end{array} \quad \begin{array}{r} 2.5 \end{array}$$

80.93

$$\begin{array}{r} 6.9 \\ 2.5 \end{array} \quad \begin{array}{r} 7.5 \\ 14 \end{array} \quad \begin{array}{r} 10.2 \\ 5 \end{array} \quad \begin{array}{r} 10.4 \\ 0 \end{array} \quad \left(\begin{array}{r} FL. \\ 12.42 \end{array} \right) \quad \left(\begin{array}{r} FL. \\ 3 \end{array} \right) \quad \begin{array}{r} 9.7 \\ 4 \end{array} \quad \begin{array}{r} 9.0 \\ 8 \end{array} \quad \begin{array}{r} 8.3 \\ 20 \end{array} \quad \begin{array}{r} 7.6 \\ 2.5 \end{array}$$

sta.	L	π	-	ele
		893.35		
32			10.1	83.3
33			10.6	82.8
34			10.9	82.5
35			11.2	82.2
36			10.9	82.5
+26.80			10.6	82.8
37			11.2	82.2
38			10.7	82.7
13.14	9.37	896.60	6.12	887.23
39			14.3	82.3
40			14.3	82.3
41			14.2	82.4
42			13.9	82.7

80.96

$$\begin{array}{r} 6.6 \quad 7.6 \quad 10.2 \quad 10.1 \\ 25 \quad 5 \quad 3 \quad 0 \end{array} \quad \begin{array}{r} 8.6 \\ 1239 \end{array} \quad \begin{array}{r} FL \\ 1246 \\ 3 \end{array} \quad \begin{array}{r} 10.3 \quad 8.2 \quad 7.7 \\ 4 \quad 6 \quad 25 \end{array}$$

$$\begin{array}{r} 8.1 \quad 8.1 \quad 9.0 \quad 10.7 \\ 26 \quad 6 \quad 3 \quad 2 \end{array} \quad \begin{array}{r} 10.3 \quad 9.1 \quad 8.0 \quad 7.5 \\ 10.6 \quad 3 \quad 4 \quad 7 \end{array} \quad \begin{array}{r} 25 \end{array}$$

$$\begin{array}{r} 7.5 \quad 7.6 \quad 8.0 \quad 8.9 \quad 10.1 \\ 25 \quad 9 \quad 6 \quad 3 \quad 2 \end{array} \quad \begin{array}{r} 10.9 \quad 9.9 \quad 8.9 \quad 8.2 \quad 7.9 \\ 2 \quad 4 \quad 8 \quad 25 \end{array}$$

$$\begin{array}{r} 7.7 \quad 7.5 \quad 8.5 \quad 8.9 \quad 10.2 \\ 25 \quad 16 \quad 6 \quad 4 \quad 2 \end{array} \quad \begin{array}{r} 11.2 \quad 10.2 \quad 8.9 \quad 7.5 \quad 7.7 \quad 7.7 \\ 2 \quad 4 \quad 7 \quad 25 \end{array}$$

$$\begin{array}{r} 7.1 \quad 7.0 \quad 8.1 \quad 8.6 \quad 10.2 \\ 25 \quad 16 \quad 13 \quad 5 \quad 2 \end{array} \quad \begin{array}{r} 10.9 \quad 10.5 \quad 8.1 \quad 7.7 \\ 2 \quad 6 \quad 25 \end{array}$$

$$\begin{array}{r} 7.0 \quad 6.7 \quad 8.0 \quad 7.1 \quad 10.1 \\ 25 \quad 18 \quad 13 \quad 3 \quad 2 \end{array} \quad \begin{array}{r} 10.6 \quad 9.8 \quad 7.9 \quad 7.5 \\ 2 \quad 4 \quad 25 \end{array}$$

$$\begin{array}{r} 6.9 \quad 7.5 \quad 9.3 \quad 9.3 \quad 11.0 \\ 25 \quad 8 \quad 7 \quad 2 \quad 1 \end{array} \quad \begin{array}{r} 11.2 \quad 10.0 \quad 8.2 \quad 7.7 \\ 2 \quad 4 \quad 25 \end{array}$$

$$\begin{array}{r} 7.2 \quad 7.1 \quad 8.3 \quad 9.0 \quad 10.4 \\ 25 \quad 19 \quad 7 \quad 6 \quad 2 \end{array} \quad \begin{array}{r} 10.7 \quad 10.0 \quad 8.6 \quad 8.1 \\ 1 \quad 3 \quad 25 \end{array}$$

Spike Fe. Po 10.4 38 + 34

$$\begin{array}{r} 11.2 \quad 11.0 \quad 11.5 \quad 13.5 \\ 25 \quad 14 \quad 4 \quad 2 \end{array} \quad \begin{array}{r} 14.3 \quad 13.6 \quad 11.4 \quad 11.2 \\ 3 \quad 2 \quad 4 \quad 25 \end{array}$$

$$\begin{array}{r} 10.3 \quad 11.3 \quad 11.0 \quad 12.8 \\ 25 \quad 13 \quad 6 \quad 2 \end{array} \quad \begin{array}{r} 14.3 \quad 13.8 \quad 11.3 \quad 11.0 \quad 11.3 \\ 1 \quad 3 \quad 14 \quad 25 \end{array}$$

$$\begin{array}{r} 9.9 \quad 10.6 \quad 13.2 \\ 25 \quad 8 \quad 3 \end{array} \quad \begin{array}{r} 14.2 \quad 13.6 \quad 10.5 \quad 10.6 \\ 1 \quad 4 \quad 25 \end{array}$$

$$\begin{array}{r} 9.8 \quad 10.0 \quad 11.8 \quad 13.0 \\ 25 \quad 8 \quad 6 \quad 2 \end{array} \quad \begin{array}{r} 13.7 \quad 12.5 \quad 10.4 \quad 10.5 \\ 3 \quad 7 \quad 25 \end{array}$$

Sta	+	π	-	Elev	
		896.60			
43			13.9	82.7	
44			14.3	82.3	
45			14.1	82.5	
+325			13.0	83.6	
+59	30" x 20' C.M.		FL. (13.60)	83.00	
+70	Field Ent		11.2	85.40	
+79	30" x 20' C.M.		FL. (14.08)	82.52	
T.P.	8.10	893.47	11.23	885.37	
46			11.1	82.4	
47			10.9	82.6	
48			11.3	82.2	
49			10.8	82.7	
+33.25	30" x 54' C.M.		FL. 10.72	82.75	Under Hand 100
+43	shldr.		4.6	88.9	
+75	shldr.		5.1	88.4	
+87	30" x 54' C.M.		FL. 9.79	83.68	

$$\frac{100}{25} \quad \frac{115}{17} \quad \frac{113}{5} \quad \frac{135}{2} \quad 13.9 \quad \frac{136}{3} \quad \frac{116}{5} \quad \frac{111}{15} \quad \frac{100}{25}$$

$$\frac{107}{25} \quad \frac{117}{12} \quad \frac{114}{4} \quad \frac{138}{2} \quad 14.3 \quad \frac{135}{3} \quad \frac{113}{4} \quad \frac{111}{17} \quad \frac{100}{25}$$

$$\frac{111}{25} \quad \frac{118}{3} \quad \frac{129}{2} \quad 14.1 \quad \frac{126}{3} \quad \frac{115}{6} \quad \frac{116}{15} \quad \frac{112}{25}$$

$$\frac{110}{25} \quad \frac{118}{13} \quad \frac{112}{4} \quad \frac{123}{3} \quad 13.0 \quad \frac{130}{2} \quad \frac{115}{4} \quad \frac{115}{15} \quad \frac{119}{25}$$

$$\frac{109}{25} \quad \frac{107}{4} \quad F.L. \quad \frac{115}{4} \quad \frac{114}{27}$$

$$\frac{109}{25} \quad \frac{114}{16} \quad \frac{117}{5} \quad \frac{124}{3} \quad F.L. \quad \frac{131}{3} \quad \frac{117}{5} \quad \frac{113}{25}$$

$$\frac{78}{25} \quad \frac{85}{10} \quad \frac{85}{7} \quad \frac{103}{3} \quad 11.1 \quad \frac{104}{2} \quad \frac{83}{4} \quad \frac{84}{13} \quad \frac{83}{25}$$

$$\frac{81}{25} \quad \frac{80}{8} \quad \frac{79}{5} \quad \frac{112}{3} \quad 10.9 \quad \frac{104}{2} \quad \frac{90}{3} \quad \frac{76}{6} \quad \frac{80}{16} \quad \frac{81}{25}$$

$$\frac{79}{25} \quad \frac{79}{19} \quad \frac{80}{4} \quad \frac{111}{3} \quad 11.3 \quad \frac{104}{3} \quad \frac{80}{6} \quad \frac{78}{19} \quad \frac{83}{25}$$

shldr

$$\frac{50}{20} \quad \frac{79}{13} \quad \frac{71}{5} \quad \frac{107}{3} \quad 10.8 \quad \frac{106}{8} \quad \frac{86}{3} \quad \frac{80}{5} \quad \frac{71}{11} \quad \frac{71}{25}$$

shldr

$$\frac{50}{14} \quad \frac{79}{2} \quad F.L. \quad \frac{76}{4} \quad \frac{87}{8} \quad \frac{87}{25}$$

Sta.	+	↑	-	Elev.
		893.47		
49 + 82.65			10.1	83.4
50			10.8	82.7
+ 87.3			11.4	82.1
51			10.9	82.6
52			10.2	83.3
53			9.8	83.7
T.P.	7.03	893.89	6.61	886.86
B.M.			1.46	892.43
Top Water at Conduit. ^{83.72} 10.17 ^N 10.32 ^{83.57}				
B.M.	1.37	893.80		
53 + 84			10.1	83.7
H. Flow Line 48" x 28' ^{C.M.} Siphon			15.70	78.10
S. F. Line 48" x 28' ^{C.M.} Siphon			17.16	76.64
+ 93			13.0	80.80
54 + 22	Top Conduit		4.68	89.12
+ 34			14.8	79.0
62 + 79.80			9.8	84.0
B.M.	4.33	896.76	1.37	892.43
T.P.	5.12	896.14	5.74	891.02

(20.00 5.40
21.34 80)

$$\begin{array}{r} 8.9 \quad 7.5 \quad 9.7 \\ 2.5 \quad 3 \quad 2 \end{array} \quad 10.2 \quad 8.5 \quad 7.0 \quad \begin{array}{r} 5.0 \\ 1.6 \end{array} \quad \text{shldr}$$

$$\begin{array}{r} 8.1 \quad 7.8 \quad 10.1 \\ 2.4 \quad 4 \quad 3 \end{array} \quad 10.2 \quad 9.1 \quad 8.0 \quad \begin{array}{r} 5.1 \\ 7.6 \end{array} \quad \text{shldr}$$

$$\begin{array}{r} 7.6 \quad 7.5 \quad 8.1 \quad 9.9 \\ 2.5 \quad 7 \quad 5 \quad 3 \end{array} \quad 11.4 \quad 10.0 \quad 8.6 \quad 7.1 \quad \begin{array}{r} 5.4 \\ 8 \quad 15 \end{array} \quad \text{shldr}$$

$$\begin{array}{r} 7.5 \quad 8.1 \quad 10.1 \\ 2.5 \quad 5 \quad 2 \end{array} \quad 10.6 \quad 8.2 \quad 8.0 \quad \begin{array}{r} 5.3 \\ 10 \quad 18 \end{array} \quad \text{shldr}$$

$$\begin{array}{r} 8.3 \quad 8.7 \quad 9.8 \\ 2.5 \quad 6 \quad 5 \end{array} \quad 10.2 \quad 7.0 \quad 9.2 \quad \begin{array}{r} 9.4 \\ 14 \quad 25 \end{array}$$

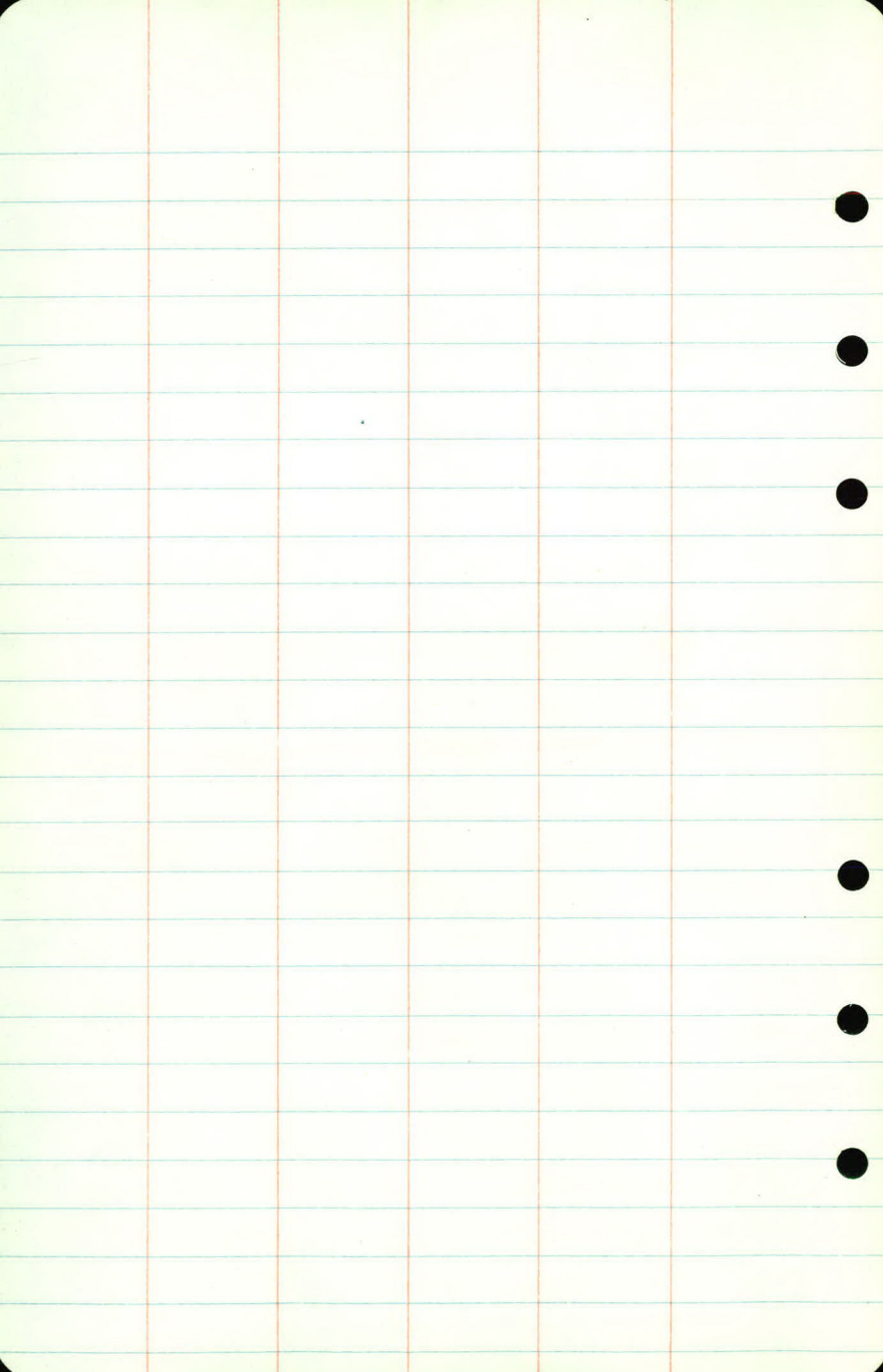
$$\begin{array}{r} 8.5 \quad 8.8 \quad 9.8 \\ 2.5 \quad 6 \quad 5 \end{array} \quad 9.8 \quad 9.1 \quad 9.5 \quad \begin{array}{r} 9.5 \\ 5 \quad 6 \quad 25 \end{array}$$

N.W. Cor M.H. on Conduit 100 Lk Sta.

$$\begin{array}{r} 9.1 \quad 8.8 \quad 10.3 \\ 2.5 \quad 12 \quad 7 \end{array} \quad 10.1 \quad 9.9 \quad 9.3 \quad \begin{array}{r} 9.2 \\ 5 \quad 8 \quad 25 \end{array}$$

Sta.	+	π	-	Elev
		896.14		
T.P.	4.77	896.03	4.88	891.26
	9.48	904.24	1.27	894.76
	3.46	905.32	2.38	901.86
B.M.			12.72	892.60
				892.58

Mon. Lexington & I



Cross Sections
from Newquist Ditch -
West - then South and into Marsden Lk.

Sta.	+	K	-	Elev.	
B.M.	2.48	895.27		892.79	
101+36					E. End F.L. 15"
0+100 = sta. 37 (Co. Rd. "I")			7.20	88.1	Newquist Ent. C.M.
101+06 +30			7.30	88.0	
100+86 +50			7.4	87.9	
100+36 1			7.6	87.7	
99+86 +50			7.8	87.5	
99+36 2			8.0	87.3	
98+86 +50			8.2	87.1	
98+36 3			8.2	87.1	
98+21 +15	FL 15" C.M.		7.80	87.47	
98+01 +35	FL 15" C.M.		7.96	87.31	
97+86 +50			8.0	87.3	
97+36 4			7.9	87.4	
96+86 +50			8.1	87.2	
96+36 5			8.0	87.3	
95+86 +50			8.2	87.1	
T.P.	4.61	894.76	5.12	890.15	
95+36 6			7.6	87.2	
94+86 +50			7.7	87.1	
94+66 +70	FL 15" C.M.		7.72	87.04	
94+36 7 + 00	FL 15" C.M.		7.65	87.11	
93+86 +50			7.8	87.0	
93+36 8	Approx PG Ditch		7.6	87.2	
92+86 +50			7.8	87.0	

Top SE. Cor Cond. M.H. 33' Lt. S₁₆ 36' (Co. Rd I)

$\frac{7.3}{25}$ $\frac{6.8}{3}$ $\frac{7.0}{20}$ $\frac{6.6}{1}$ $\frac{5.8}{3}$ $\frac{4.5}{7}$ $\frac{4.1}{20}$ $\frac{4.1}{30}$

$\frac{6.5}{25}$ $\frac{6.3}{3}$ $\frac{7.5}{2}$ $\frac{7.5}{2}$ $\frac{6.6}{3}$ $\frac{6.1}{10}$ $\frac{5.2}{13}$ $\frac{4.3}{30}$

$\frac{6.7}{25}$ $\frac{6.1}{10}$ $\frac{6.0}{6}$ $\frac{6.4}{2}$ $\frac{7.8}{2}$ $\frac{7.8}{2}$ $\frac{6.5}{3}$ $\frac{5.8}{10}$ $\frac{4.7}{15}$ $\frac{3.8}{30}$

$\frac{6.7}{25}$ $\frac{6.6}{8}$ $\frac{6.0}{4}$ $\frac{6.6}{2}$ $\frac{8.0}{2}$ $\frac{8.2}{2}$ $\frac{7.2}{3}$ $\frac{6.8}{10}$ $\frac{5.7}{14}$ $\frac{4.9}{30}$

$\frac{6.3}{25}$ $\frac{6.6}{10}$ $\frac{6.1}{7}$ $\frac{6.6}{4}$ $\frac{7.9}{3}$ $\frac{7.9}{2}$ $\frac{7.3}{3}$ $\frac{6.9}{9}$ $\frac{5.6}{14}$ $\frac{5.1}{30}$

$\frac{6.3}{25}$ $\frac{6.4}{8}$ $\frac{5.8}{6}$ $\frac{6.4}{3}$ $\frac{8.0}{2}$ $\frac{8.0}{2}$ $\frac{7.3}{5}$ $\frac{7.0}{11}$ $\frac{5.9}{15}$ $\frac{5.8}{30}$

$\frac{6.4}{25}$ $\frac{6.0}{25}$ $\frac{7.4}{2}$ $\frac{7.6}{2}$ $\frac{7.6}{3}$ $\frac{6.6}{4}$ $\frac{6.3}{10}$ $\frac{4.9}{14}$ $\frac{4.6}{30}$

$\frac{6.0}{25}$ $\frac{6.0}{9}$ $\frac{6.4}{6}$ $\frac{7.3}{3}$ $\frac{7.5}{2}$ $\frac{7.6}{2}$ $\frac{6.2}{4}$ $\frac{5.0}{7}$ $\frac{3.5}{15}$ $\frac{3.9}{30}$

$\frac{5.7}{25}$ $\frac{5.7}{2}$ $\frac{7.6}{2}$ $\frac{7.6}{2}$ $\frac{6.3}{3}$ $\frac{5.4}{8}$ $\frac{4.2}{13}$ $\frac{3.4}{30}$

Last Reading on R.H. is 4.4

Sta	+	π	-	Elev.
92+36		894.76		
9			7.9	86.9
91+86 +50			8.1	86.7
91+36				
10			8.1	86.7
90+86 +50			8.3	86.5
90+36				
11			8.3	86.5
T.P.	6.08	896.84	4.00	890.76
89+86 +50	Approx P.T. Ditch		10.3	86.5
89+36				
12			10.7	86.1
88+86 +50			10.6	86.2
88+36				
13			10.7	86.1
87+86 +50			10.5	86.3
87+36				
14			10.7	86.1
86+86 +50			10.8	86.0
86+36				
15			10.7	86.1
85+86 +50			10.6	86.2
85+36				
16			10.8	86.0
84+86 +50			10.5	86.3
84+81 +55	FL 24" C.M.		10.78	86.06
84+61 +75	FL 24" C.M.		10.74	86.10
84+36				
17			10.6	86.2
T.P.	4.86	896.97	4.73	892.11
83+86 +50			10.7	86.3
83+36				
18			11.0	86.0
82+86 +50			10.4	86.6

$$\begin{array}{r} 5.9 \ 58 \ 54 \ 57 \ 77 \\ 26 \ 8 \ 6 \ 2 \ 1 \end{array} \quad \begin{array}{r} 7.8 \ 61 \ 47 \ 45 \\ 7.9 \ 3 \ 4 \ 12 \ 25 \end{array}$$

$$\begin{array}{r} 5.8 \\ 25 \end{array} \quad \begin{array}{r} 5.4 \\ 4 \end{array} \quad \begin{array}{r} 5.8 \ 8.0 \\ 2 \ 8.1 \end{array} \quad \begin{array}{r} 8.0 \ 5.8 \ 5.0 \ 4.1 \ 4.0 \\ 2 \ 3 \ 8 \ 10 \ 25 \end{array}$$

$$\begin{array}{r} 6.0 \\ 25 \end{array} \quad \begin{array}{r} 5.3 \\ 5 \end{array} \quad \begin{array}{r} 5.9 \ 8.1 \\ 3 \ 1 \end{array} \quad \begin{array}{r} 8.1 \ 5.4 \ 4.2 \ 3.1 \\ 2 \ 3 \ 10 \ 25 \end{array}$$

$$\begin{array}{r} 9.0 \\ 25 \end{array} \quad \begin{array}{r} 8.1 \\ 6 \end{array} \quad \begin{array}{r} 9.6 \ 10.6 \\ 4 \ 2 \end{array} \quad \begin{array}{r} 10.5 \ 9.2 \ 8.3 \ 7.2 \ 5.4 \\ 2 \ 2 \ 6 \ 10 \ 30 \end{array}$$

$$\begin{array}{r} 8.3 \\ 25 \end{array} \quad \begin{array}{r} 8.5 \\ 4 \end{array} \quad \begin{array}{r} 9.2 \ 10.4 \\ 2 \ 2 \end{array} \quad \begin{array}{r} 10.6 \ 8.5 \\ 2 \ 3 \end{array} \quad \begin{array}{r} 7.0 \ 6.8 \ 5.0 \ 4.1 \\ 5 \ 9 \ 14 \ 30 \end{array}$$

$$\begin{array}{r} 7.7 \\ 25 \end{array} \quad \begin{array}{r} 8.1 \ 7.0 \\ 10 \ 5 \end{array} \quad \begin{array}{r} 8.6 \ 10.4 \\ 3 \ 2 \end{array} \quad \begin{array}{r} 10.4 \ 8.2 \\ 2 \ 3 \end{array} \quad \begin{array}{r} 6.7 \ 6.3 \ 5.9 \ 4.4 \\ 6 \ 10 \ 12 \ 30 \end{array}$$

$$\begin{array}{r} 8.3 \\ 25 \end{array} \quad \begin{array}{r} 8.7 \\ 11 \end{array} \quad \begin{array}{r} 7.7 \ 10.3 \\ 5 \ 2 \end{array} \quad \begin{array}{r} 10.4 \ 8.7 \\ 2 \ 3 \end{array} \quad \begin{array}{r} 7.2 \ 6.6 \ 5.2 \ 4.7 \\ 5 \ 8 \ 12 \ 29 \end{array}$$

$$\begin{array}{r} 8.6 \\ 25 \end{array} \quad \begin{array}{r} 8.5 \ 10.2 \\ 6 \ 3 \end{array} \quad \begin{array}{r} 10.6 \ 8.8 \\ 2 \ 3 \end{array} \quad \begin{array}{r} 7.0 \ 5.5 \ 4.7 \\ 6 \ 11 \ 28 \end{array}$$

$$\begin{array}{r} 8.5 \ 8.9 \ 8.2 \ 8.6 \ 10.4 \\ 28 \ 11 \ 6 \ 4 \ 2 \end{array} \quad \begin{array}{r} 10.6 \ 8.8 \ 6.3 \ 4.8 \ 4.5 \\ 2 \ 4 \ 8 \ 13 \ 27 \end{array}$$

$$\begin{array}{r} 8.7 \\ 28 \end{array} \quad \begin{array}{r} 8.8 \\ 10 \end{array} \quad \begin{array}{r} 7.9 \ 10.6 \\ 6 \ 2 \end{array} \quad \begin{array}{r} 10.6 \ 7.6 \ 6.3 \ 5.1 \ 4.6 \\ 2 \ 5 \ 7 \ 10 \ 26 \end{array}$$

Last Reading on R₁ is Dist to R₂.

Sta	+	π	-	Elev.
		896.97		
82+83				
18+53	FL 30" C.M.	10.94		86.03
82+72				
+64	shldr.	5.2		91.8
82+58				
+78	$\triangle$ Lexington	4.8		= 82+58
82+44				
+92	shldr	5.2		91.8
82+27				
19+09	FL 30" C.M.	10.87		86.10
B.M.				
81+86		5.39		891.58
+50		10.6		86.4
81+36				
20		10.5		86.5
80+86				
+50		10.8		86.2
80+36				
21		11.3		85.7
79+86				
+50		11.8		85.2
79+36				
22		12.0		85.0
78+86				
+50		12.6		84.4
78+36				
23		12.6		84.4
77+86				
+50		13.1		83.9
77+36				
24		12.7		84.3
76+86				
+50		13.0		84.0
76+36				
25		13.0		84.0

Spike Fe Post 25' Lk 18+97

$$\frac{9.9}{10} \quad 10.5 \quad \frac{10.5}{5} \quad \frac{9.6}{9}$$

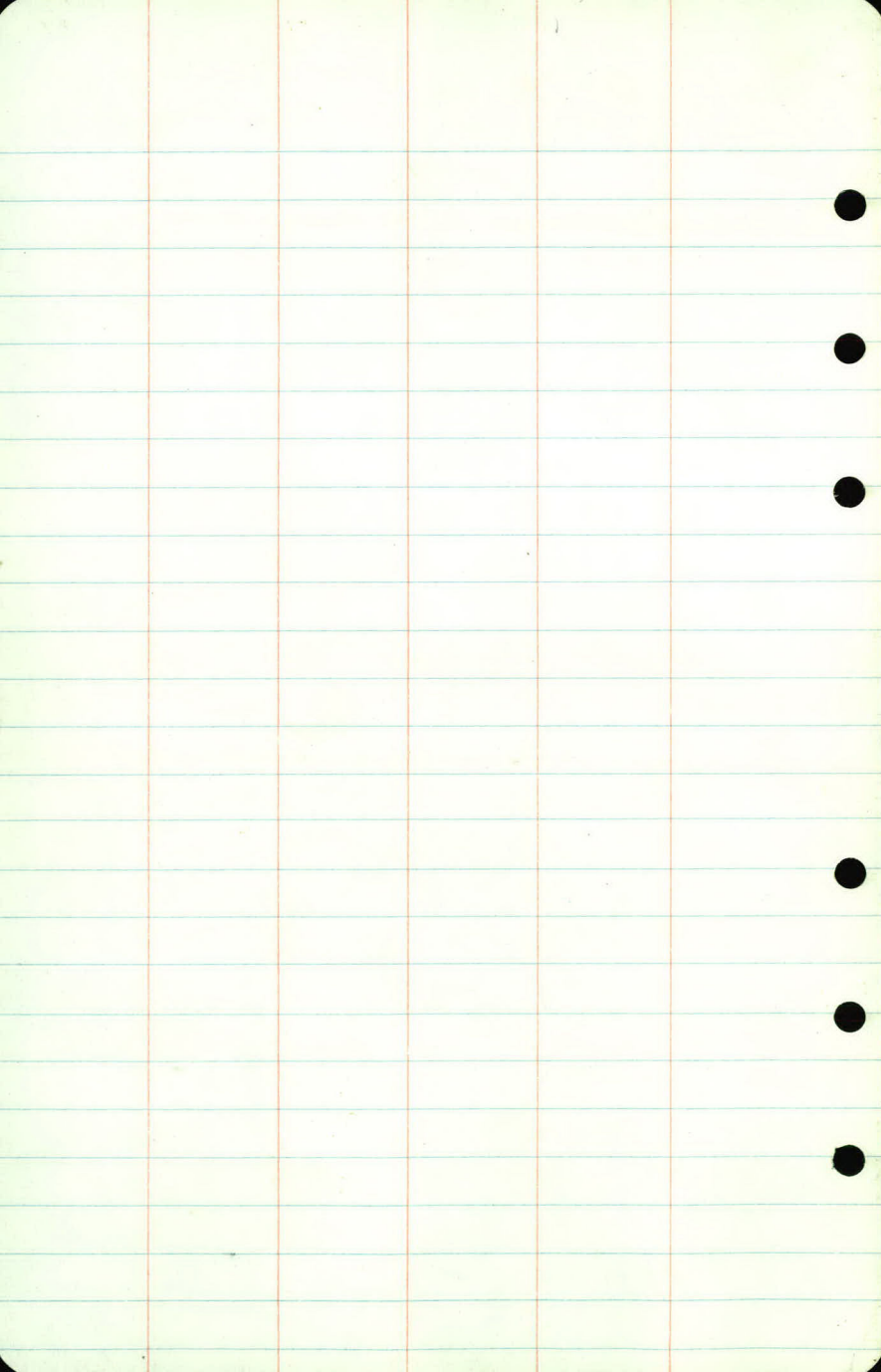
$$\frac{10.5}{10} \quad \frac{10.5}{3} \quad 11.3 \quad \frac{11.2}{3} \quad \frac{10.5}{5} \quad \frac{10.4}{10}$$

$$\frac{11.0}{14} \quad \frac{11.4}{2} \quad 12.0 \quad \frac{11.9}{2} \quad \frac{10.9}{4} \quad \frac{10.5}{10}$$

$$\frac{11.3}{10} \quad \frac{11.4}{5} \quad 12.6 \quad \frac{12.4}{2} \quad \frac{12.1}{3} \quad \frac{11.6}{10}$$

$$\frac{12.3}{10} \quad \frac{12.1}{5} \quad 12.7 \quad \frac{12.7}{4} \quad \frac{12.6}{10}$$

$$\frac{12.4}{10} \quad 13.0 \quad \frac{12.8}{2} \quad \frac{12.4}{10}$$



Profile Levels Ditch

LEXINGTON So. of I.

Ditch from Culv. W to Marsden Lk

9-25-40

Party

R. P.
A. M.
L. G.
C. F.

Sta.	+	π	-	Elev.
B.M.	5.41	897.00		891.59
F.L. 0+00			10.91	886.09
0+00 Ground			10.2	
+50			10.7	
1			10.9	
+50			11.3	
2			11.4	
+50			11.8	
3			12.2	
+50			12.5	
4			12.6	
+50			12.8	
5			12.6	
+50			12.6	
6			12.8	
+50			12.8	
7			12.8	
+50			12.8	884.20
8			13.02	883.98

Spike Fe. Post
West End. 30" G. M.

Top Water 9-25-40 (Marsden Lake)

