

Bk 70 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

Co. Rd. "A2"

From 1175' East Rice To 2000' Ea.

Road Acc't. No. 28

e Filed 6-11-41

File

PLAN SURVEY

C.O.R.D. "A" 2"

North side sta 11+75 to sta 20+00

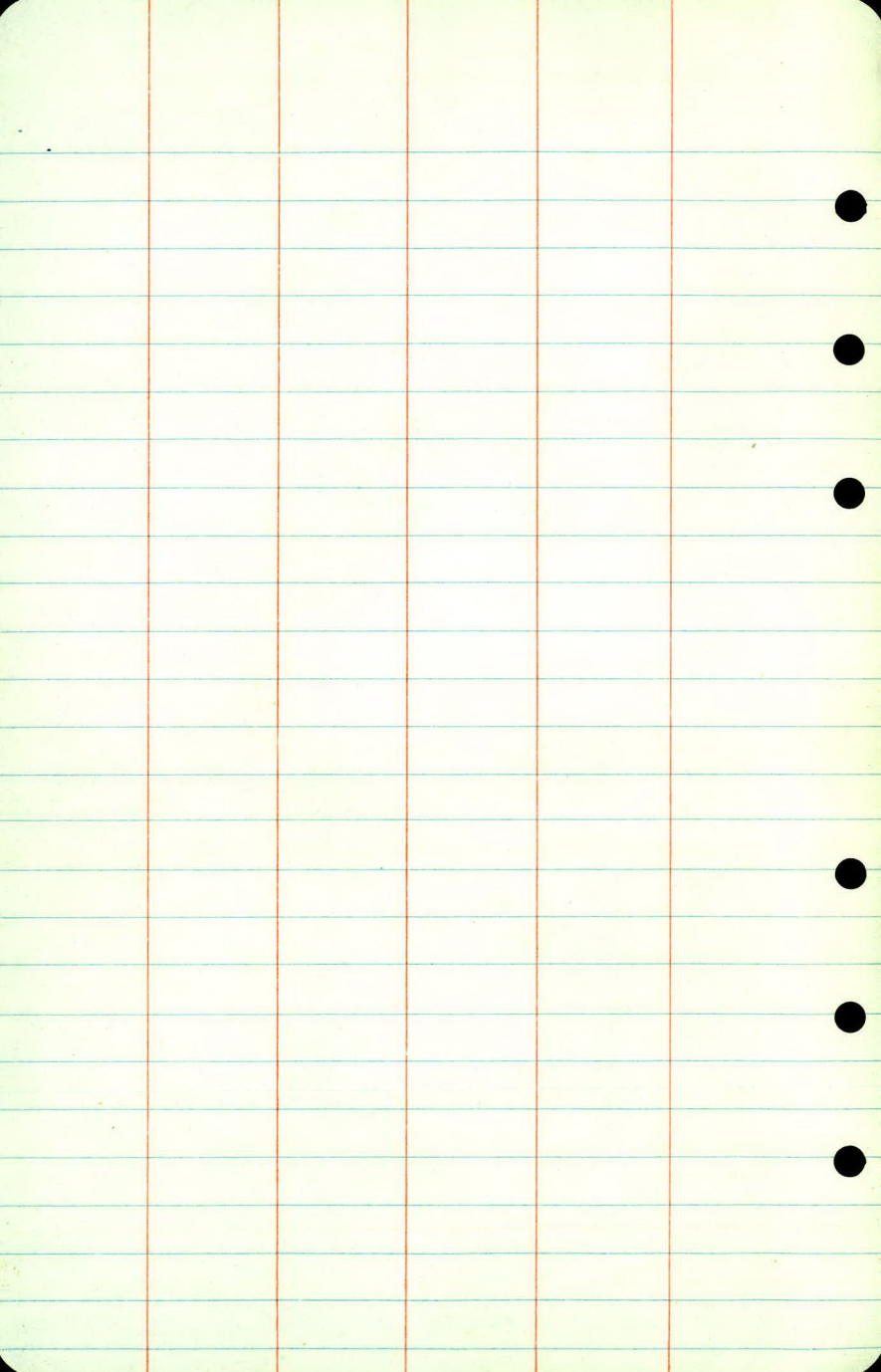
Drawn up
2/24/41

INDEX

Align. is same as 1933 Road Map Survey

Topog. - 1-3

Xsections - 4-8



2-11-41

1

Topography.

ROCK
TOP

+70-Beg Cable G.R.-12.1'

+50-G.R.-11.8'

16 G.R.-11.7' 8'

+50-G.R.-11.6'

+15-Beg G.R.-11.9'
15 +11-X Road Sign-24' 9'

14 10'

+50-End Fc-34.7'

13 Fc-34' 11'

12 12'
+87-Beg Fc-32.6' +90-End/Bed-19'
+92-End/18" C.M. X Drain-31'
+75-Gate Post-Beg Rod-33'
+65-Range TIC to E Shoulder Line

11

from x sections

Good

Water Dept. Rd.

No Plant or Cable

20 Beg. Fl. - 45' 11'

19 +08-End G.R. - 12.7'
G.R. - 12.9' 10'

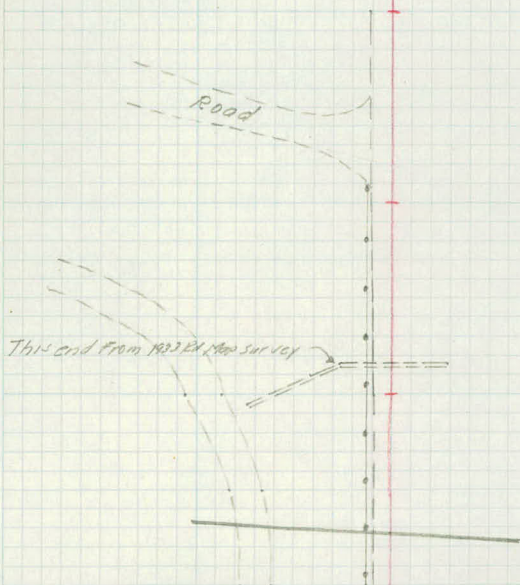
+50-G.R. - 12.3'

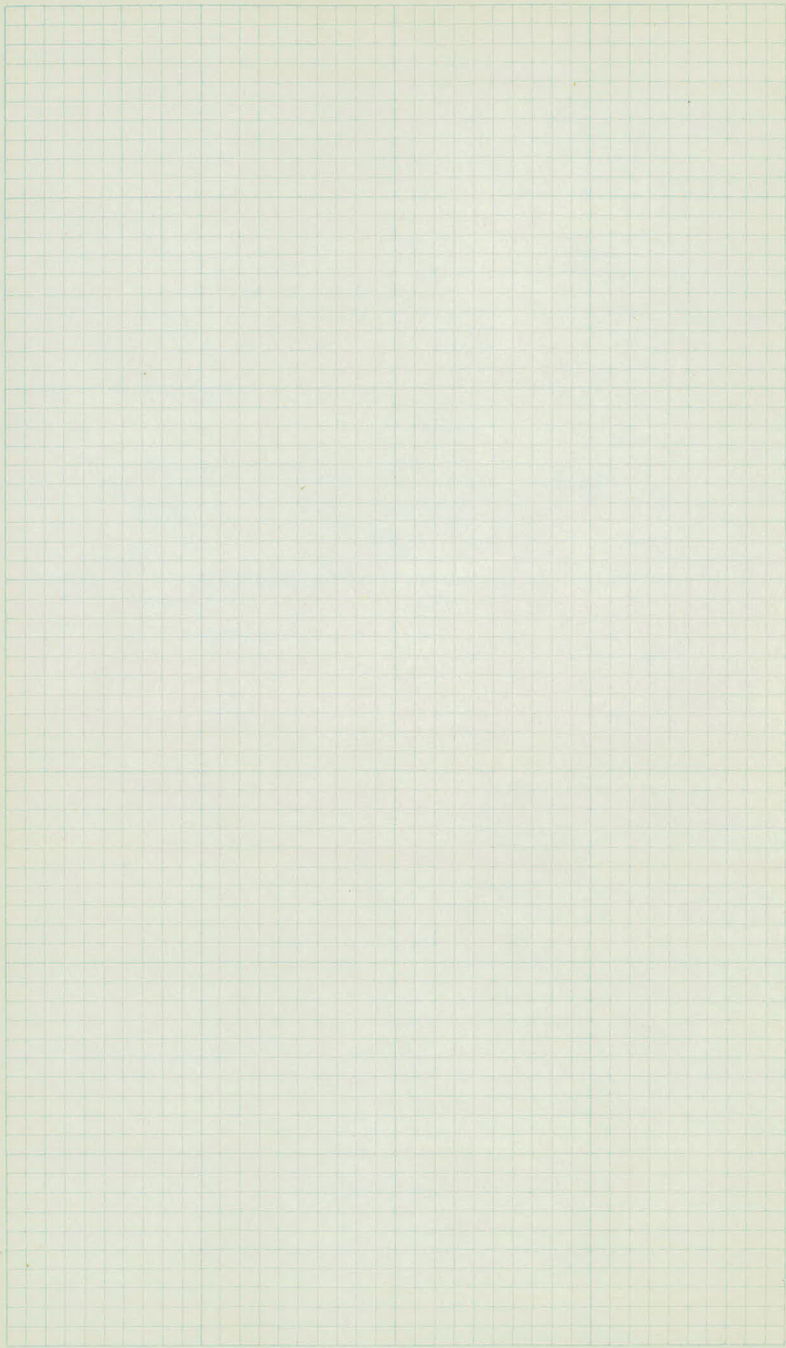
18 G.R. - 12.4' 9' +16-End 24" Cons. Culv. - 28'
+95-End 24" CM. Culv. - 74'

+50-G.R. - 12.2'

+33-End Sledge Pipe - 102' 8" C.I. Pipe
+27-Approx Xing of Sledge Pipe

17 G.R. - 12.2' 9'





X Sections

Sta	+	π	-	Elev
B.M.	8.66	870.95 ✓		862.29
T.P.	12.10	882.84 ✓	0.19	870.76 ✓
T.P.	13.34	896.06 ✓	0.14	882.72 ✓
B.M.	7.42	894.89 ✓	8.59	887.47 ✓

11 +75 91.7 ✓

+82 91.7

12 91.8

+25 92.0

+50 92.5

+85 93.0

13 93.3

+50 94.0

14 94.8

LT

R

Top Mont Rice St & Co Rd "A2"

Top N. End 18" G.M. X Drain It Sta. 11+82 (X Indicates Shoulder Line W. V. Pds.)

71	57	48	42	33	32
100	60	36	21	11	

	X		FL.						
71	64	58	90	8.90	73	39	33	32	
100	82	59	39	31	29	22	11		

	X								
104	87	116	110	42	42	50	41	34	31
150	121	103	85	40	25	24	18	12	

	X												
103	131	131	85	63	64	53	37	31	43	39	33	29	
146	140	133	119	105	100	76	47	32	24	18	12		

	X												
103	132	132	58	57	69	54	37	32	37	29	24		
141	134	128	109	103	94	51	32	23	20	12			

	X												
104	131	130	75	77	68	60	52	30	20	27	21	19	
134	127	121	107	100	82	60	51	31	21	20	12		

	X												
104	131	131	92	87	70	52	27	22	24	19	16		
131	124	119	106	100	76	48	29	22	21	12			

	X												
103	130	130	82	72	65	57	41	22	16	11	09		
112	105	99	85	61	55	53	32	18	17	10			

	X		X										
139	104	103	74	72	62	20	03	06	01				
118	115	100	81	67	48	29	23	12					

Sta	+	π	-	Elev
		894.89		
14	+50			95.6
15				96.5
T.P.	11.22	904.50	1.61	893.28
14	+50			95.6
15				96.5
	+27			96.8
	+50			97.1
16				97.8
	+36			98.1
17				98.9
	+50			99.2
18				99.4

snow & windy

2-13-41

R.F.

L.C.

G.W.

6

14

2

$$\frac{139}{83} \frac{80}{82} \frac{80}{59} \frac{128}{58} \frac{127}{32} \frac{88}{42} \frac{15}{32}$$

+0.7

$$\begin{array}{r} \times \\ 232 \quad 225 \quad 105 \quad 95 \quad 127 \quad 127 \quad 86 \\ 130 \quad 102 \quad 72 \quad 56 \quad 54 \quad 49 \quad 40 \end{array}$$

+1.6

R sta 12400

$$\frac{93}{16} \frac{92}{10} \frac{89}{}$$

$$\frac{79}{33} \frac{85}{20} \frac{83}{9} \frac{80}{}$$

$$\frac{82}{15} \frac{80}{9} \frac{77}{}$$

$$\frac{81}{15} \frac{77}{9} \frac{74}{}$$

$$\frac{74}{14} \frac{70}{9} \frac{67}{}$$

$$\frac{67}{13} \frac{66}{8} \frac{64}{}$$

$$\frac{60}{13} \frac{58}{8} \frac{56}{}$$

$$\frac{79}{23} \frac{58}{14} \frac{56}{8} \frac{53}{}$$

$$\frac{88}{42} \frac{71}{17} \frac{58}{14} \frac{54}{8} \frac{51}{}$$

Sta	+	π	-	Elev
		904.50		
18	+40			99.4.
19				99.6.
	+50			99.5.
T.P.	0.09	890.91	13.68	890.82
15	+27			96.8
	+50			97.1
16				97.8
	+36			98.1.
17				98.9.
	+50			99.2.
18				99.4.
T.P.	0.73	878.04	13.60	877.31

Lt

R

$$\text{Top Bank} \rightarrow \frac{81}{62} \frac{75}{38} \frac{71}{17} \frac{58}{14} \frac{54}{8} \frac{51}{1}$$

$$\frac{69}{50} \frac{66}{35} \frac{69}{17} \frac{53}{14} \frac{50}{9} \frac{49}{1}$$

$$\frac{73}{50} \frac{58}{48} \frac{55}{17} \frac{51}{10} \frac{50}{1}$$

$$\begin{array}{r} x \quad x \\ \frac{66}{73} \quad \frac{65}{58} \quad \frac{86}{52} \quad \frac{86}{47} \end{array}$$

+5.9

$$\begin{array}{r} x \quad x \\ \frac{64}{73} \quad \frac{64}{58} \quad \frac{88}{53} \quad \frac{86}{47} \end{array}$$

+6.2

$$\begin{array}{r} x \quad x \\ \frac{64}{75} \quad \frac{62}{80} \quad \frac{87}{54} \quad \frac{85}{48} \end{array}$$

+6.9

$$\begin{array}{r} x \quad x \\ \frac{68}{76} \quad \frac{64}{60} \quad \frac{83}{56} \quad \frac{84}{49} \end{array}$$

+7.2

$$\begin{array}{r} x \quad x \\ \frac{70}{78} \quad \frac{68}{62} \quad \frac{84}{58} \quad \frac{84}{52} \end{array}$$

+8.0

$$\begin{array}{r} x \quad x \\ \frac{67}{83} \quad \frac{66}{66} \quad \frac{80}{61} \quad \frac{80}{57} \end{array}$$

+8.3

$$\begin{array}{r} x \quad x \\ \frac{67}{106} \quad \frac{63}{88} \quad \frac{89}{83} \quad \frac{89}{77} \end{array}$$

+8.5

Sta	+	π	-	Elev
		878.04		

15	+27			96.8
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	+50			97.1
--	-----	--	--	------

16				97.8
----	--	--	--	------

	+36			98.1
--	-----	--	--	------

17				98.9
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	+50			99.2
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T.P.	12.48	890.52	0.00	878.04
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B.M.	6.69	894.16	3.08	887.44	887.47
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T.P.	1.41	881.94	13.63	820.53
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T.P.	1.65	870.87	12.72	869.22
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B.M.			8.58	862.29	862.29
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Lt.

L

$$\begin{array}{r} 61 \\ 130 \end{array} \quad \begin{array}{r} 58 \\ 104 \end{array}$$

+18.8

$$\begin{array}{r} 64 \\ 130 \end{array} \quad \begin{array}{r} 54 \\ 104 \end{array}$$

+19.1

$$\begin{array}{r} 66 \\ 130 \end{array} \quad \begin{array}{r} 54 \\ 105 \end{array}$$

+19.8

$$\begin{array}{r} 64 \\ 130 \end{array} \quad \begin{array}{r} 60 \\ 115 \end{array} \quad \begin{array}{r} 74 \\ 115 \end{array} \quad \begin{array}{r} 69 \\ 108 \end{array} \quad \begin{array}{r} 24 \\ 99 \end{array}$$

+20.1

$$\begin{array}{r} 73 \\ 130 \end{array} \quad \begin{array}{r} 61 \\ 106 \end{array} \quad \begin{array}{r} 18 \\ 96 \end{array}$$

+20.9

$$\begin{array}{r} 60 \\ 130 \end{array} \quad \begin{array}{r} 50 \\ 110 \end{array} \quad \begin{array}{r} 25 \\ 100 \end{array} \quad \begin{array}{r} 12 \\ 99 \end{array}$$

+21.2

Top N. End 18' C.M. X Drain Lt. 11+82

Top Meant Rice St. & Co Rd. "A2"

