

Bk. 51 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

-----Plan-----Survey

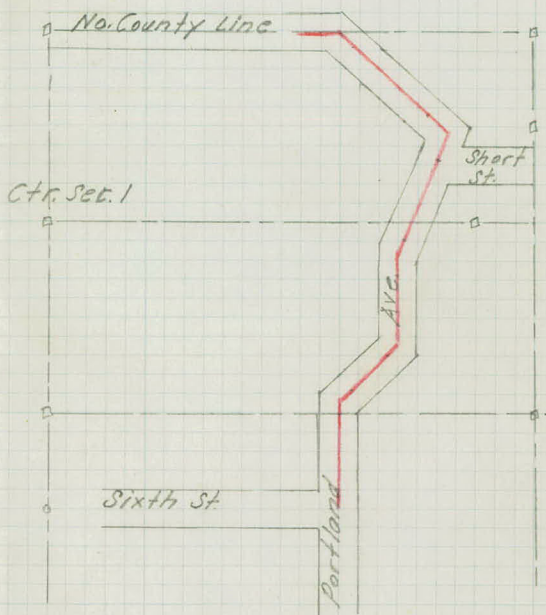
-----Portland Ave-----

From Sixth Str To No Co. Line

Road Acc't. No. 19

Date Filed 6-11-41 File-----

Sixth St. to No. County Line

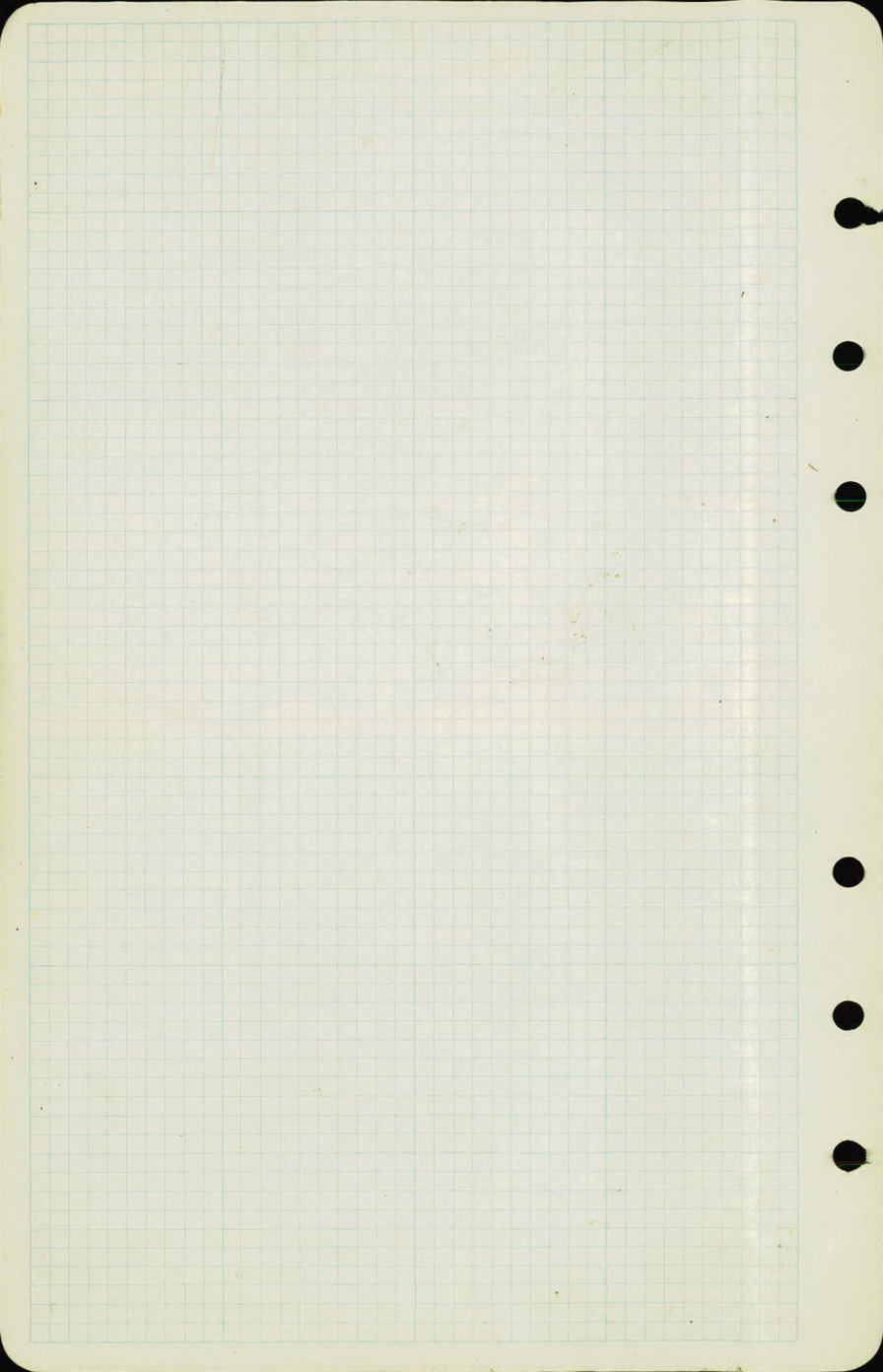


INDEX.

Align - 1-5

Topog. - 6-17

X524,16ms - 18-36



Alignment

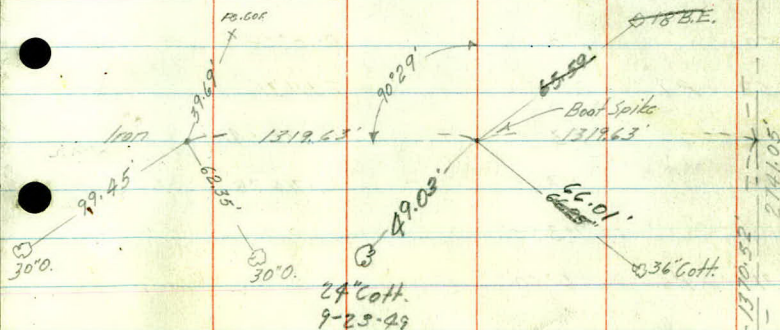
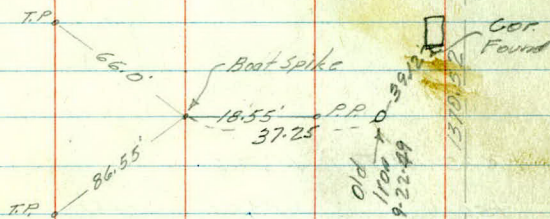
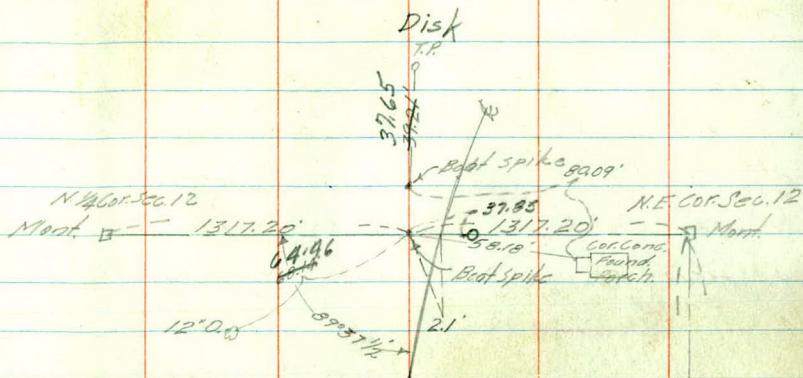
Sta	Point	Alt	Δ Lt
+14.12	P.T.		12°42.3'
15			11°43' Δ-25°25'
+50			8°13' D-14°-
14 +25.15	P.I.		² 25°25' T-92.52
13 +73.74	P.O.S.T.		2°52' L-181.49'
14			4°43' C-410.28'
+50			1°13'
13 +32.63	P.G.		0°00'

10 +23.62' P.O.T. = E Taylor Ave.

0 +00 = E Sixth St

11-4-40
K.A.
L.C.
M.B.
C.H.

2



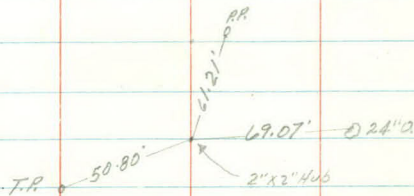
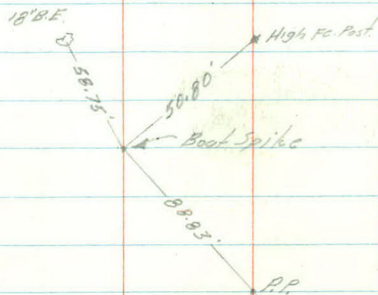
E. 1/4 Cor. Sec. 12

North

Sta	Point	ΔL	ΔR
+64.13	P.T.		5°10.5'
+50			4°53.5'
35			3°53.5' Δ -10°21'
+50			2°53.5' D-4°-
34	+35.12 P.I.		10°21' T-129.74'
34			1°53.5' L-258.75'
+50			0°53.5' R-1432.69'
33	+45.38 P.C.		0°00'
+96.25	P.T.	13°26.5'	
+50		11°35.5'	
24		9°35.5'	Δ -26°53'
+50		7°35.5'	D. 0°-
23	+31.52 P.I.	26°53'	T. 171.31'
23		5°35.5'	L. 336.04'
+50		3°35.5'	R. 716.78'
22		1°35.5'	
21	+60.21 P.C.	0°00'	

11-6-40

3



Sta	Point	ΔLt	ΔRt
-----	-------	-------------	-------------

53	+57.44	P.O.T. = R. Short St	
----	--------	----------------------	--

49	+00	P.I. = Beg. Line Change $1^{\circ}15'$	
----	-----	--	--

	+09.82	P.T.	$6^{\circ}20.5'$
--	--------	------	------------------

Sec. Line

	X ^s R.	P.O.S.T.	
--	-------------------	----------	--

41			$6^{\circ}08.7'$
----	--	--	------------------

	+50		$5^{\circ}08.7'$ $\Delta - 12^{\circ}41'$
--	-----	--	---

40			$4^{\circ}08.7'$ $P - 4^{\circ} -$
----	--	--	------------------------------------

39	+51.97	P.I.	$12^{\circ}41'$ $T - 159.23'$
----	--------	------	-------------------------------

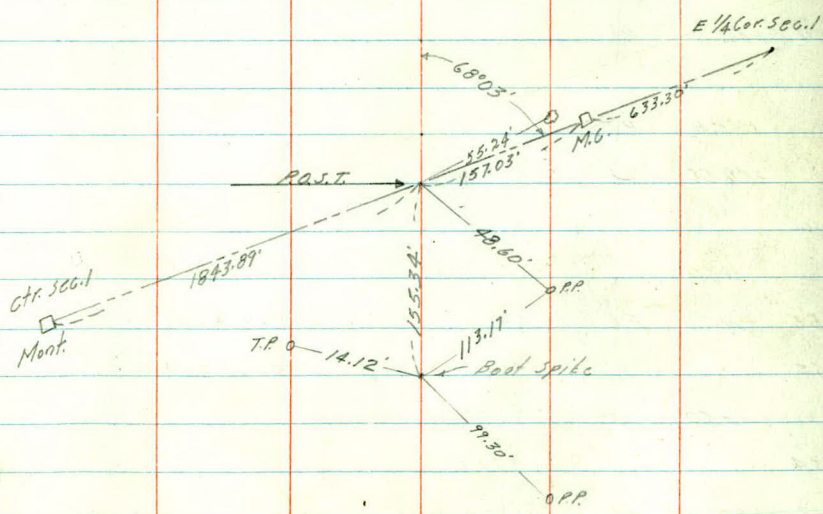
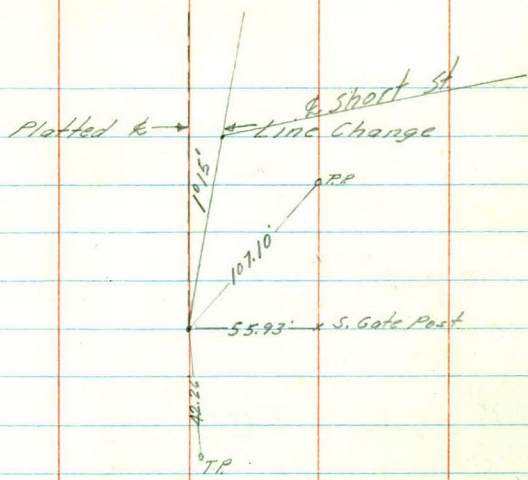
	+50		$3^{\circ}08.7'$ $L - 317.09'$
--	-----	--	--------------------------------

39			$2^{\circ}08.7'$ $R - 1432.69'$
----	--	--	---------------------------------

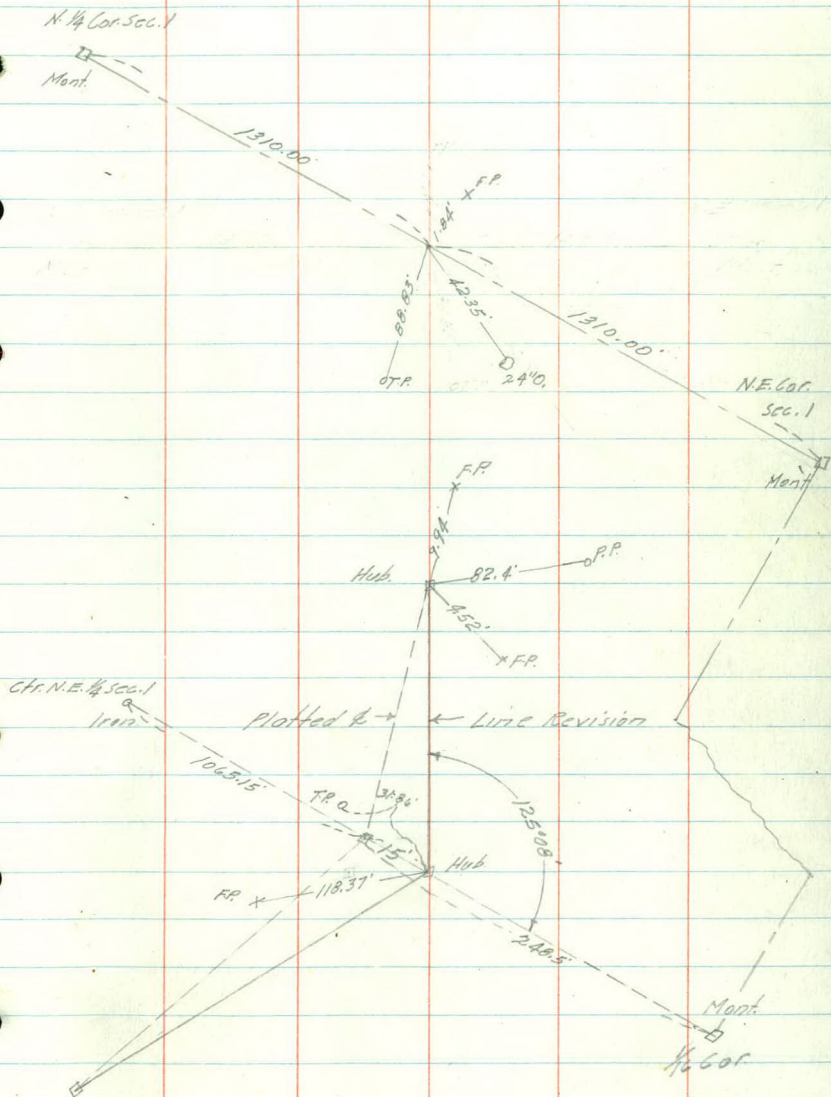
	+50		$1^{\circ}08.7'$
--	-----	--	------------------

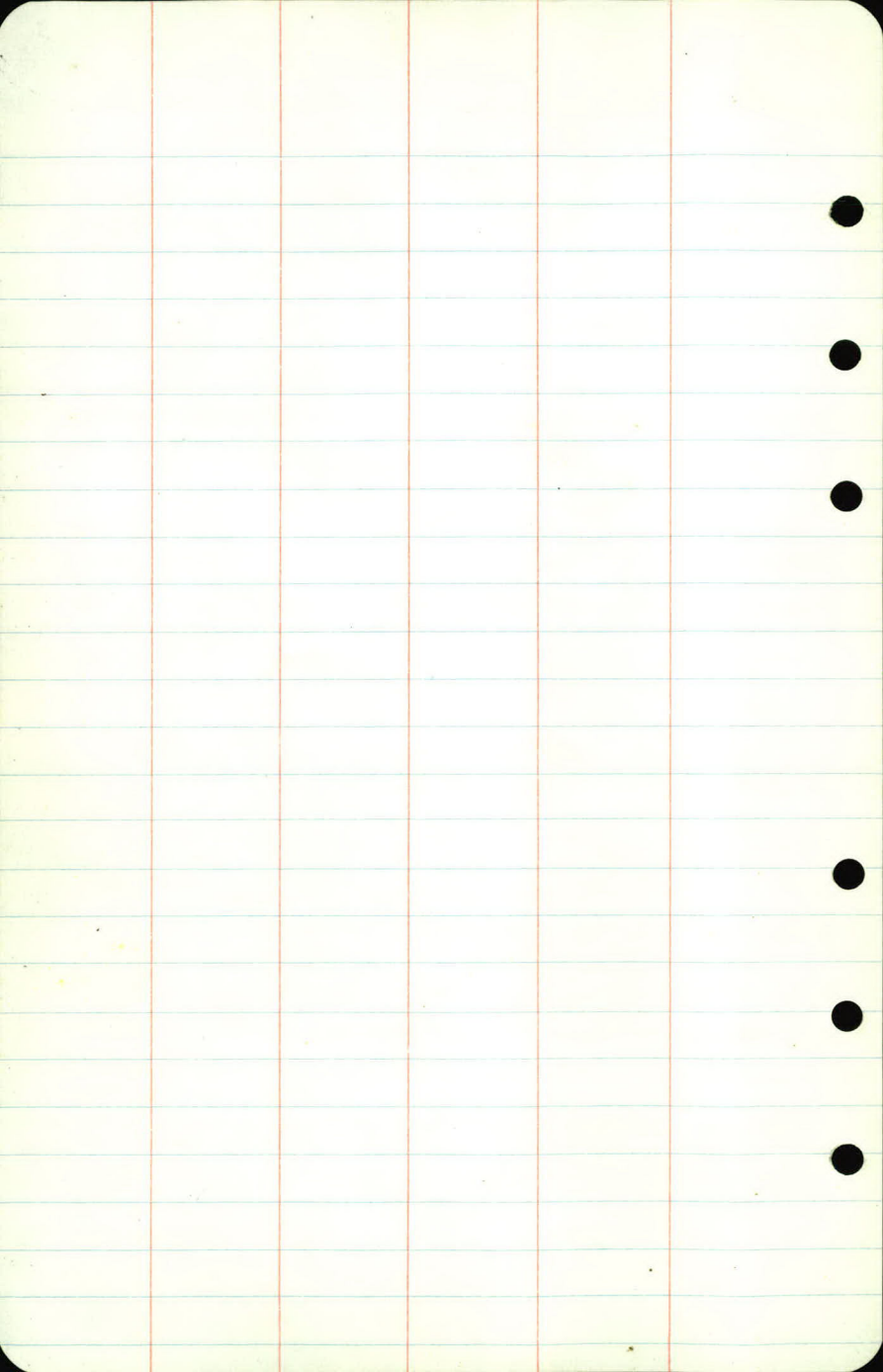
38			$0^{\circ}08.7'$
----	--	--	------------------

37	+92.74	P.C.	$0^{\circ}00'$
----	--------	------	----------------



Sta.	Point	ΔLt	ΔRt
76	+0.72 P.T.	28° 07'	
	+50	27° 30'	
		22° 30'	
75		19° 30'	Δ 56° 14'
	+50	15° 30'	D-16° -
74	+48.21 P.I.	56° 14'	T-191.95
74		11° 30'	L-351.46'
	+50	7° 30'	R-359.26'
73		3° 30'	
72	+56.24 P.C.	0° 00'	
60	+36.20 P.I.		1° 20'
	+50.58 P.T.	29° 08.5'	Δ -58° 17'
56		23° 34.7'	D-22° -
	+50	18° 04.7'	T-146.10'
55	+31.75 P.I.	58° 17'	L-264.93'
55		12° 34.7'	R-262.04'
	+50	7° 04.7'	
54		1° 34.7'	
53	+85.65 P.C.	0° 00'	





Topography

+80-End Low Colors-23'

+26-Bos Fe-29' Bog. Woods

+12-Ent

4

16' 11'

Row Trees-24'

+93-24'-41'

+64-T.P-32'

+31-PP-26'

3

14' 11'

+86-Bog Low Colors-27'

+65-24'-42'

+64-Side Rd. Sign 20'

2

+17-T.P-30'

13'

+61-Ent

+26-12' B.E.-26' +50-20' B.E.-26'

+29-5' B.E.-35'

+20-6" T.P. Box-27'

12' +66-15' W.I.I.-40'

+93-5' Cedar-25'

+88-6' B.E.-35'

+77-PP-28' +77-18' B.E.-27'

+68-15" O.-25' N.W. Cor. Ho.-91'

+61-Hedge.-26'

+57-32.5' Work. Box Top-17' Top-21'

+54-Hedge-27'

+27-15' B.E.-34' +52-24' Map-26'

+13-12' B.E.-34' +20-18' B.E.-26'

13' 14' +66-12' Map-26'

1

+81-T.P-28'

+99-12' B.E.-38'

+90-12' B.E.-38' +92-15' Map-25'

+58-15' B.E.-32' +78-14'-25'

+38-15' Map-25' +51-12' Map-25'

+19-Ent

+08-PP-29'

15'

-10-Bog. G.R.-19'

+37-End Rod-11'

+25-End 12" G.M.-17'

+16-Bog. Rod-37'

0+00

-07-Bog. Rod-37'

-11-Bog. G.R.-38'

G.R.-9 +35-6'

-39-G

Box Cul.-10.5'

-26-End-12" G.M.-18'

-57-End G.R.-10'

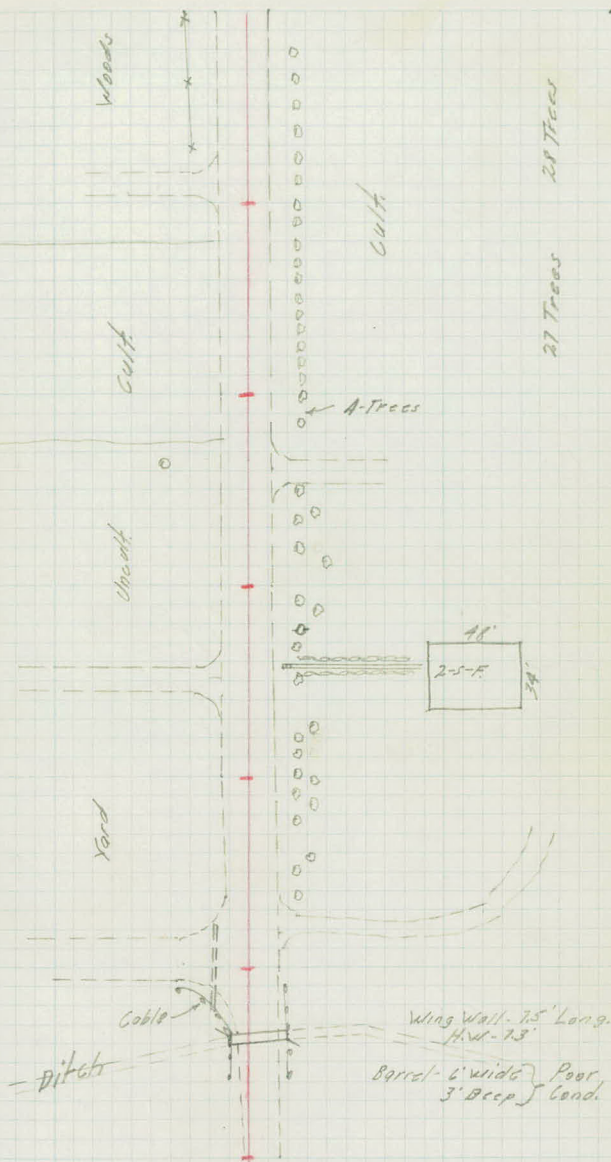
-35-G

Box Cul.-20'

-57-End G.R.-20'

-1+00

4' 16'



+83-SE Cor Ho - 89'

+58-Red 8' Wide Flower Bed - 42'

+54-Hedge - 44'

+50-10' Tw Cherry - 44'

+42-End Hedge - 40'

11

24'

+77-T.P. - 36'

+54-Red Lillies Hedge - 39'

+40-54 Sign - 29'

+236 - X Taylor Ave.

10

22'

5'

+43-T.P. - 35'

+41-End Fe - 37' + Woods

9

Fe - 33'

20'

5'

Fe - 16'

+91-54p - 33'

+50-Fe - 34'

8

+01-T.P. - 35'

Fe - 35'

21'

6'

+46-54p - 36'

7

+08-Ent

Fe - 35'

20'

8'

+77-P.G.P. - 34'

+57-T.P. - 34'

6

Fe - 32'

18'

9'

5

+04-T.P. - 33'

Fe - 33'

17'

11'

+99-Range 1162

+94-Fe Cor 17'

+85-Ent

+56-P.P. - 19' +75-15' 0 - 36'

+73-1' Silver Box - 20'

+17-12' 0 - 13' +22-12' 0 - 20'

+01-2' 0 - 23'

+01-8' B.E. - 31'

Fe - 15'

+82-3' Grillage Ho - 33'

+92- Cor Ho - 45' +92-12' 0 - 23'

+78-Shrub - 20'

+63-SE Cor Ho - 47'

+54-W. 1/2 Shrub - 28'

+39-54p - 31'

+32-Div Fe - 19'

+23-Div Fe - 32'

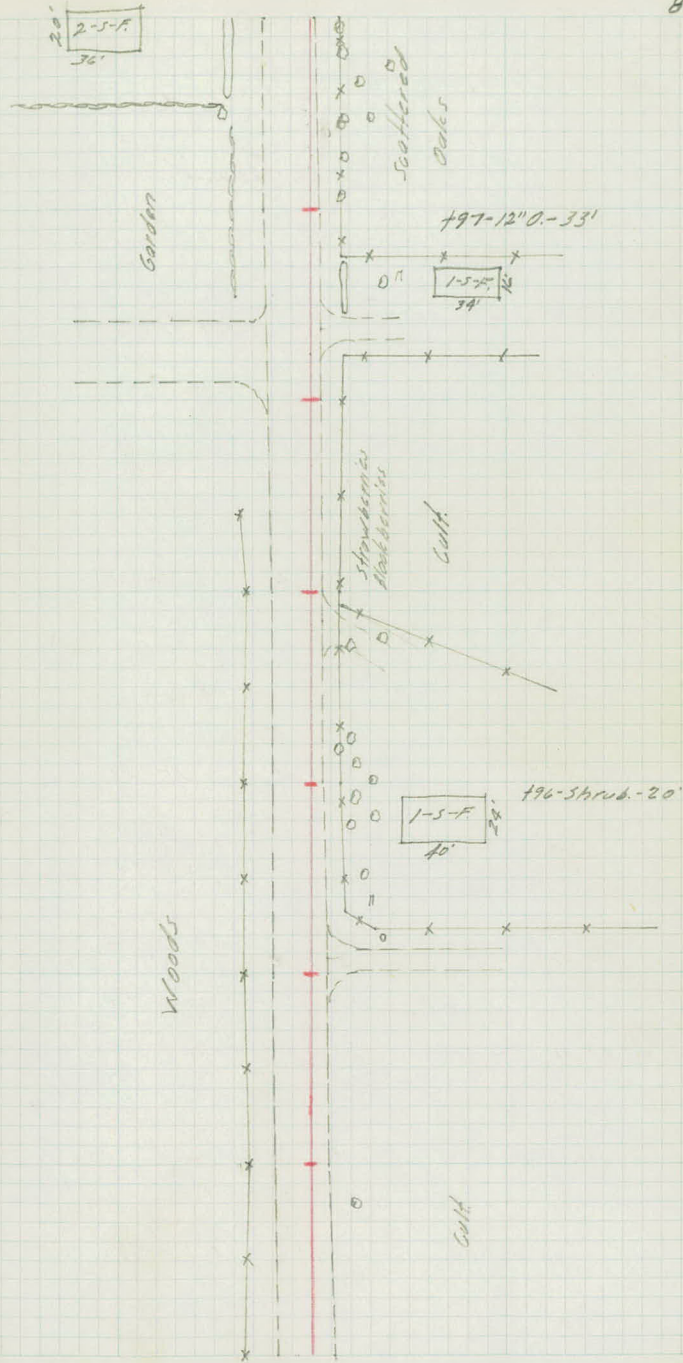
+18-Ld Iron - 37.5'

+08-Ent

+84-P.P. - 23'

+80-12' Ash - 21'

+08-P.P. - 25'



+83-T.P-25'

18 Fc 25' 6' 20' +15-Ent. Fc-34

+46-T.P-24'

+36-P.P-23'

17 Fc-23' 6' 22' +01-20'0.-46' Fc-35

16 Fc 22' 7' 23' Fc-36

+87-T.P-21'

+50-6' 22' +46-P.P-35

15 Fc-21' 5' 21' Fc-37'

+62-T.P-23'

Fc-25' 10' 17' +50 Fc-34'

14 Fc 32' 15' 10' Fc-25'

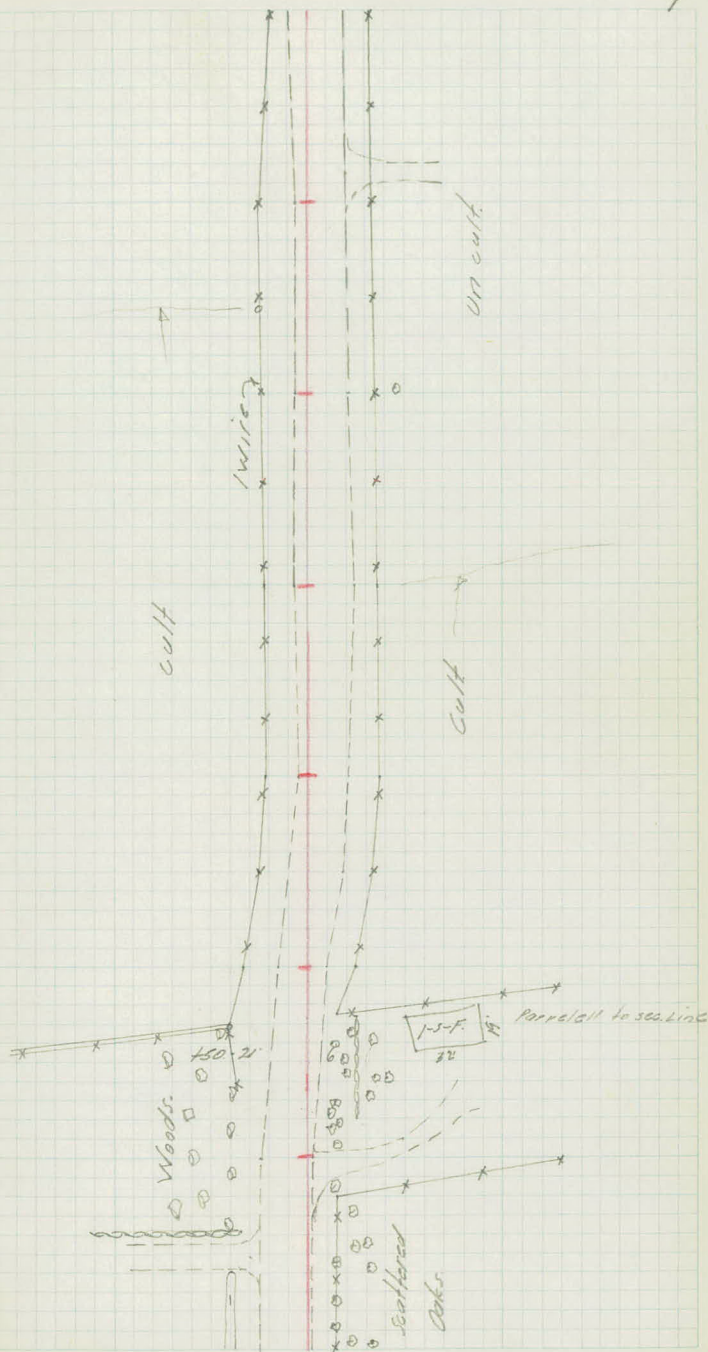
+75-Fc Cor-16' +73-Range Tie
+74-Ent/Hedge-25' +75-P.P-15'
+62-12"0.-32' +66-8"0.-23'
+55-5W Cor-Ha-56' +59-11W-14'
+46-10"0.-20' +51-12"0.-19'
+32-4"Pin-31' +41-8"0.-35' 8"0.-41'
+23-15"0.-11' +28-12"0.-13'
+20-8W Lil/Hedge-25'
+15-13"0.-13' +17-12"0.-15'
+12-15"0.-15'

+70-Fc Cor-40' +73-Range Tie
+68-P.G.P-41' +Fc Cor
+48-T.P-38'
+35-Fc-37'

+10-T.P-37'

+96-Ent
+84-15"0.-13'
+77-Range Tie +81-Fc Cor-15'
+56-12"0.-30' +71-6"0.-23'
+46-12"0.-15' +54-6"0.-24'
+25-10"0.-15' +43-10"0.-31'
+09-P.P-17' +11-12"0.-14'
+01-5"0.-33' +08-12"0.-24'
Fc-15'

12 24' 2'



+94-T.P.-21

+53-PP-28'

25 Fe-23' 13' 11' Fe-28'

Fe-22' 13' 12' Fe-29'

+37-T.P.-21'

24 Fe-24' 13' 15' Fe-34'

+93-Ent.
+86-PP-36'

Fe-24' 12' 16' Fe-32'

+01-Longe Tia

23 13' 15' Fe-29'

+96-T.P.-21' Fe. Cor-21'

+70-Ent 12" Vit. Culv -18'

12" X 38" Vit. Culv.

+74-Ent 12" Vit. Culv -19'

+67-PP-28'

Fe-27' 14' 13' Fe-29'

22 Fe-30' 16' 13' Fe-27'

+25-15" O.-27'

+63-Ent.
+58-T.P.-30'

+77-12" O.-21' 5" O.-33'

+80-6" O.-34'

+83-15" O.-49'

+31-12" O.-20' +31-12" O.-38'

+18-12" O.-27' +29-12" O.-22'

+23-20" O.-26' 5" O.-36'

21 Fe-29' 15' 14' Fe-28'

+96-PP-27'

+85-6" O.-31'

+72-10" O.-35'

+58-6" O.-35'

+41-10" O.-24'

+22-24" O.-39'

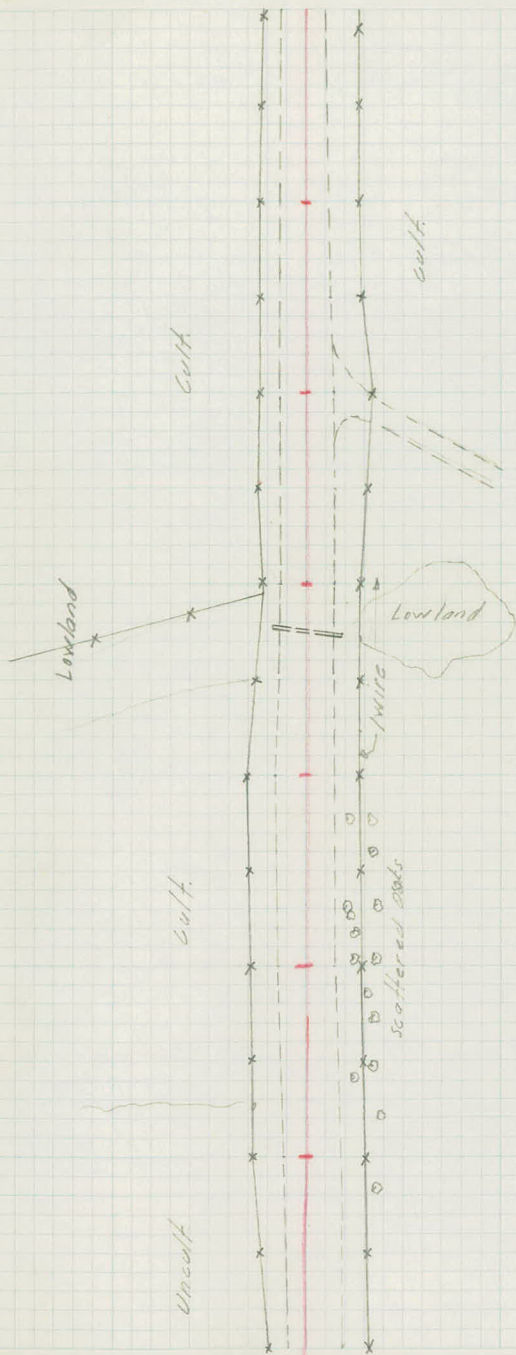
+27-T.P.-28'

20 Fe-28' 11' 16' Fe-30'

+84-12" O.-37'

+26-PP-30'

19 Fe-19' 9' 18' Fe-32'



32 +90-T.P.-19 Fc-19 14' 12' Fc-15'-28'

+53-PP-28'

31 Fc-19 15' 12' Fc-15'-29'

+46-T.P.-18'

+28-Rd sign-14'

30 Fc-19 15' 11' Fc-14'-29'

+54-PP-28'

29 +92-T.P.-19 Fc-20' 15' 11' Fc-16'-28'

28 Fc-20' 13' 11' +06-Fc Cor-19'
+05-Fc Cor-28'

+43-T.P.-20' +58-PP-28'

27 Fc-20' 12' 12' Fc-28'

26 Fc-21 12' 11' Fc-28'

Cult.

Cult.

Cult.

Uncult.

Wire



+77-54p-23'

+54-54p-22'

+49-T.P.-23' Fe-23'

13' 11'

Fe-31'

+12-54p-22'

39 Fe-23'

13' 13'

Fe-32'

+57-Fe Cor-23'

14' 13'

+60-PP-31'

Fe-31'

+21-T.P.-22'

38

16' 10'

Fe-28'

+09 Cor. Born-89

37

23' 3'

Fe-21'

+66-T.P.-30'

+58-Ent. 12" X 20" S 14-27'

+48-Cor. Lilliac Hedge-32'

+35-10" Ash-41'

+45-15" Ash-41'

+23-10" Ash-41'

+09-10" Ash-36'

+69-PP & Fe Cor-20'

+55-Ent

+45-End Fe-2'

36 Lilliacs-31'

28'-1'

Fe-2'-18'

+74-Box Lilliacs-41'-31'

+62-6" Cedar-39'

+50-6" Ash-32'

+44-12" Elm-34'

+32-Ent

+39-Runge Tr

+22-T.P.-30' Fe Cor-30'

26' 0'

Fe-2'-17'

+34-8" D.-15'

+33-8" D.-15'

+29-PP-15'

+15-8" Ash-13'

35 Fe-28'

23' 2'

Fe-3'-18'

Fe-22'

19' 5'

Fe-8'-22'

34 Fe-19'

15' 9'

Fe-11'-26'

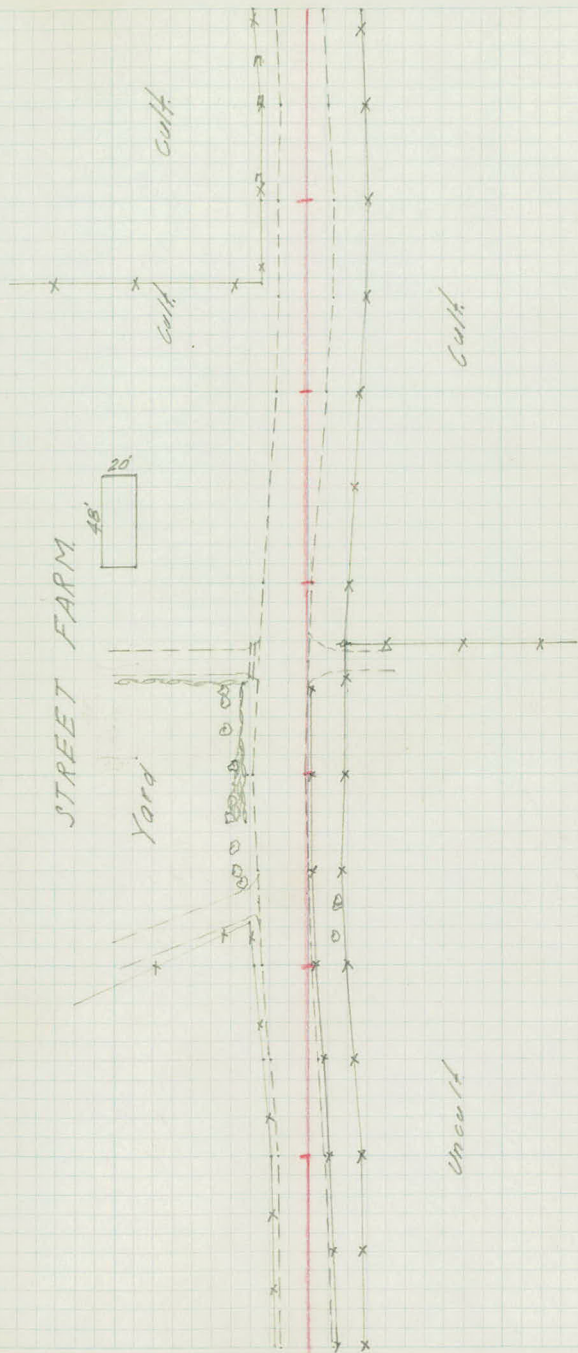
+34-T.P.-18'

+51-PP-28'

33 Fe-18'

13' 12'

Fe-14-28'



170° End Culv - 25'

10° X 30' C.M.

22' 2' 163° End Culv - 4'
FC - 11'

46

28' - 4'

FC - 5'

176° PR - 9'

+40-End. S. 40° - 38'

+41-T.P. 39'

45

+04-Str - 1'

FC -

121° FC X 6

36' - 11'

+09-Str - 5'

+68-12° D. - 3'

+89-10° D. - 2' +93-Str - 1'
+80-Str - 1' 5" D. - 3'
+73-8° D. - 2' +93-Str - 14'
+70-8° D. - 24' +95-6° D. - 1'
+68-Str - 33' +95-Str - 4'
+62-12° D. - 15' +50-Str - 26'
+23-Str - 13'
+10-Str - 36'

44

FC - 5'

38' - 14'

+88-15° D. - 9'

+84-T.P. 43'

+78-PR - 2'

+93-Str - 29'

+85-12° D. - 26'

+50-FC - 6'

39' - 16'

+58-Ent - 12° X 28° C.M.
41'

43

FC - 7'

39' - 18'

+90-Longe Tie

+88-2° Water Pipe - 7'

+41-T.P. 44'

+36-Str - 10'

+29-FC - 46'

+25-Δ 15 FC - 8'

+10-FC - 46'

+10-Dia FC - 13'

+50-39' - 17'

+17-End of Coffle Xing 11'

FC - 12'

36' - 15'

+44-Str - 16'

+07-P.P. 2'

42

+82-8° D. - 13'

+414° D. - 5'

+23-20° D. - 3'

+45-FC Cor - 1'

41

Sine Rd. 10° X 36° C.M. 27' - 5'

+08-FC Cor - 13'

+96-Ent

+85-7° P. + FC Cor - 35'

FC - 30'

21'

2'

+17-P.P. - 20'

FC - 25'

+20-8° B.E. - 29'

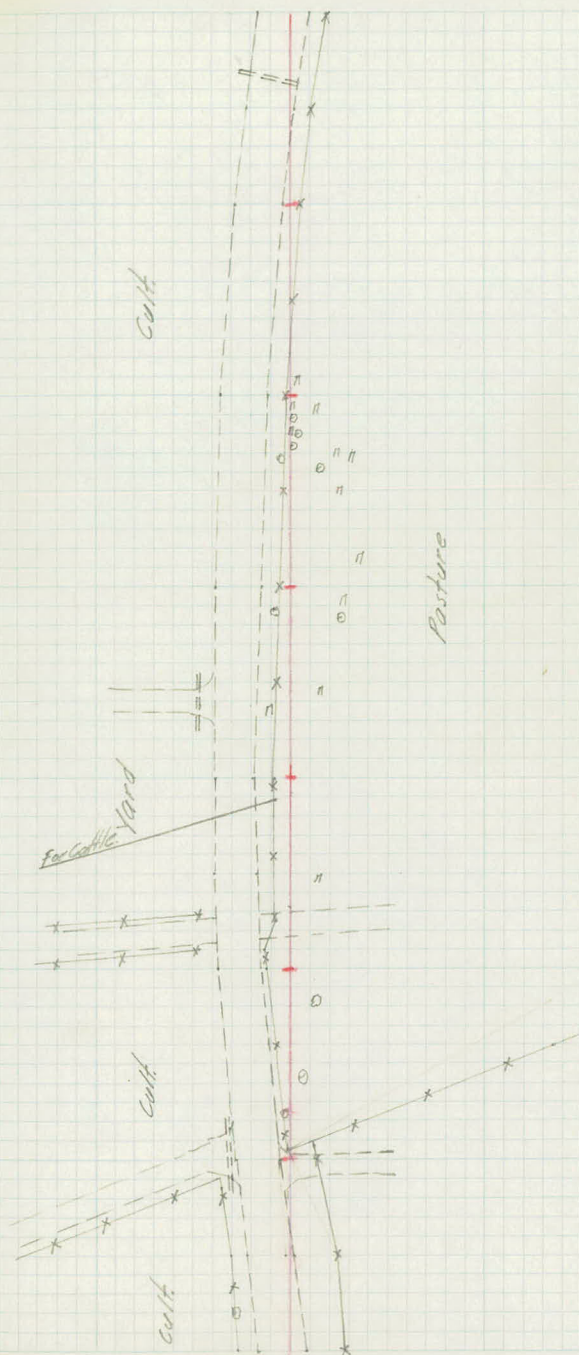
40

FC - 27'

16'

8'

FC - 28'



2.5 wide x

29' 0

+35-Bottom Step-13'
+33-Top Step-17' Arisers
+50-Cor Ho.-60'
+30-10' Elm-20'
+24-Cor Ho-56'
+17-24" PE.-41'
+08-Bog Hedge-10'
+96-Bog Bush-26'
+07-2" Pine-19'

+92-Pod Rod-2'
+87-Bog Rod-17'
+73-End Cap-30'
+70-T.P.-41'
+55-P.P.-28'
+46-Bog Rod-14'

53 Shrub-24' +02-Shrub-2' 3' 22'

+85-Top-30' +95-Shrub-30'
+73-12' Elm-23'
+62-End Plumb-10'-20'
+46-P.P.-34'
+41-4' Trip PE-12'
+30-Plum To-14'-4'

+54-T.P.-57'

52 +04-1" Plum-5'

16'-41'
+92-24" BE-4'
+83-P.P.-56'

+47-Fc 15'

+55-End PE-16'
23'-49'

51

31'-57'

+79-T.P.-28'
33'-59'

50

30'-56'
+93-T.P.-20'
+74-P.P.-68'
25'-51'

49

+08-Dio. Fc-59'
17'-46' Fc

+57-T.P.-3'

+28-Long Tie to Fc

48

0 28' Fc-37'

+76-P.P.-39'

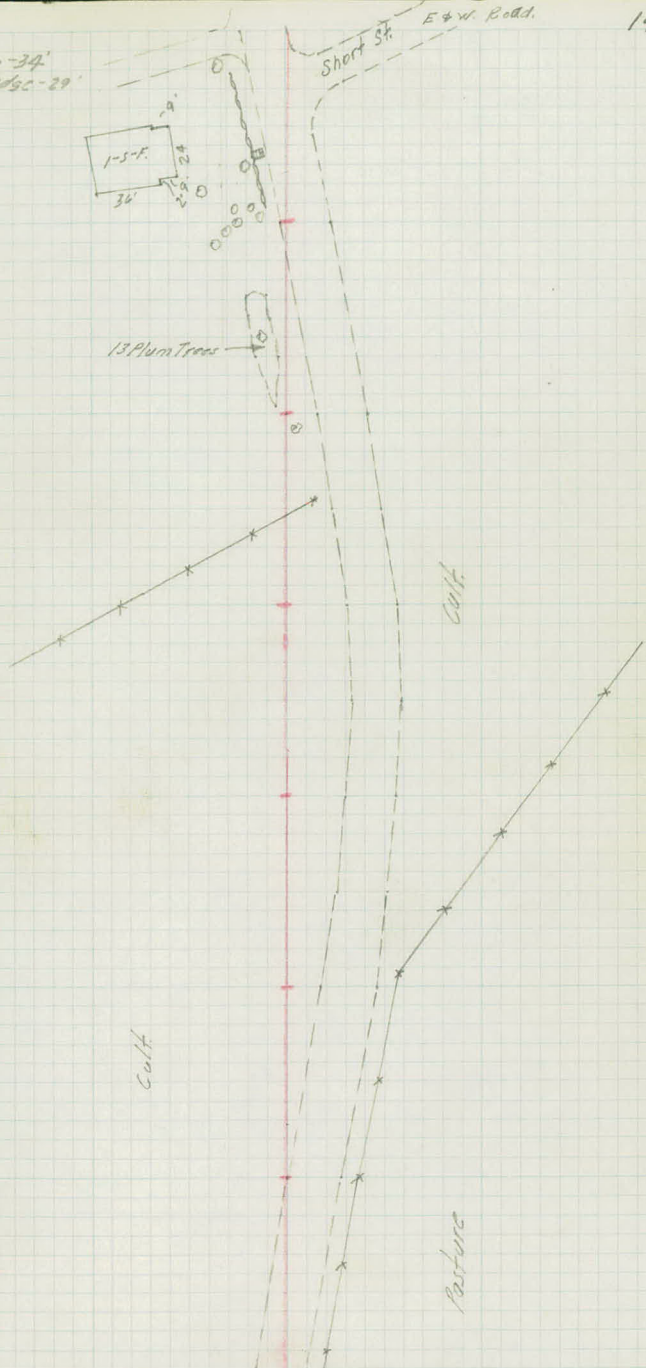
47

T.P.-20'

16' 10'

Fc-18'

+95-Ent
 +11-24' Elm - 34'
 +79-End Hedge - 29'



+86-5tp-9'

+74-5tp-40'

+48-PP-80'

+20-5tp-20'

60

Fe-2'

+81-5tp-9'

+77-5tp-4'

+2-5tp-00

+43-5tp-31'

+15-5tp-19'

59 Fe-10'

+61-PP-63'

58 Fe-10'

71'-92'

57 Fe-20'

52'-75'

+50-Fe-25'

+76-PP-28'

36'-60'

56

3'-26'

+89-Fe-22'

+46-Δm Fe-20'

13' 8'

+28-Fe Cor-35'

+22-Longe Tto.

+25-T.P-6'

55

23'-3'

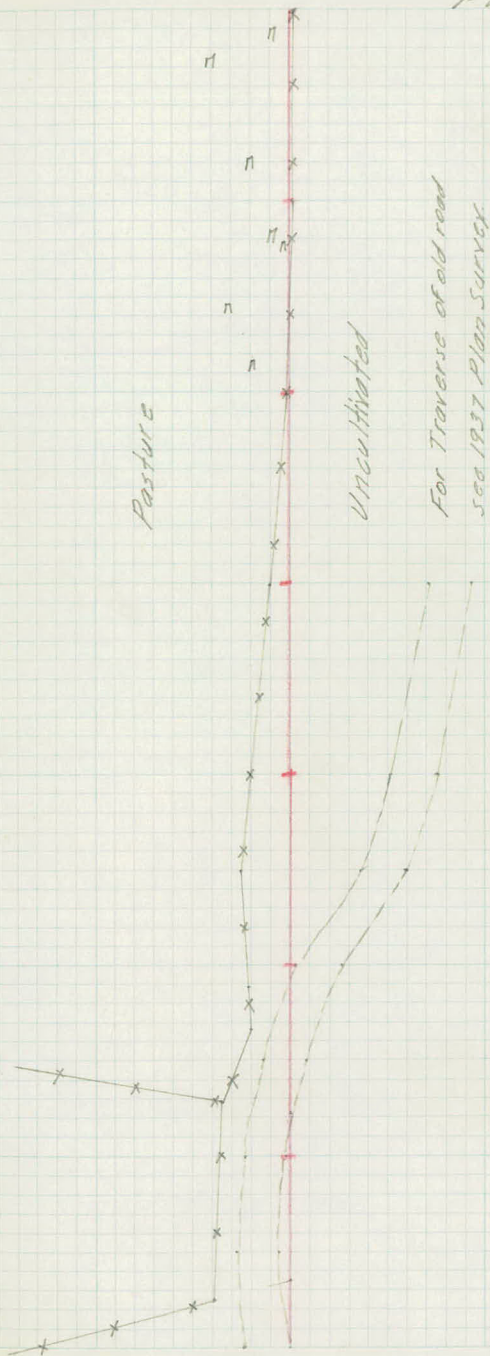
27' 6'

+25-Longe Tto

+25-Fe Cor-39'

54

24' 0'



67 FC-2'

+105-stp-6'
66 FC-4'

+88-stp-22'
+70-D in FC-4'

+59-D in FC-38'
+17-D in FC-44'

65 FC-34'

+58-D in FC-4'

64 FC-3'

+15-End Brush-5'

+15-stp-20'
+10-stp-25'
63 stp-30-22-2' FC-2'
+90-stp-21'-29'
+88-stp-3'
+72-stp-13'
+70-stp-12'-2'
+57-stp-2'
+52-stp-11'
+41-stp-14'

+14-Cor Brush-5'

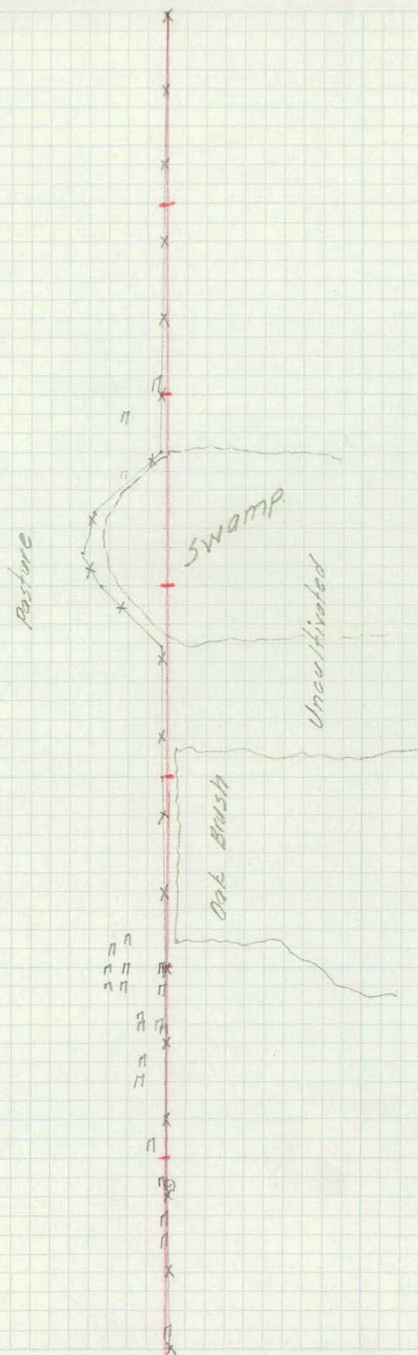
62 +58-stp-7'

+89-stp-2'

+87-30'0"-1'
+70-stp-00

+58-stp-00

+10-stp-2'
FC-2'



172-End Fe-30'

33'-5'

123-T.P.-41'

105-Range 112 to Fe. Cor.

74

39'-17'

193-Fe. Cor-50'

Fe-31'

195-Step-32'

150-Fe. Cor-68'

141-Dim Fe.-62'

73

Fe-62'

53'-31'

128-15" Pop-28" Step-26"

50' 27" 120-15" Pop-17'

115-Step-1'

112-12" Pop-20'

102-18" Pop-11'

Fe-4'

167-15" Pop-29'

156-15" D.-3'

151-6" D.-10'

150-Step-2'

146-8" D.-20'

142-Step-23'

128-18" D.-11" Step-28'

125-Step-16'

Fe-2'

72

Fe-46'

37'-15'

+ 98-5" Typ.-0-10'

195-Step-13'-21'

191-24" D.-32'

161-Dim Fe.-2'

150

146-12" D.-7'

137-15" D.-10'

134-T.P.-27'

71

Fe-24'

18' 10'

Fe-19'

194-15" D.-25' 198-15" D.-21'

163-End

150-Fe-9'

166-Step-31'

6'-26'

Fe-39'

124-Dim Fe-00

70

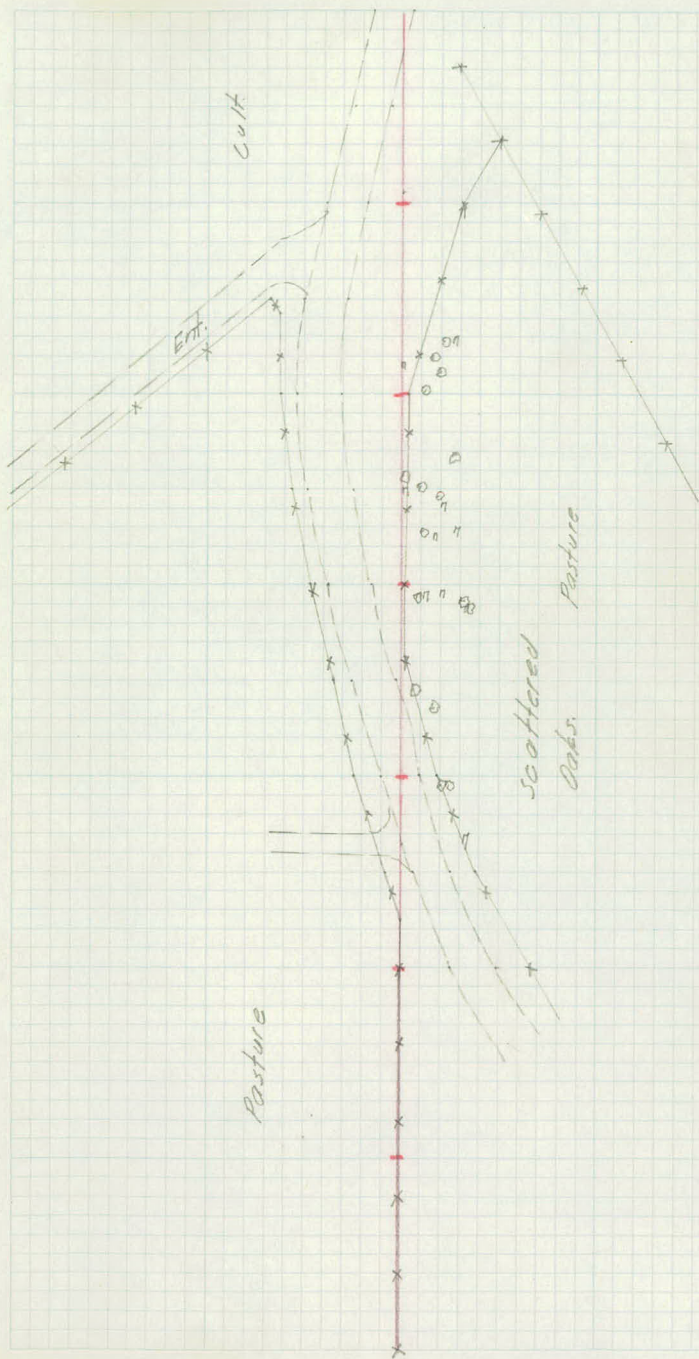
Fe-00 25'-49'

69

Fe-0.0

68

Fe-0.0



78

77

12' 11'

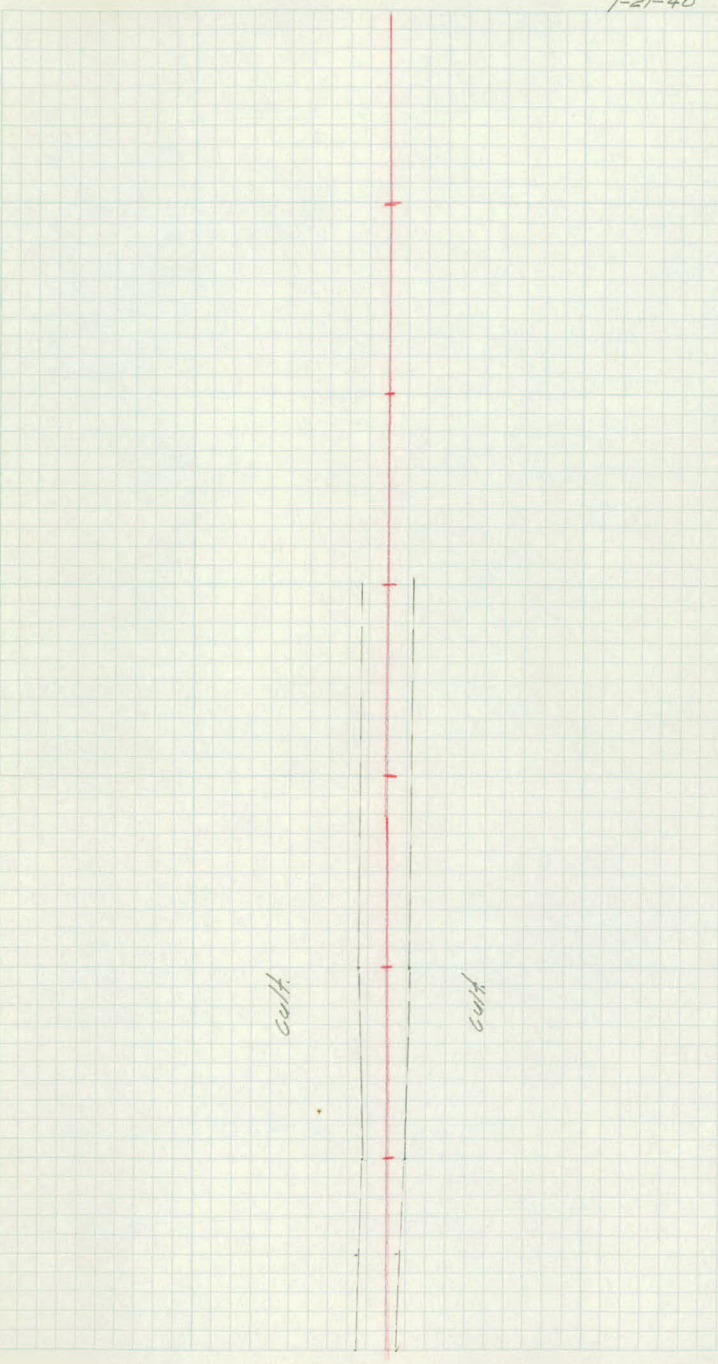
76

12' 10' HIT-TP-31'

16' 5'

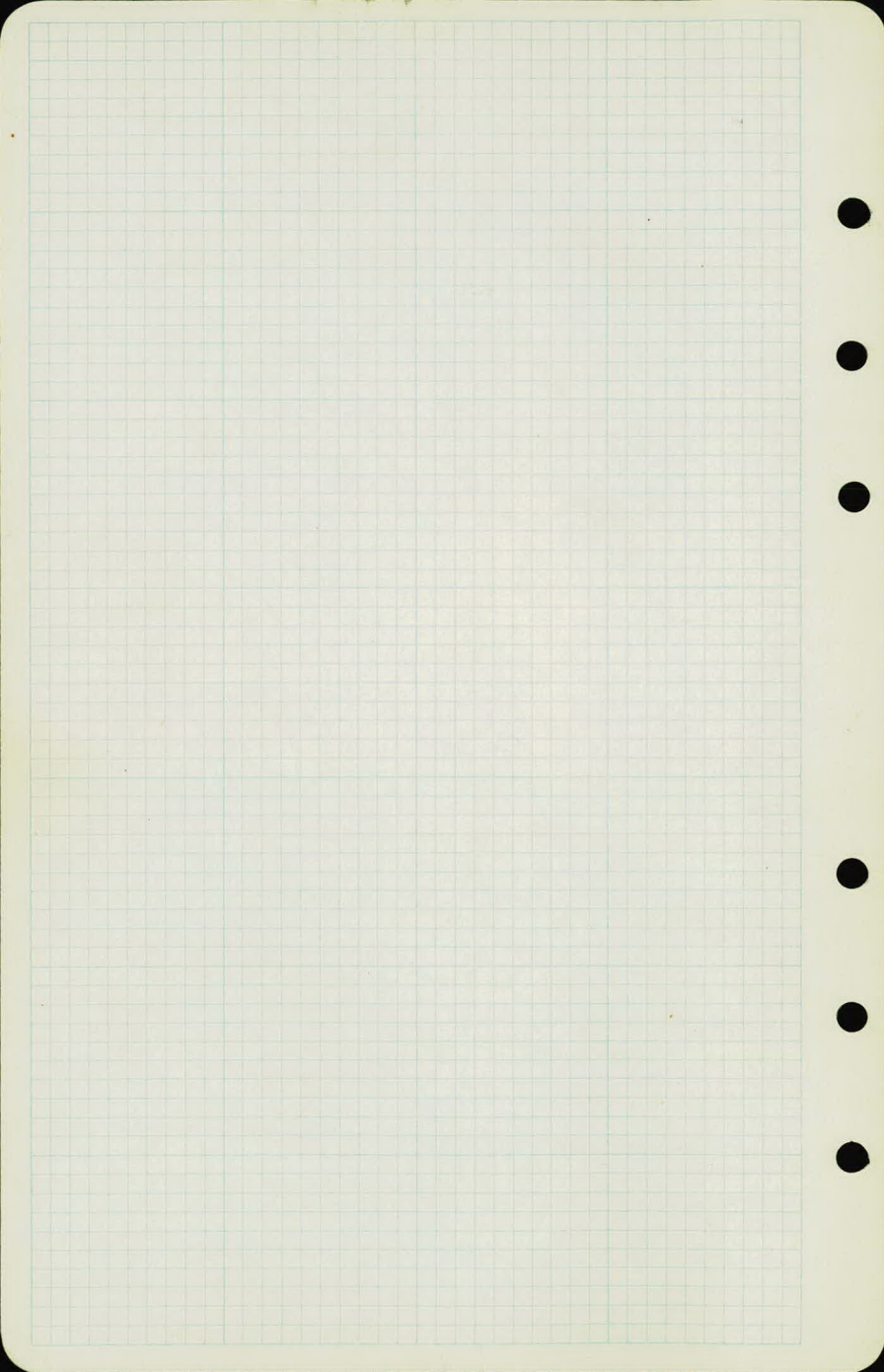
75

15' 5'



cult.

cult.



Xsections

Sta	+	T ✓	-	Elev
B.M.	8.95	930.53		(921.58)
-2 +00			7.2	
- -50			8.1	
-1			8.6	
- -50			8.8	
0 +00				22.6
+24				22.2
+34				22.0
+70				23.7
1				24.3
+34				24.9
+44				25.1

Lt

k

Lt

Top S.E. Cor. Conc. Head wall of Culv. S.E. Cor. Sixth & Portland Ave.

$$\frac{76}{100} \frac{75}{50} \frac{75}{21} \frac{79}{20} \frac{79}{52} \frac{85}{50} \frac{93}{50}$$

$$\frac{84}{50} \frac{83}{31} \frac{82}{16} \frac{75}{15} \frac{78}{31} \frac{81}{50} \frac{82}{50}$$

$$\frac{36}{50} \frac{41}{31} \frac{83}{20} \frac{78}{12} \frac{73}{15} \frac{76}{32} \frac{79}{50} \frac{73}{50}$$

$$\frac{30}{50} \frac{34}{33} \frac{77}{21} \frac{77}{17} \frac{70}{13} \frac{68}{14} \frac{72}{21} \frac{67}{38} \frac{55}{50} \frac{55}{50}$$

$$\frac{32}{50} \frac{34}{34} \frac{70}{24} \frac{63}{15} \frac{67}{14} \frac{64}{10} \frac{62}{14} \frac{66}{23} \frac{55}{34} \frac{52}{50} \frac{37}{50}$$

$$\frac{32}{50} \frac{33}{37} \frac{62}{27} \frac{58}{12} \frac{56}{15} \frac{59}{20} \frac{49}{35} \frac{36}{50} \frac{23}{50}$$

$$\frac{54}{50} \frac{58}{35} \frac{57}{13} \frac{54}{14} \frac{59}{19} \frac{48}{35} \frac{33}{50} \frac{22}{50}$$

Sta.	+	π	-	Elev.
		930.53,		
T.P.	910	935.62,	4.01	926.52
2				26.5
	+38			27.3
	+76			28.2
3				28.7
	+50			29.8
4				31.3
	+50			32.7
T.P.	10.74	945.15	1.21	934.41
5				34.5
	+50			35.9
6				37.3
	+39			38.7

Lt.

L.

Pt.

$$\frac{93}{50} \frac{82}{33} \frac{99}{26} \frac{87}{17} \frac{95}{13} \frac{91}{13} \frac{98}{20} \frac{76}{34} \frac{69}{34} \frac{62}{50}$$

$$\frac{91}{50} \frac{79}{39} \frac{74}{29} \frac{88}{24} \frac{84}{17} \frac{88}{15} \frac{83}{12} \frac{89}{19} \frac{72}{35} \frac{64}{50} \frac{63}{50}$$

$$\frac{96}{50} \frac{89}{27} \frac{80}{17} \frac{74}{15} \frac{71}{17} \frac{73}{17} \frac{71}{26} \frac{60}{50}$$

$$\frac{91}{50} \frac{91}{32} \frac{75}{15} \frac{69}{11} \frac{73}{19} \frac{80}{23} \frac{69}{40} \frac{66}{50}$$

$$\frac{81}{50} \frac{78}{31} \frac{64}{16} \frac{58}{12} \frac{63}{19} \frac{76}{23} \frac{83}{37} \frac{72}{37} \frac{68}{50}$$

$$\frac{45}{50} \frac{58}{40} \frac{50}{29} \frac{46}{20} \frac{43}{14} \frac{50}{17} \frac{63}{21} \frac{67}{34} \frac{65}{50} \frac{67}{50}$$

$$\frac{13}{50} \frac{20}{36} \frac{25}{30} \frac{34}{26} \frac{30}{20} \frac{34}{19} \frac{28}{7} \frac{29}{14} \frac{36}{19} \frac{41}{37} \frac{57}{37} \frac{64}{50}$$

107

$$\frac{97}{50} \frac{99}{34} \frac{102}{28} \frac{115}{26} \frac{109}{19} \frac{107}{7} \frac{112}{14} \frac{118}{20} \frac{133}{24} \frac{128}{25} \frac{140}{36} \frac{152}{50}$$

$$\frac{98}{50} \frac{106}{39} \frac{107}{32} \frac{105}{28} \frac{93}{22} \frac{97}{19} \frac{93}{7} \frac{92}{12} \frac{100}{12} \frac{108}{18} \frac{117}{20} \frac{128}{26} \frac{132}{37} \frac{137}{50}$$

$$\frac{70}{50} \frac{75}{41} \frac{78}{31} \frac{84}{29} \frac{83}{26} \frac{75}{22} \frac{83}{18} \frac{78}{6} \frac{79}{14} \frac{83}{17} \frac{91}{23} \frac{100}{35} \frac{95}{35} \frac{96}{50}$$

$$\frac{50}{50} \frac{50}{42} \frac{50}{33} \frac{55}{23} \frac{68}{21} \frac{64}{5} \frac{65}{9} \frac{71}{12} \frac{63}{17} \frac{65}{17} \frac{60}{20} \frac{61}{26} \frac{56}{31} \frac{60}{50}$$

Sta.	+	A	-	Elev.
		945.15		
6	+85			40.0
7				
	Profile of Ent. Rt.			
T.P.	1108	951.71'	4.52	940.63
	+22			41.3
	+50			42.2
8				44.8
	+50			45.2
9				46.2
B.M.	332	951.21'	3.82	947.89
	+50			46.8
10				46.9
	+2362 - E Taylor Ave			46.8
	+50			46.8

Lt

K

Rt

$$\frac{2.0}{50} \quad \frac{1.7}{36} \quad \frac{1.2}{29} \quad \frac{4.5}{22} \quad \frac{5.3}{20} \quad \frac{4.8}{6} \quad \frac{5.0}{10} \quad \frac{5.3}{15} \quad \frac{4.6}{21} \quad \frac{2.2}{34} \quad \frac{1.6}{50} \quad \frac{1.9}{50}$$

$$\frac{4.5}{10} \quad \frac{5.0}{22} \quad \frac{4.5}{50} \quad \frac{4.2}{50}$$

No dirt
Rt.

$$\frac{5.2}{50} \quad \frac{4.9}{31} \quad \frac{9.1}{24} \quad \frac{9.9}{22} \quad \frac{10.1}{21} \quad \frac{10.3}{7} \quad \frac{10.4}{10} \quad \frac{10.6}{18} \quad \frac{4.4}{50} \quad \frac{5.8}{50}$$

$$\frac{3.8}{50} \quad \frac{3.5}{31} \quad \frac{9.2}{24} \quad \frac{9.2}{22} \quad \frac{9.9}{21} \quad \frac{9.4}{7} \quad \frac{9.5}{7} \quad \frac{10.0}{17} \quad \frac{4.2}{33} \quad \frac{4.7}{50} \quad \frac{5.3}{50}$$

$$\frac{2.8}{50} \quad \frac{3.0}{32} \quad \frac{8.4}{21} \quad \frac{7.8}{9} \quad \frac{7.9}{7} \quad \frac{8.2}{7} \quad \frac{7.0}{80} \quad \frac{3.8}{14} \quad \frac{4.2}{36} \quad \frac{4.9}{50}$$

$$\frac{2.5}{50} \quad \frac{2.6}{32} \quad \frac{6.3}{24} \quad \frac{6.4}{22} \quad \frac{6.4}{9} \quad \frac{6.5}{6} \quad \frac{6.8}{7} \quad \frac{5.9}{13} \quad \frac{3.7}{27} \quad \frac{4.7}{50} \quad \frac{6.1}{50}$$

$$\frac{2.8}{50} \quad \frac{3.3}{28} \quad \frac{4.9}{24} \quad \frac{5.8}{21} \quad \frac{5.4}{9} \quad \frac{5.5}{7} \quad \frac{5.6}{16} \quad \frac{5.6}{28} \quad \frac{6.0}{50} \quad \frac{6.1}{50}$$

Spt in R.P. 19' Rt sta. 11+23

$$\frac{3.1}{50} \quad \frac{4.2}{30} \quad \frac{4.5}{26} \quad \frac{4.9}{22} \quad \frac{4.4}{8} \quad \frac{4.4}{8} \quad \frac{5.0}{10} \quad \frac{4.7}{32} \quad \frac{5.1}{50}$$

$$\frac{5.2}{50} \quad \frac{5.2}{42} \quad \frac{4.9}{29} \quad \frac{4.6}{20} \quad \frac{4.2}{9} \quad \frac{4.3}{9} \quad \frac{4.6}{17} \quad \frac{4.9}{29} \quad \frac{4.8}{50} \quad \frac{4.6}{50}$$

$$\frac{6.8}{150} \quad \frac{5.7}{100} \quad \frac{4.9}{50} \quad \frac{4.4}{20} \quad \frac{4.4}{20}$$

$$\frac{4.2}{50} \quad \frac{4.2}{40} \quad \frac{4.5}{29} \quad \frac{5.3}{27} \quad \frac{4.7}{22} \quad \frac{4.2}{9} \quad \frac{4.4}{13} \quad \frac{4.5}{18} \quad \frac{4.2}{35} \quad \frac{4.2}{50} \quad \frac{4.5}{50}$$

Sta	+	π	-	Elev
		951.21		
11				46.4
	+50			46.2
12				45.9
	+50			44.8
13				44.2
	+50			43.6
B.M.	1.99	949.43	3.77	947.44
14				43.0
	+50			42.4
15				41.3
	+50			40.3
16				39.0
I.P.	2.77	942.10	10.10	939.33

Lt

K

Rt

$$\frac{37}{50} \frac{42}{42} \frac{41}{29} \frac{50}{25} \frac{45}{10} \frac{48}{9} \frac{51}{6} \frac{45}{16} \frac{43}{30} \frac{50}{50}$$

✓

$$\frac{41}{50} \frac{44}{39} \frac{47}{29} \frac{52}{25} \frac{47}{12} \frac{50}{9} \frac{54}{7} \frac{50}{16} \frac{44}{31} \frac{43}{30} \frac{49}{50}$$

✓

$$\frac{50}{50} \frac{49}{31} \frac{55}{26} \frac{51}{13} \frac{53}{2} \frac{56}{7} \frac{46}{22} \frac{44}{39} \frac{51}{50} \frac{55}{50}$$

$$\frac{64}{47} \frac{62}{34} \frac{58}{13} \frac{61}{2} \frac{64}{4} \frac{58}{32} \frac{59}{50} \frac{62}{50}$$

$$\frac{84}{50} \frac{80}{29} \frac{68}{14} \frac{70}{14} \frac{74}{34} \frac{70}{50} \frac{73}{50}$$

$$\frac{100}{50} \frac{80}{35} \frac{78}{28} \frac{85}{25} \frac{80}{22} \frac{74}{10} \frac{76}{6} \frac{78}{7} \frac{74}{20} \frac{63}{30} \frac{54}{50} \frac{52}{50}$$

Top S.W. Cor. Bottom Cor. Step Front of Ho. Rt sta 14+60

$$\frac{79}{50} \frac{56}{29} \frac{52}{20} \frac{68}{17} \frac{64}{12} \frac{64}{11} \frac{70}{11} \frac{56}{18} \frac{23}{32} \frac{27}{50} \frac{31}{50}$$

$$\frac{55}{50} \frac{41}{26} \frac{38}{16} \frac{74}{9} \frac{72}{6} \frac{70}{12} \frac{74}{17} \frac{79}{17} \frac{64}{17} \frac{39}{24} \frac{10}{29} \frac{10}{50}$$

$$\frac{73}{50} \frac{62}{38} \frac{51}{17} \frac{55}{10} \frac{84}{6} \frac{81}{17} \frac{82}{22} \frac{85}{22} \frac{81}{22} \frac{79}{25} \frac{40}{30} \frac{29}{33} \frac{26}{50}$$

$$\frac{116}{50} \frac{93}{30} \frac{83}{14} \frac{85}{7} \frac{96}{6} \frac{91}{12} \frac{92}{22} \frac{95}{23} \frac{91}{25} \frac{91}{31} \frac{60}{50} \frac{54}{50}$$

$$\frac{122}{50} \frac{113}{30} \frac{107}{9} \frac{109}{6} \frac{104}{10} \frac{100}{23} \frac{106}{25} \frac{100}{28} \frac{101}{33} \frac{93}{50} \frac{83}{50}$$

Sta	+	π	-	Elev
		942.10		
16	+50			38.0
17				37.1
	+50			36.6
18				36.4
	+50			36.5
19				36.8
	+50			37.1
20				37.1
T.P.	5.83	942.91	5.02	937.08
	+50			36.9
21				36.7
	+60			36.7

Lt.

E.

Rt.

$$\frac{77}{50} \frac{76}{30} \frac{70}{16} \frac{58}{9} \frac{48}{7} \frac{41}{12} \frac{38}{26} \frac{42}{30} \frac{58}{36} \frac{58}{50}$$

$$\frac{104}{50} \frac{94}{33} \frac{96}{15} \frac{56}{7} \frac{50}{9} \frac{46}{24} \frac{48}{27} \frac{61}{33} \frac{72}{50}$$

$$\frac{108}{50} \frac{108}{26} \frac{96}{14} \frac{59}{5} \frac{55}{9} \frac{50}{24} \frac{54}{27} \frac{60}{31} \frac{63}{35} \frac{72}{50}$$

$$\frac{104}{50} \frac{100}{34} \frac{92}{16} \frac{84}{12} \frac{61}{7} \frac{57}{9} \frac{54}{25} \frac{57}{29} \frac{62}{39} \frac{68}{50}$$

$$\frac{99}{50} \frac{92}{30} \frac{77}{13} \frac{71}{10} \frac{61}{8} \frac{56}{8} \frac{56}{20} \frac{59}{23} \frac{68}{27} \frac{73}{40} \frac{67}{50}$$

$$\frac{103}{50} \frac{89}{33} \frac{73}{14} \frac{59}{10} \frac{53}{7} \frac{52}{18} \frac{57}{28} \frac{52}{42} \frac{47}{50}$$

$$\frac{78}{50} \frac{67}{36} \frac{61}{30} \frac{57}{18} \frac{56}{8} \frac{50}{7} \frac{50}{18} \frac{53}{24} \frac{53}{31} \frac{22}{50}$$

$$\frac{77}{50} \frac{69}{41} \frac{57}{29} \frac{54}{12} \frac{57}{12} \frac{50}{18} \frac{53}{22} \frac{43}{29} \frac{25}{50}$$

K 519 21100

$$\frac{71}{50} \frac{62}{28} \frac{65}{14} \frac{63}{9} \frac{60}{17} \frac{63}{23} \frac{44}{33} \frac{40}{50}$$

$$\frac{71}{50} \frac{67}{29} \frac{68}{17} \frac{65}{13} \frac{62}{12} \frac{64}{18} \frac{69}{33} \frac{59}{50}$$

$$\frac{63}{50} \frac{63}{30} \frac{68}{18} \frac{70}{17} \frac{67}{13} \frac{62}{11} \frac{63}{18} \frac{70}{27} \frac{64}{50}$$

Sta.	+	π	-	Elev.
		942.91		
22				36.9
B.M.	4.78	942.92	4.78	938.13 (938.14)
+50				37.1
23				37.4
B.M.			6.51	936.41 (936.41)
+50				37.9
24				38.8
+50				39.8
T.P.	11.74	952.59	2.07	940.85
25				40.9
+50				41.9
26				42.8
+50				43.7
27				44.5

Lt.

E

Rt.

$$\frac{68}{50} \frac{64}{29} \frac{66}{17} \frac{65}{12} \frac{60}{12} \frac{63}{12} \frac{69}{18} \frac{59}{22} \frac{61}{33} \frac{52}{50}$$

$$\frac{87}{50} \frac{76}{27} \frac{73}{21} \frac{63}{19} \frac{62}{15} \frac{67}{14} \frac{63}{9} \frac{58}{14} \frac{60}{16} \frac{63}{16} \frac{66}{29} \frac{73}{50}$$

$$\frac{96}{50} \frac{76}{24} \frac{66}{17} \frac{65}{13} \frac{62}{8} \frac{55}{16} \frac{54}{18} \frac{61}{20} \frac{68}{30} \frac{75}{30} \frac{76}{50}$$

R.R. 5pt. in 24" D. 85 Rt 5/2. 23+40 (Use this Bench)

$$\frac{93}{50} \frac{68}{27} \frac{57}{14} \frac{61}{12} \frac{61}{11} \frac{56}{8} \frac{50}{16} \frac{47}{20} \frac{55}{32} \frac{62}{50} \frac{70}{50}$$

$$\frac{66}{50} \frac{56}{31} \frac{40}{20} \frac{44}{15} \frac{53}{13} \frac{49}{10} \frac{41}{6} \frac{38}{16} \frac{41}{22} \frac{40}{35} \frac{43}{50} \frac{47}{50}$$

$$\frac{38}{50} \frac{28}{28} \frac{21}{22} \frac{30}{15} \frac{40}{13} \frac{37}{12} \frac{31}{14} \frac{34}{16} \frac{21}{29} \frac{19}{29} \frac{16}{50}$$

$$\frac{121}{50} \frac{106}{27} \frac{105}{22} \frac{115}{15} \frac{124}{13} \frac{117}{10} \frac{118}{14} \frac{123}{17} \frac{103}{28} \frac{95}{38} \frac{96}{50} \frac{89}{50}$$

$$\frac{112}{50} \frac{95}{30} \frac{82}{24} \frac{97}{17} \frac{113}{13} \frac{107}{11} \frac{110}{13} \frac{116}{14} \frac{114}{18} \frac{91}{26} \frac{86}{30} \frac{64}{50} \frac{64}{50}$$

$$\frac{110}{50} \frac{96}{37} \frac{85}{26} \frac{77}{23} \frac{84}{18} \frac{104}{12} \frac{101}{11} \frac{98}{11} \frac{100}{13} \frac{106}{14} \frac{106}{17} \frac{83}{27} \frac{74}{33} \frac{45}{50} \frac{40}{50}$$

$$\frac{88}{50} \frac{72}{35} \frac{62}{24} \frac{58}{19} \frac{94}{12} \frac{89}{13} \frac{94}{15} \frac{95}{17} \frac{77}{30} \frac{63}{35} \frac{36}{50} \frac{28}{50}$$

$$\frac{79}{50} \frac{60}{31} \frac{50}{23} \frac{46}{18} \frac{81}{14} \frac{88}{12} \frac{84}{10} \frac{81}{14} \frac{86}{19} \frac{66}{28} \frac{54}{34} \frac{26}{50} \frac{15}{50}$$

Sta.	+	π	-	Elev.
		952.59		
27	+50			45.3
28				46.1
	+50			47.0
29				48.3
	+50			49.1
30				49.8
	+50			50.4
T.P.	12.61	963.95	1.25	951.34
31				51.4
	+50			52.5
32				53.7
	+50			55.1

Lt

K

Rt

$$\frac{71}{50} \quad \frac{52}{31} \quad \frac{42}{22} \quad \frac{48}{17} \quad \frac{79}{12} \quad \frac{75}{10} \quad \frac{73}{10} \quad \frac{75}{10} \quad \frac{80}{14} \quad \frac{58}{16} \quad \frac{44}{22} \quad \frac{42}{27} \quad \frac{23}{30} \quad \frac{15}{50}$$

$$\frac{64}{50} \quad \frac{51}{36} \quad \frac{44}{24} \quad \frac{42}{19} \quad \frac{44}{16} \quad \frac{70}{13} \quad \frac{66}{11} \quad \frac{65}{10} \quad \frac{68}{13} \quad \frac{71}{16} \quad \frac{51}{21} \quad \frac{48}{28} \quad \frac{35}{50} \quad \frac{2.8}{50}$$

$$\frac{66}{50} \quad \frac{57}{35} \quad \frac{54}{23} \quad \frac{50}{17} \quad \frac{60}{14} \quad \frac{57}{11} \quad \frac{56}{14} \quad \frac{61}{17} \quad \frac{42}{29} \quad \frac{38}{50} \quad \frac{34}{50}$$

$$\frac{74}{50} \quad \frac{67}{35} \quad \frac{54}{23} \quad \frac{50}{18} \quad \frac{51}{14} \quad \frac{43}{12} \quad \frac{48}{14} \quad \frac{40}{28} \quad \frac{33}{40} \quad \frac{32}{50} \quad \frac{3.2}{50}$$

$$\frac{68}{50} \quad \frac{60}{35} \quad \frac{57}{25} \quad \frac{51}{21} \quad \frac{48}{17} \quad \frac{44}{16} \quad \frac{35}{12} \quad \frac{37}{14} \quad \frac{30}{28} \quad \frac{27}{38} \quad \frac{27}{50} \quad \frac{22}{50}$$

$$\frac{59}{50} \quad \frac{55}{32} \quad \frac{45}{21} \quad \frac{40}{18} \quad \frac{36}{16} \quad \frac{28}{10} \quad \frac{29}{12} \quad \frac{31}{14} \quad \frac{23}{28} \quad \frac{20}{38} \quad \frac{1.7}{39} \quad \frac{1.6}{50}$$

$$\frac{60}{50} \quad \frac{51}{29} \quad \frac{39}{20} \quad \frac{32}{18} \quad \frac{22}{10} \quad \frac{21}{12} \quad \frac{23}{14} \quad \frac{16}{27} \quad \frac{1.2}{38} \quad \frac{0.8}{50} \quad \frac{0.2}{50}$$

$$\frac{162}{50} \quad \frac{156}{32} \quad \frac{142}{20} \quad \frac{135}{17} \quad \frac{12.6}{10} \quad \frac{126}{10} \quad \frac{128}{12} \quad \frac{12.9}{13} \quad \frac{116}{27} \quad \frac{113}{39} \quad \frac{11.0}{50}$$

$$\frac{158}{50} \quad \frac{147}{37} \quad \frac{131}{23} \quad \frac{122}{17} \quad \frac{122}{15} \quad \frac{115}{12} \quad \frac{115}{13} \quad \frac{109}{27} \quad \frac{103}{39} \quad \frac{97}{50} \quad \frac{97}{50}$$

$$\frac{146}{50} \quad \frac{139}{34} \quad \frac{117}{22} \quad \frac{112}{19} \quad \frac{103}{13} \quad \frac{104}{14} \quad \frac{96}{27} \quad \frac{79}{39} \quad \frac{75}{50} \quad \frac{74}{50}$$

$$\frac{130}{50} \quad \frac{114}{33} \quad \frac{95}{20} \quad \frac{91}{14} \quad \frac{97}{14} \quad \frac{89}{12} \quad \frac{91}{13} \quad \frac{81}{27} \quad \frac{59}{38} \quad \frac{54}{50} \quad \frac{49}{50}$$

Sta	+	π	-	Elev.
		963.95		
33				56.5
	+50			58.0
34				59.2
I.P.	8.40	968.43	3.92	962.03
	+50			60.0
35				60.5
	+50			60.5
B.M.	3.86	965.89	6.41	962.02 (962.02)
36				61.0
	+50			60.2
	+55			60.2
37				58.8
	+50			57.1

Lt

A

Rt

$$\frac{106}{50} \quad \frac{81}{24} \quad \frac{71}{19} \quad \frac{72}{15} \quad \frac{82}{13} \quad \frac{75}{10} \quad \frac{75}{10} \quad \frac{77}{12} \quad \frac{70}{14} \quad \frac{55}{19} \quad \frac{50}{27} \quad \frac{45}{37} \quad \frac{40}{50}$$

$$\frac{81}{50} \quad \frac{63}{25} \quad \frac{53}{20} \quad \frac{59}{15} \quad \frac{66}{13} \quad \frac{64}{10} \quad \frac{40}{9} \quad \frac{62}{12} \quad \frac{65}{13} \quad \frac{57}{13} \quad \frac{46}{20} \quad \frac{44}{26} \quad \frac{32}{32} \quad \frac{27}{50}$$

$$\frac{57}{50} \quad \frac{43}{28} \quad \frac{38}{22} \quad \frac{45}{15} \quad \frac{53}{15} \quad \frac{48}{7} \quad \frac{49}{9} \quad \frac{52}{11} \quad \frac{31}{11} \quad \frac{23}{24} \quad \frac{17}{35} \quad \frac{09}{50}$$

$$\frac{88}{50} \quad \frac{78}{30} \quad \frac{75}{27} \quad \frac{77}{20} \quad \frac{87}{19} \quad \frac{84}{10} \quad \frac{84}{6} \quad \frac{86}{8} \quad \frac{56}{19} \quad \frac{53}{31} \quad \frac{43}{50} \quad \frac{35}{50}$$

$$\frac{88}{50} \quad \frac{76}{33} \quad \frac{74}{26} \quad \frac{81}{24} \quad \frac{81}{21} \quad \frac{77}{13} \quad \frac{79}{8} \quad \frac{66}{15} \quad \frac{43}{33} \quad \frac{29}{33} \quad \frac{22}{50}$$

$$\frac{77}{50} \quad \frac{71}{33} \quad \frac{77}{23} \quad \frac{74}{16} \quad \frac{79}{1} \quad \frac{71}{8} \quad \frac{68}{13} \quad \frac{35}{28} \quad \frac{29}{28} \quad \frac{22}{50}$$

Top Bolt at N.E. Cor. of Base of Gas Pump in Streetway Farm

$$\frac{35}{50} \quad \frac{35}{33} \quad \frac{53}{30} \quad \frac{49}{17} \quad \frac{53}{2} \quad \frac{49}{6} \quad \frac{44}{9} \quad \frac{23}{18} \quad \frac{17}{32} \quad \frac{14}{50} \quad \frac{07}{50}$$

$$\frac{35}{50} \quad \frac{36}{34} \quad \frac{65}{30} \quad \frac{56}{17} \quad \frac{57}{3} \quad \frac{57}{6} \quad \frac{45}{18} \quad \frac{35}{33} \quad \frac{22}{33} \quad \frac{14}{50}$$

$$\frac{50}{50} \quad \frac{58}{27} \quad \frac{56}{17} \quad \frac{57}{17}$$

$$\frac{67}{50} \quad \frac{73}{30} \quad \frac{75}{23} \quad \frac{71}{12} \quad \frac{71}{6} \quad \frac{72}{7} \quad \frac{56}{11} \quad \frac{39}{17} \quad \frac{38}{21} \quad \frac{25}{35} \quad \frac{27}{35} \quad \frac{21}{50}$$

$$\frac{80}{50} \quad \frac{84}{30} \quad \frac{93}{21} \quad \frac{88}{10} \quad \frac{88}{5} \quad \frac{89}{7} \quad \frac{95}{10} \quad \frac{73}{15} \quad \frac{45}{20} \quad \frac{39}{25} \quad \frac{28}{35} \quad \frac{27}{35} \quad \frac{30}{50}$$

Sta	+	Σ	-	Elev.
		965.88'		
38				55.4
	+50			53.6
T.P.	4.67	958.29'	12.26	958.62'
	+75			52.5
39				51.5
	+50			49.3
40				47.2
	+50			45.1
T.P.	0.84	945.94'	13.19	945.10
41				43.2
B.M.	6.06	945.92'	6.06	939.88
	+50			40.8
B.M.			6.01	939.91
42				37.7
	+50			34.9
T.P.	0.68	939.61'	6.99	938.93

Lt.

4

Rt.

$\frac{92}{50}$	$\frac{99}{29}$	$\frac{107}{19}$	$\frac{110}{16}$	$\frac{105}{6}$	$\frac{105}{10}$	$\frac{109}{10}$	$\frac{115}{12}$	$\frac{115}{13}$	$\frac{83}{15}$	$\frac{63}{22}$	$\frac{40}{28}$	$\frac{46}{37}$	$\frac{55}{50}$
-----------------	-----------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{89}{50}$	$\frac{83}{42}$	$\frac{102}{38}$	$\frac{102}{30}$	$\frac{107}{20}$	$\frac{127}{16}$	$\frac{128}{15}$	$\frac{126}{14}$	$\frac{123}{10}$	$\frac{128}{12}$	$\frac{133}{14}$	$\frac{133}{15}$	$\frac{112}{17}$	$\frac{99}{26}$	$\frac{77}{31}$	$\frac{88}{50}$
-----------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------

Ksta-38450

$\frac{1.4}{50}$	$\frac{09}{29}$	$\frac{1.0}{22}$	$\frac{61}{16}$	$\frac{64}{13}$	$\frac{61}{10}$	$\frac{58}{10}$	$\frac{58}{16}$	$\frac{63}{20}$	$\frac{47}{26}$	$\frac{48}{31}$	$\frac{20}{50}$
------------------	-----------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{2.3}{50}$	$\frac{1.2}{33}$	$\frac{06}{26}$	$\frac{2.0}{22}$	$\frac{73}{16}$	$\frac{7.5}{13}$	$\frac{7.0}{7}$	$\frac{68}{11}$	$\frac{71}{17}$	$\frac{79}{17}$	$\frac{67}{25}$	$\frac{63}{30}$	$\frac{37}{50}$	$\frac{4.0}{50}$
------------------	------------------	-----------------	------------------	-----------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

$\frac{42}{50}$	$\frac{35}{33}$	$\frac{33}{26}$	$\frac{38}{22}$	$\frac{92}{16}$	$\frac{96}{13}$	$\frac{92}{8}$	$\frac{90}{10}$	$\frac{93}{14}$	$\frac{100}{16}$	$\frac{89}{25}$	$\frac{92}{29}$	$\frac{67}{50}$	$\frac{80}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------	-----------------

$\frac{73}{50}$	$\frac{66}{33}$	$\frac{69}{26}$	$\frac{77}{24}$	$\frac{115}{19}$	$\frac{112}{11}$	$\frac{111}{10}$	$\frac{116}{9}$	$\frac{119}{11}$	$\frac{98}{13}$	$\frac{100}{26}$	$\frac{109}{33}$	$\frac{120}{50}$
-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	------------------	-----------------	------------------	------------------	------------------

$\frac{113}{50}$	$\frac{103}{34}$	$\frac{113}{30}$	$\frac{118}{29}$	$\frac{135}{24}$	$\frac{132}{17}$	$\frac{132}{6}$	$\frac{141}{8}$	$\frac{124}{21}$	$\frac{128}{26}$	$\frac{142}{33}$	$\frac{147}{50}$	$\frac{155}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{23}{50}$	$\frac{26}{27}$	$\frac{26}{17}$	$\frac{28}{5}$	$\frac{32}{2}$	$\frac{27}{14}$	$\frac{26}{28}$	$\frac{54}{50}$
-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------

$\frac{38}{50}$	$\frac{43}{34}$	$\frac{42}{24}$	$\frac{47}{11}$	$\frac{52}{8}$	$\frac{48}{7}$	$\frac{51}{25}$	$\frac{64}{50}$	$\frac{76}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------

Spt. in 16.0. 55' Rt. 41+25

$\frac{56}{50}$	$\frac{65}{36}$	$\frac{62}{27}$	$\frac{71}{13}$	$\frac{65}{12}$	$\frac{82}{25}$	$\frac{94}{50}$	$\frac{114}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

$\frac{80}{50}$	$\frac{82}{39}$	$\frac{80}{29}$	$\frac{86}{16}$	$\frac{96}{14}$	$\frac{110}{27}$	$\frac{128}{50}$	$\frac{144}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

Sta	+	π	-	Elev
		939.61		
43				33.2
	+50			32.0
44				29.7
	+50			27.8
T.P.	0.45	930.57	9.49	930.12
45				25.9
	+50			24.8
	+84			23.6
46				24.0
	+30			25.6
	+70			26.5
47				25.5

Lt

L

Rt

$$\frac{38}{50} \frac{39}{41} \frac{35}{39} \frac{35}{30} \frac{42}{17} \frac{52}{14} \frac{55}{13} \frac{64}{25} \frac{76}{50} \frac{89}{50}$$

$$\frac{45}{50} \frac{58}{41} \frac{55}{34} \frac{55}{27} \frac{62}{13} \frac{67}{10} \frac{70}{10} \frac{76}{25} \frac{87}{50} \frac{97}{50}$$

$$\frac{69}{50} \frac{75}{41} \frac{81}{40} \frac{73}{38} \frac{72}{26} \frac{77}{14} \frac{90}{11} \frac{89}{6} \frac{99}{15} \frac{105}{29} \frac{110}{29} \frac{123}{50}$$

$$\frac{91}{50} \frac{93}{39} \frac{90}{34} \frac{87}{24} \frac{91}{12} \frac{112}{9} \frac{118}{15} \frac{128}{16} \frac{141}{30} \frac{170}{50}$$

$$\frac{21}{50} \frac{12}{22} \frac{16}{10} \frac{37}{6} \frac{47}{15} \frac{66}{30} \frac{82}{30} \frac{96}{50}$$

$$\frac{39}{50} \frac{30}{30} \frac{26}{20} \frac{34}{6} \frac{57}{3} \frac{58}{15} \frac{75}{15} \frac{82}{20} \frac{95}{50}$$

$$\frac{48}{50} \frac{38}{34} \frac{35}{18} \frac{43}{5} \frac{70}{15} \frac{82}{15} \frac{89}{30} \frac{101}{50}$$

$$\frac{57}{50} \frac{43}{30} \frac{38}{16} \frac{66}{2} \frac{77}{9} \frac{82}{27} \frac{89}{27} \frac{100}{50}$$

$$\frac{57}{50} \frac{50}{28} \frac{43}{15} \frac{50}{3} \frac{70}{10} \frac{82}{10} \frac{87}{25} \frac{101}{50}$$

$$\frac{59}{50} \frac{60}{26} \frac{50}{22} \frac{47}{10} \frac{51}{7} \frac{55}{8} \frac{75}{15} \frac{85}{30} \frac{86}{30} \frac{98}{50}$$

$$\frac{58}{50} \frac{59}{35} \frac{58}{20} \frac{51}{18} \frac{51}{10} \frac{58}{10} \frac{75}{12} \frac{85}{15} \frac{92}{20} \frac{96}{32} \frac{98}{50}$$

Sta.	+	π	-	Elev.
		930.57		
47	+50			25.5
48				25.2
	+50			25.3
49				25.6
	+50			26.0
50				27.6
T.P.	7.25	935.34	2.48	928.09
	+50			28.4
51				29.3
	+50			30.1
52				32.5
T.P.	5.96	941.04	0.26	935.08
	+50			32.5

LH

K

RH

$$\frac{51}{50} \frac{54}{37} \frac{57}{15} \frac{53}{8} \frac{51}{17} \frac{61}{17} \frac{83}{21} \frac{93}{27} \frac{102}{50}$$

$$\frac{46}{50} \frac{54}{25} \frac{57}{7} \frac{54}{16} \frac{51}{29} \frac{57}{33} \frac{88}{38} \frac{91}{50}$$

$$\frac{39}{50} \frac{45}{35} \frac{51}{16} \frac{53}{7} \frac{54}{24} \frac{47}{39} \frac{51}{43} \frac{86}{50}$$

$$\frac{32}{50} \frac{40}{30} \frac{48}{13} \frac{50}{9} \frac{50}{15} \frac{48}{33} \frac{47}{50}$$

$$\frac{29}{50} \frac{31}{36} \frac{40}{16} \frac{46}{17} \frac{45}{28} \frac{44}{42} \frac{42}{50}$$

$$\frac{15}{50} \frac{25}{26} \frac{29}{11} \frac{30}{23} \frac{33}{29} \frac{40}{32} \frac{47}{35} \frac{38}{50} \frac{37}{50}$$

top & stake sta. 50 to 0

$$\frac{44}{50} \frac{58}{31} \frac{62}{17} \frac{69}{25} \frac{75}{33} \frac{81}{34} \frac{89}{35} \frac{86}{50} \frac{80}{50}$$

$$\frac{37}{50} \frac{46}{33} \frac{58}{19} \frac{60}{22} \frac{67}{30} \frac{70}{31} \frac{77}{34} \frac{73}{50} \frac{70}{50}$$

$$\frac{27}{50} \frac{36}{33} \frac{43}{16} \frac{52}{22} \frac{52}{25} \frac{70}{29} \frac{65}{39} \frac{61}{50} \frac{62}{50}$$

$$\frac{16}{50} \frac{24}{22} \frac{29}{8} \frac{23}{3} \frac{28}{11} \frac{39}{14} \frac{59}{28} \frac{54}{43} \frac{54}{50} \frac{44}{50}$$

$$\frac{73}{50} \frac{77}{35} \frac{78}{21} \frac{84}{7} \frac{85}{2} \frac{87}{6} \frac{111}{9} \frac{108}{19} \frac{104}{26} \frac{106}{31} \frac{108}{34} \frac{95}{43} \frac{80}{50} \frac{81}{50}$$

Sta	+	π	-	Elev
		941.04		31.0
53				
+26				31.6
+50				32.0
B.M.	1.59	941.02	1.59	939.45 (939.43)
+79				32.5
+856 Thru cont Lt.				32.5
54				32.5
+25				33.2
+50				33.0
55				32.3
+50				33.5
56				32.8

Lt

K

Rt

$$\frac{44}{50} \frac{52}{33} \frac{62}{15} \frac{69}{9} \frac{101}{3} \frac{100}{9} \frac{98}{20} \frac{100}{21} \frac{101}{23} \frac{94}{33} \frac{83}{50} \frac{84}{50}$$

$$\frac{36}{50} \frac{46}{32} \frac{55}{17} \frac{66}{14} \frac{96}{7} \frac{94}{17} \frac{99}{19} \frac{93}{33} \frac{88}{50} \frac{95}{50}$$

$$\frac{38}{50} \frac{43}{36} \frac{55}{23} \frac{65}{20} \frac{90}{15} \frac{90}{12} \frac{93}{15} \frac{94}{16} \frac{88}{29} \frac{84}{50} \frac{104}{50}$$

Top N.E. Cor Floor of Porch 60' Lt of 53+50

$$\frac{40}{50} \frac{47}{36} \frac{52}{29} \frac{85}{22} \frac{87}{18} \frac{85}{17} \frac{85}{31} \frac{92}{50} \frac{93}{50}$$

$$\frac{56}{50} \frac{82}{29} \frac{86}{20} \frac{85}{10} \frac{85}{20} \frac{84}{36} \frac{91}{50} \frac{87}{50}$$

$$\frac{52}{50} \frac{64}{41} \frac{74}{32} \frac{84}{22} \frac{83}{12} \frac{85}{5} \frac{81}{27} \frac{76}{50} \frac{79}{50}$$

$$\frac{46}{50} \frac{63}{35} \frac{87}{31} \frac{84}{28} \frac{82}{16} \frac{83}{6} \frac{78}{15} \frac{76}{30} \frac{74}{50} \frac{70}{50}$$

$$\frac{58}{50} \frac{68}{36} \frac{87}{32} \frac{79}{18} \frac{82}{7} \frac{80}{18} \frac{70}{32} \frac{67}{50} \frac{62}{50}$$

$$\frac{72}{50} \frac{78}{31} \frac{85}{27} \frac{77}{13} \frac{82}{2} \frac{87}{12} \frac{96}{31} \frac{97}{50} \frac{92}{50}$$

$$\frac{69}{50} \frac{66}{40} \frac{77}{20} \frac{84}{19} \frac{77}{13} \frac{75}{9} \frac{82}{15} \frac{97}{32} \frac{112}{50} \frac{118}{50}$$

$$\frac{50}{44} \frac{50}{33} \frac{53}{21} \frac{71}{10} \frac{82}{5} \frac{82}{1} \frac{76}{18} \frac{72}{33} \frac{78}{38} \frac{102}{50} \frac{103}{50}$$

Sta	+	π	-	Elev
		941.02		
56	+25			35.1
T.P.	1375	950.53	424	936.78
	+50.58			36.0
57				39.1
	+27			39.9
	+67			38.6
58				38.6
	+30			40.9
	+60			45.2
	+79			48.9
59				49.5
	+35			47.4

Lt

K

Rt

$$\frac{40}{50} \quad \frac{46}{35} \quad \frac{50}{18} \quad \frac{59}{\quad} \quad \frac{81}{10} \quad \frac{84}{19} \quad \frac{72}{22} \quad \frac{68}{34} \quad \frac{71}{50}$$

$$\frac{12.8}{50} \quad \frac{13.2}{32} \quad \frac{13.9}{21} \quad \frac{14.5}{17} \quad \frac{14.3}{24} \quad \frac{14.8}{35} \quad \frac{16.9}{50}$$

$$\frac{9.0}{50} \quad \frac{9.5}{34} \quad \frac{10.6}{22} \quad \frac{10.4}{17} \quad \frac{11.4}{\quad} \quad \frac{12.5}{16} \quad \frac{13.5}{33} \quad \frac{13.8}{50}$$

$$\frac{7.8}{50} \quad \frac{9.0}{33} \quad \frac{10.4}{20} \quad \frac{10.3}{14} \quad \frac{10.6}{\quad} \quad \frac{12.4}{15} \quad \frac{13.2}{32} \quad \frac{13.5}{50}$$

$$\frac{6.4}{50} \quad \frac{8.2}{30} \quad \frac{10.3}{15} \quad \frac{11.3}{9} \quad \frac{11.9}{\quad} \quad \frac{13.3}{15} \quad \frac{13.4}{31} \quad \frac{13.9}{50}$$

$$\frac{3.3}{50} \quad \frac{7.5}{30} \quad \frac{10.6}{13} \quad \frac{11.9}{\quad} \quad \frac{12.5}{14} \quad \frac{13.2}{33} \quad \frac{15.1}{50}$$

$$\frac{0.9}{50} \quad \frac{5.0}{29} \quad \frac{7.9}{13} \quad \frac{9.6}{\quad} \quad \frac{10.4}{16} \quad \frac{12.4}{32} \quad \frac{13.7}{50}$$

$$\frac{+1.0}{50} \quad \frac{1.9}{27} \quad \frac{3.4}{9} \quad \frac{5.3}{\quad} \quad \frac{7.9}{16} \quad \frac{9.1}{33} \quad \frac{11.5}{50}$$

$$\frac{+1.4}{50} \quad \frac{+0.7}{34} \quad \frac{2.7}{19} \quad \frac{1.4}{5} \quad \frac{1.6}{\quad} \quad \frac{3.1}{7} \quad \frac{5.7}{25} \quad \frac{8.2}{38} \quad \frac{10.0}{50} \quad \checkmark$$

$$\frac{+2.3}{50} \quad \frac{+1.5}{38} \quad \frac{+1.0}{22} \quad \frac{1.1}{4} \quad \frac{1.0}{\quad} \quad \frac{2.3}{7} \quad \frac{4.5}{21} \quad \frac{7.3}{38} \quad \frac{8.5}{50}$$

$$\frac{+1.6}{50} \quad \frac{+0.3}{32} \quad \frac{0.6}{17} \quad \frac{3.1}{\quad} \quad \frac{4.8}{7} \quad \frac{6.2}{25} \quad \frac{7.9}{40} \quad \frac{8.4}{50}$$

Sta	+	π	-	Elev.
		950.53		
59 +65				46.2
60				45.6
+36				45.0
+66				42.3
61				48.8
+28				37.5
+64				39.4
62				39.9
T.P.	10.59	951.57	9.35	940.98
+50				44.6
63				46.1
+28				45.3

Lt

4

Rt

$$\frac{0.2}{50} \frac{0.7}{38} \frac{2.4}{16} \frac{4.3}{\quad} \frac{5.8}{6} \frac{7.2}{22} \frac{8.2}{37} \frac{8.8}{50}$$

$$\frac{2.2}{50} \frac{2.8}{33} \frac{3.7}{15} \frac{4.9}{\quad} \frac{5.4}{4} \frac{7.0}{11} \frac{7.7}{31} \frac{8.5}{50}$$

$$\frac{4.8}{50} \frac{5.5}{32} \frac{5.3}{15} \frac{5.5}{\quad} \frac{5.6}{7} \frac{7.2}{10} \frac{7.7}{26} \frac{9.4}{50}$$

$$\frac{5.3}{50} \frac{7.0}{36} \frac{7.2}{14} \frac{8.3}{10} \frac{8.2}{\quad} \frac{8.0}{7} \frac{8.6}{12} \frac{9.6}{21} \frac{10.4}{34} \frac{11.2}{50}$$

$$\frac{6.2}{50} \frac{7.8}{34} \frac{9.9}{21} \frac{11.2}{10} \frac{11.7}{\quad} \frac{11.6}{7} \frac{12.5}{11} \frac{13.1}{25} \frac{12.7}{37} \frac{12.9}{50}$$

$$\frac{7.6}{50} \frac{10.2}{31} \frac{11.8}{19} \frac{12.7}{11} \frac{13.0}{\quad} \frac{12.7}{3} \frac{13.2}{8} \frac{13.4}{21} \frac{12.8}{34} \frac{12.3}{50}$$

$$\frac{10.9}{50} \frac{12.4}{30} \frac{12.7}{20} \frac{11.8}{9} \frac{11.1}{\quad} \frac{10.8}{4} \frac{11.2}{7} \frac{11.3}{23} \frac{11.5}{38} \frac{12.0}{50}$$

$$\frac{12.8}{50} \frac{12.2}{32} \frac{10.9}{13} \frac{10.6}{\quad} \frac{11.1}{8} \frac{12.3}{26} \frac{12.6}{50}$$

Transfer Lt 62/106

$$\frac{7.8}{50} \frac{7.1}{28} \frac{6.7}{12} \frac{7.0}{\quad} \frac{7.7}{6} \frac{9.5}{25} \frac{11.1}{50}$$

$$\frac{55}{50} \frac{46}{31} \frac{44}{18} \frac{51}{6} \frac{55}{8} \frac{67}{27} \frac{83}{50} \frac{100}{50}$$

$$\frac{56}{50} \frac{50}{40} \frac{53}{22} \frac{59}{8} \frac{63}{\quad} \frac{69}{6} \frac{82}{32} \frac{104}{50}$$

Sta	+	π	-	Elev
		951.57		
63	+66			41.9
64				35.9
	1.01	939.69	12.89	938.68
	+33			31.1
	+68			28.8
65				27.9
	+50			27.8
	+71			29.0
66				31.4
	+38			33.2
	+70			32.8
67				34.3

Lt

K

Rt

$$\frac{82}{50} \frac{80}{41} \frac{88}{27} \frac{91}{18} \frac{99}{4} \frac{97}{6} \frac{101}{20} \frac{102}{33} \frac{101}{50} \frac{107}{50}$$

$$\frac{128}{50} \frac{138}{36} \frac{147}{21} \frac{150}{5} \frac{157}{8} \frac{160}{24} \frac{147}{33} \frac{144}{50} \frac{141}{50}$$

$$\frac{45}{50} \frac{64}{33} \frac{78}{21} \frac{86}{7} \frac{86}{10} \frac{82}{26} \frac{69}{50} \frac{80}{50}$$

$$\frac{78}{50} \frac{90}{37} \frac{101}{22} \frac{105}{10} \frac{109}{11} \frac{110}{27} \frac{114}{50} \frac{119}{50}$$

$$\frac{96}{50} \frac{110}{31} \frac{117}{20} \frac{118}{20} \frac{120}{28} \frac{128}{50}$$

$$\frac{102}{50} \frac{106}{32} \frac{117}{14} \frac{119}{23} \frac{120}{35} \frac{111}{50} \frac{110}{50}$$

$$\frac{98}{50} \frac{98}{27} \frac{103}{13} \frac{107}{28} \frac{110}{40} \frac{98}{50} \frac{101}{50}$$

$$\frac{70}{50} \frac{67}{30} \frac{70}{14} \frac{83}{12} \frac{98}{25} \frac{101}{36} \frac{104}{50} \frac{96}{50}$$

$$\frac{38}{50} \frac{39}{29} \frac{50}{11} \frac{65}{13} \frac{87}{21} \frac{100}{36} \frac{102}{50} \frac{87}{50}$$

$$\frac{32}{50} \frac{32}{42} \frac{38}{29} \frac{52}{11} \frac{69}{12} \frac{87}{26} \frac{103}{44} \frac{102}{50} \frac{96}{50}$$

$$\frac{39}{50} \frac{36}{34} \frac{40}{18} \frac{54}{21} \frac{74}{33} \frac{81}{50} \frac{86}{50}$$

Sta	+	π	-	Elev.
		939.69		
67	+36			36.2
	+56			34.8
	+78			31.9
68				28.1
T.P.	11.04	939.85	10.88	928.81
	+30			26.4
	+45			24.9
69				25.5
	+50			27.6
70				34.4
	+26			38.4
	+36			34.7
T.P.	7.21	943.48	3.58	936.27

Lt.

K.

Rt.

$$\frac{30}{50} \quad \frac{25}{30} \quad \frac{28}{14} \quad \frac{35}{23} \quad \frac{53}{38} \quad \frac{41}{50} \quad \frac{67}{50}$$

$$\frac{38}{50} \quad \frac{37}{35} \quad \frac{39}{17} \quad \frac{49}{4} \quad \frac{58}{22} \quad \frac{66}{37} \quad \frac{75}{50}$$

$$\frac{56}{50} \quad \frac{66}{27} \quad \frac{77}{9} \quad \frac{78}{7} \quad \frac{83}{18} \quad \frac{87}{32} \quad \frac{100}{50} \quad \frac{112}{50}$$

$$\frac{77}{50} \quad \frac{88}{38} \quad \frac{101}{24} \quad \frac{112}{9} \quad \frac{116}{5} \quad \frac{121}{16} \quad \frac{125}{35} \quad \frac{124}{50} \quad \frac{132}{50}$$

Tep. Lake sta 68

$$\frac{78}{50} \quad \frac{95}{31} \quad \frac{138}{16} \quad \frac{135}{25} \quad \frac{140}{50} \quad \frac{139}{50}$$

$$\frac{135}{50} \quad \frac{14.3}{30} \quad \frac{15.0}{13} \quad \frac{150}{25} \quad \frac{149}{50} \quad \frac{13.8}{50}$$

$$\frac{14.5}{50} \quad \frac{14.8}{25} \quad \frac{14.4}{25} \quad \frac{14.2}{25} \quad \frac{13.1}{50}$$

$$\frac{13.7}{50} \quad \frac{13.6}{33} \quad \frac{12.9}{16} \quad \frac{12.3}{22} \quad \frac{10.7}{35} \quad \frac{10.5}{43} \quad \frac{10.1}{50} \quad \frac{7.3}{50}$$

$$\frac{95}{50} \quad \frac{79}{24} \quad \frac{65}{11} \quad \frac{55}{15} \quad \frac{48}{20} \quad \frac{64}{34} \quad \frac{59}{50} \quad \frac{63}{50}$$

$$\frac{40}{50} \quad \frac{28}{27} \quad \frac{1.9}{8} \quad \frac{15}{7} \quad \frac{61}{25} \quad \frac{52}{41} \quad \frac{59}{45} \quad \frac{2.3}{45} \quad \frac{2.3}{50}$$

$$\frac{27}{50} \quad \frac{2.0}{33} \quad \frac{12}{14} \quad \frac{0.9}{4} \quad \frac{52}{5} \quad \frac{58}{20} \quad \frac{49}{36} \quad \frac{56}{41} \quad \frac{2.1}{41} \quad \frac{2.3}{50}$$

Sta	+	π	-	Elev	
		943.48			
71				36.3	
	+44			36.7	
	+57			39.6	
72				39.8	
	+55			38.5	
73				38.1	
	+50			38.0	
B.M.	3.94	943.47	3.94	939.54	(939.53)
74				39.0	
B.M.	4.30	943.59	4.18	939.29	(939.29)
	+50			38.8	
75				38.9	
	+50			38.6	

K.A.

L.C.

M.B.

C.H.

Lt.

E.

Et.

$$\frac{47}{50} \frac{47}{35} \frac{47}{22} \frac{77}{16} \frac{72}{13} \frac{78}{16} \frac{50}{33} \frac{57}{50} \frac{63}{50}$$

$$\frac{39}{50} \frac{37}{32} \frac{69}{28} \frac{61}{13} \frac{68}{4} \frac{42}{23} \frac{51}{50} \frac{60}{50}$$

$$\frac{41}{50} \frac{40}{35} \frac{61}{31} \frac{57}{16} \frac{66}{4} \frac{39}{50} \frac{45}{17} \frac{49}{31} \frac{60}{50}$$

$$\frac{40}{50} \frac{39}{41} \frac{54}{38} \frac{49}{27} \frac{53}{14} \frac{44}{10} \frac{37}{29} \frac{40}{50} \frac{46}{50}$$

$$\frac{50}{50} \frac{47}{38} \frac{52}{26} \frac{44}{24} \frac{43}{17} \frac{50}{16} \frac{53}{39} \frac{54}{50} \frac{54}{50}$$

$$\frac{47}{50} \frac{52}{32} \frac{47}{25} \frac{48}{17} \frac{54}{50} \frac{60}{12} \frac{63}{30} \frac{65}{50}$$

$$\frac{48}{50} \frac{54}{29} \frac{49}{23} \frac{53}{11} \frac{55}{19} \frac{55}{38} \frac{55}{50} \frac{53}{50}$$

$$\frac{37}{50} \frac{50}{38} \frac{48}{29} \frac{53}{16} \frac{42}{13} \frac{45}{50} \frac{47}{50}$$

R.R. spike in 24" 0.50 R/L 73495

$$\frac{45}{50} \frac{41}{34} \frac{54}{23} \frac{48}{15} \frac{50}{5} \frac{48}{6} \frac{45}{22} \frac{46}{50} \frac{48}{50}$$

$$\frac{56}{50} \frac{48}{30} \frac{49}{17} \frac{47}{8} \frac{49}{9} \frac{55}{16} \frac{63}{18} \frac{51}{33} \frac{53}{50} \frac{52}{50}$$

$$\frac{66}{50} \frac{63}{24} \frac{50}{10} \frac{57}{13} \frac{66}{18} \frac{66}{36} \frac{52}{50} \frac{44}{50}$$

Sta	+	π	-	Elev
		943.59		
76				38.3
	+50			38.1
77				
	+50			
78				
	+50			
79				
B.M.		430	939.29	939.29 ✓

Lt

x

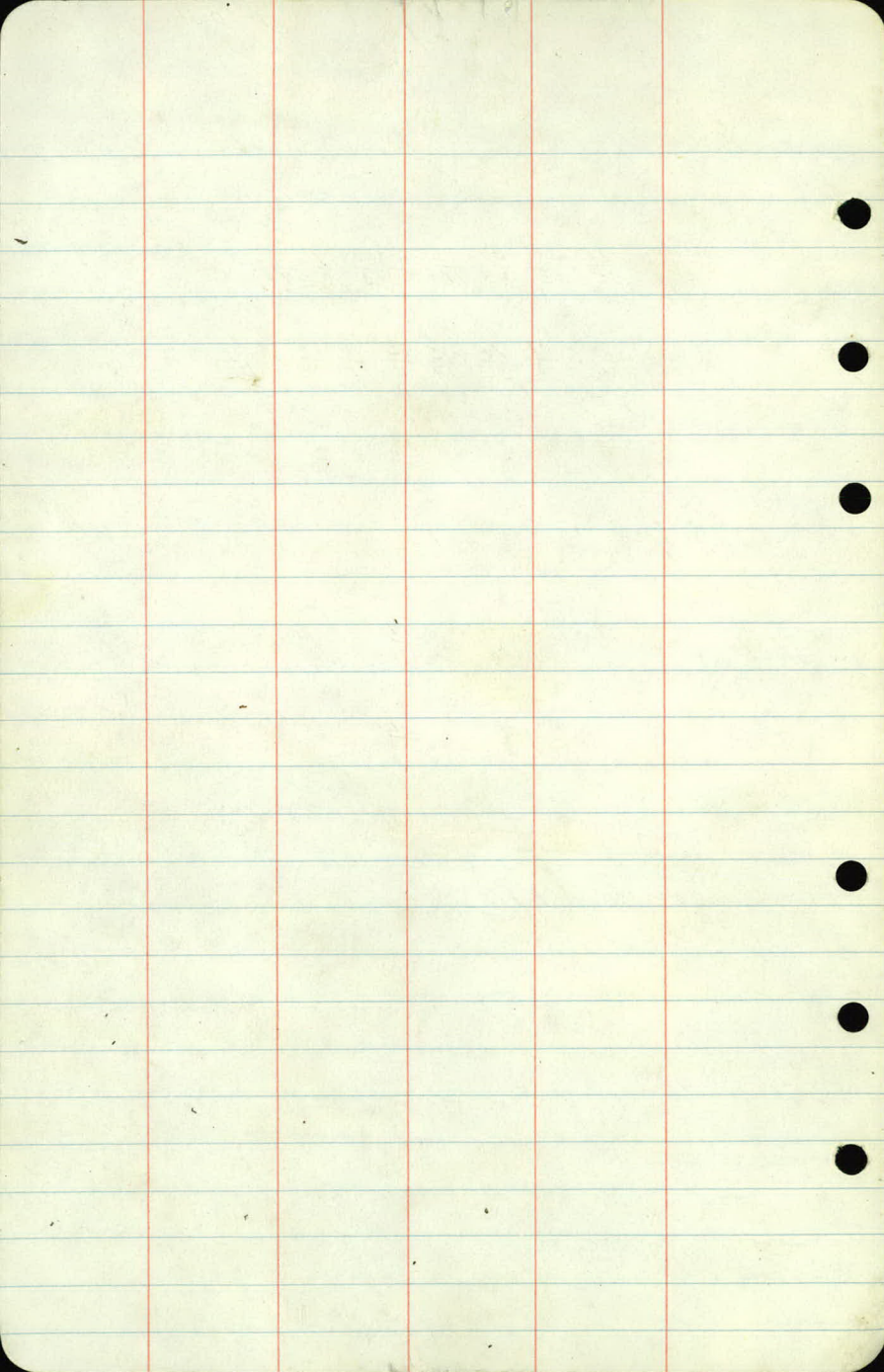
Rt

$$\frac{73}{50} \quad \frac{80}{33} \quad \frac{69}{23} \quad \frac{62}{17} \quad \frac{53}{14} \quad \frac{59}{21} \quad \frac{69}{27} \quad \frac{61}{50} \quad \frac{62}{50}$$

$$\frac{81}{50} \quad \frac{87}{31} \quad \frac{78}{22} \quad \frac{65}{17} \quad \frac{55}{14} \quad \frac{58}{24} \quad \frac{63}{41} \quad \frac{68}{50} \quad \frac{69}{50}$$

5350474438

R.R. spk. in 24' O. 50' Rt 73+95



①

Line Change

PORTLAND AVE

Short St to No. Co. Line

March 1950

Rec 3-27-50
P.M. L.C.

GB AM
MB KR

Sta.	PT	ALT	ARL	
8+39.35	PT	8°48'		N. 1°04 1/2 E
+25		8°17 1/2'		
8		7°25'		
+75		6°32 1/2'		
+50		5°40'		
+25		4°47 1/2'		$\Delta = 17.036'4$
+14.71	PI			$D = 7^\circ$
7		3°55'		$T = 126.79$
+75		3°02 1/2'		$L = 257.43$
+50		2°10'		$R = 819.02$
+25		1°17 1/2'		$E = 9.65$
6		0°25'		
5+87.92	PC	0°00'		
		121.32.		
+66.67	PT	7°30'		
+50		6°45'		
+25		5°37 1/2'		$\Delta = 15^\circ00'$
4		4°30'		$D = 9^\circ00'$
+83.90	PI			$T = 83.90$
+75		3.22 1/2'		$L = 166.67$
+50		2°15'		$R = 637.27$
3+25		1°07 1/2'		$E = 5.50'$
3+00	PC	0°00'		

2

30" Elm

60.75

520.00

333.50
5590.04
TP
φ

Short St

PP
6.61

61.95

140.55

1/4
Cor

TP
φ

110.74

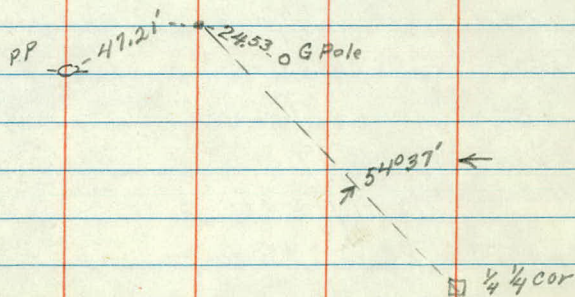
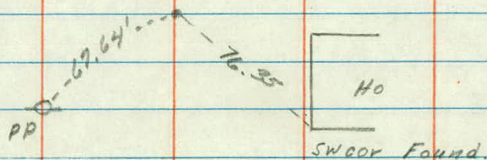
East Co.

40.60

40.30

0.00

Sta	Pt	Alt	LRT	
+11.78	PT		3°10'	N-23°45' $\frac{1}{2}$ W
16			2°59 $\frac{1}{2}$	
+75			2°37'	
+50			2°14 $\frac{1}{2}$	
+25			1°52'	
+05 ⁹³	PI			$\Delta = 6°20'$ RT D 3°00' T 105.68
15			1°29 $\frac{1}{2}$	N-30°05' $\frac{1}{2}$ W
+75			1°07'	
+50			0°44 $\frac{1}{2}$	
+25			0°22'	
14+00.67	PC		0°00'	
11+71.88	PT	15°35'		$\Delta = 31°10'$ D = 17° T = 94.34 L = 183.33 E = 12.88 R = 328.27
+50		13°43 $\frac{1}{2}$		
+25		11°36'		
11		9°28 $\frac{1}{2}$		
+82.89	PI	(31°10')		
+75		7°21'		N-1°04' $\frac{1}{2}$ E
+50		5°13 $\frac{1}{2}$		
+25		3°06'		
10		0°58 $\frac{1}{2}$		
9+88.5	PC	0°00'		



Sta	Pt.	Δ L+	Δ R+	W
27 + 02. ³⁷	P.T.		3° 30'	0° 14' 1/2
27			3° 28 1/2'	41
+ 75			3° 01'	✓
+ 50			2° 38 1/2'	
+ 25			2° 16'	Δ = 7° 00'
26			1° 53 1/2'	D = 3° 00'
+ 90. ³⁶	P.I.		7° 00'	T = 116.82
+ 75			1° 31'	L = 233.33
+ 50			1° 08 1/2'	R = 1910.08
+ 25			0° 46'	E = 3.57
25			0° 23 1/2'	
24 + 74. ⁰⁴	P.C.		0° 00'	N. 48° 19' 1/2 W
19 + 30. ⁰²	P.T.	12° 17'		
+ 25		11° 51 1/2'		
19		9° 44'		Δ = 24° 34'
+ 75		7° 36 1/2'		D = 17°
+ 59.16	PI	24° 34'		T = 73.65
+ 50		5° 29'		L = 144.51
+ 25		3° 21 1/2'		R = 338.27
18		1° 14'		E = 7.82
17 + 85. ⁵¹	P.C.	0° 00'		

(4)

60.45 --- 18" W.O.

69.48 ---

8"

TWN Oak

57.83 --- 15" O

26.88 --- 24" O

Sta	Pt	Alt	Aspt.
-----	----	-----	-------

+02.91	PT	24°04½'	
--------	----	---------	--

30		23°43½'	
----	--	---------	--

+75		20°43½'	
-----	--	---------	--

+50		17°43½'	
-----	--	---------	--

+25		14°43½'	
-----	--	---------	--

29+09.74	PI	48°09'	
----------	----	--------	--

29		11°43½'	
----	--	---------	--

+75		8°43½'	
-----	--	--------	--

+50		5°43½'	
-----	--	--------	--

+25		2°43½'	2°43½'
-----	--	--------	--------

28+02.29	P.C.	0°00'	
----------	------	-------	--

Δ 48°09'

D 24°

T = 107.45

L = 200.62

R = 240.49

E = 22.88

N 41° 10' 12" W

(5)

St Mont
N $\frac{1}{4}$ cor
Sec. 1

Mo County

1310.00

2x2 Hub

1.98

FP

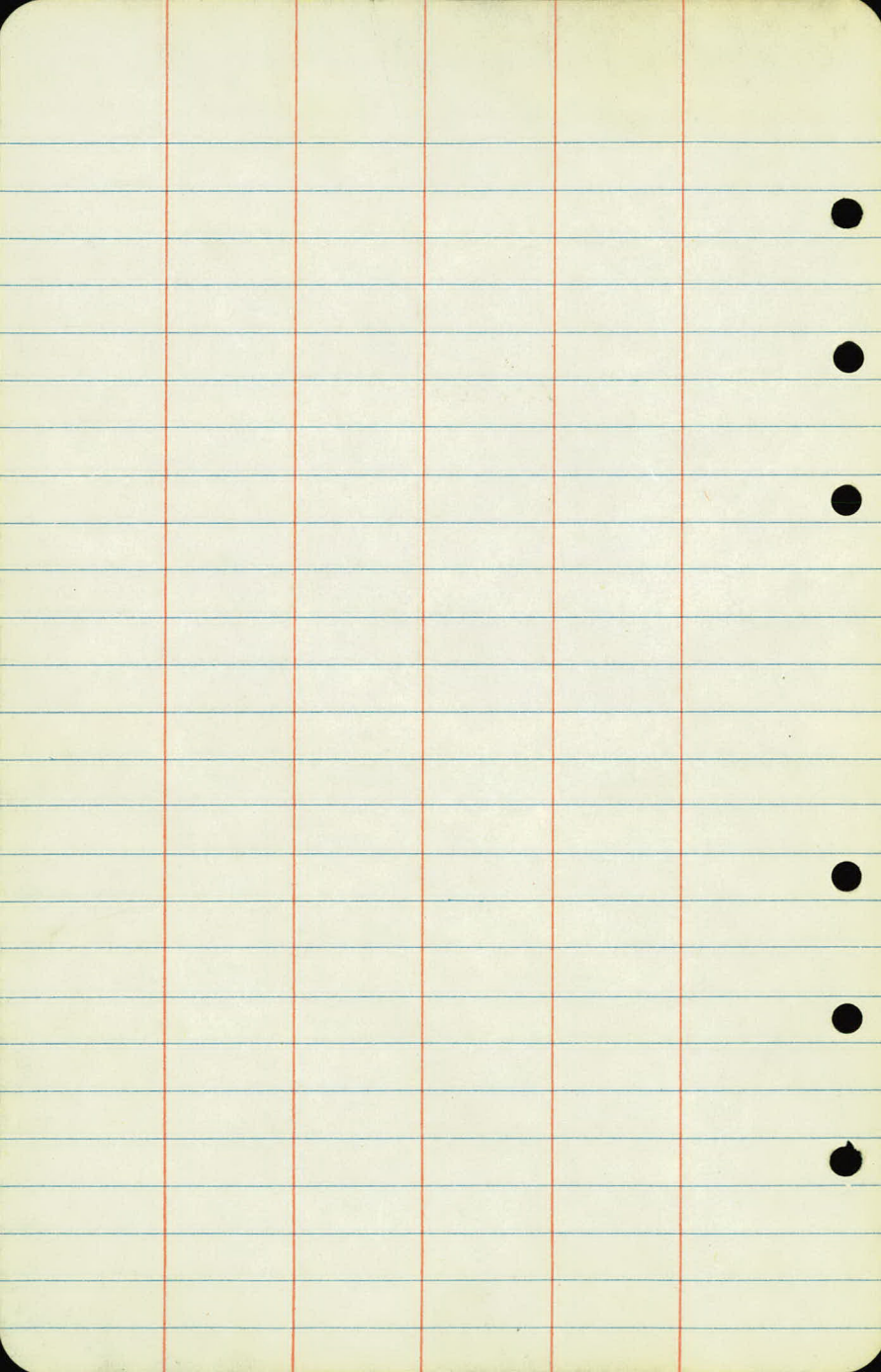
Boat Spk
= $\frac{1}{4}$ $\frac{1}{4}$ cor

1310.00

12.5

24" Oak

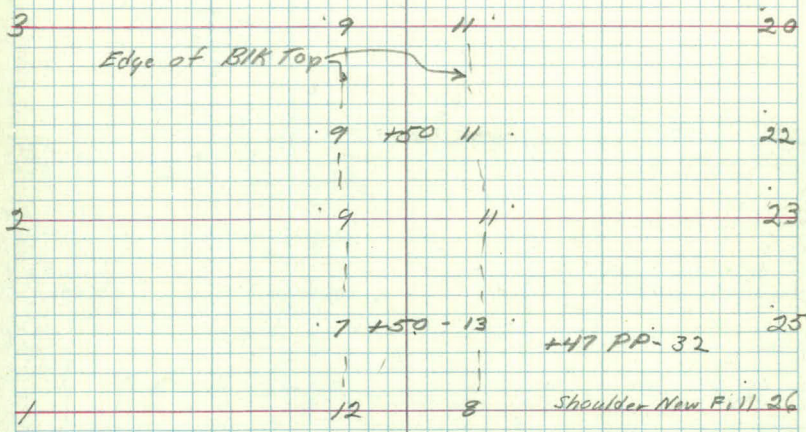
NE Cor
Sec. 1.



Topography

March 23 1950

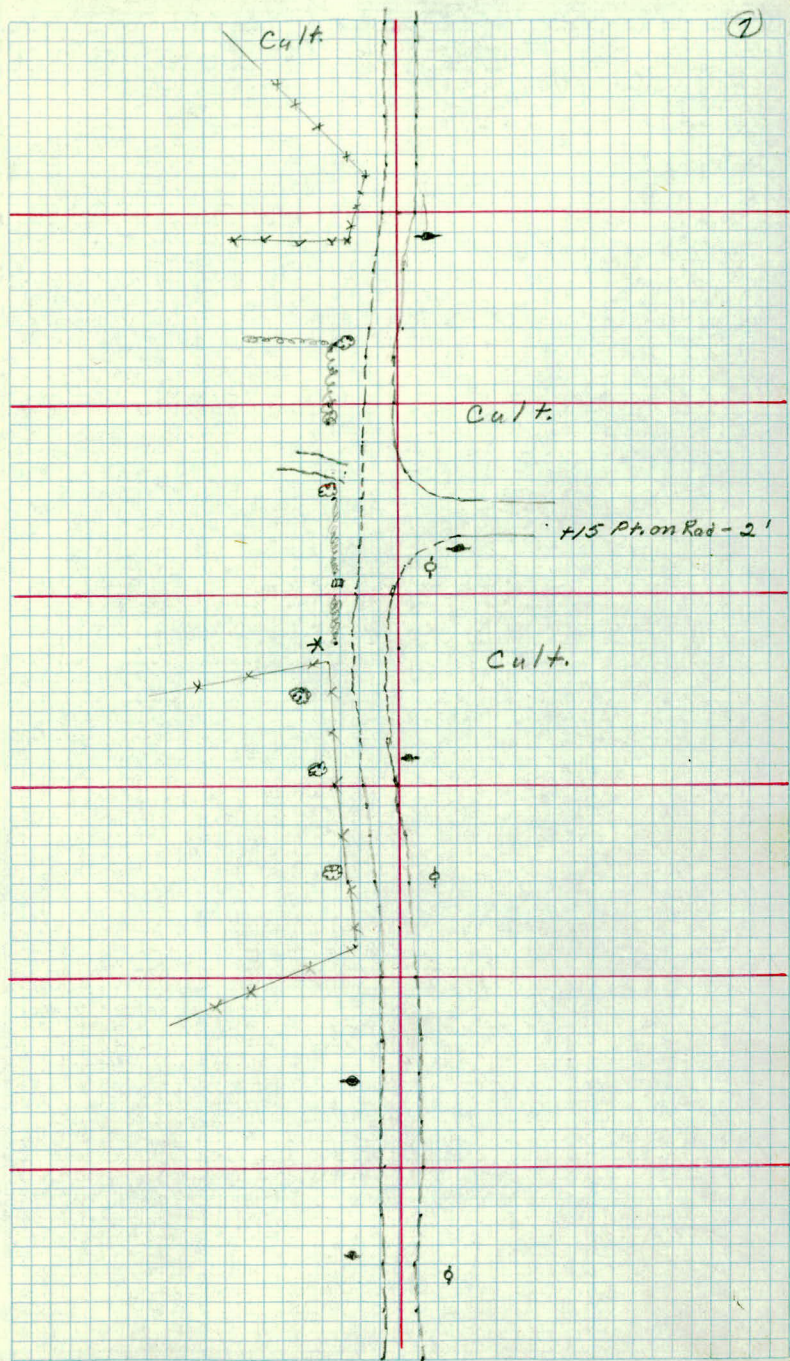
GB
AM
MB
KR

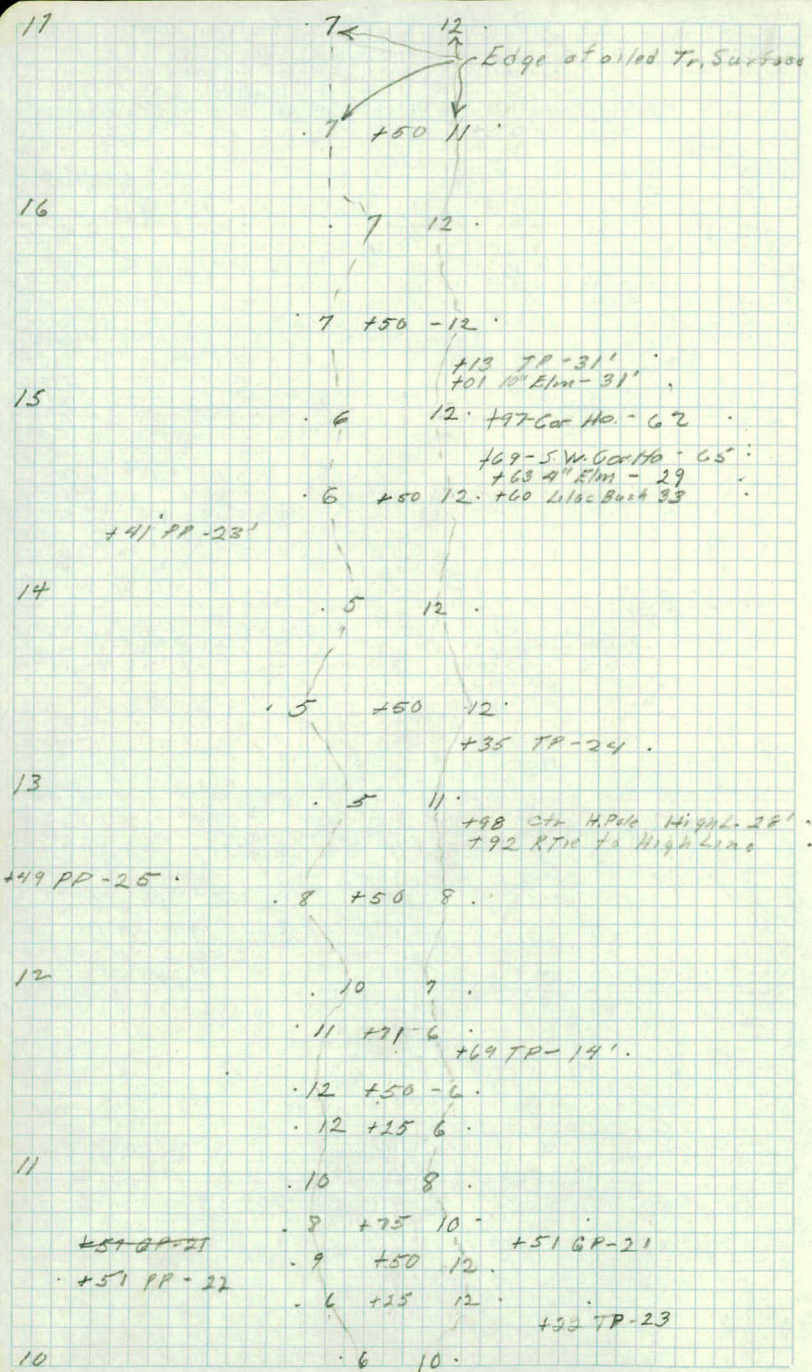


oil pp. surface

3

10	6	10	
	7 +88	10	
	7 +50 -10		
+19 Fe cor 16m			
9 R Tie to Fe	7	10	
+87 end Fe W-26	12	+70 3	+89-TP-17, Beg Fe
+31 cor Hedge-30	14	+39 2	
+81 Plum f-25	15	2 +25	
8 Hedge-32	17	1	
+90 Beg Lilac Hedge 35	19	1 +75	
+63 6 10' Ent-28			+64-end Rad -2'
+55-10' Elm-36		+50	+50 Beg R-31
+50 end Hedge-33	19	+25	+39 Approx Short St.
+04 4' conc step-28-33	20		+50 end Rad-31
+03-Beg R-2			+25 TP-32
7 Hedge 32	21	3	+15 PP-17
+75-8" Sp.-41			
+75 Beg Lilac Hedge-32	22	5 +15	
+71-R Tie Fe			
+66 Fe Cor-37	22	7 +50	
+47-24" BE-50			
+09 8" Quad BE-43	20	-5 +25	
+15 TP-7			+15 TP-7
6 Fe 33	18	0	
	17	+90-0	
	16	+75 2	
+55 24" BE-31			+52-PP-19
+50 Fe-27'	13	+50 5	
+26 R Tie to Fe			
+17 Fe cor-23			
5	9	9	
	9	+67 11	
	9	+50 10	
+45 TP-25			
	9	+25 11	
4	8	12	end Sh. Fill-20
	10	+75 10	
+54 TP-24			+46-PP-25
	10	+50 8	16
	9	+25 9	19
3	9	11	T/shoulder 20





26 N 5
23 deep.

33
26 Perron Yard.

Power Line

- +97 8"0 34'
- +86 8" TW 0 -33'
- +71 12"0 36'
- +69 SHLDR 0.0
- +28 2-STPS 37'
- +50 18"039' SHLDR RD 15' - 32'

23 FC 47'.

SHLDR 15' RD 24' - 42'

+77 15"0 531.

+50 SHLDR 20' RD 26' - 45'

22

SHLDR 15' RD 21' - 39' T.P. 55'

+57 SHLDR 0.0.

+56 TW 18"0 20'.

• +50 RD 11' - 28'

• +28 26"0 33'

• +20 18"0 34'

• +10 18" TW 10' 26'

21

• RD 2' - 20'

+76 RD 0.0.

• +76 RD 15'

+50 RD 2'.

• +50 RD 14'

• +06 T.P. 31'

20

RD 7'.

• RD 12'

+75 RD 7' SHLDR 12'.

• +75 RD 10'

+50 RD 7' SHLDR 13'.

• +50 RD 10'

+25 RD 8' SHLDR 14'.

• +25 RD 10'

19

RD 9'.

• +05 18"0 22'

• RD 7'

• +88 T.P. 16'

+75 RD 9'.

• +75 RD 7'

+50 RD 9'.

• +50 RD 8'

+25 RD 8'.

• +25 RD 8'

18

RD 7'.

RD 9'.

8 +85 9

6 - +50 -11

• +42 - 12"000 k - 32

• +41 - 15"000 k - 34

• +39 - Tw 10"0 - 32

• +36 - 12"000 k - 24

• +26 - T.P. - 27

17

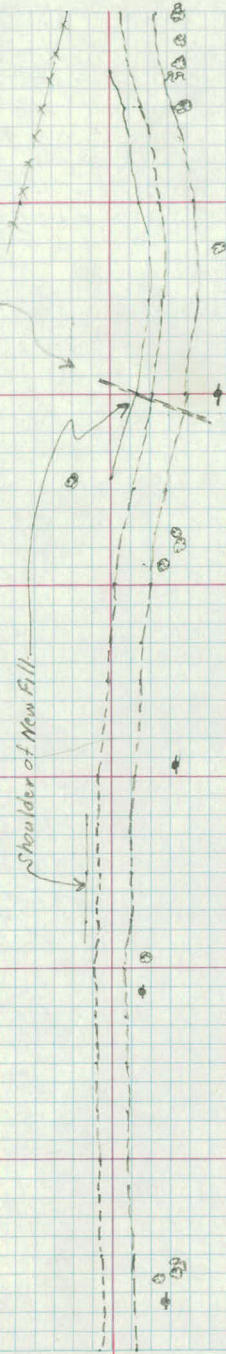
1 12

Note: Need an Add. 14'
of Calvert on Lt. Side

22+08 12" Cm - 5'

+ 89 12" Cm - 46

Shoulder of New Fill



31 RD 10' .

RD 11' .

+50 RD 9' .

+50 - RD - 11' .

+09 - T.P. 38

30 RD - 12' .

RD - 9'

+75 RD 12' .

+75 - RD 9' .

+50 - RD - 13' .

+50 - RD - 8' .

+25 RD - 12' .

+25 - RD 9' .

29 RD - 10' .

RD - 11'

+75 RD - 7' .

+75 - RD 12'

+50 - RD - 6' .

+50 - RD - 12'

+25 RD - 6' .

+25 RD 9'

+19 T.P. - 16' .

28 RD - 7' .

RD - 9'

+50 RD - 8' .

+50 RD 10'

+31 ENQ FC 32 .

27 RD - 8' FC - 22

RD - 10'

+75 RD - 9

+75 RD - 8' .

+68 T.P. 20'

+50 RD - 9' .

+50 RD 9'

+25 RD - 8' .

+25 RD 10'

+02 TRPL - 6" 0 - 36

RD - 10

26 FC - 20 RD - 9

+75 RD - 7' .

+75 RD 11'

+50 RD - 5' .

+50 - 15" 0 - 21 RD - 13' .

+25 RD - 5' .

+39 15" 0 - 30'

25 FC 16' RD - 2'

+25 - RD - 14

15" 0 - 24' RD - 15'

+97 12" 0 - 29

+75 - RD 0.0 .

+75 RD 16'

+50 FC - 14' .

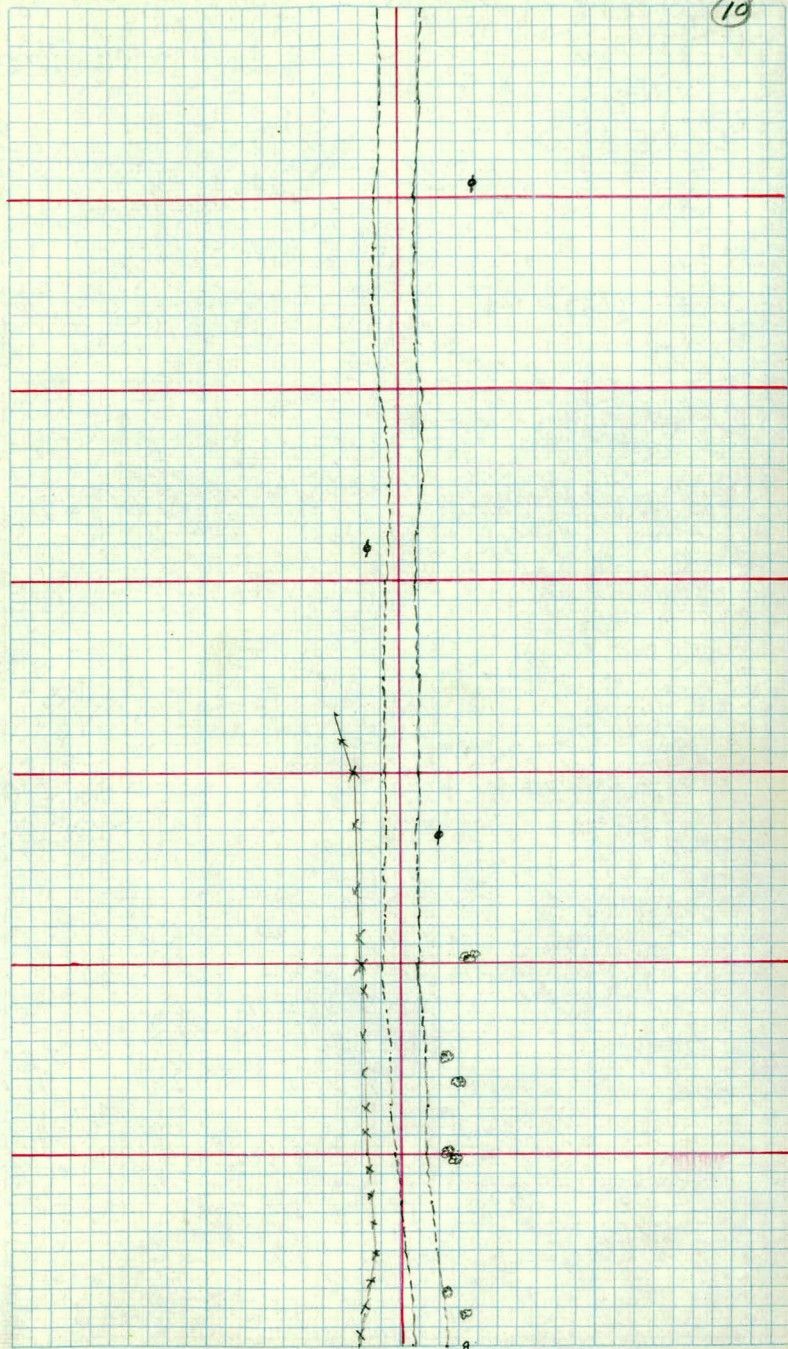
+50 - RD - 1 - 18

+28 - 8" 0 - 24

+17 - 10" 0 - 53

24 FC - 21 .

RD - 6' - 24' STP - 34'



18949