

BK. 61 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Drainage Survey

Little Canada Rd & Rice str.

From..... To.....

Road Acc't. No. 7

Date Filed 6-11-41

File.....

①

Drainage Situation

Little Canada Road.

Index :

ALIGNMENT.

Little Canada Rd - See Notes 1941

"A" Line 1-3

TOPOGRAPHY

Little Canada Rd - See Notes 1941

"A" Line 4-6

Completed 5-20-41

Party,

R. Poase

A. Moeschler

L. Gololberg

C. Fewer.

X SECT

Little Canada Rd. - 8-9

"A" Line 10-16

Note Profile of Spec. Ditch S. Side
Little Canada Rd. and Detail of M.H.
are in Little Canada Rd - 1941

Worked up

Haw

6/3/41

"A" Line

Angle

Sta.	Pt.	Lt.	Rt.
------	-----	-----	-----

3+92.5	P.I.	19°49'	
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2+17.35	P.I.	32°49'	
---------	------	--------	--

1+26.20	P.I.	80°07'	
---------	------	--------	--

0+23.86	P.I.	63°20'	
---------	------	--------	--

0+00	= 6171.8 Little Canada Sta.		
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19° 49'

32° 49'

80° 07'

63° 20'

R.I. 40523°

63° 25'

Little Gneiss

Spike

Sta.	Pt.	Angle	Rt.
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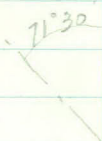
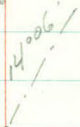
13+46.85	= 0+00	Little Canada Rd.	
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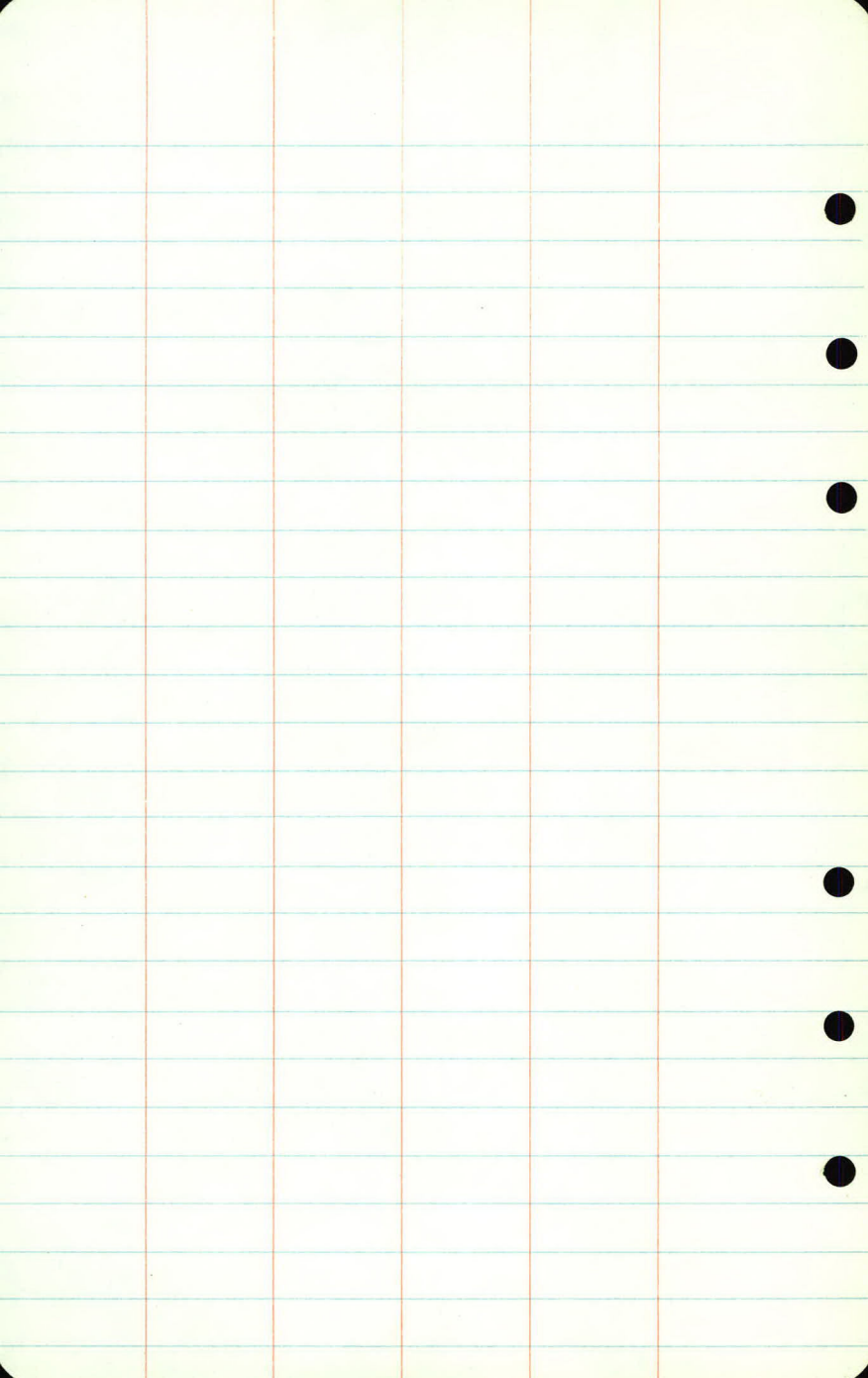
9+62.10	P.I.		E/Ric St.
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9+42.00	P.I.	14°06'	
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7+47.2	P.I.	71°30'	
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5+83.6	P.I.	21°56'	
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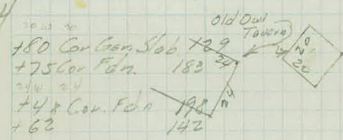


Topography "A" Line

Note See Little Canada Rd Notes

5

4



3

+04 $\frac{1}{2}$ End 6" W.I.P.

2

+48 $\frac{1}{2}$ End 6" W.I.P.

1

+67 $\frac{1}{2}$ 12" Pop.

0

+22 End 18" Vit.
 +14 Road N.
 -09 Road N.E.
 -20 End 18" Vit.

+100 P.H. 12. 35 80

+84 Bag. P.H. 66.92

+67 Will. 09

+66 Pot. Ho. 27

+46 Pot. Ho. 5-16-35

+40 Will. 25

+21 Pot. Ho. 39.60

+Int. Ditch 68

+86 End Pot. Ho. 18

+82 Ditch 62

+71 Bag. P.H. 11.26

+68 Pot. Ho. 39

+52 Pot. Ho. 43

+50 Bag. P.H. 47

+33 Pot. Ho. 37

+15 Pot. Ho. 22

+75 Twin O. 04

+71 Twin O. 11 02

+70 Cor. Outing. 06

+65 Twin O. 02

+64 Cor. Outing. 10

+45 12" Oak 04

+37 Cor. Shag 4

+29 Cor. Shag 11

+04 14" Oak 03

+06 Co. Ho. 30

+90 Cor. Ho. 47

+26 Road 9-32

Ditch 37

+88 Will. 03

+70 Ditch 34

+66 Pot. Ho. 04

Ditch 16'

+79 Bag. Ditch 10

+68 Pot. Ho. 20

+34 Pot. Ho. 23

+58 4" Oak 6

+03 15" Oak 02

+94 4" BE 02

+56 T.P. 07

LITTLE CANADA RD.

13

12

11

10

+74 Edge Ruc X3 E
+50 Edge Ruc X3 E
+42 & End - 15" x 44" Conc

9

8

+19 P.H. 5-18-26-73

7

+97 Will 19
+90 Will 18
+83 Will 08

6

A 75 P.H. 26

F 35 P.H. 26-75
F 35 Ditch 71
F 17 Beg. P.H. 26

155 Ent.
15' x 30' G.M. 26

100 Ent.

108 Cor. Ho. 58

175 Cor. Ho. 67



F 32 T.P. 13

F 18 Fe Cor. 49

Fe 17

147 Fe Cor. 04

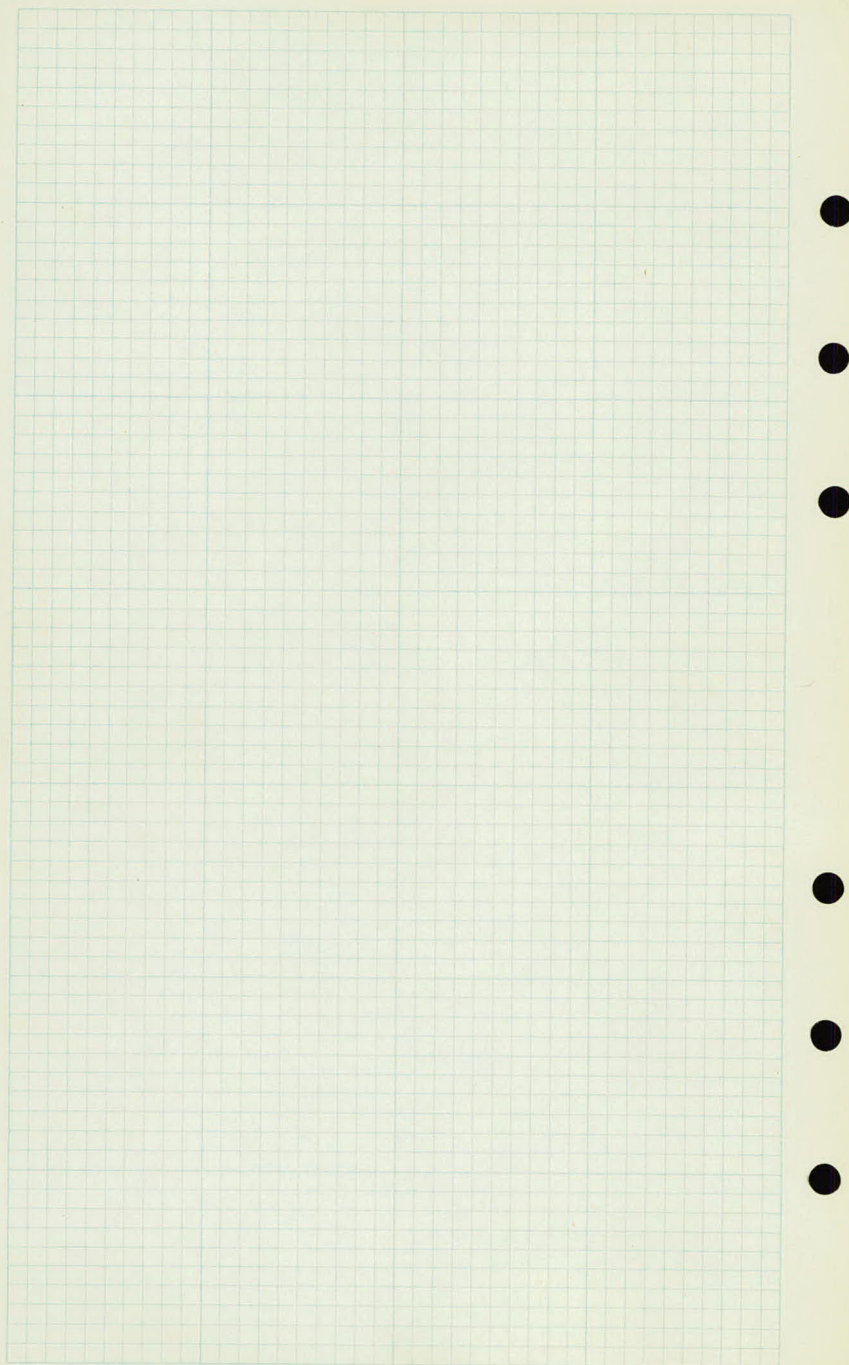
Ditch Ends 31

Ditch 37

- +85 End P.H. 11
- +78 Will 09
- +58 End P.H. 09
- +38 Will 12
- +25 Will 10
- +22 Will 18
- +11 Will 08
- +08 Will 19
- +07 Will 07
- +00 P.H. 07-16-28-68
- +82 Will 09
- +65 P.H. 5-17-28-72
- +64 Will 17
- +54 Will 17
- +47 Will 10
- +40 P.H. 5-16-46-91
- +30 Will 17
- +25 2 Wills -15-21

P.H. 12-35-84





Drainage Situation N.E. Cor.
Little Canada Rd and
Rice St.

X sect. Little Canada Rd.

Sta.	+	π	-	Elev.
B.M.	3.28	926.93		923.65
+100			4.0	22.9
+25			4.2	22.7
+30			4.2	22.7
+50			4.5	22.4
+75			4.8	22.1
2			5.2	21.7
+25			5.5	21.4
+40			5.6	21.3
+50			5.6	21.3
+75			5.4	21.4
3			5.3	21.6
+25			5.2	21.7

£

(8)

Top S.W. Cor. Conc. Platform 37' Lt. 0.35

8.4 8.4 8.5 8.5 6.8 6.4 5.8 5.5 5.1 4.9 4.4
200 175 150 127 121 100 80 70 40 19 13 4.0

Ditch

7.4 7.4 8.1 8.3 8.3 8.9 8.4 7.7 6.7 5.8 5.2 4.7
200 190 169 144 119 118 117 100 75 50 26 13 4.2

8.2 7.6 6.5 6.2 5.2 4.8
100 72 47 22 19 73 4.2

8.3 8.2 8.9 8.6 8.0 7.7 7.4 6.8 6.4 7.0 5.2 5.1
138 123 121 100 75 50 31 30 25 22-19 15 12 4.5

7.3 7.5 7.4
200 175 153

7.4 8.7 9.2 8.7 8.6 8.0 8.2 7.6 8.0 7.4 6.8 7.4 5.6 5.3
150 123 122 121 100 75 50 34 31 30 24 20 14 12 4.8

Ditch

7.2 7.9 7.4 8.7 9.3 8.6 8.5 8.1 8.2 6.9 8.1 6.2 5.7
200 175 150 127 126 125 100 75 50 25 23-17 14 12 5.2

8.1 8.0 7.6 8.5 9.4 8.2 7.9 7.6 7.5 7.2 7.8 6.2 6.1
200 175 150 129 127 125 100 75 50 22 21-18 13 10 5.5

8.5 8.0 8.3 9.1 9.6 9.3 8.0 7.6 7.1 7.3 6.4 6.1
200 175 150 130 129 128 100 75 50 22 12 9 5.6

9.5 10.3 10.5 10.8 7.6 8.2 5.8 5.7 6.0 6.8 6.2 6.1
200 173 150 125 119 100 75 50 30 21 12 9 5.6

8.8 9.7 10.3 10.0 7.3 6.5 4.9 4.1 4.8 6.8 6.8 6.0
200 190 160 134 125 100 75 50 27 20 16 9 5.4

9.6 9.0 8.5 7.2 5.9 4.3 3.7 4.3 7.1 6.0 5.7
200 175 150 125 100 75 50 27 19-16 12 9 5.3

9.3 8.1 7.9 7.5 5.9 4.1 3.9 4.1 6.0 5.7
200 175 150 125 100 75 50 25 19 9 5.2

£

Sta	L	π	-	Elev.
		926.93		

3+50			5.2	21.7
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+75			5.3	21.6
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4			5.3	21.6
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B.M.	5.03	926.19	5.27	921.16
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+25			4.7	21.5
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+50			4.8	21.4
-----	--	--	-----	------

+75			4.9	21.2
-----	--	--	-----	------

5			5.1	21.1
---	--	--	-----	------

+25			5.5	20.7
-----	--	--	-----	------

£

$\frac{10.1}{200} \frac{7.5}{75} \frac{7.9}{150} \frac{7.1}{125} \frac{6.2}{100} \frac{6.0}{75} \frac{5.6}{50} \frac{5.8}{25} \frac{5.6}{9} 5.2$

$\frac{9.5}{200} \frac{7.8}{75} \frac{9.6}{150} \frac{8.9}{125} \frac{7.8}{100} \frac{7.4}{75} \frac{7.0}{50} \frac{6.5}{24} \frac{7.3}{21.17} \frac{5.9}{13} \frac{5.7}{9} 5.3$

$\frac{9.2}{200} \frac{7.6}{188} \frac{9.1}{75} \frac{8.5}{150} \frac{8.3}{125} \frac{8.5}{100} \frac{8.1}{75} \frac{7.2}{50} \frac{5.8}{24} \frac{7.5}{20.17} \frac{6.1}{15} \frac{5.7}{8} 5.3$

Top Boulder Lt 4 + 45 19.7^{10} 19.4^{10}
 $\frac{5.8}{175} \frac{4.8}{150} \frac{6.1}{125} \frac{6.5}{100} \frac{6.2}{75} \frac{6.8}{50} \frac{6.8}{22} \frac{6.9}{15} \frac{5.4}{12} \frac{5.1}{9} 4.7$

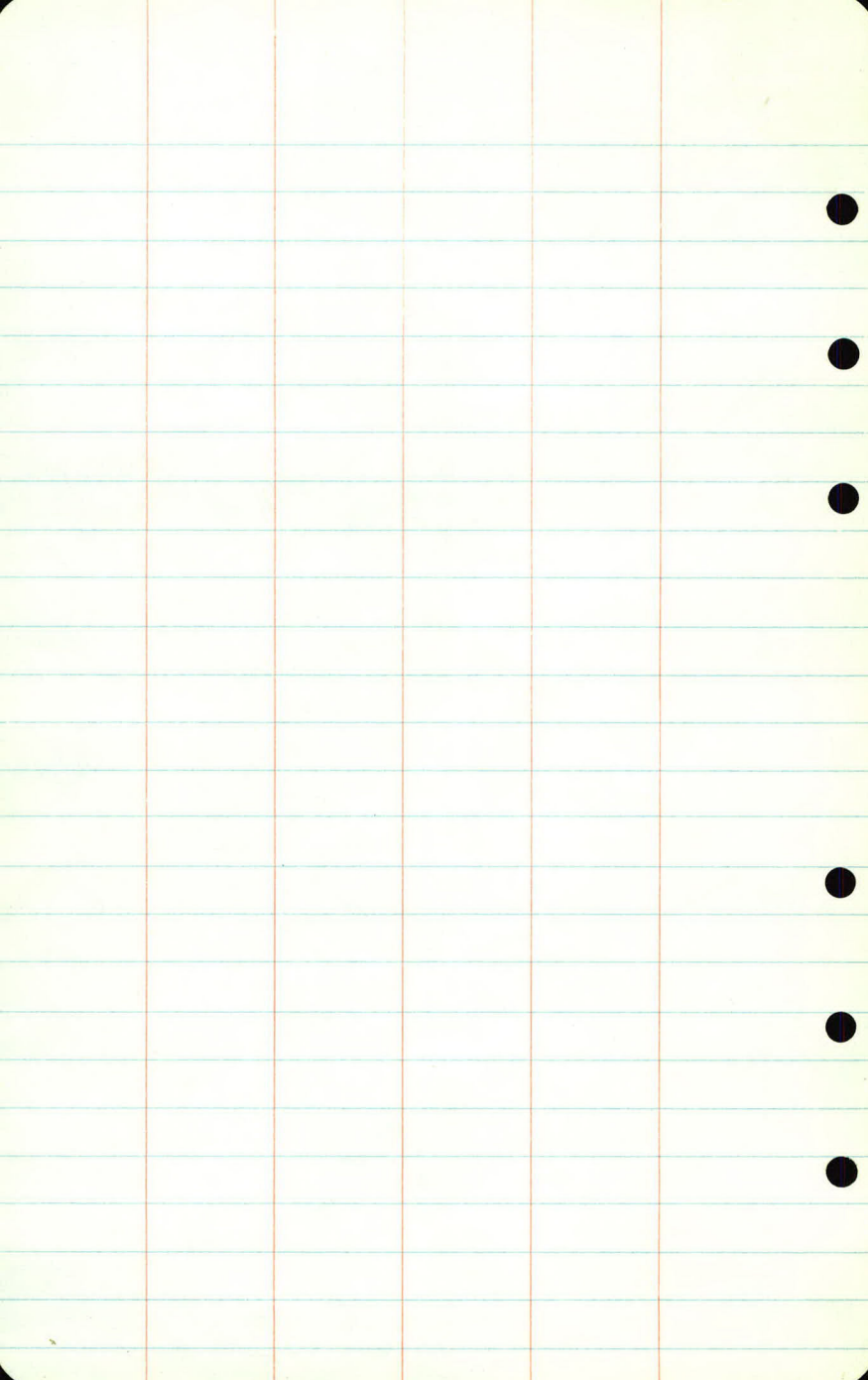
Top floor 19.2^{10} 18.2^{10} 19.8^{10} 19.1^{10} 18.2^{10} 20.1^{10} 21.0^{10}
Ho. Lt. $\frac{5.40}{130} \frac{6.1}{100} \frac{7.0}{75} \frac{8.0}{50} \frac{7.4}{23} \frac{7.0}{20.15} \frac{8.0}{13} \frac{5.7}{9} \frac{5.2}{4.8}$

$\frac{6.9}{150} \frac{6.7}{125} \frac{8.7}{100} \frac{8.4}{75} \frac{7.7}{50} \frac{6.3}{23} \frac{7.8}{20.16} \frac{5.7}{13} \frac{5.4}{10} 4.9$

$\frac{9.1}{100} \frac{8.7}{75} \frac{7.5}{50} \frac{6.0}{24} \frac{7.8}{21.17} \frac{6.0}{13} \frac{5.6}{11} 5.1$

$\frac{9.5}{100} \frac{9.5}{75} \frac{8.1}{50} \frac{6.0}{25} \frac{7.9}{21.17} \frac{6.2}{13} \frac{5.8}{10} 5.5$

£



Drainage Situation

N.E. Cor. Rice and Little Canada Rd.

X Sect. "A" Line

Sta.	T	K	-	Elev.
B.M.	5.03	926.19		921.16
0+20	F.L. 18" U.I.		11.25	914.94
0+22	F.L. 18" U.I.		10.88	915.31
+24			10.6	15.6
+50			10.9	15.3
+75			10.7	15.5
1			10.7	15.5
+25			10.4	15.8
+50			10.4	15.8
+75			10.5	15.7
2			10.5	15.7
B.M.	3.93	925.09	5.03	921.16
+25			9.3	
F.L. 6" W.I.P.			9.53	
+50			9.4	

Top Boulder L. 4+45

± L.C. Rd.

6.8	7.5	9.2	10.6	10.6	9.6	8.6	7.4	6.5	6.8	4.9
<u>18</u>	<u>7</u>	<u>2</u>	<u>1</u>	10.6	1	2	11	16	38	<u>57</u> <u>75</u>

6.6	7.3	9.9	10.0	8.4	8.2	6.7	6.3	5.3	4.5
<u>19</u>	<u>7</u>	<u>1</u>	10.9	1	6	21	50	65	<u>85</u> <u>100</u>

6.4	7.2	9.7	9.4	7.6	8.4	8.3	7.2	6.6	5.7
<u>18</u>	<u>7</u>	<u>1</u>	10.7	1	10	13	30	50	<u>75</u> <u>100</u>

6.2	7.1	9.6	9.4	7.7	7.6	8.7	9.5	9.4	7.4	7.0
<u>18</u>	<u>7</u>	<u>1</u>	10.7	1	5	11	18	37	53	<u>75</u> <u>100</u>

6.0	6.6	9.1	10.4	10.4	7.5	7.7	9.6	9.3	7.6
<u>18</u>	<u>8</u>	<u>2</u>	<u>1</u>	10.4	1	5	25	50	<u>75</u> <u>100</u>

7.2	7.5	7.7	8.2	9.2	9.6	7.9	8.8	9.1
<u>50</u>	<u>30</u>	<u>14</u>	<u>4</u>	<u>1</u>	10.4	1	4	<u>14</u> <u>25</u>

8.4	9.0	9.5	10.1	10.2	9.5	9.7	10.0
<u>50</u>	<u>30</u>	<u>16</u>	<u>1</u>	10.5	1	4	<u>18</u> <u>25</u>

9.1	9.5	9.6	9.9	9.8	8.9	9.4	8.2
<u>50</u>	<u>25</u>	<u>7</u>	<u>1</u>	10.5	1	4	<u>10</u> <u>25</u>

8.4	8.2	7.5	8.3	9.3	9.3	8.5	7.7	6.3	5.3	2.5	2.2
<u>25</u>	<u>17</u>	<u>4</u>	<u>2</u>	<u>1</u>	9.3	1	2	4	28	54	<u>83</u> <u>100</u>

8.0	8.0	7.4	7.9	9.4	9.4	8.3	7.4	6.2	5.2	2.5	2.5
<u>25</u>	<u>17</u>	<u>4</u>	<u>2</u>	<u>1</u>	9.4	1	2	5	25	50	<u>75</u> <u>100</u>

Sta.

+

π

-

Elev

925.09

2+75

8.2

3

7.4

F.L. 6" W. I. P.

8.75

+25

8.9

+50

8.8

+75

9.2

4

8.9

T.P.

5.16

923.06

7.19

917.90

+25

7.7

+50

7.6

+75

+75

6.8

5

6.1

Low Spot
9.42
205 R/L

+25

5.2

5.5 6.1 6.3 6.9 8.2 8.2 6.5 6.6 5.0 2.7 1.7
50 31 12 3 1 8.2 1 3 25 50 75 100

5.1 5.4 5.9 7.4 7.4 5.9 5.4 4.1 3.8 4.6 4.0
31 19 5 1 7.4 1 4 23 50 68 72 100

6.3 7.3 4.9 4.5 5.2 5.2 4.8 6.2 5.9 8.9 4.9 5.0 3.9 5.5 5.2 3.5 4.5 3.9
100 73 65 50 23 7 5 3 1 8.9 1 4 9 75 27 52 71 77 100

7.9 2.1 6.6 7.2 4.9 5.6 5.0 4.6 8.8 8.8 4.6 5.6 7.6 6.0 4.0 0.5
100 83 78 57 50 32 12 6 1 8.8 1 5 77 24 44 82 100

7.3 7.9 8.1 6.1 7.0 6.2 6.1 7.2 9.2 6.5 6.3 5.9 4.6 4.0
100 75 64 56 38 12 5 1 9.2 1 5 21 47 68 100

D
7.9 6.2 7.7 8.2 9.7 8.6 7.8 7.5 6.8 5.2 5.5
62 55 31 4 2 8.9 10 12 30 50 71 100

D
4.1 4.7 5.4 6.3 6.7 7.3 6.5 7.4 6.8 5.8 5.7 4.3 4.2 4.3
100 90 70 50 29 27 25 23 7.7 18 21 41 66 95 100

D LowSpot
4.1 4.6 6.4 6.8 7.2 6.7 7.5 7.9 7.5 6.9 5.8 5.9 5.3 4.7 4.1 3.7
100 89 66 46 45 43 36 21 7.6 77 23 25 47 69 100 130 139
5.5

5.5 7.1
170 200

D
5.4 5.7 5.3 5.0 5.8 6.4 7.3 7.5 6.5 5.5 5.6 5.0 4.9 5.2 6.7 7.5 8.0
100 81 57 56 55 38 33 15 6.8 18 23 56 87 100 130 155 179 200

LowSpot D D
8.1 6.2 6.7 5.4 5.7 5.3 6.9 5.3 5.9 6.3 5.6 6.3 6.5 4.0 5.1 4.8 5.0 6.6 8.2 9.0
140 126 122 115 100 66 65 63 34 20 6.1 16 18 19 25 50 82 100 134 160 182

D
5.3 6.7 5.7 6.0 4.3 5.5 5.9 7.0 7.5 6.0 5.5 4.6 6.0 3.7 5.3 4.8 5.5 7.2 9.0 9.3 7.3
200 180 152 125 109 100 75 65 43 37 23 5.2 24 26 29 50 75 100 127 142 184 200

Sta.	+	π	-	Elev
		925.06		
5+50			7.3	
+65			8.2	
+75			7.9	
6			6.9	
+25			5.7	
+50			5.3	
+75			5.0	

33 33 46 48 5.8 7.5 7.0 6.5 7.7 7.1 6.4 5.0 6.2 3.8 5.4 5.4 5.9
150 117 112 100 66 43 28 12 3 7.3 4 6 30 33 36 62 80 100

7.3 8.8 9.4 9.3
130 155 183 200

5.4 5.3 7.7 7.6 7.9 7.3 7.6 8.0 7.7 7.1 5.2 5.0
50 37 28 23 17 14 11 9 8.2 6 8 12 25

5.6 5.6 6.0 5.3 4.8 5.6 7.7 7.0 7.0 7.9 7.6 5.9 5.5 6.5 5.8 5.3 6.1 6.6 7.7
118 100 87 80 70 33 15 9 5 2 7.9 9 12 35 39 43 69 100 125 156

3.4 4.0 4.0
200 158 118

8.0 7.7
185 200

5.1 5.7 6.6 6.6 6.0 6.3 6.9 7.0 7.7 7.9 6.0 6.2 5.6 6.4 5.7 5.6 6.1 7.2
57 48 42 37 33 28 13 13 10 6 6.9 1 16 36 39 43 67 100 128

4.8 4.8 4.1 5.6 6.6 7.5 7.1
200 160 128 100 87 73 64

8.2 8.7 8.7
160 184 200

7.5 8.1 7.4 7.0 6.7 6.6 7.8 8.2 7.6 5.9 5.7 5.8 4.8 6.1 5.9 6.7 7.5
67 54 45 30 25 17 15 8 4 3 5.7 18 37 41 58 100 136 165

6.7 7.3
100 87

7.8
200

6.9 7.7 7.7 7.6 6.8 6.3 7.6 7.8 5.6 5.5 6.0 5.0 6.1 5.8 6.0 7.0
85 80 67 60 39 19 14 6 3 5.3 24 32 38 53 80 100 125

7.8 8.5 8.7
150 175 200

20 7.5 8.4 8.0 6.7 6.8 7.9 8.1 7.9 5.1 5.8 6.4 5.7 5.8 5.2 5.2
69 55 47 36 26 17 14 11 8 3 5.0 32 33 36 60 85 100

Sta.	L	π	-	Elev.
		923.06		
7			4.9	
+25			5.1	
I.P.	5.08	923.46	4.68	918.38
+50			5.5	
+67			6.4	
+75			6.7	
+86			6.4	✓
8			4.8	✓
+10			5.0	
+25			4.4	
+50			4.9	✓
+75			5.4	
9			5.4	✓

7.4 8.6 8.0 7.0 7.0 8.3 8.1 5.6 5.3 6.1 5.6 5.1 5.4 4.7
64 43 31 25 18 10 7 4 49 28 31 35 39 65 100

6.0 8.0 7.8 7.1 6.8 7.8 7.6 5.3 5.2 5.7 4.8 5.5 4.8 4.2
61 51 41 23 17 12 10 4 5.1 22 29 34 59 82 100

8.2 7.6 5.5 5.5 5.2 5.7 5.6
18 12 7 5.5 4 10 24 50

7.9 7.7 6.4 6.2 5.8 5.9 5.8
23 16 5 6.4 8 15 27 50

7.9 7.7 7.0 6.6 5.2 5.9 5.7 5.8
23 15 6 6.7 10 15 16 35 50

7.3 8.9 8.0 7.3 6.9 6.7 5.9 5.5 5.6 5.8
32 27 20 14 9 6.4 13 21 28 36 50

7.8 6.7 5.4 4.7 5.7 5.8 5.7 6.1 5.5
31 27 11 5 4.8 7 17 20 28 50

7.9 7.7 6.7 5.2 4.6 5.2 4.9 4.4 5.3 5.9 6.1 5.6
128 122 115 111 100 80 50 19 5.0 9 19 27 50

5.3 5.1 6.0 5.2 5.6 4.8 4.6 4.9 5.8 5.4 5.9 5.6
121 110 106 100 89 50 25 4.4 7 23 26 39 50

4.8 5.6 5.1 4.8 5.0 5.0 4.6 5.4 5.6 5.6 5.5
120 100 77 61 50 36 14 4.9 18 30 33 50

4.2 5.3 5.3 2.5 1.7 2.1 4.6 4.5 4.7 5.4 5.2 4.8 5.1
100 85 77 75 66 62 56 50 25 5.4 18 33 36 50

5.7 1.1 3.6 4.5 5.2 5.4 5.1 4.8 4.6 4.6
61 56 50 27 12 5.4 23 37 44 50

Sto.	+	π	-	Elev.
		923.46		
9+25			5.0	
E.F.L.	15" Conc.		5.53	
9+63			2.00	
10			1.90	
+25			1.73	
+50			1.59	
T.P.	5.67	927.46	1.67	921.79
+75			5.54	
11			5.52	
+25			5.48	
+50			5.37	
+75			5.27	
12			5.16	

$$\begin{array}{r} 1.4 \quad 2.2 \quad 4.9 \quad 4.8 \\ 72 \quad 50 \quad 34 \quad 13 \end{array} \quad \begin{array}{r} 5.3 \quad 4.7 \quad 4.0 \\ 12 \quad 30 \quad 50 \end{array}$$

$$\begin{array}{r} 5.1 \quad 5.0 \quad 2.7 \quad 2.15 \\ 50 \quad 24 \quad 18 \quad 12 \end{array} \quad 2.00$$

$$\begin{array}{r} 6.04 \\ W.F.L. 15'' \end{array}$$

$$\begin{array}{r} 1.9 \quad 2.1 \quad 3.2 \quad 5.3 \quad 2.5 \quad 2.06 \\ 50 \quad 40 \quad 32 \quad 28.25 \quad 20 \quad 12 \end{array} \quad 1.90$$

$$\begin{array}{r} 1.4 \quad 2.2 \quad 5.6 \quad 2.3 \quad 1.84 \\ 50 \quad 35 \quad 29.26 \quad 20 \quad 12 \end{array} \quad 1.73$$

$$\begin{array}{r} 1.4 \quad 1.6 \quad 5.5 \quad 2.2 \quad 1.69 \\ 50 \quad 35 \quad 29.26 \quad 20 \quad 12 \end{array} \quad 1.59$$

$$\begin{array}{r} 7.8 \quad 8.9 \quad 8.5 \quad 7.1 \quad 7.2 \quad 5.8 \quad 8.8 \quad 6.1 \quad 5.66 \\ 100 \quad 81 \quad 50 \quad 45 \quad 37 \quad 35 \quad 29.26 \quad 19 \quad 12 \end{array} \quad 5.54$$

$$\begin{array}{r} 9.0 \quad 8.7 \quad 9.4 \quad 9.0 \quad 7.8 \\ 178 \quad 150 \quad 132 \quad 110 \quad 107 \end{array}$$

$$\begin{array}{r} 8.0 \quad 9.6 \quad 9.3 \quad 8.4 \quad 8.1 \quad 8.8 \quad 8.4 \quad 6.1 \quad 5.70 \\ 180 \quad 143 \quad 110 \quad 100 \quad 52 \quad 39 \quad 25 \quad 18 \quad 12 \end{array} \quad 5.52$$

$$\begin{array}{r} 19.4 \quad 18.4 \quad 18.1 \quad 19.1 \quad 18.1 \quad 19.0 \quad 17.8 \quad 17.5 \\ 8.1 \quad 9.1 \quad 9.4 \quad 8.4 \quad 9.4 \quad 9.5 \quad 9.7 \quad 10.0 \quad 9.8 \quad 6.3 \quad 5.65 \\ 173 \quad 128 \quad 121 \quad 109 \quad 103 \quad 100 \quad 80 \quad 56 \quad 26 \quad 19 \quad 12 \end{array} \quad 5.48$$

$$\begin{array}{r} 17.8 \quad 19.8 \quad 19.3 \quad 19.3 \quad 18.2 \quad 18.3 \quad 18.0 \quad 17.2 \\ 9.7 \quad 7.7 \quad 8.2 \quad 8.2 \quad 9.3 \quad 9.2 \quad 9.5 \quad 10.3 \quad 10.2 \quad 9.4 \quad 8.5 \quad 6.1 \quad 5.60 \\ 194 \quad 171 \quad 152 \quad 117 \quad 109 \quad 100 \quad 85 \quad 61 \quad 33 \quad 31 \quad 24 \quad 19 \quad 12 \end{array} \quad 5.37$$

$$\begin{array}{r} 8.4 \quad 7.8 \quad 8.0 \quad 7.4 \quad 8.5 \quad 9.4 \quad 8.3 \quad 8.3 \quad 9.4 \quad 9.3 \quad 5.8 \quad 5.48 \\ 190 \quad 168 \quad 139 \quad 111 \quad 100 \quad 72 \quad 68 \quad 54 \quad 48 \quad 27 \quad 19 \quad 12 \end{array} \quad 5.27$$

$$\begin{array}{r} 8.4 \quad 8.3 \quad 8.2 \quad 8.7 \quad 9.2 \quad 8.3 \quad 7.1 \quad 6.4 \quad 5.40 \\ 200 \quad 146 \quad 111 \quad 100 \quad 66 \quad 43 \quad 40 \quad 26 \quad 12 \end{array} \quad 5.16$$

Sta.	+	π	-	Elev.
		927.46		
12 + 25			5.02	
+ 50			4.91	
+ 75			4.74	
B.M.			3.76	923.70 (923.65)

E

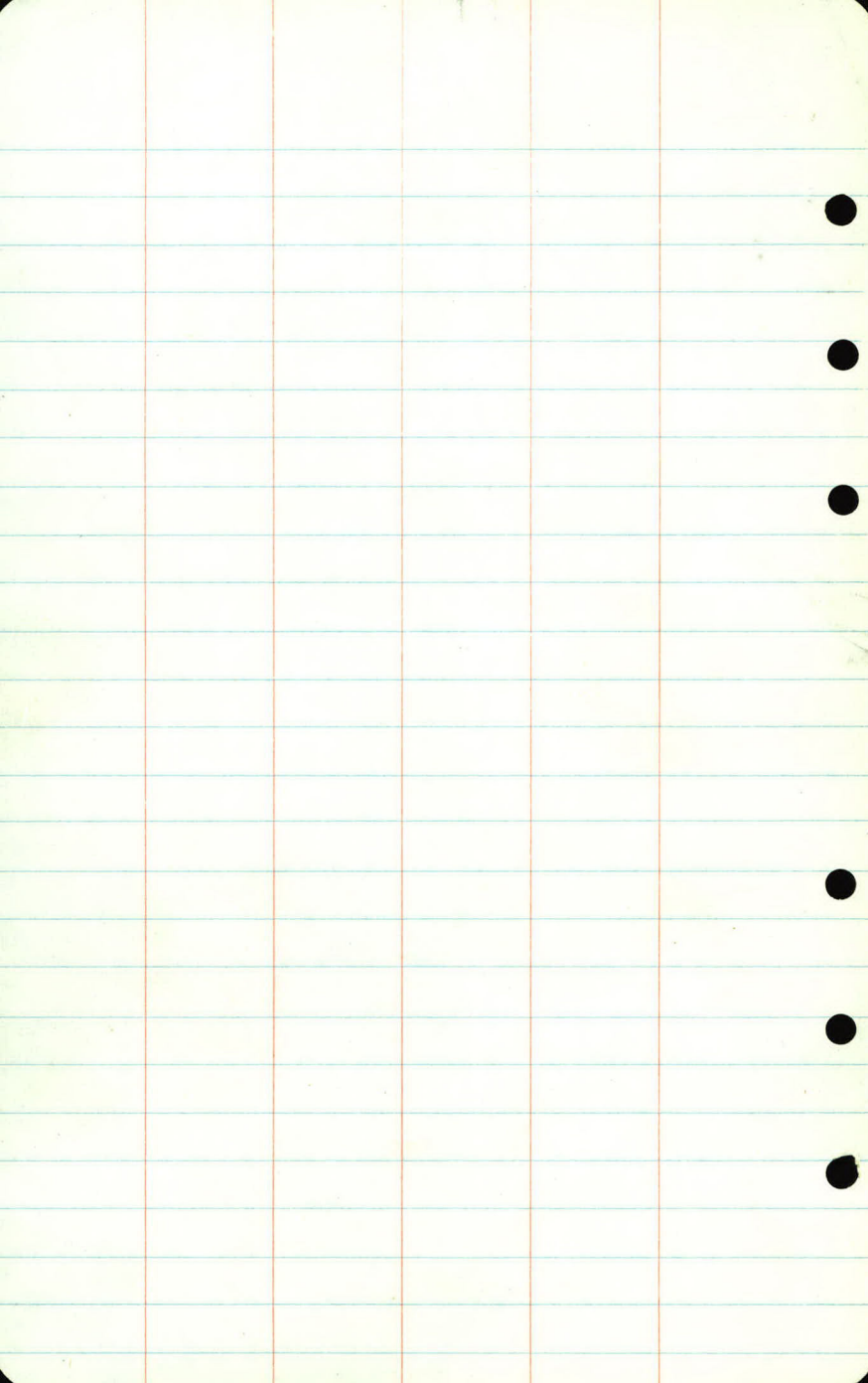
<u>8.0</u>	<u>8.1</u>	<u>8.4</u>	<u>8.8</u>	<u>9.2</u>	<u>9.2</u>	<u>7.6</u>	<u>6.5</u>	<u>5.25</u>
200	178	150	128	100	70	44	40	12
								502

<u>8.9</u>	<u>9.0</u>	<u>9.0</u>	<u>8.4</u>	<u>7.7</u>	<u>7.2</u>	<u>7.6</u>	<u>6.7</u>	<u>5.8</u>	<u>5.11</u>
200	176	150	126	108	91	76	48	42	12
								491	

<u>6.8</u>	<u>6.2</u>	<u>5.6</u>	<u>5.1</u>	<u>4.93</u>
100	78	52	28	12
				474

Top S.W. Cor. Conc. Platform

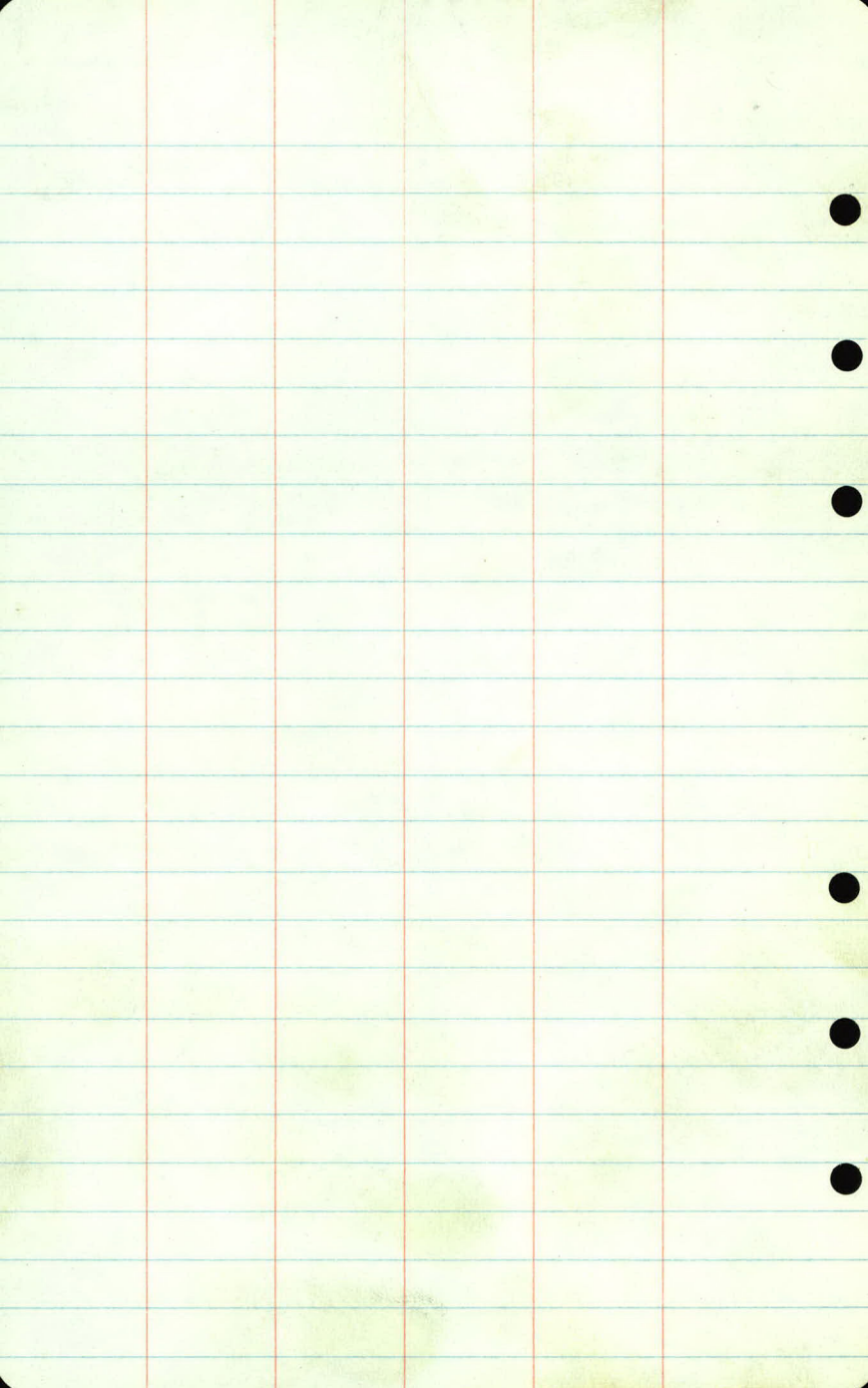
E



Little Canada Rd. - East Rice St.
Profile Prop. Line (Approx.)

Stn.	+	π	-	Elev.
B.M.	448	928.13		923.65
0+00			9.8	18.3
+02			9.8	18.3
+04			7.7	20.4
+11			7.1	21.0
+27 = 4+37 Little Con			6.7	21.4
+38			7.2	20.9
+43			9.5	18.6
+47			9.5	18.6
+50			9.2	18.9
+75			9.1	19.0
+90			9.6	18.5
1			9.0	19.1
+25			8.1	20.0
+50			8.0	20.1
+75			8.0	20.1
2			7.9	20.2
+25			9.1	19.0
+50			11.2	16.9
+64			11.3	16.8
+68			12.5	15.6
+71			12.5	15.6
+77			11.5	16.6
3			10.9	17.2

2 Spec. Ditch S. side Little Canada Rd.



Rice St.

Drainage Situation

S. of Little Canada Rd.

to Culv. N. of Little Canada Rd

B.M. 9.37 933.02 923.65

T.P. 12.02 944.87 10.17 932.85

0400 $\pm$ Ent 4.72 4015

+50 6.05 38.82

1 7.28 37.59

+50 8.41 36.46

T.P. 2.04 937.53 9.38 935.49

2 2.26 35.27

+50 3.51 34.02

+75 Thru center P. Hole 408 33.45

3 4.68 32.85

+50 5.72 31.81

4 6.81 30.72

+50 7.84 29.69

S.W. Cor. Platform 37' L + 0 + 35

$\frac{2.6}{100}$ $\frac{2.9}{70}$ $\frac{3.6}{42}$ $\frac{4.3}{21}$ $\frac{4.65}{12}$ 4.72

$\frac{4.3}{100}$ $\frac{3.8}{81}$ $\frac{3.2}{58}$ $\frac{3.3}{45}$ $\frac{3.5}{30}$ $\frac{6.7}{24}$ $\frac{6.3}{16}$ $\frac{6.11}{12}$ 6.05

$\frac{9.9}{100}$ $\frac{8.6}{80}$ $\frac{7.7}{52}$ $\frac{7.8}{34}$ $\frac{7.2}{27}$ $\frac{8.8}{25-22}$ $\frac{7.4}{20}$ $\frac{7.5}{17}$ $\frac{7.41}{12}$ 7.28

$\frac{14.3}{100}$ $\frac{13.6}{71}$ $\frac{12.4}{53}$ $\frac{10.6}{40}$ $\frac{10.7}{30}$ $\frac{10.2}{27}$ $\frac{10.6}{26-25}$ $\frac{9.9}{21}$ $\frac{9.0}{19}$ $\frac{8.75}{12}$ 8.41

$\frac{7.3}{100}$ $\frac{5.7}{68}$ $\frac{5.4}{51}$ $\frac{6.1}{39}$ $\frac{6.5}{33-36}$ $\frac{5.6}{32}$ $\frac{4.9}{28}$ $\frac{4.4}{27}$ $\frac{4.3}{23}$ $\frac{2.7}{16}$ $\frac{2.48}{12}$ 2.26

$\frac{9.3}{100}$ $\frac{9.0}{77}$ $\frac{8.6}{54}$ $\frac{8.2}{35}$ $\frac{7.7}{28}$ $\frac{6.9}{25}$ $\frac{4.3}{20}$ $\frac{3.7}{15}$ $\frac{3.67}{12}$ 3.51

$\frac{9.7}{100}$ $\frac{10.0}{80}$ $\frac{9.5}{62}$ $\frac{9.4}{46}$ $\frac{8.9}{32}$ $\frac{8.8}{27}$ $\frac{7.8}{24}$ $\frac{4.9}{18}$ $\frac{4.4}{15}$ $\frac{4.27}{12}$ 4.08

$\frac{9.2}{100}$ $\frac{9.0}{77}$ $\frac{8.6}{55}$ $\frac{8.8}{38}$ $\frac{9.1}{31}$ $\frac{8.8}{26}$ $\frac{5.1}{17}$ $\frac{4.82}{12}$ $\frac{4.7}{12}$ 4.68

$\frac{9.7}{100}$ $\frac{9.4}{85}$ $\frac{8.8}{53}$ $\frac{8.0}{31}$ $\frac{8.3}{26}$ $\frac{8.7}{24}$ $\frac{6.0}{18}$ $\frac{5.86}{12}$ 5.72

$\frac{9.4}{100}$ $\frac{8.8}{81}$ $\frac{8.8}{56}$ $\frac{9.1}{31}$ $\frac{9.0}{28}$ $\frac{9.0}{23}$ $\frac{7.5}{19}$ $\frac{6.95}{12}$ 6.81

$\frac{9.1}{100}$ $\frac{9.0}{81}$ $\frac{9.6}{55}$ $\frac{9.6}{30}$ $\frac{9.8}{28}$ $\frac{9.7}{23}$ $\frac{8.4}{17}$ $\frac{8.07}{12}$ 7.84

S/g	A	B	-	Elev.
		937.53		
5			900	28.53
T.P.	1.46	929.70	929	928.24
+50			2.38	27.32
6			3.55	26.15
+50			4.56	25.14
7			5.49	24.21
+50			6.41	23.29
8			7.04	22.66
+50			7.33	22.37
9			7.58	22.12
T.P.	4.60	926.45	7.85	921.85
+50			4.52	21.93
10			4.61	21.84
+50			4.80	21.65

$$\frac{10.8}{100} \quad \frac{10.8}{78} \quad \frac{10.3}{50} \quad \frac{9.9}{33} \quad \frac{9.0}{31} \quad \frac{9.2}{28} \quad \frac{11.4}{26-24} \quad \frac{9.2}{21} \quad \frac{9.20}{12} \quad 9.00$$

$$\frac{3.3}{100} \quad \frac{4.0}{91} \quad \frac{3.0}{68} \quad \frac{2.8}{53} \quad \frac{2.8}{34} \quad \frac{2.2}{33} \quad \frac{2.0}{27} \quad \frac{4.5}{26-24} \quad \frac{2.2}{21} \quad \frac{2.4}{16} \quad \frac{2.57}{12} \quad 2.38$$

$$\frac{4.1}{100} \quad \frac{5.2}{74} \quad \frac{4.9}{53} \quad \frac{5.0}{32} \quad \frac{4.4}{30} \quad \frac{4.3}{28} \quad \frac{5.5}{26-24} \quad \frac{3.6}{20} \quad \frac{3.68}{12} \quad 3.55$$

$$\frac{5.1}{100} \quad \frac{5.5}{70} \quad \frac{6.0}{46} \quad \frac{6.0}{33} \quad \frac{5.9}{30} \quad \frac{6.3}{26-24} \quad \frac{5.1}{22} \quad \frac{4.71}{12} \quad 4.56$$

$$\frac{5.6}{100} \quad \frac{6.2}{75} \quad \frac{6.7}{34} \quad \frac{7.2}{35} \quad \frac{6.0}{32} \quad \frac{6.5}{28} \quad \frac{6.8}{23} \quad \frac{5.7}{21} \quad \frac{5.71}{12} \quad 5.49$$

$$\frac{5.9}{100} \quad \frac{6.6}{75} \quad \frac{6.7}{56} \quad \frac{7.8}{35} \quad \frac{6.5}{33} \quad \frac{6.3}{30} \quad \frac{7.3}{27} \quad \frac{7.5}{23} \quad \frac{6.2}{20} \quad \frac{6.54}{12} \quad 6.41$$

$$\frac{6.7}{100} \quad \frac{7.3}{82} \quad \frac{8.0}{53} \quad \frac{8.0}{39} \quad \frac{8.2}{38-36} \quad \frac{7.6}{33} \quad \frac{8.1}{25} \quad \frac{7.0}{20} \quad \frac{7.09}{12} \quad 7.04$$

$$\frac{7.4}{100} \quad \frac{8.5}{66} \quad \frac{8.5}{34} \quad \frac{8.7}{31} \quad \frac{9.0}{25} \quad \frac{7.5}{19} \quad \frac{7.36}{12} \quad 7.33$$

$$\frac{7.1}{100} \quad \frac{7.5}{74} \quad \frac{8.7}{55} \quad \frac{8.8}{35} \quad \frac{9.5}{31} \quad \frac{9.8}{23} \quad \frac{8.2}{20} \quad \frac{7.80}{16} \quad \frac{7.63}{12} \quad 7.58$$

$$\frac{3.6}{100} \quad \frac{3.7}{75} \quad \frac{4.9}{56} \quad \frac{6.0}{34} \quad \frac{6.7}{29} \quad \frac{7.0}{25} \quad \frac{4.9}{20} \quad \frac{4.66}{12} \quad 4.52$$

$$\frac{4.7}{100} \quad \frac{4.9}{76} \quad \frac{5.9}{48} \quad \frac{6.5}{39} \quad \frac{6.6}{32} \quad \frac{7.4}{26} \quad \frac{5.4}{19} \quad \frac{4.29}{12} \quad 4.61$$

$$\frac{4.7}{100} \quad \frac{5.9}{70} \quad \frac{6.9}{37} \quad \frac{7.5}{36-35} \quad \frac{6.9}{34} \quad \frac{6.7}{32} \quad \frac{7.9}{28} \quad \frac{7.4}{23} \quad \frac{5.6}{19} \quad \frac{4.97}{12} \quad 4.80$$

Sta + π - Elev

926.45

11

5.08 21.37

418 Sec. thru 15' Cols 5.09 2136

B.M.

2.79 923.66 (923.68)

$\frac{48}{100}$ $\frac{61}{77}$ $\frac{74}{52}$ $\frac{73}{39}$ $\frac{81}{37}$ $\frac{76}{35}$ $\frac{83}{34}$ $\frac{78}{28}$ $\frac{60}{24}$ $\frac{522}{20}$ $\frac{508}{12}$

$\frac{48}{100}$ $\frac{59}{81}$ $\frac{73}{58}$ $\frac{80}{42}$ $\frac{82}{32}$ $\frac{FL}{23}$ $\frac{914}{24}$ $\frac{87}{19}$ $\frac{58}{12}$ $\frac{528}{509}$

