

Bk. 7 - Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ SNELLING AVE _____

From Co. Rd. "F" _____ To Co. Rd. "G" _____

Road Acc't. No. 29 _____

Date Filed 10-26-39

File _____

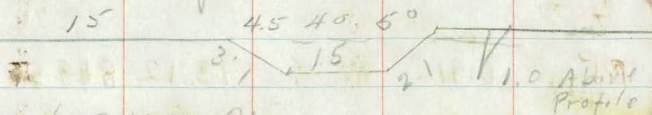
Slope stakes

Smelling Arc

Co Rd "F" To Co Rd G (5TH 96)



- 2:1 F. Slope Lt 2+50 to 6+50
- 2:1 F. Slope Lt 14+00 to 19+50
- 2:1 F Slope Rt 25+50 to 29+00
- 2:1 F Slope Lt 26+00 to 29+00



19+50 to 21+50 Rt

22+00 to 24+25 30+30 to 32+50

Sta	+	π	-	Elev	Grade Rod		
B.M	12.47	93200			919.53		
0+00	P.C. 407	923.60	59	18.5	12.7	13.5	14.3
+30							
+35				16.4	14.6-15.6-16.6		
T.P	5.86	936.05	1.81	930.19			
+35				16.4			20.7
T.P.	0.16	923.39	12.82	923.23			
1				12.6	9.8	10.8	11.8
T.P. B.T.	1.69	913.30	11.99	911.61			
+25				11.1	11.3	12.3	13.3
+50				09.6	12.8	13.8	14.8
T.P.	2.48	912.70	13.17	910.22			
2				06.7	5.1	6.0	6.9
+17	P.T.			05.7	6.2	7.0	7.8
+50				03.7	8.5	9.0	9.5
T.P	0.91	900.49	13.12	899.58			
3				00.8			00.5
T.P. B.T.	0.69	900.95	13.03	900.27			

Lt.

X

Rt

Ext Wid. Super Elev

Rt

Spk in 24" Oak 25' Lt Sta 0+70'

1.7	+1.8	-1.8	$\begin{array}{r} 4.2 \\ C 8.5 \\ \hline 33.0 \end{array}$	$\begin{array}{r} 13.0 \\ C 0.5 \end{array}$	$\begin{array}{r} 2.5 \\ C 11.8 \\ \hline 51.8 \end{array}$
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3.2	1.0	1.0	$\begin{array}{r} 6.2 \\ C 8.4 \\ \hline 33.0 \end{array}$	$\begin{array}{r} 14.8 \\ C 0.8 \end{array}$	
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 $\begin{array}{r} 2.7 \\ C 18.0 \\ \hline 65.7 \end{array}$

3.4	1.0	1.0	$\begin{array}{r} 10.0 \\ C 1.2 \\ \hline 24.1 \end{array}$	$\begin{array}{r} 5.5 \\ C 5.3 \end{array}$	$\begin{array}{r} 3.4 \\ C 8.4 \\ \hline 46.7 \end{array}$
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3.4	1.0	1.0	$\begin{array}{r} 12.1 \\ C 0.7 \\ \hline 24.9 \end{array}$	$\begin{array}{r} 8.6 \\ C 3.7 \end{array}$	$\begin{array}{r} 6.8 \\ C 6.5 \\ \hline 42.9 \end{array}$
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3.4	1.0	1.0	$\begin{array}{r} 13.8 \\ C 0.5 \\ \hline 24.5 \end{array}$	$\begin{array}{r} 13.2 \\ C 0.6 \end{array}$	$\begin{array}{r} 9.0 \\ C 5.8 \\ \hline 41.5 \end{array}$
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2.8	+0.9	+0.9	$\begin{array}{r} 6.2 \\ C 0.4 \\ \hline 24.3 \end{array}$	$\begin{array}{r} 7.3 \\ F 1.3 \end{array}$	$\begin{array}{r} 1.8 \\ C 5.1 \\ \hline 39.5 \end{array}$
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1.7	+1.8	-1.8	$\begin{array}{r} 7.7 \\ C 0.0 \\ \hline 27.5 \end{array}$	$\begin{array}{r} 8.1 \\ F 1.1 \end{array}$	$\begin{array}{r} 2.8 \\ C 5.0 \\ \hline 38.2 \end{array}$
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0.1	+1.5	-1.5	$\begin{array}{r} 10.0 \\ C 0.0 \\ \hline 22.1 \end{array}$	$\begin{array}{r} 9.5 \\ F 0.5 \end{array}$	$\begin{array}{r} 11.0 \\ C 0.0 \\ \hline 23.6 \end{array}$
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T' Lt Sta 3+00

0.0	0	0	$\begin{array}{r} 18.0 \\ F 17.5 \\ \hline 50.0 \end{array}$	$\begin{array}{r} 00.1 \\ C 0.4 \end{array}$	$\begin{array}{r} 7.4 \\ F 6.9 \\ \hline 35.7 \end{array}$
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Sta	+	π	-	Elev	
		900.45			
3+50		BT 900.90		978	2.7
T.P.	0.24	894.95	5.78	894.71	
+50				97.8	+2.8
4				95.0	0.0
+50				92.5	2.5
5				90.4	4.6
T.P.	3.74	890.92	7.77	887.18	
+50				88.6	2.3 3.8
TP	B.T. 1.12	889.53	12.55	888.41	
6				87.1	3.8
+50				85.9	4.4 5.0 5.6
+78	PC				
7				85.0	5.0 5.9 6.8
+60				84.4	5.5 6.5 7.5

Elev W. 4			Super Elev	Lt.	Z	Rt
Rt					34 F0.7	110 F8.3 / 299
				154 F18.2 / 514 15.9 F15.9 / 46.8		8.1 F8.1 / 39.3
				16.2 F13.7 / 42.4	25 F0.0	9.9 F7.1 / 37.2
				15.9 F11.1 / 39.6	47 F0.1	105 F5.9 / 32.7
				11.6 F9.3 / 33.6	23 / 2.0	6.8 F4.3 / 28.5
0.0	0.2	0.2		11.6 F8.0 / 32.0	3.7 C1.0	8.6 F4.1 / 28.8
0.2	0.6	0.6		12.4 F8.0 / 31.0	5.0 C0.0	8.6 F3.0 / 29.2
1.3	0.8	0.8		12.4 F7.4 / 29.2	6.1 F0.2	9.2 F2.4 / 24.3
2.1	0.9	0.9		12.7 F7.2 / 30.6	6.9 F0.4	10.1 F2.6 / 25.4

Sta	+	Δ	-	Elev	
		890.92			
8		889.57		84.3	56.66-7.6
+47	P.T				
+50				84.3	58.66 7.4
B.M	1.54	889.43	3.03	887.89	887.89
9				84.6	43.48 5.3
+50				84.8	4.4 4.6 4.8
10				85.1	4.3
+50				85.3	4.1 5.6
T.P <u>B.T.</u>	8.19	892.71	5.01	884.52	
11				85.6	3.4-3.8 4.2
+64.6				85.9	2.7 3.5 4.3
+68. P.C					5.8
12				86.1	2.3 3.3 4.3
+50				86.3	2.1 3.1 4.1
T.P	9.23	896.17	2.49	886.94	
13				86.6	6.7 9.6 10.5

Ext W. d Super Elev

Lt

R

Rt

Rt
2.6 10 1.0

12.2
F6.6
34.8

7.1
F0.5

10.0
F2.4
24.8

1.2 08 0.8

11.9
F6.1
33.3

6.6
C0.0

8.9
C0.0
22.8

Sp 4 in

12" 09 4 36" Rt Sta 8+18

0.0 05 0.5

10.2
F5.9
32.7

4.5
C0.3

6.2
C0.6
24.7

E 0.2 0.2

9.7
F5.3
30.9

4.4
C0.2

5.6
C0.7
24.9

9.4
F5.1
30.3

4.5
F0.2

4.8
C1.0
25.5

8.7
F4.6
28.6

4.9
F0.8

5.2
C0.4
24.3

40.4 -0.4

10.2
F6.8
35.4

5.0
F1.2

5.7
C0.9
21.5

1.4 08 -0.8

10.7
F8.0
39.0

5.0
F1.5

4.4
C1.4
27.7

2.7 1.0 1.0

10.4
F8.1
39.3

7.7
F4.4

3.8
C0.5
30.2

2.9 1.0 1.0

9.3
F7.2
36.6

5.3
F2.2

2.8
C1.3
32.0

2.8 09 0.9

10.3
C0.0
33.6

4.2
C5.4

8.8
C1.7
32.7

Sta + π - Elev

896.17

+40.15 PT

892.71

+50

86.8 8.7 9.4 10.1

14

B.M.

437

891.63

8.95

87.1 8.7 9.1 9.5

887.22 887.21

+50

87.3 ✓ 4.4

15

87.6 4.1

+50

87.8 3.9

16

88.1 3.6

+50

88.5 3.2

17

89.3 2.4

Ext
WidSuper
Elev
+
-

L+

L

R+

0.9 +0.7-0.7

Daylight
10.2
DC0.9
50.243
C5.17.6
C2.5
32.4

0.0 +0.4 -0.4

10.2
DC0.0
22.59.5
F0.48.9
C0.6
27.7

5.9

11.2
FL8
28.67.3
F3.94.7
DC1.2
25.9

+0.1 -0.1

5.6

12.3
F8.2
31.410.5
FL6.4Red
5.3
DC0.3
24.1
Offset
16'

5.4

12.3
F8.4
31.811.2
F7.3Red
5.1
DC0.3
24.1
18'

5.1

12.0
F8.4
31.810.5
F.6.9Red
4.6
DC0.5
24.5
17'

4.7

12.1
F8.9
32.810.1
FL6.9Red
3.9
DC0.8
25.1
17'

3.9

11.5
F9.1
33.010.3
F7.9Red
3.1
DC0.8
25.1
17'

Sta	+	X	-	Elev	Gr Rod
		891.63			

17+50				90.5	1.2
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18				92.1	10.4
T.P.	7.15	898.38	0.40	891.23	

+50				93.8	4.6
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19				95.6	2.8
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+50				97.3	1.1
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T.P.	12.55	910.84	0.09	898.29	End?
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20				99.1	11.7
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+50				00.8	10.0
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T.P.	9.18	913.61	6.41	904.43	
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21				02.6	11.0
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B.M	1.73	913.61	1.73	911.86	911.86
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+50				04.3	9.3
-----	--	--	--	------	-----

Ditch Rod.

Lt

Z

Rt

Offset

2.7

11.6
F10.4
33.0

8.2
F7.0

2.7
D00.0
33.8

1.1

11.4
F11.8
33.0

6.8
F7.2

Shoulder
F.4
0.5
F0.9
15.0

3.5
00.0
36.2

18'

13.8
F9.3
33.0

9.7
F5.1

(18')
C.0.0
15.0

C.0.0
37.6

4.3

7.3
F4.3
24.0

4.7
F1.9

2.7
C0.1
15.0

4.3
D00.0
32.6

(17')

2.6

3.2
F2.1
24.3

1.4
F0.3

1.1
C0.0
26.5

Daylight
0.1
C00.0
33.2

0.1
C0.0
108.6

V1

Rt

13.2

16.7

13.2
D00.0
33.0

11.6
C0.1

10.7
C1.0
28.5

Day

10.7
C0.0
28.5

10.7
C0.0
126.5

11.5

9.0

6.6
C3.4
33.0

9.4
C0.6

BT 7.0
C2.0
28.5

Daylight
C.0.0
120.00

12.5

10.0

4.4
C6.6
33.0

10.3
C0.7

BT 7.0
C3.0
28.5

10.0
C0.0
107.8

Spk in 18" Oak 23' Lt Stg 21+45

10.0

8.3

2.3
C7.0
33.0

9.0
C0.3

BT 7.3
C6.0
28.5

8.3
C0.0
63.0

Sta	+	π	-	Elev	
		913.61			
22				06.1	7.5
+50				07.8	5.8
T.P	12.51	924.24	1.88	911.73	
23				09.4	14.8
+50				10.5	13.9
24				11.2	13.0
+50				11.5	12.7
+75					
25				11.5	12.7
T.P	2.49	915.10	11.63	912.61	
+50				11.0	4.1

Lt

Z

Rt

6.5

$$\begin{array}{r} 2.0 \\ C5.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 7.4 \\ C0.9 \\ \hline \end{array}$$

$$\begin{array}{r} B.T \\ 5.5 \\ C4.0 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 6.5 \\ C0.0 \\ \hline 73.0 \end{array}$$

4.8

$$\begin{array}{r} 2.1 \\ C3.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ C0.7 \\ \hline \end{array}$$

$$\begin{array}{r} B.T \\ 3.8 \\ C1.0 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ C0.0 \\ \hline 103.00 \end{array}$$

13.8

$$\begin{array}{r} 11.8 \\ C3.0 \\ \hline 32.5 \end{array}$$

$$\begin{array}{r} 14.4 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} B.T \\ C0.0 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 13.8 \\ C0.0 \\ \hline 124.5 \end{array}$$

12.9

$$\begin{array}{r} 9.9 \\ C4.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 13.0 \\ C0.9 \\ \hline \end{array}$$

$$\begin{array}{r} B.T \\ 10.9 \\ C2.9 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 12.9 \\ C0.0 \\ \hline 134.5 \end{array}$$

12.0

$$\begin{array}{r} 6.2 \\ C6.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 12.4 \\ C0.6 \\ \hline \end{array}$$

$$\begin{array}{r} B.T \\ 7.0 \\ C5.9 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 12.0 \\ C0.0 \\ \hline 138.8 \end{array}$$

11.7

$$\begin{array}{r} 5.4 \\ C7.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 12.2 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} B.T \\ 6.7 \\ C5.0 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 11.7 \\ C0.0 \\ \hline 115.0 \end{array}$$

11.7

$$\begin{array}{r} 8.2 \\ C4.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 12.7 \\ C0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 7.5 \\ 14.2 \\ C0.0 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 11.7 \\ C0.0 \\ \hline 41.5 \end{array}$$

5.6

$$\begin{array}{r} 4.8 \\ C0.8 \\ \hline 25.1 \end{array}$$

$$\begin{array}{r} 4.3 \\ F0.2 \\ \hline \end{array}$$

Sta	+	π	-	Elev
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915.10

26				10.4 4.7
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+50				10.3 4.8
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27				10.5 4.4
----	--	--	--	----------

+50				11.1 4.0
-----	--	--	--	----------

28				12.0 3.1
----	--	--	--	----------

+50				13.4 2.7
-----	--	--	--	----------

T.P.	6.16	918.41	2.85	912.25
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28+50				13.4 5.0
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29				14.9 3.5
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T.P.	13.60	931.10	0.91	917.50
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+50				16.4 14.7
-----	--	--	--	-----------

Lt

±

Rt

$$\begin{array}{r} 6.0 \\ F1.3 \\ \hline 17.6 \end{array}$$

$$\begin{array}{r} 5.0 \\ C0.3 \end{array}$$

$$\begin{array}{r} 4.8 \\ C0.0 \end{array}$$

$$\begin{array}{r} 4.4 \\ C0.2 \end{array}$$

$$\begin{array}{r} 4.3 \\ F0.3 \end{array}$$

$$\begin{array}{r} 3.9 \\ F0.8 \end{array}$$

$$\begin{array}{r} 2.8 \\ F1.1 \end{array}$$

$$\begin{array}{r} 6.4 \\ F1.4 \end{array}$$

$$\begin{array}{r} 9.9 \\ F4.9 \\ \hline 24.8 \end{array}$$

5.0

$$\begin{array}{r} 10.5 \\ F7.9 \\ \hline 29.0 \end{array}$$

$$\begin{array}{r} 4.1 \\ F0.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ F1.6 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 13.0 \\ C1.7 \\ \hline 29.9 \end{array}$$

$$\begin{array}{r} 14.9 \\ C0.2 \end{array}$$

$$\begin{array}{r} 12.0 \\ C2.2 \\ \hline 31.9 \end{array}$$

Sta	+	π	-	Elev	
		915.10			
25	2.73	906.09	11.74	903.36	
25+50				11.0	+4.9
26				10.4	+4.3
+50				10.3	+4.2
27				10.5	+4.4
+50				11.1	+5.0
28				12.0	+5.9
T.P.		915.10			
T.P.	1.24	903.79	12.55	902.55	
26+50				10.3	+6.5
27				10.5	+6.7
+50				11.1	+7.3
28				12.0	+8.2
+50				13.4	+9.6

Lt.

2

Rt

$$\begin{array}{r} 13.0 \\ F17.9 \\ \hline 50.8 \end{array}$$

$$\begin{array}{r} 13.7 \\ F18.0 \\ \hline 51.0 \end{array}$$

$$\begin{array}{r} 13.2 \\ F17.4 \\ \hline 49.8 \end{array}$$

$$\begin{array}{r} 8.5 \\ F12.9 \\ \hline 40.8 \end{array}$$

$$\begin{array}{r} 2.9 \\ F7.9 \\ \hline 30.8 \end{array}$$

$$\begin{array}{r} 1.3 \\ F7.2 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 4.5 \\ F11.0 \\ \hline 37.0 \end{array}$$

$$\begin{array}{r} 7.1 \\ F13.8 \\ \hline 42.4 \end{array}$$

$$\begin{array}{r} 7.7 \\ F15.0 \\ \hline 45.0 \end{array}$$

$$\begin{array}{r} 9.6 \\ F17.8 \\ \hline 50.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ F15.5 \\ \hline 41.0 \end{array}$$

Sta	+	π	-	Elev	
		931.10			
30				17.9	13.2

				19.2	11.9
+50	2.98	933.41	0.67	930.43	

31				20.1	13.3
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+50				20.6	12.8
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32				20.7	12.7
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+30				20.6	12.8
T.P	3.49	923.63	13.27	920.14	

+62				20.5	3.1
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33				20.5	3.1
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LT

K

RT

$$\begin{array}{r} 6.5 \\ C6.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 13.0 \\ CO.2 \end{array}$$

$$\begin{array}{r} 7.7 \\ C5.5 \\ \hline 33.0 \end{array}$$

10.9

$$\begin{array}{r} 3.2 \\ C8.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.6 \\ CO.3 \end{array}$$

$$\begin{array}{r} BT \\ 3.9 \\ C7.1 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 10.9 \\ CO.0 \\ \hline 261.7 \end{array}$$

12.3

$$\begin{array}{r} 3.7 \\ C8.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 13.0 \\ CO.3 \end{array}$$

$$\begin{array}{r} B.T \\ 4.3 \\ C8.0 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 12.3 \\ CO.0 \\ \hline 205.4 \end{array}$$

11.8

$$\begin{array}{r} 3.3 \\ C9.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 12.7 \\ CO.1 \end{array}$$

$$\begin{array}{r} BT \\ 3.8 \\ C7.9 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 11.8 \\ CO.0 \\ \hline 147.3 \end{array}$$

11.7

$$\begin{array}{r} 4.1 \\ C8.6 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 13.1 \\ FO.4 \end{array}$$

$$\begin{array}{r} BT \\ 6.7 \\ C5.9 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 11.7 \\ CO.0 \\ \hline 95.8 \end{array}$$

11.8

$$\begin{array}{r} 7.6 \\ C5.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 13.4 \\ FO.6 \end{array}$$

$$\begin{array}{r} B.T \\ 9.8 \\ C2.0 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 11.8 \\ CO.0 \\ \hline 60.8 \end{array}$$

4.6

$$\begin{array}{r} 4.6 \\ CO.6 \\ \hline 23.5 \end{array}$$

$$\begin{array}{r} 4.1 \\ FO.0 \end{array}$$

$$\begin{array}{r} 3.0 \\ CO.6 \\ \hline 26.7 \end{array}$$

4.6

$$\begin{array}{r} 9.9 \\ FL.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ FL.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ FL.7 \\ \hline 20.1 \end{array}$$

Sta	+	π	-	Elev	
		92363			
33+50				20.4	3.2
34				20.3	3.3
+50				20.2	3.4
35				20.1	3.5
+50				20.0	3.6
36				19.9	3.7
T.P.	7.16	925.53	5.20	91843	
+50				19.8	5.8
37				19.7	5.9

L+

A

R+

$$\begin{array}{r} 10.7 \\ F7.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ F1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ F2.3 \\ \hline 21.9 \end{array}$$

4.8

$$\begin{array}{r} 8.7 \\ F5.4 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 4.7 \\ F1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ 100.0 \\ \hline 23.5 \end{array}$$

4.9

$$\begin{array}{r} 6.3 \\ F2.9 \\ \hline 22.9 \end{array}$$

$$\begin{array}{r} 4.1 \\ F0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 2.2 \\ 01.2 \\ \hline 28.9 \end{array}$$

5.0

$$\begin{array}{r} 6.9 \\ F3.4 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 4.0 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 1.8 \\ 01.7 \\ \hline 29.9 \end{array}$$

5.1

$$\begin{array}{r} 7.5 \\ F3.9 \\ \hline 26.7 \end{array}$$

$$\begin{array}{r} 4.2 \\ F0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 3.6 \\ 00.2 \\ \hline 26.9 \end{array}$$

5.2

$$\begin{array}{r} 7.9 \\ F4.2 \\ \hline 27.4 \end{array}$$

$$\begin{array}{r} 4.4 \\ F0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ 101.4 \\ \hline 26.3 \end{array}$$

7.3

$$\begin{array}{r} 7.5 \\ F1.2 \\ \hline 20.1 \end{array}$$

$$\begin{array}{r} 5.9 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ 00.7 \\ \hline 27.9 \end{array}$$

7.4

$$\begin{array}{r} 5.2 \\ 100.7 \\ \hline 27.9 \end{array}$$

$$\begin{array}{r} 5.5 \\ 00.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ 113 \\ \hline 26.1 \end{array}$$

Sta	+	π	-	Elev	
		925.53			
37+50				19.8	5.7
38				20.4	5.1
+50				21.4	4.2
39				22.9	2.7
+50				24.6	1.0
T.P.	10.63	935.34	0.82	924.71	
40				26.2	9.1
+50				27.6	7.7
41				28.8	6.5
B.M	3.45	935.32	3.45	931.89	931.87

Lt.

K

Rt

72

$$\begin{array}{r} 6.1 \\ DC1.1 \\ \hline 25.7 \end{array}$$

$$\begin{array}{r} 5.7 \\ CO.0 \end{array}$$

$$\begin{array}{r} 7.5 \\ F1.8 \\ \hline 20.4 \end{array}$$

66

$$\begin{array}{r} 9.3 \\ F4.2 \\ \hline 27.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ FO.6 \end{array}$$

$$\begin{array}{r} 12.5 \\ F7.4 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 13.4 \\ F9.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ FO.7 \end{array}$$

$$\begin{array}{r} 8.0 \\ F3.8 \\ \hline 26.4 \end{array}$$

42

$$\begin{array}{r} 10.7 \\ F8.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 3.3 \\ CO.6 \end{array}$$

$$\begin{array}{r} 5.6 \\ F2.9 \\ \hline 23.7 \end{array}$$

2.5

$$\begin{array}{r} 2.0 \\ DC0.5 \\ \hline 24.5 \end{array}$$

$$\begin{array}{r} 1.2 \\ FO.2 \end{array}$$

$$\begin{array}{r} 3.6 \\ F2.6 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 8.1 \\ CO.0 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 9.1 \\ CO.0 \end{array}$$

$$\begin{array}{r} 7.0 \\ C2.1 \\ \hline 30.7 \end{array}$$

$$\begin{array}{r} 5.6 \\ C2.1 \\ \hline 30.7 \end{array}$$

$$\begin{array}{r} 7.1 \\ CO.6 \end{array}$$

$$\begin{array}{r} 3.1 \\ C4.6 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.3 \\ C2.2 \\ \hline 30.9 \end{array}$$

$$\begin{array}{r} 5.6 \\ CO.9 \end{array}$$

$$\begin{array}{r} 1.6 \\ C4.9 \\ \hline 33.0 \end{array}$$

Spk in Cor. Fe. Post 28' Lt Stg 41/17

Sta	+	π	-	Elev	
		935.32			
41 T.P.	12.46	943.20	4.58	930.74	
41+50				29.8	13.8
42				30.6	12.6
+50				31.3	11.9
43				31.7	11.5
T.P.	2.49	936.23	9.46	933.74	
+50				32.0	4.2
44				32.1	4.1
+50				32.3	3.9
45				32.4	3.8

L+

£

R+

$$\begin{array}{r} 10.8 \\ C3.0 \\ \hline 32.5 \end{array}$$

$$\begin{array}{r} 12.4 \\ C1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ C7.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.2 \\ C4.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.6 \\ C1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C9.1 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ C5.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.0 \\ C0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 3.0 \\ C8.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ C5.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.0 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ C6.2 \\ \hline 33.0 \end{array}$$

Spk in P.R L+ 43+50

$$\begin{array}{r} 2.0 \\ C2.2 \\ \hline 30.9 \end{array}$$

$$\begin{array}{r} 4.2 \\ C0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 2.0 \\ C2.2 \\ \hline 30.9 \end{array}$$

5.6

$$\begin{array}{r} 5.8 \\ F1.7 \\ \hline 20.1 \end{array}$$

$$\begin{array}{r} 4.6 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ F1.9 \\ \hline 20.7 \end{array}$$

$$\begin{array}{r} 9.3 \\ F5.4 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ F1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 8.8 \\ F4.9 \\ \hline 29.7 \end{array}$$

$$\begin{array}{r} 12.0 \\ F8.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ F1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 9.2 \\ F5.4 \\ \hline 31.2 \end{array}$$

Sta	+	π	-	Elev	
		936.23			
45	+50			32.6	3.6
46				32.8	3.4
	+50			33.3	2.9
47				33.9	2.3
	+50			34.8	1.4
48				35.9	0.3
T.P.	13.71	949.70	0.24	935.99	
	+50			37.2	12.5
49				38.4	11.3
	+50			39.4	10.3
50				40.0	9.7
	+50			40.3	9.4
51				40.5	9.2

L +

K

R +

$$\begin{array}{r} 12.5 \\ F8.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ F1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 9.0 \\ F5.4 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 12.3 \\ F8.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.3 \\ F0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 7.3 \\ F3.9 \\ \hline 26.1 \end{array}$$

$$\begin{array}{r} 11.8 \\ F8.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ F6.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.6 \\ F3.7 \\ \hline 26.1 \end{array}$$

3.8

$$\begin{array}{r} 9.3 \\ F7.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 3.1 \\ F0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.7 \\ F3.4 \\ \hline 25.2 \end{array}$$

2.9

$$\begin{array}{r} 7.1 \\ F5.7 \\ \hline 32.1 \end{array}$$

$$\begin{array}{r} 1.9 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ F2.5 \\ \hline 22.5 \end{array}$$

1.8

$$\begin{array}{r} 4.6 \\ F4.3 \\ \hline 27.9 \end{array}$$

$$\begin{array}{r} 0.5 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 2.3 \\ F2.0 \\ \hline 21.0 \end{array}$$

140

$$\begin{array}{r} 14.7 \\ F2.2 \\ \hline 21.5 \end{array}$$

$$\begin{array}{r} 12.6 \\ C0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 14.2 \\ F1.7 \\ \hline 20.1 \end{array}$$

12.8

$$\begin{array}{r} 10.7 \\ C0.6 \\ \hline 27.7 \end{array}$$

$$\begin{array}{r} 11.0 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 11.9 \\ C0.2 \\ \hline 26.9 \end{array}$$

$$\begin{array}{r} 5.7 \\ C5.1 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.8 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 7.2 \\ C3.1 \\ \hline 32.7 \end{array}$$

$$\begin{array}{r} 2.3 \\ C7.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.5 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 2.8 \\ C6.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 2.9 \\ C7.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.7 \\ C0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 0.6 \\ C8.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 2.0 \\ C7.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.4 \\ C0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 2.2 \\ C7.8 \\ \hline 33.0 \end{array}$$

Sta	+	π	-	Elev	
		949.70			
51+50				40.6	9.1
52				40.8	8.9
+54				40.9	8.8
53				41.1	8.6
T.P.	7.55	948.43	8.82	940.88	
+50				41.2	7.2
54				41.6	6.8
+50				42.4	6.0
55				43.6	4.8
+50				45.2	3.2
56				46.7	1.7
+26				47.3	1.1
+38.				47.5	0.9
B.M			0.47	947.96	947.95

Lt.

R

Rt

$$\begin{array}{r} 4.7 \\ C4.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.5 \\ C0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ C5.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.5 \\ C0.4 \\ \hline 27.3 \end{array}$$

$$\begin{array}{r} 8.5 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.6 \\ C4.3 \\ \hline 33.0 \end{array}$$

10.3

$$\begin{array}{r} 10.0 \\ C0.3 \\ \hline 24.1 \end{array}$$

$$\begin{array}{r} 8.5 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 2.4 \\ C6.4 \\ \hline 33.0 \end{array}$$

10.1

$$\begin{array}{r} 10.5 \\ F1.9 \\ \hline 20.7 \end{array}$$

$$\begin{array}{r} 8.6 \\ C0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ C4.8 \\ \hline 33.0 \end{array}$$

8.7

12L

$$\begin{array}{r} 11.4 \\ F4.2 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 7.3 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ C1.1 \\ \hline 28.7 \end{array}$$

8.3

$$\begin{array}{r} 11.8 \\ F5.0 \\ \hline 30.8 \end{array}$$

$$\begin{array}{r} 7.1 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ C0.4 \\ \hline 22.3 \end{array}$$

7.5

$$\begin{array}{r} 12.4 \\ F6.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 6.9 \\ F0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ C0.5 \\ \hline 24.5 \end{array}$$

$$\begin{array}{r} 12.6 \\ F7.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 6.4 \\ F1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 7.8 \\ F3.0 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 11.1 \\ F7.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ F2.1 \\ \hline \end{array}$$

$$\begin{array}{r} 8.9 \\ F5.7 \\ \hline 32.1 \end{array}$$

$$\begin{array}{r} 10.5 \\ F8.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 3.3 \\ F1.6 \\ \hline \end{array}$$

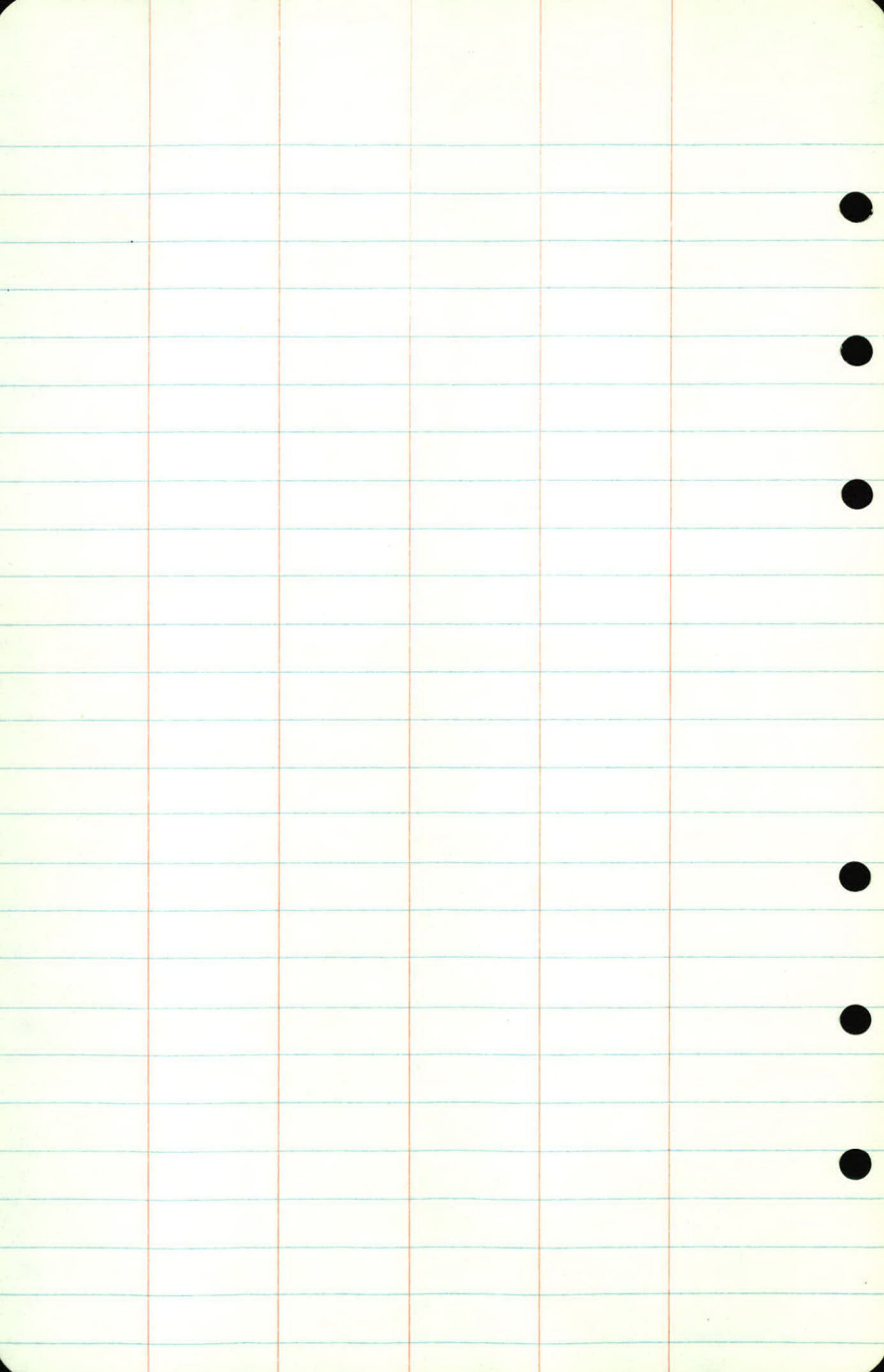
$$\begin{array}{r} 7.3 \\ F5.2 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 8.4 \\ F7.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 1.9 \\ F0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 7.4 \\ F6.3 \\ \hline 33.0 \end{array}$$

Top Mon Sta 56 + 58



New Ties

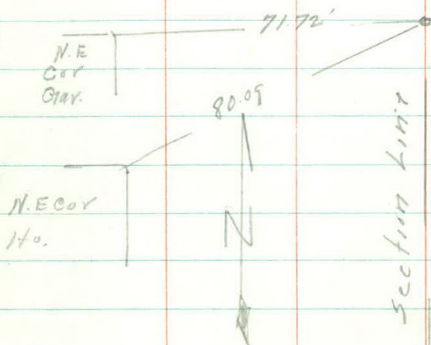
Smelling Ave

5th Point

22+89.75 P.O.T

12+54.20 P.1

Description.



Boat Spk



Iron Mark

3042653 P1

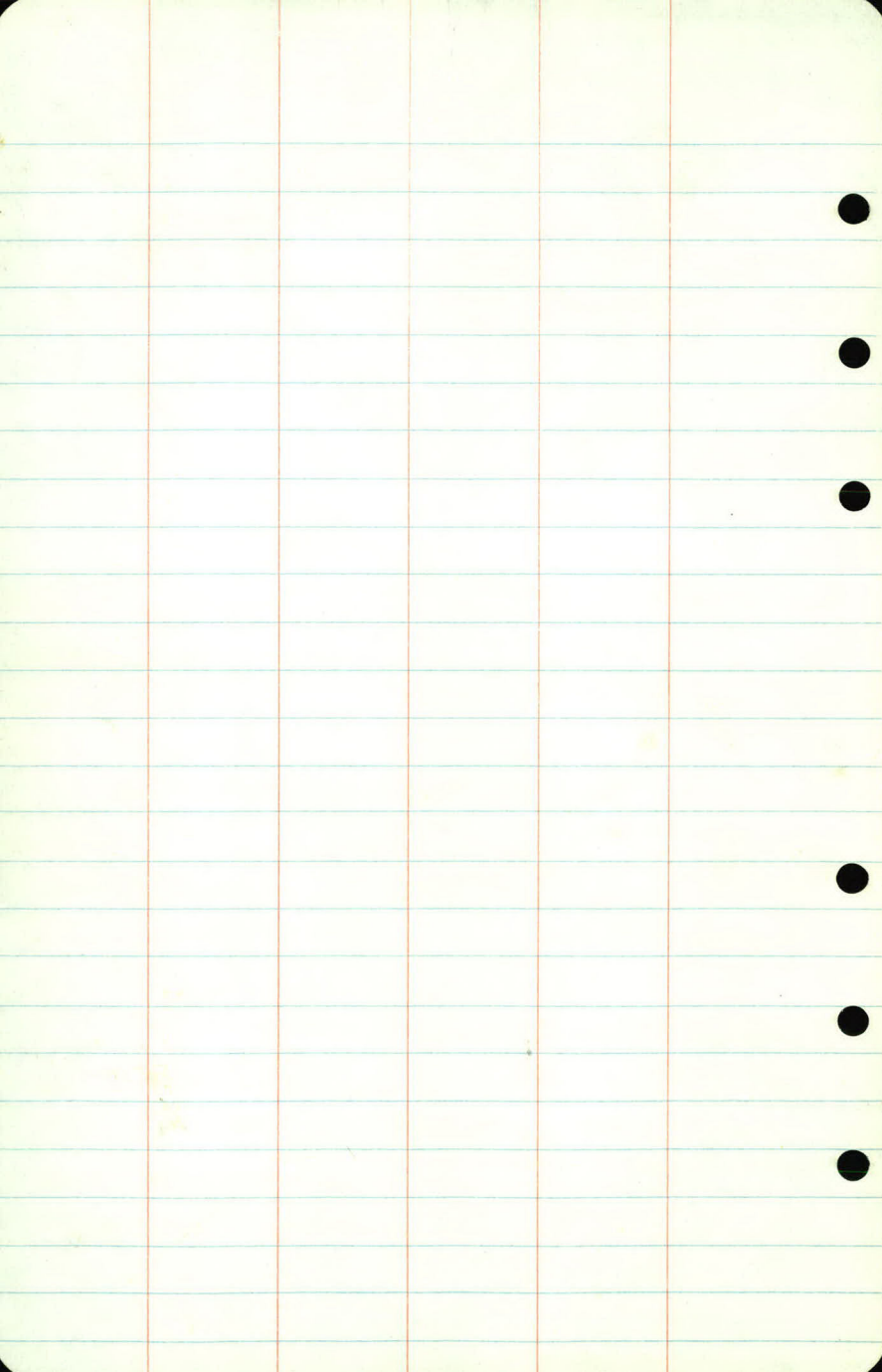
Tren p. 17

68.98'

10" Apple Tree
60

78.52'

6" Apple Tree
10



Align

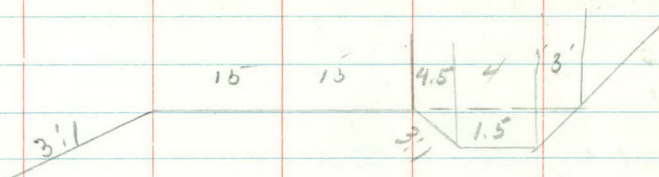
Snelling Ave
Curve Data.
Slope Stakes

62 16 47				
Sta	Point	Def.		
+40.15	P.T	13° 40'		
13		10 59 30		
+54.20	P.1			
+50		6° 24' 30		
12		2° 39' 30	D 15	
11+64.60			Δ 26° 20	
11				
+48.03 = 4795 P.T		10° 12'		
8		4° 19'		
+64.1	P.1		D 120	
+50		4° 19'	Δ 20 24	
7		10 19'		
6+78.03	P.C	0° 00'		
2+17.38	P.T = 2+16.83	21° 41'	D 20	
2		20° 03'	Δ 43.20	
+50		15° 03'		
1		10° 03'		
+50		5° 03'		
0+00		0° 03'		
10-0.55	P.C			

Slope Stakes

(Winnicake Rd.)
Co Rd "R"

STH #10 To Snelling Ave



Sta	+	π	-	Elev	Gr. Rod
B.M	6.54	89380		887.26	
0+20				92.8	1.0
+24				92.7	1.1
+30				92.6	1.2
+38				92.4	1.4
+50				92.0	1.8
1				90.0	3.8
+25				88.5	
+50				87.0	6.8
T.P	8.92	88984	12.88	880.92	
2				84.7	5.1
+52				83.1	6.7
+59				82.9	6.9

Lt.

£

Rt

Ditch Grade

Spk. S. E. Cor. Barn 350' Lt Sta 3700.

2.7

1.6
DC 1.1
25.72.4
F1.22.3
DC 0.4
24.33.8
F2.4/22.26.4
F5.07.4
F8.0/32.04.6
F2.8/23.47.5
F5.810.5
F8.7/21.17.4
F3.6/15.89.3
F5.511.4
F7.6/37.8

No Stakes

10.5
F3.7/26.111.9
F5.113.6
F6.8/35.49.4
F4.3/21.910.0
F4.910.9
F5.8/32.410.3
F3.6/25.810.9
F4.211.4
F4.7/29.1

No Stake

Sta	+	Δ	-	Elev
		889.84		
3+00				82.4 7.4
+50				82.6 7.214
+75				83.0 6.8
4				83.5 6.3 1.5
+50				84.5 5.3 7.5
5				85.5 4.3 8.5
+47				86.4 7.6
		2.57		887.28 887.26

Ditch

Lt.

R

Rt

8.9

8.6
D00.3/24.1

9.7
F2.3

10.6
F3.2/4.6

8.7

6.0
C1.2/28.9

7.7
F0.5

9.1
F1.9/20.7

8.3

1.8
C5.0/36.5

6.6
C0.2

8.5
F1.7/20.1

7.8

1.8
C4.5/35.5

5.9
C0.4

8.3
F2.2/10

6.8

5.0
C0.3/22.1

6.6
F1.3

7.1
F1.8/20.4

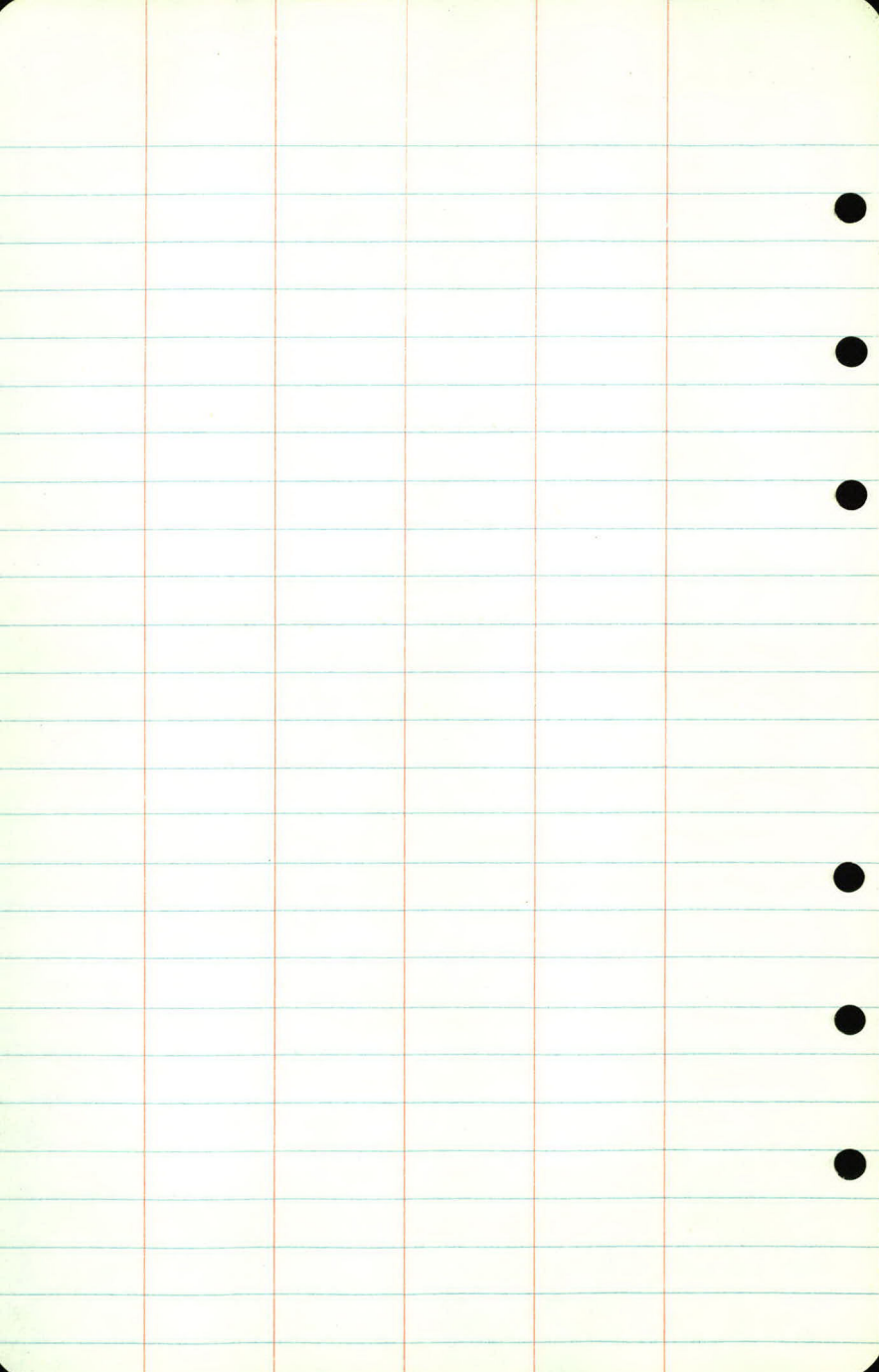
5.8

5.8
D00.0/22.5

4.8
F0.5

4.8
D01.0/25.5

Spt in S.E Cor Barn 300' Lt 3+50



Slope stakes

Co Rd "F"

From Snelling To Hamline

Sta	+	Δ	-	Elev	Gr. Rod.
B.M.	9.63	929.16		919.53	
0+72.85				18.5	
1				20.1	8.5 9.1 9.7 7.0 8.2
+35				22.1	7.1
T.P.	13.41	939.15	3.42	925.74	
2				25.7	13.5
+50				28.4	10.8
T.P.	11.90	945.35	5.70	933.45	
3				31.0	14.4
+35				32.7	12.7
4				36.0	9.4
+19				36.9	8.5

L+

Z

R+

Ext Mid Super

L+ + - Spk 24" Oak 23' R+ Sta 0-60

1.7

Sec. Snelling Arc Notes

0.3 0.6 0.6

$$\begin{array}{r} 3.5 \\ C 5.0 / 36.8 \end{array}$$

$$\begin{array}{r} 8.8 \\ C 0.3 \end{array}$$

$$\begin{array}{r} 5.1 \\ C 4.5 / 33.0 \end{array}$$

0.0 0.0 0.0

$$\begin{array}{r} 4.8 \\ C 2.3 / 31.1 \end{array}$$

$$\begin{array}{r} 6.8 \\ C 0.3 \end{array}$$

$$\begin{array}{r} 5.2 \\ C 1.9 / 30.3 \end{array}$$

$$\begin{array}{r} 8.4 \\ C 5.1 / 33.0 \end{array}$$

$$\begin{array}{r} 13.4 \\ F 0.1 \end{array}$$

$$\begin{array}{r} 10.4 \\ C 3.1 / 33.0 \end{array}$$

$$\begin{array}{r} 7.1 \\ C 3.7 / \end{array}$$

$$\begin{array}{r} 10.8 \\ F 0.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ C 6.5 / 35.0 \end{array}$$

$$\begin{array}{r} 6.9 \\ C 7.5 / 33.0 \end{array}$$

C 0.0

$$\begin{array}{r} 9.0 \\ C 5.4 / 33.0 \end{array}$$

$$\begin{array}{r} 7.9 \\ C 4.8 / 33.0 \end{array}$$

$$\begin{array}{r} 12.5 \\ C 0.2 \end{array}$$

$$\begin{array}{r} 4.6 \\ C 8.1 / 33.0 \end{array}$$

$$\begin{array}{r} 9.2 \\ C 0.2 / 26.9 \end{array}$$

$$\begin{array}{r} C 0.0 \\ 9.4 \end{array}$$

$$\begin{array}{r} 4.9 \\ C 4.5 / 33.0 \end{array}$$

$$\begin{array}{r} 8.6 \\ D 1.4 / 33.0 \end{array}$$

$$\begin{array}{r} 8.4 \\ C 0.1 \end{array}$$

$$\begin{array}{r} 7.1 \\ C 1.4 / 29.3 \end{array}$$

10.0

Sta	+	π	-	Elev	
		945.35			
4+66				39.3	6.1
5				41.0	4.4
T.P.	11.72	955.20	1.87	943.48	
+60				44.0	11.2
+85				45.2	10.0
6				46.0	9.2
+50				48.5	6.7
7				51.0	4.2
B.M.	12.77	966.49	1.58	953.78	953.72
+58				53.5	13.0
8				54.9	11.6

LT.

Z

RT

7.6

$$\begin{array}{r} 5.6 \\ 10.5 \\ \hline 17.5 \end{array}$$

$$\begin{array}{r} 60 \\ 10.1 \\ \hline \end{array}$$

$$\begin{array}{r} 7.6 \\ 10.0 \\ \hline 17.9 \end{array}$$

5.9

$$\begin{array}{r} 1.0 \\ 13.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 44 \\ 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ 10.0 \\ \hline 25.3 \end{array}$$

12.7

$$\begin{array}{r} 4.3 \\ 16.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 112 \\ 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 12.0 \\ 10.7 \\ \hline 24.9 \end{array}$$

11.5

$$\begin{array}{r} 2.6 \\ 17.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 100 \\ 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 145 \\ 14.5 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 2.0 \\ 17.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 92 \\ 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 138 \\ 14.2 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 2.2 \\ 15.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 67 \\ 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 10.9 \\ 14.2 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 10.6 \\ 14.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 42 \\ 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 8.0 \\ 13.8 \\ \hline 21.4 \end{array}$$

SpK 12" OOK 35' RT Sta 7 + 55

$$\begin{array}{r} 3.1 \\ 19.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 128 \\ 10.2 \\ \hline \end{array}$$

$$\begin{array}{r} 11.1 \\ 11.9 \\ \hline 30.3 \end{array}$$

$$\begin{array}{r} 0.8 \\ 10.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 114 \\ 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 8.3 \\ 13.3 \\ \hline 33.0 \end{array}$$

π
 96649

Sta	+	π	-	Elev	
	1368	970.28	989	956.60	
8+71				56.3	140

9				56.6	13.7
---	--	--	--	------	------

+50				56.9	13.4
-----	--	--	--	------	------

T.P.	5.49	962.79	1298	957.30	
------	------	--------	------	--------	--

10				57.2	5.6
----	--	--	--	------	-----

+50				57.5	5.3
-----	--	--	--	------	-----

11				57.8	5.0
----	--	--	--	------	-----

+50				58.1	4.7
-----	--	--	--	------	-----

12				58.4	4.4
----	--	--	--	------	-----

T.P.	5.61	967.78	0.62	962.17	
------	------	--------	------	--------	--

+50				58.8	9.0
-----	--	--	--	------	-----

13				59.7	8.1
----	--	--	--	------	-----

+50				60.8	7.0
-----	--	--	--	------	-----

L+

Z

R+

$$\begin{array}{r} 2.2 \\ C12.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 13.8 \\ C0.2 \end{array}$$

$$\begin{array}{r} 10.2 \\ C3.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ C9.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 13.6 \\ C0.1 \end{array}$$

$$\begin{array}{r} 10.9 \\ C2.8 \\ \hline 32.1 \end{array}$$

$$\begin{array}{r} 7.2 \\ C6.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 13.2 \\ C0.2 \end{array}$$

$$\begin{array}{r} 11.2 \\ C2.2 \\ \hline 30.9 \end{array}$$

7.1

$$\begin{array}{r} 4.5 \\ C1.1 \\ \hline 28.7 \end{array}$$

$$\begin{array}{r} 5.3 \\ C0.3 \end{array}$$

$$\begin{array}{r} 4.1 \\ F1.9 \\ \hline 19.5 \end{array}$$

6.8

$$\begin{array}{r} 8.3 \\ F3.9 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ C0.2 \end{array}$$

$$\begin{array}{r} 8.3 \\ F3.0 \\ \hline 24.0 \end{array}$$

6.5

$$\begin{array}{r} 8.8 \\ F3.8 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 4.9 \\ C0.1 \end{array}$$

$$\begin{array}{r} 7.3 \\ F2.3 \\ \hline 26.9 \end{array}$$

$$\begin{array}{r} 8.8 \\ F4.1 \\ \hline 27.3 \end{array}$$

$$\begin{array}{r} 4.6 \\ C0.1 \end{array}$$

$$\begin{array}{r} 8.3 \\ F3.6 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 8.1 \\ F3.7 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 4.1 \\ C0.3 \end{array}$$

$$\begin{array}{r} 8.7 \\ F4.6 \\ \hline 28.8 \end{array}$$

SpK in 24 in Oak Rt Stg 14400

$$\begin{array}{r} 12.4 \\ F3.4 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 8.4 \\ C0.6 \end{array}$$

$$\begin{array}{r} 14.2 \\ F5.0 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 10.6 \\ F2.3 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 7.6 \\ C0.5 \end{array}$$

$$\begin{array}{r} 13.8 \\ F5.2 \\ \hline 30.6 \end{array}$$

6.5

$$\begin{array}{r} 8.4 \\ DC0.1 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} 6.8 \\ C0.3 \end{array}$$

$$\begin{array}{r} 11.2 \\ F4.2 \\ \hline 27.6 \end{array}$$

Sta	+	Σ	-	Elev	
		967.78			
14				624	5.4
T.P.	12.60	977.02	3.36	964.42	
+60				647	12.3
15				665	10.5
+50				689	8.1
+86				706	6.4
16				713	5.7
+50				737	3.3
17				761	0.9
T.P.	10.28	986.31	0.99	976.03	
+50				78.5	7.8
18				80.9	5.4
+50				82.7	3.6
+70				83.7	3.1
B.M.			2.78	983.53	

L +

R

R +

6.9

7.2
F1.8/20.45.2
C0.25.9
D0.0/25.5

13.8

13.5
D0.3/24.412.4
F0.17.5
C4.8/33.0

12.0

11.7
D0.3/24.410.6
F0.19.6
C0.9/28.3

9.6

9.7
F1.6/19.88.3
F0.27.6
C0.8/27.5

7.9

7.8
D0.1/23.76.5
F0.14.2
C2.2/30.9

7.2

6.5
D0.7/24.95.8
F0.13.9
C1.8/30.1

4.8

4.0
D0.8/25.14.0
F0.76.0
F2.7/23.1

2.4

2.5
F1.0/19.82.8
F1.96.8
F5.8/32.4

19.3

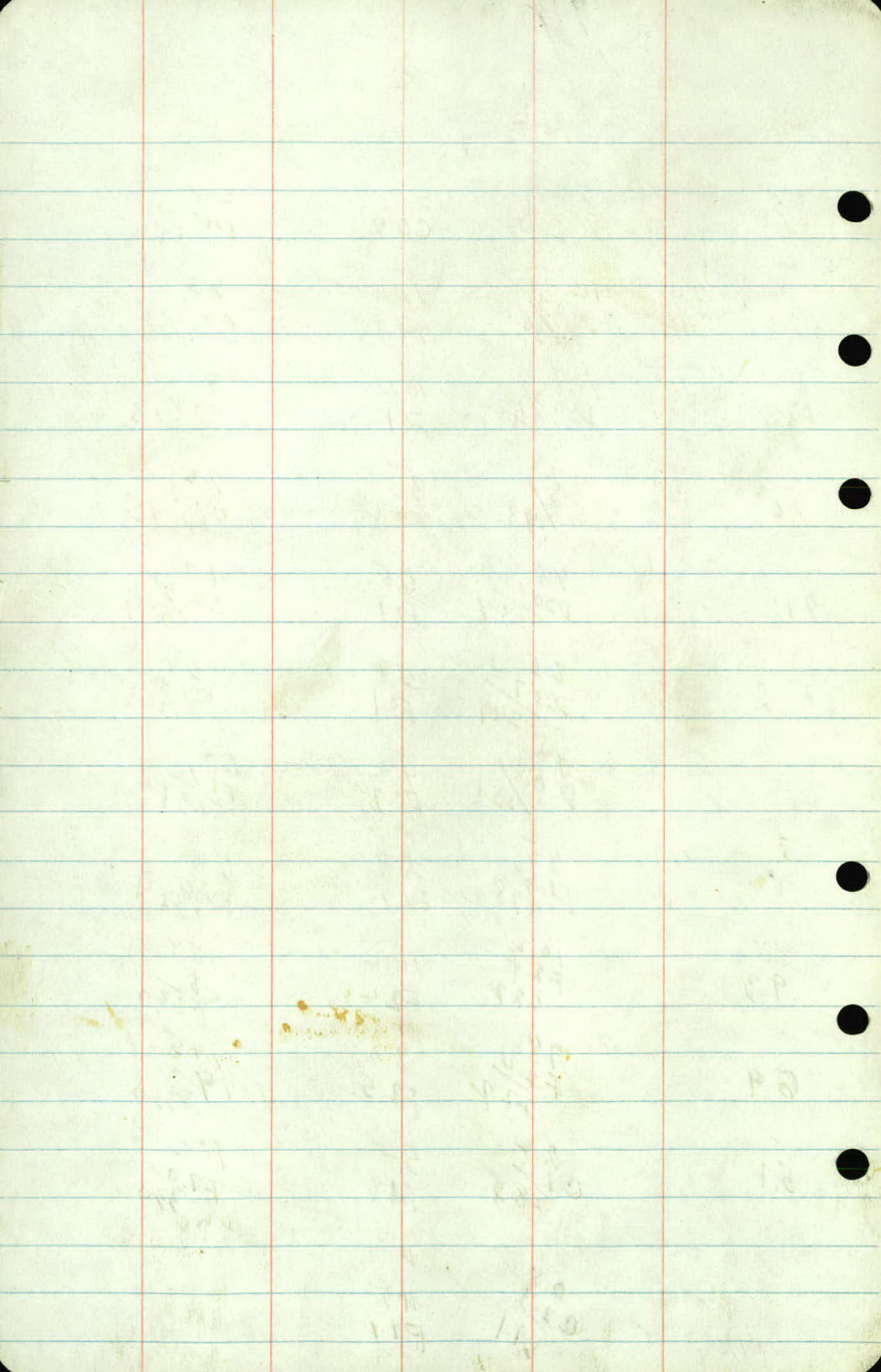
10.2
F2.4/22.210.2
F2.415.8
F8.0/33.0

6.9

7.8
F2.4/22.28.0
F1.514.5
F9.0/33.0

5.1

2.6
C1.0/28.55.4
F0.810.6
F7.0/33.00.8
C2.0/24.14.3
F1.1



Blue Tops

Co Rd "F" + Snelling Aves

4/14/44

Sta	+	π	-	Elev	Grade Rod.
B.M	11.26	930.79		919.53	3PK 24" oak

0+72.85				18.5	0.8
---------	--	--	--	------	-----

1				20.1	0.6
---	--	--	--	------	-----

+50				23.0	
-----	--	--	--	------	--

2				25.7	5.1
---	--	--	--	------	-----

+50				28.4	2.4
-----	--	--	--	------	-----

T.P	12.76	943.28	0.27	930.52	
3				31.0	12.3

+50				33.5	9.8
-----	--	--	--	------	-----

4				36.0	7.3
---	--	--	--	------	-----

+50				38.5	4.8
-----	--	--	--	------	-----

5				41.0	2.3
---	--	--	--	------	-----

T.P	13.28	955.53	1.03	942.25	
+50				43.5	12.0

6				46.0	9.5
---	--	--	--	------	-----

Sta	+	Σ	-	Elev
-----	---	----------	---	------

955.53

6480

48.5

7.0

7

51.0

4.5

+50

53.2

2.3

7+03

953.72

8

54.9

0.6

T.P.

6.71

961.64

0.60

954.93

+50

56.0

5.1

9

56.2

5.0

+50

56.9

4.7

10

57.2

4.4

+50

57.5

4.1

11

57.8

3.8

T.P.

6.20

964.00

3.84

957.80

+50

58.1

5.9

12

58.4

5.6

Sta	+	Σ	-	Elev	
		96400			
12+50				58.8	5.2
13				59.7	4.3
+50				60.8	3.2
14				62.4	1.6
T.P.	13.03	975.42	1.61	962.39	
+50				64.2	11.2
15				66.5	8.9
+50				68.9	6.5
16				71.3	4.2
+50				73.7	1.7
T.P.	10.40	984.89	0.93	974.49	
17				76.1	8.8
+50				78.5	6.4
18				80.9	4.0

18+50

82.7 2.2

19

83.4 1.5

+50

83.5

20

83.6

83.7

83.8

83.9

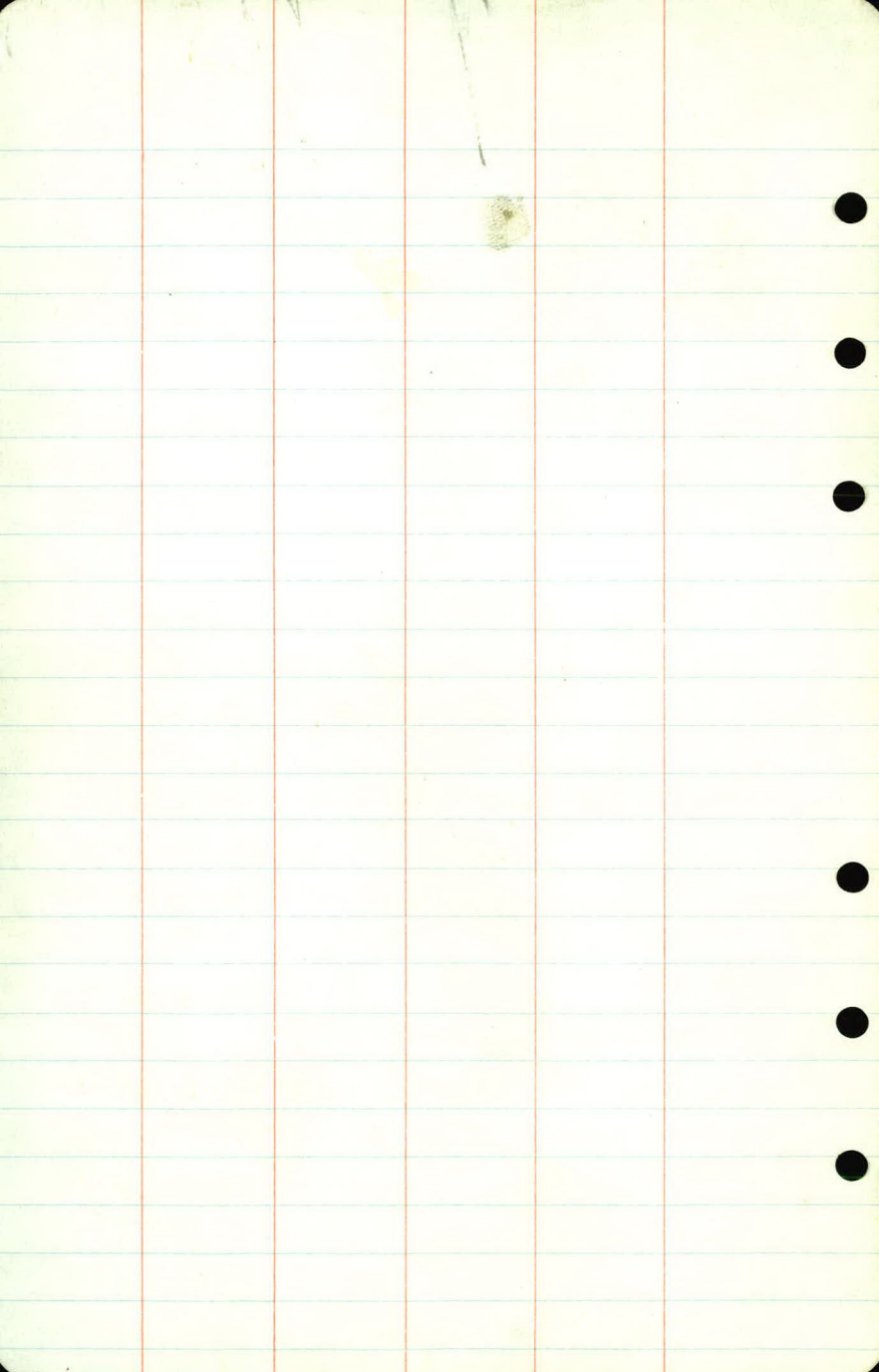
21

84.0

+50

84.1

84.2



Slope Stakes

Sta 20 to 25 to 0

Sta	+	Δ	-	Elev
		91307		
20+00				879.1 140
+50				900.8 12.3
21				902.5 10.5
+50				904.3 8.8
22				906.1 7.0
+50				907.8 19.3
23				909.4 18.0
+50				910.5
24				911.2
+50				911.5
25				11.5
+50				11.0

L

R+

$$\begin{array}{r} 13.7 \\ C \ 03 \\ \hline 27.1 \end{array}$$

$$\begin{array}{r} 8.3 \\ C \ 40 \\ \hline 32.5 \end{array}$$

1 1/2 : 1

1 1/2 : 1

$$\begin{array}{r} 5.3 \\ C \ 5.2 \\ \hline 34.3 \end{array}$$

2 : 1

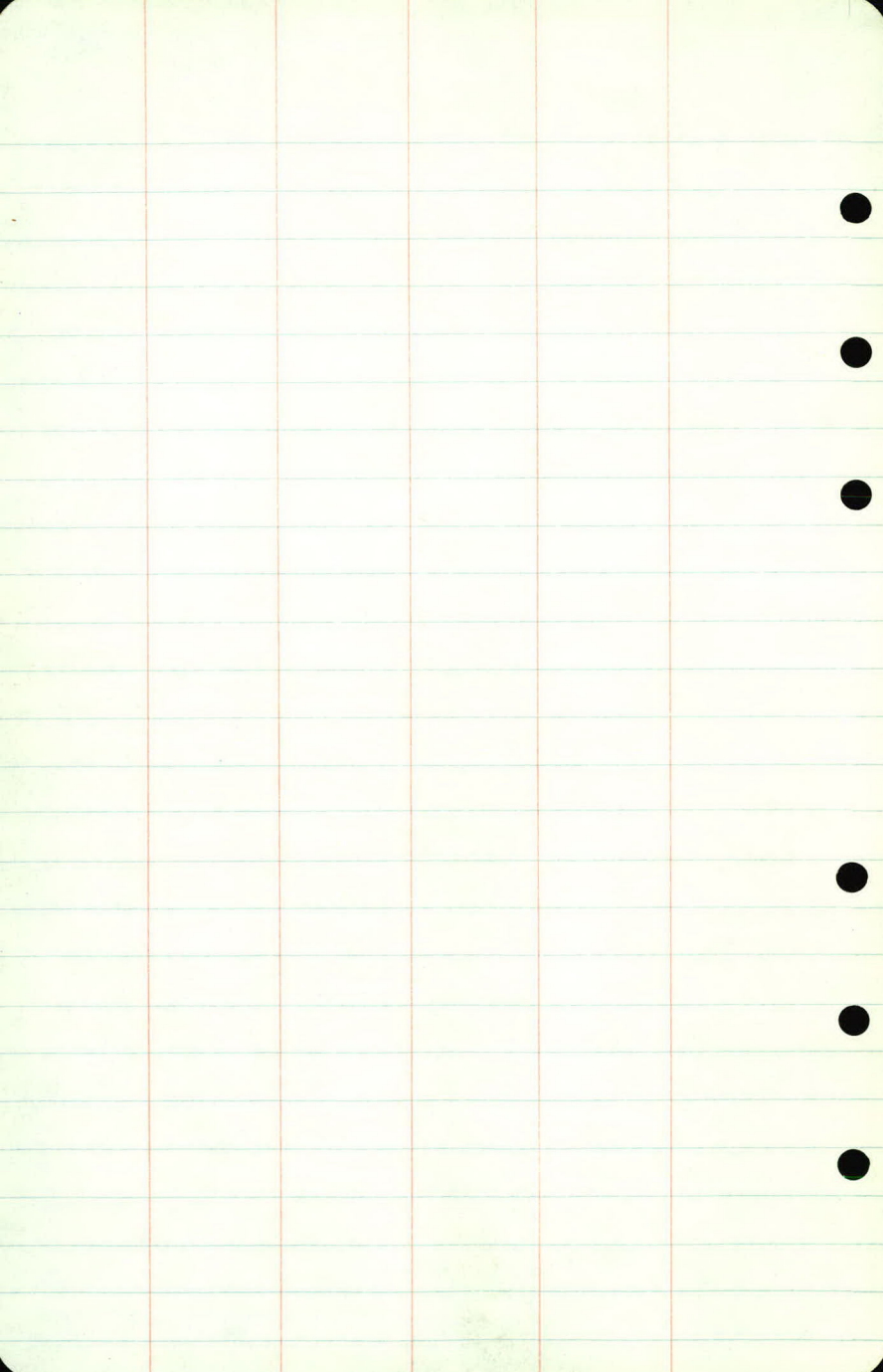
$$\begin{array}{r} 7.4 \\ C \ 14 \\ \hline 29.3 \end{array}$$

2 : 1 slope

$$\begin{array}{r} 75.8 \\ C \ 22 \\ \hline 30.9 \end{array}$$

1 1/2 : 1

$$\begin{array}{r} 14.2 \\ C \ 47 \\ \hline 33.4 \end{array}$$



New Alignment
Snelling Ave.
Co. Rd. F to G

2/6/39

RP

HW

AM

LG,

Index

Alignment - 1-4

topog - 5-14

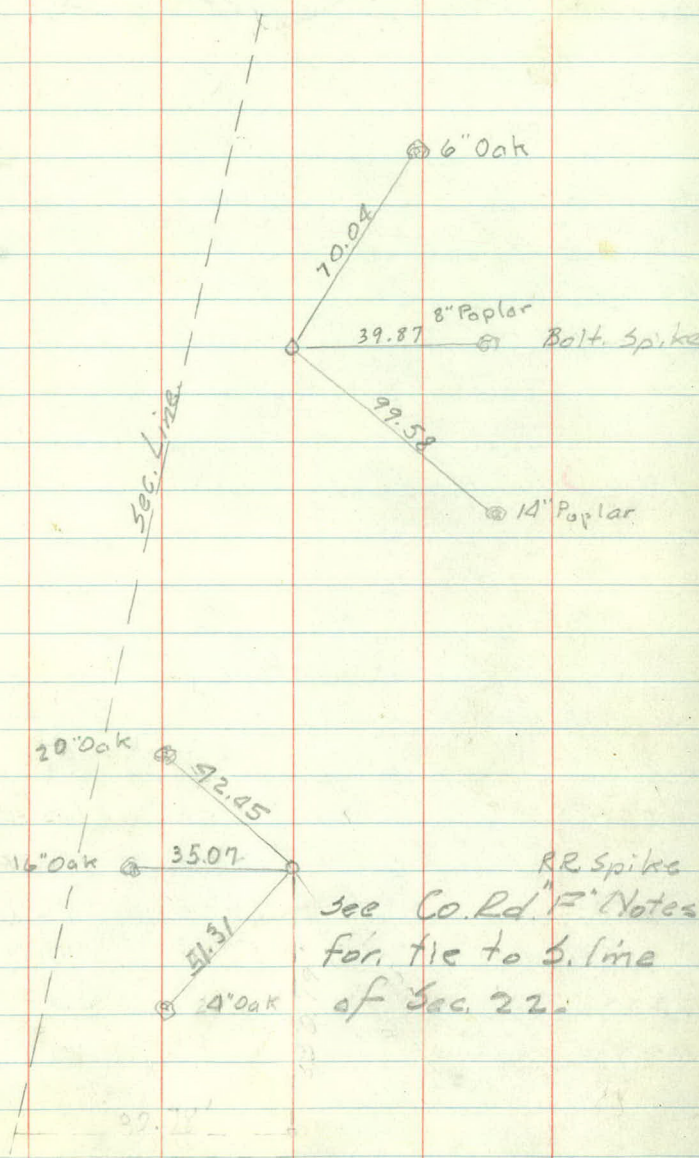
Bench levels - 15-16

X sections - 17-29

Sta	Pt.	Angle Lt Rt	Deflections
	$+48.03 = P.T.$		
	$= +47.95$ P.T.	$10^{\circ}12'$	$\Delta - 20^{\circ}24'$
8		$7^{\circ}19'$	$D = 12^{\circ}$
$7+64.10$	P.I.	$20^{\circ}24'$	$T = 86.07$
$+50$		$4^{\circ}19'$	$L = 170.0^{\circ} \checkmark$
7		$10^{\circ}19'$	$R = 478.339 \checkmark$
$6+77.95$	P.C.	$0^{\circ}00'$	
$+78.03$			

	$+1738 = P.T.$		
	$= +16.83$ P.T.	$21^{\circ}41'$	$\Delta - 43^{\circ}22' RT$
2		$20^{\circ}0'$	$D = 20^{\circ}$
$+50$		$15^{\circ}0'$	$T = 113.93$ 114.48
$1+13.93$	P.I.	$43^{\circ}22'$	$L = 216.83^{\circ} \checkmark$
1		$10^{\circ}0'$	$R = 287.9^{\circ} \checkmark$
$+50$		$5^{\circ}0''$	
$0-0.55$	P.C.	$0^{\circ}00'$	$= 0+72.3$ Co. P.I.F.
$0+00$	P.C.		

32.24



Sta.	Pt.	Angle	Dist.
		Rt	Rt

22 + 89.75 P.O.T

+40.15 ✓
 +39.93 P.T.

13
 12 + 54.20 P.I.
 + 50

12 P.C.
 11 + 64.6 P.C.

13° 10'

10° 10'

26° 20'

6° 25'

2° 40'

0° 00'

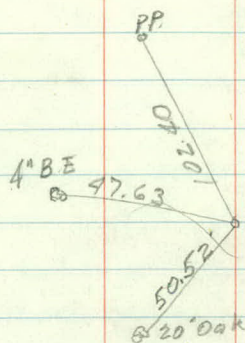
$\Delta = 26^\circ 20'$

$D = 15'$

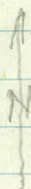
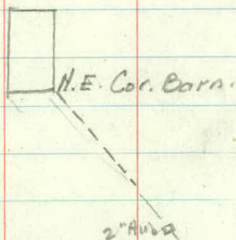
$T = 89.60$ ✓

$L = 175.33$ ✓

$R = 383.065$ ✓

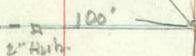


Spike



Lightning Rod

top Cupola
of Barn



Bolt Spike

Sec Line
870.67
100.72
100.72

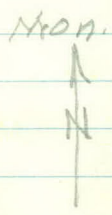
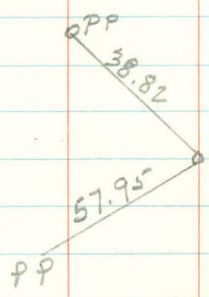
Sta.	P.T.	Lt.	Angle Rt.	Deflection
------	------	-----	--------------	------------

56+58.18 P.O.T.

30+26.53 P.I.

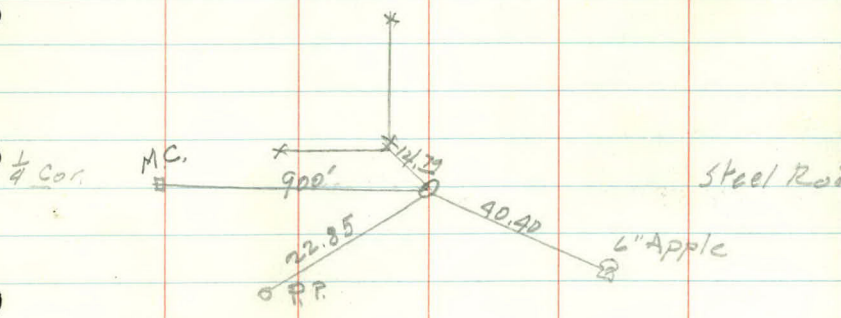
= 0°07'

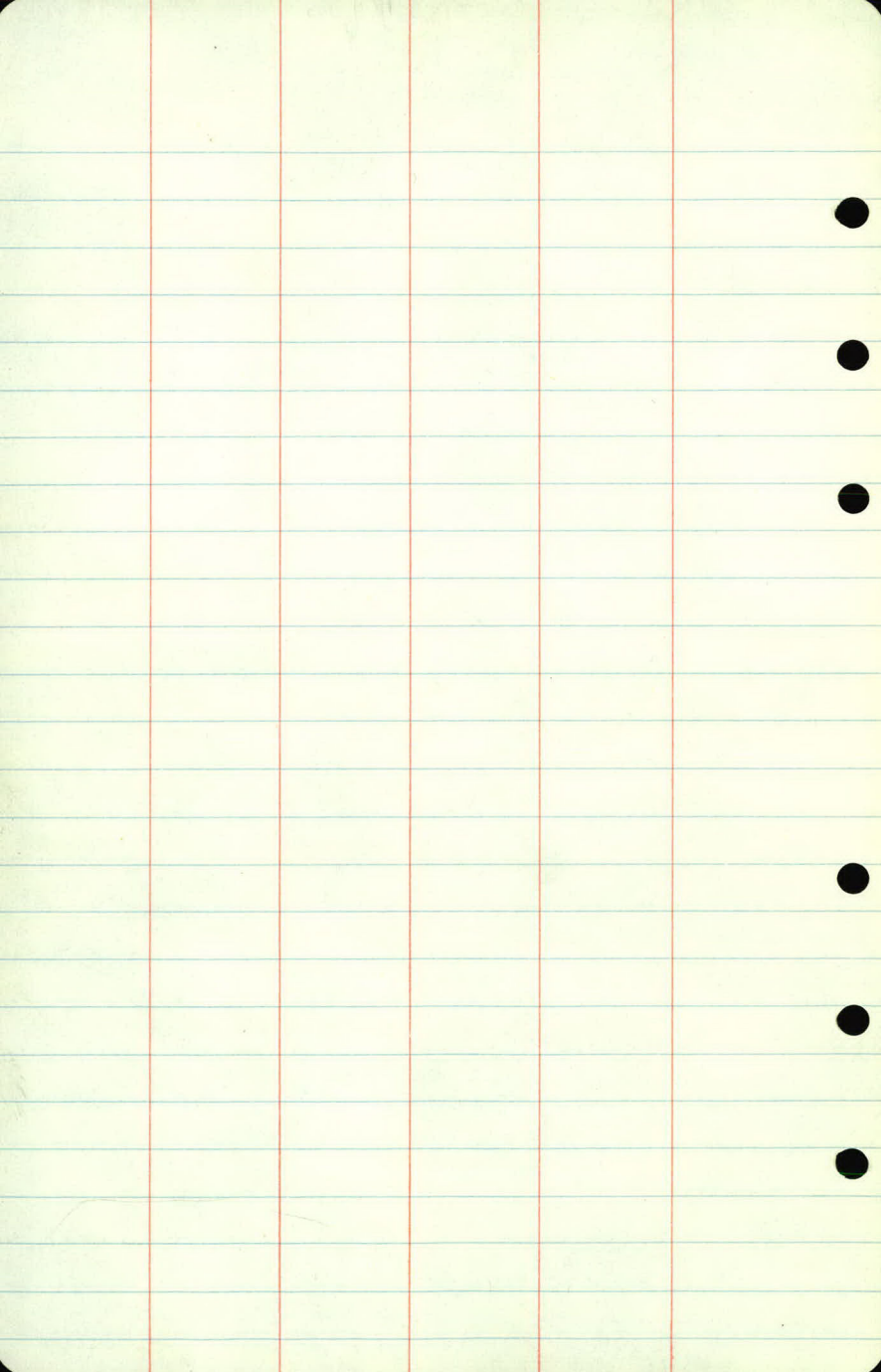
Co. Ed. G.



Sec. 21

Sec. 22





5
Topography

Snelling Ave.

Co. Rd. "F" to Co. Rd. "G"

9 13

6 9' 15'

5 5 20 .

4 3' 25' .

2' 25' .

3 8' 19' .

18' 5' .

2 35-6 .

42'-18' .

1 37'-12' .

22: 0 .

0 6' 15' .

Lake

+64	24" Pop	17'	②
+54	24" Pop	17'	②

Woods +70-24" Pop. 32.
Oaks

Shore
wampole
Lake
brush - etc.

Wooded
Oaks & Pop.

Cultivated ~~is~~ uncultivated

Fe. 54 .

+50 Fe. 40 .

Fe. 24 .

7 28

9' - 28'

13

14' - 31'

13' - 33'

12

6' - 32'

+65 0 28

11

8' 20'

13' 15'

10

14' 13'

9

16' 13'

12' 16'

8

9' 15'

10' 14'

7

18'

+06-12" 36" C.M.
9-13

18'

+90 Ent.

+60 P.P. 5'

Cult

Bluish
Scrub Oak

+50

Swamp - Brush etc.

Cult

+18 12' Oak -36'

woods

+63 12' Pop -33'

0-21

20

4-22

19

3-30

18

9-31

0

+55-12"x42' Vit. •

42.

17

11-35

16

14-37

15-37

15

12-35

9-32

14

7-28'

+64 P.P. 11'
+58 Ent.

+87 P.P. 08'

+05 P.P. 08'

+28 P.P. -06'

Swampy Low Land
Standing Water

Pot
Hole

Cut

Brush

10-11

27

9-10

26

14-9

25

12-11

24

8-14

23

7-18

22

1-20

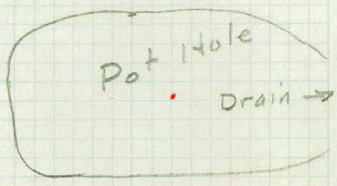
21

0-21

- +47 - Ent. Orch. 28'
- +97 - 12" B.E. 28'
- +83 - Twin B.E. 28'
- Orch. • +69 - 6" B.E. 28'
- +57 - 6" B.E. 28'
- +41 - Maple 28'
- +30 - Orch. - 46'

+93 - P.P. - 16'
 +90 - Triple Pop. 28'

Drainage ←



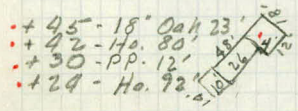
+40 P.P. 14'

Cult.

Cult.

• +92 P.P. - 12'

• +70 Ent.



- +45 - 18" Oak 23'
- +42 - Ho. 80'
- +30 - P.P. 12'
- +24 - Ho. 92'

10 - 12

34

12' 13'

33

12' 12'

32

10' 11'

31

10' 12'

30

12 - 12

29

11 - 12

28

10 - 11

Fe 13'

10

+58 PP-17'

Fe 13'

+09 PP-16'
Fe 13'

Fe. 14'

+57 PP-15'

Fe. 14'

+27 Fe. Cor. -15'
+10 P.P. -15'

+45 PP-16'

+20 End. Orch. 28'

+10 Orchard 28'

+45 Beg. Row Tr. 17'
+30 Ent.

+11 Beg. Row Tr. 34'
+00 18" Pop. 18'

9' 11'

41

11' 13'

40

10' 14'

39

9' 15'

+24-12" x 68" V.F.

38

9' 17'

37

8' 14'

36

36

9' 14'

35

10' 12'

Fe. 20' - 26'.

+60 R.P.-19.

Fe. 17' - 25'

Posture

+137 Cor. 24'
+12-PP-18' x
Fe Cor. 12' x

Fe 11'.

+03-CW/V. 28'.

CW/V.

+56 PP-18'.

+36 Ent.

Fe 12'.

CW/V.

+08-PP-17'.
Fe. 12'.

Fe 13'.

7' 16'

48

9' - 13'

47

10' 13'

46

10' 14'

45

17'

+21 - 12" 42' V. f

25'

10' - 15'

44

10' 13'

43

9 12

42

9 11

+89 Grape Arbor 19' ^{Yard}

+59 Fe. Cor. 23' ^{Yard}

+11 PP-22' ^{Hog}
Fe. 22' ^{Yard}

+36 Fe Cor. 18'-23'

Fe. 18'

+60 PP 22'

Fe. 19' ^{Hog Wallow}

+12 PP-22'
Fe. 21'

+75 Fe. Cor. 28'

+11

Fe. 21-27'

+60 PP. 20' ^{Posture.}

Fe 20-26'

+15
+71 PP-20'
Fe 20-26'

Cultivated.

+55 Rye Tie Ent.
+40 Ent.
+20 End Yard.

+10 Beg. Yard.

55

12' 13'

54

11' 10'

53

11' 11'

52

8' 13'

51

7' 16'

50

4' - 20'

49

7 16

+61 PP - 26'

o

+95 PP - 24'

o

cut.

End Yard.

+66 Apple - 36'

o

+27 P.R. 24'

o

+01 Apple - 31'

o

+48 Apple - 14'

+44 Dog Kennel - 18'

+30 Apple - 14'

+28 Apple - 30'

+18 Coach - 44 (10x42)'

+94 Dog Kennel - 41'

+97 Plum - 14'

+62 PP - 23'

+39 Maple - 24'

+18 Ent.

+04 - 50 W. 28'

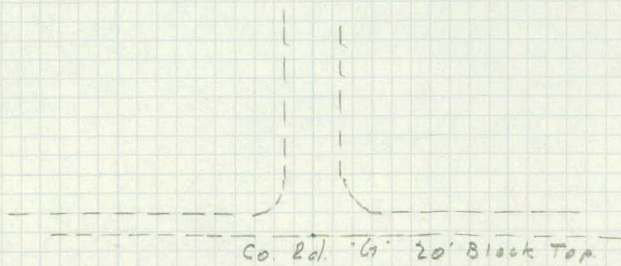
Yard

57

468 Edge Blacktop.
448 Edge Blacktop.

3-6

14' 14'



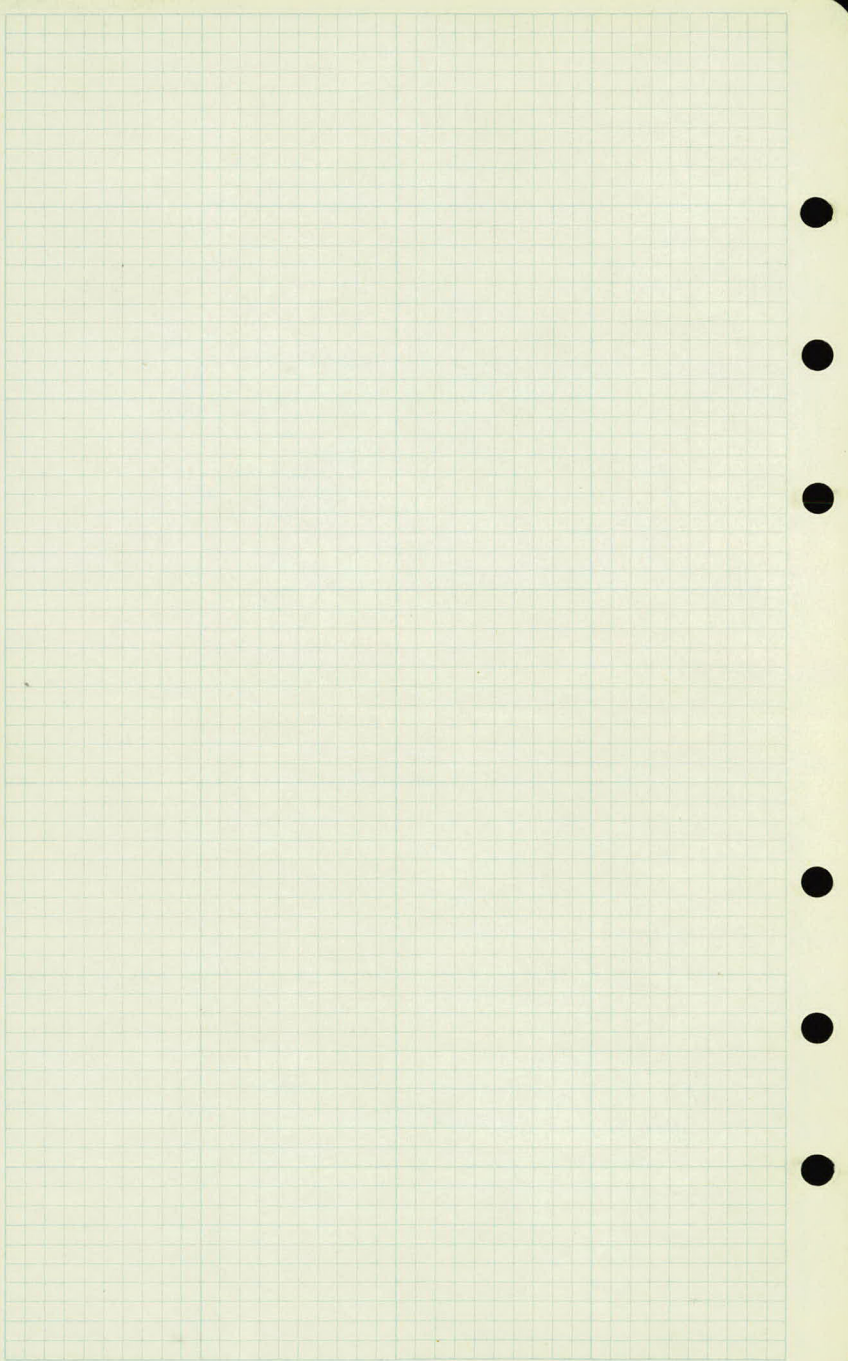
+38 End Rad 58'

Bag Rad +0.5' - 14'

+106 PP 26'

+38 End Rad 58'

Bag Rad +0.5' - 14'



Bench Levels

Snelling Ave.

Co. Rd. F to "G"

1/31/39

R.P.
H.W.
A.M.
L.G.

Pt.	+	π	-	Elev.
B.M.	0.95	920.48		919.53
T.P.	0.31	907.24	13.55	906.93
T.P.	0.15	895.14	12.25	894.99
T.P.	6.04	890.16	11.02	884.12
B.M.			2.27	887.89
T.P.	7.60	892.81	4.95	885.21
T.P.	11.47	899.16	5.12	887.69
T.P.	12.98	911.91	0.23	898.93
B.M.			0.05	911.86
T.P.	4.66	916.16	0.41	911.50
T.P.	13.72	924.89	5.04	911.12
T.P.	5.72	924.64	5.92	918.92
T.P.	12.31	932.28	4.67	919.97
B.M.			0.41	931.87
T.P.	4.22	936.36	0.14	932.14
T.P.	12.68	945.70	3.34	933.02
T.P.	7.37	948.30	4.77	940.93
B.M.			0.35	947.95

Spike in 24" Oak. 25' Lt. 0+70 (Tangent)

Spike in 12" Oak 36' Rt. Sta. 8+18

Spike in 18" Oak 23' Lt. Sta. 21+45

Spike in Fe. Post. 28' Lt. Sta. 41+17

Top. Mon. Snelling & Co. Rd 'G' Sta. 56+58.1

Sta.

+

π

-

Elev.

B.M.

919.53

0 + 00

Cross Sections
 Snelling Ave.
 Co. Rd. "F" to "G."

2/6/99

Note:

All Sections Backed in -
 Turns must be brought S.
 from Co. Rd. "G"

Sta. + ∇ - Elev.

B.M.			12.96	719.53	919.53
0+00				(19.0)	
T.P.	2.51	932.49	3.61	929.98	919.85
0+00	2.51				

0+35

(16.9)

1+00

(17.9)

1+25

(14.8)

933.59



Distances Betw Sections

2+17
2.3
2+00
6.4
1+50
2.8
1+25
2.8
1+00
7.4
+35
5.8
0+00

$$\begin{array}{r} 13.5 \\ 2.6 \quad 2.7 \quad 4.3 \quad 9.7 \quad 133 \quad 18.0 \\ \hline 29 \quad 50 \quad 100 \quad 157 \quad 300 \quad 350 \end{array}$$

$$\begin{array}{r} 16.7 \\ 10.4 \quad 2.4 \quad 5.5 \quad 7.6 \quad 12.6 \\ \hline 29 \quad 100 \quad 135 \quad 157 \quad 200 \end{array}$$

$$\begin{array}{r} 15.7 \\ 6.7 \quad 5.5 \quad 5.3 \quad 11.1 \quad 14.5 \quad 19.2 \\ \hline 100 \quad 135 \quad 153 \quad 200 \quad 227 \quad 250 \end{array}$$

$$\begin{array}{r} 18.8 \\ 10.2 \quad 7.0 \quad 11.0 \quad 14.5 \quad 18.7 \\ \hline 100 \quad 155 \quad 200 \quad 231 \quad 250 \end{array}$$

Sta	+	⌞	-	Elev.
1+50				(10.4)

2+00				(05.0)
------	--	--	--	--------

2+17				(04.5)
------	--	--	--	--------

2+50				(03.4)
------	--	--	--	--------

T.P.	13.52	933.59	0.72	920.07
0+00			1.8	19.0

0+35			3.9	16.9
------	--	--	-----	------

1+00			2.9	17.9
------	--	--	-----	------

1+25			6.0	14.8
------	--	--	-----	------

1+50				(10.4)
B.M.			1.26	919.53 ^{CH 20P} 919.53

T.P.	9.61	920.79	1.01	911.18
------	------	--------	------	--------

1+25				(14.8)
------	--	--	--	--------

+50			1.8	10.4
-----	--	--	-----	------

2+00			7.2	05.0
------	--	--	-----	------

912.19

$$\textcircled{23.2} \quad \frac{13.1}{100} \quad \frac{8.3}{149} \quad \frac{11.7}{200} \quad \frac{13.8}{222} \quad \frac{19.3}{250}$$

$$\textcircled{28.6} \quad \frac{18.7}{100} \quad \frac{14.0}{132} \quad \frac{11.1}{164} \quad \frac{12.4}{200} \quad \frac{14.0}{229} \quad \frac{18.2}{250}$$

$$\textcircled{29.1} \quad \frac{12.0}{164} \quad \frac{12.5}{190} \quad \frac{13.6}{220} \quad \frac{18.6}{250}$$

$$\textcircled{30.2} \quad \frac{16.3}{157} \quad \frac{15.8}{200} \quad \frac{19.8}{250}$$

$$\frac{+6.0}{50} \quad \frac{+6.4}{90} \quad \frac{+7.4}{31} \quad \frac{1.9}{20} \quad \frac{2.0}{17} \quad \frac{1.6}{9} \quad 1.8 \quad \frac{2.3}{7.0} \quad \frac{2.0}{12} \quad \frac{0.4}{18}$$

$$\frac{+9.0}{50} \quad \frac{+11.0}{39} \quad \frac{0.0}{29} \quad \frac{3.2}{26} \quad \frac{4.0}{20} \quad \frac{3.5}{11} \quad 3.9 \quad \frac{3.9}{4} \quad \frac{1.7}{11}$$

$$\frac{4.9}{50} \quad \frac{8.7}{47} \quad \frac{8.7}{41} \quad \frac{7.4}{39} \quad \frac{7.3}{24} \quad \frac{7.9}{12} \quad \frac{8.2}{8} \quad \frac{3.1}{2} \quad 2.9 \quad \frac{1.1}{38} \quad \frac{0.3}{46}$$

$$\frac{6.0}{7} \quad 6.0 \quad \frac{4.3}{40} \quad \frac{3.1}{50}$$

$$\textcircled{10.4} \quad \frac{8.0}{4} \quad \frac{5.5}{50}$$

Spike in 24" Oak 35' Lt. 0.70

$$\frac{2.5}{50} \quad \frac{0.2}{45} \quad \frac{0.4}{38} \quad \frac{0.3}{28} \quad \frac{1.6}{15} \quad \frac{1.8}{13} \quad \textcircled{+2.6}$$

$$\frac{1.4}{50} \quad \frac{1.9}{42} \quad \frac{2.3}{28} \quad \frac{3.4}{14} \quad \frac{3.9}{9} \quad 1.8$$

$$\frac{9.3}{50} \quad \frac{9.3}{47} \quad \frac{6.0}{35} \quad \frac{5.6}{20} \quad 7.2 \quad \frac{7.9}{18} \quad \frac{2.0}{31} \quad \frac{1.7}{50} \quad \frac{0.0}{73}$$

Sta	+	↑	-	Elev
2+17			7.7	04.5
2+50			8.8	03.4
3+00.			11.8	00.4
T.P.	13.02	912.19	0.65	899.17
3				(00.4)
3+50			2.7	97.1
4			5.2	94.6
4+50			7.3	92.5
T.P.	9.95	899.82	0.32	889.87
3				(00.4)
+50				(97.1)
4				(94.6)
+50				(92.5)
5			0.0	90.2
		890.19		

$$\begin{array}{r} 12.0 \\ 50 \end{array} \quad \begin{array}{r} 12.0 \\ 40 \end{array} \quad \begin{array}{r} 6.7 \\ 23 \end{array} \quad \begin{array}{r} 6.6 \\ 13 \end{array} \quad 7.7 \quad \begin{array}{r} 8.5 \\ 25 \end{array} \quad \begin{array}{r} 2.9 \\ 36 \end{array} \quad \begin{array}{r} 2.8 \\ 50 \end{array} \quad \begin{array}{r} 0.0 \\ 90 \end{array}$$

$$\begin{array}{r} 20.7 \\ 50 \end{array} \quad \begin{array}{r} 20.0 \\ 43 \end{array} \quad \begin{array}{r} 8.8 \\ 20 \end{array} \quad 8.8 \quad \begin{array}{r} 9.5 \\ 7 \end{array} \quad \begin{array}{r} 10.0 \\ 15 \end{array} \quad \begin{array}{r} 10.0 \\ 32 \end{array} \quad \begin{array}{r} 8.0 \\ 41 \end{array} \quad \begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 6.7 \\ 75 \end{array} \quad \begin{array}{r} 4.3 \\ 100 \end{array}$$

$$\begin{array}{r} 12.2 \\ 7 \end{array} \quad 11.8 \quad \begin{array}{r} 12.0 \\ 18 \end{array}$$

$$+0.6 \quad \begin{array}{r} 6.9 \\ 27 \end{array} \quad \begin{array}{r} 4.9 \\ 35 \end{array} \quad \begin{array}{r} 3.7 \\ 39 \end{array} \quad \begin{array}{r} 4.2 \\ 50 \end{array}$$

$$\begin{array}{r} 3.0 \\ 3 \end{array} \quad 2.7 \quad \begin{array}{r} 2.4 \\ 10 \end{array} \quad \begin{array}{r} 3.2 \\ 25 \end{array}$$

$$\begin{array}{r} 5.3 \\ 3 \end{array} \quad 5.2 \quad \begin{array}{r} 4.7 \\ 12 \end{array} \quad \begin{array}{r} 5.4 \\ 25 \end{array}$$

$$\begin{array}{r} 7.7 \\ 5 \end{array} \quad 7.3 \quad \begin{array}{r} 7.0 \\ 10 \end{array} \quad \begin{array}{r} 7.6 \\ 23 \end{array}$$

$$\begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 40 \end{array} \quad \begin{array}{r} 3.9 \\ 30 \end{array}$$

$$+10.2$$

$$\begin{array}{r} 10.6 \\ 50 \end{array} \quad \begin{array}{r} 8.4 \\ 31 \end{array} \quad \begin{array}{r} 7.0 \\ 24 \end{array}$$

$$+6.9$$

$$\begin{array}{r} 1.0 \\ 34 \end{array} \quad \begin{array}{r} 0.9 \\ 50 \end{array}$$

$$\begin{array}{r} 11.1 \\ 50 \end{array} \quad \begin{array}{r} 7.7 \\ 25 \end{array}$$

$$+4.4$$

$$\begin{array}{r} 3.7 \\ 37 \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array}$$

$$\begin{array}{r} 11.4 \\ 50 \end{array} \quad \begin{array}{r} 10.6 \\ 34 \end{array} \quad \begin{array}{r} 8.9 \\ 24 \end{array}$$

$$+2.3$$

$$\begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 37 \end{array} \quad \begin{array}{r} 4.7 \\ 50 \end{array}$$

$$\begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 10.6 \\ 33 \end{array} \quad \begin{array}{r} 9.0 \\ 19 \end{array} \quad \begin{array}{r} 0.2 \\ 5 \end{array} \quad 0.0 \quad \begin{array}{r} 10.1 \\ 11 \end{array} \quad \begin{array}{r} 0.4 \\ 20 \end{array} \quad \begin{array}{r} 5.6 \\ 31 \end{array} \quad \begin{array}{r} 5.6 \\ 45 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

Sta + π - Elev

5+50 1.6 88.6

6 2.9 87.3

+50 4.3 85.9

7 5.4 84.8

+0.6 12" x 26" X Drain

+50 6.1 84.1

8 6.3 83.9

B.M. 2.30 890.19 2.38 887.88 887.89

+50 5.8 84.5

9 5.2 85.1

+50 5.1 85.2

10 5.2 85.1

+50 5.6 84.7

11 5.8 84.5

890.26

$$\frac{11.0}{50} \frac{10.7}{32} \frac{9.2}{20} \frac{2.1}{8} \frac{1.7}{16} \frac{5.8}{27} \frac{5.7}{38} \frac{3.3}{50}$$

$$\frac{11.4}{50} \frac{10.9}{31} \frac{9.2}{19} \frac{3.5}{9} \frac{2.9}{14} \frac{3.1}{24} \frac{7.9}{31} \frac{7.8}{40} \frac{0.8}{50} + 2.2$$

$$\frac{12.3}{50} \frac{12.1}{37} \frac{10.9}{26} \frac{5.0}{13} \frac{4.3}{74} \frac{4.5}{20} \frac{7.7}{23} \frac{8.0}{27} \frac{7.5}{39} \frac{0.0}{50} + 9.6$$

$$\frac{11.9}{50} \frac{11.0}{27} \frac{9.3}{16} \frac{5.8}{10} \frac{5.4}{13} \frac{5.8}{20} \frac{9.1}{25} \frac{9.5}{31} \frac{6.6}{50} + 8.0$$

$$\frac{10.8}{79.4} \frac{10.3}{79.9}$$

$$\frac{12.4}{50} \frac{11.6}{30} \frac{10.9}{24} \frac{10.4}{21} \frac{6.3}{10} \frac{6.1}{14} \frac{6.7}{19} \frac{8.8}{24} \frac{9.6}{28} \frac{8.8}{32} \frac{7.6}{50} + 5.5$$

$$\frac{12.4}{50} \frac{11.1}{33} \frac{10.4}{22} \frac{9.6}{15} \frac{6.7}{9} \frac{6.3}{6} \frac{6.4}{15} \frac{6.9}{24} \frac{9.3}{28} \frac{9.5}{37} \frac{4.1}{50} + 5.1$$

Spike in 12" Oak 36' Rt Sta 8+18

$$\frac{12.3}{50} \frac{10.3}{24} \frac{9.4}{18} \frac{6.8}{13} \frac{5.8}{16} \frac{6.4}{24} \frac{8.9}{30} \frac{8.4}{41} \frac{1.1}{50} + 5.9$$

$$\frac{12.2}{50} \frac{10.0}{25} \frac{5.9}{17} \frac{5.5}{11} \frac{5.2}{13} \frac{5.6}{18} \frac{6.8}{23} \frac{7.5}{30} \frac{6.3}{35} \frac{3.8}{42} \frac{0.9}{50} + 3.7$$

$$\frac{11.6}{50} \frac{9.0}{20} \frac{5.8}{14} \frac{5.1}{13} \frac{5.5}{16} \frac{7.0}{24} \frac{6.5}{29} \frac{5.3}{39} \frac{2.1}{50} + 3.0$$

$$\frac{10.8}{50} \frac{9.6}{23} \frac{8.9}{19} \frac{6.1}{14} \frac{5.2}{12} \frac{5.7}{15} \frac{6.4}{22} \frac{6.0}{31} \frac{4.0}{50} + 3.0$$

$$\frac{10.8}{50} \frac{9.2}{23} \frac{8.6}{17} \frac{6.6}{13} \frac{5.6}{15} \frac{6.0}{18} \frac{6.4}{27} \frac{5.6}{36} \frac{9.9}{50} + 1.3$$

$$\frac{11.6}{50} \frac{10.7}{31} \frac{9.7}{16} \frac{6.6}{9} \frac{5.8}{21} \frac{6.1}{22} \frac{6.8}{30} \frac{6.5}{41} \frac{4.4}{50} \frac{1.7}{50}$$

Sfa.	+	π	-	Elev.
11 + 69			5.7	84.6.
12			8.6	81.7.
T.P.	4.66	890.26	12.01	885.60.
+50			13.5	84.1.
13			5.7	91.9.
+50			6.4	91.2
14			11.0	86.6
T.P.	10.64	897.61	7.48	885.91.
+50			10.9	83.6.
15			13.4	81.1.
+50			13.6	80.9.
16			13.3	81.2.
+50			12.8	81.7.
17			13.0	81.5.
		894.45		

$$\begin{array}{r} 11.7 \quad 11.0 \quad 9.8 \quad 5.8 \quad 4.9 \quad 5.1 \quad 5.8 \quad 5.2 \quad 4.1 \quad 1.7 \\ 50 \quad 26 \quad 12 \quad 2 \quad 5.7 \quad 15 \quad 32 \quad 34 \quad 40 \quad 45 \quad 50 \end{array}$$

$$\begin{array}{r} 11.6 \quad 10.2 \quad 9.9 \quad 5.0 \quad 4.4 \quad 4.4 \quad 4.3 \quad 12.0 \\ 50 \quad 18 \quad 9 \quad 8.6 \quad 6 \quad 21 \quad 33 \quad 38 \quad 50 \end{array}$$

Top 34.5 km
P.C. - 11464

$$\begin{array}{r} 12.9 \\ 5 \\ 18.0 \quad 15.7 \quad 11.1 \quad 11.2 \quad 10.8 \quad 10.7 \quad 9.3 \quad 2.6 + 3.4 \\ 50 \quad 15 \quad 13.5 \quad 8 \quad 13 \quad 26 \quad 34 \quad 39 \quad 50 \quad 58 \end{array}$$

$$\begin{array}{r} 13.2 \quad 10.0 \quad 5.9 \quad 10.2 \quad 9.9 \quad 9.8 \quad 0.9 + 12.0 \\ 50 \quad 27 \quad 5.7 \quad 5 \quad 12 \quad 24 \quad 32 \quad 45 \quad 57 \\ + 14.0 \\ 65 \end{array}$$

$$\begin{array}{r} 11.4 \quad 6.3 \quad 5.4 \quad 10.2 \quad 10.0 \quad 9.7 \quad 9.4 \quad 6.2 \quad 0.0 \\ 50 \quad 23 \quad 6 \quad 6.4 \quad 6 \quad 10 \quad 19 \quad 29 \quad 37 \quad 46 \end{array}$$

$$\begin{array}{r} 11.5 \quad 13.5 \quad 11.1 \quad 11.0 \quad 10.9 \quad 10.3 \quad 10.2 \quad 10.4 \quad 9.6 + 11.5 \\ 50 \quad 38 \quad 10 \quad 4 \quad 11.0 \quad 7 \quad 10 \quad 19 \quad 30 \quad 34 \quad 48 \end{array}$$

$$\begin{array}{r} 14.5 \quad 13.7 \quad 13.1 \quad 8.9 \quad 8.3 \quad 7.6 \quad 7.8 \quad 8.7 \\ 50 \quad 29 \quad 9 \quad 10.9 \quad 6 \quad 11 \quad 25 \quad 38 \quad 50 \end{array}$$

$$\begin{array}{r} 14.7 \quad 14.7 \quad 14.2 \quad 12.9 \quad 9.9 \quad 8.5 \quad 8.1 \quad 8.5 \quad 8.9 \quad 9.3 \\ 50 \quad 29 \quad 6 \quad 13.4 \quad 2 \quad 8 \quad 13 \quad 25 \quad 38 \quad 44 \quad 50 \end{array}$$

$$\begin{array}{r} 15.3 \quad 13.3 \quad 8.3 \quad 7.9 \quad 8.5 \quad 8.8 \\ 50 \quad 13.6 \quad 4 \quad 14 \quad 26 \quad 42 \quad 50 \end{array}$$

$$\begin{array}{r} 15.3 \quad 15.0 \quad 12.8 \quad 7.8 \quad 7.4 \quad 7.7 \quad 8.3 \\ 50 \quad 24 \quad 13.3 \quad 4 \quad 13 \quad 25 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 15.0 \quad 14.6 \quad 13.5 \quad 7.3 \quad 6.7 \quad 6.9 \quad 7.6 \quad 7.3 \\ 50 \quad 32 \quad 8 \quad 12.8 \quad 12 \quad 27 \quad 40 \quad 46 \quad 50 \end{array}$$

$$\begin{array}{r} 14.9 \quad 14.0 \quad 13.4 \quad 6.7 \quad 5.8 \quad 6.4 \quad 7.0 \quad 7.8 \\ 50 \quad 12 \quad 3 \quad 13.0 \quad 9 \quad 23 \quad 36 \quad 40 \quad 50 \end{array}$$

Sta	+	+	-	Elev	
17+50			10.7	83.8.	
+ 55	(2" x 4" x Drain				
18			9.4	85.1.	
T.P.	2.97	894.45	11.52	891.48.	
+ 50			15.4	87.6.	
19			9.2	93.8.	
+ 50			6.2	96.8.	
20			3.8	99.2.	
T.P.	1.37	903.00	10.58	901.63.	
+ 50			10.7	01.5.	
21			8.9	03.3	
+ 50			7.7	04.5	
22			6.0	06.2	
+ 50			3.7	08.5	
B.M	0.35	912.21	3.73	911.88	2-3-39 Very Cold - Clear
T.P.	4.37	915.61	10.97	911.24.	
23			12.3	09.9.	
		922.21			

$$\begin{array}{r} 15.0 \\ 50 \end{array} \quad \begin{array}{r} 14.3 \\ 18 \end{array} \quad \begin{array}{r} 12.5 \\ 6 \end{array} \quad \begin{array}{r} 5.3 \\ 9 \end{array} \quad \begin{array}{r} 4.7 \\ 22 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array} \quad \begin{array}{r} 7.3 \\ 40 \end{array} \quad \begin{array}{r} 9.8 \\ 50 \end{array}$$

$$\begin{array}{r} 13.7 \\ 10.7 \end{array} \quad \begin{array}{r} 80.8 \\ 9 \end{array}$$

$$\begin{array}{r} 12.3 \\ 82.2 \end{array}$$

$$\begin{array}{r} 14.0 \\ 50 \end{array} \quad \begin{array}{r} 13.8 \\ 22 \end{array} \quad \begin{array}{r} 12.6 \\ 12 \end{array} \quad \begin{array}{r} 9.4 \\ 9 \end{array} \quad \begin{array}{r} 3.2 \\ 9 \end{array} \quad \begin{array}{r} 2.7 \\ 21 \end{array} \quad \begin{array}{r} 3.2 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 39 \end{array} \quad \begin{array}{r} 7.6 \\ 50 \end{array}$$

$$\begin{array}{r} 20.0 \\ 50 \end{array} \quad \begin{array}{r} 17.5 \\ 28 \end{array} \quad \begin{array}{r} 17.3 \\ 12 \end{array} \quad \begin{array}{r} 15.4 \\ 6 \end{array} \quad \begin{array}{r} 10.6 \\ 6 \end{array} \quad \begin{array}{r} 9.3 \\ 20 \end{array} \quad \begin{array}{r} 9.6 \\ 34 \end{array} \quad \begin{array}{r} 13.0 \\ 58 \end{array} \quad \begin{array}{r} 13.2 \\ 50 \end{array}$$

$$\begin{array}{r} 13.8 \\ 50 \end{array} \quad \begin{array}{r} 11.8 \\ 18 \end{array} \quad \begin{array}{r} 11.0 \\ 6 \end{array} \quad \begin{array}{r} 9.2 \\ 9 \end{array} \quad \begin{array}{r} 7.8 \\ 4 \end{array} \quad \begin{array}{r} 7.3 \\ 79 \end{array} \quad \begin{array}{r} 7.8 \\ 30 \end{array} \quad \begin{array}{r} 9.4 \\ 34 \end{array} \quad \begin{array}{r} 9.7 \\ 50 \end{array}$$

$$\begin{array}{r} 9.0 \\ 50 \end{array} \quad \begin{array}{r} 7.4 \\ 14 \end{array} \quad \begin{array}{r} 6.2 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 29 \end{array} \quad \begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 35 \end{array} \quad \begin{array}{r} 4.4 \\ 43 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 3.0 \\ 13 \end{array} \quad \begin{array}{r} 1.5 \\ 5 \end{array} \quad \begin{array}{r} 3.7 \\ 3 \end{array} \quad \begin{array}{r} 3.8 \\ 12 \end{array} \quad \begin{array}{r} 3.3 \\ 24 \end{array} \quad \begin{array}{r} 3.7 \\ 29 \end{array} \quad \begin{array}{r} 2.9 \\ 36 \end{array} \quad \begin{array}{r} 1.0 \\ 45 \end{array} \quad \begin{array}{r} 15.5 \\ 50 \end{array} \quad \begin{array}{r} 15.5 \\ 50 \end{array}$$

$$\begin{array}{r} 10.7 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 5.4 \\ 11 \end{array} \quad \begin{array}{r} 10.1 \\ 5 \end{array} \quad \begin{array}{r} 10.7 \\ 2 \end{array} \quad \begin{array}{r} 10.7 \\ 10.7 \end{array} \quad \begin{array}{r} 10.7 \\ 23 \end{array} \quad \begin{array}{r} 5.0 \\ 36 \end{array} \quad \begin{array}{r} 0.4 \\ 41 \end{array} \quad \begin{array}{r} +1.5 \\ 44 \end{array} \quad \begin{array}{r} +1.6 \\ 50 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array} \quad \begin{array}{r} 3.4 \\ 18 \end{array} \quad \begin{array}{r} 2.9 \\ 14 \end{array} \quad \begin{array}{r} 8.8 \\ 5 \end{array} \quad \begin{array}{r} 8.8 \\ 3 \end{array} \quad \begin{array}{r} 8.9 \\ 8.9 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \end{array} \quad \begin{array}{r} 8.7 \\ 24 \end{array} \quad \begin{array}{r} 7.4 \\ 27 \end{array} \quad \begin{array}{r} 3.9 \\ 32 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} +0.2 \\ 50 \end{array} \quad \begin{array}{r} 2.6 \\ 19 \end{array} \quad \begin{array}{r} 7.3 \\ 8 \end{array} \quad \begin{array}{r} 7.3 \\ 3 \end{array} \quad \begin{array}{r} 7.7 \\ 7.7 \end{array} \quad \begin{array}{r} 7.0 \\ 10 \end{array} \quad \begin{array}{r} 7.3 \\ 21 \end{array} \quad \begin{array}{r} 7.5 \\ 25 \end{array} \quad \begin{array}{r} 5.8 \\ 27 \end{array} \quad \begin{array}{r} 6.8 \\ 50 \end{array}$$

$$\begin{array}{r} +1.6 \\ 50 \end{array} \quad \begin{array}{r} 2.5 \\ 16 \end{array} \quad \begin{array}{r} 5.7 \\ 7 \end{array} \quad \begin{array}{r} 6.1 \\ 3 \end{array} \quad \begin{array}{r} 6.0 \\ 6.0 \end{array} \quad \begin{array}{r} 5.7 \\ 21 \end{array} \quad \begin{array}{r} 6.0 \\ 24 \end{array} \quad \begin{array}{r} 4.2 \\ 28 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array}$$

$$\begin{array}{r} 0.1 \\ 50 \end{array} \quad \begin{array}{r} 1.4 \\ 23 \end{array} \quad \begin{array}{r} 3.3 \\ 12 \end{array} \quad \begin{array}{r} 3.6 \\ 5 \end{array} \quad \begin{array}{r} 3.7 \\ 3.7 \end{array} \quad \begin{array}{r} 4.2 \\ 19 \end{array} \quad \begin{array}{r} 4.3 \\ 22 \end{array} \quad \begin{array}{r} 3.9 \\ 27 \end{array} \quad \begin{array}{r} 10.8 \\ 34 \end{array} \quad \begin{array}{r} 10.6 \\ 41 \end{array} \quad \begin{array}{r} +0.8 \\ 50 \end{array}$$

Spike in 18" Dok 23' Lt 5th. 21 + 45

$$\begin{array}{r} 9.6 \\ 50 \end{array} \quad \begin{array}{r} 9.4 \\ 30 \end{array} \quad \begin{array}{r} 8.6 \\ 21 \end{array} \quad \begin{array}{r} 8.6 \\ 16 \end{array} \quad \begin{array}{r} 12.7 \\ 5 \end{array} \quad \begin{array}{r} 12.7 \\ 12.7 \end{array} \quad \begin{array}{r} 12.7 \\ 19 \end{array} \quad \begin{array}{r} 12.7 \\ 23 \end{array} \quad \begin{array}{r} 12.7 \\ 26 \end{array} \quad \begin{array}{r} 9.4 \\ 34 \end{array} \quad \begin{array}{r} 3.8 \\ 45 \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array}$$

Sta	+	π	-	Elev.
23 +50			11.0	11.2
24			10.2	12.0
+50			10.2	12.0
25			10.8	11.4
T.P	11.75	922.21	11.55	910.96
+50			11.3	10.7
26			11.9	10.1
+50			11.8	10.2
27			11.5	10.5
+50			11.4	10.6
28			10.9	11.1
+50			9.8	12.2
29			7.6	14.4

$$23 + 50 \quad \begin{array}{r} 9.6 \\ 50 \end{array} \quad \begin{array}{r} 7.0 \\ 24 \end{array} \quad \begin{array}{r} 6.5 \\ 20 \end{array} \quad \begin{array}{r} 11.3 \\ 12 \end{array} \quad \begin{array}{r} 11.2 \\ 7 \end{array} \quad 11.0 \quad \begin{array}{r} 11.1 \\ 17 \end{array} \quad \begin{array}{r} 10.6 \\ 20 \end{array} \quad \begin{array}{r} 9.6 \\ 30 \end{array} \quad \begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 11.3 \\ 43 \end{array} \quad \begin{array}{r} 11.3 \\ 50 \end{array}$$

$$24 \quad \begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 3.1 \\ 27 \end{array} \quad \begin{array}{r} 7.3 \\ 18 \end{array} \quad \begin{array}{r} 10.2 \\ 13 \end{array} \quad \begin{array}{r} 10.4 \\ 10 \end{array} \quad 10.2 \quad \begin{array}{r} 10.2 \\ 12 \end{array} \quad \begin{array}{r} 9.6 \\ 19 \end{array} \quad \begin{array}{r} 7.3 \\ 25 \end{array} \quad \begin{array}{r} 5.4 \\ 29 \end{array} \quad +4.0 \quad \begin{array}{r} +4.1 \\ 42 \end{array} \quad \begin{array}{r} +4.1 \\ 50 \end{array}$$

$$+50 \quad \begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 2.0 \\ 28 \end{array} \quad \begin{array}{r} 6.1 \\ 21 \end{array} \quad \begin{array}{r} 10.5 \\ 19 \end{array} \quad \begin{array}{r} 10.8 \\ 10 \end{array} \quad 10.2 \quad \begin{array}{r} 10.3 \\ 12 \end{array} \quad \begin{array}{r} 9.8 \\ 15 \end{array} \quad \begin{array}{r} 8.4 \\ 23 \end{array} \quad \begin{array}{r} 5.9 \\ 34 \end{array} \quad \begin{array}{r} 1.4 \\ 50 \end{array}$$

$$25 \quad \begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 28 \end{array} \quad \begin{array}{r} 11.4 \\ 18 \end{array} \quad \begin{array}{r} 11.2 \\ 13 \end{array} \quad 10.8 \quad \begin{array}{r} 10.9 \\ 10 \end{array} \quad \begin{array}{r} 10.7 \\ 18 \end{array} \quad \begin{array}{r} 9.4 \\ 19 \end{array} \quad \begin{array}{r} 12.7 \\ 26 \end{array} \quad \begin{array}{r} 14.5 \\ 33 \end{array} \quad \begin{array}{r} 15.3 \\ 50 \end{array}$$

$$+50 \quad \begin{array}{r} 11.3 \\ 50 \end{array} \quad \begin{array}{r} 11.5 \\ 27 \end{array} \quad \begin{array}{r} 13.1 \\ 17 \end{array} \quad \begin{array}{r} 11.3 \\ 13 \end{array} \quad 11.3 \quad \begin{array}{r} 11.7 \\ 11 \end{array} \quad \begin{array}{r} 26.7 \\ 34 \end{array} \quad \begin{array}{r} 29.4 \\ 50 \end{array}$$

$$26 \quad \begin{array}{r} 17.0 \\ 50 \end{array} \quad \begin{array}{r} 17.5 \\ 32 \end{array} \quad \begin{array}{r} 12.5 \\ 15 \end{array} \quad 11.9 \quad \begin{array}{r} 12.4 \\ 9 \end{array} \quad \begin{array}{r} 27.7 \\ 33 \end{array} \quad \begin{array}{r} 29.4 \\ 50 \end{array}$$

$$+50 \quad \begin{array}{r} 23.1 \\ 50 \end{array} \quad \begin{array}{r} 23.1 \\ 38 \end{array} \quad \begin{array}{r} 21.0 \\ 27 \end{array} \quad \begin{array}{r} 12.4 \\ 14 \end{array} \quad 11.8 \quad \begin{array}{r} 12.1 \\ 10 \end{array} \quad \begin{array}{r} 26.1 \\ 33 \end{array} \quad \begin{array}{r} 29.1 \\ 44 \end{array} \quad \begin{array}{r} 29.1 \\ 50 \end{array}$$

$$27 \quad \begin{array}{r} 25.7 \\ 50 \end{array} \quad \begin{array}{r} 23.0 \\ 29 \end{array} \quad \begin{array}{r} 12.0 \\ 12 \end{array} \quad 11.5 \quad \begin{array}{r} 11.7 \\ 10 \end{array} \quad \begin{array}{r} 23.5 \\ 32 \end{array} \quad \begin{array}{r} 24.5 \\ 42 \end{array} \quad \begin{array}{r} 24.5 \\ 50 \end{array}$$

$$+50 \quad \begin{array}{r} 20.1 \\ 50 \end{array} \quad \begin{array}{r} 25.3 \\ 34 \end{array} \quad \begin{array}{r} 22.8 \\ 28 \end{array} \quad \begin{array}{r} 11.8 \\ 10 \end{array} \quad 11.4 \quad \begin{array}{r} 11.7 \\ 12 \end{array} \quad \begin{array}{r} 19.1 \\ 27 \end{array} \quad \begin{array}{r} 19.4 \\ 34 \end{array} \quad \begin{array}{r} 20.4 \\ 38 \end{array} \quad \begin{array}{r} 20.3 \\ 50 \end{array}$$

$$28 \quad \begin{array}{r} 29.1 \\ 50 \end{array} \quad \begin{array}{r} 27.1 \\ 45 \end{array} \quad \begin{array}{r} 25.5 \\ 34 \end{array} \quad \begin{array}{r} 12.1 \\ 11 \end{array} \quad 10.9 \quad \begin{array}{r} 10.8 \\ 12 \end{array} \quad \begin{array}{r} 17.4 \\ 24 \end{array} \quad \begin{array}{r} 17.8 \\ 50 \end{array}$$

$$+50 \quad \begin{array}{r} 25.0 \\ 50 \end{array} \quad \begin{array}{r} 23.7 \\ 40 \end{array} \quad \begin{array}{r} 22.8 \\ 32 \end{array} \quad \begin{array}{r} 10.5 \\ 11 \end{array} \quad 9.8 \quad \begin{array}{r} 9.9 \\ 12 \end{array} \quad \begin{array}{r} 13.5 \\ 20 \end{array} \quad \begin{array}{r} 13.2 \\ 29 \end{array} \quad \begin{array}{r} 12.4 \\ 50 \end{array}$$

$$29 \quad \begin{array}{r} 17.2 \\ 50 \end{array} \quad \begin{array}{r} 14.7 \\ 30 \end{array} \quad \begin{array}{r} 9.1 \\ 18 \end{array} \quad \begin{array}{r} 7.8 \\ 10 \end{array} \quad 7.6 \quad \begin{array}{r} 8.2 \\ 14 \end{array} \quad \begin{array}{r} 8.8 \\ 19 \end{array} \quad \begin{array}{r} 9.5 \\ 23 \end{array} \quad \begin{array}{r} 9.0 \\ 29 \end{array} \quad \begin{array}{r} 8.0 \\ 42 \end{array} \quad \begin{array}{r} 8.0 \\ 50 \end{array}$$

Sta	+	π	-	Elev
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T.P.	1.54	922.01	12.70	920.47
29+50			16.9	16.3

30			15.0	18.2
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+50			13.7	19.5
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31			12.7	20.5
----	--	--	------	------

+50			12.4	20.8
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32			12.9	20.3
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+30			13.1	20.1
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T.P.	9.82	933.17	1.27	923.35
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+62			5.1	19.5
-----	--	--	-----	------

33			5.5	19.1
----	--	--	-----	------

+50			5.8	18.8
-----	--	--	-----	------

34			5.6	19.0
----	--	--	-----	------

+50			5.2	19.4
-----	--	--	-----	------

924.62

18.5	14.0	17.0	17.1	16.1	14.7	12.5
50	23	15	12	16	26	50

[illegible]

$\frac{6.5}{50}$	$\frac{5.4}{33}$	$\frac{5.9}{29}$	$\frac{12.3}{20}$	$\frac{13.1}{16}$	$\frac{14.1}{10}$	13.7	$\frac{14.2}{12}$	$\frac{13.8}{15}$	$\frac{12.4}{20}$	$\frac{6.7}{27}$	$\frac{6.2}{50}$
------------------	------------------	------------------	-------------------	-------------------	-------------------	------	-------------------	-------------------	-------------------	------------------	------------------

$\frac{3.4}{50}$ $\frac{2.2}{36}$ $\frac{11.3}{20}$ $\frac{12.9}{13}$ $\frac{13.1}{9}$ 12.7 $\frac{13.2}{12}$ $\frac{11.6}{19}$ $\frac{7.6}{20}$ $\frac{4.3}{28}$ $\frac{3.2}{50}$

$\frac{2.0}{50}$	$\frac{1.5}{36}$	$\frac{5.3}{30}$	$\frac{11.3}{19}$	$\frac{12.3}{12}$	$\frac{12.8}{11}$	$\frac{12.4}{13}$	$\frac{12.6}{13}$	$\frac{10.7}{18}$	$\frac{6.5}{24}$	$\frac{4.5}{28}$	$\frac{2.5}{50}$
------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------

41	47	44	1216	13.3	12911.2	9.3	6.9	5.3	5.6
58	38	31	20	12	1219	23	25	39	50

<u>7.1</u>	<u>1.7</u>	<u>13.0</u>	<u>3.7</u>	13.7		<u>13.0</u>	<u>11.1</u>	<u>8.9</u>	<u>9.3</u>
50	26	18	14	10	13.1	18	23	41	50

5.0	5.5	5.5	5.9	5.4	5.1	5.4	3.9	4.1	5.9	7.7
30	30	21	16	12		15	19	30	36	50

10.5	10.5	8.8	5.1	5.8	6.5	6.3	6.5	8.0	9.1	10.0	10.0
50	45	37	28	30	18-17	14	11	16	22	32	30

12.1	11.7	11.0	9.9	9.1	6.4		5.9	7.0	6.6	8.8	8.1
50	33	29	18	17	11	58	17	17	27	35	20

$\frac{10.9}{50}$ $\frac{9.8}{33}$ $\frac{8.6}{18}$ $\frac{6.9}{12}$ 56 $\frac{6.1}{16}$ $\frac{5.5}{19}$ $\frac{5.7}{24}$ $\frac{5.0}{50}$

$$\begin{array}{r} 9.9 \\ 50 \end{array} \begin{array}{r} 1.4 \\ 24 \end{array} \begin{array}{r} 6.2 \\ 13 \end{array} \begin{array}{r} 5.5 \\ 9 \end{array} \begin{array}{r} 5.3 \\ 14 \end{array} \begin{array}{r} 4.3 \\ 20 \end{array} \begin{array}{r} 3.0 \\ 36 \end{array} \begin{array}{r} 2.7 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.
35			5.0	19.6
+50			5.1	19.5
36			5.3	19.3
+50			5.0	19.6
37			4.6	20.0
+50			4.7	19.9
38			4.8	19.8
Sta 24 12' x 68' X Drain				
T.P.	1.11	924.62	11.73	920.51
+50			11.6	20.6
39			9.9	22.3
+50			7.9	24.3
40			5.7	26.5

932.24

$$\begin{array}{r} 11.0 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 15 \end{array} \quad \begin{array}{r} 5.5 \\ 7 \end{array} \quad \begin{array}{r} 5.5 \\ 5 \end{array} \quad 50 \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 3.1 \\ 18 \end{array} \quad \begin{array}{r} 2.6 \\ 31 \end{array} \quad \begin{array}{r} 2.3 \\ 50 \end{array}$$

$$\begin{array}{r} 10.3 \\ 50 \end{array} \quad \begin{array}{r} 8.9 \\ 29 \end{array} \quad \begin{array}{r} 7.6 \\ 15 \end{array} \quad \begin{array}{r} 7.2 \\ 12 \end{array} \quad \begin{array}{r} 6.2 \\ 9 \end{array} \quad \begin{array}{r} 5.4 \\ 5 \end{array} \quad 51 \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 4.4 \\ 19 \end{array} \quad \begin{array}{r} 4.1 \\ 24 \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array}$$

$$\begin{array}{r} 9.2 \\ 50 \end{array} \quad \begin{array}{r} 8.6 \\ 26 \end{array} \quad \begin{array}{r} 8.1 \\ 17 \end{array} \quad \begin{array}{r} 7.5 \\ 11 \end{array} \quad \begin{array}{r} 5.8 \\ 7 \end{array} \quad 5.3 \quad \begin{array}{r} 5.2 \\ 16 \end{array} \quad \begin{array}{r} 4.8 \\ 17 \end{array} \quad \begin{array}{r} 4.5 \\ 24 \end{array} \quad \begin{array}{r} 4.5 \\ 27 \end{array} \quad \begin{array}{r} 1.9 \\ 50 \end{array}$$

$$\begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 25 \end{array} \quad \begin{array}{r} 6.3 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 8 \end{array} \quad 5.0 \quad \begin{array}{r} 5.8 \\ 15 \end{array} \quad \begin{array}{r} 4.3 \\ 17 \end{array} \quad \begin{array}{r} 4.2 \\ 20 \end{array} \quad \begin{array}{r} 4.1 \\ 29 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array} \quad \begin{array}{r} 4.4 \\ 29 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 4.3 \\ 8 \end{array} \quad \begin{array}{r} 4.7 \\ 8 \end{array} \quad 4.6 \quad \begin{array}{r} 4.9 \\ 16 \end{array} \quad \begin{array}{r} 4.6 \\ 17 \end{array} \quad \begin{array}{r} 5.1 \\ 23 \end{array} \quad \begin{array}{r} 5.4 \\ 30 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array}$$

$$\begin{array}{r} 5.4 \\ 50 \end{array} \quad \begin{array}{r} 5.3 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 10 \end{array} \quad \begin{array}{r} 5.0 \\ 8 \end{array} \quad 4.7 \quad \begin{array}{r} 5.0 \\ 17 \end{array} \quad \begin{array}{r} 6.7 \\ 24 \end{array} \quad \begin{array}{r} 8.0 \\ 30 \end{array} \quad \begin{array}{r} 8.8 \\ 38 \end{array} \quad \begin{array}{r} 10.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.7 \\ 50 \end{array} \quad \begin{array}{r} 8.6 \\ 29 \end{array} \quad \begin{array}{r} 8.5 \\ 21 \end{array} \quad \begin{array}{r} 7.7 \\ 16 \end{array} \quad \begin{array}{r} 5.2 \\ 9 \end{array} \quad 4.8 \quad \begin{array}{r} 4.9 \\ 18 \end{array} \quad \begin{array}{r} 8.0 \\ 22 \end{array} \quad \begin{array}{r} 8.7 \\ 28 \end{array} \quad \begin{array}{r} 11.1 \\ 32 \end{array} \quad \begin{array}{r} 11.1 \\ 40 \end{array} \quad \begin{array}{r} 10.4 \\ 50 \end{array}$$

Burried. 12.3 12.3 .

$$\begin{array}{r} 17.8 \\ 50 \end{array} \quad \begin{array}{r} 20.0 \\ 29 \end{array} \quad \begin{array}{r} 19.8 \\ 20 \end{array} \quad \begin{array}{r} 16.0 \\ 13 \end{array} \quad \begin{array}{r} 12.3 \\ 9 \end{array} \quad 11.6 \quad \begin{array}{r} 11.8 \\ 18 \end{array} \quad \begin{array}{r} 14.2 \\ 23 \end{array} \quad \begin{array}{r} 16.7 \\ 50 \end{array}$$

$$\begin{array}{r} 18.3 \\ 50 \end{array} \quad \begin{array}{r} 16.8 \\ 27 \end{array} \quad \begin{array}{r} 16.8 \\ 18 \end{array} \quad \begin{array}{r} 13.9 \\ 15 \end{array} \quad \begin{array}{r} 10.7 \\ 9 \end{array} \quad 9.9 \quad \begin{array}{r} 10.1 \\ 15 \end{array} \quad \begin{array}{r} 12.3 \\ 20 \end{array} \quad \begin{array}{r} 12.2 \\ 50 \end{array}$$

$$\begin{array}{r} 12.3 \\ 50 \end{array} \quad \begin{array}{r} 9.8 \\ 24 \end{array} \quad \begin{array}{r} 10.5 \\ 22 \end{array} \quad \begin{array}{r} 10.6 \\ 18 \end{array} \quad \begin{array}{r} 8.8 \\ 14 \end{array} \quad 7.9 \quad \begin{array}{r} 8.3 \\ 15 \end{array} \quad \begin{array}{r} 9.0 \\ 19 \end{array} \quad \begin{array}{r} 8.8 \\ 24 \end{array} \quad \begin{array}{r} 9.0 \\ 29 \end{array} \quad \begin{array}{r} 8.1 \\ 50 \end{array}$$

$$\begin{array}{r} 7.8 \\ 50 \end{array} \quad \begin{array}{r} 4.9 \\ 27 \end{array} \quad \begin{array}{r} 6.0 \\ 17 \end{array} \quad \begin{array}{r} 6.4 \\ 11 \end{array} \quad 5.7 \quad \begin{array}{r} 6.1 \\ 11 \end{array} \quad \begin{array}{r} 6.4 \\ 14 \end{array} \quad \begin{array}{r} 6.7 \\ 22 \end{array} \quad \begin{array}{r} 3.9 \\ 29 \end{array} \quad \begin{array}{r} 3.1 \\ 50 \end{array}$$

Sta	+	∇	-	Elev.
T.P	2.55	932.24	12.92	929.69
+50			14.5	28.1

41			12.8	29.8
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+50			11.8	30.8
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42			11.0	31.6
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+50			10.5	32.1
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43			10.5	32.1
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+50			10.6	32.0
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44			11.0	31.6
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2-2-39
Cold
windy

B.M.	10.76	942.61	5.46	931.85	931.85
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+50			6.1	31.2
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45			6.1	31.2
----	--	--	-----	------

+21	12" x 42' Vit X Drain			
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+50			5.7	31.6
-----	--	--	-----	------

T.P.	5.61	937.31	9.16	931.70
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46			9.0	31.9
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940.86

$\frac{14.3}{50}$ $\frac{12.7}{28}$ $\frac{13.5}{20}$ $\frac{15.0}{16}$ $\frac{15.0}{13}$ 14.5 $\frac{14.8}{12}$ $\frac{14.7}{19}$ $\frac{11.0}{26}$ $\frac{10.0}{39}$ $\frac{10.4}{50}$

$\frac{12.1}{50}$ $\frac{11.5}{30}$ $\frac{12.0}{20}$ $\frac{13.3}{17}$ $\frac{13.6}{15}$ $\frac{13.3}{13}$ 12.8 $\frac{13.0}{12}$ $\frac{12.2}{18}$ $\frac{9.4}{29}$ $\frac{8.9}{50}$

$\frac{11.2}{50}$ $\frac{9.6}{27}$ $\frac{9.1}{18}$ $\frac{11.8}{19}$ $\frac{12.1}{10}$ 11.8 $\frac{11.8}{14}$ $\frac{10.9}{19}$ $\frac{9.9}{21}$ $\frac{5.9}{28}$ $\frac{6.5}{50}$

$\frac{9.3}{50}$ $\frac{6.9}{27}$ $\frac{6.7}{20}$ $\frac{9.9}{15}$ $\frac{10.9}{13}$ $\frac{11.2}{11}$ 11.0 $\frac{11.0}{12}$ $\frac{9.3}{21}$ $\frac{3.0}{29}$ $\frac{1.7}{50}$

$\frac{7.9}{50}$ $\frac{5.6}{29}$ $\frac{5.6}{21}$ $\frac{9.3}{16}$ $\frac{10.8}{12}$ 10.5 $\frac{10.5}{12}$ $\frac{9.7}{19}$ $\frac{9.1}{17}$ $\frac{3.9}{26}$ $\frac{1.7}{50}$

$\frac{7.3}{50}$ $\frac{5.2}{21}$ $\frac{7.3}{19}$ $\frac{10.7}{12}$ $\frac{10.8}{9}$ 10.5 $\frac{10.6}{12}$ $\frac{9.2}{17}$ $\frac{5.4}{24}$ $\frac{5.0}{50}$ $\frac{5.1}{28}$

$\frac{9.1}{50}$ $\frac{8.4}{28}$ $\frac{8.8}{27}$ $\frac{8.6}{16}$ $\frac{10.8}{12}$ $\frac{10.8}{8}$ 10.6 $\frac{10.2}{15}$ $\frac{10.0}{18}$ $\frac{8.7}{21}$ $\frac{9.4}{50}$

$\frac{12.5}{50}$ $\frac{12.5}{28}$ $\frac{12.5}{21}$ $\frac{11.8}{16}$ $\frac{12.1}{12}$ $\frac{11.3}{10}$ 11.0 $\frac{11.2}{13}$ $\frac{12.3}{18}$ $\frac{12.8}{29}$ $\frac{13.2}{50}$

Spike in Fe. Post 28' Lt Sta. 41+17

$\frac{11.0}{50}$ $\frac{10.6}{24}$ $\frac{10.5}{18}$ $\frac{6.5}{10}$ 6.1 $\frac{6.4}{17}$ $\frac{9.6}{29}$ $\frac{9.8}{28}$ $\frac{9.6}{35}$ $\frac{9.6}{50}$

$\frac{13.0}{50}$ $\frac{12.9}{23}$ $\frac{11.7}{18}$ $\frac{9.6}{13}$ $\frac{6.7}{10}$ 6.1 $\frac{6.1}{15}$ $\frac{9.4}{21}$ $\frac{10.2}{28}$ $\frac{9.4}{44}$ $\frac{9.3}{30}$

$\frac{12.6}{17}$ 24.7. $\frac{11.9}{25}$ 25.4.

$\frac{13.4}{30}$ $\frac{13.6}{25}$ $\frac{12.1}{19}$ $\frac{9.1}{13}$ $\frac{6.5}{9}$ 5.7 $\frac{5.7}{15}$ $\frac{7.7}{19}$ $\frac{9.3}{22}$ $\frac{9.8}{26}$ $\frac{10.2}{31}$ $\frac{8.7}{50}$

$\frac{16.8}{50}$ $\frac{16.2}{28}$ $\frac{14.6}{16}$ $\frac{11.2}{11}$ $\frac{9.5}{8}$ 9.0 $\frac{8.8}{14}$ $\frac{11.4}{18}$ $\frac{12.6}{22}$ $\frac{10.0}{32}$ $\frac{11.8}{50}$

Sta	+	π	-	Elev
46+50			8.7	32.2
47			7.9	33.0
+50			6.6	34.3
48			5.3	35.6
+50			3.9	37.0
49			2.2	38.7
T.P.	1.10	940.86	11.38	939.76
+50			11.2	39.9
50			10.9	40.2
+50			10.2	40.9
51			10.0	41.1
+50			9.9	41.2
52		951.14	9.9	41.2

$$\frac{16.2}{50} \quad \frac{15.5}{29} \quad \frac{14.7}{21} \quad \frac{12.5}{15} \quad \frac{9.1}{10} \quad 8.7 \quad \frac{8.8}{14} \quad \frac{11.6}{19} \quad \frac{11.8}{21} \quad \frac{11.5}{24} \quad \frac{11.6}{30} \quad \frac{11.4}{50}$$

$$\frac{14.0}{50} \quad \frac{13.8}{28} \quad \frac{12.9}{20} \quad \frac{11.6}{15} \quad \frac{8.6}{9} \quad 7.9 \quad \frac{8.0}{13} \quad \frac{10.0}{17} \quad \frac{10.6}{21} \quad \frac{11.2}{22} \quad \frac{8.4}{50} \quad \frac{10.7}{24} \quad \frac{9.8}{32}$$

$$\frac{11.1}{50} \quad \frac{11.7}{38} \quad \frac{11.4}{25} \quad \frac{11.2}{23} \quad \frac{10.1}{15} \quad \frac{7.0}{9} \quad 6.6 \quad \frac{6.7}{14} \quad \frac{8.2}{17} \quad \frac{8.3}{20} \quad \frac{9.2}{21} \quad \frac{6.5}{23} \quad \frac{6.6}{30} \quad \frac{6.6}{50}$$

$$\frac{7.7}{50} \quad \frac{9.3}{35} \quad \frac{9.4}{27} \quad \frac{9.1}{19} \quad \frac{8.5}{15} \quad \frac{5.7}{8} \quad 5.3 \quad \frac{5.2}{8} \quad \frac{5.5}{14} \quad \frac{6.9}{17} \quad \frac{7.4}{24} \quad \frac{5.4}{50}$$

$$\frac{4.1}{50} \quad \frac{6.2}{30} \quad \frac{6.1}{24} \quad \frac{4.4}{16} \quad \frac{4.4}{12} \quad \frac{4.2}{9} \quad \frac{4.1}{6} \quad 3.9 \quad \frac{3.8}{7} \quad \frac{4.9}{16} \quad \frac{5.9}{19} \quad \frac{5.5}{24} \quad \frac{5.0}{38} \quad \frac{4.2}{50}$$

$$\frac{0.9}{50} \quad \frac{2.1}{10} \quad \frac{2.3}{6} \quad 2.2 \quad \frac{2.2}{8} \quad \frac{2.4}{15} \quad \frac{2.7}{18} \quad \frac{2.8}{23} \quad \frac{2.4}{26} \quad \frac{2.3}{50}$$

$$\frac{6.3}{50} \quad \frac{7.8}{28} \quad \frac{12.0}{13} \quad \frac{11.5}{9} \quad \frac{11.3}{6} \quad 11.2 \quad \frac{11.4}{8} \quad \frac{11.9}{17} \quad \frac{12.1}{19} \quad \frac{10.7}{23} \quad \frac{8.4}{24} \quad \frac{9.7}{50}$$

$$\frac{3.3}{50} \quad \frac{3.3}{41} \quad \frac{5.3}{13} \quad \frac{11.2}{6} \quad 10.9 \quad \frac{10.6}{8} \quad \frac{11.0}{17} \quad \frac{11.4}{14} \quad \frac{11.0}{23} \quad \frac{7.3}{30} \quad \frac{3.9}{33} \quad \frac{4.9}{50}$$

$$\frac{9.9}{50} \quad \frac{4.3}{25} \quad \frac{4.9}{15} \quad \frac{10.4}{6} \quad 10.2 \quad \frac{10.0}{9} \quad \frac{10.3}{20} \quad \frac{9.6}{23} \quad \frac{2.6}{32} \quad \frac{3.1}{50}$$

$$\frac{4.4}{50} \quad \frac{3.7}{27} \quad \frac{4.5}{16} \quad \frac{10.2}{9} \quad 10.0 \quad \frac{9.8}{7} \quad \frac{10.1}{16} \quad \frac{10.6}{18} \quad \frac{10.0}{21} \quad \frac{5.4}{24} \quad \frac{3.6}{30} \quad \frac{4.8}{50}$$

$$\frac{6.9}{50} \quad \frac{6.2}{25} \quad \frac{6.5}{18} \quad \frac{10.4}{13} \quad \frac{10.2}{9} \quad 9.9 \quad \frac{10.3}{14} \quad \frac{10.3}{18} \quad \frac{10.8}{25} \quad \frac{5.6}{30} \quad \frac{6.0}{50}$$

$$\frac{9.2}{50} \quad \frac{8.9}{35} \quad \frac{10.5}{24} \quad \frac{11.0}{16} \quad \frac{10.1}{12} \quad 9.9 \quad \frac{10.2}{17} \quad \frac{10.6}{26} \quad \frac{6.4}{32} \quad \frac{6.3}{30}$$

Sta.	+	$\bar{K}$	-	Elev
T.P.	11.22	951.14	8.80	939.92
52+54			7.7	41.0
53			7.9	40.8
+50			7.6	41.1
54			7.4	41.3
+50			7.2	41.5
55			6.6	42.1
+50			5.2	43.5
56			4.6	44.1 45.1
+26			2.2	46.5
+38			1.5	47.2
+58			0.8	47.9
B.M.	0.77	948.72		947.95

Spike in P.P. 35. of "G"

$$\frac{9.7}{50} \quad \frac{8.8}{38} \quad \frac{9.1}{18} \quad \frac{8.3}{13} \quad 7.7 \quad \frac{8.1}{7} \quad \frac{1.6}{24} \quad \frac{1.4}{33} \quad \frac{1.4}{50}$$

$$\frac{12.2}{50} \quad \frac{10.1}{34} \quad \frac{9.2}{18} \quad \frac{8.3}{13} \quad 7.9 \quad \frac{7.8}{10} \quad \frac{7.6}{20} \quad \frac{7.7}{25} \quad \frac{3.0}{33} \quad \frac{2.8}{50}$$

$$\frac{13.3}{50} \quad \frac{12.1}{33} \quad \frac{10.9}{18} \quad \frac{8.1}{11} \quad 7.6 \quad \frac{7.5}{9} \quad \frac{7.2}{19} \quad \frac{7.5}{50}$$

$$\frac{13.0}{50} \quad \frac{12.6}{31} \quad \frac{11.3}{17} \quad \frac{8.0}{7} \quad 7.4 \quad \frac{7.4}{14} \quad \frac{8.1}{17-18} \quad \frac{7.2}{21} \quad \frac{6.4}{53}$$

$$\frac{13.1}{50} \quad \frac{12.7}{33} \quad \frac{11.5}{19} \quad \frac{7.1}{10} \quad 7.2 \quad \frac{7.1}{13} \quad \frac{8.7}{18} \quad \frac{8.1}{25} \quad \frac{7.2}{50}$$

$$\frac{13.7}{50} \quad \frac{13.1}{28} \quad \frac{11.9}{20} \quad \frac{7.2}{12} \quad 6.6 \quad \frac{6.8}{11} \quad \frac{8.9}{16} \quad \frac{8.3}{50}$$

$$\frac{11.8}{50} \quad \frac{11.6}{23} \quad \frac{3.8}{11} \quad 5.2 \quad \frac{5.7}{13} \quad \frac{8.9}{18} \quad \frac{8.1}{50}$$

$$\frac{11.2}{50} \quad \frac{10.5}{27} \quad \frac{9.0}{21} \quad \frac{4.1}{13} \quad \frac{3.6}{4.6} \quad \frac{3.8}{13} \quad \frac{7.7}{20} \quad \frac{8.0}{50}$$

$$\frac{9.0}{50} \quad \frac{8.3}{35} \quad \frac{3.0}{24} \quad \frac{3.0}{16} \quad 2.2 \quad \frac{2.1}{15} \quad \frac{1.9}{22} \quad \frac{8.1}{50} \quad \frac{7.7}{50}$$

$$\frac{2.5}{50} \quad \frac{2.2}{42} \quad \frac{2.6}{28} \quad 1.5 \quad \frac{0.9}{24} \quad \frac{10.1}{50}$$

$$\frac{2.2}{50}$$

$$0.8$$

$$1 \frac{1.2}{50}$$

Top. Mon. Snelling & G.

