

BK. 72 Dr. 16

OFFICE OF COUNTY ENGINEER  
RAMSEY CO. MINN.

Plan Survey

Lower Afton Rd.

Int. East Co. Line

From To

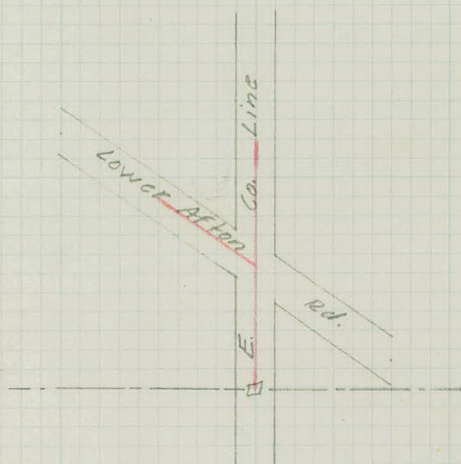
Old U.S. #61 to S.T.H. #100

Road Acc't. No. 71

Date Filed 6-11-41

File

PLAN SURVEY  
INTERSECTION  
at  
Lower Afton Rd. and E. Co. Line



Drawn up HAW  
1/27/41

INDEX.

- Align - 1-2
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- X Sections of Rd. - 13



1

Alignment

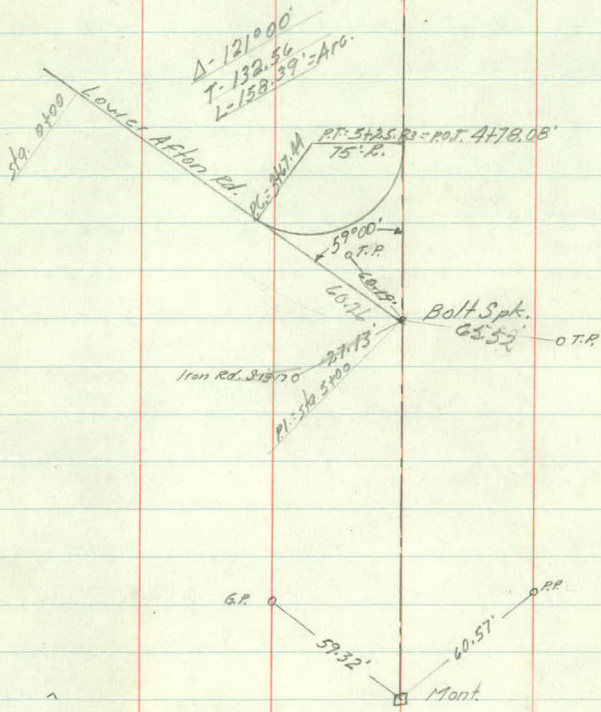
| Sta | Point | $\Delta$ Lt | $\Delta$ Rt |
|-----|-------|-------------|-------------|
|-----|-------|-------------|-------------|

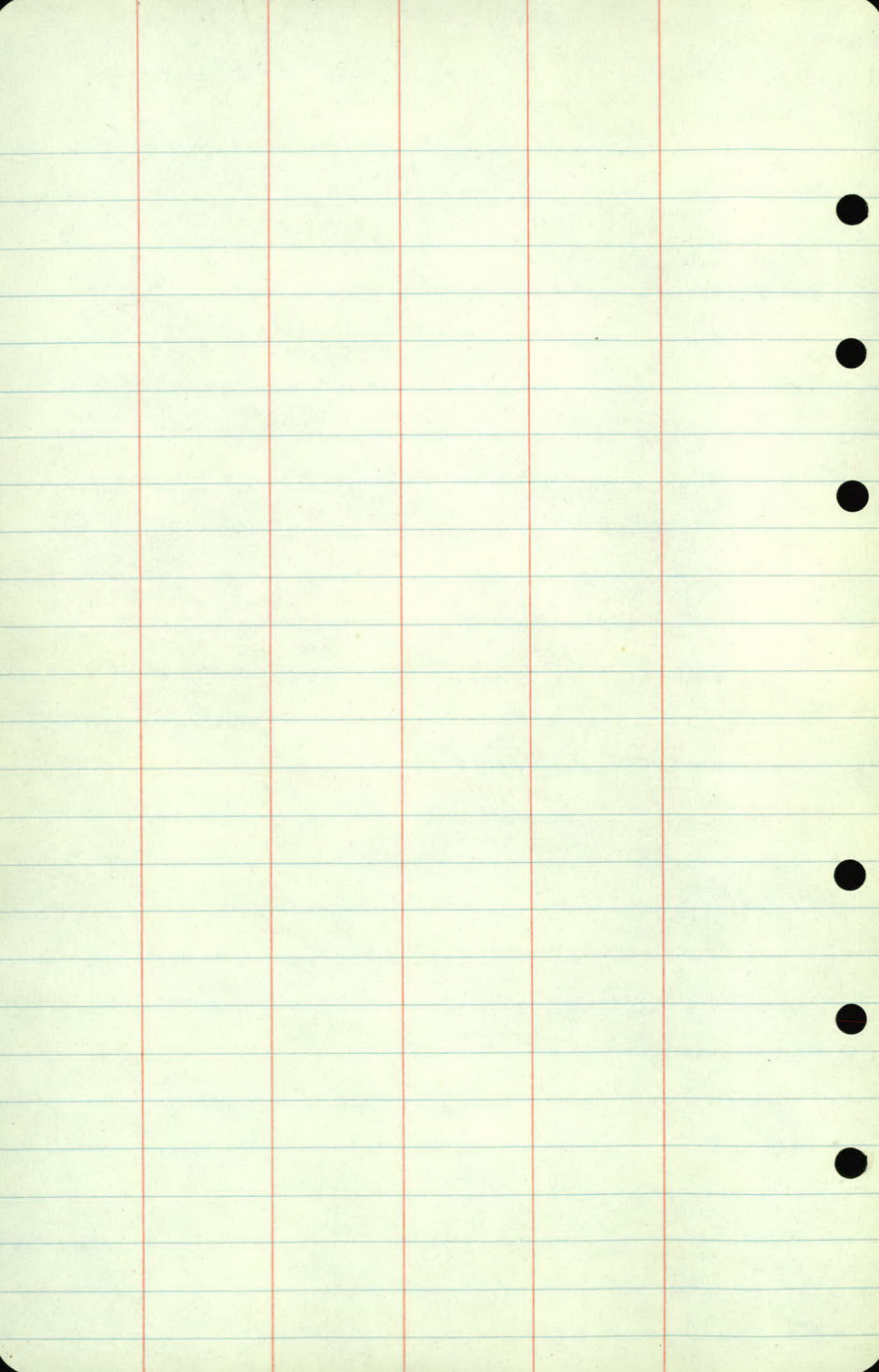
|   |                                          |  |  |
|---|------------------------------------------|--|--|
| 3 | +45.52 P.O.T = Sta. 0+00 Lower Afton Rd. |  |  |
|---|------------------------------------------|--|--|

|   |                           |  |  |
|---|---------------------------|--|--|
| 0 | +00 = E. 1/4 Cor. Sec. 12 |  |  |
|---|---------------------------|--|--|

4-18-40  
K.H.  
L.G.  
M.B.  
C.N.

2





*Topography*  
*East County Line*

11' 12'

6 11' 12'

+46-T.P.-26'

5 11' 12'

+16-End Rod.-11'  
+08-T.P. Pole Brace.-26'

4 T.P.-26' 11' 13'

+78-End Rod.-14'

+89-Trav. Rd.-30'  
+41-Stop Sign.-28'  
+34-Ed. Sign.-24'  
+35-Ed.-20'  
+14-Bog. Rod.-12'

+37-Long Tie to S. Shoulder  
+35-Bog. Rod.-38'  
+30-End 12" C.M.-49'

3 12' 12' +13-End 12" C.M.-35' End Rod.-93'

+86-Bog. Rod.-12'

2 11' 11'

1 11' 11'

+58-G.P.-17'

2.4" X 39" C.M.

+55-P.P.-28'

+42-End 24" C.M.-18'

+40-End 24" C.M.-21'

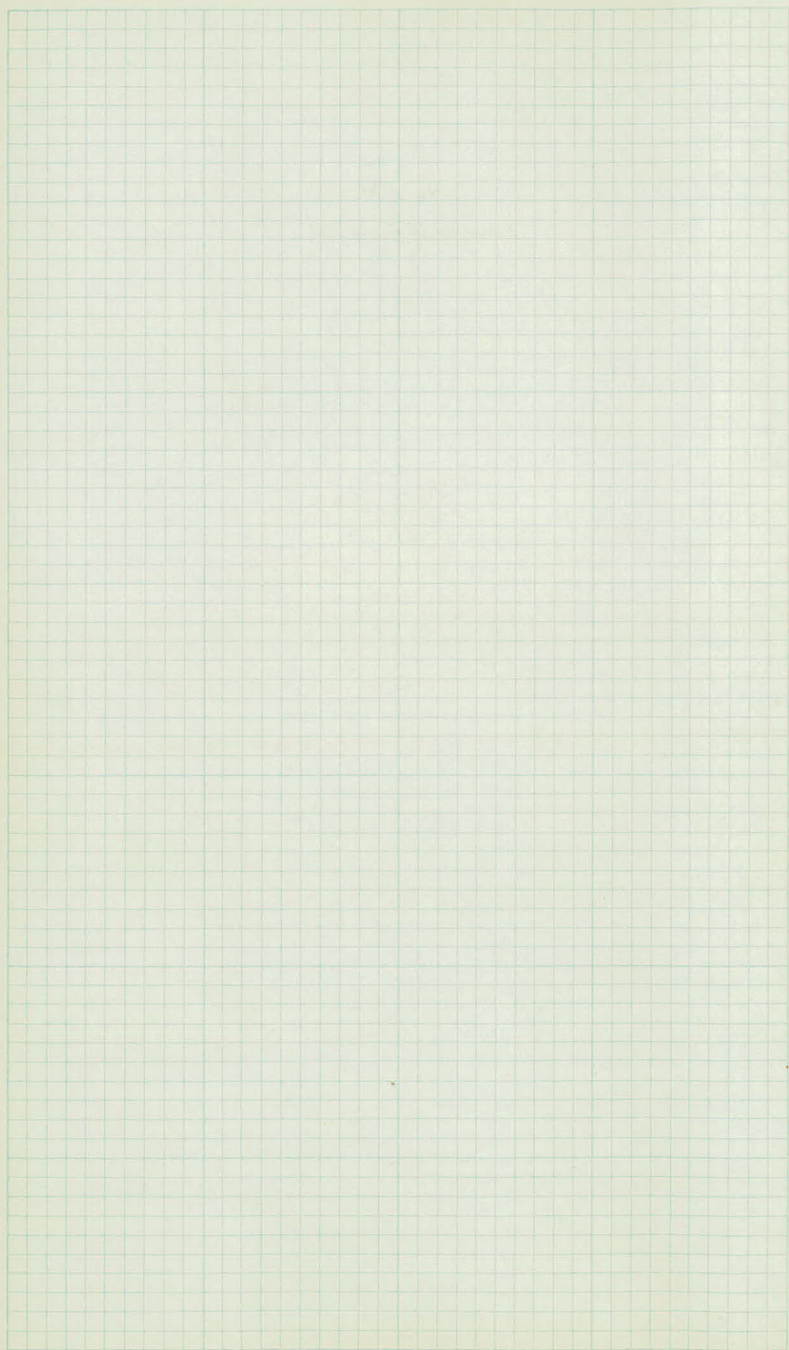
0+00 12' 12'

Cult.

Hay Land

Cult.





5

Topography  
Lower Afton Rd.

5 13' 11' Chr. 15' X 24' 6.14.22'  
+93-Longe T. 1 cto Ent.

4 12' 11'  
+85-T.P.-36'

3 13' 13'

2 14' 13' +02-T.P.-33'

1 13' 13'

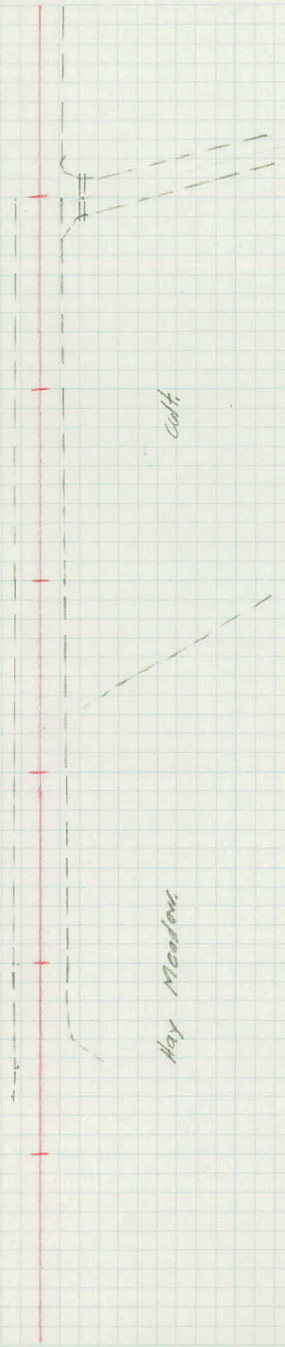
15' +62-

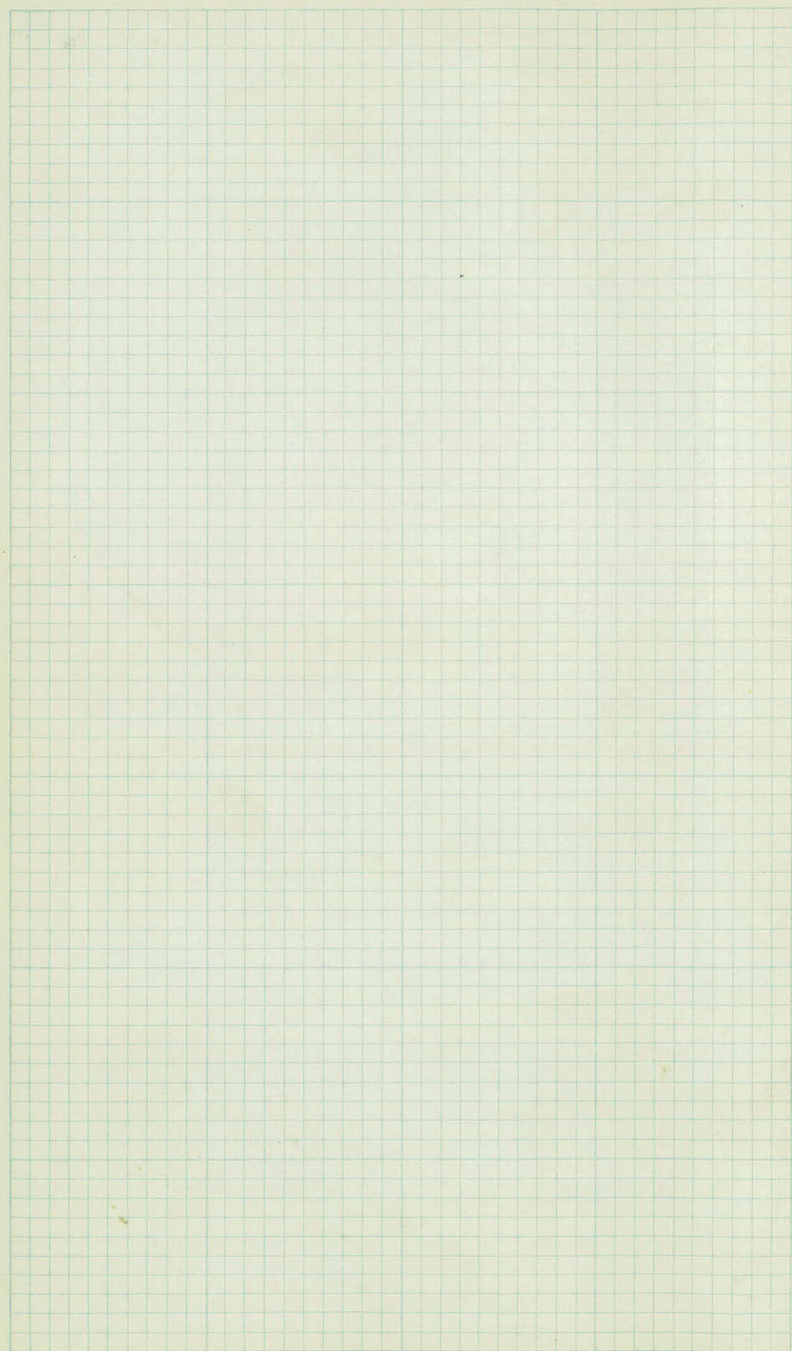
1  
of 100  
+45- 12'  
+50- 13'

Cult.

Cult.

Hay Meadow





X sections  
E. Co. Line

| Sta  | +    | -       | Elev      |
|------|------|---------|-----------|
| B.M. | 8.62 | 1039.01 | (1030.39) |

|   |     |  |      |
|---|-----|--|------|
| 0 | +00 |  | 30.4 |
|---|-----|--|------|

|  |     |     |      |
|--|-----|-----|------|
|  | +50 | 8.7 | 30.3 |
|--|-----|-----|------|

|   |  |     |      |
|---|--|-----|------|
| 1 |  | 8.7 | 30.3 |
|---|--|-----|------|

|  |     |     |      |
|--|-----|-----|------|
|  | +50 | 8.4 | 30.6 |
|--|-----|-----|------|

|   |  |  |      |
|---|--|--|------|
| 2 |  |  | 31.3 |
|---|--|--|------|

|  |     |  |      |
|--|-----|--|------|
|  | +50 |  | 32.6 |
|--|-----|--|------|

|   |  |  |      |
|---|--|--|------|
| 3 |  |  | 34.0 |
|---|--|--|------|

|  |      |  |      |
|--|------|--|------|
|  | +1.3 |  | 34.5 |
|--|------|--|------|

|  |      |  |      |
|--|------|--|------|
|  | +3.4 |  | 35.4 |
|--|------|--|------|

|  |      |  |      |
|--|------|--|------|
|  | +9.5 |  | 35.8 |
|--|------|--|------|

|  |      |  |      |
|--|------|--|------|
|  | +8.9 |  | 36.9 |
|--|------|--|------|

|      |      |           |      |           |
|------|------|-----------|------|-----------|
| T.P. | 9.60 | 1046.73 ✓ | 1.88 | 1037.13 ✓ |
|------|------|-----------|------|-----------|

Lt

Z

Rt

$$\frac{110}{50} \quad \frac{104}{50} \quad \frac{102}{21} \quad \frac{86}{13} \quad \frac{81}{9} \quad \frac{77}{11} \quad \frac{77}{18} \quad \frac{79}{20} \quad \frac{86}{26} \quad \frac{84}{26} \quad \frac{86}{50}$$

$$\frac{98}{50} \quad \frac{91}{30} \quad \frac{92}{20} \quad \frac{73}{17} \quad \frac{66}{10} \quad \frac{64}{11} \quad \frac{64}{17} \quad \frac{67}{20} \quad \frac{75}{27} \quad \frac{72}{27} \quad \frac{73}{50}$$

$$\frac{79}{50} \quad \frac{74}{33} \quad \frac{73}{20} \quad \frac{62}{17} \quad \frac{54}{10} \quad \frac{50}{10} \quad \frac{51}{19} \quad \frac{52}{23} \quad \frac{60}{43} \quad \frac{60}{43} \quad \frac{53}{50}$$

$$\frac{71}{50} \quad \frac{67}{33} \quad \frac{69}{21} \quad \frac{54}{17} \quad \frac{48}{10} \quad \frac{45}{11} \quad \frac{45}{27} \quad \frac{45}{27} \quad \frac{34}{50}$$

$$\frac{59}{50} \quad \frac{56}{38} \quad \frac{57}{27} \quad \frac{47}{21} \quad \frac{38}{9} \quad \frac{36}{10} \quad \frac{36}{29} \quad \frac{35}{46} \quad \frac{38}{46} \quad \frac{48}{50}$$

$$\frac{50}{50} \quad \frac{53}{45} \quad \frac{53}{37} \quad \frac{41}{32} \quad \frac{33}{9} \quad \frac{32}{10} \quad \frac{32}{32} \quad \frac{39}{34} \quad \frac{44}{43} \quad \frac{45}{43} \quad \frac{28}{47} \quad 4.0.$$

$$\frac{39}{30} \quad \frac{37}{29} \quad \frac{23}{8} \quad \frac{21}{10} \quad \frac{22}{23} \quad \frac{28}{28} \quad \frac{05}{28} \quad \frac{08}{50}$$

| Sta | + | $\pi$ | - | Elev |
|-----|---|-------|---|------|
|-----|---|-------|---|------|

|  |  |           |  |  |
|--|--|-----------|--|--|
|  |  | 1046.73 ✓ |  |  |
|--|--|-----------|--|--|

|   |  |  |  |      |
|---|--|--|--|------|
| 4 |  |  |  | 37.1 |
|---|--|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +17 |  |  | 37.5 |
|--|-----|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +32 |  |  | 37.9 |
|--|-----|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 5 |  |  |  | 39.9 |
|---|--|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +50 |  |  | 41.4 |
|--|-----|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 6 |  |  |  | 42.7 |
|---|--|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +50 |  |  | 43.9 |
|--|-----|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 7 |  |  |  | 44.9 |
|---|--|--|--|------|

|     |      |         |       |         |
|-----|------|---------|-------|---------|
| T.R | 1.25 | 1037.06 | 10.92 | 1035.81 |
|-----|------|---------|-------|---------|

|      |  |  |      |                     |
|------|--|--|------|---------------------|
| B.M. |  |  | 6.65 | 1030.41 ✓ (1030.39) |
|------|--|--|------|---------------------|

Lt.

C

Rt.

|                  |                  |                 |                  |                  |                |                 |                 |                  |                  |                 |                 |
|------------------|------------------|-----------------|------------------|------------------|----------------|-----------------|-----------------|------------------|------------------|-----------------|-----------------|
| $\frac{110}{50}$ | $\frac{101}{32}$ | $\frac{90}{28}$ | $\frac{107}{24}$ | $\frac{108}{16}$ | $\frac{98}{7}$ | $\frac{96}{10}$ | $\frac{98}{17}$ | $\frac{100}{22}$ | $\frac{104}{22}$ | $\frac{77}{29}$ | $\frac{81}{50}$ |
|------------------|------------------|-----------------|------------------|------------------|----------------|-----------------|-----------------|------------------|------------------|-----------------|-----------------|

|                 |                 |                 |                  |                 |                 |                 |                 |                  |                 |                 |
|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|
| $\frac{86}{50}$ | $\frac{75}{40}$ | $\frac{69}{28}$ | $\frac{102}{22}$ | $\frac{95}{10}$ | $\frac{92}{10}$ | $\frac{93}{17}$ | $\frac{96}{21}$ | $\frac{100}{30}$ | $\frac{65}{50}$ | $\frac{69}{50}$ |
|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|

|                 |                 |                 |                 |                 |                 |                 |                 |                 |                 |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| $\frac{70}{50}$ | $\frac{62}{28}$ | $\frac{97}{22}$ | $\frac{91}{11}$ | $\frac{88}{11}$ | $\frac{89}{11}$ | $\frac{91}{17}$ | $\frac{98}{21}$ | $\frac{52}{31}$ | $\frac{55}{50}$ |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|

|                 |                 |                 |                 |                |                 |                 |                 |                 |                 |                 |
|-----------------|-----------------|-----------------|-----------------|----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| $\frac{57}{50}$ | $\frac{47}{28}$ | $\frac{76}{22}$ | $\frac{71}{11}$ | $\frac{68}{9}$ | $\frac{68}{16}$ | $\frac{71}{19}$ | $\frac{81}{21}$ | $\frac{77}{33}$ | $\frac{23}{50}$ | $\frac{23}{50}$ |
|-----------------|-----------------|-----------------|-----------------|----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|

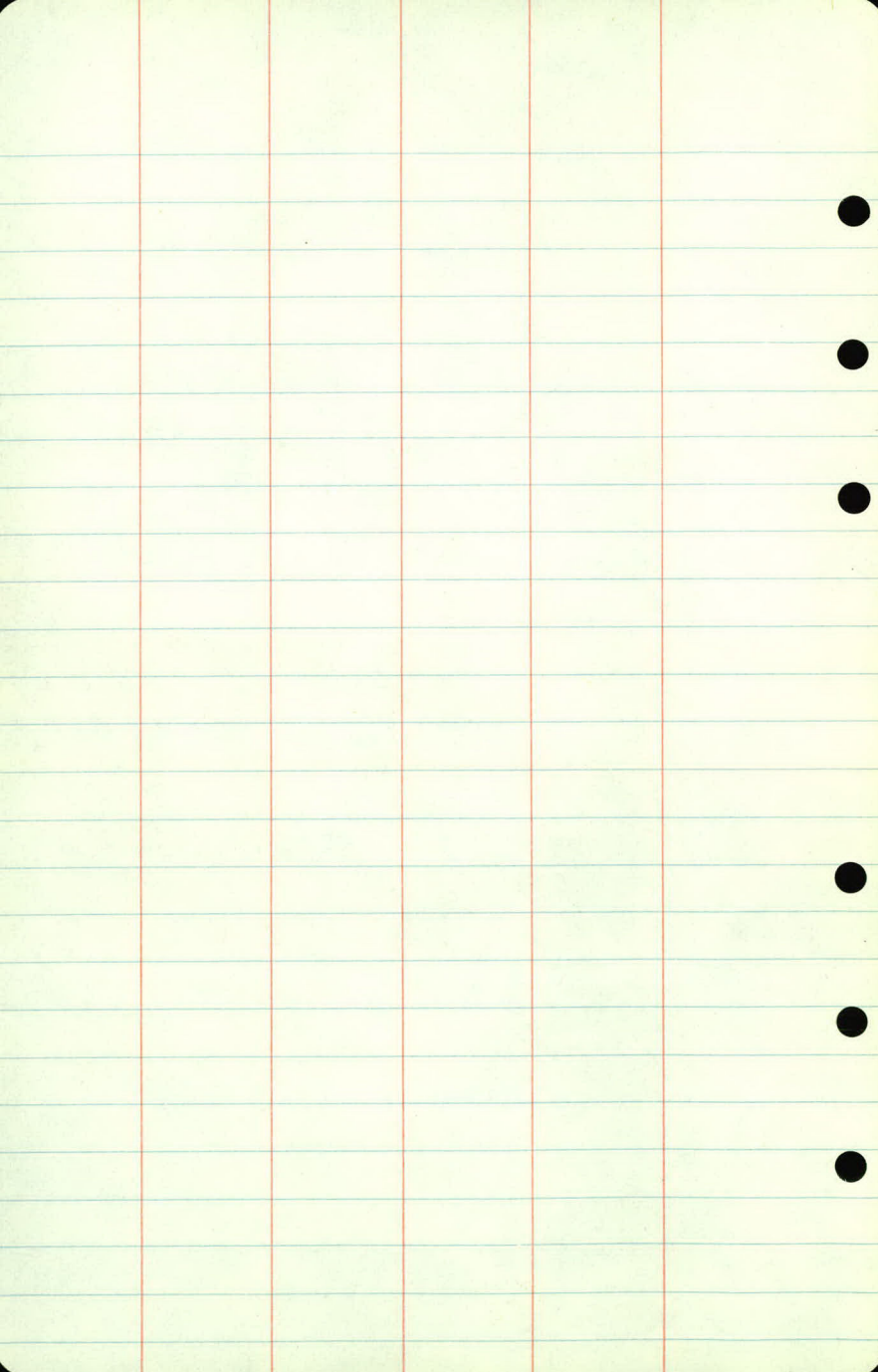
|                 |                 |                 |                 |                 |                 |                 |                 |                 |                 |                 |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| $\frac{48}{50}$ | $\frac{35}{27}$ | $\frac{63}{20}$ | $\frac{57}{10}$ | $\frac{53}{11}$ | $\frac{55}{16}$ | $\frac{58}{19}$ | $\frac{67}{21}$ | $\frac{64}{32}$ | $\frac{16}{50}$ | $\frac{12}{50}$ |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|

|                 |                 |                 |                 |                 |                 |                 |                 |                 |                 |                  |                  |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|------------------|------------------|
| $\frac{54}{50}$ | $\frac{43}{23}$ | $\frac{52}{20}$ | $\frac{47}{16}$ | $\frac{44}{10}$ | $\frac{40}{10}$ | $\frac{42}{15}$ | $\frac{45}{18}$ | $\frac{54}{21}$ | $\frac{54}{32}$ | $\frac{105}{50}$ | $\frac{110}{50}$ |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|------------------|------------------|

|                 |                 |                 |                 |                 |                |                 |                 |                 |                 |                  |
|-----------------|-----------------|-----------------|-----------------|-----------------|----------------|-----------------|-----------------|-----------------|-----------------|------------------|
| $\frac{68}{50}$ | $\frac{51}{21}$ | $\frac{39}{18}$ | $\frac{32}{10}$ | $\frac{28}{10}$ | $\frac{29}{9}$ | $\frac{31}{16}$ | $\frac{42}{19}$ | $\frac{42}{21}$ | $\frac{17}{27}$ | $\frac{0.7}{50}$ |
|-----------------|-----------------|-----------------|-----------------|-----------------|----------------|-----------------|-----------------|-----------------|-----------------|------------------|

1.8

Top Mont. E. 1/4 Cor. Sec. 12



X Sections

Lower Afton Road.

| Sta  | +     | $\pi$   | -   | Elev |             |
|------|-------|---------|-----|------|-------------|
| B.M. | 10.86 | 1041.25 |     |      | (1030.39) ✓ |
| 0    | +00   | 5       |     | 35.8 |             |
|      | +30   | +70     |     | 36.0 |             |
|      | +49   | +51     |     | 35.8 |             |
|      | +62   | 738     |     | 35.6 |             |
| 1    |       | 4+00    |     | 35.1 |             |
|      | +50   | +50     |     | 34.4 |             |
| 2    |       | 3       |     | 33.9 |             |
|      | +50   | +50     |     | 33.6 |             |
| 3    |       | 2       |     | 33.0 |             |
|      | +50   | +00     | 9.0 | 32.3 |             |
| 4    |       | 1       | 9.6 | 31.7 |             |

R+

L+

(Lt.)

R

(RH)

Top Mont. E. 1/4 Cor. Sec. 12

$$\frac{96}{50} \frac{92}{40} \frac{77}{32} \frac{71}{26} \frac{62}{18} \frac{55}{10}$$

$$\frac{92}{40} \frac{77}{32}$$

$$\frac{92}{50} \frac{77}{27} \frac{77}{17} \frac{65}{14} \frac{59}{8} \frac{53}{20} \frac{50}{33} \frac{45}{50}$$

$$\frac{90}{50} \frac{74}{27} \frac{75}{16} \frac{61}{12} \frac{55}{11} \frac{56}{18} \frac{60}{23} \frac{60}{30} \frac{54}{50}$$

$$\frac{87}{50} \frac{72}{24} \frac{76}{16} \frac{62}{14} \frac{57}{9} \frac{59}{14} \frac{62}{28} \frac{52}{44} \frac{21}{50}$$

$$\frac{90}{50} \frac{81}{39} \frac{77}{24} \frac{81}{20} \frac{81}{17} \frac{69}{15} \frac{62}{13} \frac{66}{26} \frac{58}{40} \frac{30}{50}$$

$$\frac{91}{50} \frac{84}{37} \frac{80}{25} \frac{87}{20} \frac{87}{18} \frac{76}{16} \frac{69}{17} \frac{74}{27} \frac{62}{47} \frac{26}{50}$$

$$\frac{100}{50} \frac{97}{34} \frac{91}{26} \frac{97}{21} \frac{95}{18} \frac{82}{16} \frac{74}{19} \frac{82}{27} \frac{74}{39} \frac{54}{50}$$

$$\frac{117}{50} \frac{113}{35} \frac{106}{25} \frac{106}{19} \frac{86}{15} \frac{77}{16} \frac{84}{18} \frac{94}{23} \frac{95}{37} \frac{84}{50}$$

$$\frac{127}{50} \frac{124}{36} \frac{117}{28} \frac{116}{19} \frac{92}{16} \frac{83}{16} \frac{92}{19} \frac{104}{20} \frac{104}{35} \frac{96}{50}$$

R+

L+

| Sta. | +   | $\pi$   | -     | Elev.                    |
|------|-----|---------|-------|--------------------------|
|      |     | 1041.25 |       |                          |
| 4    | 150 | +30     | 10.5  | 30.8                     |
|      | 188 |         | 13.20 | 28.05                    |
| 5    | 0   |         | 11.5  | 29.8                     |
| B.M. |     |         | 10.85 | 1030.40 . <u>1030.39</u> |

Flow Line East End 15' C.M.

Top Mont. E.  $\frac{1}{4}$  Cor. Sec. 12

| Sta   | +     | $\pi$   | - | Elev    |
|-------|-------|---------|---|---------|
| B.M.- | 13.23 | 1043.62 |   | 1030.39 |

|   |        |  |  |     |
|---|--------|--|--|-----|
| 3 | +67.44 |  |  | 345 |
|---|--------|--|--|-----|

|   |  |  |  |     |
|---|--|--|--|-----|
| 4 |  |  |  | 349 |
|---|--|--|--|-----|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +25 |  |  | 35.4 |
|--|-----|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +50 |  |  | 38.9 |
|--|-----|--|--|------|

|   |     |  |  |      |
|---|-----|--|--|------|
| 5 | +75 |  |  | 37.2 |
|---|-----|--|--|------|

|   |         |  |  |      |
|---|---------|--|--|------|
| 5 | +125.83 |  |  | 38.4 |
|---|---------|--|--|------|

|  |         |         |  |      |
|--|---------|---------|--|------|
|  | +125.83 | } Equa. |  | 39.3 |
|  | +170.08 |         |  |      |

1-29-41  
K.A.  
L.C.  
M.B.  
C.N.

Lt.

K.

Rt.

Top Mont E. 1/4 Cor Sec 12

$\frac{50}{50}$   $\frac{52}{47}$   $\frac{85}{27}$   $\frac{92}{20}$   $\frac{96}{14}$   $\frac{93}{11}$   $\frac{91}{12}$   $\frac{98}{16}$   $\frac{102}{19}$   $\frac{109}{25}$   $\frac{102}{50}$   $\frac{113}{50}$

$\frac{47}{50}$   $\frac{52}{43}$   $\frac{72}{29}$   $\frac{84}{20}$   $\frac{90}{7}$   $\frac{87}{8}$   $\frac{86}{8}$

$\frac{42}{50}$   $\frac{44}{40}$   $\frac{56}{26}$   $\frac{72}{14}$   $\frac{78}{7}$   $\frac{82}{13}$   $\frac{87}{30}$   $\frac{81}{30}$

$\frac{41}{71}$   $\frac{39}{50}$   $\frac{40}{21}$   $\frac{40}{9}$   $\frac{47}{11}$   $\frac{52}{18}$   $\frac{78}{25}$   $\frac{82}{31}$   $\frac{79}{41}$   $\frac{73}{41}$   $\frac{72}{50}$

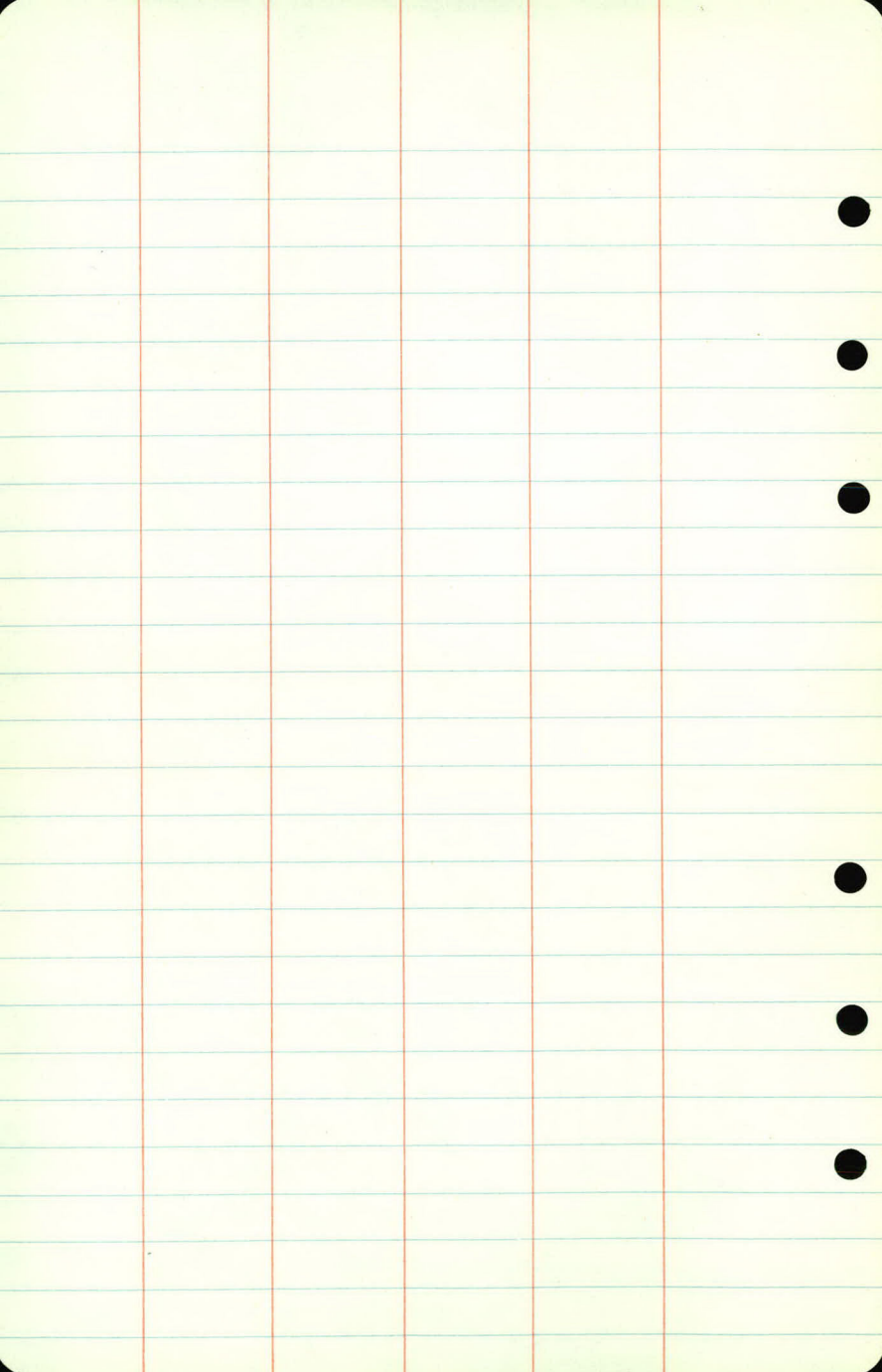
$\frac{37}{50}$   $\frac{32}{33}$   $\frac{28}{16}$   $\frac{64}{7}$   $\frac{64}{21}$   $\frac{62}{21}$

$\frac{34}{50}$   $\frac{23}{26}$   $\frac{60}{17}$   $\frac{52}{4}$   $\frac{51}{4}$

38.5

$\frac{32}{50}$   $\frac{20}{28}$   $\frac{56}{20}$   $\frac{48}{12}$   $\frac{43}{12}$

39.3



Topography  
Lower Afton Rd.

NE Knight Rd. to Century St.

12 Pages

Sta 61  
5+00

Lt

±

8' Ent Rt

5+00 Ent 27

+90 SE Cor Bar

12 10

105

12'

+68 SW Bar

+75

Ent 14

SW Cor HO

SE Cor HO

+68 Ent (Range Tie)

+12 75

+56 75

50

4+00

14

9

+91 PP 28

+91 PP 28

59

3+00

15 9

PP

+51 28

+86 NE Cor HO

3" Elm

+47 7" BE

+44 PP

63

+42 36 12" BE

+47 37

+44 22

+46 HO (NW Cor) 63

58

2+00

+99 31

15 9

HO (SW Cor)

+37 85

+52 NE Cor HO 63

+98 NW Cor HO 63

12' Ent

+41 16

57

1+00

+19.5

4' Wire Fe 28

+35 Fe Posts 63

+44 Fe Posts 63, 73, 83, 93, 103

PP

+11 28

16 8

+03 12' Ent 8

56

0+00

+87 HO 63

+61 HO 63

+60 End Radius 9

+16 Radius

15 +16 48

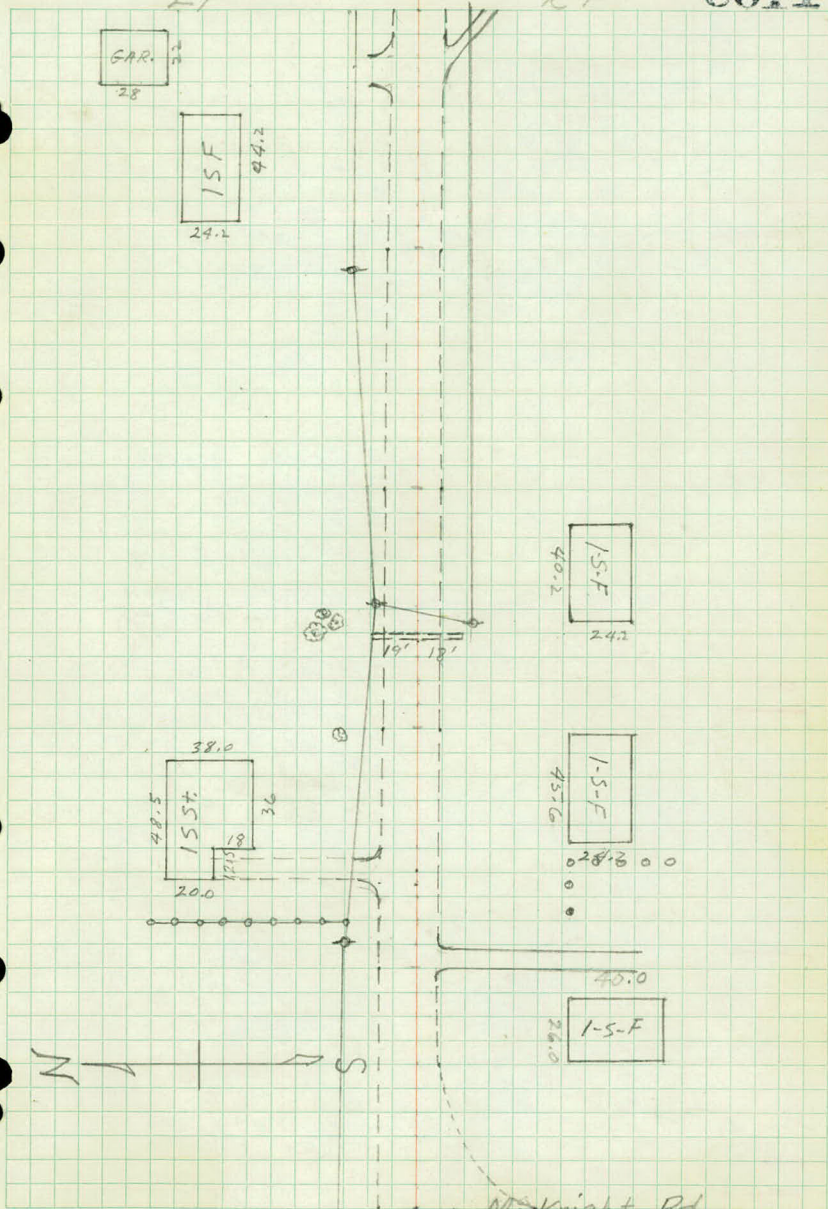
R6  
JH

Sept 4, 1959  
Cool, Clear  
Rt

CO11

Lt

+



Knight Rd.

Sta  
66  
~~10+00~~

• Fe Lt  
+00  $\frac{42}{27}$   
• PP  
+91  $\frac{27}{27}$

± RT  
12 11 +00  $\frac{BW Fe}{28}$

+68  $\frac{Stp}{38}$  +86  $\frac{Stp}{32}$   
+58  $\frac{Stp}{30}$

65  
~~9+00~~

• BW Fe  
+00  $\frac{39}{39}$

12 9 +00  $\frac{BW Fe}{27}$

64  
~~8+00~~

• Fe (BW)  
+08  $\frac{26}{26}$

BW Fence lying on ground loose,  
PP  $\frac{27}{27}$

11 10 +00  $\frac{23}{23}$   
• B.W. Fe Cor  
+76  $\frac{27}{27}$  (Rgetieat +80) +92  $\frac{14" Stump}{24}$   
• Ent (8")  
+60  $\frac{12}{12}$  (Rgetieat +69)

+60  $\frac{B.W. Fe Cor}{25}$  (Rgetieat +66)  
+26  $\frac{PP}{28}$

+39  $\frac{14" BE}{44}$  +43  $\frac{24" OAK}{35}$   
+11  $\frac{12" BE}{33}$  +25  $\frac{15" OAK}{33}$

63  
~~7+00~~

• 14" OAK  
+01  $\frac{32}{32}$

12 10

+75  $\frac{9" Elm}{41}$  +75  $\frac{End lilacs}{41}$

• PP  
+73  $\frac{27.5}{27.5}$

+38  $\frac{24" BE}{44}$  +38  $\frac{Begin lilacs}{44}$

62  
~~6+00~~

12 11 +05  $\frac{10" Elm}{41}$

+77  $\frac{24" Elm}{41}$

• 13" tree  
+59  $\frac{59}{59}$

61  
~~5+00~~

• PP  
+33  $\frac{23}{23}$  +37  $\frac{18" Elm}{39}$

12 10

R6  
JH

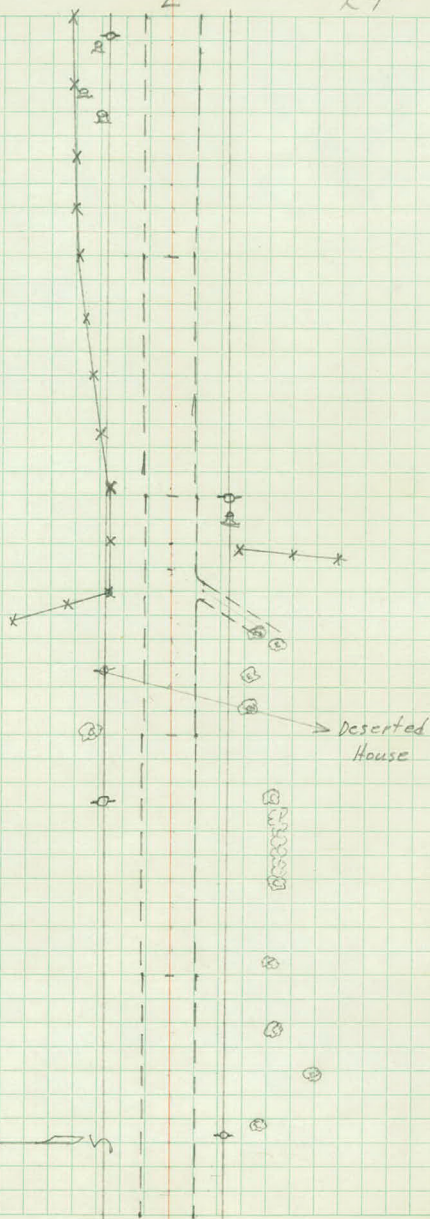
Sept 4, 1959

Lt.

E

Rt

~~0012~~



N S

|                   |                       |       |                         |
|-------------------|-----------------------|-------|-------------------------|
| Sta 71            | Lt.                   | 2     | Rt.                     |
| <del>15</del> +00 | +00 $\frac{BWFe}{26}$ | 11 10 | +00 $\frac{Fe(Bw)}{25}$ |

+13  $\frac{BWFe}{24}$   
+26 24

Iron Fe Posts  
+50 24

+18  $\frac{30" OAK}{29}$

~~40~~  
~~14~~+00

12 9

+81  $\frac{PP}{25}$

+18  $\frac{Fe Cor}{43.5}$   
PP  
+06 27

~~69~~  
~~13~~+00

+00  $\frac{Fe}{34}$

12 9

~~68~~  
~~12~~+00

+00  $\frac{Fe}{37}$

12 10

+49  $\frac{Fe Cor. (end)}{20}$

~~67~~  
~~11~~+00

+00  $\frac{Fe}{42}$

12 10

+86  $\frac{STP}{25}$

+93  $\frac{STP}{28}$

+90  $\frac{PP}{24}$

+59  $\frac{STP}{27}$

+79  $\frac{STP}{28}$

+38  $\frac{STP}{35}$

+14  $\frac{STP}{32}$

~~66~~  
~~10~~+00

+00  $\frac{Fe}{42}$

12 11+00  $\frac{BWFe}{28}$

RG  
JH

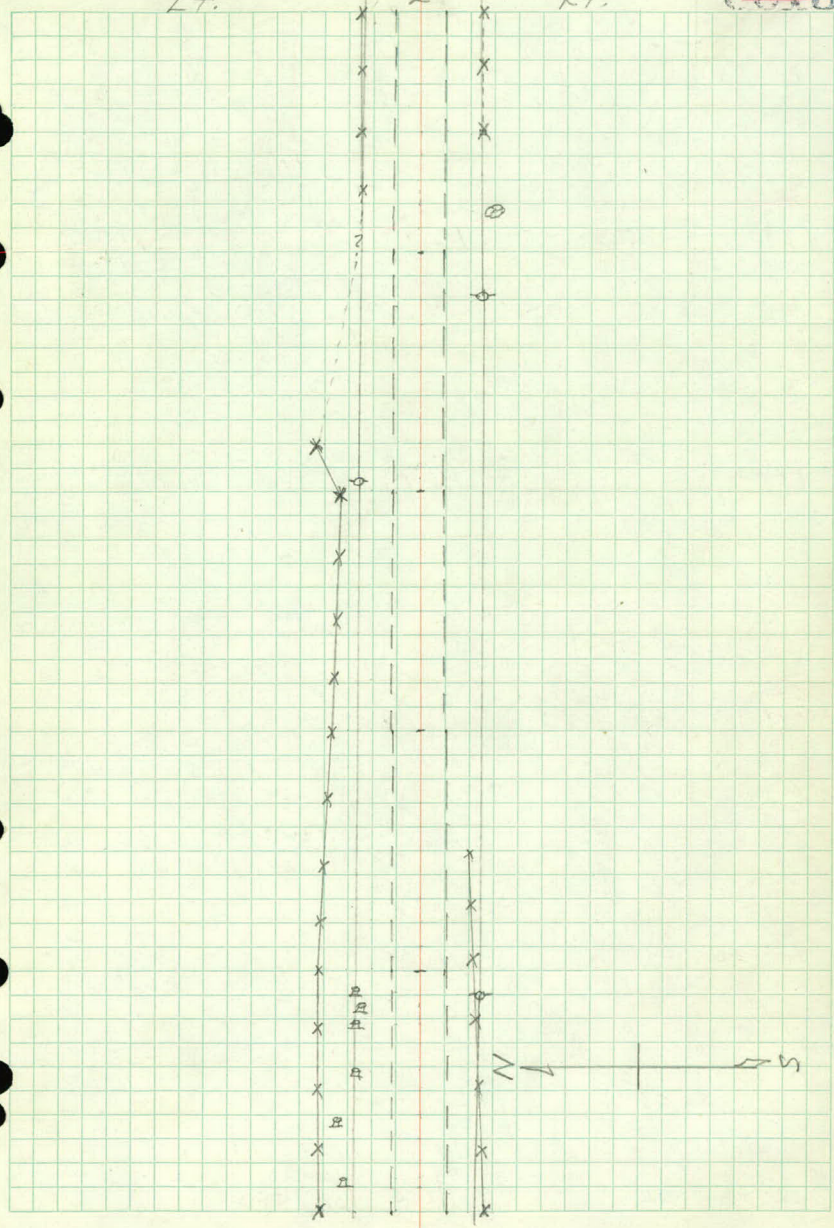
Sept 4<sup>th</sup>, 1959

~~6618~~

Lt.

£

Rt.



Lt.

£.

Rt.

20+00

End Small Tree clumps 12 11  
+80 22

PP  
+17 28

19+00

TP  
+18 27  
+06 End Culv (15" X 30' OM)  
13 11 24  
112' B.T. Eat  
+92 22  
Begin Culv 15" X 30' OM  
+76 25 +81 54 14" Elm

Begin small tree clumps  
+00 27

18+00

Fe Cor 12 9  
+75 35

PP  
+80 26  
Fe Cor BW  
+70 31  
24" Oak  
+06 29 +55 31 27" Oak

17+00

BW Fe  
+00 35

11 10

+00 BW Fe  
30

TP  
+25 27

PP  
+40 26  
BE (Multiple 6")  
+18 51 3" Elm  
Twin 4" BE  
+07 36 +25 45

16+00

BW Fe  
+00 30

11 10

10" Elm +00 BW Fe  
+98 51 28

STP  
+68 30

15+00

BW Fe  
+00 26

11 10

+00 BW Fe  
25

RG  
JH

Sept 4, 1959

 $\neq$ 

27.

Rt.

~~0014~~

Open Field

To House



Lt.

E.

Rt.

25+00

$$\begin{array}{r} 10P12'' \times 24' CM \\ +99 \quad 21 \end{array}$$

12 11

$$\begin{array}{r} +34 \quad \frac{PP}{28} \end{array}$$

24+00

12 11

$$\begin{array}{r} +02 \quad \frac{PP}{28} \end{array}$$

23+00

12 11

$$\begin{array}{r} +21 \quad \frac{PP}{27} \end{array}$$

22+00

12 11

$$\begin{array}{r} +75 \quad \frac{PP}{27} \end{array}$$

21+00

12 11

$$\begin{array}{r} +46 \quad \frac{PP}{27} \end{array}$$

20+00

12 11

RG  
KJ  
JH

Lt.

£

Sept 14, 1937  
Cool, Breezy  
Rt.

~~6015~~

N

3

Open Field

30+00 Lt.  $\frac{Fe}{13}$  4 18 +00  $\frac{Fe}{29}$  Rt

29+00  $\frac{Fe}{17}$  7 16 +00  $\frac{Fe}{28}$   
 PP  
 +92 29

PP  
 +32 15

28+00  $\frac{Fe}{20}$  9 14 +00  $\frac{Fe}{27}$

27+00 +00  $\frac{Fe}{24}$  11 13 +00  $\frac{Fe}{26}$   
 +53 G.L. Pipe Line  $\frac{Fe}{26}$  Cor G.L. Pipe Line PP  
 +05 INP 12" x 25' CM (24 x 24)  $\frac{Fe}{26}$  Cor +96 29  
 +03 14" Cott. SW Cor Gar. +36  
 +05 SEC Cor Ho INP  
 +14 Ent. (10') +05 11 6 15" x 20' CM  
 +11 22

26+00 +99 34 14" Elm 11 12  
 +80 34 14" Tree +90 98  
 SW Cor Ho (53 x 24)  
 +52 116  
 +24 PP  
 +23 29

E. End 12" x 24' CM  
 +23 21 +12 10' Ent

25+00 12 11

RE  
KJ  
JH

Sept 14, 1959

Lt.

L

Rt.

~~1959~~

Pasture

Pasture

St. Lakes Pipe Line

To House

1-5-5

53

60' x 120'

35+00

Lt.  $\frac{Fe}{143}$

10 13  $\frac{Fe}{36}$

Rt.

+50 200  $\frac{6 Trees}{36-59}$

+50  $\frac{Fe}{132}$

(+50)  
10 13

+50  $\frac{Fe}{31}$

+50  $\frac{16" Oak}{45}$

+43  $\frac{PP}{130}$

+8-12  $\frac{3-16" Oak}{27-30}$

34+00  $\frac{Fe}{121}$

R.T. +36 No End

10 12

+00  $\frac{Fe}{25}$

7 Trees (33+50 to 34+00)  
25-38  
So. End Vitrified!  
So. End only Rt. +36

+32  $\frac{15" \times 42' CM. (Imp)}{21}$

+41

+50  $\frac{Fe}{110}$

Twin

+32  $\frac{14" BE}{94}$

+32  $\frac{6" BE Group}{41}$

(+50)  
10 12

+48

Begin Fe at 24" BE

+28  $\frac{Twin 10" BE}{91}$

5" Plum

+28  $\frac{14" BE}{85}$

+28

+38  $\frac{retaining Rip Rap Wall}{21-33}$

12" x 23' Vit. (Imp)

33+00

+00  $\frac{Fe}{96}$

10 12

+28

26

+50  $\frac{Fe}{79}$

+50  
11 13

+84

NW Cor Bar  
 $\frac{66}{66}$

(24'E-W 22' N-S)  
R.T. +64

32+00

+00  $\frac{Fe}{53}$

8 15

+17

Twin 6"  $\frac{Cott.}{35}$

+92

18" Elm  
 $\frac{36}{36}$

+50  $\frac{Fe}{32}$

+50  
5 20

+56

Triple Elm  
 $\frac{6"-9" \times 12"}{36}$

+13  $\frac{PP}{25}$

31+00

+00  $\frac{Fe}{20}$

2 20

+61-85  $\frac{29}{29}$

INP 15" x 24' CM

+64  $\frac{30" BE}{41}$

+50  $\frac{Fe}{14}$

(3 20)  
+50

+50

+59

End of Fe  
 $\frac{32}{32}$

+87

24" BE  
 $\frac{42}{42}$

+74 10' End

+42  $\frac{PP}{32}$

30+00

+00  $\frac{Fe}{13}$

4 18

+00  $\frac{Fe}{29}$

Sept. 14, 1959

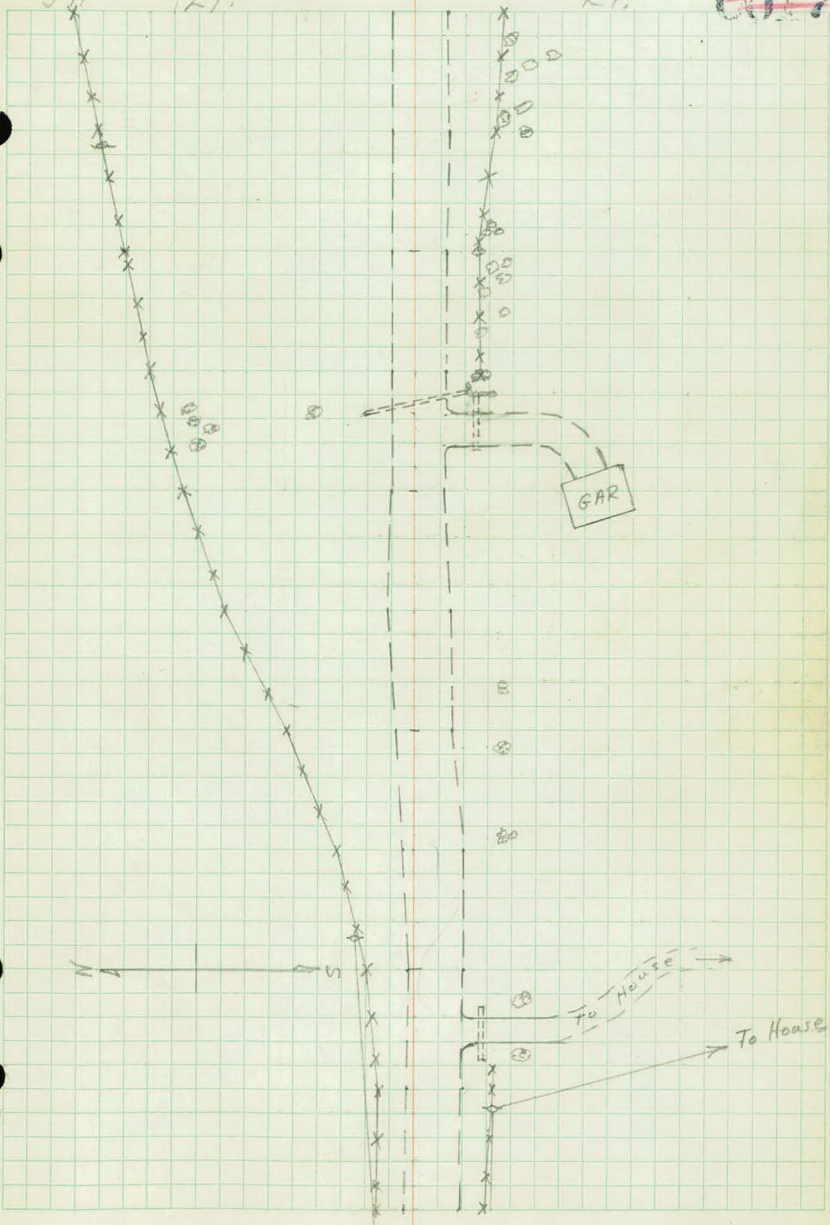
~~CO17~~

R6  
KJ  
JH

Lt.

£

Rt.



40700

$$L.f. = \frac{Fe}{+ \infty} = \frac{Fe}{31} = 7.13$$

$$\begin{array}{r} \text{Pt.} \\ \text{Fe cor} \\ \hline 24 \end{array}$$

$$+50 \frac{\text{Fe}}{25} \cdot \left( \frac{+50}{9/5} \right) + 50 \frac{\text{Fe}}{27}$$

39+00

$$\begin{array}{r} \text{Fe} \\ +00 \quad \underline{23} \end{array} \quad 814 \quad \begin{array}{r} \text{Fe} \\ +00 \quad \underline{29} \end{array}$$

38700

$$\begin{array}{r} \text{Fe} \\ +00 \ 24 \\ \hline \end{array} \quad \begin{array}{r} \text{Fe} \\ +00 \ 28 \\ \hline \end{array} \quad \begin{array}{r} \text{Fe Cor} \\ +73 \ 26-169 \\ \hline \end{array}$$

39+00

$$\begin{array}{r} 10 \cdot 13 + 0 \cdot \frac{FE}{27} \\ + 50 \cdot 6 + 66 \\ \hline 5 \text{ Trees} \\ 28 - 45 \\ \hline \end{array}$$

36+00

$$\begin{array}{r} +00 \text{ } ^{\circ} \text{Fe} \\ \underline{161} \end{array} \quad \begin{array}{r} 1012 \text{ } ^{\circ} \text{Fe} \\ +00 \\ \underline{30} \end{array} \quad \begin{array}{r} 9 \text{ Trees} \\ \underline{30} \end{array}$$

$$\begin{array}{r} (+50) \\ 1012 \end{array} \quad \begin{array}{r} \text{Fe} \\ +50 \quad 32 \\ \hline 9 \text{ Trees} \\ +100 \text{ to } +50 \quad 32 - 54 \end{array}$$

35 + 00

$$\begin{array}{r} \text{Fe} \\ +00 \quad \hline 143 \end{array} \quad \begin{array}{r} \text{Fe} \\ +00 \quad \hline 36 \end{array}$$

$$Z$$

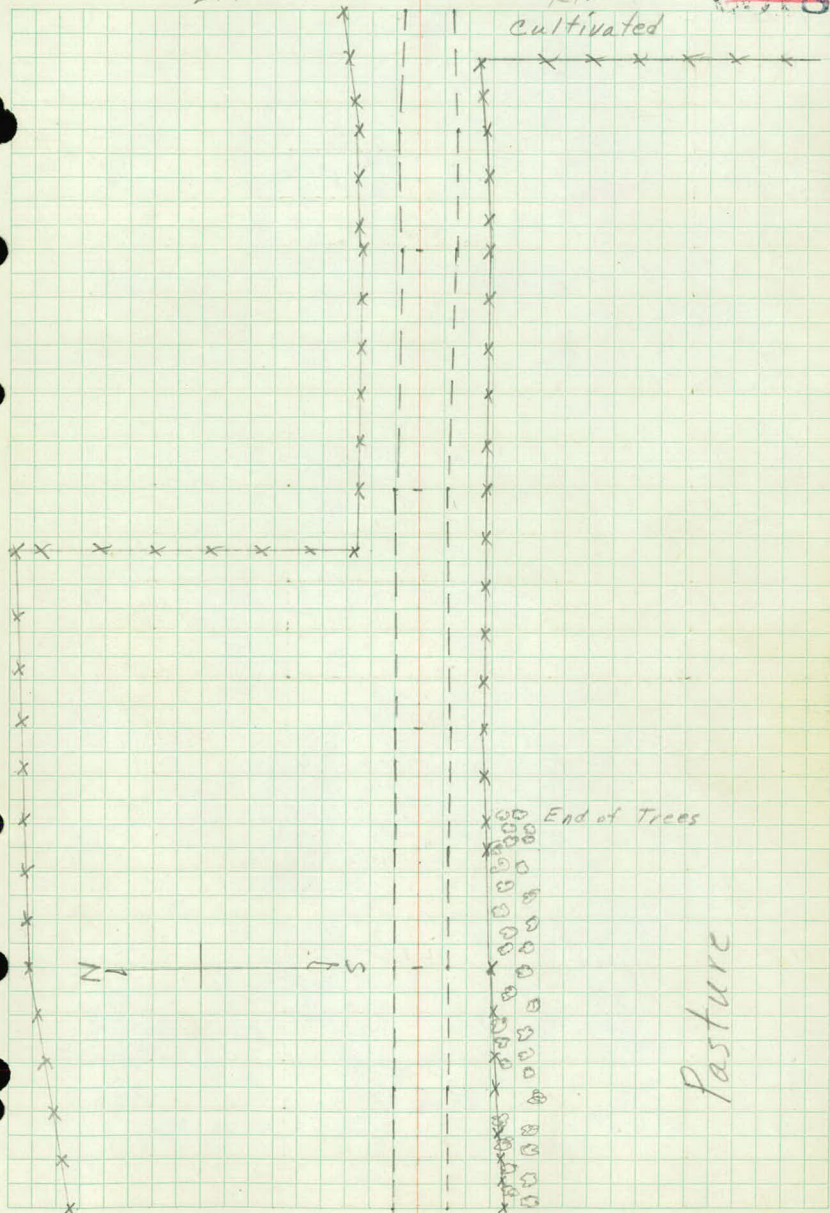
Sept 14, 1959

Warm

Rt.

cultivated

0018



Lt.

.4

Rt.

45+00

139

44+00

148

$$\begin{array}{r} \text{PP} \\ +61 \overline{34} \end{array}$$

43+00

148

42+00

139

+32 10' Ent

$$\begin{array}{r} \text{PP} \\ +39 \overline{38} \end{array}$$

$$\begin{array}{r} \text{PP} \\ +63 \overline{24} \end{array}$$

+03' End of Fc

58

$$\begin{array}{r} 26'' \text{ ORK} (+50) \\ +03 \overline{58} \quad (149) \end{array}$$

41+00

1410

$$\begin{array}{r} 10'' \text{ ORK} \\ +80 \overline{41} \end{array}$$

$$\begin{array}{r} \text{Fc} (+50) \\ +50 \overline{42} \quad (1311) \end{array}$$

40+00

$$\begin{array}{r} \text{Fc} \\ +00 \overline{31} \end{array}$$

713

R6  
KT  
IH

Sept, 14, 1959

Lt.

E

Rt.

~~CC49~~

Cultivated

Cultivated

N ——— S

To House

10  
x  
15  
x  
x  
x  
x  
x  
x

13

RT

50+00

14  
+85 Fe Line RT=50+10

66  
+94 10' ENT

+68

54  
29

RT. +00

+34

18" M  
29

+42 18" M  
29

+10 16" Maple  
28

+26 18" M  
29

49+00

7" Cott  
28

9 13

+78 24" ELM  
54

30" OAK

+56 28

PP

+27 14" BE  
27

+25 12" Maple  
23

+17 36

+11 24" Maple  
27

48+00

Fe. Cor

+92 42

11 +00

18" Maple  
23

+98 10' Ent.

47+00

FE  
+00 28

11 11

R.T. for fence

+03 25

46+00

+00 Fe  
25

12 9

Fe Cor

PP

+92 25

+88

35

45+00

13 9

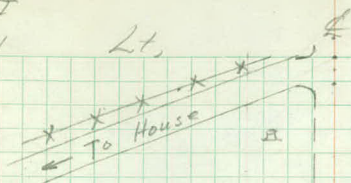
RG  
KI  
JH

Sept. 14, 1959

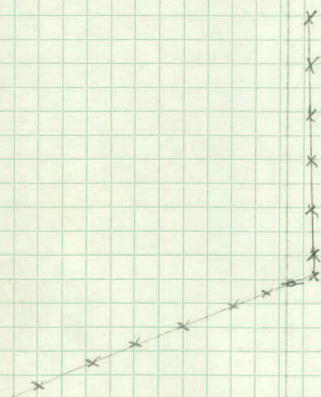
Lt,

Rt

~~CO20~~



N ——— W



Lt.  $\left( \begin{array}{l} +06 RT \\ +85 \text{ B.Rad} \\ 33 \end{array} \right)$   
 55+00 End Radius (R.T.)  
 +77  $\frac{53}{PP}$  End Radius  
 +45  $\frac{28}{56}$  46

Rt.  
 End Rad, in  
 Hwy 100  
 +77  $\frac{R.T.}{26}$   
 +89 End Radius

B.Rad RT+52.5  
 +20  $\frac{10}{38}$  Fe Cor  
 54+00 +00  $\frac{Fe}{30}$  10 14

B.Rad  
 +43 13

53+00 +00  $\frac{Fe}{31}$  11 13

End Trees  
 +25 115

52+00 +00  $\frac{Fe}{32}$  11 11  
 End Orchard  
 +85 150

51+00 +00  $\frac{Fe}{32.5}$  10 11

Orchard  
 +37  $\frac{100}{Tree Grove}$   
 +10  $\frac{88-95}{}$

50+00 +02  $\frac{Fe Cor}{33}$  13  
 RT +10

R6  
JH

Sept. 15, 1959  
470', Windy

~~0021~~

Lt  
# Hwy 100 = 54+92

Hwy 100

Z

Cultivated

Ent

Lt.

£

Rt.

56+00

11/12

$$\begin{array}{r} \text{PP} \\ +54 \quad 19 \end{array}$$

$$\begin{array}{r} 12'' \times 24' \text{ am } 1 \text{ up} \\ +42 \quad 14 \end{array}$$

$$\begin{array}{r} \text{E. Rad} \\ +34 \quad 11 \end{array}$$

$$\begin{array}{r} \text{E. Rad} \\ +39 \quad 12 \end{array}$$

55+00

+06 RT

$$\begin{array}{r} \text{B. Rad} \\ +26 \quad 40 \end{array} \quad \text{RT} +06$$

$$\begin{array}{r} \text{Beg Rad} \\ +85 \quad 33 \end{array}$$

R6  
JH

Lt.

±

Sept 15, 1959  
47° Windy  
Rt.

~~C022~~

