

Bk. 52 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

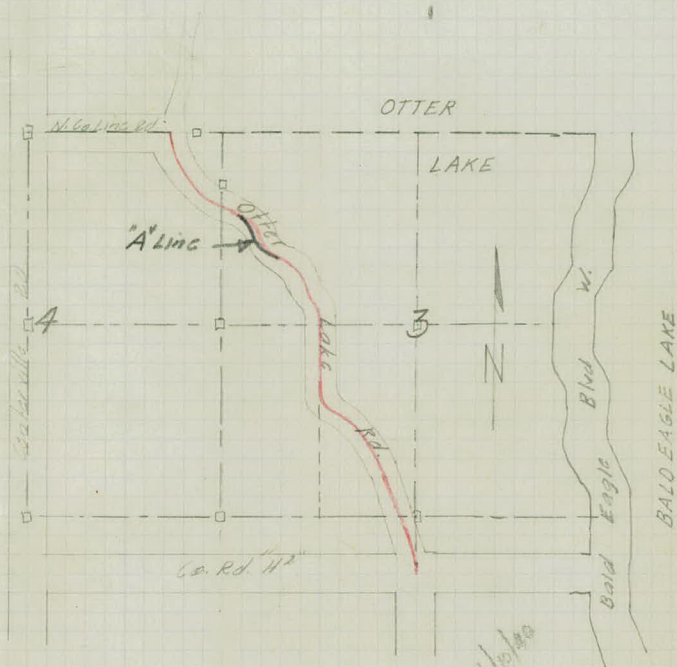
Otter Lake Rd.

From "H 2" To No. Co. Line

Road Acc't. No. 25

Date Filed 6-11-41 File

Plan Survey
OTTER LAKE RD.
Co. Rd. "H" to Co. Rd. "J"



INDEX

Align -	1-9
Topog -	9-21
X-sections -	22-40
"A" Line	41-43
Diff. Between Reg. Line and "A" Line	44

not drawn up
? x sections (at slope 4/10/00)



Alignment

Sta.	Point	Δ Lt	Δ Rt
------	-------	-------------	-------------

169.59	P.T.	13° 30'	
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+50		12° 19.5'	$\Delta 27^{\circ} 00' \text{ Lt}$
-----	--	-----------	------------------------------------

		9° 19.5'	$D - 12^{\circ}$
--	--	----------	------------------

			$T - 114.84'$
--	--	--	---------------

159.43	P.I.		
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+50		6° 19.5' .07'	$L - 225.00'$
-----	--	---------------	---------------

		3° 19.5'	$R - 476.34'$
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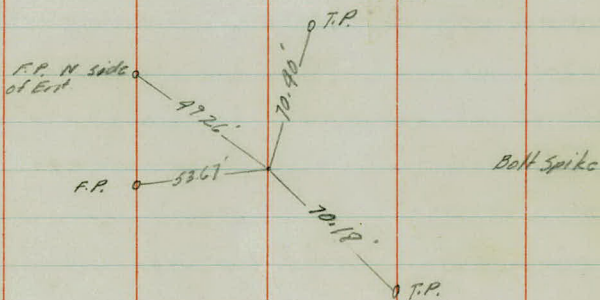
144.59	P.C.	0° 00'	
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0 +00 = Approx 14.5' of Traveled Roadway of Colld. H²
see plan survey of 1936.

1,518.62

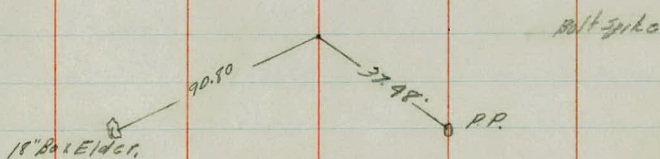
(See 1936 Plan Survey for sectionatics)



$$C = 482.01$$

$$A = 477.46$$

544.59

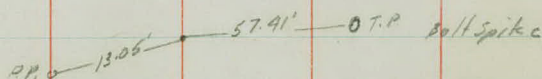


Sta.	point	Δ Lt.	Δ Rt.
	#19.74 P.T.	21°38.5'	19.77
33		20°09.7'	
	+50	16°24.7'	Δ 43°17' 10"
32		12°39.7'	D- 15°
	+83.17 P.I.		T-151.98'
	+50	8°54.7'	L- 288.55'
31		5°09.7'	R- 383.06' 1.10
	+50	1°24.7'	15.87
30	+31.19 P.C.	0°00'	

	+11.54' P.T.	8°05.6'	
26		7°47.7'	
	+50	6°32.7'	Δ 16°10' 14"
25		5°17.7'	D- 5°
24	+51.0 P.I.		T-162.79'
	+50	4°02.7'	L- 323.33'
24		2°47.7'	R- 1146.28'
	+50	1°32.7'	
23		0°17.7'	
22	+88.21 P.C.	0°00'	

2/3/39
K.A.
L.B.H.
L.C.
M.J.G.

3

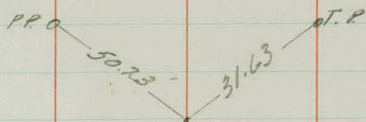


$$A = 381.96$$

$$419.65$$

$$C =$$

$$A = 1145.90$$



R.R. Spike

Sta Point ΔLt - ΔRt

47	+15.77	P.T.	25°30.5'	08		
			23°36.9'		$\Delta 51^{\circ}01' Lt$	
	+50		17°36.9'		D-24°	
46	+17.96	P.I.			T 114.75'	
46			11°36.9'	26	L 212.78	212.56
	+50		5°36.9'	23	R 240.47	
45	+03.28	P.C.	0°00'			
43	+37.48	P.O.T.				

390.80

18" Oak

⊙

37.40'

47.21'

39.19'

⊙ 30" Oak

Bolt Spike

⊙ 12" Oak

$A = 238.97$

1183.47

W. $\frac{1}{4}$ Cor. sec. 3



$\frac{1}{4}$ - $\frac{1}{4}$ Cor.

ctr. sec. 3



Sec Road Map Survey 1936

52.68' 12" Oak

Bolt Spike

52.05'

18" Oak

Sta Point ΔL ΔR

+06.80 P.T. $3^{\circ}53.5'$

60 $3^{\circ}43.3'$ $\Delta - 7^{\circ}47' L$

+50 $2^{\circ}28.3'$ D- 5°

59 +29.11 P.I. T- $77.98'$

59 $1^{\circ}13.3'$ L- $155.67'$

58 +51.13 P.C. $0^{\circ}00'$ R- $1146.28'$

+37.46 P.T. .01 $17^{\circ}19'$

53 $14^{\circ}30.9'$ $\Delta 34^{\circ}38' R$

+50 $10^{\circ}45.4'$ D- $15^{\circ}00'$

52 +26.0 P.I. T- $119.43'$

52 $7^{\circ}00.4'$ L- $230.89'$

+50 $3^{\circ}15.4'$ R- $383.06'$

51 +06.57 P.C. $0^{\circ}00'$

2/24/39
K.R.
L.B.H.
L.G.
M.J.G.

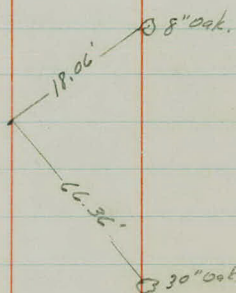
5

513.67

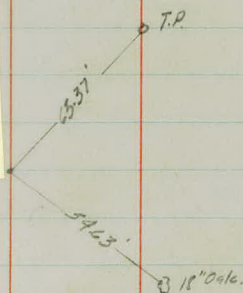
A = 381.97

498.12

revised, then
see pg. 42



Nail



Bolt Spike

Sta.	Point	ΔL	ΔR
	+04.79 P.T.	22° 43'	
67		22° 11.4'	Δ 45° 26' Lt.
	+50	16° 41.4'	D. 22°
	+07.98 P.I.		T. 109.70'
66		11° 14.4'	L. 206.51'
	+50	5° 41.4'	023' R. 262.04'
65		0° 14.4'	
64	+98.28 P.C.	0° 00'	
		93.01'	
	+03.21' P.T.		4° 53.5'
64			4° 50.6'
	+50		4° 05.6'
63			3° 20.6' Δ 9° 47' Rt
	+50		2° 35.6' D. - 3°
	+90.57 P.I.		T. - 163.49'
62			1° 50.6' L. - 329.44'
	+50		1° 05.6' R. - 1910.08'
61			0° 20.6'
60	+77.10 P.C.		0° 00'

15.05' $\rightarrow$ 18" Elm

Bolt Spike

22.85'

$\rightarrow$ 20" Oak.

95.07

Nail

36.61' $\rightarrow$ 26.1' $\rightarrow$ 12" Ash

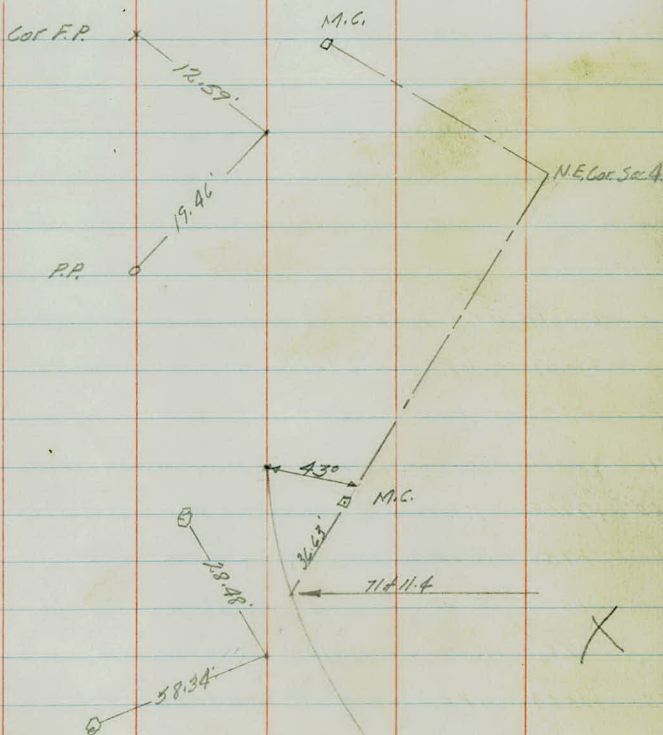
R.R. O

70.30

Sta.	Point	ΔL	ΔR
	+89.79 P.T.		18'45'
	+50		16°33.7'
79			13'48.7' Δ -37°30'
	+50		11°03.7' D-11°
	+25.96 P.I.		T-177.08'
78			8°18.7' L-340.99'
	+50		5°32.7' R-521.67'
77			2°48.7'
76	+48.88 P.C.		0°00'
	+36.98 P.T.		9°53'
72			8°52.8'
	+50		7°42.8'
71			6°27.8' Δ 19°46' R
	+50		5°12.8' D-5°
	+41.17 P.I.		T-199.72'
70			3°57.8' L-395.33'
	+50		2°42.8' R-1146.88'
69			1°27.8'
68	+41.15 P.C.		0°00'

412.10

$A = 520.99$



Spikes

$A = 1145.91$

136.66

Sta	Point	ΔLt	ΔRt
-----	-------	-------------	-------------

469+61.11 N. Co. Line Rd

130.07	P.T.	43°29.5'	.36
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125		41°33.4'	$\Delta 86°59' Lt$
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81		32°03.4'	D- 76°
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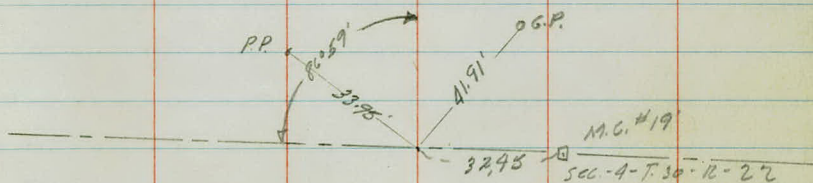
80	+92.68	P.L.	T- 77.04'
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175		22°33.4'	L- 114.45'
-----	--	----------	------------

150		13°03.4'	R- 81.21'
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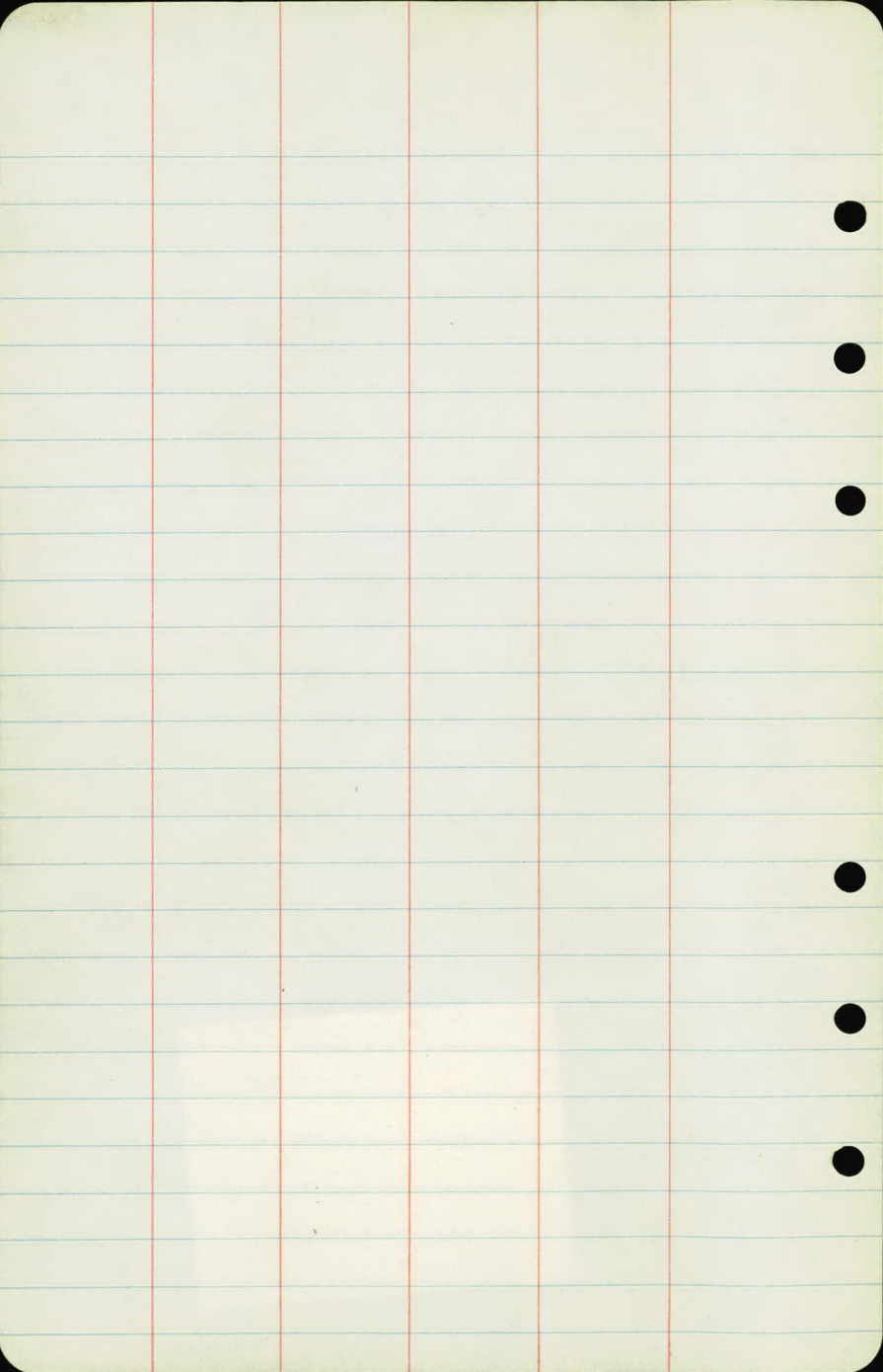
125		3°33.4'	0.70
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80	+15.64	P.C.	0°00'
----	--------	------	-------



25.85

$A = 75.39$



Topography

+92-T.P.-29'

+74-Δ in Fe-34'

5 Fe-35'

14'

15'

+52-T.P.-28'

4 Fe-36'

14'

13'

3

15'

12'

+77-T.P.-27'

2 Fe-36'

16'

11'

1

16'

10'

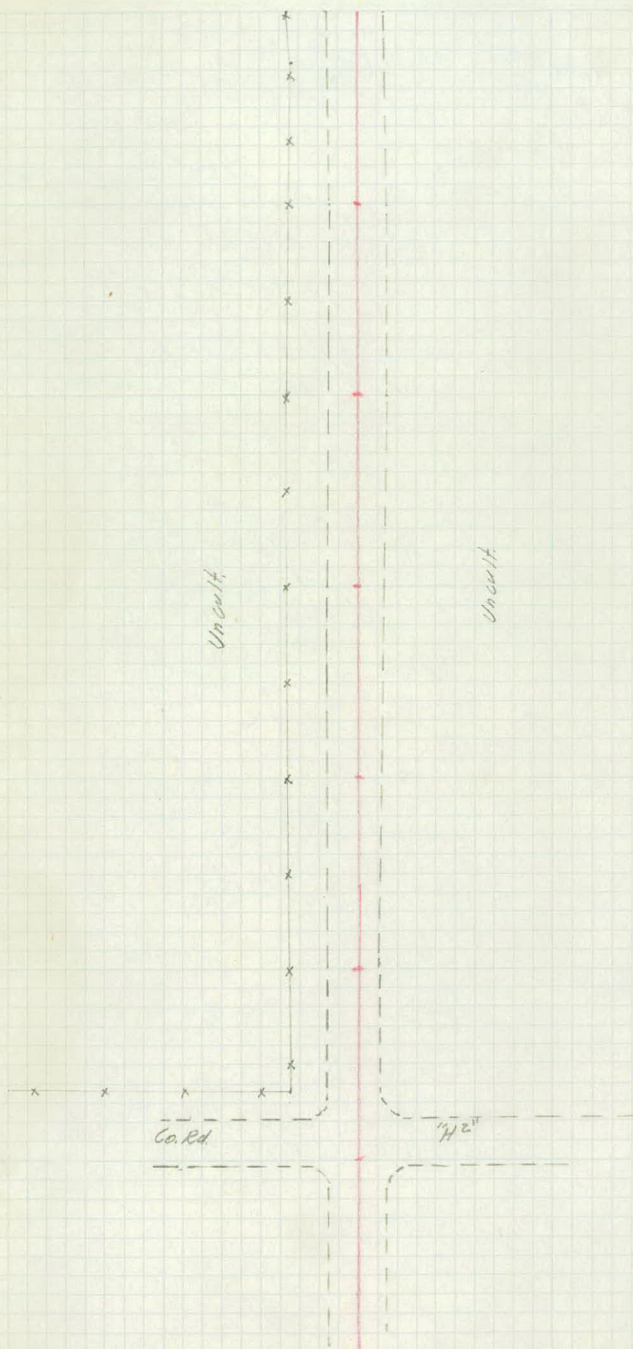
+03-T.P.-27'

+20-Fe Cor-35'

+30=N. Edge #1 Top

0+00

-02= So. Edge #1 Top



12 13' 13' Fc-35'

169-F.P.-33'

11 Fc-35 13' 14' Fc-35'

10 Fc-35 ^{NEW} 116-224' X 66' C.M. 33' 33' 121 + F.P.-33' Reg. Swamp. Fc-35

9 Fc-35' 12' 14' Fc-34'

172-F.P.-33'

8 Fc-35 12' 15' Fc-35'

FC-34 +50. 14' 14' Fc-34'

7 Fc-34' 14' 13' +25-Fc-34'-36' +21-F.P.-34' +04-Ent. 12' X 26' C.M. 27'

180-Ent. 12' X 18' C.M. 26'

150-Fc-36'

162-Reg Fc-34'

6 Fc-36 16' 12'

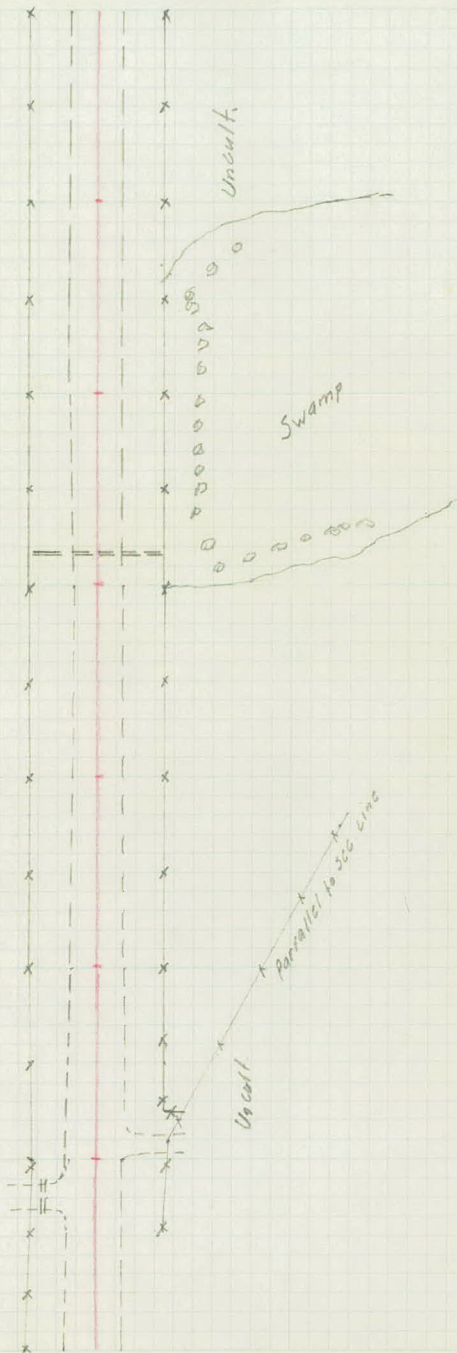
Uncult.

Uncult.

Swamp

Parallel to sec line

Uncult



19

13'

12'

+52 - P.P. - 35'

+50 - Fe. - 35'

+34 - Range Tie to Fe.

+31 - T.P. - 33'

18

13'

12'

17

13'

12'

+51 - T.P. - 33'

16

+18 - End $\frac{12' \times 202.14}{28'}$

+90 - Cor. Ho. - 144'

13'

13'

+22 - P.P. - 28'

+32 - End $\frac{12' \times 202.14}{29'}$

15

13'

13'

+71 - T.P. - 33'

14

+07 - Fe Cor. - 36'

12'

14'

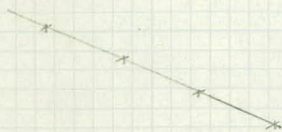
+67 - Fe. Cor. - 34'

13 Fe. - 35'

12'

14'

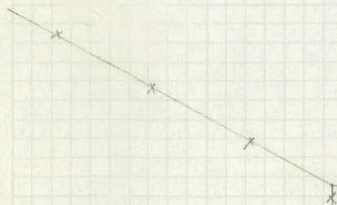
+21 - T.P. - 33'



cont.



Uncert.



x

x

x

x

x

Uncert.

x

x

+46-T.P.-28'

26

10'

13'

25

11'

13'

+78-P.P.-30'

+75-T.P.-33'

24

11'

14'

+50-Lillian Hedge-27'
+48-N.E. Cor. Ho.-67'
+35-10" B.E. Elder-34'
+15-10" B.E. Elder-30'
+10-Range Tie to Ho.
+90-10" B.E. Elder-39'

+52-T.P.-33'

23

10'

13'

+56-to Ent.
+45-Cor. Orchard-46'

22

12'

11'

+95-8" Cherry Tr.-33'
+80-3" Cherry Tr.-33'
+77-P.P.-39'
+70-Cor. Orchard-56'
+49-Range Tie to Orchard

+85-T.P.-33'

21

12'

11'

20

12'

12'

+10-T.P.-33'

Cult.

Cult.



151-T.P.-19'

33 2' 17'

150 8' 11'

32 14' 6'

172-P.P.-42'

170-T.P.-28'

150 13' 6'

31 12' 7'

150 8' 10'

30 10' 11'

197-T.P.-36'

29 10' 11'

127-P.P.-25'

126-T.P.-32'

28 9' 11'

27 110- ϕ 20"X42' C.M.

9 21' 21' 11'

Cult.

Uncult.

Lowland

+55-T.R.-37'

+23-P.R.-10'

40

4'

16

39

3'

16'

+81-T.R.-38'

38

4'

16'

+41-P.R.-12'

37

3'

16'

+05-T.R.-39'

+77-6.18" X 32.5" M.

11' 21'

36

3'

17'

+39-T.R.-39'

35

4'

16'

+55-P.R.-11'

34

3'

17'

Cult

Cult

				+40-T.P.-34'
47		6'	12'	Fe-17'
				+79-Ent
+K.P.P.-37'	+50	8'	15'	+55-12" B.E. Cor-29' + Fe.
+52-8 1/8" X 27 C.W.		1' 30"		
46		0	20'	+19-Fe Cor-43'
				+98-King's Sig to Fe.
				+93-18" Oak-42'
				+71-T.R.-38'
	+50	1'	19'	+58-18" Willow 35'
				+97-24" Willow-30'
45		3'	19'	
				+91-10" Oak-27'
				+77-8" Oak-27'
				+71-12" Oak-29'
				+55-10" Oak-28'
				+51-24" Oak-36'
44		2'	19'	+08-T.P.-36'
				+84-24" Oak-45'
				+57-12" Oak-41'
				+26-20" Oak-48'
43	+15-P.R.-14'	5'	15'	
				+98-18" Oak-36'
				+09-Ent.
				+99-18" Oak-45'
				+45-T.P.-19'
				+26-N.W. Cor No.
				+14-6.53 lap 16 1/4 in 26' Top-30'
42		4'	18'	+02-S.W. Cor Ho-32'
				+05-24" Oak-49'
				+87-24" Oak-37'
				+57-Fe-32'
41		4'	16'	

Curb

Scattered Oaks



107-18x35-19' 19' 1/2'
 Trs-50'
 54 Tr-Line-Fe-21' 10' 7' Fe-14'

+74-Tr-Line-27'
 +64-T.P.-28'
 +46-Fe+18'-35-27-50'
 +15-Fe-60-30'

53 15' 7' Fe-12'

+59-PP-69'
 +72-T.P.-28'

+50 14' 6'

52 12' 6' +04-18' Elm-33' Fe-13

+50 12' 8' +50-18' Oak-15' +Fe

51 11' 8' Fe-15'
 +90-6' Birch-20'
 +95-T.P.-30

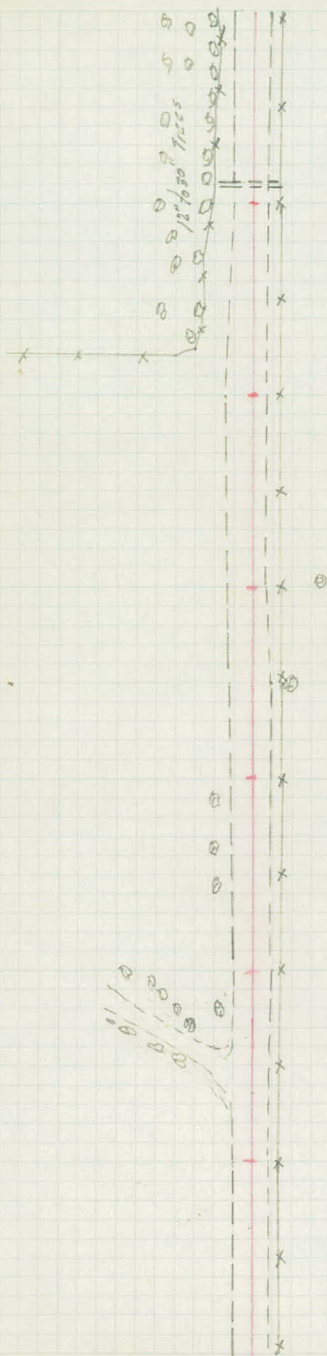
+6-18' Birch-20'
 +96-10' Oak-19'

50 10' 9' +12-TP-29'

+82-12' Oak-19'
 +71-Low. 18' 1/2' 1/2' 35'
 +51-Ent.

49 11' 8' +14-T.P.-31' Fe-12'

48 10' 10' Fe-14'



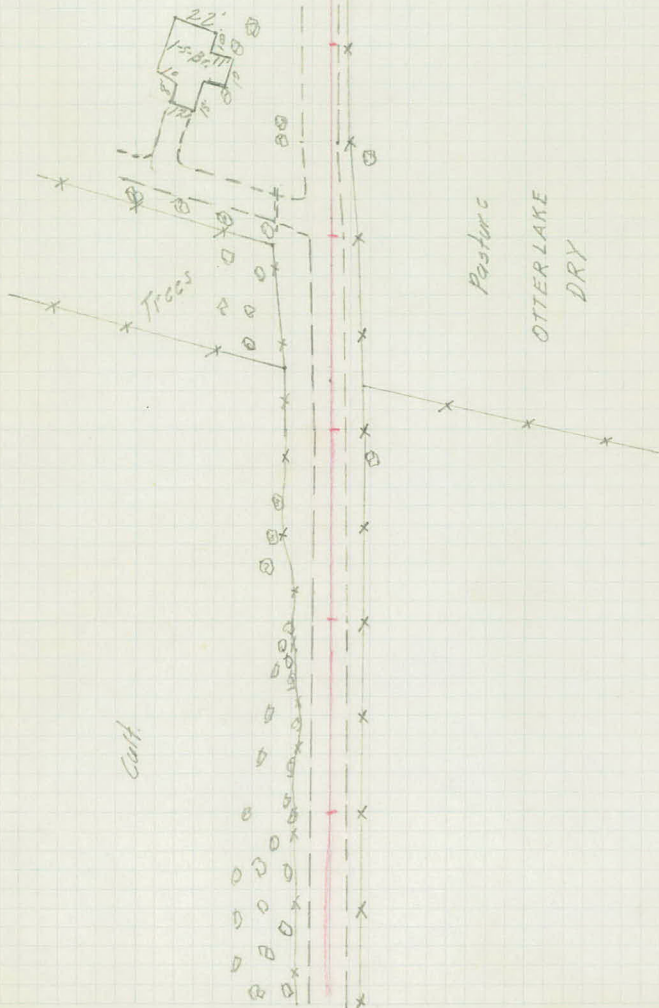
Posture

OTTER LAKE

DRY

	Fe-25'	450.	16'	3'	Fe-7'
41	Reg. Fe-30'		16'	3'	Fe-P'
		450	16'	2'	+69-15" Oak-29'
					Fe-9'
40	+08-N.E. Cor. Ho-60'		16'	2'	Fe-9'
	+67-3.5' Cor. Ho-71'				
	+60-6" Birch-28'	450.	15'	2'	
	+51-8" Birch-27'				+41-10" Oak-18'
	+32-P.P.-32'				Fe-10'
	+10-8" Birch	12" x 276" M			
	+03-New Bricks-32'	30"			+19-End
59			11"	7'	+07-10" Oak-22'
	+57-Fe Cor-30				Fe-13'
	+80-Bridge Tie				
	+84-T.P.-30'				
					+64-30" Oak-18'
	+32-Fe Cor-23'				
	+26-Bridge Tie				+25-Bridge Tie
38	Fe-23'		9'	8'	+22-12 Cor-16'
					Fe-17'
					+15-15" Oak-17'
	+64-15" Ash-22'				
	+47-12" Oak-30'				+42-P.P.-27'
	+32-15" Oak-22'				
57	+14-6P-27'		10'	9'	Fe-14'
	End of 20 Fe-20				
	+60-Tr. Line-17'				
56	Fe-12 + Tr. Line	452	10'	9'	Fe-15'
	+39-TP-39'				
	+27-Tr. Line-17'				
35	Tr. Line + Fe-19'		10'	9'	Fe-15'

Do not disturb back slope
between Ertland sta 60+30



	+95-8" Oak-31'				+99-18" Elm-26'
	+71-6" Trp-Oak-34'	20"			+68-20" Stump-19'
	+59-PP-25'				+37-15" Elm-21'
	+35-20" Oak-24'				+35-14" Elm-20'
					FC-17
68	FC-14'	8'		11'	+80-15" Elm-21'
	+96-20" Oak-28'				
					+32-15" Elm-23'
					+22-24" Elm-24'
					+17-20" Elm-25'
					FC-15'
67	FC-13'	8'		11'	+72-13" Ash-30'
	+95-2-18" X 38" C.M.			14' 24'	
	FC-13'	9'		13'	FC-19'
					+42-12" Ash-32'
	+101-10" Oak-31'				+105-18" Elm-37'
66	FC-12'	8'		13'	FC-20
	+85-12" Oak-22'				+76-FC Cor 20-20" Oak-30'
	+78-24" Oak-25'				
	FC-19'	10		10'	FC-16'
	+30-12" Oak-23'				+95-20" Oak-20'
	+27-PP-33'				+18-30" Stump-14'
	+18-14" Oak-21'				FC-15'
	+102-101'				
65	FC-22'	11'		7'	+92-15" Oak-21'
	+98-FC Cor-28'				+36-18" Oak-18'
	+49-Range FC				
64	FC-28'	13'		6'	FC-11'
					+89-15" Oak-16'
					+52-18" Oak-14'
		15'		4'	FC-10'
	+93-D in FC-28'				
	+20-D in FC-22'				
		16'		3'	
63	FC-22'				FC-10'
	+92-2-12" X 35" C.M.			25' 10'	
					+79-10" Iron Wood-18'
	FC-24'	16'		3'	FC-9'
					+34-12" Ash-19'
	+15-PP-33'				
	+17-5" High Birch-28'				
62	FC-26'	16'		3'	FC-8'

Scattered Oaks

Scattered Oaks

save trees if possible

Postup *

OTTER LAKE
*
DRY

+74-20" Elm-27'

75 Tr-50' Fc-17' 9' 9' +18-18" Elm-24' Fc-15'
+83-P.P-15'

74 Fc-19' 9' 9' +08-12" Ash-17' 2" Ash-17' +Fc-
+88-Bry. Woods-50'

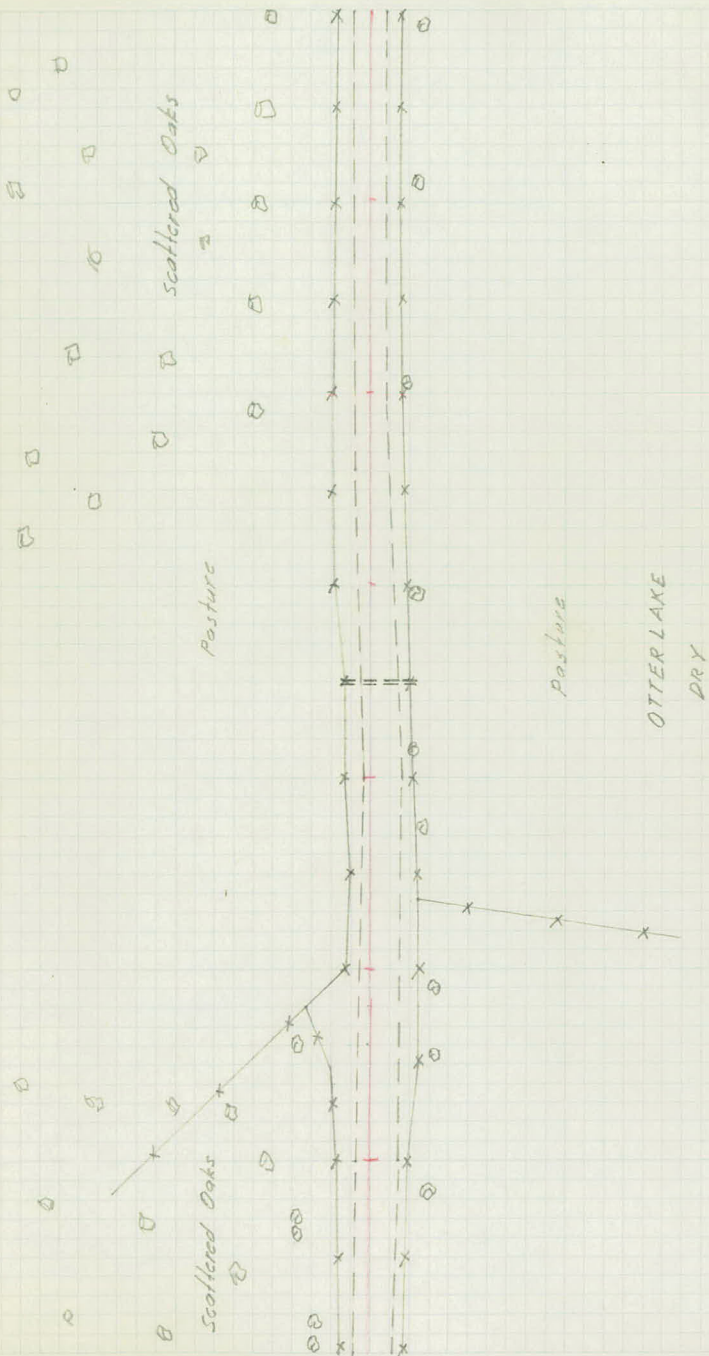
73 Fc-18' 7' 10' Fc-21'
+98-18" Elm-22'
+50-2-18" X 37-44' 14' 23' 13' Fc-20'
Fc-13'

72 Fc-12' 4' 10' +15-15" Elm-20' Fc-21'
+22-P.P-22' +76-18" Trip Elm-25'
Fc-10' 5' 10' +40-20" Elm-24'
+37-Fc Cor-24'

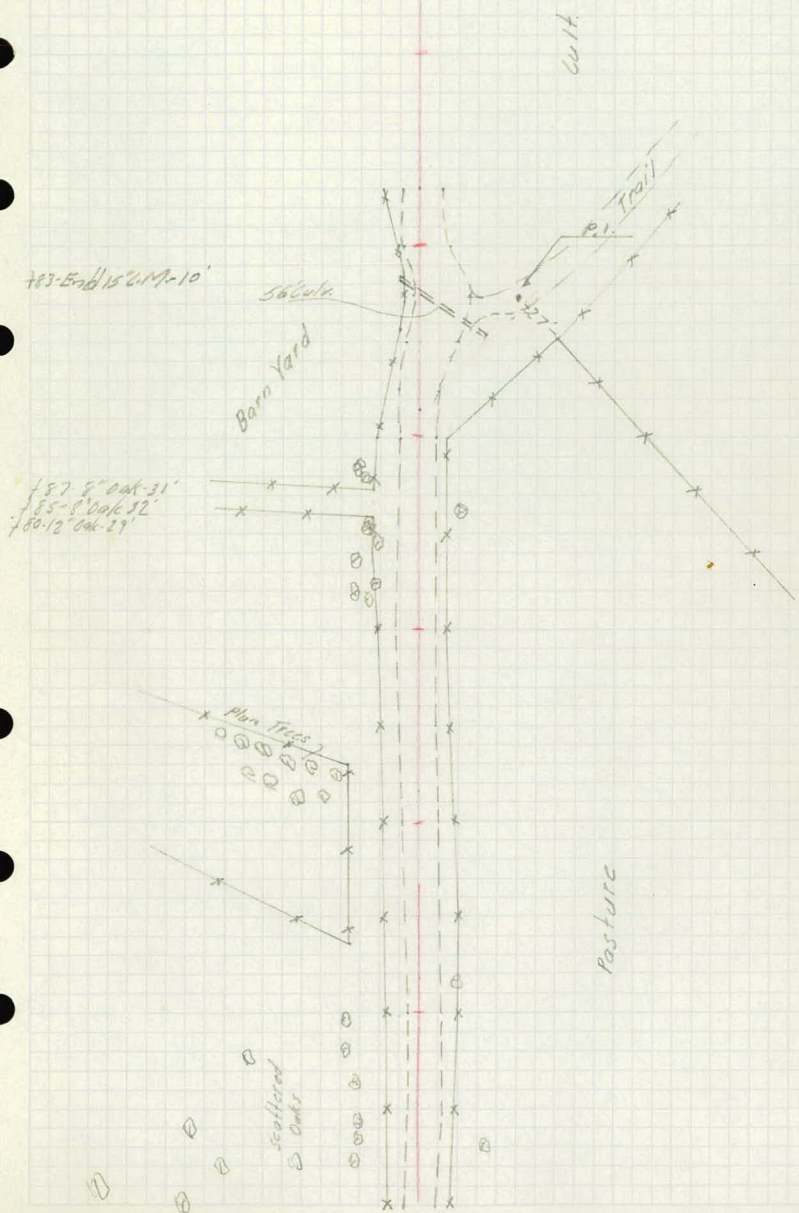
71 +01-Δ in Fc-12' 6' 15' Fc-24'
+57-12" 5' stump-15' +91-15" Elm-31'
+80-Fc Cor-23'
+02-12" 5' stump-15'
+02-12" 5' stump-24' 18" Oak-38' 13-20' +38-8" Birch-32' Fc-23'
+41-14" stump-19' 7' 13'
+30-8" stump-15'

70 +15-12" stump-10' 8' 13' Fc-19'
+98-15" stump-17-6 Fc
+80-20" stump-19' +85-12" Birch-29'
+78-8" Oak-37'
+05-15" Oak-37' Fc-10' 8' 10' Fc-17'

+17-18" Oak-29'
+06-12" Oak-27'
69 Fc-15' 9' 11' Fc-17'



	+30.27	Fc.-19'	9'	11'	
81	+95'-Δ in Fc.-12'		8'	15'	+94-P.R.-42'
	+84'-Δ in Fc.-9'				
	+71'-Δ in Fc.-8'	+75.	5'	24'	
	+36'-Δ in Fc.-10'	+50	7'	17'	+54-End 12" C.M.-34'
		12.5	11'	9'	
80	Fc.-22'		10'	8'	Fc.-12'
	+66-End - H. B. Wyman Fc. pccs				
	+36-15' Oak-24'				
	+52-12' Oak-26'				+65-Cattle Fc.
	+48-12' Oak-22'				+63-30' Oak-20'
	Fc.-24'	11'	8'		Fc.-12'
	+38-12' Oak-22'				
	+25-12' Tw Oak-21'				
	+23-18' Oak-22'				
	+19-12' Oak-22'				
79	Fc.-21'	10'	8'		Fc.-13'
	Fc.-19'	10	9'		Fc.-15'
	+30-Fc. Jan-37'				
	+16-Range Tie				
78	Fc.-35' P.R.-34' Fc.-19'	9'	10'		Fc.-18'
	Fc.-18'	8'	10'		Fc.-20'
	+36-Fc. Jan-36'				
	+17-Range Tie				
77	Fc.-16'	6'	11'		+17-6" Thorn Apple-19'
	+99-15' Tw Oak-27'				Fc.-20'
	+92-18' S. Oak-21'				
	+91-18' Tw Oak-29'				
	+25-12' Oak-29'				
	Fc.-14'	6'	11'		Fc.-17'
	+45-8' Oak-31'				
	+38-20' Oak-31'				+31-15" Ash-32'
	+33-12' Oak-33'				
76	Fc.-15'	8'	9'		Fc.-16'





x sections

1. 5. 5.

2. 5. 5.

x Sect in Current
Drawer
Haw #2

Sta	+	Σ	-	Elev.
B.M.	1.96	936.39		934.43
T.P.	7.33	935.23	8.47	927.90
T.P.	6.92	938.40	3.75	931.48
B.M.	3.95	940.47	1.88	936.52
0	+10. Approx. 4" $\pm$			37.2
	+23			37.0
	+39			36.5
1				35.0
	+50			34.0
2				33.1
	+50			32.5
3				32.1
T.P.	3.87	936.07	8.37	932.10
	+50			31.9
4				31.7

3/1/39
K.A.
L.B.H.
L.G.
M.D.G.

Lt

L

Rt.

Spike in R.P. 60 Lt 15+20

Spike in R.P. SE Cor "H2" & Otter Lake Rd.

$$\frac{29}{50}$$

$$\frac{33}{50}$$

$$\frac{48}{50}$$

$$\frac{33}{50} \quad \frac{33}{20} \quad \frac{35}{15} \quad \frac{38}{32} \quad \frac{46}{50} \quad \frac{52}{50}$$

$$\frac{13}{50} \quad \frac{26}{54} \quad \frac{59}{28} \quad \frac{67}{22} \quad \frac{45}{17} \quad \frac{40}{18} \quad \frac{45}{24} \quad \frac{64}{29} \quad \frac{69}{53} \quad \frac{65}{34} \quad \frac{72}{50}$$

$$\frac{40}{50} \quad \frac{57}{33} \quad \frac{81}{50} \quad \frac{76}{21} \quad \frac{60}{18} \quad \frac{57}{10} \quad \frac{55}{11} \quad \frac{57}{17} \quad \frac{57}{24} \quad \frac{76}{50} \quad \frac{101}{50}$$

$$\frac{71}{50} \quad \frac{81}{33} \quad \frac{93}{29} \quad \frac{88}{22} \quad \frac{71}{17} \quad \frac{69}{12} \quad \frac{65}{12} \quad \frac{69}{12} \quad \frac{71}{19} \quad \frac{92}{28} \quad \frac{100}{50}$$

$$\frac{85}{50} \quad \frac{89}{34} \quad \frac{98}{31} \quad \frac{94}{23} \quad \frac{80}{19} \quad \frac{78}{14} \quad \frac{74}{10} \quad \frac{76}{17} \quad \frac{78}{27} \quad \frac{101}{27} \quad \frac{109}{50}$$

$$\frac{91}{50} \quad \frac{92}{34} \quad \frac{107}{31} \quad \frac{100}{22} \quad \frac{86}{17} \quad \frac{84}{12} \quad \frac{80}{12} \quad \frac{83}{11} \quad \frac{83}{18} \quad \frac{104}{27} \quad \frac{107}{50}$$

$$\frac{95}{50} \quad \frac{93}{34} \quad \frac{110}{31} \quad \frac{106}{22} \quad \frac{91}{18} \quad \frac{88}{13} \quad \frac{84}{11} \quad \frac{86}{17} \quad \frac{87}{22} \quad \frac{105}{31} \quad \frac{110}{33} \quad \frac{89}{33} \quad \frac{92}{50}$$

$$\frac{53}{50} \quad \frac{50}{34} \quad \frac{74}{31} \quad \frac{65}{23} \quad \frac{50}{18} \quad \frac{44}{9} \quad \frac{42}{11} \quad \frac{45}{11} \quad \frac{46}{17} \quad \frac{45}{23} \quad \frac{69}{30} \quad \frac{41}{34} \quad \frac{46}{50}$$

$$\frac{45}{50} \quad \frac{46}{34} \quad \frac{71}{31} \quad \frac{69}{22} \quad \frac{51}{17} \quad \frac{48}{12} \quad \frac{44}{11} \quad \frac{47}{17} \quad \frac{49}{23} \quad \frac{67}{31} \quad \frac{73}{34} \quad \frac{57}{34} \quad \frac{69}{50}$$

Sta.	+	π	-	Elev.
		936.07		
4	150			31.4
5				31.1
	150			30.8
		x		
6				30.7
	150			30.7
7				30.3
	150			30.1
8				29.6
T.P.	4.01	933.68	6.40	927.67
	150			29.4
9				29.1
	150			28.8

H.

K.

Rt.

$$\frac{48}{50} \frac{47}{33} \frac{71}{31} \frac{70}{22} \frac{54}{17} \frac{50}{10} \frac{47}{12} \frac{50}{12} \frac{50}{18} \frac{71}{23} \frac{81}{30} \frac{38}{33} \frac{57}{50}$$

$$\frac{44}{50} \frac{48}{34} \frac{71}{30} \frac{71}{22} \frac{62}{19} \frac{56}{11} \frac{50}{12} \frac{50}{17} \frac{50}{22} \frac{72}{27} \frac{78}{34} \frac{46}{34} \frac{46}{50}$$

$$\frac{65}{50} \frac{67}{33} \frac{81}{31} \frac{74}{22} \frac{64}{19} \frac{59}{10} \frac{53}{12} \frac{52}{12} \frac{54}{17} \frac{78}{22} \frac{83}{30} \frac{73}{50}$$

$$\frac{79}{50} \frac{77}{34} \frac{86}{32} \frac{28}{23} \frac{67}{19} \frac{63}{11} \frac{54}{11} \frac{51}{17} \frac{50}{23} \frac{76}{31} \frac{80}{34} \frac{63}{34} \frac{61}{50} \checkmark$$

$$\frac{74}{50} \frac{72}{34} \frac{85}{32} \frac{81}{23} \frac{71}{19} \frac{63}{10} \frac{59}{11} \frac{52}{17} \frac{52}{22} \frac{80}{31} \frac{80}{34} \frac{54}{34} \frac{52}{50}$$

$$\frac{63}{50} \frac{61}{33} \frac{84}{30} \frac{82}{21} \frac{68}{17} \frac{66}{9} \frac{58}{10} \frac{54}{18} \frac{52}{23} \frac{76}{30} \frac{83}{33} \frac{58}{33} \frac{61}{50}$$

$$\frac{70}{50} \frac{63}{33} \frac{88}{30} \frac{83}{21} \frac{70}{17} \frac{67}{11} \frac{60}{13} \frac{59}{13} \frac{62}{18} \frac{85}{22} \frac{87}{31} \frac{65}{34} \frac{57}{50}$$

$$\frac{79}{50} \frac{74}{34} \frac{70}{31} \frac{84}{20} \frac{73}{17} \frac{67}{9} \frac{65}{14} \frac{63}{19} \frac{65}{24} \frac{85}{31} \frac{91}{34} \frac{74}{34} \frac{73}{50}$$

$$\frac{59}{50} \frac{55}{33} \frac{68}{31} \frac{63}{21} \frac{48}{16} \frac{47}{9} \frac{43}{14} \frac{43}{18} \frac{45}{22} \frac{61}{27} \frac{73}{33} \frac{51}{33} \frac{43}{50}$$

$$\frac{41}{50} \frac{57}{34} \frac{72}{30} \frac{65}{21} \frac{48}{16} \frac{48}{9} \frac{46}{14} \frac{48}{18} \frac{50}{22} \frac{67}{31} \frac{72}{34} \frac{56}{34} \frac{60}{50}$$

$$\frac{68}{50} \frac{70}{34} \frac{78}{31} \frac{72}{22} \frac{48}{18} \frac{53}{10} \frac{47}{13} \frac{57}{21} \frac{58}{27} \frac{87}{50}$$

sta	+	π	-	Elev
		933.68		
10				28.4
	+16 Flow Line & Culvert			
T.P.	5.35	933.17	5.86	927.82
+50				27.9
11				28.0
+50				28.4
12				28.9
+50				29.5
T.P.	8.14	938.19	3.12	930.05
13				30.1
+50				30.7
14				31.3
+50				32.1

lt.

l

rt.

$\frac{99}{30} \frac{10.8}{42} \frac{11.0}{96} \frac{10.7}{90} \frac{6.8}{20} \frac{5.7}{16} \frac{5.3}{13} \frac{5.7}{18} \frac{6.0}{31} \frac{12.0}{41} \frac{13.0}{41} \frac{13.0}{50}$

11.60

13.95

Top 2nd F.P. N. 2000

$\frac{8.2}{50} \frac{8.4}{43} \frac{9.7}{32} \frac{9.3}{24} \frac{5.9}{18} \frac{5.6}{10} \frac{5.3}{12} \frac{5.8}{18} \frac{6.2}{29} \frac{12.3}{35} \frac{12.8}{35} \frac{13.6}{50}$

$\frac{6.8}{50} \frac{7.4}{41} \frac{7.7}{33} \frac{7.6}{24} \frac{5.6}{18} \frac{5.5}{12} \frac{5.2}{13} \frac{5.8}{18} \frac{6.2}{27} \frac{12.5}{36} \frac{13.1}{36} \frac{13.7}{50}$

$\frac{3.6}{50} \frac{5.3}{34} \frac{6.9}{30} \frac{6.3}{23} \frac{5.6}{19} \frac{4.9}{9} \frac{4.8}{9} \frac{5.3}{13} \frac{5.5}{18} \frac{12.4}{29} \frac{12.8}{36} \frac{13.7}{50}$

$\frac{1.3}{50} \frac{3.0}{23} \frac{1.8}{29} \frac{5.8}{23} \frac{4.5}{17} \frac{4.5}{10} \frac{4.3}{14} \frac{4.7}{21} \frac{5.4}{29} \frac{8.7}{35} \frac{9.7}{35} \frac{11.1}{50}$

$\frac{10.6}{50} \frac{0.8}{34} \frac{5.0}{30} \frac{5.3}{22} \frac{4.2}{19} \frac{4.0}{11} \frac{3.7}{11} \frac{4.0}{15} \frac{4.4}{20} \frac{5.7}{26} \frac{5.9}{30} \frac{5.4}{32} \frac{6.0}{39} \frac{7.3}{50}$

$\frac{5.0}{50} \frac{5.8}{35} \frac{10.2}{29} \frac{10.0}{23} \frac{8.6}{17} \frac{8.5}{11} \frac{8.1}{13} \frac{8.4}{18} \frac{8.7}{21} \frac{9.4}{24} \frac{9.8}{29} \frac{10.7}{34} \frac{8.1}{41} \frac{8.1}{41} \frac{8.3}{50}$

$\frac{5.2}{50} \frac{5.6}{35} \frac{9.8}{29} \frac{7.6}{23} \frac{8.3}{19} \frac{7.5}{11} \frac{7.5}{12} \frac{7.7}{18} \frac{8.0}{22} \frac{9.0}{27} \frac{9.5}{33} \frac{6.0}{33} \frac{5.6}{50}$

$\frac{3.3}{50} \frac{3.5}{33} \frac{9.3}{27} \frac{9.1}{23} \frac{8.0}{18} \frac{7.2}{11} \frac{6.9}{12} \frac{7.2}{17} \frac{7.4}{22} \frac{8.7}{27} \frac{9.3}{34} \frac{5.8}{34} \frac{6.1}{50}$

$\frac{6.8}{50} \frac{6.9}{33} \frac{9.0}{30} \frac{8.7}{24} \frac{6.8}{18} \frac{6.5}{11} \frac{6.1}{14} \frac{6.7}{17} \frac{6.9}{22} \frac{8.6}{29} \frac{9.0}{33} \frac{7.1}{33} \frac{7.1}{50}$

Sta	+	π	-	F/cv	
		938.19			
15				32.8	
B.M.	3.74	938.17	3.74	934.45	(934.43)
+50				33.2	
16				33.3	
+50				33.4	
17				33.5	
+50				33.7	
18				33.8	
+50				34.0	
T.P.	6.22	940.54	3.85	934.32	
19				34.2	
+50				34.4	
20				34.5	

Lt.

k

Rt.

$\frac{55}{50}$ $\frac{47}{33}$ $\frac{85}{30}$ $\frac{85}{25}$ $\frac{59}{17}$ $\frac{58}{11}$ $\frac{54}{11}$ $\frac{58}{11}$ $\frac{60}{16}$ $\frac{80}{21}$ $\frac{83}{29}$ $\frac{63}{33}$ $\frac{70}{50}$

Spikes in FR 60' 4.15 + 20

$\frac{45}{50}$ $\frac{41}{33}$ $\frac{83}{28}$ $\frac{86}{21}$ $\frac{56}{15}$ $\frac{53}{10}$ $\frac{50}{12}$ $\frac{52}{19}$ $\frac{52}{26}$ $\frac{77}{30}$ $\frac{82}{34}$ $\frac{60}{50}$ $\frac{67}{50}$

$\frac{53}{50}$ $\frac{51}{37}$ $\frac{77}{31}$ $\frac{76}{22}$ $\frac{55}{16}$ $\frac{50}{10}$ $\frac{48}{13}$ $\frac{56}{19}$ $\frac{58}{23}$ $\frac{72}{28}$ $\frac{78}{50}$ $\frac{78}{50}$

$\frac{54}{50}$ $\frac{51}{34}$ $\frac{28}{29}$ $\frac{71}{22}$ $\frac{53}{17}$ $\frac{50}{10}$ $\frac{48}{13}$ $\frac{55}{19}$ $\frac{58}{19}$ $\frac{73}{25}$ $\frac{76}{31}$ $\frac{70}{50}$

$\frac{47}{50}$ $\frac{45}{34}$ $\frac{80}{28}$ $\frac{72}{22}$ $\frac{54}{17}$ $\frac{50}{10}$ $\frac{47}{12}$ $\frac{50}{18}$ $\frac{50}{23}$ $\frac{66}{32}$ $\frac{72}{35}$ $\frac{59}{50}$ $\frac{50}{50}$

$\frac{50}{50}$ $\frac{47}{33}$ $\frac{71}{30}$ $\frac{68}{23}$ $\frac{49}{17}$ $\frac{48}{11}$ $\frac{45}{12}$ $\frac{47}{18}$ $\frac{51}{23}$ $\frac{63}{32}$ $\frac{70}{34}$ $\frac{59}{50}$ $\frac{50}{50}$

$\frac{44}{50}$ $\frac{44}{34}$ $\frac{67}{30}$ $\frac{69}{24}$ $\frac{47}{17}$ $\frac{46}{9}$ $\frac{44}{12}$ $\frac{48}{18}$ $\frac{49}{23}$ $\frac{65}{34}$ $\frac{69}{50}$ $\frac{65}{50}$

$\frac{39}{50}$ $\frac{37}{35}$ $\frac{65}{31}$ $\frac{63}{24}$ $\frac{47}{18}$ $\frac{46}{11}$ $\frac{42}{12}$ $\frac{47}{13}$ $\frac{48}{20}$ $\frac{64}{25}$ $\frac{61}{50}$

$\frac{61}{50}$ $\frac{53}{34}$ $\frac{80}{29}$ $\frac{90}{26}$ $\frac{71}{18}$ $\frac{67}{13}$ $\frac{63}{11}$ $\frac{66}{17}$ $\frac{65}{23}$ $\frac{80}{30}$ $\frac{87}{34}$ $\frac{63}{50}$ $\frac{63}{50}$

$\frac{63}{50}$ $\frac{56}{33}$ $\frac{80}{29}$ $\frac{90}{24}$ $\frac{66}{17}$ $\frac{64}{15}$ $\frac{61}{9}$ $\frac{63}{21}$ $\frac{59}{25}$ $\frac{72}{29}$ $\frac{73}{34}$ $\frac{50}{50}$ $\frac{46}{50}$

$\frac{67}{50}$ $\frac{60}{34}$ $\frac{85}{29}$ $\frac{84}{23}$ $\frac{65}{19}$ $\frac{64}{12}$ $\frac{60}{10}$ $\frac{62}{10}$ $\frac{59}{18}$ $\frac{62}{24}$ $\frac{55}{34}$ $\frac{45}{50}$

Sta	+	π	-	Elev	
		940.59			
20	+50			34.7	
21				34.9	
	+50			35.2	
22				35.4	
	+50			35.8	
23				36.4	
T.P.	7.74	944.22	406	936.48	
B.M.	2.11	944.17	2.11	942.11	942.06
	+50			37.0	
24				37.5	
	+50			37.8	
25				37.6	

Lt.

C.

Rt.

$$\frac{78}{50} \frac{76}{37} \frac{87}{30} \frac{79}{24} \frac{65}{21} \frac{60}{15}$$

$$\frac{58}{7} \frac{61}{22} \frac{65}{31} \frac{66}{30} \frac{47}{30}$$

$$\frac{79}{50} \frac{81}{42} \frac{85}{31} \frac{81}{26} \frac{58}{17} \frac{58}{12} \frac{56}{10} \frac{59}{24} \frac{58}{34} \frac{45}{50}$$

$$\frac{74}{50} \frac{77}{26} \frac{54}{19} \frac{54}{13} \frac{53}{10} \frac{54}{18} \frac{54}{22} \frac{50}{31} \frac{45}{50}$$

$$\frac{67}{50} \frac{78}{28} \frac{69}{21} \frac{54}{17} \frac{52}{11} \frac{51}{12} \frac{52}{22} \frac{54}{28} \frac{60}{35} \frac{51}{50} \frac{40}{50}$$

$$\frac{56}{50} \frac{61}{27} \frac{55}{22} \frac{47}{15}$$

$$\frac{47}{19} \frac{55}{24} \frac{72}{26} \frac{68}{32} \frac{46}{35} \frac{39}{50}$$

$$\frac{18}{50} \frac{23}{31} \frac{47}{27} \frac{47}{13} \frac{41}{9} \frac{41}{8}$$

$$\frac{43}{14} \frac{48}{20} \frac{45}{32} \frac{36}{50}$$

Top S.E. Cor Wall at Front Steps of Ho. 54 231

$$\frac{50}{50} \frac{62}{28} \frac{68}{21} \frac{74}{8} \frac{72}{11} \frac{72}{23} \frac{68}{29} \frac{61}{50} \frac{57}{50}$$

$$\frac{55}{50} \frac{56}{23} \frac{66}{17} \frac{69}{8} \frac{67}{13} \frac{65}{28} \frac{58}{33} \frac{33}{50} \frac{37}{50}$$

$$\frac{24}{50} \frac{18}{30} \frac{65}{24} \frac{66}{9} \frac{64}{15} \frac{66}{26} \frac{74}{39} \frac{12}{50} \frac{15}{50}$$

$$\frac{10}{50} \frac{17}{30} \frac{65}{20} \frac{71}{10} \frac{66}{10} \frac{65}{21} \frac{79}{34} \frac{41}{50} \frac{54}{50}$$

Sta	+	π	-	Elev.
		944.17		
25	+50			37.0
26				35.9
T.P.	2.27	938.17	8.27	835.90
	+50			34.9
27				34.0
+10	Flow Line Culvert			
	+50			33.4
28				33.1
	+50			33.2
29				33.3
	+50			33.4
30				33.6

Lt.

L

Pt.

$$\frac{6.2}{50} \quad \frac{6.2}{29} \quad \frac{6.0}{19} \quad \frac{7.4}{16} \quad \frac{7.6}{9} \quad \frac{7.2}{\quad} \quad \frac{7.5}{12} \quad \frac{8.1}{23} \quad \frac{8.6}{34} \quad \frac{9.3}{50}$$

$$\frac{7.2}{50} \quad \frac{9.7}{24} \quad \frac{8.9}{14}$$

$$\frac{8.3}{13} \quad \frac{8.6}{16} \quad \frac{8.9}{22} \quad \frac{11.6}{31} \quad \frac{12.0}{50}$$

$$\frac{4.7}{50} \quad \frac{5.4}{35} \quad \frac{5.7}{20} \quad \frac{3.6}{15} \quad \frac{3.6}{7} \quad \frac{3.3}{13} \quad \frac{3.7}{17} \quad \frac{3.7}{29} \quad \frac{8.8}{39} \quad \frac{9.2}{50} \quad \frac{10.2}{\quad}$$

$$\frac{5.8}{50} \quad \frac{6.6}{39} \quad \frac{8.0}{21} \quad \frac{5.0}{14} \quad \frac{4.7}{9} \quad \frac{4.2}{11} \quad \frac{4.4}{17} \quad \frac{4.4}{27} \quad \frac{11.3}{40} \quad \frac{12.9}{50} \quad \frac{13.0}{\quad}$$

P.20

7.9.5

$$\frac{5.8}{50} \quad \frac{6.6}{30} \quad \frac{7.0}{18} \quad \frac{5.7}{12} \quad \frac{4.8}{\quad} \quad \frac{4.9}{9} \quad \frac{5.1}{15} \quad \frac{12.5}{27} \quad \frac{12.9}{40} \quad \frac{13.5}{50}$$

$$\frac{4.9}{50} \quad \frac{5.3}{31} \quad \frac{5.8}{16} \quad \frac{5.3}{9} \quad \frac{5.1}{14} \quad \frac{5.7}{22} \quad \frac{10.5}{34} \quad \frac{11.8}{50}$$

$$\frac{2.8}{50} \quad \frac{4.7}{25} \quad \frac{5.4}{15} \quad \frac{5.2}{10} \quad \frac{5.0}{\quad} \quad \frac{5.4}{14} \quad \frac{6.2}{16} \quad \frac{7.1}{22} \quad \frac{8.1}{34} \quad \frac{9.4}{50}$$

$$\frac{2.5}{50} \quad \frac{3.5}{29} \quad \frac{4.7}{24} \quad \frac{5.3}{18}$$

$$\frac{4.9}{10} \quad \frac{5.3}{14} \quad \frac{5.2}{\quad} \quad \frac{6.2}{21} \quad \frac{6.8}{27} \quad \frac{8.8}{50}$$

X

$$\frac{2.3}{50} \quad \frac{3.3}{28} \quad \frac{5.0}{19} \quad \frac{5.0}{10} \quad \frac{4.8}{\quad}$$

$$\frac{5.2}{20} \quad \frac{5.8}{26} \quad \frac{6.1}{33} \quad \frac{7.3}{50}$$

$$\frac{2.1}{50} \quad \frac{2.6}{58} \quad \frac{4.7}{17} \quad \frac{4.8}{8}$$

$$\frac{4.6}{9} \quad \frac{4.7}{16} \quad \frac{4.6}{23} \quad \frac{4.6}{39} \quad \frac{5.8}{50} \quad \frac{6.4}{\quad}$$

Sta	+	π	-	Elev
		938.17		
30	+50			33.5
31				33.3
	+50			32.8
32				33.0
T.P.	491	938.24	484	933.33
	+50			33.5
33				33.5
	+50			34.1
34				33.7
	+50			33.2
35				32.8
	+50			32.5

lt.

k.

rt.

$$\frac{28}{50} \quad \frac{41}{26} \quad \frac{48}{14} \quad \frac{47}{10} \quad \frac{47}{15} \quad \frac{44}{22} \quad \frac{60}{33} \quad \frac{70}{50} \quad \frac{83}{50}$$

$$\frac{20}{50} \quad \frac{32}{33} \quad \frac{37}{22} \quad \frac{44}{16}$$

$$\frac{47}{9} \quad \frac{51}{16} \quad \frac{52}{29} \quad \frac{67}{50}$$

$$\frac{35}{50} \quad \frac{43}{32} \quad \frac{43}{20} \quad \frac{46}{12} \quad 54$$

$$\frac{57}{15} \quad \frac{64}{23} \quad \frac{71}{34} \quad \frac{76}{50}$$

$$\frac{40}{50} \quad \frac{44}{36} \quad \frac{47}{21}$$

$$\frac{47}{11}$$

$$\frac{52}{9} \quad \frac{60}{13} \quad \frac{67}{20} \quad \frac{75}{32} \quad \frac{82}{50} \quad \frac{83}{50}$$

$$\frac{28}{50} \quad \frac{38}{36} \quad \frac{42}{20} \quad \frac{46}{10} \quad \frac{47}{13} \quad \frac{54}{19} \quad \frac{66}{26} \quad \frac{73}{41} \quad \frac{78}{50} \quad \frac{78}{50}$$

$$\frac{21}{50} \quad \frac{33}{26} \quad \frac{41}{14} \quad \frac{46}{6}$$

$$\frac{47}{16} \quad \frac{51}{21} \quad \frac{46}{24} \quad \frac{55}{33} \quad \frac{61}{50} \quad \frac{65}{50}$$

$$\frac{22}{30} \quad \frac{25}{33} \quad \frac{32}{15} \quad \frac{43}{8} \quad \frac{41}{1}$$

$$\frac{95}{18} \quad \frac{92}{25} \quad \frac{40}{33} \quad \frac{44}{50}$$

$$\frac{32}{30} \quad \frac{38}{34} \quad \frac{40}{25} \quad \frac{48}{7}$$

$$\frac{45}{25} \quad \frac{46}{29} \quad \frac{40}{42} \quad \frac{24}{30} \quad \frac{23}{50}$$

$$\frac{46}{50} \quad \frac{47}{21} \quad \frac{51}{9} \quad 50 \quad \frac{47}{8} \quad \frac{50}{22} \quad \frac{44}{27} \quad \frac{27}{38} \quad \frac{17}{50}$$

$$\frac{76}{50} \quad \frac{64}{24} \quad \frac{58}{7}$$

$$\frac{54}{8} \quad \frac{52}{23} \quad \frac{55}{28} \quad \frac{48}{40} \quad \frac{32}{50} \quad \frac{20}{50}$$

$$\frac{94}{50} \quad \frac{93}{29} \quad \frac{88}{21} \quad \frac{78}{10} \quad \frac{60}{5} \quad 57$$

$$\frac{55}{9} \quad \frac{58}{27} \quad \frac{45}{37} \quad \frac{28}{50}$$

Sta. + π - Elev.

938.24.

36

32.4

+5.0

32.2

37 +77 Flow line Culvert.

T.P.

37

32.0

T.P.

708

940.60.

472

933.52

+5.0

32.5

38

33.0

+5.0

33.5

39

33.9

+5.0

34.6

40

35.0

+5.0

35.3

Lt.

C

Rt.

$$\frac{75}{50} \quad \frac{97}{13} \quad \frac{63}{5} \quad \frac{58}{9} \quad \frac{55}{26} \quad \frac{60}{37} \quad \frac{57}{50} \quad \frac{42}{50}$$

$$\frac{94}{50} \quad \frac{97}{33} \quad \frac{97}{18} \quad \frac{91}{10} \quad \frac{65}{6} \quad \frac{60}{8} \quad \frac{57}{18} \quad \frac{63}{20} \quad \frac{73}{23} \quad \frac{80}{35} \quad \frac{70}{50} \quad \frac{60}{50}$$

112

9.75

$$\frac{87}{50} \quad \frac{80}{34} \quad \frac{98}{24} \quad \frac{58}{13} \quad \frac{67}{7} \quad \frac{62}{9} \quad \frac{59}{18} \quad \frac{64}{22} \quad \frac{76}{30} \quad \frac{72}{50} \quad \frac{55}{50}$$

T90 Cule Market at

$$\frac{98}{50} \quad \frac{107}{39} \quad \frac{113}{26} \quad \frac{115}{13} \quad \frac{100}{9} \quad \frac{86}{6} \quad \frac{81}{10} \quad \frac{78}{18} \quad \frac{83}{23} \quad \frac{97}{33} \quad \frac{85}{50} \quad \frac{76}{50}$$

$$\frac{84}{50} \quad \frac{64}{30} \quad \frac{91}{18} \quad \frac{91}{12} \quad \frac{78}{5} \quad \frac{76}{9} \quad \frac{74}{19} \quad \frac{79}{24} \quad \frac{97}{32} \quad \frac{109}{50} \quad \frac{88}{50}$$

$$\frac{64}{50} \quad \frac{64}{29} \quad \frac{70}{15} \quad \frac{73}{5} \quad \frac{71}{7} \quad \frac{70}{19} \quad \frac{76}{24} \quad \frac{83}{31} \quad \frac{87}{50} \quad \frac{70}{50}$$

$$\frac{56}{50} \quad \frac{54}{25} \quad \frac{60}{15} \quad \frac{63}{10} \quad \frac{69}{5} \quad \frac{67}{10} \quad \frac{69}{10} \quad \frac{68}{28} \quad \frac{64}{39} \quad \frac{65}{50}$$

x

$$\frac{59}{50} \quad \frac{50}{30} \quad \frac{51}{10} \quad \frac{62}{5} \quad \frac{60}{10} \quad \frac{59}{10} \quad \frac{59}{20} \quad \frac{52}{27} \quad \frac{48}{36} \quad \frac{43}{50}$$

$$\frac{79}{50} \quad \frac{74}{31} \quad \frac{64}{14} \quad \frac{60}{9} \quad \frac{56}{10} \quad \frac{56}{17} \quad \frac{54}{28} \quad \frac{37}{37} \quad \frac{28}{50} \quad \frac{18}{50}$$

$$\text{Low Price } \frac{104}{50} \quad \frac{81}{22} \quad \frac{65}{9} \quad \frac{56}{6} \quad \frac{53}{10} \quad \frac{52}{18} \quad \frac{52}{28} \quad \frac{32}{38} \quad \frac{20}{50} \quad \frac{06}{50}$$

Sta.	+	π	-	Elev.	
		940.60.			
41				35.0	
	+50			34.9	
42				34.4	
B.M.			2.68	937.92	(937.93)
	+50			32.9	
	+69	BECK RT.		32.0	
43				30.4	
T.P.	2.37	932.80.	10.17	930.43	
	+50			27.7	
44				24.9	
	+50			22.5	
45				19.9	
T.P.	2.73	922.61.	12.92	919.88	
	+50			17.5	

Lt.

E

Lt.

$$\frac{106}{30} \frac{78}{30} \frac{79}{11} \frac{57}{7}$$

$$\frac{56}{10} \frac{52}{10} \frac{51}{23} \frac{32}{30} \frac{08}{50}$$

$$\frac{106}{30} \frac{85}{17} \frac{72}{8} \frac{61}{5} \frac{57}{7}$$

$$\frac{53}{10}$$

$$\frac{55}{22} \frac{33}{30} \frac{11}{50}$$

$$\frac{102}{30} \frac{80}{17} \frac{69}{8} \frac{64}{5}$$

$$\frac{42}{11} \frac{60}{20} \frac{64}{25} \frac{62}{31} \frac{20}{50}$$

$$\frac{96}{30} \frac{84}{30} \frac{87}{14} \frac{82}{7} \frac{77}{7} \frac{74}{6} \frac{74}{18} \frac{67}{25} \frac{38}{31} \frac{26}{50}$$

$$\frac{86}{17} \frac{81}{30} \frac{70}{50}$$

$$\frac{100}{30} \frac{91}{32} \frac{108}{14} \frac{105}{7} \frac{102}{9} \frac{99}{18} \frac{105}{22} \frac{60}{35} \frac{55}{50}$$

$$\frac{42}{30} \frac{35}{32} \frac{50}{21} \frac{59}{18} \frac{59}{9} \frac{51}{8} \frac{50}{18} \frac{57}{25} \frac{52}{31} \frac{34}{36} \frac{11}{50} \frac{06}{50}$$

$$\frac{82}{30} \frac{76}{33} \frac{88}{18} \frac{83}{7}$$

$$\frac{79}{9} \frac{75}{20} \frac{80}{29} \frac{76}{36} \frac{66}{50} \frac{67}{50}$$

$$\frac{130}{30} \frac{131}{26} \frac{125}{11} \frac{105}{5} \frac{103}{10} \frac{98}{22} \frac{106}{27} \frac{119}{35} \frac{119}{50} \frac{124}{50}$$

$$\frac{165}{30} \frac{168}{28} \frac{165}{12} \frac{132}{7} \frac{129}{10} \frac{125}{21} \frac{132}{27} \frac{165}{39} \frac{160}{50} \frac{158}{50}$$

$$\frac{77}{30} \frac{77}{20} \frac{71}{11} \frac{58}{5} \frac{51}{10} \frac{42}{20} \frac{48}{25} \frac{79}{50} \frac{74}{50}$$

X

540

+

才

—

E/CV.

722.61.

46

16.0

#32 Flow line Culvert.

+50

16.5

47

17.2

T.P.

10.85

930.43.

203

919.58

+50

18.2

48

19.3

+50

20.3

49

21.1

450

21.8

50

22.8

450

23.8

Lt.

d.

Rt.

$$\frac{79}{50} \quad \frac{79}{9} \quad \frac{72}{5}$$

$$\frac{46}{12} \quad \frac{50}{23} \quad \frac{58}{27} \quad \frac{73}{29} \quad \frac{86}{39} \quad \frac{93}{50}$$

9.210.2

$$\frac{76}{50} \quad \frac{77}{29} \quad \frac{71}{19} \quad \frac{66}{7} \quad \frac{61}{10} \quad \frac{56}{13} \quad \frac{57}{23} \quad \frac{77}{30} \quad \frac{82}{50} \quad \frac{89}{50}$$

$$\frac{55}{50} \quad \frac{58}{16} \quad \frac{57}{10}$$

$$\frac{59}{13} \quad \frac{57}{18} \quad \frac{73}{22} \quad \frac{82}{50} \quad \frac{103}{50}$$

$$\frac{104}{50} \quad \frac{111}{22} \quad \frac{121}{13} \quad \frac{122}{11} \quad \frac{127}{16} \quad \frac{129}{24} \quad \frac{148}{44} \quad \frac{150}{50} \quad \frac{168}{50}$$

$$\frac{80}{50} \quad \frac{84}{32} \quad \frac{96}{20} \quad \frac{112}{15}$$

$$\frac{111}{14} \quad \frac{112}{26} \quad \frac{140}{50} \quad \frac{171}{50}$$

$$\frac{63}{50} \quad \frac{82}{25} \quad \frac{90}{21} \quad \frac{98}{14} \quad \frac{100}{10} \quad \frac{101}{7} \quad \frac{106}{12} \quad \frac{116}{22} \quad \frac{139}{22} \quad \frac{179}{50}$$

$$\frac{44}{50} \quad \frac{54}{36} \quad \frac{68}{24} \quad \frac{77}{22} \quad \frac{90}{14}$$

$$\frac{93}{8} \quad \frac{100}{14} \quad \frac{131}{33} \quad \frac{160}{50} \quad \frac{183}{50}$$

$$\frac{28}{50} \quad \frac{58}{25} \quad \frac{83}{11} \quad \frac{86}{9} \quad \frac{96}{18} \quad \frac{133}{32} \quad \frac{148}{50}$$

$$\frac{16}{50} \quad \frac{28}{32} \quad \frac{42}{19} \quad \frac{76}{12}$$

$$\frac{76}{9} \quad \frac{83}{14} \quad \frac{117}{29} \quad \frac{148}{50} \quad \frac{179}{50}$$

$$\frac{10}{50} \quad \frac{18}{35} \quad \frac{27}{22} \quad \frac{69}{12} \quad \frac{66}{9} \quad \frac{74}{16} \quad \frac{115}{21} \quad \frac{128}{34} \quad \frac{146}{50} \quad \frac{183}{50}$$

X

Sta	+	A	-	E/cv.
		930.43.		
51				23.9
	+50			23.1
T.P.	5.35	927.01.	8.77	921.66
52				21.8
	+50			20.1
53				18.2
	+23			17.7
T.P.	3.89	921.94.	9.46	917.55
	+50			17.2
54				16.6
	+09	flow line Culvert.		
	+50			16.3
55				16.2

17.

4.

21.

$$\frac{29}{50} \frac{35}{31} \frac{40}{20} \quad \frac{60}{19} \frac{67}{9} \quad \frac{65}{12} \frac{72}{18} \frac{110}{18} \quad \frac{132}{33} \frac{180}{50}$$

$$\frac{39}{50} \quad \frac{55}{26} \quad \frac{77}{17} \quad \frac{75}{11} \quad \frac{73}{1}$$

$$\frac{81}{12} \frac{105}{13} \frac{140}{34} \frac{173}{50}$$

$$\frac{46}{50} \frac{19}{35} \frac{30}{27} \quad \frac{56}{20} \frac{50}{13} \quad \frac{52}{9} \quad \frac{60}{18} \frac{78}{35} \frac{92}{50}$$

$$\frac{10}{50} \quad \frac{15}{35} \quad \frac{64}{28} \quad \frac{64}{9} \quad \frac{69}{1} \quad \frac{78}{9} \quad \frac{91}{15} \frac{139}{32} \frac{151}{50}$$

$$\frac{07}{50} \frac{16}{37} \frac{63}{29} \frac{83}{21} \quad \frac{85}{15} \frac{83}{8} \quad \frac{88}{12} \frac{92}{22} \frac{140}{50} \quad \frac{158}{50}$$

$$\frac{05}{50} \quad \frac{46}{34}$$

$$\frac{73}{23} \frac{92}{11} \frac{93}{1}$$

$$\frac{102}{11} \frac{136}{20} \frac{153}{32} \frac{155}{50}$$

$$\frac{106}{50} \quad \frac{93}{31} \frac{46}{18} \quad \frac{42}{10} \frac{48}{13} \frac{63}{21} \frac{90}{34} \frac{95}{50} \frac{100}{50}$$

$$\frac{46}{50} \frac{61}{32} \quad \frac{57}{16} \quad \frac{50}{13}$$

$$\frac{48}{11} \frac{52}{14} \frac{67}{18} \frac{82}{25} \frac{87}{50} \frac{99}{50}$$

7.48.95

$$\frac{58}{50} \frac{67}{30} \frac{66}{17} \frac{64}{14} \frac{51}{1}$$

$$\frac{57}{12} \frac{83}{19} \frac{96}{31} \frac{100}{50}$$

$$\frac{61}{50} \frac{66}{33} \frac{63}{15} \quad \frac{54}{13}$$

$$\frac{52}{12} \frac{57}{20} \frac{90}{50} \frac{103}{50}$$

Sta. + T - Elev

921.49.

55 +50

16.3

B.M.

584

915.60

915.58

56

16.4

+50

16.7

57

17.4

+50

18.5

58

19.9

#

X

T.P.

1

17.59

927.07.

1.91

919.53

+50

21.4

59

23.5

+07 Bottom End

23.9

+21

"

24.0

+35

24.3

130.9
7.5
17.5

Lt

L

Rt

$\frac{5.7}{50} \frac{6.6}{25} \frac{6.4}{15} \frac{5.5}{18} \frac{5.1}{11} \quad \frac{5.7}{12} \quad \frac{9.0}{19} \frac{9.8}{33} \frac{10.3}{50}$

Spk. in 42° E/m 80' Lt. 55' 6.5

$\frac{5.1}{50} \frac{6.8}{32} \frac{6.3}{16} \frac{5.2}{13} \frac{5.0}{11} \frac{5.5}{18} \frac{8.7}{33} \frac{10.1}{33} \frac{10.7}{50}$

$\frac{4.8}{50} \frac{5.7}{38} \frac{6.3}{17} \frac{4.8}{13} \frac{4.7}{11} \quad \frac{5.2}{13} \frac{8.9}{20} \frac{10.1}{30} \frac{10.8}{50}$

$\frac{3.4}{50} \frac{4.5}{32} \frac{7.2}{18} \quad \frac{4.2}{13} \quad \frac{4.0}{12} \frac{4.6}{19} \frac{8.3}{30} \frac{9.6}{30} \frac{10.6}{50}$

$\frac{2.6}{50} \frac{5.9}{26} \frac{6.2}{20} \frac{3.2}{13} \frac{2.9}{11} \quad \frac{3.6}{11} \quad \frac{7.6}{17} \frac{9.3}{23} \frac{10.1}{32} \frac{10.5}{50}$

$\frac{1.5}{50} \frac{4.6}{29} \frac{5.0}{24} \frac{1.8}{16} \quad \frac{1.5}{13} \frac{2.3}{13} \frac{8.1}{23} \frac{9.6}{38} \frac{10.6}{50}$

X

Near in 00° Lt.

$\frac{10.7}{50} \frac{11.5}{41} \frac{13.5}{25} \frac{15.9}{20} \frac{15.6}{17} \frac{15.7}{10} \frac{15.7}{9} \frac{15.9}{14} \frac{15.9}{14}$

$\frac{4.5}{50} \frac{6.5}{33} \frac{9.0}{28} \frac{13.7}{21} \frac{13.0}{16} \quad \frac{13.3}{12} \quad \frac{13.6}{12} \frac{14.1}{7} \frac{13.6}{12}$

$\frac{9.4}{50} \frac{10.8}{38} \frac{13.1}{13} \frac{13.2}{11}$

$\frac{9.4}{50} \frac{10.4}{38} \frac{12.7}{16} \frac{13.1}{30}$

$\frac{3.8}{50} \frac{4.6}{37} \frac{6.0}{31} \frac{7.3}{20} \frac{12.3}{14} \frac{12.8}{5} \frac{13.1}{8} \frac{7.2}{8} \frac{12.2}{16}$

Sta	+	X	-	Elev.
		93707.		
59	+60			25.0
60				25.5
	+50			25.9
61				25.4
T.P.	^H 2	0.48	926.61	10.94 926.13
	+50			24.4
62				23.4
	+25			22.9
	+64			22.3
	+92	Flow Line Culvert.		
63				21.9
	+38			21.8

Lt

A

Rt

$$\frac{16}{50} \frac{27}{39} \frac{39}{31} \frac{118}{20} \quad \frac{118}{14} \quad \frac{121}{4} \frac{126}{9} \frac{104}{11} \frac{110}{11}$$

$$\frac{13}{30} \frac{21}{37} \frac{28}{31} \frac{110}{20} \quad \frac{114}{16} \frac{111}{8} \quad \frac{116}{16}$$

$$\frac{119}{6} \frac{101}{10}$$

$$\frac{20}{30} \frac{29}{37} \frac{42}{30} \frac{110}{21} \quad \frac{110}{16} \frac{107}{7} \quad \frac{112}{3} \frac{115}{9} \frac{97}{14} \frac{122}{14}$$

$$\frac{60}{50} \frac{61}{32} \frac{101}{27} \frac{119}{23} \frac{113}{20} \quad \frac{113}{15} \frac{112}{8} \quad \frac{117}{5} \quad \frac{122}{10} \frac{111}{10} \frac{126}{14}$$

Nail in Top Ft. Rock

$$\frac{120}{30} \frac{125}{40} \frac{09}{30} \frac{15}{20} \quad \frac{18}{16} \frac{16}{7} \quad \frac{22}{5} \frac{25}{8} \frac{48}{29} \frac{133}{26} \frac{148}{30} \frac{158}{30}$$

$$\frac{125}{50} \frac{115}{38} \frac{111}{32} \frac{23}{27} \frac{25}{21} \frac{39}{16} \quad \frac{26}{7} \quad \frac{32}{7} \frac{34}{7} \frac{44}{9} \frac{135}{24} \frac{153}{30} \frac{164}{30}$$

$$\frac{105}{50} \frac{07}{32} \frac{34}{28} \frac{32}{22} \frac{35}{15} \frac{32}{7} \quad \frac{37}{6} \frac{40}{9} \frac{57}{22} \frac{130}{22} \frac{157}{29} \frac{164}{30}$$

$$\frac{42}{50} \frac{51}{35} \frac{57}{26} \frac{40}{21} \quad \frac{41}{16} \quad \frac{39}{6} \quad \frac{43}{7} \frac{49}{7} \frac{77}{12} \frac{142}{23} \frac{155}{30} \frac{161}{30}$$

820940

$$\frac{54}{50} \frac{52}{35} \frac{65}{23} \frac{48}{20} \quad \frac{45}{16} \frac{43}{7} \quad \frac{47}{6} \frac{51}{12} \frac{89}{18} \frac{128}{26} \frac{142}{40} \frac{159}{50} \frac{159}{50}$$

$$\frac{46}{50} \frac{48}{36} \frac{55}{22} \frac{49}{19} \quad \frac{44}{5} \quad \frac{48}{7} \frac{56}{18} \frac{134}{25} \frac{154}{25} \frac{168}{50}$$

Sta.	+	π	-	Elev	
		926.61.			
63	+65			21.9	
64				22.0	
	+40			21.6	
	+80			21.3	
65				21.0	
T.P.	#3		5.52	921.09	
T.P.	5.97	925.50.			919.53
58	+50			21.4	
59				23.5	
	+35			24.3	
	+60			25.0	
T.P.	9.07	926.59.	7.98	917.52	
60				25.5	
	+50			25.9	

Lt

A

Rt

$$\frac{0.8}{50} \quad \frac{0.6}{44} \quad \frac{0.9}{29} \quad \frac{5.4}{22} \quad \frac{5.4}{22} \quad \frac{4.8}{19} \quad \frac{4.4}{6} \quad \frac{4.7}{6} \quad \frac{5.4}{6} \quad \frac{12.4}{17} \quad \frac{15.3}{25} \quad \frac{16.5}{50}$$

$$\frac{12.4}{50} \quad \frac{11.7}{35} \quad \frac{11.0}{26} \quad \frac{4.7}{21} \quad \frac{4.4}{13} \quad \frac{4.3}{5} \quad \frac{4.6}{8} \quad \frac{5.5}{11} \quad \frac{4.9}{22} \quad \frac{12.7}{27} \quad \frac{15.2}{31} \quad \frac{14.2}{50}$$

$$\frac{11.0}{50} \quad \frac{10.4}{35} \quad \frac{0.0}{26} \quad \frac{6.1}{20} \quad \frac{5.4}{17} \quad \frac{4.8}{13} \quad \frac{4.7}{5} \quad \frac{5.0}{9} \quad \frac{6.0}{13} \quad \frac{5.7}{17} \quad \frac{6.6}{33} \quad \frac{15.0}{50}$$

$$\frac{4.8}{50} \quad \frac{4.2}{34} \quad \frac{4.1}{21} \quad \frac{5.6}{19} \quad \frac{5.3}{13} \quad \frac{5.1}{4} \quad \frac{5.3}{8} \quad \frac{6.2}{12} \quad \frac{6.5}{16} \quad \frac{6.0}{21} \quad \frac{7.0}{33} \quad \frac{14.0}{50}$$

$$\frac{6.0}{50} \quad \frac{5.5}{32} \quad \frac{5.2}{21} \quad \frac{6.0}{12} \quad \frac{5.6}{16} \quad \frac{6.6}{20} \quad \frac{6.9}{35} \quad \frac{14.0}{50}$$

to sta 65100

from I.R. #1

$$(4.1) \quad \frac{7.6}{23} \quad \frac{12.0}{33} \quad \frac{14.0}{42} \quad \frac{14.4}{50}$$

$$(2.0) \quad \frac{7.6}{24} \quad \frac{10.6}{32} \quad \frac{11.3}{43} \quad \frac{13.8}{50}$$

$$(1.2) \quad \frac{7.6}{26} \quad \frac{11.5}{33} \quad \frac{13.4}{50}$$

$$(0.5) \quad \frac{7.7}{26} \quad \frac{10.7}{30} \quad \frac{13.7}{39} \quad \frac{14.8}{50}$$

$$(1.1) \quad \frac{8.7}{26} \quad \frac{13.3}{35} \quad \frac{15.8}{50}$$

$$(0.7) \quad \frac{8.1}{27} \quad \frac{14.0}{37} \quad \frac{15.8}{50}$$

Sta	+	π	-	Elev.
		926.59.		
61				(25.4)
T.P.			0.47	926.12 ^{at.} (926.12)
T.P.	2.15	923.24.		921.09
65	+50			20.3
66				19.1
	+50			18.5
67	+95	Flow Line Culvert		
67				18.2
	+50			18.2
68				18.2
B.M.			5.12	918.12
	+50			18.4
69				19.0
	+50			19.3

Lt.

L

Rt.

$$\textcircled{1.2} \quad \frac{82}{24} \quad \frac{124}{29} \quad \frac{151}{36} \quad \frac{161}{50}$$

front A #2

front TP #3

$$\frac{38}{50} \quad \frac{37}{32} \quad \frac{27}{19} \quad \frac{27}{14} \quad \frac{36}{11} \quad \frac{29}{11} \quad \frac{32}{14} \quad \frac{37}{21} \quad \frac{27}{31} \quad \frac{90}{41} \quad \frac{108}{41} \quad \frac{120}{50}$$

$$\frac{57}{50} \quad \frac{67}{32} \quad \frac{70}{20} \quad \frac{71}{11} \quad \frac{51}{7} \quad \frac{41}{9} \quad \frac{27}{18} \quad \frac{39}{24} \quad \frac{65}{36} \quad \frac{93}{36} \quad \frac{123}{50}$$

$$\frac{83}{50} \quad \frac{85}{26} \quad \frac{83}{14} \quad \frac{57}{10} \quad \frac{47}{8} \quad \frac{44}{8} \quad \frac{50}{18} \quad \frac{98}{29} \quad \frac{109}{36} \quad \frac{130}{50}$$

9.19.3

$$\frac{86}{50} \quad \frac{89}{34} \quad \frac{90}{16} \quad \frac{54}{11} \quad \frac{50}{16} \quad \frac{54}{23} \quad \frac{91}{35} \quad \frac{116}{35} \quad \frac{129}{50}$$

$$\frac{83}{50} \quad \frac{87}{40} \quad \frac{88}{27} \quad \frac{80}{16} \quad \frac{54}{12} \quad \frac{50}{16} \quad \frac{58}{16} \quad \frac{100}{23} \quad \frac{117}{32} \quad \frac{128}{50}$$

$$\frac{74}{50} \quad \frac{66}{36} \quad \frac{58}{20} \quad \frac{71}{14} \quad \frac{55}{10} \quad \frac{50}{8} \quad \frac{55}{14} \quad \frac{60}{20} \quad \frac{95}{32} \quad \frac{120}{32} \quad \frac{130}{50}$$

spike in 15" oak 35' 61/15

$$\frac{40}{50} \quad \frac{46}{34} \quad \frac{48}{22} \quad \frac{59}{20} \quad \frac{58}{13} \quad \frac{53}{11} \quad \frac{48}{9} \quad \frac{51}{13} \quad \frac{58}{16} \quad \frac{66}{22} \quad \frac{97}{35} \quad \frac{122}{35} \quad \frac{126}{50}$$

$$\frac{35}{50} \quad \frac{35}{35} \quad \frac{36}{23} \quad \frac{50}{19} \quad \frac{45}{9} \quad \frac{42}{11} \quad \frac{59}{11} \quad \frac{58}{16} \quad \frac{98}{26} \quad \frac{124}{40} \quad \frac{127}{50}$$

$$\frac{42}{50} \quad \frac{31}{33} \quad \frac{28}{18} \quad \frac{48}{14} \quad \frac{42}{10} \quad \frac{39}{11} \quad \frac{47}{16} \quad \frac{51}{26} \quad \frac{80}{36} \quad \frac{123}{36} \quad \frac{124}{50}$$

sta	+	π	-	Elev.
		923.24		
70		^x 921.95		19.4
T.P.	3.00	921.98	4.29	918.98
+50				19.0
71				18.1
+50				17.0
72				16.4
+50				16.4
73				16.5
+50				16.5
74				16.6
T.P.	10.87	927.89	4.96	917.02
+50				17.4
75				18.1

Lt

K

Rt

$$\frac{61}{50} \frac{49}{36} \frac{31}{23} \frac{22}{15} \frac{43}{11} \frac{40}{7} \frac{38}{7} \frac{44}{15} \frac{32}{17} \frac{36}{20} \frac{92}{29} \frac{118}{39} \frac{130}{50}$$

4

$$\frac{66}{50} \frac{58}{37} \frac{42}{20} \frac{29}{12} \frac{40}{9} \frac{35}{5} \frac{30}{6} \frac{29}{15} \frac{35}{19} \frac{26}{19} \frac{39}{24} \frac{104}{34} \frac{109}{50}$$

$$\frac{79}{50} \frac{70}{31} \frac{56}{16} \frac{48}{10} \frac{43}{5} \frac{37}{7} \frac{38}{19} \frac{48}{19} \frac{42}{21} \frac{38}{25} \frac{87}{32} \frac{110}{50}$$

$$\frac{70}{50} \frac{78}{23} \frac{75}{11} \frac{56}{6} \frac{50}{6} \frac{47}{7} \frac{34}{20} \frac{47}{22} \frac{80}{28} \frac{101}{37} \frac{112}{50}$$

$$\frac{88}{50} \frac{89}{35} \frac{90}{17} \frac{20}{11} \frac{63}{6} \frac{56}{7} \frac{59}{18} \frac{59}{23} \frac{89}{32} \frac{99}{50} \frac{112}{50}$$

$$\frac{90}{50} \frac{88}{30} \left(\frac{101}{C4V} \right) \frac{93}{12} \frac{60}{7} \frac{56}{5} \frac{56}{5} \frac{65}{16} \frac{83}{19} \left(\frac{107}{C4V} \right) \frac{99}{22} \frac{106}{35} \frac{109}{50}$$

$$\frac{89}{50} \frac{89}{34} \frac{92}{14} \frac{77}{13} \frac{60}{7} \frac{55}{13} \frac{63}{20} \frac{67}{25} \frac{80}{34} \frac{99}{50} \frac{110}{50}$$

$$\frac{82}{50} \frac{81}{34} \frac{84}{20} \frac{68}{15} \frac{57}{9} \frac{55}{9} \frac{65}{11} \frac{68}{15} \frac{64}{17} \frac{97}{29} \frac{110}{35} \frac{118}{50}$$

$$\frac{61}{50} \frac{60}{32} \frac{63}{21} \frac{57}{15}$$

$$\frac{54}{10} \frac{60}{15} \frac{61}{22} \frac{102}{36} \frac{110}{50} \frac{118}{50}$$

N91/10 TR Rt.

$$\frac{112}{50} \frac{108}{25} \frac{114}{17} \frac{108}{10} \frac{106}{8} \frac{114}{14} \frac{118}{24} \frac{150}{37} \frac{168}{50} \frac{178}{50}$$

$$\frac{102}{50} \frac{102}{32} \frac{103}{23} \frac{105}{16} \frac{99}{9} \frac{98}{10} \frac{105}{15} \frac{107}{27} \frac{150}{50} \frac{178}{50}$$

Sta	+	π	-	Elev
		927.89		
75	+50			19.0
76				20.0
	+50			21.1
77				22.3
	+50			23.5
I.P.	5.42	929.74	257	924.32
78				24.3
	+50			25.0
79				25.4
	+50			25.2
80				24.6
	+25			24.3

3/10/39

39

K.A.

L.B.H.

L.G.

M.D.G.

R.T.

L.L.

E.

$$\frac{52}{50} \frac{74}{22} \frac{98}{15} \frac{92}{8} \frac{89}{1} \quad \frac{94}{9} \frac{104}{15} \frac{132}{24} \frac{160}{35} \frac{167}{50}$$

$$\frac{56}{50} \frac{69}{35} \frac{85}{19} \frac{87}{14} \quad \frac{81}{6} \quad \frac{79}{1} \frac{83}{9} \frac{86}{14} \frac{106}{19} \frac{141}{29} \frac{158}{40} \frac{166}{20}$$

$$\frac{55}{50} \frac{63}{33} \frac{73}{19} \frac{75}{12} \frac{71}{5} \frac{68}{6} \quad \frac{70}{10} \quad \frac{75}{16} \frac{128}{31} \frac{164}{42} \frac{171}{50}$$

$$\frac{33}{50} \frac{44}{32} \frac{47}{21} \frac{57}{13} \quad \frac{59}{7} \quad \frac{56}{1} \frac{61}{12} \frac{64}{16} \frac{79}{24} \frac{136}{40} \frac{166}{50}$$

X

$$\frac{153}{50} \frac{25}{31} \frac{59}{22} \frac{48}{18} \frac{53}{14} \quad \frac{44}{1} \frac{48}{7} \frac{48}{12} \frac{23}{18} \frac{12}{30} \frac{04}{50}$$

$$\frac{15}{50} \frac{24}{33} \frac{32}{19} \frac{64}{17} \frac{59}{11} \frac{54}{1} \frac{62}{9} \frac{62}{12} \frac{55}{15} \frac{58}{19} \frac{78}{27} \frac{130}{40} \frac{168}{50}$$

$$\frac{07}{50} \frac{14}{33} \frac{33}{18} \frac{52}{15} \quad \frac{49}{10} \quad \frac{47}{1} \frac{58}{9} \frac{60}{14} \frac{96}{21} \frac{111}{27} \frac{122}{37} \frac{167}{50}$$

$$\frac{110}{50} \frac{117}{37} \frac{115}{21} \frac{102}{26} \frac{05}{20} \frac{50}{14} \frac{43}{1} \quad \frac{50}{12} \frac{77}{18} \frac{78}{27} \frac{151}{39} \frac{166}{50}$$

$$\frac{104}{50} \frac{20}{36} \frac{28}{25} \frac{42}{18} \quad \frac{43}{14} \quad \frac{45}{10} \frac{53}{16} \frac{77}{16} \frac{109}{29} \frac{147}{39} \frac{170}{50}$$

$$\frac{110}{50} \frac{104}{42} \frac{12}{28} \frac{28}{21} \frac{49}{18} \frac{49}{11} \frac{51}{11} \frac{58}{21} \frac{93}{21} \frac{123}{33} \frac{160}{40} \frac{172}{50}$$

$$\frac{06}{50} \frac{16}{37} \frac{31}{19} \frac{48}{16} \frac{52}{9} \quad \frac{54}{1} \frac{61}{12} \frac{61}{14} \frac{86}{19} \frac{100}{26} \frac{162}{43} \frac{183}{50}$$

Sta.	+	π	-	Elev
		929.74.		
80	+50			24.2
	+54	Flow Line Culvert Rht.		
	+75			24.4
	+83	Flow Line Culvert Lft.		
81				25.4
	+30.09			27.6
B.M.			12.20	917.54 917.48

Lt.

h.

Rt.

$$\frac{26}{50} \frac{45}{33} \frac{47}{16} \frac{51}{11} \frac{56}{5} \frac{55}{5} \quad \frac{54}{7} \frac{59}{17} \frac{66}{23} \frac{99}{33} \frac{125}{50}$$

10.15

$$\frac{23}{50} \frac{44}{38} \frac{60}{24} \frac{62}{12} \frac{61}{7} \quad \frac{53}{15} \frac{52}{27} \frac{58}{27} \frac{70}{50}$$

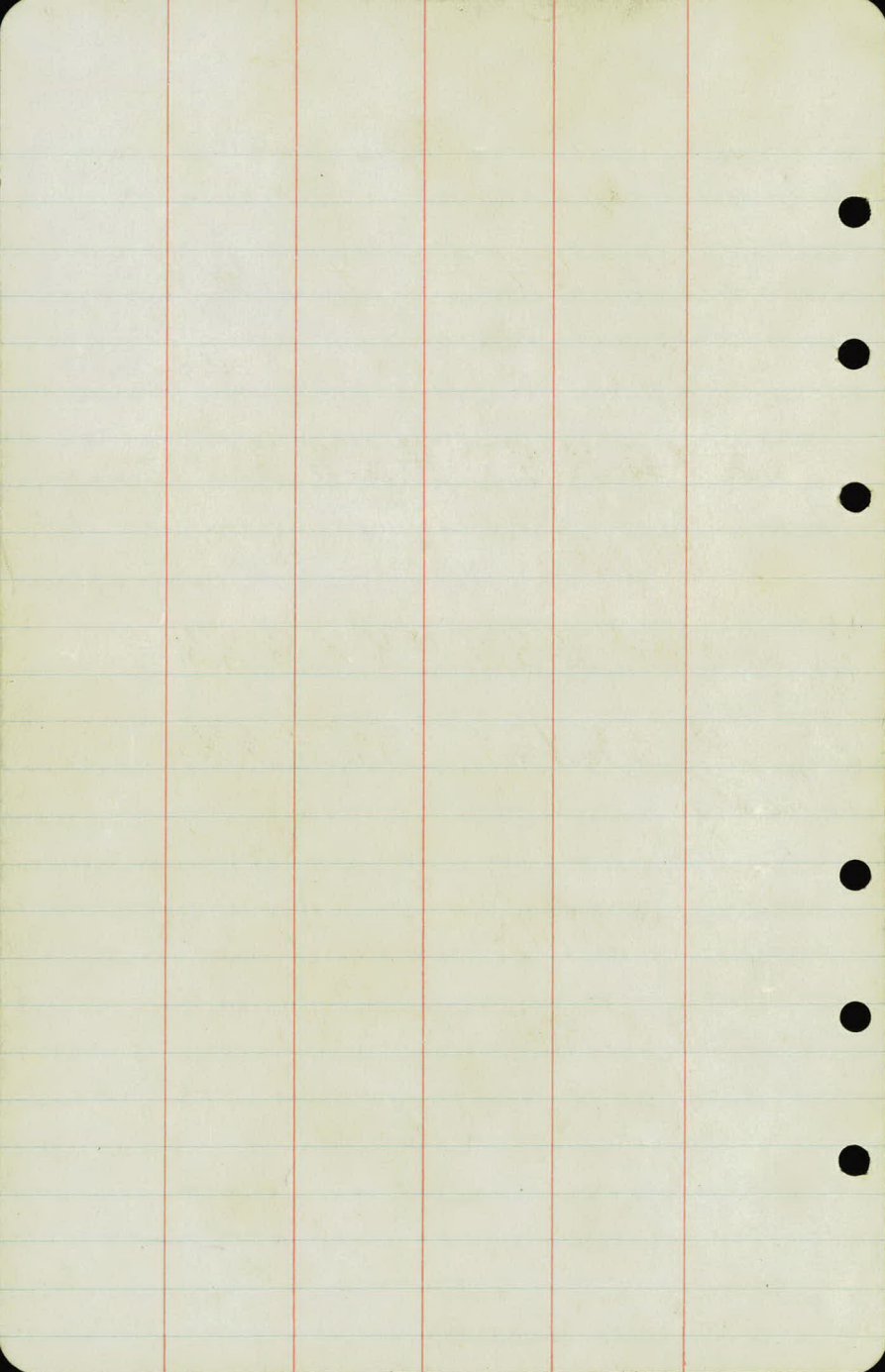
6.95

$$\frac{28}{50} \frac{57}{25} \frac{57}{13} \frac{47}{7} \frac{43}{10} \frac{43}{10} \frac{47}{18} \frac{76}{25} \frac{80}{34} \frac{72}{41} \frac{66}{50}$$

$$\frac{19}{50} \frac{29}{44} \frac{35}{32} \frac{41}{19} \frac{29}{14} \frac{25}{7} \quad \frac{21}{14} \frac{28}{18} \frac{59}{24} \frac{65}{37} \frac{58}{30} \frac{53}{50}$$

(917.61) N. Co. Line Rd

Tap M.G. Morst.



"A" LINE

Alignment

Sta Point ΔL ΔR

+93.96 P.T. 6°08'

+50 5°15.3'

63 4°15.3' $\Delta 12°16'$ R.T.

+50 3°15.3' D- 4°

+41.25 P.I. T- 153.96'

62 2°15.3' L- 306.67'

+50 1°15.3' R- 1432.69'

61 0°15.3'

60 +87.29 P.C. 0°00'

+72.66 P.T. 4°44.5'

+50 4°17.3' $\Delta 9°29'$ L.T.

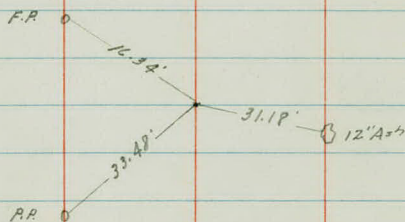
60 3°17.3' D- 4°

+54.43 P.I. T- 118.85'

+50 2°17.3' L- 237.08'

59 1°17.3' R- 1432.69'

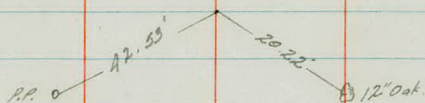
58 +35.58 P.G. 0°00'



$$A = 1432.41$$

14.63

$$A = 1432.37$$



Sta	Point	ΔL	ΔR
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$+06.95$ $+06.82 =$	Equa. P.T.		
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23'07"

67

22°22'

Δ 40'14" L

+50

16°52'

D- 22'

+08.53 P.I.

T- 111.86

66

11°22'

L- 210.15'

+50

5°52'

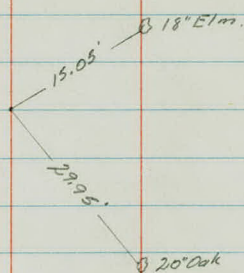
R- 242.04'

65

0°22'

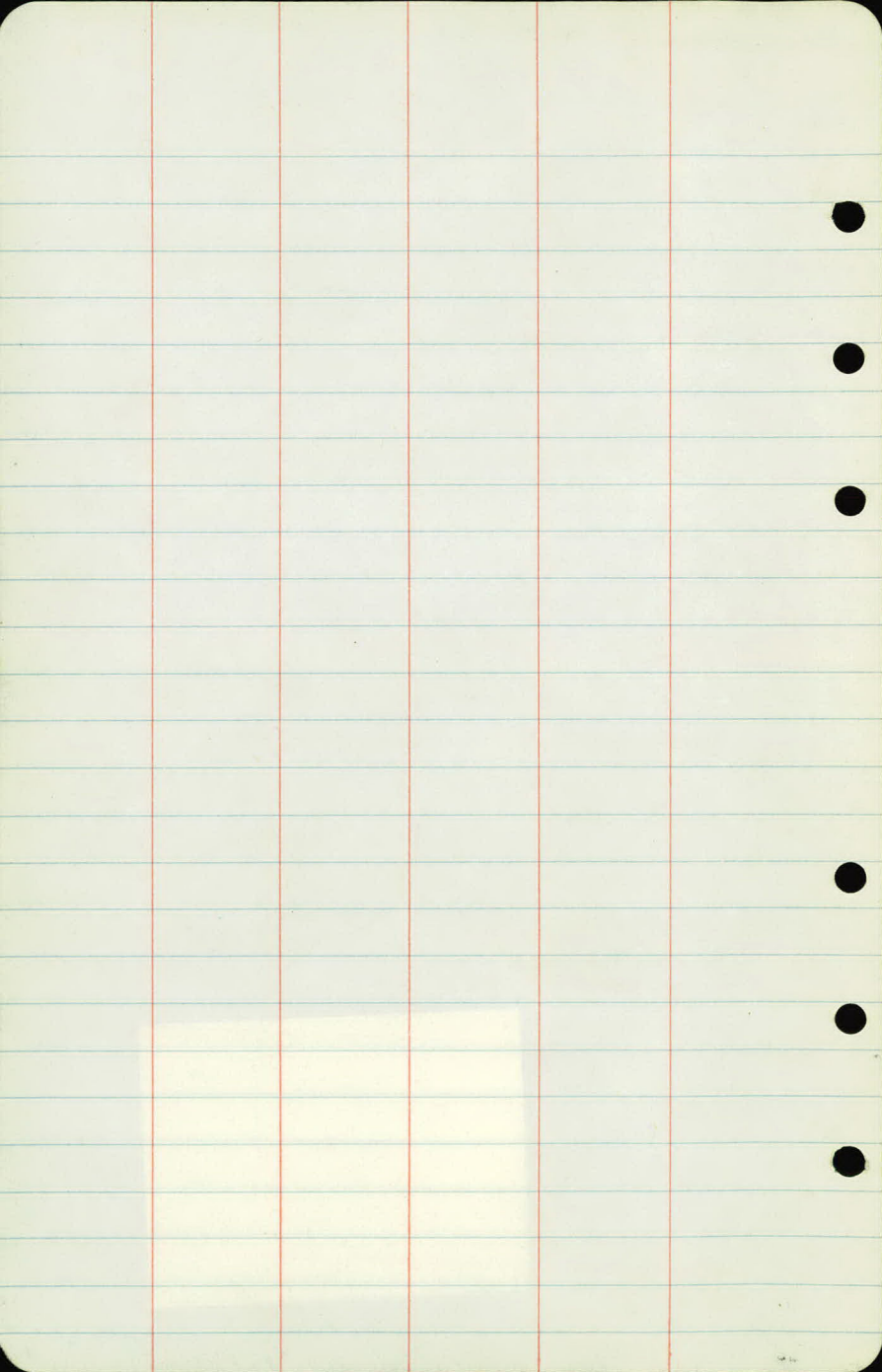
64 +96.67 P.C.

0°00'



$$A = 260.43$$

102.71



67 40 0.066 +50 0.666 1.0' $25 + 50 \quad 1.3$ 65' 1.664 3.1"

+50 4.8'

63 42

+50	4.0
-----	-----

62	3.5
----	-----

+50 2.6

61 1.3

+50	0.2
-----	-----

60	0.9
----	-----

150	0.7
-----	-----

59 0.4

"A" Line

-Base Line

