

BkG - Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- Plan ----- Survey

COUNTY ROAD H?

From Centerville Rd. To Bald Eagle Blvd. W.

Road Acc't. No. 61

Date Filed. 10/24/29

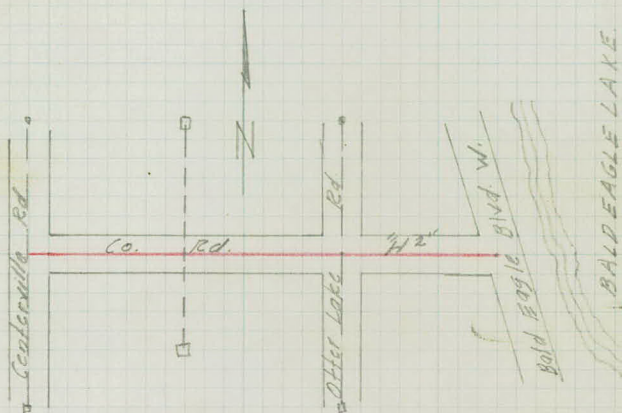
File -----

1058

PLAN SURVEY

CO. RD. "H 2"

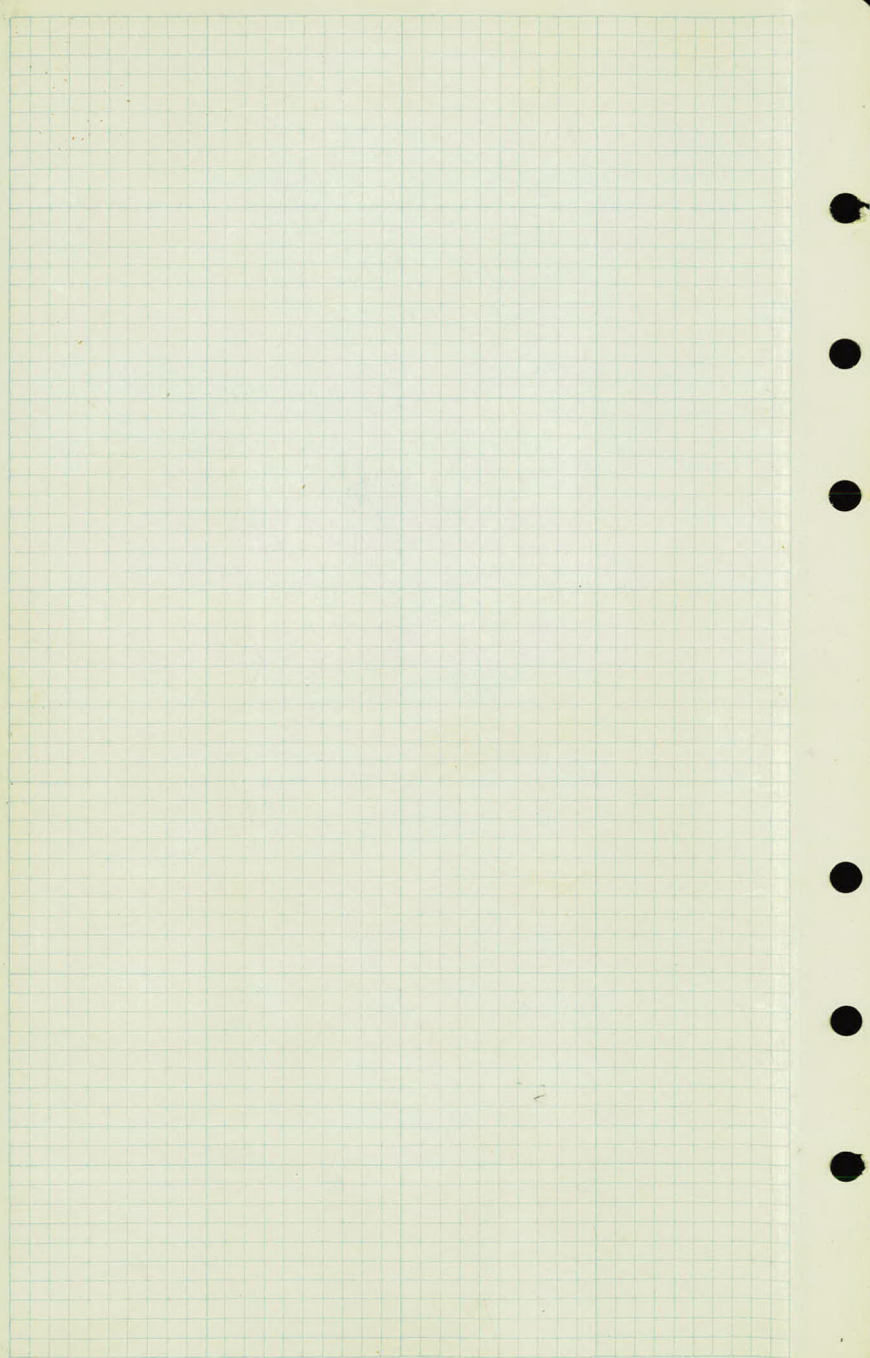
Centerville Rd. to Bald Eagle Blvd. W.



INDEX

- Align. - 1-3
- Topog. - 4-16
- X-Sections - 17-32

Completed
9/23/39



Alignment

Co. Rd. H2
From Centerville Rd
To Bald Eagle Blvd. W.

Recd.
9/14/39
J.H.C.

Sta.	Point	ΔL	ΔR
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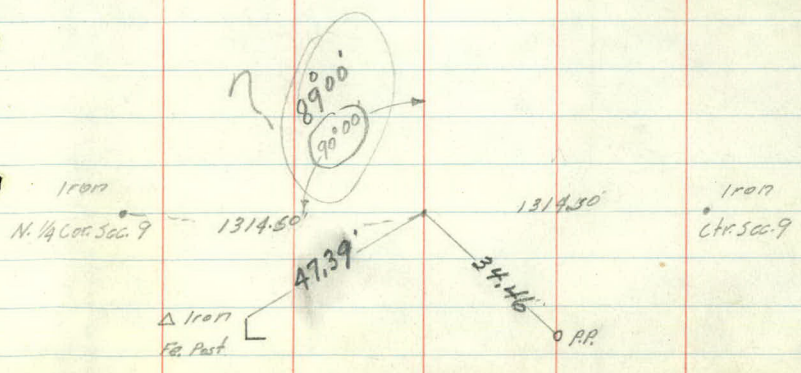
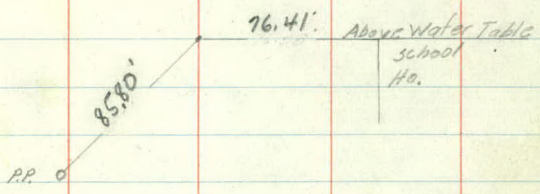
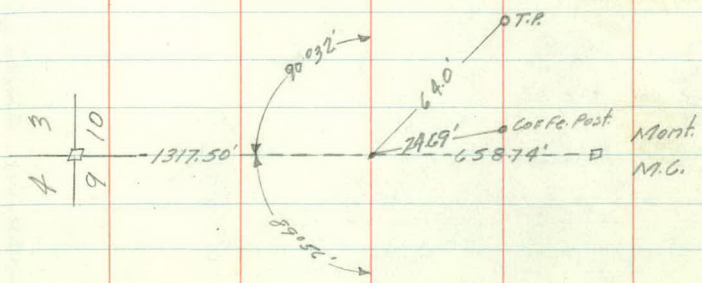
26	+54.89 P.I.		
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		$\checkmark$ $0^{\circ}28'$	
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11	+56.35 P.O.T.		
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0	+00		
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7/12/37
K.A.
A.B.
M.B.



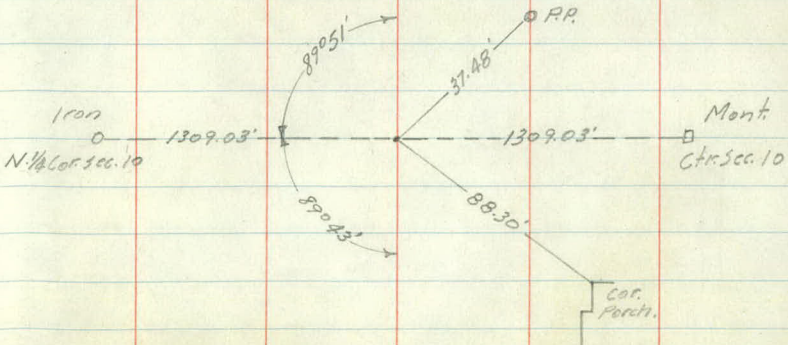
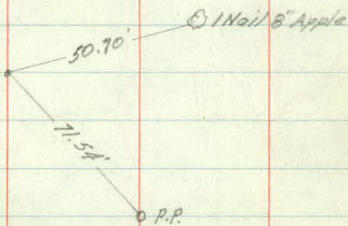
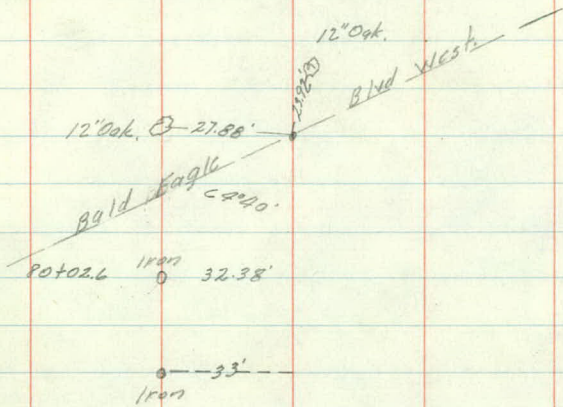
Sta.	Point	ΔL	ΔR
------	-------	------------	------------

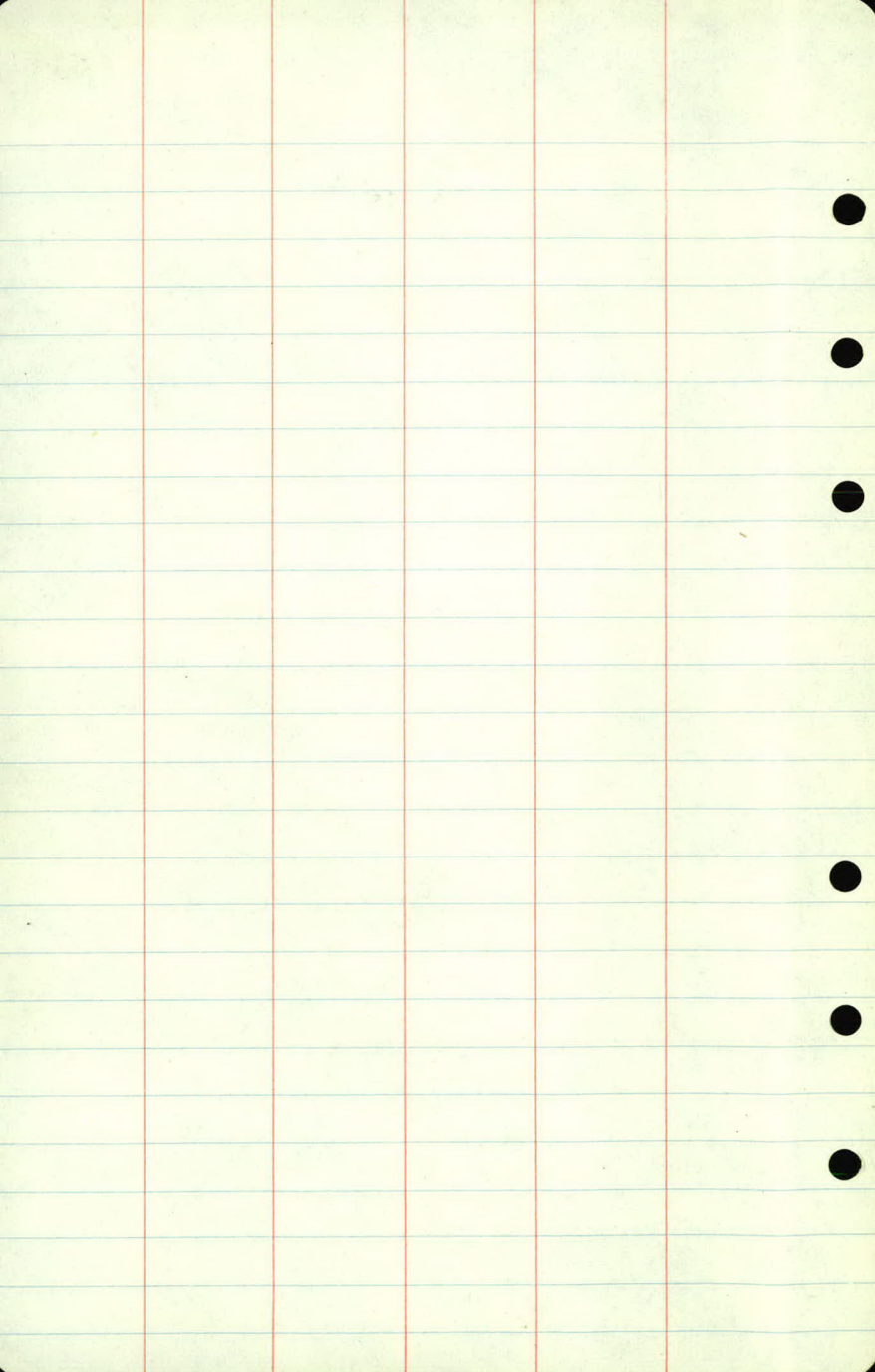
80	+56.79 = 0-08.6	Bald Eagle Blvd. W.C.	
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79	+41.34	P.O.T.	
----	--------	--------	--

65	+00	P.O.T.	
----	-----	--------	--

52	+89.60	P.I.	0°26'
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Topography

5 21' 2'

4 21' 1'

3 23' 1' +12-PR-16'

2 24' 1'

1 25' -1'

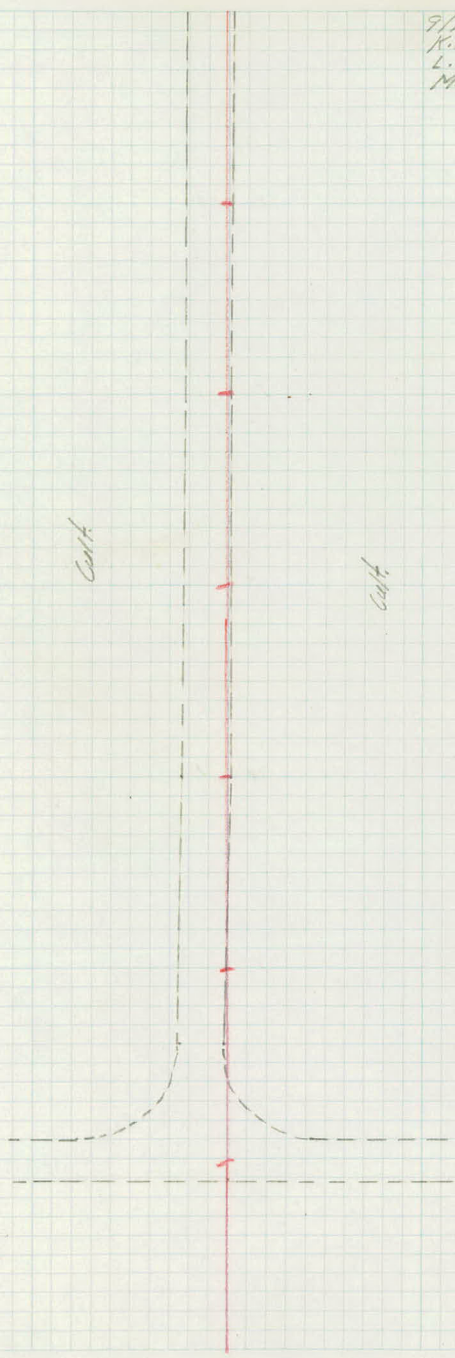
+55-End B. ad. 25' -2'

0+00 +10-Bog. Road. - 75' 44'

-11-Edge Bl. Top

9/13/39
K.H.
L.G.
M.B.

5



+48-Range Tie
+50-Ent. -37'

+78-T.P.-21'

+52-Ent.

+22-6" R Elder -46'
+06-4" R Elder -46'

12 20' 5'

+91-8" Oak -50'

+62-5" R Elder -47'

+32-F.C. Cor -44'

11 19' 5'

+81-P.P.-45'

+903-8'-7'

+02-N.W. Cor Sec. -75'

+90-Chin. 10 E/12-44' 2"
+76-10" Ash -44'

+53-19' 5' +53-T.P.-20'

+30-F.C. Cor -44'

+21-Rod -52'

+37-T.P.-27'

+30-Ent. -30'

+17-Rod -28'

10 +08-Rod -39'
+95-19'

+95-Rod Ent. -5'

+91-P.P.-18'

+31-2 12" X 44-V.H.- 29' 15'

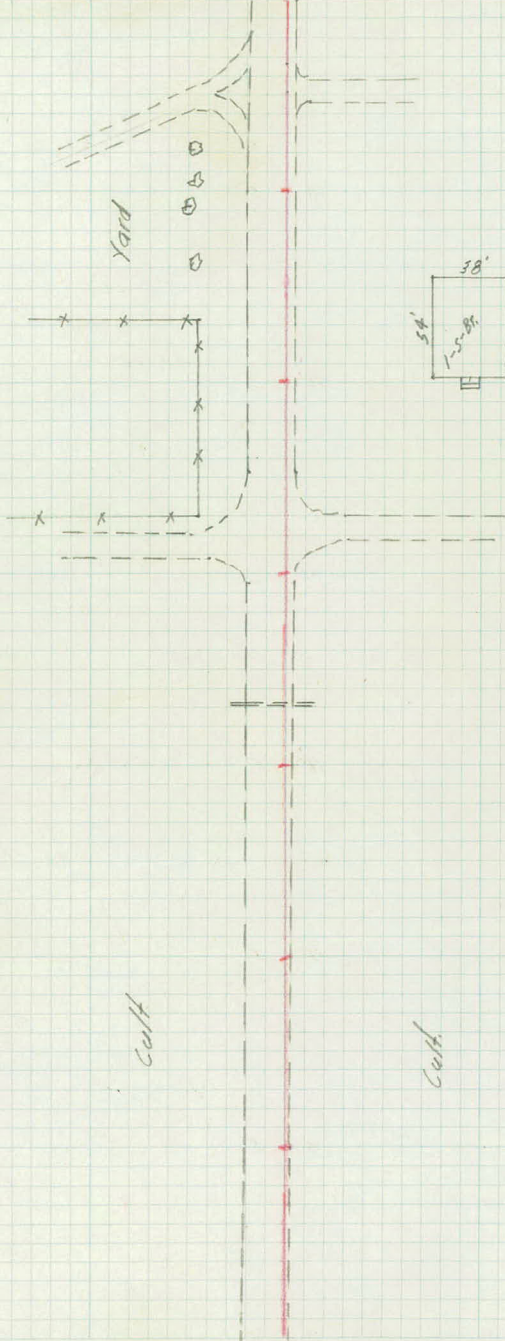
9 20' 4'

8 20' 3'

7 20' 2'

+96-P.P.-18'

6 21' 2'



19 15' 5'

152-T.P.-22'

18 16' 5'

17 17' 6'

141-T.P.-22'

16 18' 5'

15 17' 5'

134-T.P.-21'

14 18' 5'

13 16' 5'

Hay

Cult.

Cult.

Cult.

+57-Fa. Cor. -25'

26

12' 9'

25

12' 9' +07-T.P.-24'

24

13' 9'

23

14' 7'

T.P. -23'

22

14' 4'

21

14' 4'

+55-T.P.-23'

20

14' 4'

Cut - 18'

0 0 0 0



Hay

Cult.

Cult.

33 109 Ent. 16' 8' +36-PP-20'
+20-Fc Cor-21' 5' trees
+15-Bowling Green Plot-21'
+11-12'x14' C.M.-H
+05-Ent.

+95-Fc Cor-22'

32 16' 8' Fc-22'

+25-T.P-22'

31 16' 9' +95-15' Willow-18'

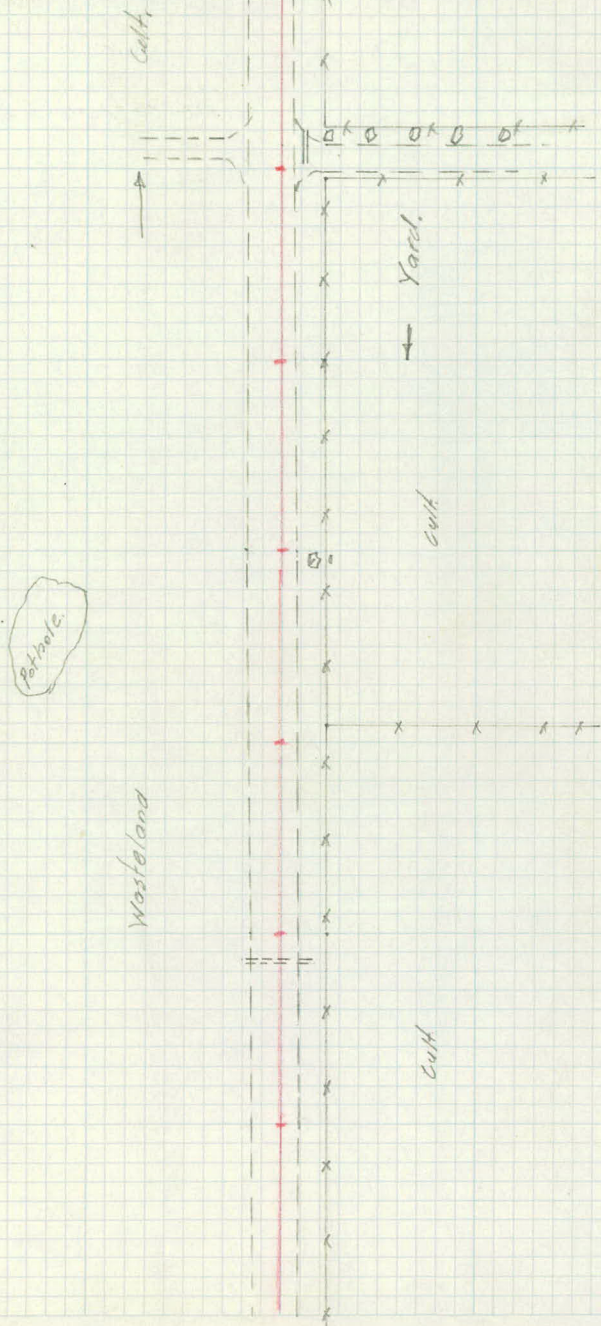
30 16' 9' +08-Fc Cor-23'

+21-T.P-23'

29 14' 9' Fc-24'
+87-L-12'x36' V/f 18' 18'

28 14' 10'

27 13' 10' +14-T.P-24'



+57-T.P. + P.P. - 17'

40 18' 5' Fc - 17'

+75-6" Tw. BE. - Fc Cor - 33'
+68-Ent.
+60-Cor Hedge - 34'

39 17' 6'

+80-Cor Hedge - 34'

+51-4-12' N36' E.M. - 25' 11' +62-T.P. + P.P. - 18'

38 16' 6' +57-Fc Cor - 19'

+56-12' Birch - 31'

37 +58-Box. Fc - 33' 16' 6' Fc - 19'

+89-T.P. + P.P. - 18'

+42-Long Tie.
+38-6" Willow - 30' Low.
+29-Ent.
+14-18" BElder - 28'
+01-3" Willow - 29'

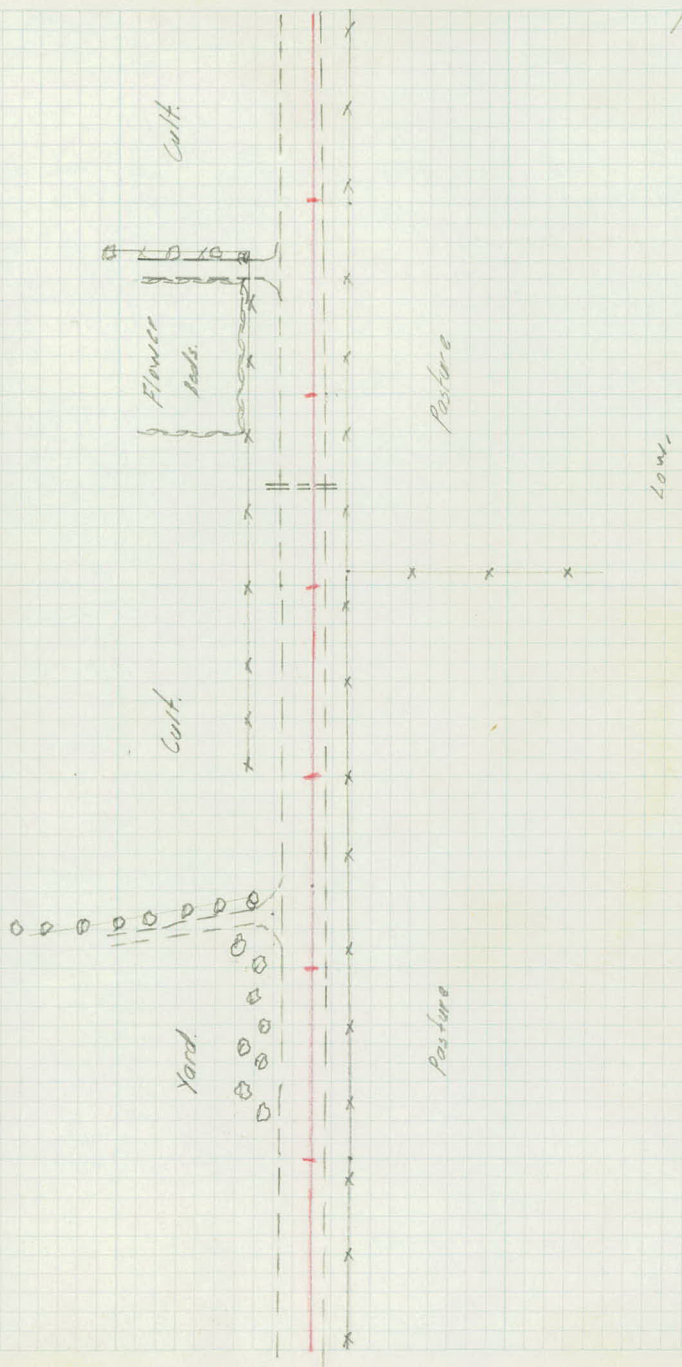
36 16' 6'

+85-6" BElder - 30'
+70-6" BElder - 25'
+59-12" BElder - 30'
+50-4" Fox Willow - 27'
+30-6" Fox Willow - 26'
+25-5" Tw Willow - 26'

+13-T.P. + P.P. - 19'

35 17' 6' Fc - 20'

34 17' 6'



Low.

+78-18" B.E. - 42'

+53-18" P.E. - 42'
+29-36" Oak - 52'
+03-18" Poplar - 40'

47

20' 2'

+88-Fc Cor. - 32'

+45-T.P. & Fc - 15'

+72-Div Fc - 18'

+35-PP-30'
+32-Div Fc - 36'

46

+18-Fc Cor. - 32'

19' 2'

+63-T.P. - 15'

45

20' 3'

+92-PP-30'
+72-Ent -
+63-End Hedge - 41'
+41-End Row Trees - 34'
+34-Mid Fc - 49'
+23-Beg. Hedge - 41'
+20 -

44

19' 4'

+97 -
+85-T.P. & P.P. - 16'
+74 -
+42 -
+31-Beg. Row's Poplars - 30'
+17-Row - 12" Poplars - 11'
+12-Ent -
+04-6 T.P. & P.P. - 30'
+02-Row Tie.
Fc Cor. - 17'

43

19' 4'

+31-Fc Cor. - 19'

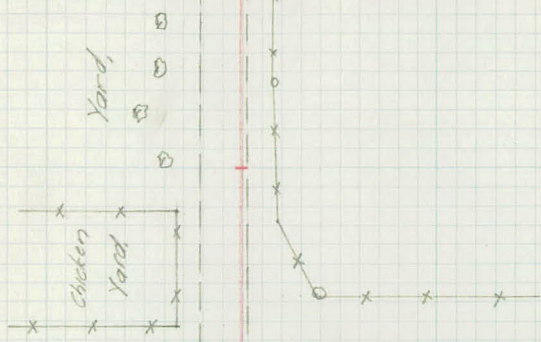
42

19' 3'

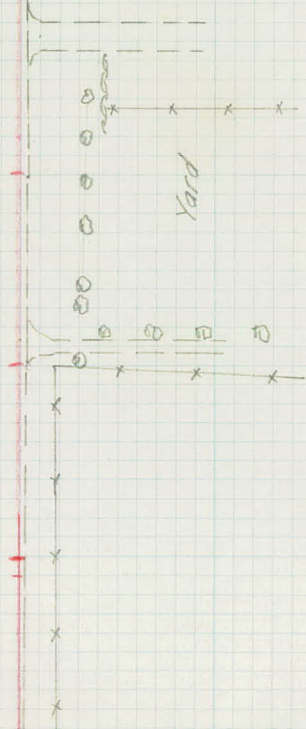
+12-T.P. & P.P. - 16'

41

18' 4'



cut.



+96-PP-27'
+92-12" B.E.-25'
+75-15" B.E.-22'

+97-12" Trip. B.E.-24'

54 +15-TP-27'

20' 1'

53

+26-Rod-23' 5' +17-PP-26'
+12-End 15" C.M.A.-17'
Rod- 50' 35'

+53-Fc. Co R-35' +51-21'-0' +74-Rod-45' +74-Rod-26'
+66-End 15" C.M.A.-17'

52

22'-0

+52-4" Pine-32'
+46-4" Pine-28'-3" Pine-35'
+37-Foss. Bushes-25-37'
+21-Foss. Bushes-25-38'
+22-15" B.E.-28'
+98-30" Willow-28'
+62-Groove-4-12" Willows-28'
+57-PP-27' +54-T.P.H. +60-4" Tw. Will.-28'
+50-12" B.E.-27' +55-12" Tw. Will.-28'
+44-15" Willow-22' +47-12" Will.-27'
+33-15" B.E.-26'-39'
+21-End. +36-4" Tw. Willow-28'
+14-20" C.E.-31-47'
+44-18" B.E.-28'

51

Fc-35'

22' 0

50

22' 0

+85-PP-8 PP-27'
+59-T.P.H. 4 PP-15'

49

Fc-32'

21'-0'

Fc-15'

+77-End.

+68-Rod 216"
+47-Fc. Co R-32'

48

+19-D 17 Fc-40'
+46-Rod R-32'

21' 2'

+11-PP-28'

+21-T.P.-6Fc.-28'

61

18' 2'

+68-PP-28'

60

19' 1'

+54-T.P.-28'

+49-20" Elm-50'

+26-18" Elm-50'

+06-15" Elm-50'

59

19' 2'

+52-12" Elm-50'

+63-18" Elm-50'

+50-Ent.

+51-Fc. Cor-15'

+79-PP-28'

58

+11-15" Elm-50'

+87-12" Elm-50'

+83-T.P.-28'

+65-8" Elm-50'

+42-16" Elm-50'

+20-18" Elm-50'

57

18' 2'

+72-8" Elm-49'

+93-PP-27'

56

+94-T.P.-27'

18' 2'

+15-10" B.E.-25'

+12-8" B.E.-25'

+95-10" B.E.-18'

+77-6" Tw. B.E.-17'

+97-8" B.E.-22' +90-8" B.E.-15'

+97-15" B.E.-24'

+34-10" B.E.-22'

+28-10" B.E.-24' 8" B.E.-30'

+23-8" B.E.-23'

+18-12" B.E.-16' -8" Tw. B.E.-23'

+11-10" B.E.-19'

+09-6" B.E.-16'

55

19' 1'



Uncult.

Uncult.

Uncult.

Uncl.

low band.

Stroms

68

17' 3'

+70-P.P.-28'

+29-T.P.-28'

67

17' 3'

+39-Ent.
 +29-Fc Cor.-12' End Hedge-31'
 +28-P.P. 28'

66

17' 2'

+95-L 10' Rd.

+48-T.P.-28'

65

17' 2'

+92-Ctr. 18" X 18" Base of Pillar - 32'

+86-Ent.-12" X 26"-C.M.A.-6'

+79-Ctr. 18" X 18" Corner Base of Pillar - 32'

+33-P.P.-28'

64

17' 2'

+97-Fc Cor. - 13' Beg. Hedge - 32'

+65-T.P.-28'

+36-Ent.

63

17' 2'

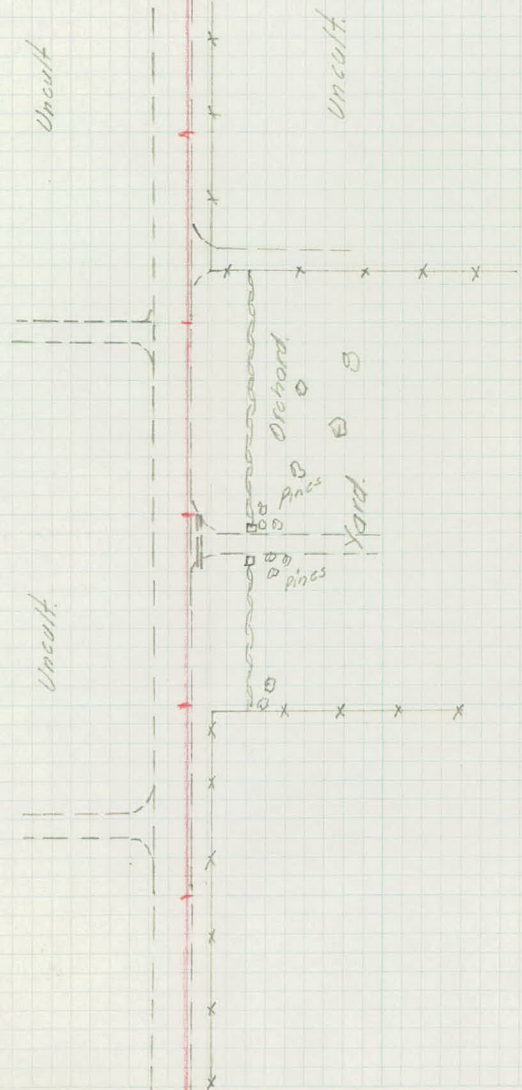
+45-T.P.-28'

+54-T.P.-28'

62

17' 2'

F.C.-18'



+90-10° B.E.-19'

+51-8° B.E.-19'

+48-T.P.-18'

+50-18° Oak-15'

+21-P.P.-29'

+02-5-18" Elm-27'

75

17' 3'

+94-End 6" T.V.C.-13'

+57-18" Willows.-28'

74

17' 3'

+65-P.P.-29'

+52-T.P.-20'

73

+04-T.P.-28'

17' 2'

72

+24-P.P.-29'

+17-4-4" Willows-16'

17' 3'

+96-Group-7-3" Willows-17'

+82-Group 8-2" Willows-15'

71

+16-T.P.-28'

18' 3'

+79-P.P.-29'

70

17' 3'

End P.C.-16'

+36-T.P.-28'

+26-P.P.-28'

69

17' 3'



Wasteland.

Wasteland.



81

+67-G.R. K&L
 +65-Edge of Rd. Top
~~76-+65-Rd.~~

26' +39-Hedge-37'

+14-End-54'
 +104-Δ in Hedge-48'
 Hedge-34

80

Hedge-30'

+90-22'

6' +75
 +68-PP-13'

+21-24" BE.-24' Reg. Hedge-18'
 +01-18" BE.-28'

79

18' 2'

+90-End 12" C.M.-25'
 +89-Reg. Hedge-35'

+77-Cor. Conc. Driv.-32'
 +64-Cor. Conc. Driv.-32'
 +48-End Culv.-29'
 +31-18" S.E.-33'

+39-PP-30'
 +38-G.P.-14'

78

18' 1'

+74-6" Pipe-23'

+57-Ent.

77

17' 2'

+17-PP-16'

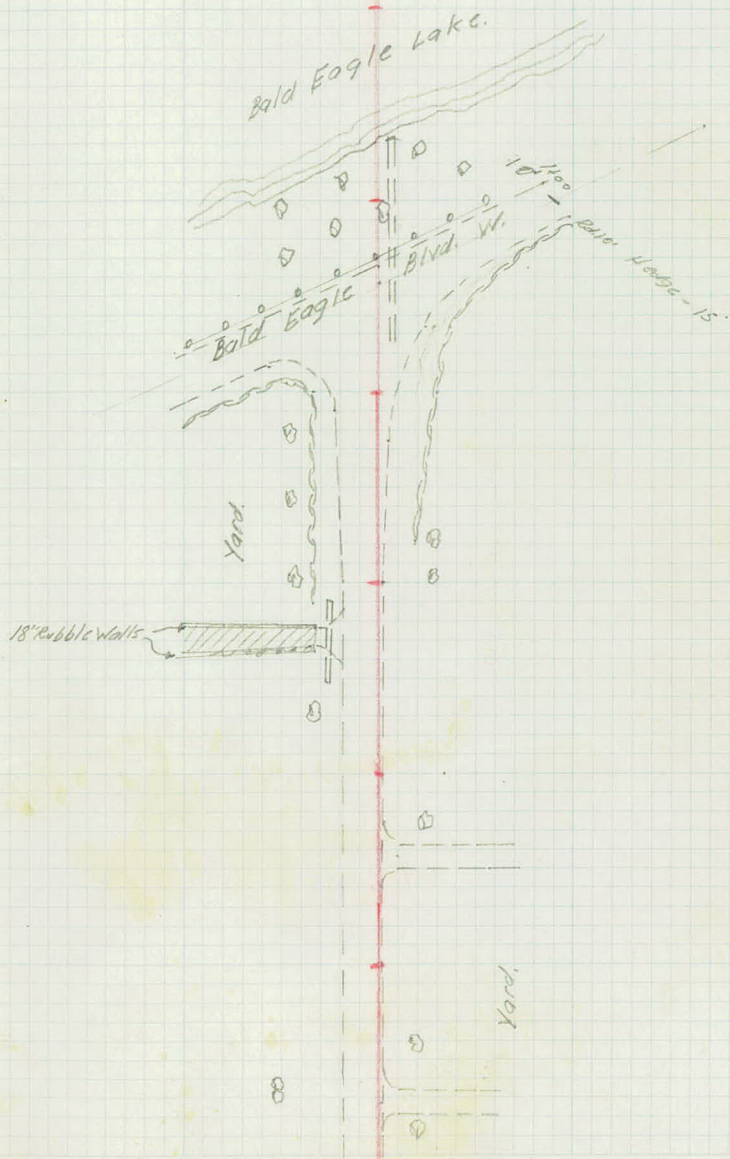
+77-PP-30'
 +60-2" E/m-17'

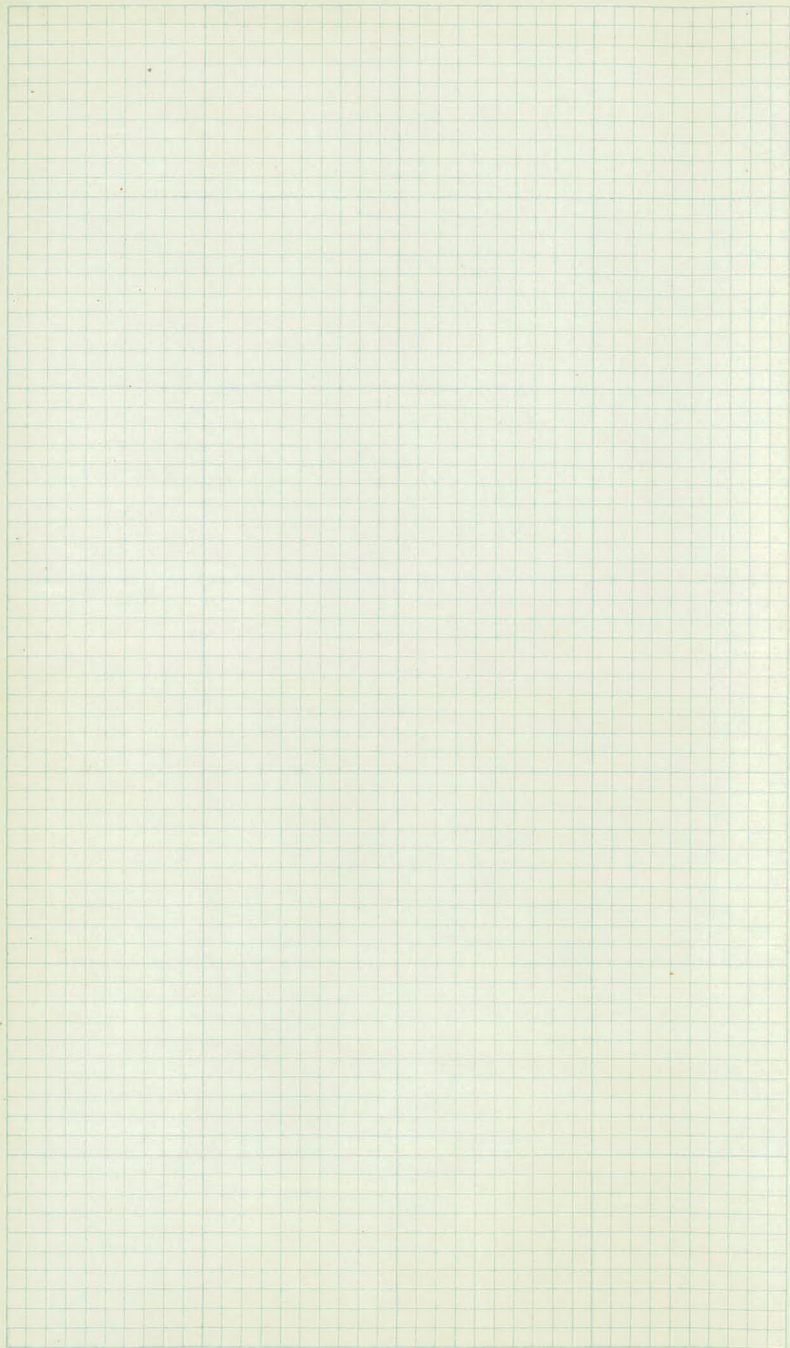
+35-18" Out-12'
 +33-18" Out-12'

+28-Ent.
 +16-4" Elm-19'

76

17' 2'





Bench Levels

Sta.	+	π	-	Elev
B.M.	11.18	940.28.		(929.10)
T.P.	8.01	943.91.	4.38	935.90.
T.P.	10.86	952.96.	1.41	942.50.
B.M.			3.53	949.83.
T.P.	2.62	947.49.	8.49	944.87.
T.P.	2.79	942.78.	7.50	939.99.
T.P.	5.32	941.58.	6.52	936.26.
B.M.			0.97	940.61.
T.P.	7.10	941.74.	6.94	934.64.
T.P.	4.22	940.94.	5.02	936.72.
B.M.			3.01	937.93.
T.P.	8.72	946.45.	3.21	937.73.
T.P.	2.39	945.48.	3.36	943.09.
B.M.			7.15	938.33.
T.P.	2.69	938.64.	9.53	935.95.
T.P.	6.16	941.53.	3.27	935.37.
B.M.			4.35	937.18.
T.P.	1.22	936.84.	5.91	935.62.
T.P.	0.63	927.16.	10.31	926.53.
T.P.	7.08	929.88.	4.36	922.80.
B.M.			2.45	927.43.

Description

Spk. in P.P. S.W. Cor. "H²" + Centerville Rd.

Top N.W. Cor Bottom step of School Ho.

Spk. in 8" Oak 80' Lt 26 + 54

Spk. in 8" Box Elder Lt 39 + 75

(P.P.)
Spk. in S.E. Cor Otter Lake Rd + Co. Rd. "H²"

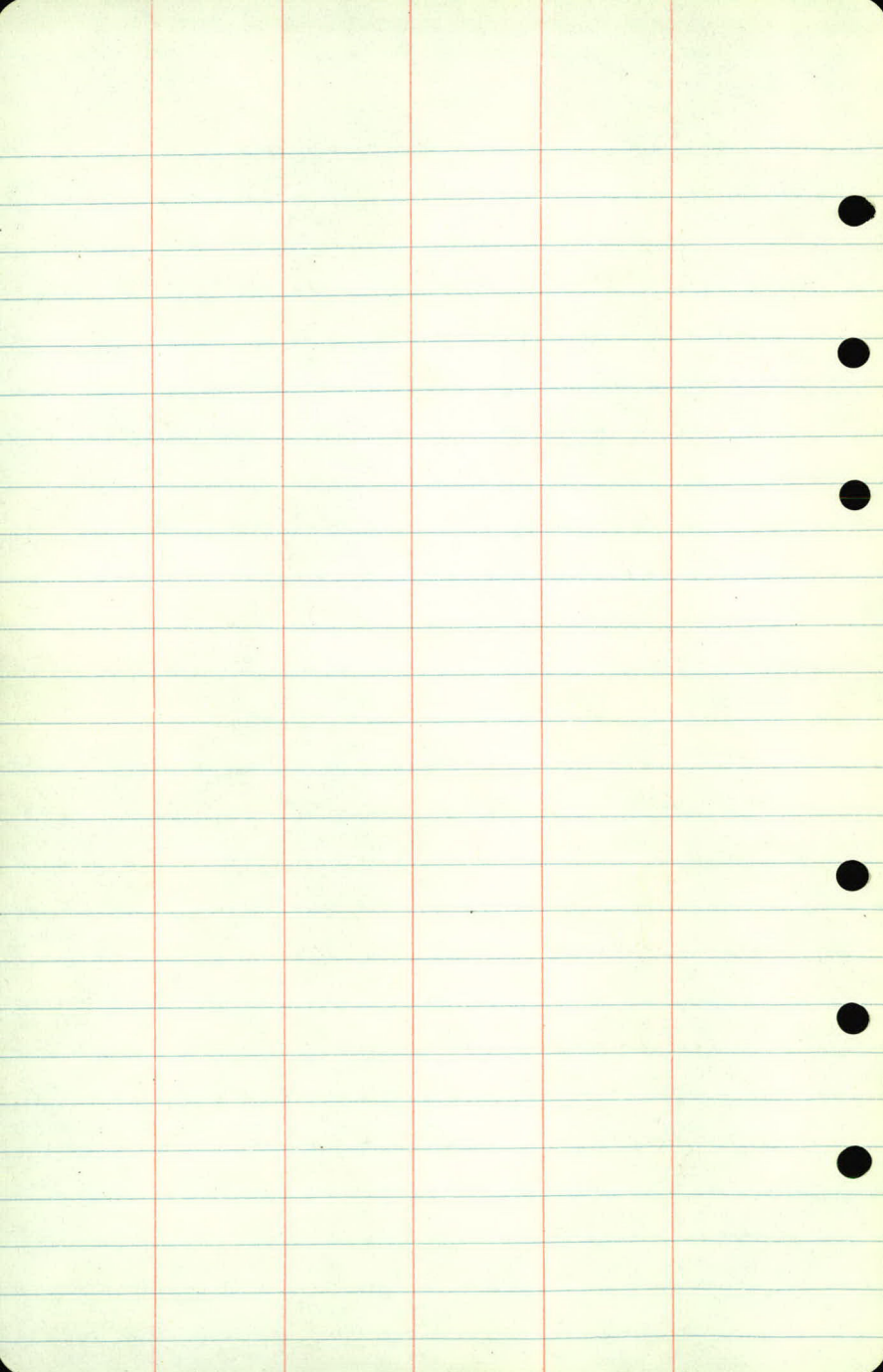
Top N.E. Cor Cong. Base of East Pillar 39' Rt. 512 64 + 91

Spk. in Light Pole East of Bald Eagle Blvd. W. + Co. Rd. "H²"

(Check Elevations with Bald Eagle Blvd. W. Survey)

These levels are 1.11' higher
than U.S.G.S. Datum.

Chk. by K.A. 3-21-95



X Sections

Sta.	+	π	-	Elev
B.M.	11.73	240.83		929.10

0	+00			29.1
---	-----	--	--	------

	+10			29.0
--	-----	--	--	------

	+14			29.1
--	-----	--	--	------

	+20			29.2
--	-----	--	--	------

	+29			29.0
--	-----	--	--	------

	+50			29.2
--	-----	--	--	------

	+70			30.4
--	-----	--	--	------

				31.1
--	--	--	--	------

	+50			32.0
--	-----	--	--	------

				33.4
--	--	--	--	------

	+50			34.4
--	-----	--	--	------

L.F.

L.

R.F.

Spk in P.P.S. W. Co. Centerville Rd & Co. Rd "H"²

$$\frac{101}{50}$$

$$\frac{117}{50} \quad \frac{134}{50}$$

$$\frac{105}{50}$$

$$\frac{118}{50}$$

$$\frac{138}{50}$$

$$\frac{108}{50}$$

$$\frac{117}{9} \quad \frac{123}{32} \quad \frac{137}{50} \quad \frac{140}{50}$$

$$\frac{110}{50} \quad \frac{108}{34} \quad \frac{109}{13} \quad \frac{116}{10} \quad \frac{127}{10} \quad \frac{134}{23} \quad \frac{138}{50}$$

$$\frac{98}{50} \quad \frac{111}{42} \quad \frac{108}{25} \quad \frac{109}{10} \quad \frac{118}{13} \quad \frac{131}{17} \quad \frac{126}{50} \quad \frac{127}{50}$$

$$\frac{79}{50} \quad \frac{108}{42} \quad \frac{111}{32} \quad \frac{105}{20} \quad \frac{105}{11} \quad \frac{116}{19} \quad \frac{115}{21} \quad \frac{106}{27} \quad \frac{103}{27} \quad \frac{104}{50}$$

$$\frac{40}{50} \quad \frac{42}{47} \quad \frac{91}{40} \quad \frac{105}{36} \quad \frac{105}{27} \quad \frac{100}{14} \quad \frac{104}{17} \quad \frac{113}{23} \quad \frac{78}{50} \quad \frac{84}{50}$$

$$\frac{37}{50} \quad \frac{39}{46} \quad \frac{91}{37} \quad \frac{99}{32} \quad \frac{98}{26} \quad \frac{92}{13} \quad \frac{97}{15} \quad \frac{103}{23} \quad \frac{35}{23} \quad \frac{37}{50}$$

$$\frac{50}{50} \quad \frac{53}{44} \quad \frac{91}{37} \quad \frac{87}{25} \quad \frac{81}{12} \quad \frac{88}{12} \quad \frac{90}{23} \quad \frac{2.0}{23} \quad \frac{0.6}{50}$$

$$\frac{39}{50} \quad \frac{42}{44} \quad \frac{76}{38} \quad \frac{77}{24} \quad \frac{69}{12} \quad \frac{74}{15} \quad \frac{18}{23} \quad \frac{14}{50}$$

$$\frac{35}{50} \quad \frac{35}{44} \quad \frac{66}{37} \quad \frac{64}{25} \quad \frac{58}{12} \quad \frac{64}{15} \quad \frac{67}{24} \quad \frac{0.9}{50} \quad \frac{0.0}{50}$$

Sta.	+	π ✓ 940.83	-	Elev.
3				35.2
	+50			35.6
4				35.8
	+50			35.7
5				35.5
	+50			35.6
6				35.6
I.P.	10.42	946.36	1.89	935.94
	+50			36.0
7				36.3
	+50			36.9
8				37.8

LH

A

RH

$$\frac{55}{50} \frac{54}{40} \frac{62}{37} \frac{57}{23} \frac{51}{11} \quad \frac{56}{14} \frac{58}{24} \frac{09}{24} \frac{21}{50}$$

$$\frac{55}{50} \frac{60}{41} \frac{53}{23} \frac{48}{10} \frac{52}{15} \frac{53}{21} \frac{30}{21} \frac{31}{50}$$

$$\frac{47}{50} \frac{49}{41} \frac{56}{36} \frac{52}{22} \frac{46}{10} \quad \frac{50}{17} \frac{55}{20} \frac{41}{20} \frac{38}{50}$$

$$\frac{51}{50} \frac{56}{37} \frac{52}{23} \frac{47}{11} \quad \frac{51}{14} \frac{56}{23} \frac{48}{23} \frac{46}{30}$$

$$\frac{72}{50} \frac{65}{28} \frac{53}{22} \frac{48}{10} \quad \frac{53}{5} \frac{53}{8} \frac{60}{13} \frac{45}{27} \frac{65}{27} \frac{60}{50}$$

$$\frac{77}{50} \frac{75}{37} \frac{68}{27} \frac{56}{23} \frac{49}{10} \quad \frac{52}{5} \frac{54}{11} \frac{80}{16} \frac{93}{16} \frac{90}{34} \frac{85}{50}$$

$$\frac{75}{50} \frac{70}{27} \frac{57}{22} \frac{49}{10} \quad \frac{52}{6} \frac{55}{15} \frac{105}{15} \frac{103}{50}$$

$$\frac{110}{50} \frac{106}{29} \frac{116}{25} \frac{110}{21} \frac{102}{9} \quad \frac{104}{7} \frac{106}{7} \frac{143}{14} \frac{141}{21} \frac{156}{50}$$

$$\frac{85}{50} \frac{73}{35} \frac{74}{31} \frac{101}{24} \frac{103}{20} \frac{99}{9} \quad \frac{101}{7} \frac{105}{7} \frac{93}{11} \frac{107}{28} \frac{122}{50}$$

$$\frac{95}{50} \frac{83}{42} \frac{72}{29} \frac{75}{24} \frac{96}{20} \frac{91}{10} \quad \frac{95}{5} \frac{97}{12} \frac{57}{19} \frac{62}{32} \frac{68}{32} \frac{77}{50}$$

$$\frac{97}{50} \frac{86}{37} \frac{77}{27} \frac{90}{24} \quad \frac{84}{9} \quad \frac{86}{7} \frac{90}{14} \frac{52}{19} \frac{52}{19} \frac{51}{50}$$

Sta	+	π	-	Elev.
		946.86		
7	+50			38.6
9				39.6
	+31			40.2
	+65			40.8
10				41.6
	+15			41.9
	+35			42.2
T.P.	10.92	953.39	3.89	949.77
	+99			42.5
11				43.3
B.M.			3.60	949.79
	+50			44.2
12				44.7

(949.79)

LH

L

RH

$$\frac{11.2}{50} \quad \frac{10.4}{40} \quad \frac{9.4}{28} \quad \frac{8.1}{23} \quad \frac{7.5}{9} \quad \frac{7.8}{6} \quad \frac{8.2}{8} \quad \frac{8.8}{12} \quad \frac{7.1}{21} \quad \frac{5.7}{50}$$

$$\frac{12.6}{50} \quad \frac{11.3}{40} \quad \frac{9.6}{29} \quad \frac{7.2}{24} \quad \frac{6.6}{9} \quad \frac{4.8}{5} \quad \frac{7.2}{9} \quad \frac{7.2}{15} \quad \frac{8.3}{32} \quad \frac{8.4}{32} \quad \frac{7.8}{50}$$

34.06
C.M.V.36.24
C.M.V.

$$\frac{14.0}{50} \quad \frac{13.7}{42} \quad \frac{12.3}{30} \quad \frac{6.4}{24} \quad \frac{6.1}{9} \quad \frac{6.2}{9} \quad \frac{6.5}{15} \quad \frac{10.1}{15} \quad \frac{7.9}{15} \quad \frac{9.1}{50}$$

$$\frac{11.4}{50} \quad \frac{9.1}{30} \quad \frac{5.8}{24} \quad \frac{5.4}{9}$$

$$\frac{5.6}{9} \quad \frac{5.8}{12} \quad \frac{7.1}{18} \quad \frac{8.5}{18} \quad \frac{8.7}{50}$$

$$\frac{6.6}{50} \quad \frac{5.7}{31} \quad \frac{4.9}{28} \quad \frac{4.7}{8} \quad \frac{4.8}{9} \quad \frac{5.3}{18} \quad \frac{6.4}{18} \quad \frac{5.6}{50}$$

$$\frac{4.7}{50} \quad \frac{4.5}{28} \quad \frac{4.5}{8} \quad \frac{4.5}{25} \quad \frac{4.5}{50} \quad \frac{4.1}{50}$$

$$\frac{3.0}{50} \quad \frac{3.5}{41} \quad \frac{4.8}{36} \quad \frac{5.0}{30} \quad \frac{4.1}{8} \quad \frac{4.2}{8} \quad \frac{4.2}{27} \quad \frac{3.9}{50}$$

$$\frac{9.0}{50} \quad \frac{9.0}{42} \quad \frac{11.7}{35} \quad \frac{11.2}{17} \quad \frac{10.9}{8} \quad \frac{10.9}{13} \quad \frac{11.4}{20} \quad \frac{10.3}{30} \quad \frac{4.9}{30} \quad \frac{4.9}{50}$$

$$\frac{5.3}{50} \quad \frac{5.3}{42} \quad \frac{10.2}{35} \quad \frac{10.4}{20} \quad \frac{9.8}{7} \quad \frac{10.1}{7} \quad \frac{10.5}{18} \quad \frac{10.2}{31} \quad \frac{5.1}{50} \quad \frac{4.6}{50} \quad \frac{4.3}{C.M.V. 500.001}$$

Top N.W. Cor. Bottom step of School Hous.

$$\frac{4.9}{50} \quad \frac{4.9}{49} \quad \frac{9.2}{32} \quad \frac{9.3}{208} \quad \frac{9.0}{8} \quad \frac{9.2}{6} \quad \frac{9.6}{18} \quad \frac{9.5}{32} \quad \frac{5.2}{50} \quad \frac{4.7}{50} \quad \frac{4.2}{77}$$

$$\frac{5.9}{50} \quad \frac{5.1}{42} \quad \frac{8.7}{35} \quad \frac{8.9}{22} \quad \frac{8.4}{7} \quad \frac{8.7}{7} \quad \frac{9.0}{6} \quad \frac{8.0}{19} \quad \frac{5.2}{32} \quad \frac{4.8}{50}$$

sta	+	π	-	E/BK
		953.39		
12	+93			44.9
13				44.7
	+50			44.2
14				43.7
T.P.	2.03	948.47	6.95	44.4
15				42.7
	+50			42.4
16				42.0
	+50			41.4
17				40.9
18				39.8
T.P.	3.44	943.11	8.80	39.6
	+50			39.3

Lt.

L

Lt.

$$\frac{5.4}{50} \frac{5.2}{42} \frac{8.3}{35} \frac{8.3}{9} \frac{8.5}{6} \frac{8.8}{19} \frac{8.9}{32} \frac{5.4}{50} \frac{5.3}{50}$$

$$\frac{6.5}{50} \frac{6.4}{36} \frac{8.0}{33} \frac{9.0}{18} \frac{8.6}{7} \frac{8.7}{6} \frac{9.0}{20} \frac{9.0}{30} \frac{6.6}{50} \frac{6.5}{50}$$

$$\frac{7.7}{50} \frac{7.5}{36} \frac{9.3}{31} \frac{9.4}{19} \frac{9.0}{7} \frac{9.2}{5} \frac{9.6}{20} \frac{9.3}{29} \frac{6.5}{29} \frac{6.9}{50}$$

$$\frac{9.1}{50} \frac{8.8}{26} \frac{9.8}{19} \quad \frac{7.5}{6} \quad \frac{9.7}{7} \frac{10.1}{9} \frac{9.6}{19} \frac{9.5}{15} \frac{7.3}{50} \frac{7.9}{50}$$

Nail in T.R. Lt. 144

$$\frac{7.0}{33} \frac{6.0}{19} \frac{5.6}{7} \frac{5.6}{8} \frac{6.1}{13} \frac{4.8}{30} \frac{4.8}{50} \frac{4.7}{50}$$

$$\frac{8.8}{50} \frac{8.2}{27} \frac{6.6}{20} \frac{6.0}{7} \frac{6.1}{7} \frac{6.3}{13} \frac{5.9}{13} \frac{6.5}{29} \frac{7.0}{50}$$

$$\frac{11.1}{50} \frac{10.0}{25} \frac{7.0}{19} \quad \frac{6.5}{7} \quad \frac{6.5}{12} \frac{6.7}{17} \frac{8.8}{32} \frac{9.0}{32} \frac{9.5}{50}$$

$$\frac{11.6}{50} \frac{11.0}{25} \frac{7.5}{19} \frac{7.0}{7} \frac{7.1}{9} \frac{7.4}{18} \frac{10.5}{34} \frac{11.3}{50} \frac{12.1}{50}$$

$$\frac{10.9}{50} \frac{10.7}{26} \frac{8.1}{19} \quad \frac{7.5}{6} \quad \frac{7.6}{10} \frac{7.9}{17} \frac{10.5}{50} \frac{12.6}{50}$$

$$\frac{10.6}{50} \frac{8.8}{23} \frac{8.9}{18} \frac{8.5}{6} \frac{8.7}{5} \frac{8.8}{10} \frac{6.7}{26} \frac{7.2}{50} \frac{7.8}{50}$$

$$\frac{5.7}{50} \frac{5.2}{27} \frac{2.8}{18} \frac{9.3}{16} \frac{3.8}{6} \frac{3.8}{5} \frac{3.8}{9} \frac{2.3}{50} \frac{2.0}{50}$$

Sta.	+	π	-	Elev.
		943.11		
19				38.8
20				38.0
	+50			37.8
21				37.6
	+50			37.4
22				37.1
	+50			36.8
23				36.6
T.P.	5.77	942.40	6.98	936.63
	+50			36.4
24				36.2
	+50			36.0

Lt

R

Lt

$$\frac{6.2}{50} \frac{6.5}{29} \frac{5.3}{25} \frac{4.5}{18} \frac{4.3}{7} \frac{4.3}{4} \frac{4.3}{8} \frac{3.0}{16} \frac{3.1}{50}$$

$$\frac{4.0}{50} \frac{6.1}{30} \frac{4.1}{24} \frac{4.7}{17} \frac{5.5}{14} \frac{5.1}{4} \frac{5.1}{9} \frac{4.2}{21} \frac{4.4}{50}$$

$$\frac{5.9}{50} \frac{5.7}{30} \frac{4.4}{24} \frac{4.6}{16} \frac{5.5}{14} \frac{5.3}{4} \frac{5.4}{8} \frac{4.7}{24} \frac{4.9}{50}$$

$$\frac{3.9}{50} \frac{4.1}{29} \frac{3.5}{23} \frac{4.7}{17} \frac{5.7}{14} \frac{5.5}{4} \frac{5.6}{9} \frac{4.7}{23} \frac{6.5}{50}$$

$$\frac{2.3}{50} \frac{3.2}{29} \frac{2.7}{23} \frac{6.0}{14} \frac{5.7}{4} \frac{5.8}{9} \frac{4.8}{23} \frac{6.2}{50}$$

$$\frac{2.0}{50} \frac{2.7}{24} \frac{6.3}{14}$$

$$\frac{6.0}{4} \frac{6.1}{11} \frac{4.3}{25} \frac{4.2}{50}$$

$$\frac{2.2}{50} \frac{2.7}{24} \frac{6.5}{14} \frac{6.3}{5} \frac{6.3}{11} \frac{4.6}{28} \frac{4.9}{50}$$

$$\frac{4.2}{50} \frac{4.1}{24} \frac{6.7}{14}$$

$$\frac{6.5}{7} \frac{6.6}{12} \frac{5.5}{26} \frac{5.8}{50}$$

$$\frac{6.3}{50} \frac{6.3}{27} \frac{5.7}{22} \frac{5.7}{15} \frac{6.2}{13} \frac{6.0}{8} \frac{6.3}{15} \frac{6.7}{21} \frac{7.8}{50}$$

$$\frac{7.8}{50} \frac{8.0}{29} \frac{6.3}{16}$$

$$\frac{6.2}{14} \frac{6.7}{18} \frac{8.2}{50}$$

$$\frac{7.1}{50} \frac{7.5}{25} \frac{6.7}{16} \frac{6.4}{12} \frac{7.1}{18} \frac{9.2}{50}$$

Sta.	+	π	-	Elev.
		942.40		
25				35.8
	+50			35.5
26				35.3
	+58			35.0
B.M.	1.83	942.44	1.83	940.57 (940.61)
27				34.8
	+50			34.4
I.P.	5.88	940.25	8.27	934.17
28				34.2
	+50			34.0
29				33.8
30				34.6
31				35.1

Lt

A

Rt.

$$\frac{39}{50} \frac{54}{22} \frac{44}{13} \quad \frac{70}{12} \quad \frac{66}{14} \frac{70}{14} \frac{80}{19} \frac{95}{50}$$

$$\frac{21}{50} \frac{30}{36} \frac{47}{22} \frac{71}{13} \quad \frac{69}{10} \frac{71}{14} \frac{65}{26} \frac{48}{50}$$

$$\frac{29}{50} \frac{34}{35} \frac{45}{22} \quad \frac{74}{12} \quad \frac{71}{9} \frac{74}{16} \frac{65}{36} \frac{74}{50}$$

$$\frac{50}{50} \frac{59}{23} \frac{77}{13} \quad \frac{74}{12} \frac{77}{18} \frac{70}{32} \frac{79}{50}$$

$$\frac{62}{50} \frac{66}{36} \frac{69}{24} \frac{80}{18} \frac{81}{14} \quad \frac{76}{11} \frac{80}{15} \frac{75}{20} \frac{81}{27} \frac{102}{50} \frac{112}{50}$$

$$\frac{64}{50} \frac{70}{38} \frac{79}{25} \frac{87}{18} \quad \frac{80}{16} \frac{84}{22} \frac{108}{28} \frac{121}{50} \frac{135}{50}$$

$$\frac{48}{50} \frac{52}{40} \frac{65}{23} \frac{69}{14} \quad \frac{59}{10} \frac{64}{16} \frac{69}{23} \frac{103}{28} \frac{129}{50} \frac{139}{50}$$

$$\frac{57}{50} \frac{73}{25} \frac{74}{18} \quad \frac{64}{15} \quad \frac{61}{17} \quad \frac{68}{23} \frac{107}{26} \frac{129}{50} \frac{150}{50}$$

$$\frac{66}{50} \frac{74}{28} \frac{68}{16} \quad \frac{63}{16} \frac{66}{23} \frac{100}{26} \frac{111}{50} \frac{124}{50}$$

$$\frac{69}{50} \frac{62}{38} \quad \frac{60}{19} \quad \frac{55}{9} \frac{59}{16} \frac{56}{21} \frac{80}{30} \frac{88}{50} \frac{99}{50}$$

$$\frac{68}{50} \quad \frac{52}{21} \frac{53}{17} \quad \frac{50}{8} \frac{53}{14} \frac{59}{17} \frac{41}{32} \frac{51}{50} \frac{64}{50}$$

Sta	+	π	-	Elev
		940.05		
31	+50			35.5
32				36.0
	+50			36.3
33				36.6
34				36.9
T.P.	4.70	941.55	3.20	936.85
35				36.7
	+50			36.8
36				36.6
	+50			36.5
37				36.4
38				36.0

6.

6.

6.

$$\frac{37}{50} \frac{31}{34} \frac{32}{25} \frac{49}{19} \frac{46}{12} \frac{52}{15} \frac{32}{22} \frac{31}{28} \frac{33}{28} \frac{49}{50}$$

$$\frac{19}{50} \frac{14}{34} \frac{19}{25} \frac{43}{19} \frac{40}{6} \frac{41}{11} \frac{47}{14} \frac{31}{21} \frac{24}{28} \frac{26}{50}$$

$$\frac{08}{50} \frac{11}{24} \frac{40}{17} \frac{36}{5} \frac{38}{11} \frac{44}{13} \frac{32}{33} \frac{35}{33} \frac{41}{50}$$

$$\frac{10}{50} \frac{12}{23} \frac{40}{17} \frac{35}{5} \frac{35}{9} \frac{38}{24} \frac{39}{24} \frac{34}{50}$$

$$\frac{17}{50} \frac{17}{23} \frac{33}{20} \frac{30}{5} \frac{32}{10} \frac{38}{14} \frac{19}{38} \frac{25}{38} \frac{24}{50}$$

$$\frac{26}{50} \frac{23}{25} \frac{51}{17} \frac{47}{6} \frac{49}{8} \frac{52}{14} \frac{21}{32} \frac{23}{32} \frac{31}{50}$$

$$\frac{27}{50} \frac{24}{24} \frac{52}{17} \frac{47}{6} \frac{48}{8} \frac{53}{15} \frac{20}{33} \frac{29}{33} \frac{41}{50}$$

$$\frac{37}{50} \frac{37}{29} \frac{51}{17} \frac{48}{6} \frac{50}{8} \frac{56}{19} \frac{38}{35} \frac{50}{35} \frac{57}{50}$$

$$\frac{55}{50} \frac{54}{30} \frac{52}{17} \frac{49}{7} \frac{51}{6} \frac{56}{14} \frac{55}{35} \frac{10}{35} \frac{18}{50}$$

$$\frac{56}{50} \frac{57}{31} \frac{51}{18} \frac{50}{7} \frac{42}{6} \frac{56}{10} \frac{51}{20} \frac{53}{20} \frac{63}{34} \frac{74}{50}$$

$$\frac{58}{50} \frac{60}{22} \frac{57}{17} \frac{54}{6} \frac{56}{7} \frac{60}{11} \frac{55}{26} \frac{57}{26} \frac{60}{50}$$

Sta.	+	π	-	Elev.
		941.55		
39				35.8
T.P.	7.73	949.93	5.85	936.20
40				36.1
B.M.	5.97	943.90	5.97	937.96 (937.93)
+50				36.6
41				36.9
42				37.4
43				38.5
+50				39.1
44				39.8
+50				40.4
45				41.0
T.P.	10.80	952.09	2.61	941.29
+50				41.6

L.L.

L.

R.L.

$$L.O. \quad \frac{54}{31} \quad \frac{40}{29} \quad \frac{55}{23} \quad \frac{57}{18} \quad \frac{56}{8} \quad \frac{58}{7} \quad \frac{60}{7} \quad \frac{65}{19} \quad \frac{45}{23} \quad \frac{71}{50}$$

$$\frac{81}{50} \quad \frac{78}{35} \quad \frac{72}{27} \quad \frac{78}{18} \quad \frac{75}{7} \quad \frac{78}{7} \quad \frac{83}{7} \quad \frac{68}{11} \quad \frac{62}{18} \quad \frac{80}{50}$$

Spk. in 8' B. Elder. L. 39475

$$\frac{77}{50} \quad \frac{78}{35} \quad \frac{70}{27} \quad \frac{75}{19} \quad \frac{71}{8} \quad \frac{73}{8} \quad \frac{75}{14} \quad \frac{66}{50} \quad \frac{67}{50} \quad \frac{83}{50}$$

$$\frac{81}{50} \quad \frac{78}{35} \quad \frac{72}{28} \quad \frac{71}{20} \quad \frac{68}{7} \quad \frac{70}{5} \quad \frac{79}{19} \quad \frac{75}{19} \quad \frac{84}{24} \quad \frac{91}{50}$$

$$\frac{87}{50} \quad \frac{85}{36} \quad \frac{80}{30} \quad \frac{87}{26} \quad \frac{69}{22} \quad \frac{62}{9} \quad \frac{65}{5} \quad \frac{68}{11} \quad \frac{67}{15} \quad \frac{84}{27} \quad \frac{95}{50} \quad \frac{107}{50}$$

$$\frac{81}{50} \quad \frac{78}{36} \quad \frac{72}{28} \quad \frac{56}{23} \quad \frac{50}{8} \quad \frac{59}{7} \quad \frac{59}{11} \quad \frac{79}{15} \quad \frac{81}{24} \quad \frac{92}{50}$$

$$\frac{73}{50} \quad \frac{68}{36} \quad \frac{60}{27} \quad \frac{49}{21} \quad \frac{45}{10} \quad \frac{48}{5} \quad \frac{51}{10} \quad \frac{58}{32} \quad \frac{68}{40} \quad \frac{74}{40} \quad \frac{82}{50}$$

$$\frac{62}{50} \quad \frac{56}{36} \quad \frac{49}{28} \quad \frac{42}{21} \quad \frac{38}{9} \quad \frac{41}{11} \quad \frac{45}{21} \quad \frac{58}{35} \quad \frac{63}{35} \quad \frac{73}{50}$$

$$\frac{42}{50} \quad \frac{38}{39} \quad \frac{30}{33} \quad \frac{28}{23} \quad \frac{36}{20} \quad \frac{32}{9} \quad \frac{35}{18} \quad \frac{38}{40} \quad \frac{54}{40} \quad \frac{58}{50}$$

$$\frac{09}{50} \quad \frac{01}{36} \quad \frac{101}{28} \quad \frac{30}{21} \quad \frac{27}{9} \quad \frac{27}{4} \quad \frac{30}{6} \quad \frac{24}{15} \quad \frac{24}{15} \quad \frac{18}{26} \quad \frac{34}{50}$$

$$\frac{75}{50} \quad \frac{60}{50} \quad \frac{63}{29} \quad \frac{103}{21} \quad \frac{101}{9} \quad \frac{105}{4} \quad \frac{107}{14} \quad \frac{82}{26} \quad \frac{75}{26} \quad \frac{78}{50}$$

Sta.	+	π .	-	Elev
		952.09.		
46				42.3.
	+40			42.6.
✓	+72			42.8.
47				43.1.
	+50			42.9.
48				42.7.
	+50			42.1.
49				41.9.
50				41.2.
T.P.	3.16	944.70.	10.55	941.54.
51				40.4.
	H20			39.6.

Lt

L

Rt

$$\frac{80}{50} \frac{69}{38} \frac{62}{28} \quad \frac{95}{20} \frac{94}{9} \quad \frac{98}{3} \frac{99}{8} \frac{84}{13} \frac{59}{24} \frac{54}{24}$$

$$\frac{79}{50} \frac{69}{28} \frac{92}{21} \frac{91}{8} \quad \frac{95}{2} \frac{95}{8} \frac{78}{16} \frac{33}{27} \frac{36}{50} \frac{35}{50}$$

$$\frac{76}{50} \frac{68}{28} \frac{90}{21} \frac{89}{9} \quad \frac{93}{2} \frac{93}{8} \quad \frac{77}{8} \frac{39}{14} \frac{48}{27} \frac{48}{50}$$

$$\frac{66}{50} \frac{74}{31} \frac{88}{20} \frac{87}{10} \quad \frac{90}{2} \frac{90}{8} \frac{80}{13} \frac{49}{23} \frac{52}{50} \frac{55}{50}$$

$$\frac{47}{50} \frac{56}{30} \frac{88}{21} \frac{87}{9} \quad \frac{92}{7} \frac{90}{13} \frac{62}{25} \frac{67}{50} \frac{73}{50}$$

$$\frac{62}{50} \frac{67}{32} \frac{75}{28} \quad \frac{92}{23} \frac{90}{10} \quad \frac{94}{7} \frac{96}{11} \frac{73}{26} \frac{80}{50} \frac{91}{50}$$

$$\frac{95}{50} \frac{93}{31} \frac{92}{26} \quad \frac{95}{22} \frac{95}{10} \quad \frac{100}{2} \frac{101}{9} \frac{95}{15} \frac{98}{26} \frac{101}{50} \frac{107}{50}$$

$$\frac{103}{50} \frac{105}{32} \frac{95}{23} \quad \frac{100}{21} \quad \frac{95}{10} \quad \frac{102}{5} \frac{105}{18} \frac{111}{37} \frac{111}{60} \frac{114}{60}$$

$$\frac{108}{50} \frac{104}{34} \frac{111}{31} \quad \frac{110}{22} \frac{105}{11} \frac{109}{11} \quad \frac{110}{3} \frac{108}{14} \frac{107}{29} \frac{112}{50}$$

$$\frac{25}{50} \frac{25}{33} \frac{51}{30} \quad \frac{46}{22} \frac{40}{9} \quad \frac{43}{10} \frac{45}{14} \frac{28}{28} \frac{32}{50} \frac{37}{50}$$

$$\frac{26}{50} \frac{24}{33} \frac{45}{29} \quad \frac{53}{22} \frac{49}{10} \quad \frac{51}{4} \frac{53}{10} \frac{45}{14} \frac{24}{33} \frac{22}{50} \frac{18}{50}$$

Sta.	+	Σ	-	Elev.
		944.70		
52				39.0.
	+56			38.3.
B.M.	2.38	940.71.	6.37	938.33. (938.33.)
	+62			38.4.
	+66			38.5.
	+72			38.6.
	+86			38.5.
53	+08			37.7.
	+13			37.4.
	+16			37.3.
	+21			37.0.
	+71			36.2.

Lt

L

Rt

$$\frac{31}{50} \quad \frac{29}{34} \quad \frac{70}{29} \quad \frac{70}{27} \quad \frac{60}{23} \quad \frac{56}{10} \quad \frac{57}{4} \quad \frac{59}{8} \quad \frac{51}{13} \quad \frac{29}{33} \quad \frac{13}{50}$$

$$\frac{58}{50} \quad \frac{55}{35} \quad \frac{91}{30} \quad \frac{91}{27} \quad \frac{68}{23} \quad \frac{61}{10} \quad \frac{64}{8} \quad \frac{65}{16} \quad \frac{15}{32} \quad \frac{14}{50}$$

Spk. in P.R.S.E. GOR Other lot c Rd. & Co. Rd. "12"

$$\frac{57}{50} \quad \frac{53}{31} \quad \frac{32}{27} \quad \frac{21}{10} \quad \frac{23}{6} \quad \frac{26}{9} \quad \frac{32}{25} \quad \frac{26}{50}$$

$$\frac{60}{50} \quad \frac{57}{38} \quad \frac{35}{33} \quad \frac{22}{13} \quad \frac{22}{10} \quad \frac{25}{17} \quad \text{Calc.} \quad \frac{395}{17} \quad \frac{3.0}{50}$$

$$\frac{38}{50} \quad \frac{35}{37} \quad \frac{23}{13} \quad \frac{21}{20} \quad \frac{20}{50}$$

$$\frac{3.4}{50} \quad \frac{2.2}{24} \quad \frac{1.5}{50}$$

$$\frac{3.7}{50} \quad \frac{40}{36} \quad \frac{31}{12} \quad \frac{30}{14} \quad \frac{29}{19} \quad \frac{2.5}{50}$$

$$\frac{58}{50} \quad \frac{54}{31} \quad \frac{44}{28} \quad \frac{33}{19} \quad \frac{33}{10} \quad \frac{35}{17} \quad \text{Calc.} \quad \frac{420}{17} \quad \frac{3.1}{50}$$

$$\frac{4.5}{50} \quad \frac{57}{31} \quad \frac{42}{28} \quad \frac{34}{11} \quad \frac{34}{7} \quad \frac{3.7}{11} \quad \frac{4.2}{50}$$

$$\frac{57}{50} \quad \frac{45}{37} \quad \frac{41}{25} \quad \frac{36}{14} \quad \frac{37}{11} \quad \frac{4.0}{11} \quad \frac{3.3}{14} \quad \frac{0.7}{50}$$

$$\frac{99}{50} \quad \frac{88}{36} \quad \frac{49}{23} \quad \frac{44}{8} \quad \frac{45}{10} \quad \frac{50}{12} \quad \frac{4.2}{22} \quad \frac{2.9}{50}$$

Sta.	+	π	-	E/cv
		940.71		
54				35.7.
	+50			34.7.
55				33.9.
	+50			33.2.
56				32.8.
T.P.	635	937.29.	777	932.94.
	+50			32.9.
57				33.2.
	+37			33.4.
	+62			33.5.
58				33.7.
	+50			34.1.

Lt.

k

Lt.

$$\frac{12.5}{50} \frac{91}{38} \frac{75}{29} \frac{63}{26} \frac{54}{19} \frac{49}{9} \frac{50}{13} \frac{60}{32} \frac{50}{50} \frac{38}{50}$$

$$\frac{13.5}{50} \frac{67}{29} \frac{62}{19} \frac{58}{9} \frac{60}{9} \frac{65}{15} \frac{87}{50} \frac{76}{50} \frac{120}{41}$$

$$\frac{14.3}{50} \frac{127}{39} \frac{76}{28} \frac{70}{19} \frac{66}{9} \frac{68}{9} \frac{71}{15} \frac{106}{31} \frac{108}{50} \frac{101}{50}$$

$$\frac{14.4}{50} \frac{132}{39} \frac{80}{26} \frac{77}{18} \frac{73}{8} \frac{75}{9} \frac{83}{16} \frac{109}{29} \frac{114}{50} \frac{110}{50}$$

$$\frac{12.9}{50} \frac{125}{41} \frac{80}{29} \frac{80}{18} \frac{76}{9} \frac{79}{9} \frac{83}{15} \frac{110}{33} \frac{112}{50} \frac{109}{50}$$

$$\frac{97}{30} \frac{97}{41} \frac{83}{37} \frac{68}{32} \frac{65}{18} \frac{62}{7} \frac{64}{8} \frac{68}{8} \frac{96}{16} \frac{103}{27} \frac{105}{50}$$

$$\frac{6.9}{50} \frac{74}{33} \frac{59}{30} \frac{62}{19} \frac{5.8}{9} \frac{6.1}{7} \frac{6.3}{13} \frac{76}{21} \frac{102}{50} \frac{106}{50}$$

$$\frac{50}{50} \frac{55}{47} \frac{59}{36} \frac{70}{28} \frac{61}{23} \frac{57}{8} \frac{59}{8} \frac{6.3}{8} \frac{90}{15} \frac{99}{29} \frac{104}{50}$$

$$\frac{4.3}{50} \frac{5.0}{45} \frac{6.4}{27} \frac{6.9}{25} \frac{5.9}{18} \frac{5.5}{8} \frac{5.8}{8} \frac{6.1}{8} \frac{7.3}{13} \frac{77}{33} \frac{81}{50}$$

$$\frac{3.1}{50} \frac{5.0}{40} \frac{5.9}{28} \frac{6.9}{24} \frac{5.7}{19} \frac{5.3}{8} \frac{5.6}{8} \frac{6.0}{6} \frac{50}{15} \frac{52.6}{25} \frac{66}{50}$$

$$\frac{2.0}{50} \frac{5.2}{37} \frac{5.6}{27} \frac{6.3}{26} \frac{5.2}{18} \frac{5.0}{9} \frac{5.2}{6} \frac{5.4}{10} \frac{40}{19} \frac{3.9}{50} \frac{4.5}{50}$$

Sta.	+	π .	-	Elck
		939.29		
59				34.3
60				35.0
T.P.	7.00	942.37	3.92	935.37
+50				35.4
61				35.6
+50				36.0
62				36.2
+50				36.4
63				36.4
+50				36.4
64				36.6
+38				36.5

Lt.

K.

Lt.

$$\frac{31}{50} \frac{36}{45} \frac{50}{27} \frac{58}{29} \frac{50}{19} \frac{47}{9} \frac{50}{5} \frac{51}{8} \frac{36}{27} \frac{44}{50} \frac{46}{50}$$

$$\frac{21}{50} \frac{25}{40} \frac{20}{27} \frac{46}{24} \frac{44}{19} \frac{40}{9} \frac{43}{5} \frac{47}{5} \frac{36}{8} \frac{45}{20} \frac{52}{50}$$

$$\frac{50}{50} \frac{53}{28} \frac{73}{20} \frac{68}{9} \frac{70}{5} \frac{72}{10} \frac{61}{20} \frac{71}{20} \frac{76}{50}$$

$$\frac{52}{50} \frac{56}{28} \frac{68}{22} \frac{70}{17} \frac{66}{8} \frac{68}{7} \frac{71}{10} \frac{56}{31} \frac{71}{50}$$

$$\frac{47}{50} \frac{52}{26} \frac{69}{22} \frac{62}{9} \frac{64}{5} \frac{71}{6} \frac{60}{9} \frac{69}{14} \frac{76}{22} \frac{85}{50}$$

$$\frac{33}{50} \frac{41}{28} \frac{60}{22} \frac{63}{18} \frac{59}{8} \frac{62}{5} \frac{68}{6} \frac{60}{8} \frac{68}{13} \frac{71}{21} \frac{85}{50}$$

$$\frac{32}{50} \frac{36}{23} \frac{59}{21} \frac{60}{17} \frac{58}{8} \frac{60}{5} \frac{62}{6} \frac{43}{11} \frac{55}{26} \frac{63}{50}$$

$$\frac{41}{50} \frac{39}{28} \frac{59}{20} \frac{61}{16} \frac{58}{7} \frac{60}{6} \frac{61}{10} \frac{43}{50} \frac{45}{50}$$

$$\frac{47}{50} \frac{47}{27} \frac{67}{21} \frac{59}{17} \frac{57}{8} \frac{60}{5} \frac{63}{5} \frac{48}{12} \frac{55}{17} \frac{50}{50}$$

$$\frac{41}{50} \frac{50}{27} \frac{60}{23} \frac{60}{16} \frac{59}{7} \frac{58}{6} \frac{62}{10} \frac{60}{29} \frac{73}{50} \frac{80}{50}$$

$$\frac{27}{50} \frac{44}{27} \frac{61}{21} \frac{60}{16} \frac{58}{7} \frac{59}{11} \frac{63}{28} \frac{72}{50} \frac{80}{50}$$

Sta.	+	π	-	Eick
		942.37		
64	+75			36.5
B.M.			521	937.16 (937.18)
65				36.3
	+35			36.9
66				35.4
	+50			34.9
T.P.	373	938.22	7.88	934.49
67				34.5
68				33.2
	+50			32.5
69				31.7
	+40			31.1
70				30.1

Lt

4

Rt.

$$\frac{39}{50} \quad \frac{45}{28} \quad \frac{64}{20} \quad \frac{61}{16} \quad \frac{58}{7} \quad \frac{59}{-} \quad \frac{61}{5} \quad \frac{52}{11} \quad \frac{57}{28} \quad \frac{63}{50}$$

Top N.E. Cor. of Conc. Base at East Pillar 39.46.64.91

$$\frac{42}{50} \quad \frac{47}{27} \quad \frac{65}{19} \quad \frac{63}{17} \quad \frac{60}{7} \quad \frac{61}{-} \quad \frac{62}{6} \quad \frac{50}{10} \quad \frac{52}{28} \quad \frac{64}{50}$$

$$\frac{44}{50} \quad \frac{50}{27} \quad \frac{64}{22} \quad \frac{65}{16} \quad \frac{63}{9} \quad \frac{65}{-} \quad \frac{67}{6} \quad \frac{53}{11} \quad \frac{56}{28} \quad \text{L.O.}$$

$$\frac{60}{50} \quad \frac{65}{27} \quad \frac{70}{20} \quad \frac{68}{8} \quad \frac{70}{-} \quad \frac{75}{8} \quad \frac{75}{28} \quad \frac{73}{50}$$

$$\frac{75}{50} \quad \frac{69}{26} \quad \frac{81}{23} \quad \frac{75}{19} \quad \frac{73}{9} \quad \frac{75}{-} \quad \frac{79}{6} \quad \frac{65}{11} \quad \frac{83}{29} \quad \frac{81}{50}$$

$$\frac{25}{50} \quad \frac{29}{40} \quad \frac{31}{26} \quad \frac{42}{23} \quad \frac{38}{17} \quad \frac{35}{8} \quad \frac{37}{-} \quad \frac{42}{7} \quad \frac{28}{11} \quad \frac{32}{15} \quad \frac{32}{33} \quad \frac{38}{50}$$

$$\frac{30}{50} \quad \frac{27}{34} \quad \frac{30}{26} \quad \frac{54}{52} \quad \frac{52}{16} \quad \frac{50}{7} \quad \frac{50}{-} \quad \frac{55}{8} \quad \frac{18}{13} \quad \frac{15}{27} \quad \frac{23}{39} \quad \frac{28}{50}$$

$$\frac{36}{50} \quad \frac{36}{28} \quad \frac{62}{23} \quad \frac{59}{16} \quad \frac{57}{7} \quad \frac{57}{-} \quad \frac{64}{9} \quad \frac{35}{14} \quad \frac{39}{27} \quad \frac{47}{50}$$

$$\frac{44}{50} \quad \frac{46}{27} \quad \frac{70}{23} \quad \frac{67}{17} \quad \frac{64}{7} \quad \frac{66}{-} \quad \frac{69}{9} \quad \frac{57}{13} \quad \frac{46}{23} \quad \frac{74}{50}$$

$$\frac{55}{50} \quad \frac{58}{29} \quad \frac{77}{24} \quad \frac{72}{17} \quad \frac{70}{7} \quad \frac{71}{-} \quad \frac{78}{10} \quad \frac{71}{15} \quad \frac{75}{26} \quad \frac{74}{50}$$

$$\frac{64}{50} \quad \frac{68}{30} \quad \frac{86}{23} \quad \frac{83}{17} \quad \frac{79}{8} \quad \frac{81}{-} \quad \frac{85}{10} \quad \frac{72}{17} \quad \frac{71}{26} \quad \frac{80}{38} \quad \frac{89}{50}$$

Sta.	+	π	-	Elev.
		938.22		
70	+50			29.2
71				28.3
72				26.5
	+60			25.6
T.P.	2.31	927.33	18.20	925.02
73				24.8
	+50			24.1
74				23.2
	+50			22.2
75				21.8
	+36			21.7
T.P.	6.00	927.92	5.41	921.92
76				21.7

Lt

L

Lt

$$\frac{98}{50} \quad \frac{76}{35} \quad \frac{93}{27} \quad \frac{98}{24} \quad \frac{92}{17} \quad \frac{89}{8} \quad \frac{90}{11} \quad \frac{95}{19} \quad \frac{98}{31} \quad \frac{102}{50} \quad \frac{108}{50}$$

$$\frac{86}{50} \quad \frac{95}{29} \quad \frac{107}{22} \quad \frac{102}{18} \quad \frac{98}{6} \quad \frac{99}{11} \quad \frac{106}{20} \quad \frac{94}{32} \quad \frac{96}{50}$$

$$\frac{102}{50} \quad \frac{106}{49} \quad \frac{116}{28} \quad \frac{126}{24} \quad \frac{79}{18} \quad \frac{77}{8} \quad \frac{117}{9} \quad \frac{119}{11} \quad \frac{127}{16} \quad \frac{127}{23} \quad \frac{78}{21} \quad \frac{75}{50} \quad \frac{81}{50}$$

$$\frac{110}{50} \quad \frac{125}{30} \quad \frac{135}{26} \quad \frac{134}{22} \quad \frac{128}{17} \quad \frac{125}{8} \quad \frac{126}{5} \quad \frac{129}{10} \quad \frac{142}{15} \quad \frac{142}{25} \quad \frac{12}{50} \quad \frac{78}{50}$$

$$\frac{41}{50} \quad \frac{34}{28} \quad \frac{35}{23} \quad \frac{26}{17} \quad \frac{24}{7} \quad \frac{25}{6} \quad \frac{28}{9} \quad \frac{38}{15} \quad \frac{38}{18} \quad \frac{06}{33} \quad \frac{06}{50} \quad \frac{07}{50}$$

$$\frac{91}{50} \quad \frac{77}{30} \quad \frac{37}{22} \quad \frac{34}{17} \quad \frac{31}{8} \quad \frac{32}{8} \quad \frac{38}{12} \quad \frac{52}{18} \quad \frac{54}{28} \quad \frac{40}{28} \quad \frac{36}{50}$$

$$\frac{124}{50} \quad \frac{111}{33} \quad \frac{51}{21} \quad \frac{42}{17} \quad \frac{40}{7} \quad \frac{41}{7} \quad \frac{46}{17} \quad \frac{74}{23} \quad \frac{82}{32} \quad \frac{81}{32} \quad \frac{72}{50}$$

$$\frac{127}{50} \quad \frac{111}{29} \quad \frac{55}{18} \quad \frac{50}{7} \quad \frac{51}{6} \quad \frac{56}{16} \quad \frac{99}{20} \quad \frac{105}{20} \quad \frac{105}{50}$$

$$\frac{101}{50} \quad \frac{82}{37} \quad \frac{87}{32} \quad \frac{106}{31} \quad \frac{106}{29} \quad \frac{88}{28} \quad \frac{60}{20} \quad \frac{54}{8} \quad \frac{55}{6} \quad \frac{60}{14} \quad \frac{86}{33} \quad \frac{82}{30} \quad \frac{83}{50}$$

$$\frac{67}{50} \quad \frac{67}{38} \quad \frac{75}{32} \quad \frac{83}{30} \quad \frac{74}{29} \quad \frac{59}{18} \quad \frac{54}{8} \quad \frac{56}{4} \quad \frac{59}{10} \quad \frac{74}{23} \quad \frac{66}{23} \quad \frac{66}{50}$$

$$\frac{55}{50} \quad \frac{64}{32} \quad \frac{75}{28} \quad \frac{67}{24} \quad \frac{62}{16} \quad \frac{60}{9} \quad \frac{62}{4} \quad \frac{65}{11} \quad \frac{80}{13} \quad \frac{81}{16} \quad \frac{67}{26} \quad \frac{63}{50} \quad \frac{56}{50}$$

Sta.	+	π	-	E/cv.
		927.92		
76	+50			21.7
77				21.8
78				22.6
	+43			23.1
	+56			23.3
	+87			23.7
79				23.9
	+50			24.6
T.P.	5.86	930.77	3.01	924.71
80				25.2
	+11			25.3
	+116			26.2
+	to Bal. & Eagle Blvd. W.			26.5
B.M.			3.34	927.43
				(927.43)

9/15/89
K.P.
L.C.
M.B.
A.B.

32

Lt.

Lt.

Lt.

$\frac{62}{50}$ $\frac{63}{33}$ $\frac{77}{28}$ $\frac{70}{22}$ $\frac{63}{16}$ $\frac{61}{9}$ $\frac{62}{5}$ $\frac{65}{10}$ $\frac{77}{15}$ $\frac{80}{18}$ $\frac{75}{28}$ $\frac{71}{50}$ $\frac{59}{50}$

$\frac{70}{50}$ $\frac{77}{39}$ $\frac{78}{29}$ $\frac{78}{24}$ $\frac{62}{18}$ $\frac{60}{9}$ $\frac{61}{3}$ $\frac{63}{7}$ $\frac{68}{12}$ $\frac{52}{22}$ $\frac{80}{50}$ $\frac{72}{50}$

$\frac{69}{50}$ $\frac{74}{42}$ $\frac{76}{25}$ $\frac{54}{17}$ $\frac{51}{9}$ $\frac{53}{2}$ $\frac{55}{11}$ $\frac{78}{25}$ $\frac{82}{50}$ $\frac{77}{50}$

$\frac{63}{50}$ $\frac{48}{29}$ $\frac{50}{17}$ $\frac{46}{8}$ $\frac{48}{3}$ $\frac{50}{10}$ $\frac{74}{19}$ $\frac{73}{50}$ $\frac{72}{50}$

$\frac{36}{50}$ $\frac{42}{35}$ $\frac{50}{28}$ $\frac{47}{12}$ $\frac{44}{9}$ $\frac{46}{3}$ $\frac{48}{10}$ $\frac{73}{20}$ $\frac{77}{50}$ $\frac{66}{50}$

$\frac{28}{50}$ $\frac{35}{39}$ $\frac{45}{28}$ $\frac{43}{18}$ $\frac{40}{8}$ $\frac{42}{3}$ $\frac{44}{10}$ $\frac{62}{15}$ $\frac{67}{26}$ $\frac{65}{50}$ $\frac{57}{50}$

$\frac{24}{50}$ $\frac{33}{36}$ $\frac{43}{31}$ $\frac{51}{27}$ $\frac{53}{22}$ $\frac{41}{18}$ $\frac{39}{7}$ $\frac{40}{3}$ $\frac{42}{9}$ $\frac{57}{17}$ $\frac{61}{35}$ $\frac{59}{50}$ $\frac{55}{50}$

L.O. $\frac{28}{32}$ $\frac{46}{26}$ $\frac{40}{22}$ $\frac{37}{18}$ $\frac{33}{9}$ $\frac{73}{6}$ $\frac{36}{11}$ $\frac{49}{14}$ $\frac{50}{16}$ $\frac{42}{16}$ $\frac{34}{50}$

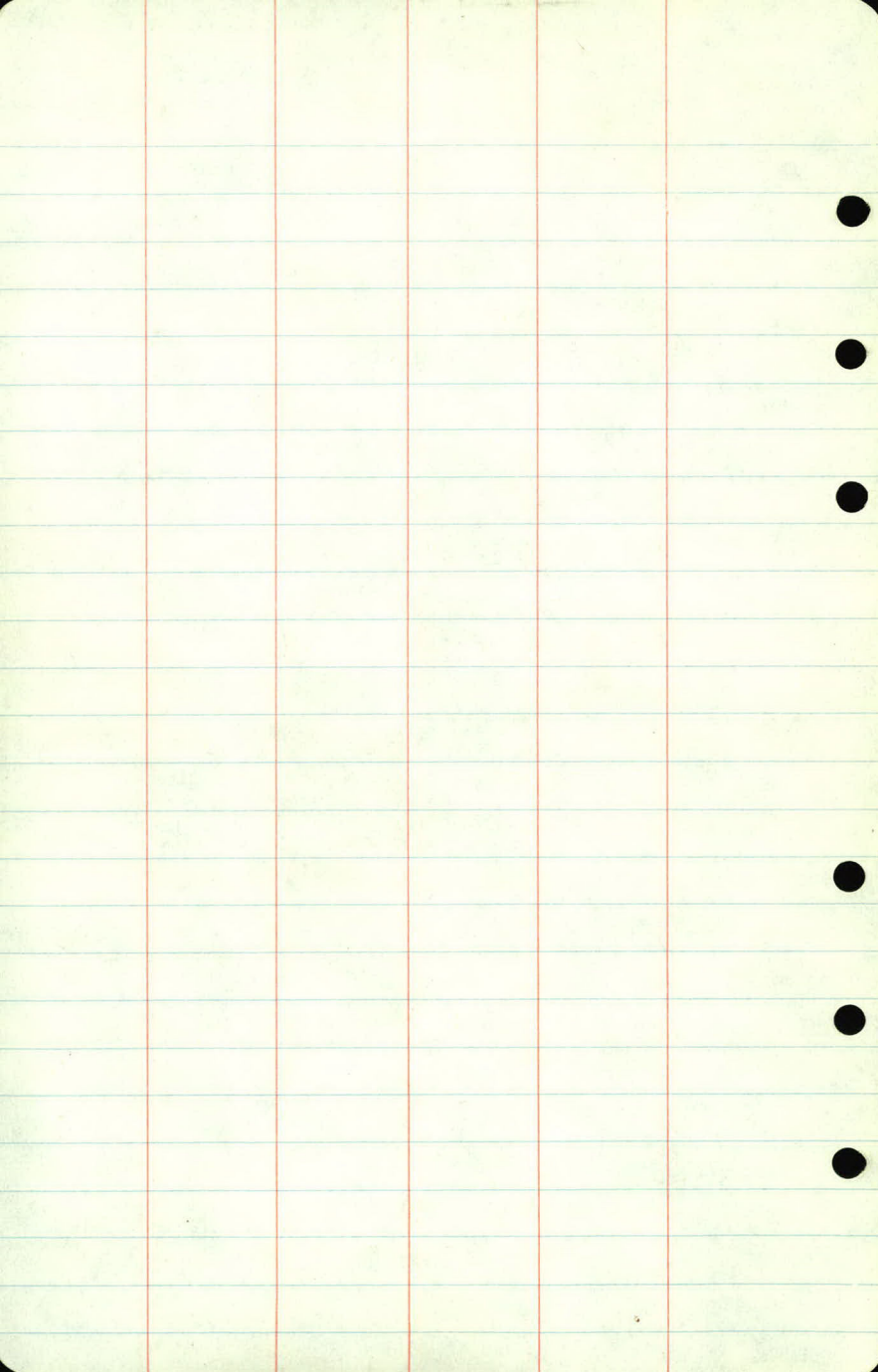
L.O. $\frac{56}{33}$ $\frac{66}{29}$ $\frac{45}{24}$ $\frac{59}{19}$ $\frac{55}{7}$ $\frac{56}{11}$ $\frac{61}{26}$ $\frac{68}{29}$ $\frac{60}{34}$ $\frac{64}{50}$ $\frac{69}{50}$

$\frac{60}{50}$ $\frac{64}{41}$ $\frac{57}{19}$ $\frac{54}{9}$ $\frac{55}{13}$ $\frac{60}{29}$ $\frac{67}{31}$ $\frac{58}{38}$ $\frac{61}{50}$ $\frac{67}{50}$

$\frac{46}{30}$ $\frac{54}{36}$ $\frac{36}{37}$ $\frac{52}{45}$ $\frac{61}{50}$ $\frac{62}{50}$

$\frac{47}{50}$ $\frac{43}{50}$ $\frac{34}{50}$ $\frac{23}{100}$

Spt. in Light Pole Bald Eagle Blvd. W. & Co. Rd. H²¹



Stape stakes

Co. Rd. "H" 2'

sta 0100 to sta 26400

Sta.	I	T	-	Grade
B.M.	11.65	940.75		(929.10)
0	+00			
	+29			29.3
	+50			29.8
	+70			30.2
1				30.9
	+50			32.0
2				33.1
	+50			34.1
3				34.8
	+50			35.2
4				35.4

9/16/40
K.A.
L.G.
M.B.

Gr. Rod Lt. R Rt

Spt. in P.P.S.W. Cor Co Rd "H" & Centerville Rd.

11.5

11.0

$$27.6' / \frac{107}{10.3}$$

$$\frac{112}{10.2}$$

$$\frac{101}{10.9} / 29.8$$

10.6

$$27.4' / \frac{104}{10.2}$$

$$\frac{104}{10.2}$$

$$\frac{76}{13.0} / 33.0$$

9.9

$$27.4' / \frac{97}{10.2}$$

$$\frac{94}{10.5}$$

$$\frac{80}{10.9} / 40.1$$

8.8

$$27.2' / \frac{87}{10.1}$$

$$\frac{83}{10.5}$$

$$\frac{87}{10.1} / 43.2$$

7.7

$$27.2' / \frac{76}{10.1}$$

$$\frac{72}{10.5}$$

$$\frac{13}{10.4} / 37.8$$

6.7

$$27.8' / \frac{43}{10.4}$$

$$\frac{41}{10.6}$$

$$\frac{0.2}{10.5} / 40.0$$

6.0

$$27.4' / \frac{38}{10.2}$$

$$\frac{33}{10.7}$$

$$\frac{14}{10.6} / 37.2$$

5.6

$$27.6' / \frac{33}{10.3}$$

$$\frac{30}{10.6}$$

$$\frac{21}{13.5} / 34.0$$

5.4

$$27.6' / \frac{31}{10.3}$$

$$\frac{49}{10.5}$$

$$\frac{32}{12.2} / 31.4$$

Sta	+	π	-	Grade
		940.75		
4	+50			35.5
5				35.5
	+50			35.6
6				35.6
	+50			35.8
I.P.	8.53	944.93	4.35	36.40
7				36.2
	+50			36.8
8				37.6
	+50			38.6
9				39.5
	+31			40.1

Gr. Red

Lt.

R

Rt.

5.3

$$27.6' / \frac{50}{103}$$

$$\frac{50}{103}$$

$$\frac{41}{11.2} / 29.4'$$

5.3

$$26.4' / \frac{56}{101}$$

$$\frac{52}{101}$$

$$\frac{65}{12.08} / 24.6'$$

5.2

$$29.4' / \frac{69}{103}$$

$$\frac{52}{0.0}$$

$$\frac{20}{-3.8} / 22.6'$$

5.2

$$26.7' / \frac{69}{103}$$

$$\frac{52}{0.0}$$

$$\frac{103}{-5.1} / 25.2'$$

5.0

$$26.6' / \frac{52}{101.8}$$

$$\frac{50}{0.0}$$

$$\frac{25}{-3.5} / 22.0'$$

8.7

$$36.4' / \frac{40}{127}$$

$$\frac{65}{103}$$

$$\frac{91}{12.16} / 26.2'$$

8.1

$$31.4' / \frac{59}{12.2}$$

$$\frac{78}{103}$$

$$\frac{5.2}{12.9} / 32.8'$$

7.3

$$29.0' / \frac{63}{110}$$

$$\frac{70}{103}$$

$$\frac{31}{14.2} / 35.0'$$

6.3

$$27.0' / \frac{77}{106}$$

$$\frac{64}{-6.1}$$

$$\frac{48}{11.5} / 30.0'$$

5.4

$$28.6' / \frac{74}{100.0}$$

$$\frac{54}{20}$$

$$\frac{71}{12.05} / 23.6'$$

4.8

$$27.4' / \frac{68}{100.0}$$

$$\frac{48}{00}$$

$$\frac{76}{-2.8} / 20.6'$$

Sta	+	π	-	Grade	
		944.93			
9	+65			40.7	
10				41.4	
T.P.	5.73	949.82	0.24	944.09	
	+15			41.7	
	+35			42.1	
	+49			42.3	
B.M.			0.02	949.80	949.79
11				43.2	
	+60			43.8	
12				44.1	
	+43			44.3	
	+50			44.3	
13				44.2	
	+50			43.9	

Gr. Rod

Lt

R

Rt

4.2

$$28.4' / \frac{62}{100}$$

$$\frac{42}{90}$$

$$\frac{49}{27} / 20.4'$$

3.5

$$31.1' / \frac{44}{101}$$

$$\frac{34}{101}$$

$$\frac{49}{106} / 24.2'$$

7.5

$$26.4' / \frac{28}{101.7}$$

$$\frac{74}{101}$$

$$\frac{12}{103} / 33.0'$$

Top N.W. Cor Lower Step Front School Ho.

6.6

$$27.0' / \frac{66}{100}$$

$$\frac{65}{101}$$

$$\frac{14}{152} / 33.0'$$

6.0

$$27.8' / \frac{56}{104}$$

$$\frac{56}{104}$$

$$\frac{14}{146} / 35.0'$$

5.7

$$27.8' / \frac{53}{104}$$

$$\frac{51}{106}$$

$$\frac{15}{142} / 35.0'$$

5.5

$$\frac{49}{106}$$

$$\frac{21}{134} / 33.0'$$

5.5

$$30.4' / \frac{38}{117}$$

5.6

$$28.0' / \frac{51}{105}$$

$$\frac{51}{105}$$

$$\frac{28}{128} / 32.6'$$

5.9

$$27.8' / \frac{55}{104}$$

$$\frac{56}{103}$$

$$\frac{27}{132} / 33.0'$$

Sta.	+	π	-	Grade
		949.82		
14				43.4
T.P.	2.81	946.55	6.08	943.74
+50				43.0
15				42.5
+50				42.1
16				41.6
+50				41.2
17				40.7
+50				40.2
18				39.8
+50				39.4
19				38.9

Gr. Rod

LH

R

RH

6.4

$$288' / \frac{55}{10.9}$$

$$\frac{41}{10.3}$$

$$\frac{37}{127.32.4}$$

3.6

$$27.4' / \frac{34}{10.2}$$

$$\frac{33}{10.3}$$

$$\frac{1.5}{121/31.2}$$

4.1

$$26.2' / \frac{45}{10.16}$$

$$\frac{3.8}{10.3}$$

$$\frac{2.9}{112/29.4}$$

4.5

$$26.6' / \frac{61}{10.4}$$

$$\frac{4.2}{10.3}$$

$$\frac{4.6}{119/26.8}$$

5.0

$$23.9' / \frac{70}{10.0}$$

$$\frac{4.7}{10.3}$$

$$\frac{2.9}{10.1/23.2}$$

5.4

$$22.0' / \frac{74}{10.0}$$

$$\frac{5.2}{10.2}$$

$$\frac{8.6}{3.2/21.4}$$

5.9

$$24.6' / \frac{79}{10.0}$$

$$\frac{5.7}{10.2}$$

$$\frac{8.5}{2.6/20.2}$$

6.4

$$25.6' / \frac{71}{10.1.3}$$

$$\frac{4.2}{10.2}$$

$$\frac{7.0}{11.4/23.8}$$

6.8

$$26.0' / \frac{73}{10.1.5}$$

$$\frac{4.8}{10.0}$$

$$\frac{5.5}{11.3/27.6}$$

7.2

$$25.8' / \frac{78}{10.1.4}$$

$$\frac{7.2}{10.0}$$

$$\frac{5.4}{11.8/30.6}$$

7.7

$$28.6' / \frac{97}{10.0}$$

$$\frac{7.8}{10.1}$$

$$\frac{7.1}{10.6/28.2}$$

Sta.	+	T	-	Grade
		946.55		
19	+50			38.5
T.P.	3.60	941.62	8.53	938.02
20				36.1
	+50			27.8
21				37.5
	+50			37.3
22				37.1
	+50			36.9
23				36.6
	+50			36.4
24				36.2
	+50			35.9

Gr. Rod

Lt

K

Rt

8.1

$$28.6' / \frac{24}{120.7}$$

$$\frac{83}{-0.2}$$

$$\frac{74}{10.1/28.4'}$$

3.5

$$29.7' / \frac{45}{12.10}$$

$$\frac{36}{-0.1}$$

$$\frac{33}{10.2/27.4'}$$

3.8

$$27.4' / \frac{36}{10.2}$$

$$\frac{38}{0.0}$$

$$\frac{34}{10.4/27.8'}$$

4.1

$$30.2' / \frac{25}{11.6}$$

$$\frac{40}{10.1}$$

$$\frac{38}{10.3/27.6'}$$

4.3

$$33.0' / \frac{13}{13.1}$$

$$\frac{42}{10.1}$$

$$\frac{39}{10.4/27.8'}$$

4.5

$$33.0' / \frac{10}{13.5}$$

$$\frac{45}{0.0}$$

$$\frac{35}{11.0/29.0'}$$

4.7

$$33.0' / \frac{0.9}{13.8}$$

$$\frac{48}{-0.1}$$

$$\frac{3.0}{11.7/30.4'}$$

5.0

$$31.6' / \frac{27}{12.3}$$

$$\frac{50}{0.0}$$

$$\frac{46}{10.8/27.8'}$$

5.2

$$27.0' / \frac{52}{10.0}$$

$$\frac{52}{0.0}$$

$$\frac{72}{10.0/25.1'}$$

5.4

$$28.5' / \frac{73}{10.1}$$

$$\frac{35}{-0.1}$$

$$\frac{70}{-1.6/18.2'}$$

5.7

$$26.8' / \frac{6.8}{12.9}$$

$$\frac{57}{0.0}$$

$$\frac{85}{-2.8/20.6'}$$

Sta	+	π	-	Grade
		941.62		
25				35.7
T.P.	5.55	941.37	5.80	935.92
+50				35.5
26				35.2
B.M.			0.77	940.60
				(940.61)

Gr Rod

Lt.

L

Rt

5.9

$$\begin{array}{r} 30.2' / 14.3 \\ 7.6 \end{array}$$

$$\begin{array}{r} 58 \\ 10.1 \end{array}$$

$$\begin{array}{r} 74 \\ 20.5 / 24.0' \end{array}$$

5.9

$$\begin{array}{r} 33.0' / 28 \\ 13.1 \end{array}$$

$$\begin{array}{r} 58 \\ 10.1 \end{array}$$

$$\begin{array}{r} 58 \\ 10.1 / 27.2' \end{array}$$

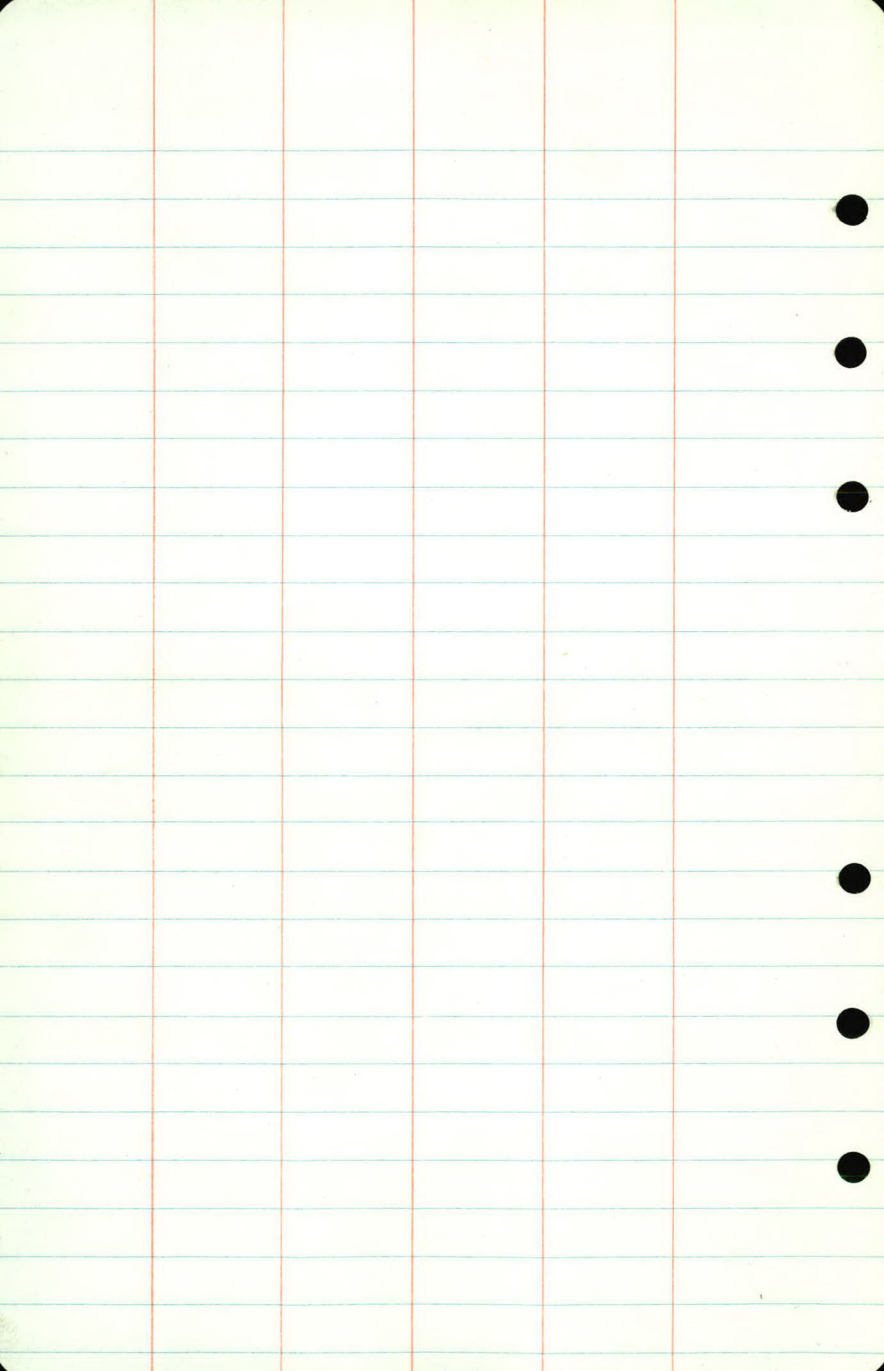
6.2

$$\begin{array}{r} 33.0' / 26 \\ 13.6 \end{array}$$

$$\begin{array}{r} 61 \\ -9.1 \end{array}$$

$$\begin{array}{r} 57 \\ 10.5 / 28.0' \end{array}$$

Spt in 8" @ 80 Lb. sta 24154



$$937.22 = PP \text{ at } H = 2$$

$$\begin{array}{r} 948.48 \\ \underline{3.73} \end{array}$$

$$\begin{array}{r} 944.75 \\ \underline{4.40} \end{array}$$

$$+ \begin{array}{r} 949.15 \\ \underline{7.32} \end{array}$$

$$\begin{array}{r} 941.835 \\ \underline{0.815} \end{array}$$

$$\begin{array}{r} 942.645 \\ \underline{10.81} \end{array}$$

$$\begin{array}{r} 931.835 \\ \underline{0.22} \end{array}$$

$$+ \begin{array}{r} 932.055 \\ \underline{6.33} \end{array}$$

$$\begin{array}{r} 925.725 \end{array}$$

B.M.
18" oak rt
124 ft
Otter Lake
Bd.

slope stakes
Co. Rd "H²"

Note: Stakes encircled are set by
separate set of levels.

Sta + π - Grade

B.M. 1236 942.46 (929.10)

0 +00 29.1

+10

+15 29.0

+20 29.1

+29 29.3

+50 29.8

+70 30.2

30.9

Gr. Rod.

Lt.

G.

Rt.

5 pk. in P.P. Gooler ville Rd & G.O. Rd "H" 2"

12.7

$$\begin{array}{r} 27.4' / 12.5 \\ \hline 10.2 \end{array}$$

-0.5

$$\begin{array}{r} 11.7 \\ \hline 11.0 / 29.0 \end{array}$$

12.3

$$\begin{array}{r} 27.2' / 12.2 \\ \hline 10.1 \end{array}$$

$$\begin{array}{r} 12.0 \\ \hline 10.3 \end{array}$$

$$\begin{array}{r} 9.0 \\ \hline 13.3 / 33.0 \end{array}$$

11.6

$$\begin{array}{r} 27.4' / 11.4 \\ \hline 10.2 \end{array}$$

$$\begin{array}{r} 11.3 \\ \hline 10.3 \end{array}$$

$$\begin{array}{r} 9.5 \\ \hline 17.1 / 33.0 \end{array}$$

Sta.	+	X	-	Grade
		942.46		

1	+50			32.0
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2				33.1
---	--	--	--	------

	+50			34.1
--	-----	--	--	------

3				34.8
---	--	--	--	------

	+50			35.2
--	-----	--	--	------

4				35.4
---	--	--	--	------

	+50			35.5
--	-----	--	--	------

5				35.5
---	--	--	--	------

	+50			35.6
--	-----	--	--	------

6				35.6
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T.P.	10.14	946.08	6.52	935.94
------	-------	--------	------	--------

	+50			35.8
--	-----	--	--	------

T.P.	9.27	945.77	6.52	935.50
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Gr. Rod

Lt.

R.

Rt.

10.5

$$27.4' / \frac{10.3}{10.2}$$

$$\frac{10.4}{10.1}$$

$$\frac{2.9}{17.6} / 33.0'$$

9.4

$$27.4' / \frac{9.2}{10.2}$$

$$\frac{9.0}{10.4}$$

$$\frac{3.0}{16.4} / 33.0'$$

8.4

$$27.8' / \frac{8.0}{10.4}$$

$$\frac{8.1}{10.3}$$

$$\frac{2.0}{16.4} / 33.0'$$

7.7

$$27.4' / \frac{7.5}{10.2}$$

$$\frac{7.2}{10.5}$$

$$\frac{2.8}{14.9} / 33.0'$$

7.3

$$27.4' / \frac{7.1}{10.2}$$

$$\frac{6.8}{10.5}$$

$$\frac{3.7}{12.4} / 32.0'$$

7.1

$$27.6' / \frac{6.8}{10.3}$$

$$\frac{6.6}{10.5}$$

$$\frac{5.1}{12.0} / 31.0'$$

7.0

$$27.4' / \frac{6.8}{10.2}$$

$$\frac{6.7}{10.3}$$

$$\frac{6.1}{10.7} / 33.0'$$

7.0

$$27.7' / \frac{8.0}{10.1}$$

$$\frac{6.9}{10.1}$$

$$\frac{8.3}{20.7} / 20.4'$$

6.9

$$27.1' / \frac{8.4}{10.5}$$

$$\frac{6.8}{10.1}$$

$$\frac{10.7}{28.7} / 22.6'$$

6.9

$$26.8' / \frac{8.5}{10.4}$$

$$\frac{6.8}{10.1}$$

$$\frac{11.9}{50.0} / 25.0'$$

10.3

$$25.6' / \frac{11.0}{11.3}$$

$$\frac{10.2}{10.1}$$

$$\frac{13.8}{35.5} / 22.0'$$

Sta.	+	π	-	Grade
		996.08		

7				36.2
---	--	--	--	------

	+50			36.8
--	-----	--	--	------

8				37.6
---	--	--	--	------

	+50			38.6
--	-----	--	--	------

9				39.5
---	--	--	--	------

	+31			40.1
--	-----	--	--	------

	+65			40.7
--	-----	--	--	------

10				41.4
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	+15			41.7
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T.P.	10.79	953.48	3.34	942.74
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	+35			42.1
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B.M.	3.93	953.22	3.69	949.19
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	+49			42.3
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949.19

Gr. Road.

$$9.9 \quad 32.4' / \frac{7.2}{12.7} \quad \frac{9.9}{0.0} \quad \frac{10.5}{12.6} / 26.2'$$

$$9.3 \quad 31.4' / \frac{7.1}{12.2} \quad \frac{9.2}{10.1} \quad \frac{6.3}{13.0} / 33.0'$$

$$8.5 \quad 29.2' / \frac{7.4}{11.1} \quad \frac{8.3}{10.2} \quad \frac{9.4}{14.1} / 33.0'$$

$$7.5 \quad 26.7' / \frac{8.8}{10.8} \quad \frac{7.5}{0.0} \quad \frac{6.3}{14.2} / 29.4'$$

$$6.6 \quad 28.2' / \frac{8.6}{10.0} \quad \frac{6.5}{10.1} \quad \frac{8.3}{10.3} / 23.6'$$

$$6.0 \quad \begin{matrix} 34.6 \\ 26' / \text{Color} \\ 9.6 \end{matrix} \quad 27.0' / \frac{8.0}{10.0} \quad \frac{5.9}{10.1} \quad \frac{8.9}{-2.9} / 20.8'' \quad \begin{matrix} 37.1 \\ 60.14' / 20.0' \\ 9.0' \end{matrix}$$

$$5.4 \quad 27.8' / \frac{7.4}{10.0} \quad \frac{5.3}{10.1} \quad \frac{8.1}{-2.7} / 20.4'$$

$$4.7 \quad 27.2' / \frac{4.6}{10.1} \quad \frac{4.6}{10.1} \quad \frac{6.0}{12.7} / 20.4'$$

Top N.W. Cor Bottom Steps School Ho.

$$10.9 \quad 26.2' / \frac{11.3}{12.6} \quad \frac{10.8}{+0.3} \quad \frac{4.6}{12.3} / 33.0'$$

Sta.	+	π	-	Grade
		953.22		
11				43.2
	+50			43.8
12				44.1
	+43			44.3
13				44.2
I.P.	3.83	948.46	1.57	44.63
	+50			43.9
14				43.4
	+50			42.9
15				42.5
	+50			42.1
16				41.6

Gr. Rod

Lt.

R

Rt

$$10.0 \quad 26.4' / \begin{array}{r} 10.2 \\ \hline 8.18 \end{array} \quad \begin{array}{r} 99 \\ + 91 \end{array} \quad \begin{array}{r} 9.8 \\ \hline 15.2 / 33.0' \end{array}$$

$$9.4 \quad 27.6' / \begin{array}{r} 91 \\ \hline 10.3 \end{array} \quad \begin{array}{r} 90 \\ + 94 \end{array} \quad \begin{array}{r} 9.8 \\ \hline 14.6 / 33.0 \end{array}$$

$$9.1 \quad 27.8' / \begin{array}{r} 8.7 \\ \hline 10.4 \end{array} \quad \begin{array}{r} 85 \\ + 96 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 14.2 / 33.0 \end{array}$$

$$8.9 \quad 30.4' / \begin{array}{r} 7.2 \\ \hline 11.7 \end{array} \quad \begin{array}{r} 86 \\ + 96 \end{array} \quad \begin{array}{r} 5.7 \\ \hline 15.2 / 33.0' \end{array}$$

$$9.0 \quad 28.0' / \begin{array}{r} 8.5 \\ \hline 10.5 \end{array} \quad \begin{array}{r} 85 \\ + 95 \end{array} \quad \begin{array}{r} 6.3 \\ \hline 12.7 / 32.4' \end{array}$$

$$4.6 \quad 27.2' / \begin{array}{r} 4.4 \\ + 0.2 \end{array} \quad \begin{array}{r} 4.3 \\ + 0.3 \end{array} \quad \begin{array}{r} 1.5 \\ \hline + 3.1 / 32.0 \end{array}$$

$$5.1 \quad 29.4' / \begin{array}{r} 3.9 \\ + 1.2 \end{array} \quad \begin{array}{r} 4.8 \\ + 0.3 \end{array} \quad \begin{array}{r} 2.4 \\ \hline + 2.7 / 32.4 \end{array}$$

$$5.6 \quad 27.6' / \begin{array}{r} 5.3 \\ + 0.3 \end{array} \quad \begin{array}{r} 5.1 \\ + 0.5 \end{array} \quad \begin{array}{r} 3.4 \\ \hline + 2.2 / 31.4 \end{array}$$

$$6.0 \quad 26.2' / \begin{array}{r} 6.4 \\ \hline 1.6 \end{array} \quad \begin{array}{r} 5.8 \\ + 0.2 \end{array} \quad \begin{array}{r} 4.8 \\ \hline + 1.2 / 29.4 \end{array}$$

$$6.6 \quad 25.8' / \begin{array}{r} 8.1 \\ \hline 0.5 \end{array} \quad \begin{array}{r} 6.0 \\ + 0.6 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 0.0 / 27.0 \end{array}$$

$$6.9 \quad 22.6' / \begin{array}{r} 8.9 \\ \hline 0.0 \end{array} \quad \begin{array}{r} 6.5 \\ + 0.4 \end{array} \quad \begin{array}{r} 8.9 \\ \hline 0.0 / 23.0 \end{array}$$

Sta.	+	π	-	Grade
		948.46		
16	+50			41.2
17				40.7
	+50			40.2
18				39.8
T.P.	4.56	944.53	8.49	939.97
	+50			39.9
19				38.9
	+50			38.5
20				38.1
	+50			37.8
21				37.5
	+50			37.3

Gr. Rad.

Lb

g

oz

$$7.3 \quad \begin{array}{r} 21.5 \\ \times 9.3 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 7.1 \\ + 0.2 \end{array}$$

$$\begin{array}{r} 10.6 \\ - 3.3 \\ \hline 21.6 \end{array}$$

$$7.8 \quad \begin{array}{r} 23.1 \\ \times 9.8 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 7.5 \\ + 0.3 \end{array}$$

$$\begin{array}{r} 10.5 \\ - 2.7 \\ \hline 20.4 \end{array}$$

$$8.3 \quad \begin{array}{r} 25.9 \\ \times 9.1 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 8.0 \\ + 0.3 \end{array}$$

$$\begin{array}{r} 8.9 \\ - 1.4 \\ \hline 25.8 \end{array}$$

$$8.7 \quad \begin{array}{r} 26.0 \\ \times 9.2 \\ \hline 21.5 \end{array}$$

$$\begin{array}{r} 8.5 \\ + 0.2 \end{array}$$

$$\begin{array}{r} 7.3 \\ + 1.4 \\ \hline 29.8 \end{array}$$

$$5.1 \quad \begin{array}{r} 25.4 \\ \times 5.9 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ - 0.1 \end{array}$$

$$\begin{array}{r} 3.6 \\ + 1.5 \\ \hline 30.0 \end{array}$$

$$5.6 \quad \begin{array}{r} 28.2 \\ \times 3.6 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ - 0.1 \end{array}$$

$$\begin{array}{r} 5.0 \\ + 0.6 \\ \hline 28.2 \end{array}$$

$$6.0 \quad \begin{array}{r} 29.7 \\ \times 3.7 \\ \hline 20.3 \end{array}$$

$$\begin{array}{r} 6.2 \\ - 0.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ + 0.6 \\ \hline 28.2 \end{array}$$

$$6.4 \quad \begin{array}{r} 30.0 \\ \times 3.6 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 6.5 \\ - 0.1 \end{array}$$

$$\begin{array}{r} 6.1 \\ + 0.3 \\ \hline 27.6 \end{array}$$

$$6.7 \quad \begin{array}{r} 27.2 \\ \times 6.6 \\ \hline 20.1 \end{array}$$

$$\begin{array}{r} 6.7 \\ 0.0 \end{array}$$

$$\begin{array}{r} 6.4 \\ + 0.3 \\ \hline 27.6 \end{array}$$

$$7.0 \quad \begin{array}{r} 20.2 \\ \times 5.4 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 6.8 \\ + 0.2 \end{array}$$

$$\begin{array}{r} 6.8 \\ + 0.2 \\ \hline 27.4 \end{array}$$

$$7.2 \quad \begin{array}{r} 22.8 \\ \times 4.3 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 7.1 \\ + 0.1 \end{array}$$

$$\begin{array}{r} 6.8 \\ + 0.4 \\ \hline 27.8 \end{array}$$

Sta.	+	X	-	Grade
		944.53		
22				32.1
	+50			31.9
23				34.6
T.P.	2.35	941.33	5.55	938.98
	+50			36.4
24				36.2
	+50			35.9
25				35.7
	+50			35.5
26				35.2
	+30			35.1
B.M.			0.71	940.62
	+58			35.0

(940.61)

Gr. Rod.

Lt.

R.

Rt.

$$7.4 \quad 33.0 / \begin{array}{r} 3.9 \\ + 3.5 \end{array}$$

$$\begin{array}{r} 7.4 \\ 0.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ + 1.5 \end{array} / 30.0$$

$$7.6 \quad 33.0 / \begin{array}{r} 3.8 \\ + 3.8 \end{array}$$

$$\begin{array}{r} 7.6 \\ 0.0 \end{array}$$

$$\begin{array}{r} 5.8 \\ + 1.8 \end{array} / 30.6$$

$$7.9 \quad 31.4 / \begin{array}{r} 5.7 \\ + 2.2 \end{array}$$

$$\begin{array}{r} 7.8 \\ + 0.1 \end{array}$$

$$\begin{array}{r} 7.2 \\ + 0.7 \end{array} / 28.4$$

Nail in T.P. Lt.

$$4.9 \quad 26.6 / \begin{array}{r} 5.1 \\ + 1.8 \end{array}$$

$$\begin{array}{r} 4.9 \\ 0.0 \end{array}$$

$$\begin{array}{r} 6.8 \\ + 0.1 \end{array} / 23.2$$

$$5.1 \quad 25.0 / \begin{array}{r} 6.1 \\ + 1.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ 0.0 \end{array}$$

$$\begin{array}{r} 7.1 \\ - 2.0 \end{array} / 19.0$$

$$5.4 \quad 25.2 / \begin{array}{r} 6.3 \\ + 1.1 \end{array}$$

$$\begin{array}{r} 5.3 \\ + 0.1 \end{array}$$

$$\begin{array}{r} 8.3 \\ - 2.9 \end{array} / 20.8$$

$$5.6 \quad 30.2 / \begin{array}{r} 4.0 \\ + 1.6 \end{array}$$

$$\begin{array}{r} 5.5 \\ + 0.1 \end{array}$$

$$\begin{array}{r} 7.1 \\ + 0.5 \end{array} / 24.0$$

$$5.8 \quad 33.0 / \begin{array}{r} 2.4 \\ + 3.4 \end{array}$$

$$\begin{array}{r} 5.8 \\ 0.0 \end{array}$$

$$\begin{array}{r} 5.8 \\ + 0.0 \end{array} / 27.0$$

$$6.1 \quad 33.0 / \begin{array}{r} 2.6 \\ + 3.5 \end{array}$$

$$\begin{array}{r} 6.0 \\ + 0.1 \end{array}$$

$$\begin{array}{r} 5.6 \\ + 0.5 \end{array} / 25.0$$

$$6.2 \quad 32.6 / \begin{array}{r} 3.4 \\ + 3.8 \end{array}$$

$$\begin{array}{r} 6.1 \\ + 0.1 \end{array}$$

$$\begin{array}{r} 6.2 \\ + 0.0 \end{array} / 27.0$$

Spt. in 8" Oak 80' Lt 26.54

$$6.3 \quad 33.0 / \begin{array}{r} 5.1 \\ + 3.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ + 0.1 \end{array}$$

$$\begin{array}{r} 6.3 \\ + 0.3 \end{array} / 26.6$$

Sta	+	π	-	Grade
		241.33		

27				34.8
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	+50			34.6
--	-----	--	--	------

28				34.3
T.P.	5.90	999.95	728'	999.05

	+50			34.2
--	-----	--	--	------

29				34.2
----	--	--	--	------

	+50			34.4
--	-----	--	--	------

30				34.6
----	--	--	--	------

	+50			35.0
--	-----	--	--	------

31				35.3
----	--	--	--	------

	+50			35.6
--	-----	--	--	------

32				36.0
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Gr. Rod

L_t

A

L_t

$$6.5 \quad \begin{array}{r} 21.5/60 \\ 105 \end{array} \quad \begin{array}{r} 29.6/5.7 \\ 108 \end{array} \quad \begin{array}{r} 65 \\ 00 \end{array} \quad \begin{array}{r} 85 \\ 200/25.8 \end{array}$$

$$6.7 \quad \begin{array}{r} 21.13 \\ 256 \end{array} \quad \begin{array}{r} 27.6/4.4 \\ 103 \end{array} \quad \begin{array}{r} 6.9 \\ -0.2 \end{array} \quad \begin{array}{r} 8.9 \\ -2.2/19.4 \end{array}$$

$$7.0 \quad \begin{array}{r} 25.4/7.5 \\ 10.2 \end{array} \quad \begin{array}{r} 7.2 \\ -0.2 \end{array} \quad \begin{array}{r} 13.8 \\ -6.8/29.6 \end{array}$$

$$5.8 \quad \begin{array}{r} 24.0/7.3 \\ 10.5 \end{array} \quad \begin{array}{r} 5.9 \\ -9.1 \end{array} \quad \begin{array}{r} 12.8 \\ -7.0/29.0 \end{array} \quad \begin{array}{r} -6.9 \\ 28.8 \end{array}$$

$$5.8 \quad \begin{array}{r} 20.9 \\ 23.8/24.0 \end{array} \quad \begin{array}{r} 7.3 \\ 10.5 \end{array} \quad \begin{array}{r} 6.1 \\ -0.3 \end{array} \quad \begin{array}{r} 10.0 \\ -4.2/29.4 \end{array}$$

$$5.6 \quad \begin{array}{r} 20.9 \\ 24.8 \end{array} \quad \begin{array}{r} 25.0/7.6 \\ 10.0 \end{array} \quad \begin{array}{r} 3.8/0.4 \\ -4.2 \end{array} \quad \begin{array}{r} 5.6 \\ 8.1/15.0 \end{array}$$

$$5.4 \quad \begin{array}{r} 25.8/6.0 \\ 11.9 \end{array} \quad \begin{array}{r} 5.3 \\ 10.0/0.0 \end{array} \quad \begin{array}{r} 7.4 \\ 10.0/20.3 \end{array}$$

$$5.0 \quad \begin{array}{r} 21.11 \\ 25.2 \end{array} \quad \begin{array}{r} 25.8/5.6 \\ 11.9 \end{array} \quad \begin{array}{r} 5.1/0.2 \\ -0.1 \end{array} \quad \begin{array}{r} 6.1 \\ 10.9/24.8 \end{array}$$

$$4.7 \quad \begin{array}{r} 26.0/5.2 \\ 11.5 \end{array} \quad \begin{array}{r} 3.8/0.3 \\ -0.1 \end{array} \quad \begin{array}{r} 4.8 \\ 11.9/26.8 \end{array}$$

$$4.4 \quad \begin{array}{r} 29.8/3.0 \\ 11.4 \end{array} \quad \begin{array}{r} 1.5 \\ -0.1 \end{array} \quad \begin{array}{r} 4.4 \\ 11.0/29.0 \end{array} \quad \begin{array}{r} 10.7 \\ 28.4 \end{array}$$

$$4.0 \quad \begin{array}{r} 31.8/1.6 \\ 12.4 \end{array} \quad \begin{array}{r} 1.0 \\ 0.0 \end{array} \quad \begin{array}{r} 2.6 \\ 11.4/29.8 \end{array}$$

Sta	+	π	-	Grade
		9999.5'		

32	+50			36.3
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33				36.6
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	+50			36.8
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34				36.9
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I.P.	4.96	991.40	3.01	996.94
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	+50			36.9
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35				36.9
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	+50			36.8
--	-----	--	--	------

36				36.8
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	+50			36.7
--	-----	--	--	------

37				36.7
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37	+50			36.6
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Gr. Rod.

Lt.

R.

Rt.

3.7

$$32.8' / \frac{0.8}{42.9}$$

$$\frac{37}{00}$$

$$\frac{32}{105} / 29.0'$$

3.4

$$\left(\frac{421}{312} \right) 31.4' / \frac{605}{10.2}$$

$$\frac{34}{00}$$

$$\frac{34}{100} / 27.0'$$

$$\left(\frac{0619}{268} \right)$$

3.2'

$$28.0' / \frac{2.2}{41.0}$$

$$\frac{32}{-01} \text{ (0.2)}$$

$$\frac{2.2}{104} / 27.8'$$

$$\left(\frac{100}{27.0} \right)$$

3.1

$$\left(\frac{413}{296} \right) 29.8' / \frac{1.7}{41.4}$$

$$\frac{31}{00}$$

$$\frac{2.2}{108} / 28.6'$$

$$\left(\frac{107}{28.8} \right)$$

4.5

$$30.4' / \frac{2.8}{41.7}$$

$$\frac{46}{-01} \text{ (0.0)}$$

$$\frac{2.8}{41.7} / 30.4'$$

$$\left(\frac{118}{30.6} \right)$$

4.5

$$31.6' / \frac{2.2}{42.3}$$

$$\frac{47}{-0.2}$$

$$\frac{21}{12.9} / 31.8'$$

✓

4.6

$$31.4' / \frac{2.9}{42.2}$$

$$\frac{46}{00}$$

$$\frac{25}{12.1} / 31.2'$$

✓

4.6

$$28.8' / \frac{3.7}{40.3}$$

$$\frac{48}{-0.2}$$

$$\frac{22}{10.8} / 27.4'$$

$$\left(\frac{10.3}{27.6} \right)$$

4.7

$$\left(\frac{R.17}{26.4} \right) 26.2' / \frac{5.1}{40.6}$$

$$\frac{49}{-0.2} \text{ (0.3)}$$

$$\frac{6.2}{10.5} / 24.0'$$

$$\left(\frac{R.07}{24.4} \right)$$

4.7

$$26.0' / \frac{5.2}{41.5}$$

$$\frac{50}{-0.3}$$

$$\frac{5.8}{10.9} / 24.8'$$

4.8

$$\left(\frac{R.12}{25.4} \right) 25.2' / \frac{4.7}{41.1}$$

$$\frac{5.2}{-0.4}$$

$$\frac{5.8}{11.0} / 25.0'$$

Sta.	+	x	-	Grade
		941.40		
38				36.7
	+50			36.7
T.P.	6.86	942.79	5.47	935.73
39				36.8
	+50			37.0
B.M.		942.79	4.85	937.94
				937.95 (937.33)?
40				37.2
	+50			37.4
41				37.7
	+50			38.0
42				38.4
	+50			38.8
43				39.2

Gr. Rod.

Lt

R

Rt

$$4.7 \quad \frac{\text{R.07}}{250} \quad 25.2' / \frac{56}{\text{R.11}} \quad \frac{54}{-0.7} \quad \frac{55}{\text{R.12}} / 25.4'$$

$$4.7 \quad \frac{\text{R.09}}{248} \quad 24.6' / \frac{59}{\text{R.08}} \quad \frac{56}{-0.9} \quad \frac{61}{\text{R.06}} / 24.2' \quad \frac{\text{R.07}}{244}$$

+51

$$6.0 \quad \frac{\text{R.05}}{251} \quad 25.1' / \frac{6.9}{\text{R.11}} \quad \frac{7.0}{-1.0} \quad \frac{\text{R.03}}{236} \quad \frac{7.8}{\text{R.02}} / 23.4$$

$$5.8 \quad \frac{\text{R.10}}{25.9} \quad 25.9' / \frac{6.9}{\text{R.0.9}} \quad \frac{6.8}{-1.0} \quad \frac{7.0}{\text{R.0.8}} / 24.6$$

Spk. in 8" R. Elder. Lt. 39175

$$5.6 \quad \frac{\text{R.16}}{26.21} \quad 26.21' / \frac{6.7}{\text{R.1.5}} \quad \frac{6.7}{-1.1} \quad \frac{\text{R.02}}{274} \quad \frac{6.6}{\text{R.0.8}} / 27.0$$

$$5.4 \quad \frac{\text{R.15}}{26.0} \quad 26.0' / \frac{6.7}{\text{R.1.4}} \quad \frac{6.7}{-1.2} \quad \frac{\text{R.02}}{274} \quad \frac{5.7}{\text{R.1.7}} / 26.4 \quad \frac{\text{R.1.7}}{26.8}$$

$$5.1 \quad \frac{\text{R.09}}{248} \quad 24.8' / \frac{6.7}{\text{R.1.1}} \quad \frac{5.1}{-0.8} \quad \frac{7.1}{\text{R.0.9}} / 21.0$$

$$4.8 \quad \frac{\text{R.03}}{24.0} \quad 24.0' / \frac{6.4}{\text{R.0.0}} \quad \frac{5.6}{-0.8} \quad \frac{8.0}{\text{R.0.2}} / 21.4 \quad \frac{-2.9}{20.8}$$

$$4.4 \quad \frac{\text{R.05}}{24.0} \quad 24.0' / \frac{6.4}{\text{R.0.0}} \quad \frac{5.4}{-1.0} \quad \frac{7.7}{\text{R.0.3}} / 21.6$$

$$4.0 \quad \frac{\text{R.07}}{24.4} \quad 24.4' / \frac{6.0}{\text{R.0.0}} \quad \frac{4.8}{-0.8} \quad \frac{7.3}{\text{R.0.3}} / 21.6$$

$$3.5 \quad \frac{\text{R.07}}{24.4} \quad 24.4' / \frac{5.5}{\text{R.0.0}} \quad \frac{4.3}{+0.6} \quad \frac{6.5}{\text{R.0.2}} / 21.0 \quad \frac{-2.8}{20.6}$$

Sta	+	π	-	Grade
		94'2.79		
43	+50			39.8
T.P.	12.03	952.60	2.82	939.97 ✓
44				40.2
	+50			40.7
				41.2
45				41.6
	+50			42.0
46				42.1
	+40			42.2
	+72			42.3
47				42.3
	+50			42.3
48				42.1

Gr. Rod.

Lt

R

Rt.

3.0

$$\begin{array}{r} 27.3 \\ \times 0.0 \\ \hline 0.0 \end{array} \quad \begin{array}{r} R.08 \\ 24.6 \\ \hline 3.6 \\ - 0.6 \end{array}$$

$$\begin{array}{r} 5.6 \\ - 2.6 \\ \hline 3.0 \end{array} \quad \begin{array}{r} R.24 \\ 19.8 \\ \hline 2.4 \\ - 1.8 \end{array}$$

11.8

$$\begin{array}{r} 25.4 \\ \times 1.2 \\ \hline 30.5 \end{array} \quad \begin{array}{r} R.15 \\ 26.0 \\ \hline 12.2 \\ - 0.4 \end{array}$$

$$\begin{array}{r} 13.8 \\ \times 0.0 \\ \hline 2.1 \end{array}$$

11.3

$$\begin{array}{r} 27.6 \\ \times 0.3 \\ \hline 10.3 \end{array} \quad \begin{array}{r} 11.6 \\ - 0.3 \end{array}$$

$$\begin{array}{r} 12.4 \\ \times 0.9 \\ \hline 24.8 \end{array}$$

R 0.0

10.8

$$\begin{array}{r} 6.8 \\ \times 2.8 \\ \hline 19.0 \end{array} \quad \begin{array}{r} 12.7 \\ 12.9 \\ \hline 10.9 \\ - 0.1 \end{array}$$

$$\begin{array}{r} 10.1 \\ + 0.7 \\ \hline 28.4 \end{array} \quad \begin{array}{r} 10.8 \\ 28.6 \\ \hline 10.8 \\ - 1.5 \end{array}$$

10.4

$$\begin{array}{r} 32.0 \\ \times 6.1 \\ \hline 4.3 \end{array}$$

$$\begin{array}{r} 10.4 \\ \times 0.0 \\ \hline 10.2 \end{array}$$

$$\begin{array}{r} 7.3 \\ + 3.1 \\ \hline 33.0 \end{array}$$

10.0

$$\begin{array}{r} 33.0 \\ \times 6.0 \\ \hline 4.0 \end{array}$$

$$\begin{array}{r} 9.4 \\ + 0.4 \\ \hline 10.6 \end{array}$$

$$\begin{array}{r} 5.7 \\ + 4.3 \\ \hline 33.0 \end{array}$$

9.9

$$\begin{array}{r} 32.4 \\ \times 7.2 \\ \hline 12.7 \end{array}$$

$$\begin{array}{r} 9.4 \\ + 0.9 \\ \hline 10.3 \end{array}$$

$$\begin{array}{r} 9.6 \\ + 4.3 \\ \hline 33.0 \end{array}$$

9.8

$$\begin{array}{r} 32.4 \\ \times 7.2 \\ \hline 12.6 \end{array} \quad \begin{array}{r} 12.8 \\ 12.6 \\ \hline 12.8 \\ - 1.0 \end{array}$$

$$\begin{array}{r} 9.4 \\ + 0.7 \\ \hline 10.1 \end{array}$$

$$\begin{array}{r} 9.5 \\ + 5.3 \\ \hline 33.0 \end{array}$$

9.7

$$\begin{array}{r} 32.2 \\ \times 7.1 \\ \hline 12.6 \end{array} \quad \begin{array}{r} 12.5 \\ 12.0 \\ \hline 12.5 \\ + 0.8 \end{array} \quad \begin{array}{r} 8.9 \\ + 0.8 \\ \hline 10.7 \end{array}$$

$$\begin{array}{r} 5.2 \\ + 4.5 \\ \hline 33.0 \end{array}$$

Sta.	+	π	-	Grade	
		952.00			
47	+50			42.3	
48				42.1	
	+50			41.9	
T.P.	2.28	944.73	9.55	942.45	
49				41.6	939.6
	+50			41.2	5.3 939.95
50				40.8	5.4 939.3
	+50			40.4	5.6 939.15
51				40.0	5.7 939.0
	+30			39.7	6.00 938.75
	+60			39.5	6.2 938.5
52				39.2	6.5 938.2

Gr. Rod.

LH

L

RH

9.7

$$33.0' / \frac{53}{14.4} \left(\frac{14.3}{33.0} \right)$$

$$9.7 / 10.7 \left(+0.8 \right)$$

$$6.7 / 33.0' \left(\frac{13.1}{33.0} \right)$$

9.9

$$33.0' / \frac{6.6}{13.3} \left(\frac{13.4}{33.0} \right)$$

$$9.9 / 10.7 \left(+0.8 \right)$$

$$8.1 / 30.6'$$

10.1

$$29.6' / \frac{9.0}{11.1} \left(\frac{11.2}{29.9} \right)$$

$$10.1 / 10.7 \left(+0.3 \right)$$

$$10.0 / 27.2'$$

3.1

$$27.6' / \frac{2.8}{10.3} \left(\frac{10.4}{27.8} \right)$$

$$3.1 / 10.3$$

$$3.5 / 26.2'$$

3.5

$$28.2' / 10.6$$

$$3.2 / 10.3$$

$$3.4 / 24.9' \left(\frac{11.1}{26.0} \right)$$

3.9

$$\left(\frac{11.04}{27.9} \right) 27.4' / \frac{3.7}{10.2}$$

$$3.5 / 10.4$$

$$3.4 / 26.0'$$

4.3

$$27.2' / \frac{4.2}{10.1}$$

$$4.0 / 10.3$$

$$3.1 / 26.6'$$

4.7

$$26.6' / \frac{4.9}{11.8}$$

$$4.3 / 10.4$$

$$3.2 / 21.8' \left(\frac{11.24}{25.8} \right)$$

5.0

$$\left(\frac{11.19}{26.8} \right) 26.6' / \frac{5.2}{11.8}$$

$$4.6 / 10.4$$

$$3.2 / 22.2'$$

5.2

$$25.6' / \frac{5.9}{11.3}$$

$$5.1 / 10.1 \left(+0.2 \right)$$

$$2.6 / 23.4'$$

5.5

$$\left(\frac{11.2}{25.4} \right) 25.2' / \frac{6.4}{11.1}$$

$$5.8 / 10.3$$

$$1.5 / 25.5'$$

Sta.	+	π	-	Grade	Ditch Rt
		944.73			
52	+30			38.9	6.80 37.95
	+56			38.7	6.7 37.8
B.M.	2.81	941.14	6.40	38.33	938.33
53	+21			37.7	
	+71			36.5	
54				35.8	
	+50			34.7	
T.P.	3.68	938.01	6.64	34.50	
55				33.9	
	+50			33.3	
56				33.0	
	+50			32.9	
57				33.1	
T.P.	2.11	940.49	4.70	33.38	

7/25/39
K.F.
L.C.
M.V.G.
M.B.

Cor. Rod

Lf

R

Rt.

$$5.1 \quad 283' / \frac{77}{R.00} \quad \frac{64}{-06} \quad \frac{89}{R.59/26.9}$$

$$6.0 \quad 258' / \frac{80}{R.00} \quad \frac{64}{-04} \quad \frac{15}{R.54/26.1'}$$

Spk. in P.P.S.E. Cor. off Lake Rd. to Rd. H²⁴

$$3.4 \quad 248' / \frac{45}{R.09} \quad \frac{40}{-06} \quad \frac{20}{H.4/29.8'}$$

$$4.6 \quad 27.6' / \frac{66}{R.00} \quad \frac{49}{-03} \quad \frac{24}{R.2/30.4'}$$

$$5.3 \quad 27.3' / \frac{73}{R.00} \quad \frac{54}{-01} \quad \frac{59}{R.4/25.8}$$

$$6.4 \quad 31.8' / \frac{89}{R.00} \quad \frac{64}{00} \quad \frac{94}{-3.0/21.0}$$

$$4.2 \quad 30.1' / \frac{62}{R.00} \quad \frac{41}{+01} \quad \frac{82}{-4.0/23.0'}$$

$$4.8 \quad 30.7' / \frac{68}{R.00} \quad \frac{49}{-01} \quad \frac{89}{-4.1/23.2'}$$

$$5.1 \quad 26.4' / \frac{55}{R.17} \quad \frac{52}{-01} \quad \frac{87}{-3.6/22.2'}$$

$$5.2 \quad 26.8' / \frac{52}{R.19} \quad \frac{52}{00} \quad \frac{92}{-4.0/23.0}$$

$$5.0 \quad 27.6' / \frac{47}{R.03} \quad \frac{48}{+02} \quad \frac{94}{-4.4/23.8}$$

7.11

Sta	+	π	-	Grade
		940.49		

57	+37			33.3
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	+62			33.4
--	-----	--	--	------

58				33.7
----	--	--	--	------

	+50			34.0
--	-----	--	--	------

59				34.3
----	--	--	--	------

	+50			34.6
--	-----	--	--	------

60				34.9
----	--	--	--	------

	+50			35.2
--	-----	--	--	------

61				35.5
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	+50			35.8
--	-----	--	--	------

T.P.	5.11	941.37	4.23	936.26
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62				36.0
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Gr. Rod

Lt

K

Rt.

7.2

$$25.6 / \frac{7.9}{16.13}$$

$$\frac{71}{101}$$

$$\frac{106}{-3.4} / 21.8'$$

7.1

$$25.0 / \frac{81}{16.10}$$

$$\frac{71}{00}$$

$$\frac{88}{16.13} / 23.6'$$

6.8

$$26.0 / \frac{7.3}{16.15}$$

$$\frac{68}{01}$$

$$\frac{69}{10.4} / 22.8'$$

6.5

$$26.2 / \frac{6.9}{16.16}$$

$$\frac{64}{10.1}$$

$$\frac{51}{11.4} / 29.8'$$

6.2

$$27.3 / \frac{6.1}{10.1}$$

$$\frac{6.2}{0.0}$$

$$\frac{5.6}{10.6} / 28.2'$$

5.9

$$28.8 / \frac{5.4}{10.5}$$

$$\frac{5.9}{0.0}$$

$$\frac{5.3}{10.6} / 28.2'$$

5.6

$$30.0 / \frac{4.1}{11.5}$$

$$\frac{5.5}{10.1}$$

$$\frac{6.1}{11.5} / 26.0'$$

5.3

$$30.4 / \frac{4.6}{11.7}$$

$$\frac{5.1}{10.2}$$

$$\frac{5.1}{10.2} / 27.4'$$

5.0

$$29.8 / \frac{3.6}{11.4}$$

$$\frac{4.9}{10.1}$$

$$\frac{4.8}{10.2} / 27.4'$$

4.7

$$30.0 / \frac{3.2}{11.6}$$

$$\frac{4.5}{10.2}$$

$$\frac{4.0}{11.6} / 24.4'$$

5.4

$$31.8 / \frac{3.0}{12.4}$$

$$\frac{5.2}{10.2}$$

$$\frac{6.1}{11.3} / 25.6'$$

Sta.	+	π	-	Grade
		941.37		
62	+50			36.2
63				36.3
	+50			36.3
64				36.3
	+38			36.1
	+75			36.1
B.M.	A.19		4.19	937.18 (937.18)
65				35.9
	+35			35.7
	+70			35.5
66				35.3
	+50			34.8

Gr. Red.

L.H.

Z

R.H.

$$5.2 \quad 32.0' / \frac{2.7}{12.5} \quad \frac{5.0}{10.2} \quad \frac{4.5}{10.7/28.4'}$$

$$5.1 \quad 31.2' / \frac{3.0}{12.8} \quad \frac{5.0}{10.1} \quad \frac{3.5}{11.2/30.2'}$$

$$5.1 \quad 31.0' / \frac{3.1}{12.0} \quad \frac{5.0}{10.1} \quad \frac{4.5}{10.4/28.2'}$$

$$5.1 \quad 29.2' / \frac{4.0}{11.1} \quad \frac{4.8}{10.3} \quad \frac{6.9}{12.07/29.4'}$$

$$5.3 \quad 30.8' / \frac{3.4}{11.9} \quad \frac{4.9}{10.9} \quad \frac{6.1}{12.12/28.4'}$$

$$5.3 \quad 30.4' / \frac{3.6}{11.7} \quad \frac{4.9}{10.9} \quad \frac{4.7}{10.6/28.2'}$$

Top N.E. Cor. Conc. Base of East Pillar 33' R.L. 64+91

$$5.5 \quad 31.0' / \frac{3.5}{12.0} \quad \frac{5.1}{10.9} \quad \frac{4.2}{11.3/29.6'}$$

$$5.7 \quad 30.6' / \frac{3.9}{11.8} \quad \frac{5.5}{10.2} \quad \frac{4.6}{11.1/29.2'}$$

$$5.9 \quad 29.2' / \frac{4.8}{11.1} \quad \frac{5.7}{10.2} \quad \frac{5.8}{10.1/27.2'}$$

$$6.1 \quad 27.0' / \frac{6.1}{10.0} \quad \frac{5.9}{10.2} \quad \frac{6.3}{11.8/26.6'}$$

$$6.6 \quad 28.2' / \frac{6.0}{10.6} \quad \frac{6.5}{10.1} \quad \frac{6.2}{10.9/27.8'}$$

Sta	+	π	-	Grade
		941.31		
67				34.3
T.P.	3.06	939.30	5.13	936.24
+50				33.7
68				33.1
+50				32.3
T.P.	4.52	936.58	7.24	932.06
69				31.5
+40				30.8
70				29.9
+50				29.1
71				28.3
+50				27.5
72				26.7

Ger. Rod.

Lt

R

Rt

7.1

$$28.6' / \frac{6.3}{10.8}$$

$$\frac{6.9}{10.2}$$

$$\frac{6.8}{10.8} / 28.6$$

Nail in T.P. L 1674

5.6

$$30.4' / \frac{3.9}{11.7}$$

$$\frac{5.9}{10.2}$$

$$\frac{3.9}{11.7} / 30.4$$

6.2

$$31.8' / \frac{3.8}{12.4}$$

$$\frac{6.1}{10.1}$$

$$\frac{6.2}{13.0} / 33.0$$

7.0

$$31.8' / \frac{4.6}{12.4}$$

$$\frac{6.8}{10.2}$$

$$\frac{4.8}{12.2} / 31.4'$$

5.3

$$31.4' / \frac{3.1}{12.2}$$

$$\frac{4.8}{10.5}$$

$$\frac{5.0}{10.3} / 27.6$$

5.8

$$30.2' / \frac{4.2}{11.6}$$

$$\frac{5.4}{10.4}$$

$$\frac{5.7}{10.1} / 27.2$$

6.7

$$30.0' / \frac{5.2}{11.5}$$

$$\frac{6.9}{10.3}$$

$$\frac{5.6}{11.1} / 29.2$$

7.5

$$26.8' / \frac{7.6}{11.9}$$

$$\frac{7.3}{10.2}$$

$$\frac{8.3}{15.12} / 25.4'$$

8.3

$$28.0' / \frac{7.8}{10.5}$$

$$\frac{8.2}{10.1}$$

$$\frac{7.4}{10.9} / 28.8'$$

9.1

$$24.6' / \frac{10.3}{10.8}$$

$$\frac{7.2}{10.1}$$

$$\frac{6.8}{12.3} / 31.6'$$

9.9

$$25.0' / \frac{10.9}{11.0}$$

$$\frac{10.1}{10.2}$$

$$\frac{6.0}{13.9} / 39.0$$

Sta	+	π	-	Grade
		936.58		

72	160			25.7
----	-----	--	--	------

73				25.1
T.P.	2.81	927.52	11.87	924.71

	150			24.3
--	-----	--	--	------

74				23.5
----	--	--	--	------

	150	Corr. (120/90.0)		22.8
--	-----	---------------------	--	------

75				22.2
----	--	--	--	------

Red.
pitch Lt.

	136			22.0
--	-----	--	--	------

8.0

	160			21.9
--	-----	--	--	------

7.9

T.P.	6.03	927.94	5.61	921.91
------	------	--------	------	--------

76				21.7
----	--	--	--	------

	150			21.7
--	-----	--	--	------

77				21.9
----	--	--	--	------

Gr. Rod.

LH

R

RH

10.7

$$25.0' / \frac{11.9}{R.10}$$

$$\frac{10.9}{.00}$$

$$\frac{6.0}{14.9 / 33.0}$$

11.5

$$24.0' / \frac{13.0}{R.0.5}$$

$$\frac{11.7}{-.02}$$

$$\frac{10.0}{11.5 / 30.0}$$

3.2

$$24.7' / \frac{5.2}{R.00}$$

$$\frac{3.4}{-.02}$$

$$\frac{5.2}{R.00 / 23.0'}$$

4.0

$$22.4' / \frac{6.0}{R.90}$$

$$\frac{4.3}{-.03}$$

$$\frac{8.4}{-4.4 / 23.8'}$$

4.7

$$20.7' / \frac{6.7}{R.00}$$

$$\frac{5.2}{-.05}$$

$$\frac{10.8}{-6.1 / 27.2'}$$

5.3

$$22.7' / \frac{7.3}{R.00}$$

$$\frac{5.7}{-.04}$$

$$\frac{6.8}{-3.5 / 22.0'}$$

5.5

$$24.8' / \frac{7.6}{R.04}$$

$$\frac{5.8}{-.03}$$

$$\frac{6.8}{R.03 / 24.4}$$

5.6

$$24.2' / \frac{7.8}{R.06}$$

$$\frac{5.8}{-.02}$$

$$\frac{6.6}{R.10 / 25.0'}$$

5.8
6.2

$$25.6' / \frac{6.9}{R.1.3}$$

$$\frac{6.2}{.00}$$

$$\frac{6.3}{10.0 / 27.0'}$$

6.2

$$25.0' / \frac{7.2}{R.10}$$

$$\frac{6.2}{.00}$$

$$\frac{7.4}{R.08 / 24.6'}$$

6.0

$$22.4' / \frac{7.8}{R.02}$$

$$\frac{6.1}{-.01}$$

$$\frac{8.1}{-2.1 / 17.2'}$$

Sta.	+	π	-	Grade
		927.94		
77	+45			22.3
78				22.9
	+43			23.4
	+56			23.6
	+87			24.0
79				24.2
	+50			24.8
80				25.5
	+11			25.6
	+46			26.1
	+52.79			26.2
B.M.			0.51	927.43

Gr. Rad.

Lt

L

Rt

5.6

$$22.7' / \frac{76}{2.00}$$

$$\frac{58}{-0.2}$$

$$\frac{82}{-2.6/202'}$$

5.0

$$22.7' / \frac{70}{2.00}$$

$$\frac{5.3}{-0.3}$$

$$\frac{83}{-3.3/21.6'}$$

4.5

$$23.0' / \frac{65}{2.00}$$

$$\frac{4.8}{-0.3}$$

$$\frac{78}{-3.3/21.6'}$$

4.3

$$25.6' / \frac{50}{2.13}$$

$$\frac{46}{-0.3}$$

$$\frac{77}{-3.4/21.8'}$$

3.9

3.7

$$23.8' / \frac{53}{2.04}$$

$$\frac{41}{-0.4}$$

$$\frac{57}{2.00/22.0}$$

3.1

$$23.8' / \frac{47}{2.04}$$

$$\frac{32}{-0.3}$$

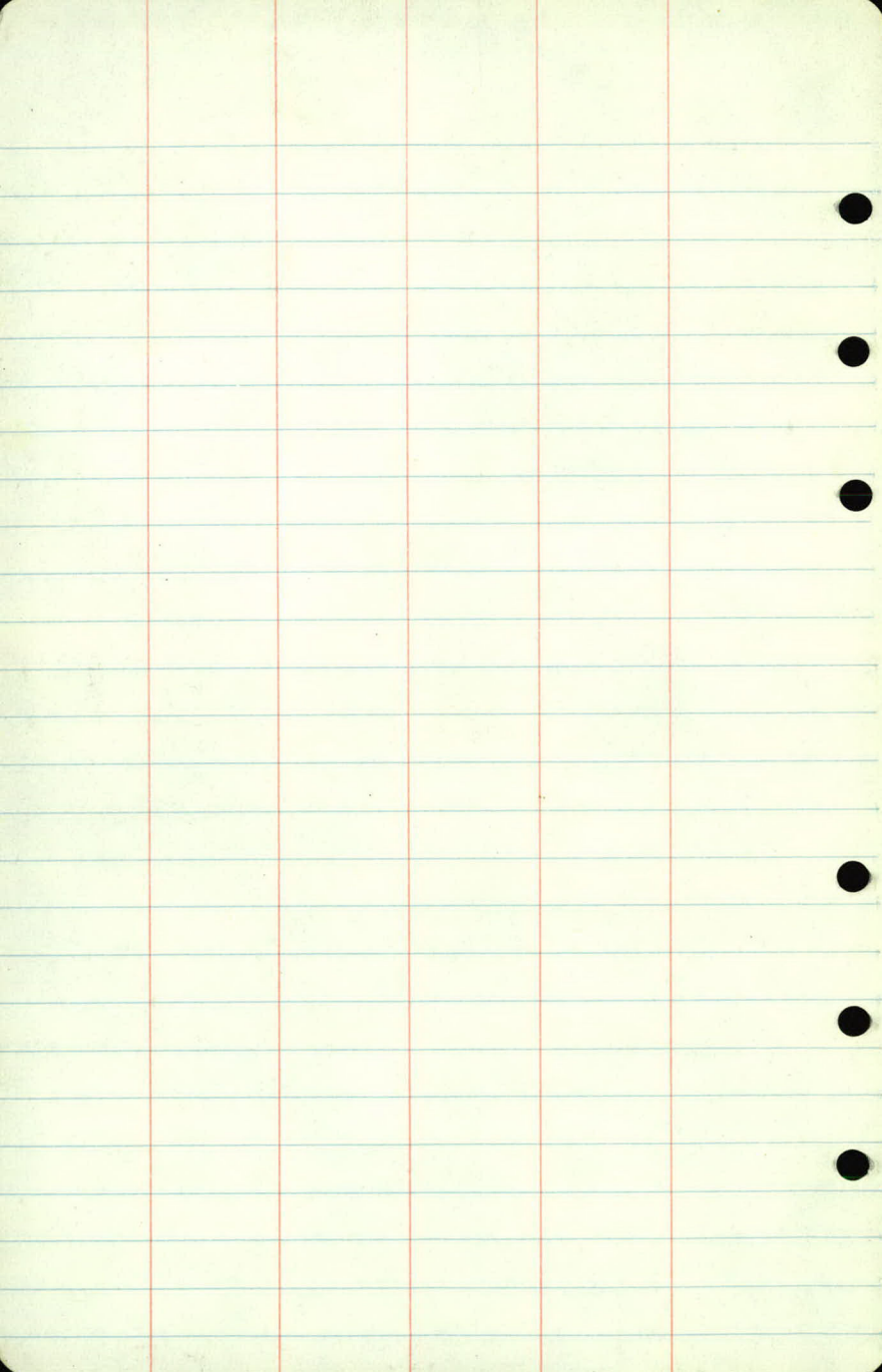
$$\frac{44}{2.07/20.4}$$

2.4

$$\frac{2.8}{-0.4}$$

$$\frac{39}{2.05/29.0}$$

Spk. in Light Pole 3. Eagle Blk W. 96 Rd "H" 20



slope stakes
Otter Lake Rd.
142 to 145

Sta	+	X	-	Grade
B.M.	9.60	947.93		(938.33)
142				44.1
+50				43.5
143				42.6
+50				41.9
150				41.5
144				41.1
144 +05				41.0
+40				40.3
+75				39.4

$$\begin{array}{r}
 47.7 \\
 8.9 \\
 \hline
 9.5
 \end{array}$$

Gr. Rod.

Lk

R

Pt.

Sph. in R.R. S. E. Cor. Otter Lake Rd. P.C. Rd. "H" 2nd

3.8

 $\frac{2.1}{4.7/33.0}$

4.4

 $\frac{33.0'}{R.00} \frac{6.0}{R.00}$ $\frac{0.9}{13.5/33.0}$

5.3

 $\frac{33.0'}{R.11} \frac{5.7}{R.11}$ $\frac{1.9}{13.5/33.0}$

6.0

 $\frac{33.0'}{R.13} \frac{6.2}{R.13}$ $\frac{4.3}{11.7/33.0}$

6.4

 $\frac{33.0'}{R.05} \frac{5.9}{R.05}$

6.8

 $\frac{6.8}{R.15/33.0}$

6.9

 $\frac{33.0'}{R.06} \frac{4.3}{R.06}$

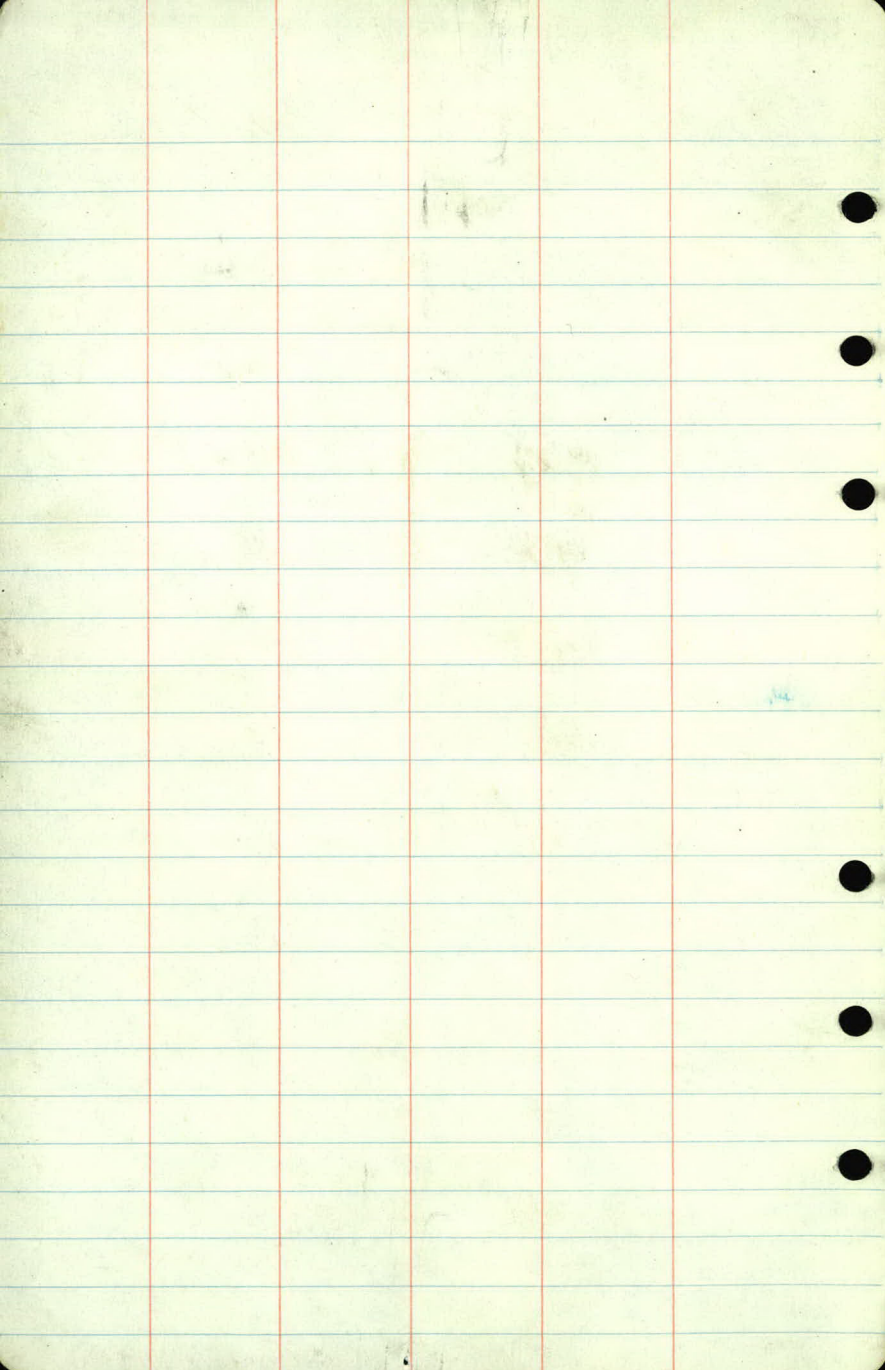
R.15/33.0

7.6

 $\frac{33.0'}{R.04} \frac{4.2}{R.04}$ $\frac{7.8}{R.13/33.0}$

8.5

 $\frac{33.0'}{R.08} \frac{4.7}{R.08}$ $\frac{8.5}{R.15/33.0}$



Slope stakes

Hv

Sta 36+00 to 46+00

Restaking using Crown of
Road

Stg + π - Elev

36+00

+50

37

+50

38

+50

39

+50

40

+50

41.

+50

$$\begin{array}{r} L+ \\ 3.7 \\ C \quad 0.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ DC1.8 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 5.3 \\ DC1.9 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ DC1.4 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 5.1 \\ DC1.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 5.7 \\ DC1.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC1.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC1.8 \\ \hline 26.5 \end{array}$$

$$\begin{array}{r} 5.8 \\ CO.2 \\ \hline 27.4 \end{array}$$

$$\begin{array}{r} 5.6 \\ CO.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ DC1.4 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 6.2 \\ DC0.8 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} L \\ 4.6 \\ 8.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ 8.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ 8.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ 8.0 \end{array}$$

$$5.3/8.0$$

$$5.4/8.0$$

$$5.4/8.0$$

$$5.3/8.0$$

$$6.0/8.0$$

$$5.6/8.0$$

$$5.3/8.0$$

$$5.0/8.0$$

$$\begin{array}{r} R+ \\ 4.3 \\ C.08 \\ \hline 27.5 \\ 6.1 \\ \hline DC0.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 5.8 \\ DC1.1 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 5.8 \\ DC1.2 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC1.8 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 4.1 \\ DC1.3 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 6.4 \\ DC1.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ DC1.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ C.0.7 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 5.3 \\ CO.3 \\ \hline 27.6 \end{array}$$

$$\begin{array}{r} 4.0 \\ DC0.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 7.3 \\ F2.3 \\ \hline 19.6 \end{array}$$

Sta + π - Elev,

42,

+50

43

+50

44

+50

45

+50

46

+40

+70

47

Lt

Z

R4

$$\begin{array}{r} 61 \\ R07 \\ \hline 244 \end{array}$$

$$\begin{array}{r} 48 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 72 \\ F2.4 \\ \hline 178 \end{array}$$

$$\begin{array}{r} 5.7 \\ R05 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 42 \\ \hline 00 \end{array}$$

$$\begin{array}{r} 69 \\ F27 \\ \hline 264 \end{array}$$

$$\begin{array}{r} 47 \\ R10 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 37 \\ \hline 1.0 \end{array}$$

$$\begin{array}{r} 61 \\ F2.4 \\ \hline 178 \end{array}$$

$$\begin{array}{r} 41 \\ R10 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 31 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ R00.0 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 2.8 \\ R01.2 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 1.5 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 45 \\ R00.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 5.5 \\ C0.6 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline 00 \end{array}$$

$$\begin{array}{r} 48 \\ R01.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 2.5 \\ C2.7 \\ \hline 32.4 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 44.8 \\ C0.8 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} B.T. \\ \hline 10.2 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 47 \\ R01.8 \\ \hline 26.6 \end{array}$$

$$B.T. 9.1$$

$$\begin{array}{r} 3.7 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 00 \\ C3.7 \\ \hline 33.0 \end{array}$$

$$B.T. 9.0$$

$$\begin{array}{r} 4.8 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 1.4 \\ C5.4 \\ \hline 33.0 \end{array}$$

$$P. 1.0$$

$$\begin{array}{r} 6.7 \\ \hline 00 \end{array}$$

$$\begin{array}{r} 2.3 \\ C4.4 \\ \hline 33.0 \end{array}$$

$$B.T. 8.8$$

$$\begin{array}{r} 6.5 \\ \hline 00 \end{array}$$

$$\begin{array}{r} 3.0 \\ C3.3 \\ \hline 33.0 \end{array}$$

Sta + π - Elev

47+50

48

+50

49

L+

L

R+

B.T/8.7

6.5
0.0

7.2
201.4
25.8

B.T/86

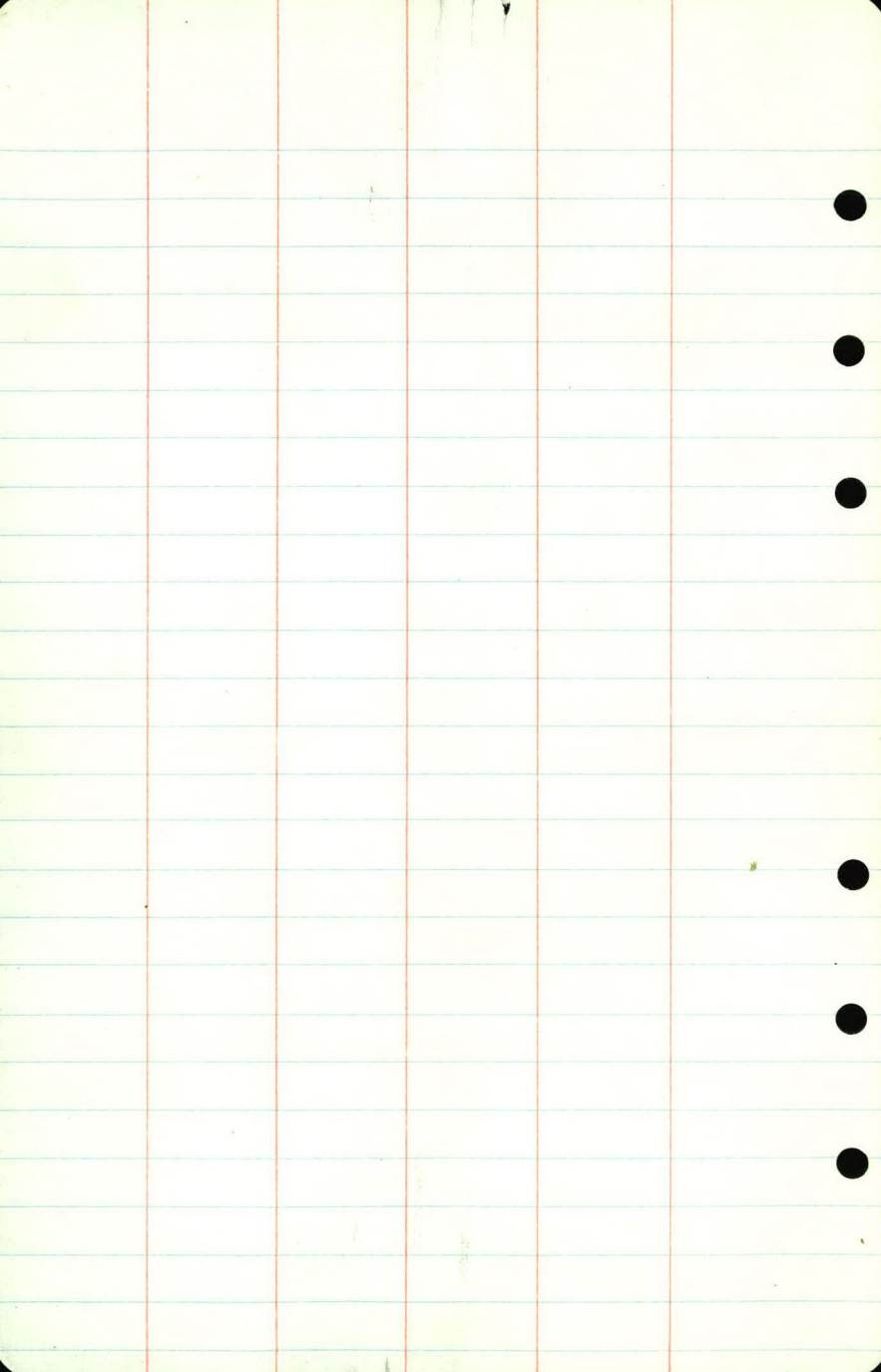
6.9
0.0

7.8
201.0
25.0

7.3
0.0

8.8
201.6
26.0

7.6
0.0



Slope stakes

COUNTY RD. H²

Otter Lake Rd to
Bold Eagle Blvd.

Sta.	+	π	-	Elev.
B.M.				938.33
52+89.60				38.4
53+13				37.8
+21				37.7
+71				36.5
54				35.8
+50				34.7
55				33.9
+50				33.3
56				33.0
+50				32.9
57				33.1
+37				33.3

Gr. Rod.	Lt	&	Rt.
Spk. P.P.	S.E. Cor.	Officer	Lk. Rd & Co. Rd H ²

57+62

33.4

58

33.7

+50

34.0

59

34.3

+50

34.6

60

34.9

+50

35.2

61

35.5

+50

35.8

62

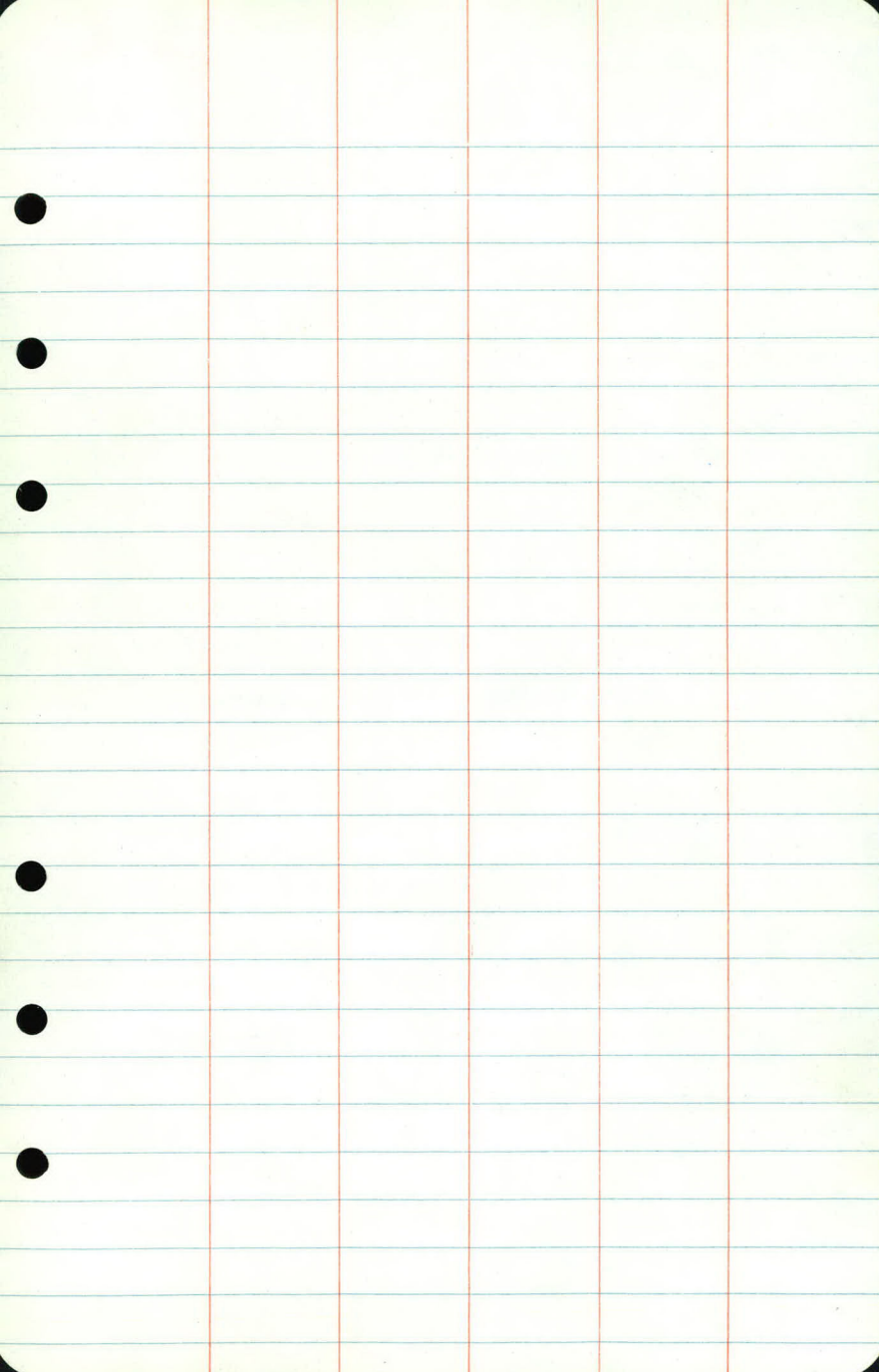
36.0

+50

36.2

63

36.3



63 36.3

+50 36.3

64 36.3

+38 36.1

+75 36.1

65 35.9

+35 35.7

66 35.3

+50 34.8

67 34.3

+50 33.7

59' 10" 64.91

68

38.1

+50

32.3

69

31.5

+40

30.8

70

29.9

+50

29.1

71

28.3

+50

27.5

72

26.7

+60

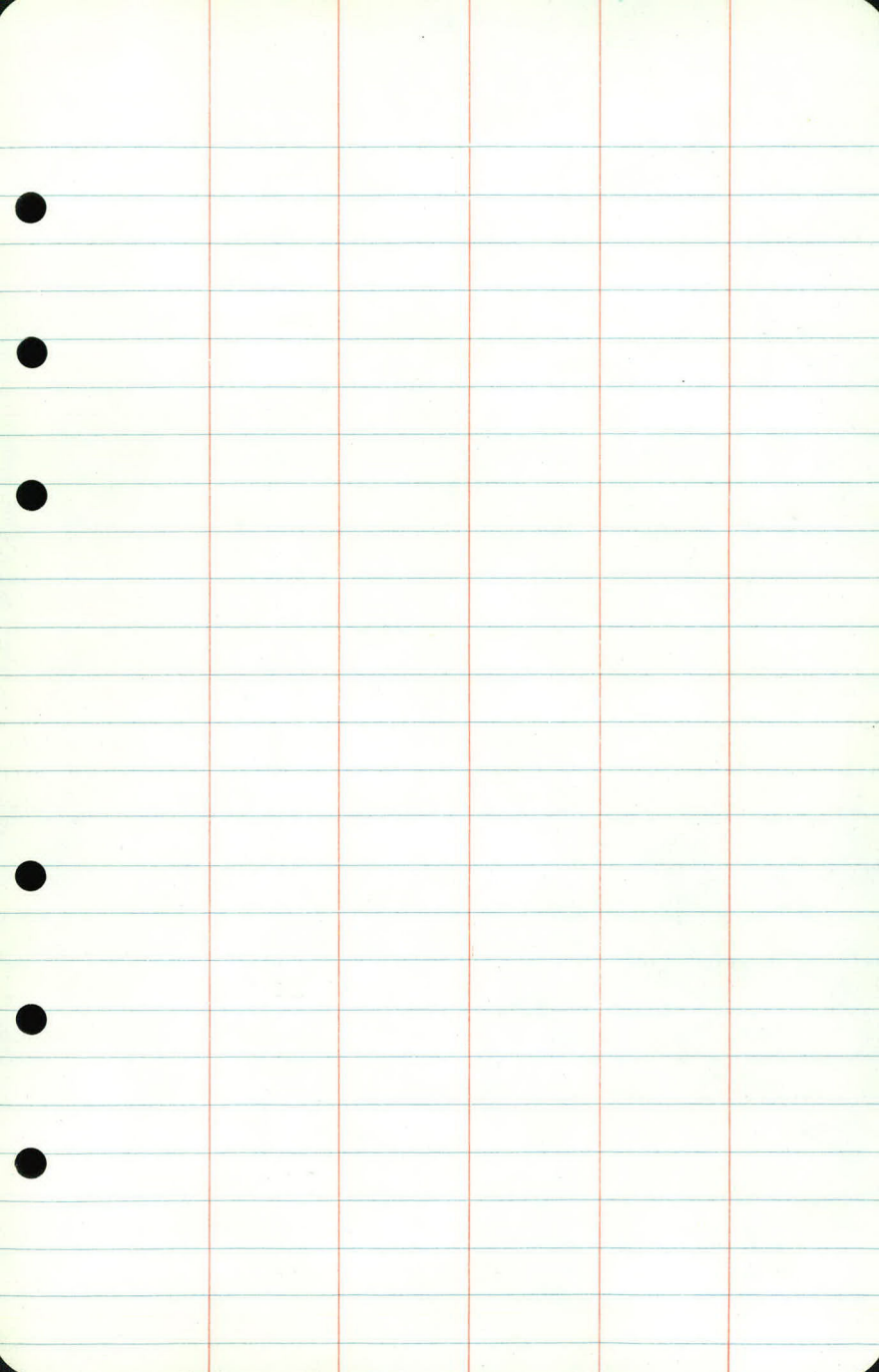
25.7

73

25.1

+50

24.0



74 23.5

+50 22.8

75 22.2

+36 22.0

76 21.7

+50 21.7

77 21.9

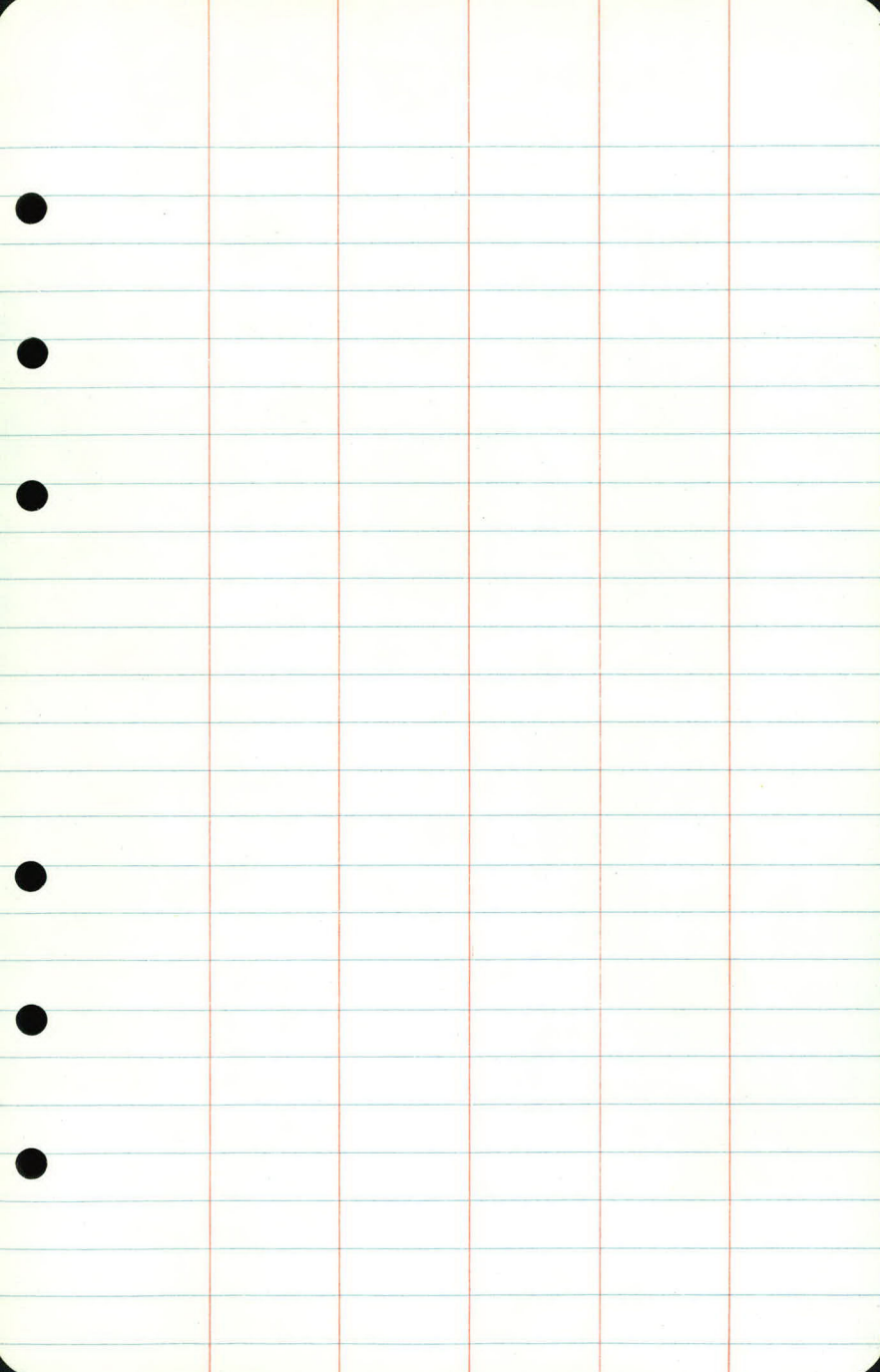
+50 22.3

78 22.9

+43 23.4

+56 23.6

+87 24.0



79		24.2
+50		24.8
80		25.5
+11		25.6
+46		26.1
+56.79		26.2
B.M.		927.43

Spk Light Pole Bald Eagle - H²

