

BK. 75 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Drainage Survey

Ditch # 5

From Wilson Lk. To Jones Lk.

Road Acc't. No.

Date Filed. 6-11-41

File

DRAINAGE SURVEY

DITCH No. 5

Wilson Lake to Jones Lake

INDEX. P

Align - 1-6

Topog. - 7-17

Levels - 18-42

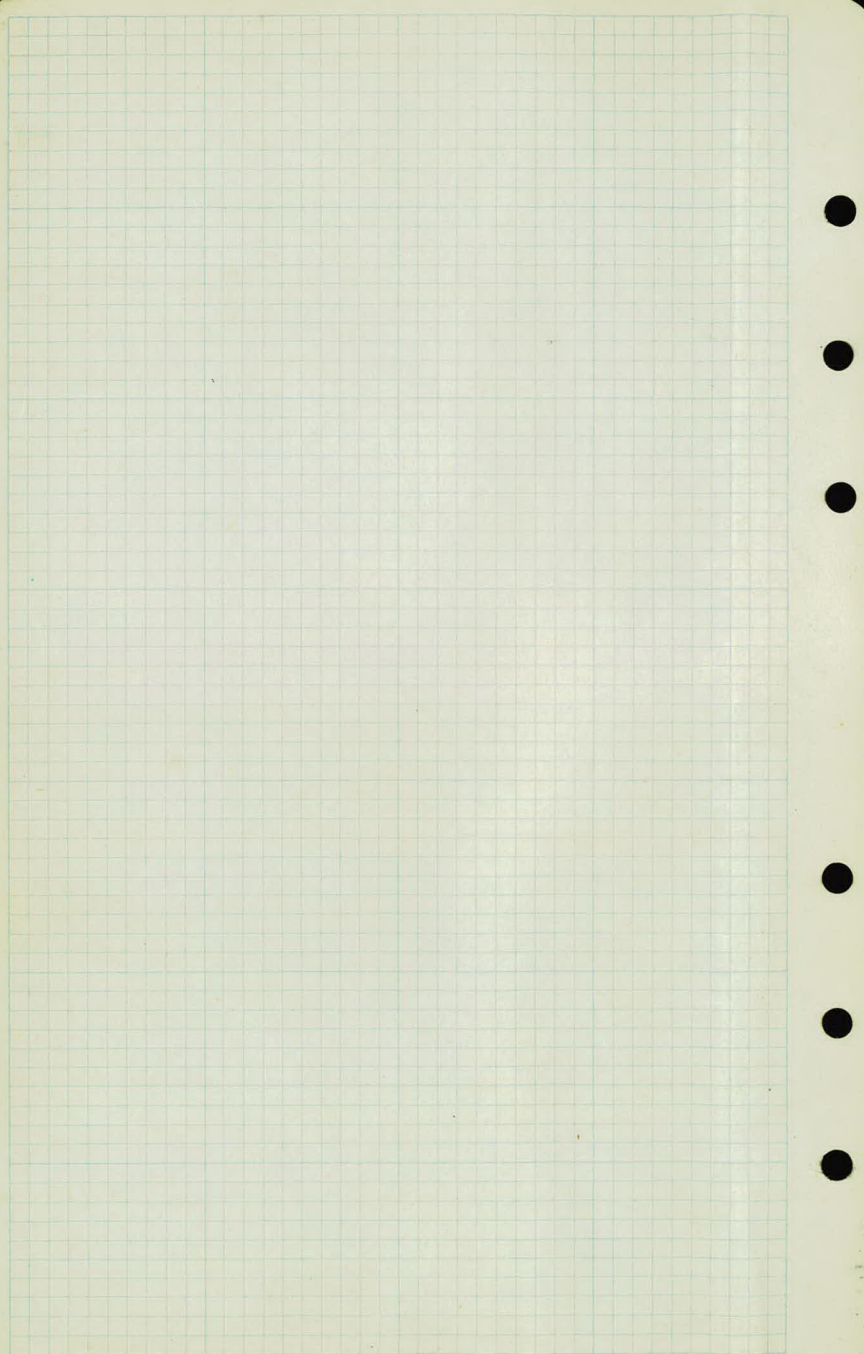
Stadia - 43-50

Done 4-22-41

Planis Comphatut

5/9/41

Alfred



Alignment

Sta	Point	ΔL	ΔR
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9	+49.45 P.I.	10°43'	
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7	+21.22 P.I.	32°11'	
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3	+97.73 P.I.	22°38'	
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0	+38.4 P.O.T.		
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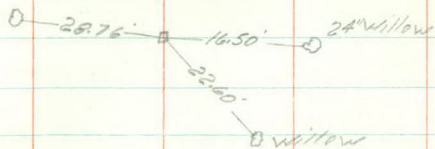
0	+100 = E. & Bag. 20" Vitr. Sewer		
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□ 2" X 2" Hub.

• Ctr. M.H.

• Ctr. M.H.

30" Girth



Sta	Point	ΔL	ΔB
-----	-------	------------	------------

24 + 93.37	P.O.T.		There seems to be some depth as to location of sewer between sta 16 + 87.55 and 30 + 41.0
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23 + 39.63	P.I.	3° 29'	
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16 + 87.55	P.I.		12° 09'
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11 + 34.90	P.O.T.		
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10 + 92.37	P.I.	9° 09'	
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N $\frac{1}{4}$ Cor. Sec. 5

4-15-41

3



808.87'

4' x 2" x 2" stake

N.E. Cor. Sec. 5

90° 55'

Chr. M. H.

43° 34'

1069.22'

2' x 2' Hub

E. $\frac{1}{4}$ Cor. Sec. 5

Sta	Point	ΔLt	ΔRt
-----	-------	-------------	-------------

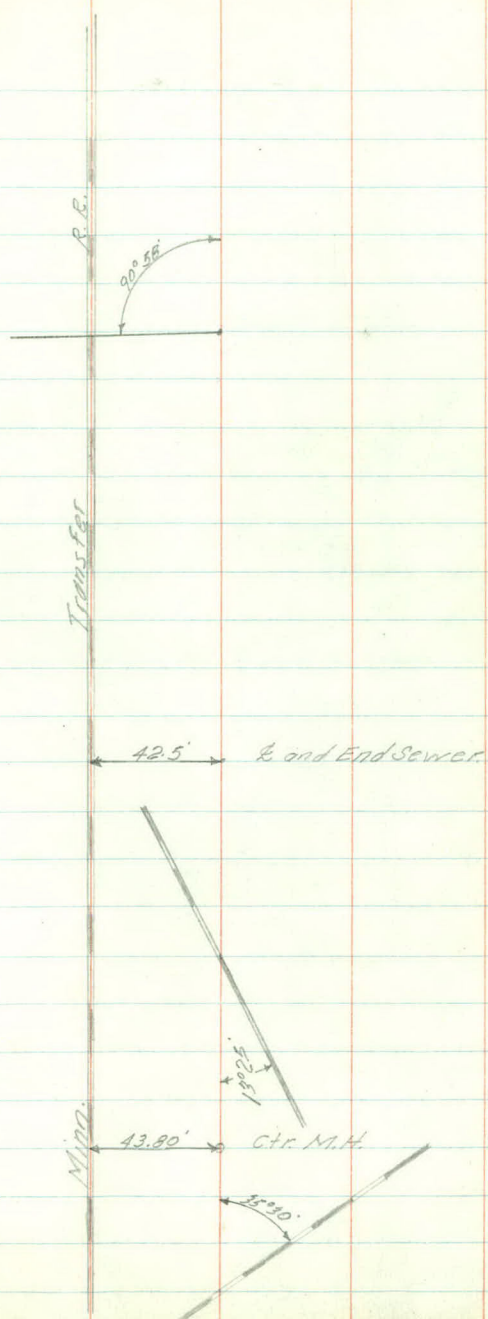
43 + 72.44	P.I.	90° 58'	
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37 + 74.56	P.O.T.		
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36 + 75.5	P.O.T. = E. Main Spur Track.		
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30 + 40.47	} Equiv. P.I.	48° 55'
30 + 41.00		

27 + 87.45	P.O.T. = E. Main Spur Track.		
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Sta	Point	ΔLt	ΔRt
-----	-------	-------------	-------------

51	+00	P.I.	28°38'
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49	+27.40	P.I.	31°01'
----	--------	------	--------

47	+68.85	P.I.	2°38'
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44	+37.25	P.I.	11°53'
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44	+14.75	P.O.T. =	Min. Transfer Ry. Track.
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End 24" Conc. Culf.

Sta	Point	ΔLt	ΔRt
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54 +89.15	P.I.	15°35'	
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53 +87.35	P.I.		1°50'
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53 +85.0	P.O.T	} End of Borral Mono Calk	
53 +70.0	P.O.T		

53 +67.50	P.I.	8°36'	
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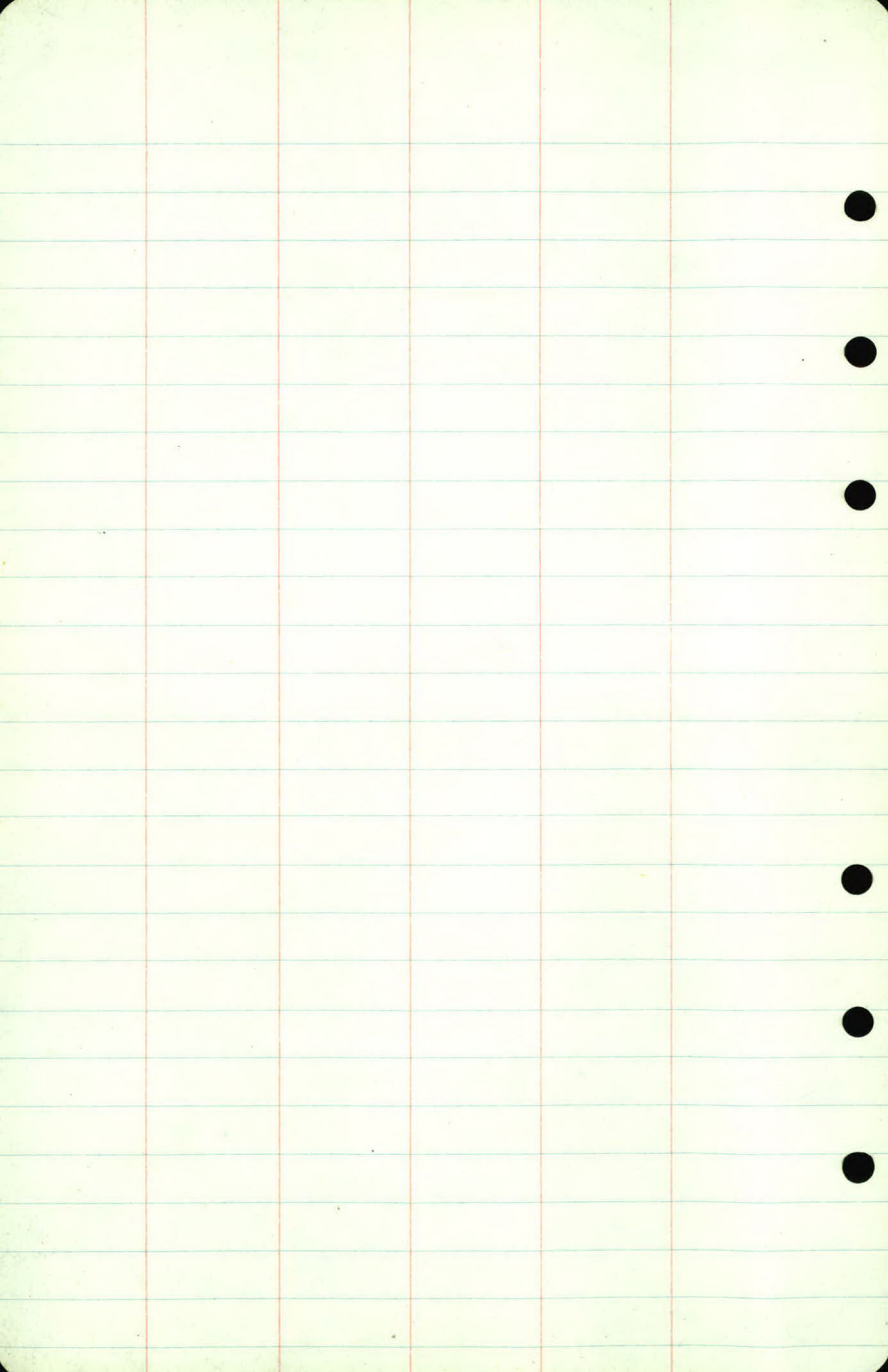
52 +37.55	P.I.		19°11'
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Ct. Sec. 32

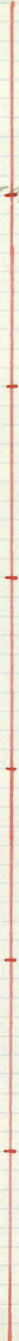
1/4 Cor

 $\angle 15^{\circ} 35'$ $52^{\circ} 32'$ $\angle 34^{\circ} 15'$

198.02'



Topography.



+91 Hand Ditch 10' R

+27-4" Elm - 15'

36' Long. Gully on End

+26-M.H.-o. Cesspool-1'

+17-Gar Ho. - 59

Sta. 3+

+16-Gar Garden - 22'

2

+91-Road to Ho.

Sta. 2+

+84-Gar Gar - 33'

+16-Road to Ho.

+15-Garden - 15'

1

Ditch - 81'

+31-24" Willow - 16'

+32-4" Willow - 10'

+29-End 12' Vt. Cor. - 41' 34' Long.

+15-18" Fl. Willow - 10'

+02-End 12" Cnr - 2.5'

0+00



1' Bottom.

Garden

Cult.

225'

4' Bottom

2' H.W. with 2' W.W.

2'

+48-Range Tie
+37-Fc Cor-19'

6

+58-Fc Cor-2'
+49-Bus Wood Fc-60'
+38-Cor Cor-6'
+37-Cor Shed-1.5'

+58-Fc XSE

+16-Cor Cor-2'

+22-Cor Shed-20'

+17-Cor Hol'head-4'

+04-Cor Hol'head-4'

5

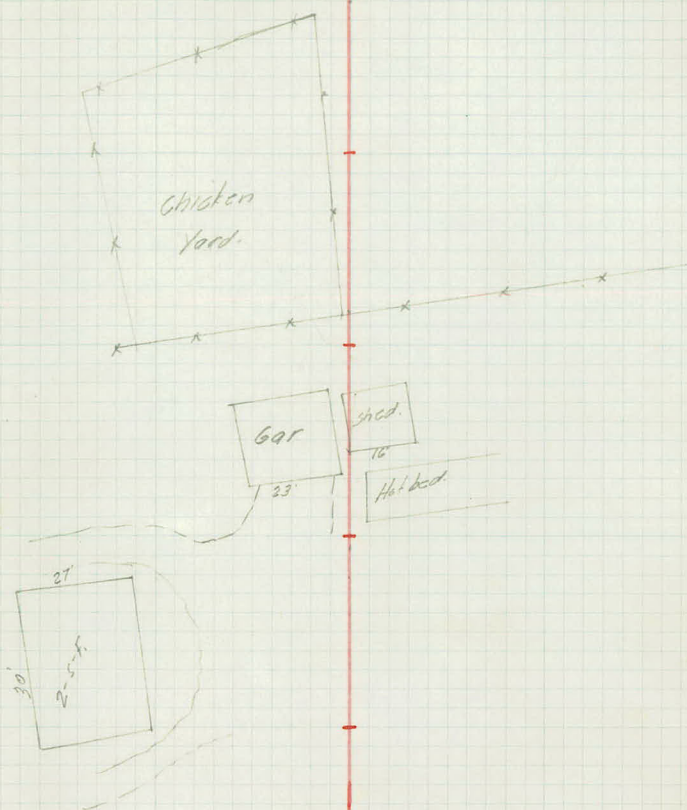
+97-Range Tie to Ho

+89-Cor Ho-56'

4

+57-Cor Pump-14'

3



+59-Fc Xs & +59 w/h
+40-10" wide drive Xs &

+21-Bog. Fc-36'

12

+50-B1 Top-0.0

+35-Bog. Fc-46'

+21-Edge sl. Top-0.0

11

+91-PP-3'

+91-Fc Xs &

10

+38-Fc Coc-88'

9

+95-Fc Xs &

+79-Cor Strawberry-12'

8

+77-Cor Strawberry-39'

+60-Bog. Wood Fc-4'

+50-PP-13'

+45-Fc Xs &

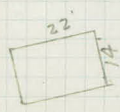
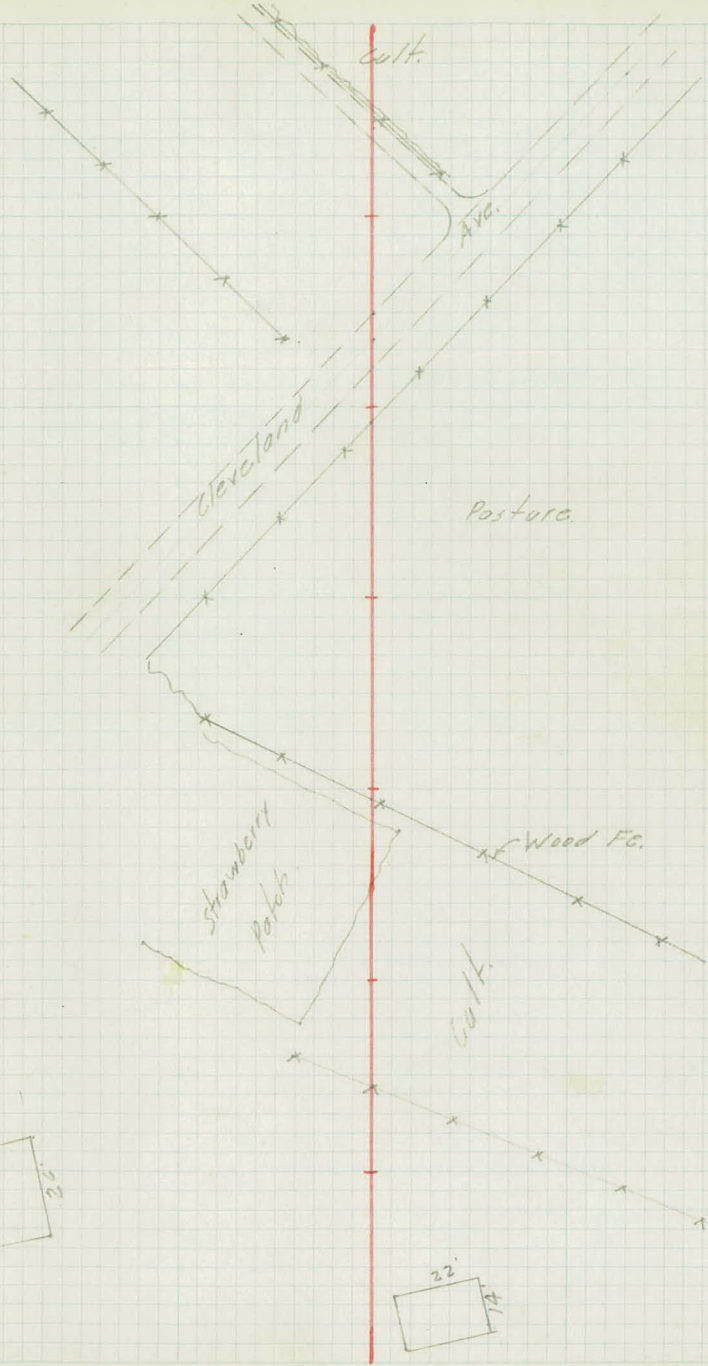
7 Longe Tie to Ho.

+83-Cor Ho-83'

+69-PP-7'

+67-Cor. Coop-6'

+55-Cor Chickens Coop-8'



+20 - T.P. 25'

+47 - High Line X 5' 6"
+23 - Trail X 5' 6"
+28 - Tele. Line X 5' 6"
+11 - High Line X 5' 6"
Ditch 0.0

+98 - Fe. Cor. - 8'
+98 - Bang Tie to Fe. Cor.

Ditch - 2'

Ditch - 1'

Fe - 30'

+60 Fe X 5' 6"

Ditch - 2'

Ditch 0.0

+26 - Fe. X 5' 6" Reg. ditch 0.0
H 2-8" Wide Drive X 5' 6"

Fe - 26'

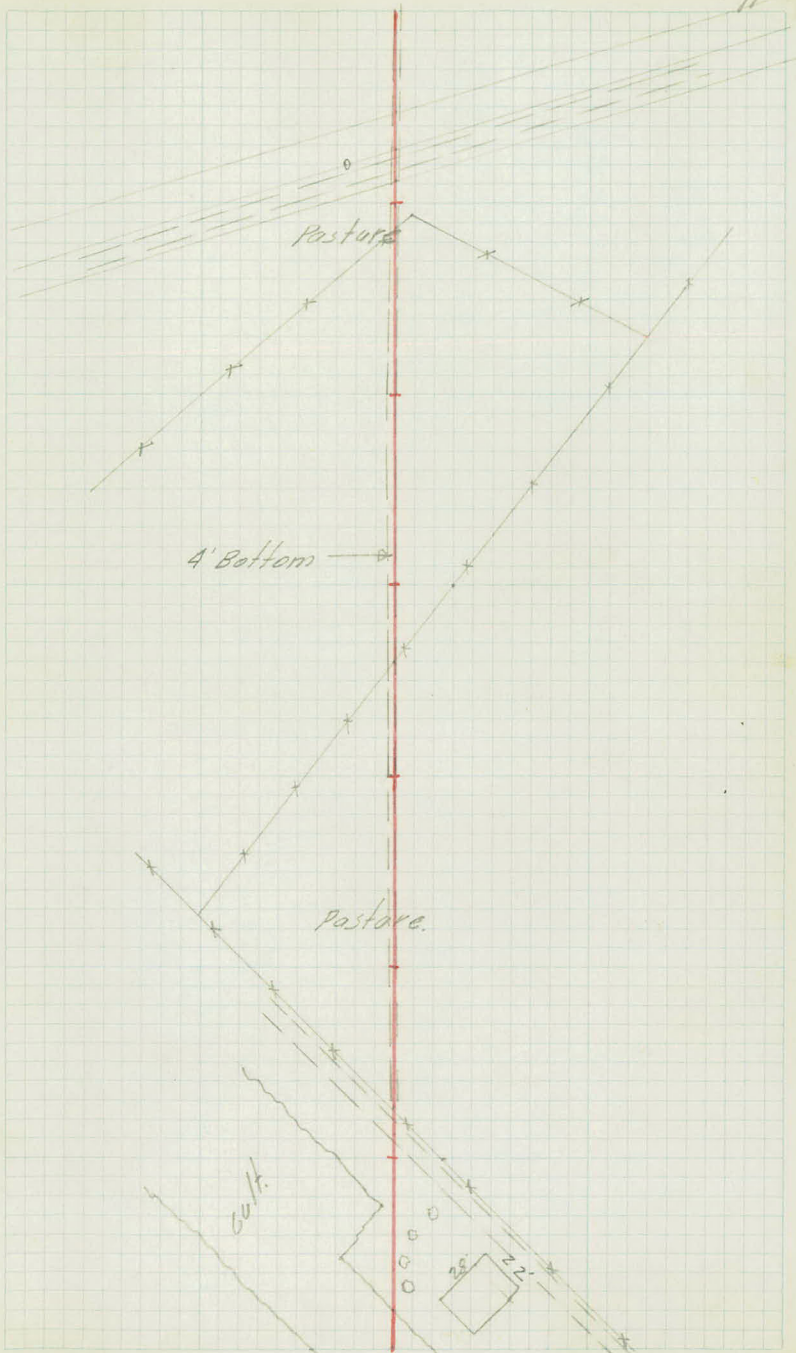
+75 - Con. Garden - 4'

+71 - 2" Apple Tr. - 20'
+66 - 2" Apple Tr. - 10'
+45 - 2" Apple Tr. - 5'
+33 - 1" Tree - 7'

+20 - Wt. 0.0

+26 - Con. Found. - 25'

tot Bang Tie to Found.



26

+25-Fc X^o 2

25

+03-Edge Bl. Top-0.0

~~+95-Fc X^o 2~~

+96-End 12' C.M. - 2.6'

+80-Edge Bl. Top-0.0

+59-Fc X^o 2

+77-End 12' C.M. - 4'

+27-NE Cor Ho-98'

24

+15-Wood Box for tile outlet from Ho 0.0

+96-Fc X^o 2

+62-Range Tie to Ho.

+98-Fc X^o 2

23

Fc - 31'

Ditch-0.0

22

Fc - 29'

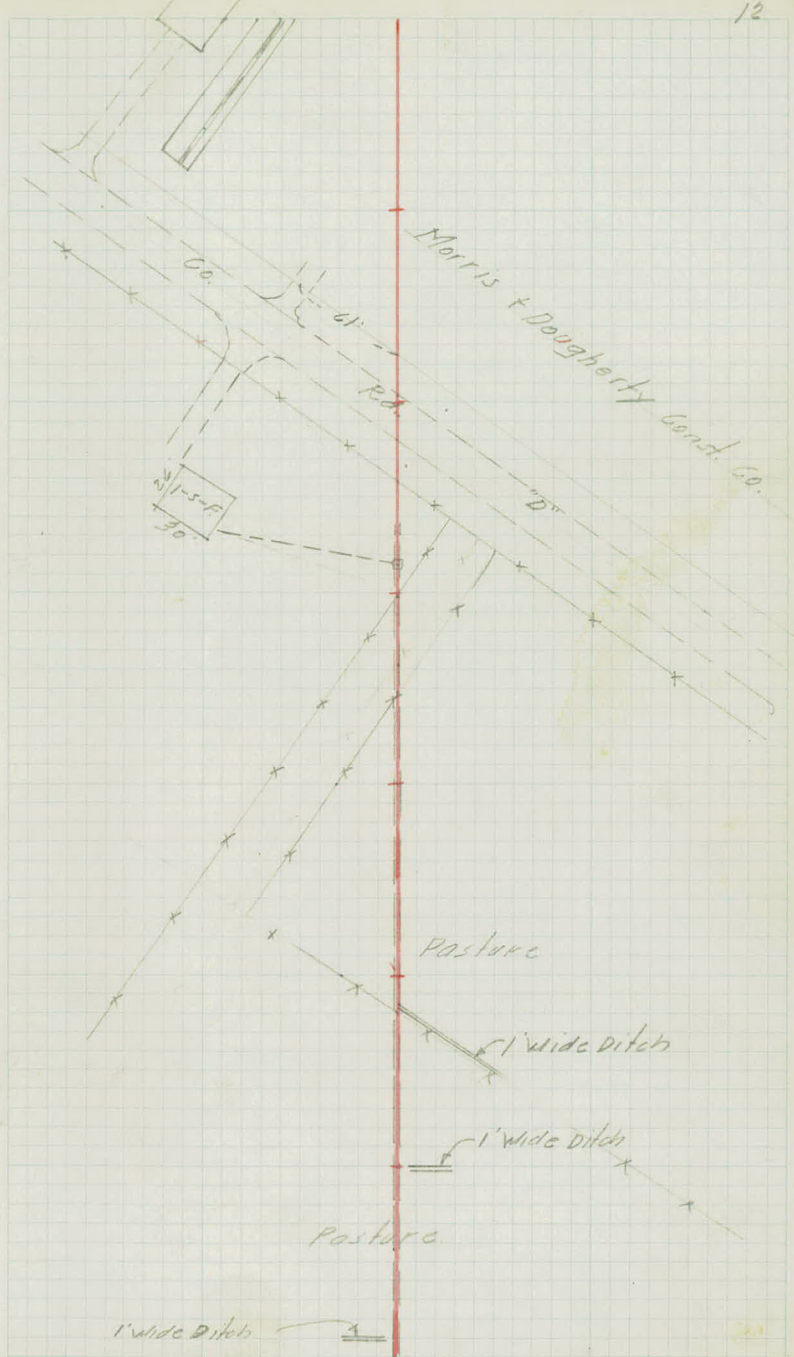
Ditch-0.0

+80-Fc X^o 2

21

Ditch-0.0

20



+90-24" CoH-12'

+54-8" BE-6'

33

Spur Track - 52'

+66-T.P.-7'

+43-Fc Cor-6'
+40-Fc Cor-40'

32

31

FC-5'

+85-T.P.-6'

30

FC-42'

+46.5-Track 15 ft

29

+29-End Spur Track - 39' $\curvearrowright$

+70-PP-22'

+53-Cor Chicken Coop - 53'

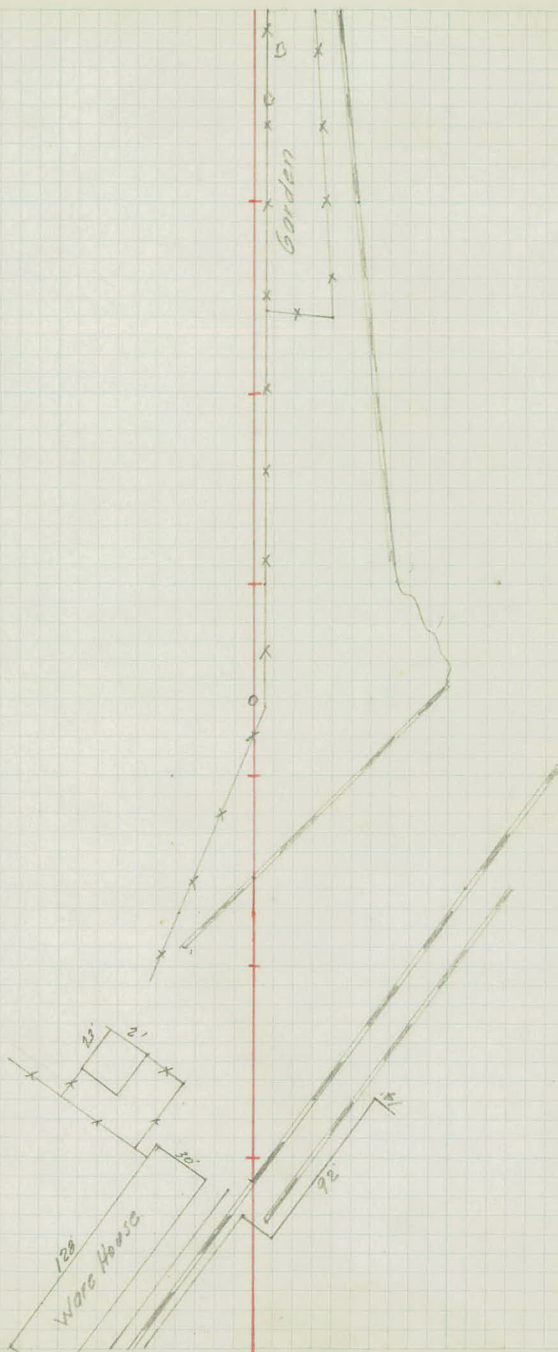
+31-Fc Cor-31'

28

+88-Cor Ware Ho - 26'
+85-End Loading Pit - 12'
+70-Cor Loading Pit - 5'

+67-End Spur Tr-6'
+58-Cor Loading Pit - 10'

27



40

Fc-7'

+45-Pt. of Switch

+28-T.P.-4'

39

Fc-7'

38

+72-T.P.-5'

37

+16-Fc. Cor.-8'
+14-Range Tie

36

+04-T.P.-7'

+16-Fc. Cor.-26'
+02-Fc. Cor.-7'

+75-Pt. of Switch

35

+24-Beg. Curve.-33'
Pt. of Switch

34

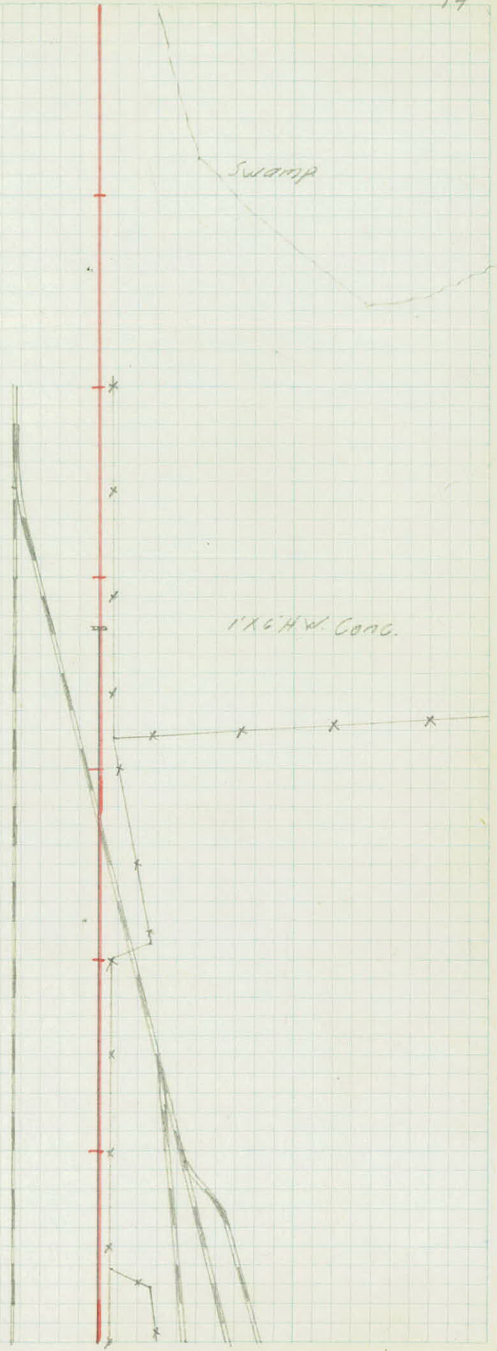
+25-T.P.-7'

+38-Fc. Cor.-7'
+29-Fc. Cor.-28'

Fc-6' E. Terml.-44.6'

Swamp

1' x 6" H.W. CONC.



+34-18" Tr Willow - 2'

47

+38-30" Cott - 7'

+38-30" Cott - 8'

46

+39-18" Cott - 5'

+35-36" Cott - 5'

+62-6" B.E. - 3'

+56-24" Cott - 4'

45

+73-Fe. Cor - 9'

+73-Fe. X's R

+77-25" End 24" Gms. Culv. 0.0

+34-B.C. Tie Retaining Wall X's R.

44

+92-End 24" Gms. Culv. 0.0

+20-T.P. - 4'

43

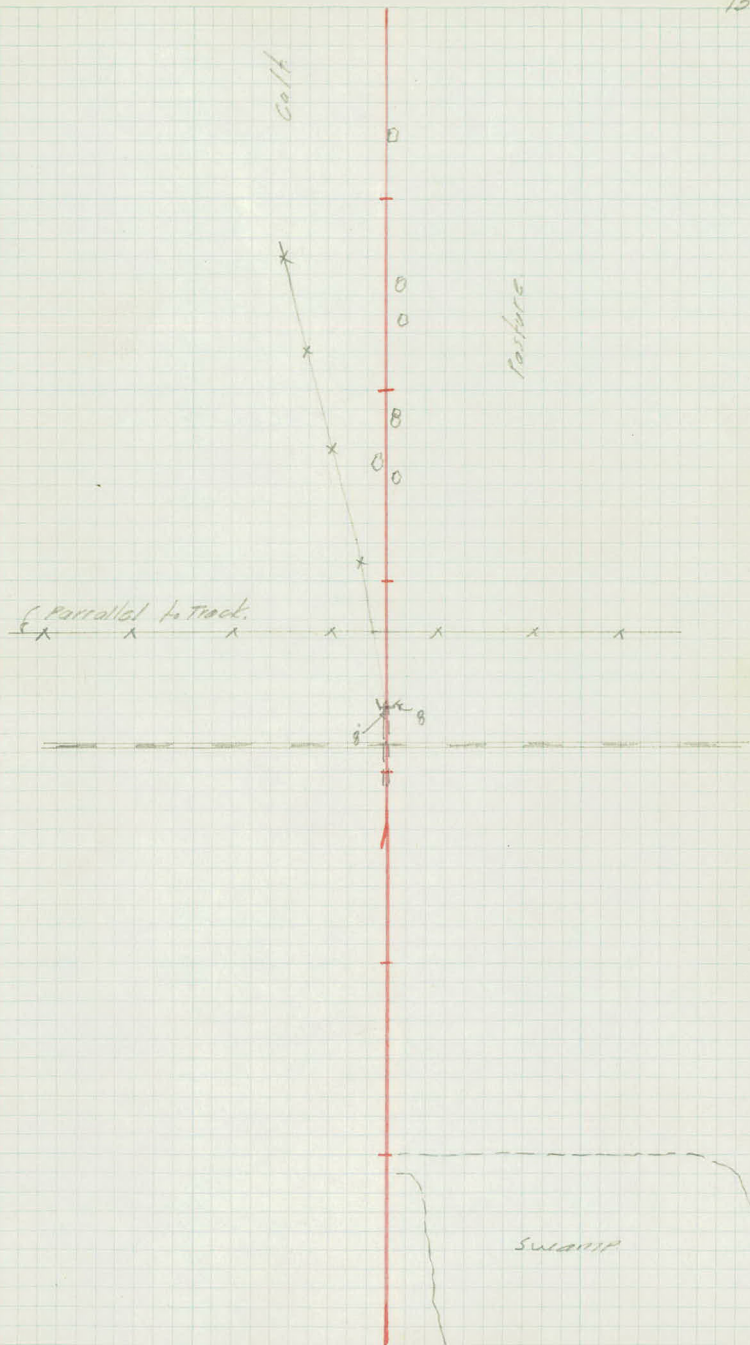
Fe - 7'

42

+66-T.P. - 4'

41

Fe - 7'



+49-24' Tw. Coll. Willow w/B

55

+73-Range T. 8
+70-Fe. Cor. -16'

54

+84-Fe. Cor. -14'
+82-Fe. Cor. -40'

+85-End Barrel } 3.3 wide No Bottom.
+70-End Barrel } Cons. Box Culv.

53 FC - 24'

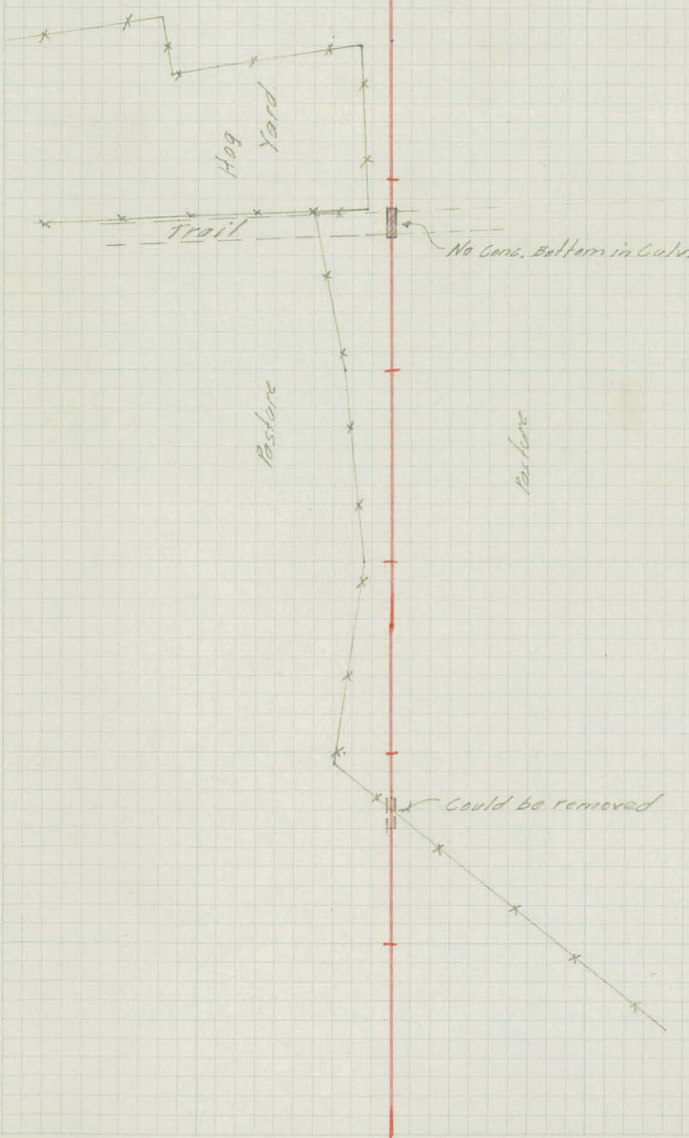
52 Fe - 14'

51 FC - 24'
+95-Fe. Cor. - 30'

+77-End 30' G.M. - 20
+70-Fe. N.R.
+60-End 30' G.M. - 0.0

50

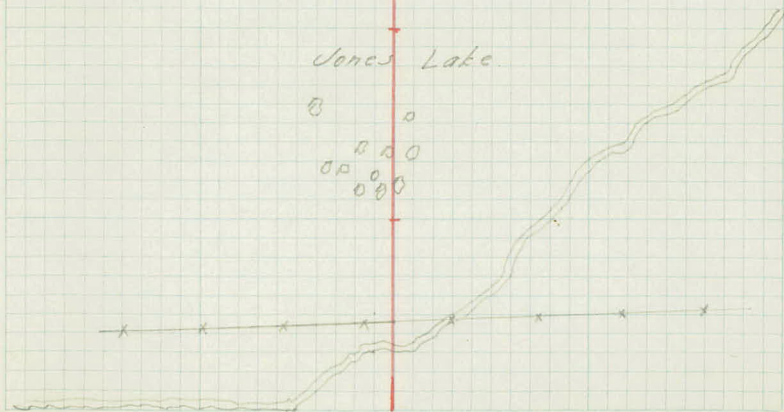
49

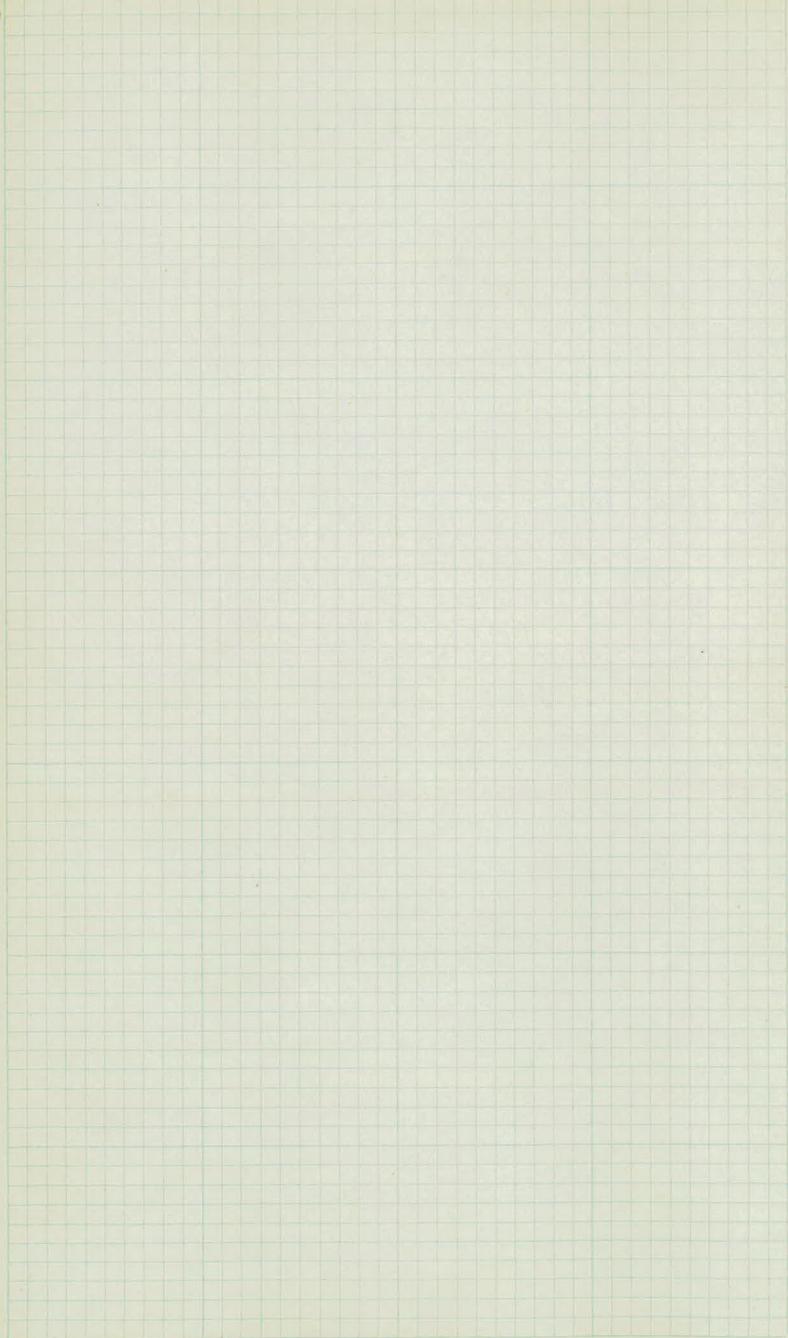


152-18" Willow-5
151-12" Willow-2 446-E+ W. R. X 5 X

Jones Lake

0
0 0 0
0 0 0 0
0 0 0





Levels.

Sta	+	π	-	Elev
B.M.	4.81	910.33		905.52
0 +00			13.91 12.16	96.42 98.17
0 +00			12.7	97.6
			10.48	899.85 ✓
+02			11.54	98.79
+04			8.3	02.0
+15			7.6	02.7
+26			2.0	08.3
+29			10.5	99.8
+40			1.7	08.6
+49			6.8	03.5
+71			7.1	03.2
1			6.9	03.4

11.8
12.76

100.52

Top and E.M.H. to sta. 3+97.73

Computed Flow Line 21" Vit.

Top inside edge Vit

Top dirt at Box Sewer

Top H.W.

F.L. Curb 25' Pt.

F.L. Curb 41' Pt.

sta + T - Elev

910.33

1 10.1 00.2

+50 5.8 04.5

2 4.8 05.5

+28 4.7 05.6

+38 5.5 04.8

+55 5.4 04.9

+79 6.0 04.3

3 5.4 04.9

+21 5.4 04.9

+26 3.86 06.47

+26 11.99 98.34

in ditch 81' E.

Top M.H. Canal

Top sewer?

sta	+	π	-	E/cx
		910.33.		

3	+37		5.1	05.2
---	-----	--	-----	------

	+41		9.0	01.3
--	-----	--	-----	------

	+57		10.0	00.3
--	-----	--	------	------

	+70		9.2	01.1
--	-----	--	-----	------

	+70		6.5	03.8
--	-----	--	-----	------

	+82		5.2	05.1
--	-----	--	-----	------

	+95		5.6	04.7
--	-----	--	-----	------

	+97.73		10.25	00.08
--	--------	--	-------	-------

	+97.73		11.42	98.91
--	--------	--	-------	-------

	+97.73		14.08	896.25
--	--------	--	-------	--------

4			5.4	04.9
---	--	--	-----	------

11.2
12.88
14.08

21

Top water in M.H.

Top dirt in M.H.

Flowline

Sta	+	Σ	-	Elev
		910.33		
4	+28		4.8	05.5
	+45		3.5	06.8
	+63		3.1	07.2
5			2.9	07.4
	+22		2.8	07.5
T.P.	460	913.48	1.45	908.88
	+37		6.0	07.5
	+58		7.0	06.5
	+74		7.6	05.9
6			7.8	05.7
	+30		8.4	05.1
	+70		8.9	04.6

Sta	+	π	-	Elev.
		913.48		
7			9.2	04.3
+20			9.6	03.9
+21.22			9.00	904.48
+21.22			14.35	99.15
+21.22			15.6	97.9
+21.22			17.53	895.95
+42			9.7	03.8
+70			9.9	03.6
8			9.9	03.6
T.P.	8.97	913.16	9.29	904.19
+50			10.2	03.0
+95			9.7	03.5

to Top M.H.

Top water in M.H.

Top dirt in M.H.

Flow Line

Sta	T	π	-	Elev
		913.16		
9			10.3	02.9
	+49		11.1	02.1
	+81		10.5	02.7
10			11.1	02.1
	+32		10.2	03.0
	+52		11.0	02.2
	+64		10.4	02.8
	+67		13.4	99.8
	Computed FlowLine		17.24	895.92
	+70		15.34	97.82
	+71.5		13.4	99.8
	+76		10.8	02.4

Top & End Wood Box

1

Top Sewer Pipe

15.34

.15

1.75

17.24

Top & End Wood Box

Sta.	T	π	-	Elev.
		913.16		
11			10.0	03.2
+12			5.5	07.7
+34.9			5.1	08.1
+56			5.7	07.5
+67			9.5	03.7
+78			9.9	03.3
+85			11.3	01.9
+93			10.7	02.5
12			10.7	02.5
+06			11.1	02.1
+10			13.4	99.8

Sta + π - Elev

9/13/16

12 +14 11.6 01.6

+35 11.0 02.2

+41 9.8 03.4

+53 10.0 03.2

+56 11.4 01.8

+59 11.2 02.0

+61 10.4 02.8

13 10.0 03.2

+30 10.3 02.9

+36 9.9 03.9

+50 9.3 03.9

Sta	+	T	-	Elev.
		913.16 913.15		
13	+56		10.0	03.2
	+72		9.9	03.3
	+77		9.2	04.0
14			8.8	04.4
	+21		8.9	04.3
	+27		10.4	02.8
T.P.	7.28	909.99 909.98	10.45	02.71 902.70
	+60			02.6
	+81			01.0
15				02.3
	+21			01.7
	+25			02.9

904.1

Lt.

K

Et.

$$\frac{56}{25} \frac{56}{12} \frac{60}{4} \frac{74}{1} \frac{74}{1} \frac{74}{1} \frac{63}{7} \frac{60}{24} \frac{66}{25}$$

$$\frac{54}{25} \frac{58}{15} \frac{69}{7} \frac{90}{2} \frac{90}{3} \frac{82}{7} \frac{67}{14} \frac{58}{25} \frac{65}{25}$$

$$\frac{48}{25} \frac{52}{11} \frac{57}{6} \frac{79}{2} \frac{77}{9} \frac{59}{25} \frac{56}{25}$$

$$\frac{44}{25} \frac{45}{9} \frac{59}{5} \frac{79}{2} \frac{83}{5} \frac{59}{8} \frac{54}{12} \frac{53}{12} \frac{58}{26}$$

$$\frac{41}{25} \frac{43}{12} \frac{59}{4} \frac{71}{1} \frac{71}{1} \frac{68}{8} \frac{51}{11} \frac{51}{11} \frac{58}{25}$$

Sta	+	π	-	Elev
		909.99		
		909.98		

15	+47			03.7
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16				04.2
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	+50			02.6
--	-----	--	--	------

2 shot = F.L. 8" tile inlet
+855 to M.H.

	+87.55		5.82	02.18
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	+87.55		12.30	97.69
--	--------	--	-------	-------

	+87.55		12.70	97.29
--	--------	--	-------	-------

	+87.55		13.96	896.03
--	--------	--	-------	--------

B.M.	5.62	904.79	5.82	904.17
		909.78		904.16

17				01.8
----	--	--	--	------

	+50			03.9
--	-----	--	--	------

18				03.0
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Lt.

E.

Pt.

$$\frac{35}{25} \frac{35}{15} \frac{41}{7} \frac{64}{1} \frac{63}{6} \frac{47}{11} \frac{42}{16} \frac{54}{25} \frac{57}{25}$$

$$\frac{39}{25} \frac{43}{17} \frac{38}{13} \frac{40}{7} \frac{72}{3} \frac{68}{4} \frac{46}{9} \frac{45}{25} \frac{43}{25}$$

$$\frac{47}{25} \frac{47}{14} \frac{48}{8} \frac{74}{3} \frac{74}{4} \frac{48}{12} \frac{52}{25} \frac{53}{25}$$

$$\frac{47}{25} \frac{46}{16} \frac{44}{8} \frac{71}{3} \frac{71}{4} \frac{65}{10} \frac{48}{25} \frac{53}{25}$$

Top to M.H.

Top water in M.H.

Top dirt in M.H.

Flow line

Top to M.H.

$$\frac{49}{25} \frac{46}{8} \frac{81}{3} \frac{80}{5} \frac{45}{19} \frac{50}{25} \frac{47}{25}$$

$$\frac{55}{25} \frac{43}{8} \frac{64}{3} \frac{70}{2} \frac{59}{7} \frac{35}{25} \frac{31}{25}$$

$$\frac{51}{25} \frac{47}{7} \frac{75}{3} \frac{75}{1} \frac{68}{4} \frac{48}{11} \frac{40}{15} \frac{45}{25} \frac{42}{25}$$

Sta	+	π	-	Elev
		909.79 909.78		
18	+50			02.7
19				03.0
	+50			02.7
20				02.6
	+50			02.4
21				02.8
21	Ditch Profile Et.			02.8
	+50			02.5
+82				03.0
Profile of ditch Along Fe. Et.				907.00
T.P.	8.87	915.87	2.79	906.99
22				03.3
	+50			04.5

LH

R

RH

$$\frac{52}{25} \frac{54}{18} \frac{48}{13} \frac{48}{6} \frac{70}{2} \frac{71}{5} \frac{50}{11} \frac{47}{14} \frac{52}{25} \frac{47}{25}$$

$$\frac{57}{25} \frac{57}{15} \frac{51}{12} \frac{55}{6} \frac{68}{2} \frac{68}{15} \frac{68}{4} \frac{50}{12} \frac{46}{15} \frac{50}{25} \frac{46}{25}$$

$$\frac{59}{50} \frac{58}{25} \frac{57}{16} \frac{52}{13} \frac{54}{9} \frac{71}{4} \frac{71}{2} \frac{67}{6} \frac{48}{11} \frac{46}{15} \frac{53}{25} \frac{48}{25}$$

$$\frac{59}{50} \frac{59}{25} \frac{54}{14} \frac{47}{12} \frac{53}{6} \frac{71}{2} \frac{72}{2} \frac{70}{6} \frac{48}{11} \frac{47}{16} \frac{57}{25} \frac{53}{25}$$

$$\frac{55}{25} \frac{49}{13} \frac{54}{7} \frac{72}{3} \frac{74}{3} \frac{72}{6} \frac{49}{12} \frac{48}{17} \frac{58}{25} \frac{56}{25}$$

$$\frac{58}{25} \frac{48}{11} \frac{53}{6} \frac{61}{4} \frac{70}{4} \frac{67}{7} \frac{50}{13} \frac{47}{25} \frac{54}{25}$$

$$\frac{70}{7} \frac{64}{25} \frac{61}{25}$$

$$\frac{53}{25} \frac{54}{15} \frac{48}{11} \frac{52}{5} \frac{69}{1} \frac{73}{3} \frac{72}{7} \frac{50}{14} \frac{48}{17} \frac{57}{25} \frac{58}{25}$$

$$\frac{68}{23} \frac{66}{50} \frac{66}{50}$$

$$\begin{array}{c} \text{N.S.} \\ 58 \\ 50 \end{array}$$

Top Rock 1122

$$\frac{101}{25} \frac{106}{17} \frac{99}{12} \frac{97}{8} \frac{123}{2} \frac{126}{3} \frac{124}{8} \frac{105}{13} \frac{102}{20} \frac{112}{25} \frac{112}{25}$$

$$\frac{91}{25} \frac{85}{13} \frac{97}{4} \frac{119}{7} \frac{114}{12} \frac{100}{25} \frac{100}{25}$$

Sta	+	T	-	Elev
		915.87 915.86		

23				05.7
----	--	--	--	------

	+50			06.7
--	-----	--	--	------

24				07.1
----	--	--	--	------

	+23		9.0	06.9
--	-----	--	-----	------

	+41		8.2	07.7
--	-----	--	-----	------

	+58		8.7	07.2
--	-----	--	-----	------

	+60		8.0	07.9
--	-----	--	-----	------

	+67		8.68	07.19
--	-----	--	------	-------

	+75		5.7	10.2
--	-----	--	-----	------

	+79		5.3	10.6
--	-----	--	-----	------

	+92		5.1	10.8
--	-----	--	-----	------

Lt.

K

Rt.

$$\frac{84}{25} \frac{83}{14} \frac{91}{7} \frac{100}{3} \frac{102}{3} \frac{100}{3} \frac{82}{10} \frac{77}{25}$$

$$\frac{76}{25} \frac{80}{11} \frac{85}{5} \frac{92}{1} \frac{92}{4} \frac{81}{4} \frac{70}{12} \frac{65}{25}$$

$$\frac{72}{26} \frac{76}{17} \frac{85}{6} \frac{88}{5} \frac{87}{5} \frac{78}{11} \frac{75}{25}$$

FL. 12" G.M. 4 Rk.

Sta	+	π 51587 915.86	-	Elev
24	+96		8.37	07.50
25	+107		5.4	10.5
	+11		6.9	09.0
	+23		7.6	08.3
	+34		5.8	10.1
	+50		5.6	10.3
26			6.2	09.7
	+50		6.1	09.8
27			6.1	09.8
	+14		6.6	09.3
	+31		6.8	09.1

FL. 12° C. 19. 25' Pt.

Sta	+	π	-	Elev
		915.86		

27	+66		6.9	09.0
----	-----	--	-----	------

	+66		10.1	05.8
--	-----	--	------	------

	+67		14.84	900.03
			12.94	02.93

	+83.2		9.89	05.98
--	-------	--	------	-------

	+87.45		10.3	05.6
--	--------	--	------	------

	+91.6		9.88	05.99
--	-------	--	------	-------

28			9.9	06.0
----	--	--	-----	------

T.P.	4.67	910.40		905.73
		910.39	10.14	905.72

	+50		4.9	05.5
--	-----	--	-----	------

29			5.7	04.7
----	--	--	-----	------

	+46.5		6.1	04.3
--	-------	--	-----	------

30			6.4	04.0
----	--	--	-----	------

Computed F.L.

Top sewer. Dig out tile but cannot strike tile on either side

Top E. Rail

Top W. Rail

Ground at track.

Sta.	+	π	-	Elev
		910.39		
30 + 34			6.5	03.9
+ 39			6.9	03.5
+41.00 = +40.47 } Equa.			6.15	04.25
			12.98	97.42
			15.0	95.4
+41.00 = +40.47 } Equa.			15.32	895.08
B.M.			6.15	904.23
+43			6.8	03.6
+65			7.8	02.6
31			7.3	03.1
+36			7.0	03.4
+50			7.5	02.9

to Top M.H.

Top Water

Top dirt in M.H.

Flow Line

Top to M.H. sta 30+41.0 = 30+42.47

Sta	+	π	-	Elev
		910.39		
31	+91		7.9	02.5
	+93		7.8	00.6
32			10.4	00.0
	+04		7.7	02.7
	+43		7.4	03.0
	+63		8.5	01.9
33			8.0	02.6
	+50		7.8	02.6
	+84		7.8	02.6
34			8.1	01.7
T.P.	334	910.51	3.22	907.17
	+25		9.9	00.6

910.51

907.18

Top Rail Lts 34100 = 2.89 07.23

Sta.	+	π 710.52 910.51	-	Elev
34	+54		9.9	00.6
35			10.9	99.5
	+30		10.8	99.7
	+60		10.7	99.8
	+78		9.7	00.8
36			11.1	99.4
	+05		10.1	00.4
	+15		8.2	02.3
	+24		7.2	03.3
	+42		6.6	03.9
	+65.0		5.73	04.79

Top Rail

Sta	+	π	-	Elev
		910.52 910.51		
36	+75.3		6.0	04.5
	+86		5.52	05.00
37			5.9	04.6
	+10		5.7	04.8
	+35		6.1	04.4
	+95		6.3	04.2
B.M. +74.56			12.48	98.04
+74.56			13.23	97.29
+74.56			15.23	95.29 95.27
+79.56				96.4
38				97.6

Lt

C

Rt

Top Rail

$$\begin{array}{r}
 12.48 \\
 2.75 \\
 \hline
 13.23 = \text{Fl.} \\
 13.30 = \text{Top Inside Edge} \\
 \hline
 1.93
 \end{array}$$

Top H. W. L. at End Sewer.

Top Water

Flow Line 24" Vitr. Sewer

Top Rail 13

4.46	51	50	11.4	11.7	13.1	14.1	13.2	11.8	8.9	7.9	7.9	9.3
19	19	13	9	3	2	3	3	8	11	13	25	

4.18	4.7	5.0	7.4	12.7	13.5	13.7	12.9	12.9	10.5	7.4
2.5	17	12	4	3	1	1	1	1	11	25

Sta.	f	π	-	Elev.
		910.5V 910.51		
38	+50			97.2
39				96.2
T.P.	3.04	910.01 910.00	3.55	906.97 906.96
	+50			96.7
40				96.0
	+50			95.9
41				95.9
	+50			95.8
42				95.4
T.P.	3.11	910.63 910.62	2.49	907.52 907.51
	+50			95.9
43			95.4	95.4
	+50			95.4

Lt

R

Rt

(Two Col)

$$\begin{array}{r} 360 \quad 42 \quad 47 \quad 77 \quad 72 \quad 72 \quad 104 \quad 128 \quad 135 \quad 193 \\ \hline 32 \quad 25 \quad 19 \quad 15 \quad 12 \quad 6 \quad 35 \quad 3 \end{array}$$

$$\begin{array}{r} 101 \quad 83 \quad 81 \quad 88 \\ \hline 35 \quad 7 \quad 10 \quad 25 \end{array}$$

$$\begin{array}{r} 345 \quad 39 \quad 40 \quad 67 \quad 74 \quad 86 \quad 113 \quad 139 \quad 143 \quad 104 \quad 85 \quad 78 \quad 88 \\ \hline 38 \quad 33 \quad 27 \quad 17 \quad 10 \quad 6 \quad 25 \quad 4 \quad 7 \quad 14 \quad 25 \end{array}$$

$$\begin{array}{r} 280 \quad 33 \quad 37 \quad 88 \quad 98 \quad 88 \quad 87 \quad 132 \quad 133 \\ \hline 40 \quad 30 \quad 22 \quad 18 \quad 14 \quad 85 \quad 3 \end{array}$$

$$\begin{array}{r} 131 \quad 118 \quad 94 \quad 90 \quad 91 \quad 97 \\ \hline 2 \quad 4 \quad 7 \quad 10 \quad 18 \quad 25 \end{array}$$

$$\begin{array}{r} 371 \quad 33 \quad 41 \quad 95 \quad 107 \quad 112 \quad 102 \quad 103 \quad 133 \quad 140 \quad 132 \quad 120 \quad 102 \quad 110 \\ \hline 39.5 \quad 31 \quad 23 \quad 17 \quad 13 \quad 9 \quad 6 \quad 15 \quad 35 \quad 5 \quad 8 \quad 25 \end{array}$$

$$\begin{array}{r} 255 \quad 32 \quad 38 \quad 103 \quad 126 \quad 112 \quad 113 \quad 150 \quad 141 \quad 134 \quad 125 \quad 114 \quad 108 \quad 108 \quad 123 \quad 123 \\ \hline 39.5 \quad 32 \quad 22 \quad 13 \quad 9 \quad 5 \quad 2 \quad 35 \quad 50 \quad 9 \quad 11 \quad 13 \quad 18 \quad 25 \end{array}$$

$$\begin{array}{r} 248 \quad 32 \quad 39 \quad 117 \quad 126 \quad 115 \quad 124 \quad 134 \quad 141 \quad 130 \quad 121 \quad 115 \quad 118 \quad 131 \quad 130 \\ \hline 39.5 \quad 30 \quad 18 \quad 12 \quad 7 \quad 4 \quad 2 \quad 4 \quad 6.5 \quad 11 \quad 15 \quad 20 \quad 25 \end{array}$$

$$\begin{array}{r} 233 \quad 30 \quad 38 \quad 129 \quad 135 \quad 118 \quad 121 \quad 133 \quad 142 \quad 135 \quad 127 \quad 132 \quad 118 \\ \hline 39 \quad 30 \quad 18 \quad 13 \quad 9 \quad 4 \quad 2 \quad 5 \quad 6 \quad 25 \end{array}$$

$$\begin{array}{r} 219 \quad 28 \quad 31 \quad 129 \quad 131 \quad 116 \quad 119 \quad 128 \quad 135 \quad 146 \quad 135 \quad 126 \quad 117 \quad 120 \quad 129 \\ \hline 39 \quad 31 \quad 17 \quad 13 \quad 10 \quad 6 \quad 4 \quad 2 \quad 3.5 \quad 7 \quad 10 \quad 15 \quad 25 \end{array}$$

$$\begin{array}{r} 262 \quad 32 \quad 38 \quad 132 \quad 136 \quad 126 \quad 131 \quad 142 \quad 147 \quad 141 \quad 127 \quad 123 \quad 130 \\ \hline 39 \quad 31 \quad 17 \quad 13 \quad 11 \quad 6 \quad 5 \quad 4.5 \quad 7 \quad 17 \quad 25 \end{array}$$

$$\begin{array}{r} 244 \quad 30 \quad 34 \quad 132 \quad 138 \quad 125 \quad 126 \quad 148 \quad 152 \quad 145 \quad 120 \quad 122 \quad 123 \\ \hline 39 \quad 31 \quad 17 \quad 12 \quad 9 \quad 7 \quad 3 \quad 4 \quad 7 \quad 17 \quad 25 \end{array}$$

$$\begin{array}{r} 117 \quad 130 \quad 119 \quad 119 \quad 136 \quad 144 \quad 152 \quad 144 \quad 137 \quad 123 \quad 124 \quad 124 \\ \hline 18 \quad 13 \quad 10 \quad 7 \quad 5 \quad 25 \quad 25 \quad 4 \quad 7 \quad 10 \quad 25 \end{array}$$

Sta	+	π	-	Elev
		910.63 910.62		
43	+85			97.0
	+92		14.4	96.2
	+92		15.95	94.68
	+92		11.1	99.5
44			5.4	05.2
	+02		36	07.0
	+10		2.9	07.7
Top Rail			2.21	08.42
Top Rail			2.23	08.40
	+19		2.9	07.7
	+25		3.4	07.2

Lt

C

Rt

118	118	143	136	137	123	126
25	5	25	3	6	25	

Top dirt of culv.

Flow Line 24" Gang Culv.

sta	+	π	-	Elev.
		910.63		
		910.62		
		904.79		899.14
T.P.	5.65	904.18	11.49	899.13
44	+34		4.3	00.5
	+37.25		10.91	93.88 ✓
	+37		10.6	94.2 ✓
	+51		9.0	95.8
	+65			95.8
45				96.0
	+50			95.5
46				95.5
	+50			95.8
47				95.5
	+38			95.5

Lt

R

Rt

Flow Line 24° 6' 14"

$\frac{7.1}{25}$ $\frac{6.1}{12}$ $\frac{5.9}{7}$ $\frac{8.0}{3}$ $\frac{8.4}{2}$ $\frac{9.0}{-}$ $\frac{9.0}{2}$ $\frac{8.3}{4}$ $\frac{6.4}{9}$ $\frac{5.2}{14}$ $\frac{5.6}{25}$

$\frac{6.2}{25}$ $\frac{6.5}{5}$ $\frac{8.2}{3}$ $\frac{8.8}{-}$ $\frac{8.4}{4}$ $\frac{5.2}{9}$ $\frac{5.2}{18}$ $\frac{5.6}{25}$

$\frac{6.2}{25}$ $\frac{5.5}{12}$ $\frac{5.5}{8}$ $\frac{6.9}{4}$ $\frac{8.7}{2}$ $\frac{9.3}{-}$ $\frac{8.9}{2}$ $\frac{7.8}{5}$ $\frac{4.6}{11}$ $\frac{4.9}{17}$ $\frac{5.0}{25}$

$\frac{5.4}{25}$ $\frac{5.8}{16}$ $\frac{5.0}{12}$ $\frac{5.0}{8}$ $\frac{8.5}{3}$ $\frac{9.3}{-}$ $\frac{9.0}{4}$ $\frac{8.1}{5}$ $\frac{4.3}{12}$ $\frac{4.4}{25}$

$\frac{5.6}{25}$ $\frac{5.5}{10}$ $\frac{4.1}{7}$ $\frac{8.5}{3}$ $\frac{9.0}{-}$ $\frac{8.9}{4}$ $\frac{6.2}{8}$ $\frac{4.5}{15}$ $\frac{4.5}{25}$

$\frac{4.4}{25}$ $\frac{4.5}{10}$ $\frac{5.2}{7}$ $\frac{8.7}{3}$ $\frac{9.3}{-}$ $\frac{8.7}{3}$ $\frac{5.8}{8}$ $\frac{4.0}{12}$ $\frac{4.1}{25}$

$\frac{2.8}{25}$ $\frac{2.7}{11}$ $\frac{8.8}{2}$ $\frac{9.3}{-}$ $\frac{8.7}{3}$ $\frac{7.8}{5}$ $\frac{3.4}{12}$ $\frac{3.1}{25}$

Sta	+	π	-	Elev
		904.79 904.78		
47+69				95.4
48				95.7
+50				95.3 ✓
49				95.3
T.P.	9.16	906.30 906.29	1.65	897.14 897.13
+50				95.3
50				95.6
+50				95.3
+60 F.L. 30" C.M.				93.73
+77 F.L. 30" C.M.				93.30
51				95.3
+50				95.2

Lt

R

Rt

$$\frac{2.4}{25} \frac{2.4}{11} \frac{7.8}{3} \frac{9.1}{2} \frac{9.4}{1} \frac{9.1}{3} \frac{3.2}{12} \frac{3.3}{25}$$

$$\frac{2.8}{25} \frac{2.6}{12} \frac{7.2}{5} \frac{8.9}{2.5} \frac{9.1}{3} \frac{8.6}{5} \frac{7.7}{12} \frac{3.6}{25}$$

$$\frac{3.1}{25} \frac{3.3}{12} \frac{5.7}{8} \frac{7.4}{4} \frac{9.0}{1.5} \frac{9.5}{3} \frac{9.1}{13} \frac{2.9}{25} \frac{2.1}{25}$$

$$\frac{3.4}{25} \frac{3.2}{12} \frac{7.8}{4} \frac{8.8}{3} \frac{9.5}{2.5} \frac{8.9}{5} \frac{7.0}{12} \frac{2.6}{12} \frac{1.5}{25}$$

$$\frac{4.4}{25} \frac{4.5}{18} \frac{5.7}{12} \frac{8.8}{7} \frac{9.4}{5} \frac{10.7}{2} \frac{11.0}{2} \frac{10.5}{13} \frac{4.6}{25} \frac{3.0}{25}$$

$$\frac{3.8}{25} \frac{4.5}{12} \frac{8.8}{5} \frac{10.8}{2} \frac{10.7}{2} \frac{10.2}{12} \frac{4.5}{12} \frac{3.0}{25}$$

$$\frac{3.9}{25} \frac{5.0}{12} \frac{10.0}{2} \frac{10.6}{1} \frac{11.0}{0.5} \frac{10.7}{2} \frac{10.0}{5} \frac{8.0}{11} \frac{5.2}{25} \frac{3.3}{25}$$

12.57

12.0

$$\frac{4.5}{25} \frac{5.5}{10} \frac{7.6}{5} \frac{10.6}{15} \frac{11.0}{2} \frac{10.8}{2} \frac{9.8}{4} \frac{7.5}{10} \frac{5.5}{17} \frac{4.6}{25}$$

$$\frac{5.0}{25} \frac{4.8}{12} \frac{4.8}{8} \frac{11.0}{2} \frac{11.1}{3} \frac{10.6}{4} \frac{9.9}{8} \frac{8.7}{17} \frac{5.4}{25} \frac{5.2}{25}$$

Sta.	+	π	-	Elev.
		906.30 906.29		
52				95.4
	+50			95.0
53				95.1
	+35			95.4
	+70			94.9
	+85			94.9
T.P.	4.65	903.62	7.33	898.96
54				95.0
	+50			94.8
55				95.0
	+50			94.8
56				94.8

L.A.

4

L.A.

$$L.O. \frac{60}{15} \frac{77}{9} \frac{98}{5} \frac{107}{15} \frac{109}{3} \frac{110}{6} \frac{82}{12} \frac{58}{25} \frac{60}{25}$$

$$L.O. \frac{64}{13} \frac{77}{7} \frac{113}{15} \frac{110}{15} \frac{107}{10} \frac{77}{14} \frac{68}{14} \frac{58}{25}$$

$$\frac{65}{25} \frac{70}{20} \frac{68}{11} \frac{110}{4} \frac{112}{3} \frac{114}{4} \frac{101}{13} \frac{64}{25} \frac{66}{25}$$

$$\frac{63}{25} \frac{74}{16} \frac{82}{10} \frac{108}{3} \frac{109}{5} \frac{114}{7} \frac{94}{12} \frac{75}{13} \frac{78}{25} \frac{73}{25}$$

$$\frac{57}{25} \frac{62}{16} \frac{87}{11} \frac{100}{4} \frac{115}{3} \frac{114}{2} \frac{114}{3} \frac{91}{8} \frac{75}{15} \frac{78}{15} \frac{74}{25}$$

$$\frac{55}{25} \frac{62}{14} \frac{75}{9} \frac{114}{15} \frac{114}{2} \frac{115}{11} \frac{78}{11} \frac{77}{25}$$

$$\frac{35}{25} \frac{38}{14} \frac{52}{10} \frac{81}{2} \frac{86}{3} \frac{87}{5} \frac{78}{12} \frac{47}{25} \frac{51}{25}$$

$$\frac{55}{25} \frac{53}{10} \frac{62}{7} \frac{90}{4} \frac{88}{3} \frac{85}{8} \frac{60}{25} \frac{55}{25}$$

$$\frac{68}{25} \frac{60}{12} \frac{70}{6} \frac{82}{4} \frac{86}{3} \frac{88}{11} \frac{58}{11} \frac{56}{25}$$

94%

$$\frac{62}{25} \frac{63}{9} \frac{85}{5} \frac{90}{3} \frac{88}{4} \frac{88}{7} \frac{70}{12} \frac{55}{12} \frac{66}{25}$$

$$\frac{64}{25} \frac{82}{10} \frac{90}{6} \frac{88}{4} \frac{90}{9} \frac{89}{7} \frac{79}{10} \frac{82}{25}$$

Sta.	+	T 903.62 903.61	-	Elev
56	+50			93.9
57			10.0	93.6
	+50		10.5	93.1
58			10.7	92.9
Elev. Jones Lake			9.10	94.5
B.M.			3.36	900.26 900.25

Lb.

L

Rt.

95	93	86	20	97	97	97	88	92
25	15	11	4	2	2	4	25	

Top Most 1/2 Cor.

Sta

+

π

-

Elev

stadia

Sta	Azimuth	Dist	Red	Elev
At E. 1/4 Cor. Sec. 5	0°00' = N to N.E. Cor. Sec. 5			
B.M.	+5.45	H.I. = 908.48		903.03
Elev. Water			7.6	900.9
N.G. = Nat. Ground	147° 50'	107.0	10.4	
"	124° 40'	147.0	10.4	
"	117° 40'	194.0	10.3	
"	118° 30'	258.0	12.1	
"	113° 30'	295.0	11.1	
"	114° 10'	370.0	11.3	
"	118° 45'	435.0	10.5	
"	119° 45'	350.0	11.5	
"	125° 10'	260.0	12.6	95.9
"	128° 00'	230.0	11.6	
"	143° 00'	176.0	11.1	
"	158° 45'	145.0	10.8	
"	166° 45'	210.0	11.6	
"	151° 30'	230.0	11.8	
"	138° 30'	276.0	12.6	
"	128° 00'	340.0	11.3	
"	125° 00'	420.0	10.4	
"	134° 15'	410.0	9.9	
"	148° 15'	335.0	11.1	
"	148° 45'	315.0	12.5	
"	167° 15'	283.0	11.6	
"	173° 00'	368.0	11.1	

Description

96.7
758

Top Mont. E 1/4 Cor. Sec. 5

S.E. Cor. Cleveland & Co. Rd. E²

Lowest Spot Found


 Lowest Spot Found

Sta
AT E $\frac{1}{4}$
Cor. Sec. 5

Azimuth	Dist	Rod	Elev
H.I. = 908.48			

N.G. 159° 45' 360.0 12.3

" 149° 30' 390.0 10.4

" 164° 30' 430.0 10.2

" 169° 45' 435.0 11.6

" 174° 10' 470.0 11.4

" 157° 10' 320.0 11.7

123° 10' 255.0 12.6

Waters
Edge

128° 30' 24.0

" 99° 15' 124.0

" 94° 30' 270.0

" 93° 00' 413.0

" 93° 15' 500.0

" 94° 45' 518.0

" 101° 00' 508.0

" 107° 30' 520.0

" 113° 30' 520.0

" 120° 30' 510.0

" 125° 30' 505.0

" 134° 30' 476.0

" 143° 15' 455.0

" 151° 30' 465.0

" 159° 30' 445.0

" 167° 00' 555.0

" 170° 30' 600.0

Descriptions

lowest spot found

Sta	Azimuth	Dist	Red	Elev.
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H.I. = 908.48

Waters
Edge

172° 30'	630.0		
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172° 15'	644.0		
----------	-------	--	--

177° 45'	605.0		
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178° 20'	532.0		
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177° 45'	448.0		
----------	-------	--	--

176° 00'	313.0		
----------	-------	--	--

174° 00'	182.0		
----------	-------	--	--

172° 30'	120.0		
----------	-------	--	--

153° 00'	40.0		
----------	------	--	--

136° 00'	32.0		
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Culv.

95° 45'	266.0	11.05	97.45
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85° 30'	267.0	10.85	97.65
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Waters
Edge

213° 30'	35.0		
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189° 30'	95.0		
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234° 00'	38.0		
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184° 15'	177.0		
----------	-------	--	--

248° 15'	60.0		
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183° 00'	259.0		
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258° 30'	110.0		
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182° 00'	360.0		
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262° 30'	155.0		
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181° 45'	447.0		
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262° 45'	192.0		
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261° 30'	220.0		
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Description

Flow Line S. End 36" G.M. X Drain

" " N. " "

Sta	Azimuth	dist	Red	Elev
		H. I. =	908.48	
Waters Edge	181° 30'	560.0		
"	254° 00'	230.0		
"	182° 00'	665.0		
"	250° 00'	274.0		
"	185° 45'	667.0		
"	244° 45'	345.0		
"	190° 00'	667.0		
"	244° 00'	388.0		
"	195° 00'	638.0		
"	239° 00'	414.0		
"	201° 15'	595.0		
"	230° 30'	418.0		
"	205° 45'	528.0		
"	221° 30'	434.0		
"	209° 30'	473.0		
"	215° 00'	440.0		
Culv.	240° 00'	43.0	9.80	
"	295° 00'	51.0	9.20	
N.G.	198° 45'	82.0	10.0	
"	193° 00'	115.0	10.9	
"	189° —	200.0	11.5	
"	189° 30'	290.0	11.5	
"	189° —	378.0	11.3	
"	188° —	453	11.3	

Flow line So. End. 24" CONC. X Drain

" " No. " " " "

Sta	Azimuth	Dist	Rod	Elev
H.I. = 908.48				
Cleveland Ave	180°—	660.0	3.9'	
"		560.0	6.1	
"		460'	6.1	
"		376'	6.9	
"		275'	6.8	
"		172'	6.3	
"		70'	5.9	
N.G.	64°45'	295'	11.5	92.0
"	50°—	347'	11.8'	96.7
"	39°30'	420'	12.2	96.3
"	32°—	490'	12.2	96.3
"	25°30'	590'	11.4	97.1
"	21°50'	676'	10.7	97.8
"	32°—	605'	10.4	98.1
"	37°—	535'	11.2	97.3
"	40°45'	510'	10.5	98.0
"	47°45'	460'	13.0	95.5
"	54°30'	420'	11.5	97.0
"	63°—	397'	11.8	96.7
"	76°30'	380'	11.5	97.0
Waters Edge	49°00'	42'		
"	"	52°00'	58'	
"	"	73°00'	123'	
"	"	77°30'	188'	

8.63

48

Small Hole

Sta	Azimuth	Dist	Rod	Elev
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H.I.-908.48

Waters Edge	61° —	220'		
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"	"	38° 30'	274'	
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"	"	25° 30'	315'	
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"	"	12° 30'	340'	
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"	"	6° —	450'	
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"	"	9° 45'	555'	
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"	"	6° 30'	674'	
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"	"	13° 30'	652'	
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"	"	15° 45'	615'	
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"	"	22° 30'	631'	
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H.V.	17° 56'	812'	8.69	
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Waters Edge	25° 15'	730'		
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"	"	25° 15'	795'	
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"	"	33° —	688'	
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"	"	40° —	560'	
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"	"	51° —	565'	
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"	"	60° 30'	653'	
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"	"	69° 15'	638'	
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"	"	78° 30'	575'	
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"	"	87° —	418'	
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"	"	88° 15'	432'	
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"	"	88° 45'	332'	
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"	"	86° —	217'	
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"	"	81° —	112'	
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2 and Top H.W. of Reg. Sewer.

Sta	Azimuth	Dist	Red	Elev
		HI-908.48		
6 Co. Rd. "C2"	90° 25'	96'	6.1	
"		195'	6.1	02.4
"		293'	6.7	01.80
"		396'	6.8	
"		500'	3.5	

4-26-41

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Sta.	Azimuth	Dist.	Red.	Elev.
1	110° 15'	100		
2	110° 15'	100		
3	110° 15'	100		
4	110° 15'	100		
5	110° 15'	100		
6	110° 15'	100		
7	110° 15'	100		
8	110° 15'	100		
9	110° 15'	100		
10	110° 15'	100		
11	110° 15'	100		
12	110° 15'	100		
13	110° 15'	100		
14	110° 15'	100		
15	110° 15'	100		
16	110° 15'	100		
17	110° 15'	100		
18	110° 15'	100		
19	110° 15'	100		
20	110° 15'	100		
21	110° 15'	100		
22	110° 15'	100		
23	110° 15'	100		
24	110° 15'	100		
25	110° 15'	100		
26	110° 15'	100		
27	110° 15'	100		
28	110° 15'	100		
29	110° 15'	100		
30	110° 15'	100		
31	110° 15'	100		
32	110° 15'	100		
33	110° 15'	100		
34	110° 15'	100		
35	110° 15'	100		
36	110° 15'	100		
37	110° 15'	100		
38	110° 15'	100		
39	110° 15'	100		
40	110° 15'	100		
41	110° 15'	100		
42	110° 15'	100		
43	110° 15'	100		
44	110° 15'	100		
45	110° 15'	100		
46	110° 15'	100		
47	110° 15'	100		
48	110° 15'	100		
49	110° 15'	100		
50	110° 15'	100		
51	110° 15'	100		
52	110° 15'	100		
53	110° 15'	100		
54	110° 15'	100		
55	110° 15'	100		
56	110° 15'	100		
57	110° 15'	100		
58	110° 15'	100		
59	110° 15'	100		
60	110° 15'	100		
61	110° 15'	100		
62	110° 15'	100		
63	110° 15'	100		
64	110° 15'	100		
65	110° 15'	100		
66	110° 15'	100		
67	110° 15'	100		
68	110° 15'	100		
69	110° 15'	100		
70	110° 15'	100		
71	110° 15'	100		
72	110° 15'	100		
73	110° 15'	100		
74	110° 15'	100		
75	110° 15'	100		
76	110° 15'	100		
77	110° 15'	100		
78	110° 15'	100		
79	110° 15'	100		
80	110° 15'	100		
81	110° 15'	100		
82	110° 15'	100		
83	110° 15'	100		
84	110° 15'	100		
85	110° 15'	100		
86	110° 15'	100		