

Bk. 58

Dr. 16

OFFICE OF COUNTY ENGINEER
HAMSEY CO. MINN.

Plan

Survey

Little Canada Rd.

From Rise Str. To Edgerton St.

Road Acc't. No. 7

Date Filed 6-11-41

Dr. 16
File Bk. 58

PLAN SURVEY

LITTLE CANADA RD

From
Rice to Edgerton

Completed - 4-3-'41

Index:

Alignment - 1-8

Topog. - 9-22

Bench Levels - 23-24

X Sections - 25-43

Profile Spec. Ditch 44-47

Party:

R. Pease

A. Moeschter

L. Goldberg

C. Fawer

X

Sta	Pt.	Angle Lt. Rt.	Mag. Calc. Data
-----	-----	------------------	--------------------

+14.11	P.T.	$1^{\circ}08\frac{1}{2}'$	
12		$1^{\circ}04'$	
+50		$0^{\circ}49'$	$\Delta 2^{\circ}17' \text{ Rt.}$
11		$0^{\circ}34'$	$D 1^{\circ}$
10+99.96	P.I.	$2^{\circ}17'$	$T 114.18$
+50		$0^{\circ}19'$	$L 228.33$
10		$0^{\circ}04'$	$R 5729.65$
9+85.78	P.C.		

$N 88^{\circ} E.$

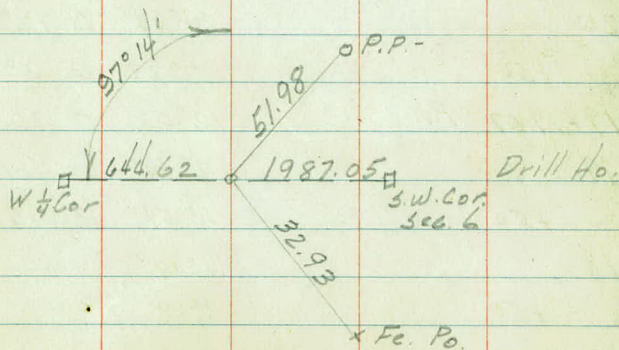
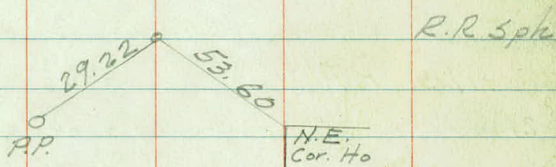
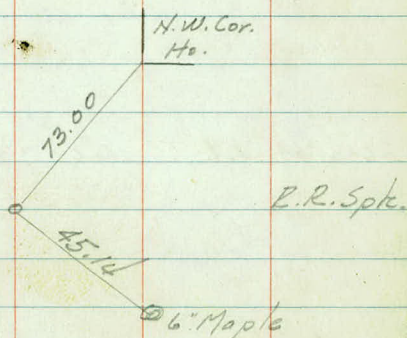
$582^{\circ}08'E$

4+52.30	P.I.	$0^{\circ}38'$
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$582^{\circ}46'E$

0+00 $\frac{1}{2}$ Rice St. - (W. Line Sec. 6

Note: P.I. Placed
at apparent
Land Line Xing L.



Sta.	Pt.	Angle Lt. Rt.	Mag. Data.	Calc.
------	-----	------------------	---------------	-------

568°12'E

32+35.08	P.I.	0°24' - 32+52 = 25'	W.H.C. Notes - 10-52	
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0.27 short to Boat Spike

S 76° E

24+65.88	P.O.T.	on N & S $\frac{1}{4}$ Line		
----------	--------	-----------------------------	--	--

23.85
27

567°40'E

+19.13	P.T.	6°01' $\frac{1}{2}$		
--------	------	---------------------	--	--

21		5°44'		
----	--	-------	--	--

+50		4°59'		
-----	--	-------	--	--

20		4°14'	Δ 12°03' Rt.	
----	--	-------	---------------------	--

+50		3°29'	D 3°	
-----	--	-------	------	--

19+19.07	P.I.	12°03'	T 201.61	
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19		2°44'	L 401.67	
----	--	-------	----------	--

+50		1°59'	12 1910.08	
-----	--	-------	------------	--

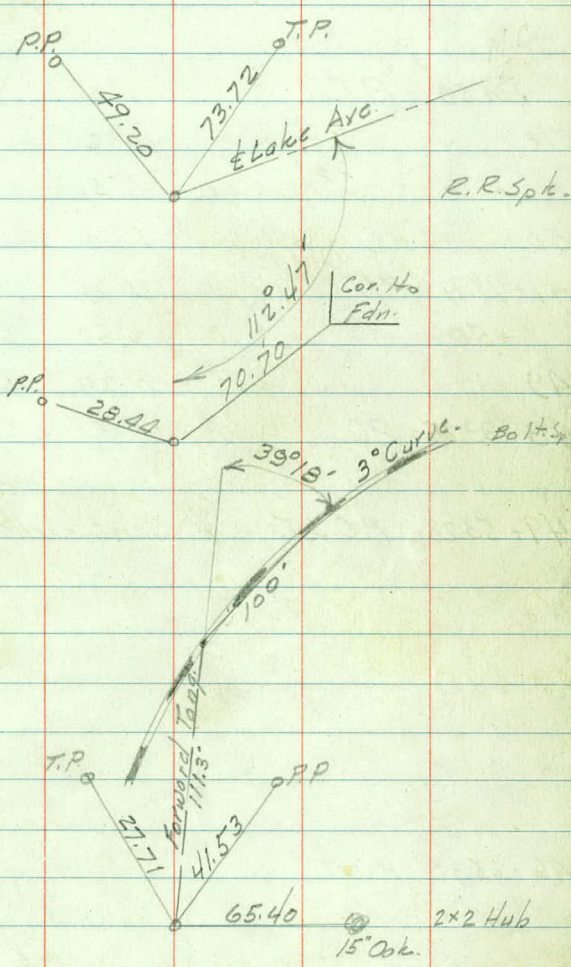
18		1°14'		
----	--	-------	--	--

+50		0°29'		
-----	--	-------	--	--

17+17.46	P.C.			
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S 89°30' E

579°51'E



X

Sta.	Pt.	Angle	Mag.	Colo.
		Lt. Rt.	Data	

+01.58	P.T.	10°25'		
51+		10°20'		
+50		7°50'	Δ 20°50' Rt.	
50		5°20'	D 10°	
49+98.71	P.I.	20°50'	T 105.46	
+50		2°50'	L 208.33	
49		0°20'	R 573.686	
48+93.25	P.C.			

49+53.28 P.O.S.T. - E Centerville Rd.

46+25.32 P.O.T.

S 76°30'E

347°22'E

321.895

S.W.
Cor. Ho.

80.32

56.43

N.E. Cor.
Ho.

R.R. Spk

Approx. 27.
68°55'

N.W. Cor.
Ho.

79.08

68.48

P.P.

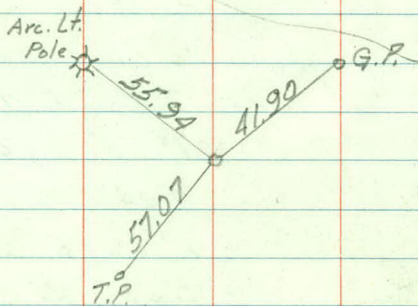
Spike

Sta.	Pt.	Angle Lt. Rt.	Mag. Data.	Calc. N 62° 16' E
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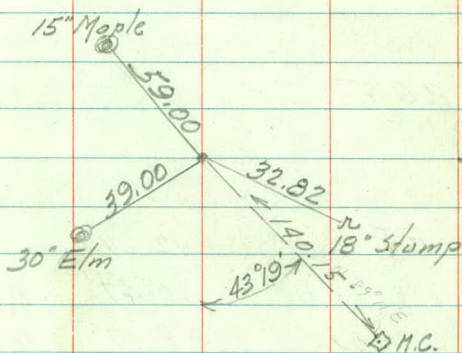
				N 48° 30' E
1.17 +67.07	P.T.	35° 11'		
+50		30° 55'	Δ 70° 22' Lt.	
+25		24° 40'	D 50°	
61 + 09.75	P.I.	70° 22'	T 83.41	
61 1.08		18° 25'	L 140.73	
+75		12° 10'	R 118.31	
+50		5° 55'	L.C. 136.34	
60 + 26.34	P.C.			

58 + 69.50	P.O.T.			
				S 47° 22' E
			S 33° E.	

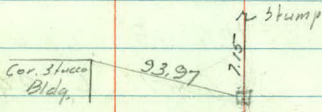
53 + 88.16 P.O.T.



R.R. Spk.



Spk



Grain Mon. M.C.

Sta.	Pt.	Lt.	Angle	Rt.	Mag	Calc
					Data	

+32.35	P.T.			3° 42'		
72				3° 23'		
+50				2° 53'		
71				2° 23'	Δ 7° 24' Rt.	
+50				1° 53'	D 2°	
70+47.63	P.I.			7° 24'	T 185.28	
70				1° 23'	L 370.00	
+50				0° 53'	R 2864.93	
69				0° 23'		

68+62.35 P.C.

69+05.35 P.O.S.T.

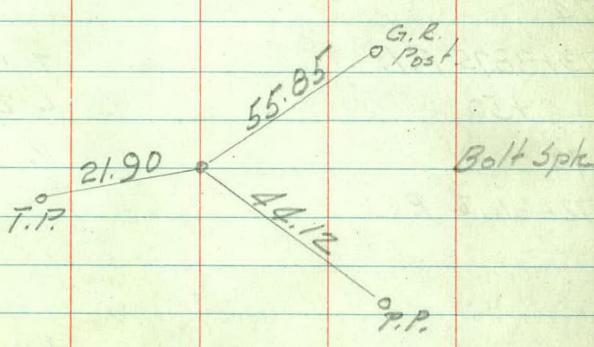
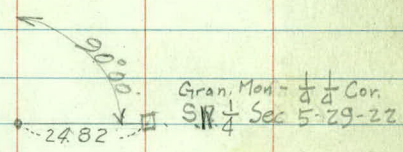
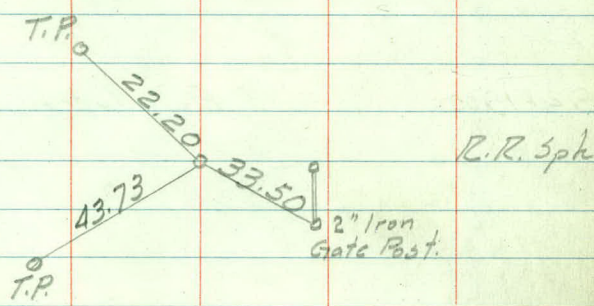
+82.30 ⁰⁴	P.T.			12° 24'		
+50				10° 47'	Δ 24° 48' Rt.	
65				8° 17'	D 10°	
64+60.43	P.I.			24° 48'	T 126.13	
+50				5° 47'	L 248.00	
64 ⁰⁵				3° 17'	R 573.686	
+50				0° 47'		

63+34.30 P.C.

225.585

240.68

291.264



Sta.	Pt.	Angle Lt. Rt.	Mag Calc Data.
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B2+19.00 ± Edgerton

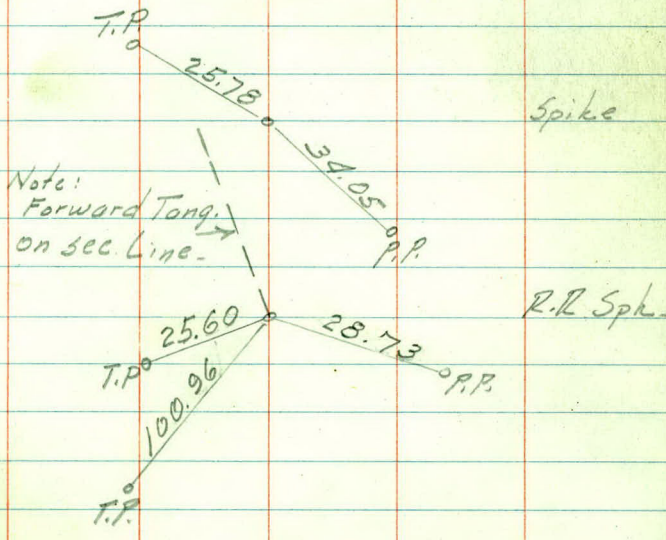
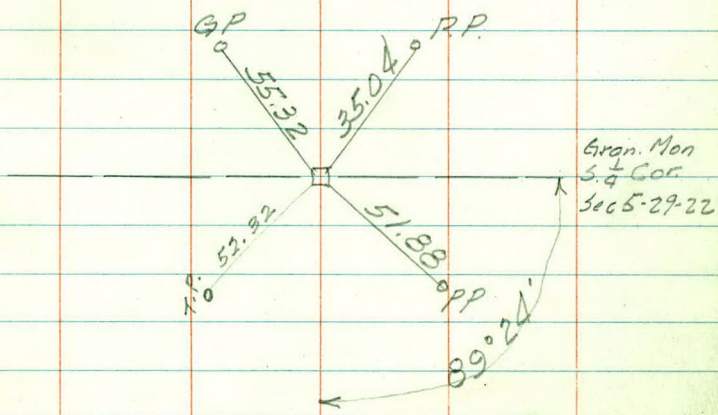
N 81°30'E

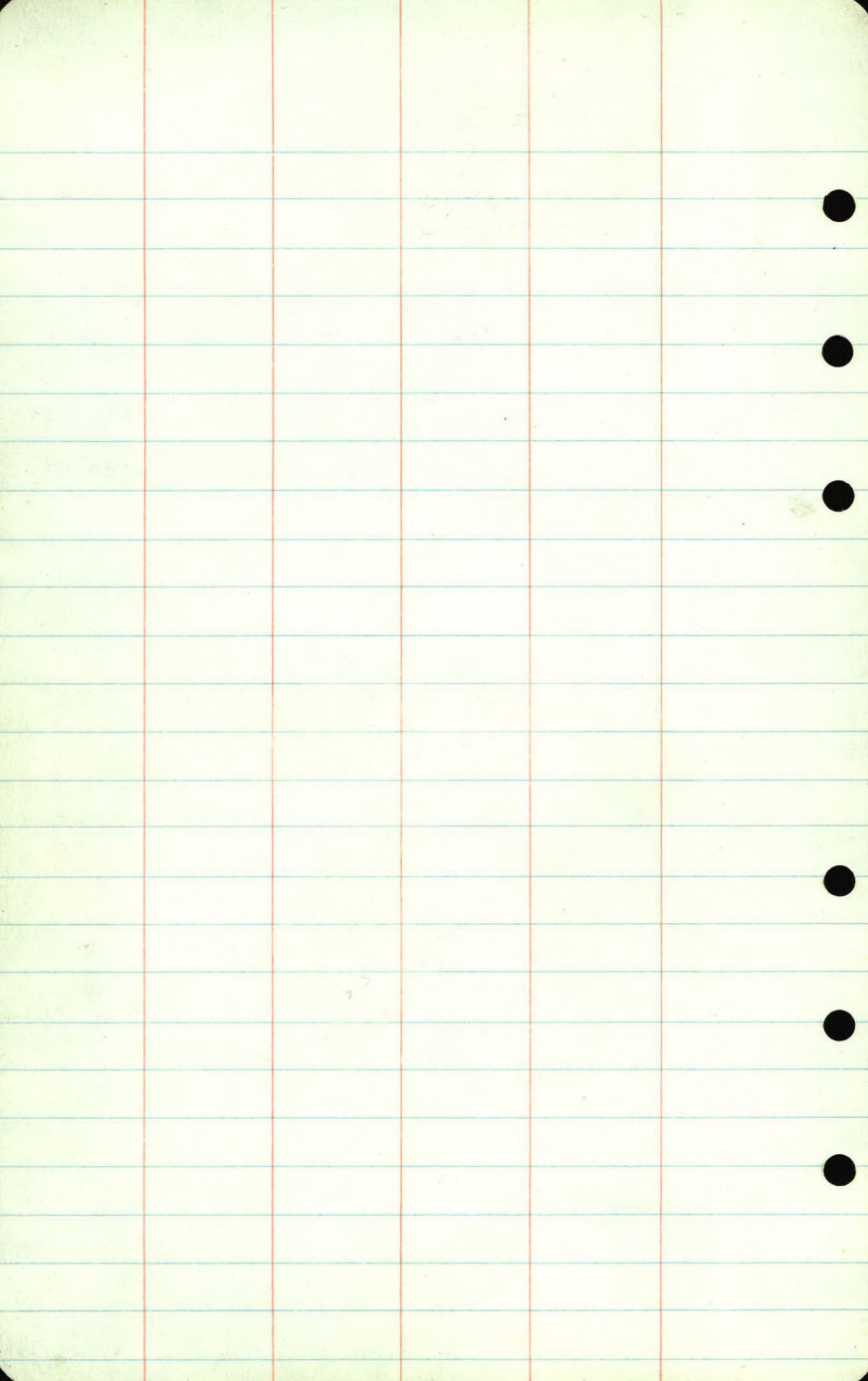
N 89°22'E

+16.15	P.T.	2° 33'	
75		2° 23.4'	
+50		1° 53.4'	Δ 5° 06' Lt.
74		1° 23.4'	D 2°
73+88.75	P.I.		T 127.60
+50		0° 53.4'	L 255.00
73		0° 23.4'	R 2864.93
72+61.15	P.C.	0° 00'	

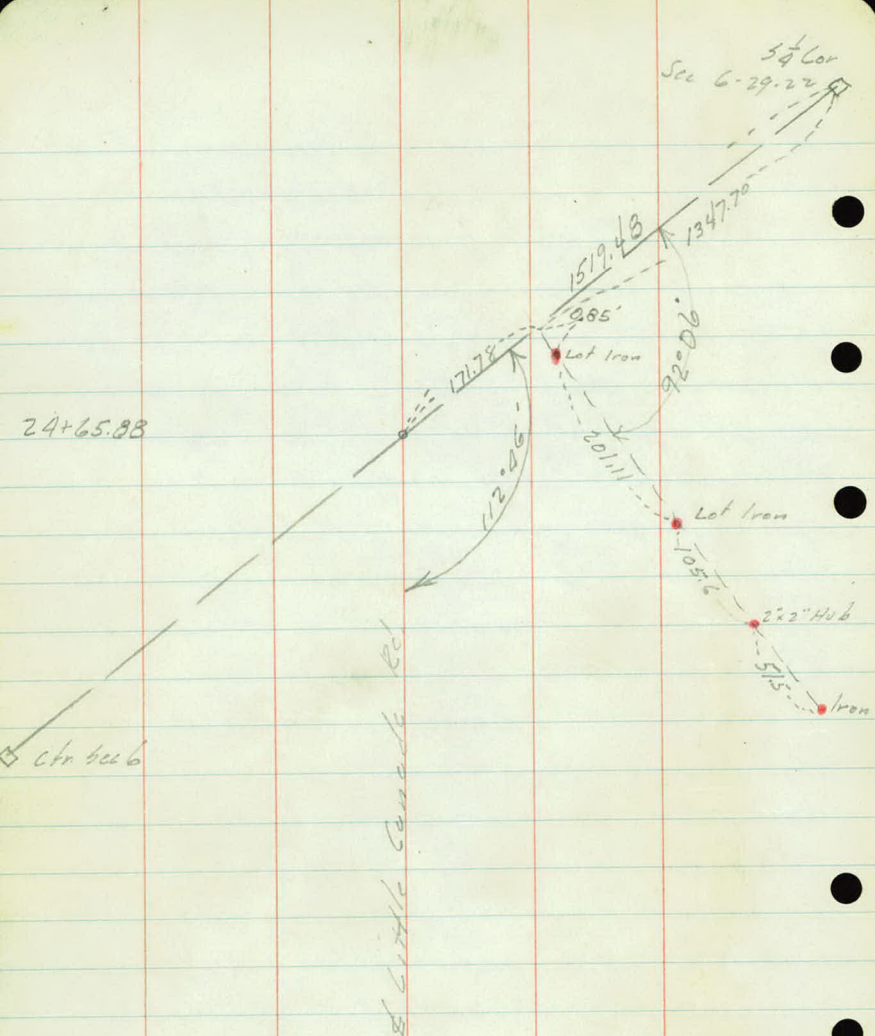
N 86°15'E

N 85°32'E



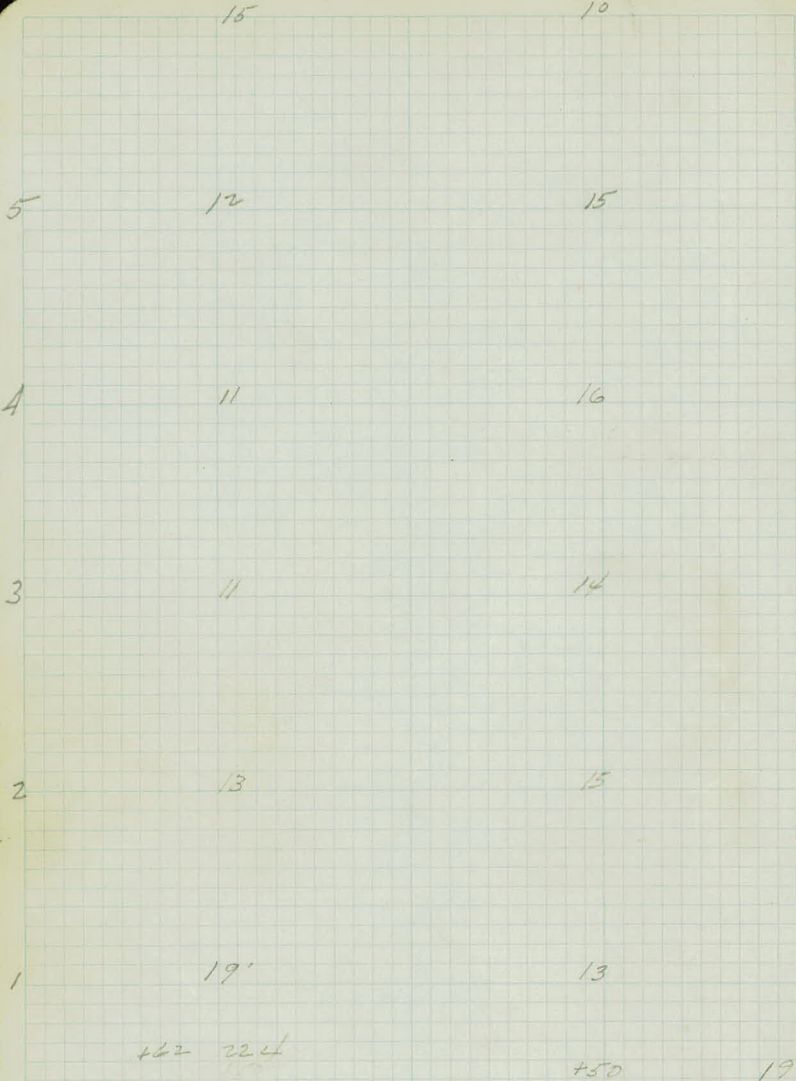


LITTLE CANADA RD
LAND TIES



Topography

LITTLE CANADA ROAD



+11.0 Edge Rvc.

-13.0 Edge Pave.

-31 Fc x s e

+57 Ditch 26
+35 Stump 26

2' Bottom
n

+96 Stump 33

+56 Field Ent
18" x 12" C.M. 25'

+48 Stump 33
+40 T.P. 20

+38 P.P. 26
+22 Ent

+84 B.E. 32
+82 B.E. 29

2' Ditch

+36 Ditch 27'
+26 Lilac 36
+04 Cor. Ho 46'
+00 Ent
12" x 22" C.M. 28'
+89 Maple 34.50
+75 End Gult
+74 T.P. 22

+30 Elm 34
+15 Edge 3' Conc 253
+01 Elm 34
+87 P.P. 25
+84 Plum 46
+70 Maple 43

3' Conc. Wall

+47-2 Elms 35-50

+23 T.P. 21

+00 Beg. Cult

+37 P.P. 24

+63 Oak 32'

+27 Oak 32'

+26 T.P. 21

+20 Cor Bldg. 57

+02 Cor. Gar. 67
+95 Elm 30
+87 Elm 30
+76 Cor. Ho 48'
+66 Cor. Conc 40

1.5' (Joint)
75°

+87 Cor Bldg - 61'

+40 Cor. Ho 44
+35 Cor. Conc 37.0

+30 P.P. 43

+24 Beg. Rad 50

RICE ST.
24" Conc. Pavement

Cultivated

		20	Lake 125
12	4		20 Lake 125
	8		16
11	10	+05-18" x 40" C.M.	18 +06 Lot Iron-35.2
	12		11
10	15		9
9	17		10
8	17	+21-12" x ? Perf. C.M.	17
			11
7	12		10
		+72 18" x 42" V.I.	
6	15		10

+25 Ent. 100
+14 Oak 36
+100 Ent. 39

+75 Ent. 11
+69 P.P. 24

+27 Lot Iron 63

+02 End 18" C.M. 14
+94 Lot Iron 32
+90 Oak 36
+72 Ent. 15" x 20" C.M. 18

+09 Arc Lt. Pk. 35

+63 End Cult. 32

+18 P.P. 31

+76 Beg. Cult. 28
+66 Ent.
+56 End Hedge - B.E. 37
+39 B.E. 37
+22 B.E. 37
+16 Beg. Hedge 37
+08 Cor. Ho. 62
+07 B.E. 38
+00 End Cult.

+61 End 18" W. 20"

+27 P.P. 30
+25 Beg. Cult.

Uncult.

Uncultivated

Rasberries

Garden

Yard

Yard

Yard

+00 Twin 40
+94 Oak 38
+91 Oak 49
+89 Stump 42
+75 Oak 46
+72 Oaks 40-50
+43 Oak 41
+24 Stump 42
+13 Oak 48
+95 Oak 50

+72 T.P. 25

+50 Cor. Ho. 64

+27 Cor. Ho. 68

+05 X.Fe. 31

+10 M.H. 28

+00 Rca. Tie Fe.

+98 End 18" C.M. 26

+87 Ash 34

+72 Maple 33

+47 Stump 30

+44 Ash 29

+28 Maple 23

+15 Ash 26

+02 T.P. 14

+83 B.E. 24

+73 Ent.

+18" x 30" C.M. 15

+63 B.E. 24

+41 Cedar 50

+36 Cor. Ho. 67

+02 Bush 32

+96 Birch 40

+75 End Cult.

+52 T.P. 15

+08 Stump 26

+03 T.P. 18

+82 End 18" W. 18

+75 Stump 32

Cultivated

24
26
15F

96-18" C.M.

25ST
43

32.5
15F 16"

16 - 38

19 - 39

19 - 42

20 - 44

18 - 42 Lake 153

16 - 41

16 - 40 Lake 132

+50 Ent

9 - 35 Lake - 122

6 - 32 Lake - 107

3 - 29 Lake 130

24 Lake 125

+00 Ent (12)
 +82 End Fe 49
 178 T.P. 42

+59 P.P. 01
 +37 R.R. Tel. P. 31

2.5' W. 20' 15F +40 Conc. Walk 47
 24' +30 Cor. Ho - 77

+00 End Cult 12

+05 Beg. Fe. 54

+00 Cult 10

Yards

128 T.P. 54

+50 Cult 07

+72 P.P. 02
 +63 Cor. Ho 86
 +42 Cor. Ho 81
 +40 End Hedge 47

+00 Cult 12

Cultivated

15' 19' 177 Cor. Ho 66
 123' 157 Beg. Hedge 45
 15F 157 Cor. Ho 56
 38' 142 Cor. Ho 54
 137 T.P. 47

+00 Cult 16

+72 P.P. 05

Cultivated

+00 Cult. 34

102 T.P. 40

ROUND LAKE

+00 Cult. 28

+72 P.P. 14

+38 Oak 23
 +28 Oak 29
 +10 Begin Cult 33

15F +46 Oak 49
 +29 T.P. 33
 +22 Oak 50
 +17 Oak 50
 +09 Cor. Ho 77
 22 +07 Steep 48

26

12

11

25

10

12

24

12

12

+46.15" x 40' C.M.

+50 End 15' 23

+93 Stump 32

+92 RE 50

+83 RE 25

23

7

15

22

7

15

2

22

21

5 - 26

20

10-20

+35.3 R.R. End 15' E

+27.7 R.R. End 15' E

16-38

+86 B.E. 20

+61 P.P. 27

+100 B.E. (13) 39
+91 B.E. 35
+87 B.E. 29
+80 B.E. 29
+67 Twin B.E. 30

+18 B.E. 38
+107 T.P. 18
+101 B.E. 43
+83 Ent.
+76 End Fe. 24
+73 Cor. to 27

+37 Cor. Steps 35
+27 B.E. 35
+18 Cor. Ho. 46
+10 B.E. 38
+81 B.E. 35
+79 R. Cor. 29
+70 Rgc Tie Fe.
+57 Ent.
+51 Rgc Tie Ent.
+34 Ash 35
+22 T.P. 24
+14 Apple 31
+06 Apple 27
+02 Apple 33
+99 Stump 28
+90 Plum 22
+88 2 Plum 24-27

+81 P.P. 25

+50 Rgc Tie Ditch
+43 End 15" & 17
+43 2' Ditch -17

+18 Ent.
12"x20' C.M. 18'

+73 Ash 34

+46 Lot Iron 133.2

+11 Ent.
+02 Rgc Tie Barr.
+00 Cor. Barr. 38
+88 P.P. 23
+87 Will 46

+66 Elm 43

+48 Fir 41
+28 Cor. Con. Walk 30 15F
+21 Cor. Bldg 40
+15 Fir 42

+99 Elm 42
+82 Elm 41
+67 Elm 40
+65 Rgc Barr. 37

+49 Stump 44

+86 Arc. Lt P. 13

+85 T.P. 31

+19 Oak 36

+48 T.P. 38'

+44 Plank Xing 7
+38 Plank Xing 10
+34 R.R. Tel P. 55

11

10

33

10

15

32

10

10

+ 96 T.P. 18
+ 96 Will 34

31

11

11

30

10

11

29

10

12

+ 92 Rye Tie Cord

28

10

13

27

12

11

12

12

40

13

12

39

13

13

38

12

11

+ 98 Ent

+ 91 Fc Cor 33'

37

12

11

36

35

11

12

34

11

10

16

7

47

15

8

46

13

10

45

12

11

44

11

11

43

10

11

42

12

12

41

12

12

+102 T.P. 29

Uncultivated

+106 T.P. 28

+66 Stump 37

+41 T.P. 28

+40 Stump 36

+76 T.P. 28

+45 T.P. 27

Uncultivated

+80 Ent

+18 T.P. 26

+16 Stump 35

+56 Stump 36



Cultivated

+76 Ent

+53 Cedar 29

+45 P.P. 20

+39 Elm 29

+20 Lilac 28

+100 End Hedge 30

+89 Cor. Ho 45

+73 Beg. Hedge 31

+65 B.E. 40

+60 P.P. 25

+43 Stump 33

+31 B.E. 33

+21 B.E. 34

+86 Stump 33

+37 Stump 33

+77 Field Division

+70 B.E. 26

+55 P.P. 26

+75 B.E. 30

+08 Plum 32

+83 Maple 31

+62 P.P. 26

+31 Plum 33

+25 Plum 35

+17 Plum 34

45-20

Swamp 121

44-19

54

46-19

+97 stump on £

Swamp 123

44-16

+19 T.P. on £

53

40-12

Swamp 149

33-4

52

26

Swamp 186

51

13

13 Swamp 224

12

16

50

11

14

+70 Ed 24

+97 Ent.

+80 Cor. Ho 45

53

12

49

23

8

48

16

7

+64 Cor. Ho. 100 29
 +52 Cor. Ho 98
 +50 Ent.
 +44 T.P. 14 21
 +24 Stump 02
 +16 Cor. Ho. 91
 +00 Cor. Ho. 87
 +00 P.P. 58 20

+38 Cor. Bldg 79 49 11
 25 ST Joint
 +05 Cor. Bldg 75 47 33

+93 P.P. 38
 +67 B.E. 44
 +49 B.E. 39

+00 B.E. 29
 +83 Cor. Ho. 41
 +69 Cor. Ho. 39
 +59 Ent.
 +36 B.E. 32

+73 Arc Lt. Po. 31
 +66 G.P. 36

+20 End Rod 55

+88 Elm 44
 +87 T.P. 30
 +80 Elm 37
 +68 Beg Rod 15'

+14 T.P. 31

+10 3 Stumps 20-24-2
 +09 2 Stumps 18-21
 +06 2 Stumps 21-29
 +99 Stump 38
 +97 Stump 41

+40 3 Stump 37
 +39 B.E. 07
 +29 B.E. 12
 +20 B.E. 28
 +10 B.E. 27
 +01 B.E. 40

+50 Stump 20

+23 Stump 25

+74 T.P. 17
 +73 B.E. 39
 +50 Stump 36
 +47 B.E. 43
 +37 Fe Cor 27
 +33 Rye Tie Fe

Fe W. Wire 31

+50 T.P. or 29
 +47 Spruce 38
 +25 Bush 39
 +10 Bush 38
 +02 Bush 39
 +00 Fe. 34
 +74 B.E. 40
 +57 T.P. 23
 +45 Cor. Ho 43
 +40 B.E. 31
 +22 B.E. 40
 +15 Stump 27
 +14 Fe. Cor. 22
 +05-2 B.E. 30-46
 +00 Rye Tie Fe
 +01 P.P. 16

+87 B.E. 25
 +81 B.E. 39

+28 Tree 23

Uncultivated

Yard

Yards

Wire

Yards

14

11

+67-19
20+67-8
11

+25-20

93

19

73

+75-19

29

17

19

+26-14

17

14

12

17

9

23-0

29-5

33-7

37-13

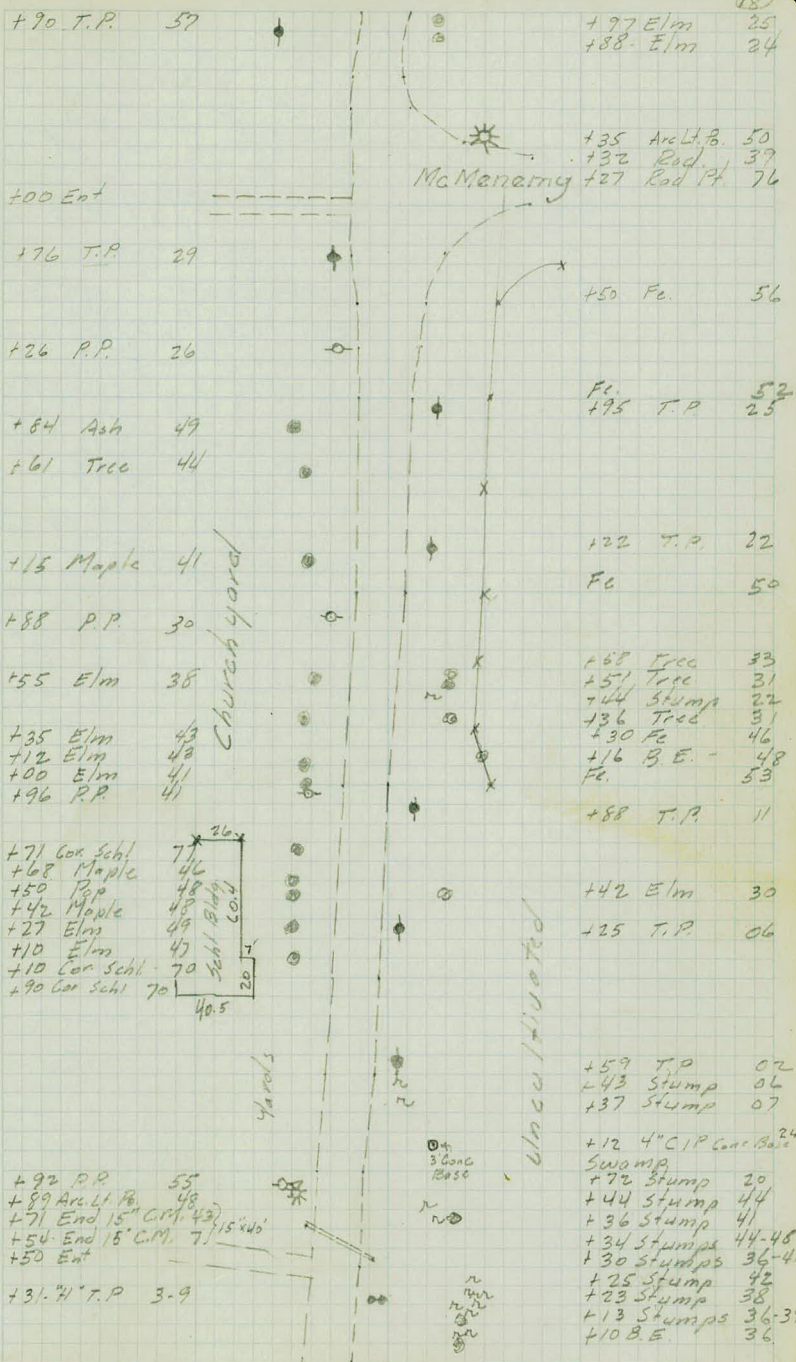
Swamp 15-6

40-16

+76 E/m 36
+75 Swamp 26

45-20

Swamp 121



8

17

68

8

14

67

9

15

66

9

15

+02-7

+02-16

5

16

65

10

11

10

13

64

12

9

11

11

63

13

10

11

12

62

14

11

100 Wall 28.7

+65 Elm 37
+62 Wall 28.3

+39 T.P. 22
+26 Elm 37

+100 Wall 28.3
+87 Elm 37

+48 Elm 37
+06 T.P. 22
+05 Elm 37
+100 Wall 28.3

+62 Elm 37

+38 Conc Walk 8' 28.2
+20 Elm 37

Wall 28.2

+77 Elm 36
+76 T.P. 21
+58 Beg Wall 29
+50 Ent

+37 - Cor. 2' x 2' Per 30'

100 G.R. 16

+86 Beg G.R. 17'
+65 End 10' W.I.P. 46'
+57 T.P. 36
+65 B.E. 35
+40 Ent
(S.P.W.D. Service Rd)

+00 Ent 24
+91 End 10' x 84' W.I.P. 19'

+65 T.P. 65
+50 Ent 50'

+82 Elm 40
+76 T.P. 61

+19 Elm 49
+12 P.P. 42

School yard

Uncultivated

Church yard

Cable

10' x 84' W.I.P.

100 Fe 27.7 (19)
+87 Fe Cor 27.3
+75 Maple 28
+65 Ent
+51 Maple 28

Uncultivated

+96 Oak 29

+67 Maple 30'

+39 End G.R. 19

100 G.R. 22
+99 Pop 50
+95 Pop 45
+81 Pop 33

+50 G.R. 32
+40 B.E. 40

+78 Beg G.R. 17'
+60 Ent
(S.P.W.D. Service Rd)

Uncultivated

+33 P.P. 22

+32 Elm 25

12

13

75

10

12

11

13

74

9

14

10

14

73

11

12

72

10

9

71

10

12

11

12

70

9

14

9

16

69

8

17

100 Fc. 37' (20)

+55 Oak 36

123 T.P. 26

+100 Fc. 35
+194 P.P. 26

+162 Oak 43
+150 Fc. 36

183 T.P. 23

100 Fc. 38

178 P.P. 30

+150 Fc. 40

100 Fence 43

+186 Ash 39
+180 G.P. 34

+88 T.P. 19
+75 Apple 31
+69 Cor. Cor. 34
+62 End 12' 90' W.P. 50'

+30 Ent.
+23 Cor. 52
+12 End 10' 14' G.P. 39
+07 Cor. 50
+98 B.E. 43
+87 T.P. 40

+18 Fc. Cor. 52
+02 Arc. L.P. 20
+100 Fc. Cor. 196

+43 T.P. 35

+63 Elm 25
+150 Fc. 23.4

+55 T.P. 28
+50 P.P. 44

+100 Fc. 26
+96 Elm 28
+77 Ash 29

+10 T.P. 25

+150 Ent 27.7
+150 Fc. 27.7
+23 Tree 30
+100 Fc. 38.7

+85 Ent

+56 T.P. 23
+50 B.E. 51

+67 Spruce 30'
+50 Fc. 28.5

+06 Cor. Wall - 29.0
+04 Elm 37
+00 Wall 28.7

+00 Fc. 27.7

Uncultivated

Wooded

Uncultivated

Wire Fc

Woven

Note: Suggest spec. sec. along cemetery fence as grows are very close

Cemetery

83

+28.2 Edge Pave x 5.4
-08.2 Edge Pave x 5.4

82

81

13

9

80

11

9

79

14

7

78

13

7

77

13

11

76

12

13

100 Road 18

+70 Road 17

+45 Rad. 30
+33 Rad. Pl. 46

100 Rad. 50
+92 T.P. 50
+91 G.P. 30
+75 Rad. 13
+75 T.P. 30
150 Rad. Pl. 11

+01 T.P. 29

102 T.P. 29

+20 Ent.
(N.G.) 12" x 20" G.M. 20"
+00 T.P. 29
+05 Stump 46

+74 Stump 50
+61 Oak 44
+57 Oak 49
+48 Stump 49
+43 Stump 50
+24 Stump 43

+96 Oak. 44
+89 T.P. 29
+75 Oak 46
+57 Stump 38
+53 Oak 47

+35 Stump 42

+56 T.P. 28

EDGERTON
20' Conc. Pave.

100 Road 7
+70 Road 9
+45 Rad. 18
+33 Rad. Pl. 40

+00 Rad. 50
+76 P.P. 26
+75 Rad. 17
+70 Oak 43
+50 Rad. Pl. 10
+40 Oak 40

+57 P.P. 25

+24 End Fe. 22
+17 Oak 21

+92 Oak 23

+57 Oak 26
+47 P.P. 24

+19 Oak 21
+00 Fe. 26

+87 Oak 42

+39 P.P. 24

+09 Oak 44
+00 Fe. 31
+92 Oak 38
+80 2 Oaks 30-50
+69 Oak 33
+55 Stump 31
+53 Oak 33

+32 Oak 24
+20 P.P. 23

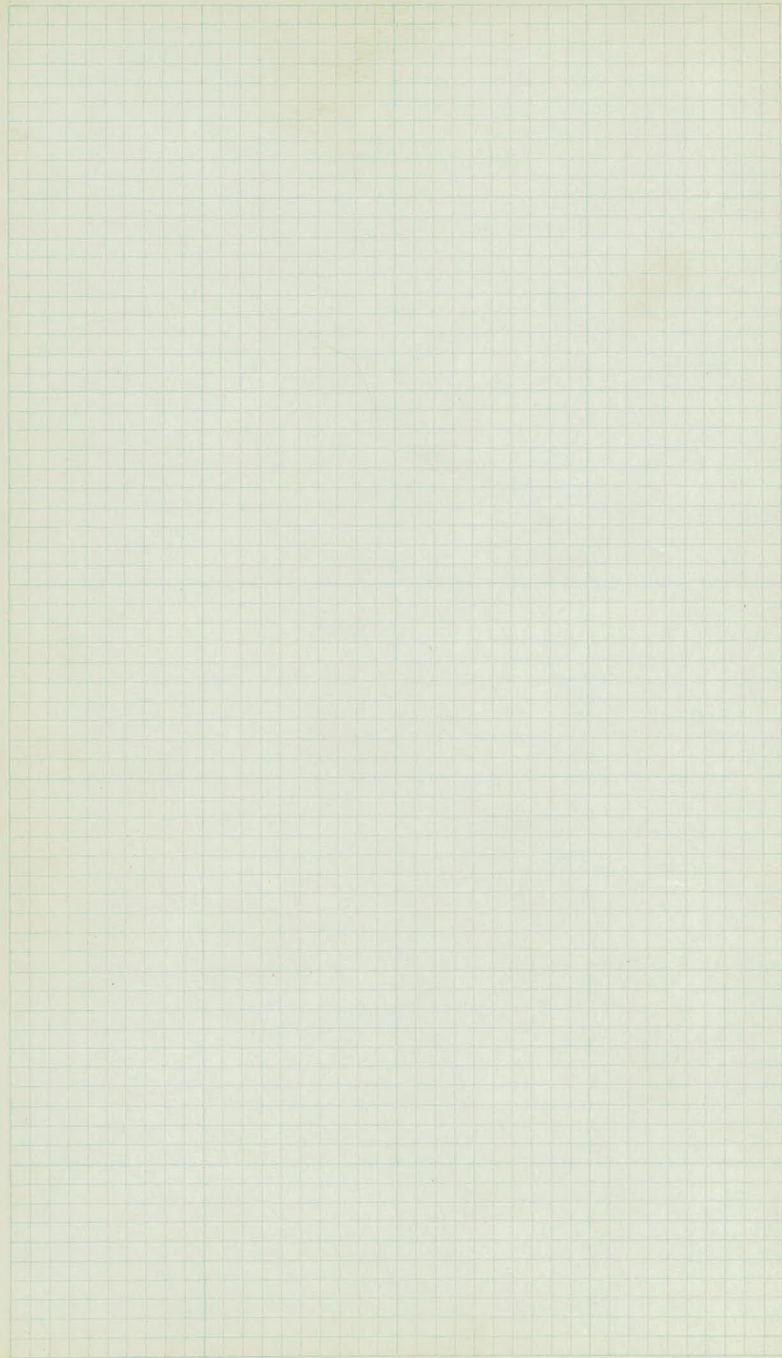
+00 Fe. 39
+96 Oak 39

+47 Oak 38

+09 P.P. 25
+00 Fe. 37

Uncultivated

Uncultivated

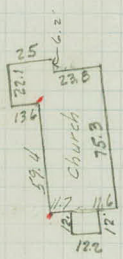


22

3100

200

+50 Cor. 25.5

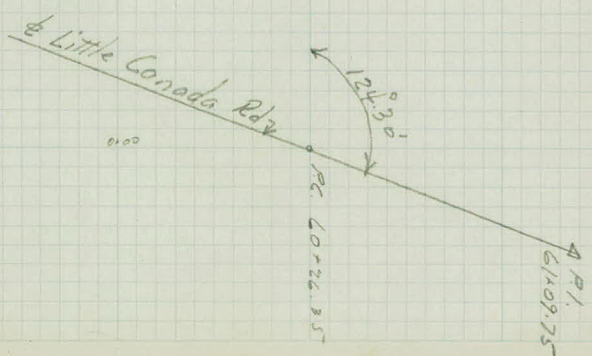


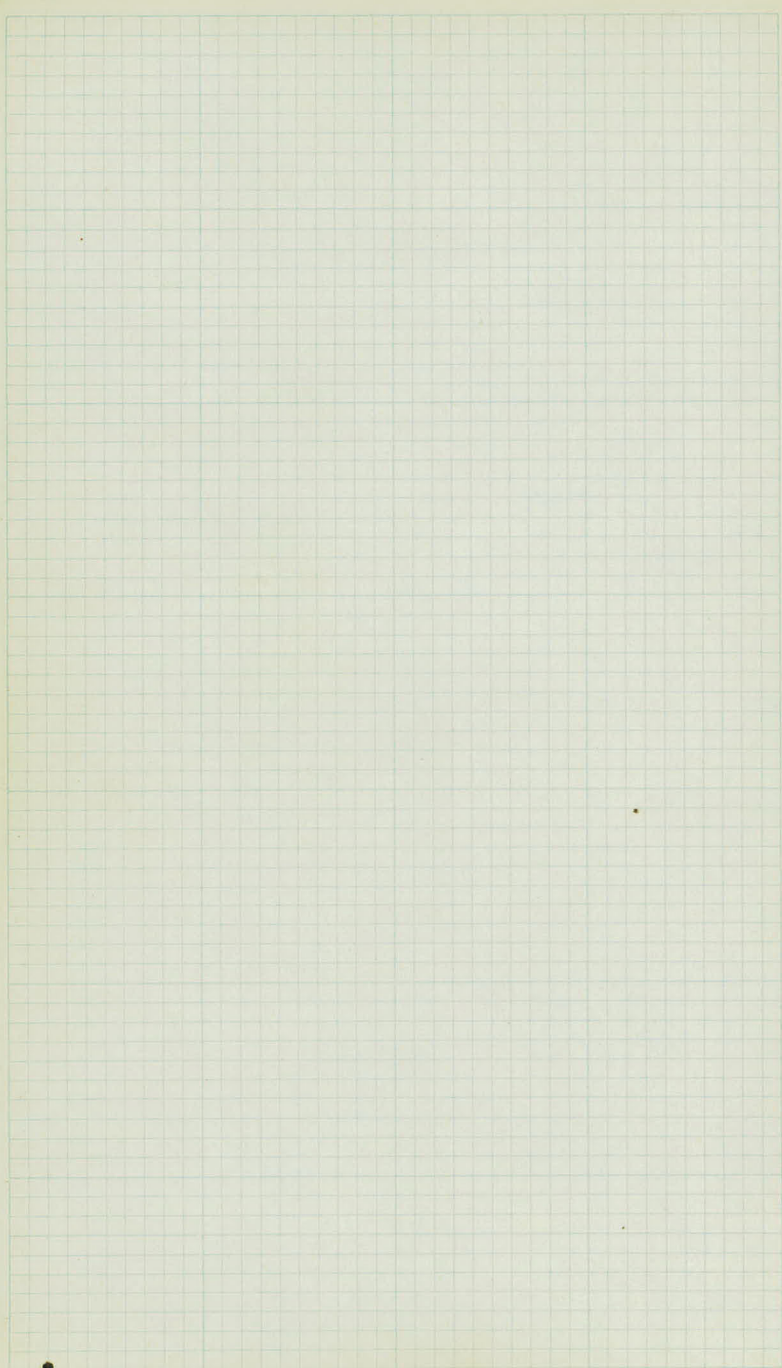
#03 - 27.5

 $+45 - 33.6$

1400

200





LITTLE CANADA RD.

Bench Levels

Pt.	+	π	-	Elev.
B.M.	3.53	961.44		957.91
T.P.	2.57	957.36	6.65	954.79
T.P.	1.47	947.77	11.06	946.30
T.P.	1.33	938.97	10.13	937.64
T.P.	1.95	931.56	9.36	929.61
B.M.	3.32	926.97	7.91	923.65
T.P.	3.37	924.81	5.53	921.44
T.P.	4.01	923.19	5.63	919.18
T.P.	6.87	927.52	2.54	920.65
T.P.	6.01	929.94	3.59	923.93
B.M.	3.79	927.37	6.36	923.58
T.P.	4.26	926.20	5.43	921.94
B.M.	6.62	925.47	7.35	918.85
T.P.	4.64	925.60	4.51	920.96
T.P.	2.93	920.86	7.67	917.93
B.M.	3.23	913.01	11.08	909.73
T.P.	10.76	918.98	4.79	908.22
T.P.	2.32	916.62	4.68	914.30
T.P.	1.37	907.07	10.92	905.70
B.M.	1.57	901.71	6.93	900.14
T.P.	7.39	899.54	9.56	892.15
T.P.	1.25	892.14	8.65	890.89
T.P.	1.39	881.78	11.75	880.39
B.M.	15.95		8.94	872.84

Top Mon. "C" and Rice

Top S.W. Cor. Conc. Platform 37' Lt. 0+35

Spike P.R. Drt. Rt. 17+72

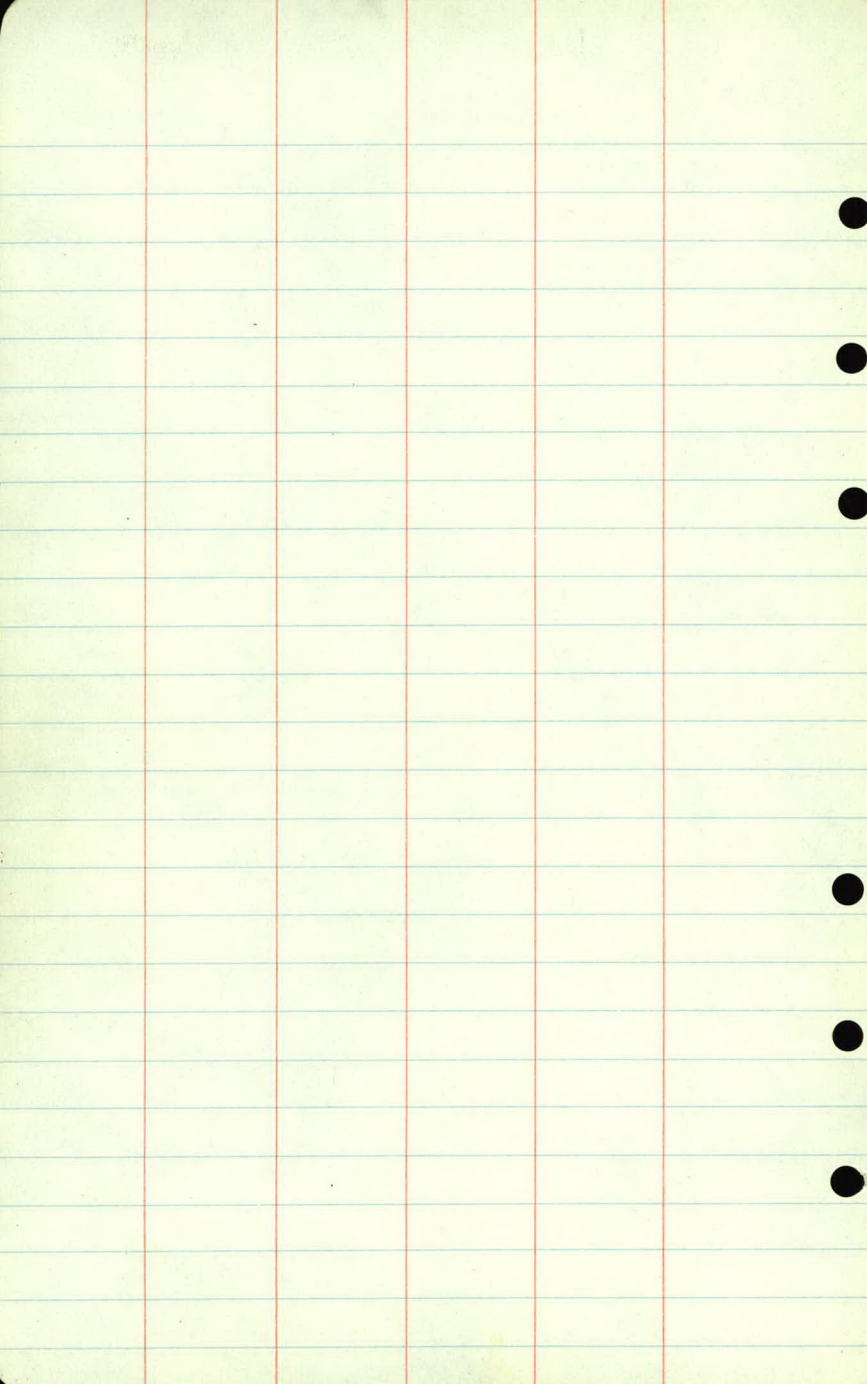
Top
Top S.E. Cor. Step 35' Lt. Sta. 22+28

Spike Arc Light Pole 22' Lt. Sta. 32+80

Spike Arc Light Pole 31' Lt. Sta. 49+73

Top S.W. Cor. Conc. Slab W. of Steps - School House

Top Mon. Little Canada Rd. and Edgerton



LITTLE CANADA RD

CROSS SECTIONS

Sta.	+	π	-	Elev.
B.M.	4.09	927.74		923.65
0+00			4.11	23.63

+12			4.29	23.45
-----	--	--	------	-------

+50			4.4	23.3
-----	--	--	-----	------

1			4.8	22.9
---	--	--	-----	------

+50			5.3	22.4
-----	--	--	-----	------

2			6.0	21.7
---	--	--	-----	------

+40			6.2	21.5
-----	--	--	-----	------

3			6.1	21.6
---	--	--	-----	------

+50			6.1	21.1
-----	--	--	-----	------

4			6.1	21.5
---	--	--	-----	------

T.P.	3.62	924.82	6.54	921.20
------	------	--------	------	--------

+50			3.4	6+60
-----	--	--	-----	------

Profile ditch Rt.	4+36			21.4
-------------------	------	--	--	------

Top S.W. Cor Conc. Platform 37' Lt. 560 x 35

$$\frac{4.69}{50} \quad 4.11 \quad \frac{3.04}{50}$$

$$\frac{4.95}{50} \quad 4.29 \quad \frac{3.18}{50}$$

$$\frac{3.96}{44} \quad \frac{4.15}{37} \quad \frac{4.9}{37} \quad 4.4 \quad \frac{4.5}{7} \quad \frac{4.9}{23} \quad \frac{4.0}{50}$$

$$\frac{5.9}{50} \quad \frac{5.8}{29} \quad \frac{5.2}{12} \quad 4.8 \quad \frac{5.3}{15} \quad \frac{5.0}{34} \quad \frac{4.3}{50}$$

Low Spot → $\frac{9.3}{100} \quad \frac{8.2}{50} \quad \frac{8.2}{31} \quad \frac{7.5}{30} \quad \frac{7.2}{24} \quad \frac{8.0}{22-20} \quad \frac{5.8}{15} \quad 5.3 \quad \frac{5.4}{8} \quad \frac{5.7}{18} \quad \frac{6.6}{25-27} \quad \frac{5.4}{31} \quad \frac{5.0}{50}$

$$\frac{8.7}{50} \quad \frac{8.7}{31} \quad \frac{7.8}{30} \quad \frac{7.7}{25} \quad \frac{9.0}{23} \quad \frac{6.5}{19} \quad \frac{6.0}{12} \quad \frac{6.1}{15} \quad \frac{6.6}{21} \quad \frac{8.1}{25-28} \quad \frac{6.0}{31} \quad \frac{6.5}{50}$$

$$\frac{7.8}{50} \quad \frac{8.4}{32} \quad \frac{8.2}{22} \quad \frac{6.8}{11} \quad 6.2 \quad \frac{6.4}{15} \quad \frac{7.1}{20} \quad \frac{9.0}{25} \quad \frac{8.3}{41} \quad \frac{8.1}{50}$$

$$\frac{4.5}{50} \quad \frac{5.0}{28} \quad \frac{7.5}{22} \quad \frac{7.9}{17} \quad \frac{6.7}{13} \quad 6.0 \quad \frac{6.4}{16} \quad \frac{7.2}{23} \quad \frac{9.0}{26} \quad \frac{9.2}{33} \quad \frac{8.1}{50}$$

5.21 Conc. Work Lt.

$$\frac{3.4}{50} \quad \frac{5.5}{30} \quad \frac{6.6}{13} \quad \frac{6.4}{16} \quad \frac{6.8}{21} \quad \frac{9.6}{27-31} \quad \frac{7.4}{33} \quad \frac{7.3}{50}$$

$$\frac{8.1}{50} \quad \frac{6.6}{24} \quad \frac{8.6}{20-17} \quad \frac{6.7}{13} \quad 6.1 \quad \frac{6.7}{20} \quad \frac{9.4}{26-30} \quad \frac{6.7}{31} \quad \frac{6.8}{50}$$

Top Rock Lt. 189 195 191 191 210 213 207 181

$$\frac{5.9}{50} \quad \frac{5.3}{35} \quad \frac{5.7}{22} \quad \frac{6.7}{21-17} \quad \frac{3.8}{10} \quad 3.4 \quad \frac{3.5}{12} \quad \frac{4.1}{23} \quad \frac{6.7}{26-28} \quad \frac{3.0}{32} \quad \frac{2.0}{35} \quad \frac{2.7}{50}$$

$$\frac{6.6}{27} \quad \frac{6.4}{50} \quad \frac{5.7}{100} \quad \frac{5.2}{150} \quad \frac{4.9}{200}$$

Sta.	+	π	—	Elev.	
		92482			
5			3.7	21.1	6+10
+50			4.4	20.4	5+60
Profile Ditch Lt. 5+57					
6			4.9	19.9	5+10
+50			5.3	19.5	4+60
+72	Note: Do not use this Sec. for yardage		5.5	19.3	whole section is skewed
7			5.7	19.1	4+10
+50			5.7	19.1	3+60
8			5.6	19.2	3+10
+50			5.8	19.0	2+60
9			5.8	19.0	2+10
T.P.	4.18	923.12	5.88	918.94	
+50			4.6	18.5	1+60
+86 P.C.			5.1	18.0	1+24

17.3

6.1 47 45 6.6 4.3 4.0 4.6 7.5 2.4 2.5
50 31 24 22 18 11 3 7 11 20 24 26 33 50

16.7

7.4 5.9 5.6 7.4 4.9 4.7 5.3 8.1 5.3 5.3
50 38 26 23 19 13 4 4 11 18 24 26 30 50

9.0 2.0 9.1 9.2 9.3 Low Spot 6.5 6.1 7.5 8.7
26 50 100 150 200

7.7 7.3 6.6 7.0 9.4 5.8 4.9 5.1 5.7 8.7 6.0 5.7
50 39 32 27 24 23 15 4 8 15 23 25 28 50

18.6

5.7 7.1 7.4 9.5 6.0 5.5 5.8 9.2 7.1 7.0
50 37 26 23 21 15 5 3 7 13 21 24 29 50

15.20
FL 18"

FL 18" 14.78 15.1

5.8 6.9 7.5 9.5 9.4 6.2 6.1 10.09 9.7 7.8 8.3
50 40 30 23 23 17 5 5 14 19 19 24 32 50

14.9

4.0 5.0 6.4 6.8 6.0 6.2 9.9 7.8 8.5
50 34 26 18 15 5.7 11 21 23 28 50

14.4

3.9 4.3 5.7 5.8 6.1 6.6 10.9 7.6 8.7 9.0
50 36 20 13 5.7 7 13 20 22 26 31 50

14.3

4.6 5.9 6.2 5.7 6.2 10.5 5.9 7.1 7.8
50 27 21 18 5.6 16 18 21 26 29 50

14.6

4.5 5.1 6.3 5.9 6.0 10.2 5.6 5.7 6.9
50 34 23 18 5.8 13 19 20 22 28 50

14.4

3.9 4.1 6.5 6.0 5.9 6.2 10.4 6.0 6.1
50 35 22 19 15 5.8 12 15 17 19 50

13.5

2.8 3.3 5.5 4.7 5.0 9.6 5.2 5.0
50 35 21 18 4.6 10 14 16 18 50

13.1

3.7 4.0 4.9 6.1 5.3 5.5 10.0 6.2 6.0 6.2
50 39 29 20 17 5.1 11 15 17 19 36 50

Sta.	+	π	-	Elev	
		923.12			
10			5.2	17.9	H10
+50			5.5	17.6	+60
+98			5.3	17.8	0+12
11			5.3	17.8	
+50			5.1	18.0	
12			4.3	18.8	
+14			4.1	19.0	
+50			3.6	19.5	
T.P.	9.34	929.56	2.90	920.22	
13			9.8	19.8	
+50			9.8	19.8	
14			9.5	20.1	
T.P.	3.31	928.23	4.64	924.92	
+50			7.8	20.4	

13.0

$\frac{3.9}{50}$ $\frac{4.0}{40}$ $\frac{5.7}{25}$ $\frac{6.2}{22}$ $\frac{5.3}{20}$ $\frac{5.5}{16}$ $\frac{10.1}{12}$ $\frac{6.3}{16}$ $\frac{6.2}{19}$ $\frac{6.2}{21}$ $\frac{36}{50}$

12.7

$\frac{4.7}{50}$ $\frac{5.1}{36}$ $\frac{5.8}{23}$ $\frac{6.5}{19}$ $\frac{5.6}{17}$ $\frac{5.5}{15}$ $\frac{6.1}{20}$ $\frac{10.4}{22}$ $\frac{7.0}{25}$ $\frac{8.4}{50}$

12.3

$\frac{3.9}{50}$ $\frac{3.9}{39}$ $\frac{5.1}{19}$ $\frac{7.1}{15}$ $\frac{5.6}{13}$ $\frac{5.8}{11}$ $\frac{10.8}{53}$ $\frac{7.1}{19}$ $\frac{8.3}{23}$ $\frac{8.4}{27}$ $\frac{35}{30}$ $\frac{50}{50}$

$\frac{3.9}{50}$ $\frac{3.9}{39}$ $\frac{5.1}{19}$ $\frac{7.1}{15}$ $\frac{5.6}{13}$ $\frac{5.8}{11}$ $\frac{10.8}{53}$ $\frac{7.1}{19}$ $\frac{8.3}{23}$ $\frac{8.4}{27}$ $\frac{35}{30}$ $\frac{50}{50}$

$\frac{6.8}{50}$ $\frac{5.8}{40}$ $\frac{5.6}{17}$ $\frac{6.1}{14}$ $\frac{5.5}{13}$ $\frac{5.1}{10}$ $\frac{5.6}{17}$ $\frac{6.3}{25}$ $\frac{7.0}{41}$ $\frac{7.3}{50}$

4

$\frac{5.0}{50}$ $\frac{4.3}{30}$ $\frac{4.2}{11}$ $\frac{4.9}{8}$ $\frac{4.2}{43}$ $\frac{4.6}{10}$ $\frac{6.1}{21}$ $\frac{7.9}{38}$ $\frac{50}{50}$ ✓

4

$\frac{3.7}{50}$ $\frac{2.7}{25}$ $\frac{3.3}{13}$ $\frac{4.4}{8}$ $\frac{3.9}{41}$ $\frac{4.1}{8}$ $\frac{4.1}{21}$ $\frac{6.4}{36}$ $\frac{9.2}{50}$ ✓

4

$\frac{0.3}{50}$ $\frac{1.5}{11}$ $\frac{4.0}{7}$ $\frac{3.3}{3.6}$ $\frac{3.9}{9}$ $\frac{10.2}{26}$ $\frac{50}{50}$ ✓

4

$\frac{5.2}{50}$ $\frac{5.4}{36}$ $\frac{6.4}{13}$ $\frac{9.9}{6}$ $\frac{9.2}{9.8}$ $\frac{9.5}{73}$ $\frac{10.6}{21}$ $\frac{14.5}{33}$ $\frac{50}{50}$ ✓

4

$\frac{5.7}{50}$ $\frac{5.7}{28}$ $\frac{5.0}{15}$ $\frac{9.9}{4}$ $\frac{9.1}{9.8}$ $\frac{9.8}{13}$ $\frac{9.3}{30}$ $\frac{12.5}{33}$ $\frac{50}{50}$ ✓

4

$\frac{5.7}{50}$ $\frac{5.6}{24}$ $\frac{4.5}{12}$ $\frac{9.3}{5}$ $\frac{8.8}{9.5}$ $\frac{9.6}{15}$ $\frac{8.3}{32}$ $\frac{10.5}{35}$ $\frac{11.5}{42}$ $\frac{50}{50}$ ✓

Spitz. P.P. 4.15.72

4

$\frac{4.2}{50}$ $\frac{4.2}{26}$ $\frac{2.5}{13}$ $\frac{7.8}{7.8}$ $\frac{7.4}{6}$ $\frac{7.1}{17}$ $\frac{7.7}{34}$ $\frac{6.4}{37}$ $\frac{9.1}{50}$ ✓

Sta.	+	π	-	Elev
		928.23		
15			7.0	21.2
+50			6.8	21.4
16			6.7	21.5
+50			5.8	22.4
		Water Table Ho. Rt.	8.52	
17			4.3	23.9
+17	P.C.		4.2	24.0
+50			4.6	23.6
18			4.9	23.3
+50			4.6	23.6
19			4.3	23.9
		Water Table Ho. Rt.	4.38	
+50			5.2	23.0
+67			5.8	22.4

41 41 2.4 5.9 7.7 7.2 6.9 7.6 7.1 9.0 ✓
50 22 12 7 7.0 3 9 21 35 40 50

46 42 31 31 6.7 7.4 7.0 6.6 7.0 8.0 9.2 ✓
50 26 15 11 3 6.8 5 12 21 32 47 50

5.0 4.5 4.2 3.2 3.2 7.2 6.7 6.4 6.8 7.6 9.1
50 25 15 12 9 6.7 6 13 22 34 41 50

5.7 5.2 4.5 3.7 3.7 6.9 6.3 5.9 6.3 6.7 7.7
50 34 13 9 6 5.8 5 15 25 35 42 50

6.4 6.0 5.4 4.1 6.3 6.4 6.2 5.8 6.1 6.4 7.3
50 29 8 3 43 1 10 17 27 38 47 50

6.7 5.8 5.3 4.2 5.5 6.4 6.1 5.8 6.1 6.5 7.8
50 24 8 4 4.2 6 11 17 27 37 46 50

6.7 6.5 5.2 5.3 4.8 5.6 6.3 6.1 5.5 6.3 7.2
50 32 16 6 4.6 5 12 18 29 44 50

6.7 6.2 5.8 5.1 4.8 5.4 6.0 5.6 5.1 5.7
50 23 4 2 4.9 6 9 15 20 30 50

6.6 6.2 5.7 4.7 4.5 5.6 5.9 5.5 5.1 5.3 5.6
50 25 5 2 4.6 2 8 15 22 32 41 50

5.4 6.0 5.7 4.5 5.5 5.2 5.8 5.5 5.1 5.5 5.3
50 26 8 3 4.3 9 11 16 22 32 46 50

6.0 7.0 5.8 5.4 5.3 5.2 4.9 5.2 4.9
50 47 32 18 11 18 29 42 50

Top Rail
2.3 2.0 3.5 7.6 8.8 5.0 5.2 4.8 4.6 5.1 5.0
50 46 39 26 13 5.8 8 14 20 29 41 50

Sta.	+	π	-	Elev
		928.23		
19 +82		1.6 926.6	8.6	
20			7.0	
+24			2.6	
+27.7	Top Rail		1.67	
+35.3	Top Rail		1.42	
+41			2.0	
+57			3.0	
+81			2.8	
T.P.	1.52	927.21	2.53	925.70
21			2.3	
+19	P.T.		2.9	
+50			3.5	
22			4.1	

Sta.	+	π	-	Elev.	
		927.21			
22+50			4.5		
23			4.8		
B.M.	3.59	927.17	3.59	923.62	923.58
+50			4.9		
24			5.0	22.2	
+46	Note: Do not use this Sect. for Yardage.		5.0		whole sec. is skewed
	Profile Ditch Lt.				
+50			5.0	22.2	
T.P.	2.64	926.94	2.87	924.30	
25			4.7	22.2	
+50			4.7	22.2	
26			4.6	22.3	
+50			4.6	22.3	
27			4.8	22.1	
+50			5.0	21.9	

$$\begin{array}{ccccccc} & & & & \epsilon & & \\ \frac{4.5}{50} & \frac{4.5}{36} & \frac{5.0}{22} & \frac{4.9}{6} & 4.5 & \frac{4.2}{7} & \frac{4.5}{17} & \frac{3.7}{29} & \frac{4.3}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & & \epsilon & & \\ \frac{5.3}{50} & \frac{5.3}{21} & \frac{5.1}{5} & 4.8 & \frac{4.6}{5} & \frac{4.6}{19} & \frac{4.2}{35} & \frac{4.7}{50} \end{array}$$

Top S.E. Cor. ^{Top} Step 35' Lt. 22+28

$$\begin{array}{ccccccc} \frac{5.3}{50} & \frac{5.3}{36} & \frac{5.5}{20} & \frac{5.8}{18} & \frac{5.3}{6} & 4.9 & \frac{4.8}{6} & \frac{4.9}{19} & \frac{4.3}{28} & \frac{5.0}{36} & \frac{5.0}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{5.3}{50} & \frac{5.2}{36} & \frac{5.4}{20} & \frac{6.2}{19-17} & \frac{5.6}{14} & 5.0 & \frac{5.1}{12} & \frac{4.8}{20} & \frac{5.1}{24} & \frac{4.3}{32} & \frac{4.6}{46} & \frac{5.0}{50} \end{array}$$

FL 15' C.M.

$$\begin{array}{ccccccc} \frac{5.6}{50} & \frac{5.6}{34} & \frac{7.4}{26} & \left(\frac{7.9}{17} \right) & \frac{5.9}{15} & \frac{5.3}{9} & 5.0 & \frac{5.1}{11} & \frac{5.5}{14} & \frac{5.3}{16} & \frac{5.1}{22} & \left(\frac{7.2}{23} \right) & \frac{5.8}{28} & \frac{5.4}{50} \end{array}$$

FL 15' C.M.

$$\begin{array}{ccccccc} \frac{8.8}{200} & \frac{8.5}{150} & \frac{8.2}{100} & \frac{8.1}{50} & \frac{7.8}{17} & & & \frac{5.1}{50} & \frac{5.6}{11} & \frac{5.4}{16} & \frac{5.6}{22} & \frac{5.9}{37} & \frac{5.9}{50} \end{array}$$

Top Culv. Post.

$$\begin{array}{ccccccc} \frac{5.4}{50} & \frac{5.6}{34} & \frac{5.3}{17} & \frac{5.2}{12} & 4.7 & \frac{5.0}{16} & \frac{4.8}{25} & \frac{4.8}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{6.1}{50} & \frac{5.5}{23} & \frac{5.1}{12} & 4.7 & \frac{4.7}{15} & \frac{4.4}{28} & \frac{4.4}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{6.3}{50} & \frac{5.5}{38} & \frac{5.4}{24} & \frac{5.2}{12} & 4.6 & \frac{4.7}{14} & \frac{4.6}{26} & \frac{4.3}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{6.1}{50} & \frac{5.3}{28} & \frac{5.1}{14} & 4.6 & \frac{4.8}{12} & \frac{4.8}{25} & \frac{4.4}{27} & \frac{4.0}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{6.1}{50} & \frac{5.2}{30} & \frac{5.5}{22} & \frac{5.0}{13} & 4.8 & \frac{5.0}{11} & \frac{5.1}{15} & \frac{4.4}{24} & \frac{4.2}{41} & \frac{4.9}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{5.4}{50} & \frac{5.3}{30} & \frac{6.3}{23} & \frac{5.2}{15} & 5.0 & \frac{5.2}{14} & \frac{5.3}{27} & \frac{5.2}{50} \end{array}$$

Sta.	+	π	-	Elev.	
		926.94			
28			5.1	21.8	
+50			5.4		
29			5.5		
+50			5.6		
30			5.7		
+50			5.9		
31			6.0		
+50			6.0		
B.M.	6.63	925.48	8.01	918.93	918.85
32			4.6		
	E Lake Ave.		4.7		
+50			4.7		
33			5.0		
+50			5.4		

$\frac{6.0}{50}$ $\frac{5.5}{32}$ $\frac{5.1}{23}$ $\frac{5.4}{13}$ $\frac{5.4}{14}$ $\frac{5.4}{33}$ $\frac{5.5}{50}$

$\frac{7.5}{50}$ $\frac{6.5}{34}$ $\frac{6.4}{21}$ $\frac{5.8}{19}$ $\frac{5.5}{14}$ $\frac{5.4}{25}$ $\frac{5.1}{50}$

$\frac{7.4}{50}$ $\frac{6.0}{25}$ $\frac{5.8}{12}$ $\frac{5.5}{5.5}$ $\frac{5.7}{13}$ $\frac{5.7}{24}$ $\frac{5.1}{32}$ $\frac{4.9}{50}$

$\frac{7.8}{50}$ $\frac{6.3}{24}$ $\frac{7.9}{20-18}$ $\frac{6.0}{14}$ $\frac{5.7}{5.6}$ $\frac{5.7}{13}$ $\frac{5.1}{25}$ $\frac{5.1}{50}$

$\frac{8.2}{50}$ $\frac{6.3}{24}$ $\frac{7.8}{21-18}$ $\frac{6.3}{14}$ $\frac{5.8}{5.7}$ $\frac{6.3}{15}$ $\frac{4.7}{26}$ $\frac{4.8}{32}$ $\frac{4.8}{50}$

$\frac{7.3}{50}$ $\frac{6.0}{27}$ $\frac{7.5}{20-18}$ $\frac{6.2}{14}$ $\frac{6.3}{8}$ $\frac{5.9}{5.9}$ $\frac{5.6}{12}$ $\frac{6.3}{17}$ $\frac{4.9}{23}$ $\frac{4.7}{30}$ $\frac{4.7}{50}$

$\frac{7.6}{50}$ $\frac{6.3}{24}$ $\frac{7.2}{20-18}$ $\frac{6.5}{13}$ $\frac{6.0}{6.0}$ $\frac{5.9}{10}$ $\frac{5.4}{18}$ $\frac{5.5}{33}$ $\frac{5.5}{50}$

$\frac{7.0}{50}$ $\frac{6.8}{21}$ $\frac{6.5}{13}$ $\frac{6.0}{6.0}$ $\frac{5.9}{12}$ $\frac{5.7}{19}$ $\frac{6.1}{21}$ $\frac{5.6}{26}$ $\frac{5.5}{50}$

Spike Arc. Lt. Pole 22' Lt. Sta 32+80

$\frac{8.8}{50}$ $\frac{7.7}{38}$ $\frac{5.8}{18}$ $\frac{5.3}{14}$ $\frac{4.7}{4.6}$ $\frac{4.5}{12}$ $\frac{4.3}{21}$ $\frac{3.5}{42}$ $\frac{3.5}{50}$

$\frac{4.4}{50}$ $\frac{4.3}{100}$ $\frac{3.9}{150}$ $\frac{3.4}{200}$ $\frac{2.5}{250}$

$\frac{10.3}{50}$ $\frac{7.9}{29}$ $\frac{5.3}{12}$ $\frac{4.5}{4.7}$ $\frac{4.4}{18}$ $\frac{4.4}{50}$

$\frac{10.7}{50}$ $\frac{8.8}{30}$ $\frac{7.1}{16}$ $\frac{5.6}{12}$ $\frac{5.3}{5.0}$ $\frac{5.2}{15}$ $\frac{4.6}{25}$ $\frac{3.9}{33}$ $\frac{3.9}{50}$

$\frac{10.9}{50}$ $\frac{9.3}{32}$ $\frac{7.8}{17}$ $\frac{6.2}{13}$ $\frac{5.4}{5.4}$ $\frac{5.5}{7}$ $\frac{5.7}{19}$ $\frac{6.1}{21}$ $\frac{4.8}{25}$ $\frac{4.1}{30}$ $\frac{4.1}{50}$

OK
3/55

Sta.	+	⌈	-	Elev.
		925.48		
34			5.7	
+50			5.4	
35			5.2	
+50			5.2	
36			5.0	
+50			4.5	
37			4.3	
+50			4.3	
38			4.5	
T.P.	4.41	925.30	4.59	920.89
+50			4.4	
39			4.4	
+50			4.3	

$$\begin{array}{cccccccc} 11.2 & 9.4 & 7.6 & 6.3 & & 5.7 & 6.3 & 5.3 & 4.8 & 4.8 \\ 50 & 32 & 18 & 13 & 5.7 & 15 & 19-23 & 26 & 31 & 50 \end{array}$$

$$\begin{array}{cccccccc} 11.2 & 9.4 & 7.9 & 6.0 & & 5.7 & 6.6 & 4.8 & 4.8 \\ 50 & 33 & 19 & 14 & 5.4 & 14 & 19-24 & 30 & 50 \end{array}$$

$$\begin{array}{cccccccc} 10.4 & 9.5 & 8.5 & 7.5 & 5.7 & & 5.6 & 6.4 & 5.0 & 4.9 \\ 50 & 38 & 33 & 18 & 12 & 5.2 & 15 & 20-24 & 30 & 50 \end{array}$$

$$\begin{array}{cccccccc} 9.4 & 8.5 & 7.2 & 5.7 & & 5.5 & 6.0 & 5.2 & 3.8 \\ 50 & 37 & 16 & 11 & 5.2 & 15 & 21 & 28 & 50 \end{array}$$

$$\begin{array}{cccccccc} 6.9 & 6.3 & 5.2 & & & 5.6 & 6.5 & 4.5 & 3.7 \\ 50 & 28 & 9 & 5.0 & 17 & 21-24 & 28 & 50 \end{array}$$

$$\begin{array}{cccccccc} 6.2 & 6.2 & 5.0 & & & 5.0 & 4.5 & 4.1 & 3.5 & 3.5 \\ 50 & 28 & 14 & 4.5 & 14 & 17 & 30 & 37 & 50 \end{array}$$

$$\begin{array}{cccccccc} 6.9 & 5.3 & 5.1 & 5.5 & 4.7 & & 4.9 & 5.3 & 3.3 & 2.9 \\ 50 & 40 & 27 & 23 & 11 & 4.3 & 20 & 22 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccc} 6.5 & 5.7 & 6.1 & 4.9 & & 4.7 & 4.9 & 4.9 & 3.0 & 2.9 & 2.8 \\ 50 & 28 & 25-23 & 19 & 4.3 & 11 & 14 & 22 & 32 & 38 & 50 \end{array}$$

$$\begin{array}{cccccccc} 6.2 & 5.7 & 5.9 & 4.7 & & 4.9 & 5.2 & 4.1 & 2.9 \\ 50 & 29 & 26-24 & 19 & 4.5 & 12 & 21 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccc} 5.5 & 4.8 & 6.0 & 4.9 & & 4.8 & 5.3 & 3.9 & 3.3 \\ 50 & 33 & 24 & 17 & 4.4 & 16 & 19 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccc} 6.2 & 5.7 & 6.3 & 6.2 & 4.9 & & 4.6 & 4.8 & 4.2 & 4.0 \\ 50 & 36 & 30 & 22 & 14 & 4.4 & 9 & 17 & 25 & 50 \end{array}$$

$$\begin{array}{cccccccc} 6.2 & 5.6 & 6.1 & 6.5 & 5.5 & 4.8 & & 4.6 & 5.0 & 4.3 \\ 50 & 38 & 29 & 27-21 & 18 & 14 & 4.3 & 16 & 21 & 50 \end{array}$$

Sta.	t	π	—	Elev.
		925.30		
40			4.6	
+50			4.8	
41			5.2	
+50			5.8	
42			6.4	
+50			6.9	
43			7.3	
+50			7.3	
44			7.4	
T.P.	3.97	921.90	7.37	917.93
+50			3.5	
45			3.4	
+50			3.5	

$$\begin{array}{cccccccc} \frac{6.1}{50} & \frac{5.6}{37} & \frac{6.6}{25.22} & \frac{5.0}{14} & 46 & \frac{49}{14} & \frac{4.6}{24} & \frac{4.3}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{5.5}{50} & \frac{5.4}{21} & \frac{5.4}{14} & 4.8 & \frac{5.3}{17} & \frac{5.5}{20} & \frac{4.5}{28} & \frac{4.2}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{7.0}{50} & \frac{5.8}{36} & \frac{6.2}{30} & \frac{6.8}{25} & \frac{5.4}{15} & 5.2 & \frac{5.7}{10} & \frac{5.9}{21} & \frac{4.7}{29} & \frac{4.5}{39} & \frac{5.1}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{9.2}{50} & \frac{7.7}{37} & \frac{7.7}{23} & \frac{6.3}{15} & 5.8 & \frac{6.2}{11} & \frac{6.3}{21} & \frac{4.8}{30} & \frac{5.3}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{11.4}{50} & \frac{10.3}{38} & \frac{8.9}{22} & \frac{6.8}{14} & 6.4 & \frac{6.9}{15} & \frac{6.8}{20} & \frac{5.6}{28} & \frac{5.3}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{12.9}{50} & \frac{11.2}{29} & \frac{9.9}{19} & \frac{7.4}{14} & 6.9 & \frac{7.3}{15} & \frac{7.6}{20} & \frac{6.1}{29} & \frac{6.0}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{13.9}{50} & \frac{12.0}{34} & \frac{10.7}{22} & \frac{8.0}{11} & 7.3 & \frac{7.5}{17} & \frac{8.0}{20} & \frac{6.0}{28} & \frac{5.6}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{14.0}{50} & \frac{11.9}{35} & \frac{10.8}{19} & \frac{8.0}{13} & 7.3 & \frac{7.6}{15} & \frac{7.7}{19} & \frac{5.5}{29} & \frac{5.9}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{13.9}{50} & \frac{11.8}{35} & \frac{10.1}{20} & \frac{8.0}{12} & 7.4 & \frac{7.7}{15} & \frac{8.1}{21} & \frac{5.8}{32} & \frac{5.9}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{10.0}{50} & \frac{9.3}{39} & \frac{7.8}{37} & \frac{6.7}{26} & \frac{5.5}{20} & \frac{4.1}{14} & 3.5 & \frac{4.1}{14} & \frac{4.7}{18} & \frac{2.1}{32} & \frac{2.0}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{8.9}{50} & \frac{8.5}{41} & \frac{6.5}{37} & \frac{6.0}{27} & \frac{3.9}{15} & 3.4 & \frac{3.7}{15} & \frac{4.3}{22} & \frac{2.0}{30} & \frac{2.0}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{8.0}{50} & \frac{7.4}{42} & \frac{6.0}{37} & \frac{5.1}{24} & \frac{4.0}{17} & 3.5 & \frac{3.9}{15} & \frac{4.1}{17} & \frac{2.3}{28} & \frac{2.6}{43} & \frac{2.1}{50} \end{array}$$

Sta.	+	π	-	Elev.	
		921.90			
46			3.8		
+50			4.0		
47			5.1		
+50			6.9		
48			9.1		
+50			11.4		
+93	P.C.		12.8		
B.M.	2.90	912.68	12.10	909.80	909.78
49			3.5		
+50			4.2		
	Profile Centerville				
+75			4.2		
50			4.2		
+50			3.8		

7.1	6.6	4.7	4.1	4.4	4.0	4.1	4.3	2.4	2.3
50	41	37	26	21	16	14	19	27	50

6.5	5.9	4.4	5.8	4.2	4.4	3.2	2.6	2.7		
50	39	33	26	22	17	4.0	13	29	42	50

6.1	5.9	4.8	6.0	5.4	5.6	4.8	3.3	
50	37	30	26	23	18	5.1	43	50

8.0	7.6	7.5	7.3	7.5	6.4	5.1	4.5	4.1	
50	30	25	18	6.9	9	11	25	37	50

9.6	8.8	8.7	9.5	9.2	9.5	7.9	6.4	
50	35	29	26	22	9.1	11	17	50

10.4	11.2	11.8	12.0	11.6	11.2	10.9	11.1	
50	38	26	17	11.4	9	12	25	50

13.2	13.8	14.9	14.1	12.9	13.2	12.5	13.2	13.2	
50	41	33	23	10	12.8	10	13	38	50

Spike Arc Lt. Pole 31' Lt. 49+73

5.2	6.5	5.3	4.5	3.6	3.9	3.2	3.4	4.0	3.5	
50	43	28	20	10	3.5	8	13	27	41	50

Floor Ho. Rt. 4.03

7.4	7.0	5.2	4.5	4.5	4.3	5.0	5.7	5.9	
50	42	26	17	4.2	11	19	31	44	50
133	11.1	8.7	6.9	4.5					
260	150	100	50	10	4.2				

Daylight? 2.8 2.4 2.8 5.5 4.5 4.7 5.0 5.5

75	50	39	24	10	4.2	12	30	9.4
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3.4	3.4	4.6	4.7	5.0	5.7	
50	28	12	4.2	15	33	50

2.1	3.2	3.9	4.3	5.1	5.1	5.1	
50	24	18	3.8	12	21	39	50

Sta	+	π	-	Elev.
		912.68		
51	P.T.		4.0	
+50			4.6	
52			5.4	
T.R.	5.31	913.17	4.82	907.86
+41			6.3	
+64			6.6	
53			8.2	
+28			7.2	
+34			6.6	
+50			7.5	
54			10.0	
+50			10.7	
55			9.4	

3.0 4.2 4.1 5.0 5.5 5.7
 47 25 12 40 13 30 50

Floor Ho. Lt. 2.17 4
 3.7 4.1 4.5 4.3 5.8 6.2 5.9
 50 28 17 8 4.6 15 29 50

4
 4.5 5.4 5.1 4.7 5.1 6.0 6.8 7.5
 50 36 25 13 2 5.4 15 27 50

4
 6.2 6.3 5.8 5.3 6.0 6.9 8.3 10.7
 50 40 29 16 5 6.3 6 30 50

4
 6.3 6.3 5.8 5.4 5.8 7.8 11.0 12.0
 50 39 31 20 10 6.6 11 20 50

4
 6.0 5.7 5.5 6.2 6.4 10.2 11.5
 50 35 25 13 8 8.2 21 50

4
 5.8 5.5 5.3 5.7 5.1 5.1 8.5 12.0 13.7
 50 38 27 15 9 6 7.2 10 30 50

at Tavern Lt. d 9rd. 6.3 Floor 4.75
 5.9 5.5 5.3 5.6 5.1 5.0 8.5 13.1 14.1 14.3
 50 38 29 16 9 6 6.6 7 17 37 50

4
 6.4 5.6 5.2 5.5 5.0 8.9 13.9 14.8 15.4
 50 39 29 19 7 7.5 4 15 27 50

4
 6.3 5.8 5.2 5.5 5.3 12.3 14.2 14.5 15.2
 50 44 32 21 15 10.0 5 19 41 50

4
 6.2 5.5 5.0 5.3 5.5 12.5 14.5 14.6 15.6
 50 42 32 21 16 10.7 7 28 41 50

4
 5.3 4.6 4.5 4.1 4.5 4.8 11.5 12.7 14.4
 50 46 41 31 20 16 9.4 17 36 50

Sta.	+	∇	-	Elev
		913.17		
55	+50		3.9	
56			2.0	
T.P.	7.81	919.83	1.15	9.12.02
	+50		7.5	
57			6.2	
	+50		5.5	
58			5.5	
	+50		5.3	
59			5.6	
	+50		6.6	
60			7.2	
	+26	P.C.	7.4	
	+50		7.6	

d

$\frac{3.3}{50}$	$\frac{3.0}{37}$	$\frac{2.7}{29}$	$\frac{3.2}{18}$	$\frac{3.5}{9}$	$\frac{5.1}{8.6}$	$\frac{3.9}{5}$	$\frac{3.9}{11}$	$\frac{5.4}{21}$	$\frac{6.7}{21}$	$\frac{9.9}{37}$	$\frac{12.9}{50}$
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F.L. on 15" x 40' C.M. $\frac{4.09}{48}$ $\pm$ $\frac{5.18}{57}$ on Lt.

$\frac{0.0}{50}$	$\frac{2.3}{41}$	$\frac{1.6}{34}$	$\frac{1.3}{25}$	$\frac{1.8}{14}$	$\frac{2.2}{2.0}$	$\frac{5.1}{34}$	$\frac{5.1}{50}$
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d

$\frac{3.5}{50}$	$\frac{4.8}{47}$	$\frac{7.0}{37}$	$\frac{7.2}{32}$	$\frac{6.8}{21}$	$\frac{7.4}{10}$	$\frac{7.2}{7.5}$	$\frac{8.2}{12}$	$\frac{8.8}{37}$	$\frac{8.8}{50}$
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d

$\frac{1.6}{50}$	$\frac{6.0}{33}$	$\frac{6.1}{28}$	$\frac{5.9}{18}$	$\frac{6.2}{9}$	$\frac{6.2}{6.2}$	$\frac{5.3}{13}$	$\frac{5.9}{28}$	$\frac{7.0}{50}$
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d

$\frac{1.7}{50}$	$\frac{1.7}{48}$	$\frac{5.3}{30}$	$\frac{5.4}{25}$	$\frac{5.2}{15}$	$\frac{5.7}{4}$	$\frac{5.5}{5.5}$	$\frac{5.0}{6}$	$\frac{5.3}{2.4}$	$\frac{5.9}{50}$
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d

$\frac{2.2}{50}$	$\frac{2.0}{41}$	$\frac{4.9}{29}$	$\frac{5.3}{22}$	$\frac{5.0}{12}$	$\frac{5.3}{7}$	$\frac{5.5}{5.5}$	$\frac{4.3}{6}$	$\frac{4.6}{20}$	$\frac{4.9}{29}$	$\frac{4.9}{50}$
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d

$\frac{2.4}{50}$	$\frac{3.5}{41}$	$\frac{5.0}{28}$	$\frac{5.1}{18}$	$\frac{5.3}{9}$	$\frac{5.3}{5.3}$	$\frac{5.5}{4}$	$\frac{6.1}{17}$	$\frac{4.9}{41}$	$\frac{4.6}{50}$
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d

$\frac{2.5}{50}$	$\frac{2.4}{34}$	$\frac{5.7}{29}$	$\frac{5.6}{19}$	$\frac{5.4}{5}$	$\frac{5.4}{5.6}$	$\frac{6.1}{7}$	$\frac{6.2}{2.4}$	$\frac{6.2}{42}$	$\frac{5.7}{46}$	$\frac{5.6}{50}$
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$\frac{2.7}{50}$	$\frac{4.6}{25}$	$\frac{6.5}{18}$	$\frac{6.8}{12}$	$\frac{6.6}{6.6}$	$\frac{6.9}{10}$	$\frac{7.5}{25}$	$\frac{8.3}{50}$
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$\frac{2.4}{50}$	$\frac{4.0}{36}$	$\frac{7.8}{21}$	$\frac{7.7}{11}$	$\frac{7.2}{7.2}$	$\frac{7.4}{11}$	$\frac{7.7}{15}$	$\frac{9.4}{23}$	$\frac{11.4}{50}$
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$\frac{3.7}{50}$	$\frac{5.0}{32}$	$\frac{8.2}{23}$	$\frac{8.1}{14}$	$\frac{7.4}{7.4}$	$\frac{7.9}{16}$	$\frac{10.7}{24}$	$\frac{14.5}{50}$
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$\frac{4.9}{50}$	$\frac{5.3}{36}$	$\frac{8.8}{24}$	$\frac{8.6}{18}$	$\frac{7.6}{7.6}$	$\frac{8.3}{18}$	$\frac{13.3}{33}$	$\frac{14.4}{50}$
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Sta.	+	π	-	Elev.
		919.83		
60+75			7.9	
61			8.4	
Profile of McManemy				
+25			8.9	
+50			9.4	
T.P.	4.08	914.61	9.30	910.53
+67	P.T.		4.5	
62			5.5	
+50			6.7	
63			7.6	
+34	P.C.		8.3	
+50			8.6	
64			9.9	
+50			11.5	

$$\begin{array}{r} 5.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 41 \end{array} \quad \begin{array}{r} 7.7 \\ \hline 31 \end{array} \quad \begin{array}{r} 8.8 \\ \hline 25 \end{array} \quad 7.9 \quad \begin{array}{r} 7.6 \\ \hline 19 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 31 \end{array} \quad \begin{array}{r} 8.6 \\ \hline 37 \end{array} \quad \begin{array}{r} 14.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline 50 \end{array} \quad \begin{array}{r} 8.8 \\ \hline 36 \end{array} \quad \begin{array}{r} 9.2 \\ \hline 20 \end{array} \quad \begin{array}{r} 8.6 \\ \hline 10 \end{array} \quad 8.4 \quad \begin{array}{r} 8.1 \\ \hline 18 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 43 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 50 \end{array}$$

$$8.4 \quad \begin{array}{r} 7.5 \\ \hline 50 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 100 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 150 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 200 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 250 \end{array}$$

$$\begin{array}{r} 6.6 \\ \hline 50 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 45 \end{array} \quad \begin{array}{r} 9.4 \\ \hline 27 \end{array} \quad \begin{array}{r} 9.7 \\ \hline 18 \end{array} \quad 8.9 \quad \begin{array}{r} 8.6 \\ \hline 26 \end{array} \quad \begin{array}{r} 8.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 6.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 9.0 \\ \hline 31 \end{array} \quad \begin{array}{r} 10.5 \\ \hline 22 \end{array} \quad \begin{array}{r} 9.8 \\ \hline 11 \end{array} \quad 9.4 \quad \begin{array}{r} 9.8 \\ \hline 10 \end{array} \quad \begin{array}{r} 10.3 \\ \hline 20 \end{array} \quad \begin{array}{r} 14.9 \\ \hline 38 \end{array} \quad \begin{array}{r} 14.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 0.9 \\ \hline 50 \end{array} \quad \begin{array}{r} 3.3 \\ \hline 33 \end{array} \quad \begin{array}{r} 5.4 \\ \hline 24 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 18 \end{array} \quad 4.5 \quad \begin{array}{r} 5.2 \\ \hline 11 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 20 \end{array} \quad \begin{array}{r} 9.3 \\ \hline 30 \end{array} \quad \begin{array}{r} 9.8 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 1.1 \\ \hline 50 \end{array} \quad \begin{array}{r} 2.8 \\ \hline 38 \end{array} \quad \begin{array}{r} 6.4 \\ \hline 17 \end{array} \quad 5.5 \quad \begin{array}{r} 6.5 \\ \hline 14 \end{array} \quad \begin{array}{r} 9.6 \\ \hline 22 \end{array} \quad \begin{array}{r} 11.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 0.4 \\ \hline 50 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 21 \end{array} \quad \begin{array}{r} 7.3 \\ \hline 12 \end{array} \quad 6.7 \quad \begin{array}{r} 7.5 \\ \hline 14 \end{array} \quad \begin{array}{r} 10.7 \\ \hline 26 \end{array} \quad \begin{array}{r} 12.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 2.2 \\ \hline 50 \end{array} \quad \begin{array}{r} 3.0 \\ \hline 40 \end{array} \quad \begin{array}{r} 7.9 \\ \hline 30 \end{array} \quad \begin{array}{r} 8.1 \\ \hline 13 \end{array} \quad 7.6 \quad \begin{array}{r} 8.7 \\ \hline 18 \end{array} \quad \begin{array}{r} 11.8 \\ \hline 33 \end{array} \quad \begin{array}{r} 13.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 50 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 42 \end{array} \quad \begin{array}{r} 6.7 \\ \hline 33 \end{array} \quad \begin{array}{r} 9.4 \\ \hline 24 \end{array} \quad \begin{array}{r} 8.6 \\ \hline 15 \end{array} \quad 8.3 \quad \begin{array}{r} 9.0 \\ \hline 17 \end{array} \quad \begin{array}{r} 11.1 \\ \hline 31 \end{array} \quad \begin{array}{r} 13.6 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 5.4 \\ \hline 50 \end{array} \quad \begin{array}{r} 6.7 \\ \hline 32 \end{array} \quad \begin{array}{r} 9.5 \\ \hline 24 \end{array} \quad \begin{array}{r} 9.0 \\ \hline 12 \end{array} \quad 8.6 \quad \begin{array}{r} 9.3 \\ \hline 14 \end{array} \quad \begin{array}{r} 11.4 \\ \hline 33 \end{array} \quad \begin{array}{r} 13.8 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 10.92 \\ \hline 19 \end{array} \quad \begin{array}{r} 7.9 \\ \hline 50 \end{array} \quad \begin{array}{r} 8.7 \\ \hline 40 \end{array} \quad \begin{array}{r} 9.1 \\ \hline 37 \end{array} \quad \begin{array}{r} 9.9 \\ \hline 13 \end{array} \quad 9.9 \quad \begin{array}{r} 11.0 \\ \hline 12 \end{array} \quad \begin{array}{r} 12.3 \\ \hline 21 \end{array} \quad \begin{array}{r} 14.7 \\ \hline 35 \end{array} \quad \begin{array}{r} 16.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 11.5 \\ \hline 50 \end{array} \quad \begin{array}{r} 11.7 \\ \hline 27 \end{array} \quad \begin{array}{r} 11.8 \\ \hline 15 \end{array} \quad 11.5 \quad \begin{array}{r} 12.1 \\ \hline 72 \end{array} \quad \begin{array}{r} 13.1 \\ \hline 27 \end{array} \quad \begin{array}{r} 15.50 \\ \hline 50 \end{array}$$

Sta.	+	π	-	Elev.	
		214.61			
64+75			12.5		
T.P.	0.28	902.71	12.18	902.43	
65			1.6		
+50			3.0		
+82			3.7		
66			4.1		
+22			4.6		
+50			5.4		
B.M.	1.07	901.21	2.64	900.07	900.14
67			4.8		
+50			5.9		
68			6.6		
+62	P.C.		7.0		
69			7.3		

$$\begin{array}{r} 23.9 \\ 50 \end{array} \quad \begin{array}{r} 16.9 \\ 36 \end{array} \quad \begin{array}{r} 13.0 \\ 26 \end{array} \quad \begin{array}{r} 12.8 \\ 15 \end{array} \quad 12.5 \quad \begin{array}{r} 12.9 \\ 12 \end{array} \quad \begin{array}{r} 13.3 \\ 28 \end{array} \quad \begin{array}{r} 14.1 \\ 50 \end{array}$$

$$\begin{array}{r} 3.9 \\ 50 \end{array} \quad \begin{array}{r} 3.9 \\ 46 \end{array} \quad \begin{array}{r} 3.2 \\ 31 \end{array} \quad \begin{array}{r} 1.6 \\ 14 \end{array} \quad 1.6 \quad \begin{array}{r} 2.1 \\ 17 \end{array} \quad \begin{array}{r} 2.5 \\ 29 \end{array} \quad \begin{array}{r} 9.6 \\ 41 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 3.8 \\ 50 \end{array} \quad \begin{array}{r} 3.6 \\ 34 \end{array} \quad \begin{array}{r} 3.2 \\ 19 \end{array} \quad 3.0 \quad \begin{array}{r} 3.4 \\ 21 \end{array} \quad \begin{array}{r} 4.1 \\ 20 \end{array} \quad \begin{array}{r} 17.4 \\ 50 \end{array}$$

$$\begin{array}{r} 4.1 \\ 50 \end{array} \quad \begin{array}{r} 4.1 \\ 30 \end{array} \quad \begin{array}{r} 2.09 \\ 30-28 \end{array} \quad \begin{array}{r} 4.2 \\ 28 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 3.8 \\ 6 \end{array} \quad 3.7 \quad \begin{array}{r} 4.3 \\ 20 \end{array} \quad \begin{array}{r} 14.3 \\ 40 \end{array} \quad \begin{array}{r} 16.3 \\ 50 \end{array}$$

$$\begin{array}{r} 3.9 \\ 50 \end{array} \quad \begin{array}{r} 4.2 \\ 30 \end{array} \quad \begin{array}{r} 2.14 \\ 30-28 \end{array} \quad \begin{array}{r} 4.1 \\ 28 \end{array} \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad 4.1 \quad \begin{array}{r} 4.6 \\ 20 \end{array} \quad \begin{array}{r} 5.6 \\ 27 \end{array} \quad \begin{array}{r} 14.7 \\ 43 \end{array} \quad \begin{array}{r} 15.6 \\ 50 \end{array}$$

$$\begin{array}{r} 4.0 \\ 50 \end{array} \quad \begin{array}{r} 4.3 \\ 30 \end{array} \quad \begin{array}{r} 2.28 \\ 30-28 \end{array} \quad \begin{array}{r} 4.2 \\ 28 \end{array} \quad \begin{array}{r} 5.4 \\ 16 \end{array} \quad \begin{array}{r} 4.8 \\ 6 \end{array} \quad 4.6 \quad \begin{array}{r} 5.3 \\ 19 \end{array} \quad \begin{array}{r} 8.1 \\ 39 \end{array} \quad \begin{array}{r} 8.9 \\ 50 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array} \quad \begin{array}{r} 4.3 \\ 30 \end{array} \quad \begin{array}{r} 2.27 \\ 30-28 \end{array} \quad \begin{array}{r} 4.4 \\ 28 \end{array} \quad \begin{array}{r} 5.9 \\ 16 \end{array} \quad \begin{array}{r} 5.6 \\ 6 \end{array} \quad 5.4 \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 6.9 \\ 30 \end{array} \quad \begin{array}{r} 8.5 \\ 40 \end{array} \quad \begin{array}{r} 9.5 \\ 50 \end{array}$$

S.W. Cor. Conc. Slob W. Steps of Schoolhouse (67+00)

$$\begin{array}{r} 2.7 \\ 50 \end{array} \quad \begin{array}{r} 2.9 \\ 30 \end{array} \quad \begin{array}{r} 1.25 \\ 30-28 \end{array} \quad \begin{array}{r} 3.9 \\ 28 \end{array} \quad \begin{array}{r} 5.4 \\ 17 \end{array} \quad \begin{array}{r} 5.1 \\ 6 \end{array} \quad 4.8 \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 26 \end{array} \quad \begin{array}{r} 8.3 \\ 43 \end{array} \quad \begin{array}{r} 8.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 30 \end{array} \quad \begin{array}{r} 3.14 \\ 30-28 \end{array} \quad \begin{array}{r} 5.3 \\ 28 \end{array} \quad \begin{array}{r} 6.2 \\ 19 \end{array} \quad \begin{array}{r} 6.0 \\ 6 \end{array} \quad 5.9 \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad \begin{array}{r} 6.7 \\ 29 \end{array} \quad \begin{array}{r} 8.9 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 5.1 \\ 30 \end{array} \quad \begin{array}{r} 3.35 \\ 30-28 \end{array} \quad \begin{array}{r} 5.4 \\ 28 \end{array} \quad \begin{array}{r} 7.1 \\ 18 \end{array} \quad \begin{array}{r} 6.8 \\ 7 \end{array} \quad 6.6 \quad \begin{array}{r} 7.0 \\ 13 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array} \quad \begin{array}{r} 7.0 \\ 28 \end{array} \quad \begin{array}{r} 8.3 \\ 41 \end{array} \quad \begin{array}{r} 8.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.9 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 30 \end{array} \quad \begin{array}{r} 3.47 \\ 30-28 \end{array} \quad \begin{array}{r} 5.6 \\ 28 \end{array} \quad \begin{array}{r} 7.6 \\ 17 \end{array} \quad \begin{array}{r} 7.2 \\ 7 \end{array} \quad 7.0 \quad \begin{array}{r} 7.5 \\ 14 \end{array} \quad \begin{array}{r} 7.5 \\ 26 \end{array} \quad \begin{array}{r} 7.7 \\ 50 \end{array}$$

$$\begin{array}{r} 5.3 \\ 50 \end{array} \quad \begin{array}{r} 5.3 \\ 30 \end{array} \quad \begin{array}{r} 3.63 \\ 30-28 \end{array} \quad \begin{array}{r} 5.7 \\ 28 \end{array} \quad \begin{array}{r} 8.0 \\ 17 \end{array} \quad \begin{array}{r} 7.7 \\ 8 \end{array} \quad 7.3 \quad \begin{array}{r} 7.8 \\ 15 \end{array} \quad \begin{array}{r} 7.9 \\ 20 \end{array} \quad \begin{array}{r} 7.1 \\ 27 \end{array} \quad \begin{array}{r} 6.6 \\ 50 \end{array}$$

Sta	+	π	-	Elev.
		901.21		
69+06			7.3	
+50			7.6	
70			7.8	
+50			8.0	
71			8.6	
+50			9.2	
T.P.	9.91	901.93	9.19	892.02
72			10.3	
+32	P.T.		10.4	
+61	P.C.		10.1	
73			9.5	
+50			8.6	
74			7.8	

no pot grade beyond 100

$\frac{7.7}{50}$ $\frac{8.0}{32}$ $\frac{8.2}{18}$ $\frac{7.6}{8}$ 7.3 $\frac{7.8}{15}$ $\frac{7.9}{20}$ $\frac{7.1}{27}$ $\frac{6.6}{50}$

$\frac{9.2}{50}$ $\frac{9.4}{34}$ $\frac{9.4}{17}$ $\frac{8.0}{10}$ 7.6 $\frac{8.0}{14}$ $\frac{8.2}{20}$ $\frac{6.8}{28}$ $\frac{5.0}{50}$

$\frac{9.4}{50}$ $\frac{9.7}{37}$ $\frac{9.6}{21}$ $\frac{8.2}{10}$ 7.8 $\frac{8.3}{19}$ $\frac{6.6}{28}$ $\frac{5.8}{50}$

$\frac{10.0}{50}$ $\frac{9.7}{33}$ $\frac{10.2}{23}$ $\frac{8.7}{19}$ $\frac{8.5}{9}$ $\frac{8.2}{8.0}$ $\frac{8.0}{11}$ $\frac{6.6}{18}$ $\frac{5.8}{28}$ $\frac{5.0}{50}$

$\frac{11.9}{50}$ $\frac{10.4}{39}$ $\frac{11.4}{34}$ $\frac{10.5}{23}$ $\frac{9.1}{16}$ $\frac{8.8}{10}$ 8.6 $\frac{9.0}{10}$ $\frac{9.1}{13}$ $\frac{8.7}{16}$ $\frac{7.4}{25}$ $\frac{6.0}{50}$

$\frac{13.3}{50}$ $\frac{12.0}{39}$ $\frac{10.9}{26}$ $\frac{9.7}{17}$ 9.2 $\frac{9.7}{9}$ $\frac{9.4}{14}$ $\frac{7.7}{23}$ $\frac{6.0}{50}$

$\frac{13.0}{50}$ $\frac{11.2}{21}$ $\frac{10.4}{10}$ 10.3 $\frac{10.6}{12}$ $\frac{9.4}{20}$ $\frac{8.6}{50}$

$\frac{14.2}{50}$ $\frac{12.9}{33}$ $\frac{10.6}{11}$ 10.4 $\frac{10.8}{11}$ $\frac{11.9}{21}$ $\frac{9.9}{34}$ $\frac{8.6}{50}$

$\frac{14.9}{50}$ $\frac{12.8}{27}$ $\frac{10.6}{12}$ 10.1 $\frac{10.3}{14}$ $\frac{11.2}{25}$ $\frac{9.7}{36}$ $\frac{7.5}{42}$ $\frac{7.5}{50}$

$\frac{13.8}{50}$ $\frac{11.6}{20}$ $\frac{10.2}{12}$ 9.5 $\frac{10.0}{15}$ $\frac{10.7}{20}$ $\frac{9.5}{26}$ $\frac{8.6}{34}$ $\frac{6.5}{40}$ $\frac{5.7}{50}$

$\frac{11.2}{50}$ $\frac{9.5}{32}$ $\frac{8.5}{16}$ $\frac{9.1}{11}$ 8.6 $\frac{8.9}{11}$ $\frac{9.2}{17}$ $\frac{8.6}{26}$ $\frac{4.6}{35}$ $\frac{4.2}{50}$

$\frac{7.0}{50}$ $\frac{5.5}{24}$ $\frac{8.4}{14}$ 7.8 $\frac{8.2}{18}$ $\frac{8.5}{21}$ $\frac{7.8}{26}$ $\frac{2.9}{37}$ $\frac{2.9}{50}$

Sta.	+	π	-	Elev.
		901.93		
74+50			7.3	
75			7.1	
+16	P.T.		7.0	
+50			6.6	
76			7.0	
+50			8.3	
77			10.1	
T.P.	13.04	913.39	1.58	900.35
75				
+16				
+50				
76				
+50				
T.P.	8.14	914.53	7.00	906.39

$$\frac{1.7}{50} \quad \frac{0.7}{29} \quad \frac{5.0}{21} \quad \frac{7.5}{15} \quad 7.3 \quad \frac{8.0}{17} \quad \frac{7.6}{23} \quad \frac{1.1}{35} \quad \frac{1.0}{39} \quad \frac{1.4}{50}$$

$$\frac{7.5}{16} \quad 7.1 \quad \frac{7.4}{14} \quad \frac{7.9}{17}$$

$$\frac{7.4}{16} \quad 7.0 \quad \frac{7.2}{14} \quad \frac{7.7}{16}$$

$$\frac{6.9}{17} \quad 6.6 \quad \frac{7.0}{14} \quad \frac{8.0}{16}$$

$$\frac{7.2}{19} \quad 7.0 \quad \frac{7.4}{13} \quad \frac{8.5}{16}$$

$$\frac{8.6}{20} \quad 8.3 \quad \frac{8.7}{12} \quad \frac{9.5}{15}$$

$$\frac{10.2}{20} \quad 10.1 \quad \frac{10.5}{9} \quad \frac{11.2}{15} \quad \frac{8.2}{29} \quad \frac{10.7}{50}$$

$$\frac{12.7}{31} \quad \frac{10.2}{33} \quad \frac{11.0}{50} \quad \frac{13.2}{75}$$

$$\frac{9.2}{33} \quad \frac{10.3}{50} \quad \frac{12.5}{75}$$

$$\frac{8.0}{36} \quad \frac{9.1}{50} \quad \frac{11.5}{75}$$

$$\frac{8.4}{33} \quad \frac{10.3}{50} \quad \frac{12.7}{75}$$

$$\frac{13.3}{32} \quad \frac{16.1}{50}$$

Sta.	+	π	-	Elev
		914.53		

75

+16

+50

76

+50

77

T.P.	0.83	902.63	12.73	901.80
------	------	--------	-------	--------

+50			12.6	
-----	--	--	------	--

78

+43

T.P.	0.75	890.08	13.30	889.33
------	------	--------	-------	--------

78 + 78			2.1	
---------	--	--	-----	--

1

+43			3.8	
-----	--	--	-----	--

80 + 78			5.2	
---------	--	--	-----	--

$$\frac{8.5}{75} \quad \frac{7.6}{50} \quad \frac{8.2}{35}$$

$$\frac{6.8}{75} \quad \frac{7.0}{50} \quad \frac{6.5}{37}$$

$$\frac{3.9}{75} \quad \frac{3.8}{50} \quad \frac{3.3}{38}$$

$$\frac{3.2}{50} \quad \frac{3.0}{50} \quad \frac{2.8}{42}$$

$$\frac{5.2}{75} \quad \frac{5.2}{50} \quad \frac{5.6}{42}$$

$$\frac{9.2}{75} \quad \frac{10.9}{50} \quad \frac{11.9}{40}$$

$$\frac{0.0}{75} \quad \frac{1.1}{50} \quad \frac{1.4}{47} \quad \frac{10.8}{26} \quad \frac{13.0}{20} \quad \frac{13.2}{14} \quad 12.6 \quad \frac{12.9}{10} \quad \frac{13.7}{14} \quad \frac{12.8}{19} \quad \frac{16.6}{37} \quad \frac{17.7}{50}$$

$$\frac{2.4}{75} \quad \frac{4.7}{50} \quad \frac{5.4}{46}$$

$$\frac{7.9}{50} \quad \frac{14.0}{28}$$

$$\frac{10.1}{28} \quad \frac{2.9}{20} \quad \frac{2.5}{14} \quad 2.1 \quad \frac{2.5}{12} \quad \frac{10.7}{31} \quad \frac{10.8}{35} \quad \frac{13.6}{50}$$

$$\frac{4.5}{21} \quad \frac{4.2}{17} \quad \frac{4.2}{13} \quad 3.8 \quad \frac{4.3}{13} \quad \frac{13.9}{30} \quad \frac{17.4}{50}$$

$$\frac{+2.3}{50} \quad \frac{0.9}{37} \quad \frac{4.7}{30} \quad \frac{4.7}{23} \quad \frac{5.9}{21} \quad \frac{5.5}{16} \quad 5.2 \quad \frac{5.9}{13} \quad \frac{14.4}{29} \quad \frac{17.8}{50}$$

Sta.	+	π	-	Elev.
		890.08		
79			5.9	
+50			7.8	
80			9.9	
T.P.	0.90	879.86	11.12	878.96
+33			0.9	
+66			2.4	
+78			2.9	
81			3.8	
+50			5.7	
+82			6.5	
82			6.7	
+19	E Edgerton		7.09	
B.M.			7.09	872.77 (872.84)

$$\frac{4.3}{50} \quad \frac{0.8}{37} \quad \frac{5.2}{24} \quad \frac{6.3}{22} \quad \frac{5.9}{15} \quad 5.9 \quad \frac{6.5}{13} \quad \frac{13.7}{26} \quad \frac{16.6}{50}$$

$$\frac{6.8}{50} \quad \frac{2.6}{39} \quad \frac{6.9}{30} \quad \frac{8.0}{22} \quad \frac{7.9}{11} \quad 7.8 \quad \frac{8.1}{14} \quad \frac{9.9}{28} \quad \frac{11.9}{50}$$

$$\frac{6.7}{50} \quad \frac{6.3}{38} \quad \frac{10.6}{29} \quad \frac{10.3}{18} \quad 9.9 \quad \frac{10.0}{13} \quad \frac{10.7}{17} \quad \frac{9.9}{24} \quad \frac{12.4}{50}$$

$$\frac{10.4}{50} \quad \frac{10.9}{38} \quad \frac{3.1}{29} \quad \frac{1.5}{24} \quad \frac{1.2}{20} \quad 0.9 \quad \frac{1.5}{14} \quad \frac{4.5}{22} \quad \frac{4.6}{36} \quad \frac{5.8}{50}$$

$$\frac{4.7}{50} \quad \frac{4.4}{38} \quad \frac{5.3}{32} \quad \frac{2.7}{19} \quad \frac{2.6}{11} \quad 2.4 \quad \frac{3.3}{16} \quad \frac{6.9}{23} \quad \frac{8.0}{50}$$

$$\frac{5.7}{50} \quad \frac{6.6}{34} \quad \frac{6.1}{26} \quad \frac{3.3}{18} \quad \frac{3.1}{11} \quad 2.9 \quad \frac{3.5}{16} \quad \frac{9.4}{29} \quad \frac{11.6}{50}$$

$$\frac{8.3}{50} \quad \frac{9.6}{39} \quad \frac{8.9}{30} \quad \frac{4.3}{19} \quad \frac{4.0}{11} \quad 3.8 \quad \frac{4.5}{15} \quad \frac{11.4}{29} \quad \frac{12.8}{50}$$

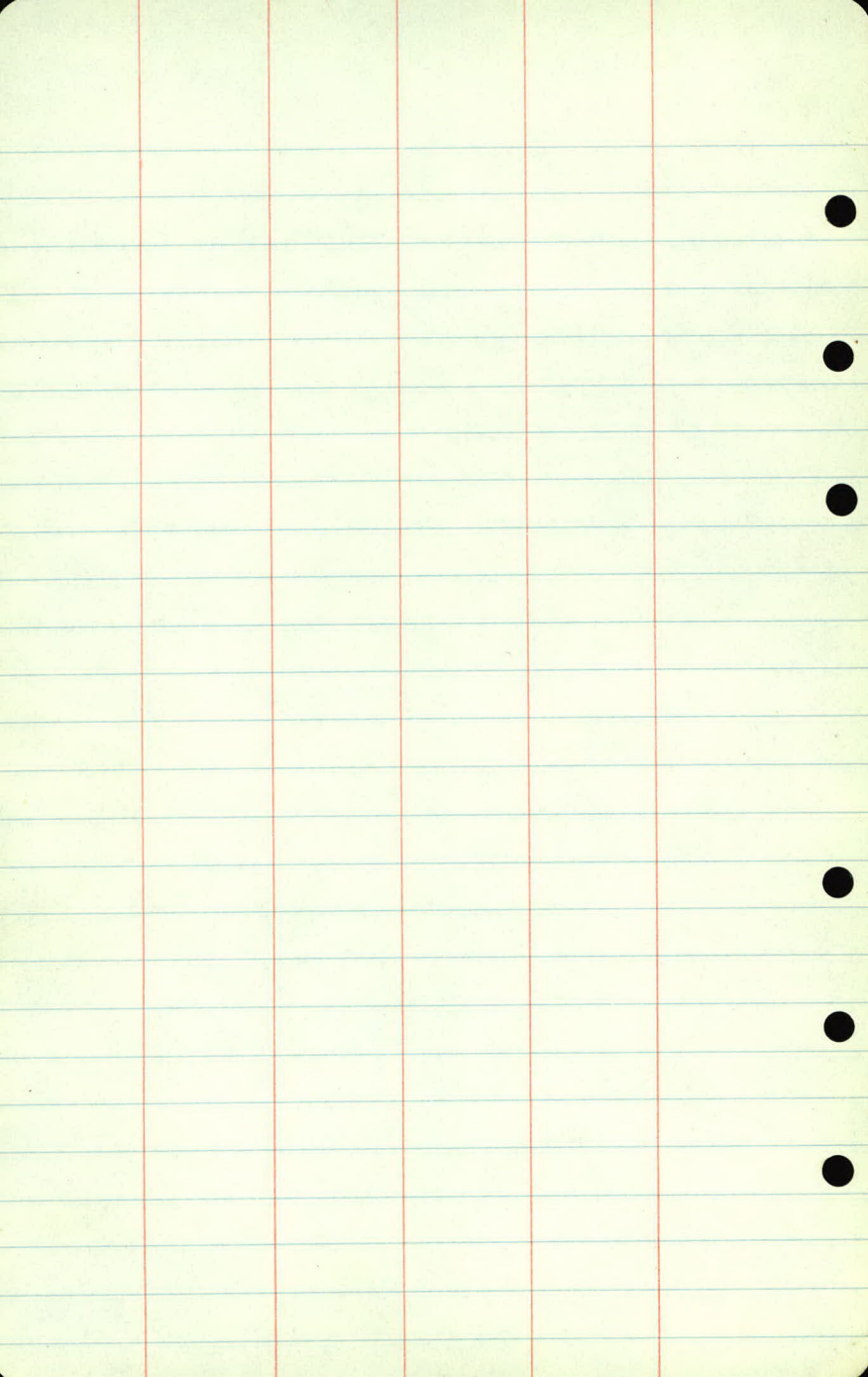
$$\frac{13.6}{50} \quad \frac{12.6}{35} \quad \frac{6.7}{22} \quad \frac{6.1}{10} \quad 5.7 \quad \frac{6.1}{10} \quad \frac{6.5}{18} \quad \frac{12.3}{31} \quad \frac{13.5}{50}$$

$$\frac{11.7}{50} \quad \frac{11.7}{39} \quad \frac{7.5}{29} \quad \frac{7.0}{13} \quad 6.5 \quad \frac{7.1}{17} \quad \frac{7.5}{28} \quad \frac{11.5}{38} \quad \frac{12.2}{50}$$

$$\frac{6.4}{50} \quad \frac{6.8}{19} \quad 6.7 \quad \frac{7.1}{19} \quad \frac{7.6}{50}$$

$$\frac{6.21}{50} \quad 7.09 \quad \frac{7.58}{50}$$

Top Mon. Little Canada Rd & Edgerton



LITTLE CANADA RD.

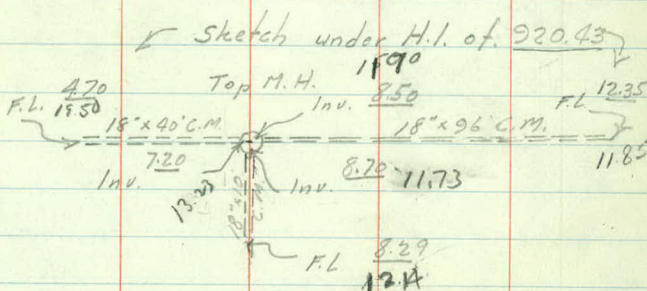
Profile Levels in E of
Special Ditch on Rt.
from Sta. 1+25 to Sta. 10+98

Sta.	+	π	-	Elev.	
B.M.	3.35	927.00		923.65	
1 + 25			5.8	21.2	9 + 85
+ 50			6.3	20.7	9 + 60
+ 75			6.6	20.4	9 + 35
2			7.2	19.8	9 + 10
+ 25			7.8	19.2	8 + 85
+ 50			8.5	18.5	8 + 60
+ 75			8.6	18.4	8 + 35
3			8.7	18.3	8 + 10
+ 25			8.6	18.4	7 + 85
+ 50			8.8	18.2	7 + 60
+ 75			8.7	18.3	7 + 35
+ 89	F.L. 12" C.M.		9.03	17.97	7 + 21
4 + 11	F.L. 12" C.M.		9.12	17.88	6 + 99
+ 25			8.7	18.3	6 + 85
+ 50			8.8	18.2	6 + 60
T.P.	3.01	924.20	5.81	921.19	
+ 75			6.5	17.7	6 + 35
5			6.9	17.3	6 + 10
+ 25			7.0	17.2	5 + 85
+ 50	F.L. 18" C.M.		7.77	16.43	5 + 60
+ 62	F.L. 18" C.M.		7.81	16.39	5 + 48
+ 75			7.6	16.6	5 + 35
6			8.1	16.1	5 + 10
+ 25			8.2	16.0	4 + 85

Top SW. Cor. Conc. Platform 37' Lt 0435

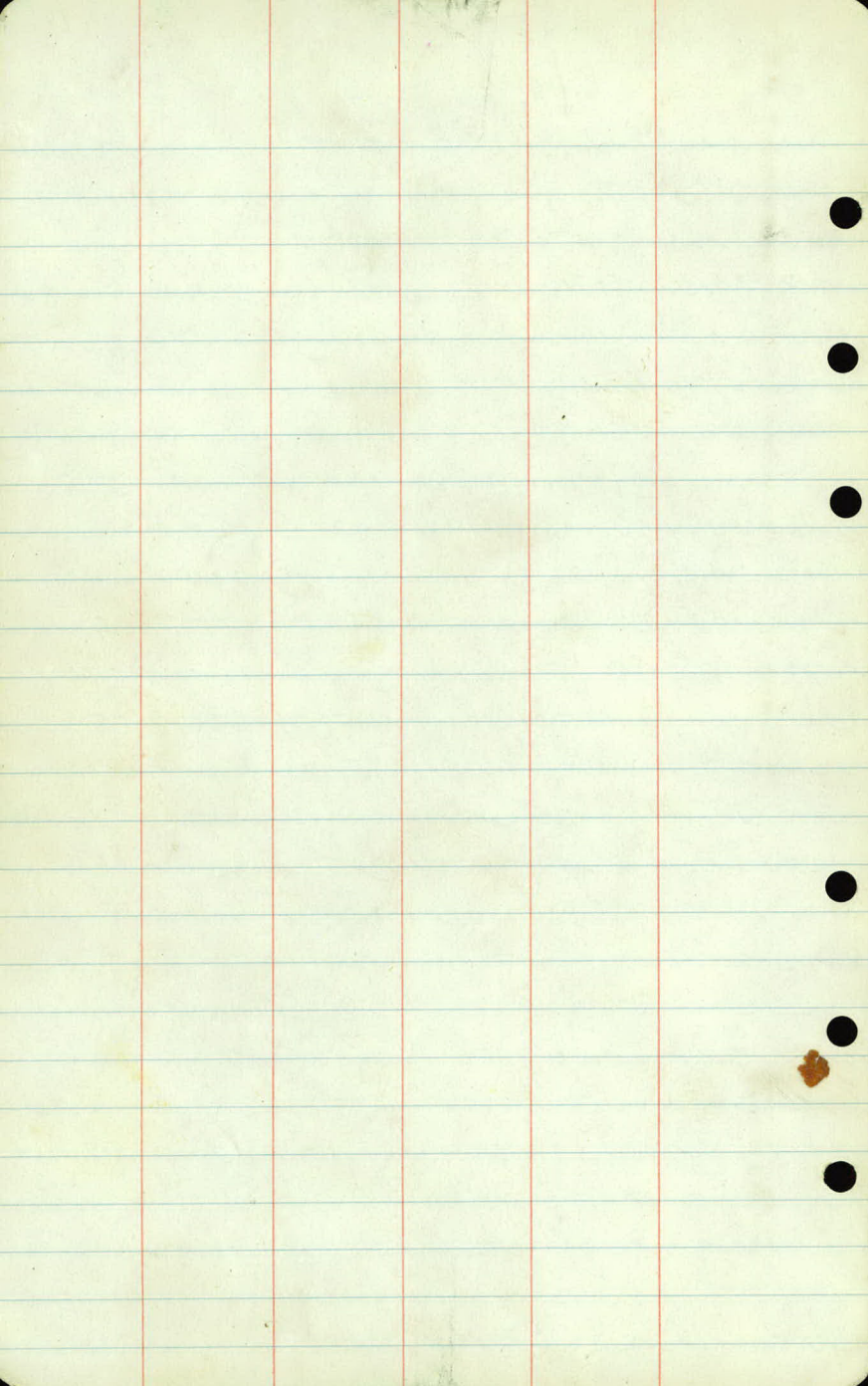
Sta	+	π	-	Elev.	
		924.20			
6+50			8.5	15.7	4+60
+75			8.7	15.5	4+35
7			9.4	14.8	4+10
+25			9.6	14.6	3+85
+50			9.9	14.3	3+60
+75			9.7	14.5	3+35
8			9.7	14.5	3+10
+21	X Drain F.L. 9" Perf. C.M.		9.14	15.06	2+89
+25			9.9	14.8	2+85
+50			9.3	14.9	2+60
+75			9.3	14.9	2+35
9			9.7	14.5	2+10
+25			10.1	14.1	1+85
+50			10.7	13.5	1+60
+57	F.L. 18" C.M.		11.21	12.99	1+53
+91	F.L. 18" C.M.		11.87	12.33	1+19
10			11.2	13.0	1+10
+25			11.2	13.0	0+85
T.P.	2.50	920.43	6.27	917.93	
+50			7.7	12.70	0+60
+75			7.8	12.60	0+35
+98	F.L. 18" C.M.		8.29	12.11	0+12
Lake Level Bench.			7.64	912.79	8.17
Top Water - 4-1-41			14.90	97.86	

Pipe Placed to Drain Spring in Road Bed
 Suggest Placing Pipe in wet spot at 8+50



Sta.	L	π	-	Elev.	
		920.43			
T.P.	9.61	929.51	0.53	919.90	
T.P.			4.58	924.93	924.93 -

Spk P.P. Lt. 15+72



PLAN SURVEY

Little Canada Road

Cemetery to Edgerton

INDEX:

Alignment	1-3
Topography	4-7
X-Sections	7-19

Rec'd Mar. 23, 1959
R.C.

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

+32.35	P.T.		$3^{\circ} 42'$
--------	------	--	-----------------

72			$3^{\circ} 23'$
----	--	--	-----------------

+50			$2^{\circ} 53'$
-----	--	--	-----------------

71			$2^{\circ} 23' \Delta = 7^{\circ} 24' R$
----	--	--	--

+50			$1^{\circ} 53' D = 2^{\circ}$
-----	--	--	-------------------------------

+47.63	P.I.		$T = 185.28$
--------	------	--	--------------

70			$1^{\circ} 23' L = 370.00$
----	--	--	----------------------------

+50			$0^{\circ} 53' R = 2864.93$
-----	--	--	-----------------------------

69			$0^{\circ} 23'$
----	--	--	-----------------

68+62.35	PC		$0^{\circ} 00'$
----------	----	--	-----------------

69+05.35	POST.		
----------	-------	--	--

FK
RG
KP
JH

March 17, 1959
Clear Calm 30°

2

RT

11

TP

22.20

34.66

R.R. Spike

TP

43.73

33.09

60.91

x

x

x

x

Fe Post in Conc

24.70

Granite Mount 1/4 1/4 Cor

SW 1/4 Sec 5-29-22

Sta Point ΔL ΔR

82+18.70 ∇ Edgerton

+16.15 P.T. $2^{\circ}33'$

75 $2^{\circ}23.4'$

+50 $1^{\circ}53.4'$ $\Delta = 5^{\circ}06' Lt$

74 $1^{\circ}23.4'$ $D = 2^{\circ}$

73+88.75 P.I. $T = 127.60$

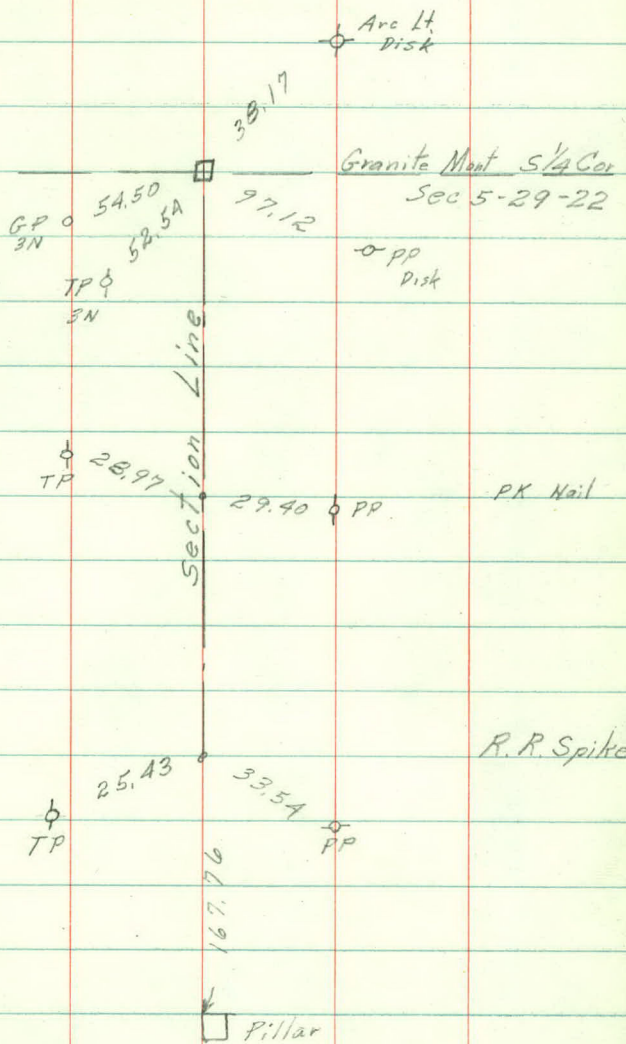
+50 $0^{\circ}53.4'$ $L = 255.00$

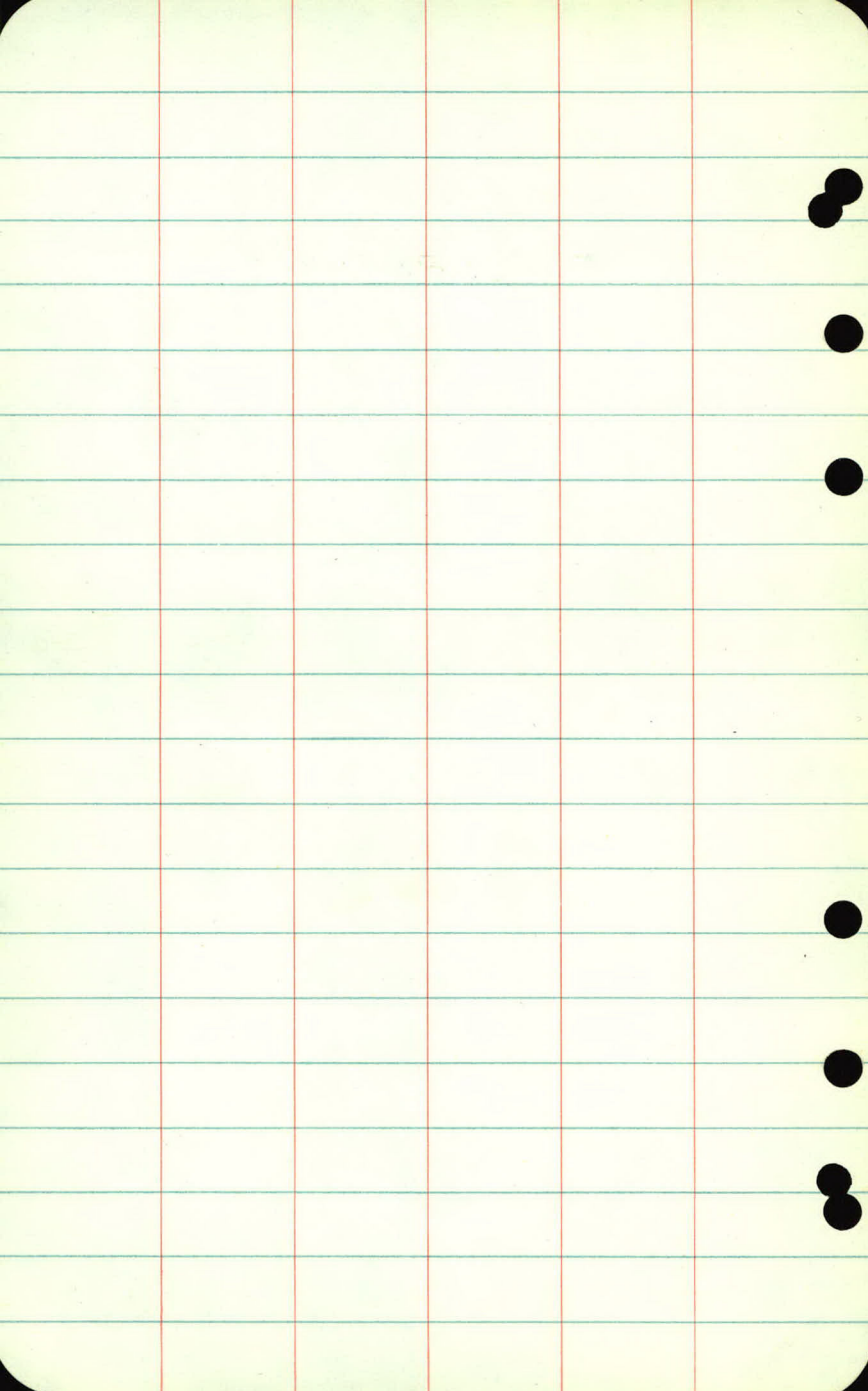
73 $0^{\circ}23.4'$ $R = 2864.93$

72+61.15 P.C. $0^{\circ}00'$

March 17, 1959
Clear 30° Calm

3





TOPOGRAPHY

	LT	£	RT
73		BT 14 15	
+90 TP 19		+73 BT 17-15	+90 20 BE 39
		+20 R. Tie Fe BT	+81 GP 34
+35 Ent LT		+12 R. Tie Ho LT	+28 GP 34
+04 S.W. Cor Ho 49.5	+32 BT 17-13	+21 2' P. 1/4 18.5	+24 Arc LT 19
72		+00 BT End Fe 17 12 20	+22 E. Fe 16.5
	+85 TP 39		
+84 GP 28		+50 BT Fe 18 12 23	
	+17 TP 32.5		
71		+00 BT Fe 13-12 26	
		+50 BT 14 13.5	+84 PP 25
	+39 Ent 12"x26" CM 23		+96 8"E 28
+50 PP 44		+55 T.P. 28	+60 2' P. 1/4 27
		+50 Ent RT	+77 29
	+10 T.P. 25		
		+23 6"E 30	
70		BT Fe 13 16 28.7	+42 2' P. 7/16 28
+85 Ent 12"x24" CM 22.5	+76 Tw. 20' Lt 51		+67 14"P 30
+92 E. Fe 27	+50 16" BE 51	+50 Fe 28.5	+96 6"E 31
			+53 PP 27
		+50 BT 10-17	
+06 Cor. Wall 29.0	+25 TP 23		
69	+04 20"E Wall 37	B.T. Fe 28.7 10-17 27.7	
+67 MH 11		+88 2' P. 1/4 27	+75 E.E. 28
	+65 12"E 37	+87 Fe Cor 27	+51 32" BE 28
		+62 Wall 28.2	+65 Ent RT
	+41 TP 21		
68		+00 Wall 28.3	

March 17, 1959

March 19, 1959

5

16.7

38.2

16.7
38.2

60" Chain Link

Cemetery

13" Wall Wire

4' Stone Wall

5' Chain Link Fe

M.H. 30' Deep
Tall Cable 5.3' Deep
It Can be Lowered 0.55'

2' Stone Wall

AT 88° LT

.K

RT

78

19 15 10

$$+91 \frac{TP}{21}$$

$$+91 \frac{PP}{26}$$

$$+48 \frac{STP}{47}$$

$$+79 \frac{18''0}{43}$$

$$+89 \frac{18''0}{37}$$

$$+83 \frac{STP}{45}$$

$$+80 \frac{20''0}{30}$$

$$+95 \frac{STP}{44}$$

$$+53 \frac{14''0}{33}$$

$$+69 \frac{17''0}{32}$$

77

$$\frac{BT}{18 \ 12}$$

$$+32 \frac{20''0}{29}$$

$$+97 \frac{18''0}{39}$$

$$+55 \frac{18''0}{48}$$

$$+55 \frac{TP}{28}$$

$$+53 \frac{PP}{27}$$

$$+48 \frac{16''0}{50}$$

$$+47 \frac{24''0}{39}$$

76

$$\frac{BT}{16 - 13.5}$$

$$+57 \frac{28''0}{36}$$

$$+31 \frac{TP}{26}$$

$$+15 \frac{PP}{27}$$

75

$$\frac{BT}{12 \ 13}$$

$$+60 \frac{30''0}{43}$$

$$+50 \frac{BT}{11 \ 14}$$

$$+02 \frac{MH}{12.5}$$

74

$$\frac{BT}{10 \ 15}$$

$$+83 \frac{TP}{22}$$

$$+69 \frac{PP}{31}$$

$$+60 \frac{BR}{31}$$

$$+24 \frac{ER}{11}$$

$$+50 \frac{BT}{16}$$

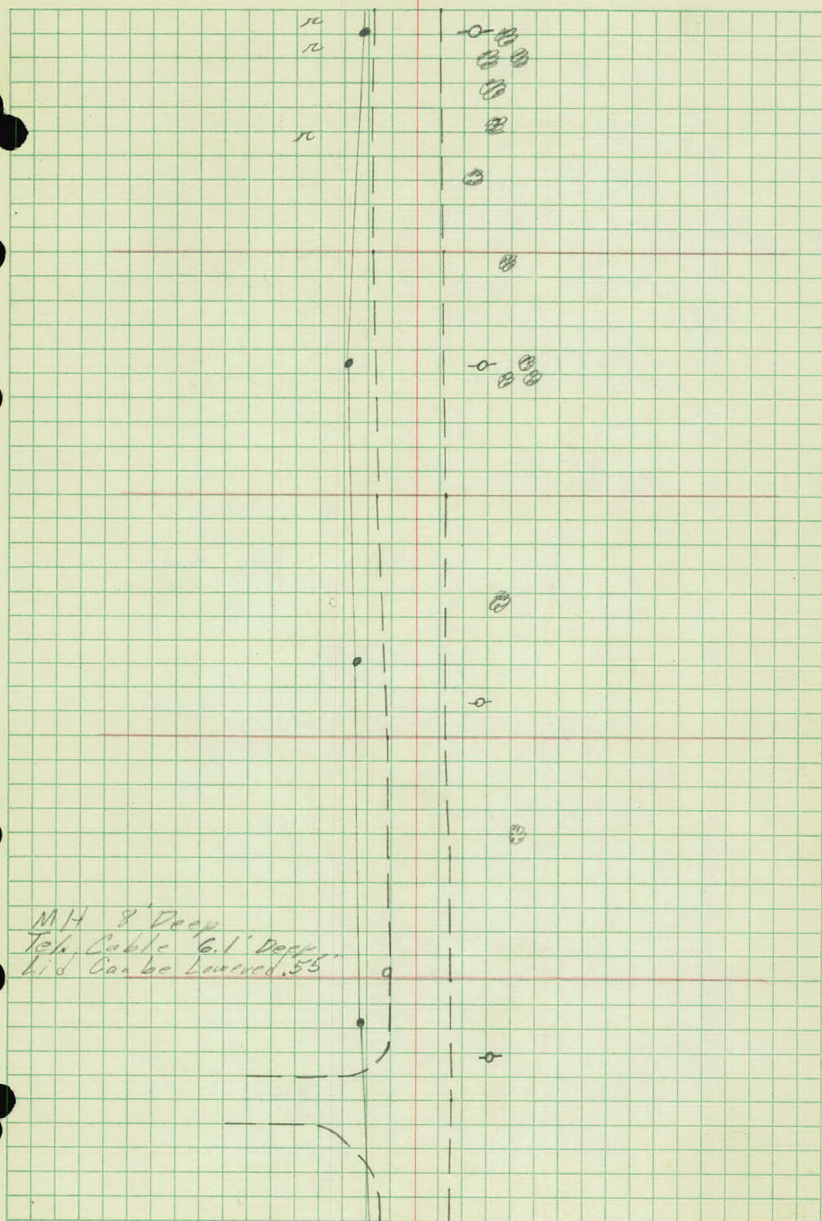
$$+38 \frac{ER}{40}$$

$$+12 \frac{BR}{15}$$

73

March 19, 1959

6



MH 8' Deep
Tch Cable 6.1' Deep
Lid Can be Lowered .55'

Lt

E

RT

$$+07 \frac{ER}{61}$$

$$+07 \frac{ER}{76}$$

82

$$+93 \frac{GP}{48}$$

$$+79 \frac{POR}{24}$$

$$+92 \frac{GP}{56}$$

$$+93 \frac{POR}{37}$$

$$+75 \frac{TP}{30.5}$$

$$+70 \frac{30^{\circ}O}{55}$$

$$+58 \frac{BR}{17}$$

$$+77 \frac{BR}{19}$$

$$+27 \frac{10^{\circ}E}{38}$$

$$+16 \frac{10^{\circ}E}{40}$$

81

$$+02 \frac{TP}{29}$$

$$\frac{BT}{18 \ 13}$$

$$+11 \frac{4^{\circ}W}{35}$$

$$+13 \frac{STP}{28}$$

$$+83 \frac{PP}{27}$$

$$+13 \frac{Pine}{55}$$

$$+34 \frac{Pine}{55}$$

80

$$+02 \frac{TP}{29}$$

$$\frac{BT}{19-11}$$

$$+16 \frac{TW/8^{\circ}O}{21}$$

$$+87 \frac{Pine}{43}$$

$$+92 \frac{30^{\circ}O}{23}$$

$$+68 \frac{Pine}{42}$$

$$+37 \frac{R.Tie}{Ent}$$

$$+57 \frac{26^{\circ}O}{26}$$

$$+44 \frac{EEnt}{28}$$

$$+30 \frac{PP}{24.5}$$

$$+21 \frac{20^{\circ}O}{21}$$

79

$$+09 \frac{TP}{29}$$

$$\frac{BT}{19 \ 10}$$

$$+55 \frac{MH}{18.5}$$

$$+88 \frac{Tw. 18^{\circ}E}{40}$$

$$+60 \frac{STP}{42}$$

$$+80 \frac{6^{\circ}E}{44}$$

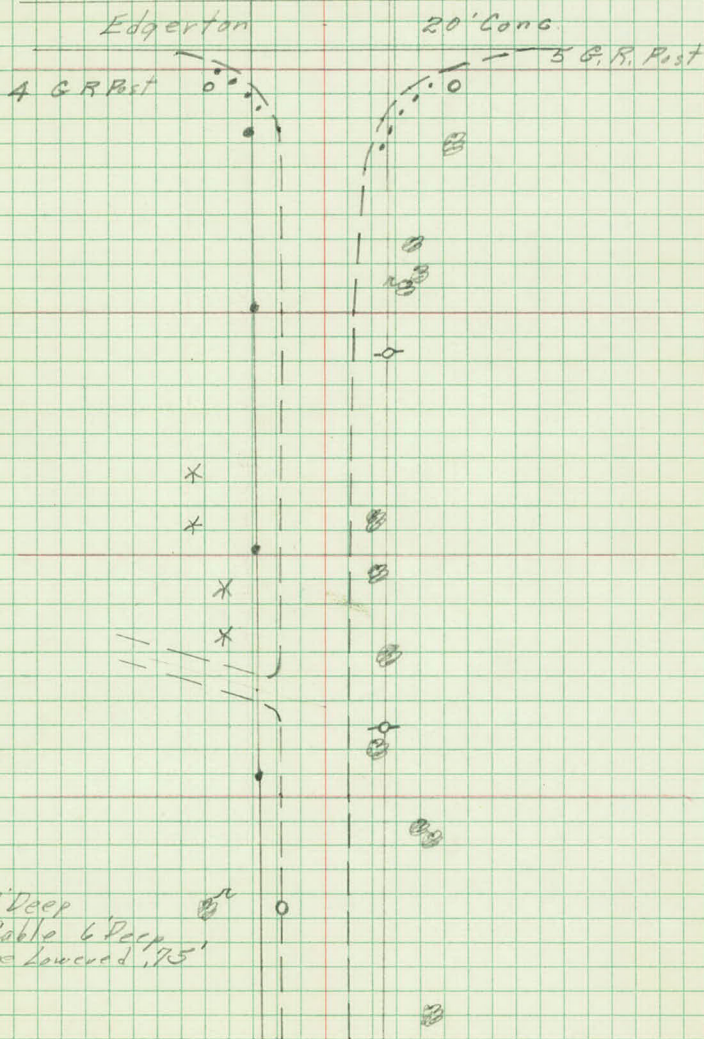
$$+56 \frac{18^{\circ}O}{49}$$

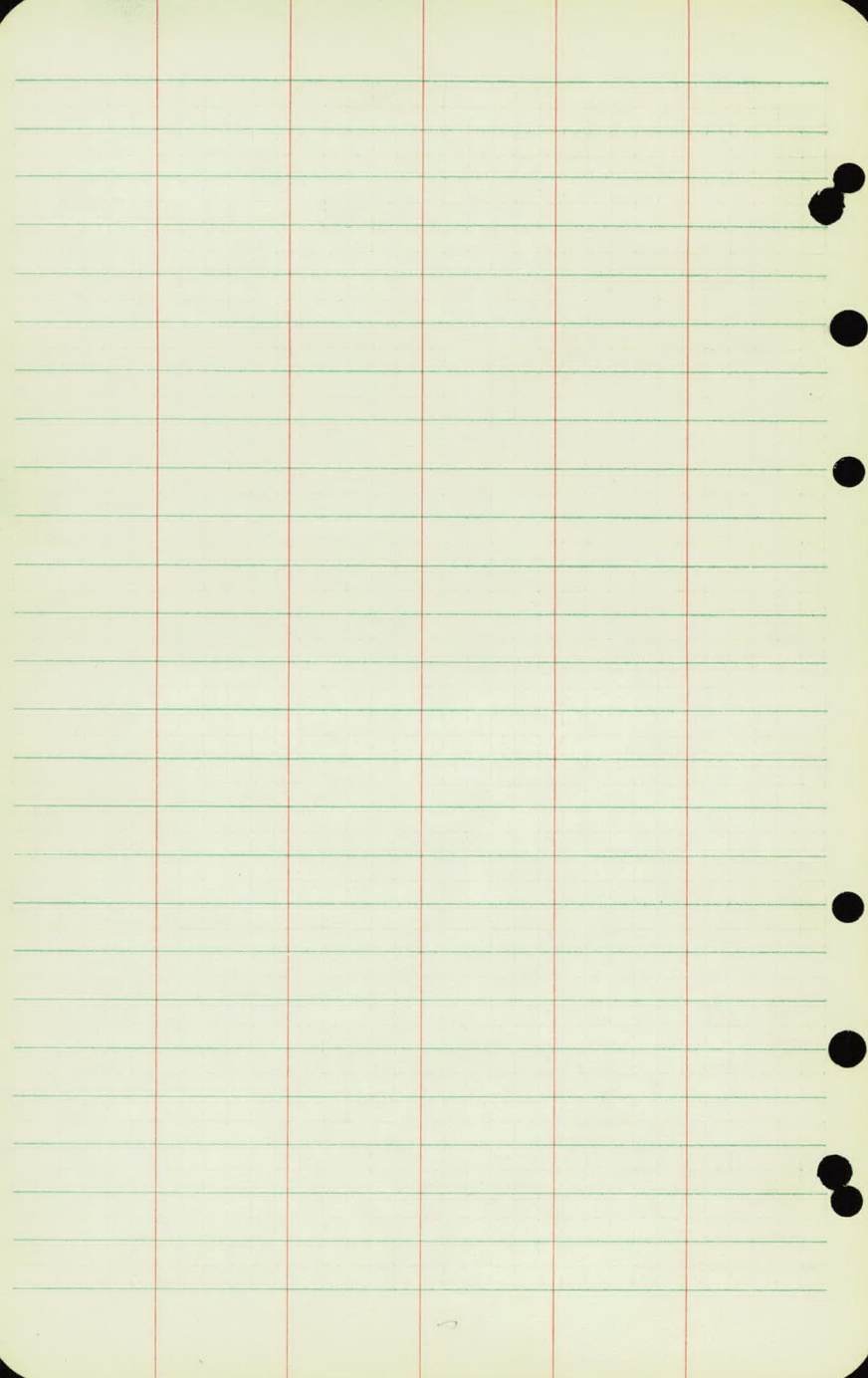
78

$$+10 \frac{16^{\circ}O}{43}$$

± March 19, 1959

7





March 19, 1959

8

x-sections

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	0.06	900.20		
----	------	--------	--	--

				900.14
--	--	--	--	--------

			94.3	
--	--	--	------	--

68+62				
-------	--	--	--	--

			5.9	
--	--	--	-----	--

			94.0	
--	--	--	------	--

69				
----	--	--	--	--

			6.2	
--	--	--	-----	--

			93.7	
--	--	--	------	--

+50				
-----	--	--	--	--

			6.5	
--	--	--	-----	--

			93.6	
--	--	--	------	--

70				
----	--	--	--	--

			6.6	
--	--	--	-----	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

71				
----	--	--	--	--

March 19, 1959

9

Lt

Rt

Top S.W. Cor Conc Slab W. of Steps - School House

PC

90.39

92.0

92.6

93.0

93.3

93.1

94.1

94.5

94.8

9.81 8.2 7.6 7.2 6.9 7.1 6.1 5.7 5.4
FLIP CM 19 15 9 13 24 37 50
23

91.2

91.6

91.6

91.2

✓

9.0 8.6 8.6 9.0
28 35 40 50

90.1

90.9

91.9

92.4

92.6

92.3

92.4

93.7

94.0

10.1 9.3 8.3 7.8 7.6 7.9 7.8 6.5 6.2
32 20 17 11 12 15 22 26
Fe

90.2

89.2

✓

10.0 11.0
39 50

Sta	+	π	-	Elev.
-----	---	-------	---	-------

900.20

71+50

✓

TP	6.39	898.46	8.13	892.07
----	------	--------	------	--------

72

✓

+22 in Line With Fe

+40

March 18, 1939

9

Lt

Rt

88.7	90.0	90.6	91.6	91.9	92.0	91.8	92.2	92.9	93.6
5	10.2	9.6	8.6	8.3	8.2	8.4	8.0	7.3	6.6
40	28	22	18	11		11	15	18	23
									Fe

87.4

12.8

50

71+50



88.2	88.8	90.7	91.3	91.4	91.8	91.7	92.0	92.9	93.1
10.3	9.7	7.8	7.2	7.1	6.7	6.8	6.5	5.6	5.4
46	36	22	18	13		10	16	20	32
									Fe

88.3

10.2

H0

50



89.0	88.6	89.4	90.1	91.0	91.5	91.7	91.7	92.5	93.3	93.4	93.8
9.5	9.9	9.1	8.4	7.5	7.0	6.8	6.8	6.0	5.2	5.1	4.7
50	48	36	23	17	11	✓	11	16	27	38	50

89.9

88.7

89.8

90.6

91.4

91.8

91.7

91.7

90.7

91.5

91.7

10.6	9.8	8.7	7.9	7.1	6.7	6.8	6.8	7.8	7.0	6.8
50	35	22	18	11		10	14	24	29	33

94.1

93.8

4.4

4.7



50

42

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		898.46		
--	--	--------	--	--

72+67				
-------	--	--	--	--

✓				
---	--	--	--	--

+93				
-----	--	--	--	--

73				
----	--	--	--	--

✓				
---	--	--	--	--

TP	8.11	902.30	4.27	894.19
----	------	--------	------	--------

+23				
-----	--	--	--	--

March 19, 1959

10

		Lt						Rt			
89.0	89.8	90.1	91.0	91.8	92.0	92.0	91.6	90.9	92.4	94.4	
25	8.7	8.4	7.5	6.7	6.5	6.5	6.9	7.6	6.1	4.1	
33	25	20	15	6		14	18	26	36	42	
		88.3	88.0							94.6	
		10.2	10.5							39	
		37	50							50	
88.7	88.4	89.0	89.6	91.1	92.1	92.4	92.3	91.3	91.3	95.7	95.8
28	10.1	9.5	8.9	7.4	6.4	6.1	6.2	7.2	7.2	2.8	2.7
60	39	30	23	17	6	✓	13	21	24	44	50
		90.2	91.3	91.5	92.1	92.5	92.5	91.6	91.6	92.6	93.6
		8.3	7.2	7.0	6.4	6.0	6.0	6.9	6.9	5.9	4.9
		50	35	22	9	✓	12	21	23	27	35
										96.0	95.8
										2.5	2.7
										50	44
90.8	91.2	91.7	91.2	92.5	92.9	92.9	92.4	91.9	91.9	93.7	
11.5	11.1	10.6	11.1	9.8	9.4	9.4	9.9	10.4	10.4	8.6	
50	39	27	23	10		6	18	20	24	32	
										97.2	96.5
										5.1	5.8
										50	38

Sta	+	π	-	Elev
-----	---	-------	---	------

		902.30		
--	--	--------	--	--

73 +35				
--------	--	--	--	--

+47	± Noel Drive			
-----	--------------	--	--	--

+63				
-----	--	--	--	--

+67				
-----	--	--	--	--

✓				
---	--	--	--	--

74				
----	--	--	--	--

			893.42	
--	--	--	--------	--

+02				
-----	--	--	--	--

		8.88	893.42	
--	--	------	--------	--

T.P.				
------	--	--	--	--

12.03				
-------	--	--	--	--

906.22				
--------	--	--	--	--

8.11				
------	--	--	--	--

894.19				
--------	--	--	--	--

March 19, 1957

11

11

RT

89.8	90.3	91.6	93.0	93.1	93.0	92.3	92.3	97.2	97.5
125	120	107	93	92	93	100	100	51	48
50	36	19	A	✓	14	21	24	38	50

87.9	90.1	91.0	92.2	93.3	93.4	93.3	92.8	93.5	97.4	97.8
14.4	12.2	11.3	10.1	9.0	8.9	9.0	9.5	8.8	4.9	4.5
100	50	31	12	4	✓	12	21	25	38	50

89.5	90.7	91.7	92.9	93.6	93.6	93.4	93.2	94.0	97.9	98.6	98.2
12.8	11.6	10.6	9.4	8.7	8.7	8.9	9.1	8.3	4.4	3.7	4.1
50	33	18	10	3	✓	15	21	26	36	40	50

90.4	90.9	91.5	92.4	93.2	93.7	93.7	93.4	93.3	94.1	98.0
11.9	11.4	10.8	9.9	9.1	8.6	8.6	8.9	9.0	8.2	4.3
50	41	29	16	9	✓	7	16	20	26	36

98.4	98.5
3.9	3.8
50	42

90.8	91.9	93.2	93.3	94.0	94.2	94.0	93.9	93.9	94.6	99.1	99.4
11.5	10.4	9.1	9.0	8.3	8.1	8.3	8.4	8.4	7.7	3.2	2.9
50	33	18	14	A		13	18	22	26	36	41

MH 13' RT

98.9
3.4
50

Sta 74

Sta	+	π	-	Elev,
-----	---	-------	---	-------

		906.22		
--	--	--------	--	--

74+50				
-------	--	--	--	--

✓				
---	--	--	--	--

75				
----	--	--	--	--

✓				
---	--	--	--	--

+ 50				
------	--	--	--	--

FK
RG
KP
HA

March 20, 1959

12

LT

RT

93.3	93.8	94.1	94.3	94.8	94.5	94.4	94.0	94.0
12.9	12.4	12.1	11.9	11.4	11.7	11.8	12.2	12.2
50	33	21	10		11	15	18	20

✓	900.2	900.5	900.7	99.5	98.1	97.4
	605.7	556.7	8.1	8.8		
	5044	36	34	31	29	

94.5	94.4	94.4	94.5	95.0	95.8	95.7	98.1	90.7	92.7
11.7	11.8	11.8	11.7	11.2	11.4	11.5	8.1	5.5	3.5
39	26	14	10		9	17	25	35	39

94.5	94.5	94.5	94.5	94.5	94.5	94.5	94.5	94.5	94.5
11.7	11.7	11.7	11.7	11.7	11.7	11.7	11.7	11.7	11.7
50	50	50	50	50	50	50	50	50	50

95.9	95.5	95.2	95.0	95.3	95.1	94.9	94.5	94.5
10.3	10.7	11.0	11.2	10.9	11.1	11.3	11.7	11.7
50	31	18	11		10	14	17	20

✓	93.2	4.5	05.5	05.5
	3.0	1.7	0.7	0.7
	60	50	43	37

Sta	+	π	-	Elev
-----	---	-------	---	------

		906.22		
--	--	--------	--	--

76				
----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+63				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	1.93	896.93	11.22	895.00	75 ±
----	------	--------	-------	--------	------

4 March 20, 1959 13

L1

B+

95.8	95.3	94.8	94.8	95.0	94.8	94.5	94.5	94.8
10.4	10.9	11.4	11.4	11.2	11.4	11.7	11.7	1.4
50	35	18	11		13	16	19	33

✓

02.6	03.6	04.5
3.6	2.6	1.7
60	50	39

96.0	95.1	94.3	93.7	94.1	93.8	93.6	93.3	93.3
10.2	11.1	11.9	12.5	12.1	12.4	12.6	12.9	12.9
50	36	21	16		11	14	15	17

✓

99.1	900.0	900.3	01.6	02.0
71	6.2	5.9	4.6	4.2
60	50	47	38	32

06.0	92.7	92.7	93.0	93.2	92.9	92.3	92.3	98.4
0.2	13.5	13.5	13.2	13.0	13.3	13.9	13.9	7.8
45	19	17	11		11	16	19	32

07.7	08.7	09.2	10.1	11.2		96.2	97.2
+1.5	+2.5	+3.0	+3.9	+5.0		10.0	9.0
50	55	63	76	92	✓	50	42

Sta	+	π	-	Elev
-----	---	-------	---	------

		896.93		
--	--	--------	--	--

77+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+35				
-----	--	--	--	--

✓				
---	--	--	--	--

+84				
-----	--	--	--	--

TP ₁				
-----------------	--	--	--	--

		3.55	893.38	TP
--	--	------	--------	----

TP ₂				
-----------------	--	--	--	--

1.00	889.16	8.77	888.16	
------	--------	------	--------	--

78'				
-----	--	--	--	--

2 March 2019 59 14

Lt

Rt

96.9	91.2	91.2	91.7	91.9	91.7	91.4	91.1	91.1
0.0	5.7	5.7	5.2	5.0	5.2	5.5	5.8	5.8
30	19	18	12		10	14	16	18



91.3	92.0	93.8	94.0	93.2
5.6	4.9	3.1	2.9	3.7
50	46	34	30	22

96.3	91.2	90.2	90.5	90.6	90.4	90.0	90.0	90.6
0.6	5.7	6.7	6.4	6.3	6.5	6.9	6.9	6.3
33	22	18	12		11	16	18	21



86.4	86.8	89.3
10.5	10.1	7.6
50	48	32

95.6	91.6	90.9	88.1	88.6	88.7	88.5	88.0	82.3	77.9
1.3	5.3	6.0	8.8	8.3	8.2	8.4	8.9	14.6	19.0
40	30	27	20	13	✓ 9	15	28	50	

88.7	87.5	87.5	88.0	88.2	87.9	87.4	80.7	77.5	76.1
0.5	1.7	1.7	1.2	1.0	1.3	1.8	8.5	11.7	13.1
25	22	19	14		10	14	29	43	50



Sta	+	π	-	Elev.
-----	---	-------	---	-------

		889.16		
--	--	--------	--	--

			85.52	
--	--	--	-------	--

78+50				
-------	--	--	--	--

+55	Top M.H. 18.51		3.66	885.50
-----	----------------	--	------	--------

79				
----	--	--	--	--

✓				
---	--	--	--	--

+16				
-----	--	--	--	--

✓				
---	--	--	--	--

+21				
-----	--	--	--	--

4 March 20, 1959 15

89.2	87.4	14	85.8	86.2	86.2	85.8	85.2	87.3	87.7
20	18	35	34	30	30	34	40	11.9	16.5
33	25	21	16	14	✓	11	16	30	50

85.0	84.7	84.1	84.4	84.4	84.1	83.4	78.4	75.1	73.9
4.2	4.5	5.1	4.8	4.8	5.1	5.8	10.8	14.1	15.3
25	22	20	14		10	16	24	37	50

88.2	89.2	91.5	93.2
1.0	0.0	+2.3	+4.0
34	38	50	60

87.9	85.5	83.8	83.9	83.9	83.5	83.1	79.6	77.1
1.3	3.7	5.4	5.3	5.3	5.7	6.1	9.6	12.1
35	24	19	13		10	15	21	31

89.2	90.7	92.4	75.4	75.5
0.0	+1.5	+3.2	13.8	13.7
44	50	60	50	45

87.2	86.3	84.6	83.5	83.7	83.4	83.0	79.4	76.5	75.6
2.0	2.9	4.6	5.7	5.5	5.5	6.2	9.8	12.7	13.6
50	44	24	19	13	9	13	23	38	50

Sta + π - Elev

889.16

79+58

+84

80

TP

8.74 880.42 80 $\neq$

TP, 12.44 905.82

893.38

see
page 14

77

+35

+84

March 20, 1959

16

LT

RT

85.7	84.8	82.9	82.0	82.0	82.2	81.9	82.2	79.8	78.6
2.5	4.4	6.3	7.2	7.2	7.0	7.3	7.0	9.4	10.6
50	42	26	18	14	✓10	18	37	50	

83.7	82.7	81.5	80.8	80.8	81.0	81.2	81.0	80.7	81.5	80.2	78.4
5.5	6.5	7.7	8.4	8.4	8.2	8.0	8.2	8.5	7.7	9.0	10.8
50	39	22	19	17	14	✓10	13	24	33	50	

82.3	80.8	80.5	80.0	80.2	80.5	80.0	79.7	77.8	77.3
6.9	8.4	8.7	9.2	9.0	8.7	9.2	9.5	11.4	11.9
50	33	23	18	14	✓11	22	45	50	

05.8	04.5	03.9	03.5
0.0	1.3	1.9	2.3
80	67	51	43

✓

04.3	03.7	02.5	02.6	01.2
1.5	2.1	3.3	3.2	4.6
83	76	63	54	44

✓

03.5	01.4	00.2	99.7	98.8
2.3	4.4	5.6	6.1	7.0
90	72	67	56	49

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

		905.82		
--	--	--------	--	--

78				
----	--	--	--	--

+50				
-----	--	--	--	--

TP				
----	--	--	--	--

			10.85	894.97 75 ±
--	--	--	-------	-------------

TP	0.98	881.40		
----	------	--------	--	--

			880.42	80 ±
--	--	--	--------	------

See p. 16

80 + 29				
---------	--	--	--	--

✓				
---	--	--	--	--

+38				
-----	--	--	--	--

+62				
-----	--	--	--	--

March 20, 1959 17
 Lt Rt

00.5 00.1 98.9 97.7
 5.3 5.7 6.9 8.1
 75 73 59 49

✓

99.8 97.3 92.6
 6.0 8.5 12.2
 83 68 50

✓

79.5 78.6 78.7 78.7 79.0 79.2 78.9 78.6 76.9 76.6 76.9
 1.9 2.8 2.7 2.7 2.4 2.2 2.5 2.8 4.5 4.8 4.5
 50 39 21 18 14 11 18 22 26 31

✓

75.5 76.4
 5.9 5.0
 50 40

78.8 77.9 77.6 78.3 78.4 78.6 78.9 78.5 77.2 75.9 74.5 73.1
 2.6 3.5 3.8 3.1 3.0 2.8 2.5 2.9 3.2 5.5 6.9 8.3
 50 40 27 22 17 13 11 16 22 37 50

✓

76.4 75.5 76.2 76.9 77.4 77.7 77.8 77.5 77.0 74.4 73.1 72.6
 5.0 5.9 5.2 4.5 4.0 3.7 3.6 3.9 4.4 7.0 8.3 8.8
 50 37 26 22 15 12 12 18 24 35 50

✓

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		881.40		
--	--	--------	--	--

80+76				
-------	--	--	--	--

TP	1.34	877.55	5.19	876.21 81 ±
----	------	--------	------	-------------

81				
----	--	--	--	--

+47				
-----	--	--	--	--

+76				
-----	--	--	--	--

+91				
-----	--	--	--	--

82				
----	--	--	--	--

March 20, 1959 18

L+

RT

74.8	74.7	74.6	74.4	74.6	77.1	77.2	76.7	73.2	70.8	69.2	68.2
66.7	68.50	4.8	4.3	4.2	4.7	8.2	10.6	12.2	13.2		
50	37	29	22	18	12	✓ 16	24	34	42	50	

73.3	73.0	73.0	74.8	75.8	75.9	76.3	75.8	75.3	71.0	68.8	67.3
43.9	46.4	6.2	8.1	1.8	1.7	1.3	1.8	2.3	6.6	8.8	10.3
50	43	29	24	20	14	✓ 13	19	27	34	50	

69.5	70.7	71.4	73.7	73.8	74.1	74.4	73.9	73.3	68.4	66.4	66.3
71.6	6.9	6.2	3.9	3.8	3.5	3.2	3.7	4.3	9.2	11.2	11.3
50	40	29	23	19	12	✓ 15	23	31	43	50	

69.7	70.7	72.6	73.2	73.1	73.7	73.1	72.4	69.0	69.8
7.9	6.9	5.0	4.4	4.5	3.9	4.5	5.2	8.6	9.8
50	32	27	20	15	✓ 19	27	36	50	

70.9	71.5	72.8	72.7	73.1	73.4	72.9	72.5	72.3	71.8
6.7	6.1	4.8	4.9	4.5	4.2	4.7	5.1	5.3	5.8
50	47	38	28	15	✓ 20	33	43	50	

73.3	72.9	73.1	73.3	73.3	72.8	72.3	72.2
4.3	4.7	4.5	4.4	4.3	4.8	5.3	5.4
50	39	28	12	21	44	50	

Sta + π - Elev

877.55

82+08

+18.70 $\pm$ Edgerton

BM

4.78 872.77 (872.84)

March 20, 1959

19

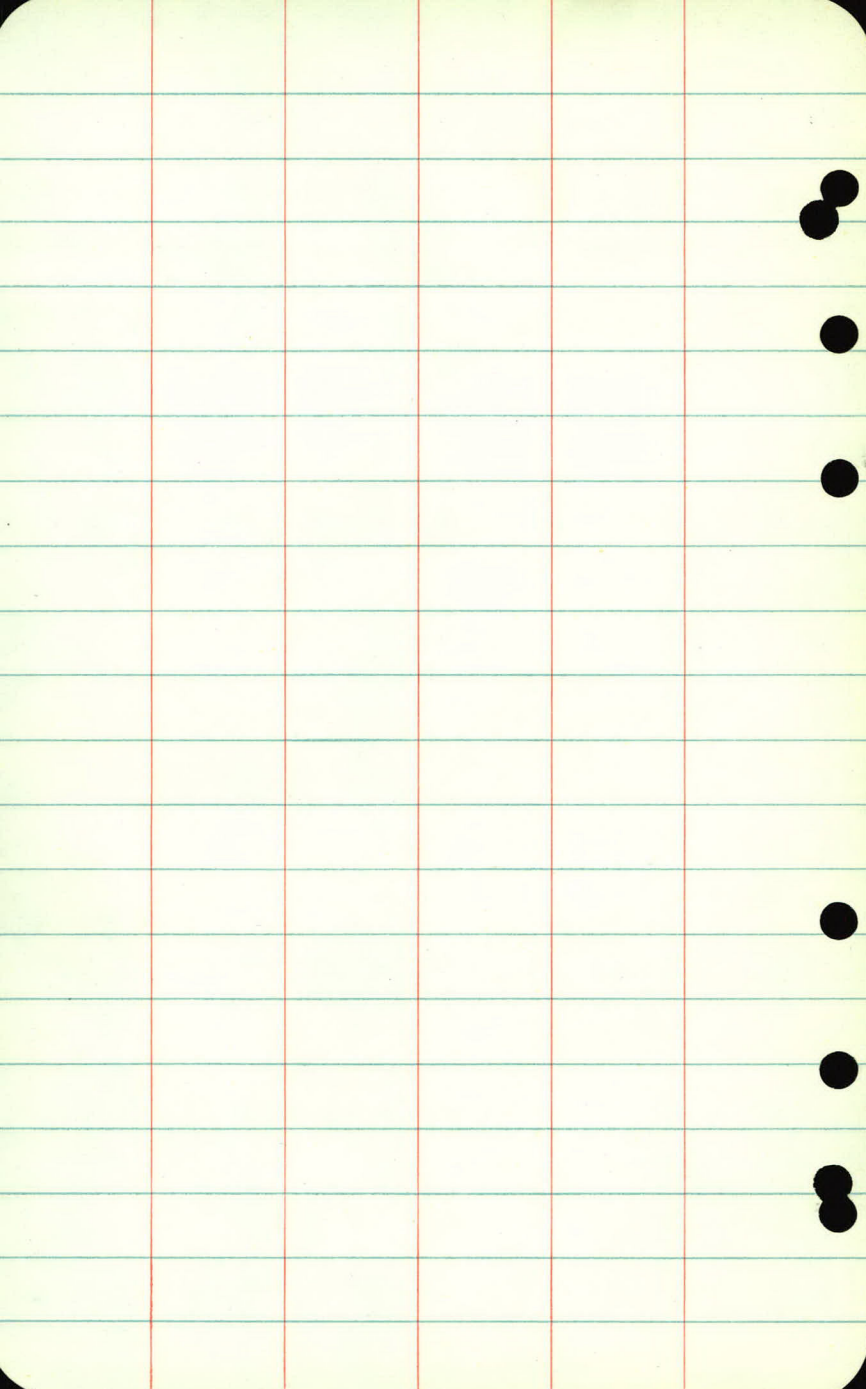
Lt

~~Rt~~

Rt

73.7	73.6	73.3	73.1	73.1	72.9	72.6	72.5	
39	40	43	45	45	47	50	51	
50	45	29	13	✓	15	32	50	
75.6	73.7	73.4	73.2	73.0	72.8	72.7	72.6	72.2
20	39	42	44	46	48	49	50	54
100	50	33	16		20	36	50	

Top Mont at Edgerton



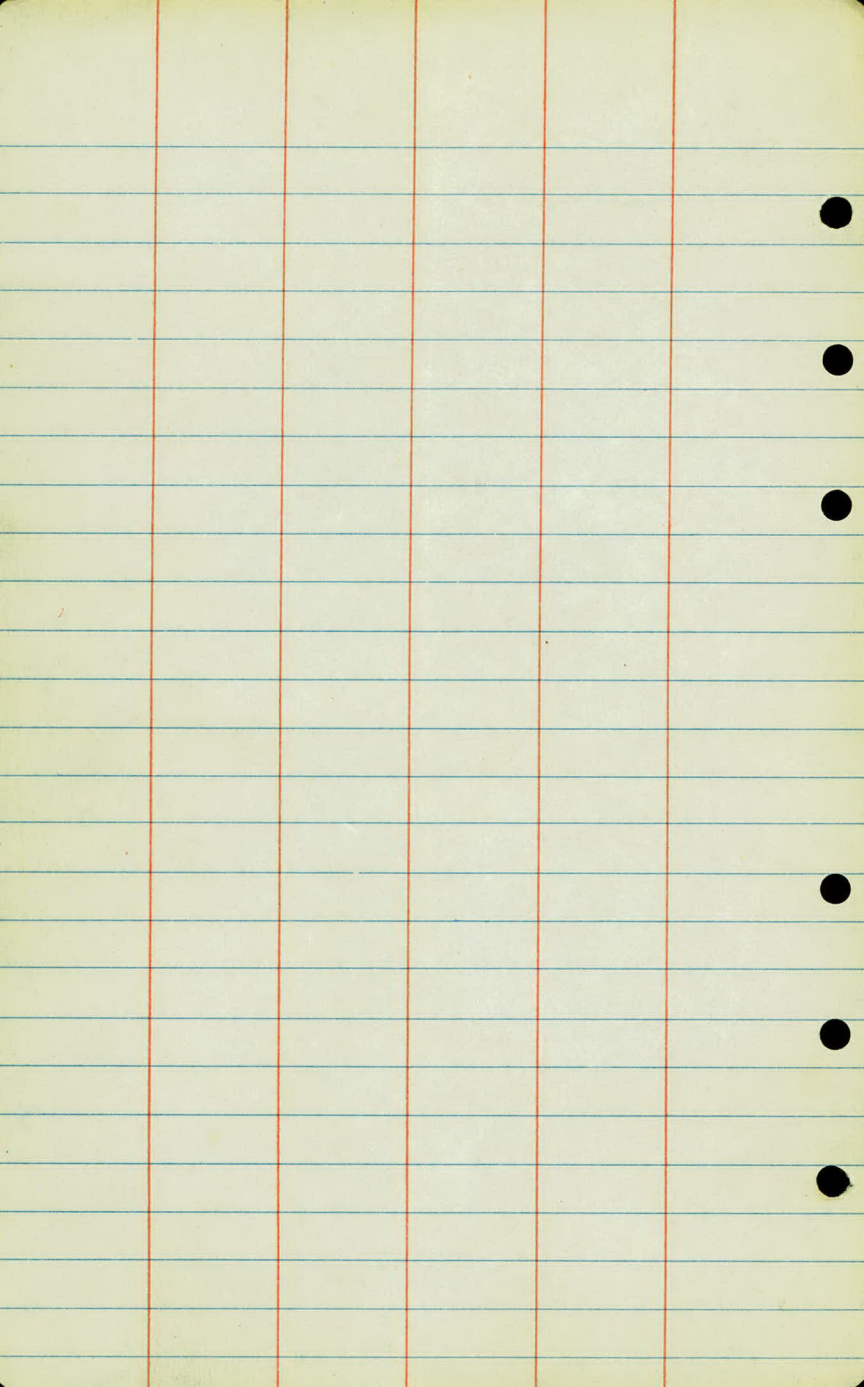
1

Plan Survey
Little Canada Rd
At Soo Line RR.

Index	Pages	6-4-51
Align	1 to 5	HAW
Topog	5 to	L.C.
		M.B.
		K.R.

Rec 6/5/51

drawn up.



✓

Align.

Sta

Pt

Δ RT

AL

20+49.79 POST

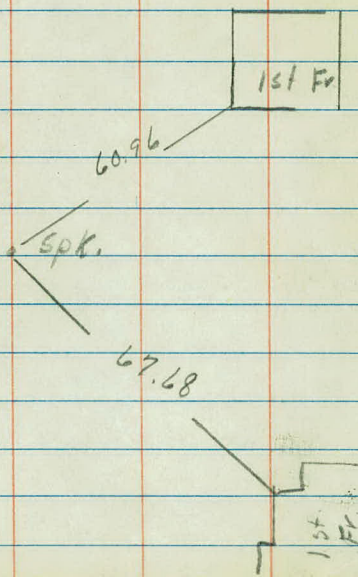
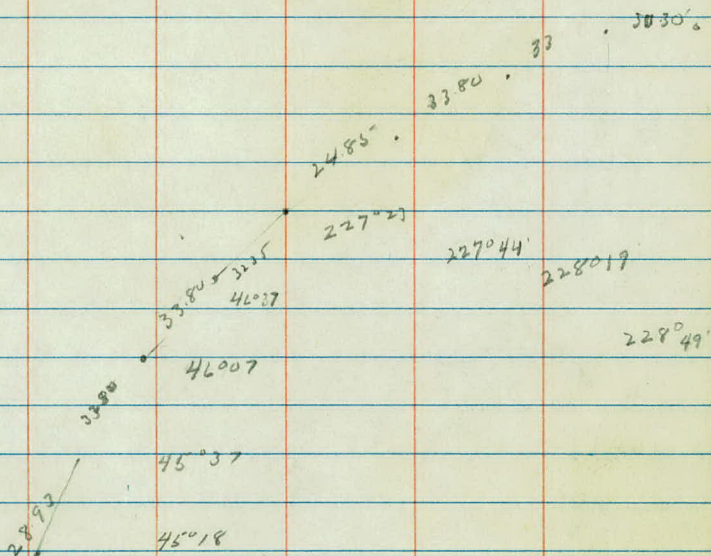
20+35.41 PC

17+00

P.I

1°23'

Description



Sta	Pt	P.O.F	Δ RT	Δ LI
-----	----	-------	------	------

24+60.58	P.O.T			
----------	-------	--	--	--

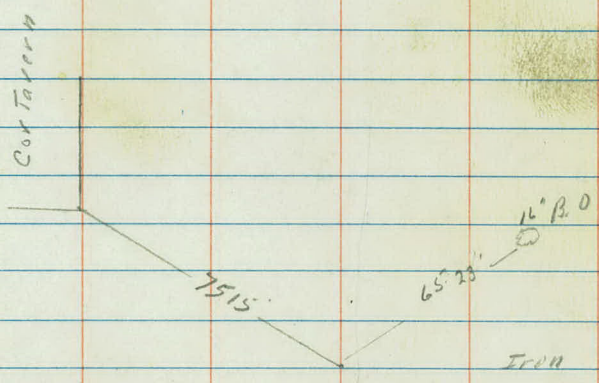
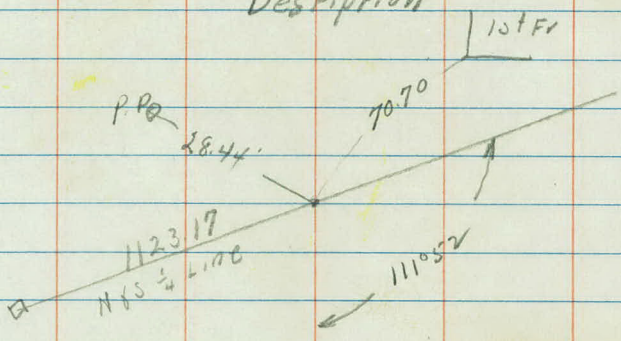
+76.52 +76.62	P.T	3°38'		3'37'
+50		3°13'		3°13.5'
22		2°28'		2°51'

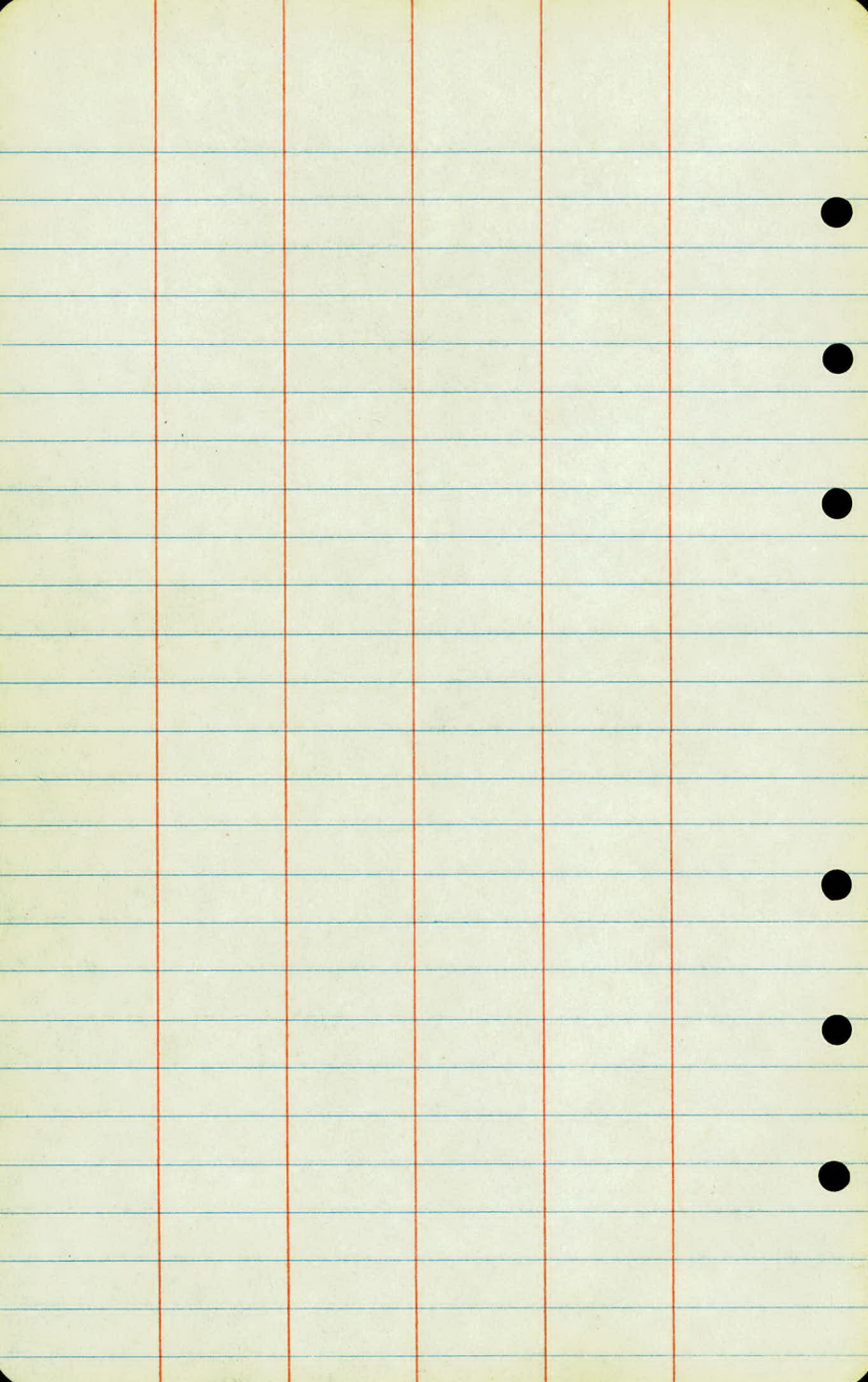
21+56.15	P.I		7°14'	2°28.5'
+50		1°43'	D 3°	2°06'
21		0°58'	T 120.74 120.74	1°21'
+50		0°18'	L 241.11	36'

20+35.41	P.C	0°00'	R. 1910.08	0°00'
----------	-----	-------	------------	-------

50	25	17
17	4.9	
45	725	

Description





5

Торос.

23

Pd
10' 11"

+91' Car Barricade 41'

22

12' 12"

21

12' 9"

+53.15 East Rail

+46.65 West Rail

20

9' 11"

- +85 Ent
- +82 Gr. 3 Oaks 63'
- +71 X Hedge 21'
- +71 Tr 20'
- +64 N.W. Car Gr 84'
- +60 30. Oak 31'

19

10' 10"

18

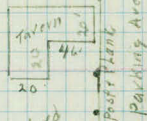
12' 10"

+37 4" Apple Tr 24'

17

11' 11"

- + 82 P.P. 26'
- + 42 4" Spruce 46'
- + 16 SW Cor Tavern 46'
- + 10 6" Spruce 48'
- + Barricade 44'



- + 79 Tr 49'
- + 62 Bag Barricade 45'
- + 47 SW Cor Sign 48'
- + 34 NW Cor Conc Sign 47'

+ 84 Ave Lt Pole 30'

+ 57 X Buck 18'

+ 77 P.P. 30'

+ 77 TP 27'

+ 13 30" Oak 29'

+ 41 TP 27'

+ 44 X Buck 15'
+ 31 TP 33'

+ 13 NW Cor Ho 9' 0"
+ 18 Lilac Bush 23'
+ 100 Elm 1'

+ 75 End Fe 2'
+ 46 6" Pine 30'
+ 42 4" Spruce 28'
+ 40 NE Cor Ho 495'
+ 34 3" Conc No 18'
+ 25 4" Pine 26'
+ 21 4" Pine 27'
+ 22 NW Cor Ho 475'
+ 105 Bag Fe 22'
+ 102 24" Oak 24'

+ 88 Lilac Bush 32'
+ 78 30" Oak 29'

+ 78 TP 21'
+ 75 End Hedge 18'
+ 66 Plum Tr 39'
+ 51 NE Cor Ho 5' 0"
+ 31 NW Cor Ho 5' 1"
+ 26 Tr 0.535'
+ 22 4" Oak 37'
+ 17 Tr 33'
+ 100 Apple Tr 29'
+ 100 Bag Hedge 18'

+ 68 P.P. 29'



24

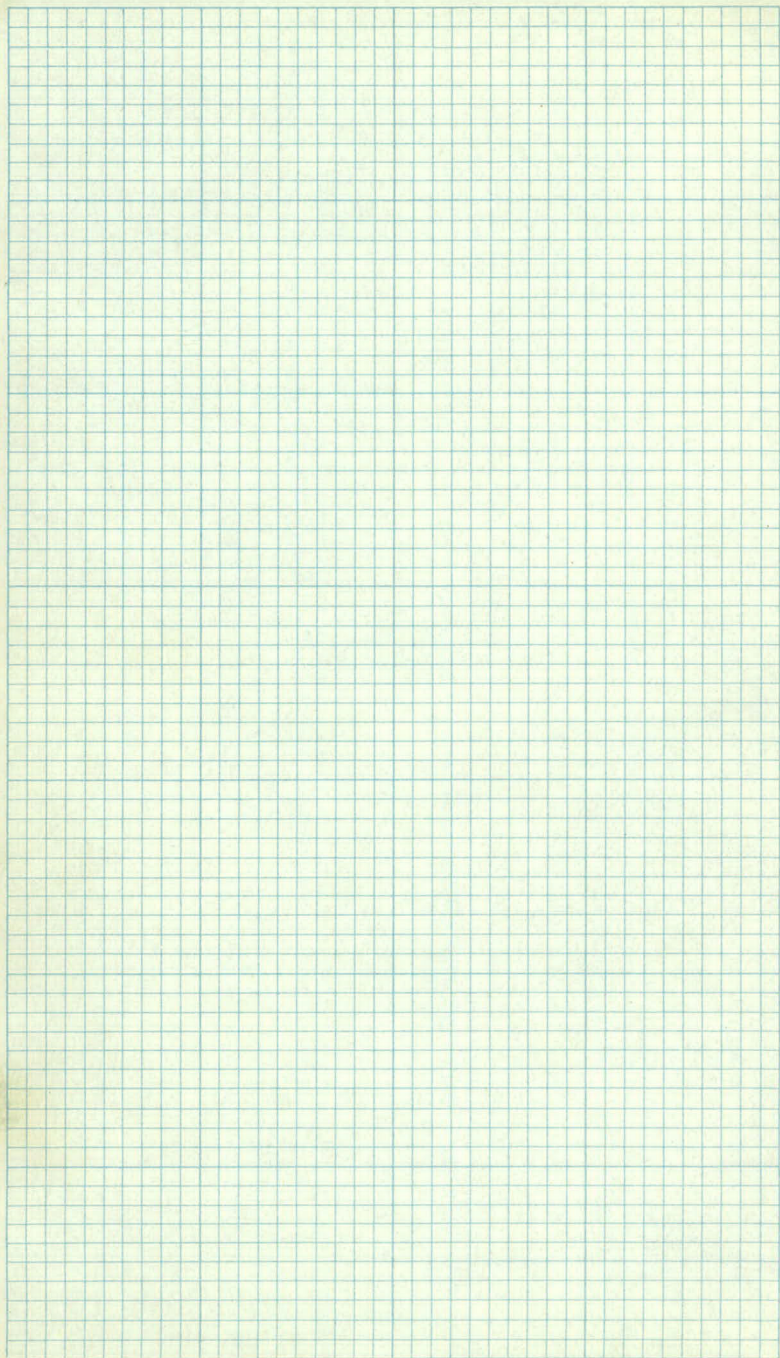
10' 10'

23

10' 11'

- + 78 Rgc Tie Trees
- + 60 Bag Row Trees
- + 106 & 40 Ent

Q_u 17



x Sections

Sta	+	π	-	Elev
B.M	7.08	930.66		923.58
17+00				22.5

+50				22.7
-----	--	--	--	------

18				23.1
----	--	--	--	------

+50				23.3
-----	--	--	--	------

19				23.3
----	--	--	--	------

+50				23.5
-----	--	--	--	------

+40				23.8
-----	--	--	--	------

+88				24.3
-----	--	--	--	------

L1

L2

Rt

Top SE Cor Top Step Tavern Lt 22+28

79	81	79	67	84	89	86		87	88	99	112	128	134	
50	36	32	29	17	12	10	82	70	17	21	31	38	50	✓

78	78	70	72	88	86	84		82	88	96	105	112		
50	36	32	28	17	12	11	80	7	15	19	33	50	✓	

80	83	74	74	84	83	80		77	80	85	83	100		
50	36	33	28	17	13	11	76	8	10	26	33	50	✓	

81	80	72	70	82	82	77		78	81	77	81	84		
50	37	32	27	19	11	10	74	10	22	26	44	50	✓	

82	82	64	78	82	81	78	74		78	78	81	77		
50	39	32	26	18	10	8			10	20	31	50	✓	

85	77	75	74	76	74		72	76	76	73	72		Elev Or at Ho	
50	34	28	20	11	8			10	16	21	33	72	50	✓

100	112	98	74	72		75	77	75	78	77				
50	35	26	15	8	69	12	18	22	43	50	✓			

53	96	105	102	67	65		68	72	78	77				
50	35	26	21	12	8	64	10	15	40	50	✓			

Sta	+	λ	-	Elev
-----	---	-----------	---	------

930.66

20

24.8

+20

25.7

+35

26.5

+46.65

West Rail

26.58

+50

Tracks

26.7

+53.15

East Rail

26.81

+75

26.6

21

25.5

Lt

K

Rt

$\frac{45}{50}$

$\frac{50}{43} \frac{64}{37} \frac{88}{27} \frac{92}{19} \frac{61}{11} \frac{60}{6} 59 \frac{63}{10} \frac{76}{28} \frac{80}{50}$ ✓

$\frac{76}{50} \frac{52}{44} \frac{44}{37} \frac{50}{23} \frac{54}{18} \frac{50}{12} \frac{53}{9} 50 \frac{50}{7} \frac{55}{11} \frac{61}{16} \frac{70}{22} \frac{77}{39} \frac{77}{50}$ ✓

2207
East
Rd.

West R.

$\frac{84}{50} \frac{75}{37} \frac{45}{24} \frac{389}{19} \frac{413}{11} \frac{42}{9} 4.2$

$\frac{45}{10} \frac{78}{20} \frac{80}{27} \frac{75}{38} \frac{72}{50}$ ✓

26.53
20+35.4
 $\frac{413}{15}$

26.58
408

20+55.4
26.16
 $\frac{410}{15}$ ✓

$\frac{73}{50} \frac{74}{44} \frac{94}{34} \frac{73}{24} \frac{43}{16} \frac{39}{12} 40 \frac{44}{10} \frac{57}{18} \frac{84}{30} \frac{93}{38} \frac{70}{50}$ ✓

26.78
20+41.3
 $\frac{388}{15}$

26.81
20+66.4
 $\frac{386}{15}$

26.80 ✓

$\frac{71}{38} \frac{76}{34} \frac{58}{28} \frac{54}{18} \frac{47}{13} \frac{47}{11} 41 \frac{43}{9} \frac{45}{15} \frac{48}{17} \frac{45}{21} \frac{48}{35} \frac{74}{50}$ ✓

$\frac{73}{50} \frac{66}{34} \frac{58}{15} \frac{56}{10} 52 \frac{54}{9} \frac{56}{12} \frac{76}{20} \frac{77}{24} \frac{49}{37} \frac{44}{41} \frac{46}{50}$ ✓

Sta	+	Δ	-	Elev
-----	---	----------	---	------

93066

21+50

24.1

22

Section West Edge Tavern 23.6

+50

East Side Tavern

23.0

23

22.6

+50

22.5

24

22.3

B.M

708 923.58

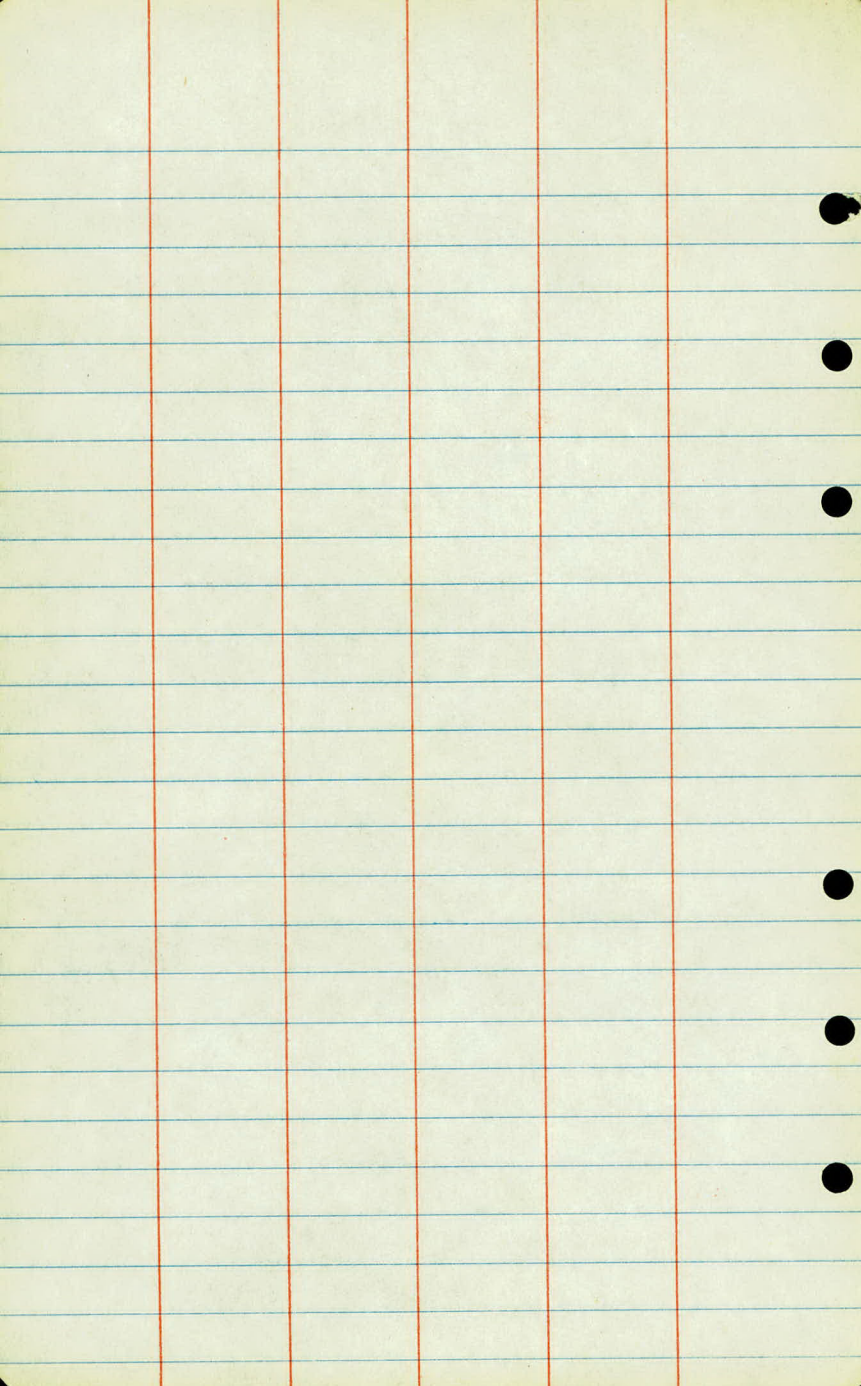
Lt

K

Rt

 $\frac{7.3}{50} \frac{7.4}{36} \frac{7.5}{20} \frac{7.1}{12} 6.6 \frac{6.8}{10} \frac{6.8}{19} \frac{6.5}{29} \frac{6.0}{50} \checkmark$
 $\frac{7.9}{50} \frac{7.9}{43} \frac{8.3}{31} \frac{8.2}{24} \frac{7.7}{11} 7.1 \frac{7.2}{10} \frac{7.5}{19} \frac{6.6}{29} \frac{6.5}{34} \frac{8.0}{50} \checkmark$
 $\frac{8.1}{50} \frac{8.2}{36} \frac{8.6}{30} \frac{8.4}{18} \frac{8.3}{10} 7.7 \frac{8.1}{12} \frac{7.9}{16} \frac{7.1}{22} \frac{6.8}{33} \frac{7.6}{40} \frac{7.5}{50} \checkmark$
 $\frac{9.1}{50} \frac{9.1}{37} \frac{9.0}{27} \frac{8.6}{12} 8.1 \frac{8.3}{11} \frac{8.0}{19} \frac{7.3}{25} \frac{7.2}{30} \frac{8.1}{37} \frac{8.2}{50} \checkmark$
 $\frac{8.7}{50} \frac{8.9}{26} \frac{9.3}{22} \frac{8.9}{11} 8.2 \frac{8.5}{10} \frac{7.6}{23} \frac{7.7}{27} \frac{8.4}{30} \frac{8.7}{50} \checkmark$
 $\frac{8.8}{50} \frac{8.9}{22} \frac{9.9}{19} \frac{9.2}{18} \frac{9.1}{10} 8.4 \frac{8.6}{10} \frac{8.4}{12} \frac{8.6}{24} \frac{7.7}{30} \frac{7.5}{39} \frac{8.7}{50} \checkmark$

Top S.E. Cor Top Step At Sta 22+28



DIST.

VERT.
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV.

Location

Little Canada Rd + Soc Line CR

April 1951

DETECT

82

STADIA

Hub #1

£ Tr. + L.H/c Canada Rd

H.I 905.55

0-00 = £ L.H/c Canada Rd West of Tr.

£ Tr.	46°40'	0.62
" "	46°07'	0.94
" "	45°45'	1.24
" "	45°10'	1.57
" "	44°55'	1.89
" "	44°22'	2.20
" "	44°10'	2.50
" "	43°50'	2.83
" "	43°35'	3.10
" "	43°20'	3.42
" "	43°04'	3.74
" " Tan	42°30'	4.97
" " "	41°54'	7.25
" " Curve	228°18'	0.58
" "	228°45'	0.92
" "	229°10'	1.22
" "	229°45'	1.55
" "	230°10'	1.85
" "	230°48'	2.15
" "	231°10'	2.45
" "	231°45'	2.77

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

Assumed Elev

6.2

6.3

6.5

6.7

6.9

7.0

7.1

7.2

7.3

7.3

7.2

7.8

8.0

6.0

6.0

5.9

5.8

5.9

5.8

5.7

5.8

OBJECT

AZI

STADIA

Z Tracks

			232°10'	3.08
	"	"	232°40'	3.38
	"	"	234°03'	4.34
	"	"	235°00'	4.95
	"	"	235°55'	5.54
	"	"	231°52'	6.18
20' Top	East of Tr. Z Rd	10-10	179°57'	0.38
	"	10-10	183°37'	1.14
	"		184°40'	2.04
	"		185°30'	3.18
	"		186°20'	4.40
			186°40'	5.80
20' Top	Z Rd West of Tr.		359°40'	0.20
	"		0°03'	0.64
	"		0°18'	1.22
	"		0°43'	2.26
	"		0°40'	3.32
	"		0°20'	4.30
	"		0°05'	5.30
	"		359°55'	6.33

DIST	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
------	----------------	---------------	-----	-------	-------

5.6

5.4

5.0

4.9

4.8

4.7

00.9

6.3

99.3

8.3

97.3

9.2

96.4

9.8

96.8

9.9

96.7

9.9

96.7

6.0

99.6

8.0

97.6

9.0

96.6

9.0

96.6

9.6

96.0

10.1

95.5

10.9

94.7

11.2

94.4

OBJECT

221

STADIA

1

10/10

AM

L.C

M.B

SO. DITCH - PROFILE

LITTLE - CANADA RD

FROM 22' EAST-OF - RICE-ST-TO-ROUND-LAKE

Rec'd. 10-10-51

R.C.

Drawn up 10-25-51

R.C.

STA	+	π	-	ELEV
B.M	2.56	92621		923.65

0+00 = 222' EAST of RICE ST 21.6

+50 21.5

1 21.8

+50 21.8

+58 10" X 2' VIT

+90 12" X 20 C.M

21.6

+14 DITCH TO-50

+50 21.5

3 20.9

+28 18" X 12' C.M

+40 " " "

£
DITCH

S. W. COR. PLATFORM 37' LT STA 0+35

19.6

46

6.6

18.7

19.1

47

7.5

7.1

18.5

40

44

7.7

18.4

44

7.8

18.09

F.L.
8.12

17.98

F.L.
8.23

18.4

46

7.8

18.4

19.4

20.0

7.8

6.8

6.2

18.1

7.5

12.5

47

8.1

17.6

53

8.6

F.L. 16.5+

9.67

16.49

F.L.

9.72

STA	+	π	-	ELEV
		926.21		

3+50				20.3
------	--	--	--	------

4				19.8
---	--	--	--	------

T.B.M	4.92	923.83	7.36	918.91
-------	------	--------	------	--------

+38	18" X 42'	V.I.T X DRAIN = North Ditch		
-----	-----------	-----------------------------	--	--

+56	18" X 42'	V.I.T X DRAIN = So. Ditch		
-----	-----------	---------------------------	--	--

5				19.1
---	--	--	--	------

+50				19.2
-----	--	--	--	------

6				19.1
---	--	--	--	------

+50				19.2
-----	--	--	--	------

7				19.0
---	--	--	--	------

+31	18" X 34'	C.M		
-----	-----------	-----	--	--

+65	18" X 34'	C.M		
-----	-----------	-----	--	--

8				17.6
---	--	--	--	------

♀
DITCH

17.3

5.9

8.9

16.5

6.4

9.7

15.2

F.L.

8.6

14.8

15 Kew

F.L.

9.0

15.1

15.4

4.7

8.7

8.4

15.3

40.9

4.6

8.5

6.9

15.6

40

4.7

8.2

15.4

4.6

8.4

14.6

4.8

9.2

13.06

F.L.

10.77

12.3

F.L.

11.5

13.8

6.7

10.1

STA + π — ELEV

923.83

8+50

17.7

+74

18" CM INVERT ^{LAKE} _{TO} _{ROUND}

17.8

B.M

7.24 916.59

T.P.

7.16 926.07

4.92 918.91

B.M.

2.44 923.63

923.65

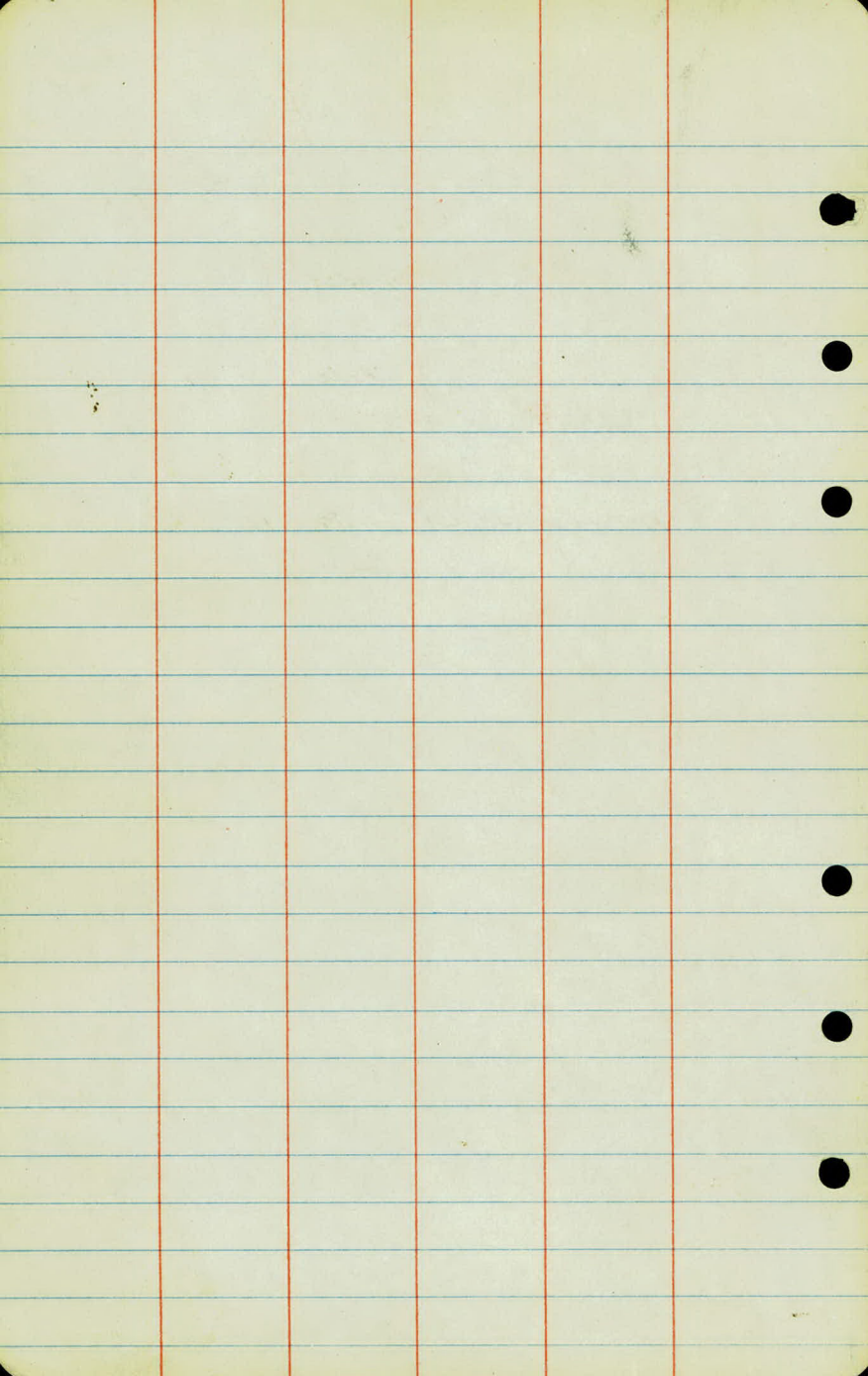
$\frac{1}{2}$ $\frac{1}{2}$
 DITCH
 12.9

6.1 10.9
 12.1

6.0 F.L.
 11.7

S. END M. HOLE RIM LT STA 8+84

S.W. COR PLATFORM 37' LT STA 0+35



Little Canada Rd

x-section checks

Sta	+	π	-	Elev
-----	---	-------	---	------

77+84				
-------	--	--	--	--

✓				
---	--	--	--	--

78				
----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

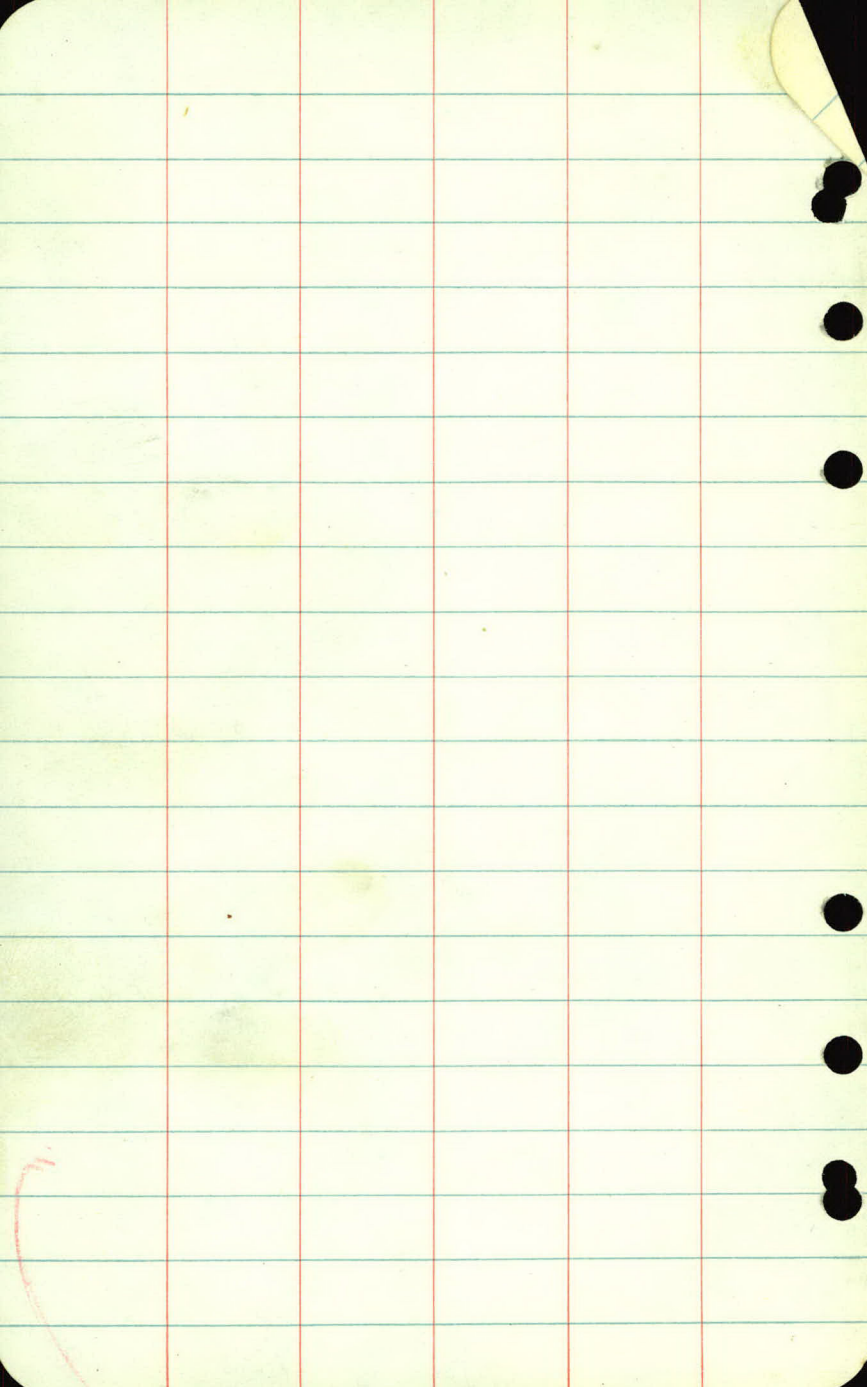
✓				
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Sept 1, 1959

3a

PK Nail

PK Nail



FK
RG

4 April 23, 1959

6

LF

RT

0.0	-0.7	-0.2	0.0	-0.6	-6.8	-10.8
22	19	14		15	29	50

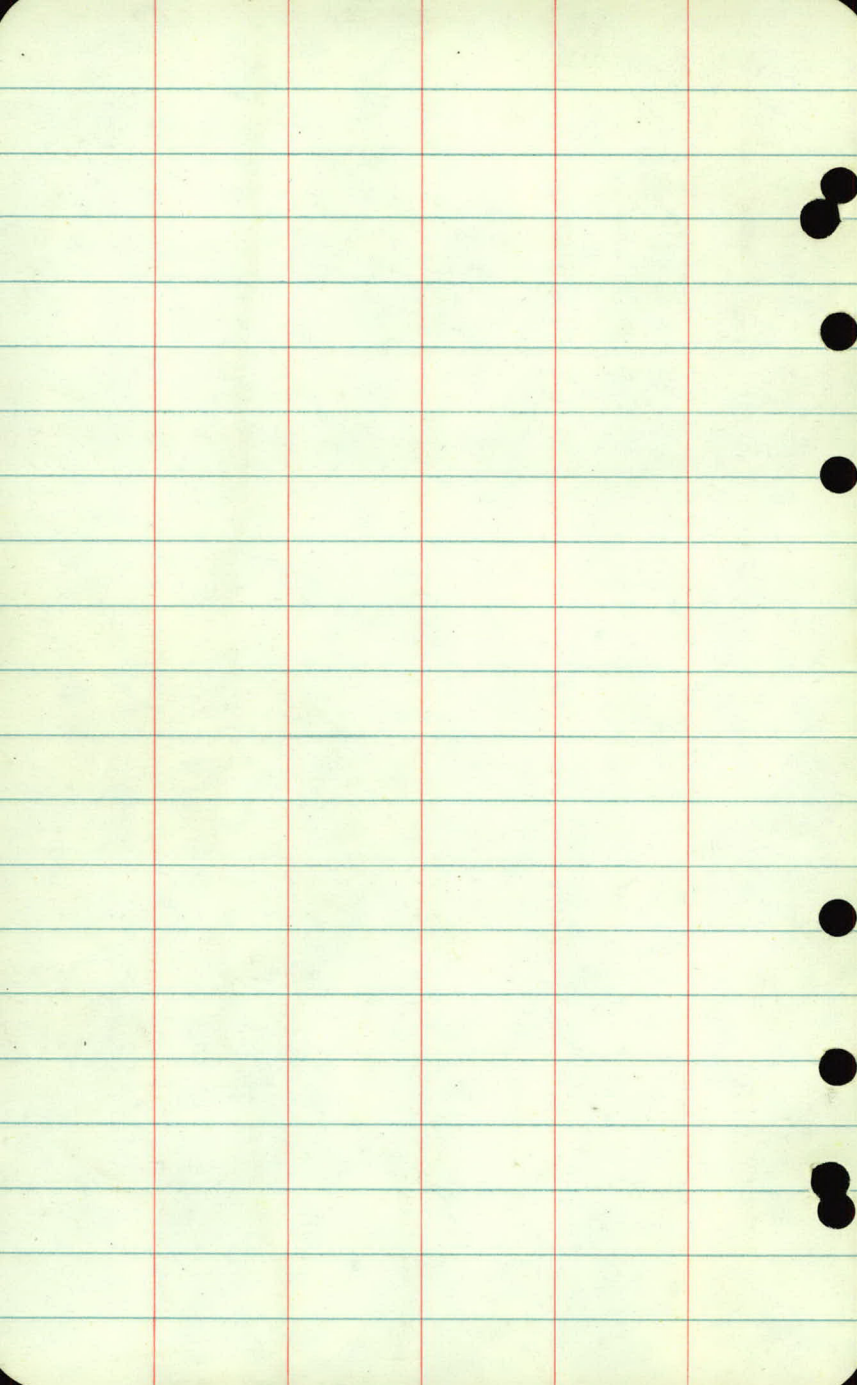
+2.4	+5.1	+10.5	+12.0
28	36	50	65

+1.4	-0.8	-0.2	0.0	-0.3	-0.9	-2.6	-11.7
26	20	14		11	15	29	50

+3.0	+5.0	+9.4	+11.4
32	36	48	67

-0.4	-0.3	+0.1	0.0	-0.7	-8.0	-13.6
21	15	13		15	28	50

+3.0	+5.0	+10.0	-16.0
32	39	60	62



27 AUG 1959

1.

KP
UH
RL
RR

LITTLE CANADA ROAD.
McMenamy to Edgerton
Re-alignment

3 pages

43+38.42 West Edge
Bridge (Red in
Wood Header)

Sta Point ΔL ΔR

+24.70 P.T.

3°42'

73

3°27'

+50

2°57'

72

2°27' Δ 7°24'

+50

1°57' D 2°

+39.94 P.I.

T 185.25

71

1°27' D 370.0

+50

0°57' L 2868.9

70

0°27'

69+54.70 P.C.

0°00'

69+05.30 P.O.T

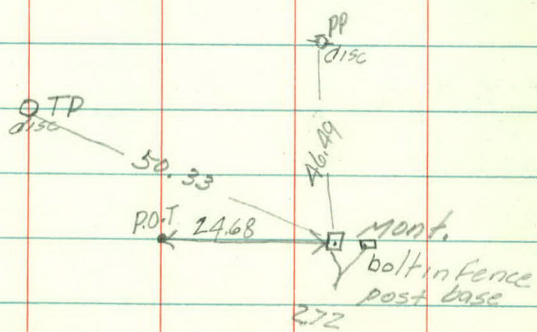
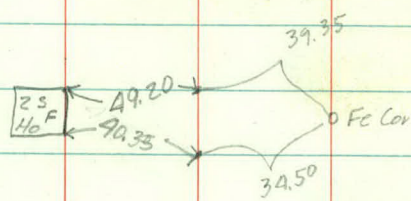
28 AUG 1954

2.

Lt

E

Rt



Sta Point ΔL ΔR

+51.15	PT	2°33'	
+50		2°32'	
76		2°02'	$\Delta 5^{\circ}06'$
+50		1°32'	D 2°
75+23.72	PI		T 127°57'
75		1°02'	L 255.0
+50		0°32'	R 2868.9
74		0°02'	
73+96.15	P.C.	0°00'	

KP
UH
RL
RR

28 AUG 1959

3.

on section line

on section line

£ for Paving

$$\Delta = 5^\circ 14\frac{1}{2}'$$

$$D = 1^\circ$$

$$T =$$

$$L =$$

$$R = 1146.28 \text{ Chord}$$

10100

P.L.

KP
JH
RL
RR.

28 AUG. 1959 1.

LITTLE CANADA ROAD
McMENEMY to Edgerton
P.I. TIES.

Save

Sta Point Alt DR#

82+19th Edgerton

75-23.72

5°06'

71+39.94 P1

7°22'

Lt

d

28 Aug. 1959

Rt

2.

2x2 hub



56.92

PP 26.07

58.73

2x2 hub



USED

NO

SW cor house

75.93

89.06

NW cor Fence Post (Stone)

87.46

NE cor Stone Fence Post

Sta	Point	ΔL	ΔR
+33.34	P.T.	$2^{\circ}33.5'$	
+25		$2^{\circ}24'$	
76		$2^{\circ}01.5'$	$\Delta = 5^{\circ}07'$
+75		$1^{\circ}39'$	$D = 3^{\circ}$
75+50.13	P.I.	$5^{\circ}07'$	$T = 85.34'$
+50		$1^{\circ}16.5'$	$L = 170.56$
+23		$0^{\circ}54'$	$R = 1910.08$
75		$0^{\circ}31.5'$	
+75		$0^{\circ}09'$	
+64.79	PC	$0^{\circ}00'$	
74+00.08	P.T.	$2^{\circ}33.5'$	
+50		$1^{\circ}48.5'$	
+14.86	P.I.	$5^{\circ}07'$	
73		$1^{\circ}03.5'$	
+50		$18.5'$	
+29.52	PC	$0^{\circ}00'$	