

Bk 574 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

Carver Ave
From City Limits To E. Co. Line

Road Acc't. No. 72

Date Filed 6-11-41

File

City Limits to East Ave. } 1950
S.A.P. 62-542-01 50-43A }

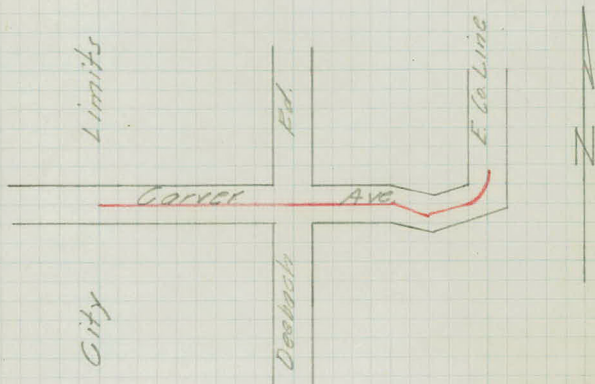
5-13-69

Bob:

Judge Stewart's court has
the const. diary. We should get it
back in a couple weeks

Carver Ave.

PLAN SURVEY
CARVER AVE.
East Ave to E. Co. Line

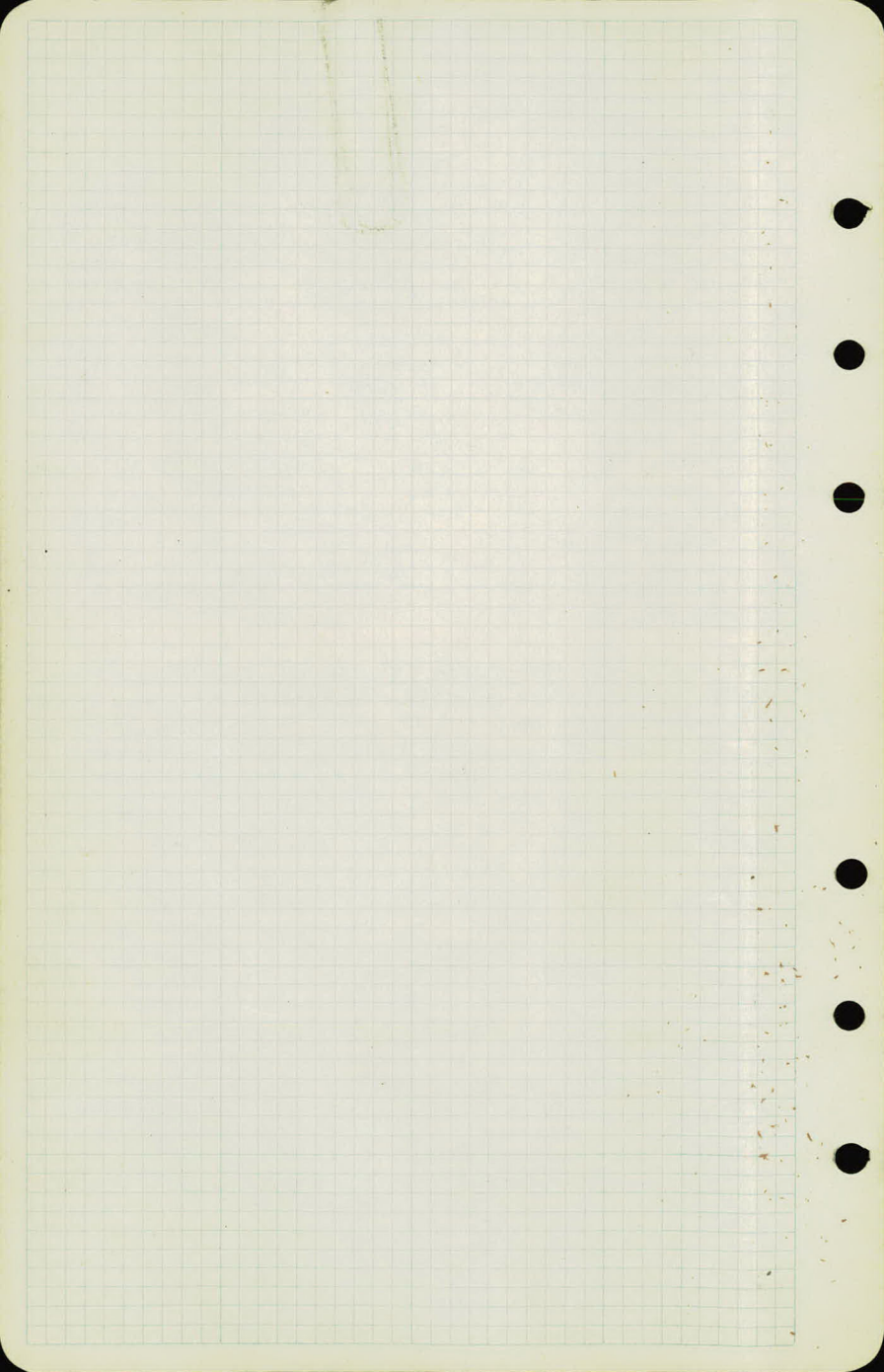


INDEX.

Align. - 1-4
Topog. - 5-14
Benchmark - 15-16
X Sections - 17-32

L' LINE.

Align 33-34
Topog. 35-36
X Sections 37-39
Completed 6-2-41



1

Alignment

Sta	Point	ΔLt	ΔRt
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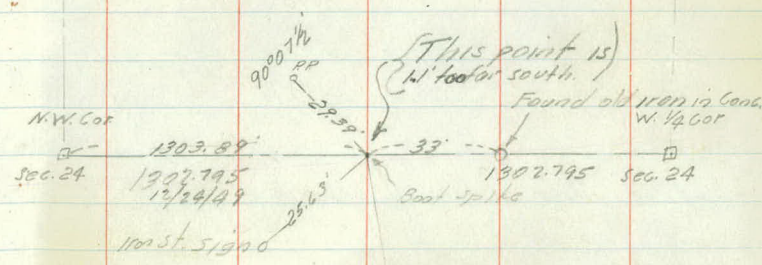
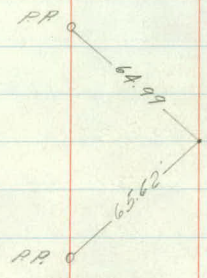
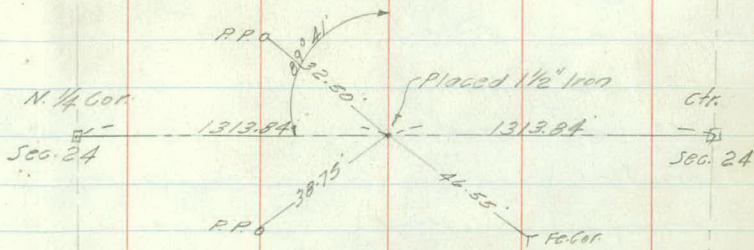
26	+03.89	P.I.	
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			0°01'30"
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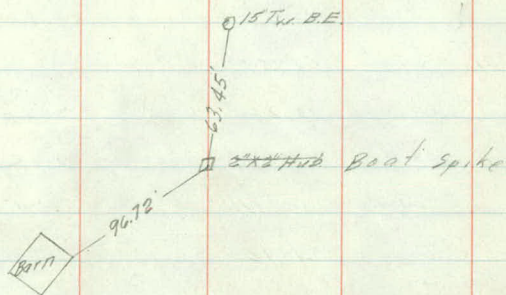
1	+8556	P.O.T.	
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0	+00	East City Limits	1°34'
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N.E. Cor. 271.46.2 2377.3 427.41 E 1/4 Cor 2
 Sec. 24 1324.37' Sec. 24



Sta	Point	ΔLt	ΔRt
+97.85	P.T.	28°35.5'	
+75		24°15'	$\Delta 57^{\circ}11'$
+50		19°30'	D-38°—
46 +50.98	P.I.		T-83.60
+25		14°45'	L-150.47'
46		10°00'	R-153.58'
+75		5°15'	
45 +47.38	P.C.	0°00'	
+68.51	P.T.		19°42'
+50			18°12.9' X 39°24'
40			14°12.9' D-16°—
39 +50.95	P.I.		39°24' T-128.63'
+50			10°12.9' L-246.25'
39			6°12.9' R-359.26'
+50			2°12.9'
38 +22.32	P.C.		0°00'
32 +21.55	P.O.T.		



74 Sta.



New P.I. for
Paving Page 5

2" x 2" Hub.
Iron

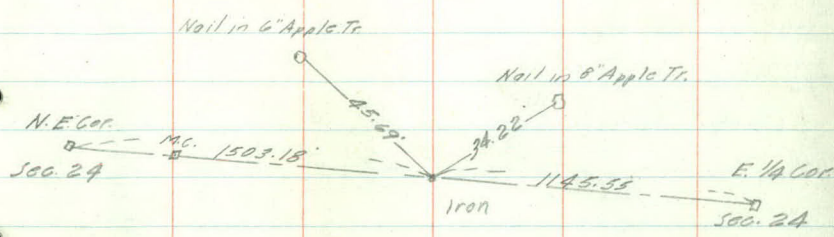
F.R.



Sta	Point	Δ Lt	Δ Ct
56.9		DCE = 173' Per Ft	
+26.91	PT	45° 15.65'	
54		35° 32.8'	Δ 86° 31'
+75		28° 22.8'	D-60°-
53	+70.10 P.L.	86° 31'	T-94.10'
+50		21° 12.8'	L-150.91' Actual Arc.
+25		14° 02.8'	R-100.00'
53		6° 32.8'	
52	+76.0 P.C.	0° 00'	

+27.01	P.T.	7° 16'-	
52		6° 27.4'	Δ 14° 32'
		5° 42.4'	
+50		4° 57.4'	D-6°-
51	+06.62 P.L.	14° 32'	T-121.83'
		4° 12.4'	
51		3° 27.4'	L-242.22'
		2° 42.4'	
+50		1° 57.4'	R-955.37'
		1° 12.4'	
50		0° 27.4'	
49	+84.77 P.C.	0° 00'	

K.A.
L.C.
M.B.
C.N.



+47.41 PT

+25

40

+75

+30

39+42.1 PT

+25

39

+75

+50

38+26.5

220.91

247.41

19°53'

17°52'

15°37'

13°22' $\Delta = 39'46''$

11°07' $D = 18''$

$T = 115.60$

8°52' $L = 220.91$

6°37' $R = 319.62$

4°22'

2°07'

0°00'

Tic

Conduit

Topography

+88-10' Pnc - 29' +96-10' Pnc - 35'
 +89-10' Pnc - 35'
 +75-PP-28'

+80-G.P.-21'

3 +Ent-50' 12' 13'

+81-15' X 20' G.M. - 19'

+64-End Row Elms - 35'

+54-PP-28'

+40-Elm -

+25-Ent- $\frac{15' \times 20' G.M.}{23'}$

2 +14-Elm - 12' 12'

+87-Elm -

+61-Elm -

+34-PP-27-Elm -

1 +10-Elm - 12' 13'

+82-Elm -

+56-Elm - +50-11' 14'

+30-End Row 3' Elms - 32'

+16-PP-26'

0 +00 Ent. $\frac{15' \times 20' G.M.}{19'}$ 9' 16' FC. - 35'

-50-2' 17'

-1 2'-18'

-50 5'-21'

-2 6'-24'



0

0

0

0

0

cut

0

0

0

0



+95-4"E/m -

+85-PP-28'

+67-3"E/m -

+40-3"E/m -

10 +13-3"E/m

13'

+36-3"E/m -

+68-PP-28

+59-3"E/m -

+36-3"E/m -

9 +40-3"E/m -

13' 13'

+83-3"E/m -

+50-2"E/m -

+44-PP-28'

+29-2"E/m -

8 +102-4"E/m-34

13'

+12-Ent $\frac{18 \times 20 \times 19}{18}$
Ent Fc - 21'

+79-3"E/m -

+50-10' Gully Line - 18.5'

+47-4"E/m -

+26-PP-29'

+20-6"E/m

7 12' 14'

+92-4"E/m -

+66-5 Elm-35' Beg Row

+58-End 12' Row - 17.5'

+54-End 24' Row - 17.5'

+38-Row 12' Pines - 40'

+32-Range T18

+26-Row 12' Pines - 44'

+08-Ent

6 12' 13'

+96-PP & Fc Cor - 28'

+87-Fc Cor - 28'

+73-End Row Elm - 34'

+72-Div Fc - 23'

+50-Elm -

+24-3"E/m -

5 13' 11'

+96-Elm -

+84-PP-28

+70-Elm -

+81-8'0-31' Stp-22'

+79-8'0-32' Stp-23'

+74-6'0-30'

+67-8'0-36'

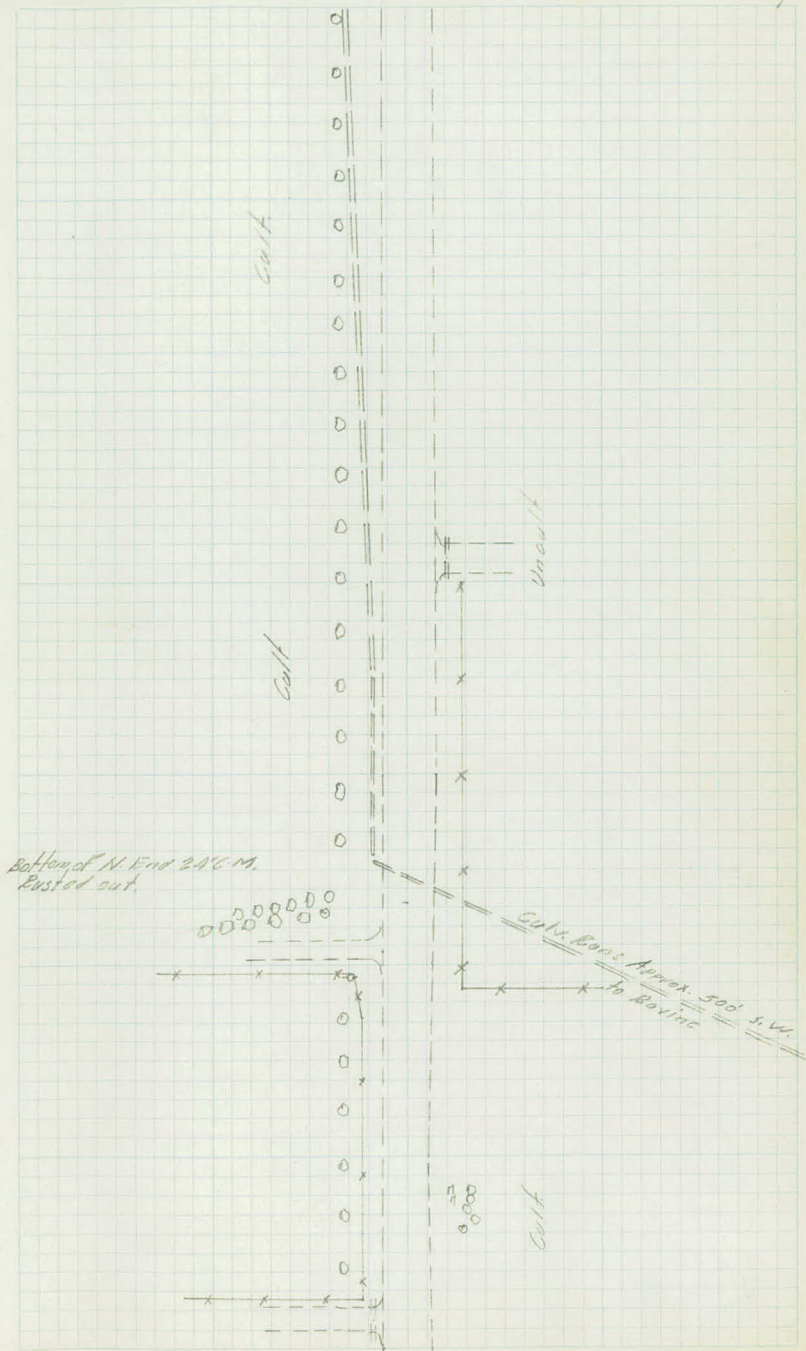
+63-10'0-29'

+42-Beg Row 3"E/m-33'

+25-Fc Cor - 23'

+15-Ent

4 12' 13'



+65-End Swamp

17 11' 13' +10-Beg Fe - 22'
+82-PP - 27'

16 11' 13'
+64-PP - 27'

15 11' 13'
+45-PP - 28'

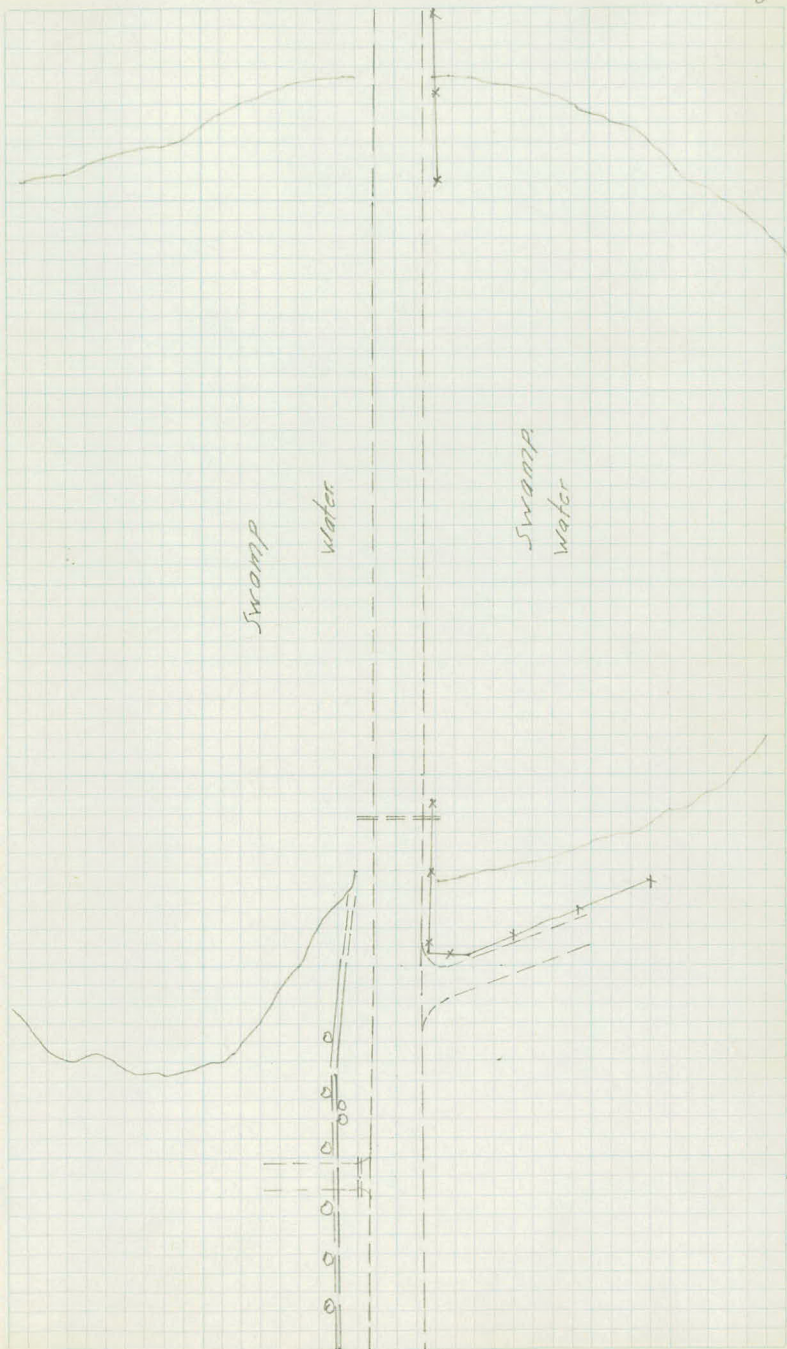
14 11' 13'
+177-X Drawn - 24' X 42' Conc. Col'n. 20' 22' +86-End Fe - 19'

+50-Swamp - 20'
+37-End Ditch - 23'
+29-PP - 27'
+17-15' X 20' C.M. - 24' Uncovered 11' Laying in ditch
13 12' +107-Fe Cor - 15 Ditch - 28'
+84-Ent - 54'

+63-2" Elm - 35'
+55-Beg Swamp - 85' 1' wide
+43-End 12" C.M. 19-31-Beg Ditch
+36-2" Elm - 35'
+32-2" PP - 28'
+30-2" Elm - 28'
+09-PP - 28'
12 +25-2" Elm - 35' 13' 12'

+90-Ent 15' X 20' C.M.
+75-3" Elm -
+48-4" Elm -
+22-2" Elm -

11 13' 13'



+73-Ent/12" G.M. - 20.5'

+53-Motor P-31'

24 P.P.-28'

13' 13'

+96-Fc. Cor-33'

23 Fc.-32

13' 13'

+89-P.P.-27'

+54-Ent - $\frac{12" \times 18" G.M.}{19'}$

22

13' 13'

+69-M.P.-26'

+50-End cult.

21 Fc.-32
+90-Box Cult.

14' 13'

+46-P.P.-27'

20

13' 14'

+54-Fc. Cor-33'

+29-P.P.-27'

19

11' 13'

+62-Ent $\frac{12" \times 24" G.M.}{21'}$

+60-End Fc-42'

+40-Δ in Fc-19' & Ent-43'

18 +65-P.P.-27'

10' 13'

Great Lakes
Pipe Line Co.
Plant.

x x x

Cult

+50-T.P.-32' FC-36'

31 FC-39' 17' 10'

+65-Ent.

~~126~~-Group 7 B.E.-31'

30 17' 10'

+75-T.P.-30'

+23-Beg. FC-34'

29

14' 11'

+39-Ent. $\frac{24 \times 20 \times 14}{20}$

+29-24' Maple-26'

+22-24' Ash-26'

+97-20' Maple-24'

+86-8' Ash-25'

+76-Ent 12' C.M.-18'

+55-Ent.

+55-30' Maple-27'

+36-2' Elm-30'

28 +103-PP-29'

13' 13'

+106-Ent 12' C.M.-18'

27 13' 13'

+26-FC-23'
+23-PP-27'

12'-133'

+21-Ent 12' C.M.-20'

30-115'

26 Approx E. Rd.

37+94' 12' C.M.

+77-High Line PP-29' Euns N. & S.

+75-Ent C.M.-20'

+71-FC Cor-33'

+71-FC Cor-33'

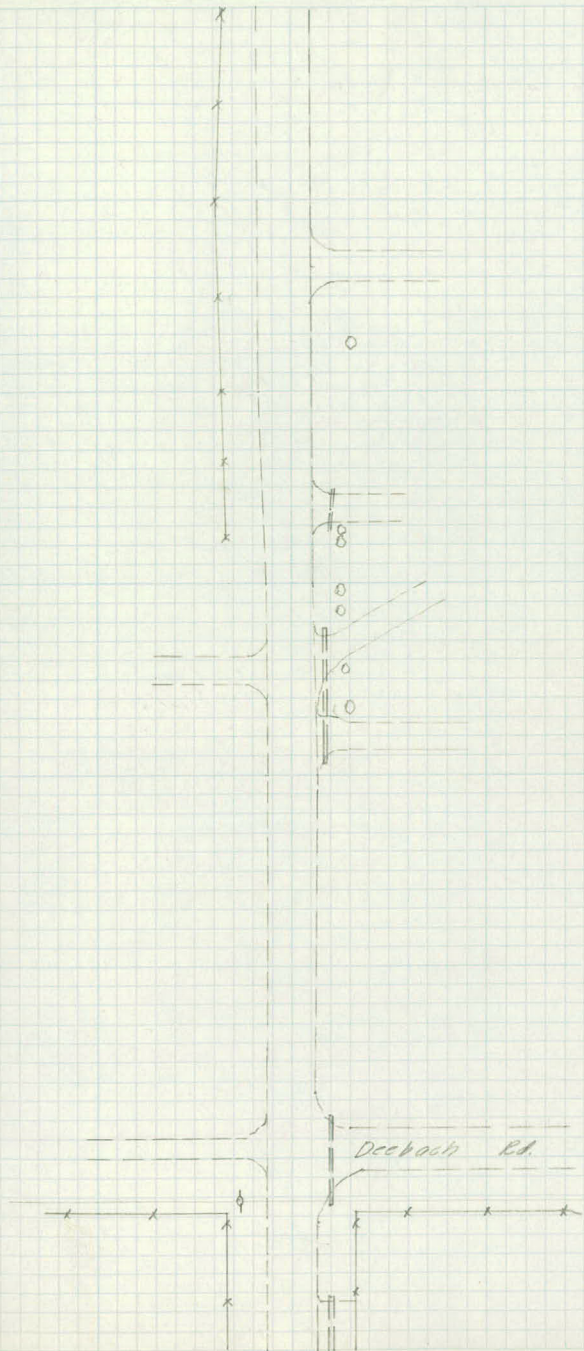
+65-Broad St. App-30'

14'-167'

25 +109-PP-27'

13' 13'

+27-Ent 12' C.M.-20'



FC-34

19' 8'

Brush-14'

38 FC-37

19' 6'

Brush-10'

+50-Box Brush-12'

+56'-24" X 20' C.M. - 45'

+29-Ent-

+10-Ent 42' C.M. - 29'

37 FC-35

19' 6'

42' X 49' C.M. X Drain

+98-Ent 42' C.M. - 19'

+92-Just. of Ditch 25-32'

+78-Div Ditch - 33'

+64-Div Ditch - 57'-87'

+52-Ent 40' H

+67-T.P.-34'

36 FC-33

18' 7'

+91-Ent 15' X 20' C.M. - 25'

+36-Widening Rd. Side - 9'

+01-T.P.-33'

35 FC-33

18' 8'

+78-8" B.E.-37'

+06-Ent

34 FC-34

17' 8'

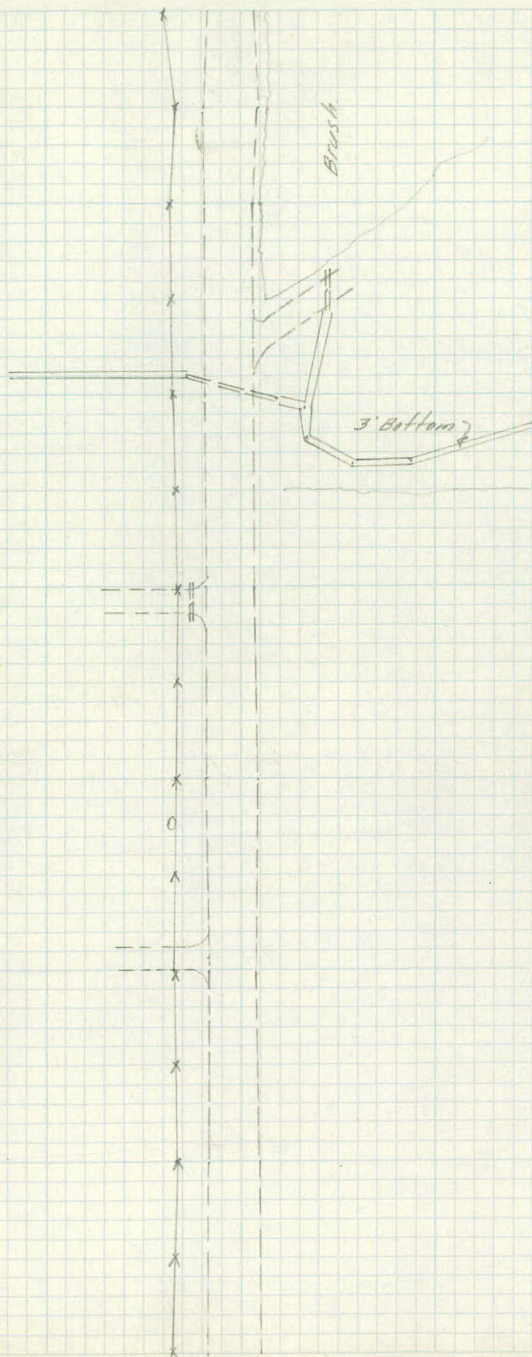
+24-T.P.-33

33 FC-33

17' 10'

32 FC-35

17' 10'



+50-12' 8'

+28 Cor Barr. - 57'

+11 - Dia Fc - 31' - 37'

+15 - Ent.

45

11' 9'

+78-24" B.E. - 45

+62-24" Elm - 46

+53-30" Elm - 45 +95 Dia Fc - 57'

+26 Range Tie +91 Dia Fc - 26'

+30 Cor No - 67'

+27 Reg. Fc - 25'

+29-24" Elm - 46

+17-20" Elm - 45

+66-20" Elm - 45

44

13' 9'

+88-24" B.E. - 47

+84-24" B.E. - 43'

43 7 Ent - 39'

12' 10'

+56 - Ent 15' X 34 C/M - 19'

42

10' 11'

41

11' 11'

11' 11' +65 - End Brush - 37'

40

12' 8'

Brush - 18'

Fc - 41'

17' 7'

Brush - 15'

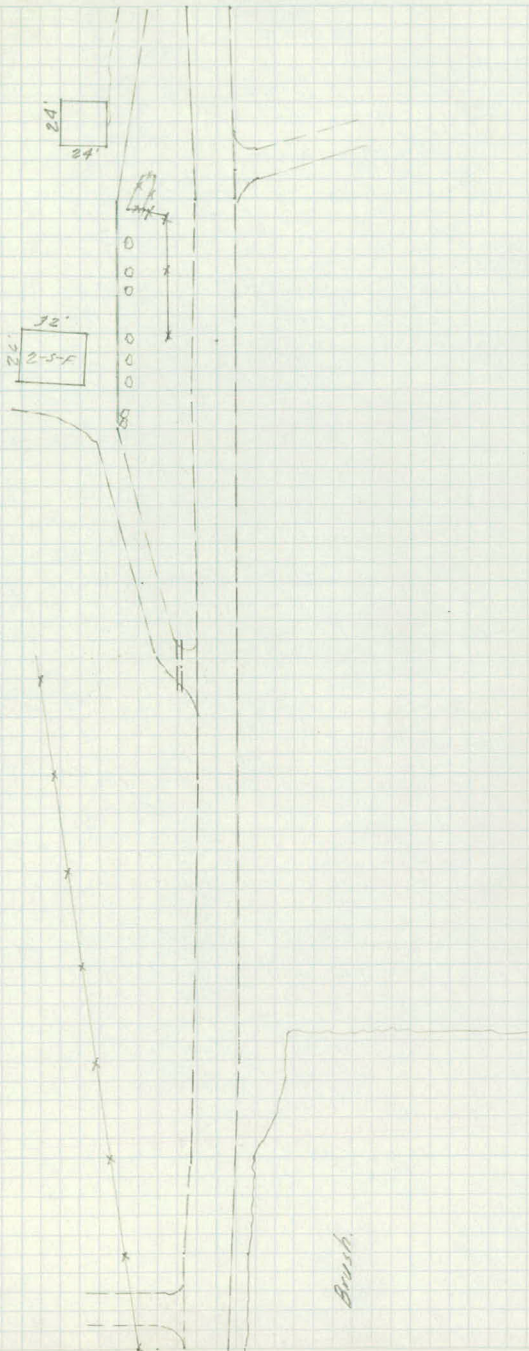
+22 - Ent.

39

Fc - 40'

16' 6'

Brush - 14'



+75-10 10

52 10 10'

10' - 10'

51 9' 11'

10' - 10'

50 10' 9'

+40-36" x 12' C.M. - 2.5'

49 10' 8'

+54-36" x 14' C.M. - 2.4'

48 9' 9'

10' 11'

47 12' 10'

+75-12" Tw BE. - 3.2'

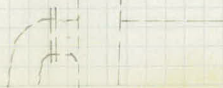
+50-15' 8' +40-Ent-

+25-Ent-15" x 20' C.M. - 2.7'

46 15' 6'

||

||

0
0
0
0

+26.91 11' 10'

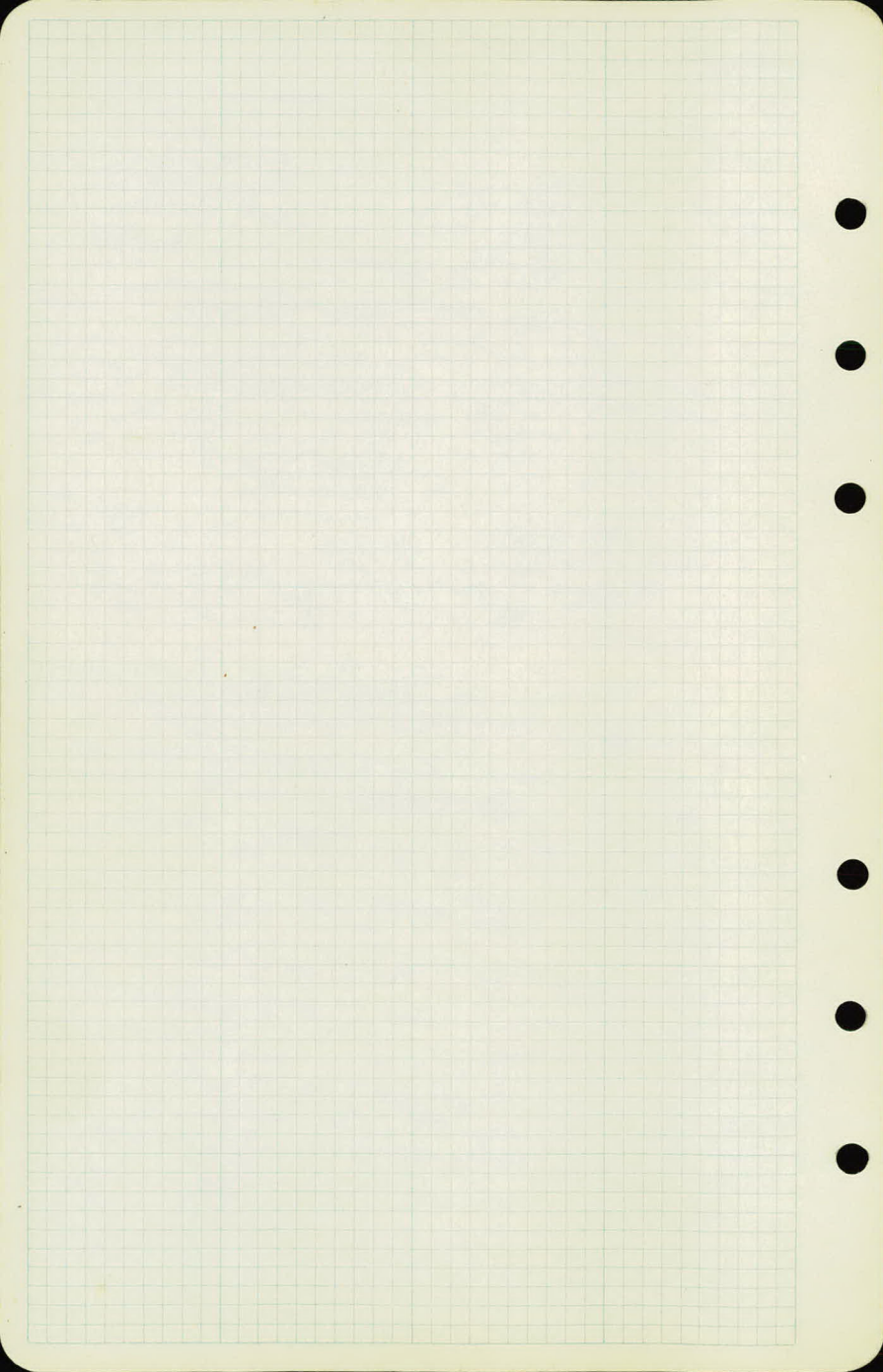
54 12' 10'

11' 14'

+34-Ent.

53 11' 10'





Lt

d

Rt

Bench Levels

Note: Use figures in red as levels
were 0.29' to high.

sto.	t	T	-	E/CN	
B.M.	6.48	861.48			854.71 855.00
T.P.	13.36	874.35	0.49	860.99	
T.P.	7.97	880.59	1.73	872.62	
T.P.	7.90	885.64	2.85	877.4	
T.P.	6.80	886.53	5.91	879.73	
T.P.	11.29	896.55	1.27	885.26	
T.P.	12.78	908.96	0.37	896.18	
B.M.			2.00	906.96	906.67
T.P.	6.39	915.13	0.16	908.80	
T.P.	0.94	915.39	0.68	914.45	
T.P.	10.06	914.95	10.50	904.89	913.32
B.M.			1.34	913.61	913.32
B.M.			0.84	914.11	913.82
T.P.	12.98	927.76	0.18	914.78	
T.P.	9.06	933.40	3.42	924.34	
B.M.			10.00	923.40	923.11
B.M.	13.27	938.67	8.00	925.40	925.11
T.P.	13.37	952.03	0.01	938.66	
T.P.	13.63	965.51	0.15	951.88	
T.P.	13.24	972.71	0.04	965.47	
T.P.	5.69	984.35	0.05	978.66	
B.M.			368	980.67	980.38

Description

Spikes in P.R. 26 Lt Sta 0416

Spk. in P.R. N.W. Cor. Deedock Rd + Carver Ave.

599.54

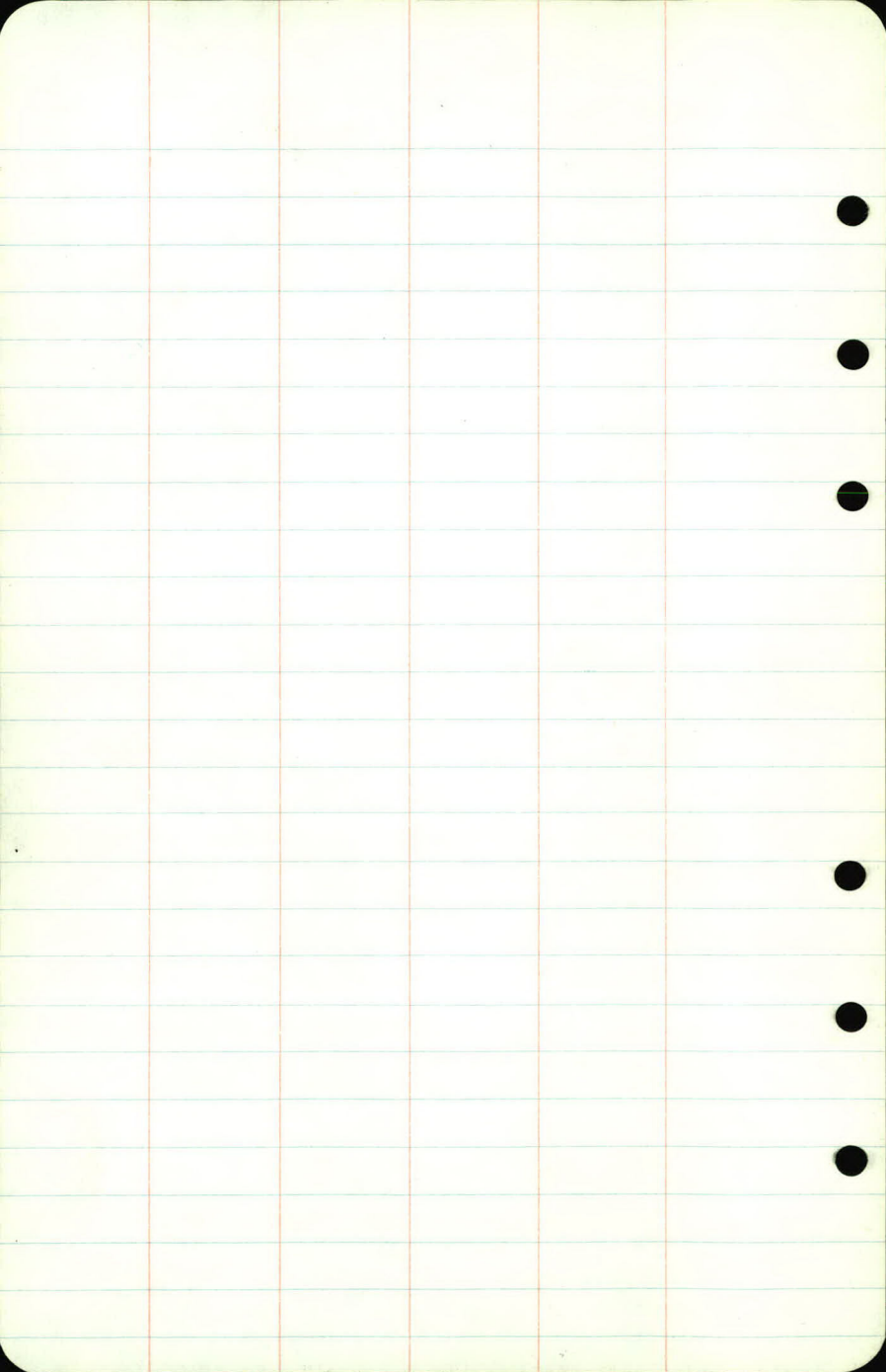
Spk in stump Lt. 39 + 90

P.R. Spike in Top Stump 50 Lt Sta. 39 + 90

Spk in 15" B.R. 40 Lt. Sta. 46 + 60

Top E. End Ent. Culv. 27 Lt 46 + 35

Top Cons. Base of St. Sign at Carver Ave + E. Co. Line



X sections

Sta	+	π	-	Elev
B.M.	6.48	861.19		854.71

0	-50		7.6	
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-1			9.1	
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-1	+50		11.4	
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-2	+00		13.2	
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0	+00	= 13 + 94.85		54.3
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	+50			55.2
--	-----	--	--	------

1				56.1
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	+50			57.5
--	-----	--	--	------

2				59.2
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T.P.	13.36	874.06	0.49	860.70
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	+50			61.3
--	-----	--	--	------

3				63.5
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Lt.

K

Rt

spike in PP 20 Lt sta 0+16

63	71	80	71	69	69	76	85	84	50	49	63
50	39	23	17	8	18	21	23	29	35	50	

66	74	82	73	74	65	60	64	81	81	65	65	71	69
50	24	19	18	15	12	16	19	22	25	30	39	50	

70	70	72	67	58	51	54	70	69	68
50	38	23	16	13	15	19	37	50	

64	65	70	44	37	41	57	57	57
50	34	22	13	13	19	20	50	

57	51	56	27	20	21	33	32	22	17
50	33	22	13	14	16	23	28	50	

158	160	175	133	128	127	148	148	94	88
50	34	25	12	13	19	22	32	50	

109	108	121	121	113	106	107	124	124	41	55
50	26	22	17	14	14	18	22	35	50	

569 + π - E/cv

874.06

3 +34 65.0

+69 66.3

4 67.2

+21 67.7

+44 68.3

+72 69.1

5 69.5

+34 70.2

+80 71.1

6 71.5

T.R. 7.97 880.30 1.73 872.33.

+50 72.3

Lt

2

Rt

$$\frac{76}{50} \quad \frac{59}{37} \quad \frac{70}{26} \quad \frac{108}{16} \quad \frac{97}{13} \quad \frac{91}{14} \quad \frac{94}{18} \quad \frac{109}{21} \quad \frac{109}{33} \quad \frac{30}{50}$$

$$\frac{68}{50} \quad \frac{61}{33} \quad \frac{65}{25} \quad \frac{95}{19} \quad \frac{97}{17} \quad \frac{82}{14} \quad \frac{78}{16} \quad \frac{82}{18} \quad \frac{96}{21} \quad \frac{96}{30} \quad \frac{41}{50} \quad \frac{74}{50}$$

$$\frac{7.2}{50} \quad \frac{66}{25} \quad \frac{86}{19} \quad \frac{88}{17} \quad \frac{74}{13} \quad \frac{67}{15} \quad \frac{74}{19} \quad \frac{90}{36} \quad \frac{12.4}{50}$$

$$\frac{66}{50} \quad \frac{73}{22} \quad \frac{81}{20} \quad \frac{81}{16} \quad \frac{67}{13} \quad \frac{64}{15} \quad \frac{69}{29} \quad \frac{135}{50} \quad \frac{17.1}{50}$$

$$\frac{5.5}{50} \quad \frac{70}{23} \quad \frac{75}{21} \quad \frac{76}{15} \quad \frac{62}{12} \quad \frac{5.8}{15} \quad \frac{6.5}{28} \quad \frac{12.6}{50} \quad \frac{16.5}{50}$$

$$\frac{52}{50} \quad \frac{59}{22} \quad \frac{69}{20} \quad \frac{70}{17} \quad \frac{55}{12} \quad \frac{5.1}{15} \quad \frac{57}{18} \quad \frac{71}{21} \quad \frac{71}{23} \quad \frac{6.9}{50} \quad \frac{13.2}{50}$$

$$\frac{53}{50} \quad \frac{58}{22} \quad \frac{61}{20} \quad \frac{61}{16} \quad \frac{49}{13} \quad \frac{46}{14} \quad \frac{5.0}{18} \quad \frac{64}{21} \quad \frac{64}{24} \quad \frac{5.3}{40} \quad \frac{54}{50} \quad \frac{8.7}{50}$$

$$\frac{3.7}{50} \quad \frac{5.3}{31} \quad \frac{5.3}{15} \quad \frac{42}{12} \quad \frac{39}{15} \quad \frac{4.5}{19} \quad \frac{5.6}{22} \quad \frac{5.7}{26} \quad \frac{9.3}{40} \quad \frac{3.7}{50} \quad \frac{4.7}{50}$$

$$\frac{1.7}{50} \quad \frac{26}{27} \quad \frac{38}{16} \quad \frac{32}{12} \quad \frac{30}{15} \quad \frac{26}{18} \quad \frac{4.8}{22} \quad \frac{4.9}{24} \quad \frac{3.9}{43} \quad \frac{4.9}{50} \quad \frac{6.3}{50}$$

$$\frac{0.8}{50} \quad \frac{2.1}{27} \quad \frac{2.5}{9}$$

$$\frac{26}{13} \quad \frac{3.2}{18} \quad \frac{4.4}{30} \quad \frac{5.2}{50} \quad \frac{6.6}{50}$$

$$\frac{5.1}{50} \quad \frac{6.0}{28} \quad \frac{96}{21} \quad \frac{101}{18} \quad \frac{82}{13} \quad \frac{80}{14} \quad \frac{88}{21} \quad \frac{101}{25} \quad \frac{10.4}{50} \quad \frac{9.9}{50}$$

Sta	+	π	-	Elev
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880.30

6	+59 FL 24°C.M. LT			
---	-------------------	--	--	--

	+50 FL 12°C.M. LT			
--	-------------------	--	--	--

	+65			72.5
--	-----	--	--	------

7				73.0
---	--	--	--	------

	+50			73.7
--	-----	--	--	------

8				74.7
---	--	--	--	------

	+50			75.3
--	-----	--	--	------

9				76.3
---	--	--	--	------

	+50			77.1
--	-----	--	--	------

T.P.	12.75	890.20	2.85	877.45
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10				
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	+50			
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$$\begin{array}{r} 880.30 \\ 11 \overline{) 49} \\ 868.81 \\ \hline 11.49 \end{array}$$

$$\underline{11.49}$$

$$\begin{array}{r} 49.2 \\ 11.1 \end{array}$$

$$\begin{array}{r} 52 \ 54 \ 60 \ 90 \ 95 \ 83 \ 78 \ 86 \ 100 \ 99 \ 95 \ 9.3 \\ 50 \ 34 \ 27 \ 21 \ 16 \ 13 \ 15 \ 19 \ 23 \ 25 \ 50 \end{array}$$

$$\begin{array}{r} 50 \ 51 \ 55 \ 82 \ 84 \ 77 \ 13 \ 19 \ 89 \ 88 \ 80 \ 8.2 \\ 50 \ 37 \ 27 \ 22 \ 16 \ 13 \ 15 \ 17 \ 22 \ 24 \ 50 \end{array}$$

$$\begin{array}{r} 34 \ 41 \ 49 \ 14 \ 74 \ 68 \ 66 \ 68 \ 81 \ 80 \ 66 \ 6.3 \\ 50 \ 35 \ 26 \ 21 \ 13 \ 13 \ 14 \ 17 \ 22 \ 26 \ 50 \end{array}$$

$$\begin{array}{r} 30 \ 34 \ 44 \ 99 \ 38 \ 72 \ 72 \ 60 \ 56 \ 57 \ 68 \ 69 \ 55 \ 51 \ 48 \\ 50 \ 24 \ 29 \ 27 \ 26 \ 20 \ 16 \ 13 \ 15 \ 17 \ 22 \ 26 \ 24 \ 50 \end{array}$$

$$\begin{array}{r} 17 \ 26 \ 38 \ 32 \ 39 \ 63 \ 65 \ 53 \ 50 \ 55 \ 68 \ 68 \ 50 \ 40 \\ 50 \ 36 \ 30 \ 29 \ 25 \ 21 \ 17 \ 13 \ 14 \ 18 \ 22 \ 28 \ 50 \end{array}$$

$$\begin{array}{r} 0.7 \ 20 \ 27 \ 55 \ 57 \ 46 \ 40 \ 47 \ 58 \ 61 \ 45 \ 17 \\ 50 \ 34 \ 26 \ 21 \ 16 \ 14 \ 14 \ 17 \ 24 \ 30 \ 50 \end{array}$$

$$\begin{array}{r} 10.8 \ 00 \ 08 \ 48 \ 50 \ 37 \ 32 \ 37 \ 47 \ 46 \ 36 \ 25 \\ 50 \ 36 \ 28 \ 21 \ 17 \ 13 \ 14 \ 18 \ 23 \ 26 \ 50 \end{array}$$

Tar offset stake 1/4 stake 10/100

$$\begin{array}{r} 70 \ 78 \ 83 \ 140 \ 142 \ 129 \ 125 \ 125 \ 142 \ 142 \ 12.3 \ 114 \ 117 \ 108 \\ 50 \ 34 \ 30 \ 21 \ 17 \ 14 \ 14 \ 18 \ 21 \ 25 \ 30 \ 35 \ 50 \end{array}$$

$$\begin{array}{r} 70 \ 77 \ 87 \ 135 \ 134 \ 121 \ 117 \ 120 \ 135 \ 135 \ 120 \ 113 \\ 50 \ 36 \ 29 \ 21 \ 16 \ 14 \ 14 \ 17 \ 22 \ 25 \ 30 \end{array}$$

Sta	+	π	-	Elev
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		890.20		
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11

+50

12

+43

+68

T.P.	4.20	884.76	9.64	880.56
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13

+50

14

+50

15

+50

Lt

L

Rt

$$\frac{87}{50} \frac{89}{36} \frac{93}{26} \frac{127}{20} \frac{126}{16} \frac{116}{14} \frac{110}{14} \frac{114}{18} \frac{120}{22} \frac{128}{25} \frac{116}{25} \frac{107}{50}$$

$$\frac{97}{50} \frac{97}{35} \frac{102}{29} \frac{97}{25} \frac{121}{20} \frac{121}{17} \frac{109}{14} \frac{103}{15} \frac{106}{18} \frac{121}{22} \frac{121}{26} \frac{76}{38} \frac{76}{50}$$

$$\frac{114}{50} \frac{94}{35} \frac{92}{26} \frac{117}{21} \frac{115}{16} \frac{103}{14} \frac{100}{15} \frac{104}{18} \frac{117}{29} \frac{111}{35} \frac{28}{35} \frac{47}{50}$$

 CULV
 266

$$\frac{119}{50} \frac{103}{33} \frac{127}{31} \frac{93}{28} \frac{91}{25} \frac{115}{21} \frac{114}{16} \frac{100}{19} \frac{98}{15} \frac{102}{18} \frac{111}{24} \frac{129}{35} \frac{24}{41} \frac{33}{50}$$

$$\frac{122}{50} \frac{106}{32} \frac{131}{30} \frac{131}{29} \frac{100}{25} \frac{104}{22} \frac{116}{20} \frac{116}{17} \frac{100}{19} \frac{97}{15} \frac{99}{18} \frac{109}{23} \frac{110}{33} \frac{35}{33} \frac{53}{50}$$

$$\frac{74}{50} \frac{66}{30} \frac{79}{28} \frac{79}{27} \frac{58}{24} \frac{58}{22} \frac{66}{19} \frac{62}{17} \frac{46}{13} \frac{42}{14} \frac{43}{18} \frac{56}{22} \frac{55}{24} \frac{44}{33} \frac{36}{33} \frac{26}{50}$$

$$\frac{88}{50} \frac{84}{23} \frac{76}{20} \frac{46}{19} \frac{42}{15} \frac{50}{20} \frac{68}{34} \frac{71}{34} \frac{71}{50}$$

$$\frac{88}{50} \frac{85}{23} \frac{78}{18} \frac{47}{11} \frac{44}{15} \frac{52}{19} \frac{72}{25} \frac{76}{25} \frac{81}{50}$$

 26
 26

$$\frac{84}{50} \frac{83}{23} \frac{79}{19} \frac{53}{12} \frac{49}{16} \frac{56}{21} \frac{84}{36} \frac{90}{36} \frac{88}{50}$$

$$\frac{85}{50} \frac{84}{23} \frac{82}{18} \frac{52}{11} \frac{51}{15} \frac{62}{21} \frac{82}{21} \frac{90}{50}$$

$$\frac{82}{50} \frac{84}{24} \frac{78}{17} \frac{52}{11} \frac{51}{9} \frac{55}{15} \frac{62}{20} \frac{84}{33} \frac{91}{33} \frac{91}{50}$$

Sta	+	π	-	Elev.
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		884.76		
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16

+50

17

+50

T.P.	9.62	890.92	3.46	881.30
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18

+45

+75

19

+25

+58

20

Lt

R

Rt

$$\frac{8.5}{50} \frac{8.4}{27} \frac{8.3}{18} \frac{5.3}{12} \frac{4.9}{9} \frac{5.4}{15} \frac{6.2}{19} \frac{8.0}{30} \frac{8.8}{30} \frac{8.5}{50}$$

$$\frac{7.7}{50} \frac{8.0}{24} \frac{7.6}{18} \frac{5.0}{12} \frac{4.8}{7} \frac{5.0}{15} \frac{5.7}{20} \frac{7.6}{26} \frac{8.2}{26} \frac{8.2}{50}$$

$$\frac{7.4}{50} \frac{7.5}{31} \frac{7.2}{18} \frac{4.6}{13} \frac{4.1}{9} \frac{4.5}{15} \frac{5.1}{21} \frac{7.3}{29} \frac{7.8}{29} \frac{7.7}{50}$$

$$\frac{7.3}{50} \frac{7.5}{30} \frac{6.8}{18} \frac{4.0}{12} \frac{3.6}{15} \frac{4.7}{22} \frac{7.1}{31} \frac{7.6}{31} \frac{7.6}{50}$$

$$\frac{1.34}{50} \frac{1.28}{20} \frac{9.3}{12} \frac{9.0}{15} \frac{9.7}{23} \frac{1.27}{28} \frac{1.34}{28} \frac{12.7}{50}$$

$$\frac{1.31}{50} \frac{1.33}{25} \frac{1.25}{21} \frac{8.5}{13} \frac{8.1}{16} \frac{8.7}{20} \frac{1.05}{25} \frac{1.06}{25} \frac{9.5}{32} \frac{9.6}{50}$$

$$\frac{1.30}{50} \frac{1.27}{30} \frac{1.18}{21} \frac{8.07}{12} \frac{8.1}{15} \frac{9.5}{18} \frac{7.7}{27} \frac{1.1}{36} \frac{+4.9}{47} \frac{+9.1}{55} \text{ L.O.}$$

$$\frac{1.27}{50} \frac{1.21}{30} \frac{1.14}{22} \frac{7.7}{12} \frac{7.2}{14} \frac{7.7}{16} \frac{8.5}{21} \frac{8.2}{31} \frac{1.1}{34} \frac{+7.3}{4.1} \frac{+8.6}{4.6} \text{ L.O.}$$

$$\frac{1.21}{50} \frac{1.10}{33} \frac{8.3}{28} \frac{7.8}{23} \frac{8.4}{21} \frac{8.3}{17} \frac{7.1}{13} \frac{6.8}{14} \frac{7.2}{16} \frac{7.8}{22} \frac{6.4}{32} \frac{0.3}{40} \frac{+9.5}{4.0} \text{ L.O.}$$

$$\frac{8.8}{50} \frac{6.8}{41} \frac{6.9}{26} \frac{8.2}{21} \frac{8.2}{17} \frac{6.7}{13} \frac{6.3}{13} \frac{6.6}{17} \frac{7.8}{24} \frac{6.2}{24} \frac{+6.3}{42} \text{ L.O.}$$

$$\frac{1.08}{50} \frac{5.9}{37} \frac{6.2}{23} \frac{7.5}{20} \frac{7.4}{17} \frac{6.1}{14}$$

$$\frac{5.7}{14} \frac{6.1}{17} \frac{7.2}{22} \frac{7.3}{22} \frac{+0.2}{34} \frac{1.04}{50}$$

Sta	+	π	-	Elev
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		890.92		
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20	+50			
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	+82			
--	-----	--	--	--

21				
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	+50			
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22				
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	+50			
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T.P.	12.25	903.17	0.00	890.92
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23				
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	+50			
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24				
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	+38			
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	+68			
--	-----	--	--	--

Lt.

4

Rt.

$$\frac{12.0}{50} \frac{11.6}{36} \frac{10.4}{25} \frac{5.4}{14} \frac{5.1}{14} \frac{5.5}{17} \frac{6.8}{21} \frac{6.8}{21} \frac{3.5}{26} \frac{3.1}{50}$$

$$\frac{11.7}{50} \frac{11.8}{35} \frac{10.1}{26} \frac{5.2}{14} \frac{4.8}{13} \frac{5.1}{17} \frac{6.3}{22} \frac{6.2}{22} \frac{4.3}{28} \frac{3.7}{50}$$

$$\frac{11.7}{50} \frac{11.4}{35} \frac{10.1}{25} \frac{5.1}{14} \frac{4.6}{19} \frac{5.0}{17} \frac{6.0}{21} \frac{5.9}{21} \frac{4.3}{26} \frac{3.2}{50}$$

$$\frac{10.1}{50} \frac{8.4}{34} \frac{7.4}{22} \frac{4.1}{14} \frac{3.7}{15} \frac{3.8}{16} \frac{4.8}{22} \frac{4.7}{22} \frac{1.0}{28} \frac{0.7}{50}$$

$$\frac{5.0}{50} \frac{2.9}{34} \frac{2.2}{24} \frac{3.7}{21} \frac{3.6}{16} \frac{2.8}{14} \frac{2.3}{17} \frac{2.4}{17} \frac{3.6}{22} \frac{1.2}{26} \frac{1.5}{50}$$

$$\frac{4.8}{50} \frac{3.3}{33} \frac{2.6}{24} \frac{2.4}{18} \frac{1.0}{14} \frac{0.5}{14} \frac{1.0}{17} \frac{2.0}{17} \frac{2.0}{22} \frac{1.5}{25} \frac{2.3}{50}$$

Nailin PR Lt. 22+

$$\frac{18.3}{50} \frac{16.9}{26} \frac{11.5}{14} \frac{16.9}{13} \frac{11.2}{17} \frac{12.3}{22} \frac{12.2}{22} \frac{11.1}{25} \frac{11.7}{30} \frac{11.6}{50}$$

$$\frac{17.2}{50} \frac{14.7}{33} \frac{13.1}{23} \frac{9.3}{14} \frac{8.4}{13} \frac{9.1}{16} \frac{10.1}{21} \frac{10.0}{21} \frac{6.4}{28} \frac{5.7}{50}$$

$$\frac{11.1}{50} \frac{8.4}{32} \frac{6.8}{23} \frac{7.9}{21} \frac{7.8}{17} \frac{6.8}{14} \frac{6.3}{14} \frac{6.6}{14} \frac{7.9}{17} \frac{7.8}{21} \frac{3.0}{28} \frac{3.5}{50}$$

$$\frac{6.6}{50} \frac{4.0}{33} \frac{3.4}{27} \frac{6.3}{21} \frac{6.3}{17} \frac{5.0}{14} \frac{4.5}{13} \frac{4.2}{17} \frac{6.2}{21} \frac{6.2}{21} \frac{1.1}{29} \frac{L.O.}{50}$$

$$\frac{7.1}{50} \frac{4.8}{32} \frac{3.9}{25} \frac{5.4}{22} \frac{5.2}{17} \frac{3.7}{13} \frac{3.1}{13} \frac{3.1}{19} \frac{4.9}{18} \frac{4.9}{21} \frac{1.2}{28} \frac{L.O.}{50}$$

Sta + π - E/EX

903.17

25

T.P. 10.63 913.54 0.26 902.91

+29

+71

B.M. 6.87 906.67 (906.67)

26 +03.89

+27

+59

27

+27

+68

28

+40

Lt

R

Rt

$$\frac{6.6}{50} \frac{5.4}{33} \frac{4.4}{19}$$

$$\frac{2.2}{14}$$

$$\frac{1.6}{13} \frac{1.6}{32} \frac{0.8}{32} \text{ L.O.}$$

$$\frac{13.8}{50} \frac{13.2}{33} \frac{12.5}{17} \frac{11.2}{14} \frac{10.6}{14} \frac{10.9}{18} \frac{12.3}{21} \frac{12.4}{25} \frac{11.0}{32} \frac{10.9}{32} \text{ L.O.}$$

$$\frac{8.1}{50} \frac{7.7}{28} \frac{7.8}{22} \frac{10.0}{16} \frac{9.2}{13}$$

$$\frac{8.8}{15} \frac{9.2}{19} \frac{10.7}{25} \frac{10.8}{27} \frac{10.1}{50}$$

Spk 12 P.R.N.W. Cor Deebach Rd + Corner Ave.

$$\frac{9.9}{100} \frac{8.4}{50} \frac{7.4}{50} \frac{7.3}{100} \frac{6.7}{150} \frac{5.8}{150}$$

$$\frac{6.4}{50} \frac{5.4}{25} \frac{8.5}{20} \frac{8.4}{18} \frac{7.1}{15} \frac{6.6}{14} \frac{6.9}{17} \frac{8.0}{21} \frac{8.1}{24} \frac{5.5}{29} \frac{3.6}{36} \frac{5.5}{50}$$

$$\frac{6.6}{50} \frac{5.4}{25} \frac{7.4}{21} \frac{7.6}{18} \frac{6.3}{14} \frac{5.8}{15} \frac{6.2}{18} \frac{7.4}{22} \frac{7.3}{29} \frac{3.2}{38} \frac{3.7}{50} \frac{3.3}{50}$$

$$\frac{8.1}{50} \frac{5.6}{24} \frac{6.7}{21} \frac{6.5}{17} \frac{5.5}{14}$$

$$\frac{5.1}{15} \frac{5.7}{17} \frac{6.6}{22} \frac{6.3}{27} \frac{3.8}{30} \frac{3.5}{36} \frac{1.8}{50} \frac{1.7}{50}$$

$$\frac{9.1}{50} \frac{5.6}{22} \frac{6.0}{21} \frac{6.2}{18} \frac{5.1}{15} \frac{4.9}{14} \frac{5.3}{17} \frac{6.7}{20} \frac{6.7}{25} \frac{4.2}{32} \frac{2.6}{50} \frac{3.1}{50}$$

$$\frac{10.2}{50} \frac{8.0}{20} \frac{5.1}{14}$$

44

$$\frac{4.6}{14} \frac{5.0}{17} \frac{6.5}{19} \frac{6.5}{20} \frac{6.1}{29} \frac{4.7}{30} \frac{4.5}{50}$$

$$\frac{10.0}{50} \frac{9.5}{31} \frac{8.7}{22} \frac{5.2}{14} \frac{4.7}{13} \frac{5.0}{16} \frac{6.3}{19} \frac{6.6}{21} \frac{5.8}{25} \frac{4.7}{50}$$

$$\frac{7.9}{50} \frac{7.2}{25} \frac{6.8}{18} \frac{5.3}{15} \frac{4.8}{21} \frac{4.9}{24} \frac{3.6}{35} \frac{3.4}{50} \frac{1.5}{50}$$

Sta	+	π	-	E/cK
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913.54

28 +81

29

+15

T.R	5.89	914.42	5.01	908.52
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+30

+65

30

+17

+39

+59

T.R	11.73	923.52	2.63	911.79
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31

+30

Lt.

4

Rt.

$$\frac{71}{50} \quad \frac{60}{25} \quad \frac{69}{23} \quad \frac{68}{18} \quad \frac{54}{14} \quad \frac{50}{12} \quad \frac{51}{14} \quad \frac{66}{19} \quad \frac{65}{22} \quad \frac{25}{22} \quad \frac{2.3}{39} \quad \frac{1.4}{50}$$

$$\frac{86}{50} \quad \frac{82}{32} \quad \frac{72}{19} \quad \frac{54}{15} \quad \frac{50}{12} \quad \frac{55}{16} \quad \frac{74}{18} \quad \frac{74}{22} \quad \frac{29}{27} \quad \frac{2.0}{50}$$

$$\frac{118}{50} \quad \frac{115}{36} \quad \frac{99}{25} \quad \frac{55}{15} \quad \frac{51}{10} \quad \frac{55}{16} \quad \frac{83}{19} \quad \frac{84}{29} \quad \frac{2.7}{29} \quad \frac{1.7}{50}$$

$$\frac{141}{50} \quad \frac{134}{32} \quad \frac{64}{17} \quad \frac{59}{12} \quad \frac{64}{17} \quad \frac{101}{32} \quad \frac{104}{50}$$

$$\frac{154}{50} \quad \frac{144}{35} \quad \frac{129}{29} \quad \frac{6.7}{16}$$

$$\frac{58}{12} \quad \frac{62}{30} \quad \frac{144}{50}$$

$$\frac{136}{50} \quad \frac{134}{37} \quad \frac{113}{26} \quad \frac{61}{17} \quad \frac{5.3}{12} \quad \frac{54}{12} \quad \frac{156}{30} \quad \frac{17.8}{50}$$

$$\frac{125}{50} \quad \frac{122}{36} \quad \frac{104}{26} \quad \frac{5.6}{16} \quad \frac{50}{12} \quad \frac{53}{28} \quad \frac{134}{33} \quad \frac{144}{50} \quad \frac{16.0}{50}$$

$$\frac{9.2}{50} \quad \frac{90}{36} \quad \frac{85}{25} \quad \frac{52}{17} \quad \frac{44}{17} \quad \frac{48}{20} \quad \frac{81}{50} \quad \frac{11.4}{50}$$

$$\frac{39}{50} \quad \frac{40}{29} \quad \frac{54}{26} \quad \frac{54}{20} \quad \frac{44}{17} \quad \frac{38}{17} \quad \frac{43}{17} \quad \frac{47}{13} \quad \frac{47}{19} \quad \frac{30}{25} \quad \frac{2.7}{35} \quad \frac{4.3}{50}$$

$$\frac{4.9}{50} \quad \frac{42}{39} \quad \frac{117}{29} \quad \frac{130}{24} \quad \frac{131}{22} \quad \frac{122}{17} \quad \frac{11.7}{12} \quad \frac{123}{14} \quad \frac{130}{20} \quad \frac{127}{29} \quad \frac{6.8}{50} \quad \frac{8.7}{50}$$

$$\frac{1.8}{50} \quad \frac{0.7}{37} \quad \frac{11.2}{27} \quad \frac{11.8}{20} \quad \frac{11.3}{17}$$

$$\frac{110}{12} \quad \frac{116}{15} \quad \frac{12.3}{20} \quad \frac{12.2}{30} \quad \frac{51}{50} \quad \frac{6.3}{50}$$

Sta	+	π	-	Elev.
		923.52		
31	+69			
32				
	+50			
33				
T.P.	6.53	917.51	12.54	910.98
	+50			
34				
	+50			
35				
	+50			
36				
T.P.	2.83	909.72	10.62	906.89
	+50			

Lt

E

Rt

$$\frac{30}{50} \quad \frac{2.0}{36} \quad \frac{108}{24} \quad \frac{114}{20} \quad \frac{103}{17} \quad \frac{99}{-}$$

$$\frac{103}{12} \quad \frac{112}{14} \quad \frac{109}{20} \quad \frac{45}{30} \quad \frac{31}{50}$$

$$\frac{56}{50} \quad \frac{53}{43} \quad \frac{44}{35} \quad \frac{106}{25} \quad \frac{108}{20} \quad \frac{98}{18} \quad \frac{91}{12} \quad \frac{96}{14} \quad \frac{106}{22} \quad \frac{100}{31} \quad \frac{37}{50} \quad \frac{24}{50}$$

$$\frac{113}{50} \quad \frac{115}{43} \quad \frac{100}{27} \quad \frac{105}{25} \quad \frac{104}{21} \quad \frac{93}{18} \quad \frac{86}{21} \quad \frac{88}{26} \quad \frac{64}{34} \quad \frac{58}{50} \quad \frac{4.0}{50}$$

$$\frac{133}{50} \quad \frac{133}{36} \quad \frac{120}{24} \quad \frac{98}{18}$$

$$\frac{92}{9} \quad \frac{94}{24} \quad \frac{85}{50} \quad \frac{4.7}{50}$$

Nail in T.P. Lt sta +

$$\frac{75}{50} \quad \frac{75}{33} \quad \frac{46}{23} \quad \frac{48}{18} \quad \frac{45}{8} \quad \frac{44}{14} \quad \frac{48}{21} \quad \frac{42}{35} \quad \frac{21}{50} \quad \frac{05}{50}$$

$$\frac{72}{50} \quad \frac{74}{32} \quad \frac{6.9}{22} \quad \frac{5.7}{18} \quad \frac{5.4}{9} \quad \frac{5.4}{9} \quad \frac{60}{19} \quad \frac{69}{20} \quad \frac{6.2}{31} \quad \frac{4.2}{50} \quad \frac{3.4}{50}$$

$$\frac{6.7}{50} \quad \frac{6.5}{30} \quad \frac{8.4}{26} \quad \frac{8.4}{21} \quad \frac{6.9}{19} \quad \frac{6.6}{6} \quad \frac{6.8}{9} \quad \frac{7.1}{12} \quad \frac{8.1}{27} \quad \frac{6.0}{50} \quad \frac{6.3}{50}$$

$$\frac{8.7}{50} \quad \frac{9.2}{34} \quad \frac{9.1}{28} \quad \frac{100}{26} \quad \frac{100}{21} \quad \frac{8.4}{18} \quad \frac{8.0}{7} \quad \frac{8.0}{8} \quad \frac{8.5}{11} \quad \frac{9.1}{31} \quad \frac{7.9}{50} \quad \frac{7.2}{50}$$

$$\frac{7.9}{50} \quad \frac{9.4}{31} \quad \frac{11.3}{26} \quad \frac{11.4}{23} \quad \frac{9.4}{19} \quad \frac{9.2}{11} \quad \frac{9.2}{8} \quad \frac{9.7}{10} \quad \frac{10.6}{19} \quad \frac{10.1}{40} \quad \frac{7.6}{50} \quad \frac{6.8}{50}$$

$$\frac{100}{50} \quad \frac{10.5}{30} \quad \frac{12.2}{27} \quad \frac{12.4}{21} \quad \frac{11.0}{18} \quad \frac{10.3}{8} \quad \frac{10.5}{7} \quad \frac{11.0}{12} \quad \frac{12.2}{25} \quad \frac{13.0}{50} \quad \frac{12.0}{50}$$

$$\frac{4.5}{50} \quad \frac{5.1}{32} \quad \frac{5.7}{29} \quad \frac{5.6}{24} \quad \frac{4.1}{19} \quad \frac{3.6}{7} \quad \frac{3.8}{7} \quad \frac{4.3}{16} \quad \frac{8.3}{33} \quad \frac{9.0}{50} \quad \frac{9.8}{50}$$

Sta	+	π	-	Elev
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90972

36	+80			
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+98

37	+10			
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+35

38				
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+50

39				
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+50

T.P.	7.30	915.51	1.51	908.21
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+75

B.M.	1.65	915.97	1.65	913.86	(913.82)
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40				
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+50

11.8

L.H.

E

R.H.

$$\frac{91}{50} \quad \frac{86}{31} \quad \frac{76}{25} \quad \frac{48}{19} \quad \frac{43}{8} \quad \frac{44}{50} \quad \frac{107}{17} \quad \frac{116}{22} \quad \frac{111}{25} \quad \frac{122}{30} \quad \frac{133}{32} \quad \frac{133}{36} \quad \frac{115}{36} \quad \frac{105}{50}$$

(FL. 6/14)

$$\frac{108}{50} \quad \frac{101}{36} \quad \frac{90}{27} \quad \frac{52}{20} \quad \frac{46}{6} \quad \frac{48}{7} \quad \frac{52}{15} \quad \frac{25}{18} \quad \frac{1301}{37} \quad \frac{131}{41} \quad \frac{105}{41} \quad \frac{95}{50}$$

(FL. 6/14)

$$\frac{128}{50} \quad \frac{1298}{29.4} \quad \frac{95}{27} \quad \frac{5.2}{20} \quad \frac{4.7}{9} \quad \frac{50}{8} \quad \frac{54}{14} \quad \frac{84}{18} \quad \frac{94}{33} \quad \frac{100}{35} \quad \frac{121}{39} \quad \frac{123}{39} \quad \frac{100}{39} \quad \frac{9.3}{50}$$

$$\frac{111}{50} \quad \frac{112}{35} \quad \frac{101}{30} \quad \frac{55}{21} \quad \frac{50}{8} \quad \frac{53}{6} \quad \frac{59}{12} \quad \frac{91}{19} \quad \frac{101}{34} \quad \frac{103}{34} \quad \frac{96}{50}$$

$$\frac{110}{50} \quad \frac{109}{37} \quad \frac{100}{34} \quad \frac{92}{28} \quad \frac{55}{20} \quad \frac{53}{6} \quad \frac{57}{7} \quad \frac{62}{14} \quad \frac{99}{23} \quad \frac{104}{23} \quad \frac{103}{50}$$

$$\frac{104}{50} \quad \frac{104}{35} \quad \frac{98}{31} \quad \frac{53}{22} \quad \frac{50}{9} \quad \frac{56}{9} \quad \frac{66}{14} \quad \frac{96}{30} \quad \frac{106}{30} \quad \frac{103}{50}$$

$$\frac{95}{50} \quad \frac{95}{35} \quad \frac{35}{24} \quad \frac{36}{9} \quad \frac{44}{50} \quad \frac{45}{9} \quad \frac{53}{16} \quad \frac{82}{28} \quad \frac{98}{28} \quad \text{L.O.}$$

9074

$$\frac{6.0}{50} \quad \frac{5.7}{29} \quad \frac{1.2}{21} \quad \frac{16}{7} \quad \frac{23}{9} \quad \frac{31}{18} \quad \frac{65}{30} \quad \frac{81}{30} \quad \text{L.O.}$$

$$\frac{86}{50} \quad \frac{103}{40} \quad \frac{98}{25} \quad \frac{62}{17} \quad \frac{70}{11} \quad \frac{77}{16} \quad \frac{110}{22} \quad \frac{12.6}{22} \quad \frac{14.3}{50}$$

R.R. Sph. in Top Stamp. 50' L.H. Sta. 39 + 90

$$\frac{0.3}{50} \quad \frac{28}{30} \quad \frac{6.3}{25} \quad \frac{80}{22} \quad \frac{80}{20} \quad \frac{53}{16} \quad \frac{61}{14} \quad \frac{6.9}{16} \quad \frac{84}{21} \quad \frac{7.5}{34} \quad \frac{90}{34} \quad \frac{78}{50}$$

$$\frac{41}{22} \quad \frac{41}{16} \quad \frac{34}{13} \quad \frac{37}{16} \quad \frac{47}{20} \quad \frac{6.0}{20} \quad \frac{106}{34}$$

Sta	+	π	-	Elev.
		915.47		
T.P.	10.41	922.38	3.50	911.97

40 +50

+75

41

+50

42

T.P. #1			4.82	917.56
---------	--	--	------	--------

T.P.	13.27	935.65	0.00	922.38
------	-------	--------	------	--------

40 +50

T.P.	12.80	944.44	4.01	931.64
------	-------	--------	------	--------

40 +50

+75

41

+50

42

T.P.	0.43	931.42	13.45	930.99
------	------	--------	-------	--------

Lt

Z

Rt

$$\frac{31}{35} \text{ L.O.}$$

$$\frac{76}{23} \quad \frac{97}{16} \quad \frac{95}{13} \quad \frac{95}{17} \quad \frac{106}{17} \quad \frac{114}{19} \quad \frac{109}{24} \quad \frac{25}{37} \quad \frac{0.2}{37} \quad \frac{1.5}{50}$$

$$\frac{103}{35} \quad \frac{86}{19} \quad \frac{93}{15} \quad \frac{88}{12} \quad \frac{85}{16} \quad \frac{94}{19} \quad \frac{101}{24} \quad \frac{90}{37} \quad \frac{66}{31} \quad \frac{30}{35} \quad \frac{0.8}{35} \quad \frac{32}{50}$$

$$\frac{104}{33} \quad \frac{83}{17} \quad \frac{84}{15} \quad \frac{76}{13} \quad \frac{69}{15} \quad \frac{76}{18} \quad \frac{91}{22} \quad \frac{93}{28} \quad \frac{68}{28} \quad \frac{100}{50}$$

$$\frac{31}{29} \quad \frac{68}{16} \quad \frac{63}{13} \quad \frac{58}{12} \quad \frac{61}{16} \quad \frac{68}{29} \quad \frac{91}{29} \quad \frac{12.0}{50}$$

$$\frac{51}{43} \quad \frac{116}{43} \quad 13.9$$

$$\frac{30}{100} \quad \frac{83}{75} \quad 32.6$$

$$\text{S.S.} \quad \frac{12.3}{96} \quad \frac{50}{75} \quad \frac{74}{32} \quad \frac{114}{82}$$

$$\frac{165}{100} \quad \frac{0.2}{75} \quad \frac{64}{49} \quad \frac{103}{49}$$

$$\frac{164}{100} \quad \frac{25}{75} \quad \frac{91}{46} \quad \frac{131}{46}$$

$$\text{S.S.} \quad \frac{50}{68} \quad \frac{14.2}{40} \quad \frac{17.5}{40}$$

Sta + π - Elev.

931.42

42 138

+75

T.P. 5.06 922.81 13.67 917.75

42 138

+75

T.P. 5.26 917.55

(917.56)

43

+50

44

+50

45

+47

T.P. 10.55 931.67 1.69 921.12

45

4

4

4

$$s.s. \frac{1.5}{50} \frac{7.5}{51}$$

$$s.s. \frac{4.8}{50} \frac{6.8}{49}$$

$$\frac{1.4}{30} \frac{6.6}{22} \frac{6.5}{14} \frac{5.8}{12} \frac{5.6}{13} \frac{6.0}{22} \frac{10.5}{28} \frac{11.5}{50} \frac{13.3}{50}$$

$$\frac{0.0}{43} \frac{3.4}{36} \frac{3.8}{25} \frac{7.0}{21} \frac{7.0}{19} \frac{5.4}{15} \frac{5.4}{13} \frac{5.7}{23} \frac{10.7}{27} \frac{11.7}{50} \frac{13.8}{50}$$

from T.P. Marker #1

$$\frac{+2.0}{48} \frac{1.6}{42} \frac{2.3}{30} \frac{4.4}{25} \frac{6.7}{22} \frac{4.3}{16} \frac{5.5}{13} \frac{5.2}{14} \frac{5.7}{25} \frac{11.6}{29} \frac{10.6}{50} \frac{13.7}{50}$$

$$\frac{+1.0}{50} \frac{5.5}{27} \frac{6.1}{21} \frac{5.6}{15} \frac{5.0}{13} \frac{5.5}{25} \frac{11.2}{29} \frac{12.3}{50} \frac{13.8}{50}$$

$$\frac{+3.5}{50} \frac{4.7}{29} \frac{5.3}{17} \frac{4.2}{14} \frac{4.7}{27} \frac{11.1}{29} \frac{11.9}{50} \frac{13.7}{50}$$

$$L.O. \frac{4.9}{40} \frac{2.7}{31} \frac{3.1}{24} \frac{4.0}{24} \frac{4.3}{16} \frac{3.2}{14} \frac{3.5}{26} \frac{10.4}{30} \frac{11.4}{50} \frac{13.0}{50}$$

$$\frac{1.7}{13} \frac{2.0}{27} \frac{2.1}{32} \frac{10.0}{50} \frac{11.6}{50}$$

$$\frac{0.0}{12} \frac{5.5}{23} \frac{6.4}{27} \frac{8.2}{31} \frac{9.6}{50}$$

$$\frac{6.1}{50} \frac{2.0}{40} \frac{9.4}{32} \frac{11.4}{27} \frac{12.1}{17} \frac{11.6}{15} \frac{10.6}{50}$$

Sta + T — Elev

931.67

45 +47

+75

46

B.M.

6.57

925.10

925.11

+50

+75

T.P. 10.63 942.22 0.08 931.59

47

+50

48

T.P. 11.04 953.25 0.01 942.21

+41

+66

49

T.P. 13.33 966.44 0.14 953.11

Lt

R

Lt

$$\begin{array}{r} 50 \quad 60 \quad 94 \quad 101 \quad 95 \quad 87 \\ 50 \quad 34 \quad 31 \quad 27 \quad 11 \end{array}$$

$$\begin{array}{r} 35 \quad 45 \quad 92 \quad 85 \quad 84 \quad 71 \quad 70 \quad 112 \quad 118 \quad 164 \quad 174 \\ 50 \quad 35 \quad 29 \quad 17 \quad 14 \quad 12 \quad 26 \quad 32 \quad 40 \quad 50 \end{array}$$

$$\begin{array}{r} 30 \quad 37 \quad 86 \quad 88 \quad 73 \quad 74 \quad 58 \quad 55 \quad 70 \quad 110 \quad 136 \\ 50 \quad 34 \quad 29 \quad 23 \quad 17 \quad 15 \quad 12 \quad 16 \quad 40 \quad 50 \end{array}$$

Top E. End. Ent. Calc. 27 Lt sta 46 t 35

$$\begin{array}{r} 17 \quad 2768 \quad 62 \quad 44 \quad 50 \quad 2865 \quad 81 \quad 92 \quad 92 \\ 50 \quad 33 \quad 26 \quad 21 \quad 16 \quad 17 \quad 23 \quad 35 \quad 43 \quad 50 \end{array}$$

$$\begin{array}{r} 15 \quad 24 \quad 50 \quad 55 \quad 25 \quad 15 \quad 14 \quad 67 \quad 82 \\ 50 \quad 30 \quad 25 \quad 22 \quad 16 \quad 13 \quad 22 \quad 50 \end{array}$$

Ent P.T.

$$\begin{array}{r} 113 \quad 121 \quad 118 \quad 134 \quad 126 \quad 115 \quad 105 \quad 102 \quad 153 \quad 157 \\ 50 \quad 32 \quad 26 \quad 23 \quad 19 \quad 16 \quad 13 \quad 24 \quad 50 \end{array}$$

$$\begin{array}{r} 82 \quad 84 \quad 91 \quad 92 \quad 75 \quad 64 \quad 64 \quad 98 \quad 100 \quad 111 \quad 111 \quad 100 \quad 88 \\ 50 \quad 23 \quad 21 \quad 19 \quad 14 \quad 16 \quad 22 \quad 25 \quad 26 \quad 27 \quad 29 \quad 50 \end{array}$$

$$\begin{array}{r} 31 \quad 35 \quad 34 \quad 21 \quad 17.1 \quad 66 \quad 75 \quad 33 \quad 10 \\ 50 \quad 31 \quad 15 \quad 12 \quad 16 \quad 21 \quad 26 \quad 29 \quad 50 \end{array}$$

$$\begin{array}{r} 89 \quad 106 \quad 102 \quad 92 \quad 87 \quad 88 \quad 132 \quad 132 \quad 87 \quad 54 \\ 50 \quad 30 \quad 17 \quad 13 \quad 15 \quad 21 \quad 26 \quad 29 \quad 50 \end{array}$$

$$\begin{array}{r} 43 \quad 69 \quad 68 \quad 63 \quad 63 \quad 65 \quad 86 \quad 92 \quad 53 \quad 26 \\ 50 \quad 32 \quad 12 \quad 12 \quad 16 \quad 19 \quad 25 \quad 27 \quad 50 \end{array}$$

$$\begin{array}{r} 13.5 \quad 12.7 \quad 31 \quad 42 \quad 39 \quad 31 \quad 26 \quad 25 \quad 62 \quad 64 \quad 04 \quad 126 \\ 50 \quad 41 \quad 32 \quad 26 \quad 17 \quad 14 \quad 15 \quad 20 \quad 27 \quad 32 \quad 50 \end{array}$$

Sta	+	T	-	Elev
-----	---	---	---	------

		966.49		
--	--	--------	--	--

49	+30			
----	-----	--	--	--

	+56			
--	-----	--	--	--

50				
----	--	--	--	--

	+29			
--	-----	--	--	--

T.P	12.26	978.22	0.48	965.96
-----	-------	--------	------	--------

49	+56			
----	-----	--	--	--

50				
----	--	--	--	--

	+29			
--	-----	--	--	--

	+62			
--	-----	--	--	--

51				
----	--	--	--	--

	+32			
--	-----	--	--	--

T.P	8.39	984.19	2.42	975.80
-----	------	--------	------	--------

	+69			
--	-----	--	--	--

Lt

Q

Rt

S.S. $\frac{21}{50}$ $\frac{31}{44}$ $\frac{123}{33}$ $\frac{146}{26}$ $\frac{147}{21}$ $\frac{131}{19}$ $\frac{125}{19}$ $\frac{128}{20}$ $\frac{168}{20}$ $\frac{166}{28}$ $\frac{104}{33}$ $\frac{78}{31}$ $\frac{6.2}{50}$

$\frac{1.2}{45}$ $\frac{88}{34}$ $\frac{125}{26}$ $\frac{126}{21}$ $\frac{107}{14}$ $\frac{100}{19}$ $\frac{105}{22}$ $\frac{124}{28}$ $\frac{24}{34}$ $\frac{54}{38}$ $\frac{40}{38}$ $\frac{25}{50}$

$\frac{46}{30}$ $\frac{87}{22}$ $\frac{90}{19}$ $\frac{63}{14}$ $\frac{57}{16}$ $\frac{64}{19}$ $\frac{85}{28}$ $\frac{84}{28}$

$\frac{31}{29}$ $\frac{61}{26}$ $\frac{60}{24}$ $\frac{39}{22}$ $\frac{29}{14}$ $\frac{2.7}{20}$ $\frac{36}{25}$ $\frac{66}{29}$ $\frac{6.5}{29}$

$\frac{42}{75}$ $\frac{26}{48}$

S.S. $\frac{00}{60}$ $\frac{40}{47}$ $\frac{8.8}{42}$ $\frac{3.9}{75}$

S.S. $\frac{40.2}{58}$ $\frac{2.3}{47}$ $\frac{3.8}{44}$ $\frac{0.8}{66}$

$\frac{33}{60}$ $\frac{47}{50}$ $\frac{4.5}{49}$ $\frac{11.1}{34}$ $\frac{120}{27}$ $\frac{120}{76}$ $\frac{110}{15}$ $\frac{110}{11}$ $\frac{11.9}{22}$ $\frac{123}{22}$ $\frac{197}{24}$ $\frac{197}{27}$ $\frac{2.3}{41}$ $\frac{0.6}{50}$ S.S.

$\frac{6.1}{50}$ $\frac{56}{45}$ $\frac{88}{39}$ $\frac{91}{18}$ $\frac{76}{14}$ $\frac{76}{10}$ $\frac{84}{20}$ $\frac{9.5}{23}$ $\frac{11.2}{28}$ $\frac{11.2}{28}$ $\frac{3.2}{36}$ $\frac{1.2}{50}$

L.O. $\frac{40}{48}$ $\frac{61}{40}$ $\frac{49}{34}$ $\frac{67}{18}$ $\frac{50}{16}$ $\frac{30}{10}$ $\frac{58}{20}$ $\frac{69}{20}$ $\frac{94}{24}$ $\frac{94}{26}$ $\frac{2.8}{32}$ $\frac{0.6}{50}$

$\frac{1.5}{54}$ $\frac{102}{40}$ $\frac{109}{21}$ $\frac{84}{16}$ $\frac{83}{10}$ $\frac{91}{19}$ $\frac{98}{22}$ $\frac{110}{22}$ $\frac{11.3}{23}$ $\frac{5.8}{33}$ $\frac{4.6}{50}$

Sta + π - Elev

984.19

52

+44

+76

53

+50

54

+26.91

B.M.

3.80

980.39

(980.38)

Lt.

: R.

Rt.

$$\frac{11}{52} \quad \frac{81}{41} \quad \frac{88}{18} \quad \frac{73}{15} \quad \frac{70}{11} \quad \frac{78}{16} \quad \frac{84}{21} \quad \frac{100}{23} \quad \frac{101}{31} \quad \frac{54}{31} \quad \frac{43}{50}$$

$$\frac{60}{50} \quad \frac{71}{37} \quad \frac{73}{17} \quad \frac{63}{12} \quad \frac{62}{14} \quad \frac{66}{19} \quad \frac{82}{22} \quad \frac{82}{27} \quad \frac{67}{27} \quad \frac{6.5}{50}$$

$$\frac{71}{50} \quad \frac{71}{29} \quad \frac{68}{13} \quad \frac{58}{14} \quad \frac{58}{31} \quad \frac{66}{30} \quad \frac{6.5}{50}$$

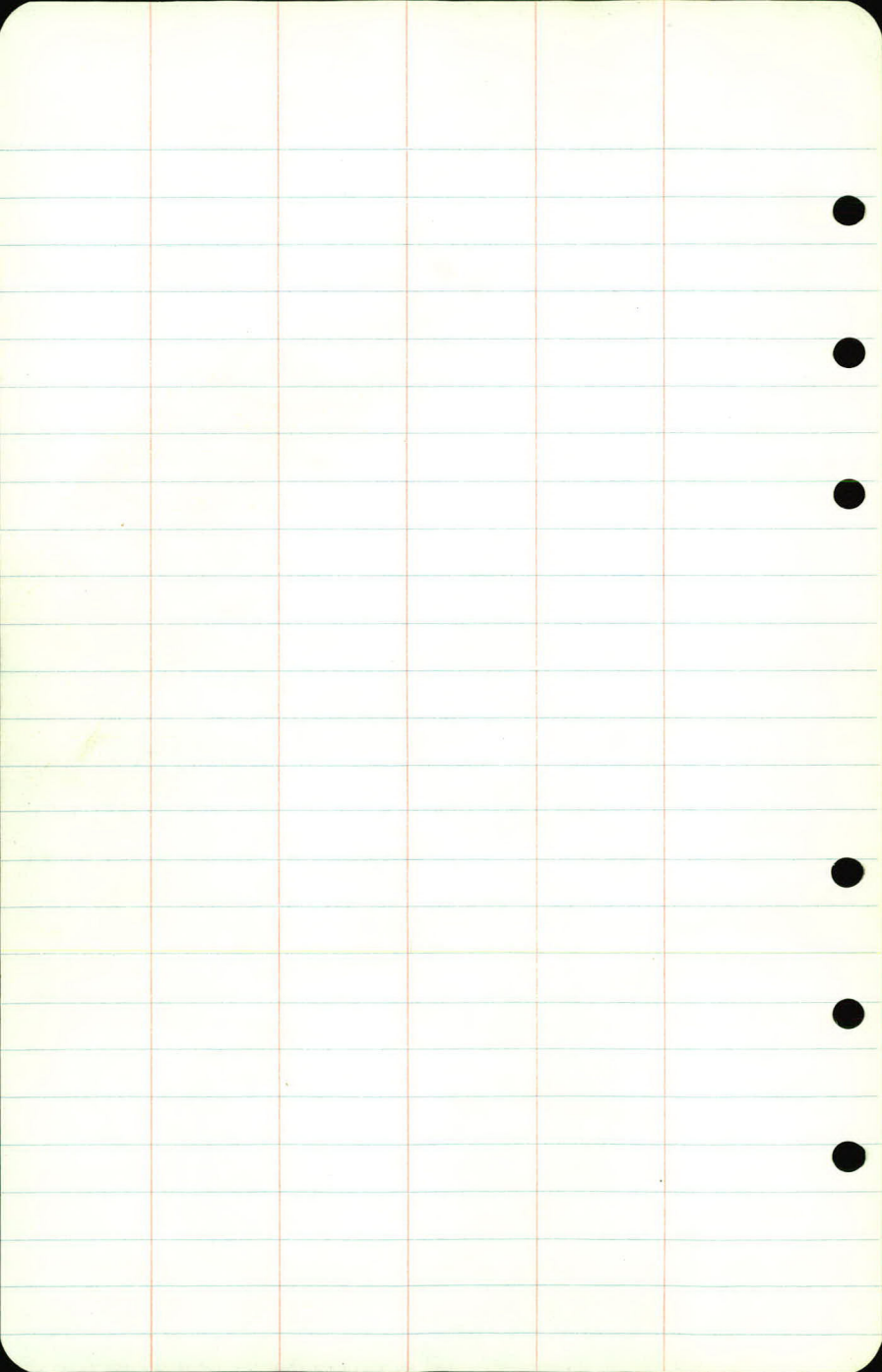
$$\frac{70}{50} \quad \frac{69}{30} \quad \frac{67}{12} \quad \frac{56}{15} \quad \frac{56}{19} \quad \frac{63}{26} \quad \frac{62}{30} \quad \frac{6.2}{50}$$

$$\frac{71}{50} \quad \frac{65}{34} \quad \frac{60}{17} \quad \frac{67}{11} \quad \frac{56}{8} \quad \frac{50}{22} \quad \frac{47}{26} \quad \frac{55}{33} \quad \frac{52}{39} \quad \frac{31}{50}$$

$$\frac{67}{50} \quad \frac{63}{34} \quad \frac{60}{16} \quad \frac{53}{13} \quad \frac{42}{14} \quad \frac{40}{18} \quad \frac{51}{25} \quad \frac{49}{31} \quad \frac{27}{31} \quad \frac{0.9}{50}$$

$$\frac{70}{50} \quad \frac{67}{35} \quad \frac{60}{19} \quad \frac{43}{14} \quad \frac{39}{10} \quad \frac{34}{12} \quad \frac{34}{16} \quad \frac{43}{24} \quad \frac{40}{30} \quad \frac{11}{30} \quad \frac{11.6}{50}$$

Top Conc. Base of St. Sign at Carvers Ave. & E. Co. Line



Alignment
L'line.

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

+67.18	P.T.	36°00'	
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+50		32°54.5'	
-----	--	----------	--

+25		28°24.5'	$\Delta-72^{\circ}-$
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54		23°54.5'	D-36°-
----	--	----------	--------

53	+84.73 P.I.	72°00'	T-117.55'
----	-------------	--------	-----------

+75		19°24.5'	L-200'00'
-----	--	----------	-----------

+50		14°54.5'	E-161.80'
-----	--	----------	-----------

+25		10°24.5'	
-----	--	----------	--

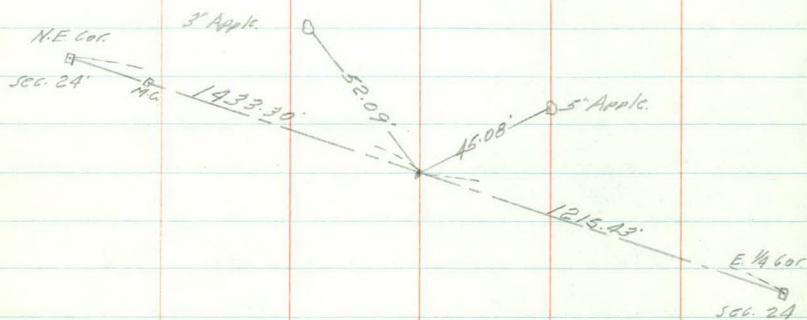
53		5°54.5'	
----	--	---------	--

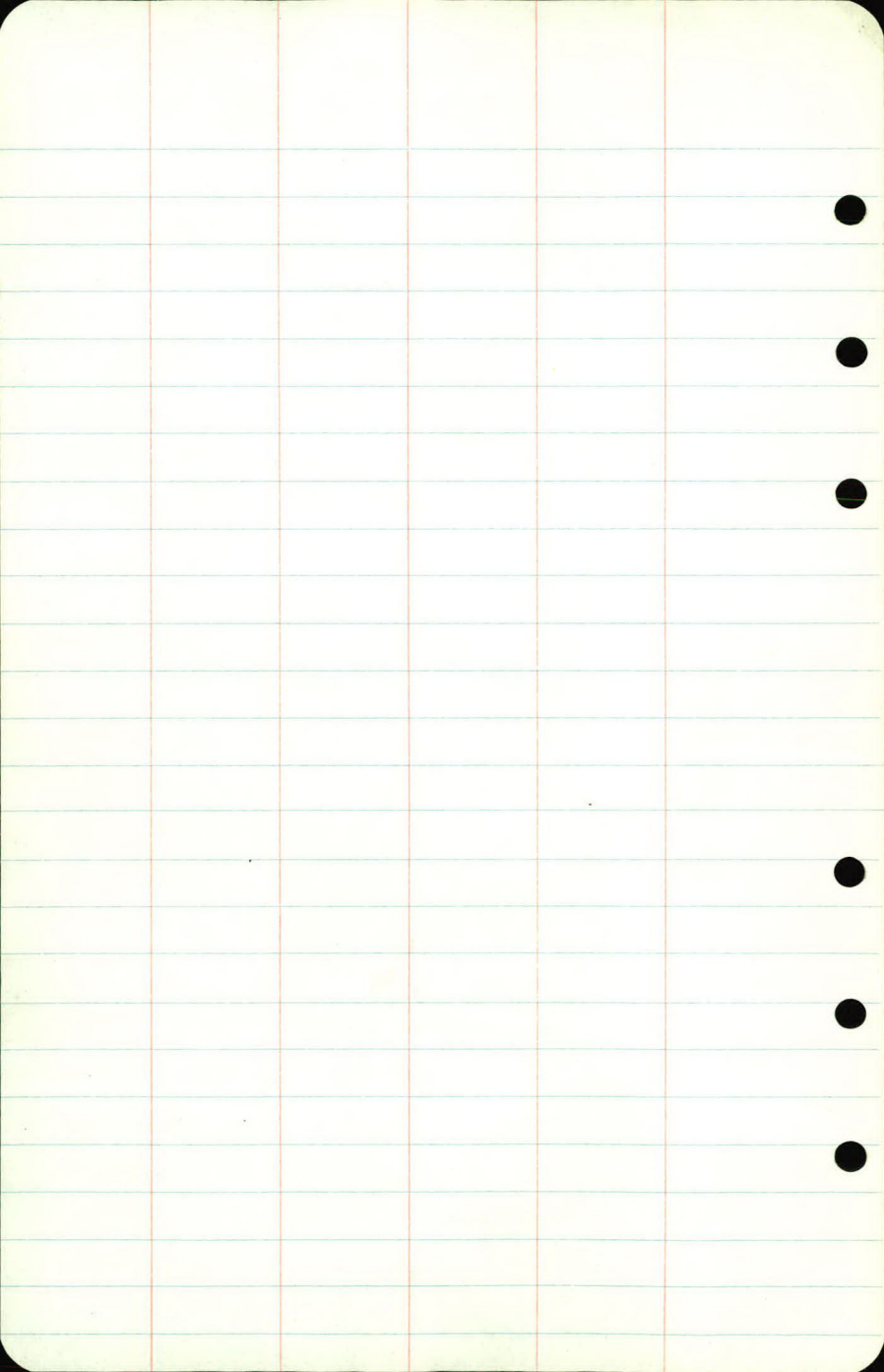
+75		1°24.5'	
-----	--	---------	--

52	+67.18 P.C.	0°00'	
----	-------------	-------	--

49 +84.79 P.O.T. L'line

49 +84.79 P.G. =





Topography

+25- End Cuff.

+67- 10' 11'

54 7'-26'

+75 19'-41'

+50 30'-54'

+25 38'-65'

53 38'-61'

+67- 32'-55'

+40- 50 1/4 - 0.0

52 14'-35'

6'-25'

51 2' 18'

8' 12'

50 10 9

coll.





L'Line

Xsections

Sta.	t	π	-	Elev.
B.M.	0.25	980.62		(980.38)

50 +00

+29

+62

51

+34

+54

I.P.	11.98	989.13	3.47	977.15
------	-------	--------	------	--------

+85

52

+44

+67.18

53

Lt.

K

Rt.

Top CONC Base of St Sign at Corner Ave & E. Co. Line

$$\begin{array}{r} 25 \quad 67 \quad 179 \quad 229 \quad 229 \quad 204 \quad 199 \quad 205 \quad 225 \quad 224 \quad 114 \quad 84 \\ 60 \quad 47 \quad 32 \quad 27 \quad 19 \quad 14 \quad 15 \quad 19 \quad 29 \quad 42 \quad 60 \end{array}$$

$$\begin{array}{r} 1.7 \quad 48 \quad 203 \quad 203 \quad 17.2 \\ 60 \quad 45 \quad 24 \quad 22 \quad 14 \end{array}$$

$$\begin{array}{r} 170 \quad 174 \quad 177 \quad 210 \quad 210 \quad 60 \quad 41 \\ 13 \quad 24 \quad 28 \quad 32 \quad 47 \quad 60 \end{array}$$

$$\begin{array}{r} 61 \quad 70 \quad 141 \quad 146 \quad 136 \quad 134 \quad 14.3 \quad 148 \quad 173 \quad 173 \quad 47 \quad 19 \\ 50 \quad 40 \quad 29 \quad 14 \quad 11 \quad 14 \quad 25 \quad 27 \quad 30 \quad 45 \quad 60 \end{array}$$

$$\begin{array}{r} 79 \quad 84 \quad 74 \quad 85 \quad 11.3 \quad 11.9 \quad 10.2 \quad 9.9 \quad 107 \quad 116 \quad 125 \quad 133 \quad 56 \quad 49 \\ 50 \quad 42 \quad 40 \quad 38 \quad 31 \quad 11 \quad 7 \quad 16 \quad 28 \quad 32 \quad 35 \quad 48 \quad 50 \end{array}$$

$$\begin{array}{r} 71 \quad 73 \quad 68 \quad 90 \quad 91 \quad 74 \quad 74 \quad 73 \quad 80 \quad 91 \quad 114 \quad 119 \quad 49 \quad 43 \\ 50 \quad 39 \quad 36 \quad 31 \quad 7 \quad 4 \quad 12 \quad 22 \quad 32 \quad 36 \quad 37 \quad 45 \quad 50 \end{array}$$

$$\begin{array}{r} 47 \quad 39 \quad 66 \quad 81 \quad 76 \quad 61 \quad 56 \quad 57 \quad 64 \quad 72 \quad 95 \quad 95 \quad 30 \\ 50 \quad 42 \quad 34 \quad 14 \quad 3 \quad 6 \quad 15 \quad 25 \quad 35 \quad 39 \quad 42 \quad 47 \end{array}$$

$$\begin{array}{r} 63 \quad 64 \quad 137 \quad 149 \quad 147 \quad 129 \quad 125 \quad 134 \quad 146 \quad 144 \quad 102 \\ 50 \quad 33 \quad 22 \quad 14 \quad 4 \quad 20 \quad 33 \quad 39 \quad 49 \quad 53 \end{array}$$

$$\begin{array}{r} 48 \quad 58 \quad 134 \\ 50 \quad 30 \quad 17 \end{array}$$

$$\begin{array}{r} 140 \quad 137 \quad 125 \quad 120 \quad 132 \quad 150 \quad 149 \\ 6 \quad 9 \quad 25 \quad 41 \quad 44 \quad 50 \end{array}$$

$$\begin{array}{r} 68 \quad 89 \quad 97 \quad 125 \quad 126 \quad 123 \quad 113 \quad 112 \quad 114 \\ 50 \quad 27 \quad 18 \quad 9 \quad 79 \quad 23 \quad 38 \quad 50 \end{array}$$

$$\begin{array}{r} 95 \quad 117 \\ 50 \quad 20 \end{array}$$

$$\begin{array}{r} 12.2 \quad 121 \quad 117 \quad 10.8 \quad 10.8 \\ 24 \quad 29 \quad 44 \quad 50 \end{array}$$

$$\begin{array}{r} 114 \quad 122 \quad 119 \quad 118 \quad 118 \quad 10.7 \\ 50 \quad 28 \quad 26 \quad 39 \quad 50 \end{array}$$

sta + π - Elev

989.13

53 +50

+95

54

+35

+67.18

B.M.

B75 980.38 980.38

6-2-41
K.A.
L.G.
M.R.
C.N.

39

Lt.

E

Lt.

$\frac{122}{50}$ $\frac{127}{41}$ $\frac{126}{26}$ $\frac{119}{16}$ $\frac{115}{20}$ $\frac{113}{22}$ $\frac{110}{31}$ $\frac{107}{50}$ $\frac{95}{50}$

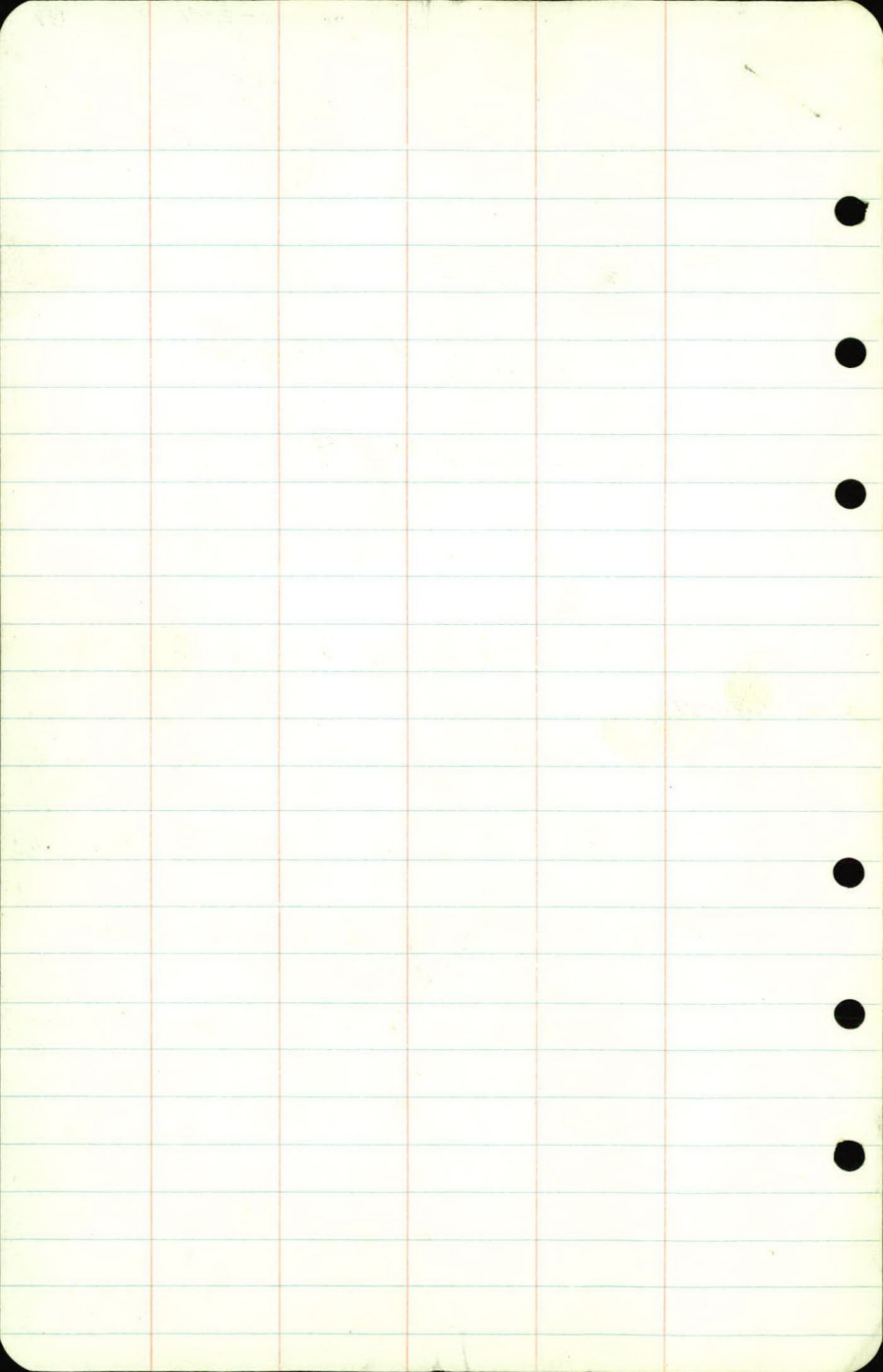
$\frac{130}{50}$ $\frac{122}{41}$ $\frac{113}{26}$ $\frac{108}{6}$ $\frac{87}{25}$ $\frac{82}{37}$ $\frac{85}{39}$ $\frac{82}{50}$ $\frac{93}{50}$

$\frac{126}{50}$ $\frac{112}{26}$ $\frac{100}{4}$ $\frac{84}{17}$ $\frac{78}{30}$ $\frac{82}{33}$ $\frac{86}{42}$ $\frac{88}{50}$ $\frac{58}{50}$

$\frac{117}{50}$ $\frac{100}{30}$ $\frac{90}{15}$ $\frac{71}{10}$ $\frac{66}{16}$ $\frac{70}{20}$ $\frac{77}{25}$ $\frac{79}{28}$ $\frac{75}{35}$ $\frac{32}{50}$ $\frac{15}{50}$

$\frac{111}{50}$ $\frac{78}{27}$ $\frac{75}{18}$ $\frac{60}{14}$ $\frac{54}{19}$ $\frac{59}{17}$ $\frac{74}{22}$ $\frac{70}{32}$ $\frac{12}{50}$ $\frac{0.5}{50}$

Top Cor. Base of St. Sign at Corner Ave & E. Co. Line



Corver Ave.

Levels

Pt. Douglas Rd. to City Limits

4150 to 6425 widen lt. side

Platted

Sta + π - Elev.

0 +00 = 4 ft. Douglas Rd.

00

00

↓

1 +00 12' Pav.

+4.6

04.6

↑

↓

3 +00 12' Pav.

+15.0

19.6

↑

↓

4

+10.0

29.6

↑

↓

+13

+8.9

38.5

+73

↑

↓

5 +22

+6.0

44.5

↑

↓

6 +25

+11.9

56.4

↑

↓

7 +25

+10.3

66.7

4-12-49

2

Lt

E

Rt

-1.3 +1.5 +1.1 -0.4 0.0
22 14 11 8-7 6

-0.2 0.0 +1.0 +1.6 -2.0
6 8.5 11 13-16 30

-8.3 +1.5 0.0 -0.1
29 14-12 9 6

-0.0 -0.4 +0.7 -9.5
6 8 10-14 30

-7.0 +1.5 -0.1 +0.1
31 16-11 8 6

-0.1 -0.5 +0.9 -8.1
6 8 12-16 34

+6.5 +3.4 -0.4 0.0
37 16 9 6

-0.3 -0.8 +2.5 down 2.15/40
6 9 15-19

Up 1.1 +2.6 +1.2 -0.2 0.0
18 12 10 7

-0.2 -0.8 +0.8 +2.0 L.O. 20'
7 9 12 18

Up 1/2" +2.0 +1.2 -0.2 -0.1
21 12 10 7

-0.2 -0.6 +5.1 L.O.
7 9 20

Up 3/4" +2.6 -0.2 0.0
14 10 7

-0.1 0.0 +2.1 L.O.
7 10 16

sta.	+	π	-	Elev
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8	+15	widen rt.	+8.5	75.2
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9	+00	widen rt.	+7.3	82.5
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	+50	= End steep grade	+3.5	86.0
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10			+1.6	87.6
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11			+2.6	90.2
----	--	--	------	------



12			+2.7	92.9
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13			+1.1	94.0
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	+78		+1.6	95.6
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L
ent. road

E

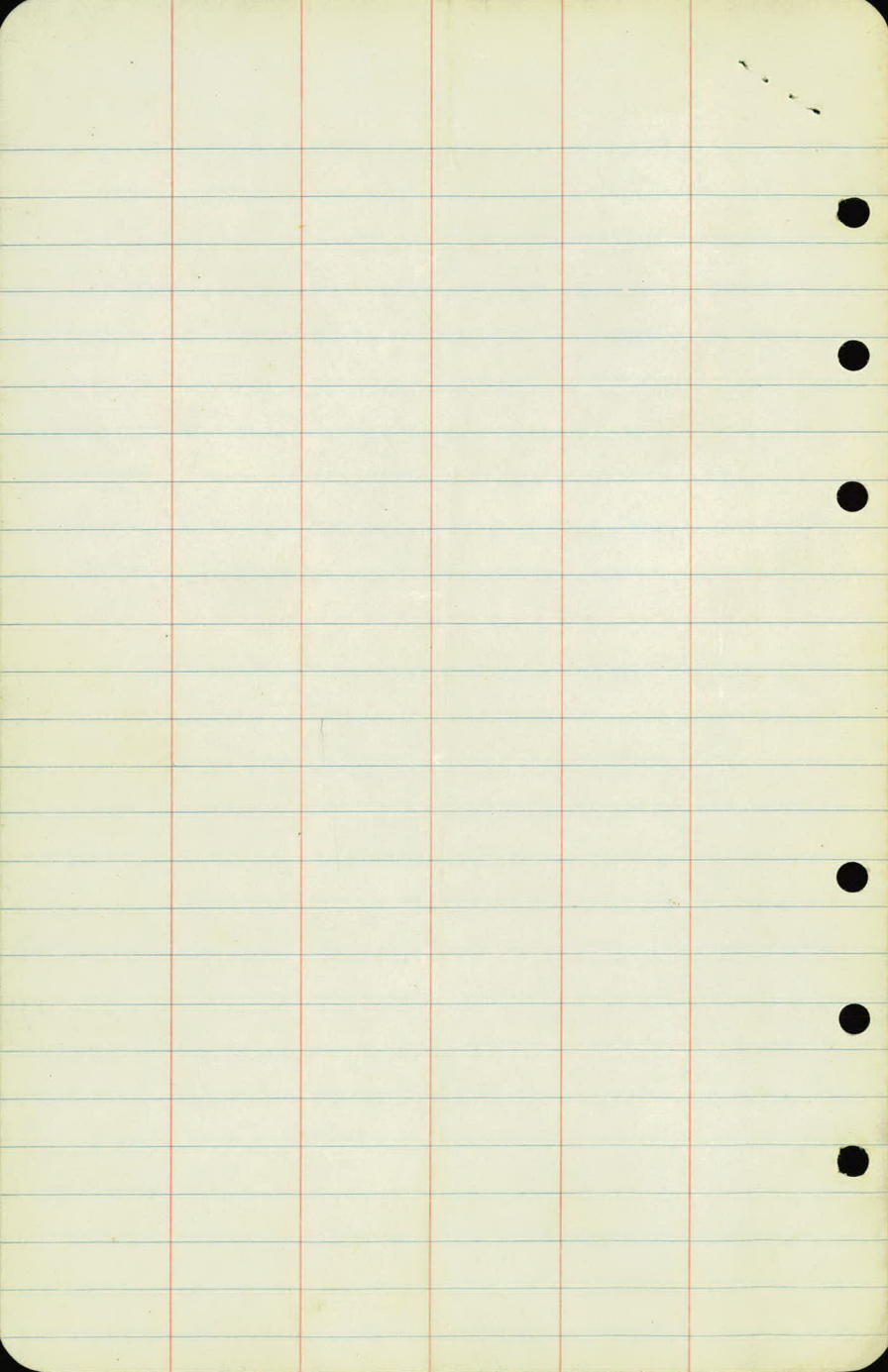
R

+60	+42	+53	+0.500	-0.1	-0.7	+0.7	+1.9	up 1.7 for 5'
40	29	19	11	7	7	8-9	12	17

L.O.	+50	-0.1	00	0.0	0.0	+1.9	+6.0
	17	9	7	7	10	15	21

+50 = End of old par.

= city limits



+16.30 PT 28°35.5'

47 26°08.8' $\Delta = 57^{\circ}11'$

+75 22°23.8' $\frac{1}{2}\Delta = 28^{\circ}35.5'$

+50 18°38.8' $D = 30^{\circ}$

46+30.98 P1 T = 105.29

+25 14°53.8' L = 190.61

46 11°08.8' R = 193.18

+75 7°23.8'

+50 3°38.8'

+25.69 PC 0°00'

