

Bk. 63 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

S. Co. Rd. "C"

From W. Co. Line to Victoria St.

Road f'cc't. No. 7

Date Filed. 6-11-41

File

P'

Align

4-29-30

HPW

AM

LC

LL

CF

Sta

Pt

ΔLt

ΔRt

12+83.67 = P.I.

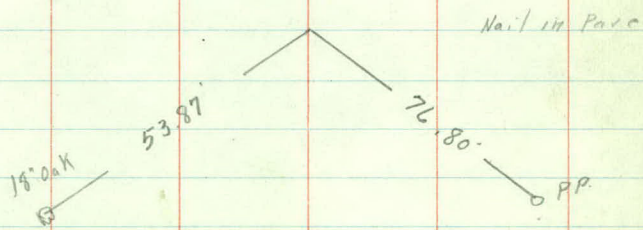
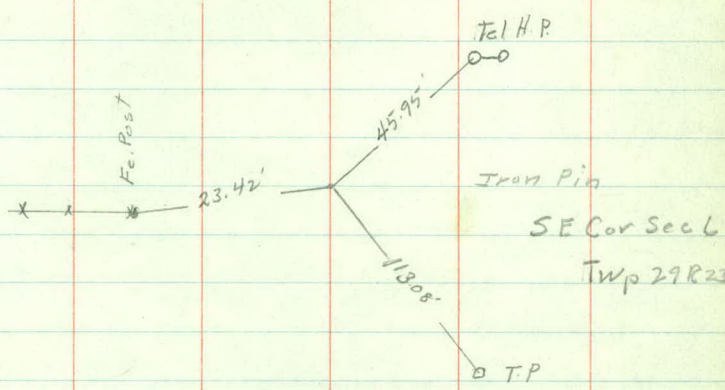
$0^{\circ}27'$

0+00 = West Co Line

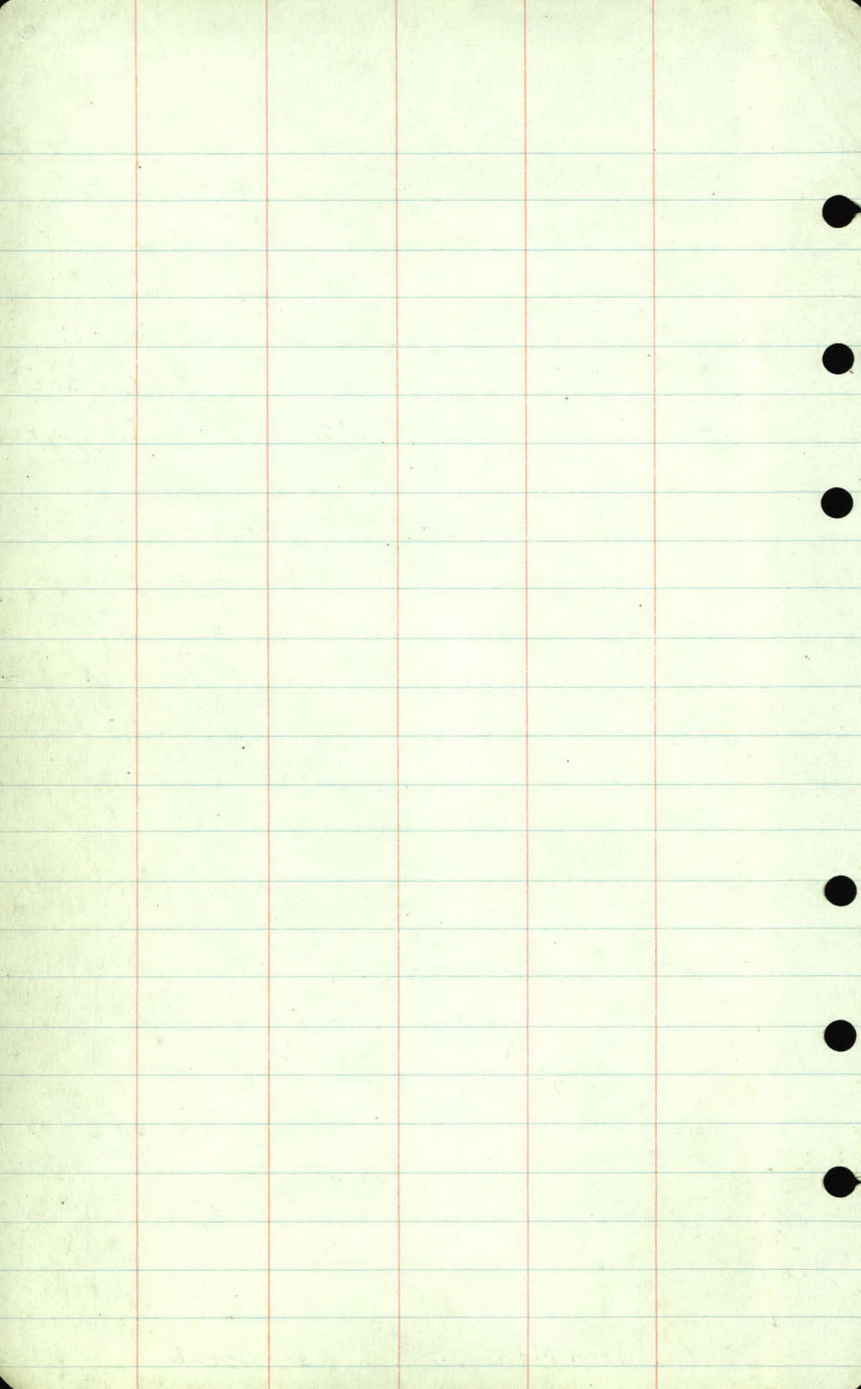
0+00 P.O.T. Δ S.T.H # 8

2° Curve

Description



Iron Mon . 5 1/4 Sec 6



Plan Survey

Co Rd C

from ~~at~~ Co Line S.T.H. #8
to Victoria St.

Index:

Alignment - 1-7
Topography - 8-34
Bench Levels 35-38
X Sections 39-77

Plan completed
1/4/51

Angle

Sta Pt Lt Rt

26+52.28 P I. $0^{\circ}04'$

26+35.90 P.O.T. $\frac{1}{2}$ Main Track

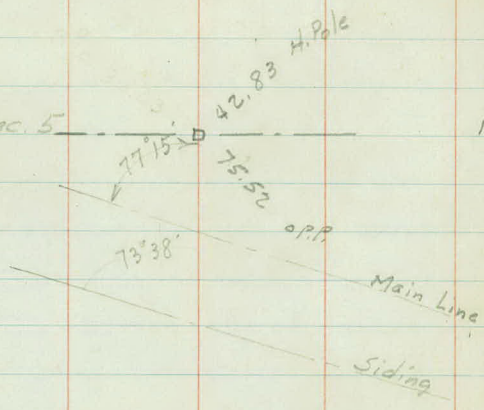
25+52.65 P.O.T. $\frac{1}{2}$ Spur Track

5+00 P.O.T.

0+00 W. Co. Line

1/4 Cor. S. Line Sec. 5

Mon.



17th Iron
Post
from
Corner.

34.35

84.19
O.T.P.

52.73

O.T.P.

R.R. Spike

H Pole

S.W. Cor. 5-29-23

45.95

27.04

Iron Road
Sign

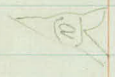
Iron Plug

113.05 O.T.P.

Sta.	Pt.	Angle	
		Lt.	Rt.
+85.25	P.T.	5° 33'	
+50		5° 10'	
61		4° 37'	
+50		4° 04'	
60		3° 30'	$\Delta = 11^{\circ} 06' 14''$
+50		2° 57'	$D = 2^{\circ} 12' 4''$
57+34.55	P.I.	11° 06'	$T = 252.32'$
59		2° 24'	$L = 503.02'$
+50		1° 51'	$R = 2596.68'$
58		1° 18'	
+50		0° 45'	
57		0° 12'	
56+82.23	P.C.	0° 00'	

53+02.60 P.I. 0° 36.5'

Cleveland Ave
S.E. Cor. Sec. 5



P.P.
o

47.69

72.68
o T.P.

36.17

T.P.

Bolt Spoke

90038.5

P.P.
o

38.00

47.86

P.P.
o

38.30

45.85
P.P.
o

T.P.
o

Mon.

45.30

Sta.	Pt.	Angle	
		Lt.	Rt.
+53.76	P.T.		$2^{\circ} 59'$
+50			$2^{\circ} 57'$
73			$2^{\circ} 27'$ $\Delta = 3^{\circ} 58' \text{ Rt}$
+50			$1^{\circ} 57'$ $D = 2^{\circ}$
72+04.75	P.L.		$5^{\circ} 58'$ $T = 149.32$
72			$1^{\circ} 27'$ $L = 298.33$
+50			$0^{\circ} 57'$ $R = 2864.93$
71			$0^{\circ} 27'$
70+55.43	P.C.		

			$\Delta = 2^{\circ} 35' \text{ Rt}$
+87.79	P.T.		$1^{\circ} 17\frac{1}{2}'$ $D = 2^{\circ}$
+50			$0^{\circ} 55'$ $T = 64.60$
69+23.22	P.L.		$2^{\circ} 35'$ $L = 129.17$
69			$0^{\circ} 25'$ $R = 2864.93$
68+58.62	P.C.		

TP

101.60

R.R. Spike

22.18

21.10

16.15

TP

P.P.

G.P.

TP

44.51

R.R. Spike

39.71

07.35

Punch Mark

End Com. R.R. Culv.

P.P.

Sta. Pt. Lt. Angle Rt.

87+22.10 P.I. 0°04' Lt.

0°04' Lt
WJB

19+51.75 P.O.T

New Brighton Rd.

+50.04 P.T

79

78+80.11 P.I.

+50

78+10.04 P.C.

2°48'

10°48'

3°36'

0°48'

0°00'

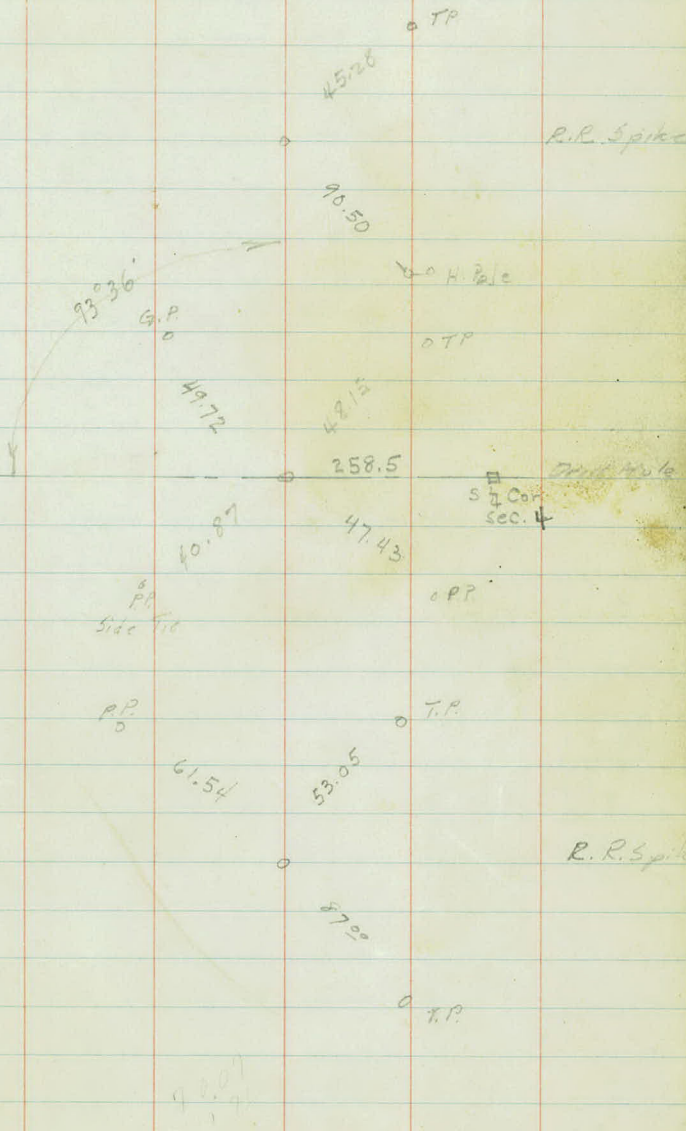
$\Delta = 5^{\circ}36'$ Rt.

$D = 4^{\circ}$

$T = 70.07$ -

$L = 140.00$

$R = 1432.69$



Angle

Sta

Pl

Lt

Rt

Curve Data

+08.48 P.T.

$1^{\circ} 03\frac{1}{2}'$

121

$1^{\circ} 01'$

$\Delta = 2^{\circ} 07'$

+50

$0^{\circ} 46'$

$D = 1^{\circ}$

120 +02.69 P.I.

$2^{\circ} 07'$

$T = 105.88$?

120

$0^{\circ} 31'$

$L = 211.67$

+50

$0^{\circ} 16'$

$E = 5729.65$

119

$0^{\circ} 01'$

118 +96.81 P.C.

105 +89.07

P.I.

$0^{\circ} 20'$

Snelling Ave

o T.P.

58.16

R.R. Spikes

114.98

11.8

6" Twin Oak

oo T.P.
H.P.
Side
T.P.

93 17 1/2
93 0 37

PP 0 93 0 0

T.P.
204.P

68.30 68.12 79.63

120.5'

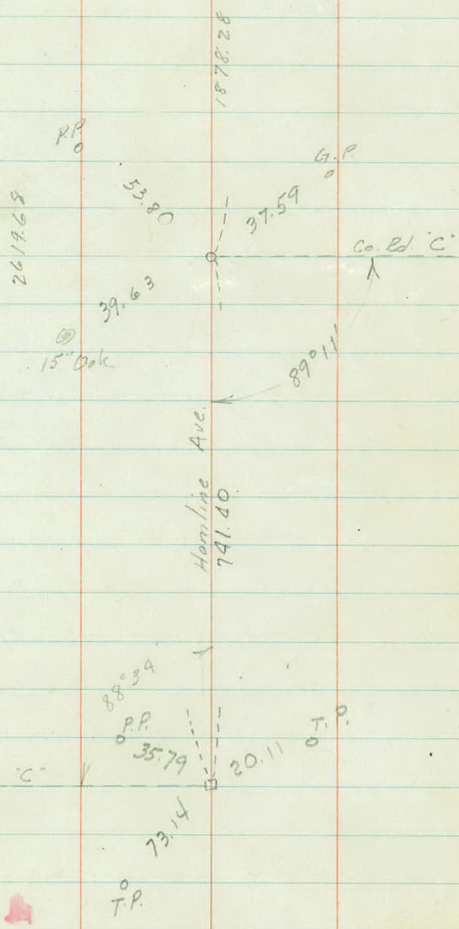
□ R.R. Spk
S.E. Cor.
Sec. 4

Sta.	Pt	Lt	Angle Rt
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32+10.65	P.I		90°49'	Hamline Ave.
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132+10.65	P.I	71°26'		Hamline Ave. S & Cor. 3
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N



Sta	Pt.	Angle
		Lt. Rt.

0° 18'

158+32.15 P.I. = Plan Survey
Co. Rd. "C" Lexington Ave.
Lex. Ave. to Victoria
File Dr. B - Book 153

145+22.65 P. I.

0° 13½'

136+41.90 P.O.T.

Cor.
Bldg.

3
2
5
84.69

2636.90

W 1/4 Cor
[]
Sec. 3

1892.09

744.81

SE
Cor.
[]
Sec. 3 Spike

57.20

34.77

° T.P.

15" W.D.

po H Pole

58.61

R.R. Spike

1.

27.44

° P.P.

Spike

Sta	Pt	Angle	Lt	Rt
-----	----	-------	----	----

177+74.87	P.O.T.			
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174+80.93	P.O.T.			
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170+63.47	P.O.T.			
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170+14.45	P.O.T.			
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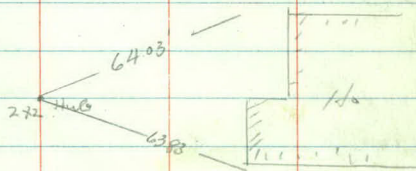
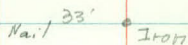
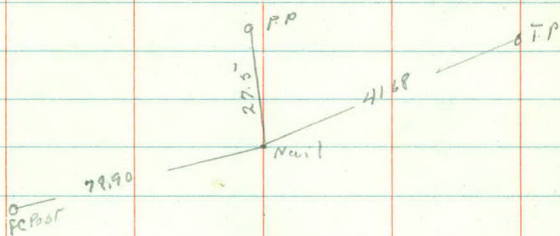
164+91.15	P.O.T.			
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CHANGE

LINE

SEE

Voip

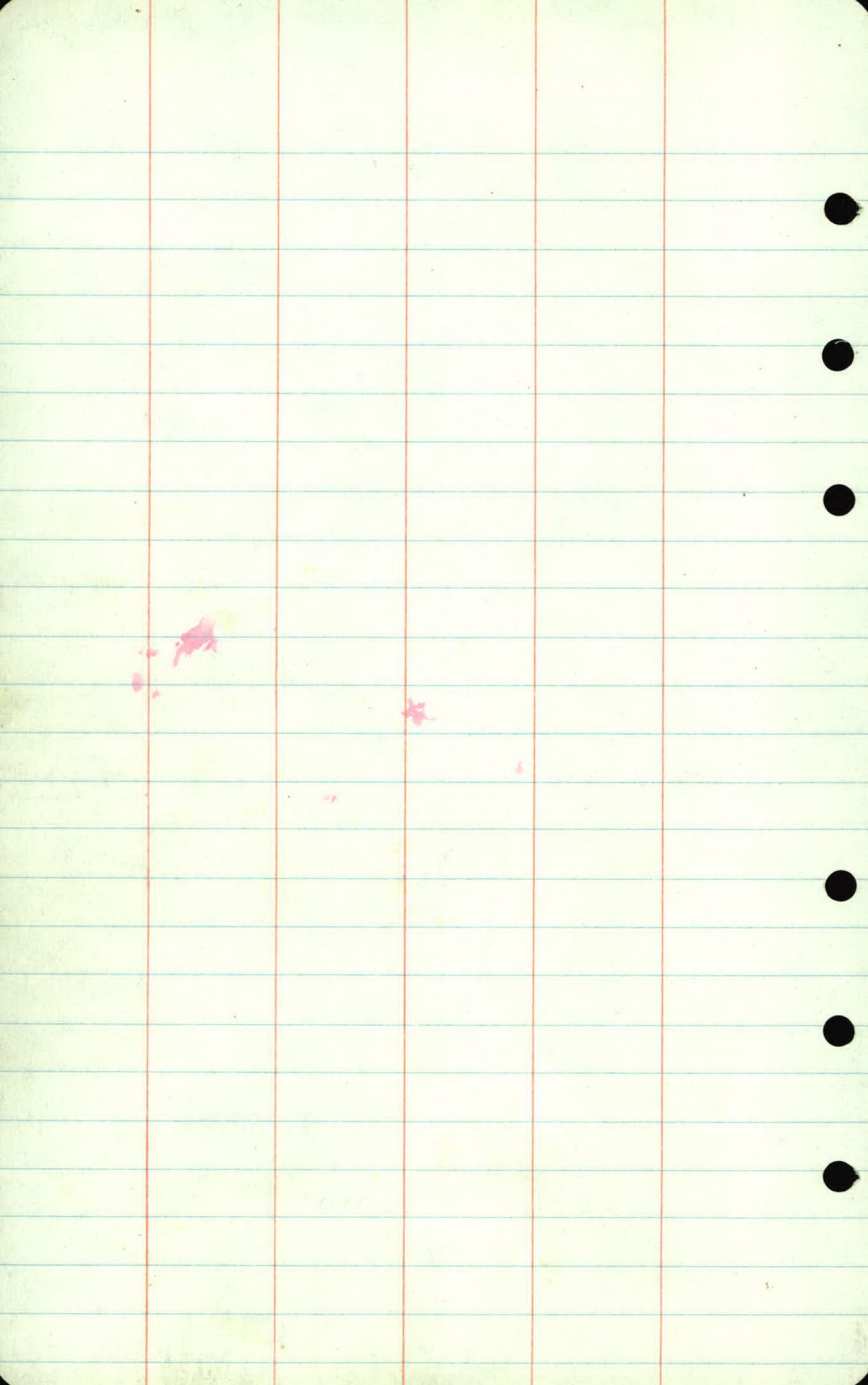


Iron

2 Oxford

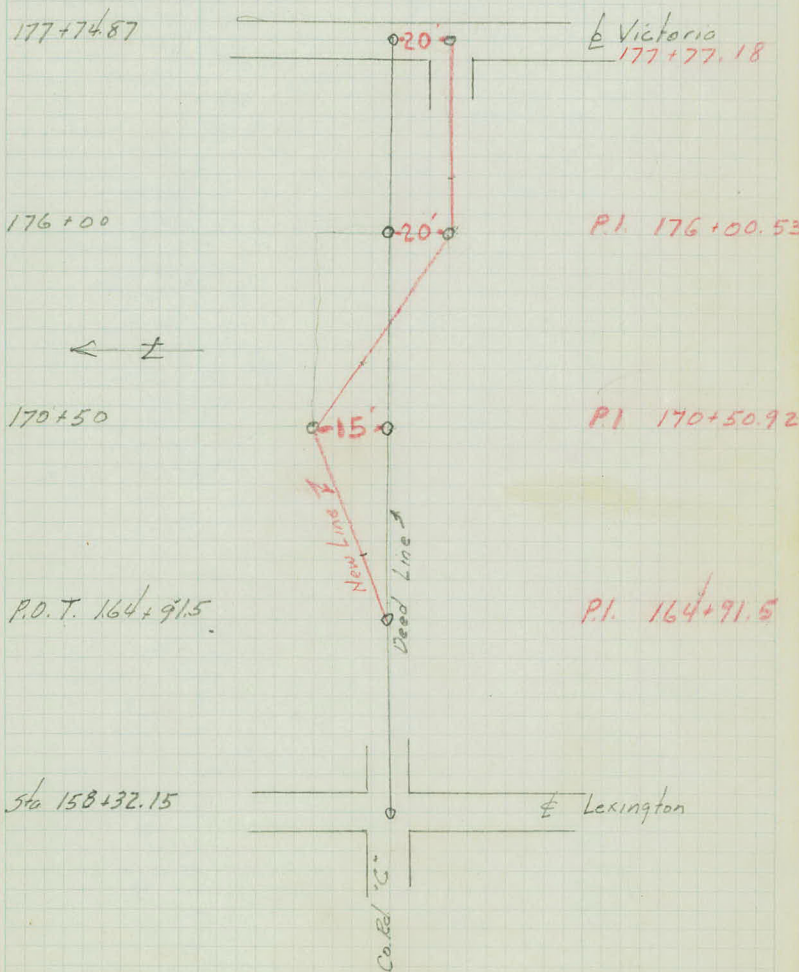
33.0

Iron



LINE CHANGE Co. Rd "C"

Between Lexington + Victoria





Alignment Notes
on Co. Rd "C"
Line Change Between
Lexington & Victoria

PARTY:
R.P.
A.M.
L.G.
C.F.

Completed - 1-17-41

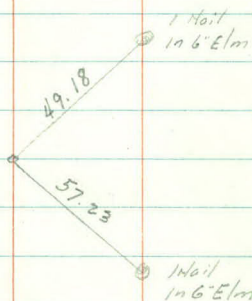
Sta.	Pt.	Angle Lt. Rt.	Data.
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+37.51	P.T.		$2^{\circ} 36'$ Δ $5^{\circ} 12'$ Rt.
171		$1^{\circ} 02'$	D 3°
170+50.92	P.I.	$5^{\circ} 12'$	T 86.74.
+50		$1^{\circ} 17'$	L 173.33.
170		$0^{\circ} 32'$	R 1910.08
169+64.18	P.C.		E 1.97

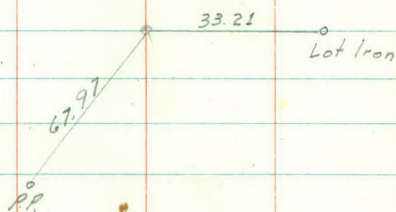
+29.49	P.T.	$0^{\circ} 46'$	Δ $1^{\circ} 32'$ Lt.
165		$0^{\circ} 28'$	D 2°
164+91.15	P.I.	$1^{\circ} 32'$	T 38.33
+75		$0^{\circ} 13'$	L 76.67
164+52.82	P.C.		R 2864.93
			E 0.304

158+32.15	P.I.	E Lexington	
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7C



R.R. Spk.



Bolt Spk.

Sta.	Pt.	Angle	Angle	Data.
		Lt.	Rt.	

177+77.18	P.O.T.			Victoria
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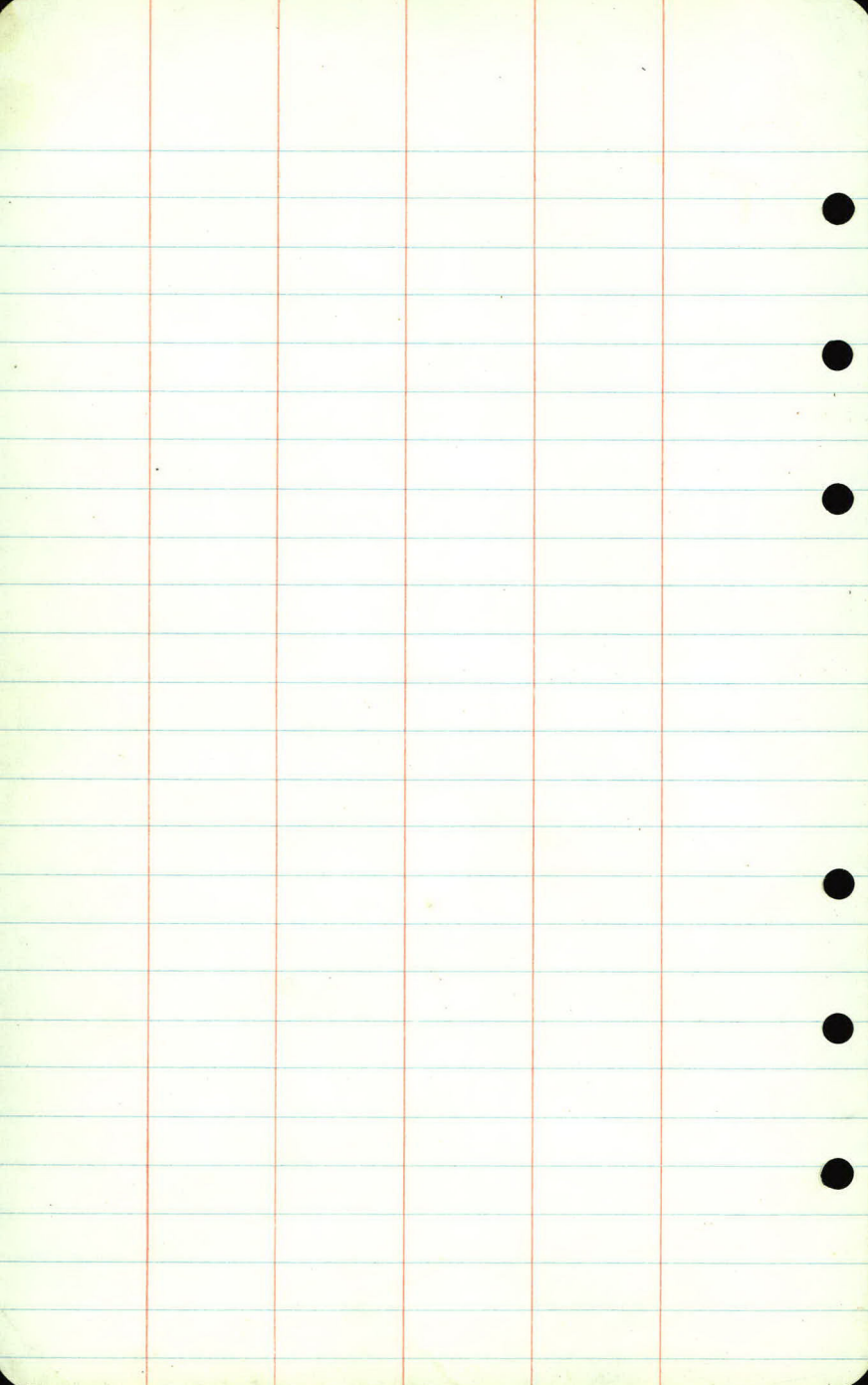
176+86.74	P.T.	1° 43½'		A 3° 27' Lt.
+50		1° 21½'		D 2°
176+00.53	P.I.	3° 27'		T 86.29
176		0° 51½'		L 172.50
+50		0° 21½'		R 2864.93
75+14.25	P.C.			E 1.299



R.R. Spk.



R.R. Spk.



Topography

6

Rd. Rd.
13' 12'

18.5"

+57' 24" X 10 CM X Drain LH
15" X 28.5" " Rt.

20'

5

13' 12'

4

13' 11'

3

14' 10'

2

15' 9'

1

18' 7'

p

+17.6 Edge Pare
2° Curve

End Swp 26-250'

+37 T.P. 39'

Swp 27-150'

+35 Beg Swp 30-80'

100 End Rad 18'

+73 Beg Rad 82'

1400 20" Oak 59'

Cultivated

Swamp

Cultivated

+07 T.P. 22'

+92 T.P. 21'

+22 T.P. 21'

+52 T.P. 20'

+62 T.P. 60'

+54 P.P. 30'

+54 End Rad 10'

+00 Beg Rad 24'

27' Pav

50' 45"

50' 45"

50' 45"

50' 45"

130' 65"

130' 45"

130' 45"

130' 45"

130' 45"

13

$$+ 8367 = 0400$$

11'

15'

12

11'

16'

11

10'

15'

10

10

14'

9

11'

14'

8

+ 17 X Drain

12'

10" X 33' V. T. RT
 15" X 6' CMS Lt.
 13'

7

12'

13'

6

13'

12

+80 Fe Cor 23'

Fe 23'

Fe 24'

Fe 25'

Fe 25'

+44 Fe Cor 25'

+40 Rgc tie Fe

+19 End 15" CM X Dr. 18'

Pasture

Uncultivated

Cultivated

+74 T.P. 26'

+44 T.P. 25'

+08 T.P. 24'

+13 End X Dr. 21'
20" V, + Rt.

+81 T.P. 23'

+43 T.P. 22'



Topography

COUNTY ROAD "C"

W. Co. Line

to

Victoria St.

Note: All RR. Ties to $\frac{1}{2}$ track.

11, 14

Road

14

6 12'

14'

5 11'

15'

4 13

16

3 13

16

2 13

17

1 11

16

0 9

16

+64 PP-28'

+63 Hedge-33'

+53 T.P. 23

+28 PP-28'

+31 T.P. : 24

+93 PP-28'

+83 T.P. 24'

+64 Ent.

15"x 20' C.M.-21

Cultivated

+35-8" Pop 19

+11 Twin 6" Pop-20'

Cultivated

+83-TP 24'

+65-T.P. 25

+41-H Pole-23-29

L 13'

Roos

Rt 14

13

15'

12

12

14

14

11

14

13

10

14

13

9

13

15'

8

13

14

7 24' 409 - 24" x 50' Conc. X Drain

14

14

26'

Fe. 34'

Oil tanks

Woven Wire

+28-24" O.-103' X
+27 Fe Cor. 34' X Woven Wire
+2 L.P. - 49'
Fe. 33'

+16 H. Pole - 19-25'

+77 PP - 28'

Fe. 27

+58 T.P. 22'

Fe. 26'

Cultivated

+72 P.P. - 28'

This Fe. gone 22-5-92

+60 T.P. 23

Fe. 24

Cultivated

+50 Fe. - 27'

+30 T.P. 23'

Fe. 32

Single Strand B.W. Electric

+69 PP - 28

+45 Fe. Cor. - 36'

+26 Ent
12x20' C.M. - 20'

Cultivated

+91 T.P. 23'

Lt.
16

Road

Rt.
15

20

16

15

19

16

15

18

16

15

17

16

15

16

16

14

15

16

14

14

15

14

Fe. 34
+95 RP.-28

x E

+50 - T.P. 21'

Fe. 34

x

x

•

+24 T.P. 21'

Fe. 34

x

+89 RP.-28

x

•

+30 T.P. 21'

Fe. 34

x

x

Cultivated

Fe. 34

x

•

+11 T.P. 21'

+85 RP.-28

Oil Tank Form

+88 Field Ent.

x

Fe. 34

x

•

+81 T.P. 22'

x

Fe. 34

x

+81 RP.-28

•

+51 T.P. 21'

x

Fe. 34

x

15

13

27

13

10

+97 Vent Pipe 23'
 +97 P.P. 26'
 +89 P.P. 26'
 +85 T.P. 20'
 +86 Rye h'd Fe.
 13'

11

+36 RR xs $\frac{1}{2}$

26

11

10

+49 End Rad. - 20'
 18' +
 +43 Rad. 37'
 +31 $\frac{1}{2}$ Pav. 20'
 +28 Range 1st Pav. 20'
 +23 End Rad. 34'
 +52 $\frac{1}{2}$ RR xs $\frac{1}{2}$
 +15 End Rad. - 29'
 +07 Conc. Wa. 11-62'
 +04 Vent Pipe - 62'
 15'

14'

25

13

24

14

13

23

13

12

22

15

14

21

16

15

+97 12" Elm 32'

+49 12" Elm 32'
+48 PP 16'

+20 Ent.
+06 RR X Sign 15'
+90 G.P. 34'
+89 Cross Fe. 37'

Cultivated

H. Tension
Transmission
Wire

H. Tension
Trans. Line

Plank

+18 PP 19'

+91 G.P. - 43

+73 RR Cross Sign 14'

+44 Rod 38'
+18 Rod 33'
+04 PP 20'
+02 Fe. Cor. 34'
+97 Rqc Tie Fe.

Ent. to Oil Co.

+70 T.P. - 35'

+12 gate Valve - 50' X
Fe 34'

+62 RR - 22
Fe 34'

Farm
Tank
Oil

Fe. 34'

Fe. 34'

Fe. 24'
+91 Vent. box - 58'
+88 Vent. box 65'
2' x 3.5'

+28 PP 28'
+21 PP 27'
+08 PP 25'
Fe. 24'
+81 Fe Cor. 24'
+72 Vent. Pipe 22'
+71 G.P. 36'

Pasture

+20 RR Cross Sign 18'

+80 T.P. 20'

+35 RR Cross Sign 13'

+00 G.P. 20'

+63 T.P. 20'

+31 RR Sign 13'
+24 T.P. 20'

Cultivated

+89 T.P. 21'

17

14

34

19

15

33

15

15

32

+94.16" O. 34 15

13

31

13

15

30

+15-20" B.E. -84'

13

+87.12" B.E. -99'

+87.56" B.E. -82'

+84.20" B.E. -54'

+64.3" Pinc -63'

+55.54" B.E. -73'

+40.15" B.E. -102'

+19.8" Oak -85'

13

+09-20" Elm -100'
 +09-20" Elm 84'
 +08-20" Elm 68'

X +61-15 B.E. -89'

29

15

14

28

15

13

Fe. 24
+95 P.P. 24

Fe. (13) 28

+67 T.P. 27

Fe. 36

Fe. 27

+21- P.P. 22

Fe. 35

+38- T.P. 25

Fe. 26

+50 Beg. Cult.

+34-24 Oak 32

Fe. 35

+93 X Fe. 35

+67 P.P. 21

+55 Ent

12" x 20" C.M. 21

+33 X Fe. 25-35

+31 15" B.E. 34

+15 15" B.E. 34

+00 Fe. 24

+00 15" B.E. 34

+83 15" B.E. 34

+18- T.P. 24

Fe. 25

Uncultivated

Fe. 26

+79 T.P. 24

Live Stock Yard

+36 24" B.E. 34

+20 15" B.E. 39

+12 Fe. Cor. 25

+11 P.P. 20

+94 Ent

15" x 22" C.M. 21

+78 End Hedge 33

+61 12" B.E. 40

+50 Beg Hedge 31

+32 20" B.E. 35

+17 15" B.E. 34

+05 P.P. 20

+99 15" B.E. 35

+83 15" B.E. 35

+70 Beg 34

+69 15" B.E. 35

+55 15" B.E. 35

+37 15" B.E. 34

+07 15" B.E. 33

+13- T.P. 28

Fe. 25

X +94 Ent. 15" x 16" C.M. 21

X +78-15" Elm-84

X +77-15" Elm-52

+64 Stump 37

+53 T.P. 21

+48 6" Fir 40

+32 Stump 36

Fe. 25

+91 Fruit Tree 41

X +74 6" apple Tr.-56

+38 T.P. 21

Fe. 24

Yard

	15	15
41	16	16
40	16	15
39	17	13
38	17	14
37	18	14
		+ 06-6" apple Tr. - 59' + 90.6" apple Tr. 61' + 89.4" apple Tr. 76' + 68-12" B.E. - 67' + 43.2-10" B.E. 53'-65'
36	16	+ 18 N.W. Cor 1 1/2" S.F. House. 14'  92' out
		+ 91.8" P.M. - 72" + 88 hedge - 91"
35	17	14

Fe 37

+36 P.P. 27

Fe. 37

+87 Stump 35

+23 12" Oak 34

+19 P.P. 27

Fe. 37

+38 Stump 34

Fe. 37

+91 Stump 36

+38 P.P. 26

+29 12" Oak 34

+03 Stump 35

Fe. 37

+50 15" Oak 34

+33 15" Oak 35

+22 15" Oak 35

Fe. 37

+74 8" Oak 35

+63 8" Oak 35

+53 P.P. 26

Fe. 36

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

x x

Fe (14) 29

+14 T.P. 28

Fe. 29

Fe. 29

+86 T.P. 29

Fe. 29

+52 H.P. 26-31

Fe. 29

+88 T.P. 28

+23 T.P. 28

+12 Fe. Cor. 29

+59 Ent. 20

15" x 20" C.M.

+14 Stubs-79'

+06-6" 45h-83'

+04-6" 45h-57'

+94 T.P. 28

+87 Fe. Cor. 29

+41 P.P. 35

Fe. 28

Cultivated

Cultivated

Yard

15

13

48

14

13

27

+ 52-24" x 50' Conc. X Drain

23

47

15

12

46

15

13

45

14

13

44

15

15

43

14

16

42

15

15

Fe

30

Fe

(15)

23

Fe.

33

Uncultivated
Swamp

+46- P.P.

26

Fe

34

Fe

34

+100 End Cult

+66 P.P.

26

Fe

34

Fe.

36

+80- P.P.

27

+78- 12 Oak

36

Fe.

37

+52 P.P.

27

Fe.

37

143 T.P.

24

Fe

24

+123- ^{T.P.} H.Pole - 22-28

Fe

24

144- T.P.

26

+43 X Fe.

26

+100- T.P.

26

Fe.

26

Fe.

26

+82- T.P.

26

Fe

26

+61- T.P.

27

Fe.

27

+42 T.P.

28

Fe.

29

21

13

46

+63-12" x 68" C.M. X Drain

28'

+24 StP - 46' X

+08 15" O 50'

55

+95-StP-24-66'
 +93 15" O - 56'
 +84 15" O - 63' - 76'
 +69 StP - 78 - 52'
 +66 StP - 83'
 +63 12" O - 71'
 +53 - 15" O - 61' X
 +41 - StP - 88'
 +27 - 15" O - 89'

13 Brush - 30' - 80'

X

54

20

15

32'

+46-12" x 58" C.M. X Drain

26

53

+80 beg Brush - 31' - 80'

X

+74 g.p. - 76'

+

52

14

13

51

15

14

+20 N.W. cor. 1.5. Stue. House



50

15

13

49

15

13

Fe. 40
+228" Oak 46
+21 Stump 39

Fe. 39
+98" P.P. 28

Fe. 38

+53 End Rad. 18
+53 Fe. Cor. 39
+42 P.P. 27

+118 Beg. Rad. 50

+84 End Rad. 46
+74 P.P. 24
+71 Stump 27
+69 Fe Cor. 39
+65 Beg. Rad. 17'

+16" 8" Oak 42
Fe 39

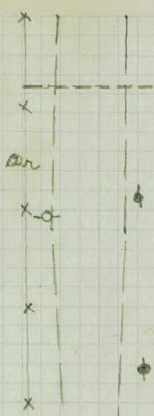
+12 P.P. 25
Fe 29

+50 End Swamp 30

Fe 28

+32 P.P. 25

Fe 30
+00 Beg Swamp 30



CLEVELAND AVE.

Uncultivated

Swamp

Uncultivated

Uncultivated

+08 T.P. 20
R.P. 16.5.3

+19 T.P. 22.1

+72 End Pot Hole 19'

+52 End Rad. 8
+32 Beg Pot Hole 24' 60"
+34 T.P. 23

+21 Beg. Rad. 42

+02.60 R.R. 304.62

+84 End Rad. 45
+77 P.P. 37
+66 End 4
+54 Beg. Rad. 12

+38 End Fe. 23

+05 T.P. 22
Fe 24

? cul. buried. +93-Ent. X

+72 Cross Fe 23

+80 15" O.-65'
+73-12" O.-66'
+52 6" E/M-73'
+23 End 4" Tile drain 34'

Fe 24

+85 T.P. 23

+73-Row 3" Trs (12)

Fe 25

+80 beg. Row 3" P.P. Trs. 49'
+64 T.P. 23
+61 End. Row 3" P.P. Trs.
6 Trees 46
6 Spgs 1

Fe 23

12

12

62

17

11X End brush - 30'-51'

+ 50 Trees + Brush 35'-76'

61

19

17

V + 50 Trees + Brush - 38'-100'

60

19

15

59

21

13 End brush 35'-45'

58

25

X 9 Brush 32'-60'

57

22

X 12 Brush - 28'-50'

+ 54 6" Trees - 54'
 + 22 Tapir 10" O - 87' X
 + 18 12" O - 25'
 + 12 12" O - 51'

56

21

V 13 Brush 28'-60'

+85 4" P.P. 12
 +82 3" P.P. 39
 +78 4" P.P. 46
 +62 P.P. 25
 +51 8" O. - 40'
 +49 Twin 4" O. 39
 +37 15" O. 41
 +16 12" Oak 41

Uncultivated

RR 83.3
 +93 T.P. 35

+36 3" Oak 36.38.43
 +33 4" Oak 37
 +14 4" Oak 39
 +08 P.P. 24
 +00 6" Oak 50
 +95 4" Oak 38
 +93 3" Oak 37
 +90 4" Twin 43
 +78 Stump 36
 +58 4" Oak 38
 +50 End Cult.

+52 T.P. 23

R.R. 84.3

+07 T.P. 25

+55 P.P. 30

R.R. 97.3
 +99 T.P. 20

+04 T.P. 29

+67 Ent.
 15" x 20" C.M. 32

+47 T.P. - 18

R.R. 126.3

+54 Fe. Cor 41
 +51 P.P. 28

+38 T.P. 17

Fe. 40

Uncultivated

Uncultivated

11

15

69

9

14

13' + 65' 21" x 32' C.M. 1 Drain 19'

68

10

13

67

12

16

66

13

13

L+ T 25 Fe. Cor - 29'

65

13

16

64

13

12

+ 58 Fe. Cor - 30'

L+ 10' x 29' C.M. - 25

63

12

12

L+ 10' x 20' O - 47'

+68 End Pothole 70'
 +58 T.P. 29
 +50 Pothole 32'-70'

RR 87.3
 +00 Pothole 27'-70'

+77 R.R. Cul. - 60
 Dist. 24' 30" x 39" Conc.
 RR 86.3
 +50 Pothole 26'-70'

+00 Beg Pothole 35'
 RR 85.3

+74 T.P. 28

RR 84.3

+64 T.P. 28
 +50 RR 84.3

+30 End Pothole 22'-35'
 R.R. - 84.3
 +00 Pothole 25'-50'

+50 Pothole 22'-62'
 +38 T.P. 27

R.R. 84.3
 +00 Pothole 23'-62'

+00 Pothole 23'-62'

+14 T.P. - 26
 +00 Pothole 25'-62'

+50 Pothole 23'-62'

+20 Beg Pothole 37'
 RR 83.3

+00 End Pothole 17'-31'
 +92 P.P. 25

+67 Swp 140
 Pitch outlet
 +50 Swp 17

+00 Swp 19'-140'

+60 Beg Pothole 25'-140'
 +32 P.P. 26

+30 Beg Cult.

+00 End Pothole 20

+75 P.P. - 26

+50 Pothole 20'-100'

+00 Pothole 17'-60'

+30 Beg Pothole 18'

+16 R.P. 26

+97 Field Ent

+78 End Pothole 18'-46'

+00 Beg Pothole 18'-46'

Cultivated

Pothole

Pothole

Uncultivated

Pothole

Pothole

Pothole

12

12

76

13

15

4 1/2 x Drain

29'

10" x 56' CM.

27'

75

16

14

74

14

13

73

13

14

72

15

13

71

12

15

70

11

15

+35 End Pot Hole 35-130
 129 R.P. 25

Pot Hole - 30-150

+85 R.P. 26

Pot Hole

+50 Beg Pot Hole 35-125
 +40 R.P. 23

+97 R.P. 24
 +96 G.P. 16

Cultivated

+47 R.P. - 24

R.R. 81.3 (19)

173 T.P. - 29

150 R.R. 79.3

R.R. 80.3

+53 T.P. - 26
 +50 R.R. 80.3

R.R. 81.3
 +00 End Pothole 27-41

+75 Pothole 27-45

+50 R.R. 81.3
 +40 Beg Pothole 26
 +34 T.P. - 25

R.R. 86.3

+50 R.R. 84.3

+15 End Pothole 15-30
 +04 T.P. 22
 R.R. 86.3
 +00 Pothole 22-72

+50 R.R. 87.3
 +50 Pothole 50-74

+00 Pothole 50-73
 R.R. 88.3

+96 T.P. 17

+50 R.R. - 89.3
 +50 Pothole 55-78

+11 Beg Pothole 61-73
 R.R. 87.3
 +99 T.P. 23

+50 R.R. 89.3

R.R. 88.3

Uncultivated

Pothole

Pothole

14

13

83

13

13

44

+41-24" x 76" C.M. X Drain

32

82

13

13

81

13

13

80

+62 Edge Bv. x 2 $\frac{1}{2}$
 +42 Edge Bv. x 5 $\frac{1}{2}$

79

13 Rod Pl.

14

Rod Pl.

78

14

15

77

12

12

100. T. P. 29 20

+ 58 Δ Ditch 44
+ 49 Fe. Cor. 42*

Ditch 44'

R.R. 81.3

+ 61 T.P. 27

Uncultivated

Cultivated

+ 57 R.R. Culm. - 60
Oval Conc. 3.3' x 3.0' x 5'

+ 26 T.P. 27

R.R. 88.3

+ 09 End Rod 14
+ 84 G.P. 38
+ 83 G.P. 41
+ 70 Beg Rod 57

+ 09 End Rod 12
+ 93 T.P. 27

+ 70 Beg Rod 47

+ 37 End Rod 45'
+ 32 P.P. 36

NEW BRIGHTON ROAD
20' Pavement

+ 51.75 R.R. 84.50
+ 37 End Rod 48
+ 27 P.P. 46
+ 23 T.P. 31

R.R. 86.3

+ 50 R.R. 85.3

R.R. 84.3
+ 00 T.P. - 32

Uncultivated

+ 74 P.P. 28

Cultivated

+ 50 R.R. 83.3

R.R. 81.3

12

13

U +82-20"0-83'

90

13

13

89

14

14

88

15

+44-2-10"0-57'
 +39-12"0-89'
 24+ +32-20"0-82'
 +19-2-12"0-93'-103'
 14

87

15

+55-15"0-85'
 +45-2-8"0-65'
 45+ +30-3-10"0-71'
 +27-6"0-67'
 +25-6"0-78'
 +10-15"0-93'
 13

86

16

12'

85

16'

14'

84

14

13

Fe 32

x

R.R. 82.3

(2)

Fe 33

x

189 T.P. 28

Fe 33

x

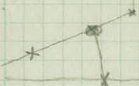
R.R. 82.3

172 T.P. - 29

Fe 33

x

+49 Rgc. Tie. Fe.
 +36 Δ Fe. 33
 +27 Fe. Cor. 53
 +27-12.0ch. 5p
 Fe. 48
 +100 End Cult.



Uncultivated

159 T.P. 28

R.R. 83.3

135 H.P. 25-30

Fe 45

x

Cultivated

139 T.P. 27

Fe 41

x

R.R. 81.3

Fe 42

x

12

11

97

11

11

96

13

11

95

13

11

94

13

+29-24" O.-103'
 +28-12" O.-64'
 +15-10" O.-35'
 +03-20" O.-90'

11

+83-15" O.-85'
 +76-15" O.-85'
 +75-12" O.-66'
 +71-15" O.-98'
 +64-10" O.-105'
 +47-15" O.-53'
 +37-15" O.-70'
 +20-15" O.-65'
 +13-2-12" O 90-95'

13

93

14

+95-15" O. 95'
 +35-20" O.-52'
 +10-10" O.-88'

13

92

14

+83-18" O.-100'
 +75-18" O.-75'
 +57-18" O.-102'
 +54-10" O. 78'
 +46-20" 74'
 +30-12" O 61'
 +18-10" O.-66'
 +12 51p-80'

13

91

12

Fe.

31

+51' X Fe. - 31

+38 T.P. 29

Fe.

31

R.R. 84.3

Fe.

31

Pasture

+05 T.P. 29

Fe

31

R.R. 83.3

+13-6" W.D. 35

Fe. 31

+00 8" O. 63

+93-24" O. - 55

Uncultivated

+78-7 P. 29

⊙

x

x

+48 H Pole - 27-31

Fe.

31

Pasture

R.R. 83.3

x

x

+26-2 Stump 37-44

+29 T.P. 29

Fe.

31

x

x

+25 Stump 35

Fe

32

R.R. 84.3

x

12'

9

17'
10413 + 16-24' x 32' Conc (12' South End
C.M. (20' x Drain
11

15'

103

13

11

102

13

13

101

12

+ 1/6 End row 4" Trs. - 73'
+ 1/6 End row 9" Trs. - 65'
+ 1/6 End row 2" Trs. - 88'
11

100

13

11

99

12

11

98

12

11

Fe 2
+80 48" Stump 14'

Fe 21

Fe 21

+10 AFe 21

+99 Fe. Con- 35

+89 Ent
12" x 32' C.M. 22

+35 Fe. Con- 32

Fe 32

+95 X Fe. 32

Fe 32

Fe 31

Fe 31

Cultivated

Pasture



2000

+70 Beg. Co. R. 9'

+38 T.P. 34

+70 T.P. 32

R.R. 85.3

+42 T.P. 31

+16 T.P. 31
R.R. 85.3

+85 H P.C. 283

R.R. 84.3

+63 T.P. 29

Uncultivated

12

11

111

11

11

110

11

11

109

12

12

108

12

15

107

12

15

?

149- 15" x ? (Buried) G.M.

20'

+89° E.R. - 8640

106

105

12

9

CR - 70.3 - 84.3
 Fe - 35 (24)

+48 T.P. - 31

+100 Bq. Fe. - 35

+21 T.P. - 31

R.R. - 72.3 - 84.3

+30 Ph. Frog 80.3 - 85.3

+103 T.P. 31

+151 Ph. Switch. 85.3

+21 T.P. 31

+14 End Burr 37

R.R. 85.3

+53 Bq. Burr. 37

+37 T.P. 33

+62 H.Pole - 29 - 36

+48 End Rod - 13

+108 Bq. Rod 45

+89 Culv. - 50

24" x 82' Conc.

+173 End Rod - 40

+36 R.R. Culv. - 63

Oval Conc. 24" x 30" x 48"

+135 End G.R. 9

+134 Bq. Rod 9

+05 T.P. 34

+47 Stump 28

+30 Stump 27

+16 Stump - 27

+61 Groups 2" - 21

+81 Stump 25

+74 Stump 24

+69 Stump 25

+61 P.P. 25

+60 2" Oak 25

+48 Stump 22

+41 2" Oak 22

+66 End Rod 13

+52 P.P. 26

+108 Bq. Rod - 53

+75 End Rod - 32

+65 A.Fc. 41

+45 Fe. Cor 23

+45 Bq. Rod. 14

Fe 22

Cultivated

Spur
Main Line

Uncultivated

Barricade

SNELLING AVE

Plant G.R.

14

11

118

12

13

117

10

11

116

10

11

115

11

10

114

12

10

113

13

10

112

12

11

+100 X Fe. 29
+100 - 2' 2" Oak 22 x

23

+50 - 2' Oak 20

R.R. 67.3 - 81.3
+97 T.P. - 27

Cultivated

Cultivated

+68 T.P. 28

R.R. 68.3 - 82.3

+38 T.P. 28

+107 - 2' Oak - 18

+41 - 2' Oak 29
+31 - 2' Oak 20

+53 End Fe 34

+106 Stamp 21

+10 T.P. 29
R.R. 69.3 - 83.3
+100 Fe. 35

+41 T.P. 29

Fe. 34

+176 H Pole - 27-31

R.R. 70.3 - 84.3
Fe. 35

14

11

125

14

10

124

13

8

123

15

9'

122

15

8

121

15

8

120

14

8

119

14

11

R.R. 86.3-100.3

(26)

+62 H Pole-43-48-

+50 End Fe 46
+43 T.P. 42

Fe 44
+100 R.R. 79.3-94.3

+112 T.P. -37
Fe 41

+76 Ent.

R.R. 73.3-87.3
+100 Fe 38
+84 T.P. 33

+103 Beg. Fe. 36

+58 T.P. 28

R.R. 87.3-92.3

+29 H Pole-25-29

Cultivated

Uncultivated

132

131

15

10

130

15

10

129

16

10

128

14

10

127

12

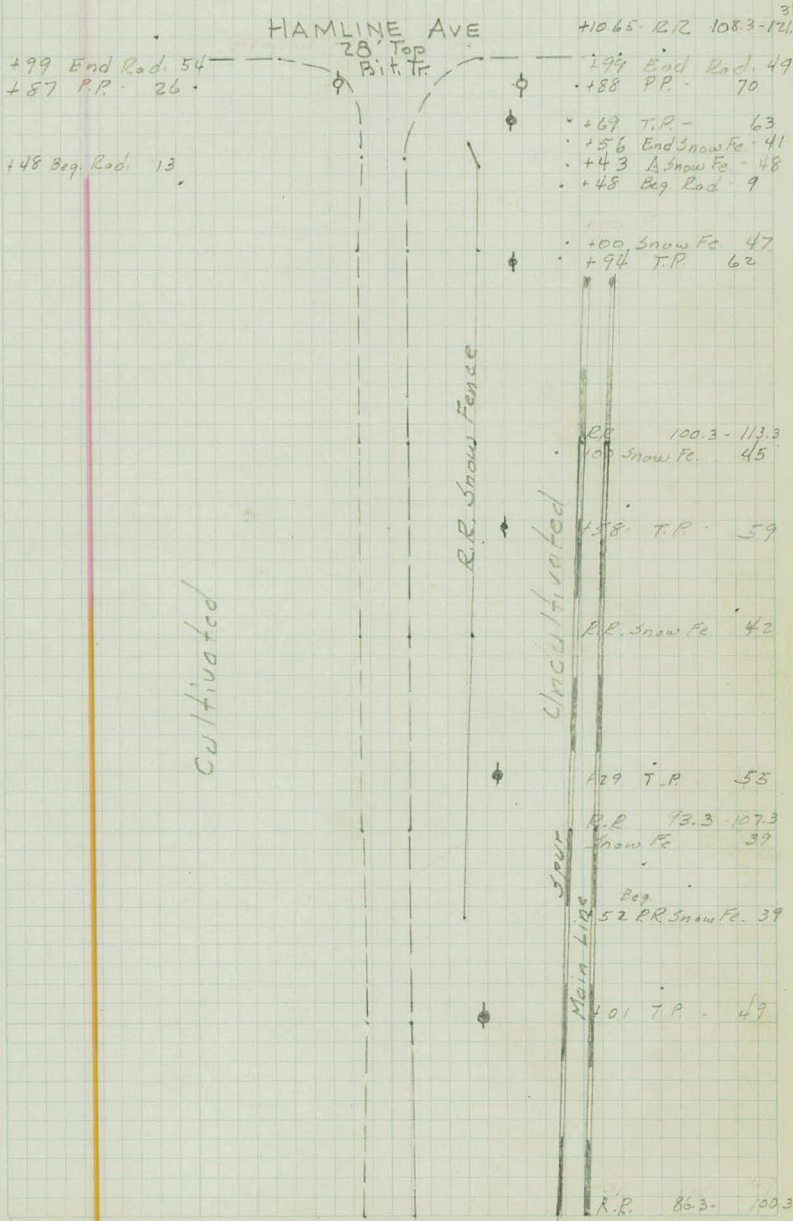
9

126

14

11

Continues 700' North



12

10

137

14

12

136

15

10

135

15

11

134

12

14

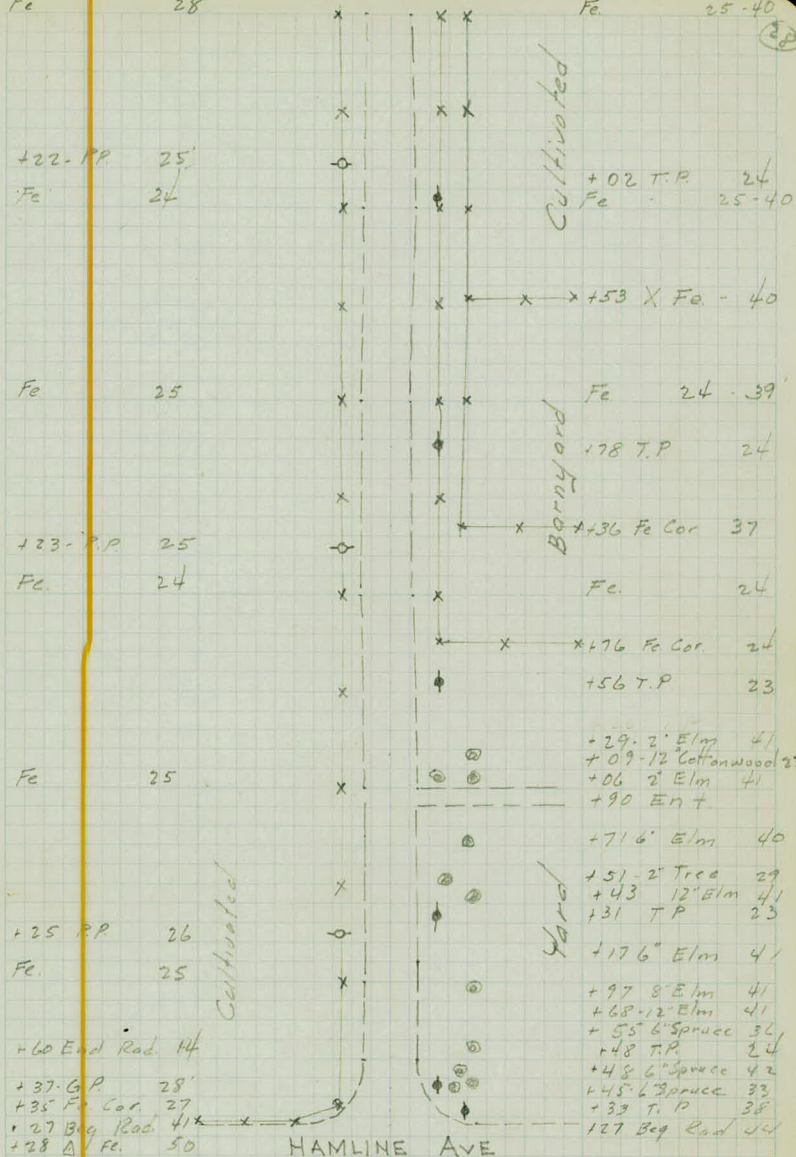
133

13

13

+60 End Rad- 13'

132



7

14

144

7

14

16

+55-24" x 42' C.M. X Drain

24

143

7

14

142

7

13

141

13

14

140

12

11

139

12

11

138

12

10

G.R. 21 8
Fe.

+50 Beg. Fe. 21

+30 End Swamp

G.R. 8
+00 Swamp 25-150

+24 P.P. 26

G.R. 8
Swamp 25-125

+36 15" Will. 18

+00 Beg. Swamp 26

G.R. 8

+86 Stump 13

+84 Beg. G.R. 9

+76 End. Fe. 33

+23 P.P. 26

Fe. 31

Fe. 25

+26 P.P. 25

+08 X Fe. 25

Fe. 25

Fe. 28

Fe 37 39
G.R. 15 (39)

+52 Fe. Cor. 39
+45 T.P. 26

G.R. 15

+33 T.P. 25

G.R. 15

+21 T.P. 25

G.R. 14

+75 G.R. & Fe. 14

+56 A Fe. 25

+14 Fe. Cor. 47
Fe. 26-43
+94 T.P. 26

Fe. 26-42

+67 T.P. 25

Fe. 26-41

+31 Hble 24-28

Fe. 25-40

Cult

Swamp

Cable G.R.

Cable G.R.

Uncultivated

Cultivated

Cultivated

10

13

151

10

12

150

11

13

149

10

13

148

8

14

147

7

13

146

7

13

145

7

14

Fe 21

Fe 22
+90 P.P. 29

+13 X Fe. 24
Fe. 24

Fe. 27
+99 P.P. 28

Fe 32

+29 End G.R. 8
+09 P.P. 27
G.R. 8
Fe 29

Cultivated

G.R. 8
Fe 29

+13 P.P. 26
G.R. 8
Fe 21

Fe 27 (30)

Fe 28
+95 T.P. 27

Fe 29

+59 T.P. 26

Fe. 28

+36 T.P. 27

Fe 27

Cultivated

+03 T.P. 27
+03 End G.R. 14
Fe 28
G.R. 14
+88 Fe. 29
+76 A Fe. 36

Fe. 36
G.R. 14

+78 H.Pole 23.3

Fe. 39
G.R. 15

+ 38.15 = 0+00

+ 19 Edge Pav't. x = 4

158

157

11

11

156

12

11

155

10

13

154

10

12

153

9

12

152

10

13

LEXINGTON AVE - 27' Pave.

+05 Apr Lt. Pale - 35

+17 End Rad. 35

+00 Beg Rad 14

+82-6" Oak 31

+75-6" O. Fe. 31

+57-A Fe. 24

+07 Stump 22

Fe. 23

+76-PP 33

Fe. 23

Fe 23

+73 PP 31

Fe 22

+85 Rge Tie Fe.

+83 Fe Cor. 23

Fe 22

+85 PP 30

Fe 21

+08 T.P. 25

+17 End Rad. 32

+00 Beg Rad 11

+66 End Gr.R. 12

+66-6" Oak 38

+46 T.P. 26

GR. 12

+22 Beg. Gr.R. 12

+15 T.P. 26

+09 Fe Cor. 26

+09 T.P. 22

+77 2" Elm 46

+76 2" Elm 36

+70 X Fe 29

Fe 28

+67 T.P. 27

Fe 27

+26 H B/o 25-29

Fe 27

Cultivated

Cultivated

164 22' 1'

163 21' 2'

26'	+ 83 x 12" x 42'	16'
27'	+ 82 x 15" x 44' CM	17'

162 19' 4'

161 18' 4'

160 17' 5'

159 15' 5'

158

+93 End G.Rail 158'
+90 End Rad. 50'

G. Rail 00 32
+91 K.Fc 5'

+69 Beg G. Rail Rad. 24'
+31 P.P. 31'
G. Rail 23'

+21 T.P. 7'
G. Rail 2'

+07 P.P. 31'
G. Rail 22'

+05 T.P. 8'
G. Rail 15'

G. Rail 20'

+50 End of
Auto. Graveyard

G. Rail 5'

+79 P.P. 31'

+89 T.P. 9'

G. Rail 19'

G. Rail 5'

+83 Beg G. Rail 19'

+65 T.P. 10'

+56 End Yard

+56 P.P. 32'

+56 End Grape Vines 32'

+39 Beg Grape Vines 36'

+49 Beg G. Rail 6'
+49 End Fc 10'

+93, 15" Elm. 26'

+75 24" Elm. 26'

+13 8" Tree 32'

+50 End Lilac Shrubs 31'

+28 Beg Lilac Shrubs 31'

+28 P.P. 31'

+16 6" Tree 25'

+94 12" x 4 CM. 17'

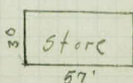
+90 E. Rad. 15'

+46 B. Rad. 57'

Auto. Graveyard.

+01 Beg Fc. 12'

+75 Ent
+47 T.P. 11'



+34 Cor Bldg 42'
+04 Cor Bldg 43'
+04 Inn Sign 26'



+84 G. Ramp 32.5
+84 E. Rad. 9'
+46 Beg Rad. 39'

Lexington

27' Park Ave

748 Lot Iron 33'

171

23' 4'

+66 End Yard.

+60 2" Pine 11'

+33 Cor Ho 56'

170

26' 6'

169

25' 3'

168

22' 2'

+80 4" Pine 42'+50'

+74 4" Pine 47'

167

23' 2'

166

23' 2'

165

+81 P.P. 31'

+41 G Pole 31'
+36 Ent

+55 P.P. 31

+32 P.P. 32'

+05 P.P. 32
+04 V Bow Trees & Endyard 42'

+96 Ent 15' x 20' CM. 29'

+41 6" Tree 42' Begyard

+81 P.P. 31'

+94 Fc Cor. 33'
+67 End G. Rail 1'
+57 P.P. 32'+29 End Rad 25'
+25 Fc Cor. 34'
+15 Beg Rad 43'
+04 Rd 16' x 36' CM. 35'

Plat Roll

Cultivated

Cultivated

Yard

Cultivated

+45 T.P. 4'

+60 6" Elm. 34'

+40 8" Elm. 34'

+37 2" Walk 50'

+35 2" 4' Walk 37'

+20 T.P. 1'

+20 6" Elm. 34'

+17 2" 4' Walk 24'

+03 Ent

+95 P.P. 14'

+74 2" Elm. 36'

+24 2" Elm. 36'

+95 T.P. 2'

+76 2" Tree 36'

+21 2" Tree 36'

+72 2" Elm. 36'

+70 T.P. 3'

+23 2" Elm. 36'

+97 Stump 10'

+75 Stump 11' 2" Tree 36'

+56 T.P. 4'

+23 2" Tree 36'

+72 2" Tree 36'

+45 T.P. 4'

178

+97 G-Rail Vio
+93 Edge Rail
+60 End Rail 69'
+50 Rail 40'
+25 Rail 16'

+42 End Rail 77
+25 Rail 36'

177

Trees 15'

8 Plum

+90 Beg Clump Fruit/Trees 20'

176

2

25'

+98 3" Tree 21'
+95 3" Tree 33'
+86 Twin Oak 19'

175

4

19'

+91 Ent 15" X 30 CM 9'
+91 End Pines 35'
+65 Bush 22'
+65 Beg Pines 33'

174

8'

13'

173

15'

8'

172

20'

2'

+37 End Culvert 35'

15" x 102" CM

+35 End Culvert 35'

+28 Fc 34'

+25 Fc 28'

+23 Ry Tie Fc

+00 Beg Rad 4'

Fc 15'

+85 AP 13

+81 2" Plum 24'-34'

+65 2" Apple 22'-32'-42'

+54 Pine 34'

+46 Pine 25'

+39 Pine 22'

+22 6" Apple 27'

+00 Beg Fc 19'

+65 Stump 23'

+68 2-3 Pines 23-28'

+58 P.P. 17'

+34 Tree 21'

+26 Pine 28'

+23 Tree 18'

+14 Pine 25'

+08 3-3" Pines 25-32-38'

+63 Pine 30'

+62 Pine 34'

+59 Pine 29'

+52 Pop 16'

+50 Pines 30-39'

+40 Row Birch 32'

+33 P.P. 22'

+31 Tree 17'

+31 End Cult. Beg Yard

+05 T.P. 30'

+00 Beg Rad. 25'

+31 T.P. 30'

+16 T.P. 30'

+11 T.P. 29'

+65 T.P. 14'

Orchard

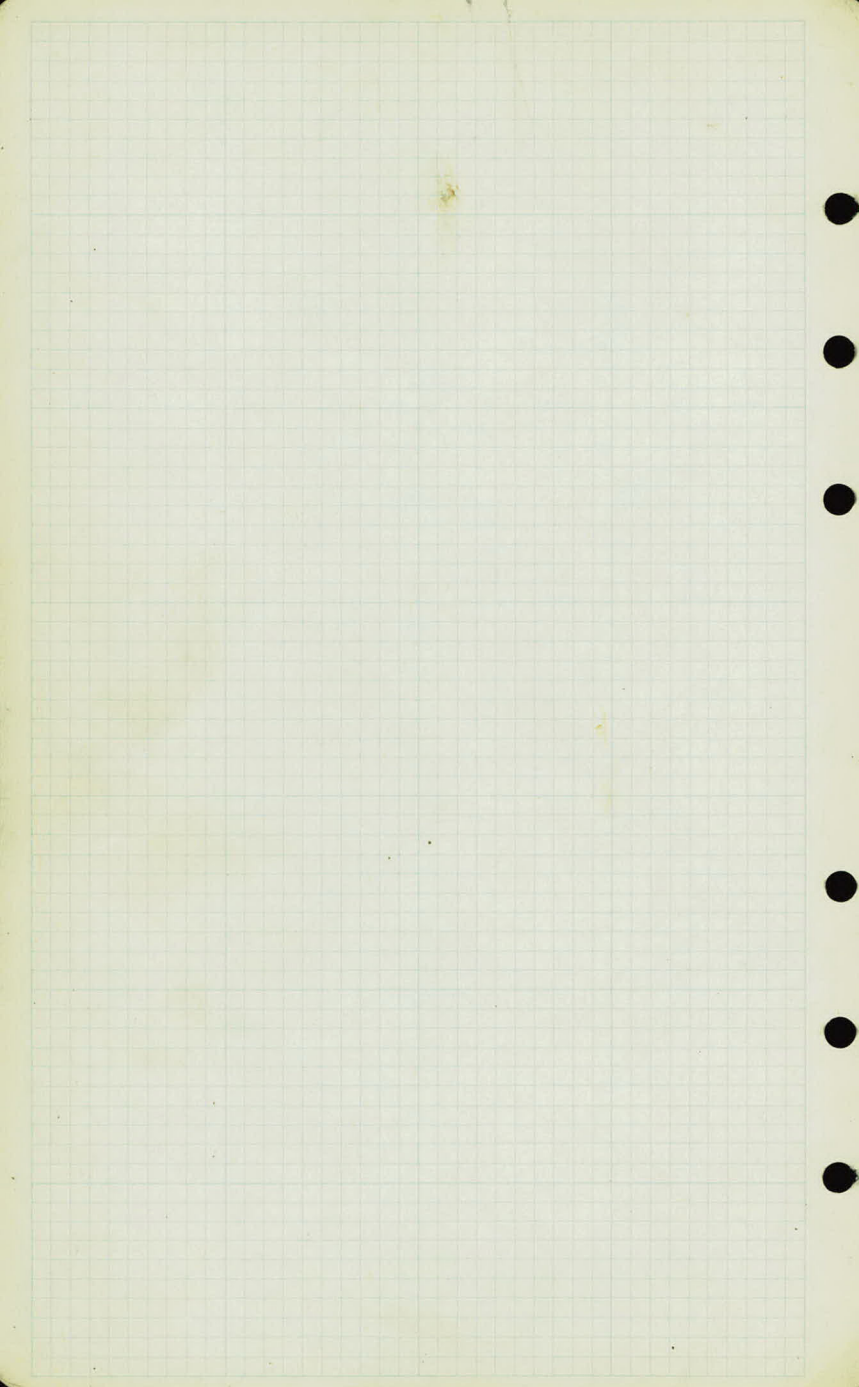
Scattered
Trees

Scattered
Trees

Cultivated

Cultivated

+06 P.P. 27'



Bench Levels

Co. Rd. C"
S.T.H. # 8 to Snelling Ave.

Sta	+	Σ	-	Elev
B.M.	2.14	951.35.		949.21
T.P.	2.67	942.87.	11.15	940.20.
T.P.	8.54	946.91.	4.50	938.37.
B.M.			2.58	944.33.

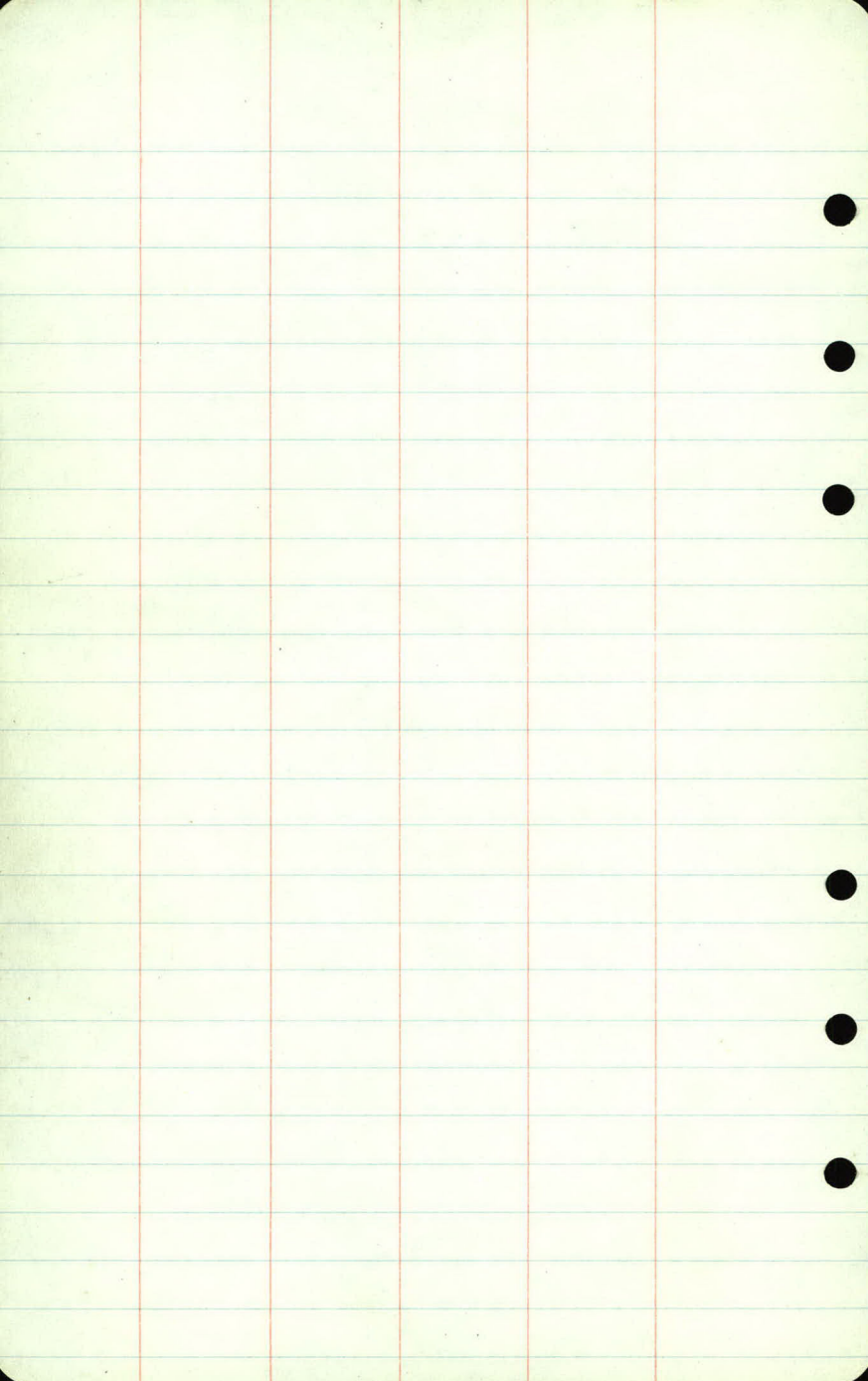
Lt.

2

R+

Top from Mon 0+00 W.Co. Line

SPK. in 20" Oak 50' Lt. Sta 1+00



Co. Rd. "C"

Bench Levels

Pt.	+	π	-	Elev.
B.M.	2.43	941.50.		939.07.
	2.45	934.31.	9.64	931.86.
	0.90	922.76.	12.45	924.86.
	0.18	910.91.	12.03	910.73.
B.M.	13.62	918.59.	5.94	904.97.
	9.19	927.29.	0.49	918.10.
B.M.	6.58	929.79.	4.08	923.21.
B.M.	7.00	934.19.	2.60	927.19.
	3.18	931.42.	5.95	928.24.
	2.11	927.19.	6.34	925.08.
	4.38	923.49.	8.08	919.11.
B.M.	4.26	920.14.	7.61	915.88.
	5.90	921.50.	4.54	915.60.
	11.72	932.18.	1.04	920.46.
	1.66	933.10.	0.74	931.44.
	1.67	925.17.	9.60	923.50.
B.M.	3.44	928.19.	0.42	924.75.
	6.60	930.51.	4.28	923.91.
	5.25	931.14.	4.62	925.89.
B.M.	6.51	934.45.	3.20	927.94.
	0.51	924.46.	10.50	923.95.
B.M.	1.78	916.83.	9.41	915.05.
	4.08	910.48.	10.43	906.40.
	7.63	917.06.	1.05	909.43.
	12.06	929.06.	0.06	917.00.

6/18/40

Spike in 15" Oak N.W. Cor. Co. Rd "C" & Lex.

Spike T.P. 25' Rt 142 + 21

Spike G.P. 28' Lt. 132 + 37 - N.E. Cor "C" & Hamline

Top Mon 132 + 10.65 - $5\frac{1}{4}$ Cor Sec 3 - Rose -

Spike H Pole S.E. Cor "C" and Snelling - 29' Rt 106 + 62

Spike P.P. N.W. Cor "C" & H.B. Rd. - 36' Lt. 79 + 33

Spike P.P. 26' Lt. Sta 64 + 16

Top Mon Cleveland & "C"

+	⌵	-	Elev.
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	929.06		
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8.50	937.09	0.47	928.59
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B.M.	10.52	945.78	1.83	935.26
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10.22	953.77	0.23	945.55
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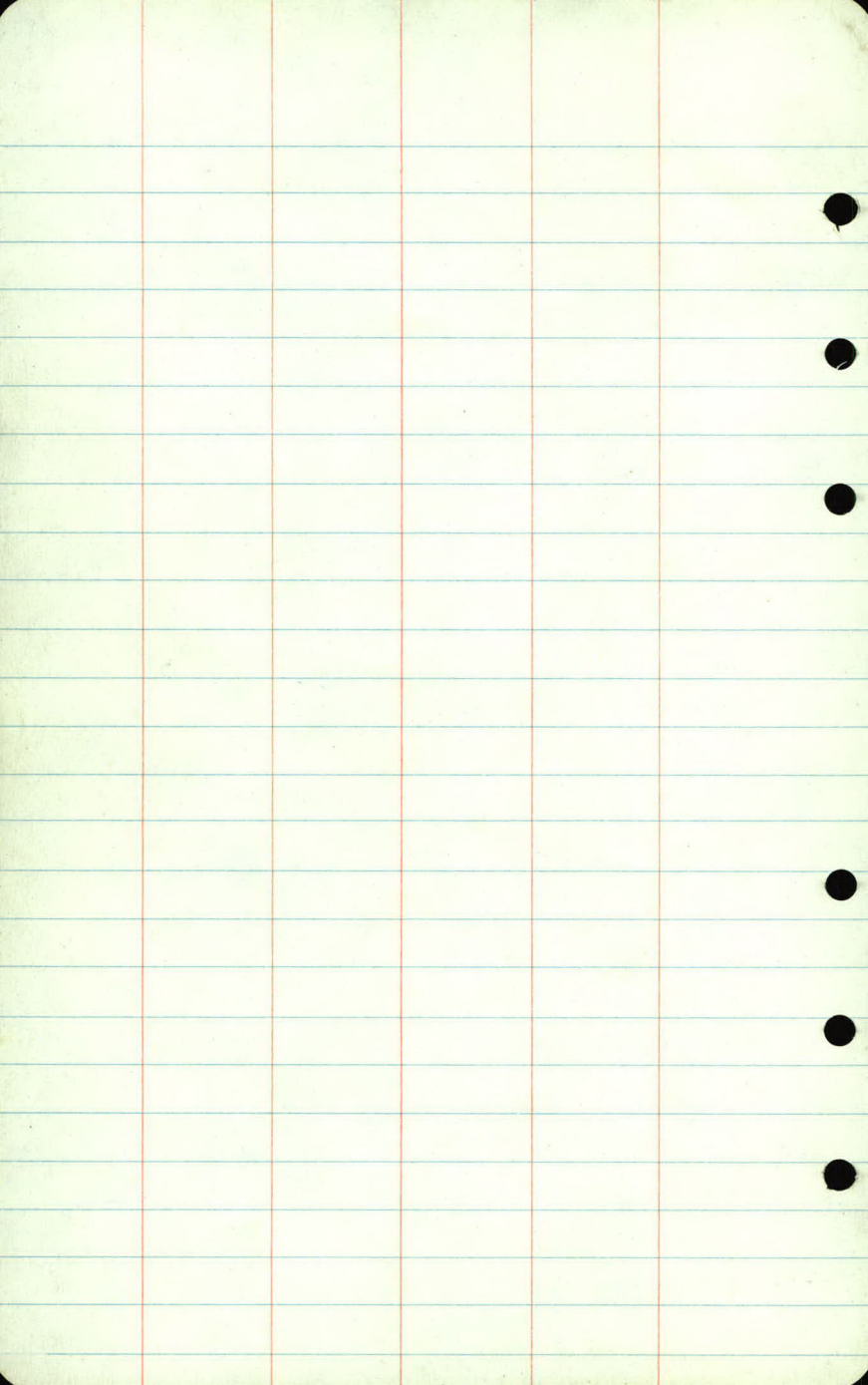
2.39	957.49	0.67	955.10
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5.16	953.15	9.50	947.99
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B.M.		3.94	949.21
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Top Mon. 26+52.28

Top Mon. 0+00 (Iron



Co. Rd. C.

W Co. Line to Lexington

sta	+	π	-	Elev
B.M.	4.78	953.99		949.21
0+00			4.8	49.2
+50			4.2	49.8
1			4.6	49.4
+50			4.7	49.3
2			4.9	49.1
+50			5.0	49.0
3			5.0	49.0
+50			5.1	48.9
4			4.9	49.1
+50			4.8	49.2
5			4.7	49.3
+60			4.8	49.2

Top Mon.

0+00 (Iron)

<u>4.5</u>	<u>4.7</u>	<u>6.0</u>	<u>5.4</u>		<u>4.8</u>	<u>5.2</u>	<u>6.2</u>	<u>3.8</u>	<u>3.2</u>	<u>3.2</u>
50	23	18-16	14	48	8	17	19-21	24	32	50

<u>5.5</u>	<u>5.0</u>	<u>5.0</u>	<u>5.3</u>	<u>4.9</u>		<u>4.2</u>	<u>4.6</u>	<u>4.9</u>	<u>2.5</u>	<u>2.9</u>	<u>2.3</u>
50	33	26	18-16	15	42	7	18	21-23	26	36	50

<u>5.1</u>	<u>5.5</u>	<u>5.9</u>	<u>5.9</u>	<u>4.8</u>		<u>4.9</u>	<u>5.5</u>	<u>2.8</u>	<u>3.5</u>	<u>2.9</u>
50	24	21	16	13	46	17	20-23	27	34	50

<u>6.2</u>	<u>6.1</u>	<u>6.3</u>	<u>6.7</u>	<u>5.1</u>		<u>5.0</u>	<u>6.1</u>	<u>4.7</u>	<u>4.5</u>	<u>4.7</u>	<u>4.2</u>
50	27	21	19-16	13	47	18	22-24	26	30	37	50

<u>5.7</u>	<u>6.2</u>	<u>6.5</u>	<u>5.2</u>		<u>5.2</u>	<u>6.8</u>	<u>6.5</u>	<u>6.5</u>
50	23	19-16	13	49	17	20	25	50

<u>5.1</u>	<u>5.8</u>	<u>6.1</u>	<u>5.2</u>		<u>5.4</u>	<u>6.9</u>	<u>6.9</u>	<u>7.8</u>	<u>8.1</u>
50	22	18-16	13	50	16	21	26	35	50

<u>5.9</u>	<u>6.2</u>	<u>6.7</u>	<u>5.5</u>		<u>5.3</u>	<u>7.3</u>	<u>8.0</u>	<u>8.5</u>	<u>8.9</u>
50	32	16	14	50	17	21	30	36	50

<u>6.4</u>	<u>6.2</u>	<u>6.9</u>	<u>5.7</u>		<u>5.4</u>	<u>6.5</u>	<u>6.1</u>	<u>6.1</u>
50	26	21-19	15	51	16	20-22	32	50

<u>5.2</u>	<u>4.8</u>	<u>5.7</u>	<u>6.4</u>	<u>5.1</u>		<u>5.2</u>	<u>6.1</u>	<u>4.6</u>	<u>4.2</u>	<u>4.9</u>	<u>5.0</u>
50	40	24	21-18	14	49	16	17-22	24	28	32	50

<u>5.5</u>	<u>5.8</u>	<u>5.8</u>	<u>6.1</u>	<u>5.0</u>		<u>5.0</u>	<u>6.4</u>	<u>5.0</u>	<u>5.6</u>	<u>5.6</u>
50	31	22	20-18	14	48	15	19-23	25	36	50

<u>5.0</u>	<u>5.7</u>	<u>5.7</u>	<u>5.0</u>		<u>5.0</u>	<u>6.8</u>	<u>6.9</u>	<u>5.6</u>	<u>5.9</u>	<u>5.7</u>
50	25	16	14	47	15	21-25	27	31	44	50

<u>3.2</u>	<u>4.4</u>	<u>5.7</u>	<u>4.9</u>		<u>5.0</u>	<u>6.8</u>	<u>7.2</u>	<u>6.4</u>	<u>1.1</u>	<u>1.6</u>
50	26	19	14	48	16	20	24	30	38	50

Sta.	L	π	-	Elev
		953.99.		
5+68			4.8	49.2
6			5.0	49.0
T.P.	4.58	952.99.	5.58	948.41.
+58			4.8	48.2
+70			5.0	48.0
7			5.3	47.7
L09	24"x50' Conc.		5.3	47.7
+50			5.3	47.7
8			5.3	47.7
+40			5.1	47.9
9			5.0	48.0
+50			5.1	47.9
10			5.1	47.9

$\frac{2.8}{50} \quad \frac{2.4}{39} \quad \frac{2.1}{29} \quad \frac{5.1}{24} \quad \frac{6.1}{21.7} \quad \frac{4.9}{14} \quad \frac{5.1}{15} \quad \frac{7.2}{21.26} \quad \frac{6.4}{31} \quad \frac{1.4}{37} \quad \frac{2.0}{50}$

$\frac{3.9}{50}$	$\frac{3.2}{36}$	$\frac{3.0}{28}$	$\frac{6.5}{23}$	$\frac{6.2}{17}$	$\frac{5.1}{14}$	$\frac{5.3}{50}$	$\frac{7.5}{14}$	$\frac{8.0}{21}$	$\frac{7.2}{28}$	$\frac{4.3}{31}$	$\frac{4.8}{35}$	$\frac{4.2}{41}$
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$\frac{6.0}{50}$	$\frac{6.4}{37}$	$\frac{6.8}{30}$	$\frac{6.7}{21}$	$\frac{4.8}{15}$	$\frac{4.8}{15}$	$\frac{5.2}{23}$	$\frac{8.8}{24}$	$\frac{9.1}{37}$	$\frac{10.3}{37}$	$\frac{11.1}{50}$
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$\frac{8.7}{50}$	$\frac{8.6}{35}$	$\frac{8.2}{26}$	$\frac{7.1}{19}$	$\frac{5.1}{15}$	$\frac{5.4}{15}$	$\frac{9.5}{25}$	$\frac{10.2}{31}$	$\frac{11.2}{38}$	$\frac{11.3}{50}$
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$\frac{9.8}{50}$	$\frac{9.4}{38}$	$\frac{10.0}{27}$	$\frac{9.6}{23}$	$\frac{5.4}{15}$	$\frac{5.7}{15}$	$\frac{10.2}{24}$	$\frac{11.8}{31}$	$\frac{13.0}{50}$	8
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FL 4251 4179

9.6	9.3	10.2	10.48	8.8	5.6	5.9	9.8	11.20	10.9	12.0	12.8	13.4
5.0	3.7	2.5	2.4	2.2	1.4	5.3	15.23	26	24	33	40	50

$\frac{9.0}{50}$	$\frac{8.2}{36}$	$\frac{8.4}{24}$	$\frac{8.2}{21}$	$\frac{5.5}{15}$	$\frac{5.7}{5.3}$	$\frac{9.6}{14}$	$\frac{11.3}{21}$	$\frac{12.8}{26}$	$\frac{12.8}{50}$
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5.1 5.1 7.1 5.3 5.6 10.8 10.7 9.9 10.8
50 29 23-19 15 5.3 16 27 30 35 50

$\frac{1.6}{56}$ $\frac{2.1}{32}$ $\frac{4.7}{28}$ $\frac{6.0}{23}$ $\frac{6.3}{18}$ $\frac{5.1}{15}$ $\frac{5.3}{15}$ $\frac{9.8}{23}$ $\frac{10.0}{29}$ $\frac{7.9}{33}$ $\frac{8.4}{50}$

<u>26</u>	<u>27</u>	<u>53</u>	<u>64</u>	<u>52</u>	<u>51</u>	<u>90</u>	<u>96</u>	<u>82</u>	<u>78</u>	<u>86</u>	
50	30	25	20-18	16	50	16	24	29	31	36	50

5.3	5.9	6.8	6.5	5.3	5.3	8.6	9.6	9.6	10.1
50	27	24	19	15	5.1	14	22	25	35

$\frac{7.0}{50}$	$\frac{7.3}{32}$	$\frac{7.0}{24}$	$\frac{6.9}{19}$	$\frac{5.3}{15}$	5.1	$\frac{5.3}{14}$	$\frac{8.3}{19}$	$\frac{9.3}{24}$	$\frac{9.6}{30}$	$\frac{10.4}{36}$	$\frac{11.3}{50}$
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Sta.	t	π	-	Elev.
		95299.		
10 + 50			4.8	48.2
11			4.2	48.8
+50			3.3	49.7
T.P.	9.36	959.07	3.28	949.71.
12			8.7	50.4
+50			8.1	51.0
13			7.3	51.8
+50			6.4	52.7
14			5.3	53.8
+50			4.7	54.4
15			4.3	54.8
T.P.	2.52	957.97	3.62	955.45.
+50			3.0	55.0
16			3.2	54.8

7.2	7.3	7.4	5.5	5.2	9.3	10.5	11.2
50	35	19	14	4.8	14	25	33
							50

$\frac{6.2}{50}$	$\frac{6.5}{33}$	$\frac{6.4}{18}$	$\frac{4.7}{15}$	$\frac{4.4}{14}$	$\frac{8.0}{22}$	$\frac{8.5}{27}$	$\frac{9.7}{35}$	$\frac{9.6}{50}$
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$\frac{2.3}{50}$	$\frac{2.5}{25}$	$\frac{4.9}{22.18}$	$\frac{4.0}{15}$	3.3	$\frac{3.4}{11}$	$\frac{6.6}{24}$	$\frac{6.7}{27}$	$\frac{7.4}{28.36}$	$\frac{4.0}{39}$	$\frac{4.8}{50}$
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<u>7.9</u>	<u>8.1</u>	<u>9.8</u>	<u>9.0</u>		<u>8.9</u>	<u>10.3</u>	<u>10.8</u>	<u>11.5</u>	<u>7.9</u>	<u>8.5</u>
50	25	22-17	15	87	16	20	27	28-37	39	50

$\frac{76}{50}$	$\frac{79}{37}$	$\frac{75}{23}$	$\frac{93}{21}$	$\frac{83}{18}$	$\frac{8}{16}$	$\frac{94}{21}$	$\frac{6.2}{26}$	$\frac{6.2}{30}$
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$\frac{6.7}{50}$ $\frac{7.6}{24}$ $\frac{8.5}{22-18}$ $\frac{7.7}{16}$ $\frac{7.3}{16}$ $\frac{8.3}{19-23}$ $\frac{5.8}{28}$ $\frac{4.1}{50}$

<u>8.5</u>	<u>8.0</u>	<u>7.9</u>	<u>8.5</u>	<u>6.8</u>	<u>6.4</u>	<u>7.5</u>	<u>3.5</u>	<u>2.1</u>
50	34	24	22-19	16	6.4	15	20-24	28
								50

7.0 6.7 6.1 6.9 5.6 5.4 6.8 4.1 3.1
50 34 25 23-19 15 53 14 18-22 27 50

$$\begin{array}{r} 57 \\ 50 \end{array} \begin{array}{r} 53 \\ 34 \end{array} \begin{array}{r} 46 \\ 26 \end{array} \begin{array}{r} 63 \\ 23-19 \end{array} \begin{array}{r} 49 \\ 15 \end{array} \begin{array}{r} 48 \\ 14 \end{array} \begin{array}{r} 62 \\ 17-23 \end{array} \begin{array}{r} 35 \\ 27 \end{array} \begin{array}{r} 31 \\ 35 \end{array} \begin{array}{r} 26 \\ 50 \end{array}$$

2.0	2.7	2.7	5.6	4.4	4.5	5.9	3.2	3.3	2.4
5.0	3.4	2.9	23-19	16	4.3	17.22	26	4.2	5.0

TP 21 15+

$\frac{1.0}{50}$	$\frac{16}{34}$	$\frac{1.3}{28}$	$\frac{4.1}{24.20}$	$\frac{3.1}{16}$	$\frac{3.1}{30}$	$\frac{4.6}{14}$	$\frac{3.5}{26}$	$\frac{4.0}{47}$	$\frac{3.6}{50}$
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$\frac{1.8}{50}$	$\frac{1.8}{34}$	$\frac{2.3}{28}$	$\frac{4.6}{22-19}$	$\frac{3.5}{16}$	3.2	$\frac{3.5}{15}$	$\frac{4.7}{19-23}$	$\frac{2.5}{26}$	$\frac{3.2}{40}$	$\frac{3.2}{50}$
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Sta.	L	π	-	Elev
		957.97.		
16+50			3.8	54.2
17			4.7	53.3
+50			5.7	52.3
18			6.5	51.5
+50			7.6	50.4
19			8.7	49.3
+50			9.7	48.3
20			10.7	47.3
+50			11.7	46.3
21			12.8.	45.2
T.P.	0.64	945.85	12.76	945.21.
+50			1.7	44.2
22			2.7	43.2

$\frac{4.5}{50}$	$\frac{4.9}{34}$	$\frac{4.3}{25}$	$\frac{5.4}{22-19}$	$\frac{4.2}{16}$	3.8	$\frac{4.0}{15}$	$\frac{5.2}{19-23}$	$\frac{1.8}{27-28}$	$\frac{2.2}{29}$	$\frac{1.8}{39}$	$\frac{1.7}{50}$
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$\frac{4.5}{50}$	$\frac{4.5}{34}$	$\frac{5.8}{24}$	$\frac{6.9}{23-20}$	$\frac{5.2}{16}$	4.7	$\frac{4.6}{14}$	$\frac{5.9}{18-23}$	$\frac{4.1}{25}$	$\frac{3.4}{34}$	$\frac{3.6}{40}$	$\frac{2.8}{50}$
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$\frac{7.8}{50}$	$\frac{8.2}{33}$	$\frac{7.6}{25}$	$\frac{8.0}{23-21}$	$\frac{6.3}{16}$	5.7	$\frac{5.9}{14}$	$\frac{7.2}{18-22}$	$\frac{6.1}{24}$	$\frac{5.8}{32}$	$\frac{5.8}{50}$
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$\frac{8.0}{50}$	$\frac{8.7}{33}$	$\frac{8.4}{21}$	$\frac{6.9}{17}$	6.5	$\frac{6.9}{14}$	$\frac{8.2}{20-24}$	$\frac{6.2}{27}$	$\frac{6.5}{39}$	$\frac{7.1}{41}$	$\frac{7.2}{50}$
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$\frac{12.0}{50}$	$\frac{12.0}{33}$	$\frac{10.9}{20}$	$\frac{8.3}{16}$	7.6	$\frac{7.9}{14}$	$\frac{9.2}{17}$	$\frac{9.5}{24}$	$\frac{9.5}{27}$	$\frac{9.2}{50}$
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oil Tank
Embankment

$\frac{11.0}{50}$	$\frac{12.1}{33}$	$\frac{11.4}{21}$	$\frac{9.6}{15}$	8.7	$\frac{9.0}{14}$	$\frac{10.5}{18}$	$\frac{10.1}{28}$	$\frac{10.4}{38}$	$\frac{9.2}{50}$
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$\frac{11.2}{50}$	$\frac{11.5}{36}$	$\frac{12.1}{33}$	$\frac{12.2}{26}$	$\frac{11.7}{22}$	$\frac{10.3}{16}$	9.7	$\frac{9.8}{14}$	$\frac{11.5}{18-21}$	$\frac{10.8}{23}$	$\frac{11.3}{40}$	$\frac{10.9}{50}$
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$\frac{11.0}{50}$	$\frac{11.5}{33}$	$\frac{12.3}{27}$	$\frac{11.5}{21}$	$\frac{11.2}{15}$	10.7	$\frac{10.8}{15}$	$\frac{12.1}{19-22}$	$\frac{10.9}{25}$	$\frac{11.1}{33}$	$\frac{11.6}{50}$
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$\frac{11.0}{50}$	$\frac{12.3}{31}$	$\frac{13.4}{27-24}$	$\frac{12.1}{17}$	11.7	$\frac{11.9}{15}$	$\frac{12.9}{18-22}$	$\frac{11.5}{27}$	$\frac{8.8}{31}$	$\frac{8.9}{50}$
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$\frac{11.4}{50}$	$\frac{11.7}{34}$	$\frac{14.0}{27-21}$	$\frac{13.3}{16}$	12.8	$\frac{12.9}{15}$	$\frac{13.4}{20-23}$	$\frac{12.8}{26}$	$\frac{7.8}{33}$	$\frac{8.5}{50}$
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$\frac{11.2}{50}$	$\frac{11.0}{34}$	$\frac{2.5}{27}$	$\frac{3.0}{19}$	$\frac{2.1}{16}$	1.7	$\frac{1.8}{16}$	$\frac{2.7}{19}$	$\frac{1.7}{25}$	$\frac{0.2}{28}$	$\frac{1.55}{32}$	$\frac{1.5.0}{50}$
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$\frac{10.2}{50}$	$\frac{0.0}{34}$	$\frac{4.0}{26}$	$\frac{4.1}{19}$	$\frac{3.0}{15}$	2.7	$\frac{2.8}{15}$	$\frac{4.0}{19-23}$	$\frac{1.1}{26}$	$\frac{2.5}{39}$	$\frac{2.6}{50}$
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Sta.	+	⌒	-	Elev.
		945.85		
22+50			3.8	42.1
23			4.9	41.0
+50			6.3	39.6
24			7.4	38.5
+50			8.5	37.4
25			9.4	36.5
B.M.	439	939.65	10.62	935.23
+18			3.4	36.3
+35			3.6	36.1
+50	Top Rail		4.00	35.15
+52			4.0	35.7
+55.3	Top Rail		4.01	35.64
+58			4.0	35.7

935.26

$\frac{+1.5}{50}$ $\frac{0.4}{34}$ $\frac{5.0}{26}$ $\frac{5.8}{21-19}$ $\frac{4.1}{14}$ $\frac{3.8}{13}$ $\frac{4.9}{17}$ $\frac{5.7}{18-22}$ $\frac{4.2}{26}$ $\frac{4.2}{50}$

(0.1 ton/c)
Emb.

$\frac{+4.2}{50}$ $\frac{+1.0}{40}$ $\frac{2.8}{34}$ $\frac{3.4}{32}$ $\frac{6.7}{25}$ $\frac{7.5}{23-19}$ $\frac{5.4}{14}$ $\frac{5.1}{12}$ $\frac{5.9}{15}$ $\frac{7.4}{18-21}$ $\frac{4.8}{27}$ $\frac{4.4}{36}$ $\frac{2.1}{50}$

$\frac{0.7}{50}$ $\frac{9.7}{34}$ $\frac{10.7}{26}$ $\frac{10.0}{21}$ $\frac{6.8}{15}$ $\frac{6.3}{15}$ $\frac{7.5}{17}$ $\frac{8.9}{20}$ $\frac{8.9}{25}$ $\frac{8.0}{27}$ $\frac{8.3}{36}$ $\frac{7.1}{50}$

$\frac{12.8}{50}$ $\frac{13.5}{34}$ $\frac{12.8}{25}$ $\frac{8.0}{15}$ 7.4 $\frac{7.6}{14}$ $\frac{9.3}{19}$ $\frac{10.2}{25}$ $\frac{9.7}{36}$ $\frac{8.5}{50}$

$\frac{14.0}{50}$ $\frac{14.2}{34}$ $\frac{14.1}{24}$ $\frac{8.7}{15}$ 8.5 $\frac{8.7}{14}$ $\frac{11.8}{19}$ $\frac{12.2}{22-26}$ $\frac{11.8}{29}$ $\frac{12.9}{50}$

$\frac{14.6}{50}$ $\frac{14.4}{33}$ $\frac{13.8}{25}$ $\frac{10.0}{15}$ 9.4 $\frac{9.5}{13}$ $\frac{11.9}{19}$ $\frac{13.0}{24}$ $\frac{13.1}{50}$

Top Mon 26 + 52.28

$\frac{4.8}{50}$ $\frac{4.5}{22}$ $\frac{3.8}{12}$ 3.4 $\frac{3.4}{12}$ $\frac{4.5}{16}$ $\frac{7.2}{22}$ $\frac{7.7}{28}$ $\frac{6.7}{50}$

$\frac{4.6}{50}$ $\frac{4.3}{26}$ $\frac{3.8}{11}$ 3.6 $\frac{3.7}{12}$ $\frac{7.0}{21}$ $\frac{6.7}{39}$ $\frac{4.8}{50}$

$\frac{5.0}{50}$ $\frac{4.7}{21}$ 4.0 $\frac{4.6}{25}$ $\frac{4.6}{50}$

$\frac{5.2}{50}$ $\frac{4.9}{30}$ $\frac{4.2}{17}$ 4.0 $\frac{4.0}{13}$ $\frac{5.0}{20}$ $\frac{4.8}{30}$ $\frac{4.8}{50}$

Sta.	+	π	-	Elev.
		939.65		
25+66			3.9	35.8
26			4.3	35.4
+16			4.1	35.6
+28			4.2	35.5
+33.5	Top Rail		4.22	35.43
+38.0	Top Rail		4.26	35.39
+43	Co		4.3	35.4
+59			4.5	35.2
B.M.	0.30	935.56	4.39	935.26
+76			0.6	35.0
+89			0.8	34.8
27			0.9	34.7
+50			1.5	34.1

$$\begin{array}{cccccccccccc} \frac{6.0}{50} & \frac{5.4}{25} & \frac{4.9}{16} & \frac{4.1}{11} & 3.9 & \frac{4.1}{12} & \frac{6.0}{19} & \frac{8.1}{26} & \frac{8.8}{40} & \frac{7.4}{45} & \frac{7.6}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{8.2}{50} & \frac{8.4}{30} & \frac{7.4}{23} & \frac{5.6}{17} & \frac{4.8}{12} & 4.3 & \frac{4.3}{12} & \frac{9.4}{24} & \frac{10.7}{35} & \frac{10.3}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{8.0}{50} & \frac{9.1}{35} & \frac{8.4}{27} & \frac{6.2}{18} & \frac{4.5}{13} & 4.1 & \frac{4.3}{12} & \frac{6.2}{18} & \frac{8.0}{23} & \frac{9.7}{28} & \frac{8.6}{43} & \frac{8.6}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{5.1}{50} & \frac{5.0}{31} & \frac{4.3}{12} & 4.2 & & \frac{4.2}{10} & & \frac{5.4}{31} & \frac{5.0}{50} \end{array}$$

$$\frac{4.22}{1}$$

$$\frac{4.26}{1}$$

$$\begin{array}{cccccccc} \frac{5.1}{50} & \frac{5.3}{24} & \frac{5.4}{17} & \frac{4.3}{12} & 4.3 & \frac{4.3}{12} & \frac{5.0}{18} & \frac{5.8}{35} & \frac{5.3}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{12.6}{50} & \frac{11.6}{37} & \frac{10.0}{27} & \frac{5.4}{17} & & 4.8 & \frac{10.2}{26} & \frac{11.7}{37} & \frac{12.1}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{7.8}{50} & \frac{7.6}{37} & \frac{6.6}{25} & \frac{0.7}{14} & 0.6 & \frac{0.8}{10} & \frac{0.9}{16} & \frac{4.8}{23} & \frac{6.9}{31} & \frac{8.5}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{2.7}{50} & \frac{3.2}{35} & \frac{5.3}{29} & \frac{5.9}{27} & \frac{0.7}{15} & 0.8 & \frac{1.0}{11} & \frac{2.0}{15} & \frac{5.0}{22} & \frac{5.6}{25} & \frac{6.2}{36} & \frac{6.3}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{5.7}{50} & \frac{4.9}{39} & \frac{3.8}{35} & \frac{4.6}{30} & \frac{5.3}{24} & \frac{0.9}{14} & 0.9 & \frac{1.1}{12} & \frac{5.2}{21} & \frac{5.5}{27} & \frac{6.4}{40} & \frac{5.8}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{7.5}{50} & \frac{6.8}{41} & \frac{6.6}{39} & \frac{5.5}{24} & \frac{1.8}{16} & 1.5 & \frac{1.6}{14} & & \frac{5.3}{24} & \frac{6.1}{37} & \frac{5.6}{50} \end{array}$$

Sta.	+	π	-	Elev
		935.56		
28			2.2	33.4
	+50		3.0	32.6
29			3.6	32.0
	+50		4.3	31.3
30			5.2	30.4
	+50		6.0	29.6
31			6.8	28.8
	+50		7.6	28.0
32			8.2	27.4
	+50		9.0	26.6
T.P.	2.79	928.46	9.89	925.67
33			2.8	25.7
	+50		3.6	24.9

$\frac{6.6}{50}$ $\frac{6.6}{38}$ $\frac{5.7}{30}$ $\frac{5.8}{22}$ $\frac{2.5}{15}$ $\frac{2.2}{2.2}$ $\frac{2.4}{12}$ $\frac{4.9}{20}$ $\frac{5.0}{26}$ $\frac{5.3}{39}$ $\frac{5.0}{50}$

$\frac{5.9}{50}$ $\frac{5.9}{40}$ $\frac{4.9}{36}$ $\frac{4.9}{30}$ $\frac{6.0}{24}$ $\frac{3.3}{21}$ $\frac{3.3}{15}$ $\frac{3.3}{3.0}$ $\frac{5.5}{13}$ $\frac{3.2}{17}$ $\frac{2.4}{22}$ $\frac{2.2}{25}$ $\frac{2.2}{36}$ $\frac{2.2}{50}$

$\frac{5.7}{50}$ $\frac{5.5}{38}$ $\frac{5.9}{32}$ $\frac{6.0}{24}$ $\frac{3.9}{19}$ $\frac{3.9}{15}$ $\frac{3.8}{3.6}$ $\frac{5.9}{13}$ $\frac{3.6}{17}$ $\frac{3.1}{22}$ $\frac{3.1}{25}$ $\frac{3.1}{36}$ $\frac{3.1}{50}$

$\frac{5.7}{50}$ $\frac{5.0}{32}$ $\frac{5.3}{28}$ $\frac{6.4}{24}$ $\frac{4.6}{21}$ $\frac{4.6}{15}$ $\frac{4.4}{4.3}$ $\frac{5.7}{15}$ $\frac{4.2}{17}$ $\frac{3.7}{22}$ $\frac{3.7}{25}$ $\frac{3.7}{33}$ $\frac{3.7}{50}$

$\frac{6.2}{50}$ $\frac{6.3}{24}$ $\frac{6.5}{22}$ $\frac{5.4}{20}$ $\frac{5.3}{14}$ $\frac{6.9}{52}$ $\frac{6.1}{13}$ $\frac{5.5}{17}$ $\frac{5.5}{19}$ $\frac{5.5}{22}$ $\frac{5.5}{25}$ $\frac{5.5}{36}$ $\frac{5.5}{50}$

$\frac{8.0}{50}$ $\frac{7.8}{29}$ $\frac{8.1}{20}$ $\frac{6.2}{15}$ $\frac{6.7}{6.0}$ $\frac{8.0}{14}$ $\frac{7.7}{17}$ $\frac{7.3}{20}$ $\frac{7.7}{23}$ $\frac{7.3}{50}$

$\frac{7.1}{50}$ $\frac{8.5}{24}$ $\frac{8.5}{20}$ $\frac{6.9}{15}$ $\frac{7.0}{6.8}$ $\frac{8.5}{14}$ $\frac{7.3}{18}$ $\frac{8.0}{21}$ $\frac{7.5}{24}$ $\frac{7.5}{30}$ $\frac{7.5}{37}$ $\frac{7.5}{50}$

$\frac{8.7}{50}$ $\frac{8.7}{34}$ $\frac{8.6}{24}$ $\frac{7.5}{23}$ $\frac{7.9}{20}$ $\frac{8.0}{7.6}$ $\frac{9.5}{13}$ $\frac{8.2}{19}$ $\frac{8.6}{23}$ $\frac{8.2}{25}$ $\frac{8.2}{27}$ $\frac{8.2}{50}$

$\frac{9.8}{50}$ $\frac{9.5}{37}$ $\frac{8.8}{34}$ $\frac{8.2}{26}$ $\frac{9.4}{23}$ $\frac{8.4}{19}$ $\frac{8.4}{15}$ $\frac{10.2}{8.2}$ $\frac{8.9}{13}$ $\frac{9.3}{18}$ $\frac{8.6}{23}$ $\frac{8.6}{25}$ $\frac{8.6}{30}$ $\frac{8.6}{50}$

$\frac{9.6}{50}$ $\frac{10.0}{40}$ $\frac{9.3}{36}$ $\frac{9.5}{26}$ $\frac{10.5}{24}$ $\frac{9.1}{20}$ $\frac{9.2}{9.0}$ $\frac{10.6}{14}$ $\frac{8.5}{20}$ $\frac{9.0}{24}$ $\frac{8.7}{26}$ $\frac{8.7}{29}$ $\frac{8.7}{50}$

$\frac{1.8}{50}$ $\frac{1.5}{37}$ $\frac{0.8}{35}$ $\frac{2.6}{29}$ $\frac{3.7}{22}$ $\frac{3.0}{18}$ $\frac{2.9}{2.8}$ $\frac{4.1}{15}$ $\frac{2.2}{20}$ $\frac{2.1}{23}$ $\frac{2.0}{26}$ $\frac{1.8}{30}$ $\frac{1.8}{39}$ $\frac{1.8}{50}$

$\frac{1.8}{50}$ $\frac{1.4}{38}$ $\frac{0.9}{36}$ $\frac{3.1}{27}$ $\frac{4.4}{22}$ $\frac{4.3}{18}$ $\frac{3.8}{3.6}$ $\frac{5.0}{16}$ $\frac{1.5}{17}$ $\frac{2.0}{23}$ $\frac{1.8}{27}$ $\frac{1.8}{33}$ $\frac{1.8}{50}$

Sta.	+	π	-	Elev.
		928.46		
34			4.7	23.8
+50			5.3	23.2
35			6.2	22.3
+50			7.0	21.5
36			7.9	20.6
+50			8.7	19.8
37			9.8	18.7
+50			10.7	17.8
T.P.	1.83	919.67	10.62	917.84
38			2.9	16.8
+50			3.7	16.0
39			4.6	15.1
+50			5.2	14.5

$\frac{4.1}{50}$ $\frac{4.1}{41}$ $\frac{3.3}{39}$ $\frac{2.8}{32}$ $\frac{4.2}{28}$ $\frac{5.5}{23-21}$ $\frac{4.8}{18}$ $\frac{4.6}{14}$ $\frac{6.0}{19-22}$ $\frac{2.1}{28}$ $\frac{2.0}{37}$ $\frac{1.6}{50}$

$\frac{6.8}{50}$ $\frac{6.0}{39}$ $\frac{5.5}{37}$ $\frac{4.4}{34-31}$ $\frac{5.9-6.5}{35}$ $\frac{5.8}{23-21}$ $\frac{5.6}{17}$ $\frac{6.6}{5.3}$ $\frac{2.7}{15}$ $\frac{2.4}{20-24}$ $\frac{2.2}{29}$ $\frac{2.2}{37}$ $\frac{2.2}{50}$

$\frac{7.9}{50}$ $\frac{7.3}{41}$ $\frac{6.7}{36}$ $\frac{6.0}{32}$ $\frac{6.6}{29}$ $\frac{7.1}{25}$ $\frac{7.4}{23-21}$ $\frac{6.5}{17}$ $\frac{6.4}{6.2}$ $\frac{7.1}{13}$ $\frac{2.7}{17-23}$ $\frac{2.7}{29}$ $\frac{3.3}{33}$ $\frac{3.3}{50}$

$\frac{8.2}{50}$ $\frac{7.6}{40}$ $\frac{6.7}{35}$ $\frac{6.4}{30}$ $\frac{7.3}{28}$ $\frac{8.1}{22-20}$ $\frac{7.3}{17}$ $\frac{7.1}{7.0}$ $\frac{8.1}{14}$ $\frac{3.4}{20-24}$ $\frac{4.0}{30}$ $\frac{4.0}{37}$ $\frac{4.0}{50}$

$\frac{8.3}{50}$ $\frac{7.8}{41}$ $\frac{7.1}{37}$ $\frac{6.7}{31}$ $\frac{8.4}{24}$ $\frac{9.1}{22-20}$ $\frac{8.2}{18}$ $\frac{8.0}{7.9}$ $\frac{8.6}{15}$ $\frac{4.5}{18-21}$ $\frac{3.6}{29}$ $\frac{3.6}{50}$

$\frac{8.8}{50}$ $\frac{8.7}{41}$ $\frac{7.2}{37}$ $\frac{7.0}{31}$ $\frac{7.9}{22-20}$ $\frac{8.8}{17}$ $\frac{8.2}{8.7}$ $\frac{9.8}{17}$ $\frac{8.2}{20-23}$ $\frac{5.0}{25}$ $\frac{3.9}{30}$ $\frac{3.9}{50}$

$\frac{11.9}{50}$ $\frac{11.7}{41}$ $\frac{10.8}{38}$ $\frac{10.6}{30}$ $\frac{11.5}{27-23}$ $\frac{9.9}{18}$ $\frac{9.9}{9.8}$ $\frac{11.2}{14}$ $\frac{9.5}{18-21}$ $\frac{8.3}{27}$ $\frac{8.3}{50}$

$\frac{13.4}{50}$ $\frac{13.4}{38}$ $\frac{12.5}{33}$ $\frac{13.5}{29}$ $\frac{11.0}{18}$ $\frac{10.9}{10.7}$ $\frac{13.0}{14}$ $\frac{12.6}{19-24}$ $\frac{12.8}{28}$ $\frac{12.8}{50}$

$\frac{5.3}{50}$ $\frac{5.0}{38}$ $\frac{4.7}{32}$ $\frac{5.1}{29}$ $\frac{5.0}{22}$ $\frac{3.1}{18}$ $\frac{3.3}{2.9}$ $\frac{4.9}{14}$ $\frac{4.6}{19}$ $\frac{4.7}{28}$ $\frac{4.9}{32}$ $\frac{4.9}{50}$

$\frac{5.7}{50}$ $\frac{5.4}{41}$ $\frac{4.9}{37}$ $\frac{5.0}{30}$ $\frac{5.9}{28-22}$ $\frac{4.1}{19}$ $\frac{4.0}{3.7}$ $\frac{5.5}{14}$ $\frac{4.4}{19-23}$ $\frac{4.6}{26}$ $\frac{4.8}{34}$ $\frac{4.8}{50}$

$\frac{6.1}{50}$ $\frac{6.1}{42}$ $\frac{5.6}{37}$ $\frac{5.7}{31}$ $\frac{6.8}{27}$ $\frac{6.4}{21}$ $\frac{4.9}{18}$ $\frac{5.0}{4.6}$ $\frac{6.4}{15}$ $\frac{4.9}{21-23}$ $\frac{5.2}{28}$ $\frac{5.2}{50}$

$\frac{6.3}{50}$ $\frac{6.1}{41}$ $\frac{5.5}{36}$ $\frac{5.7}{33}$ $\frac{8.1}{28}$ $\frac{7.8}{24}$ $\frac{5.6}{16}$ $\frac{5.2}{5.2}$ $\frac{6.5}{15}$ $\frac{6.8}{18}$ $\frac{4.9}{24}$ $\frac{5.4}{28}$ $\frac{5.4}{50}$

Sta.	+	π	-	Elev.
		919.67.		
40			5.8	13.9
+50			6.5	13.2
41			7.1	12.6
+50			7.7	12.0
42			8.4	11.3
T.P.	2.96	913.96.	8.67	911.00.
150			2.9	11.1
43			3.4	10.6
+35			3.7	10.3
+80			4.2	09.8
44			4.4	09.6
+50			5.2	08.8
T.P.	0.84	910.31.	4.49	909.47.
45			2.2	08.1

$\frac{7.0}{50}$	$\frac{6.2}{42}$	$\frac{5.4}{35}$	$\frac{8.7}{28}$	$\frac{8.1}{21}$	$\frac{6.3}{16}$	$\frac{6.1}{15}$	$\frac{7.3}{19-22}$	$\frac{5.0}{27}$	$\frac{5.1}{30}$	$\frac{5.7}{50}$
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$\frac{8.5}{50}$	$\frac{7.8}{42}$	$\frac{6.5}{37}$	$\frac{6.6}{34}$	$\frac{9.5}{28}$	$\frac{9.7}{22}$	$\frac{6.9}{16.5}$	$\frac{6.7}{17}$	$\frac{7.7}{19}$	$\frac{7.8}{26}$	$\frac{5.6}{29}$	$\frac{6.2}{40}$	$\frac{6.1}{50}$
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$\frac{9.9}{50}$	$\frac{10.0}{43}$	$\frac{9.3}{38}$	$\frac{9.5}{31}$	$\frac{9.9}{28}$	$\frac{9.8}{20}$	$\frac{7.5}{15}$	$\frac{7.4}{17}$	$\frac{8.9}{19-23}$	$\frac{6.9}{26}$	$\frac{7.3}{31}$	$\frac{7.3}{50}$
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$\frac{10.5}{50}$	$\frac{10.4}{39}$	$\frac{10.2}{34}$	$\frac{10.9}{26}$	$\frac{10.5}{21}$	$\frac{8.3}{16}$	$\frac{8.0}{7.7}$	$\frac{8.6}{14}$	$\frac{9.6}{17}$	$\frac{8.4}{19-23}$	$\frac{8.7}{27}$	$\frac{8.6}{31}$	$\frac{8.6}{50}$
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$\frac{10.6}{50}$	$\frac{10.3}{38}$	$\frac{10.1}{26}$	$\frac{10.9}{23-20}$	$\frac{8.8}{16}$	$\frac{8.4}{8.4}$	$\frac{8.5}{15}$	$\frac{10.0}{18-23}$	$\frac{8.5}{25}$	$\frac{8.7}{30}$	$\frac{8.9}{50}$
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$\frac{4.5}{50}$	$\frac{3.5}{40}$	$\frac{3.9}{36}$	$\frac{3.1}{23}$	$\frac{4.9}{22-18}$	$\frac{3.2}{15}$	$\frac{3.1}{2.9}$	$\frac{4.6}{15}$	$\frac{4.5}{20}$	$\frac{3.8}{25}$	$\frac{3.5}{28}$	$\frac{1.7}{35}$	$\frac{2.2}{4}$	$\frac{2.2}{50}$
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$\frac{4.2}{50}$	$\frac{4.0}{38}$	$\frac{3.5}{33}$	$\frac{3.6}{26}$	$\frac{5.6}{22-19}$	$\frac{3.8}{15}$	$\frac{3.6}{3.4}$	$\frac{5.0}{17}$	$\frac{3.8}{20-25}$	$\frac{3.4}{27}$	$\frac{2.4}{31}$	$\frac{2.5}{34}$	$\frac{2.5}{50}$
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$\frac{4.3}{50}$	$\frac{3.9}{39}$	$\frac{3.4}{36}$	$\frac{3.1}{25}$	$\frac{5.7}{20-18}$	$\frac{4.0}{15}$	$\frac{4.0}{3.7}$	$\frac{5.1}{16}$	$\frac{5.4}{21}$	$\frac{4.7}{26}$	$\frac{1.9}{31}$	$\frac{3.1}{38}$	$\frac{2.6}{46}$	$\frac{2.6}{50}$
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$\frac{4.1}{50}$	$\frac{3.8}{41}$	$\frac{3.2}{35}$	$\frac{2.9}{31}$	$\frac{6.2}{24-20}$	$\frac{4.5}{14}$	$\frac{4.1}{4.2}$	$\frac{4.3}{14}$	$\frac{5.6}{26}$	$\frac{5.8}{26}$	$\frac{5.1}{30}$	$\frac{0.9}{36}$	$\frac{1.0}{50}$
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$\frac{4.0}{50}$	$\frac{3.6}{41}$	$\frac{2.8}{32}$	$\frac{6.7}{24-20}$	$\frac{4.7}{15}$	$\frac{4.4}{4.4}$	$\frac{4.6}{15}$	$\frac{5.8}{17}$	$\frac{6.5}{24}$	$\frac{5.5}{30}$	$\frac{1.3}{35}$	$\frac{1.3}{50}$
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$\frac{3.2}{50}$	$\frac{2.8}{40}$	$\frac{2.2}{36}$	$\frac{7.3}{24-20}$	$\frac{5.4}{15}$	$\frac{5.2}{5.2}$	$\frac{5.4}{15}$	$\frac{6.6}{19}$	$\frac{7.2}{21}$	$\frac{7.1}{26}$	$\frac{6.3}{31}$	$\frac{3.2}{35}$	$\frac{4.2}{50}$
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Spk T.P. Rt 446

$\frac{2.5}{50}$	$\frac{1.8}{39}$	$\frac{1.4}{33}$	$\frac{5.4}{26}$	$\frac{5.0}{20}$	$\frac{2.5}{15}$	$\frac{2.2}{2.2}$	$\frac{2.6}{15}$	$\frac{4.4}{19}$	$\frac{4.3}{25}$	$\frac{4.2}{30}$	$\frac{3.6}{33}$	$\frac{3.8}{50}$
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Sta.	+	Σ	-	Elev
		910.31		
45 + 50			2.9	07.4
46			3.7	06.6
+ 50			4.3	06.0
47			5.0	05.3
+ 52	24" x 50' Conc.		5.7	04.6
48			6.2	04.1
+ 50			6.3	04.0
49			5.8	04.5
+ 50			4.5	05.8
50			3.0	07.3
+ 50			1.5	08.8
51			0.1	10.2
T.P.	7.35	917.37	0.29	910.02

$$\begin{array}{ccccccc} \frac{5.6}{50} & \frac{5.5}{38} & \frac{5.1}{32} & \frac{6.6}{27.24} & \frac{3.2}{15} & \frac{3.1}{13} & \frac{5.4}{20} & \frac{5.6}{26} & \frac{5.5}{31} & \frac{5.6}{50} \end{array} \checkmark$$

$$\begin{array}{ccccccc} \frac{7.6}{50} & \frac{7.6}{39} & \frac{7.2}{37} & \frac{7.1}{36} & \frac{8.2}{28.24} & \frac{4.2}{15} & \frac{4.1}{14} & \frac{7.3}{23} & \frac{7.1}{28} & \frac{7.4}{50} \end{array} \checkmark$$

$$\begin{array}{ccccccc} \frac{9.6}{50} & \frac{9.1}{37} & \frac{8.9}{31} & \frac{8.4}{22} & \frac{4.9}{15} & \frac{4.9}{14} & \frac{8.5}{25} & \frac{9.0}{29} & \frac{9.0}{50} \end{array} \checkmark$$

$$\begin{array}{ccccccc} \frac{10.8}{50} & \frac{11.0}{32} & \frac{10.0}{24} & \frac{5.4}{15} & \frac{5.4}{50} & \frac{9.7}{14} & \frac{10.0}{22} & \frac{9.8}{32} & \frac{9.8}{50} \end{array} \checkmark$$

9881

$$\begin{array}{ccccccc} \frac{11.7}{50} & \frac{11.5}{39} & \left(\frac{11.50}{27} \right) & \frac{10.7}{26} & \frac{6.1}{15} & \frac{6.0}{14} & \left(\frac{10.7}{23} \right) & \frac{11.1}{24} & \frac{10.7}{34} & \frac{10.1}{50} \end{array} \checkmark$$

$$\frac{10.02}{10.02} \text{ w.L. } \frac{6.13}{40} \quad 900.29$$

$$\begin{array}{ccccccc} \frac{11.2}{50} & \frac{11.0}{33} & \frac{10.5}{23} & \frac{6.6}{15} & \frac{6.6}{6.2} & \frac{9.7}{14} & \frac{10.2}{20} & \frac{10.0}{24} & \frac{10.0}{50} \end{array} \checkmark$$

$$\begin{array}{ccccccc} \frac{11.5}{50} & \frac{10.8}{32} & \frac{10.7}{23} & \frac{6.8}{15} & \frac{6.9}{6.3} & \frac{9.5}{15} & \frac{10.2}{19} & \frac{10.5}{23} & \frac{10.2}{32} & \frac{10.2}{50} \end{array} \checkmark$$

$$\frac{10.02}{10.02} \text{ w.L. } \frac{6.13}{40} \quad 900.29$$

$$\begin{array}{ccccccc} \frac{11.6}{50} & \frac{10.8}{31} & \frac{10.7}{23} & \frac{6.5}{16} & \frac{6.2}{5.8} & \frac{10.0}{15} & \frac{10.2}{22} & \frac{9.8}{30} & \frac{9.8}{50} \end{array} \checkmark$$

$$\begin{array}{ccccccc} \frac{11.1}{50} & \frac{10.6}{33} & \frac{10.0}{24} & \frac{5.2}{16} & \frac{4.8}{4.5} & \frac{8.3}{14} & \frac{9.0}{22} & \frac{9.2}{24} & \frac{8.4}{35} & \frac{8.4}{50} \end{array} \checkmark$$

$$\begin{array}{ccccccc} \frac{10.2}{50} & \frac{9.8}{39} & \frac{8.6}{30} & \frac{7.9}{25} & \frac{3.7}{14} & \frac{3.2}{3.0} & \frac{7.9}{14} & \frac{8.2}{24} & \frac{6.9}{27} & \frac{6.3}{39} & \frac{6.3}{50} \end{array} \checkmark$$

$$\begin{array}{ccccccc} \frac{8.5}{50} & \frac{7.6}{34} & \frac{7.6}{26} & \frac{6.1}{21} & \frac{6.9}{15} & \frac{1.8}{1.5} & \frac{6.7}{15} & \frac{7.4}{53} & \frac{4.5}{41} & \frac{4.4}{50} \end{array} \checkmark$$

$$\begin{array}{ccccccc} \frac{6.4}{50} & \frac{5.9}{34} & \frac{5.2}{31} & \frac{4.2}{23} & \frac{0.7}{15} & \frac{0.5}{0.1} & \frac{5.2}{15} & \frac{4.6}{23} & \frac{0.3}{36} & \frac{0.4}{41} & \frac{0.4}{50} \end{array} \checkmark$$

Sta.	+	⌘	-	Elev.
		917.37		
51 + 25			6.5	10.9
+ 67			5.5	11.9
52			5.0	12.4
+ 30			4.4	13.0
+ 50			3.9	13.5
+ 75			2.9	14.5
+ 87	shldr.		2.5	14.9
53 + 02.60	±	Cleveland	2.3	15.1
+ 18	shldr.		2.2	15.2
+ 25			2.2	15.2
+ 46	12" x 58" C.M.		2.4	15.6
B.M.	8.62	923.67	2.32	915.05
54			2.9	15.8

915.05

112 108 10.3 9.6 6.9 6.9 11.0 10.8 5.7 5.4
50 45 29 23 13 6.5 14 24 29 39 50 ✓

142 136 51 6.7 6.1 5.9 8.0 8.6 11.0 7.6 6.5 4.5 3.6
50 34 24 18 15 5.5 15 20 23 25 27 31 37 50 ✓

173 150 14.4 5.0 6.1 5.5 5.3 6.4 6.4 10.6 6.1 6.9 9.4
50 38 32 24 18 15 5.0 14 20 24 26 28 35 50 ✓

0.1 1.1 1.7 6.7 4.8 4.5 8.4 9.0
50 38 28 22 19 14 4.4 15 25 50 ✓

4.0 3.3 3.4 3.4 6.1 4.5 4.1 5.5 5.6 5.8
50 42 34 25 22 20 15 29 15 20 37 50 ✓

7.3 6.1 4.4 3.7 3.1 4.0 3.5
50 35 27 21 6.9 26 31 50 ✓

4.5 3.6 3.0 2.1 1.7
50 34 16 2.5 24 50 ✓

3.6 0.8
50 50 ✓

4.1 3.1 1.7 1.3
50 30 2.2 33 50 ✓

7.0 5.1 3.8 3.2 2.5 2.6 4.5 4.5
50 42 32 26 2.2 19 27 33 50 ✓

10.47

2.4 (6.90) 8.0 5.5 3.5 2.7 2.8 3.9 5.3 5.7 (6.08) 6.1
50 32 32 30 23 16 2.4 11 17 23 26 26 50 ✓

11.29

Top Mon. Cleveland

9.6 9.6 9.2 9.5 8.3 8.4 9.7 9.3 9.0
50 40 32 29 25 23 7.9 73 19 27 50 ✓

Sta.	+	$\bar{\Delta}$	-	Elev.
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923.67.

54/450			6.8	16.9
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55			5.8	17.9
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+50			5.0	18.7
-----	--	--	-----	------

463	1222' C.M.		4.8	18.9
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56			4.2	19.5
----	--	--	-----	------

T.P.	952	931.35	184	921.83-
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+50			10.8	20.6
-----	--	--	------	------

+82	PC		10.1	21.3
-----	----	--	------	------

57			9.7	21.7
----	--	--	-----	------

+50			8.5	22.9
-----	--	--	-----	------

58			7.3	24.1
----	--	--	-----	------

+50			6.0	25.4
-----	--	--	-----	------

59			4.9	26.5
----	--	--	-----	------

$$\begin{array}{cccccccccccc} 81 & 6.4 & 5.7 & 8.3 & 7.2 & 7.4 & 10.3 & 10.2 & 3.6 & 3.7 & & \\ 50 & 39 & 35 & 29.26 & 23 & 68 & 14 & 21 & 30 & 39 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 10.9 & 10.0 & 9.6 & 6.5 & & 6.6 & 8.3 & 9.2 & 7.5 & 7.7 & & \\ 50 & 39 & 33 & 26 & 58 & 11.14 & 22.27 & 29 & 50 & & & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 13.7 & 12.4 & & 5.8 & & & 5.7 & 9.6 & 10.6 & 10.9 & & \\ 50 & 38 & & 22 & 50 & & 15 & 23 & 30 & 50 & & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} & & & \text{FL. } 10.13 & & & & & & & & \text{FL. } 12.26 \\ 140 & 133 & (13.54) & 12.4 & 5.6 & & 5.5 & 10.4 & 10.7 & (10.7) & 11.3 & 11.4 \\ 50 & 41 & (40) & 38 & 24 & 4.8 & 13 & 24 & 28 & (28) & 32 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 12.4 & 12.1 & 6.6 & 5.1 & & 4.7 & 9.1 & 9.7 & 9.4 & & & \\ 50 & 40 & 27 & 23 & 4.2 & 13 & 2.2 & 32 & 50 & & & \checkmark \end{array}$$

Spk. T.P. R. 56+

$$\begin{array}{cccccccccccc} 16.0 & 14.3 & 11.3 & 10.7 & & 11.0 & 11.5 & 13.5 & 14.0 & 14.0 & 14.3 & \\ 50 & 33 & 23 & 8 & 10.8 & 7 & 10 & 19 & 22 & 33 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 14.1 & 12.8 & 11.2 & 10.9 & 10.0 & 10.3 & 11.0 & 11.8 & 12.7 & 12.0 & & \\ 50 & 35 & 27 & 25 & 9 & 10.1 & 7 & 11 & 15 & 23 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 13.9 & 13.8 & 12.8 & 10.9 & 10.1 & 9.5 & 10.0 & 11.1 & 12.4 & 12.3 & 12.0 & \\ 50 & 44 & 32 & 28 & 23 & 9 & 9.7 & 8 & 14 & 23 & 34 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 10.0 & 9.0 & 9.0 & 11.0 & 8.8 & 8.3 & 8.5 & 10.0 & 9.3 & 8.7 & 9.2 & \\ 50 & 44 & 36 & 32.29 & 26 & 8 & 8.5 & 13 & 17 & 27 & 42 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 8.3 & 8.3 & 7.4 & 9.2 & 7.7 & 7.1 & 7.3 & 8.8 & 8.0 & 8.4 & & \\ 50 & 50 & 36 & 32.29 & 25 & 8 & 7.3 & 11 & 16 & 31 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 3.8 & 3.7 & 7.7 & 6.2 & 5.9 & & 6.2 & 7.5 & 7.4 & 8.3 & & \\ 50 & 39 & 32.29 & 25 & 8 & 6.0 & 14 & 16 & 30 & 50 & & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} 0.4 & 0.4 & 1.4 & 5.2 & 6.2 & 5.1 & 5.2 & 6.4 & 6.9 & 2.2 & & \\ 50 & 46 & 40 & 32 & 29 & 24 & 4.9 & 14 & 16 & 41 & 50 & \checkmark \end{array}$$

Sta.	+	⌞	—	Elev.
		731.35		
59+50			3.5	27.9
T.P.	5.61	934.46	2.50	928.85
60			5.6	28.9
+50			4.9	29.6
61			4.6	29.9
+50			4.6	29.9
+85 RT			4.9	29.6
62			4.9	29.6
+50			5.1	29.4
63			5.6	28.9
B.M.	3.96	931.90	6.51	927.95
+25			3.4	28.5
+50			3.6	28.3
64			3.5	28.4

$\frac{15.4}{50} + \frac{5.8}{44} + \frac{5.4}{41} \frac{4.6}{28-25} \frac{3.5}{23}$ $\frac{4.0}{35} \frac{5.3}{14} \frac{4.8}{17} \frac{4.3}{30} \frac{3.6}{33} \frac{5.9}{46} \frac{5.0}{50}$ ✓

* $\frac{3.7}{50} \frac{3.2}{40} \frac{5.5}{29} \frac{6.6}{24} \frac{5.8}{22} \frac{5.8}{19}$ $\frac{6.1}{5.6} \frac{7.5}{15} \frac{6.3}{19} \frac{6.2}{36} \frac{10.9}{42} \frac{5.0}{50}$ ✓

* $\frac{3.5}{50} + \frac{3.0}{38} \frac{5.8}{26} \frac{6.3}{24-22} \frac{5.2}{21}$ $\frac{5.3}{4.9} \frac{6.6}{17} \frac{5.7}{20-27} \frac{5.4}{31} \frac{11.6}{41} \frac{5.0}{50}$ ✓

$\frac{3.2}{50} \frac{2.1}{35} \frac{6.2}{25-22} \frac{4.8}{17}$ $\frac{5.0}{4.6} \frac{6.3}{18} \frac{5.0}{22-25} \frac{5.1}{33} \frac{10.4}{40} \frac{5.0}{50}$ ✓

$\frac{8.2}{50} \frac{7.3}{33} \frac{5.2}{17}$ $\frac{4.8}{4.6} \frac{4.9}{11} \frac{4.6}{21} \frac{9.2}{39} \frac{5.0}{50}$ ✓

$\frac{10.4}{50}$ $\frac{8.6}{29} \frac{5.5}{17}$ $\frac{5.1}{4.9} \frac{5.8}{13} \frac{5.1}{15} \frac{5.2}{20} \frac{10.4}{38} \frac{5.0}{50}$ ✓

$\frac{6.3}{50} \frac{7.0}{31} \frac{7.0}{22} \frac{5.5}{17}$ $\frac{5.0}{4.9} \frac{5.3}{13} \frac{5.3}{17} \frac{6.3}{39} \frac{9.5}{43} \frac{5.0}{50}$ ✓

$\frac{5.3}{50} \frac{5.3}{22} \frac{6.6}{19-17} \frac{5.6}{14}$ $\frac{5.7}{5.1} \frac{6.3}{16} \frac{8.0}{45} \frac{5.0}{50}$ ✓

$\frac{8.9}{50} \frac{8.4}{36} \frac{8.7}{20-18} \frac{6.1}{14}$ $\frac{6.5}{5.6} \frac{6.2}{13} \frac{7.9}{24} \frac{7.7}{30} \frac{5.0}{50}$ ✓

Spike PP

26' Lt. $\frac{6.0}{50} \frac{6.2}{41} \frac{6.5}{28} \frac{6.5}{16} \frac{3.7}{14}$ $\frac{3.9}{3.4} \frac{4.7}{12} \frac{5.0}{14} \frac{6.3}{27} \frac{6.3}{30} \frac{6.3}{50}$ ✓

$\frac{6.0}{50} \frac{6.6}{33} \frac{6.7}{16} \frac{4.0}{13}$ $\frac{4.0}{3.6} \frac{5.1}{12} \frac{6.5}{19} \frac{6.6}{25} \frac{6.7}{30} \frac{6.7}{50}$ ✓

$\frac{5.4}{50} \frac{6.0}{26} \frac{6.2}{17} \frac{3.6}{13}$ $\frac{4.0}{3.5} \frac{4.5}{13} \frac{5.2}{15} \frac{6.9}{23} \frac{7.0}{28} \frac{7.3}{41} \frac{5.0}{50}$ ✓

Sta.	L	π	-	Elev.
		931.90		
64 + 50			3.8	28.1
65			4.3	27.6
+ 50			4.5	27.4
66			4.6	27.3
+ 50			4.9	27.0
67			5.3	26.5
+ 50			5.8	26.1
T.P.	4.33	930.53	5.70	26.20
68			4.7	25.8
+ 30			4.7	25.8
69			4.8	25.7
+ 65	21' x 32' C.M.		4.8	25.7
69			4.1	25.8

$$\begin{array}{cccccccccccc} \underline{6.3} & \underline{6.6} & \underline{6.6} & \underline{4.1} & & \underline{4.4} & \underline{5.1} & \underline{6.7} & \underline{7.7} & \underline{7.9} & \underline{7.6} & \\ 50 & 32 & 17 & 12 & 3.8 & 12 & 18 & 24 & 28 & 37 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} \underline{6.9} & \underline{7.2} & \underline{7.4} & \underline{6.8} & \underline{4.5} & & \underline{4.8} & \underline{6.0} & \underline{7.3} & \underline{8.3} & \underline{7.8} & \\ 50 & 40 & 26 & 18 & 14 & 4.3 & 15 & 22 & 36 & 42 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} \underline{6.9} & \underline{7.1} & \underline{7.2} & \underline{5.0} & & \underline{4.9} & \underline{6.0} & \underline{7.2} & \underline{8.1} & \underline{7.8} & \underline{7.3} & \\ 50 & 35 & 21 & 15 & 4.5 & 15 & 20 & 27 & 35 & 38 & 50 & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} \underline{5.7} & \underline{6.2} & \underline{6.6} & \underline{6.0} & \underline{5.2} & & \underline{4.9} & \underline{6.4} & \underline{7.4} & \underline{6.6} & \underline{5.2} & \\ 50 & 34 & 23 & 20 & 14 & 4.6 & 14 & 25 & 28 & 42 & 46 & 50 \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} \underline{3.8} & \underline{4.2} & \underline{4.7} & \underline{6.7} & \underline{5.4} & & \underline{5.4} & \underline{5.2} & \underline{6.8} & \underline{4.4} & \underline{4.2} & \\ 50 & 35 & 31 & 23 & 20 & 16 & 4.9 & 15 & 20 & 23 & 26 & 30 & 50 \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} \underline{5.8} & \underline{4.9} & \underline{3.8} & \underline{7.1} & \underline{5.9} & & \underline{5.7} & \underline{6.5} & \underline{3.0} & \underline{2.3} & \underline{2.9} & \\ 50 & 42 & 32 & 22 & 19 & 15 & 5.3 & 17 & 21 & 24 & 31 & 37 & 50 \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} \underline{9.9} & \underline{9.1} & \underline{8.7} & \underline{6.4} & & \underline{6.3} & \underline{7.3} & \underline{6.7} & \underline{3.8} & \underline{4.0} & & \\ 50 & 36 & 22 & 16 & 5.8 & 17 & 23 & 32 & 38 & 50 & \checkmark \end{array}$$

T.P. R.L. 68-

$$\begin{array}{cccccccccccc} \underline{11.6} & \underline{11.3} & \underline{10.6} & \underline{5.0} & & \underline{4.8} & \underline{8.8} & \underline{9.3} & \underline{3.8} & & & \\ 50 & 33 & 20 & 11 & 4.7 & 15 & 26 & 36 & 50 & & & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} \underline{11.5} & \underline{11.3} & \underline{10.6} & \underline{5.0} & & \underline{5.1} & \underline{10.0} & \underline{10.4} & \underline{7.3} & & & \\ 50 & 29 & 18 & 12 & 4.7 & 16 & 25 & 37 & 50 & & & \checkmark \end{array}$$

$$\begin{array}{cccccccccccc} \underline{10.8} & \underline{10.1} & \underline{9.6} & \underline{5.1} & & \underline{5.1} & \underline{8.0} & \underline{9.3} & \underline{10.7} & \underline{11.0} & & \\ 50 & 28 & 16 & 10 & 4.8 & 15 & 24 & 28 & 36 & 50 & & \checkmark \end{array}$$

FL 19.18

$$\begin{array}{cccccccccccc} \underline{10.8} & \underline{9.8} & \underline{9.4} & \underline{11.35} & \underline{5.3} & & \underline{5.1} & \underline{11.45} & \underline{9.3} & \underline{10.0} & \underline{11.0} & \\ 50 & 29 & 19 & 13 & 9 & 4.8 & 16 & 19 & 22 & 29 & 50 & \checkmark \end{array}$$

FL Buried 19.08

$$\begin{array}{cccccccccccc} \underline{10.0} & \underline{9.4} & \underline{9.4} & \underline{5.3} & & \underline{5.2} & \underline{7.8} & \underline{10.3} & \underline{11.1} & & & \\ 50 & 28 & 16 & 10 & 4.7 & 15 & 24 & 33 & 50 & & & \checkmark \end{array}$$

Sto.	f	$\bar{x}$	-	Glcv.
		930.53		
69 + 50			4.5	26.0
+ 88 P.T.			4.4	26.1
70			4.5	26.0
+ 30			4.4	26.1
+ 55 P.C.			4.4	26.1
71			4.3	26.2
+ 50			4.3	26.2
72			4.5	26.0
+ 50			4.7	25.8
73			5.3	25.2
+ 54 P.T.			5.6	24.9
74			6.0	24.5

$\frac{3.0}{50}$ $\frac{3.0}{38}$ $\frac{3.9}{27}$ $\frac{6.5}{21-18}$ $\frac{5.1}{13}$ $\frac{4.5}{19}$ $\frac{5.2}{29}$ $\frac{7.6}{36}$ $\frac{9.2}{50}$ $\frac{10.2}{50}$ ✓

$\frac{10.0}{50}$ $\frac{10.2}{35}$ $\frac{6.0}{21-17}$ $\frac{4.8}{13}$ $\frac{4.8}{16}$ $\frac{7.7}{28-32}$ $\frac{6.0}{35}$ $\frac{7.1}{45}$ $\frac{7.8}{50}$ ✓

$\frac{11.0}{50}$ $\frac{11.0}{36}$ $\frac{5.8}{21-18}$ $\frac{4.8}{13}$ $\frac{4.5}{17}$ $\frac{5.1}{27-31}$ $\frac{7.7}{35}$ $\frac{5.4}{43}$ $\frac{6.4}{50}$ $\frac{7.2}{50}$ ✓

$\frac{11.0}{50}$ $\frac{11.1}{36}$ $\frac{5.7}{21-17}$ $\frac{4.8}{14}$ $\frac{4.8}{16}$ $\frac{7.0}{26-30}$ $\frac{3.7}{35}$ $\frac{5.2}{50}$ ✓

$\frac{7.0}{50}$ $\frac{1.1}{41}$ $\frac{0.5}{33}$ $\frac{5.7}{22-18}$ $\frac{4.8}{14}$ $\frac{4.8}{15}$ $\frac{5.9}{24-28}$ $\frac{2.3}{36}$ $\frac{3.9}{50}$ ✓

$\frac{5.3}{50}$ $\frac{3.7}{38}$ $\frac{2.7}{29}$ $\frac{5.8}{22}$ $\frac{5.6}{15}$ $\frac{4.8}{12}$ $\frac{4.9}{13}$ $\frac{6.6}{14}$ $\frac{4.2}{27-31}$ $\frac{5.1}{36}$ $\frac{6.0}{44}$ $\frac{6.0}{50}$ ✓

$\frac{5.4}{50}$ $\frac{4.3}{40}$ $\frac{3.7}{31}$ $\frac{6.6}{23-19}$ $\frac{4.8}{13}$ $\frac{4.8}{43}$ $\frac{5.6}{14}$ $\frac{6.9}{22}$ $\frac{6.1}{27}$ $\frac{7.0}{44}$ $\frac{7.0}{50}$ ✓

$\frac{4.2}{50}$ $\frac{3.3}{41}$ $\frac{2.3}{30}$ $\frac{5.9}{22-18}$ $\frac{4.8}{13}$ $\frac{4.8}{45}$ $\frac{7.1}{15}$ $\frac{6.5}{27}$ $\frac{7.5}{37}$ $\frac{7.5}{50}$ ✓

$\frac{0.6}{50}$ $\frac{0.0}{36}$ $\frac{5.5}{23}$ $\frac{6.2}{18}$ $\frac{5.3}{15}$ $\frac{5.1}{47}$ $\frac{5.8}{14}$ $\frac{7.4}{23}$ $\frac{7.2}{29}$ $\frac{7.2}{50}$ ✓

$\frac{4.3}{50}$ $\frac{4.2}{39}$ $\frac{4.4}{29}$ $\frac{6.8}{22-19}$ $\frac{5.6}{13}$ $\frac{5.8}{5.3}$ $\frac{6.2}{15}$ $\frac{7.2}{19}$ $\frac{8.3}{25}$ $\frac{8.9}{29}$ $\frac{9.0}{39}$ $\frac{9.0}{50}$ ✓

$\frac{9.6}{50}$ $\frac{8.6}{25}$ $\frac{6.2}{14}$ $\frac{5.9}{5.6}$ $\frac{6.0}{14}$ $\frac{7.2}{20}$ $\frac{5.8}{23-27}$ $\frac{5.4}{31}$ $\frac{5.4}{50}$ ✓

$\frac{10.7}{50}$ $\frac{8.8}{23}$ $\frac{6.5}{14}$ $\frac{6.4}{6.0}$ $\frac{7.4}{14}$ $\frac{5.8}{23-26}$ $\frac{5.8}{30}$ $\frac{5.8}{50}$ ✓

Sta.	+	⌒	-	Elev.
		930.53		
74+50			6.3	24.2
75			6.6	23.9
+50			6.7	23.8
T.P.	5.66	929.38	6.81	923.72
76			5.5	23.9
+50			5.3	24.1
77			5.7	23.7
+50			6.1	23.3
78 + 10 PC			6.5	22.9
+50			6.9	22.5
79			6.4	23.0
+ 32			5.4	24.0
+ 40			5.2	24.2

$\frac{11.4}{50}$	$\frac{10.6}{26}$	$\frac{7.6}{18}$	$\frac{7.3}{17}$	$\frac{6.8}{14}$	$\frac{7.6}{17}$	$\frac{7.5}{22}$	$\frac{9.1}{38}$	$\frac{8.4}{50}$	
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<u>11.3</u>	<u>10.1</u>	<u>7.1</u>	<u>7.0</u>	<u>7.6</u>	<u>7.6</u>	<u>9.0</u>	<u>8.8</u>	<u>7.7</u>	
50	22	13	66	14	17	23	26	39	50

<u>11.3</u>	<u>10.5</u>	<u>9.8</u>	<u>7.4</u>		<u>7.3</u>	<u>7.5</u>	<u>8.0</u>	<u>7.1</u>	<u>6.2</u>	✓
50	32	23	14	6.7	14	20	28	33	50	

$\frac{10.3}{50}$	$\frac{9.0}{25}$	$\frac{7.5}{17}$	$\frac{6.1}{13}$	$\frac{6.0}{5.5}$	$\frac{7.3}{14}$	$\frac{7.2}{26}$	$\frac{6.3}{30}$	$\frac{4.5}{33}$	$\frac{4.5}{50}$
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9.2 9.1 9.2 7.3 6.1 5.7 6.2 6.9 6.3 5.2 4.2
50 37 28 20 15 5.5 9 16 25 32 37 50 ✓

$\frac{7.0}{50}$ $\frac{6.9}{33}$ $\frac{7.6}{19}$ $\frac{6.2}{74}$ $\frac{6.0}{15}$ $\frac{6.2}{22}$ $\frac{6.9}{25}$ $\frac{5.8}{27}$ $\frac{5.0}{30}$ $\frac{5.0}{50}$ ✓

$\begin{array}{r} 5.5 \\ \underline{5.0} \\ 50 \end{array}$
 $\begin{array}{r} 5.0 \\ \underline{33} \\ 33 \end{array}$
 $\begin{array}{r} 6.2 \\ \underline{26} \\ 26 \end{array}$
 $\begin{array}{r} 7.6 \\ \underline{23-18} \\ 14 \end{array}$
 $\begin{array}{r} 6.4 \\ \underline{6.1} \\ 6.1 \end{array}$
 $\begin{array}{r} 6.4 \\ \underline{21} \\ 21 \end{array}$
 $\begin{array}{r} 6.9 \\ \underline{24-26} \\ 27 \end{array}$
 $\begin{array}{r} 6.3 \\ \underline{27} \\ 33 \end{array}$
 $\begin{array}{r} 5.8 \\ \underline{33} \\ 50 \end{array}$
 $\begin{array}{r} 4.7 \\ \underline{50} \\ 50 \end{array}$

<u>42</u>	<u>3.8</u>	<u>80</u>	<u>7.0</u>	<u>6.8</u>		<u>6.8</u>	<u>6.7</u>	<u>7.6</u>	<u>7.3</u>	
50	35	22-19	16	14	65	16	20	29	50	✓

$\frac{72}{50}$	$\frac{62}{35}$	$\frac{69}{27}$	$\frac{86}{24}$	$\frac{70}{20}$	$\frac{71}{16}$	$\frac{72}{20}$	$\frac{79}{42}$	$\frac{83}{50}$	✓
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$\frac{9.4}{50}$ $\frac{8.7}{38}$ $\frac{7.3}{31}$ $\frac{6.8}{15}$ 6.4 $\frac{6.8}{16}$ $\frac{7.1}{22}$ $\frac{7.2}{44}$ $\frac{6.9}{50}$ ✓

$\frac{5.8}{50}$	$\frac{5.6}{42}$	$\frac{5.6}{25}$	$\frac{5.5}{26}$	$\frac{5.7}{30}$	$\frac{7.2}{36}$	$\frac{7.2}{50}$
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$$\begin{array}{r} 5.3 \\ \underline{50} \end{array} \quad \begin{array}{r} 5.4 \\ \underline{19} \end{array} \quad 5.2 \quad \begin{array}{r} 5.2 \\ \underline{52} \end{array} \quad \begin{array}{r} 5.0 \\ \underline{50} \end{array}$$

Sta.	+	K	-	Elev.
		929.38.		
79 + 51.75 ^{PT}	± New Brighton Rd.	5.10	24.28	9
B.M.	2.32	927.07.	4.66	924.72. (924.72)
+67			2.8	24.3
+76			2.9	24.2
80			3.5	23.6
+50			5.7	21.4
81			7.0	20.1
+50			7.2	19.9
+57 F.L. R.R. Over 3.5' x 30' x 50' Conc.				
T.P.	3.97	922.81	8.23	918.84.
82			3.0	19.8
+41 ⁴⁴	24" x 76' C.M. ³²		3.7	19.1
83			4.5	18.3
+50			3.6	19.2

$\frac{5.20}{50}$

$\frac{5.10}{50}$

$\frac{5.01}{50}$

✓

Spike P.P. N.W. Cor. Co. Rd. C of New Brighton Rd.

$\frac{3.3}{50}$ $\frac{3.1}{37}$ $\frac{3.0}{2.8}$ $\frac{3.3}{33}$ $\frac{2.9}{43}$ $\frac{2.7}{50}$

✓

$\frac{4.0}{50}$ $\frac{4.2}{44}$ $\frac{3.2}{38}$ $\frac{3.2}{23}$ 2.9 $\frac{3.1}{25}$ $\frac{2.8}{30}$ $\frac{3.4}{42}$ $\frac{4.9}{50}$

✓

$\frac{3.4}{50}$ $\frac{3.9}{33}$ $\frac{6.6}{29-26}$ $\frac{3.8}{22}$ 3.5 $\frac{3.7}{15}$ $\frac{5.1}{26}$ $\frac{5.4}{50}$

✓

$\frac{3.1}{50}$ $\frac{4.3}{38}$ $\frac{7.5}{22-18}$ $\frac{6.1}{13}$ 5.7 $\frac{6.3}{13}$ $\frac{8.7}{19-23}$ $\frac{5.7}{26}$ $\frac{5.2}{35}$ $\frac{4.4}{50}$

✓

$\frac{4.1}{50}$ $\frac{4.8}{42}$ $\frac{7.7}{27}$ $\frac{8.9}{15}$ $\frac{7.4}{13}$ 7.0 $\frac{7.7}{15}$ $\frac{10.2}{20-22}$ $\frac{7.3}{27}$ $\frac{7.0}{50}$

✓

$\frac{9.8}{50}$ $\frac{10.5}{31}$ $\frac{10.2}{19}$ $\frac{7.5}{12}$ 7.2 $\frac{7.7}{13}$ $\frac{12.2}{23}$ $\frac{13.6}{43}$ $\frac{11.4}{50}$

✓

09.22

N. FL. 18.32

08.75

1785 S. FL.

$\frac{12.8}{50}$ $\frac{12.1}{27}$ $\frac{3.3}{12}$ $\frac{3.6}{12}$ $\frac{12.0}{27}$ $\frac{12.4}{35}$ $\frac{12.0}{41}$ $\frac{14.5}{45-48}$ $\frac{12.1}{50}$

✓

FL. 07.24

FL. 707.72

$\frac{14.2}{50}$ $\frac{15.3}{44}$ $\frac{15.3}{44}$ $\frac{13.5}{38}$ $\frac{12.4}{25}$ $\frac{14.4}{13}$ 3.7 $\frac{4.3}{14}$ $\frac{11.6}{24}$ $\frac{15.0}{32}$ $\frac{15.6}{33}$ $\frac{14.0}{42}$ $\frac{13.3}{50}$

✓

$\frac{13.9}{52}$ $\frac{15.1}{50-47}$ $\frac{13.9}{43}$ $\frac{12.2}{26}$ $\frac{4.8}{13}$ 4.5 $\frac{4.8}{12}$ $\frac{11.8}{24}$ $\frac{13.5}{35}$ $\frac{13.6}{50}$

✓

$\frac{14.3}{50}$ $\frac{13.9}{39}$ $\frac{13.7}{29}$ $\frac{4.0}{13}$ 3.6 $\frac{4.0}{13}$ $\frac{12.0}{27}$ $\frac{13.6}{23}$ $\frac{14.0}{39}$ $\frac{13.2}{50}$

L

Sta.	+	$\bar{\Delta}$	-	Elev.
		922.81.		
84			15	21.3
+50			+0.3	923.1
+75			+0.6	23.4
T.P.	9.52	932.23	0.10	922.71.
85			8.0	24.2
+50			6.7	25.5
86			5.4	26.8
+50			4.1	28.1
87			2.7	29.5
+22			2.2	30.0
+50			1.7	30.5
T.P.	10.94	941.60	1.57	930.66. 1
88				26.8
+50				28.1

$$\begin{array}{r} 13.9 \\ 50 \end{array} \quad \begin{array}{r} 13.2 \\ 43 \end{array} \quad \begin{array}{r} 2.7 \\ 17 \end{array} \quad \begin{array}{r} 1.9 \\ 1.5 \end{array} \quad \begin{array}{r} 12.3 \\ 14 \end{array} \quad \begin{array}{r} 13.4 \\ 42 \end{array} \quad \begin{array}{r} 12.2 \\ 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 11.1 \\ 50 \end{array} \quad \begin{array}{r} 10.8 \\ 43 \end{array} \quad \begin{array}{r} 9.0 \\ 37 \end{array} \quad \begin{array}{r} 0.8 \\ 20 \end{array} \quad +0.3 \quad \begin{array}{r} 0.2 \\ 16 \end{array} \quad \begin{array}{r} 9.3 \\ 31 \end{array} \quad \begin{array}{r} 10.6 \\ 37 \end{array} \quad \begin{array}{r} 11.4 \\ 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 10.8 \\ 50 \end{array} \quad \begin{array}{r} 9.9 \\ 41 \end{array} \quad \begin{array}{r} 10.3 \\ 16 \end{array} \quad +0.6 \quad \begin{array}{r} 10.2 \\ 16 \end{array} \quad \begin{array}{r} 8.0 \\ 33 \end{array} \quad \begin{array}{r} 9.4 \\ 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 17.5 \\ 50 \end{array} \quad \begin{array}{r} 15.4 \\ 35 \end{array} \quad \begin{array}{r} 8.5 \\ 18 \end{array} \quad \begin{array}{r} 8.0 \\ 8.0 \end{array} \quad \begin{array}{r} 8.5 \\ 15 \end{array} \quad \begin{array}{r} 14.1 \\ 27 \end{array} \quad \begin{array}{r} 15.9 \\ 36 \end{array} \quad \begin{array}{r} 16.0 \\ 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 44 \end{array} \quad \begin{array}{r} 5.6 \\ 37 \end{array} \quad \begin{array}{r} 4.5 \\ 33 \end{array} \quad \begin{array}{r} 8.4 \\ 24 \end{array} \quad \begin{array}{r} 7.2 \\ 21 \end{array} \quad \begin{array}{r} 7.2 \\ 14 \end{array} \quad \begin{array}{r} 8.1 \\ 21 \end{array} \quad \begin{array}{r} 6.2 \\ 26 \end{array} \quad \begin{array}{r} 6.0 \\ 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 7.0 \\ 24 \end{array} \quad \begin{array}{r} 6.0 \\ 20 \end{array} \quad \begin{array}{r} 5.9 \\ 16 \end{array} \quad \begin{array}{r} 7.1 \\ 5.4 \end{array} \quad \begin{array}{r} 5.9 \\ 13 \end{array} \quad \begin{array}{r} 7.1 \\ 17 \end{array} \quad \begin{array}{r} 6.2 \\ 24 \end{array} \quad \begin{array}{r} 4.7 \\ 29 \end{array} \quad \checkmark$$

$$\begin{array}{r} 5.1 \\ 24 \end{array} \quad \begin{array}{r} 4.4 \\ 20 \end{array} \quad \begin{array}{r} 4.3 \\ 17 \end{array} \quad \begin{array}{r} 5.2 \\ 4.1 \end{array} \quad \begin{array}{r} 4.2 \\ 13 \end{array} \quad \begin{array}{r} 1.7 \\ 15 \end{array} \quad \begin{array}{r} 4.2 \\ 20 \end{array} \quad \begin{array}{r} 1.7 \\ 25 \end{array} \quad \checkmark$$

$$\begin{array}{r} 0.4 \\ 30 \end{array} \quad \begin{array}{r} 2.3 \\ 23 \end{array} \quad \begin{array}{r} 3.1 \\ 14 \end{array} \quad \begin{array}{r} 3.2 \\ 2.7 \end{array} \quad \begin{array}{r} 4.1 \\ 14 \end{array} \quad \begin{array}{r} 1.4 \\ 17 \end{array} \quad \begin{array}{r} 1.4 \\ 28 \end{array} \quad \checkmark$$

$$\begin{array}{r} 0.3 \\ 25 \end{array} \quad \begin{array}{r} 1.9 \\ 21 \end{array} \quad \begin{array}{r} 2.4 \\ 15 \end{array} \quad \begin{array}{r} 2.2 \\ 2.2 \end{array} \quad \begin{array}{r} 2.7 \\ 14 \end{array} \quad \begin{array}{r} 3.5 \\ 17 \end{array} \quad \begin{array}{r} 2.1 \\ 25 \end{array} \quad \checkmark$$

$$\begin{array}{r} 1.3 \\ 24 \end{array} \quad \begin{array}{r} 2.1 \\ 15 \end{array} \quad \begin{array}{r} 1.9 \\ 1.7 \end{array} \quad \begin{array}{r} 0.8 \\ 13 \end{array} \quad \begin{array}{r} 0.8 \\ 23 \end{array} \quad \checkmark$$

$$\begin{array}{r} 9.3 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 43 \end{array} \quad (14.8) \quad \begin{array}{r} 6.8 \\ 38 \end{array} \quad \begin{array}{r} 6.9 \\ 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 4.5 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 48 \end{array} \quad (13.5) \quad \begin{array}{r} 3.7 \\ 35 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array} \quad \checkmark$$

Sta.	L	K	-	Elev.
		941.60		
87				29.5
+22				30.0
+50				30.5
88			10.3	31.3
+50			10.1	31.5
89			10.2	31.4
+50			10.6	31.0
90			11.3	30.3
+50			12.2	29.4
91			13.4	28.2
T.P.	472	933.02	13.30	928.30
+50			5.9	27.1
92			7.2	25.8

$$\frac{3.7}{50} \quad \frac{3.4}{47} \quad (12.1) \quad \frac{3.0}{37} \quad \frac{3.0}{50} \quad \checkmark$$

$$\frac{2.7}{50} \quad \frac{2.7}{43} \quad (11.6) \quad \frac{2.8}{37} \quad \frac{2.9}{50} \quad \checkmark$$

$$\frac{3.0}{50} \quad \frac{2.7}{35} \quad (11.1) \quad \frac{2.3}{34} \quad \frac{2.6}{45} \quad \frac{5.6}{50} \quad \checkmark$$

$$\frac{3.0}{50} \quad \frac{3.5}{31} \quad \frac{9.1}{20} \quad \frac{10.6}{15} \quad \frac{11.0}{15} \quad \frac{11.4}{20} \quad \frac{10.0}{29} \quad \frac{3.4}{38} \quad \frac{3.7}{47} \quad \frac{5.8}{50} \quad \checkmark$$

$$\frac{4.3}{50} \quad \frac{4.0}{31} \quad \frac{9.9}{20} \quad \frac{10.7}{14} \quad \frac{10.7}{15} \quad \frac{10.8}{24} \quad \frac{5.0}{30} \quad \frac{4.8}{44} \quad \frac{9.0}{50} \quad \checkmark$$

$$\frac{5.1}{50} \quad \frac{5.1}{34} \quad \frac{5.0}{27} \quad \frac{10.2}{18} \quad \frac{10.6}{13} \quad \frac{10.7}{16} \quad \frac{10.3}{25} \quad \frac{5.3}{32} \quad \frac{5.6}{46} \quad \frac{8.0}{50} \quad \checkmark$$

$$\frac{5.8}{50} \quad \frac{6.0}{28} \quad \frac{9.5}{21} \quad \frac{11.0}{14} \quad \frac{10.9}{15} \quad \frac{11.2}{27} \quad \frac{7.0}{29} \quad \frac{7.0}{48} \quad \frac{8.9}{50} \quad \checkmark$$

$$\frac{7.3}{50} \quad \frac{7.3}{32} \quad \frac{6.9}{25} \quad \frac{10.9}{17} \quad \frac{11.6}{12} \quad \frac{12.0}{16} \quad \frac{11.2}{20} \quad \frac{7.2}{25} \quad \frac{7.4}{46} \quad \frac{9.9}{50} \quad \checkmark$$

$$\frac{8.4}{50} \quad \frac{8.3}{32} \quad \frac{7.6}{25} \quad \frac{12.0}{20} \quad \frac{12.6}{12} \quad \frac{12.7}{14} \quad \frac{12.3}{18} \quad \frac{11.0}{22} \quad \frac{7.7}{24} \quad \frac{7.9}{50} \quad \checkmark$$

$$\frac{8.6}{50} \quad \frac{8.6}{32} \quad \frac{8.2}{25} \quad \frac{13.4}{15} \quad \frac{13.8}{11} \quad \frac{13.9}{14} \quad \frac{14.2}{17} \quad \frac{8.9}{25} \quad \frac{9.8}{50} \quad \checkmark$$

$$\frac{1.5}{50} \quad \frac{2.0}{33} \quad \frac{1.7}{26} \quad \frac{6.1}{12} \quad \frac{6.5}{14} \quad \frac{6.7}{17} \quad \frac{2.5}{24} \quad \frac{2.9}{50} \quad \checkmark$$

$$\frac{3.1}{50} \quad \frac{3.5}{32} \quad \frac{3.3}{26} \quad \frac{7.4}{17} \quad \frac{7.7}{13} \quad \frac{8.3}{17} \quad \frac{3.2}{24} \quad \frac{3.3}{34} \quad \frac{3.6}{50} \quad \checkmark$$

Sta.	+	K	-	E/cv.
		933.02		
92+50			8.0	25.0
93			9.0	24.0
+50			10.1	22.9
94			11.3	21.7
T.P.	1.38	921.78	12.62	920.40
+50			1.2	20.6
95			2.3	19.5
+50			3.5	18.3
96			4.3	17.5
+50			4.9	16.9
97			5.4	16.4
+50			5.9	15.9
98			6.1	15.7

$\frac{4.2}{50}$ $\frac{4.4}{32}$ $\frac{4.4}{24}$ $\frac{6.4}{20}$ $\frac{8.3}{12}$ 8.0 $\frac{8.4}{13}$ $\frac{9.3}{16-18}$ $\frac{4.7}{23}$ $\frac{4.7}{50}$

$\frac{5.3}{50}$ $\frac{5.8}{33}$ $\frac{5.7}{26}$ $\frac{9.1}{16}$ $\frac{9.3}{12}$ 9.0 $\frac{9.5}{13}$ $\frac{10.2}{14-16}$ $\frac{6.2}{22}$ $\frac{6.1}{50}$

$\frac{8.5}{50}$ $\frac{8.0}{31}$ $\frac{7.8}{21}$ $\frac{10.4}{14}$ 10.1 $\frac{10.3}{13}$ $\frac{11.3}{16-18}$ $\frac{9.3}{23}$ $\frac{9.1}{42}$ $\frac{9.3}{50}$

$\frac{10.8}{50}$ $\frac{11.3}{33}$ $\frac{11.5}{22}$ $\frac{11.8}{13}$ 11.3 $\frac{11.8}{14}$ $\frac{13.6}{17-23}$ $\frac{13.0}{24}$ $\frac{12.8}{28}$ $\frac{13.4}{50}$

Spoke T.P. 94 +

$\frac{2.6}{50}$ $\frac{3.0}{30}$ $\frac{3.1}{20}$ $\frac{1.7}{14}$ 1.2 $\frac{1.6}{12}$ $\frac{3.7}{19}$ $\frac{4.2}{31}$ $\frac{4.1}{50}$

$\frac{5.0}{50}$ $\frac{5.2}{30}$ $\frac{5.0}{19}$ $\frac{2.9}{14}$ 2.3 $\frac{2.8}{13}$ $\frac{4.2}{17}$ $\frac{5.1}{26}$ $\frac{5.8}{35}$ $\frac{6.2}{50}$

$\frac{7.0}{50}$ $\frac{6.5}{30}$ $\frac{7.6}{20}$ $\frac{4.0}{14}$ 3.5 $\frac{4.2}{12}$ $\frac{6.7}{18}$ $\frac{7.0}{30}$ $\frac{7.3}{50}$

$\frac{8.1}{50}$ $\frac{7.5}{30}$ $\frac{7.6}{18}$ $\frac{4.9}{13}$ 4.3 $\frac{4.8}{12}$ $\frac{7.3}{19}$ $\frac{7.7}{35}$ $\frac{7.8}{50}$

$\frac{8.5}{50}$ $\frac{8.0}{30}$ $\frac{8.2}{19}$ $\frac{5.6}{13}$ 4.9 $\frac{5.4}{13}$ $\frac{8.4}{19}$ $\frac{8.7}{34}$ $\frac{8.7}{50}$

$\frac{9.4}{50}$ $\frac{9.2}{30}$ $\frac{9.3}{22}$ $\frac{7.9}{17}$ $\frac{6.1}{12}$ 5.4 $\frac{5.8}{11}$ $\frac{9.5}{22}$ $\frac{9.8}{34}$ $\frac{9.5}{50}$

$\frac{9.8}{50}$ $\frac{9.7}{31}$ $\frac{10.0}{20}$ $\frac{6.5}{12}$ 5.9 $\frac{6.3}{12}$ $\frac{9.5}{19}$ $\frac{10.4}{29}$ $\frac{10.5}{50}$

$\frac{10.1}{50}$ $\frac{10.0}{31}$ $\frac{10.2}{22}$ $\frac{8.9}{17}$ $\frac{6.9}{12}$ 6.4 $\frac{8.9}{21}$ $\frac{10.5}{36}$ $\frac{10.8}{50}$

Sta.	+	π	-	Elev.
		921.78		
98+50			6.2	15.6
99			6.2	15.6
T.P.	466	920.26	6.18	915.60
+50			4.6	15.7
100			4.7	15.6
+50			4.7	15.6
101			4.7	15.6
+50			4.7	15.6
102			4.8	15.5
+50			5.0	15.3
103			5.0	15.3
+50			5.0	15.3
104			4.6	15.7

Sta.	+	∇	-	Elev.
		920.26 Cone. R.R.		
104 + 16	24" x 32' C.M.	4.4	15.9	
+ 50		4.3	16.0	
105		4.2	16.1	
+ 35		4.3	16.0	
+ 36 Inv. 24" x 20" x 48" R.R. Cone. Cul.				
+ 55		4.1	16.2	
+ 65		4.0	16.3	
+ 75		4.0	16.3	
+ 89.07	± Snelling	3.7	16.6	
B.M.	6.86	922.74	442	915.84 (915.88)
106 + 07		6.3	16.4	
+ 22		6.4	16.3	
+ 49	15" x 7' C.M.	6.4	16.3	
107		6.5	16.2	

11.36

10.83

FL FL
 $\frac{6.6}{50}$ $\frac{7.2}{33}$ $\frac{9.3}{23}$ $\frac{8.7}{17}$ $\frac{8.90}{17}$ $\frac{5.2}{15}$ $\frac{4.8}{11}$ $\frac{9.43}{15}$ $\frac{8.8}{16}$ $\frac{9.8}{26}$ $\frac{10.5}{37}$ $\frac{10.9}{50}$

$\frac{7.1}{50}$ $\frac{7.1}{40}$ $\frac{8.5}{26}$ $\frac{8.8}{20}$ $\frac{5.0}{13}$ $\frac{4.6}{10}$ $\frac{11.0}{23}$ $\frac{10.8}{33}$ $\frac{11.2}{50}$

$\frac{7.6}{50}$ $\frac{8.0}{33}$ $\frac{9.0}{25}$ $\frac{9.6}{23}$ $\frac{4.7}{11}$ $\frac{4.5}{9}$ $\frac{10.5}{23}$ $\frac{11.4}{36}$ $\frac{11.8}{50}$

$\frac{8.3}{50}$ $\frac{8.6}{28}$ $\frac{8.7}{23}$ $\frac{4.6}{12}$ $\frac{4.5}{9}$ $\frac{10.0}{22}$ $\frac{11.7}{31}$ $\frac{11.9}{50}$

$\frac{12.52}{H.F.L.}$

07.74

$\frac{13.95}{S.F.L.}$

06.31

$\frac{8.4}{50}$ $\frac{8.0}{32}$ $\frac{7.5}{29}$ $\frac{5.9}{22}$ $\frac{4.9}{17}$ $\frac{4.6}{17}$ $\frac{8.0}{29}$ $\frac{9.5}{39}$ $\frac{10.5}{50}$

$\frac{6.9}{50}$ $\frac{6.9}{41}$ $\frac{5.3}{35}$ $\frac{4.7}{24}$ $\frac{4.6}{32}$ $\frac{5.1}{50}$

$\frac{4.5}{50}$ $\frac{4.2}{17}$ $\frac{4.2}{18}$ $\frac{4.4}{50}$

$\frac{3.8}{50}$ $\frac{4.0}{50}$

Spike H. Pole SE Cor Snelling & Co. Rd. "C"

$\frac{6.3}{50}$ $\frac{6.3}{21}$ $\frac{6.5}{21}$ $\frac{7.1}{50}$

$\frac{8.6}{50}$ $\frac{7.5}{45}$ $\frac{7.0}{40}$ $\frac{6.5}{28}$ $\frac{6.7}{20}$ $\frac{7.2}{29}$ $\frac{12.3}{43}$ $\frac{12.6}{50}$

FL N. 0.66

$\frac{9.0}{50}$ $\frac{9.1}{32}$ $\frac{8.6}{25}$ $\frac{7.6}{19}$ $\frac{6.8}{11}$ $\frac{7.1}{11}$ $\frac{11.70}{20}$ $\frac{10.2}{21}$ $\frac{11.4}{30}$ $\frac{12.4}{40}$ $\frac{12.6}{50}$

$\frac{7.6}{50}$ $\frac{7.3}{31}$ $\frac{8.5}{18}$ $\frac{7.1}{12}$ $\frac{7.6}{13}$ $\frac{7.8}{23}$ $\frac{7.9}{32}$ $\frac{8.2}{42}$ $\frac{10.2}{50}$

Sta.	+	π	-	Elev.
		922.74		
107 + 50			6.2	16.5
108			5.8	16.9
+ 24			5.5	17.2
+ 28			5.5	17.2
+ 60			5.3	17.4
109			5.2	17.5
+ 50			4.9	17.8
110			4.7	18.0
+ 50			4.6	18.1
111			4.4	18.3
+ 50			4.1	18.6
112			4.2	18.5
T.P.	5.27	923.85	4.16	918.58.

Sta.		π	-	Elev.
------	--	-------	---	-------

923.85

112 +50			5.2	18.7
---------	--	--	-----	------

113			4.8	19.1
-----	--	--	-----	------

+50			4.6	19.3
-----	--	--	-----	------

114			4.5	19.4
-----	--	--	-----	------

+50			4.5	19.4
-----	--	--	-----	------

115			4.5	19.4
-----	--	--	-----	------

+50			4.1	19.8
-----	--	--	-----	------

116			3.3	20.6
-----	--	--	-----	------

+50			2.6	21.3
-----	--	--	-----	------

117			1.9	22.0
-----	--	--	-----	------

T.P.	9.71	931.56	2.00	921.85
------	------	--------	------	--------

+50			8.7	22.9
-----	--	--	-----	------

118			7.9	23.7
-----	--	--	-----	------

$$\begin{array}{r} 112 \\ 50 \end{array} \quad \begin{array}{r} 111 \\ 44 \end{array} \quad \begin{array}{r} 88 \\ 21 \end{array} \quad \begin{array}{r} 59 \\ 17 \end{array} \quad 5.2 \quad \begin{array}{r} 5.5 \\ 12 \end{array} \quad \begin{array}{r} 7.1 \\ 16-21 \end{array} \quad \begin{array}{r} 4.0 \\ 27 \end{array} \quad \begin{array}{r} 2.8 \\ 39 \end{array} \quad \begin{array}{r} 3.9 \\ 47 \end{array} \quad \begin{array}{r} 4.7 \\ 50 \end{array}$$

$$\begin{array}{r} 9.1 \\ 50 \end{array} \quad \begin{array}{r} 9.1 \\ 74 \end{array} \quad \begin{array}{r} 7.6 \\ 34 \end{array} \quad \begin{array}{r} 7.3 \\ 18 \end{array} \quad \begin{array}{r} 5.6 \\ 13 \end{array} \quad \begin{array}{r} 4.8 \\ 48 \end{array} \quad \begin{array}{r} 5.1 \\ 11 \end{array} \quad 15.20 \quad \begin{array}{r} 3.6 \\ 26 \end{array} \quad \begin{array}{r} 2.7 \\ 36 \end{array} \quad \begin{array}{r} 2.7 \\ 42 \end{array} \quad \begin{array}{r} 4.6 \\ 50 \end{array}$$

$$\begin{array}{r} 8.2 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 43 \end{array} \quad \begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 6.4 \\ 18 \end{array} \quad \begin{array}{r} 5.2 \\ 14 \end{array} \quad \begin{array}{r} 4.6 \\ 46 \end{array} \quad \begin{array}{r} 4.9 \\ 12 \end{array} \quad \begin{array}{r} 6.8 \\ 15-20 \end{array} \quad \begin{array}{r} 3.4 \\ 26 \end{array} \quad \begin{array}{r} 2.6 \\ 40 \end{array} \quad \begin{array}{r} 3.9 \\ 50 \end{array}$$

$$\begin{array}{r} 8.1 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 42 \end{array} \quad \begin{array}{r} 6.7 \\ 20 \end{array} \quad \begin{array}{r} 5.1 \\ 12 \end{array} \quad 4.5 \quad \begin{array}{r} 5.0 \\ 11 \end{array} \quad \begin{array}{r} 6.8 \\ 15-19 \end{array} \quad \begin{array}{r} 4.0 \\ 24 \end{array} \quad \begin{array}{r} 3.2 \\ 40 \end{array} \quad \begin{array}{r} 4.6 \\ 50 \end{array}$$

$$\begin{array}{r} 8.4 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 33 \end{array} \quad \begin{array}{r} 7.5 \\ 18 \end{array} \quad \begin{array}{r} 5.1 \\ 12 \end{array} \quad 4.5 \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 7.8 \\ 19-22 \end{array} \quad \begin{array}{r} 6.0 \\ 25 \end{array} \quad \begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 5.4 \\ 50 \end{array}$$

$$\begin{array}{r} 7.8 \\ 50 \end{array} \quad \begin{array}{r} 8.4 \\ 39 \end{array} \quad \begin{array}{r} 7.4 \\ 34 \end{array} \quad \begin{array}{r} 8.2 \\ 25 \end{array} \quad \begin{array}{r} 8.0 \\ 18 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 4.5 \\ 45 \end{array} \quad \begin{array}{r} 4.9 \\ 12 \end{array} \quad \begin{array}{r} 8.6 \\ 19 \end{array} \quad \begin{array}{r} 7.3 \\ 37 \end{array} \quad \begin{array}{r} 6.4 \\ 50 \end{array}$$

$$\begin{array}{r} 8.5 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 33 \end{array} \quad \begin{array}{r} 7.7 \\ 18 \end{array} \quad \begin{array}{r} 4.7 \\ 12 \end{array} \quad 4.1 \quad \begin{array}{r} 4.5 \\ 10 \end{array} \quad \begin{array}{r} 8.0 \\ 21 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 8.1 \\ 50 \end{array} \quad \begin{array}{r} 7.7 \\ 33 \end{array} \quad \begin{array}{r} 8.0 \\ 23 \end{array} \quad \begin{array}{r} 7.5 \\ 18 \end{array} \quad \begin{array}{r} 3.8 \\ 12 \end{array} \quad 3.3 \quad \begin{array}{r} 3.7 \\ 12 \end{array} \quad \begin{array}{r} 7.8 \\ 22 \end{array} \quad \begin{array}{r} 8.6 \\ 50 \end{array}$$

$$\begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 30 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array} \quad \begin{array}{r} 3.1 \\ 12 \end{array} \quad 2.6 \quad \begin{array}{r} 3.0 \\ 12 \end{array} \quad \begin{array}{r} 8.0 \\ 25 \end{array} \quad \begin{array}{r} 8.4 \\ 34 \end{array} \quad \begin{array}{r} 7.6 \\ 37 \end{array} \quad \begin{array}{r} 7.8 \\ 50 \end{array}$$

$$\begin{array}{r} 3.4 \\ 50 \end{array} \quad \begin{array}{r} 4.0 \\ 29 \end{array} \quad \begin{array}{r} 4.5 \\ 27 \end{array} \quad \begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 2.6 \\ 11 \end{array} \quad 1.9 \quad \begin{array}{r} 2.4 \\ 11 \end{array} \quad \begin{array}{r} 6.2 \\ 21 \end{array} \quad \begin{array}{r} 6.4 \\ 31 \end{array} \quad \begin{array}{r} 5.6 \\ 38 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 7.2 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 27 \end{array} \quad \begin{array}{r} 7.3 \\ 29 \end{array} \quad \begin{array}{r} 9.2 \\ 16 \end{array} \quad \begin{array}{r} 9.1 \\ 12 \end{array} \quad 8.7 \quad \begin{array}{r} 9.0 \\ 7 \end{array} \quad \begin{array}{r} 9.8 \\ 17 \end{array} \quad \begin{array}{r} 9.5 \\ 22 \end{array} \quad \begin{array}{r} 9.0 \\ 31 \end{array} \quad \begin{array}{r} 9.6 \\ 38 \end{array} \quad \begin{array}{r} 10.8 \\ 50 \end{array}$$

$$\begin{array}{r} 3.0 \\ 50 \end{array} \quad \begin{array}{r} 2.8 \\ 30 \end{array} \quad \begin{array}{r} 8.5 \\ 19 \end{array} \quad \begin{array}{r} 8.2 \\ 12 \end{array} \quad 7.9 \quad \begin{array}{r} 8.3 \\ 11 \end{array} \quad \begin{array}{r} 9.2 \\ 16-19 \end{array} \quad \begin{array}{r} 6.4 \\ 23 \end{array} \quad \begin{array}{r} 7.6 \\ 44 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array}$$

Sto.	+	π	-	Elev.
		931.56.		
118 + 50			7.2	244
+ 97 RC			6.6	25.0
119 + 13			6.3	25.3
+ 50			5.7	25.9
120			5.5	26.1
+ 50			5.6	26.0
121			5.8	25.8
+ 08 AT			5.8	25.8
+ 42			5.9	25.7
+ 78			5.7	25.9
T.P.	7.34	933.23	5.67	925.89
122			7.1	26.1
+ 50			6.7	26.5

$\frac{2.3}{50}$ $\frac{1.7}{34}$ $\frac{2.2}{29}$ $\frac{7.5}{16}$ $\frac{7.7}{11}$ 7.2 $\frac{7.6}{12}$ $\frac{8.0}{18}$ $\frac{5.1}{23}$ $\frac{5.8}{39}$ $\frac{6.9}{50}$

$\frac{4.1}{50}$ $\frac{5.0}{21}$ $\frac{7.1}{15}$ $\frac{6.9}{12}$ 6.6 $\frac{6.7}{9}$ $\frac{7.1}{15}$ $\frac{4.8}{19}$ $\frac{5.5}{47}$ $\frac{7.0}{50}$

$\frac{7.3}{50}$ $\frac{6.7}{23}$ $\frac{6.8}{14}$ 6.3 $\frac{6.7}{13}$ $\frac{7.3}{16}$ $\frac{4.4}{21}$ $\frac{4.5}{46}$ $\frac{7.1}{50}$

$\frac{6.7}{50}$ $\frac{6.1}{24}$ $\frac{6.1}{16}$ 5.7 $\frac{6.0}{9}$ $\frac{6.5}{16}$ $\frac{3.7}{20}$ $\frac{3.8}{42}$ $\frac{7.6}{50}$

$\frac{4.8}{50}$ $\frac{4.5}{27}$ $\frac{3.7}{22}$ $\frac{5.8}{15}$ 5.5 $\frac{5.8}{8}$ $\frac{6.8}{14-17}$ $\frac{3.6}{22}$ $\frac{3.6}{45}$ $\frac{6.6}{50}$

$\frac{6.3}{50}$ $\frac{5.6}{29}$ $\frac{4.5}{23}$ $\frac{5.8}{16}$ 5.6 $\frac{6.1}{9}$ $\frac{7.2}{13-17}$ $\frac{4.7}{20}$ $\frac{4.6}{45}$ $\frac{7.0}{50}$

$\frac{9.9}{50}$ $\frac{9.0}{25}$ $\frac{6.3}{16}$ 5.8 $\frac{6.2}{10}$ $\frac{8.4}{15-20}$ $\frac{7.2}{24}$ $\frac{8.2}{50}$

$\frac{10.3}{50}$ $\frac{9.8}{26}$ $\frac{6.6}{16}$ 5.8 $\frac{6.3}{9}$ $\frac{8.6}{15-20}$ $\frac{7.8}{24}$ $\frac{8.3}{34}$ $\frac{8.4}{50}$

$\frac{11.1}{50}$ $\frac{10.4}{24}$ $\frac{7.1}{20}$ $\frac{6.4}{16}$ 5.9 $\frac{6.4}{10}$ $\frac{9.6}{18}$ $\frac{10.9}{24}$ $\frac{11.1}{41}$ $\frac{9.9}{44}$ $\frac{9.5}{50}$

$\frac{10.8}{50}$ $\frac{10.2}{23}$ $\frac{6.3}{16}$ 5.7 $\frac{6.5}{10}$ $\frac{8.2}{17}$ $\frac{10.5}{21-26}$ $\frac{9.8}{29}$ $\frac{9.5}{38}$ $\frac{8.9}{50}$

$\frac{12.0}{50}$ $\frac{11.6}{26}$ $\frac{7.6}{16}$ 7.1 $\frac{7.9}{10}$ $\frac{9.1}{14}$ $\frac{10.9}{23}$ $\frac{10.2}{38}$ $\frac{9.6}{50}$

$\frac{11.5}{50}$ $\frac{10.9}{25}$ $\frac{7.1}{16}$ 6.7 $\frac{6.9}{8}$ $\frac{7.5}{12}$ $\frac{8.8}{21}$ $\frac{9.6}{50}$

Sta.	+	π	-	Elev.
		933.23		
123			6.5	26.7
+50			6.3	26.5
124			5.9	27.3
+50			5.4	27.8
125			4.9	28.3
+50			4.9	27.3
126			5.0	28.2
+50			4.9	28.3
127			4.7	28.5
+50			4.4	28.8
128			4.3	28.9
+50			4.2	29.0

$\frac{10.8}{50}$ $\frac{10.8}{24}$ $\frac{6.7}{16}$ $\frac{6.7}{6.5}$ $\frac{7.6}{7}$ $\frac{10.0}{10}$ $\frac{10.1}{17}$ $\frac{9.5}{35}$ $\frac{9.5}{50}$

$\frac{8.2}{50}$ $\frac{8.2}{24}$ $\frac{6.6}{14}$ $\frac{6.6}{6.3}$ $\frac{6.8}{10}$ $\frac{9.4}{20}$ $\frac{9.7}{28}$ $\frac{11.2}{40}$ $\frac{11.5}{50}$

$\frac{5.3}{50}$ $\frac{5.1}{23}$ $\frac{6.1}{13}$ $\frac{6.1}{59}$ $\frac{6.4}{9}$ $\frac{9.6}{21}$ $\frac{9.6}{26}$ $\frac{7.5}{35}$ $\frac{8.6}{50}$

$\frac{4.1}{50}$ $\frac{4.1}{22}$ $\frac{5.0}{17}$ $\frac{5.6}{14}$ $\frac{5.6}{54}$ $\frac{5.9}{11}$ $\frac{8.0}{20}$ $\frac{8.2}{36}$ $\frac{5.1}{45}$ $\frac{6.0}{50}$

$\frac{3.5}{50}$ $\frac{4.1}{21}$ $\frac{5.1}{14}$ $\frac{5.1}{49}$ $\frac{5.7}{12}$ $\frac{8.1}{23}$ $\frac{7.8}{30}$ $\frac{6.8}{34}$ $\frac{4.7}{38}$ $\frac{4.7}{50}$

$\frac{3.8}{50}$ $\frac{3.6}{23}$ $\frac{5.1}{13}$ $\frac{5.1}{49}$ $\frac{5.3}{12}$ $\frac{6.7}{15}$ $\frac{7.3}{19}$ $\frac{7.6}{31}$ $\frac{4.5}{39}$ $\frac{4.1}{50}$

$\frac{4.6}{50}$ $\frac{4.8}{34}$ $\frac{4.8}{17}$ $\frac{5.1}{15}$ $\frac{5.1}{50}$ $\frac{5.6}{11}$ $\frac{6.3}{25}$ $\frac{6.2}{33}$ $\frac{7.7}{36}$ $\frac{6.7}{40}$ $\frac{6.6}{50}$

$\frac{4.7}{50}$ $\frac{5.3}{28}$ $\frac{5.2}{14}$ $\frac{5.2}{49}$ $\frac{5.5}{11}$ $\frac{6.4}{13-16}$ $\frac{5.9}{19}$ $\frac{6.1}{33}$ $\frac{7.9}{38}$ $\frac{6.1}{50}$

$\frac{4.1}{50}$ $\frac{4.8}{23}$ $\frac{4.5}{18}$ $\frac{4.9}{14}$ $\frac{4.9}{47}$ $\frac{5.2}{10}$ $\frac{6.4}{16}$ $\frac{5.8}{22}$ $\frac{5.3}{31}$ $\frac{6.9}{39}$ $\frac{5.6}{42}$ $\frac{5.7}{50}$

$\frac{4.1}{50}$ $\frac{4.5}{26}$ $\frac{4.3}{19}$ $\frac{4.7}{13}$ $\frac{4.7}{44}$ $\frac{4.9}{18}$ $\frac{5.8}{16}$ $\frac{5.2}{30}$ $\frac{5.9}{37}$ $\frac{6.4}{50}$

$\frac{3.9}{50}$ $\frac{4.2}{34}$ $\frac{4.0}{20}$ $\frac{4.6}{18}$ $\frac{4.6}{43}$ $\frac{4.8}{10}$ $\frac{5.8}{15}$ $\frac{4.9}{38}$ $\frac{5.3}{38}$ $\frac{5.1}{50}$

$\frac{4.0}{50}$ $\frac{4.3}{32}$ $\frac{4.1}{19}$ $\frac{4.1}{42}$ $\frac{4.8}{10}$ $\frac{5.6}{13}$ $\frac{4.9}{18}$ $\frac{5.0}{39}$ $\frac{4.7}{45}$ $\frac{4.0}{50}$

Sta.	+	π	-	Elev.
		933.23		
129			4.0	29.2
+50			3.8	29.4
130			4.2	29.0
+50			4.7	28.5
T.P.	3.88	933.23	3.88	929.35
131			5.2	28.0
+50			5.6	27.6
+80			5.8	27.4
132			5.9	27.3
+10.65	$\pm$ Hamline		6.0	27.2
B.M.			5.98	927.25 (927.19)

HAMLINE

B.M.	3.71	926.92		923.21
132+10.65	$\pm$ Hamline		4.0	22.9

$$\begin{array}{r} 55 \\ 50 \end{array} \quad \begin{array}{r} 5.9 \\ 24 \end{array} \quad \begin{array}{r} 4.3 \\ 17 \end{array} \quad 4.0 \quad \begin{array}{r} 4.8 \\ 10 \end{array} \quad \begin{array}{r} 5.4 \\ 15 \end{array} \quad \begin{array}{r} 5.4 \\ 41 \end{array} \quad \begin{array}{r} 4.0 \\ 44 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 25 \end{array} \quad \begin{array}{r} 4.3 \\ 17 \end{array} \quad 3.8 \quad \begin{array}{r} 4.0 \\ 13 \end{array} \quad \begin{array}{r} 4.4 \\ 24 \end{array} \quad \begin{array}{r} 4.4 \\ 43 \end{array} \quad \begin{array}{r} 4.5 \\ 50 \end{array}$$

$$\begin{array}{r} 6.6 \\ 50 \end{array} \quad \begin{array}{r} 6.7 \\ 25 \end{array} \quad \begin{array}{r} 4.6 \\ 17 \end{array} \quad 4.2 \quad \begin{array}{r} 4.6 \\ 10 \end{array} \quad \begin{array}{r} 5.0 \\ 30 \end{array} \quad \begin{array}{r} 4.8 \\ 44 \end{array} \quad \begin{array}{r} 5.7 \\ 48 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 7.1 \\ 31 \end{array} \quad \begin{array}{r} 7.7 \\ 29 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad 4.7 \quad \begin{array}{r} 5.3 \\ 8 \end{array} \quad \begin{array}{r} 5.1 \\ 14 \end{array} \quad \begin{array}{r} 5.1 \\ 30 \end{array} \quad \begin{array}{r} 4.4 \\ 45 \end{array} \quad \begin{array}{r} 5.3 \\ 50 \end{array}$$

$$\begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 7.4 \\ 32 \end{array} \quad \begin{array}{r} 6.9 \\ 21 \end{array} \quad \begin{array}{r} 5.6 \\ 15 \end{array} \quad 5.2 \quad \begin{array}{r} 5.6 \\ 9 \end{array} \quad \begin{array}{r} 4.8 \\ 15 \end{array} \quad \begin{array}{r} 4.6 \\ 26 \end{array} \quad 4.2 \quad 5.0$$

$$\begin{array}{r} 8.0 \\ 50 \end{array} \quad \begin{array}{r} 7.2 \\ 33 \end{array} \quad \begin{array}{r} 6.9 \\ 21 \end{array} \quad \begin{array}{r} 6.2 \\ 16 \end{array} \quad 5.6 \quad \begin{array}{r} 5.9 \\ 10 \end{array} \quad \begin{array}{r} 4.8 \\ 15 \end{array} \quad \begin{array}{r} 5.6 \\ 30 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

$$\begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 25 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \end{array} \quad 5.8 \quad \begin{array}{r} 6.3 \\ 19 \end{array} \quad \begin{array}{r} 5.8 \\ 28 \end{array} \quad \begin{array}{r} 5.9 \\ 50 \end{array}$$

$$\begin{array}{r} 7.1 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 26 \end{array} \quad 5.9 \quad \begin{array}{r} 6.1 \\ 23 \end{array} \quad \begin{array}{r} 7.0 \\ 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 25 \end{array} \quad 6.0 \quad \begin{array}{r} 6.1 \\ 25 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

Top Men Co. Rd C at Hamline

Spike G.P. N.E. Cor. C and Hamline

$$\begin{array}{r} 4.7 \\ 50 \end{array}$$

$$4.0$$

$$\begin{array}{r} 3.8 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.
		926.92		
132 + 29			4.3	21.5
+ 39			4.3	21.5
133			4.5	21.4
+ 50			4.5	21.4
134			4.5	21.4
B.M.	3.41	926.61	3.71	923.21
+ 50			4.2	22.4
135			4.1	22.5
+ 30			4.3	22.3
+ 70			4.5	22.1
136			4.6	22.0
+ 40			4.9	21.7
+ 85			5.4	21.2

$$\frac{5.8}{50} \quad \frac{5.7}{37} \quad \frac{5.1}{28} \quad 4.3 \quad \frac{4.4}{32} \quad \frac{4.6}{50}$$

$$\frac{5.4}{50} \quad \frac{5.4}{26} \quad \frac{5.2}{19} \quad 4.3 \quad \frac{4.7}{24} \quad \frac{4.5}{50}$$

$$\frac{6.7}{50} \quad \frac{6.1}{29} \quad \frac{5.2}{28} \quad \frac{4.9}{24} \quad \frac{5.2}{16} \quad \frac{4.7}{12} \quad 4.5 \quad \frac{4.8}{13} \quad \frac{5.4}{16} \quad \frac{4.6}{26} \quad \frac{3.6}{50}$$

$$\frac{7.6}{50} \quad \frac{7.0}{31} \quad \frac{6.1}{28} \quad \frac{6.0}{16} \quad \frac{4.9}{12} \quad 4.5 \quad \frac{5.0}{13} \quad \frac{5.6}{16} \quad \frac{6.0}{50}$$

$$\frac{6.9}{50} \quad \frac{7.1}{25} \quad \frac{6.5}{20} \quad \frac{6.4}{16} \quad \frac{5.1}{13} \quad \frac{4.9}{11} \quad 4.5 \quad \frac{4.8}{9} \quad \frac{5.7}{19} \quad \frac{5.3}{24} \quad \frac{5.4}{50}$$

$$\frac{5.9}{50} \quad \frac{5.9}{27} \quad \frac{6.1}{22-19} \quad \frac{4.6}{14} \quad 4.2 \quad \frac{4.5}{11} \quad \frac{5.2}{17} \quad \frac{4.6}{25} \quad \frac{4.3}{50}$$

$$\frac{4.0}{50} \quad \frac{3.6}{31} \quad \frac{3.5}{24} \quad \frac{4.7}{15} \quad 4.1 \quad \frac{4.6}{12} \quad \frac{5.2}{15-17} \quad \frac{3.5}{22} \quad \frac{3.3}{39} \quad \frac{3.4}{50}$$

$$\frac{4.0}{50} \quad \frac{3.2}{27} \quad \frac{2.8}{24} \quad \frac{3.4}{18} \quad \frac{4.6}{14} \quad 4.3 \quad \frac{4.5}{11} \quad \frac{4.8}{15} \quad \frac{3.6}{17} \quad \frac{2.7}{24} \quad \frac{2.9}{35} \quad \frac{2.6}{50}$$

$$\frac{4.6}{50} \quad \frac{3.6}{27} \quad \frac{3.0}{24} \quad \frac{3.4}{19} \quad \frac{4.8}{14} \quad 4.5 \quad \frac{4.9}{13} \quad \frac{5.0}{15} \quad \frac{2.9}{15} \quad \frac{2.8}{23} \quad \frac{2.2}{35} \quad \frac{2.2}{50}$$

$$\frac{5.4}{50} \quad \frac{4.9}{35} \quad \frac{3.8}{25} \quad \frac{4.1}{19} \quad \frac{5.0}{14} \quad 4.6 \quad \frac{5.3}{15} \quad \frac{2.7}{24} \quad \frac{3.0}{27} \quad \frac{3.2}{36} \quad \frac{2.6}{39} \quad \frac{3.1}{50}$$

$$\frac{6.3}{50} \quad \frac{5.3}{28} \quad \frac{5.1}{23} \quad \frac{5.0}{17} \quad \frac{5.3}{14} \quad 4.9 \quad \frac{5.0}{11} \quad \frac{5.2}{16} \quad \frac{4.5}{22-24} \quad \frac{5.0}{27} \quad \frac{4.2}{39} \quad \frac{4.6}{50}$$

$$\frac{4.5}{50} \quad \frac{3.9}{30} \quad \frac{4.4}{22} \quad \frac{5.7}{13} \quad 5.4 \quad \frac{5.7}{12} \quad \frac{6.0}{18-21} \quad \frac{4.9}{25} \quad \frac{4.8}{39} \quad \frac{5.4}{50}$$

Sta.	+	π	-	Elev
		926.61		
137+00			5.7	20.9
T.P.	8.37	929.22	5.76	920.85
+24			8.7	20.5
+50			9.2	20.0
138			10.2	19.2
+50			11.4	17.8
+74			11.9	17.3
139			12.5	16.7
+50			14.1	15.1
+70			14.8	14.4
T.P.	6.43	923.11	12.54	916.68
140			9.6	13.5
+32			10.5	12.6
+68			11.4	11.7

$\frac{4.1}{50}$	$\frac{3.3}{28}$	$\frac{4.0}{23}$	$\frac{6.2}{17}$	$\frac{6.0}{13}$	$\frac{5.9}{57}$	$\frac{5.9}{12}$	$\frac{3.7}{16}$	$\frac{4.1}{24}$	$\frac{4.8}{39}$	$\frac{4.8}{50}$
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$\frac{5.3}{50}$	$\frac{4.7}{31}$	$\frac{5.3}{24}$	$\frac{8.8}{18}$	$\frac{9.0}{13}$	$\frac{8.7}{8.7}$	$\frac{9.0}{11}$	$\frac{9.0}{15}$	$\frac{3.6}{26}$	$\frac{3.8}{33}$	$\frac{4.4}{39}$	$\frac{6.0}{50}$
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$\frac{4.0}{50}$	$\frac{3.6}{33}$	$\frac{4.4}{25}$	$\frac{8.7}{18}$	$\frac{9.4}{13}$	$\frac{9.4}{9.2}$	$\frac{8.9}{12}$	$\frac{3.5}{18}$	$\frac{3.3}{24}$	$\frac{5.0}{39}$	$\frac{5.0}{50}$
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$\frac{3.0}{50}$	$\frac{2.7}{40}$	$\frac{2.5}{28}$	$\frac{9.3}{16}$	$\frac{10.4}{13}$	$\frac{10.4}{10.2}$	$\frac{10.4}{12}$	$\frac{4.6}{17}$	$\frac{2.8}{25}$	$\frac{2.9}{40}$	$\frac{4.5}{43}$	$\frac{4.5}{50}$
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$\frac{2.1}{50}$	$\frac{2.3}{30}$	$\frac{2.5}{27}$	$\frac{10.6}{16}$	$\frac{11.7}{10}$	$\frac{11.6}{11.4}$	$\frac{11.1}{12}$	$\frac{5.3}{16}$	$\frac{4.3}{23}$	$\frac{3.6}{25}$	$\frac{5.3}{43}$	$\frac{5.3}{50}$
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$\frac{4.1}{50}$	$\frac{3.7}{33}$	$\frac{3.6}{25}$	$\frac{11.4}{16}$	$\frac{12.1}{11}$	$\frac{12.3}{11.9}$	$\frac{11.8}{13}$	$\frac{4.7}{15}$	$\frac{4.9}{25}$	$\frac{4.2}{38}$	$\frac{5.7}{41}$	$\frac{5.7}{50}$
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$\frac{6.9}{50}$	$\frac{6.7}{35}$	$\frac{6.4}{25}$	$\frac{12.3}{16}$	$\frac{12.9}{12}$	$\frac{12.8}{12.5}$	$\frac{12.5}{12}$	$\frac{6.0}{16}$	$\frac{6.3}{25}$	$\frac{5.5}{38}$	$\frac{6.8}{42}$	$\frac{6.8}{50}$
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$\frac{13.1}{50}$	$\frac{12.8}{29}$	$\frac{12.1}{27}$	$\frac{12.4}{22}$	$\frac{14.5}{17}$	$\frac{14.6}{12}$	$\frac{14.4}{14.1}$	$\frac{13.9}{13}$	$\frac{9.6}{16}$	$\frac{9.6}{26}$	$\frac{8.9}{38}$	$\frac{9.5}{42}$	$\frac{9.5}{50}$
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$\frac{13.9}{50}$	$\frac{13.5}{37}$	$\frac{14.2}{28}$	$\frac{14.0}{22}$	$\frac{15.5}{16}$	$\frac{15.2}{12}$	$\frac{15.2}{14.8}$	$\frac{14.1}{13}$	$\frac{11.6}{18}$	$\frac{10.4}{23}$	$\frac{9.8}{27}$	$\frac{10.2}{43}$	$\frac{10.2}{50}$
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139

$\frac{7.8}{50}$	$\frac{8.7}{21}$	$\frac{9.7}{16}$	$\frac{10.0}{12}$	$\frac{9.6}{9.6}$	$\frac{9.9}{13}$	$\frac{9.7}{19}$	$\frac{2.1}{26}$	$\frac{6.7}{29}$	$\frac{4.2}{36}$	$\frac{3.8}{45}$	$\frac{3.7}{50}$
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$\frac{7.1}{50}$	$\frac{7.6}{33}$	$\frac{8.0}{25}$	$\frac{10.4}{17}$	$\frac{11.0}{12}$	$\frac{10.8}{10.5}$	$\frac{10.8}{14}$	$\frac{9.2}{18}$	$\frac{7.1}{20}$	$\frac{6.3}{26}$	$\frac{3.2}{30}$	$\frac{2.9}{36}$	$\frac{2.9}{50}$
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$\frac{6.0}{50}$	$\frac{5.9}{44}$	$\frac{7.1}{29}$	$\frac{11.5}{23}$	$\frac{11.8}{11.6}$	$\frac{11.6}{13}$	$\frac{11.6}{18}$	$\frac{9.1}{22}$	$\frac{8.1}{26}$	$\frac{7.4}{31}$	$\frac{3.6}{38}$	$\frac{2.8}{50}$
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Sta.	+	π	-	$\pm$ lev.
		923.11		
141			12.5	10.6
+34			13.7	09.4
+75			14.9	08.2
T.P.	0.41	911.67	1185	911.26
+91			3.6	08.1
142			3.9	07.8
+30			4.4	07.3
+69			5.2	06.5
143			5.7	06.0
+55	24" x 42" C.M.		6.4	05.3
144			6.3	05.4
B.M.	6.11	911.08	6.68	904.99 (904.97)
+38			5.6	05.5
+70			5.6	05.5

$\frac{5.6}{50}$ $\frac{6.7}{32}$ $\frac{11.9}{26}$ $\frac{13.2}{19}$ $\frac{13.1}{14}$ $\frac{12.9}{12.5}$ $\frac{13.2}{14}$ $\frac{2.7}{18}$ $\frac{8.5}{27}$ $\frac{5.5}{31}$ $\frac{4.9}{39}$ $\frac{4.8}{42}$ $\frac{4.8}{50}$

$\frac{8.1}{50}$ $\frac{8.1}{39}$ $\frac{8.2}{33}$ $\frac{13.6}{25}$ $\frac{14.1}{12}$ $\frac{14.1}{13.7}$ $\frac{15.2}{15}$ $\frac{14.3}{21-24}$ $\frac{13.6}{27}$ $\frac{9.4}{31}$ $\frac{8.8}{36}$ $\frac{8.8}{50}$

$\frac{14.1}{50}$ $\frac{14.5}{34}$ $\frac{14.8}{21}$ $\frac{16.8}{18.14}$ $\frac{15.3}{10}$ $\frac{15.4}{14.9}$ $\frac{17.5}{14}$ $\frac{19.8}{31}$ $\frac{16.4}{32-35}$ $\frac{16.0}{37}$ $\frac{16.0}{50}$

$\frac{5.6}{50}$ $\frac{7.8}{28}$ $\frac{3.8}{9}$ $\frac{3.9}{3.6}$ $\frac{8.4}{14}$ $\frac{10.6}{41}$ $\frac{12.1}{50}$

$\frac{10.5}{50}$ $\frac{11.1}{27}$ $\frac{10.0}{17}$ $\frac{4.5}{9}$ $\frac{4.2}{3.9}$ $\frac{5.7}{15}$ $\frac{10.2}{19}$ $\frac{11.8}{26}$ $\frac{12.5}{35}$ $\frac{12.5}{50}$

$\frac{13.8}{50}$ $\frac{12.5}{23}$ $\frac{4.8}{10}$ $\frac{5.2}{4.4}$ $\frac{12.9}{14}$ $\frac{14.5}{28}$ $\frac{14.1}{34}$ $\frac{14.1}{50}$

$\frac{15.0}{50}$ $\frac{13.2}{24}$ $\frac{5.5}{11}$ $\frac{5.5}{5.2}$ $\frac{12.3}{16}$ $\frac{13.7}{23}$ $\frac{14.7}{30}$ $\frac{15.0}{34}$ $\frac{15.0}{50}$

$\frac{14.8}{50}$ $\frac{14.7}{26}$ $\frac{13.7}{20}$ $\frac{6.1}{11}$ $\frac{6.0}{5.7}$ $\frac{12.6}{16}$ $\frac{16.1}{24}$ $\frac{15.3}{31}$ $\frac{15.2}{40}$ $\frac{15.2}{50}$

FL. 96.77

FL. 97.47

$\frac{150}{50}$ $\frac{148}{34}$ $\frac{14.9}{18}$ $\frac{13.3}{18}$ $\frac{6.9}{10}$ $\frac{6.5}{6.4}$ $\frac{14.2}{15}$ $\frac{13.4}{25}$ $\frac{14.0}{30}$ $\frac{15.4}{50}$

$\frac{15.5}{50}$ $\frac{15.1}{40}$ $\frac{14.1}{30}$ $\frac{13.5}{28}$ $\frac{12.6}{21}$ $\frac{8.1}{12}$ $\frac{6.6}{10}$ $\frac{6.6}{6.3}$ $\frac{12.4}{15}$ $\frac{14.2}{26}$ $\frac{14.4}{30}$ $\frac{14.4}{50}$

Spike T.P. 25' RL $\frac{14.2}{14.2} + 21$

$\frac{13.4}{50}$ $\frac{12.3}{22}$ $\frac{6.0}{10}$ $\frac{5.9}{5.6}$ $\frac{12.3}{17}$ $\frac{13.1}{31}$ $\frac{12.9}{38}$ $\frac{12.9}{50}$

$\frac{9.5}{50}$ $\frac{9.0}{23}$ $\frac{10.8}{21}$ $\frac{5.9}{17}$ $\frac{5.8}{18}$ $\frac{12.7}{32}$ $\frac{10.0}{36}$ $\frac{10.3}{40}$ $\frac{10.3}{50}$

Sta.	+	π	-	Elev.
		911.08		
145			5.5	05.6
442			5.5	05.6
175			5.1	06.0
146			4.7	06.4
T.P.	291	912.70	1.29	909.79
+50			5.5	07.2
147			4.5	08.2
+50			3.0	09.7
T.P.	1231	923.16	1.85	910.85
148			11.7	11.5
+50			10.0	13.2
+85			8.8	14.4
149			8.3	14.9
+50			6.8	16.4

2

$\frac{11.7}{50}$ $\frac{11.5}{28}$ $\frac{11.0}{21}$ $\frac{6.0}{11}$ $\frac{5.9}{5.5}$ $\frac{12.1}{18}$ $\frac{12.7}{36}$ $\frac{11.3}{43}$ $\frac{11.1}{50}$

$\frac{12.4}{50}$ $\frac{12.3}{25}$ $\frac{11.5}{23}$ $\frac{5.8}{11}$ $\frac{5.7}{5.5}$ $\frac{11.9}{16}$ $\frac{12.6}{27}$ $\frac{11.8}{37}$ $\frac{11.0}{38}$ $\frac{11.2}{44}$ $\frac{11.2}{50}$

$\frac{12.0}{50}$ $\frac{11.5}{36}$ $\frac{11.2}{23}$ $\frac{5.5}{11}$ $\frac{5.4}{5.1}$ $\frac{11.9}{16}$ $\frac{12.7}{28}$ $\frac{11.6}{36}$ $\frac{10.7}{40}$ $\frac{10.7}{50}$

$\frac{10.8}{50}$ $\frac{10.4}{29}$ $\frac{9.8}{22}$ $\frac{5.2}{12}$ $\frac{5.0}{4.7}$ $\frac{11.0}{17}$ $\frac{12.6}{28}$ $\frac{11.6}{33}$ $\frac{11.0}{35}$ $\frac{10.0}{36}$ $\frac{10.0}{40}$ $\frac{10.0}{44}$ $\frac{10.0}{50}$

Bolt End GR. Pt. 147

$\frac{8.3}{50}$ $\frac{8.6}{31}$ $\frac{10.8}{27}$ $\frac{10.5}{21}$ $\frac{6.3}{13}$ $\frac{5.7}{10}$ $\frac{5.7}{5.5}$ $\frac{6.2}{15}$ $\frac{12.2}{17}$ $\frac{13.3}{29}$ $\frac{9.5}{33}$ $\frac{9.0}{36}$ $\frac{10.0}{41}$ $\frac{10.0}{47}$ $\frac{9.9}{50}$

$\frac{4.1}{50}$ $\frac{4.3}{32}$ $\frac{7.5}{27}$ $\frac{8.2}{20}$ $\frac{5.4}{15}$ $\frac{4.8}{9}$ $\frac{4.5}{4.5}$ $\frac{4.9}{10}$ $\frac{4.9}{15}$ $\frac{7.3}{21}$ $\frac{7.5}{27}$ $\frac{6.9}{37}$ $\frac{8.0}{50}$

$\frac{0.1}{50}$ $\frac{1.3}{29}$ $\frac{5.3}{24}$ $\frac{5.6}{20}$ $\frac{3.7}{14}$ $\frac{3.3}{9}$ $\frac{3.0}{3.0}$ $\frac{3.3}{17}$ $\frac{4.0}{20}$ $\frac{4.6}{24}$ $\frac{3.5}{27}$ $\frac{3.1}{31}$ $\frac{4.6}{41}$ $\frac{5.2}{50}$

$\frac{7.7}{53}$ $\frac{9.0}{31}$ $\frac{14.3}{24}$ $\frac{14.3}{22}$ $\frac{13.3}{19}$ $\frac{12.2}{12}$ $\frac{11.7}{11.7}$ $\frac{12.0}{17}$ $\frac{12.3}{24}$ $\frac{11.2}{27}$ $\frac{12.2}{38}$ $\frac{13.3}{50}$

$\frac{7.1}{50}$ $\frac{7.2}{32}$ $\frac{12.5}{25}$ $\frac{12.2}{17}$ $\frac{10.7}{14}$ $\frac{10.0}{10.0}$ $\frac{10.3}{18}$ $\frac{10.6}{20}$ $\frac{9.2}{25}$ $\frac{9.4}{37}$ $\frac{10.5}{50}$

$\frac{7.3}{50}$ $\frac{7.8}{28}$ $\frac{9.6}{23}$ $\frac{9.4}{14}$ $\frac{8.8}{8.8}$ $\frac{8.9}{7}$ $\frac{9.5}{18}$ $\frac{7.5}{23}$ $\frac{8.7}{30}$ $\frac{9.7}{50}$

$\frac{7.7}{50}$ $\frac{8.4}{31}$ $\frac{7.9}{17}$ $\frac{8.8}{14}$ $\frac{9.0}{10}$ $\frac{8.3}{8.3}$ $\frac{8.4}{7}$ $\frac{8.8}{18}$ $\frac{7.0}{23}$ $\frac{8.2}{30}$ $\frac{9.2}{50}$

$\frac{9.3}{50}$ $\frac{9.4}{26}$ $\frac{8.8}{22}$ $\frac{7.9}{20}$ $\frac{7.0}{8}$ $\frac{6.8}{6.8}$ $\frac{7.2}{15}$ $\frac{7.0}{21}$ $\frac{7.3}{29}$ $\frac{7.8}{50}$

Sta	+	π	-	Elev
		923.16		
150			5.3	17.9
+50			3.7	19.5
T.P.	11.02	932.60	1.58	921.58
151			11.4	21.2
+50			9.7	22.9
152			8.4	24.2
+22			7.8	24.8
+50			7.0	25.6
153			5.6	27.0
T.P.	7.16	936.77	2.99	929.61
+21			9.1	27.7
+50			8.3	28.5
154			7.0	29.8
+50			5.9	30.9

X

$$\frac{78}{50} \frac{72}{27} \frac{72}{24} \frac{60}{21} \frac{61}{15} \frac{55}{10} 53 \frac{51}{11} \frac{57}{16} \frac{33}{24} \frac{54}{29} \frac{57}{50}$$

$$\frac{51}{50} \frac{45}{24} \frac{40}{18} \frac{42}{15} \frac{39}{8} 37 \frac{41}{11} \frac{41}{16} \frac{25}{23} \frac{33}{25} \frac{33}{27} \frac{23}{28} \frac{18}{30} \frac{23}{50}$$

$$\frac{91}{50} \frac{91}{22} \frac{94}{20} \frac{111}{17} \frac{119}{13} 114 \frac{118}{12} \frac{117}{16} \frac{86}{21} \frac{96}{27} \frac{83}{30} \frac{88}{50}$$

$$\frac{69}{50} \frac{66}{36} \frac{70}{21} \frac{92}{17} \frac{100}{11} 97 \frac{100}{11} \frac{103}{16} \frac{70}{23} \frac{81}{28} \frac{76}{33} \frac{81}{50}$$

$$\frac{55}{50} \frac{60}{38} \frac{68}{23} \frac{75}{17} \frac{88}{15} \frac{85}{9} 84 \frac{87}{11} \frac{89}{15} \frac{74}{20} \frac{84}{27} \frac{77}{33} \frac{81}{50}$$

$$\frac{50}{50} \frac{57}{37} \frac{68}{21} \frac{72}{16} \frac{81}{14} \frac{80}{8} 78 \frac{81}{10} \frac{85}{15} \frac{70}{21} \frac{80}{27} \frac{72}{33} \frac{77}{50}$$

$$\frac{48}{50} \frac{60}{34} \frac{64}{23} \frac{68}{17} \frac{75}{15} \frac{73}{9} 70 \frac{73}{10} \frac{74}{16} \frac{57}{20} \frac{68}{27} \frac{65}{31} \frac{67}{50}$$

$$\frac{43}{50} \frac{50}{34} \frac{44}{22} \frac{43}{16} \frac{61}{13} \frac{59}{9} 56 \frac{59}{16} \frac{34}{21} \frac{34}{25} \frac{19}{31} \frac{25}{37} \frac{28}{50}$$

$$\frac{80}{50} \frac{81}{35} \frac{70}{23} \frac{76}{17} \frac{95}{14} \frac{94}{9} 91 \frac{93}{10} \frac{92}{15} \frac{61}{21} \frac{62}{26} \frac{46}{31} \frac{54}{38} \frac{55}{50}$$

$$\frac{78}{50} \frac{76}{39} \frac{71}{23} \frac{79}{18} \frac{89}{14} \frac{86}{9} 83 \frac{85}{10} \frac{85}{15} \frac{62}{22} \frac{73}{25} \frac{60}{33} \frac{66}{50}$$

$$\frac{57}{50} \frac{62}{40} \frac{54}{30} \frac{52}{23} \frac{62}{18} \frac{76}{15} \frac{73}{9} 70 \frac{73}{10} \frac{74}{16} \frac{51}{22} \frac{63}{27} \frac{70}{38} \frac{71}{50}$$

$$\frac{75}{50} \frac{76}{38} \frac{69}{24} \frac{63}{22} \frac{64}{17} \frac{72}{15} \frac{67}{13} 59 \frac{61}{10} \frac{67}{18} \frac{60}{23} \frac{72}{26} \frac{84}{40} \frac{84}{50}$$

Sta	+	π	-	Elev
		936.77		
155			4.9	31.9
+20			45	32.3
+50			39	32.9
156			32	33.6
T.B	7.57	940.98	3.36	933.41
+40			7.1	33.9
+80			6.7	34.3
157			6.4	34.6
+50			52	35.8
B.M	1.65	940.72	1.86	939.12 939.07
181			4.1	36.6
158			3.8	36.9
+19		Edge Pave	3.78	36.94
+32.15			3.5	37.2

X

$$\frac{3.7}{50} \frac{2.5}{27} \frac{3.1}{18} \frac{5.5}{14} \frac{5.2}{10} 4.9 \frac{5.0}{9} \frac{5.3}{14} \frac{5.7}{18} \frac{5.8}{21} \frac{5.6}{23} \frac{6.0}{50}$$

$$\frac{2.7}{50} \frac{1.1}{33} \frac{1.5}{20} \frac{5.0}{15} \frac{4.8}{9} 4.5 \frac{4.7}{9} \frac{4.8}{16} \frac{3.5}{18} \frac{3.7}{36} \frac{4.6}{50}$$

$$\frac{1.1}{50} \frac{0.5}{34} \frac{0.8}{22} \frac{4.0}{17} \frac{4.2}{10} 3.9 \frac{4.2}{9} \frac{4.3}{14} \frac{2.7}{17} \frac{2.6}{28} \frac{4.2}{50}$$

$$\frac{0.6}{50} \frac{0.2}{38} \frac{0.1}{22} \frac{4.0}{14} \frac{3.5}{10} 3.2 \frac{3.7}{11} \frac{4.6}{16} \frac{5.5}{22} \frac{7.1}{50}$$

$$\frac{7.8}{50} \frac{9.0}{29} \frac{9.2}{22} \frac{9.6}{21} \frac{9.6}{17} \frac{7.5}{13} 7.1 \frac{7.5}{11} \frac{8.4}{16} \frac{9.2}{20} \frac{10.6}{25} \frac{13.5}{31} \frac{14.8}{50}$$

$$\frac{9.3}{50} \frac{9.3}{30} \frac{9.3}{18} \frac{7.5}{14} \frac{7.1}{10} 6.7 \frac{7.2}{8} \frac{7.8}{13} \frac{12.9}{21} \frac{13.9}{28} \frac{15.0}{50}$$

$$\frac{8.0}{50} \frac{4.2}{41} \frac{8.1}{25} \frac{9.5}{21} \frac{8.5}{16} \frac{6.9}{14} 6.4 \frac{6.8}{8} \frac{7.0}{13} \frac{12.6}{21} \frac{13.6}{30} \frac{14.1}{50}$$

$$\frac{3.3}{50} \frac{3.8}{36} \frac{4.2}{23} \frac{6.3}{18} \frac{6.2}{16} \frac{5.6}{11} 5.2 \frac{5.8}{12} \frac{6.7}{17} \frac{7.6}{23} \frac{9.0}{29} \frac{10.3}{37} \frac{11.9}{50}$$

Spk 17 15" Oak N.W. Cor C & Exp.

$$\frac{1.4}{53} \frac{2.6}{28} \frac{4.3}{25} \frac{4.4}{20} 4.1 \frac{4.7}{11} \frac{5.6}{18} \frac{6.4}{30} \frac{7.6}{43} \frac{7.1}{50}$$

$$\frac{3.0}{50} \frac{3.8}{35} \frac{4.2}{28} \frac{3.9}{24} 3.8 \frac{4.3}{15} \frac{5.2}{20} \frac{4.7}{24} \frac{6.5}{50}$$

$$\frac{3.4}{50} 3.8 \frac{4.1}{23} \frac{4.1}{50}$$

$$\frac{3.1}{50} 3.5 \frac{4.3}{50}$$

Sta	+	π	-	Elev
		940.72		
158+46			3.76	36.96
+40			5.2	35.5'
159			7.1	33.6
+50			9.4	31.3
+68			10.1	30.6
T.P.	3.30	933.70	10.32	930.40
160			4.4	29.3
+50			6.6	27.1
161			8.8	24.9
T.P.	1.35	925.40	9.65	924.05
+50			2.4	23.0
162			4.4	21.0
+50			5.7	19.7
+81		sect thru. X Drains	6.1	19.3

A

$$\frac{3.35}{50} \quad 3.8 \quad \frac{4.5}{50}$$

$$\frac{4.7}{50} \quad \frac{5.4}{29} \quad \frac{5.0}{12} \quad 5.2 \quad \frac{6.2}{13} \quad \frac{6.1}{28} \quad \frac{5.4}{44} \quad \frac{5.4}{50}$$

$$\frac{5.5}{75} \quad \frac{5.3}{50} \quad \frac{6.6}{28} \quad \frac{7.3}{25} \quad \frac{7.3}{16} \quad 7.1 \quad \frac{7.9}{7} \quad \frac{7.2}{12} \quad \frac{6.0}{34} \quad \frac{5.5}{50} \quad \frac{4.99}{\text{Floor Bldg.}}$$

$$\frac{5.6}{30} \quad \frac{7.7}{24} \quad \frac{9.8}{21} \quad \frac{9.4}{73} \quad 9.4 \quad \frac{9.8}{7} \quad \frac{9.1}{13} \quad \frac{10.1}{28} \quad \frac{12.7}{50}$$

$$\frac{5.2}{50} \quad \frac{8.2}{25} \quad \frac{10.5}{21} \quad \frac{10.2}{14} \quad 10.1 \quad \frac{10.6}{6} \quad \frac{11.2}{11} \quad \frac{12.6}{23} \quad \frac{13.7}{50}$$

$$\frac{1.0}{50} \quad \frac{2.5}{28} \quad \frac{4.8}{23} \quad \frac{4.6}{16} \quad \frac{4.2}{11} \quad 4.4 \quad \frac{4.4}{6} \quad \frac{5.7}{12} \quad \frac{6.1}{22} \quad \frac{7.8}{26} \quad \frac{7.6}{50}$$

$$\frac{3.7}{50} \quad \frac{5.1}{37} \quad \frac{6.5}{19} \quad \frac{6.4}{14} \quad 6.6 \quad \frac{6.9}{7} \quad \frac{8.8}{12} \quad \frac{10.3}{28} \quad \frac{12.1}{50}$$

$$\frac{10.5}{50} \quad \frac{11.5}{26} \quad \frac{9.0}{20} \quad \frac{8.6}{9} \quad 8.8 \quad \frac{9.0}{6} \quad \frac{12.8}{13} \quad \frac{13.9}{27} \quad \frac{15.4}{50}$$

$$\frac{7.0}{50} \quad \frac{6.9}{28} \quad \frac{2.7}{20} \quad \frac{2.2}{10} \quad 2.4 \quad \frac{2.7}{6} \quad \frac{9.1}{17} \quad \frac{10.4}{50}$$

$$\frac{7.8}{50} \quad \frac{8.2}{26} \quad \frac{4.6}{20} \quad \frac{4.1}{8} \quad 4.4 \quad \frac{4.8}{7} \quad \frac{13.9}{23} \quad \frac{15.6}{50}$$

$$\frac{8.9}{50} \quad \frac{9.7}{27} \quad \frac{5.9}{20} \quad \frac{5.4}{11} \quad 5.7 \quad \frac{6.2}{5} \quad \frac{20.0}{29} \quad \frac{22.5}{50}$$

$$\frac{12.82}{\text{FL}} \quad 12.58$$

$$\frac{12.82}{\text{FL}} \quad 12.58$$

$$\frac{9.8}{50} \quad \frac{10.7}{32} \quad \frac{13.28}{27\text{FL}} \quad \frac{6.3}{22} \quad \frac{5.7}{10} \quad 6.1 \quad \frac{6.4}{3} \quad \frac{16.65}{\text{FL}} \quad \frac{14.9}{18} \quad \frac{18.0}{32} \quad \frac{18.4}{50}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

925.40

163			6.1	19.3
-----	--	--	-----	------

+50			6.1	19.3
-----	--	--	-----	------

164			5.5	19.9
-----	--	--	-----	------

+50			4.9	20.5
-----	--	--	-----	------

+86			4.1	21.3
-----	--	--	-----	------

+95			3.9	21.5
-----	--	--	-----	------

165+05	Profile Oxford St Lt.		3.6	21.8
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+15			3.4	22.0
-----	--	--	-----	------

+22			3.0	22.4
-----	--	--	-----	------

+50	13.39		1.7	23.7
-----	-------	--	-----	------

T.P.	13.39	936.76	2.03	923.37
------	-------	--------	------	--------

166			11.8	25.0
-----	--	--	------	------

+22			11.4	25.4
-----	--	--	------	------

d

$$\frac{9.9}{50} \frac{10.2}{30} \frac{6.4}{22} \frac{5.7}{11} 6 \mid \frac{6.3}{4} \frac{16.4}{22} \frac{20.0}{50}$$

$$\frac{10.0}{50} \frac{9.3}{29} \frac{6.3}{23} \frac{5.8}{13} 6 \mid \frac{6.2}{2} \frac{13.9}{17} \frac{15.7}{32} \frac{17.7}{43} \frac{18.0}{50}$$

$$\frac{9.1}{50} \frac{7.1}{32} \frac{5.5}{23} \frac{5.0}{12} 5.5 \quad \frac{7.8}{2} \frac{11.9}{14} \frac{13.9}{50}$$

$$\frac{8.7}{50} \frac{8.4}{30} \frac{4.8}{24} \frac{4.3}{13} 4.9 \frac{5.1}{1} \frac{14.4}{19} \frac{15.5}{50}$$

$$\frac{6.5}{50} \frac{4.0}{39} \frac{3.7}{28} \frac{3.5}{11} 4 \mid \frac{15.1}{21} \frac{16.0}{50}$$

$$\frac{3.6}{50} \frac{3.6}{34} \frac{3.3}{13} 3.9 \frac{15.1}{21} \frac{16.0}{50}$$

$$\frac{2.4}{100} \frac{3.3}{50} \frac{3.0}{28} \frac{3.0}{11} 3.6$$

$$\frac{3.4}{50} \frac{3.3}{31} \frac{2.7}{11} 3.4 \frac{3.9}{3} \frac{13.1}{17} \frac{14.0}{31} \frac{16.8}{50}$$

$$\frac{5.2}{50} \frac{5.0}{34} \frac{2.9}{27} \frac{2.4}{11} 3.0 \frac{3.7}{2} \frac{12.2}{19} \frac{13.6}{24} \frac{13.9}{50}$$

$$\frac{4.3}{50} \frac{4.4}{39} \frac{4.2}{32} \frac{1.8}{26} \frac{1.4}{11} 1.7 \frac{1.7}{2} \frac{8.7}{18} \frac{10.5}{22-25} \frac{9.5}{26} \frac{9.6}{50}$$

$$\frac{9.7}{50} \frac{10.2}{46} \frac{12.8}{38} \frac{12.7}{27} \frac{11.7}{24} \frac{11.5}{15} 11.8 \frac{12.1}{2} \frac{13.6}{5} \frac{13.8}{11} \frac{9.8}{18} \frac{10.4}{32} \frac{11.8}{50}$$

$$\frac{8.9}{50} \frac{12.0}{38} \frac{12.0}{27} \frac{11.3}{25} \frac{11.0}{13} 11.4 \frac{11.7}{3} \frac{12.6}{5} \frac{12.7}{11} \frac{11.6}{18} \frac{6.9}{35} \frac{7.9}{50}$$

Sta	+	π	-	Elev	
		936.72			
XLL+50			10.6	26.2	
167			9.3	27.5	
+50			7.9	28.9	
168			6.6	30.2	
+50			4.9	31.9	
T.P	12.72	944.87	4.61	932.15	
169			11.8	33.1	
+50			9.6	35.3	
170			8.7	36.2	
B. M.	4.31	944.93	4.31	940.56	940.62
+50			8.3	36.6	
171			8.6	36.3	
+50			9.3	35.6	
172			10.5	34.4	
T.P	2.54	937.38	10.09	934.84	

E

$$\frac{70}{50} \quad \frac{106}{37} \quad \frac{108}{31} \quad \frac{104}{29} \quad \frac{101}{13} \quad 106 \quad \frac{108}{4} \quad \frac{121}{6} \quad \frac{119}{10} \quad \frac{53}{20} \quad \frac{46}{38} \quad \frac{56}{50}$$

$$\frac{47}{50} \quad \frac{89}{34} \quad \frac{89}{26} \quad \frac{90}{24} \quad \frac{87}{74} \quad 93 \quad \frac{94}{4} \quad \frac{99}{6} \quad \frac{99}{9} \quad \frac{37}{17} \quad \frac{48}{50}$$

$$\frac{33}{50} \quad \frac{77}{30} \quad \frac{75}{14} \quad 79 \quad \frac{80}{5} \quad \frac{83}{8} \quad \frac{60}{13} \quad \frac{61}{32} \quad \frac{64}{50}$$

$$\frac{27}{50} \quad \frac{62}{27} \quad \frac{61}{14} \quad 66 \quad \frac{51}{5} \quad \frac{54}{24} \quad \frac{48}{50}$$

$$\frac{04}{50} \quad \frac{49}{25} \quad \frac{47}{15} \quad 49 \quad \frac{38}{16} \quad \frac{30}{38} \quad \frac{23}{50}$$

$$\frac{71}{50} \quad \frac{108}{35} \quad \frac{119}{25} \quad \frac{117}{15} \quad \frac{120}{2} \quad 118 \quad \frac{111}{2} \quad \frac{101}{21} \quad \frac{89}{50}$$

$$\frac{66}{50} \quad \frac{88}{39} \quad \frac{108}{27} \quad \frac{104}{14} \quad \frac{108}{4} \quad 96 \quad \frac{87}{10} \quad \frac{76}{26} \quad \frac{65}{50}$$

$$\frac{53}{50} \quad \frac{70}{41} \quad \frac{94}{28} \quad \frac{91}{14} \quad \frac{90}{7} \quad 87 \quad \frac{81}{6} \quad \frac{73}{28} \quad \frac{65}{50}$$

Top of Bottom Step Ho 50' at Sta 170+30

$$\frac{30}{50} \quad \frac{52}{42} \quad \frac{75}{33} \quad \frac{85}{25} \quad \frac{94}{14} \quad \frac{86}{7} \quad \frac{85}{1} \quad 83 \quad \frac{78}{1} \quad \frac{69}{18} \quad \frac{61}{34} \quad \frac{49}{50} \quad \frac{471}{50}$$

Flow on Walk
at Ho

$$\frac{31}{50} \quad \frac{65}{37} \quad \frac{73}{28} \quad \frac{80}{25} \quad \frac{82}{15} \quad \frac{85}{9} \quad \frac{81}{3} \quad 96 \quad \frac{81}{8} \quad \frac{73}{19} \quad \frac{69}{36} \quad \frac{63}{50}$$

$$\frac{33}{50} \quad \frac{61}{35} \quad \frac{79}{30} \quad \frac{82}{26} \quad \frac{91}{24} \quad \frac{89}{12} \quad 93 \quad \frac{89}{39} \quad \frac{79}{10} \quad \frac{65}{17} \quad \frac{62}{31} \quad \frac{71}{50}$$

$$\frac{61}{50} \quad \frac{74}{36} \quad \frac{90}{29} \quad \frac{103}{23} \quad \frac{101}{10} \quad 105 \quad \frac{108}{6} \quad \frac{104}{7} \quad \frac{106}{30} \quad \frac{107}{50}$$

Sta	+	π	-	Elev
		93738.		

172+50			4.4	33.0
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173			6.0	31.4
-----	--	--	-----	------

+50			4.7	29.7
-----	--	--	-----	------

174			9.7	27.7
-----	--	--	-----	------

+50			12.0	25.4
-----	--	--	------	------

175			14.0	23.4
-----	--	--	------	------

T.P.	8.02	93263.	12.77	924.61
------	------	--------	-------	--------

+50			11.3	21.3
-----	--	--	------	------

176			13.3	19.3
-----	--	--	------	------

+50				17.3
-----	--	--	--	------

T.P.	0.23	920.84.	12.02	920.61.
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176+50			3.5	17.3
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177			5.5	15.3
-----	--	--	-----	------

+40			6.2	14.6
-----	--	--	-----	------

E

$$\frac{0.1}{50} \frac{0.4}{43} \frac{1.2}{30} \frac{4.1}{23} \frac{4.5}{20} \frac{4.2}{10} 44 \frac{4.8}{8} \frac{4.6}{10} \frac{4.6}{28} \frac{5.1}{50}$$

$$\frac{1.7}{50} \frac{1.8}{38} \frac{2.4}{27} \frac{5.9}{20} \frac{6.3}{15} \frac{6.0}{6} 60 \frac{6.4}{9} \frac{4.8}{19} \frac{4.4}{32} \frac{5.0}{50}$$

$$\frac{3.1}{50} \frac{4.1}{31} \frac{6.1}{19} \frac{7.2}{15} \frac{8.1}{12} 77 \frac{8.4}{12} \frac{7.7}{15} \frac{6.1}{25} \frac{4.5}{37} \frac{5.2}{50}$$

$$\frac{5.8}{50} \frac{4.7}{36} \frac{9.0}{22} \frac{10.6}{12} \frac{10.0}{6} 9.7 \frac{10.0}{10} \frac{10.5}{15} \frac{9.7}{28} \frac{6.7}{41} \frac{7.9}{50}$$

$$\frac{9.2}{50} \frac{9.4}{28} \frac{9.9}{17} \frac{12.3}{11} 12.0 \frac{11.9}{7} \frac{12.6}{18} \frac{11.7}{21} \frac{9.9}{35} \frac{10.9}{50}$$

$$\frac{10.5}{50} \frac{11.2}{40} \frac{12.3}{19} \frac{14.0}{8} 14.0 \frac{14.0}{9} \frac{14.2}{19} \frac{13.6}{35} \frac{13.3}{50}$$

$$\frac{5.3}{50} \frac{6.7}{31} \frac{8.1}{13} \frac{11.5}{6} 11.3 \frac{10.9}{10} \frac{11.5}{33} \frac{6.9}{43} \frac{6.1}{50} \frac{4.1}{75}$$

$$\frac{6.2}{50} \frac{5.8}{41} \frac{4.8}{18} \frac{14.3}{8} \frac{14.3}{6} \frac{13.4}{2} 13.3 \frac{12.8}{12} \frac{13.0}{26} \frac{14.1}{29} \frac{13.8}{33} \frac{4.8}{43} \frac{4.4}{50} \frac{3.9}{75}$$

$$\frac{11.9}{50} \frac{11.9}{42} \frac{11.8}{25} \frac{11.3}{14} (15.3) \frac{9.4}{46} \frac{9.2}{50} \frac{7.7}{75}$$

$$\frac{4.6}{10.4} \frac{3.7}{1} 3.5 \frac{3.0}{13} \frac{3.2}{29} \frac{4.6}{33} \frac{4.6}{36}$$

$$\frac{6.5}{50} \frac{6.5}{15} \frac{7.5}{13} \frac{6.0}{11} \frac{6.0}{8} 5.5 \frac{5.4}{12} \frac{5.6}{32} \frac{6.9}{35} \frac{6.7}{41} \frac{6.0}{50}$$

$$\frac{8.6}{50} \frac{8.6}{46} \frac{7.0}{35} 6.2 \frac{6.6}{32} \frac{6.9}{50}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

		920.84		
--	--	--------	--	--

177+25				
--------	--	--	--	--

B.M				
-----	--	--	--	--

			67	
--	--	--	----	--

				14.1
--	--	--	--	------

			9.55	
--	--	--	------	--

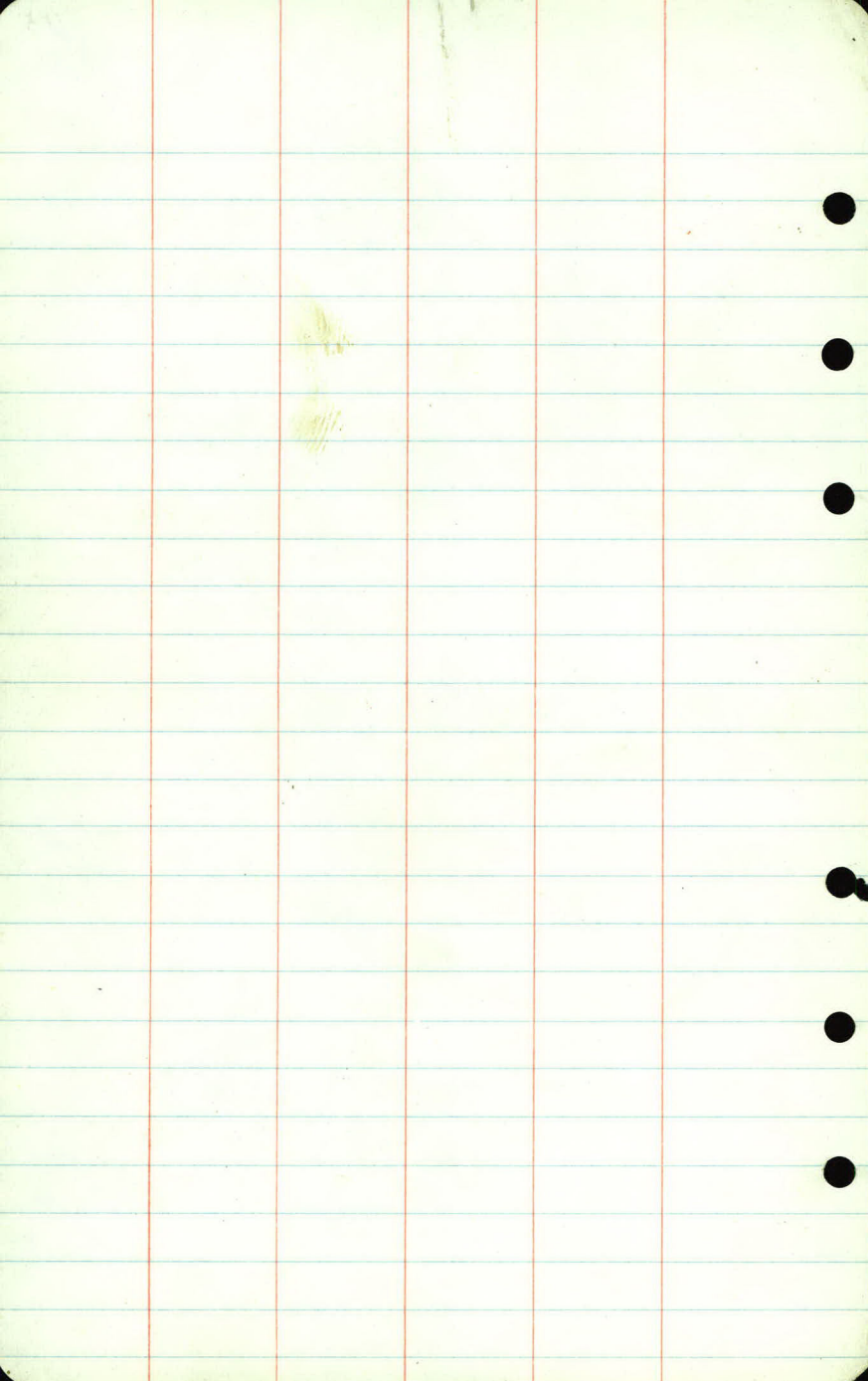
				911.29
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				911.30
--	--	--	--	--------

$\frac{1}{2}$

$$\frac{73}{50} \quad \frac{6.9}{25} - 67 \quad \frac{6.7}{25} \quad \frac{70}{50}$$

Spk in P.P 10' L1 Sta 178+02



Profile Levels

LINE CHANGE

COUNTY ROAD "C"

Between

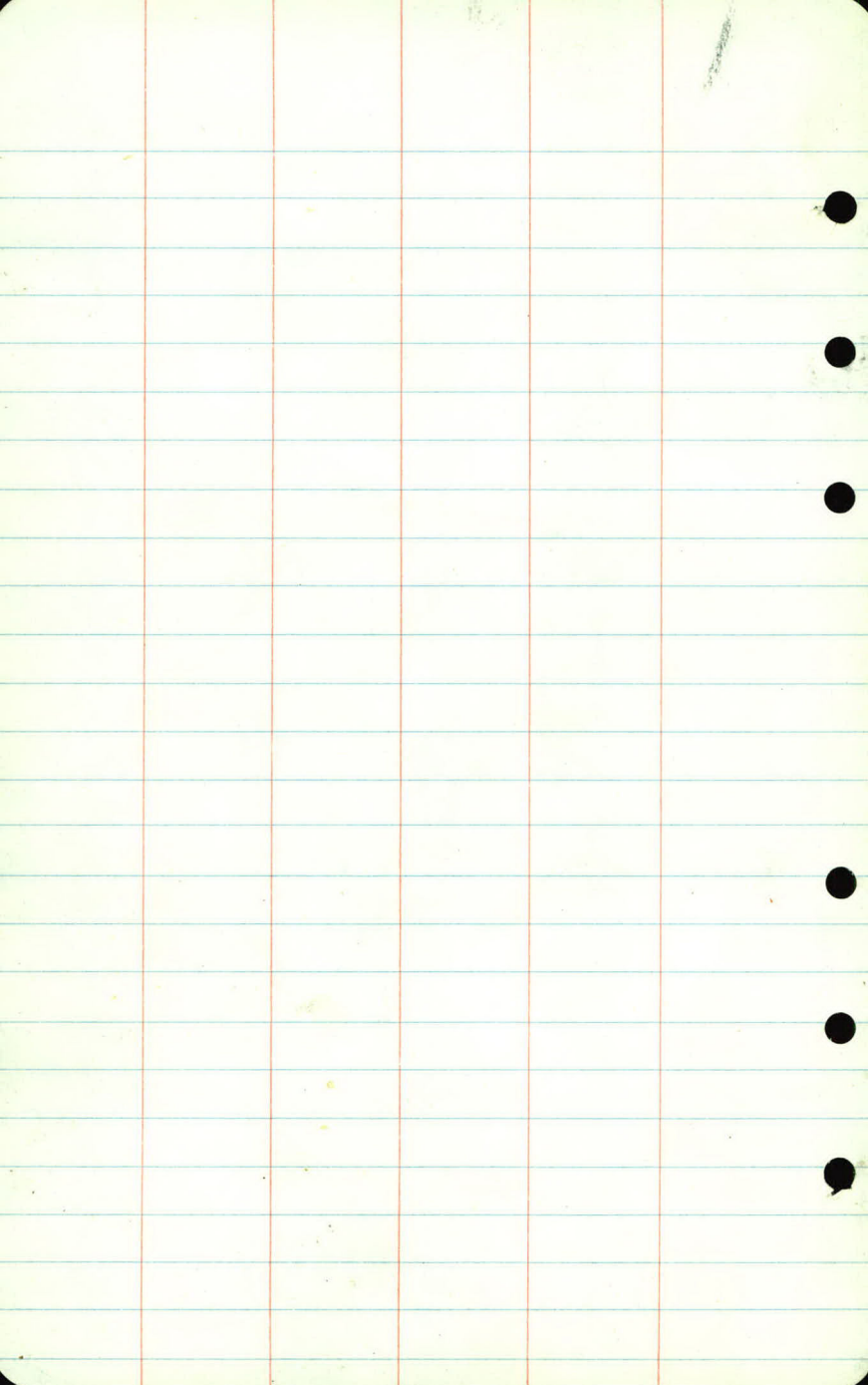
Lexington and Victoria

Sta	+	π	ϵ	Elev.
B.M.	0.22	940.84		940.62
	3.54	933.35	1.03	929.81
164+95			11.7	21.7
165+05			11.4	22.0
+15			11.1	22.3
+22			10.8	22.6
+50			9.5	23.9
166			8.2	25.2
+22			7.6	25.8
+50			6.8	26.6
167			5.4	28.0
+50			4.0	29.4
168			2.7	30.7
+50			1.2	32.2
169			0.0	33.4
T.P.	7.67	940.66	0.36	932.99
+50			6.2	34.5
170			4.8	35.9
+50			4.1	36.6
171			4.0	36.7
+50			4.6	36.1
172			5.8	34.9
+50			7.4	33.3
73			9.0	31.7

Top Bottom Step 50 R.L. 170 + 30

Sta.	+	π	$\pm$	Elev	
		940.66			
173 +50			10.9	29.8	
174			13.1	27.6	
T.P.	0.80	928.35	13.11	927.55	
174 +50			2.9	25.5	
175			5.0	23.4	
+50			6.6	21.8	
176			8.5	19.9	
+50			10.5	17.9	
177			12.6	15.8	
T.P.	6.68	922.39	12.64	915.71	
+40			7.9	14.5	
+75?			8.2	14.2	
+77.18			8.2	14.2	
B.M.			11.07	911.32	911.30

Top Spk in P.P. 10' Lt. 178+02





6 Co Rd C

15" x 52' Conc. Pipe

80

New Brighton Rd
5+53 Ditchline

79+51.75
Int N.B. Rd

79

- 5

78

- 4

77

- 3

P1 2+15

2+00

1+00

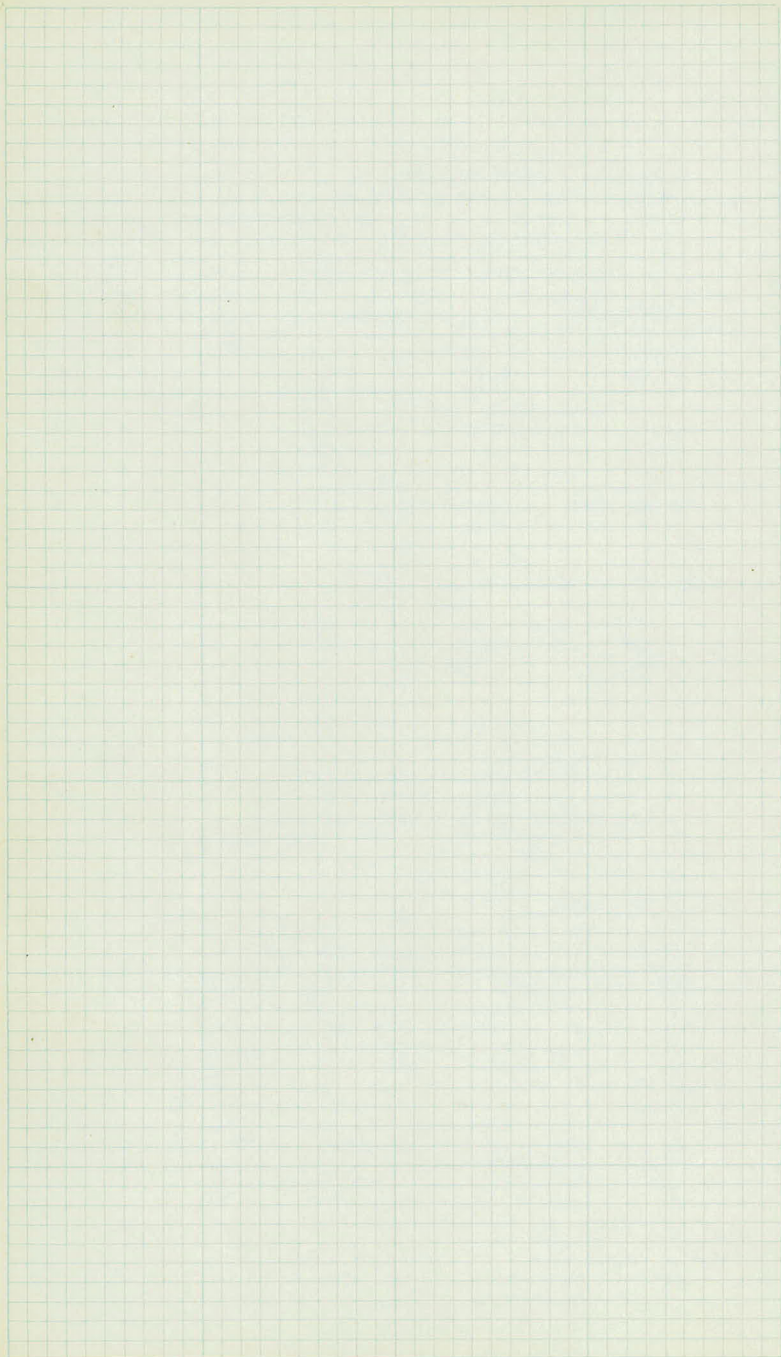
0+00 P.1

76

$\Delta 90^{\circ}00'$

$\Delta 90^{\circ}00'$

Swamp



Profile & X Sections
Proposed Trenching From
Swamp To Culv: 256' No of
"C" on New Brighton Rd.

Sta	+	π	-	Elev
	6.27	931.02		924.75

76+00 = 0+00 P.I. Δ 90°00'

0+15

0+26

+50

1+00

2

+15 P.I. Δ 90°00'

+50

3

+25

+50

4

Lt.

~~Z~~

Rt

6.9

7.4

10.7

11.5

12.1 Low Pt Swamp

12.1

$$\frac{10.4}{15}$$

10.5

$$\frac{12.1}{25}$$

10.4

$$\frac{8.3}{25}$$

9.2

$$\frac{9.0}{20}$$

$$\frac{8.0}{18}$$

8.8

$$\frac{8.3}{25}$$

$$\frac{8.6}{25}$$

$$\frac{8.6}{15}$$

8.7

$$\frac{7.4}{25}$$

$$\frac{10.3}{25}$$

9.4

$$\frac{7.7}{25}$$

Sta + π - Elev

4+50

5

+53

Lt.

Z

Rt

$$\frac{10.4}{25}$$

9.4

$$\frac{2.9}{25}$$

$$\frac{11.2}{25}$$

10.4

$$\frac{8.8}{25}$$

Culv.

$$\frac{14.3}{17.6}$$

$$\frac{13.7}{18}$$

12.9

$$\frac{11.6}{25}$$

Sta

+

π

-

Elav

Co Rd "C" Survey
Elev of Swamp
Lt Sta 75+00

2/18/42

HAW

AM

LL

C.N

Sta	+	π	-	Elev
B.M.	434	929.09		92475

76+00

77+00

B.M.	378	928.53		92475
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X Drain & N.B. Rd. 256' No. of "C"

76

✓

✓

-

✓

76+00

77+00

78+00

79+00

LT. . . Z

RT

Spk in P.P. NW Cor "C" v N Brighton Rd

$$\begin{array}{r} 20.6 \\ 8.5 \\ \hline 200 \end{array} \quad \begin{array}{r} 919.0 \\ 19.5 \\ 10.195 \\ \hline 100.50 \end{array}$$

$$\begin{array}{r} 922.5 \\ 6.6 \\ \hline 200 \end{array}$$

Spk in P.P. NW Cor C + N.B.Rd

916.7

11.80

Inv West End 15

12.65

Inv East End

$$\begin{array}{r} 2.5 \\ \hline \text{Top Rail} \end{array} \quad 926.7$$

$$\begin{array}{r} 2.9 \\ \hline \text{Top Rail} \end{array} \quad 926.2$$

$$\begin{array}{r} 3.5 \\ \hline \text{Top Rail} \end{array} \quad 925.7$$

$$\begin{array}{r} 4.0 \\ \hline \text{Top Rail} \end{array} \quad 925.1$$

Sta + π - Elev

X sections

Sta	+	π	-	Elev.
B.M.	3.54	947.87.		944.33.

0+00 Profile along π Curve 44.55

+17.6 Profile along Edge Pav 44.89

+25 — 45.2

+62 — 45.2

1+00 — 44.6

+20 — 44.1

+50 — 43.4

2 — 42.5

+50 — 41.8

3 — 41.2

+30 — 40.9

Lt £ Rt

SPK. in 20" Oot 50' Lt. Sta. 1 + 00
 $\frac{200}{100}$ $\frac{2.53}{50}$ 332 $\frac{455}{50}$ $\frac{5.82}{100}$

$\frac{1.82}{100}$ $\frac{2.27}{50}$ 2.98 $\frac{412}{50}$ $\frac{5.38}{100}$

*
 Pave Edge Pave
 $\frac{2.67}{32}$ $\frac{2.79}{9}$ 27 $\frac{3.3}{16}$ $\frac{3.6}{21}$ $\frac{5.1}{25}$ $\frac{4.9}{30}$ $\frac{4.2}{33}$ $\frac{5.6}{52}$ $\frac{6.6}{75}$

Edge
 Pav
 $\frac{202}{52}$ $\frac{22}{40}$ $\frac{22}{14}$ 27 $\frac{3.0}{7}$ $\frac{3.3}{11}$ $\frac{7.0}{20}$ $\frac{7.0}{24}$ $\frac{6.1}{27}$ $\frac{7.4}{55}$ $\frac{8.7}{75}$

$\frac{4.3}{75}$ $\frac{4.6}{60}$ $\frac{5.7}{36}$ $\frac{6.6}{30}$ $\frac{3.5}{23}$ $\frac{3.4}{20}$ $\frac{3.3}{14}$ $\frac{3.2}{7}$ 33 $\frac{3.4}{6}$ $\frac{3.6}{10}$ $\frac{8.0}{19}$ $\frac{8.4}{25}$ $\frac{9.0}{50}$ $\frac{9.7}{75}$

$\frac{9.8}{75}$ $\frac{9.4}{50}$ $\frac{8.2}{28}$ $\frac{4.3}{19}$ $\frac{3.8}{15}$ $\frac{3.8}{7}$ $\frac{4.0}{11}$ $\frac{7.4}{19}$ $\frac{8.6}{28}$ $\frac{9.5}{50}$ $\frac{9.6}{75}$

$\frac{10.9}{75}$ $\frac{11.0}{47}$ $\frac{10.3}{27}$ $\frac{4.8}{17}$ $\frac{4.6}{13}$ $\frac{4.5}{7}$ $\frac{4.6}{10}$ $\frac{4.9}{18}$ $\frac{8.1}{28}$ $\frac{8.9}{58}$ $\frac{9.4}{61}$ $\frac{8.6}{75}$ $\frac{8.7}{75}$

$\frac{12.2}{75}$ $\frac{11.6}{46}$ $\frac{11.1}{38}$ $\frac{11.1}{26}$ $\frac{6.0}{16}$ $\frac{5.6}{12}$ 5.4 $\frac{5.5}{8}$ $\frac{5.8}{13}$ $\frac{8.1}{19}$ $\frac{8.5}{36}$ $\frac{8.1}{54}$ $\frac{7.1}{75}$

$\frac{12.1}{75}$ $\frac{11.9}{63}$ $\frac{11.7}{58}$ $\frac{11.8}{40}$ $\frac{10.6}{24}$ $\frac{6.5}{16}$ $\frac{6.2}{10}$ $\frac{6.1}{9}$ $\frac{6.2}{13}$ $\frac{6.8}{19}$ $\frac{8.8}{25}$ $\frac{8.6}{37}$ $\frac{9.7}{46}$ $\frac{9.0}{59}$ $\frac{9.2}{75}$ $\frac{8.5}{75}$

$\frac{11.0}{75}$ $\frac{10.9}{50}$ $\frac{10.4}{23}$ $\frac{7.0}{15}$ $\frac{6.8}{10}$ 6.7 $\frac{6.8}{9}$ $\frac{7.1}{13}$ $\frac{9.7}{18}$ $\frac{9.3}{24}$ $\frac{9.8}{28}$ $\frac{10.1}{43}$ $\frac{9.5}{47}$ $\frac{9.6}{75}$

$\frac{9.0}{75}$ $\frac{9.0}{50}$ $\frac{9.0}{36}$ $\frac{10.3}{32}$ $\frac{10.9}{29}$ $\frac{10.8}{24}$ $\frac{7.6}{16}$ $\frac{7.2}{11}$ 7.0 $\frac{7.2}{9}$ $\frac{7.6}{13}$ $\frac{9.8}{17}$ $\frac{9.6}{24}$ $\frac{10.1}{50}$ $\frac{10.1}{75}$

Sta	+	π	-	Elev.
		947.81		
3	+60			40.5
4				40.1
	+50			39.4
T.P.	4.40	943.02	9.25	938.62
5	+100			
	+35	-? Wilke		38.3
	+58	X Drain		38.2
6				38.0
	+50			37.8
7				37.9
	+50			37.9
8				37.8
	+17	X Drain	Skewed	37.8

Lt.

\$

Rt.

8.0 8.8 8.6 10.7 10.7 7.7 7.5 7.4 7.7 7.8 10.2 9.4 10.5 10.5
75 50 35 28 21 16 12 10 12 18 21 34 75

7.3 7.6 7.6 9.6 11.3 11.3 7.8 7.7 7.8 8.3 9.7 9.7 8.6 9.6 10.2 11.3
75 50 36 29 26 23 16 13 10 13 17 19 24 30 46 75

8.5 8.4 8.4 12.2 12.2 8.7 8.5 8.5 8.7 9.0 10.5 10.4 9.6 11.0 12.0
75 50 39 27 24 17 12 11 15 18 20 25 50 75

7.7 7.5 7.3 8.2 8.2 5.0 4.7 4.9 5.2 7.8 7.8 7.9 8.1
75 50 27 26 21 15 10 47 10 14 19 29 30 75

Inv

Inv

8.8 8.8 7.7 8.2 8.2 8.3 5.0 4.9 5.0 5.1 8.5 7.8 8.8 9.2
75 50 27 26 20 18 15 11 48 12 15 20 22 53 75

7.1 7.7 7.6 8.1 8.2 5.2 5.0 5.2 5.3 7.6 8.8 9.7
75 50 27 26 20 15 11 50 11 15 19 30 75

6.0 5.9 6.0 5.5 7.4 7.6 5.3 5.2 5.4 5.4 7.5 9.0 9.8
75 50 35 25 23 19 14 11 5.2 12 15 20 45 75

5.0 5.4 5.9 5.9 7.5 7.5 5.2 5.1 5.4 5.4 8.0 8.6 9.3 10.0
75 50 32 25 23 19 15 11 5.1 12 15 22 33 50 75

5.1 5.1 5.1 7.6 7.6 5.3 5.1 5.4 5.5 7.9 9.1 9.9
75 50 26 23 19 15 10 5.1 13 16 20 50 75

6.5 6.9 7.3 6.9 8.0 8.0 5.5 5.2 5.3 5.4 7.4 8.4 8.8 9.2
75 50 30 26 24 19 14 10 5.2 13 15 23 29 50 75

Inv.

Inv

7.0 7.3 7.0 8.3 8.3 8.3 5.5 5.2 5.3 5.5 7.3 9.2 8.0 7.4 8.7
50 30 25 23 18 18 15 10 5.2 13 16 22 22 27 28 50

6.7
75

8.8
75

Sta	+	+	-	Elev
-----	---	---	---	------

94302.

8+50

38.0

9

38.5

+50

39.4

10

41.1

T.P.

11.61

953.03.

1.60

941.42.

+50

43.0

11

44.8

+50

46.1

12

47.1

+50

48.4

+8367 = 0+00 West Co Line

49.2
49.3

B.M

3.79

949.24 949.21

Lt

E

Rt

$\frac{64}{75}$ $\frac{70}{50}$ $\frac{74}{32}$ $\frac{76}{24}$ $\frac{80}{22}$ $\frac{80}{19}$ $\frac{53}{14}$ $\frac{51}{10}$ 5.0 $\frac{5.0}{13}$ $\frac{5.2}{17}$ $\frac{67}{20}$ $\frac{73}{22}$ $\frac{70}{27}$ $\frac{75}{32}$ $\frac{80}{50}$

$\frac{6.9}{75}$ $\frac{6.9}{46}$ $\frac{6.3}{38}$ $\frac{6.2}{23}$ $\frac{7.1}{22}$ $\frac{7.1}{19}$ $\frac{6.2}{18}$ $\frac{4.9}{13}$ $\frac{4.7}{10}$ 4.5 $\frac{4.6}{14}$ $\frac{4.6}{18}$ $\frac{6.4}{21}$ $\frac{6.4}{24}$ $\frac{5.5}{25}$ $\frac{6.3}{31}$ $\frac{7.1}{50}$ $\frac{80}{75}$

$\frac{5.1}{75}$ $\frac{4.5}{50}$ $\frac{3.5}{23}$ $\frac{4.5}{22}$ $\frac{3.6}{18}$ $\frac{3.4}{9}$ 3.6 $\frac{3.5}{13}$ $\frac{3.5}{17}$ $\frac{5.2}{20}$ $\frac{3.6}{23}$ $\frac{4.5}{25}$ $\frac{5.4}{32}$ $\frac{6.0}{50}$ $\frac{7.0}{75}$

$\frac{23}{75}$ $\frac{2.1}{50}$ $\frac{1.7}{24}$ $\frac{3.5}{21}$ $\frac{3.1}{17}$ $\frac{2.2}{12}$ $\frac{2.1}{9}$ 1.9 $\frac{2.0}{13}$ $\frac{2.4}{17}$ $\frac{3.7}{21}$ $\frac{1.7}{23}$ $\frac{2.3}{25}$ $\frac{2.6}{32}$ $\frac{2.6}{50}$ $\frac{4.0}{75}$

$\frac{10.4}{75}$ $\frac{9.7}{50}$ $\frac{9.6}{24}$ $\frac{11.6}{21}$ $\frac{11.4}{18}$ $\frac{10.3}{14}$ $\frac{10.2}{10}$ 10.0 $\frac{10.1}{13}$ $\frac{10.3}{19}$ $\frac{11.6}{21}$ $\frac{9.1}{22}$ $\frac{8.5}{25}$ $\frac{8.8}{30}$ $\frac{8.4}{38}$ $\frac{9.3}{50}$ $\frac{9.3}{75}$

$\frac{11.7}{75}$ $\frac{11.0}{50}$ $\frac{9.4}{23}$ $\frac{10.1}{21}$ $\frac{9.7}{17}$ $\frac{8.3}{14}$ $\frac{8.3}{10}$ 8.2 $\frac{8.3}{14}$ $\frac{8.5}{18}$ $\frac{9.5}{21}$ $\frac{5.8}{22}$ $\frac{5.4}{26}$ $\frac{5.5}{30}$ $\frac{6.0}{50}$ $\frac{6.0}{75}$

$\frac{11.8}{75}$ $\frac{10.8}{50}$ $\frac{9.4}{27}$ $\frac{8.9}{22}$ $\frac{9.0}{19}$ $\frac{7.6}{14}$ $\frac{7.1}{10}$ 6.9 $\frac{7.1}{14}$ $\frac{7.4}{19}$ $\frac{8.1}{21}$ $\frac{4.3}{22}$ $\frac{4.3}{27}$ $\frac{4.2}{50}$ $\frac{4.1}{75}$

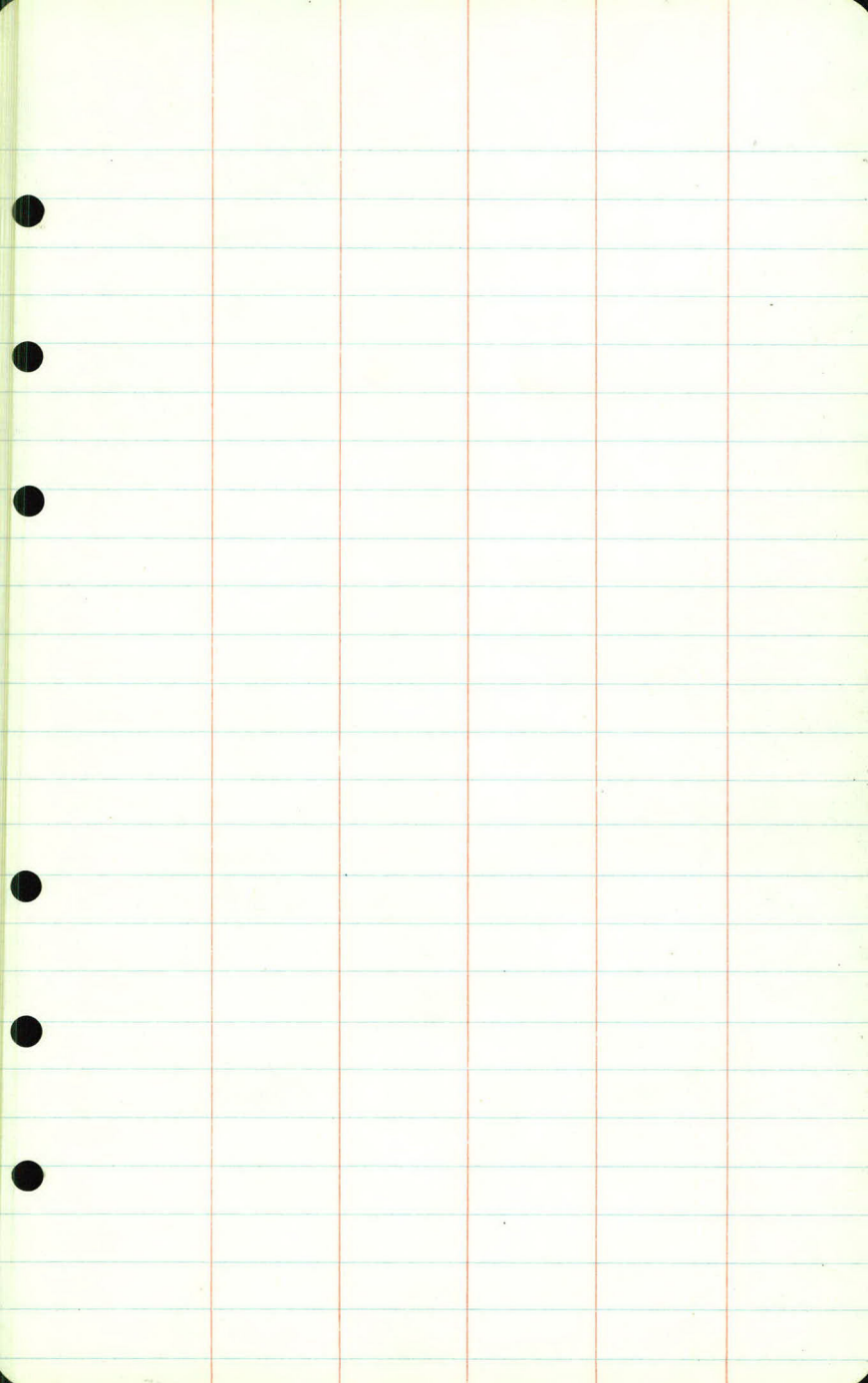
$\frac{9.4}{75}$ $\frac{8.7}{50}$ $\frac{8.1}{48}$ $\frac{6.9}{21}$ $\frac{7.6}{20}$ $\frac{7.4}{17}$ $\frac{6.2}{14}$ $\frac{6.0}{10}$ 5.9 $\frac{6.0}{14}$ $\frac{6.3}{18}$ $\frac{7.2}{21}$ $\frac{4.9}{23}$ $\frac{3.9}{25}$ $\frac{3.7}{29}$ $\frac{3.7}{50}$ $\frac{3.7}{75}$

$\frac{6.0}{75}$ $\frac{5.7}{50}$ $\frac{5.1}{22}$ $\frac{6.0}{20}$ $\frac{5.5}{16}$ $\frac{4.9}{14}$ $\frac{4.9}{10}$ 4.6 $\frac{5.0}{15}$ $\frac{5.3}{18}$ $\frac{6.3}{20}$ $\frac{3.8}{22}$ $\frac{3.5}{25}$ $\frac{2.8}{29}$ $\frac{2.8}{50}$ $\frac{2.8}{75}$

$\frac{4.1}{75}$ $\frac{3.6}{50}$ $\frac{3.4}{30}$ $\frac{3.8}{23}$ $\frac{4.9}{19}$ $\frac{4.5}{14}$ $\frac{4.2}{11}$ 3.8 $\frac{4.1}{16}$ $\frac{4.3}{18}$ $\frac{5.1}{20}$ $\frac{5.1}{22}$ $\frac{2.8}{24}$ $\frac{2.1}{30}$ $\frac{1.9}{50}$ $\frac{1.9}{75}$

Top Iron Pin $12 + 83.67 = 0100$ West Co Line

Sta. + π - Elev



Sta	+	Δ	-	Elev
B.M.	4.76	953.97		949.21
0+00				49.2
+50				49.8
1+00				49.4
+50				49.3
2				49.1
+50				49.0
3				49.0
+50				49.0
4				49.1
+50				49.2
5				49.4
+60				49.3

Lt.

K

Rt

Top Iron Pin 0400 Co Rd "C" x West Co Line

$$\frac{5.2}{75} \quad \frac{4.5}{50} \quad 4.8 \quad \frac{3.0}{50} \quad \frac{2.2}{75}$$

$$\frac{6.6}{75} \quad \frac{5.4}{50} \quad 4.2 \quad \frac{2.4}{50} \quad \frac{2.2}{75} \quad \frac{2.5}{80}$$

$$\frac{5.8}{75} \quad \frac{5.1}{50} \quad 4.6 \quad \frac{3.0}{50} \quad \frac{2.4}{75}$$

$$\frac{6.3}{75} \quad \frac{6.1}{50} \quad 4.7 \quad \frac{4.1}{50} \quad \frac{3.4}{75}$$

$$\frac{4.4}{75} \quad \frac{5.6}{50} \quad 4.9 \quad \frac{6.2}{50} \quad \frac{5.8}{75}$$

$$\frac{3.9}{75} \quad \frac{5.0}{50} \quad 5.0 \quad \frac{7.5}{50} \quad \frac{7.5}{75}$$

$$\frac{4.3}{75} \quad \frac{5.6}{50} \quad 5.0 \quad \frac{8.7}{50} \quad \frac{9.0}{75}$$

$$\frac{6.1}{75} \quad \frac{6.2}{50} \quad 5.0 \quad \frac{6.1}{50} \quad \frac{6.1}{75}$$

$$\frac{5.3}{75} \quad \frac{4.9}{50} \quad 4.9 \quad \frac{5.0}{50} \quad \frac{5.3}{75}$$

$$\frac{5.4}{75} \quad \frac{5.6}{50} \quad 4.8 \quad \frac{5.5}{50} \quad \frac{5.1}{75}$$

$$\frac{4.6}{75} \quad \frac{4.9}{50} \quad 4.6 \quad \frac{5.7}{50} \quad \frac{5.1}{75}$$

$$\frac{3.8}{75} \quad \frac{3.1}{50} \quad 4.7 \quad \frac{1.4}{50} \quad \frac{1.6}{75}$$

Sta	+	Σ	-	Elev
		953.97		
5+68				49.7
6				49.0
T.P.	438	953.20	5.15	948.82
+58				48.3
+70				48.2
7				47.9
+09				47.9
+50				47.7
8				47.8
+40				48.0
9				48.1
+50				48.0
10				48.0

Lt

A

Rt

$$\frac{3.5}{75} \quad \frac{2.8}{50} \quad 4.7 \quad \frac{1.7}{50} \quad \frac{1.7}{75}$$

$$\frac{5.1}{75} \quad \frac{4.4}{50} \quad 5.0 \quad \frac{4.1}{50} \quad \frac{4.2}{75}$$

$$\frac{7.3}{75} \quad \frac{6.7}{50} \quad 4.9 \quad \frac{11.0}{50} \quad \frac{11.6}{75}$$

$$\frac{8.6}{75} \quad \frac{8.6}{50} \quad 5.0 \quad \frac{11.4}{50} \quad \frac{12.5}{75}$$

$$\frac{9.5}{75} \quad \frac{9.7}{50} \quad 5.3 \quad \frac{12.8}{50} \quad \frac{13.9}{75}$$

$$\frac{9.4}{75} \quad \frac{9.5}{50} \quad 5.3 \quad \frac{12.8}{50} \quad \frac{13.9}{69} \quad \frac{14.1}{75}$$

$$\frac{9.0}{75} \quad \frac{9.0}{50} \quad 5.5 \quad \frac{13.0}{50} \quad \frac{14.1}{75}$$

$$\frac{5.4}{75} \quad \frac{5.2}{50} \quad 5.4 \quad \frac{10.4}{50} \quad \frac{11.1}{69} \quad \frac{12.0}{75}$$

$$\frac{1.5}{75} \quad \frac{1.3}{50} \quad 5.2 \quad \frac{8.4}{50} \quad \frac{9.5}{75}$$

$$\frac{2.5}{75} \quad \frac{2.6}{50} \quad 5.1 \quad \frac{8.9}{50} \quad \frac{10.3}{75}$$

$$\frac{4.2}{75} \quad \frac{5.3}{50} \quad 5.2 \quad \frac{10.0}{50} \quad \frac{10.7}{59} \quad \frac{10.7}{75}$$

$$\frac{5.8}{75} \quad \frac{7.0}{50} \quad 5.2 \quad \frac{11.4}{50} \quad \frac{11.8}{59} \quad \frac{12.1}{75}$$

Sta	+	Δ	-	Elev
		953.20		
10+50				48.2
11				48.8
+50				49.7
12				50.5
T.P.	9.14	960.16,	2.18	951.02
+50				51.2
13				51.9
B. M	8.66	960.16.	8.66	951.50
+50				52.9
14				53.8
+50				54.5
15				54.9
+50				55.1
16				54.8

Lt.

R

Rt

$$\frac{6.2}{75} \quad \frac{7.3}{50} \quad 5.0 \quad \frac{11.3}{50} \quad \frac{11.5}{67} \quad \frac{12.1}{75}$$

$$\frac{5.3}{75} \quad \frac{6.1}{50} \quad 4.4 \quad \frac{9.7}{50} \quad \frac{9.6}{75}$$

$$\frac{1.5}{75} \quad \frac{2.5}{50} \quad 3.5 \quad \frac{6.0}{50} \quad \frac{4.1}{75}$$

$$\frac{0.9}{75} \quad \frac{1.9}{50} \quad 2.7 \quad \frac{2.1}{50} \quad \frac{1.8}{75}$$

$$\frac{7.7}{75} \quad \frac{8.7}{50} \quad 9.0 \quad \frac{7.1}{50} \quad \frac{5.7}{75}$$

$$\frac{7.3}{75} \quad \frac{7.5}{50} \quad 8.3 \quad \frac{4.9}{50} \quad \frac{3.8}{59} \quad \frac{2.8}{75}$$

SpK in 30" Oak 103 Lt Sta 13+26

$$\frac{10.4}{75} \quad \frac{9.4}{50} \quad 7.3 \quad \frac{3.1}{50} \quad \frac{2.4}{56} \quad \frac{1.8}{75}$$

$$\frac{9.0}{75} \quad \frac{8.0}{56} \quad \frac{7.8}{50} \quad 6.4 \quad \frac{4.1}{50} \quad \frac{3.0}{62} \quad \frac{2.7}{75}$$

$$\frac{7.3}{75} \quad \frac{6.7}{61} \quad \frac{6.4}{58} \quad \frac{6.2}{50} \quad 5.7 \quad \frac{3.6}{50} \quad \frac{3.1}{59} \quad \frac{2.6}{75}$$

$$\frac{5.3}{75} \quad \frac{2.1}{67} \quad \frac{1.8}{64} \quad \frac{3.6}{58} \quad \frac{3.6}{50} \quad 5.3 \quad \frac{3.7}{50} \quad \frac{2.4}{75}$$

$$\frac{4.8}{75} \quad \frac{3.9}{64} \quad \frac{1.4}{58} \quad \frac{1.5}{54} \quad \frac{3.3}{49} \quad 5.1 \quad \frac{5.7}{50} \quad \frac{5.6}{75}$$

$$\frac{6.7}{75} \quad \frac{2.9}{67} \quad \frac{2.6}{62} \quad \frac{4.7}{54} \quad \frac{4.9}{50} \quad 5.4 \quad \frac{5.1}{50} \quad \frac{5.2}{75}$$

Sta	+	π	-	Elev
		960.16		
16+50				54.3
17				53.3
+50				52.3
18				51.6
+19				51.1
+34				50.8
+50				50.5
T.P.	8.00	956.99	11.17	948.99
19				49.3
+50				48.2
20				47.3
+50				46.4
T.P.	7.95	952.71	12.23	944.76
21				45.2

Lt.

L

Rt

$$\frac{6.6}{75} \quad \frac{7.0}{75} \quad \frac{6.7}{54} \quad 5.9 \quad \frac{3.8}{50} \quad \frac{3.4}{75}$$

$$\frac{8.8}{75} \quad \frac{8.8}{50} \quad 6.9 \quad \frac{4.8}{50} \quad \frac{3.8}{64} \quad \frac{3.8}{75}$$

$$\frac{9.6}{75} \quad \frac{10.2}{65} \quad \frac{10.1}{50} \quad 7.9 \quad \frac{7.8}{50} \quad \frac{2.6}{75}$$

$$\frac{10.1}{75} \quad \frac{10.8}{61} \quad \frac{11.1}{50} \quad 8.6 \quad \frac{9.2}{50} \quad \frac{8.9}{75}$$

$$\frac{4.0}{88} \quad \frac{9.5}{75} \quad \frac{10.3}{73} \quad \frac{10.5}{50} \quad \frac{10.6}{34} \quad \frac{9.6}{17} \quad \frac{9.3}{13} \quad 9.1 \quad \frac{9.4}{11} \quad \frac{9.6}{15} \quad \frac{10.3}{18} \quad \frac{10.5}{23} \quad \frac{9.9}{26} \quad \frac{10.0}{37} \quad \frac{10.2}{43} \quad \frac{10.2}{59}$$

$$\frac{10.0}{75}$$

$$\frac{4.0}{79} \quad \frac{12.1}{64} \quad \frac{12.9}{60} \quad \frac{13.6}{38} \quad \frac{12.5}{34} \quad \frac{13.2}{32} \quad \frac{13.1}{25} \quad \frac{9.9}{16} \quad 9.4 \quad \frac{9.8}{14} \quad \frac{10.7}{17} \quad \frac{11.3}{24} \quad \frac{11.0}{42} \quad \frac{11.0}{57} \quad \frac{10.5}{75}$$

$$\frac{4.4}{75} \quad \frac{4.4}{70} \quad \frac{13.1}{54} \quad \frac{13.9}{50} \quad 9.7 \quad \frac{11.2}{50} \quad \frac{10.6}{75}$$

$$\frac{10.2}{75} \quad \frac{7.4}{70} \quad \frac{1.2}{62} \quad \frac{0.9}{55} \quad \frac{11.2}{37} \quad 7.7 \quad \frac{8.3}{50} \quad \frac{6.8}{66} \quad \frac{6.0}{75}$$

$$\frac{9.8}{74} \quad \frac{0.8}{59} \quad \frac{0.7}{56} \quad \frac{11.0}{37} \quad 8.8 \quad \frac{9.9}{50} \quad \frac{8.1}{75}$$

$$\frac{1.6}{75} \quad \frac{1.1}{69} \quad \frac{9.8}{51} \quad \frac{9.9}{50} \quad 9.7 \quad \frac{10.4}{50} \quad \frac{10.3}{75}$$

$$\frac{11.3}{75} \quad \frac{11.4}{62} \quad \frac{10.5}{50} \quad 10.6 \quad \frac{7.9}{50} \quad \frac{8.3}{75}$$

$$\frac{7.2}{75} \quad \frac{7.2}{61} \quad \frac{6.2}{54} \quad 7.5 \quad \frac{3.3}{50} \quad \frac{4.0}{75}$$

Sta	+	↑	-	Elev
		952.71'		
21+50				44.1
22				43.2
+50				42.1
23				40.9
+50				39.5
24				38.3
T.P.	1.50	940.84.	1337	93934.
+50				37.3
25				36.5
+18				36.2
+35				36.0
+47				35.8
+52				35.7

At

K

Rt

$$\frac{61}{75} \quad \frac{6.2}{50} \quad 86 \quad \frac{3.7}{50} \quad \frac{4.2}{75}$$

$$\frac{5.7}{75} \quad \frac{6.6}{50} \quad 95 \quad \frac{9.4}{50} \quad \frac{9.6}{75}$$

$$\frac{7.0}{75} \quad \frac{2.0}{66} \quad \frac{2.1}{63} \quad \frac{5.3}{55} \quad \frac{5.9}{50} \quad 106 \quad \frac{11.1}{50} \quad \frac{9.7}{75}$$

$$\frac{9.6}{75} \quad \frac{9.2}{71} \quad \frac{6.4}{67} \quad \frac{2.4}{55} \quad \frac{2.4}{53} \quad \frac{5.4}{46} \quad 11.8 \quad \frac{9.4}{50} \quad \frac{8.4}{59} \quad \frac{6.7}{75}$$

$$\frac{9.6}{75} \quad \frac{3.1}{62} \quad \frac{3.1}{59} \quad \frac{7.5}{50} \quad 132 \quad \frac{13.9}{50} \quad \frac{10.3}{75}$$

$$\frac{2.7}{80} \quad \frac{19.1}{50} \quad 144 \quad \frac{15.2}{50} \quad \frac{13.9}{75}$$

$$\frac{8.9}{75} \quad \frac{9.2}{50} \quad 35 \quad \frac{7.8}{50} \quad \frac{8.7}{75}$$

$$\frac{10.1}{75} \quad \frac{9.6}{50} \quad 43 \quad \frac{8.0}{50} \quad \frac{8.3}{75}$$

$$\begin{array}{ccccccc} & & & \text{Edge slab} & & & \\ 10.3 & 10.2 & 8.6 & 4.96 & & \frac{7.6}{50} & \frac{7.0}{75} \\ \frac{75}{75} & \frac{60}{60} & \frac{50}{50} & \frac{19.5}{19.5} & 4.6 & & \end{array}$$

$$\begin{array}{ccccccc} & & & \text{Edge slab} & & & \\ 5.50 & & & & & & \\ \frac{75}{75} & \frac{5.17}{50} & \frac{4.96}{19.3} & 48 & & \frac{5.8}{50} & \frac{6.0}{75} \end{array}$$

$$\begin{array}{ccccccc} & & & \text{Edge slab} & & & \\ \frac{7.1}{75} & \frac{6.7}{50} & \frac{5.8}{20} & \frac{5.19}{19.3} & 50 & \frac{5.1}{13} & \frac{5.7}{14} & \frac{5.3}{49} & \frac{6.4}{64} & \frac{6.5}{75} \end{array}$$

$$\frac{6.3}{75} \quad \frac{6.5}{50} \quad 5.1 \quad \frac{6.6}{50} \quad \frac{7.6}{61} \quad \frac{6.5}{75}$$

Sta	+	Δ	-	Elev
		940.84		
25+58				35.7
+66				35.7
26				35.4
+16				35.5
+28				35.4
+43				35.3
+59				35.1
B.M			5.59	935.25. 935.26
+76				
+89				
27				

L+

R

R+

$$\frac{63}{75} \quad \frac{6.2}{50} \quad 5.1 \quad \frac{8.9}{50} \quad \frac{69}{75}$$

$$\frac{63}{75} \quad \frac{6.1}{50} \quad 5.1 \quad \frac{8.6}{50} \quad \frac{88}{6.2} \quad \frac{7.1}{75}$$

$$\frac{10.4}{75} \quad \frac{9.5}{50} \quad 5.4 \quad \frac{10.7}{50} \quad \frac{8.2}{75}$$

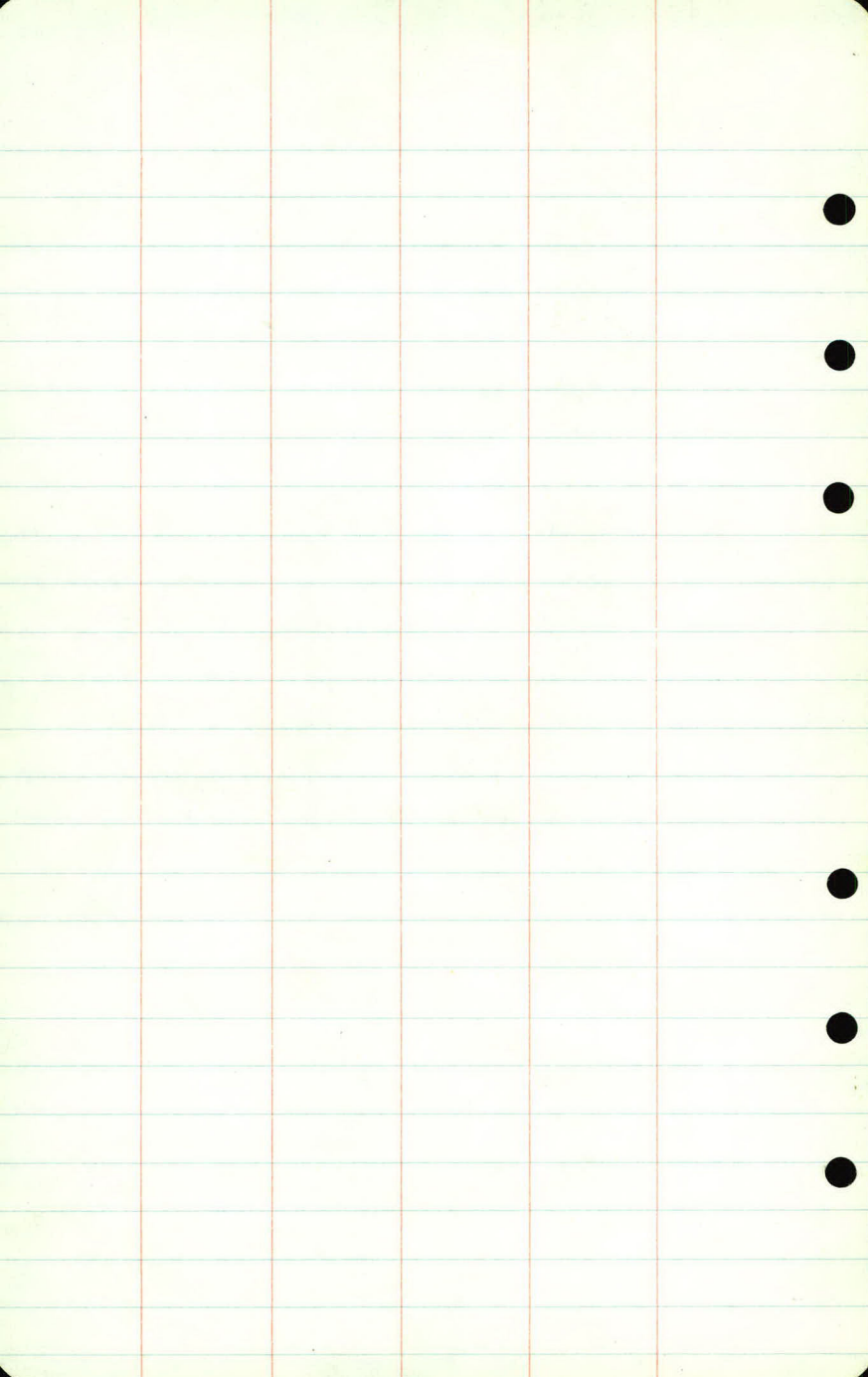
$$\frac{8.6}{75} \quad \frac{9.1}{50} \quad 5.3 \quad \frac{6.1}{50} \quad \frac{6.0}{75}$$

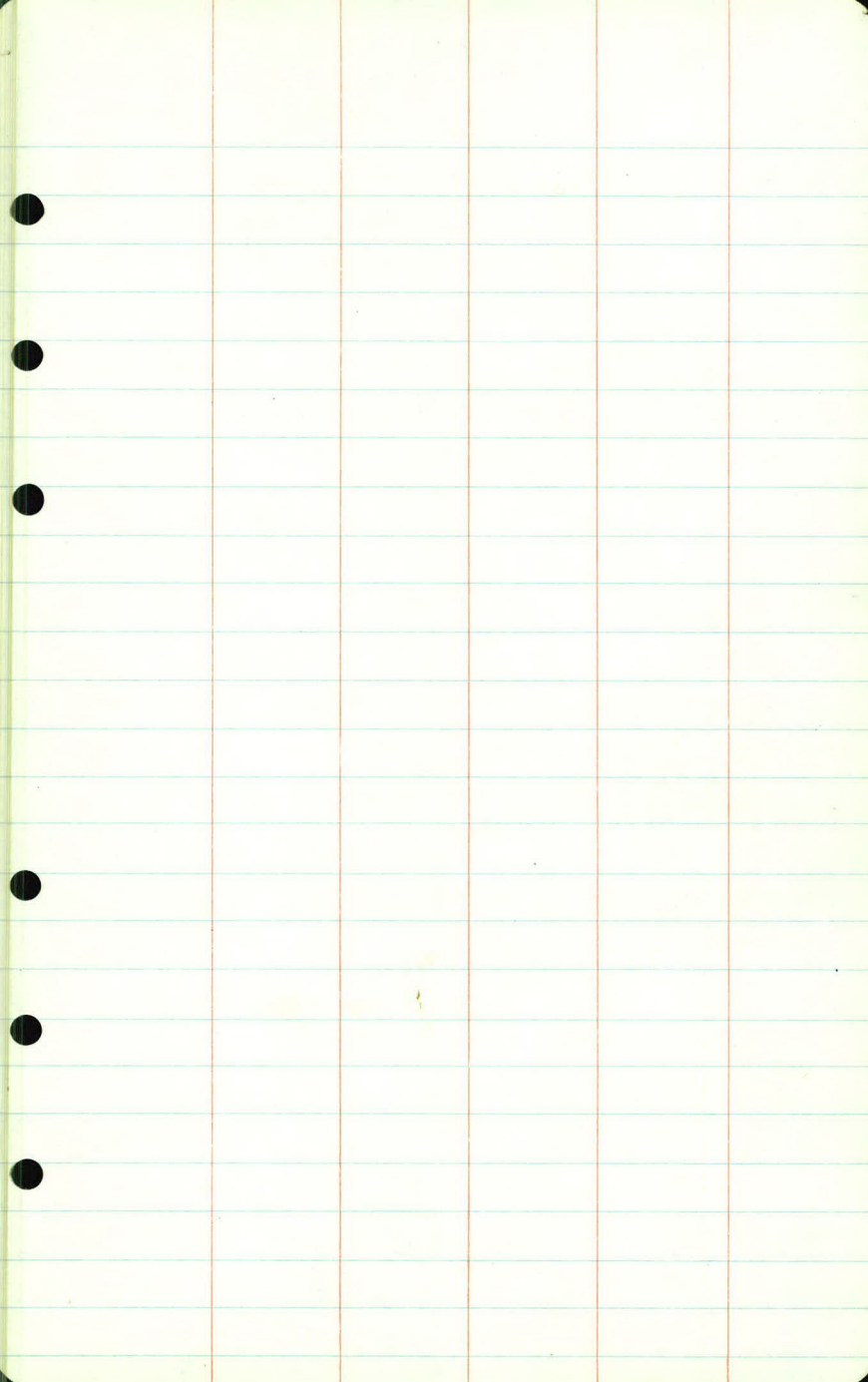
$$\frac{8.3}{75} \quad \frac{6.9}{69} \quad \frac{6.6}{50} \quad 5.4 \quad \frac{6.0}{50} \quad \frac{6.2}{75}$$

$$\frac{6.2}{75} \quad \frac{6.2}{50} \quad 5.5 \quad \frac{8.2}{50} \quad \frac{11.2}{75}$$

$$\frac{6.3}{75} \quad \frac{6.4}{50} \quad 5.7 \quad \frac{13.9}{50} \quad \frac{13.8}{75}$$

Top Mon Stg 26+52.28





Sta	+	π	-	Elev
B.M	3.03	938.29.		935.26
26776				34.9
+89				348
27				347
+50				341
28				33.4
+50				32.6
29				31.9
+50				31.2
30				30.5
+50				29.5
31				28.8
T.P.	0.05	929.42.	8.92	929.37.
+50				27.9

L1

L

R1

$$\frac{12.0}{75} \quad \frac{11.5}{50} \quad 3.4 \quad \frac{9.8}{50} \quad \frac{9.0}{75}$$

$$\frac{6.1}{75} \quad \frac{5.5}{50} \quad 3.5 \quad \frac{9.0}{50} \quad \frac{8.7}{61} \quad \frac{8.0}{75}$$

$$\frac{8.0}{75} \quad \frac{6.8}{50} \quad 3.6 \quad \frac{8.9}{50} \quad \frac{8.3}{63} \quad \frac{7.6}{67} \quad \frac{8.1}{75}$$

$$\frac{11.0}{75} \quad \frac{10.0}{50} \quad 4.2 \quad \frac{8.4}{61} \quad \frac{8.7}{66} \quad \frac{8.3}{75}$$

$$\frac{10.0}{75} \quad \frac{9.8}{50} \quad 4.9 \quad \frac{7.9}{50} \quad \frac{7.7}{75}$$

$$\frac{8.5}{75} \quad \frac{8.5}{50} \quad 5.7 \quad \frac{4.7}{50} \quad \frac{3.2}{75}$$

$$\frac{7.8}{75} \quad \frac{8.4}{50} \quad 6.4 \quad \frac{5.8}{50} \quad \frac{5.4}{58} \quad \frac{4.9}{75}$$

$$\frac{8.3}{75} \quad \frac{8.5}{50} \quad 7.1 \quad \frac{6.5}{50} \quad \frac{5.8}{75}$$

$$\frac{9.7}{75} \quad \frac{9.0}{50} \quad 7.8 \quad \frac{8.2}{50} \quad \frac{7.5}{75}$$

$$\frac{11.0}{75} \quad \frac{10.8}{50} \quad 8.8 \quad \frac{10.2}{50} \quad \frac{9.6}{59} \quad \frac{9.4}{75}$$

$$\frac{11.8}{75} \quad \frac{10.3}{50} \quad 9.5 \quad \frac{10.4}{50} \quad \frac{10.0}{59} \quad \frac{10.4}{75}$$

$$\frac{3.9}{75} \quad \frac{3.3}{50} \quad 1.5 \quad \frac{2.0}{50} \quad \frac{1.6}{60} \quad \frac{1.7}{75}$$

Sta	+	Δ	-	Elev
-----	---	----------	---	------

929.42.

32				27.3
----	--	--	--	------

+50				26.5
-----	--	--	--	------

33				25.7
----	--	--	--	------

+50				24.8
-----	--	--	--	------

34				23.7
----	--	--	--	------

+50				23.1
-----	--	--	--	------

35				22.3
----	--	--	--	------

+50				21.4
-----	--	--	--	------

36				20.6
----	--	--	--	------

+50				19.7
-----	--	--	--	------

37				18.7
----	--	--	--	------

T.P.	0.15	919.26.	10.31	919.11.
------	------	---------	-------	---------

+50			11	17.7
-----	--	--	----	------

L1 2 R1

$$\frac{4.2}{75} \quad \frac{3.7}{50} \quad 2.1 \quad \frac{2.5}{50} \quad \frac{1.9}{62} \quad \frac{1.7}{75}$$

$$\frac{4.1}{75} \quad \frac{3.6}{50} \quad 2.9 \quad \frac{2.6}{50} \quad \frac{2.4}{60} \quad \frac{1.9}{67} \quad \frac{2.0}{75}$$

$$\frac{3.1}{75} \quad \frac{2.4}{65} \quad \frac{2.7}{50} \quad 3.7 \quad \frac{2.8}{50} \quad \frac{2.8}{75}$$

$$\frac{3.3}{75} \quad \frac{2.9}{50} \quad 4.6 \quad \frac{2.6}{50} \quad \frac{2.8}{75}$$

$$\frac{5.9}{75} \quad \frac{5.2}{50} \quad 5.7 \quad \frac{2.7}{50} \quad \frac{2.6}{75}$$

$$\frac{8.8}{75} \quad \frac{7.8}{50} \quad 6.3 \quad \frac{3.2}{50} \quad \frac{3.3}{75}$$

$$\frac{10.5}{75} \quad \frac{9.0}{50} \quad 7.2 \quad \frac{4.2}{50} \quad \frac{4.2}{75}$$

$$\frac{10.7}{75} \quad \frac{9.2}{50} \quad 8.0 \quad \frac{5.0}{50} \quad \frac{4.9}{75}$$

$$\frac{10.8}{75} \quad \frac{9.3}{50} \quad 8.8 \quad \frac{4.6}{50} \quad \frac{4.4}{75}$$

$$\frac{11.0}{75} \quad \frac{9.8}{50} \quad 9.7 \quad \frac{4.9}{50} \quad \frac{4.0}{75}$$

$$\frac{13.4}{75} \quad \frac{12.9}{50} \quad 10.7 \quad \frac{9.2}{50} \quad \frac{8.0}{75}$$

$$\frac{4.7}{75} \quad \frac{4.9}{50} \quad 1.6 \quad \frac{3.4}{50} \quad \frac{2.7}{75}$$

Sta	+	Δ	-	Elev
-----	---	----------	---	------

919.26

38				16.8
----	--	--	--	------

+50				15.9
-----	--	--	--	------

39				15.0
----	--	--	--	------

+50				14.4
-----	--	--	--	------

40				13.9
----	--	--	--	------

+50				13.1
-----	--	--	--	------

41				12.5
----	--	--	--	------

+50				11.8
-----	--	--	--	------

42				11.2
----	--	--	--	------

+50				10.9
-----	--	--	--	------

43				10.4
----	--	--	--	------

+35				10.2
-----	--	--	--	------

L1

K

R1

$$\frac{4.9}{75} \quad \frac{5.2}{50} \quad 2.5 \quad \frac{4.5}{50} \quad \frac{4.7}{75}$$

$$\frac{5.3}{75} \quad \frac{5.3}{50} \quad 3.4 \quad \frac{4.5}{50} \quad \frac{4.6}{75}$$

$$\frac{5.9}{75} \quad \frac{5.8}{50} \quad 4.3 \quad \frac{4.8}{50} \quad \frac{4.6}{75}$$

$$\frac{6.1}{75} \quad \frac{5.9}{50} \quad 4.9 \quad \frac{5.1}{50} \quad \frac{4.8}{75}$$

$$\frac{6.6}{75} \quad \frac{6.2}{58} \quad \frac{6.8}{50} \quad 5.4 \quad \frac{5.2}{50} \quad \frac{5.5}{75}$$

$$\frac{8.9}{75} \quad \frac{8.3}{50} \quad 6.2 \quad \frac{5.8}{50} \quad \frac{6.3}{75}$$

$$\frac{10.0}{75} \quad \frac{9.6}{50} \quad 6.8 \quad \frac{6.9}{50} \quad \frac{7.4}{58} \quad \frac{7.5}{75}$$

$$\frac{10.5}{75} \quad \frac{10.2}{50} \quad 7.5 \quad \frac{8.2}{50} \quad \frac{8.4}{75}$$

$$\frac{10.8}{75} \quad \frac{10.3}{50} \quad 8.1 \quad \frac{8.5}{50} \quad \frac{8.2}{75}$$

$$\frac{10.4}{75} \quad \frac{10.0}{50} \quad 8.4 \quad \frac{7.6}{50} \quad \frac{7.6}{75}$$

$$\frac{10.5}{75} \quad \frac{9.8}{50} \quad 8.9 \quad \frac{7.7}{43} \quad \frac{7.9}{50} \quad \frac{8.7}{55} \quad \frac{8.7}{57} \quad \frac{7.9}{59} \quad \frac{6.7}{68} \quad \frac{5.6}{75}$$

$$\frac{10.2}{75} \quad \frac{9.8}{50} \quad 9.1 \quad \frac{7.5}{42} \quad \frac{8.5}{48} \quad \frac{7.9}{50} \quad \frac{9.0}{71} \quad \frac{5.8}{75}$$

Sta + π - Elev

919.26.

43+80

09.7

44

09.5

T.P. 1.98 910.29 - 10.95 908.31.

+50

08.8

45

08.0

+50

07.4

46

06.6

+50

06.0

47

05.2

+50

04.4

48

04.0

+50

03.9

49

04.4

L1

L

R1

$$\frac{10.3}{75} \quad \frac{9.6}{50} \quad 9.6 \quad \frac{6.1}{50} \quad \frac{4.3}{42} \quad \frac{8.9}{68} \quad \frac{8.6}{75}$$

$$\frac{10.1}{75} \quad \frac{9.4}{50} \quad 9.8 \quad \frac{6.8}{50} \quad \frac{7.2}{75}$$

$$\frac{2.7}{75} \quad \frac{0.0}{50} \quad 1.5 \quad \frac{0.6}{50} \quad \frac{2.0}{75}$$

$$\frac{4.0}{75} \quad \frac{2.5}{50} \quad 2.3 \quad \frac{3.7}{50} \quad \frac{4.5}{75}$$

$$\frac{5.9}{75} \quad \frac{5.7}{50} \quad 2.9 \quad \frac{5.7}{50} \quad \frac{5.8}{75}$$

$$\frac{7.7}{75} \quad \frac{7.8}{50} \quad 3.7 \quad \frac{7.4}{50} \quad \frac{7.4}{75}$$

$$\frac{9.4}{75} \quad \frac{9.4}{50} \quad 4.3 \quad \frac{9.0}{50} \quad \frac{8.9}{75}$$

$$\frac{10.8}{75} \quad \frac{10.8}{50} \quad 5.1 \quad \frac{9.8}{50} \quad \frac{9.6}{75}$$

$$\frac{11.4}{75} \quad \frac{11.7}{50} \quad 5.9 \quad \frac{10.3}{50} \quad \frac{9.8}{75}$$

$$\frac{11.7}{75} \quad \frac{11.3}{50} \quad 6.3 \quad \frac{10.2}{50} \quad \frac{9.6}{75}$$

$$\frac{11.5}{75} \quad \frac{11.8}{50} \quad 6.4 \quad \frac{10.4}{50} \quad \frac{9.5}{75}$$

$$\frac{11.5}{75} \quad \frac{11.4}{50} \quad 5.9 \quad \frac{9.7}{50} \quad \frac{8.7}{75}$$

Sta	+	Σ	-	Elev	
		910.29.			
49+50				05.7	
50				07.3	
+50				08.7	
51				10.1	
T.P	13.27	919.97	3.55	906.70.	
+25				10.8	
+67				11.8	
52				12.3	
+30				12.9	
+50				13.4	
+75				14.4	
+87				14.8	
53+02.60				15.2	
B.M	4.97	920.02	4.97	915.00	915.05

Lt.

Σ

Rt.

$$\frac{11.3}{75} \quad \frac{11.2}{50}$$

46

$$\frac{8.2}{50}$$

$$\frac{6.6}{75}$$

$$\frac{10.9}{75} \quad \frac{10.4}{50}$$

30

$$\frac{6.3}{50}$$

$$\frac{5.2}{75}$$

$$\frac{9.4}{75}$$

$$\frac{8.9}{50}$$

1.6

$$\frac{1.9}{50}$$

$$\frac{0.0}{75}$$

$$\frac{7.2}{75}$$

$$\frac{6.4}{50}$$

0.2

$$\frac{+1.5}{50}$$

$$\frac{+2.4}{64}$$

$$\frac{+3.2}{75}$$

$$\frac{14.9}{75}$$

$$\frac{13.7}{50}$$

9.2

$$\frac{7.6}{50}$$

$$\frac{6.9}{75}$$

$$\frac{3.7}{75}$$

$$\frac{0.0}{50}$$

8.2

$$\frac{7.4}{50}$$

$$\frac{6.6}{75}$$

$$\frac{+6.1}{75}$$

$$\frac{+5.0}{50}$$

77

$$\frac{6.8}{50}$$

$$\frac{7.1}{75}$$

$$\frac{10.7}{75}$$

$$\frac{1.7}{50}$$

71

$$\frac{77}{28}$$

$$\frac{67}{36}$$

$$\frac{72}{45}$$

$$\frac{74}{72}$$

$$\frac{91}{75}$$

$$\frac{5.9}{75}$$

$$\frac{6.5}{50}$$

66

$$\frac{8.0}{50}$$

$$\frac{8.4}{59}$$

$$\frac{77}{75}$$

$$\frac{10.0}{75}$$

$$\frac{10.1}{50}$$

5.6

$$\frac{6.1}{50}$$

$$\frac{5.4}{75}$$

$$\frac{7.5}{75}$$

$$\frac{7.1}{50}$$

5.2

$$\frac{4.2}{50}$$

$$\frac{3.8}{75}$$

$$\frac{6.7}{75}$$

$$\frac{6.2}{50}$$

4.8

$$\frac{3.5}{50}$$

$$\frac{2.7}{75}$$

Top Mon C' + Cleve.

Sta	+	Δ	-	Elev
		919.97 920.02		
53+18				15.2
+25				15.1
+46				15.0
54				15.8
+50				16.8
55				17.8
T.P.	8.19	925.16 925.21	3.00	916.97 917.02
+50				18.7
+63				18.9
56				19.5
+50				20.6
+82				21.3
57				21.8

Lt

Z

Rt

$$\frac{7.4}{75} \quad \frac{6.9}{50} \quad 4.8 \quad \frac{4.0}{50} \quad \frac{3.9}{75}$$

$$\frac{10.0}{75} \quad \frac{9.0}{50} \quad 4.9 \quad \frac{6.4}{50} \quad \frac{5.6}{75}$$

$$\frac{10.6}{75} \quad \frac{9.5}{50} \quad 5.0 \quad \frac{8.5}{50} \quad \frac{7.6}{75}$$

$$\frac{7.6}{75} \quad \frac{6.1}{50} \quad 4.2 \quad \frac{5.2}{50} \quad \frac{5.3}{75}$$

$$\frac{7.4}{75} \quad \frac{4.5}{50} \quad 3.2 \quad \frac{0.3}{50} \quad \frac{2.4}{75} \quad \frac{4.2}{100}$$

$$\frac{9.0}{75} \quad \frac{7.0}{50} \quad 3.2 \quad \frac{4.2}{50} \quad \frac{5.2}{75}$$

$$\frac{16.5}{75} \quad \frac{15.1}{50} \quad 6.5 \quad \frac{12.4}{50} \quad \frac{12.5}{75}$$

$$\frac{16.4}{75} \quad \frac{15.4}{50} \quad 6.3 \quad \frac{12.5}{50} \quad \frac{12.7}{75}$$

$$\frac{13.2}{75} \quad \frac{14.3}{50} \quad 5.7 \quad \frac{10.7}{50} \quad \frac{10.6}{75} \quad \frac{11.3}{100}$$

$$\frac{11.1}{75} \quad \frac{10.2}{50} \quad 4.6 \quad \frac{7.5}{50} \quad \frac{7.7}{75} \quad \frac{8.6}{100}$$

$$\frac{7.5}{75} \quad \frac{7.8}{50} \quad 3.9 \quad \frac{5.6}{50} \quad \frac{6.4}{62} \quad \frac{7.1}{75} \quad \frac{7.6}{100}$$

$$\frac{8.8}{75} \quad \frac{7.5}{50} \quad 3.4 \quad \frac{5.8}{50} \quad \frac{6.1}{62} \quad \frac{6.6}{75} \quad \frac{6.9}{100}$$

Sta	+	Δ	-	Elev
		925.15 925.21		
57+50				23.0
T.P.	16.18	939.27 939.32	2.07	923.09 923.14
58				24.2
+50				25.3
59				26.5
+50				27.9
60				28.9
+50				29.5
61				29.9
T.P.	3.25	934.64 934.69	7.88	931.35 931.44
+50				29.8
+85				29.5
62				29.5
+50				29.3

L1

K

R+

$$\frac{5.2}{75} \frac{3.8}{50} 2.2 \frac{2.5}{50} \frac{3.1}{75} \frac{3.1}{100}$$

$$\frac{17.2}{75} \frac{15.8}{50} 15.1 \frac{12.3}{50} \frac{12.2}{23} \frac{17.1}{80} \frac{16.7}{88} \frac{15.5}{93} \frac{15.6}{100}$$

$$\frac{11.8}{75} \frac{11.7}{50} 14.0 \frac{16.6}{50} \frac{17.3}{24} \frac{17.0}{85} \frac{16.2}{89} \frac{14.4}{100} \text{Ballast RRT.}$$

$$\frac{6.8}{75} \frac{8.2}{50} 12.8 \frac{14.9}{50} \frac{14.6}{75} \frac{14.6}{89} \frac{13.8}{92} \frac{13.23}{95} \text{Ballast RR T.}$$

$$\frac{2.6}{75} \frac{2.9}{50} 11.4 \frac{11.7}{46} \frac{12.0}{54} \frac{12.7}{20} \frac{12.8}{75} \frac{14}{85} \frac{13.2}{88} \frac{12}{98} \text{Bal RR}$$

$$\frac{1.1}{75} \frac{1.4}{50} 10.4 \frac{10.9}{42} \frac{17.1}{53} \frac{17.3}{60} \frac{16.9}{71} \frac{13.8}{77} \frac{12.4}{84} \text{Bal}$$

$$\frac{1.2}{75} \frac{1.0}{50} 9.7 \frac{10.3}{40} \frac{17}{50} \frac{16.9}{69} \frac{12.0}{81} \text{Bal}$$

61

$$\frac{7.5}{75} \frac{8.0}{50} 9.4 \frac{10.0}{40} \frac{15.2}{51} \frac{15.8}{70} \frac{11.5}{79} \text{Bal.}$$

$$\frac{8.5}{75} \frac{8.3}{50} 4.8 \frac{4.7}{39} \frac{9.2}{47} \frac{11.2}{55} \frac{10.9}{65} \frac{7.7}{73} \frac{6.6}{77} \text{Bal}$$

$$\frac{9.6}{75} \frac{9.3}{50} 5.1 \frac{5.4}{38} \frac{10.3}{48} \frac{11.0}{56} \frac{10.5}{65} \frac{7.8}{70} \frac{6.5}{77} \text{Bal}$$

$$\frac{7.4}{75} \frac{7.1}{50} 5.1 \frac{5.4}{39} \frac{10.6}{50} \frac{10.5}{66} \frac{7.6}{72} \frac{6.4}{77} \text{Bal.}$$

$$\frac{4.8}{75} \frac{5.4}{50} 5.3 \frac{5.8}{44} \frac{8.1}{49} \frac{8.2}{66} \frac{6.8}{71} \frac{6.8}{72} \frac{6.1}{78} \text{Bal}$$

Sta	+	π	-	Elev
		934.64		
		934.69		

63				28.7
----	--	--	--	------

+25				28.3
-----	--	--	--	------

+50				28.2
-----	--	--	--	------

64				28.2
----	--	--	--	------

B.M	6.70	934.64	6.70	927.94	927.94
-----	------	--------	------	--------	--------

+50				27.9
-----	--	--	--	------

65				27.6
----	--	--	--	------

+50				27.3
-----	--	--	--	------

66				27.0
----	--	--	--	------

T.P	3.39	931.29	6.74	927.90
-----	------	--------	------	--------

+50				26.9
-----	--	--	--	------

67				26.6
----	--	--	--	------

+50				25.9
-----	--	--	--	------

68				25.8
----	--	--	--	------

Lt R Rt

$$\frac{49}{75} \frac{64}{60} \frac{78}{50} 5.9$$

$$\frac{82}{50} \frac{87}{55} \frac{75}{62} \frac{70}{76} \frac{62}{79}$$

Ball

$$\frac{64}{75} \frac{79}{63} \frac{88}{50} 4.3$$

$$\frac{88}{50} \frac{87}{65} \frac{73}{77} \frac{63}{78}$$

Ball

$$\frac{66}{75} \frac{74}{68} \frac{83}{63} \frac{81}{50} 4.4$$

$$\frac{95}{50} \frac{93}{63} \frac{71}{75} \frac{63}{78}$$

Ball

$$\frac{42}{75} \frac{71}{50} 6.4$$

$$\frac{10.2}{50} \frac{10.3}{61} \frac{101}{68} \frac{7.2}{76} \frac{63}{79}$$

Ball

Spk in P.P 26 Lt Sta 64A 16

$$\frac{84}{75} \frac{91}{50} 6.7$$

$$\frac{10.6}{50} \frac{10.1}{68} \frac{65}{79}$$

Ball

$$\frac{91}{75} \frac{99}{50} 7.0$$

$$\frac{10.6}{50} \frac{9.8}{68} \frac{64}{79}$$

Ball

$$\frac{95}{75} \frac{98}{50} 7.3 \frac{98}{50} \frac{98}{66} \frac{83}{69} \frac{6.4}{79}$$

$$\frac{75}{75} \frac{86}{50} 7.6 \frac{79}{50} \frac{75}{53} \frac{87}{60} \frac{86}{69} \frac{63}{79}$$

Nail TR

$$\frac{2.8}{75} \frac{3.4}{67} \frac{3.2}{50} 4.4 \frac{3.6}{50} \frac{3.2}{76} \frac{3.9}{77} \frac{3.1}{79} \frac{242}{82}$$

Rail

$$\frac{5.6}{75} \frac{5.3}{50} 4.7 \frac{25}{50} \frac{3.2}{74} \frac{3.7}{77} \frac{3.1}{79}$$

$$\frac{9.2}{75} \frac{91}{50} 5.4 \frac{3.6}{50} \frac{3.7}{74} \frac{4.3}{77} \frac{3.4}{80} \frac{2.85}{82}$$

Rail

$$\frac{12.6}{75} \frac{12.4}{50} 5.5 \frac{4.7}{50} \frac{5.0}{73} \frac{4.8}{77} \frac{4.0}{80}$$

Sta	+	Δ	-	Elev
		931.29		
68+30				25.8.
+59				25.7.
+65				25.6.
69				25.8.
+50				26.0.
+88				26.1.
70				26.1.
+30				26.1.
T.P.	5.28	931.11	5.46	925.83.
+55				26.1.
71				26.2.
+50				26.3.
72				26.1.

Lt.

L

Rt

$\frac{12.4}{75}$	$\frac{11.4}{50}$	$\frac{10.1}{50}$	$\frac{10.1}{57}$	$\frac{9.2}{71}$	$\frac{5.2}{78}$	$\frac{4.2}{81}$
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$\frac{11.8}{75}$	$\frac{11.8}{50}$	5.6	$\frac{11.8}{50}$	$\frac{10.9}{67}$	$\frac{5.5}{80}$	$\frac{4.5}{80}$	Rail $\frac{3.7}{83}$
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$\frac{11.6}{75}$	$\frac{11.4}{50}$	5.7	$\frac{11.8}{50}$	$\frac{10.1}{68}$	$\frac{5.7}{79}$	$\frac{4.5}{82}$
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$\frac{8.6}{75}$	$\frac{9.0}{50}$	5.5	$\frac{12.0}{50}$	$\frac{10.7}{71}$	$\frac{4.8}{82}$	Rail $\frac{4.0}{84}$
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$\frac{6.3}{100}$	$\frac{5.3}{75}$	$\frac{4.5}{50}$	5.3	$\frac{11.2}{50}$	$\frac{11.0}{70}$	$\frac{7.4}{74}$	$\frac{4.8}{83}$
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$\frac{5.1}{100}$	$\frac{2.8}{75}$	$\frac{1.4}{50}$	5.2	$\frac{8.5}{50}$	$\frac{9.5}{70}$	$\frac{6.3}{77}$	$\frac{6.1}{81}$	Rail $\frac{5.1}{83}$
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$\frac{5.2}{100}$	$\frac{4.0}{92}$	$\frac{2.4}{75}$	$\frac{0.5}{50}$	5.2	$\frac{7.6}{50}$	$\frac{8.7}{73}$	$\frac{6.0}{80}$	$\frac{5.1}{84}$
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$\frac{6.9}{100}$	$\frac{3.3}{75}$	$\frac{1.7}{58}$	$\frac{0.0}{50}$	5.2	$\frac{5.9}{50}$	$\frac{6.9}{63}$	$\frac{6.8}{71}$	$\frac{5.7}{80}$	$\frac{5.1}{85}$
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$\frac{8.0}{100}$	$\frac{5.6}{75}$	$\frac{2.6}{50}$	5.0	$\frac{4.4}{50}$	$\frac{5.9}{65}$	$\frac{5.9}{81}$	$\frac{5.0}{83}$	Rail $\frac{4.3}{86}$
-------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	--------------------------

$\frac{10.1}{100}$	$\frac{9.4}{84}$	$\frac{8.3}{76}$	$\frac{5.8}{50}$	4.9	$\frac{4.3}{50}$	$\frac{8.5}{75}$	$\frac{5.7}{81}$	$\frac{5.0}{84}$
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$\frac{10.4}{100}$	$\frac{8.3}{75}$	$\frac{6.3}{50}$	4.8	$\frac{7.6}{50}$	$\frac{8.6}{59}$	$\frac{9.3}{75}$	$\frac{6.5}{79}$	$\frac{5.2}{84}$	Rail $\frac{4.6}{86}$
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$\frac{7.4}{100}$	$\frac{6.2}{75}$	$\frac{4.6}{50}$	5.0	$\frac{8.0}{50}$	$\frac{8.7}{59}$	$\frac{9.3}{73}$	$\frac{6.8}{77}$	$\frac{6.4}{80}$	$\frac{5.5}{83}$	$\frac{4.8}{85}$
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Swamp So. of Tr. Water Level 7.69

5/19/42

Sta	+	π	-	Elev
		931.11		
72+50				25.9.
73				25.3.
+54				24.9.
74				24.6.
+50				24.2.
+66				
75				24.0.
T.P	3.95	928.13	693	924.18
+50				23.8.
+66		X Drain 10" x 50' CM		
76				23.8.
+50				23.9.
77				23.9.
+50				23.5.
78+10				22.9.

Lt

Z

Rt

$$\frac{3.9}{100} \quad \frac{2.3}{75} \frac{1.9}{69} \quad \frac{1.3}{50} \quad 5.2 \quad \frac{7.9}{50} \frac{8.4}{53} \frac{9.4}{58} \frac{9.2}{73} \frac{6.5}{80} \frac{5.8}{82}$$

$$\frac{5.6}{100} \quad \frac{5.0}{75} \frac{4.7}{50} \quad 5.8 \quad \frac{9.9}{50} \frac{9.6}{25} \frac{8.5}{72} \frac{6.9}{74} \frac{6.9}{77} \frac{6.0}{80} \frac{5.20}{82} \text{ Rail}$$

$$\frac{10.8}{100} \quad \frac{10.5}{75} \quad \frac{10.1}{50} \quad 6.2 \quad \frac{5.9}{50} \frac{6.2}{70} \frac{6.6}{76} \frac{5.7}{78} \frac{5.07}{81} \text{ Rail}$$

$$\frac{12.0}{100} \quad \frac{11.9}{75} \quad \frac{11.3}{50} \quad 6.5 \quad \frac{6.4}{50} \frac{6.9}{66} \frac{6.5}{74} \frac{5.8}{76}$$

$$\frac{12.5}{75} \quad \frac{11.8}{50} \quad 6.9 \quad \frac{8.9}{50} \frac{8.2}{64} \frac{6.4}{73} \frac{5.6}{76} \frac{5.05}{78} \text{ Rail}$$

$$\frac{12.7}{75} \quad \frac{11.9}{50} \quad 7.1 \quad \frac{8.0}{50} \frac{6.4}{66} \frac{5.6}{75}$$

$$\frac{9.4}{75} \quad \frac{8.9}{50} \quad 4.3 \quad \frac{3.7}{50} \frac{3.6}{71} \frac{2.7}{75} \frac{2.12}{77} \text{ Rail}$$

$$\frac{8.75}{\text{Inv } 29}$$

$$\frac{9.4}{75} \quad \frac{8.7}{50} \quad 4.3 \quad \frac{2.9}{50} \frac{3.5}{72} \frac{2.8}{75} \frac{6.54}{\text{Inv } 27} \frac{2.20}{77} \text{ Rail}$$

$$\frac{8.1}{75} \quad \frac{8.2}{50} \quad 4.2 \quad \frac{3.0}{50} \frac{2.6}{56} \frac{3.9}{73} \frac{2.9}{76} \frac{2.32}{78} \text{ Rail}$$

$$\frac{5.6}{75} \quad \frac{6.0}{50} \quad 4.2 \quad \frac{3.5}{50} \frac{3.2}{65} \frac{3.9}{67} \frac{4.0}{73} \frac{3.2}{76} \frac{2.63}{78} \text{ Rail}$$

$$\frac{3.8}{75} \quad \frac{4.1}{50} \quad 4.6 \quad \frac{2.8}{50} \frac{3.5}{56} \frac{3.4}{66} \frac{4.0}{68} \frac{4.1}{76} \frac{3.5}{78} \frac{2.86}{80} \text{ Rail}$$

$$\frac{2.4}{75} \quad \frac{3.0}{50} \quad 5.2 \quad \frac{5.9}{50} \frac{4.5}{57} \frac{4.9}{77} \frac{4.0}{80} \frac{3.27}{81} \text{ Rail}$$

Sta	+	Δ	-	Elev
		928.13		
78+50				22.5
79				22.9
+32				24.0
+40				24.1
+42				24.13
+51.75				24.27
+62	Edge Point			24.13
+67				24.2
+76				24.1
B.M.	3.41	928.16	3.41	924.72
80				23.6
+50				21.5
81				20.2
T.P.	5.19	925.00	8.35	919.81

L1

K

R+

Ra.1

$$\frac{45}{75} \quad \frac{5.4}{50} \quad 5.4 \quad \frac{64}{50} \quad \frac{49}{57} \quad \frac{51}{64} \quad \frac{6.4}{69} \quad \frac{41}{80} \quad \frac{3.43}{83}$$

$$\frac{7.8}{75} \quad \frac{81}{50} \quad 5.2 \quad \frac{46}{50} \quad \frac{41}{72} \quad \frac{47}{78} \quad \frac{42}{81} \quad \frac{Ra.1}{36.5/83}$$

$$\frac{21}{75} \quad \frac{5.1}{65} \quad \frac{45}{50} \quad 41 \quad \frac{6.1}{50} \quad \frac{5.2}{67} \quad \frac{45}{70} \quad \frac{44}{79} \quad \frac{Ra.1}{376/82}$$

$$\frac{42}{75} \quad \frac{40}{50} \quad 40 \quad \frac{37}{50} \quad \frac{36}{75}$$

$$\frac{4.20}{75} \quad \frac{4.25}{50} \quad 400 \quad \frac{3.90}{50} \quad \frac{3.84}{75}$$

$$\frac{4.06}{75} \quad \frac{4.09}{50} \quad 386 \quad \frac{3.77}{50} \quad \frac{3.72}{75}$$

$$\frac{4.19}{75} \quad \frac{4.22}{50} \quad 400 \quad \frac{3.94}{50} \quad \frac{3.86}{75}$$

$$\frac{41}{75} \quad \frac{4.4}{50} \quad 39 \quad \frac{3.9}{50} \quad \frac{36}{75} \quad \frac{Ra.1}{3.70/81}$$

$$\frac{5.1}{75} \quad \frac{47}{50} \quad 40 \quad \frac{5.6}{50} \quad \frac{5.2}{61} \quad \frac{6.6}{67} \quad \frac{47}{75} \quad \frac{4.5}{79}$$

Spk in P.P. N.W. Cor G + New Brighton Rd

$$\frac{4.8}{75} \quad \frac{4.6}{50} \quad 46 \quad \frac{6.5}{50} \quad \frac{5.2}{57} \quad \frac{6.2}{64} \quad \frac{6.2}{69} \quad \frac{5.3}{75} \quad \frac{4.9}{79}$$

$$\frac{3.4}{75} \quad \frac{3.4}{63} \quad \frac{4.3}{50} \quad 67 \quad \frac{6.0}{50} \quad \frac{4.8}{71} \quad \frac{5.4}{74} \quad \frac{5.0}{77} \quad \frac{4.27}{79} \quad \frac{Ra.1}{5.0}$$

$$\frac{4.4}{75} \quad \frac{4.4}{66} \quad \frac{5.1}{50} \quad 8.0 \quad \frac{8.1}{50} \quad \frac{7.8}{54} \quad \frac{5.4}{63} \quad \frac{5.5}{73} \quad \frac{5.0}{76} \quad \frac{4.51}{78} \quad \frac{Ra.1}{5.0}$$

Sta	+	Δ	-	Elev
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925.00.

81+50

199

82

198

+41

190

83

19.3

+50

192

84

212

+50

23.0

+75

23.6

85

243

T.P.

11.99 936.64. 0.35

924.65

+39

25.2

T.P.

13.50 941.77. 8.37

928.27

+50

25.5

86

26.9

L7.

Z

R4

$$\frac{45}{75} \quad \frac{84}{50} \quad 5.1 \quad \frac{10.5}{60} \quad \frac{14.2}{55} \quad \frac{14.2}{58} \quad \frac{96}{61} \quad \frac{3.0}{75}$$

Rail

$$\frac{15.0}{75} \quad \frac{146}{50} \quad 5.2 \quad \frac{140}{50} \quad \frac{129}{57} \quad \frac{40}{69} \quad \frac{3.7}{73} \quad \frac{28}{75} \quad \frac{201}{78}$$

Rail

$$\frac{161}{75} \quad \frac{15.4}{58} \quad 6.0 \quad \frac{146}{58} \quad \frac{44}{69} \quad \frac{38}{74} \quad \frac{28}{76} \quad \frac{210}{78}$$

Rail

$$\frac{168}{75} \quad \frac{16.0}{50} \quad 6.7 \quad \frac{161}{50} \quad \frac{146}{55} \quad \frac{51}{69} \quad \frac{46}{72} \quad \frac{31}{71} \quad \frac{2.20}{78}$$

Rail

$$\frac{168}{75} \quad \frac{16.3}{50} \quad 5.8 \quad \frac{15.4}{50} \quad \frac{44}{70} \quad \frac{4.2}{74} \quad \frac{29}{76} \quad \frac{2.08}{78}$$

Rail

$$\frac{158}{75} \quad \frac{15.9}{50} \quad 3.8 \quad \frac{14.9}{50} \quad \frac{43}{67} \quad \frac{3.7}{73} \quad \frac{2.7}{75} \quad \frac{1.91}{78}$$

Rail

$$\frac{15.2}{75} \quad \frac{134}{50} \quad 2.6 \quad \frac{133}{50} \quad \frac{121}{59} \quad \frac{4.0}{68} \quad \frac{24}{75} \quad \frac{1.77}{78}$$

Rail

$$\frac{134}{75} \quad \frac{125}{50} \quad 1.4 \quad \frac{112}{50} \quad \frac{107}{58} \quad \frac{3.7}{68} \quad \frac{23}{75} \quad \frac{1.61}{78}$$

Rail

$$\frac{11.0}{75} \quad \frac{103}{50} \quad 0.7 \quad \frac{70}{50} \quad \frac{63}{64} \quad \frac{3.4}{71} \quad \frac{21}{75} \quad \frac{142}{78} \quad 23.6$$

$$\frac{13.2}{75} \quad \frac{132}{50} \quad \frac{123}{39} \quad \frac{114}{28} \quad \frac{13.2}{24-21} \quad \frac{120}{18} \quad \frac{11.9}{10} \quad 11.4 \quad \frac{117}{8} \quad \frac{120}{13} \quad \frac{126}{16-19} \quad \frac{10.9}{27} \quad \frac{9.7}{53} \quad \frac{14.2}{60} \quad \frac{148}{71} \quad \frac{128}{76}$$

$$\frac{17.0}{144} \quad \frac{17.0}{100} \quad \frac{165}{75} \quad \frac{157}{50} \quad \frac{143}{33} \quad \frac{18.2}{25-21} \quad \frac{16.9}{18} \quad \frac{16.6}{11} \quad 16.3 \quad \frac{16.7}{9} \quad \frac{17.9}{18} \quad \frac{178}{35} \quad \frac{143}{43} \quad \frac{13.9}{54} \quad \frac{18.9}{63} \quad \frac{20.0}{71} \quad \frac{18.7}{76} \quad 23.8$$

$$\frac{9.2}{200} \quad \frac{10.1}{150} \quad \frac{10.8}{100} \quad \frac{10.3}{75} \quad \frac{91}{50} \quad 14.9 \quad \frac{15.3}{9} \quad \frac{16.2}{20} \quad \frac{17.0}{23} \quad \frac{16.2}{48} \quad \frac{10.5}{54-57} \quad \frac{20.0}{71} \quad \frac{18.5}{76}$$

Rail

23.9

Sta	+	$\bar{x}$	-	Elev
		941.77.		

86+28				27.6
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+38				27.8
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+50				28.1
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87				29.6
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+22				30.1
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+50				30.6
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88				31.3
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+20				31.5
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+50				31.6
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+62				31.6
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+65'				31.6
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89				31.5
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Lt

✱

Rt

$$\frac{74}{125} \frac{73}{150} \frac{6.4}{200}$$

$$\frac{75}{100} \frac{65}{75} \frac{53}{45} \frac{147}{28} \frac{154}{24} \frac{154}{20} \frac{146}{18} \frac{146}{10} 14.2 \frac{145}{9} \frac{135}{15} \frac{155}{42} \frac{125}{50} \frac{93}{57} \frac{200}{70} \frac{183}{77} \frac{1778}{79}$$

$$\frac{5.5}{200} \frac{6.2}{163} \frac{63}{117} \frac{6.5}{100} \frac{53}{72} \frac{42}{47} \frac{143}{28} \frac{148}{20} \frac{143}{18} \frac{143}{10} 14.0 \frac{142}{10} \frac{145}{14} \frac{150}{15} \frac{145}{21} \frac{42}{36} \frac{42}{50} \frac{194}{71} \frac{182}{78} \frac{177}{79}$$

$$\frac{5.6}{200} \frac{6.0}{150} \frac{5.6}{138} \frac{5.7}{100} \frac{3.9}{50} 13.7 \frac{41}{50} \frac{194}{70} \frac{182}{78} \frac{1772}{79} \frac{241}{241}$$

$$\frac{32}{200} \frac{35}{150} \frac{3.3}{125} \frac{3.3}{100} \frac{3.4}{75} \frac{3.6}{50} 12.2 \frac{32}{48} \frac{193}{70} \frac{182}{77} \frac{1772}{79} \frac{241}{241}$$

$$\frac{3.1}{200} \frac{3.0}{150} \frac{3.0}{125} \frac{3.2}{100} \frac{3.2}{75} \frac{2.9}{50} 11.7 \frac{28}{48} \frac{95}{57} \frac{193}{72} \frac{182}{78} \frac{1772}{79} \frac{241}{241}$$

$$\frac{27}{200} \frac{3.0}{150} \frac{2.9}{125} \frac{2.7}{100} \frac{2.6}{75} \frac{3.1}{50} 11.2 \frac{2.6}{45} \frac{8.3}{53} \frac{12.5}{62} \frac{19.1}{70} \frac{18.1}{77} \frac{17.61}{79} \frac{241}{241}$$

$$\frac{22}{200} \frac{23}{150} \frac{2.4}{135} \frac{2.8}{100} \frac{2.9}{75} \frac{3.2}{50} 10.5 \frac{38}{45} \frac{85}{51} \frac{128}{61} \frac{194}{70} \frac{181}{77} \frac{17.60}{79} \frac{241}{241}$$

$$\frac{2.6}{200} \frac{2.7}{150} \frac{3.8}{100} \frac{3.9}{75} \frac{4.1}{50} \frac{3.9}{27} \frac{10.1}{20} \frac{11.0}{15} \frac{10.6}{9} 10.3 \frac{10.7}{10} \frac{11.3}{23} \frac{10.3}{38} \frac{4.4}{43} \frac{8.4}{52} \frac{14.2}{64} \frac{19.5}{71} \frac{18.2}{77}$$

$$\frac{3.5}{200} \frac{3.5}{150} \frac{3.8}{100} \frac{4.2}{75} \frac{4.5}{50} 10.2 \frac{10.5}{10} \frac{10.9}{21} \frac{10.3}{25} \frac{9.7}{39} \frac{5.0}{42} \frac{13.7}{59} \frac{14.1}{63} \frac{19.2}{71} \frac{18}{70}$$

$$\frac{37}{200}$$

$$\frac{34}{150} \frac{42}{100} \frac{4.5}{75} \frac{4.8}{50} \frac{4.6}{31} \frac{9.0}{23} \frac{10.7}{18} \frac{10.6}{9} 10.2 \frac{10.5}{10} \frac{11.0}{21} \frac{10.4}{25} \frac{8.7}{38} \frac{4.9}{40} \frac{13.9}{58} \frac{14.6}{63} \frac{15.4}{70}$$

$$\frac{37}{200}$$

$$\frac{34}{150} \frac{42}{100} \frac{4.5}{75} \frac{4.8}{50} \frac{4.6}{31} \frac{9.0}{23} \frac{10.7}{18} \frac{10.6}{9} 10.2 \frac{10.5}{10} \frac{11.0}{21} \frac{4.9}{29} \frac{5.0}{42} \frac{13.9}{58} \frac{14.6}{63} \frac{15.4}{70} \frac{18.2}{78}$$

$$\frac{3.9}{200} \frac{4.1}{150} \frac{4.5}{100} \frac{4.6}{75} \frac{5.1}{50} 10.3 \frac{5.9}{46} \frac{14.6}{60} \frac{15.2}{65} \frac{19.4}{70} \frac{18.2}{77} \frac{19.6}{79}$$

Sta	+	Δ	-	Elev
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941.77.

89+50

31.1

90

30.4

+50

29.4

91

28.3

T.P.

6.98

935.21

13.54

928.23.

+50

27.1

92

25.9

+50

25.0

93

24.1

T.P.

3.12

926.53

11.80

923.41.

+50

22.9

94

21.8

+50

20.6

95

19.5

Lt.

L

Rt

$$\frac{38}{200} \quad \frac{44}{150} \quad \frac{54}{100} \quad \frac{56}{75} \quad \frac{58}{50} \quad 10.7 \quad \frac{74}{47} \quad \frac{15.5}{60} \quad \frac{15.8}{65} \quad \frac{19.7}{70} \quad \frac{184}{77}$$

R. 24.0

$$\frac{46}{200} \quad \frac{62}{150} \quad \frac{69}{100} \quad \frac{73}{75} \quad \frac{75}{50} \quad 11.4 \quad \frac{76}{45} \quad \frac{16.3}{60} \quad \frac{16.9}{66} \quad \frac{19.7}{70} \quad \frac{184}{79} \quad \frac{1782}{79}$$

$$\frac{71}{200} \quad \frac{83}{150} \quad \frac{84}{100} \quad \frac{84}{75} \quad \frac{85}{50} \quad 12.4 \quad \frac{82}{49} \quad \frac{161}{62} \quad \frac{16.3}{65} \quad \frac{20.0}{70} \quad \frac{185}{77}$$

R. 23.8

$$\frac{88}{200} \quad \frac{90}{150} \quad \frac{89}{100} \quad \frac{89}{75} \quad \frac{88}{50} \quad 13.5 \quad \frac{10.1}{50} \quad \frac{16.4}{61} \quad \frac{16.9}{66} \quad \frac{20.0}{70} \quad \frac{186}{77} \quad \frac{17.98}{79}$$

R

$$\frac{2.7}{200} \quad \frac{3.1}{150} \quad \frac{3.2}{100} \quad \frac{3.2}{75} \quad \frac{3.6}{50} \quad 8.1 \quad \frac{4.9}{50} \quad \frac{5.4}{55} \quad \frac{10.5}{63} \quad \frac{13.5}{71} \quad \frac{12.3}{78}$$

R.

$$\frac{3.8}{200} \quad \frac{41}{150} \quad \frac{48}{100} \quad \frac{53}{75} \quad \frac{53}{50} \quad 9.3 \quad \frac{5.7}{50} \quad \frac{6.5}{57} \quad \frac{141}{70} \quad \frac{125}{77} \quad \frac{1202}{79} \quad \frac{23.2}{79}$$

$$\frac{44}{200} \quad \frac{55}{150} \quad \frac{59}{100} \quad \frac{61}{75} \quad \frac{63}{50} \quad 10.2 \quad \frac{6.7}{50} \quad \frac{7.1}{58} \quad \frac{141}{71} \quad \frac{129}{78}$$

$$\frac{5.5}{200} \quad \frac{6.2}{150} \quad \frac{6.9}{100} \quad \frac{7.4}{75} \quad \frac{76}{50} \quad 11.1 \quad \frac{8.4}{50} \quad \frac{9.1}{61} \quad \frac{145}{72} \quad \frac{132}{79} \quad \frac{12.73}{80} \quad \frac{22.5}{79}$$

R.

$$\frac{0.0}{100} \quad \frac{0.8}{75} \quad \frac{1.0}{50} \quad 3.6 \quad \frac{3.0}{50} \quad \frac{2.8}{67} \quad \frac{6.4}{72} \quad \frac{5.0}{77}$$

$$\frac{3.5}{100} \quad \frac{3.7}{75} \quad \frac{4.2}{50} \quad 4.7 \quad \frac{6.7}{50} \quad \frac{6.8}{56} \quad \frac{43}{66} \quad \frac{66}{71} \quad \frac{5.6}{79} \quad \frac{468}{80} \quad \frac{21.9}{79}$$

R

$$\frac{6.8}{75} \quad \frac{7.5}{50} \quad 5.9 \quad \frac{8.7}{50} \quad \frac{8.7}{63} \quad \frac{61}{68} \quad \frac{7.3}{72} \quad \frac{5.8}{79}$$

R

$$\frac{9.5}{75} \quad \frac{9.8}{50} \quad 7.0 \quad \frac{10.8}{50} \quad \frac{10.7}{64} \quad \frac{7.2}{70} \quad \frac{7.6}{73} \quad \frac{6.2}{79} \quad \frac{5.44}{80} \quad \frac{21.1}{79}$$

Sta	+	K	-	Elev
		926.53.		
95+50				18.3
96				17.4
+50				16.8
97				16.3
T.P.	469	920.59	10.63	915.90
+50				15.9
98				15.7
+50				15.6
99				15.6
+50				15.6
100				15.6
+50				15.6
101				15.6

L+

Z

R+

$$\frac{11.7}{75} \quad \frac{11.7}{50} \quad 8.2 \quad \frac{12.0}{50} \quad \frac{11.6}{66} \quad \frac{7.8}{73} \quad \frac{6.7}{79}$$

$$\frac{12.7}{75} \quad \frac{12.8}{50} \quad 9.1 \quad \frac{12.6}{50} \quad \frac{12.4}{65} \quad \frac{8.2}{72} \quad \frac{7.2}{78} \quad \frac{6.24}{81}$$

$$\frac{13.2}{75} \quad \frac{13.4}{50} \quad 9.7 \quad \frac{13.4}{50} \quad \frac{13.3}{64} \quad \frac{8.7}{73} \quad \frac{7.5}{79}$$

$$\frac{13.7}{75} \quad \frac{14.0}{50} \quad 10.2 \quad \frac{14.5}{50} \quad \frac{13.3}{66} \quad \frac{9.0}{73} \quad \frac{7.9}{79} \quad \frac{7.09}{81} \quad R$$

$$\frac{8.5}{75} \quad \frac{8.6}{50} \quad 4.7 \quad \frac{9.3}{50} \quad \frac{8.8}{65} \quad \frac{3.3}{73} \quad \frac{3.0}{78} \quad \frac{3.3}{80}$$

$$\frac{8.7}{75} \quad \frac{8.9}{50} \quad 4.9 \quad \frac{9.6}{50} \quad \frac{9.1}{68} \quad \frac{3.9}{74} \quad \frac{2.8}{79} \quad \frac{1.68}{80} \quad R$$

$$\frac{8.5}{75} \quad \frac{8.5}{50} \quad 5.0 \quad \frac{8.7}{50} \quad \frac{8.7}{63} \quad \frac{4.0}{73} \quad \frac{3.8}{77} \quad \frac{2.7}{80}$$

$$\frac{8.0}{75} \quad \frac{8.0}{50} \quad 5.0 \quad \frac{8.3}{50} \quad \frac{8.0}{65} \quad \frac{4.0}{74} \quad \frac{3.8}{78} \quad \frac{2.8}{80} \quad \frac{2.06}{82} \quad R$$

$$\frac{7.4}{75} \quad \frac{7.7}{50} \quad 5.0 \quad \frac{8.4}{50} \quad \frac{7.4}{68} \quad \frac{4.2}{74} \quad \frac{3.9}{77} \quad \frac{2.9}{80}$$

$$\frac{6.9}{75} \quad \frac{7.3}{50} \quad 5.0 \quad \frac{8.3}{50} \quad \frac{8.2}{66} \quad \frac{4.1}{74} \quad \frac{3.1}{77} \quad \frac{2.31}{82}$$

$$\frac{7.5}{75} \quad \frac{7.8}{50} \quad 5.0 \quad \frac{7.2}{50} \quad \frac{7.0}{69} \quad \frac{4.3}{73} \quad \frac{4.1}{77} \quad \frac{3.3}{80}$$

$$\frac{7.4}{75} \quad \frac{7.5}{50} \quad 5.0 \quad \frac{6.9}{50} \quad \frac{6.8}{64} \quad \frac{4.8}{70} \quad \frac{4.2}{77} \quad \frac{3.3}{80} \quad \frac{2.71}{82}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

		920.59		
--	--	--------	--	--

101+50				
--------	--	--	--	--

				15.6
--	--	--	--	------

102				
-----	--	--	--	--

				15.5
--	--	--	--	------

+50				
-----	--	--	--	--

				15.3
--	--	--	--	------

103				
-----	--	--	--	--

				15.3
--	--	--	--	------

+50				
-----	--	--	--	--

				15.3
--	--	--	--	------

104				
-----	--	--	--	--

				15.7
--	--	--	--	------

T.P				
-----	--	--	--	--

	252			
--	-----	--	--	--

		920.82		
--	--	--------	--	--

			229	
--	--	--	-----	--

				918.30
--	--	--	--	--------

+16				
-----	--	--	--	--

				15.8
--	--	--	--	------

+50				
-----	--	--	--	--

				15.9
--	--	--	--	------

105				
-----	--	--	--	--

				16.0
--	--	--	--	------

+35				
-----	--	--	--	--

				15.7
--	--	--	--	------

				15.9
--	--	--	--	------

+55				
-----	--	--	--	--

				16.0
--	--	--	--	------

+65				
-----	--	--	--	--

				16.1
--	--	--	--	------

LH.

2

R1

$$\frac{6.8}{75} \quad \frac{7.1}{50} \quad 5.0 \quad \frac{8.5}{50} \quad \frac{8.5}{66} \quad \frac{4.8}{72} \quad \frac{3.5}{80}$$

$$\frac{6.5}{75} \quad \frac{6.9}{50} \quad 5.1 \quad \frac{9.0}{50} \quad \frac{8.5}{67} \quad \frac{4.9}{73} \quad \frac{4.7}{76} \quad \frac{3.7}{80} \quad \frac{R}{3.02} \quad \frac{3.02}{82}$$

$$\frac{6.8}{75} \quad \frac{7.4}{50} \quad 5.3 \quad \frac{9.5}{50} \quad \frac{9.7}{65} \quad \frac{5.0}{74} \quad \frac{4.9}{77} \quad \frac{3.7}{81}$$

$$\frac{6.7}{75} \quad \frac{7.5}{50} \quad 5.3 \quad \frac{11.0}{50} \quad \frac{10.6}{67} \quad \frac{5.1}{74} \quad \frac{4.9}{79} \quad \frac{4.1}{81} \quad \frac{R}{3.31} \quad \frac{3.31}{83}$$

$$\frac{6.1}{75} \quad \frac{7.1}{50} \quad 5.3 \quad \frac{11.8}{50} \quad \frac{11.6}{60} \quad \frac{10.4}{69} \quad \frac{5.9}{76} \quad \frac{4.3}{81}$$

$$\frac{5.6}{75} \quad \frac{6.9}{50} \quad 4.9 \quad \frac{11.8}{50} \quad \frac{10.8}{69} \quad \frac{4.8}{76} \quad \frac{4.3}{81} \quad \frac{R}{3.58} \quad \frac{3.58}{83}$$

$$\frac{6.0}{75} \quad \frac{7.0}{50} \quad 5.0 \quad \frac{11.3}{50} \quad \frac{11.5}{66} \quad \frac{11.1}{68} \quad \frac{4.9}{76}$$

$$\frac{6.5}{75} \quad \frac{7.5}{50} \quad 4.9 \quad \frac{12.1}{50} \quad \frac{12.0}{59} \quad \frac{11.0}{67} \quad \frac{4.6}{76}$$

$$\frac{6.8}{75} \quad \frac{7.9}{50} \quad 4.8 \quad \frac{12.5}{50} \quad \frac{11.3}{66} \quad \frac{4.6}{76} \quad \frac{R}{3.92} \quad \frac{3.92}{83}$$

$$\frac{8.2}{75} \quad \frac{8.8}{50} \quad 4.9 \quad \frac{12.6}{50} \quad \frac{12.9}{63} \quad \frac{11.6}{67} \quad \frac{4.8}{77}$$

$$\frac{8.2}{75} \quad \frac{8.7}{50} \quad 4.8 \quad \frac{10.3}{50} \quad \frac{9.1}{68} \quad \frac{5.1}{76}$$

$$\frac{7.8}{75} \quad \frac{8.0}{50} \quad 4.7 \quad \frac{5.1}{50} \quad \frac{4.6}{75}$$

Sta + π - Elev

920.82

105+76

16.2

+89.07

164

B.M

5.00 915.82 915.88

L1

X

R1

$$\frac{5.6}{75} \quad \frac{5.4}{30}$$

4.6

$$\frac{5.1}{50} \quad \frac{4.4}{75}$$

$$\frac{4.5}{75}$$

$$\frac{4.5}{30}$$

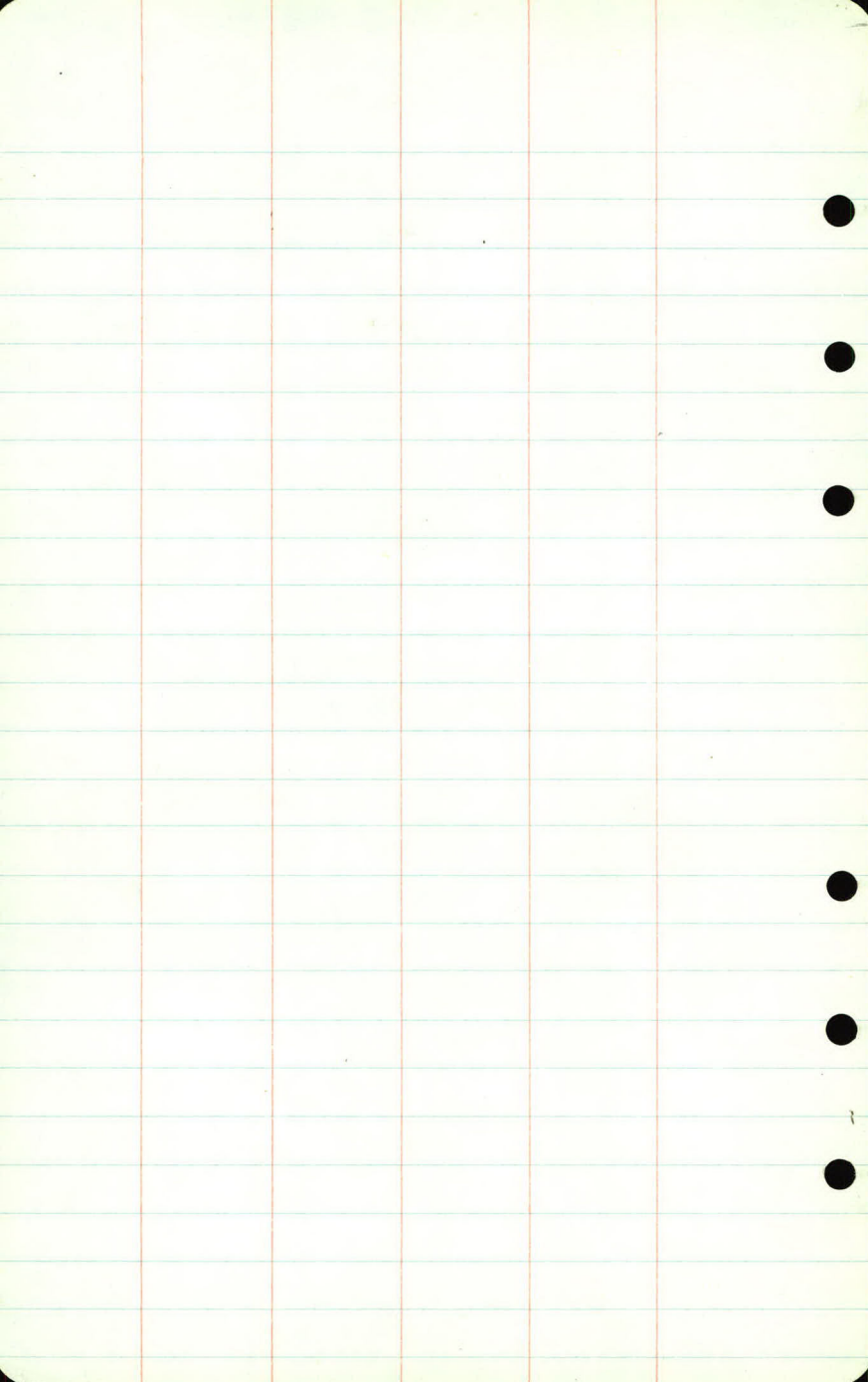
4.4

$$\frac{4.7}{30}$$

$$\frac{4.3}{75}$$

$$\frac{R}{420} \\ 83$$

Spk in H Pole S.E. Cor Snelling + @ Rd 'C'



Ditch Elev
Sta 69+83 to 76+00

Sta	+	$\bar{X}$	-	Elev
-----	---	-----------	---	------

B. M.	4.08	928.83		924.75
-------	------	--------	--	--------

74 +00				
--------	--	--	--	--

+50				
-----	--	--	--	--

75				
----	--	--	--	--

+50				
-----	--	--	--	--

76				
----	--	--	--	--

Elev. Top of Water	8.32			
--------------------	------	--	--	--

T.P.	5.54	930.83	3.59	925.29
------	------	--------	------	--------

68 +59				
--------	--	--	--	--

Elev. of Water Lt. 1260				
-------------------------	--	--	--	--

u	920.24			
---	--------	--	--	--

69 +83				
--------	--	--	--	--

Elev Water Rt. 9.34			X drain R.R.	
---------------------	--	--	--------------	--

T.P.	3.47	928.77	5.53	925.30
------	------	--------	------	--------

B.M.				
------	--	--	--	--

398	924.79	924.75		
-----	--------	--------	--	--

LT

¢

Rt.

Spk. in p.p. N.W. Cor. Co. Rd "C" + New Brighton Rd.

9.8	9.8	10.0	9.8	4.1
150	125	100	75	

10.0	10.2	10.3	9.9	4.6
150	125	100	75	

10.1	10.3	10.3	10.4	4.9
150	125	100	75	

10.3	10.2	10.3	10.1	5.0
150	125	100	75	

10.2	10.0	10.1	9.9	4.9
150	125	100	75	

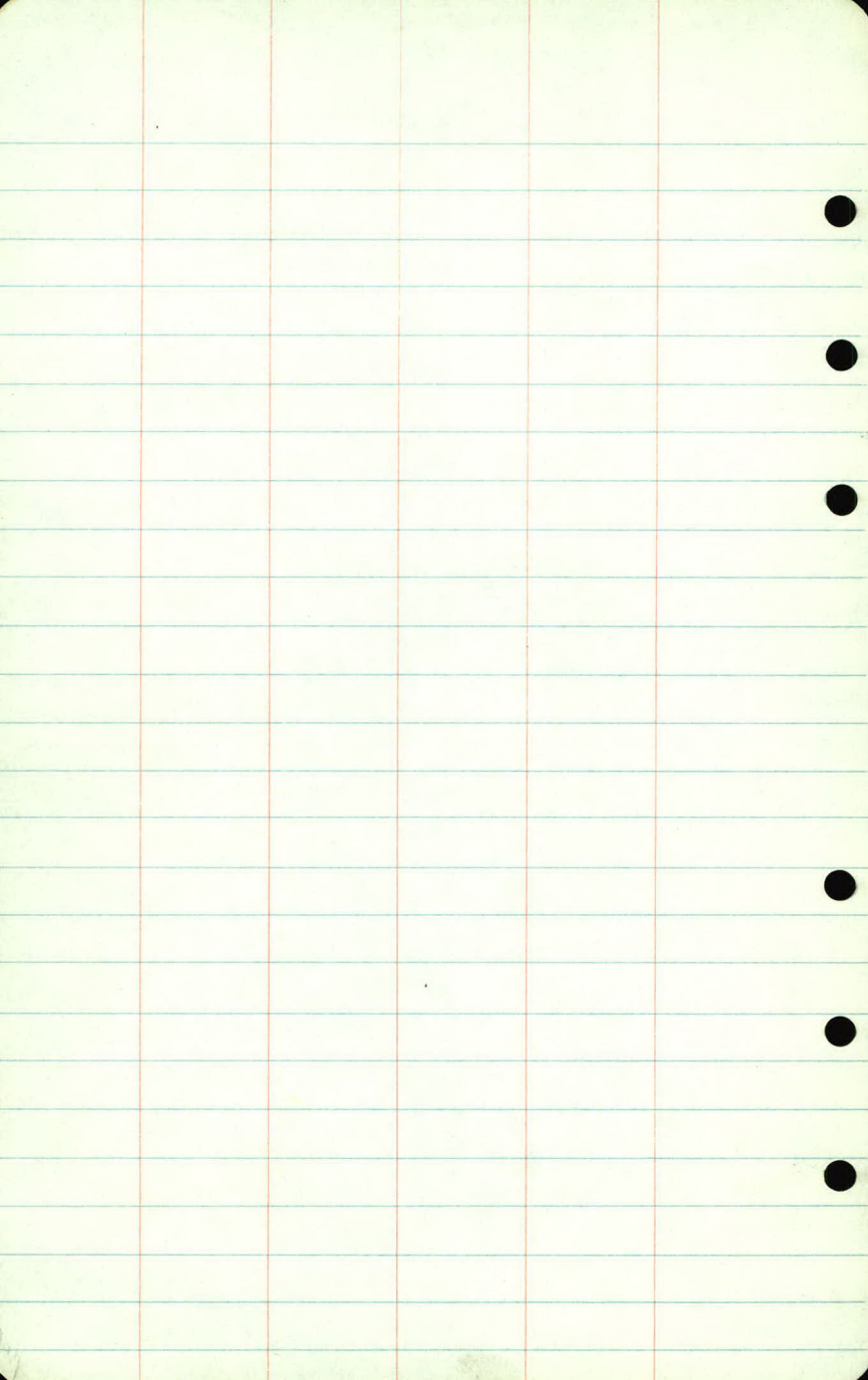
11.8	10.8	12.0	11.7	12.0	11.0
215	210	185	150	135	100

Beg. ditch 135' Lt.

12.9	13.0	14.2	14.2	14.7	15.0	15.2	15.3	15.4	17.1
250	300	350	400	450	500	550	600	650	700

F.I.	F.I.
10.53	10.50
67	106

Spk. in p.p. N.W. Cor. Co. Rd "C" + New Brighton Rd.



Borrow Pit
Sta 51+25 to 52+87
Ext. Sections

Sta	+	π	-	Elev
B.M.	12.19	927.24		915.05

51+25

51+50

11.4 11.2

+67

11.9 11.9

+80

12.0

52

12.3 12.4

+30

12.9 13.0

+50

13.4 13.5 $\frac{19.1160 \cdot 1244}{243 \cdot 217} \frac{2000}{2000}$

+62

13.9

+75

14.4 14.5

B.M

12.19 915.05

Lx.

Rt. 2

Top Mon & Cord "C" v Cleveland

$$\begin{array}{r} 21.2 \ 198 \ 184 \ 12.5 \ 12.2 \ 12.6 \ 17.2 \ 17.7 \ 16.3 \\ 88 \ 75 \ 66 \ 43 \ 38 \ 30 \ 23 \ 20 \ 13 \end{array} \quad 15.8 \quad \checkmark$$

$$\begin{array}{r} 20.1 \ 140 \ 9.4 \ 7.7 \ 6.8 \ 140 \ 14.6 \ 15.9 \\ 114 \ 86 \ 66 \ 51 \ 35 \ 26 \ 17 \ 13 \end{array} \quad 15.5 \quad \checkmark$$

$$\begin{array}{r} 21.0 \ 11.1 \ 6.3 \ 3.2 \ 4.2 \ 5.1 \ 6.5 \ 15.0 \ 16.8 \ 15.6 \\ 141 \ 105 \ 73 \ 56 \ 49 \ 39 \ 36 \ 25 \ 19 \ 13 \end{array} \quad 15.2$$

$$\begin{array}{r} 20.9 \ 10.8 \ 5.9 \ 1.9 \ 2.3 \ 1.1 \ 21 \ 40 \ 5.4 \ 14.5 \ 16.0 \ 15.3 \\ 170 \ 137 \ 113 \ 90 \ 68 \ 60 \ 50 \ 42 \ 34 \ 26 \ 18 \ 13 \end{array} \quad 14.9$$

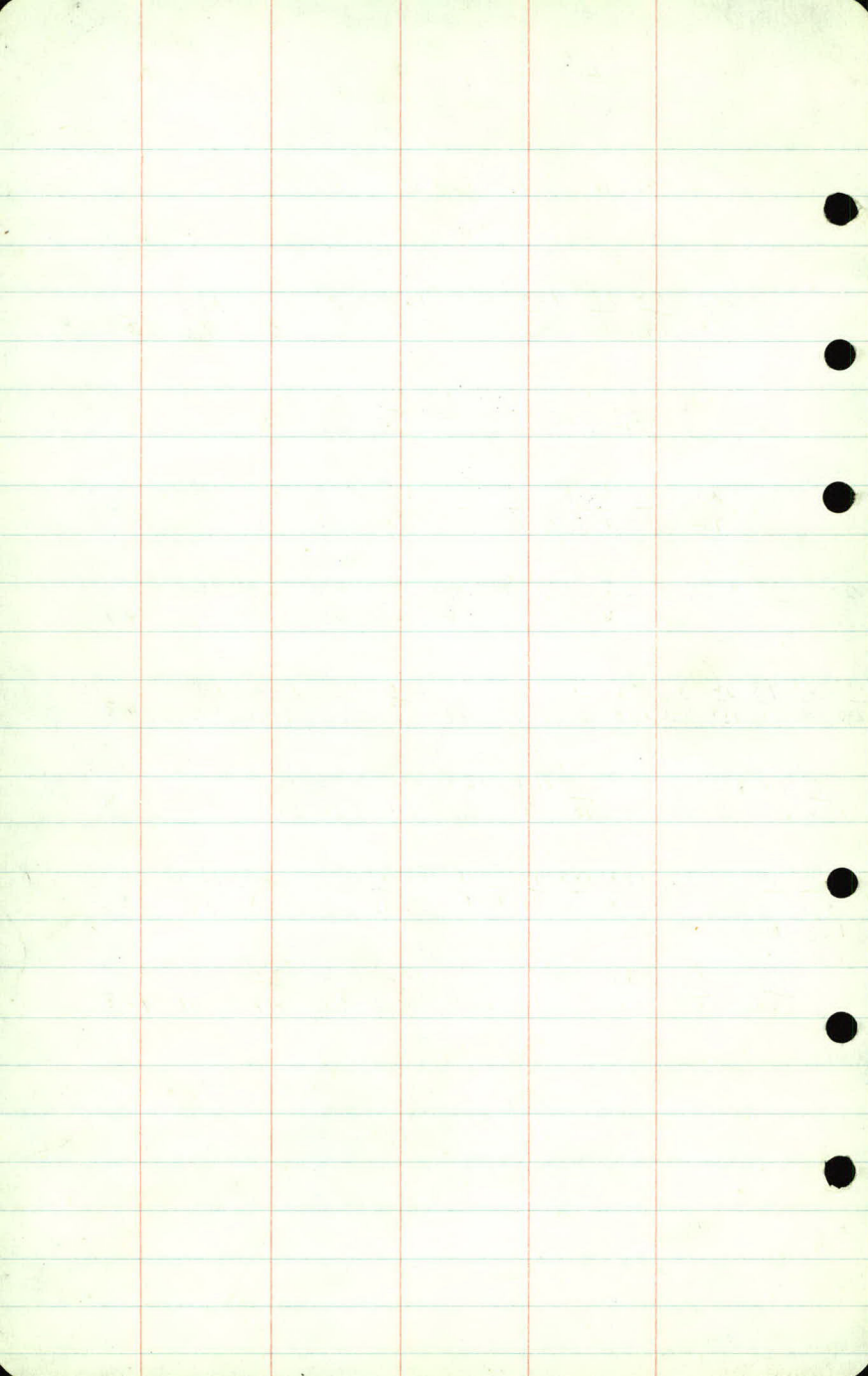
$$\begin{array}{r} 18.7 \ 16.7 \ 9.3 \ 3.6 \ 3.7 \ 4.6 \ 5.2 \ 5.8 \ 8.9 \ 10.8 \ 11.2 \ 16.5 \ 14.8 \\ 200 \ 186 \ 170 \ 154 \ 136 \ 128 \ 100 \ 75 \ 49 \ 35 \ 29 \ 21-19 \ 13 \end{array} \quad 14.3$$

$$\begin{array}{r} 8.9 \ 7.8 \ 8.3 \ 10.2 \ 11.5 \ 11.8 \ 11.9 \ 12.9 \ 13.6 \ 13.3 \ 16.0 \ 14.3 \\ 184 \ 171 \ 158 \ 137 \ 119 \ 100 \ 85 \ 73 \ 57 \ 26 \ 21-19 \ 15 \end{array} \quad 13.8$$

$$\begin{array}{r} 11.5 \ 11.8 \ 11.5 \ 11.3 \ 13.8 \ 14.8 \ 14.9 \ 15.1 \ 16.0 \ 15.7 \ 14.7 \ 14.4 \ 15.2 \ 13.9 \\ 217 \ 200 \ 182 \ 159 \ 137 \ 122 \ 100 \ 86 \ 67 \ 53 \ 45 \ 25 \ 22-20 \ 16 \end{array} \quad 13.3 \quad \checkmark$$

$$\begin{array}{r} 12.8 \ 18.2 \\ 233 \ 262 \end{array}$$

$$\begin{array}{r} 19.8 \ 18.9 \ 17.9 \ 18.1 \ 17.7 \ 17.2 \ 16.3 \ 14.5 \ 13.6 \\ 290 \ 250 \ 200 \ 150 \ 100 \ 52 \ 38 \ 29 \ 21 \end{array} \quad 12.8$$



X Sections

Gluck's Borrow Pit

10-1-42

Haw

AM

L.C

C.F

L.L

Sta	+	$\bar{A}$	-	Elev
B.M	5.29	919.84		914.55

51+50				10.8
-------	--	--	--	------

+67				11.1
-----	--	--	--	------

52				11.9
----	--	--	--	------

+30				12.9
-----	--	--	--	------

+50				13.4
-----	--	--	--	------

B.M	5.29			914.55
-----	------	--	--	--------

Lt

±

Sp4 in 12" oak 125' Rt Sta 52+65

$$\frac{143}{100} \quad \frac{13.2}{82} \quad \frac{9.5}{70} \quad \frac{11.1}{35} \quad \frac{8.9}{21} \quad 9.0$$

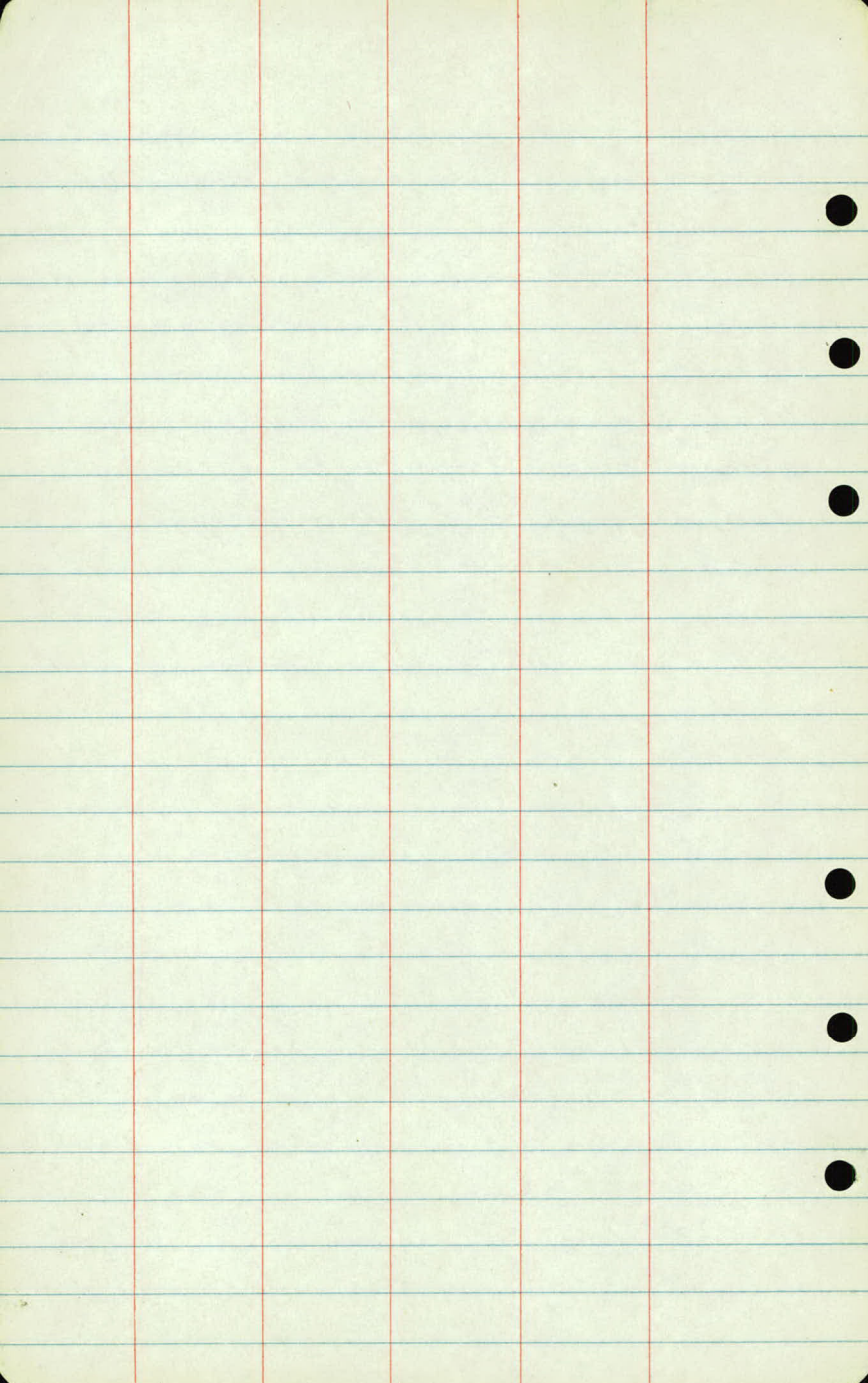
$$\frac{8.9}{100} \quad \frac{7.5}{86} \quad \frac{10.3}{62} \quad \frac{10.0}{46} \quad \frac{10.7}{30} \quad \frac{8.5}{20} \quad 8.7$$

$$\frac{130}{127}$$

$$\frac{2.7}{133} \quad \frac{+2.7}{116} \quad \frac{30}{100} \quad \frac{6.8}{53} \quad \frac{10.8}{36} \quad \frac{10.3}{28} \quad \frac{9.0}{21} \quad 7.9$$

$$\frac{+1.8}{158} \quad \frac{+4.3}{146} \quad \frac{+3.7}{120} \quad \frac{0.0}{100} \quad \frac{9.2}{50} \quad \frac{9.8}{31} \quad \frac{7.6}{18} \quad 6.9$$

$$\frac{1.7}{124} \quad \frac{2.1}{100} \quad \frac{2.8}{89} \quad \frac{8.5}{48} \quad \frac{8.9}{31} \quad \frac{6.8}{18} \quad 6.4$$



Location of Standing
Corn

On Armour's + Glueks Prop

8-27-42

HAW
AM
LL
CF

17

+50

18

+50

17

+50

16

+50

15

+50

14

+56

13

Row. 570k
1 38.0 390

1 38.1 387

1 41.3 42.3

1 41.0 42.0

3 40.8 48.8

3 42.5 49.5

1 43.1 44.1

1 40.7 41.7

2 41.0 47

2 42.5 46.5

2 42.5 46.5

4 42.4 53.4

comp 3 43.5 49.5'

22

+50

21

+50

20

+50

19

0	44.1
---	------

3	47.6	58.6
---	------	------

4	44.8	55.8
---	------	------

3	42.3	51.3
---	------	------

1	41.0	41.4
---	------	------

1	39.5	40.2
---	------	------

1	38.8	39.0
---	------	------

39

+50

38

+50

37

+50

36

+50

35

+50

34

756

33

Stake Inside Rows

39.6

0

4

39.0

0

36.9

0

36.0

0

39.0 - 38.0

0

43.2

40.2

2

43.2

40.1

2

41.4

40.4

1

39.6

39.0

1

40.5

40.0

1

43.5

38.5

2

47.7

40.7

2

46.2

40.6

3

46

450

39

42.3

0

39.6

2

