

BK 53 Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

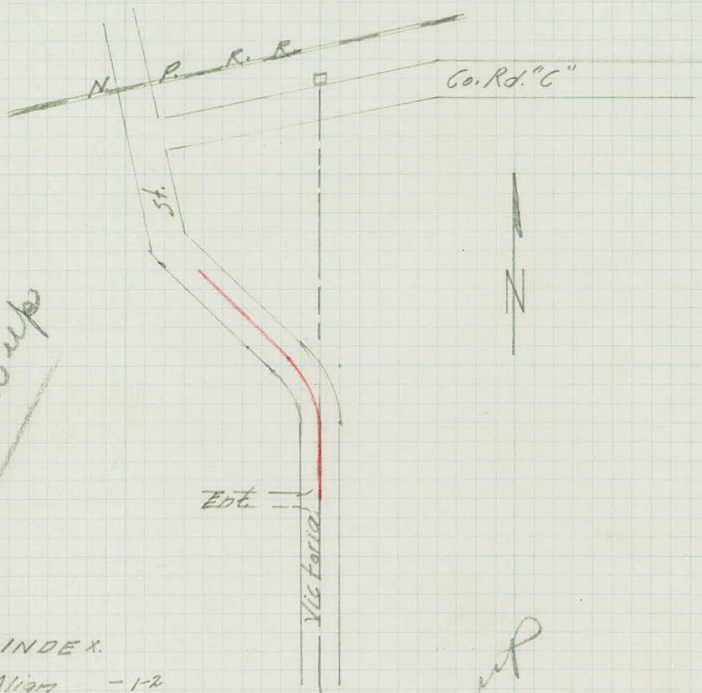
Victoria St. Curve

From 700' so-Co Rd "C"

Road Acc't. No. 21

Date Filed 6-11-41 File

PLAN SURVEY
Victoria St. Curve
Approx. 700' 50' Co. Rd. "C"



Not drawn up

INDEX.

Align - 1-2
Topog. - 3-4
Sections - 5-8

Drawn up
8/23/49
J.C.



Alignment

Sta	Point	ΔLt	ΔRt
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D-6°-R^L

R-955.37

5	+37.0	P.L.	
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	+60.99	P.T.	24°01.5'
--	--------	------	----------

	+50		22°49'
--	-----	--	--------

Δ 48°03'

			17°19'
--	--	--	--------

D-22°

2	+59.38	P.L.	
---	--------	------	--

T-116.80'

	+50		11°49'
--	-----	--	--------

L-218.41'

			6°19'
--	--	--	-------

R-262.04'

	+50		0°49'
--	-----	--	-------

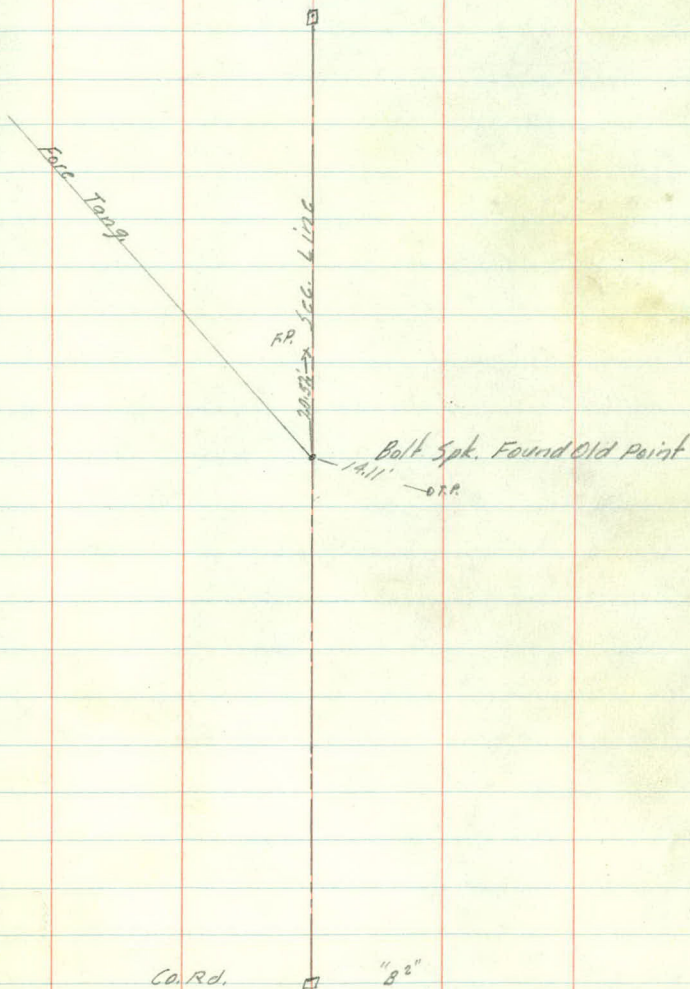
1	+42.58	P.L.	0°00'
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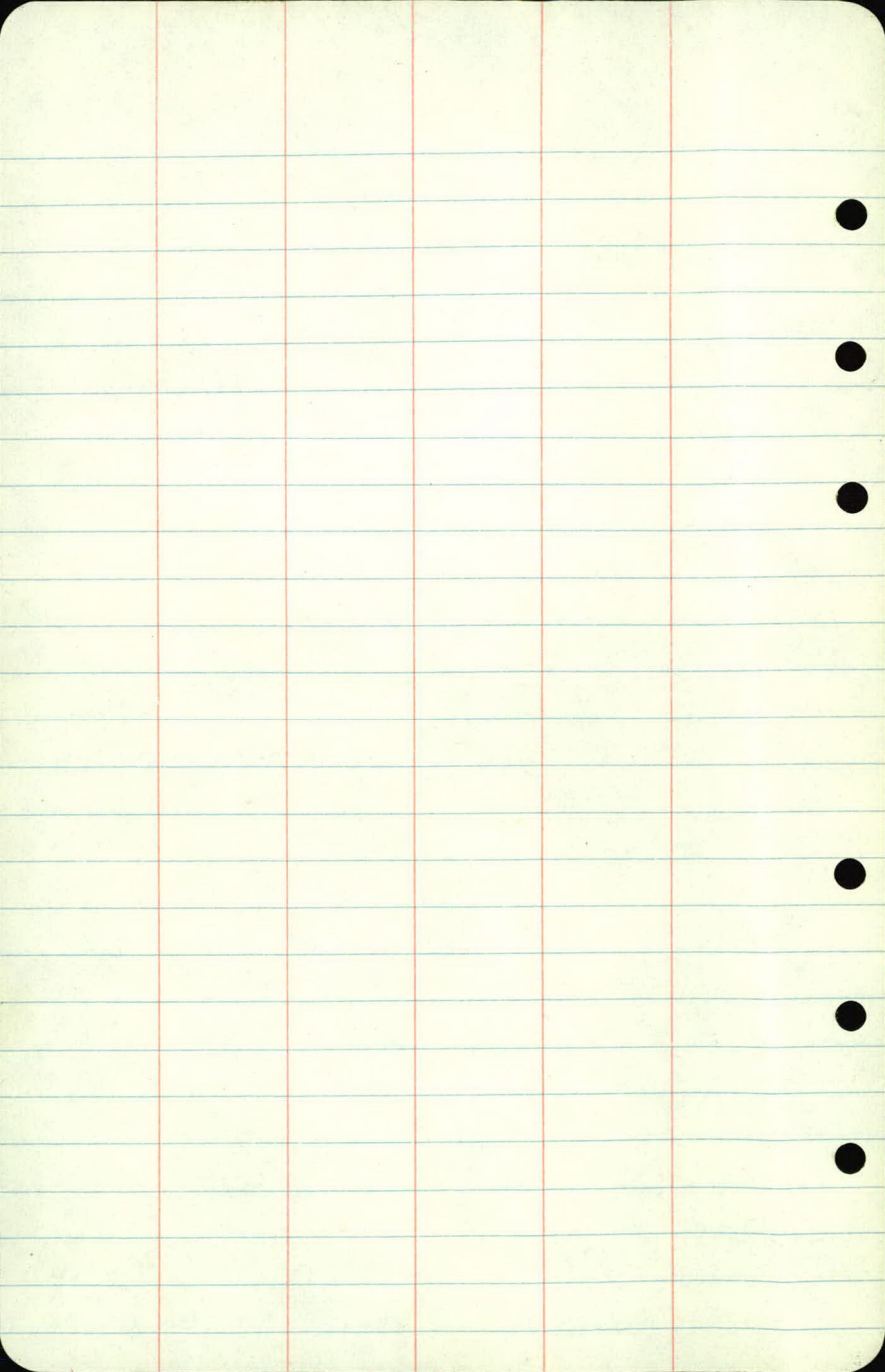
0	+00	P.O.T.	
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10/26/39
K.A.
L.C.
M.J.G.
M.B.

2

N. 1/4 Cor. Sec. 11





Topography

+92- R. 24' X 26' C.M.A.-

18.5' 17.5'

+97-

9' 10'

Fe-20'

5 Ent-26'

10' 10'

+112-Range Tie

9' 10'

Fe-22'

4

10' 11'

Fe-26'

10' 10'

Fe-25'

3

10' 10'

Fe-29'

12' 9'

+166-Fe Cor-33'

+192-RR-34'

2

15' 6'

Ditch-48 Fe-50'

14' 5'

Ditch-41'

+130-RR-26'

1

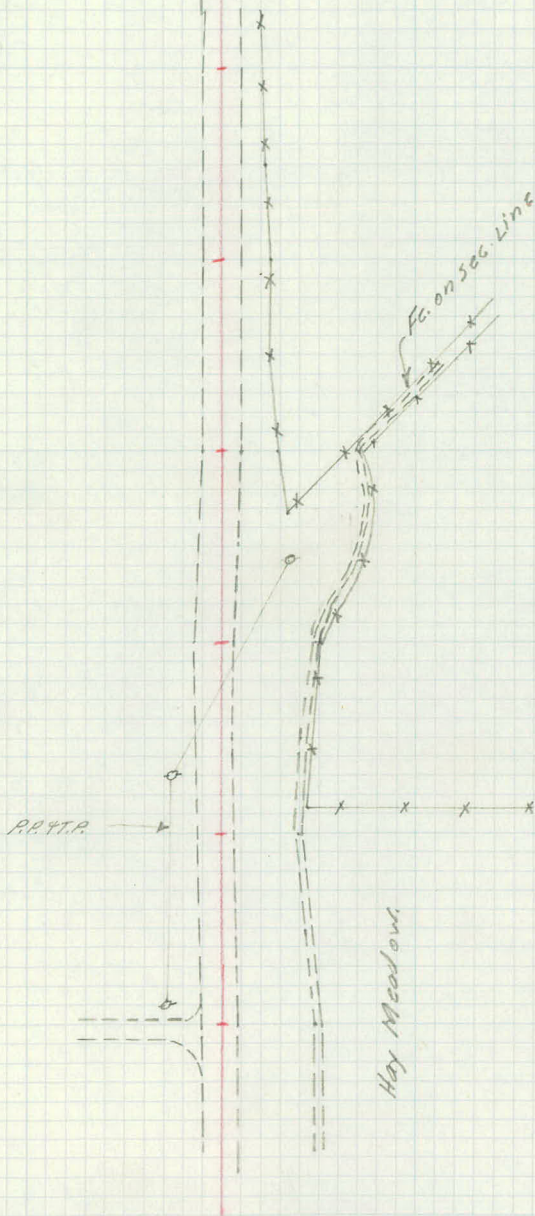
12' 7'

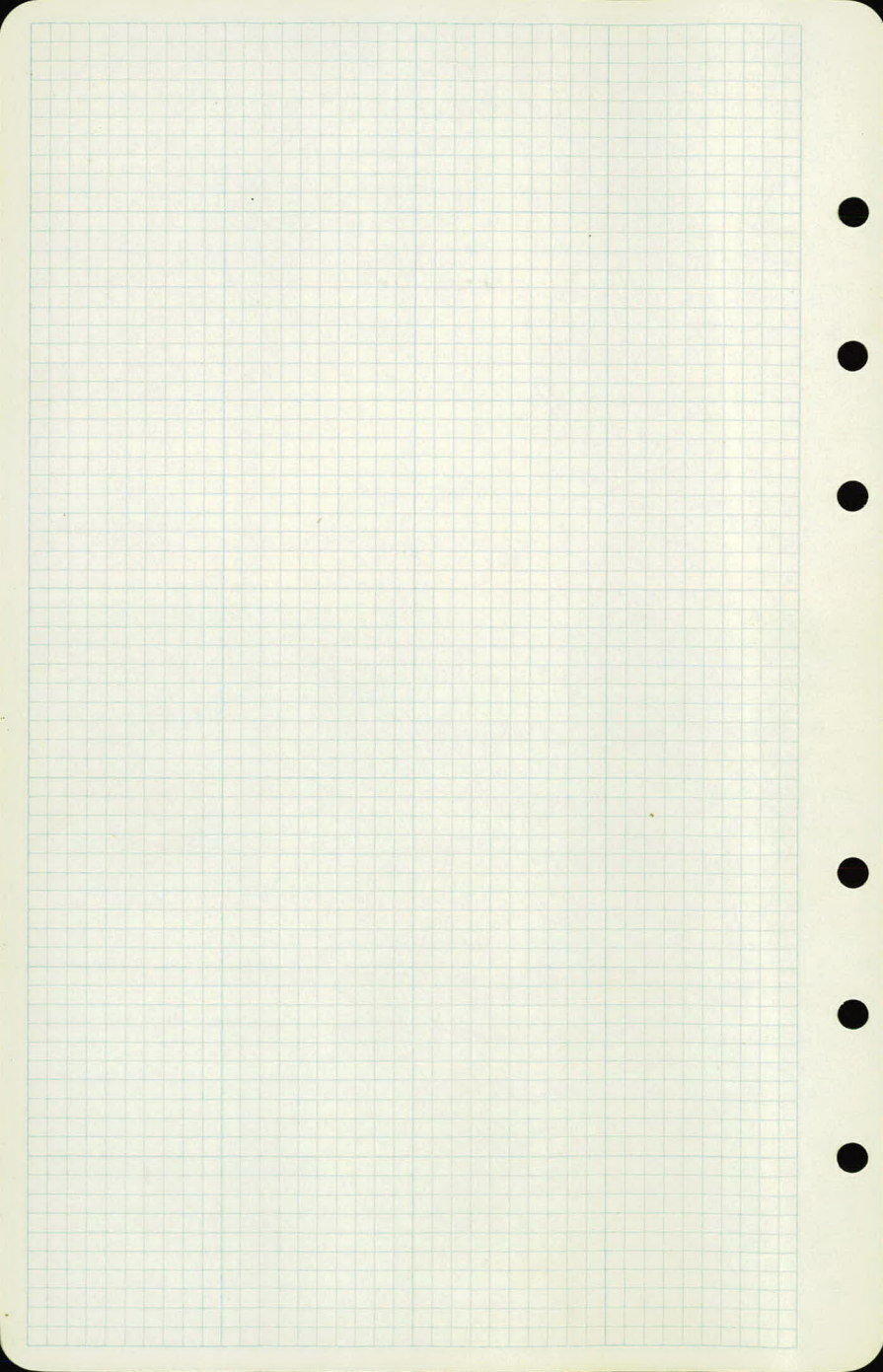
+114-Fe Cor-43'
Ditch-40'

0+00 +110-RR-28'
-0.3-Ent

10' 9'

R. 2' Bot. Ditch-48'





X sections

Sta	+	π	-	Elev.
B.M.	8.75	899.64		(890.89)
T.P.	13.28	900.07	12.83	896.81
B.M.	4.68	901.33	3.44	896.65

0 +0.3 96.1

+07 96.2

+50 96.2

1 96.3

+50 96.3

2 96.6

+50 96.5

3 95.9

+50 95.2

4 94.4

Lt.

L

Rt.

Top Bottom Δ Plate W. Plate NW Cor. Tower Lt. 5475 Cal'd "C"

Spk. in RR 34' Rt. 2142

1195	176	134	24	42	53	52	57	60	80	95	111	131	131	118	✓
200	150	100	50	30	10		9	18	24	40	46	48	50	52	

34	53	51	✓
27	10		

49	53	51	55	57	83	95	116	132	132	120	126	✓
24	10		8	19	19	30	37	41	48	45	50	

47	54	53	50	55	57	101	119	140	140	150	133	✓
24	19	12		7	12	18	33	39	41	44	50	

50	53	50	54	55	95	121	144	144	135	87.8	✓
25	14		5	10	19	34	40	42	43	L.O.	

14	28	49	54	47	47	50	104	118	141	141	13.2	87.2	88.1	✓
50	29	23	15		6	12	26	42	47	49	50			

00	14	59	57	48	50	51	66	91	106	✓
50	28	20	12		8	23	34	43	50	

57	61	54	53	59	86	100	116	✓
19	8		8	26	33	41	50	

63	67	41	63	67	118	132	139	✓
18	10		10	21	30	39	50	

76	74	69	74	74	120	127	134	✓
19	9		10	20	27	34	50	

Sta	+	X	-	Elev.
		901.33		
A	+17			94.1
	+50			93.6
5				92.8
T.P.	13.52	914.21	0.64	900.69
0	+07			96.2
	+50			96.2
1				96.3
	+50			96.3
2				96.6
	+50			96.5
3				95.9
	+50			95.2

Lt.

4.

Bt.

$$\frac{59}{25} \quad \frac{80}{17} \quad \frac{77}{8} \quad \frac{72}{10} \quad \frac{77}{18} \quad \frac{78}{25} \quad \frac{121}{29} \quad \frac{128}{50} \quad \frac{136}{50}$$

✓

$$\frac{83}{19} \quad \frac{80}{8} \quad \frac{77}{10} \quad \frac{84}{15} \quad \frac{88}{21} \quad \frac{121}{25} \quad \frac{130}{50} \quad \frac{142}{50}$$

✓

$$\frac{35}{50} \quad \frac{78}{20} \quad \frac{87}{18} \quad \frac{87}{13} \quad \frac{89}{9} \quad \frac{85}{9} \quad \frac{92}{14} \quad \frac{94}{17} \quad \frac{103}{21} \quad \frac{121}{26} \quad \frac{129}{36} \quad \frac{137}{50} \quad \frac{149}{50}$$

✓

$$\frac{107}{200} \quad \frac{10}{167} \quad \frac{31}{144} \quad \frac{65}{90} \quad \frac{105}{56} \quad \frac{116}{52}$$

18.0

✓

$$\therefore \frac{105}{200} \quad \frac{17}{155} \quad \frac{60}{100} \quad \frac{80}{65} \quad \frac{106}{52} \quad \frac{118}{53}$$

18.0

✓

$$\frac{140}{200} \quad \frac{110}{179} \quad \frac{10}{160} \quad \frac{52}{130} \quad \frac{82}{100} \quad \frac{98}{66} \quad \frac{116}{47} \quad \frac{129}{31}$$

17.9

✓

$$\frac{148}{200} \quad \frac{148}{184} \quad \frac{87}{157} \quad \frac{27}{140} \quad \frac{84}{100} \quad \frac{134}{56} \quad \frac{146}{50}$$

17.9

✓

$$\frac{123}{200} \quad \frac{138}{191} \quad \frac{95}{155} \quad \frac{36}{136} \quad \frac{92}{100} \quad \frac{120}{75}$$

17.6

✓

$$\frac{153}{200} \quad \frac{126}{170} \quad \frac{26}{135} \quad \frac{80}{100} \quad \frac{112}{75}$$

17.7

✓

$$\frac{160}{200} \quad \frac{134}{179} \quad \frac{124}{145} \quad \frac{26}{126} \quad \frac{64}{100} \quad \frac{104}{62} \quad \frac{120}{27}$$

18.3

✓

$$\frac{163}{200} \quad \frac{133}{169} \quad \frac{106}{147} \quad \frac{09}{133} \quad \frac{50}{100} \quad \frac{74}{80} \quad \frac{85}{50} \quad \frac{94}{51}$$

19.0

✓

sta.	+	π	-	Elev.
------	---	-------	---	-------

914.21

94.4

+17

94.1

+50

93.6

5

92.8

T.P.

1.22

902.34

13.09

901.12

+37

92.3

+92

92.3

B.M.

11.50

890.84

(890.89)

Lt.

2

Pt.

$$\frac{+4.9}{200} \frac{+1.2}{150} \frac{0.6}{126} \frac{2.5}{111} \frac{2.8}{89} \frac{5.5}{60} \frac{5.9}{38}$$

19.8 ✓

$$\frac{+4.2}{200} \frac{+3.0}{184} \frac{+0.8}{145} \frac{1.8}{100} \frac{4.9}{66} \frac{5.4}{40}$$

20.1 ✓

$$\frac{+2.0}{200} \frac{+1.0}{148} \frac{1.0}{125} \frac{4.4}{100} \frac{8.0}{68} \frac{11.0}{32}$$

20.6 ✓

$$\frac{+2.7}{200} \frac{1.7}{134} \frac{4.7}{139} \frac{8.8}{100}$$

21.4 ✓

$$\frac{6.8}{50} \frac{9.8}{22} \frac{10.5}{17} \frac{10.0}{8} \frac{10.0}{9} \frac{10.8}{15} \frac{11.0}{20} \frac{13.4}{36} \frac{15.0}{36} \frac{15.5}{50} \checkmark$$

$$\frac{8.7}{50} \frac{10.2}{28} \frac{10.9}{23} \frac{12.5}{19} \frac{12.6}{18} \frac{10.6}{18.5} \frac{10.2}{9} \frac{10.0}{10} \frac{10.9}{15} \frac{11.2}{17.5} \frac{12.0}{17.5} \frac{14.0}{17.5} \frac{13.5}{19} \frac{15.3}{50} \checkmark$$

Top Bottom Δ Plate W. Plate N.W. Cor. Tower Lt 5+75 Co. Rd. 6"

sta.

+

π

-

Elev.

X Sections

Victoria Street Curve

700' So. Co. Rd C

= Sta 0+00 to Sta 5+70 ^{K.A.} 10-26-39

= Sta 101+36.35 to 106+73.35 -

(Victoria Plan Survey - 10-21-41)

8-8-49

G.B.

A.M.

M.B.

B.C.

Rec 8-9-49

Sta + π - Elev

BM (No old BM found)

0 + 00

96.1

0 + 03

+ 07

96.2

+ 50

96.2

+ 50

96.3

2

96.6

+ 50

96.5

3

96.9

2

edge of Black Top

Bottom ditch

2.7 $\frac{4.0}{8}$ $\frac{3.9}{19}$ $\frac{5.7}{24}$ $\frac{8.7}{43}$ $\frac{13.5}{50}$ ✓

3.5 $\frac{4.0}{8}$ $\frac{3.8}{10}$ $\frac{3.8}{20}$ $\frac{5.3}{23}$ $\frac{8.7}{42}$ $\frac{13.5}{50}$ ✓

3.4 $\frac{4.0}{8}$ $\frac{3.8}{10}$ $\frac{4.4}{17}$ $\frac{6.3}{21}$ $\frac{7.9}{30}$ $\frac{10.1}{37}$ $\frac{14.3}{39}$ ✓
 $\frac{14.3}{50}$ ✓

3.3 $\frac{3.7}{6}$ $\frac{3.6}{8}$ $\frac{4.5}{14}$ $\frac{7.9}{19}$ $\frac{9.3}{25}$ $\frac{10.6}{35}$ $\frac{13.1}{37}$ $\frac{16.1}{42}$ ✓

3.3 $\frac{3.8}{5}$ $\frac{3.6}{6}$ $\frac{4.1}{14}$ $\frac{7.9}{20}$ $\frac{11.0}{35}$ $\frac{13.6}{37}$ $\frac{16.6}{45}$ ✓
 $\frac{16.6}{50}$ ✓

3.0 ~~3.6~~ $\frac{3.2}{7}$ $\frac{3.9}{16}$ $\frac{6.7}{22}$ $\frac{8.7}{28}$ $\frac{10.9}{39}$ $\frac{11.0}{42}$ $\frac{16.0}{50}$ ✓

3.1 $\frac{3.1}{9}$ $\frac{2.9}{23}$ $\frac{6.8}{40}$ $\frac{8.7}{50}$ ✓

3.7 $\frac{3.5}{11}$ $\frac{3.9}{27}$ $\frac{7.9}{38}$ $\frac{10.1}{50}$ ✓

Sta	+	π	-	Elev
3+50				95.2
4				94.4
+ 17				94.1
+ 50				93.6
5				92.8
+ 37				92.3
+ 92				92.3

2

$$4.3 \quad \frac{4.6}{10} \quad \frac{7.8}{22} \quad \frac{10.6}{33} \quad \frac{11.8}{50} \quad \checkmark$$

$$5.2 \quad \frac{5.8}{10} \quad \frac{5.4}{14} \quad \frac{5.6}{20} \quad \frac{10.7}{30} \quad \frac{11.7}{50} \quad \checkmark$$

$$5.5 \quad \frac{6.0}{10} \quad \frac{5.8}{12} \quad \frac{5.8}{20} \quad \frac{10.7}{28} \quad \frac{11.8}{50} \quad \checkmark$$

$$6.1 \quad \frac{7.1}{9} \quad \frac{6.9}{12} \quad \frac{7.2}{16} \quad \frac{11.2}{24} \quad \frac{12.4}{50} \quad \checkmark$$

$$6.8 \quad \frac{7.6}{9} \quad \frac{8.1}{17} \quad \frac{11.1}{25} \quad \frac{12.5}{50} \quad \checkmark$$

$$7.3 \quad \frac{8.2}{9} \quad \frac{8.1}{11} \quad \frac{8.4}{18} \quad \frac{10.3}{20} \quad \frac{11.5}{28} \quad \frac{12.5}{50} \quad \checkmark$$

FL-15"cm

$$7.4 \quad \frac{8.2}{10} \quad \frac{8.3}{17} \quad \frac{10.6}{18.5} \quad \frac{10.6}{20} \quad \frac{12.5}{50} \quad \checkmark$$

Sta + π - Elev