

BK. 67 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

Co. Rd. "C"

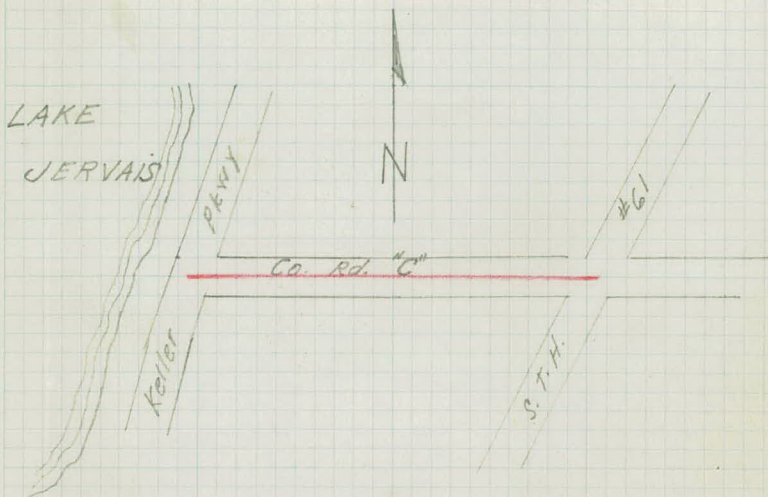
from Keller Pkwy. To S.T.H. #61

Road Acc't. No. 7

Date Filed 6-11-41

File

PLAN SURVEY
CO. RD. "C"
Keller Pkwy to S.T.H. #61



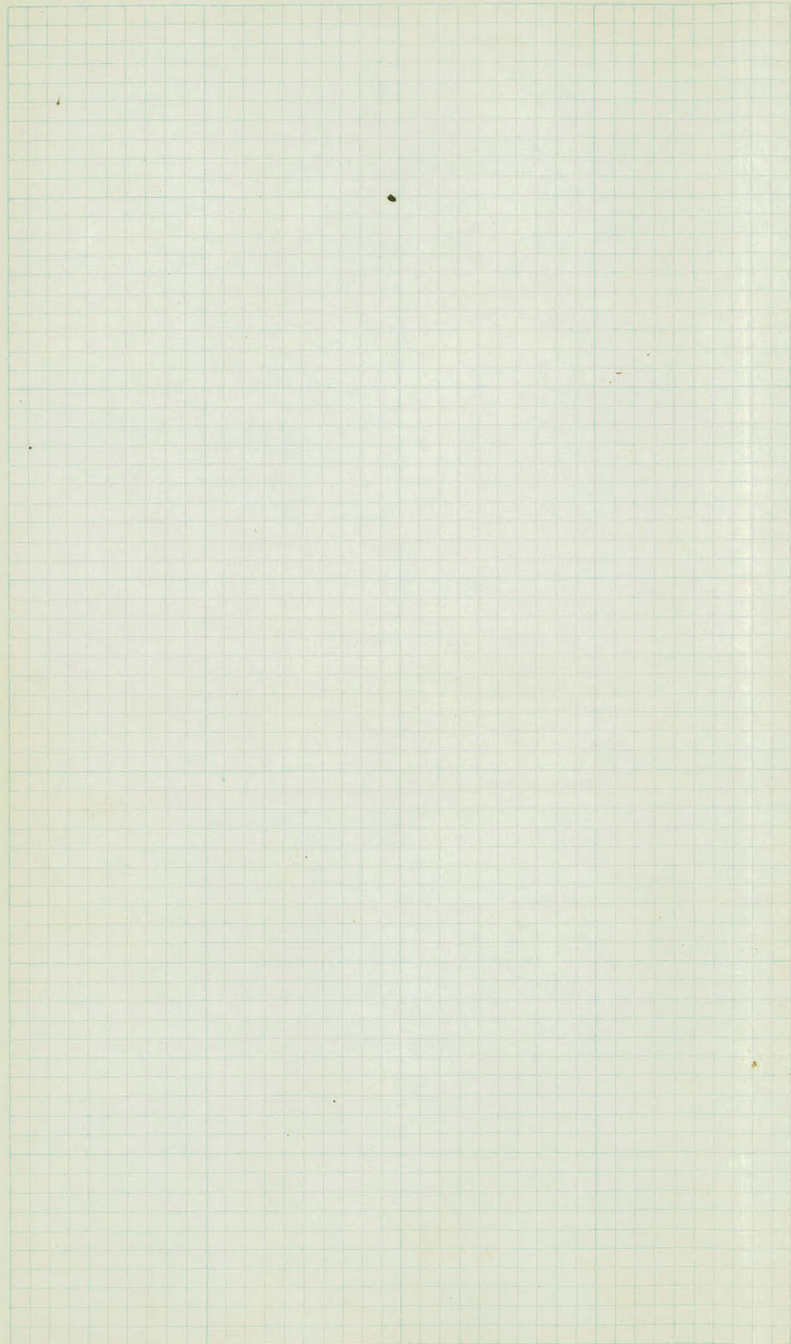
INDEX

Align - 1-3
Topog. - 4-10
Xsections - 11-24

Party:
K.A. & Co.
R.P.
A.M.
L.G.
C.F.

Survey Completed
1-8-41

Drawn up 3/41 WJB
HAW.



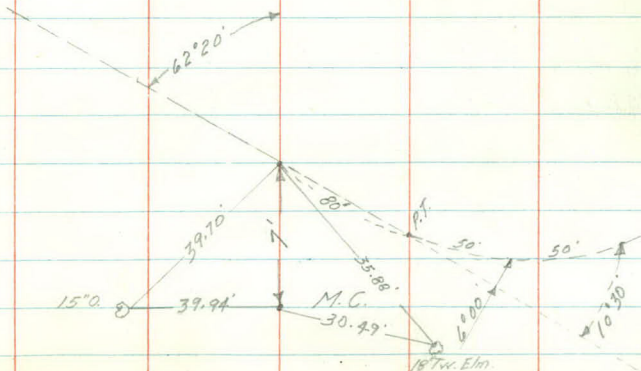
Alignment

Sta	Point	ΔLt	ΔRt
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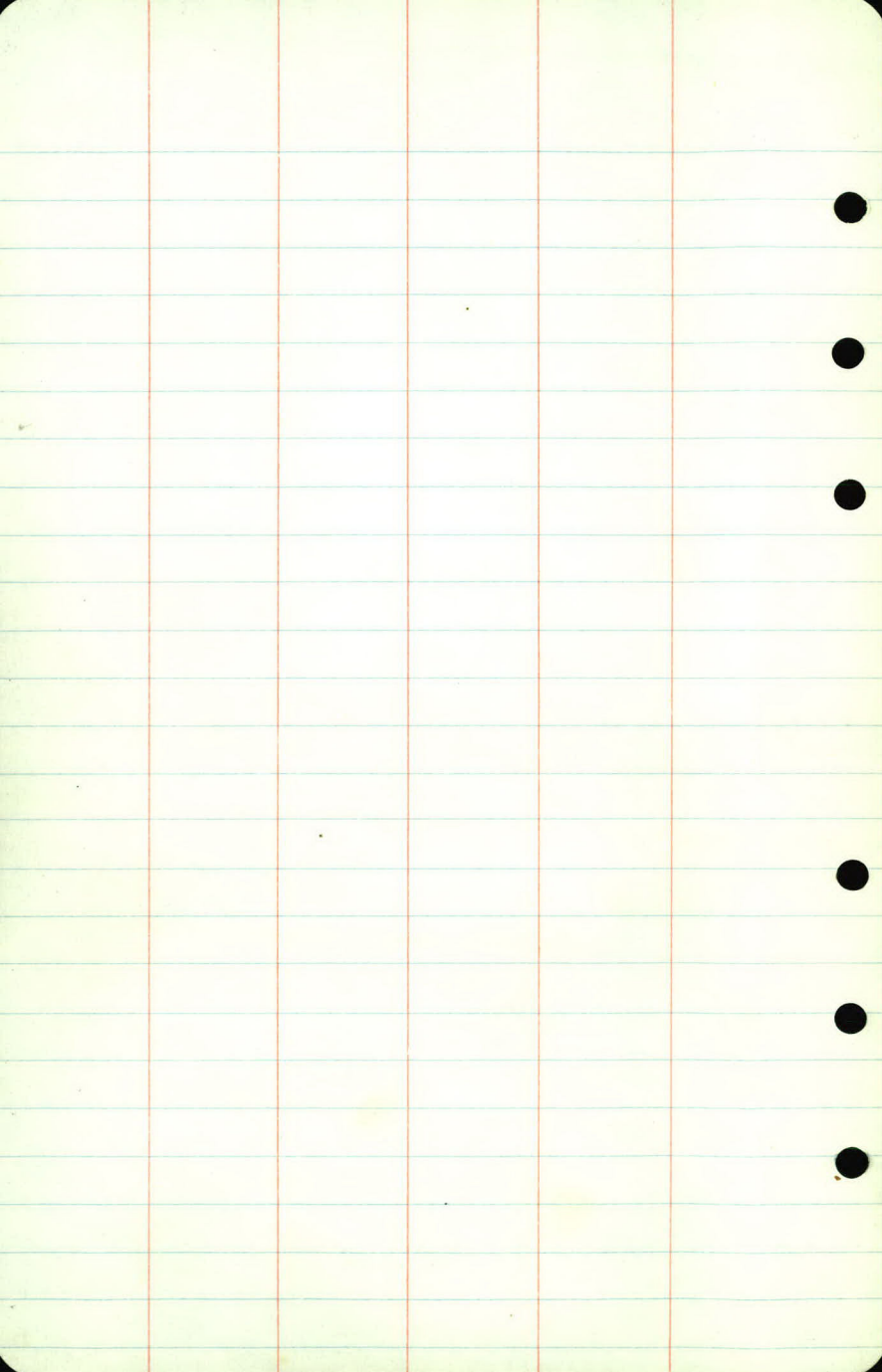
25	+81.34 P.I.	0° 09'	
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12	+11.7 P.O.T.		
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0	+00 = $\pm$ Keller Pkwy.		
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38 + 48.3 P.O.T. = S.T.H. #61



Topography

+92-PP-28

+88-Pe. Cor-33'

+40-Peg. Water-32'

5 Fe-26' 2' 18' Tree Line-41'

+80-Peg. Swamp-24'

+65-Peg. Swamp-30'

+44-Slow E. Sign-13'

+36-PP-29'

4 3' 19' Tree Line-42'-50'

+77-8" O.-30'

+60-20" O.-38'

+70-15" O.-33'

+67-End Box Culv.-21'

+68-Pe. Cor-25'

+44-18" O.-37'

+38-End 15" C.N.-9'

+28-Group 5 Pass-37'

+90-30" W.II.-26'

+61-15" R.E.-36'

+87-Range Tie to Fe.

+30-12" O.-37' P. Fe. Cor.

+07-Hr. 36'

3 3' 17' Fe.-34'

+70-PP-16'

+48-PP-28'

+42-8" Ark-47'

+15-12" Tw. Barr-47'

2 3' 17' Fe.-41'

+99-S.W. Cor. Ho.-67'

1 6' 18' Fe.-38'

+96-PP-28'

+85-Range Tie to Fe.

+46-Slow Sign-17' +50-6' +45-End End-28'

+36-PP-23'

+48-Dim Fe.-39'

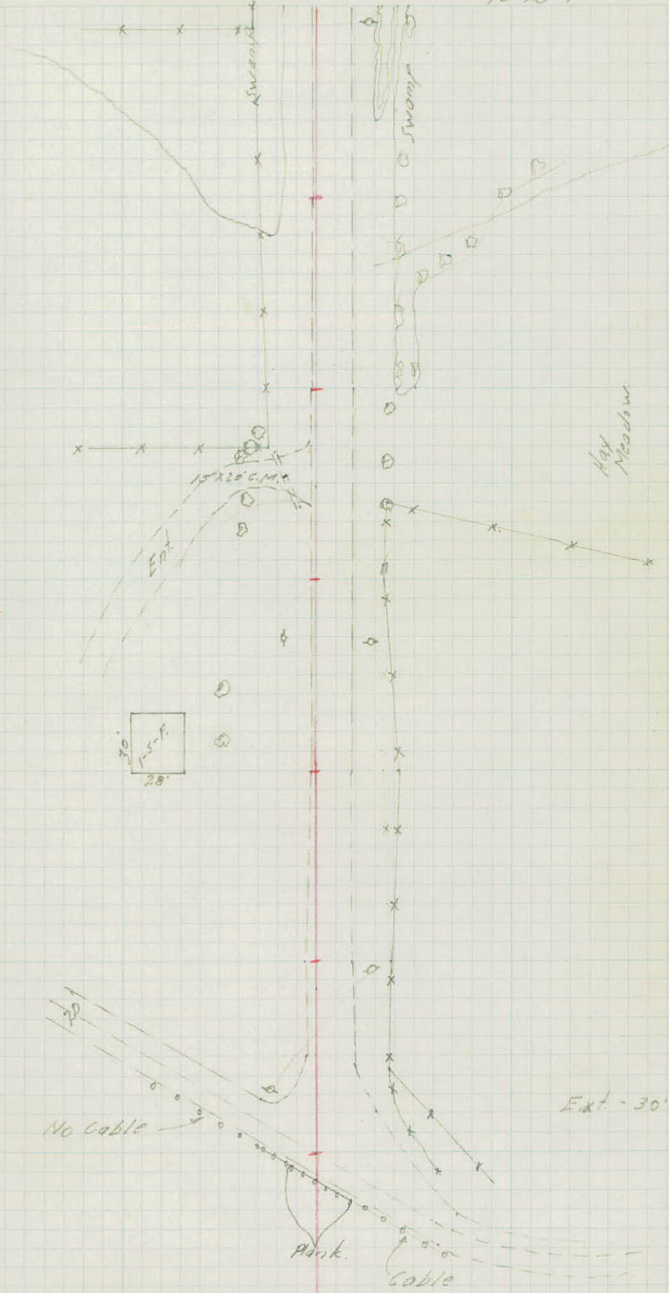
+28-Peg. Rod-29'

0 -14- G.P. X.E.

End Plank G.B.-13'

End Plank b-20'

End Cable-36'



+50-Fc-46'

12 Fc-34'
+90-T.P.-21'
+90-Fc-31'
+88-Stops-20'

+89-PP-26'
+04 End Pothole-30'
15

+50-30'-74'

11 Fc-30' 5' 15' Pothole-31'-58'

+65-T.P.-16'

+84-N.E. Cor. 40-126'

+58-PP-26'
+52-15'-Q-41'

+38-Ent.

10 E. Trail-46' Fc-30' 5' 16'

+44-Fc Cor. 54'

+72-Δ in Fc-46' + Fc. Cor.

+47-Beg. Fc-29'

9 E. Ent-25' 4' +07-PP-27' Fc-43'

+85-Ent Fc-29'
+82-E. Ent-13'

+44-Field Ent

8 End Swamp-21' Fc-32' 4' 17'

+94-8" Willow-41'

+58-Fc. Cor-34' + End Swamp

+44-Turn Rd Sign.-10'

+41-F.P.-28'

7 Fc-35' Swamp-16' 4' 18'

+65-End Traces-40'

+14-24'x42' C.M.R.

6 14' 3' 27' 18' 32'-42' Traceline-47'

← to Ho.

steps cut in bank

Wooded

Uncult.

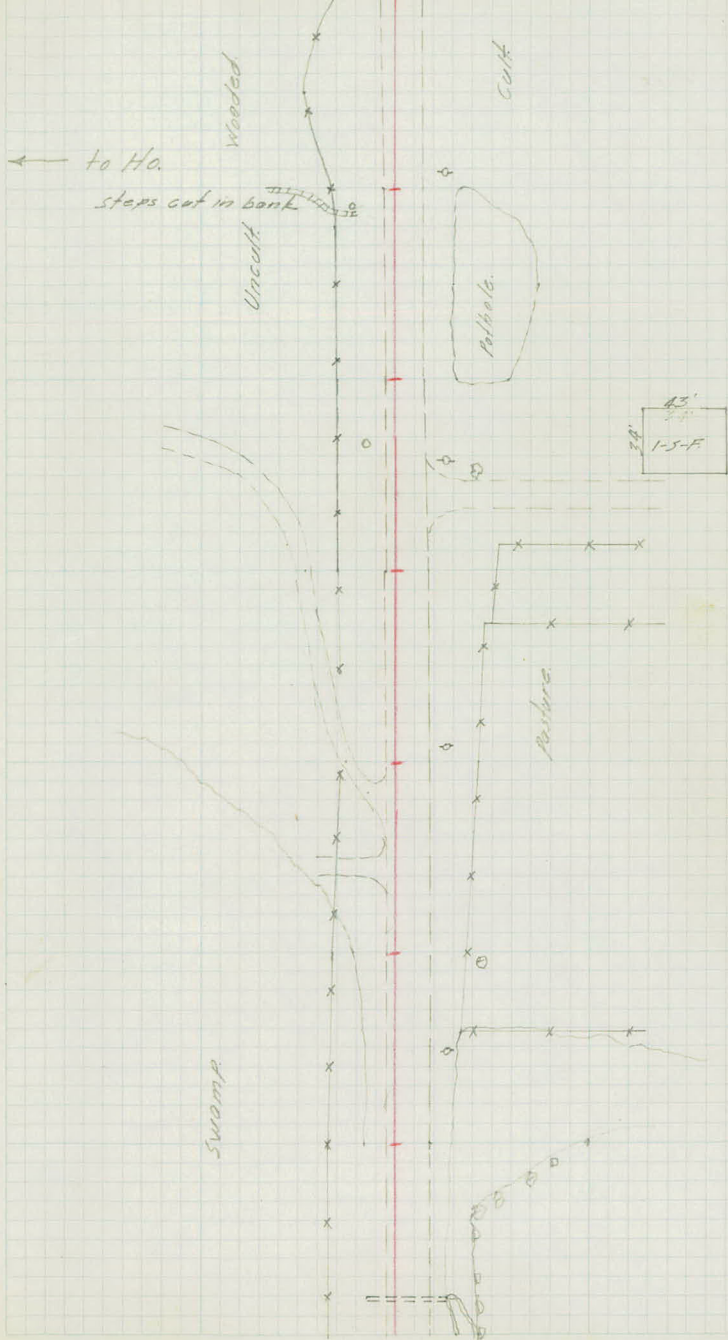
Cult.

Palhato.

45'
34'
1-5-F

Barbed.

Swamp



+62-Ent 12'x24' G.M. - 20'
+53-T.P. - 25'
+48-Ent P.C. - 26'

+18-G.P. - 19' P.P. - 24'

+50-P.C. - 29'

19 F.C. - 27' 9' 13'

+24-T.P. - 22'

+24-P.P. - 25'

18 F.C. - 31' 9' 13'

+95-Ent

+95-F. Ent

+55-20' O. - 47'
+46-15' O. - 40'
+30-12' O. - 43'
+28-S.W. Cor. Ho. - 62'
+01-4' B.E. - 25'

17 F.C. - 29' 9' 15'

+97-T.P. - 23'
+93-10' O. - 36'
+88-10' O. - 35'
+78-8' O. - 37'
+65-F.C. - 28'
+33-12' P.C. - 20'
+21-S.P. - 35'
+15-12' O. - 34'
+04-10' O. - 36'

+72-P.P. - 25'
+50-24' B.E. - 46'
+38-24' Maple - 47'
+30-20' Maple - 47'
+15-18' Maple - 47'
+10-N.W. Cor. Ho. - 95'

16 F.C. - 26' 8' 15'

+78-T.P. - 21'
+55-15' O. - 33'
+52-15' O. - 31'
+38-15' O. - 35'

+90-15' B.E. - 53'
+82-20' B.E. - 48'
+55-N.W. Cor. Ho. - 88'

15 F.C. - 29' 8' 12'

+10-30' O. - 34'

+48-Ent - 26'
+16-P.P. - 24'
+01-N.W. Cor. Veg Stand - 21'

+77-Ent 15' G.M. - 19'

+75-Brick M.H. - 28.5' 2' Dia.
+75-Ent 15' G.M. - 27.3'
15'x46' G.M.

+50-T.P. - 22'

+39-G Cherry - 27'

14 F.C. - 28' 8' 12'

+95-Ent
+77-15' O. - 40'
+67-12' O. - 37'

+86-Ent

+50-5' Ash - 30'

+66-P.P. - 26'

+34-5' Cherry - 25'
+24-4' O. - 20'
+21-T.P. - 21'

13 F.C. - 32' 8' 14'

+10-B. M.H. - 33'

Big Lowland

Lowland

40' Under Const. 26'

1 1/2 - 5 - F 35' 24'

1 - 5 - F 34' 26'

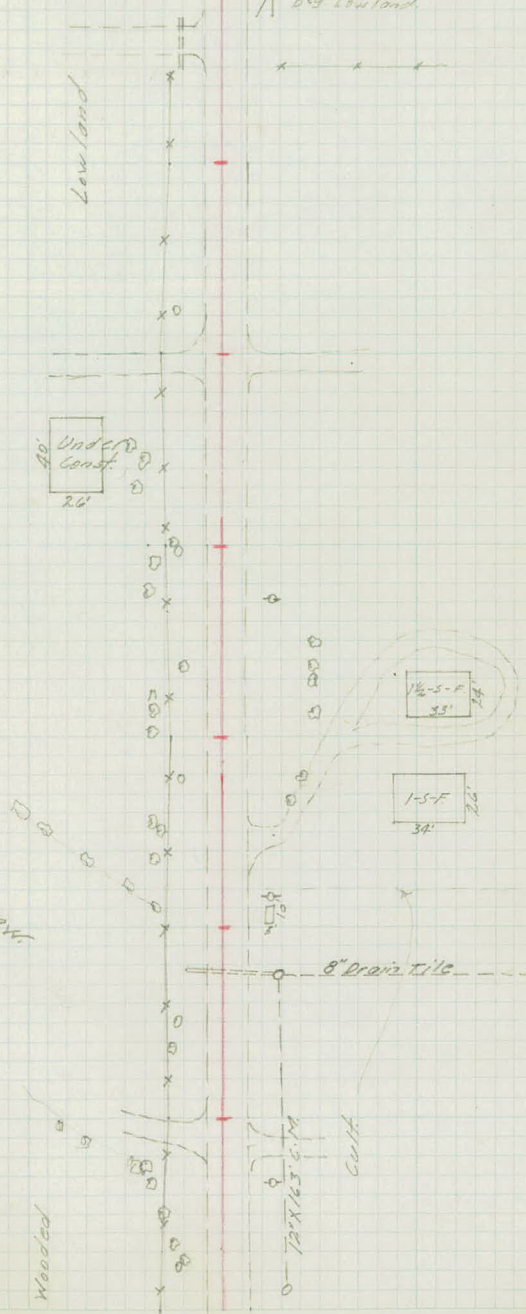
Draw.

8" Drain Tile

Cult.

Wooded

0 - 72" X 163' 6" M



26
+92-T.P.-25'
+72-Ent. $\frac{12' \times 26' \text{ C.M.}}{19'}$

11' 10'
+89-P.P.-25'
+81-Fg. Cor.-26'

25

11' 10'

+67-T.P.-25'

+56-G.P.-18' P.P.-26'

24

10' 11'

+33-T.P.-24'

23

10' 12'

+83-G.P.-18' -P.P.-26'

+12-Ent. 30' C.M.-19'
+09-T.P.-24'

30' X 42' C.M. +13-3' Bottom Ditch-33'
30' C.M.-23'

22 Swamp-100'-21'

11' 11'

+20-G.P.-20' P.P.-26'

21

9' 12'

+83-T.P.-24'

+49-S.E. Cor. Hb.-157'
+45-Swamp.-100'

+25-S.W. Cor. Hb.-152' 860 Swamp.

20

9' 13'

Lower land

Good Meadow.

Low
Hay

Pothole
Swamp.

30°
1-5-11
20°

+65-Fc-36'
+44-5" Trip. Pop-25'
+40-5" Pop-26'

+24-T.P-23'

+35-PP-26'

33 Brush Linc. - 28'

12' 9'

Fc-29'

+46-Bog. Trees + Brush - 22'

+34-End Wood - 33'

+20-Bog. Lillies Wood - 32'

+16-S.W. Cor. Ho. - 96'

+15-T.P-23'

+08-Ent.

+28-Bog Fc-28'

+24-20" O. - 34'

32 12' 9'

+26-PP-25'

+19-N.W. Cor. Ho. - 83'

+53-10" O. - 40'

+16-12" O. - 37'

+08-12" O. - 40'

+64-End Fc-27

+32-20" O. - 44'

31 12' 10'

Fc-28'

+98-T.P-23'

+76-Ent.

+63-End Brush - 22'

+12-Bog. Brush - 36' - 33'

+04-5" O. - 35'

+35-PP-26'

30 12' 10'

Fc-29'

+84-S.W. Cor. Ho. - 63'

+82-T.P-23' +74-Karbo. Tls to Ho.

+74-Ent. Brush - 44' - 21'

+42-Bog. Brush - 31'

+39-12" O. - 38'

+87-8" Pop - 31'

+16-6 2' Wdg Bridge Wall - 16' - 21'

+01-S.W. Cor. Ho - 74'

29 11' 10'

Fc-27

+86-PP-26'

+48-T.P-24'

+21-Ent. Tlcs + Brush - 23'

+04-Ent.

+45-Fc. Cor. - 28'

28 11' 10'

Fc-28'

+44-18" O. - 30'

+29-12" Tlcs O. - 57'

+27-T.P-24'

+10-Bog. Trees + Brush - 23'

+53-5" - 24'

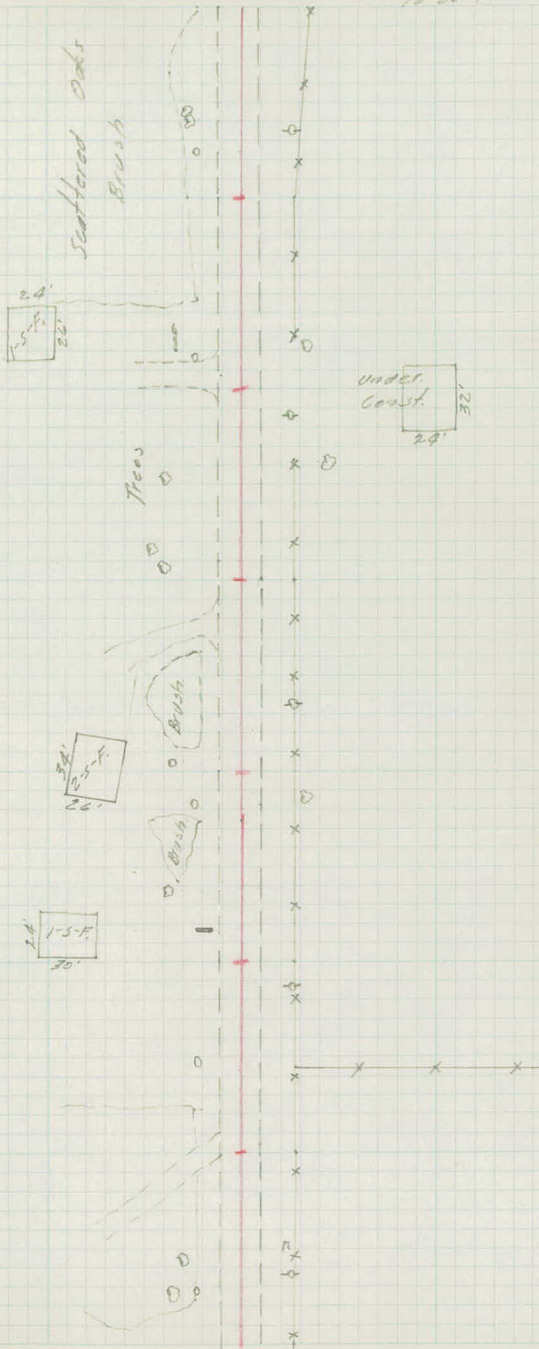
+36-PP-26'

27 11' 10'

Fc-27'

10-28-40

9



+55 End Rod 50

38

+60 End Rod 100

+ +60 Beg Rod 17'

+32 Beg Rod 10'

37

16 9'

450 Brush 35

24'

+21-18" x 48' C.M. Cross Drain

24'

36 Brush 35

14' 9'

Fe. 33

35 Brush 35

14' 9'

Fe. 31

+50 Fe. 32

34 Brush - 22'

12' 9'

Fe. 36

+54 End 24' G.M. - 47

+53 Ent

+47 RP 23'
+32 End 24' G.M. 29'
+20 B.P. 87'

+95 End Brush 30
+94 T.P. 24
+90 Clump Br 25
+74 Clump Br 24
+55 Clump Br 28
+43 4 Trees 53

+97 Stump 44
+84 F.C. Cor 35
+65 2 Trees 26-33
+60 Tree 33
+53 Tree 33
+34 Ground Sp. 40
+31 RP 25
+20 End G.R. 10
Brush 19 - 65

+68 Bee Brush 24
+66 Bee G.R. 10
+65 Tree 17
+52 Sp 18

+96 Clump Brush 20
+70 Clump Brush 19
+49 Brush 27-40
+44 T.P. 23
+41 Sp 25
+38 Sp 24
+18 Oak 41
+02 Sp 43
+00 Oak 35
+88 Sp 23
+85 Sp 22

+41 Triple Maple 39

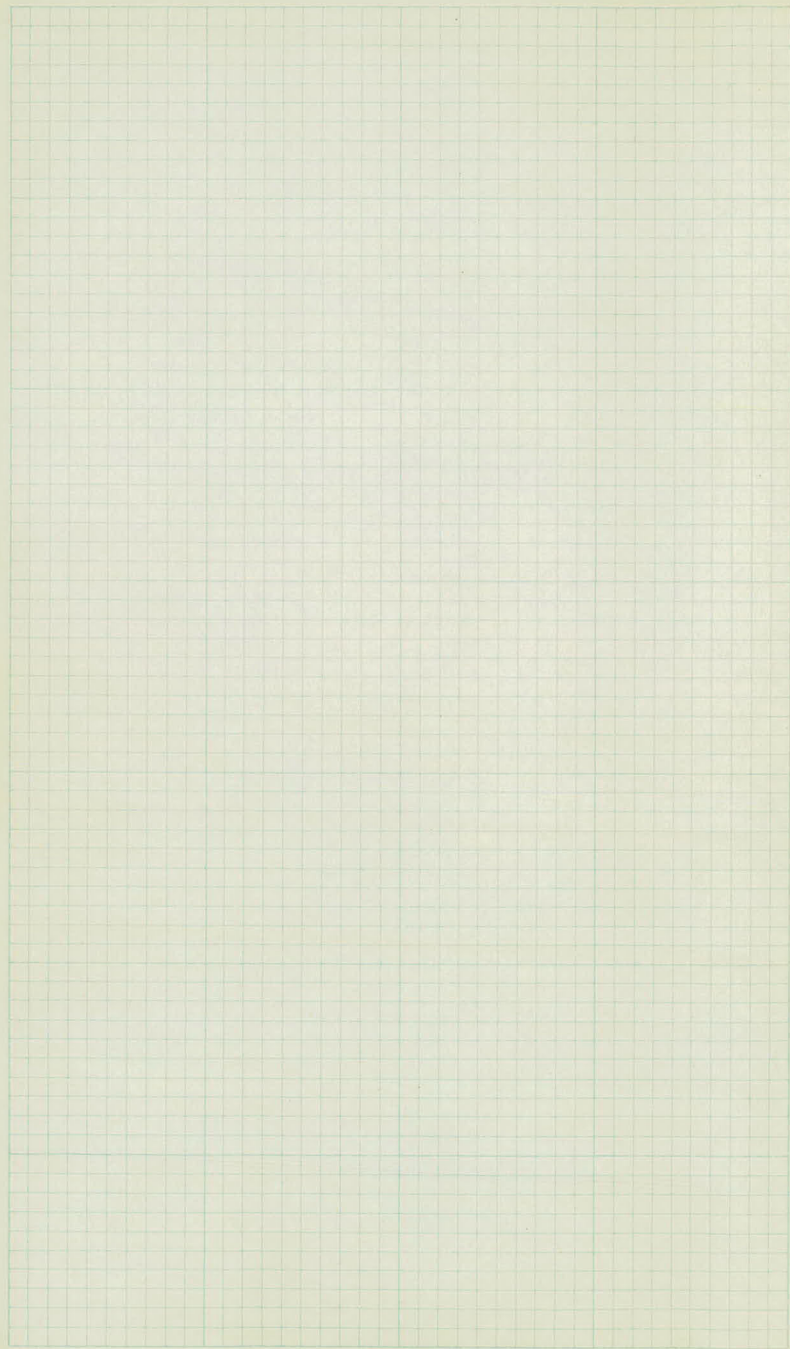
+32 T.P. 23

+89 Tree 47
+87 RP 25
+84 Tree 34
+76 Tree 35

Brush

G.R. Tree
No Cable

Brush



Bench Levels

Co. R.I.C. to STH #61

Sta	+	π	-	Elev
B.M	12.15	871.15		859.00
	7.62	878.30	0.47	870.68
B.M	6.00	877.82	2.48	871.82
	0.40	869.56	8.66	869.16
	9.84	872.15	7.25	862.31
	8.52	879.74	0.93	871.22
B.M	5.52	879.74	5.52	874.22
	2.18	875.97	5.95	873.79
	0.91	868.77	8.11	867.86
	5.53	868.29	6.01	862.76
B.M	6.45	869.42	5.32	862.97
	10.50	878.91	1.01	868.41
	6.90	884.81	1.00	877.91
	3.67	887.00	1.48	883.33
B.M			1.35	885.65

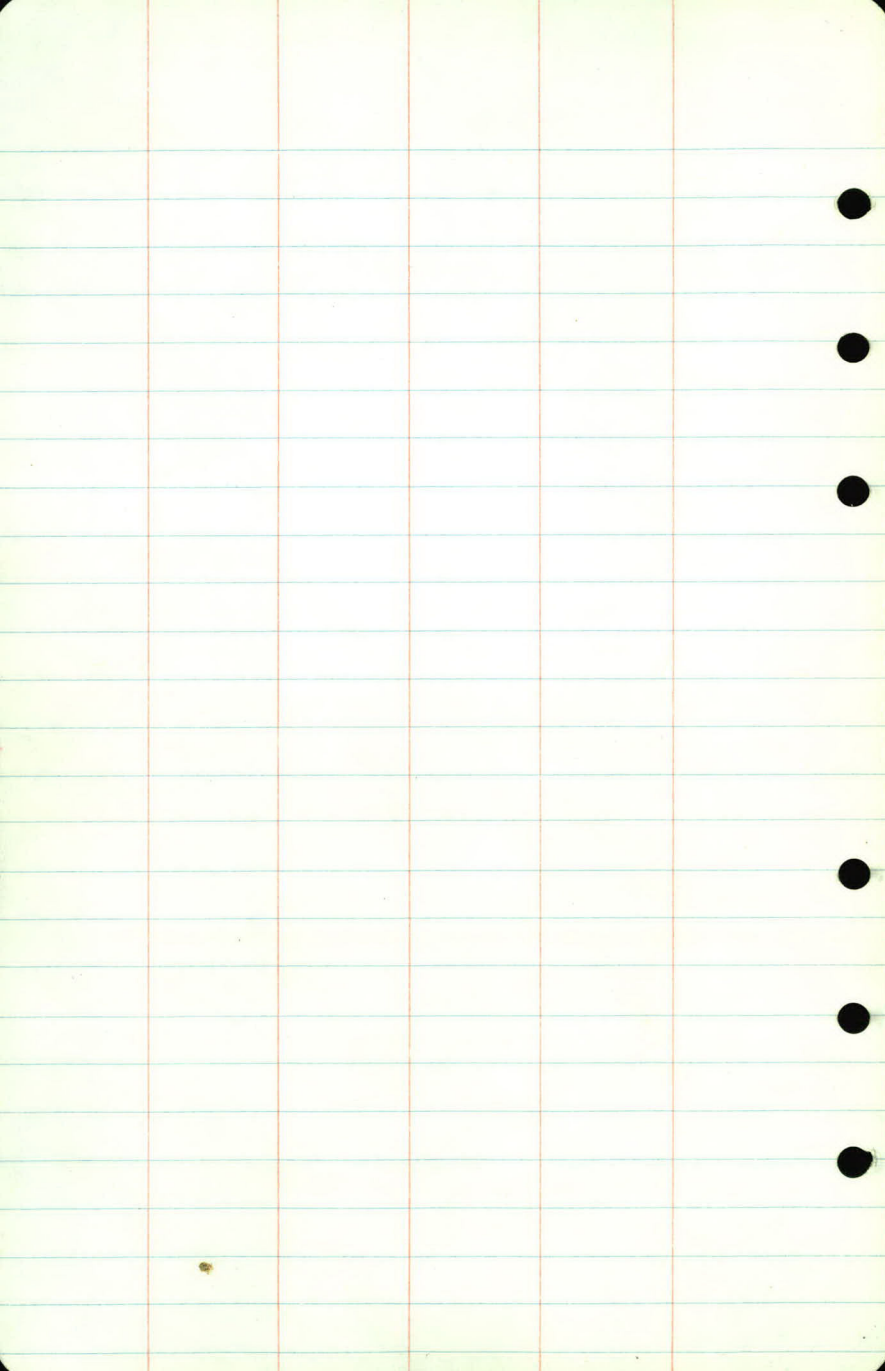
Top Iron Set in Conc East Side Gervais Lake

SpK in Twin 12" Elm SW Cor "C"

SpK in 18" Oak 40' RT Sta 10+50

SpK in 18" Oak 110' LT Sta 24+25

Spike P.P. S.W. Cor. "C" and S.T.H. #61



Cross Sections

Co. Rd. "C"

Gervais Lake to S.T.H. #61

Sta	+	⌊	-	Elev.
B.M.	6.62	878.44		871.82
0+00			5.0	73.4
+15			5.0	73.4
+30			5.0	73.4
+50			4.9	73.5
1			5.3	73.1
+21			5.5	72.9
+51			6.0	72.4
2			6.8	71.6
+50			7.5	70.9
3			8.7	69.7
TP	11.13	889.20	0.37	878.07
0+30				73.4
+50				73.5

Spike in Twin 12" Elm S.W. Cor. "C"

4.1
50

50

6.5
50

4.2 4.8 5.5 6.8 4.5 4.4
50 28 5.0 15 34 42 50

1.2 3.8 4.8 5.2 6.2 4.9 3.4
50 22 20 5.0 12 24 30 34

2.1 5.5 5.3 4.8 5.4 5.9 5.7
24 16 10 4.9 8 18 21 27

5.5 5.7 5.5 5.1 5.7 5.8 5.9
10 7 5 5.3 10 19 21 26

5.6 6.0 5.7 5.3 5.9 6.0 6.2
10 5 3 5.5 9 22 23 27

5.0 5.7 5.9 5.8 6.2 6.5 6.5
9 7 3 6.0 11 21 23 27

4.6 6.3 6.6 6.5 6.7 6.8 5.4
12 8 4 6.8 10 19 21 27

5.4 7.6 7.9 7.7 7.3 7.7 7.6 7.6 6.9
11 6 4 3 7.5 12 20 22 24 26

6.8 7.7 9.1 8.8 8.7 9.1 9.1 9.0
12 7 5 3 8.7 12 19 21 24

15.8

10.8 10.8
47 50

15.7

10.1 10.3 10.7
50 37 50

Sta	+	π	-	Elev.
		689.20		
1				73.1
+21				72.9
+51				72.4
2				71.6
+50				70.9
3				69.7
T.P	45.4	882.61	11.13	878.07
T.R	3.49	973.23	12.87	869.74
+30			4.4	68.8
+50			4.9	68.3
+75			5.6	67.6
4			6.3	66.9
+50			8.3	64.9

$$\begin{array}{r} 6.2 \\ 50 \end{array} \quad \begin{array}{r} 7.5 \\ 26 \end{array} \quad \begin{array}{r} 16.1 \\ 37 \end{array} \quad \begin{array}{r} 10.2 \\ 50 \end{array}$$

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 25 \end{array} \quad \begin{array}{r} 16.3 \\ 40 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 4.3 \\ 50 \end{array} \quad \begin{array}{r} 6.2 \\ 26 \end{array} \quad \begin{array}{r} 16.8 \\ 45 \end{array} \quad \begin{array}{r} 3.2 \\ 50 \end{array}$$

$$\begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 27 \end{array} \quad \begin{array}{r} 17.6 \\ 44 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 28 \end{array} \quad \begin{array}{r} 18.3 \\ 41 \end{array} \quad \begin{array}{r} 6.6 \\ 50 \end{array}$$

$$\begin{array}{r} 8.6 \\ 50 \end{array} \quad \begin{array}{r} 10.4 \\ 25 \end{array} \quad \begin{array}{r} 19.5 \\ 37 \end{array} \quad \begin{array}{r} 12.3 \\ 50 \end{array}$$

$$\begin{array}{r} 0.4 \\ 50 \end{array} \quad \begin{array}{r} 0.3 \\ 20 \end{array} \quad \begin{array}{r} 4.0 \\ 12 \end{array} \quad \begin{array}{r} 4.6 \\ 9 \end{array} \quad \begin{array}{r} 4.5 \\ 4 \end{array} \quad \begin{array}{r} 4.3 \\ 2 \end{array} \quad \begin{array}{r} 4.4 \\ 44 \end{array} \quad \begin{array}{r} 4.2 \\ 8 \end{array} \quad \begin{array}{r} 4.6 \\ 21 \end{array} \quad \begin{array}{r} 4.9 \\ 25 \end{array} \quad \begin{array}{r} 6.0 \\ 32 \end{array} \quad \begin{array}{r} 6.4 \\ 50 \end{array}$$

Driveway

$$\begin{array}{r} 1.2 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 26 \end{array} \quad \begin{array}{r} 4.8 \\ 49 \end{array} \quad \begin{array}{r} 5.4 \\ 11 \end{array} \quad \begin{array}{r} 8.6 \\ 22 \end{array} \quad \begin{array}{r} 10.6 \\ 31 \end{array} \quad \begin{array}{r} 10.6 \\ 50 \end{array}$$

$$\begin{array}{r} 9.6 \\ 50 \end{array} \quad \begin{array}{r} 9.4 \\ 25 \end{array} \quad \begin{array}{r} 6.3 \\ 17 \end{array} \quad \begin{array}{r} 6.2 \\ 11 \end{array} \quad \begin{array}{r} 5.9 \\ 5 \end{array} \quad \begin{array}{r} 5.6 \\ 56 \end{array} \quad \begin{array}{r} 5.6 \\ 11 \end{array} \quad \begin{array}{r} 6.6 \\ 22 \end{array} \quad \begin{array}{r} 11.4 \\ 31 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array}$$

$$\begin{array}{r} 12.1 \\ 50 \end{array} \quad \begin{array}{r} 11.9 \\ 26 \end{array} \quad \begin{array}{r} 7.6 \\ 18 \end{array} \quad \begin{array}{r} 7.4 \\ 12 \end{array} \quad \begin{array}{r} 6.7 \\ 6 \end{array} \quad \begin{array}{r} 6.3 \\ 63 \end{array} \quad \begin{array}{r} 6.4 \\ 9 \end{array} \quad \begin{array}{r} 7.5 \\ 21 \end{array} \quad \begin{array}{r} 13.0 \\ 32 \end{array} \quad \begin{array}{r} 13.8 \\ 50 \end{array}$$

$$\begin{array}{r} 13.8 \\ 50 \end{array} \quad \begin{array}{r} 13.6 \\ 27 \end{array} \quad \begin{array}{r} 10.3 \\ 18 \end{array} \quad \begin{array}{r} 9.4 \\ 13 \end{array} \quad \begin{array}{r} 8.8 \\ 9 \end{array} \quad \begin{array}{r} 8.3 \\ 83 \end{array} \quad \begin{array}{r} 8.1 \\ 11 \end{array} \quad \begin{array}{r} 8.8 \\ 21 \end{array} \quad \begin{array}{r} 14.0 \\ 30 \end{array} \quad \begin{array}{r} 14.9 \\ 50 \end{array}$$

Sta.	t	π	-	Elev.
		873.23		
5			9.7	63.5.
T.P.	4.00	867.50	9.73	863.50
+50			50	62.5.
6			4.9	62.6.
+19	24" x 1/2" C.M.		4.6	62.9.
+50			4.9	62.6.
7			4.9	62.6.
+50			3.6	63.9.
8			1.2	66.3.
T.P.	10.72	877.52	0.70	866.80
+54			9.5	68.0.
9			7.8	69.7.
+28			6.7	70.8.
+66			5.4	72.1.

13.9 14.4 13.1 10.7 10.2 7.6 11.6 14.7 14.8
50 27 17 13 5 9.7 8 20 28 50

540.5

80 83 83 5.6 4.9 55 10.1 11.1 10.8 10.5
50 30 16 11 5.0 10 20 30 32 38 50

7.9 85 9.2 9.3 8.8 6.1 4.8 55 10.4 11.0 10.0 8.7
50 36 25 20 18 11 4.9 10 21 30 34 44 50

57.41

57.47

8.5 8.4 9.0 9.9 9.5 10.09 6.0 4.7 5.6 10.03 10.1 10.8 9.5
50 39 39 21 14 14 10 4.6 10 22 28 31 37 50

8.5 8.6 8.7 9.6 10.0 8.8 5.7 4.9 5.6 10.7 10.6 10.0
50 38 33 28 21 16 11 4.9 9 23 29 35 50

8.2 9.7 10.0 9.3 6.0 4.8 5.7 9.7 9.6 9.5
50 28 21 16 10 4.9 10 20 28 34 50

8.4 8.2 9.2 8.7 4.3 3.4 4.2 7.4 8.4 8.0
50 31 23 18 11 3.6 8 20 26 32 50

8.3 8.2 7.9 2.3 11 2.0 6.3 7.0 7.2
50 28 20 11 12 10 21 29 40 50

15.8 13.9 12.8 10.2 9.7 9.6 10.3 11.0 12.7 12.7
50 30 16 7 4 9.5 10 21 25 40 50

5.3 8.5 8.5 7.9 7.6 8.4 8.3 5.1 2.2
18 14 10 4 7.8 10 21 24 34 38

0.7 7.1 7.2 6.8 6.6 7.2 7.8 3.0
22 14 9 4 6.7 9 20 22 32

5.0 5.8 5.3 6.0 6.8 6.6
10 6 5.4 9 19 21 26

Sta.	+	π	-	Elev.
		877.52		
9 + 85			4.9	72.6
10			4.5	73.0
+ 21			3.8	73.7
+ 50			3.3	74.2
11			2.7	74.8
+ 36			2.6	74.9
+ 50			2.5	75.0
+ 91			2.4	75.1
12			2.4	75.1
B.M.	11.85	886.07	3.25	874.27
T.P.	7.69	891.25	2.51	883.56
9				69.7
+ 28				70.8

$$\begin{array}{r} 4.8 \quad 5.1 \\ 10 \quad 7 \end{array} \quad 4.8 \quad 5.3 \quad 6.2 \quad 6.1 \\ 49 \quad 9 \quad 20 \quad 22 \quad 26$$

$$\begin{array}{r} 4.5 \quad 4.5 \\ 12 \quad 8 \end{array} \quad 4.4 \quad 5.0 \quad 5.4 \quad 5.3 \quad 3.2 \quad 2.0 \\ 4.5 \quad 7 \quad 20 \quad 22 \quad 25 \quad 27 \quad 31$$

$$\begin{array}{r} 4.1 \quad 4.1 \\ 14 \quad 9 \end{array} \quad 3.8 \quad 4.2 \quad 3.7 \quad 2.4 \\ 3.8 \quad 10 \quad 18 \quad 24 \quad 50$$

$$\begin{array}{r} 3.0 \quad 3.7 \\ 13 \quad 8 \end{array} \quad 3.3 \quad 3.2 \quad 3.5 \quad 3.2 \quad 3.0 \\ 3.3 \quad 9 \quad 20 \quad 37 \quad 50$$

$$\begin{array}{r} 2.5 \quad 4.1 \quad 4.1 \quad 3.4 \\ 18 \quad 16 \quad 13 \quad 10 \end{array} \quad 2.7 \quad 3.2 \quad 5.2 \quad 5.6 \\ 27 \quad 9 \quad 19 \quad 28 \quad 50$$

$$\begin{array}{r} 2.3 \quad 4.3 \quad 4.4 \quad 3.7 \quad 3.3 \\ 31 \quad 27 \quad 16 \quad 12 \quad 11 \end{array} \quad 3.1 \quad 4.7 \quad 6.6 \quad 8.1 \quad 7.6 \\ 26 \quad 20 \quad 24 \quad 30 \quad 37 \quad 50$$

$$\begin{array}{r} 2.7 \quad 4.0 \quad 4.4 \quad 5.4 \quad 2.9 \quad 2.0 \\ 32 \quad 24 \quad 21 \quad 19 \quad 12 \quad 9 \end{array} \quad 2.5 \quad 3.2 \quad 6.7 \quad 7.3 \quad 7.5 \\ 2.5 \quad 8 \quad 19 \quad 28 \quad 33 \quad 50$$

$$\begin{array}{r} 0.5 \quad 3.2 \quad 3.1 \\ 20 \quad 15 \quad 10 \end{array} \quad 2.4 \quad 2.9 \quad 6.8 \quad 7.2 \quad 7.2 \\ 2.4 \quad 7 \quad 18 \quad 27 \quad 34 \quad 50$$

$$\begin{array}{r} 3.2 \quad 3.2 \\ 14 \quad 11 \end{array} \quad 2.4 \quad 2.9 \quad 6.5 \quad 7.2 \quad 7.2 \\ 2.4 \quad 7 \quad 18 \quad 27 \quad 34 \quad 50$$

Spike 18" Oak 40 Rt Sta. 10 + 50

$$\begin{array}{r} 18.8 \quad 17.8 \quad 18.7 \\ 50 \quad 35 \quad 20 \end{array}$$

21.6.

$$\begin{array}{r} 14.5 \quad 16.0 \\ 45 \quad 50 \end{array}$$

$$\begin{array}{r} 13.1 \quad 14.0 \\ 50 \quad 40 \end{array}$$

20.5.

$$\begin{array}{r} 9.3 \quad 9.0 \\ 42 \quad 50 \end{array}$$

Sta

+

↑

-

Elev.

891.25 ✓

9 + 66

72.1

+ 85

72.6

10

73.0

+ 21

73.7

+ 50

74.2

11

74.8

+ 34

74.9

+ 50

75.0

+ 91

75.1

12

75.1

BM

4.99

879.21 ✓

874.32

+ 25

4.3

74.9

+ 42

74.9

$$\begin{array}{r} 7.7 \\ 50 \end{array} \quad \begin{array}{r} 8.3 \\ 25 \end{array} \quad 19.2 \quad \begin{array}{r} 5.6 \\ 44 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 8.5 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 27 \end{array} \quad 18.7 \quad \begin{array}{r} 5.0 \\ 44 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.4 \\ 50 \end{array} \quad \begin{array}{r} 3.8 \\ 30 \end{array} \quad 18.3 \quad \begin{array}{r} 8.7 \\ 43 \end{array} \quad \begin{array}{r} 8.6 \\ 50 \end{array}$$

$$\begin{array}{r} 3.7 \\ 50 \end{array} \quad \begin{array}{r} 2.5 \\ 31 \end{array} \quad 17.6$$

$$\begin{array}{r} 4.3 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 27 \end{array} \quad 17.1$$

$$\begin{array}{r} 8.5 \\ 50 \end{array} \quad \begin{array}{r} 12.3 \\ 33 \end{array} \quad 16.5$$

$$\begin{array}{r} 11.9 \\ 50 \end{array} \quad 16.4$$

$$\begin{array}{r} 12.1 \\ 50 \end{array} \quad 16.3$$

$$\begin{array}{r} 5.3 \\ 50 \end{array} \quad 16.2$$

$$\begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 11.9 \\ 25 \end{array} \quad 16.2$$

Spike 18' Oak 40' R.L. Sta. 10+50
$$\begin{array}{r} +16.0 \\ 63 \end{array} \quad \begin{array}{r} +12.7 \\ 50 \end{array} \quad \begin{array}{r} +7.2 \\ 32 \end{array} \quad \begin{array}{r} 4.2 \\ 15 \end{array} \quad \begin{array}{r} 5.2 \\ 11 \end{array} \quad \begin{array}{r} 5.0 \\ 10 \end{array} \quad \begin{array}{r} 4.3 \\ 43 \end{array} \quad \begin{array}{r} 4.5 \\ 7 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 6.7 \\ 23 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

$$\begin{array}{r} +17.4 \\ 63 \end{array} \quad \begin{array}{r} +14.7 \\ 50 \end{array} \quad \begin{array}{r} +12.1 \\ 43 \end{array} \quad \begin{array}{r} 2.0 \\ 23 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 11 \end{array} \quad \begin{array}{r} 4.5 \\ 6 \end{array} \quad \begin{array}{r} 4.3 \\ 43 \end{array} \quad \begin{array}{r} 4.2 \\ 7 \end{array} \quad \begin{array}{r} 4.5 \\ 18 \end{array} \quad \begin{array}{r} 5.1 \\ 23 \end{array} \quad \begin{array}{r} 6.8 \\ 50 \end{array}$$

3 rd	π	-	E _K
	879.21 ✓		
12 + 68		4.4	74.8
13		4.7	74.5
+26		5.0	74.2
+60		5.4	73.8
14		5.8	73.4
+50		6.6	72.6
15		7.1	72.1
+50		7.7	71.5
+68		8.1	71.1
7 th P	9.40	8.05	871.16
16		9.9	70.7
+50		10.6	70.0
17		11.5	69.1

$$\begin{array}{r} 1167 \\ 65 \end{array} + \begin{array}{r} 139 \\ 50 \end{array} + \begin{array}{r} 110 \\ 38 \end{array} \begin{array}{r} 2.3 \\ 23 \end{array} \begin{array}{r} 4.2 \\ 16 \end{array} \begin{array}{r} 4.8 \\ 12 \end{array} \begin{array}{r} 5.0 \\ 10 \end{array} \begin{array}{r} 4.7 \\ 7 \end{array} \begin{array}{r} 4.3 \\ 7 \end{array} \begin{array}{r} 4.7 \\ 17 \end{array} \begin{array}{r} 5.6 \\ 24 \end{array} \begin{array}{r} 7.6 \\ 50 \end{array}$$

$$\begin{array}{r} 482 \\ 50 \end{array} + \begin{array}{r} 4.2 \\ 35 \end{array} \begin{array}{r} 4.6 \\ 20 \end{array} \begin{array}{r} 5.3 \\ 12 \end{array} \begin{array}{r} 5.5 \\ 9 \end{array} \begin{array}{r} 5.1 \\ 6 \end{array} \begin{array}{r} 4.6 \\ 47 \end{array} \begin{array}{r} 5.0 \\ 7 \end{array} \begin{array}{r} 7.9 \\ 17 \end{array} \begin{array}{r} 7.6 \\ 24 \end{array} \begin{array}{r} 7.6 \\ 50 \end{array}$$

$$\begin{array}{r} 10.8 \\ 50 \end{array} \begin{array}{r} 1.1 \\ 42 \end{array} \begin{array}{r} 4.3 \\ 29 \end{array} \begin{array}{r} 6.2 \\ 17 \end{array} \begin{array}{r} 6.0 \\ 11 \end{array} \begin{array}{r} 5.3 \\ 6 \end{array} \begin{array}{r} 4.9 \\ 50 \end{array} \begin{array}{r} 5.6 \\ 6 \end{array} \begin{array}{r} 8.5 \\ 16 \end{array} \begin{array}{r} 8.4 \\ 24 \end{array} \begin{array}{r} 8.4 \\ 50 \end{array}$$

$$\begin{array}{r} 8.6 \\ 50 \end{array} \begin{array}{r} 9.0 \\ 28 \end{array} \begin{array}{r} 8.3 \\ 17 \end{array} \begin{array}{r} 6.1 \\ 10 \end{array} \begin{array}{r} 5.8 \\ 7 \end{array} \begin{array}{r} 5.2 \\ 54 \end{array} \begin{array}{r} 5.6 \\ 7 \end{array} \begin{array}{r} 7.7 \\ 16 \end{array} \begin{array}{r} 7.3 \\ 23 \end{array} \begin{array}{r} 7.3 \\ 50 \end{array}$$

$$\begin{array}{r} 123 \\ 50 \end{array} \begin{array}{r} 9.3 \\ 31 \end{array} \begin{array}{r} 6.9 \\ 16 \end{array} \begin{array}{r} 6.6 \\ 12 \end{array} \begin{array}{r} 6.2 \\ 7 \end{array} \begin{array}{r} 5.8 \\ 7 \end{array} \begin{array}{r} 6.3 \\ 16 \end{array} \begin{array}{r} 7.1 \\ 22 \end{array} \begin{array}{r} 6.4 \\ 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \end{array} \begin{array}{r} 11.5 \\ 29 \end{array} \begin{array}{r} 10.0 \\ 20 \end{array} \begin{array}{r} 7.4 \\ 11 \end{array} \begin{array}{r} 6.5 \\ 66 \end{array} \begin{array}{r} 6.9 \\ 6 \end{array} \begin{array}{r} 8.4 \\ 17 \end{array} \begin{array}{r} 8.0 \\ 22 \end{array} \begin{array}{r} 8.0 \\ 50 \end{array}$$

$$\begin{array}{r} 13.1 \\ 50 \end{array} \begin{array}{r} 12.7 \\ 29 \end{array} \begin{array}{r} 11.6 \\ 20 \end{array} \begin{array}{r} 7.9 \\ 12 \end{array} \begin{array}{r} 7.1 \\ 71 \end{array} \begin{array}{r} 7.0 \\ 7 \end{array} \begin{array}{r} 7.1 \\ 16 \end{array} \begin{array}{r} 7.4 \\ 21 \end{array} \begin{array}{r} 7.3 \\ 50 \end{array}$$

$$\begin{array}{r} 12.8 \\ 50 \end{array} \begin{array}{r} 10.8 \\ 28 \end{array} \begin{array}{r} 8.9 \\ 16 \end{array} \begin{array}{r} 8.5 \\ 14 \end{array} \begin{array}{r} 7.7 \\ 77 \end{array} \begin{array}{r} 7.6 \\ 6 \end{array} \begin{array}{r} 7.6 \\ 19 \end{array} \begin{array}{r} 5.8 \\ 35 \end{array} \begin{array}{r} 2.9 \\ 50 \end{array}$$

$$\begin{array}{r} 12.3 \\ 50 \end{array} \begin{array}{r} 10.7 \\ 26 \end{array} \begin{array}{r} 9.1 \\ 16 \end{array} \begin{array}{r} 8.5 \\ 11 \end{array} \begin{array}{r} 8.1 \\ 8.1 \end{array} \begin{array}{r} 7.9 \\ 6 \end{array} \begin{array}{r} 7.9 \\ 16 \end{array} \begin{array}{r} 8.1 \\ 22-24 \end{array} \begin{array}{r} 4.7 \\ 28 \end{array} \begin{array}{r} 3.8 \\ 44 \end{array} \begin{array}{r} 0.9 \\ 50 \end{array}$$

$$\begin{array}{r} 11.4 \\ 50 \end{array} \begin{array}{r} 7.4 \\ 20 \end{array} \begin{array}{r} 10.8 \\ 11 \end{array} \begin{array}{r} 9.9 \\ 9.9 \end{array} \begin{array}{r} 9.8 \\ 7 \end{array} \begin{array}{r} 10.0 \\ 16 \end{array} \begin{array}{r} 10.8 \\ 20 \end{array} \begin{array}{r} 2.5 \\ 23 \end{array} \begin{array}{r} 2.0 \\ 33 \end{array} \begin{array}{r} 2.0 \\ 50 \end{array}$$

$$\begin{array}{r} 6.0 \\ 50 \end{array} \begin{array}{r} 1.7 \\ 26 \end{array} \begin{array}{r} 10.4 \\ 16 \end{array} \begin{array}{r} 11.3 \\ 13 \end{array} \begin{array}{r} 11.1 \\ 8 \end{array} \begin{array}{r} 10.6 \\ 106 \end{array} \begin{array}{r} 11.3 \\ 6 \end{array} \begin{array}{r} 11.5 \\ 17 \end{array} \begin{array}{r} 11.5 \\ 21-23 \end{array} \begin{array}{r} 2.7 \\ 33 \end{array} \begin{array}{r} 1.6 \\ 50 \end{array}$$

$$\begin{array}{r} 3.6 \\ 50 \end{array} \begin{array}{r} 1.5 \\ 29 \end{array} \begin{array}{r} 12.6 \\ 15 \end{array} \begin{array}{r} 12.2 \\ 10 \end{array} \begin{array}{r} 11.5 \\ 115 \end{array} \begin{array}{r} 12.1 \\ 57 \end{array} \begin{array}{r} 13.6 \\ 16 \end{array} \begin{array}{r} 6.0 \\ 20 \end{array} \begin{array}{r} 5.8 \\ 23 \end{array} \begin{array}{r} 5.8 \\ 33 \end{array} \begin{array}{r} 5.8 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.
		880.56		
17+50			12.4	68.2
T.P.	0.64	868.86	12.34	868.22
18			1.8	67.1
+30			2.6	66.3
+50			3.1	65.8
19			4.2	64.7
+50			4.9	64.0
20			5.4	63.5
+50			5.8	63.1
21			6.0	62.9
+50			6.0	62.9
22			5.7	63.2
T.P.	5.35	868.53	5.68	863.18
+12	30" x 42" C.M.		5.4	63.1
Profile Ditch Rt.				

$\frac{5.9}{50}$ $\frac{6.4}{34}$ $\frac{14.4}{18}$ $\frac{13.7}{13}$ $\frac{12.6}{7}$ $\frac{12.4}{12.4}$ $\frac{13.0}{7}$ $\frac{14.6}{14}$ $\frac{15.3}{19}$ $\frac{12.2}{22}$ $\frac{12.3}{24}$ $\frac{3.1}{31}$ $\frac{50}{50}$

$\frac{0.4}{50}$ $\frac{2.1}{20}$ $\frac{3.2}{13}$ $\frac{2.1}{7}$ $\frac{1.9}{1.8}$ $\frac{2.5}{7}$ $\frac{3.6}{15}$ $\frac{3.4}{20}$ $\frac{50}{50}$

$\frac{3.3}{50}$ $\frac{4.5}{40}$ $\frac{5.2}{28}$ $\frac{5.4}{19}$ $\frac{4.8}{14}$ $\frac{2.8}{7}$ $\frac{2.7}{7}$ $\frac{3.3}{14}$ $\frac{6.7}{22}$ $\frac{8.3}{33}$ $\frac{7.7}{50}$

$\frac{5.7}{50}$ $\frac{7.2}{28}$ $\frac{6.3}{17}$ $\frac{4.0}{11}$ $\frac{3.3}{7}$ $\frac{3.3}{3.1}$ $\frac{3.8}{8}$ $\frac{8.6}{15}$ $\frac{9.0}{28}$ $\frac{50}{50}$

$\frac{9.4}{50}$ $\frac{9.4}{28}$ $\frac{9.0}{17}$ $\frac{4.9}{10}$ $\frac{4.4}{7}$ $\frac{4.3}{4.2}$ $\frac{5.0}{8}$ $\frac{9.8}{15}$ $\frac{9.7}{27}$ $\frac{9.7}{50}$

$\frac{10.1}{50}$ $\frac{10.0}{27}$ $\frac{9.4}{18}$ $\frac{6.0}{12}$ $\frac{5.2}{8}$ $\frac{5.0}{4.9}$ $\frac{5.4}{7}$ $\frac{9.7}{14}$ $\frac{10.0}{22}$ $\frac{50}{50}$

$\frac{10.3}{50}$ $\frac{10.3}{16}$ $\frac{6.2}{11}$ $\frac{5.8}{5}$ $\frac{5.7}{5.4}$ $\frac{6.1}{11}$ $\frac{10.4}{15}$ $\frac{10.3}{27}$ $\frac{50}{50}$

$\frac{12.2}{33}$ $\frac{12.3}{34}$ $\frac{10.6}{19}$ $\frac{6.7}{11}$ $\frac{6.1}{8}$ $\frac{5.8}{5.8}$ $\frac{6.2}{6}$ $\frac{6.7}{11}$ $\frac{10.3}{15}$ $\frac{10.3}{26}$ $\frac{50}{50}$

Top Water 1-7-41 10.63

$\frac{12.6}{50}$ $\frac{12.3}{34}$ $\frac{10.4}{20}$ $\frac{6.8}{12}$ $\frac{6.2}{8}$ $\frac{6.0}{6.0}$ $\frac{6.3}{6}$ $\frac{7.0}{11}$ $\frac{10.0}{15}$ $\frac{10.3}{23}$ $\frac{10.3}{50}$

$\frac{12.3}{50}$ $\frac{11.9}{34}$ $\frac{10.7}{19}$ $\frac{6.8}{12}$ $\frac{6.1}{18}$ $\frac{5.9}{6.0}$ $\frac{6.4}{6}$ $\frac{10.2}{13}$ $\frac{10.3}{22}$ $\frac{50}{50}$

$\frac{11.8}{50}$ $\frac{11.2}{34}$ $\frac{10.8}{20}$ $\frac{6.9}{13}$ $\frac{6.0}{7}$ $\frac{6.0}{5.7}$ $\frac{6.7}{10}$ $\frac{10.0}{14}$ $\frac{10.1}{20}$ $\frac{10.1}{50}$

56.79

57.39

$\frac{10.7}{50}$ $\frac{11.1}{19}$ $\frac{11.74}{19}$ $\frac{6.4}{13}$ $\frac{5.6}{7}$ $\frac{5.4}{5.4}$ $\frac{5.9}{6}$ $\frac{11.14}{14}$ $\frac{11.0}{23}$ $\frac{11.0}{23}$ $\frac{50}{50}$

$\frac{11.0}{23}$ $\frac{11.0}{50}$ $\frac{10.5}{100}$ $\frac{10.4}{150}$ $\frac{10.3}{200}$

Sta	+	Σ	-	Elev
		868.53		
22+50			5.2	63.3.
23			5.0	63.5.
+50			4.9	63.6.
24			4.9	63.6.
+50			4.8	63.7.
25			4.8	63.7.
B.M.	6.53	869.50	5.59	862.94
+50			5.6	63.9.
26			5.4	64.1.
+50			5.1	64.4.
27			4.9	64.8.
+50			4.1	65.4.
28			3.1	66.4.
T.P	6.80	875.63	2.67	866.83

$\frac{9.3}{50}$ $\frac{9.4}{35}$ $\frac{9.5}{19}$ $\frac{6.0}{12}$ $\frac{5.2}{50}$ $\frac{6.0}{6}$ $\frac{9.2}{14}$ $\frac{9.9}{18}$ $\frac{9.3}{25}$ $\frac{9.3}{50}$

$\frac{9.0}{50}$ $\frac{8.9}{30}$ $\frac{8.5}{18}$ $\frac{5.8}{13}$ $\frac{5.2}{8}$ $\frac{5.0}{50}$ $\frac{5.7}{4}$ $\frac{7.8}{13}$ $\frac{9.2}{19}$ $\frac{8.5}{22}$ $\frac{8.5}{50}$

$\frac{8.5}{50}$ $\frac{8.5}{19}$ $\frac{5.4}{12}$ $\frac{5.0}{4.9}$ $\frac{5.7}{6}$ $\frac{8.4}{13}$ $\frac{8.7}{20}$ $\frac{8.7}{30}$ $\frac{8.7}{50}$

$\frac{8.9}{50}$ $\frac{9.0}{32}$ $\frac{9.5}{19}$ $\frac{5.6}{12}$ $\frac{4.9}{4}$ $\frac{5.8}{13}$ $\frac{9.4}{21}$ $\frac{9.8}{37}$ $\frac{9.5}{50}$

$\frac{9.0}{50}$ $\frac{9.3}{35}$ $\frac{9.3}{21}$ $\frac{5.75}{14}$ $\frac{5.1}{8}$ $\frac{5.4}{4.8}$ $\frac{9.1}{12}$ $\frac{9.5}{19}$ $\frac{9.4}{33}$ $\frac{9.4}{50}$

$\frac{9.2}{50}$ $\frac{9.2}{34}$ $\frac{9.9}{20}$ $\frac{5.5}{12}$ $\frac{5.6}{48}$ $\frac{9.0}{12}$ $\frac{9.0}{20}$ $\frac{9.1}{33}$ $\frac{9.1}{50}$

Spk 18" Oak 110' Lt 24+50

$\frac{9.6}{50}$ $\frac{9.5}{36}$ $\frac{8.8}{19}$ $\frac{6.1}{13}$ $\frac{5.6}{5.6}$ $\frac{6.4}{6}$ $\frac{9.0}{11}$ $\frac{9.3}{18}$ $\frac{9.4}{31}$ $\frac{9.4}{50}$

$\frac{8.5}{50}$ $\frac{8.6}{30}$ $\frac{8.7}{19}$ $\frac{6.2}{13}$ $\frac{5.8}{10}$ $\frac{5.5}{5.4}$ $\frac{6.2}{4}$ $\frac{8.1}{12}$ $\frac{8.9}{18}$ $\frac{8.9}{36}$ $\frac{8.9}{50}$

$\frac{8.6}{50}$ $\frac{8.7}{35}$ $\frac{8.7}{18}$ $\frac{5.7}{12}$ $\frac{5.3}{9}$ $\frac{5.2}{5.1}$ $\frac{5.9}{5}$ $\frac{6.0}{12}$ $\frac{8.8}{17}$ $\frac{8.8}{30}$ $\frac{8.8}{50}$

$\frac{8.1}{50}$ $\frac{7.9}{34}$ $\frac{7.7}{19}$ $\frac{5.4}{14}$ $\frac{4.7}{9}$ $\frac{4.9}{4.7}$ $\frac{5.4}{6}$ $\frac{7.5}{13}$ $\frac{7.8}{18}$ $\frac{7.8}{33}$ $\frac{7.8}{50}$

$\frac{5.6}{50}$ $\frac{5.3}{33}$ $\frac{6.4}{19}$ $\frac{4.7}{14}$ $\frac{4.2}{8}$ $\frac{4.1}{4.1}$ $\frac{4.6}{5}$ $\frac{6.2}{13}$ $\frac{6.7}{17}$ $\frac{6.6}{27}$ $\frac{6.6}{50}$

$\frac{3.2}{50}$ $\frac{4.4}{25}$ $\frac{4.5}{18}$ $\frac{4.0}{13}$ $\frac{3.4}{8}$ $\frac{3.3}{3.1}$ $\frac{3.8}{7}$ $\frac{5.6}{13}$ $\frac{5.5}{17}$ $\frac{5.4}{37}$ $\frac{5.4}{50}$

Sta	+	π	-	Elev
		875.63 ✓		
28750			8.2	67.4.
29			6.9	68.7.
+50			5.5	70.1.
30			4.2	71.4.
+50			2.8	72.8. ✓
T.P	8.77	883.01 ✓	1.39	874.24
31			8.6	74.4.
+50			7.1	75.9.
32			5.8	77.2.
+50			4.8	78.2. ✓
T.P	13.39	896.17 ✓	0.23	882.78
33				79.0.
+31				79.4.
+75				79.7.

$$\begin{array}{cccccc} 7.2 & 8.3 & 9.7 & 9.6 & 9.0 & 8.4 \\ 50 & 29 & 20 & 17 & 13 & 10 \end{array} \quad \begin{array}{cccccc} 82 & 8.5 & 9.1 & 11.4 & 11.3 & 10.5 \\ 82 & 4 & 9 & 13 & 19 & 28 & 50 \end{array}$$

$$\begin{array}{cccccc} 4.7 & 6.0 & 8.8 & 8.5 & 7.4 \\ 50 & 24 & 19 & 16 & 13 \end{array} \quad \begin{array}{cccccc} 7.0 & 7.5 & 9.7 & 10.3 & 10.1 & 8.2 & 8.9 \\ 69 & 5 & 12 & 18 & 23 & 31 & 35 & 50 \end{array}$$

$$\begin{array}{cccccc} 3.1 & 5.1 & 7.4 & 7.5 & 5.8 \\ 50 & 23 & 19 & 17 & 11 \end{array} \quad \begin{array}{cccccc} 5.5 & 6.2 & 7.5 & 8.2 & 8.1 & 5.1 & 4.6 \\ 55 & 5 & 13 & 18 & 22 & 31 & 35 & 50 \end{array}$$

$$\begin{array}{cccccc} 2.7 & 3.8 & 5.7 & 5.1 & 4.1 \\ 30 & 22 & 18 & 16 & 10 & 4.2 \end{array} \quad \begin{array}{cccccc} 4.2 & 4.8 & 6.0 & 6.5 & 6.1 & 3.8 & 2.7 \\ 4 & 14 & 18 & 23 & 29 & 36 & 50 \end{array}$$

$$\begin{array}{cccccc} 3.2 & 1.9 & 3.9 & 3.5 & 3.1 \\ 30 & 25 & 19 & 16 & 14 & 10 & 2.8 \end{array} \quad \begin{array}{cccccc} 2.8 & 3.3 & 4.0 & 4.3 & 4.0 & 2.2 & 1.7 \\ 4 & 14 & 18 & 21 & 28 & 35 & 50 \end{array}$$

$$\begin{array}{cccccc} 11.5 & 10.7 & 10.0 & 9.8 & 9.0 \\ 50 & 35 & 20 & 16 & 14 & 8.4 \end{array} \quad \begin{array}{cccccc} 8.6 & 9.2 & 8.8 & 8.8 & 9.1 & 6.3 & 6.8 \\ 4 & 14 & 18 & 22 & 29 & 34 & 50 \end{array}$$

$$\begin{array}{cccccc} 7.6 & 6.8 & 6.0 & 8.1 & 7.7 \\ 50 & 36 & 22 & 17 & 15 & 13 & 7.1 \end{array} \quad \begin{array}{cccccc} 7.2 & 7.7 & 7.4 & 7.4 & 6.3 & 6.3 \\ 4 & 12 & 19 & 27 & 31 & 50 \end{array}$$

$$\begin{array}{cccccc} 6.2 & 7.6 & 7.9 & 6.8 \\ 50 & 27 & 22 & 19 & 14 & 5.8 \end{array} \quad \begin{array}{cccccc} 5.9 & 6.2 & 5.8 & 5.3 & 5.1 & 5.6 \\ 13 & 18 & 24 & 28 & 50 \end{array}$$

$$\begin{array}{cccccc} 4.8 & 5.0 & 5.1 & 5.4 & 4.9 \\ 50 & 28 & 16 & 12 & 4 & 4.8 \end{array} \quad \begin{array}{cccccc} 5.3 & 3.5 & 1.4 \\ 15 & 20 & 50 \end{array}$$

$$\begin{array}{cc} 7.2 & 9.0 \\ 30 & 32 \end{array} \quad 17.2 \quad \begin{array}{cc} 12.3 & 14.6 \\ 27 & 50 \end{array}$$

$$\begin{array}{cc} 6.9 & 5.5 \\ 50 & 38 \end{array} \quad 16.8 \quad \begin{array}{cc} 9.0 & 11.2 \\ 31 & 50 \end{array}$$

$$\begin{array}{cc} 14.7 & 10.1 \\ 50 & 32 \end{array} \quad 16.5 \quad \begin{array}{cc} 2.9 & 4.3 \\ 39 & 50 \end{array}$$

Sta.	+	π	-	Elev.
		896.17		
34				79.8
+20				79.8
+50				79.6
T.P.	1.75	884.53	13.39	882.78
33			5.5	79.0
+31			5.1	79.4
+75			4.8	79.7
34			4.7	79.8
+20			4.7	79.8
+50			4.9	79.6
35			5.0	79.5
+50			5.0	79.5
36			4.5	80.0

16.4.

$$\frac{1.9}{47} \quad \frac{1.8}{50}$$

16.4.

$$\frac{1.7}{40} \quad \frac{1.3}{50}$$

16.6.

$$\frac{9.3}{31} \quad \frac{5.9}{40} \quad \frac{3.9}{50}$$

$$\frac{6.2}{17} \quad \frac{6.0}{15} \quad \frac{5.6}{10} \quad 5.5 \quad \frac{5.5}{4} \quad \frac{6.1}{4} \quad \frac{6.5}{16.18}$$

$$\frac{5.8}{17} \quad \frac{5.6}{14} \quad \frac{5.3}{10} \quad 5.1 \quad \frac{5.2}{11} \quad \frac{5.6}{11} \quad \frac{7.0}{15.18}$$

$$\frac{5.8}{17} \quad \frac{5.2}{14} \quad 4.8 \quad \frac{5.3}{12} \quad \frac{6.1}{15.17}$$

$$\frac{8.8}{50} \quad \frac{5.1}{34} \quad \frac{1.7}{24} \quad \frac{5.3}{18} \quad \frac{5.3}{15} \quad 4.7 \quad \frac{5.3}{11} \quad \frac{5.6}{15.17}$$

$$\frac{12.1}{50} \quad \frac{5.8}{31} \quad \frac{3.9}{22} \quad \frac{6.1}{17} \quad \frac{5.1}{14} \quad 4.7 \quad \frac{5.4}{10} \quad \frac{5.1}{15.18}$$

$$\frac{11.8}{50} \quad \frac{8.8}{32} \quad \frac{5.4}{16} \quad 4.9 \quad \frac{5.4}{11} \quad \frac{6.4}{15.17}$$

$$\frac{11.6}{50} \quad \frac{10.9}{34} \quad \frac{9.9}{26} \quad \frac{5.7}{15} \quad \frac{5.2}{11} \quad 5.0 \quad \frac{5.4}{11} \quad \frac{7.5}{18} \quad \frac{8.5}{25} \quad \frac{3.6}{50}$$

$$\frac{11.9}{50} \quad \frac{12.3}{39} \quad \frac{12.4}{28} \quad \frac{5.8}{15} \quad \frac{5.5}{50} \quad \frac{12.0}{9} \quad \frac{12.0}{21} \quad \frac{9.2}{32} \quad \frac{9.2}{50}$$

$$\frac{13.8}{50} \quad \frac{12.4}{35} \quad \frac{10.7}{26} \quad \frac{5.4}{15} \quad \frac{5.1}{12} \quad 4.5 \quad \frac{4.9}{9} \quad \frac{12.2}{22} \quad \frac{12.3}{50}$$

Sta.	+	Σ	-	Elev.
		884.53		
36 + 21	18' x 48' C.M.		4.2	80.3
T.P.	581	889.12	1.22	888.31
+50			8.0	81.1
37			6.2	82.9
+29			5.0	84.1
+50			4.1	85.0
38			1.8	87.3
+32			0.7	88.4
+64			1.5	87.6
B.M.			3.51	885.61

885.61

70.83

71.55

$\frac{13.5}{50}$ $\frac{13.0}{24}$ $\frac{13.70}{24}$ $\frac{5.0}{15}$ 4.2 $\frac{4.4}{10}$ $\frac{12.7}{24}$ $\frac{12.98}{24}$ $\frac{13.2}{36}$ $\frac{13.3}{50}$
 FL.

End G.R. Post Lt.

$\frac{17.0}{50}$ $\frac{16.7}{30}$ $\frac{9.1}{16}$ $\frac{8.4}{10}$ 8.0 $\frac{8.2}{9}$ $\frac{8.5}{12}$ $\frac{15.2}{24}$ $\frac{16.7}{50}$

$\frac{13.7}{50}$ $\frac{13.3}{36}$ $\frac{11.2}{27}$ $\frac{7.0}{16}$ 6.2 $\frac{6.7}{10}$ $\frac{7.1}{18}$ $\frac{13.3}{30}$ $\frac{13.6}{39}$ $\frac{12.7}{50}$

24" G.I. x 0.1m
FL.

$\frac{11.7}{50}$ $\frac{8.6}{35}$ $\frac{6.3}{23}$ $\frac{5.8}{18}$ $\frac{5.3}{9}$ 5.0 $\frac{5.6}{10}$ $\frac{5.5}{12}$ $\frac{5.0}{14}$ $\frac{5.5}{18}$ $\frac{10.4}{27}$ $\frac{10.74}{28}$ $\frac{10.0}{34}$ $\frac{10.1}{50}$

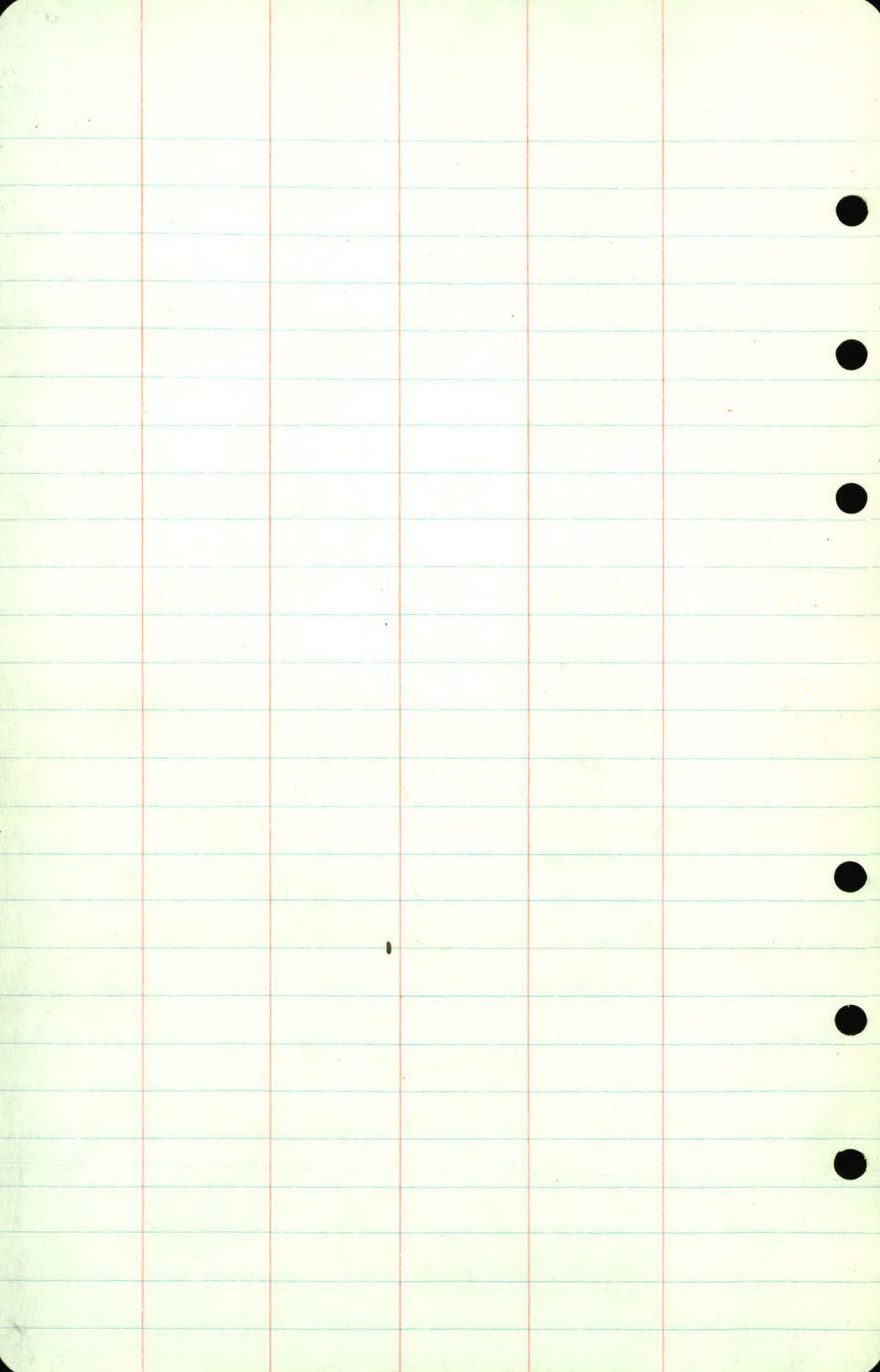
$\frac{6.6}{50}$ $\frac{5.6}{31}$ $\frac{5.4}{21}$ $\frac{5.1}{17}$ 4.1 $\frac{4.5}{10}$ $\frac{5.0}{12}$ $\frac{4.7}{20}$ $\frac{4.3}{33}$ $\frac{5.4}{50}$

$\frac{2.5}{50}$ $\frac{2.4}{32}$ $\frac{2.8}{21}$ $\frac{2.6}{13}$ 1.8 $\frac{1.8}{20}$ $\frac{1.5}{50}$

$\frac{.41}{50}$ $\frac{0.8}{25}$ 0.7 $\frac{0.8}{25}$ $\frac{0.8}{50}$

$\frac{.69}{50}$ 1.5 $\frac{1.1}{50}$

Spike P.P. SW. Cor. "C" and S.T.H. #61



Co. Rd. "C"

Extension of X sections
to 100' on Lt. and Rt.
Sta. 33 to 34

Sta.	+	π	-	Elev.
B.M.	4.11	889.72		885.61
F.L. E End 24 "C.M. under #61			9.80	879.92
F.L. W. End. 24 "C.M. under #61			12.34	977.38
F.L. 18 "C.M. approx. Sta. 36				
T.P.	6.07	888.56	7.23	882.49
33			9.4	879.2
+31			9.2	879.4
+75			8.8	879.8
34			8.7	879.7
T.P.	9.71	897.32	0.95	887.61
33				
+31				
+75				
34				
T.P.	0.82	883.60	14.54	882.78
T.P.	1.43	873.90	11.13	872.47
T.P.	4.23	869.14	8.99	864.91
B.M.			6.16	862.98

862.97

Lt.

4

Spike P.P. S.W. Cor. C 4 #61

$$\begin{array}{r} 70.93 \\ \hline 18.79 \end{array}$$

$$\begin{array}{r} 71.65 \\ \hline 18.07 \end{array}$$

$\frac{100}{19}$	$\frac{104}{18-16}$	$\frac{9.8}{14}$	$\frac{9.7}{10}$	$\frac{9.4}{9}$	$\frac{9.8}{9}$	$\frac{9.9}{11}$	$\frac{10.9}{14}$	$\frac{11.0}{16}$
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$\frac{9.3}{19}$	$\frac{9.8}{18}$	$\frac{9.9}{15}$	$\frac{9.3}{10}$	$\frac{9.2}{9}$	$\frac{9.6}{11}$	$\frac{10.0}{13}$	$\frac{10.8}{15}$	$\frac{10.9}{17}$
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$\frac{9.7}{17}$	$\frac{9.6}{15}$	$\frac{9.0}{11}$	$\frac{8.8}{8}$	$\frac{9.1}{11}$	$\frac{9.6}{14}$	$\frac{9.4}{17}$
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$\frac{9.6}{18}$	$\frac{9.9}{17}$	$\frac{9.4}{15}$	$\frac{9.0}{10}$	$\frac{8.7}{8}$	$\frac{8.9}{10}$	$\frac{9.4}{12}$	$\frac{9.4}{17}$
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$\frac{11.6}{100}$	$\frac{8.3}{96}$	$\frac{7.8}{64}$	$\frac{8.7}{50}$	$\frac{10.2}{31}$	$\frac{13.5}{25}$	$\frac{14.3}{31}$	$\frac{14.7}{38}$	$\frac{16.0}{50}$	$\frac{16.4}{72}$	$\frac{16.7}{100}$
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$\frac{19.8}{100}$	$\frac{12.8}{78}$	$\frac{10.8}{65}$	$\frac{8.1}{50}$	$\frac{6.7}{37}$	$\frac{9.8}{29}$	$\frac{10.1}{40}$	$\frac{11.9}{50}$	$\frac{12.9}{72}$	$\frac{14.1}{100}$
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$\frac{27.4}{100}$	$\frac{22.6}{72}$	$\frac{17.6}{50}$	$\frac{12.2}{31}$	$\frac{12.1}{29}$	$\frac{3.6}{38}$	$\frac{5.1}{50}$	$\frac{8.1}{65}$	$\frac{9.2}{100}$
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$\frac{29.0}{100}$	$\frac{24.8}{68}$	$\frac{22.4}{50}$	$\frac{19.1}{38}$	$\frac{14.6}{25}$	$\frac{2.9}{38}$	$\frac{3.0}{50}$	$\frac{3.7}{76}$	$\frac{5.7}{100}$
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Spike 18" Oak 110' Lt. 24+50

