

BK48 Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan.....Survey

Lexington Ave

From Co. Rd. "E" To 1/2 Mi. N. Co. Rd. 1

Road Acc't. No. 3

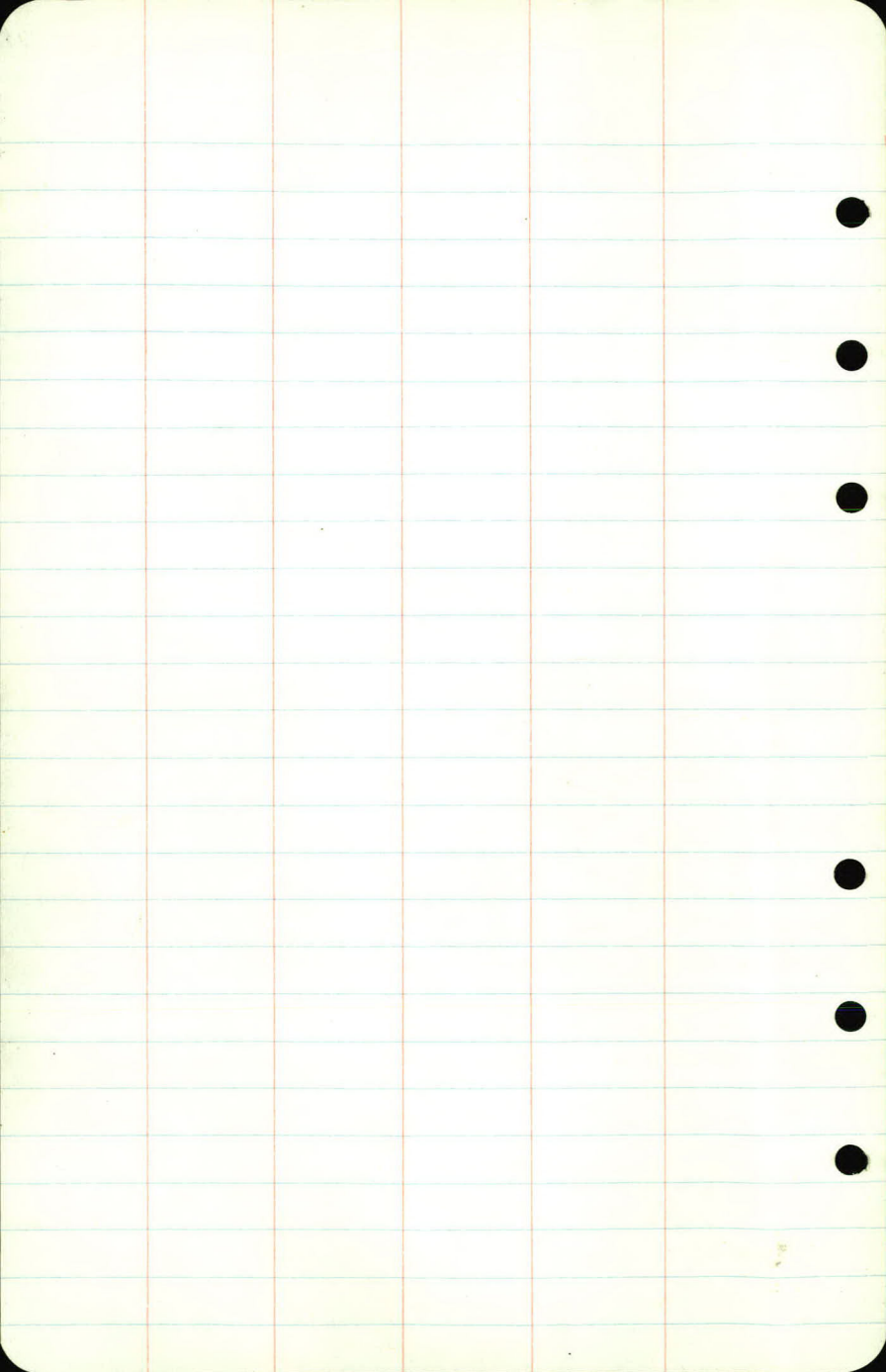
Date Filed.....

File.....

PLAN SURVEY
 LEXINGTON AVE.
 Co. Rd. E. to 1/2 Mi. No.

INDEX

Align	1-2
Topog	3-7
Xsection	8-20



Alignment

Sta	Point	ΔL	ΔR
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26 + 41.17	P.I.		
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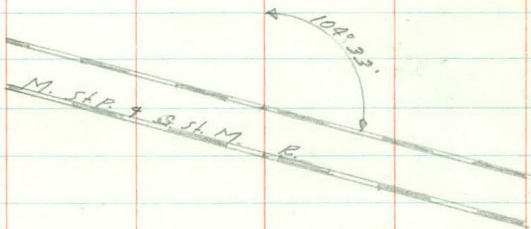
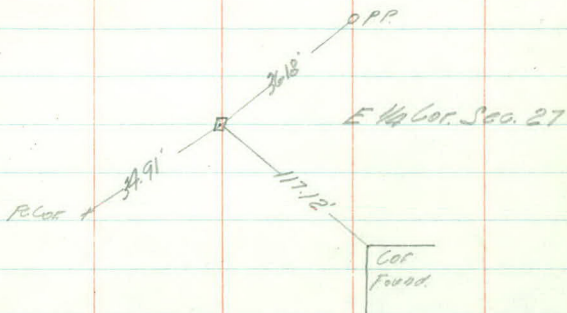
3 + 12.39	P.O.T	=	Track
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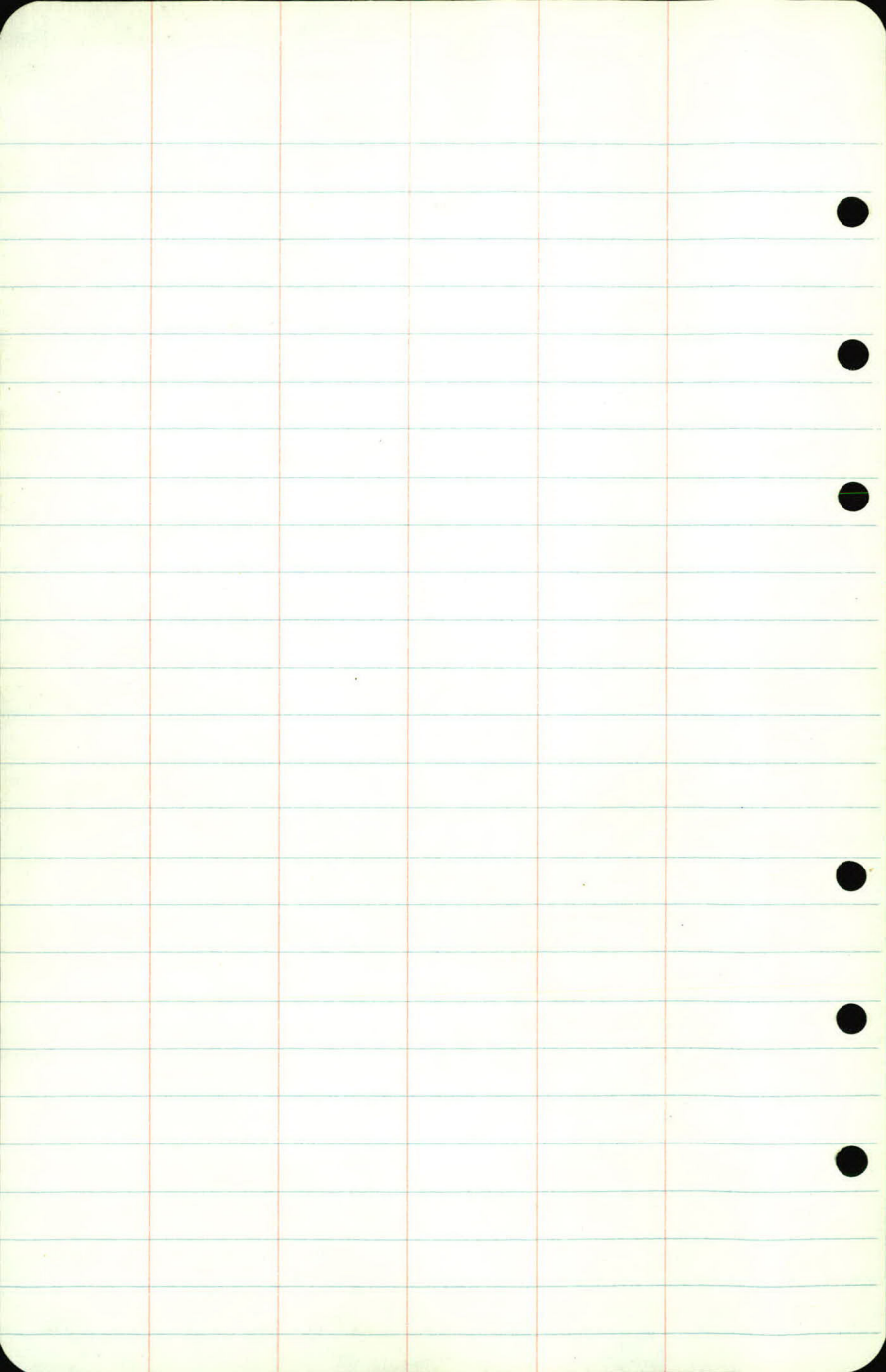
2 + 96.84	P.O.T	=	Track
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0 + 00	=	CORD E"	
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9-19-41
 R.H.
 L.G.
 A.M.
 C.F.
 C.N.

2





Topography

5 G.R.-146 11 11' G.R.-14.8

144-T.P.-30'

4 FG-35 G.R.-147' 11' 11' G.R.-147'

155-FG Cor-35'
137-Bog FG-38'
136-Xing Sign-15'
133-Bog G.R.-15.2'

120-10' 9' 129-Bog G.R.-146'
Point Xing 13' 11'
Point Xing 13' 11'

162-T.P.-25'
152-FG Cor-23'

178-Xing Sign-17'
174-End Spur Track-19'
147-T.P.-49'

123-Rd Sign-14'

122-Cor Coal Bin-61'

2 8' 12'

197-1" Beam Anchor-32'
H.C. Corbin-61'

G Base 2

142-FG Cor-22'
138-Road Tie

139-Chr. Wind Plier-54'
137-R.P.-50'
122-S.W. Cor 6' x 5' " 11'-45'
119-S.W. Cor 4' x 4' Mate 140.-96'
111-Chr. Wind Plier-53'

1 8' 14'

194-Rd Sign-26'

145-Rd-8' 100-Rd-14'

134-R.P.-29'

120-Rd-42'

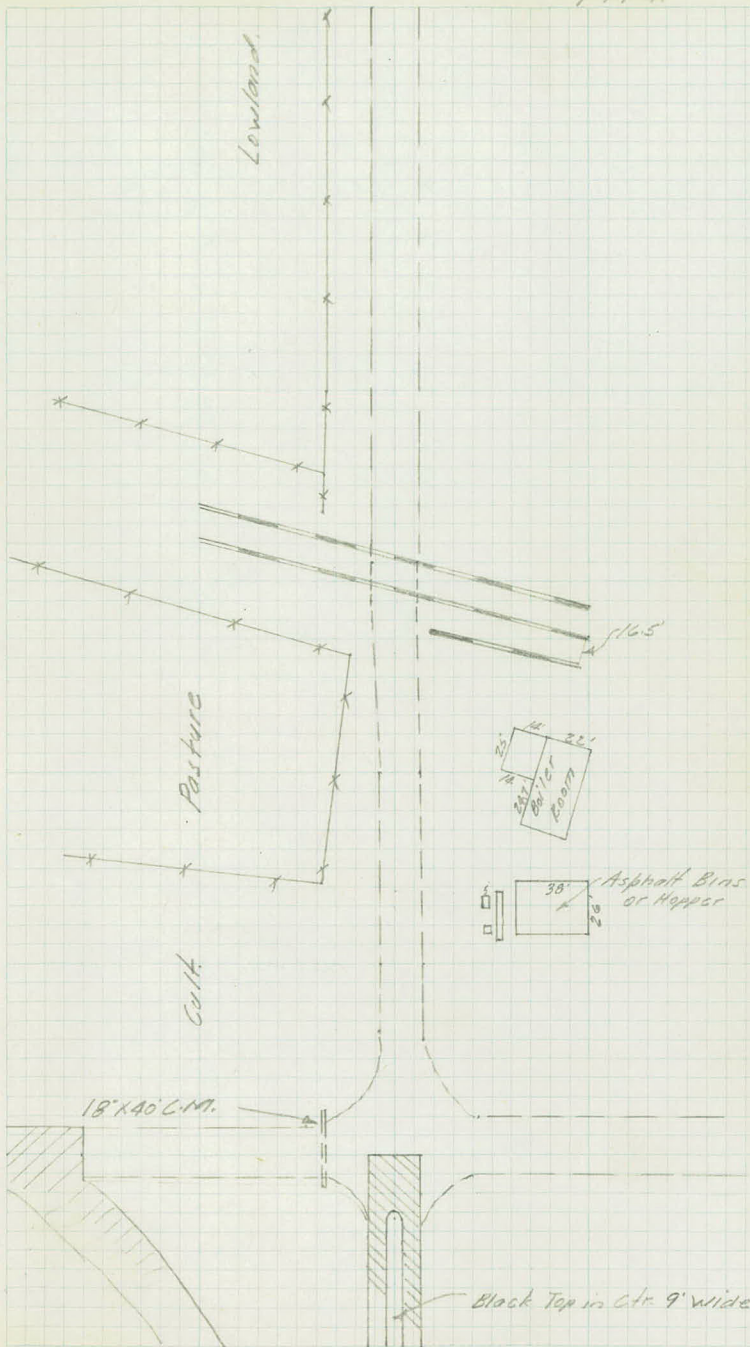
116-Rd-47'

0+00

-0.8-Cor 15. Pav. 135 13.5
-1.5 End 18' 6" 17-33'
-17-4.5 Rd-00

7-14-41

4



12 Fe-33' 11' 11' 120-Lowland-33'

145-TP-31'

11 GR-144 11' 11' G.R.-147'

10 Fe-34' 11' 11'

149-TP-32'

9 G.R.143 11' 11' G.R.147'

8 Fe-34' 11' 11' Lowland-30-60
195-TP-32'

7 G.R.143 11' 11' G.R.149

120-Lowland-33'
120-TP-31'

6 Fe-33' GR-143 11' 11' G.R.-148'

9-16-41

3

Page 2

Hay Land.

Pasture

Reg. Lowland
 +69-Fc Cor-35'±
 +68-T.P.-32
 +69-Range Hc

19 Fc-51-36' G.R-143' 11' 11' G.R-14'

+33-Range Hc
 +66-Div Fc-512

+24-T.P.-31'

18 Fc-37' 11' 11'

17 Fc-41' G.R-141' 11' 11'
 +33-Reg G.C.-141'
 +14-Ent-18' x 44' Cor-29
 +19-Ent G.R-141'

+67-T.P.-32'

16 Fc-36' 11' 11'

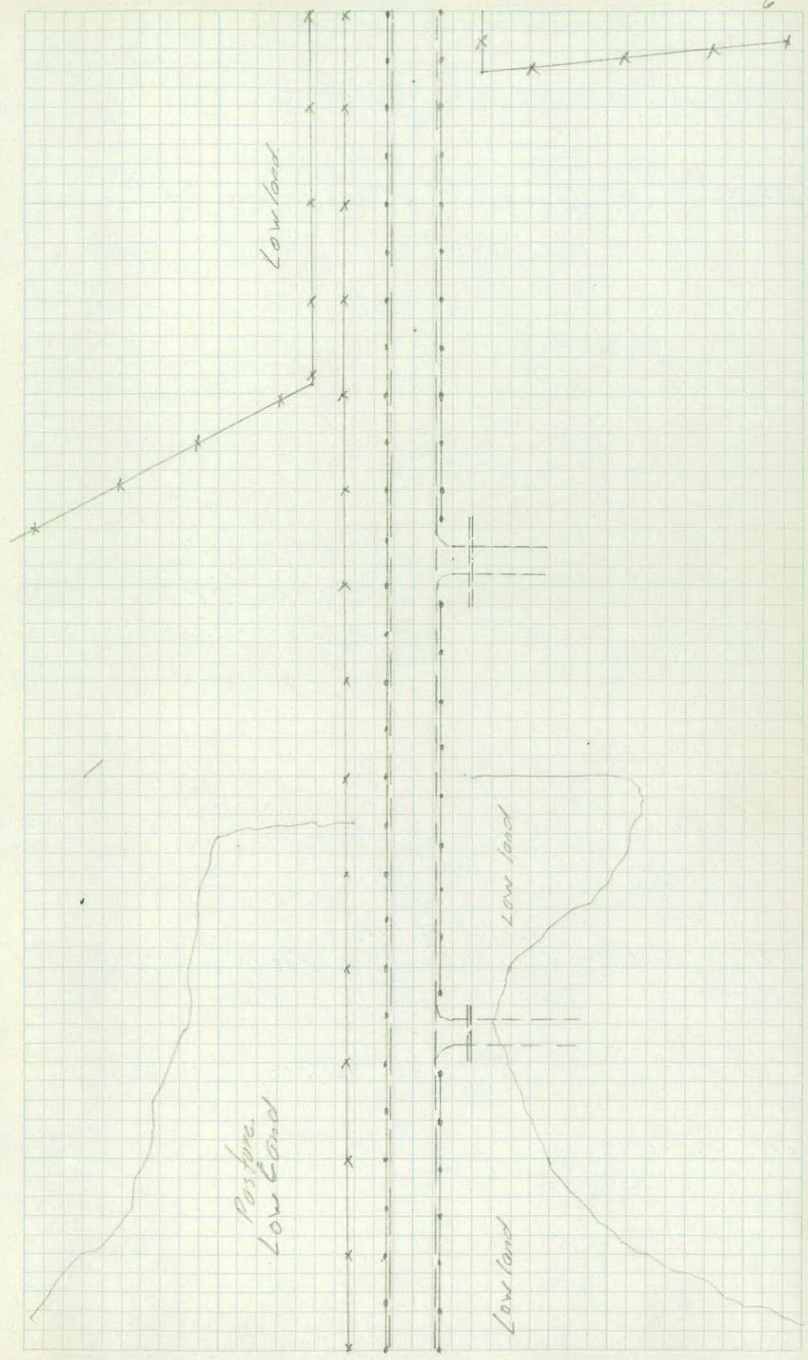
+15-Ent Lowland-30'

+03-X Drain 28' x 56' C.M. 27.5' 28.5'
 15 G.R-141' 11' 11'

+94-T.P.-31'
 +87-Ent G.R-143'
 +66-Ent-18' x 30' W.F.-29'
 +45-Ent G.C.-14.5'

14 Fc-34' 11' 11'

13 G.R-143' 11' 11' +19.7-231' G.R.-141'



+67- 11'

+54- 24'

+41- End

+37- 27'

+24- Fe Cor. 31'

+22- Mangrove

+20- 11'

11'

10'

26

+85- Fe. Cor. 56'

+57- SW Cor Ho - 106'

+08- End G.R. 141'

25 Fe-53'-26'

11'

11'

+90- T.P. - 28'

24 Fe-23'

G.R. 141' 11'

11'

End Lowland

+91- Fe Cor. 24'

+92- End G.R. 13.8'

23 Fe-53-25'

+18- T.P. 39'

Fe-29'

+85- End Lowland

+99- End 24' C.M. 27.5'

X Drain - 24' X 50' C.M.

22 Fe-53-31' G.R. 143'

11'

11'

G.R. 13.8'

Fe-35'

+98- End Phak King - 43'

+82- End 24' C.M. 29'

+50- End 16' Wide Phak King 42'

+43- T.P. 32'

21 Fe-52-34'

G.R. 143'

11'

11'

G.R. 14'

Fe-35.5'

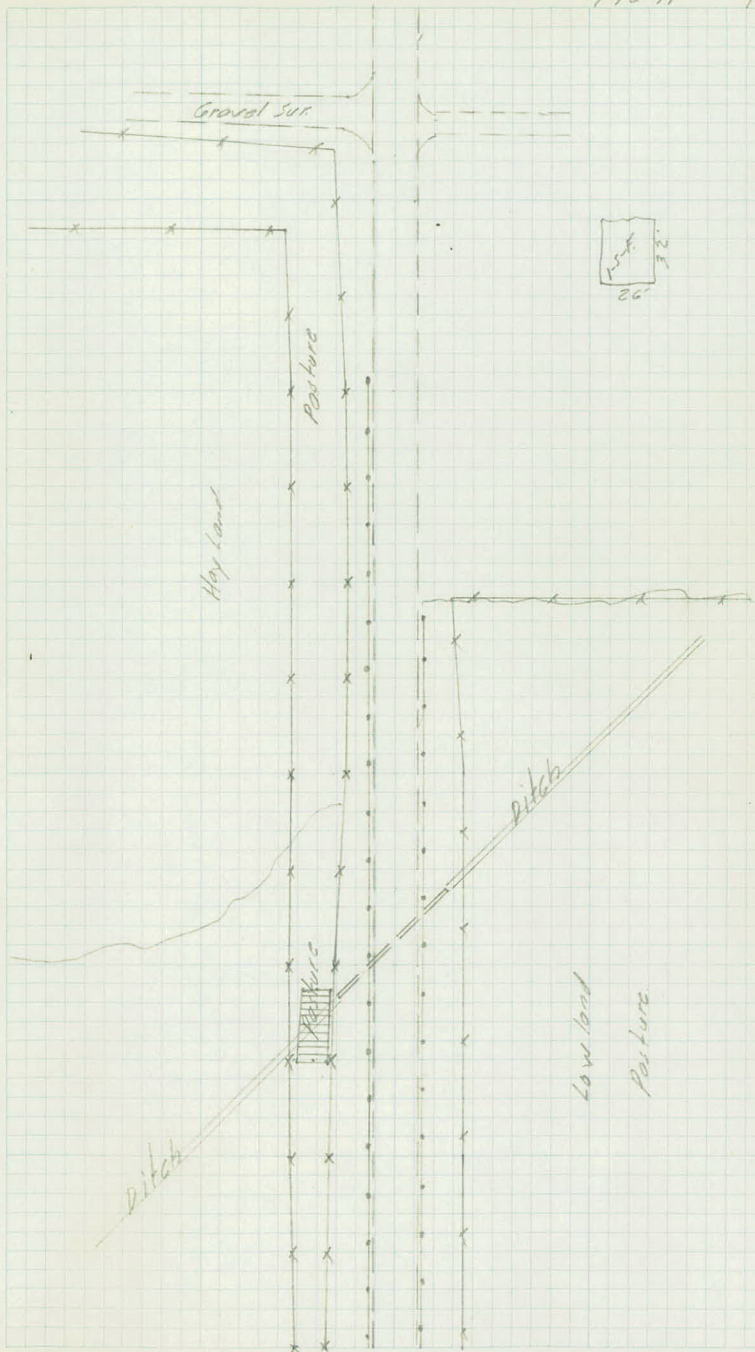
20

11'

11'

9-16-41

7

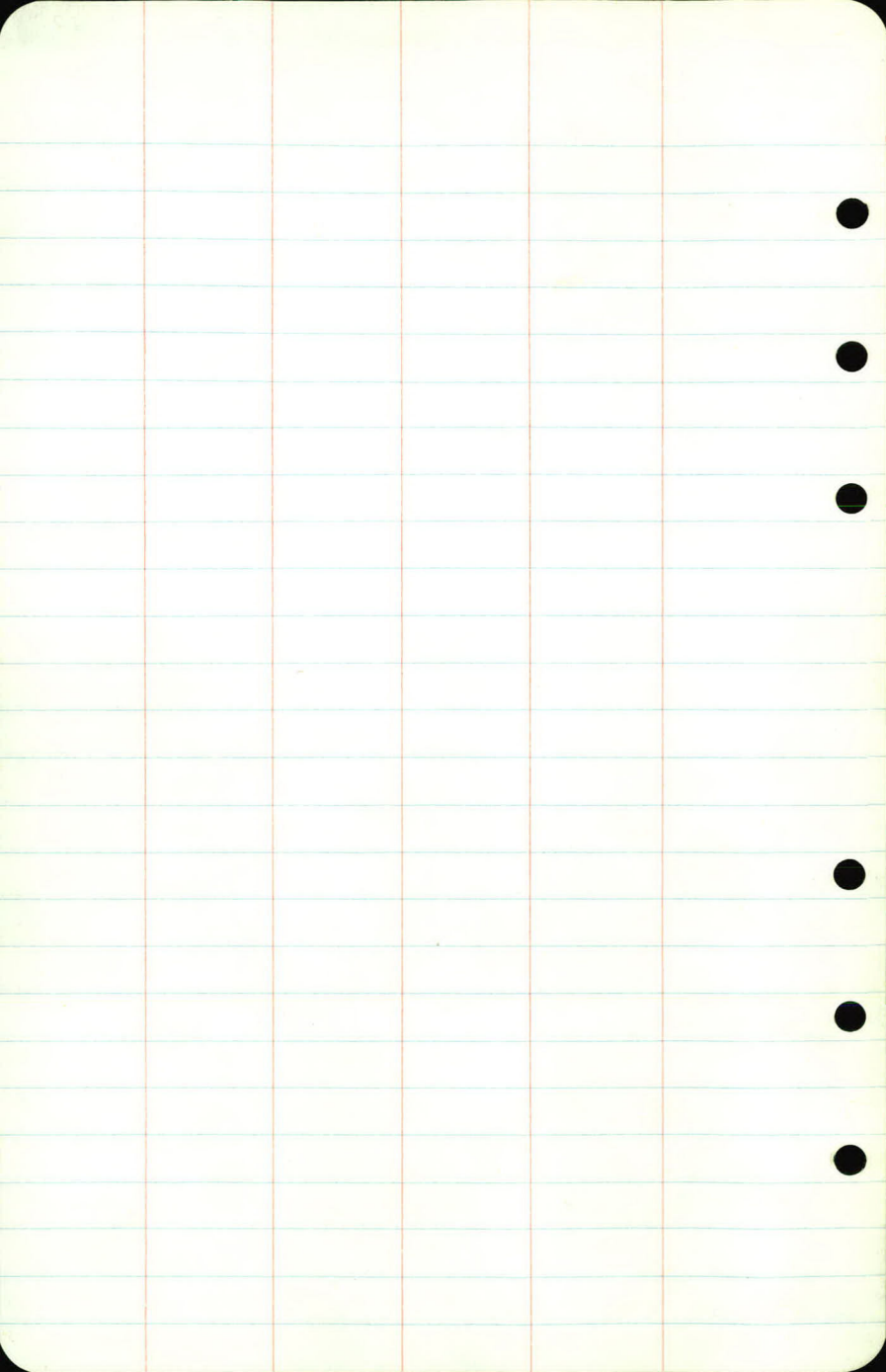




9-15-41
K.A.
L.G.
A.M.
C.F.
G.N.

End 24° 6' 17"

F.L. 18" Tila



X sections

Sta	+	π	-	Elev
B.M.	427	950.58.		(946.31)
0	-25			
	-50			
	-75			
-1	+00			
0	+00.8			46.23
	+19			45.9
	+50			45.4
1				44.7

93717

9-14-91

9

Lt.

4

Rt.

Top Mont. Co. Rd. "E" + Lexington Ave.

402

407

4.5

4.5

365

367

4.5

4.5

3.30

3.29

4.5

4.5

288

290

4.5

4.5

Edge Pav.

6.42	6.2	5.7	5.1	4.40	4.35	4.45	4.2	3.9	3.2
161.4	150	100	50	13.5		13.5	13.5	50	100

5.6	5.5	4.9	4.7	4.7	4.7	5.0
50	37	10		11	21	50

7.2	8.3	5.9	5.5	5.2	5.4	5.9	L.O
50	23	17	11		11	29	

9.2	10.2	6.7	6.2	5.9	6.3	6.5	L.O
50	21	15	8		14	23	

Sta.	+	π	-	Elev
		950.58		

1	+50			44.4
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	+76			44.0
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2				43.8
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	+50			43.6
--	-----	--	--	------

	+86			43.8
--	-----	--	--	------

	+94.4	Top Rail	690	43.68
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	+99.3	" "	688	43.70
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3	+09.9	" "	697	43.61
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Lt

E

Rt

116 113 73 67 62 68 67 L.O
50 22 16 9 12 29

128 119 78 69 66 70 66 6.5
50 22 15 8 12 29 50

117 113 101 75 71 68 71 6.9 6.7
50 22 19 15 8 11 30 50

115 82 72 71 70 72 72 7.2
50 23 16 9 10 27 50

139 112 75 70 68 70 7.4
50 25 18 8 9 20

134 123 88 72 70 69
50 42 25 18 9

Sta.	+	π	-	Elev
		950.53		

3	+149 Top Rail		6.99	43.59
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	+17			43.6
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T.P	326	946.43	7.41	943.17
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	+28			43.6
--	-----	--	--	------

	+A5			43.5
--	-----	--	--	------

	+60			43.4
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4				42.8
---	--	--	--	------

	+50			41.6
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Lt

E

Rt

7.0 6.9 7.6 8.2 11.3 11.9
8 21 26 38 50

3.9 3.4 2.8 2.8 2.9 3.0 8.6 8.5
34 20 9 8 14 29 50

12.4 11.5 3.1 3.0 2.9 2.9 3.2 9.9 10.8
50 34 16 10 9 14 29 50

13.1 13.0 3.5 3.2 3.0 3.0 3.5 10.7 11.7
50 36 15 9 10 16 31 50

13.0 12.2 9.2 4.4 3.8 3.6 3.7 4.1 10.0 11.2 11.8
50 33 27 14 11 10 16 29 36 50

11.4 10.2 9.5 5.2 4.9 4.8 4.9 5.3 10.6 11.9 11.8
50 35 28 16 11 10 15 28 36 50

Sta	+	π	-	Elev
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946.43.

5

40.1

T P.

0.99

939.51. 7.86

938.57.

+50

38.5

6

36.9

+50

35.5

7

34.5

+50

33.8

8

33.3

Lt.

Z

Rt.

16.3	15.2	14.0	7.0	6.5	6.3	6.5	7.0	13.3	14.5
50	36	31	16	11		11	15	29	50

10.5	10.1	9.3	1.8	1.2	1.0	1.2	1.6	7.8	9.1	9.4
50	39	33	15	11		10	15	28	36	50

12.0	11.4	10.8	3.2	2.9	2.6	3.0	3.3	9.7	10.7	11.0
50	37	32	16	11		11	16	29	35	50

11.6	11.6	10.6	1.6	9.4	4.0	4.3	4.7	11.4	11.9
50	34	28	14	12		11	16	29	50

11.6	11.4	12.5	11.7	5.8	5.4	5.0	5.2	5.4	12.2	11.8
50	33	32	27	15	12		11	15	28	50

11.3	11.3	12.4	12.2	6.6	6.0	5.7	5.9	6.1	12.6	12.5	11.7	11.3
50	33	32	28	15	12		11	15	28	31	34	50

11.5	11.5	12.6	12.6	11.5	6.9	6.5	6.2	6.3	6.8	12.4	12.4	11.4	11.2
50	34	31	28	27	15	12		11	15	27	32	34	50

Sta	+	π	-	Elev
		939.51.		

8	+50			33.1
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9				33.1
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	+50			33.0
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10				32.9
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	+50			32.8
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T. P.	4.44	937.43	6.52	932.99
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11				33.0
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	+50			33.1
--	-----	--	--	------

12				33.2
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Lt.

F

Rt.

11.7	11.6	12.5	12.5	7.2	6.6	4.4	6.5	7.0	12.5	12.5	11.3	11.0
50	33	30	28	16	11		11	16	29	32	34	50

11.9	12.0	12.5	12.6	7.0	6.6	6.4	4.5	6.9	12.6	12.6	11.0	10.6
50	33	32	28	16	11		11	16	28	31	33	50

11.9	12.1	12.5	12.7	10.1	7.4	6.7	6.5	6.7	7.1	12.9	12.9	11.3	10.8
50	34	33	29	22	17	11		11	17	29	32	34	50

12.1	12.0	12.8	12.8	10.6	7.4	6.9	6.6	6.7	7.3	12.6	12.6	11.6	11.2
50	33	31	28	23	16	11		11	17	28	32	33	50

12.1	12.2	13.0	13.0	9.9	7.2	6.9	6.7	6.7	7.1	13.3	13.3	11.7	11.3
50	34	31	28	21	16	11		11	16	28	32	34	50

10.3	10.2	10.8	10.5	8.9	4.9	9.6	4.4	4.6	5.1	11.0	11.0	9.6	8.9
50	34	33	28	24	15	12		11	15	27	31	33	50

10.5	10.4	10.6	9.3	4.7	4.5	4.3	4.5	5.1	9.5	11.0	11.0	9.0	8.8
50	34	31	25	15	12		12	16	25	28	31	34	50

10.0	10.1	10.6	10.3	4.7	4.4	4.2	4.4	4.8	10.8	10.8	9.4	8.1
50	34	32	28	15	11		12	15	28	31	33	50

Sta + T - Elev

937.43

12 + 50

33.0

13

32.7

+ 50

32.8

14

32.8

+ 50

32.9

15

32.9

+ 08 X prain

+ 50

32.9

Lt.

£

Rt.

9.5	10.2	10.8	10.8	10.4	4.7	4.5	4.4	4.5	4.9	11.0	11.0	10.0	9.5
50	39	32	30	27	15	12		11	15	28	31	34	50

10.8	10.9	10.6	5.0	4.7	4.5	4.7	5.1	9.5	11.1	11.1	10.7	10.4
50	33	27	15	12		12	16	29	27	30	33	50

10.8	10.7	11.0	11.0	5.0	4.8	4.4	4.7	5.0	11.0	11.0	10.4	10.6
50	34	32	27	14	12		12	16	27	31	34	50

10.5	10.5	11.2	11.2	5.2	4.8	4.6	4.6	5.1	11.3	11.3	10.4	10.0
50	33	31	28	17	11		11	16	28	33	33	50

10.6	10.5	11.2	11.0	5.1	4.6	4.5	4.6	5.0	10.8	10.8	9.8	9.3
50	34	31	28	16	11		11	16	28	32	33	50

10.1	10.3	11.3	11.3	5.1	4.6	4.5	4.7	5.3	11.3	11.3	10.0	9.4
50	34	32	28	16	11		11	16	28	32	33	50

11.57	F.L. 24" C.M.X Colv.	11.28
27		29

10.3	10.2	11.3	11.0	10.3	5.1	4.6	4.5	4.7	5.1	11.3	11.3	10.3	10.0
50	33	31	29	26	16	11		11	16	28	32	34	50

Sta	+	π	-	Elev
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		937.43		
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16				32.9
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T.P	4.55	937.48	4.50	932.93
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+35				33.0
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+60				33.0
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+85				33.1
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12	Flow Line Entails			
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				33.1
--	--	--	--	------

17				
----	--	--	--	--

+24				33.1
-----	--	--	--	------

Lt.

±

R+

9.6 9.8 11.2 10.9 4.9 4.6 4.5 4.6 4.9 11.4 11.4 9.7 9.2
 50 39 31 27 16 11 11 16 28 32 34 50

8.3 8.3 10.4 10.4 5.0 4.5 4.5 4.8 5.1 11.3 11.3 7.7 8.0
 50 37 31 28 16 11 12 16 27 30 37 50

6.8 6.9 10.5 11.1 11.0 4.9 4.5 4.6 4.5 4.8 11.5 11.5 6.4 5.8
 50 38 33 30 27 16 11 11 16 28 32 39 50

5.0 4.6 11.1 11.1 4.7 4.4 4.4 4.4 4.6 11.2 11.2 4.1 3.8
 50 39 32 27 15 12 11 16 28 32 32 50

11.48

4.9 4.6 11.3 11.3 5.0 4.5 4.4 4.3 4.5 4.7 3.4
 50 40 32 27 16 12 11 17 27 50

6.4 5.9 11.1 11.1 5.0 4.5 4.4 4.4 4.5 4.4 3.9
 50 38 32 27 16 11 11 16 26 50

11.58

Sta	+	π	-	Elev
		937.48		
17	+3.8			33.0
B.M.	10.08	937.71	9.85	927.63
	+65			33.0
18				32.9
	+50			32.9
19				32.8
	+50			32.7
20				32.7
	+50			32.7

Lt.

#

Rt.

7.2 6.5 11.3 11.3 4.9 4.5 4.5 4.5 4.5 11.3 11.3 4.6 4.7
 50 38 31 27 16 11 11 16 27 31 41 50
 Top N. End Ent. Culm R. Sta 17+34

8.4 8.1 7.5 11.4 11.1 5.1 4.8 4.7 4.9 5.2 9.2 11.4 11.2 6.6 6.2
 50 41 37 31 27 16 11 11 16 29 28 32 39 50

9.7 9.5 11.5 11.5 5.1 4.9 4.8 5.0 5.4 11.7 11.7 8.4 8.0
 50 36 32 27 16 11 11 16 27 31 37 50

10.7 10.5 11.5 11.5 5.3 5.0 4.8 4.9 5.1 11.8 11.8 8.9 8.6
 50 35 30 27 16 11 11 16 27 31 36 50

10.2 10.1 12.0 12.0 5.3 5.0 4.9 5.1 5.4 12.0 12.0 9.4 8.7
 50 35 32 28 16 11 11 16 27 31 36 50

10.3 10.3 12.1 12.1 5.6 5.2 5.0 5.0 5.2 12.1 12.1 10.0 9.2
 50 34 31 27 16 11 11 16 27 31 35 50

10.4 10.7 12.1 12.1 5.5 5.2 5.0 5.2 5.5 12.1 12.1 10.9 10.2
 50 34 31 27 16 11 11 16 28 32 34 50

10.4 10.0 12.1 12.1 5.5 5.2 5.0 5.1 5.6 12.4 12.4 10.9 10.3
 50 34 31 27 16 11 11 16 28 32 34 50

Sta	+	π	-	Elev
		937.71		

21				32.8
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	+50			32.8
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	+82			32.8
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	T.P.	6.55	939.39	4.87	932.84
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22				32.8
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	+39			32.9
--	-----	--	--	------

	+65			33.1
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23				33.3
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Lt,

£

Rt

10.1	10.0	12.1	12.1	5.4	5.1	4.9	5.0	5.5	12.4	12.4	10.5	10.4
50	34	32	28	16	11		11	16	28	32	33	50

10.1	10.1	12.3	12.3	5.4	5.2	4.9	5.2	5.6	12.4	12.4	10.4	10.5
50	33	32	28	16	11		11	16	27	31	33	50

FL 29" cm.

Lp.	9.6	12.4	12.4	5.4	5.1	4.9	5.0	5.5	12.1	12.2	10.5	10.5
	33	30	29	16	11		11	16	28	31	33	50

12.0	11.9	12.6	12.6	7.2	6.8	6.6	6.7	7.1	14.0	14.0	12.0	11.9
50	31	30	28	16	11		11	16	28	31	33	50

FL 29" cm

11.8	11.9	7.1	6.6	6.5	6.5	6.8	19.07	14.2	13.1	11.4	11.3
50	26	16	11		11	16	27	28	31	34	50

11.2	11.8	6.8	6.4	6.3	6.5	6.8	12.0	11.4	10.7
50	27	16	11		11	16	26	31	50

10.0	10.5	9.8	6.5	6.2	6.1	6.4	6.7	11.2	11.7
50	26	23	16	11		11	16	27	50

Sta + π - Elev

939.39

23 +50

33.7

24

34.5

+32

34.8

+75

35.3

T.P. 11.97 942.54 3.82 935.57

25

35.5

+32

36.0

+65

36.3

26

36.7

Lt

#

Rt

8.9	8.5	5.9	5.7	5.7	5.9	6.1	9.9	10.3	10.9
50	22	16	11		11	16	22	28	50

8.4	7.9	5.3	5.0	4.9	5.1	5.5	8.1	8.7
50	24	16	11		11	16	23	50

7.2	6.5	6.0	5.0	4.7	4.6	4.7	4.9	7.2	7.7
50	24	18	16	11		11	16	23	50

8.1	8.0	7.2	4.6	4.3	4.1	4.3	4.3	6.9	6.4	5.9
50	25	19	16	11		11	16	20	28	50

16.2	15.2	15.0	12.4	12.1	12.9	12.1	12.2	13.8	13.8	11.9	11.0
50	31	21	16	11		11	16	20	24	29	50

14.6	13.3	12.8	13.4	13.4	12.2	11.8	11.5	11.6	11.6	13.6	13.6	8.8	7.6	6.1
50	33	27	24	20	16	11		11	16	19	25	32	41	50

13.3	11.1	10.7	13.1	13.1	11.7	11.5	11.2	11.3	11.4	13.2	13.0	2.2	6.1	4.1
50	33	28	24	20	16	11		11	16	20	25	33	38	50

10.6	9.6	12.4	12.6	11.2	11.2	10.8	10.9	11.0	12.6	12.5	10.6	6.9	3.7
50	31	24	20	16	11		11	16	20	24	29	36	50

Sta	+	π	-	Elev
-----	---	-------	---	------

947.54

26 + 27

37.0

+ 33

37.1

26 + 41.17

37.2

B.M.

10.34

937.20

937.12

Lt.

±

Rt.

10.0	9.5	12.3	12.3	10.8	10.7	10.5	10.6	10.8	11.3	11.5	8.3	5.3
50	30	25	20	16	11		11	16	19	25	32	50

10.6	10.8	10.6	10.5	10.4	10.5	10.0	8.9	6.5
50	30	18	11		10	16	29	50

8.2	9.1	9.7	10.0	10.9	10.3	10.9	9.7	6.0	1.8	1.8
200	150	100	50	11		8	11	50	100	200

Top Mont sta 26 + 41.17

Levels in Pitch S.W. From End Culv. Lt Sta 21+82

Culv = Sta 0+00

Sta f π - Elev

0+00 12.60

0+50 12.4

1 12.3

+50 12.6

2 12.8

+50 12.7

3 12.8

+50 12.8

4 12.8

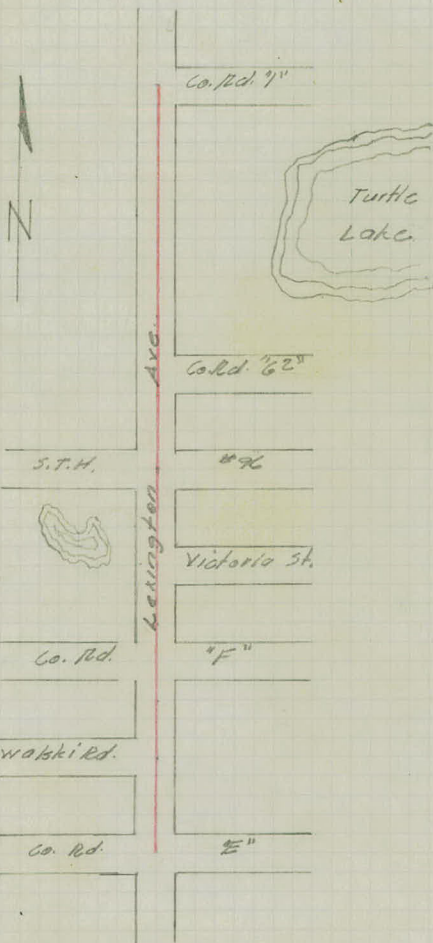
+50 13.0

5 13.2

+82 13.55

PLAN SURVEY
LEXINGTON AVE.

Co. Rd. "E" to Co. Rd. "I"



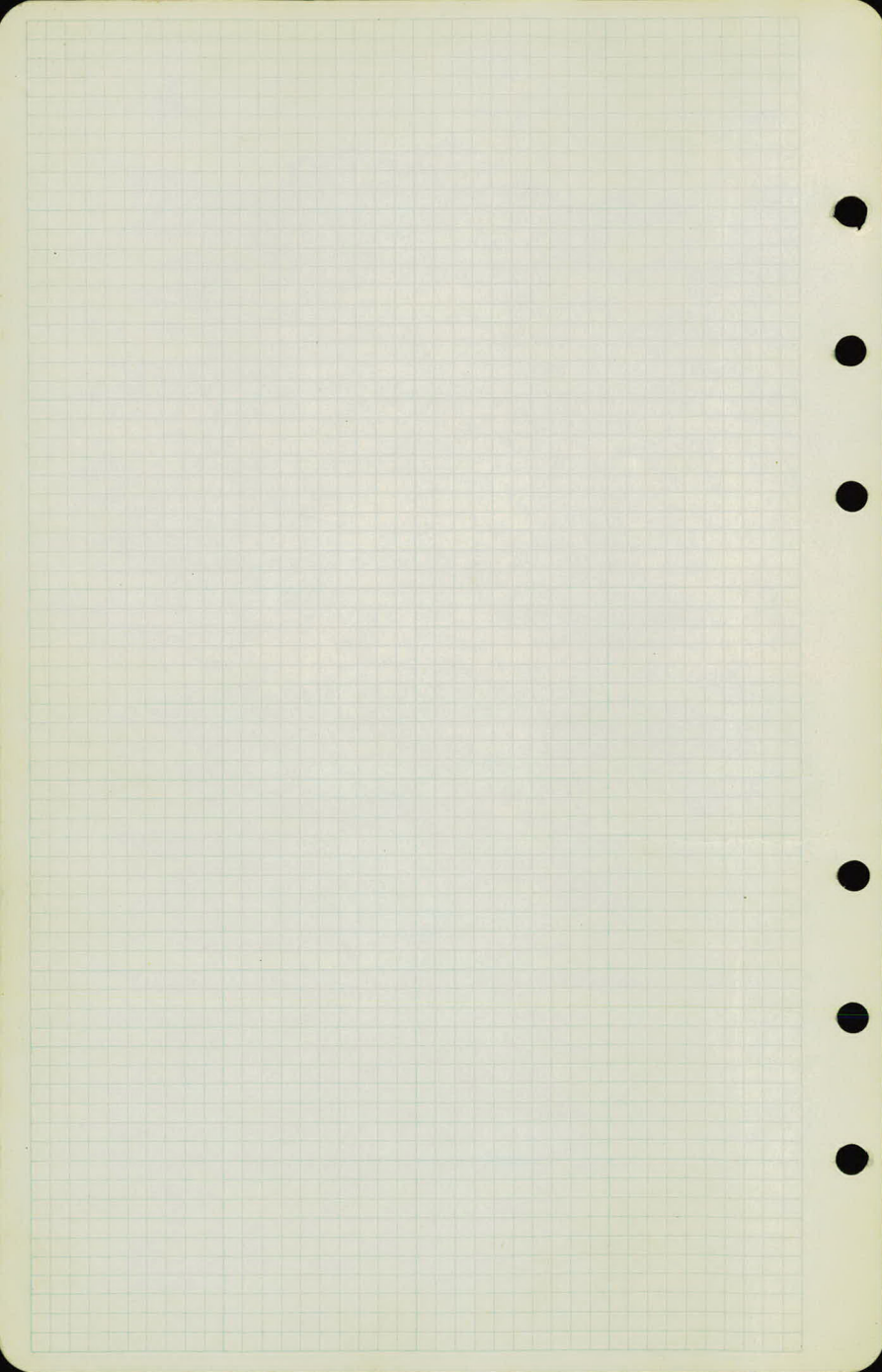
INDEX.

Align - - 1-5

Topog - - 6-38

Levels - - 39-41

Assestion - - 43-73



1
Alingement

Sta.

P.T.

Alt

A.R.T.

52+81.98

P.I. = 4 Co. Rd "F"

0°05'

26+41.17

P.I. = 4 Kaslo Rd

0°07'

3+12.39

200 RR

No Tracks

2+96.84

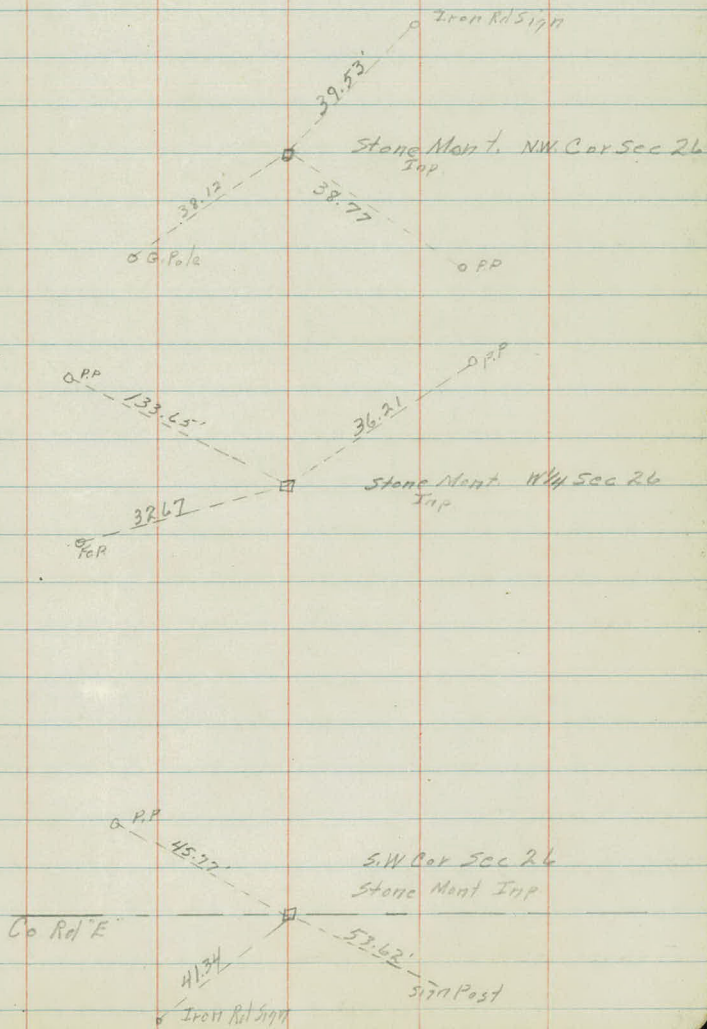
So Tracks

104°33'

0+00

P.I.

89°40'



5th

Pt

DL+

DR+

95+00

P.O.T.

79+18.18

P.I. = Victoria St

0° 01'

67+82.72

P.O.T.

61+59.88

P.O.T.

Boat Spike

0 7.19

10136

63.20

O.T.P.

GPole

o T. P.

معا: ۱۰۰

$$\underline{50.30}$$

E'4 Sec 22

85.52

Iron 48.31

15" oak

Guard Rail Post

Boat Spike

31.03 - D.R.P.

130.97

opp opp

13.98

R.R. Sp, Kc

75.81

o p p

Sta

PT

$\Delta L +$

$\Delta R +$

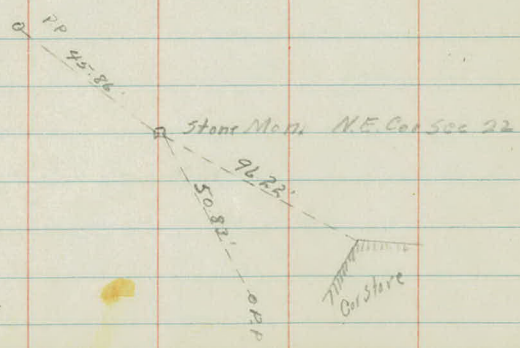
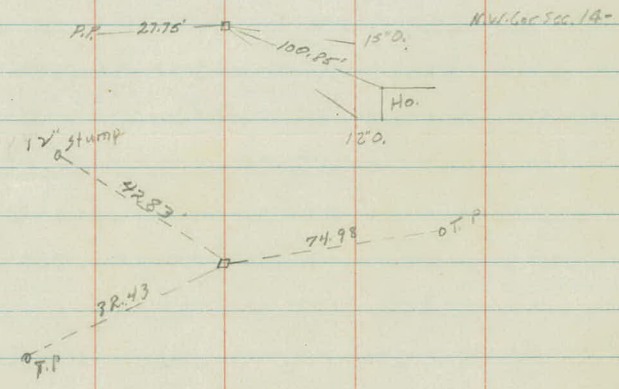
158 +23.60 P.I.

$0^{\circ}14'$

131 +92.75 P.O.T. = 60.25' 6" 2"

105+56.92 P.I. = 45.14' 2"

$0^{\circ}11'$



Sta

Point

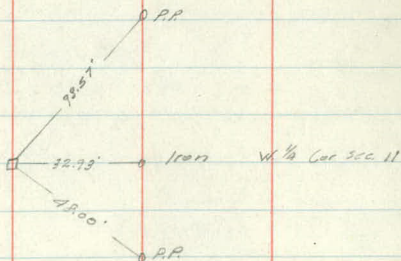
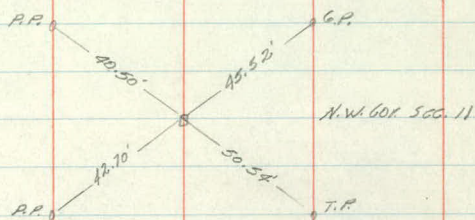
Δ Lt

Δ Rt

211 +21.32 = ϕ Co. Rd. "1"

184 +65.02 P.L.

$0^{\circ}12'$



Sta.

Point

Δ Rt.

Δ Lt.

546E
1935
Align

Lexington Ave Ext

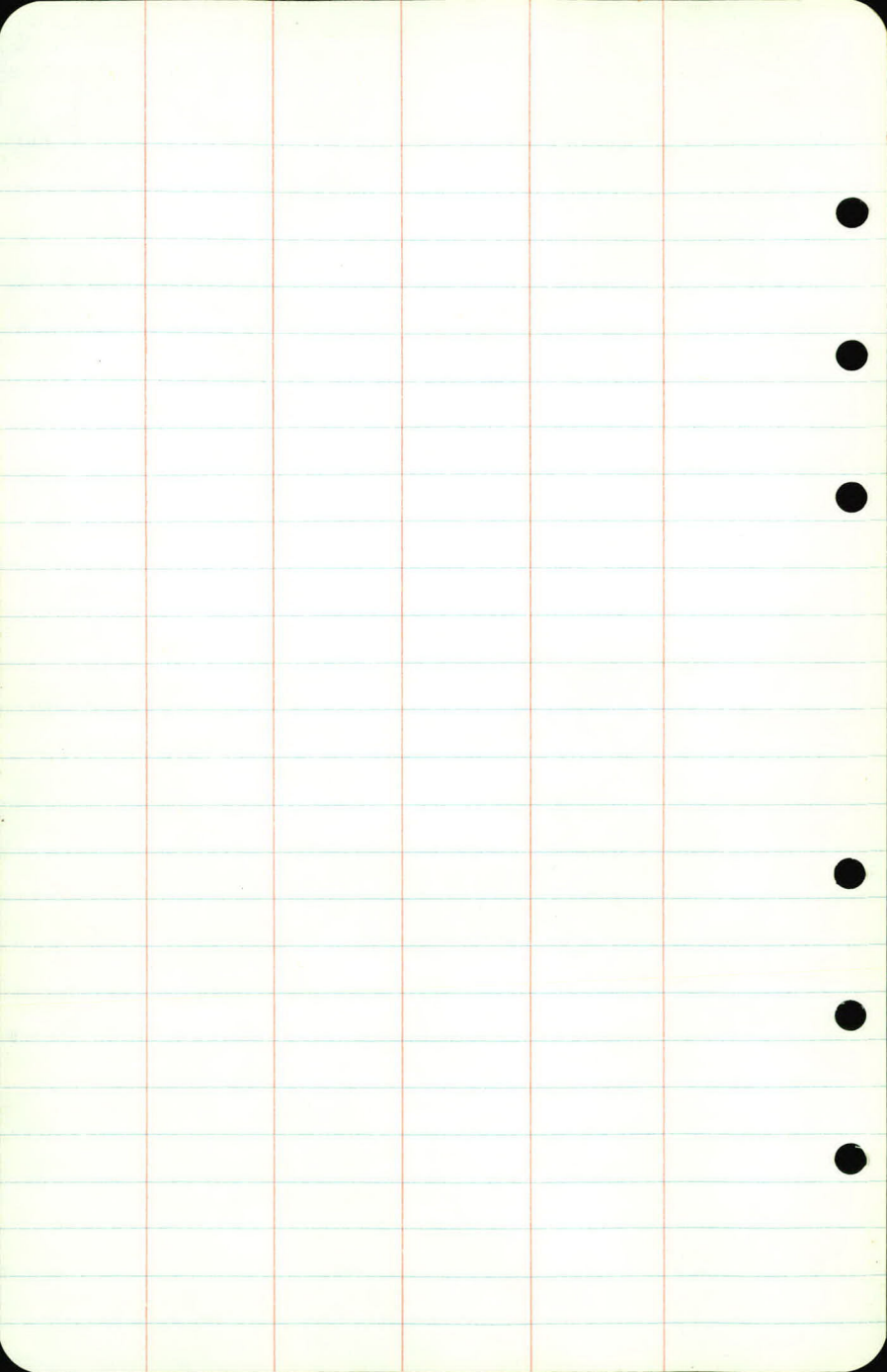
From Co Rd I To S.T. H #8

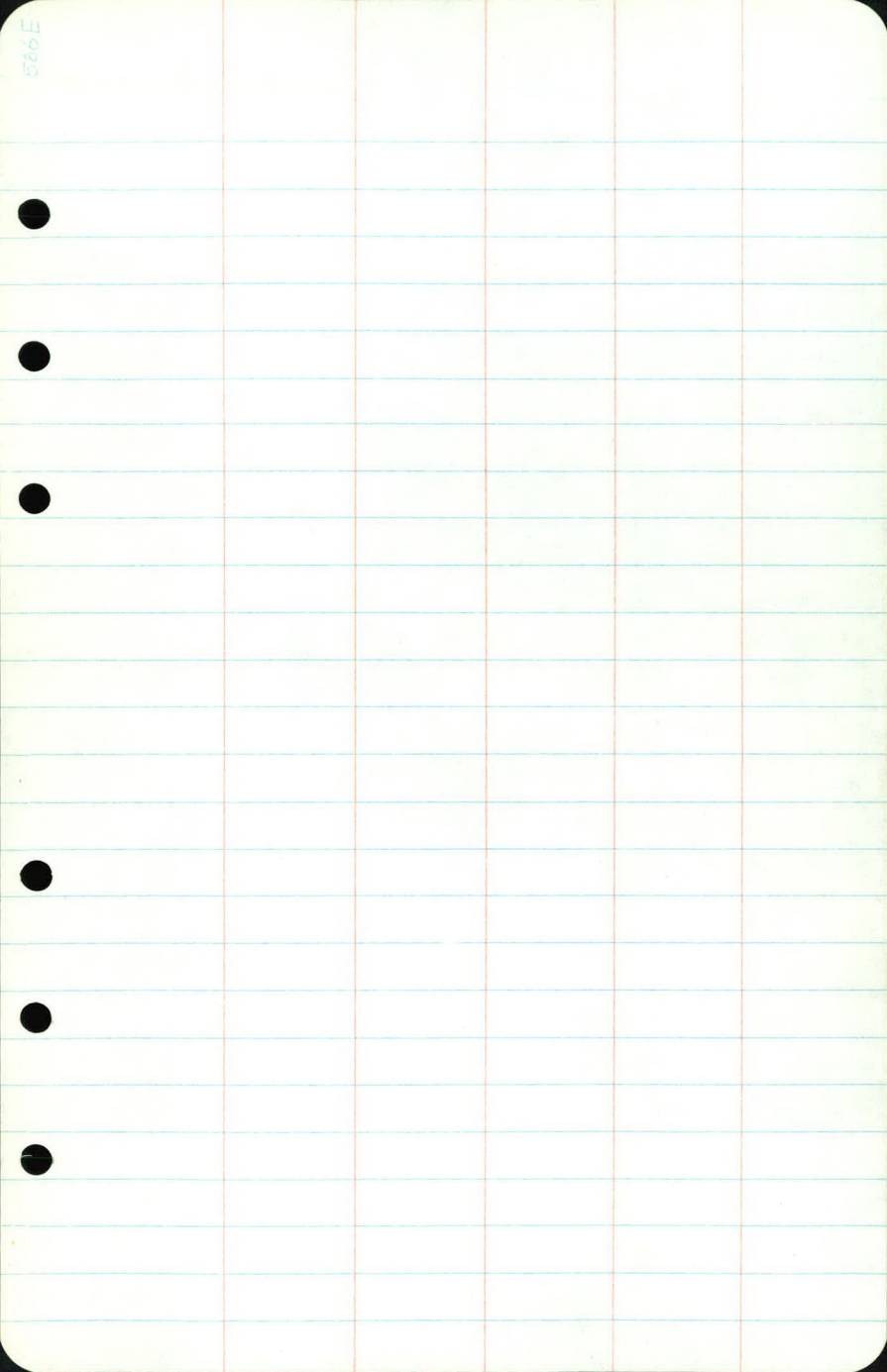
8-5-41

Wilke

Moeschter

Goldberg





Sta

Pt.

Alt

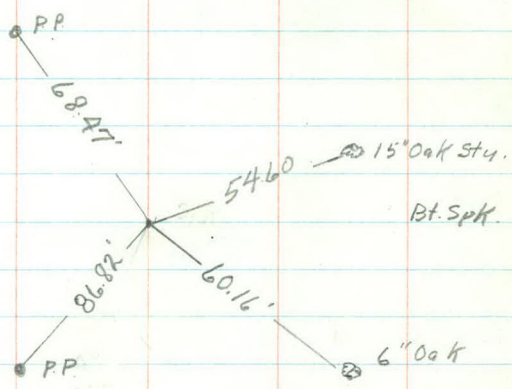
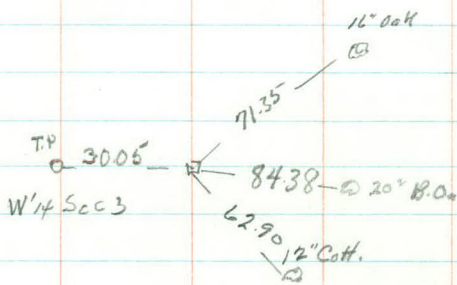
Asht

237+37⁹⁰ P.1

220+00 P.O.T.

211+01⁵⁰ P.1

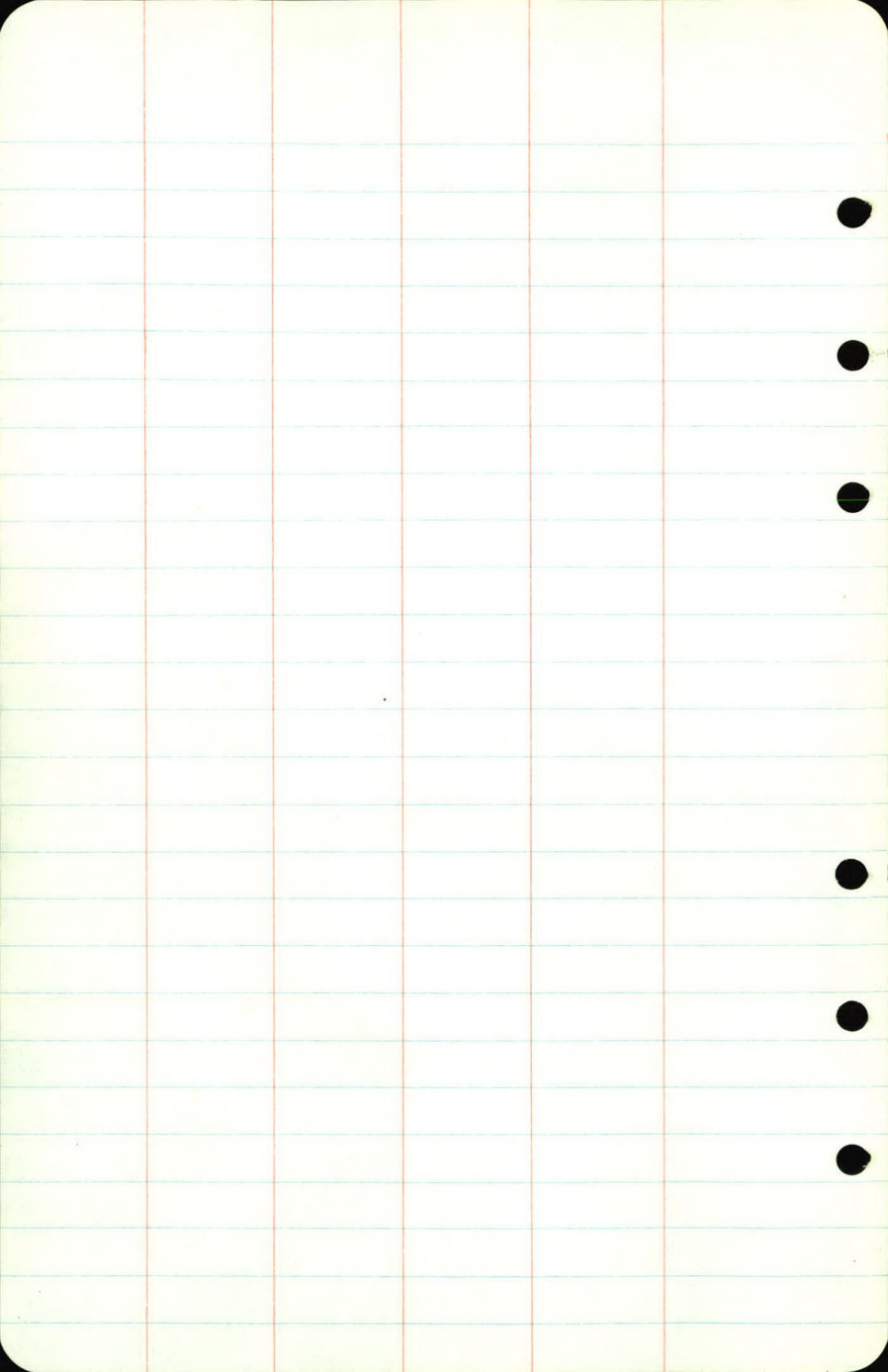
0°04'



All ties 10' Penny Nail
Tru Disk

Bt. Spk.

Mon. S.E. Cor. Sec 3



6
Topography

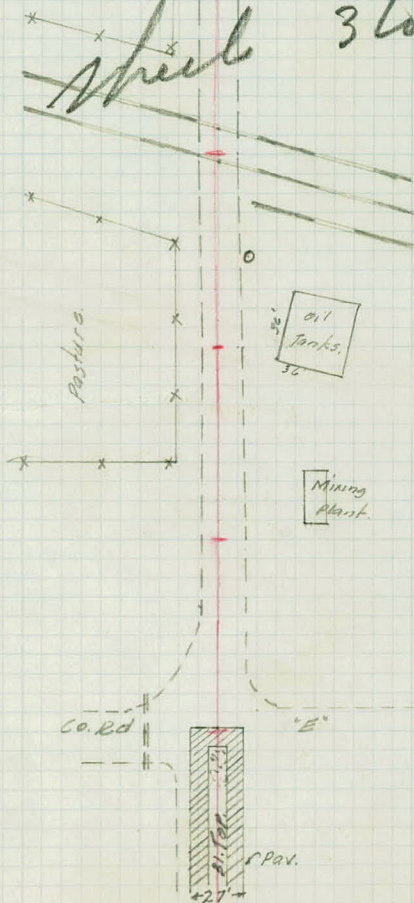
Word pages 6-10
see revised Topog.

K.A.
L.B.H.
L.C.
K.A.

7

Hay Meadow.

see *Sheet* 3 to 7



+36-FC-29'

+40-FC-28'

12' FC-27'

11'

9'

+44-TM-28'

11' FC-25'

11'

9'

10' FC-24'

11'

9'

+48-TM-29'

9' FC-23'

10'

10'

8' FC-22'

10'

10'

+54-TM-30'

7' FC-21'

10'

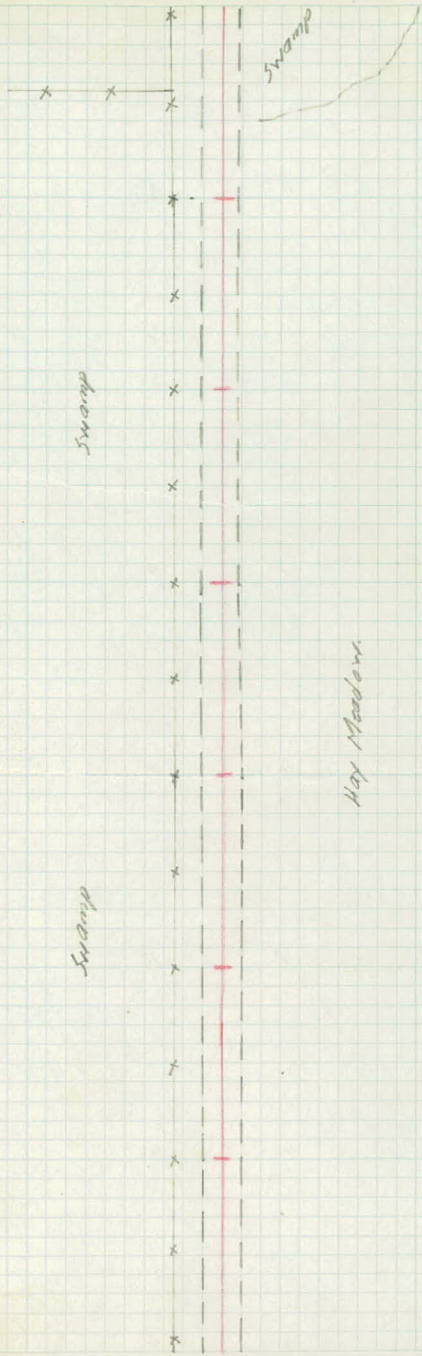
10'

+59-TM-31'

6' FC-20'

10'

10'



+120-Fe.Loc.-29'

+69-T.P.-27'

19 Fe-29'

11'

9'

+115-Beg. Swamp

+121-T.P.-27'

18 Fe-29'

11'

9'

17 Fe-30'

11'

9'

+125-24 Elm-33'
+10-Ent.

+115-20 Elm-32'

+114-15 Elm-31'

+113-12 Elm-28'

+113-24 Swamp-22'

16 Fe-29' End Swamp

11'

9'

+102-24 Elm-21'

15 Fe-28'

11'

24'

24'

9'

+109-T.P.-28'

+109-Ent.-18"x15 Vit.-27'

14 Fe-27'

11'

9'

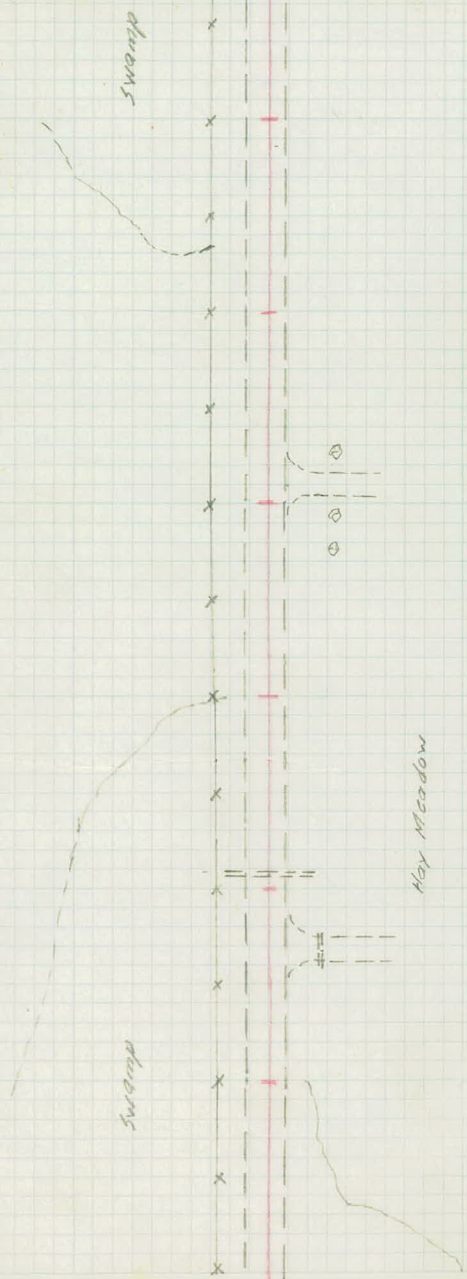
End Swamp

13 Fe-27

11'

9'

+117-T.P.-28'



+87-T.P.-27'

+96-Rd.

+98-Ent.

+22-Fc. Cor.-27'

26

11'

9'

25 Fc.-26'

10'

9'

+92-T.P.-28'

24 Fc.-23'

10'

9'

+90-Fc. Cor.-26'

+80-End Swamp.

23 Fc.-26'

10'

9'

+77-T.P.-28'

Fc.-25'

+60-End Swamp.

+98-Fc. Cor.

+95-End 24' C.P.-25'

22 Fc.-26'

24' X 70' C.P.

11'

9'

Fc.-26'

+85-End C.P.-24'

+90-T.P.-28'

21 Fc.-28'

12'

9'

Fc.-26'

20 Fc.-28'

11'

9'

Koalski Rd.

Cult

Meadow

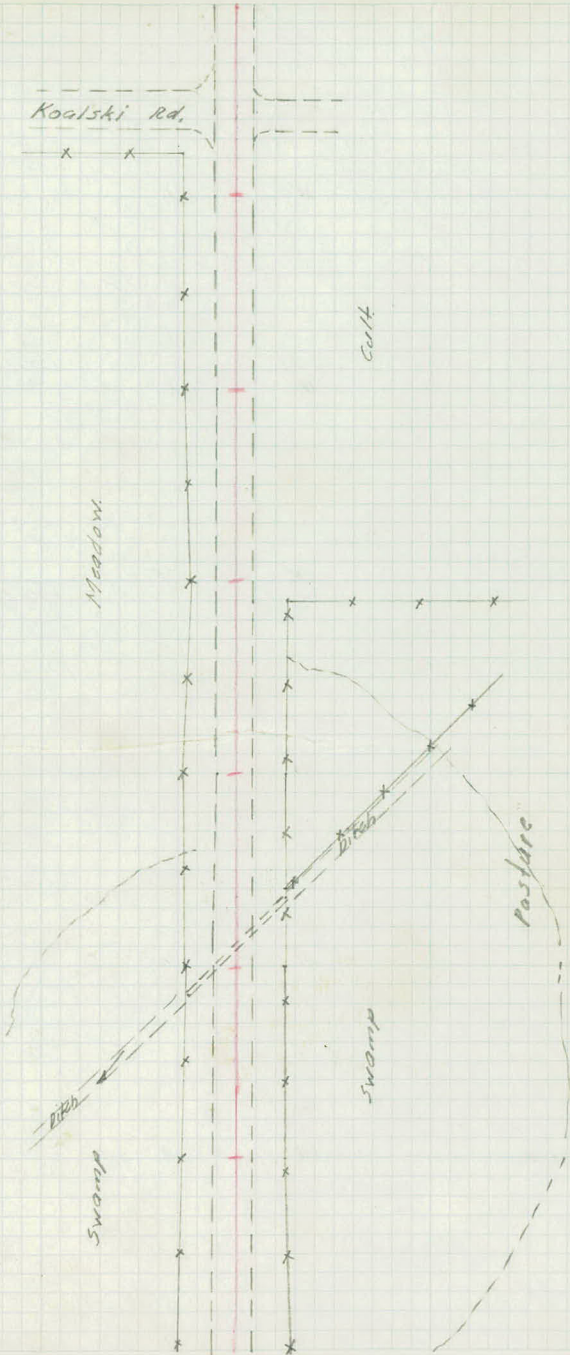
Pasture

Swamp

Swamp

Ditch

Ditch



188-T.P.-27'

33 Woods-92'

10'

10'

192-T.P.-28'

32

10'

10'

+25-Reg. Woods-82'
+13-15" Oak-20'

31

10'

10'

+96-T.P.-28'

30

10'

10'

151-T.P.-28'

29

10'

10'

28 823.5 W. 1/2 mp.

11

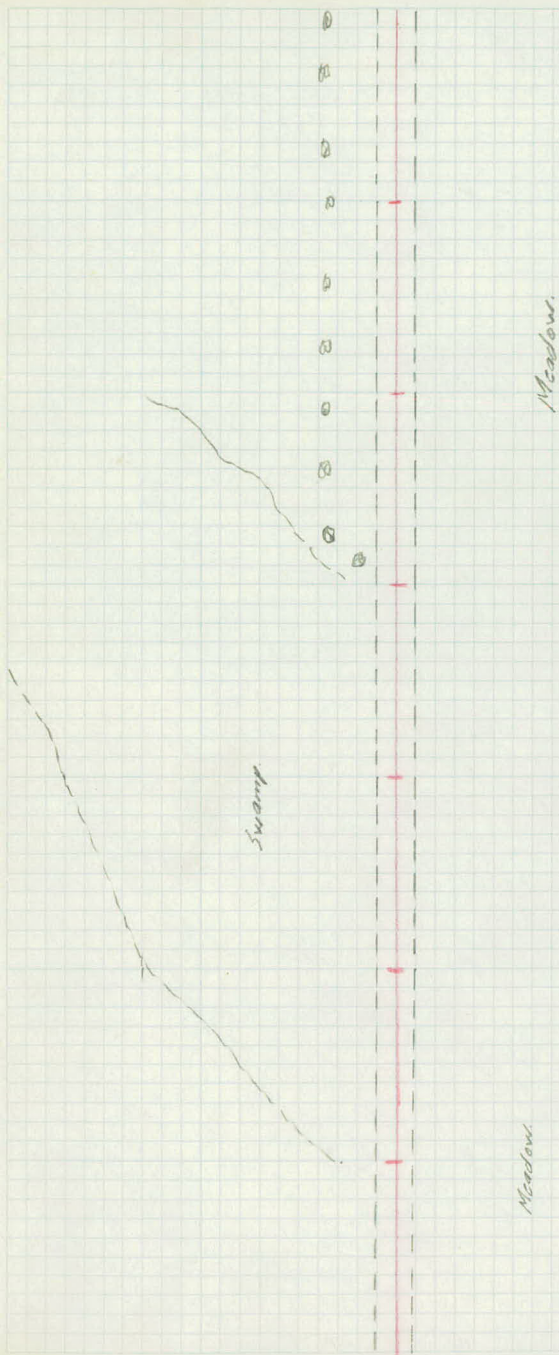
9

106-T.P.-28'

27

11'

9'



40

11'

9'

+15-Box, Swamp

+68-T.A.-27'

39 Woods-32'

11'

9'

+45-End 15'K26 C.M.R.-27'

+23-T.P.-28'

38

11'

9'

37

11'

9'

+62-End Cult-18'

18"K#2'Vit.

+77-T.P.-25'

+50-End Cult-24'

36 Woods-35'

10'

10'

+32-T.A.-27'

35 Woods-33'

10'

10'

34

10'

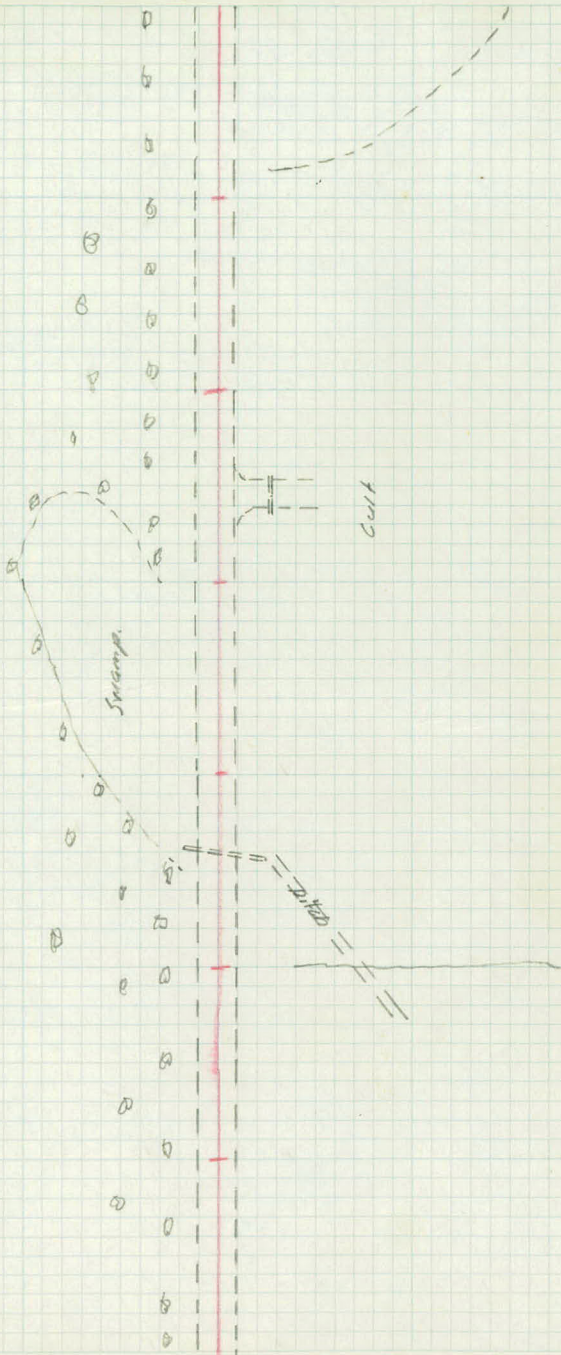
10'

Scattered Oaks

Swamp

Cult

Ditch



12" x 64' C.P.P.

#24-End LWN -31'

#38-End LWN -29'

#7 End Trs. -35'

12'

8'

#4-Ed. Cor 25'

#96-T.P.-28'

#47-Ho.-115'

#25-18" Willow -13'

#13-Ent.

#6

12'

7'

#55-Sharp -14'

#82-18" Willow -14'

#80-T.P.-28'

#5 Tr. Line -35'

11'

8'

#4

11'

8'

#5-T.P.-27'

#3 Tr. Line -34'

11'

9'

#2-T.P.-27'

#2

11'

9'

#50-End Swampy.

#1 Woods -37'

11'

9'

#12-T.P.-26'

Scattered Oaks

Cult.

Swamp

Swamp

Swamp



10 20 30 40 50

60

54 11' 9' 191-T.P.-28'

53 192-N. End of Tga
178-S. End of Tga
135 G.R.-27' 103-N. End of C.M.-19'
161-S. End of C.M.-19'
157-F.C.C.-25'
154-T.P.-28'

52 10' 9'

51 11' 9' 146-T.P.-28'
F.C.-26'

50 11' 9'

175-T.P.-27'

49 10' 8' F.C.-26'

135-T.P.-28'
130-End of Survey

48 10' 8'

Wasteland

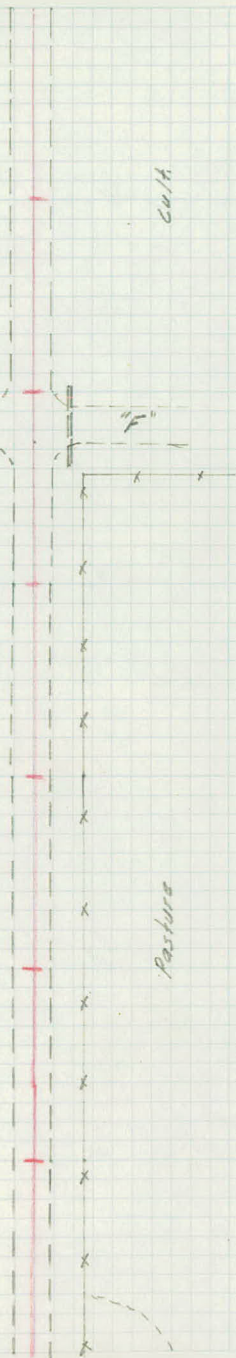
cult.

Co. Rd.

"F"

Wasteland

Pasture



61

10'

10'

+89-T.P.-27'

60

10'

10'

+50-T.P.-27'

59

11'

9'

59

11'

9'

+10-T.P.-27'

57

11'

9'

+71-T.P.-28'

+58-Ent.-12" X 20 G.M.-23'

56

11'

9'

+30-T.P.-28'

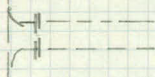
55

11'

9'

Wash land

Cult.



68 11' 10' +98-T.P.-28'

67 11' 10'

+61-Ent-12" No 6 CM-25'
+58-Cor Woods-31'

+55-P.P.-28'

66 11' 10'

+83-Cor Woods-47'

+25-Ent-12" No 6 CM-25' +27-FE-28'

65 11' 10' +08-P.P.-27'

+92-Ent
+78-FE Cor-27'
+65-12" Box-18' 12" B.E. Box-34'

+40-U.W. Cor Ho-15'

+29-R 4' Side Walk-13'

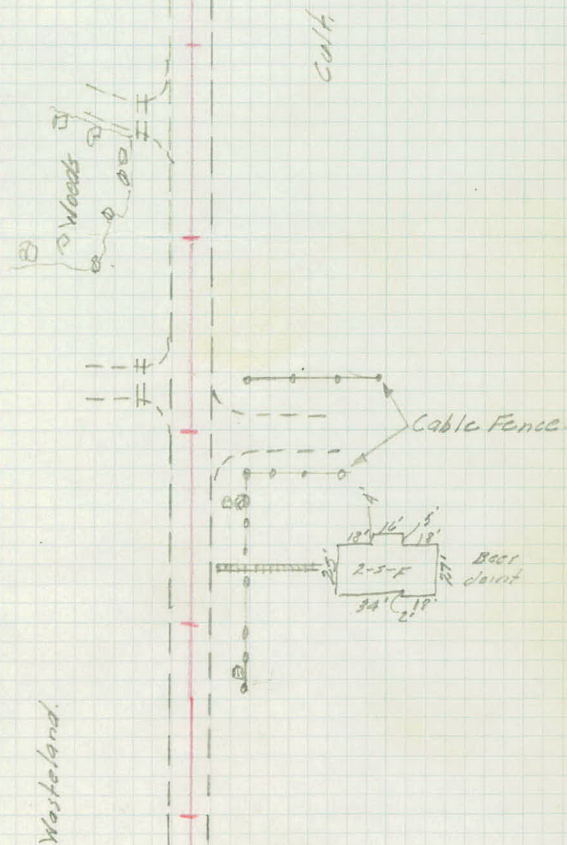
64 11' 7'

+75-12" Ave 16 Fe-28'
+08-T.P.-27'
+05-Box FE-27'

63 11' 9'

+30-T.P.-27'

62 10' 10'



175- Δ in Fe-22'

+46-Bog. G.R.-14'
+53- Δ in Fe-33'
+38- Δ in Fe-55'

13 147- Δ in Tower-33'

+17-T.P.-20'

+11-T.P.-22'

-Fe-43'

+89- Δ in "H" Mk.-59'

+75-Bog. G.R.-16'

75

10'

10'

74

10'

11'

Fe-50'

+67-T.P.-64'

+54-High Line Tower-88' 10' wide

+37-"H" Pole-63'

+73-T.P.-23'

73

10'

11'

Fe-52'

+34-Bog. Tie to Fe.
+30-T.P.-25'

72

9'

10'

+39- Δ in Fe-53'

71

9'

10'

+85-T.P.-27'

70

11'

10'

+92-T.P.-21'

69

11'

10'

11' wide

Wasteland

11' square

5 wires

+84-End G.R.-14'

+37-T.P.-28'

82 Fc-36'

8'

11'

Fc-30'

+83-End G.R.-16'

+91-Lake-68'

+88-End Row Trees-39'

+90-Fc Cox-39'

81 G.R.-14'

9'

11'

G.R.-16'

Fc-33'

+98-T.P.-27

+92-Rubble Spillway-12'

+30-Lake-10'

80 Fc-45' G.R.-14' 9'

11'

G.R.-16'

+90-Row Willow-45'

+Cott-45'

+53-End 24' L.M. Calk-64'

+85-G.R.-19'

+88-20' Cott-41'

+28-20' Cott-48'

79 Fc-40' G.R.-14'

9'

G.R.-75'

165'

24' x 75' C.M.

+68-P.B. End G.R.-17'

+55-End 24' L.M.-79'

+50-Rubble Spillway-15'

+97-Fc Cox-24'

+38-Row Tree

+12-T.P.-25'

G.R.-16'

Fc-28'

78 Fc-39' G.R.-14'

10'

11'

77 Fc-28' G.R.-14'

10'

10'

Fc-Fc G.R.-16'

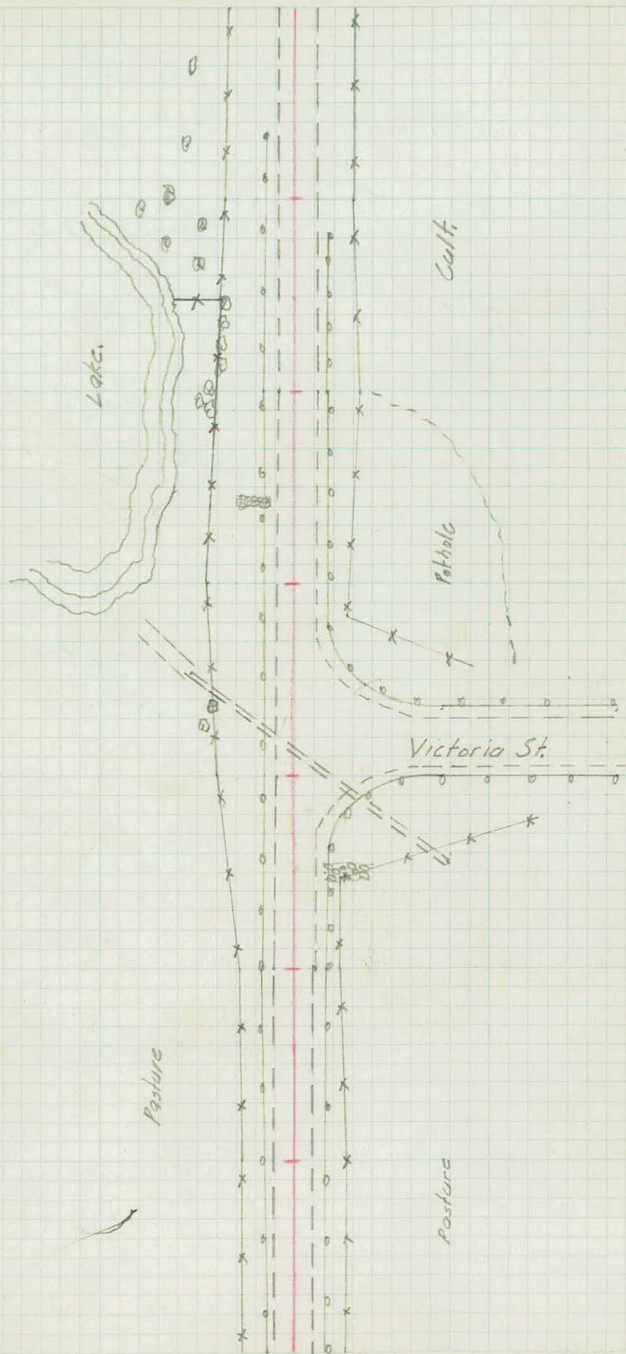
+66-T.P.-23'

76 G.R.-14 Fc-28'

10'

10'

G.R.-16'



+80-T.P.-28'
+75-Grass 1-Willow-35'

89

11'

9'

+79-10" Tw Oak-26'
+67-4" Poplar-27'
+55-6" Oak-28'
+45-5" Poplar-28'
+44-4" Willow Bush-29'
+39-2" Willow Bush-29'
+27-T.P.-28'
+18-Ent-12"X12" C.M.-22'
+71-5" Poplar-28'
+60-Cor Orchard-40
+79-Willow Bush-28'

88

11'

9'

+57-Orchard-37'

87

11'

9'

+67-T.P.-28'

86

10'

10'

+62-Fe Cor-26'

+78-Fe Cor-33'

+33-10" Oak-26'

+15-Box-110'

85

Fe-34

9'

10'

+13-T.P.-28'
Fe-36'

+64-P.P.-32'

84

+64-Ent-12"X16" C.M.-24'
Fe-32'

9'

11'

+65-Ent-12"X16" C.M.-25'
Fe-29'

+57-T.P.-28'

+68-S.W. Cor Ho-110'

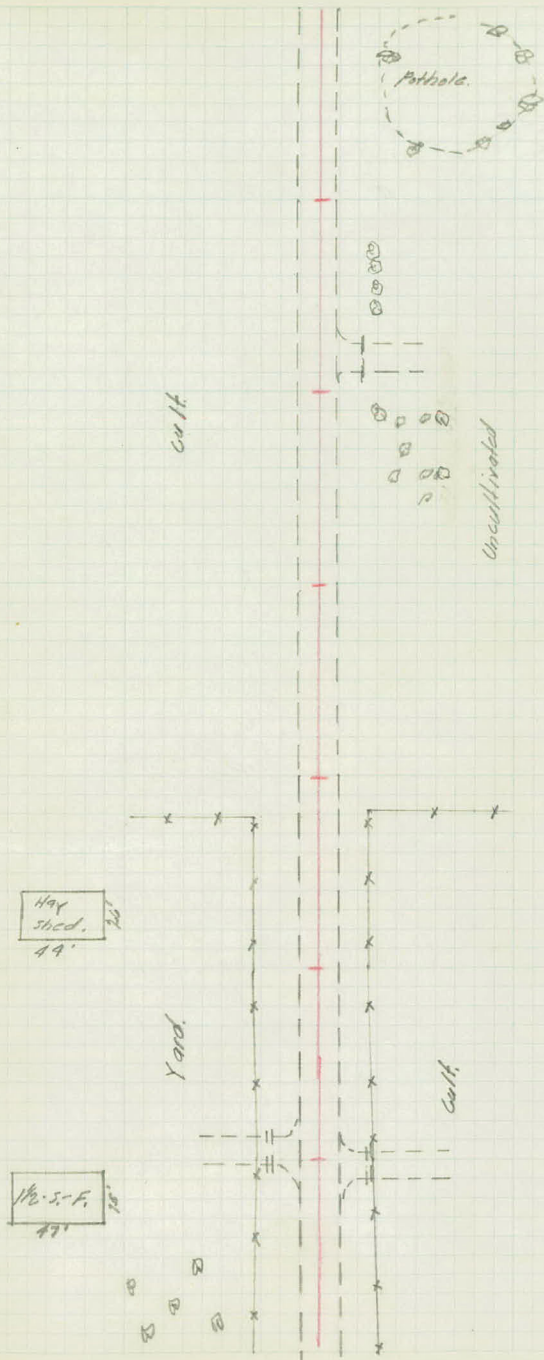
+43-Fe Cor-33'

83 Fe-34'

9'

11'

Fe-31'



+95-Bos. Fc.-45'

+80-Bos. Hedge-32'

+80-8" Tw. Barwood-44'

+53-Range Tie to Ho.

+96-S.W. Cor Ho.-77'

+43-End 12" W.G.C.M.-28'

+12-8" Field Cr.-46'

96 +04-6" Bar Elder-45' 13'

8'

+98-T.P.-28'

+13-End

95 +03-F.C. Cor-36'

11'

7'

+97-Range Tie

+42-T.P.-28'

94 Fc.-28'

11'

9'

93

11'

10'

+81-T.P.-28'

+33-Fc. Cor.-28'

92

11'

10'

+83-8" 12" W.G.C.M.

24'

26'

+55-T.P.-28'

91

10'

10'

90

11'

9'

18-5-18
33'



Cult

Cult

==

+66-S. Rd. Cor. Loc. Ho. - 34'
+62-T.P. - 28'

103 13' 9'

102 13' 8' +67-T.P. - 28'

101 12' 9'

+60-T.P. - 27'

100 13' 8'

+66-6.15" x 4.25" 6.00 20' 21'

99 13' 8' +68-T.P. - 27'

98 13' 8'

+79-Range Tie
+76-Pe. Cor. - 48'

+52-End Hedge - 38'

+53-T.P. - 27'

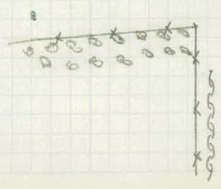
97 117' P.P. - 45' 10' 7'

11/22/98
K.R.
L.B.H.
L.C.
M.W.G.

10' 2" 20' KCHouse

Cult.

Cult.



+59-1" Pine - 44' - 6" Pine - 52'
 +52-8" Pine - 38'
 +48-5" Pine - 45-12" Pine - 59'
 +50-10" Pine - 45-10" Pine 59' PA - 22'
 +17-10" 39'
 +11-10" 52'
 +10-8" P.O.C. - 44'

+54-Ent. - 12' x 32' C.M. - 19'

110 Ent. 12' x 32' C.M. - 19'

8'

11'

109

9'

11'

+81-12" - 28'
 +85-12" x 10' 8" - 21' W.A.K. - 27'
 +82-Cor. Ho. - 46'
 +74-Rings Tie to Ho.
 +32-Cor. Orchard - 43'
 +39-Fc. Cor. - 32'
 +28-T.P. - 28'

108

9'

12'

+88-12" Apple Tr. - 27'

+90-Apple Tr. - 25'

107

Fc. - 31'

10'

13'

+93-R.P. - 31'

+73-Cor. Orchard - 30'
 +62-Fc. Cor. - 33'
 +57-Rings Tie

106

11'

13'

+84-R.P. - 37'

+69-N. Edge Bl. Top.

+97-S. Edge Bl. Top.

+82-Ent. Cul. - 27'

15' x 40' C.M.

105

10'

15'

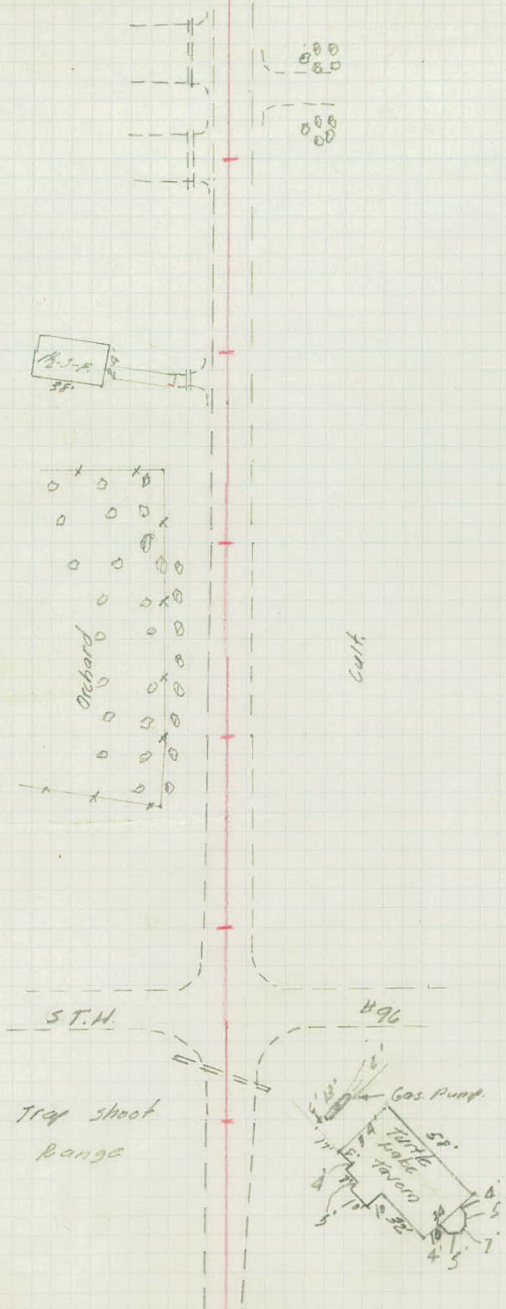
+16-Ent. 18' C.M. - 21'
 +13-T.P. - 28'

+82-Cor. Build. - 58'

104

12'

2'



117 $Fe_2 - 36'$ 9' 12'

+75-PP-28'

116 $Fe_2 - 40'$ 7' 12' G.L-15' $Fe_2 - 33'$

115 $Fe_2 - 36'$ PP-28' 9' 12'

+20-80y G.L-15'

114 $Fe_2 - 30$ 8' 13'

+20-PP-28'

113 $Fe_2 - 37'$ 9' 13'

+56- Δ 10 $Fe_2 - 34'$
+42-Long TIC
+34-Fe Cor-49'

+63-Fe Cor-33'

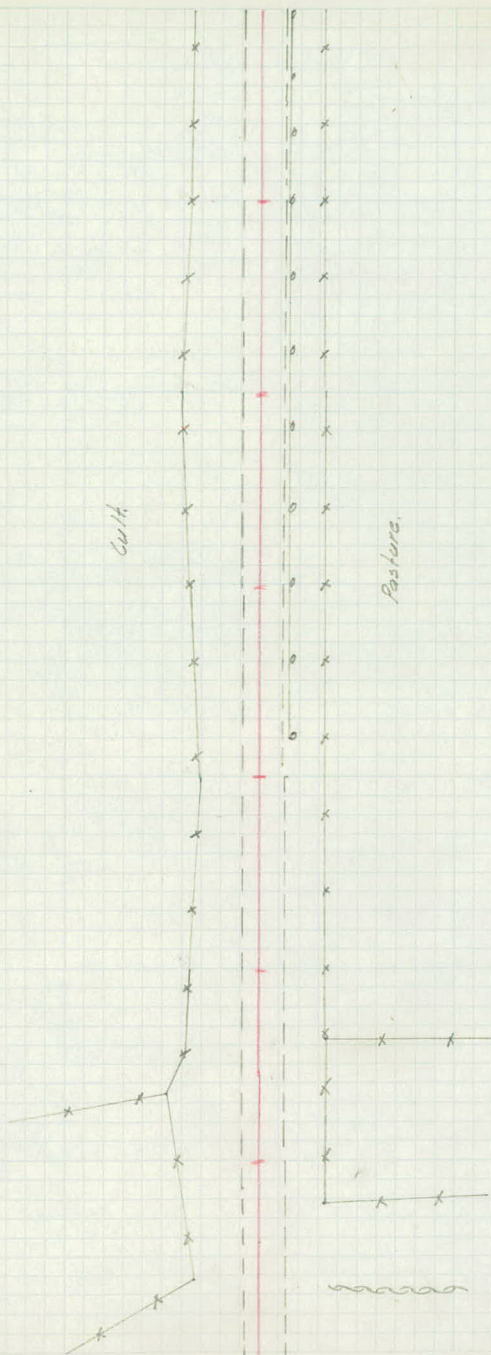
112 9' 13'

+57-Brace TIC
+49-PP-28'
+37-Fe Cor-34'

+77-Fe Cor-38'
+75-Brace TIC

+33-Hedge-37'

111 8' 12'



124 H3-Ent-15' K20/G.M.-29'

8'

14'

H97-FCOR-31'

H59-PP-28'

123 FC-33'

8'

14'

FC-30'

122

9'

14'

H87-PP-28'

H55-PP-28'

121 FC-33'

9'

18'

FC-30'

120

H18-PP+TP-28'

9'

12'

H97-Ent/G.R-15'

FC-30'

119

9'

12'

H86-Ent.
H76-FC Cor-39'

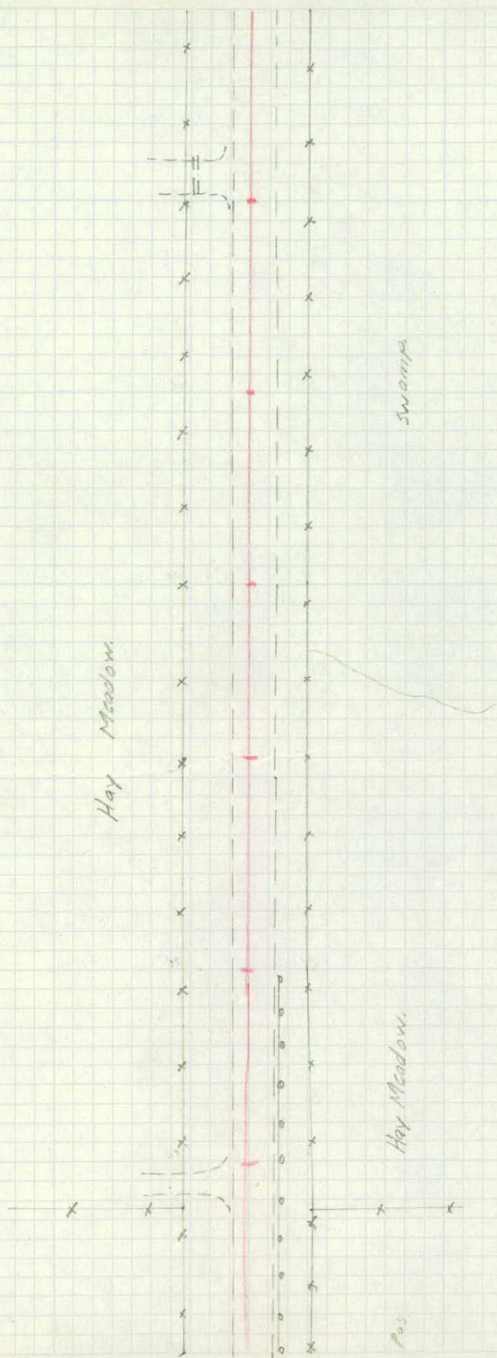
H76-FC Cor-31'

H95-TP-28'

118 FC-39'

9'

12'



+78-Fc. Cor- 23'

+80-W. End. Cul- 18' G.M. 15'

+73-P.P.-28'

+84-E. End. #1. Top

18' x 97' G.M.

+77-S. End- 18' G.M. -37'

+70-E. End- 18' G.M. -31'

131 Fc-33'

8'

15'

+95-P.P.-28'

130

7'

16'

129 Fc- 33'

7'

17'

+75-T.P.-28'

128

7'

15'

127 Fc-33'

6'

16'

+90-P.P.-28'

126

7'

14'

+25-P.P.-28'

125 Fc-33'

8'

14'

Co. Rd. "G"

Swamp

Swamp.

+75-End.

138

10'

11'

+108-T.P.-28'

+85-End Trees 1000-57'

+76-Fe. Cap.-33'

+58-R.P.-25'

137

9'

11'

+79-T.P.-28'

+84-End. 10°C. 100-21'

+52-End 10" V. 14' - 15'

136

8'

11'

Fe.-32'

+93-T.P.

135 Bush + Trees - 57'

9'

11'

+65-R.P.-28'

134

9'

11'

+10-T.P.-27'

Fe.-31'

133 Redoubt Ling - 33'

9'

12'

Fe.-30'

+70-T.P.-27'

132 Brush Ling - 36'

+62-N. End 81. 100'

+22-T.P.-26'

+19-Δ 10 Fe.-30'

+9-Fe.-30'

+17-N. End - 10' 61? 38'

Bush, Tamarack, Birch, Elms, willows

Pasture.

==P

120-Box 100-35'

145

11'

12'

153-T.P.

13

125-Box 100-35'

12-6" Ladder - 34'

144

10'

173-Eok

177-12" Box 100-41

174-Box 12-34

143

9'

11'

150-PR

124-T.P.

142

9'

11'

T.P.

F2-35'

141

9'

11'

170-T.P.

152-PR

140

10'

11'

124-Box 100-35'

193-T.P.-28'

139

9'

12'



Uncult.

Cult.



152

10'

9'

Box w/100ds
170° to Cor - 33'

+30-PR-

+34-T.R.

+10-T.R.-

151 Brush - 21'

11'

9'

150 Brush - 20'

11'

9'

+21-T.R.

+38-PR.

149 Brush - 70'

11'

9'

+50-T.R.-

148 Brush - 70'

11'

9'

+34-12' (208 V.L.)

32' 18'

+33-T.R.

147 Brush - 35'

11'

9'

+44-PR.

+17-T.R.-

+22-End Line Tracer 29'

146 Brush - 35'

10'

11'



Brush

Cult.

470-T.R.

159

9'

11'

463-T.R.-

130-Ent.

422-PR

420-Ent Brush-31'

426-Ent Hodge-31'

158

11'

9'

467-5.1 Cor Ho.-24'

448-Ent.

439-T.H.-24'

425-FG Cor-38' Reg. Hodge-31'

157 Brush-32'

10'

10'

156

10'

10'

414-T.R.-

423-T.H.-28'

155 Brush-34'

10'

9'

FG-33'

461-T.R.

154

11'

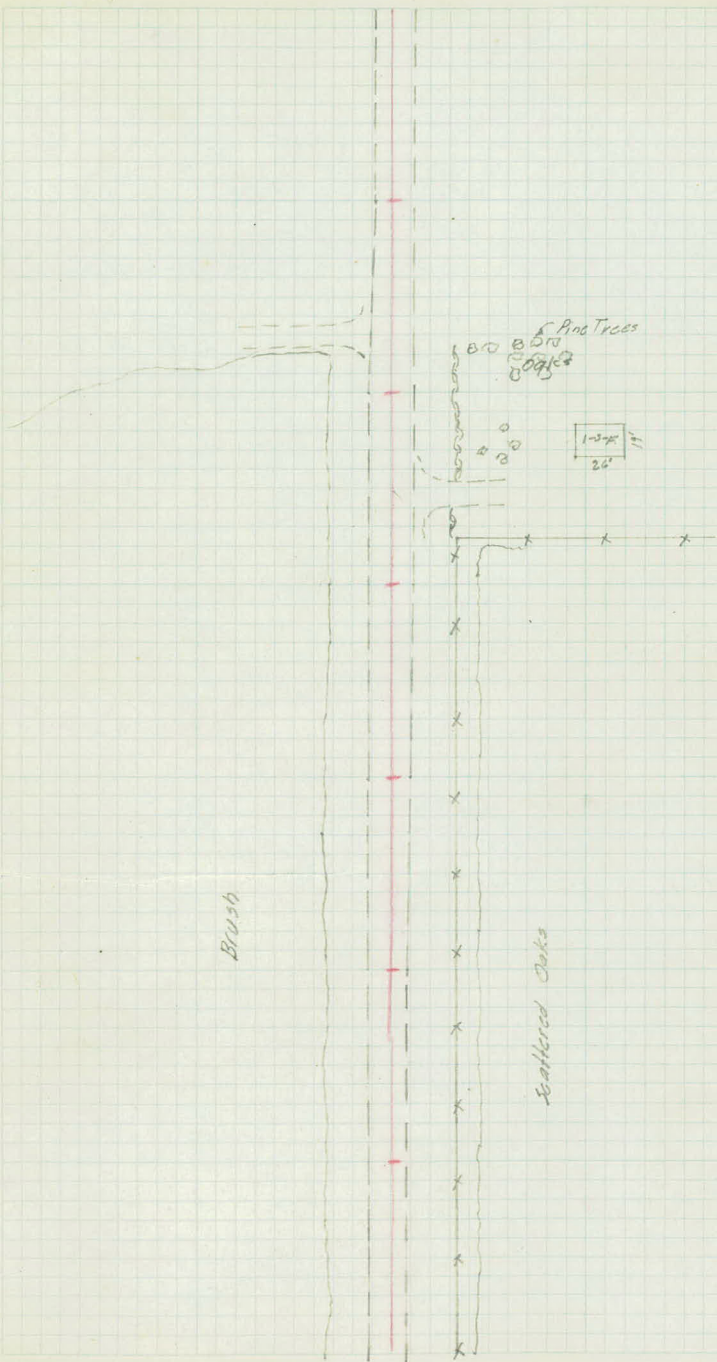
9'

462-T.R.-

153 Brush-32'

11'

9'



+ T.R.
 + 33-How Wadsw. 33'
 + 25-Low 5' Sparwax-33'

166 9' 10'

165 9' 10'

+ 09-T.R.-29' End Pt.-33'

+ 25-P.R.

164 9' 11'

+ 88-T.R.

163 8' 11'

+ 44-Fs Cor-33'
 + 01-T.R.

162 9' 11'

+ 28-N.R.

161 9' 10'

+ 18-T.R.

160 9' 11'

+ 04-Ext-12' N16' 64A-24'

0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0 0

Uncult.

Uncult.

Uncult.

Uncult.



+50-Ent-15'x20'CM-22'

173

10'

9'

+02-T.P.-

+95-End Bud to Row Trass 29'

172

11'

9'

+70-Bgs. Bud to Row 2" Elms-32'-43'

+72-4 1/4" Cedar-33'

+66-Row 1" Cedar-31'

+52-Ent

+43-T.P.-

+35-End Oak-Woods-42'

+44-PR-
+33-Ent

171

10

9'

170

10'

9'

+99-T.P.-

+92-PR

+45-Ent-15'x20'CM-20'

+32-Bgs. Oak Woods-36'

+44-End Pine 2 Trees 33'-50'

169

10'

9'

+63-T.P.

168

10'

9'

Bgs. Pine Trass-33'-50'

+58-T.P.-

+40-Ent

+25-PR

167

9'

9'

Hay Meadow.

57/40

Oaks

Uncult.

Uncult.

2" to 15" Traces

f. 30-T.P. -

180

10'

8'

179

10'

8'

f. 07-T.P. -

178

11'

9'

f. 70-T.P. -

177

11'

9'

f. 65-Ent.

f. 44-Ent.

f. 13-T.P.

176

11'

9'

175

11'

9'

f. 57-T.P.

174

11'

9'

Hay Meadow.

Hay Meadow.

Uncult.

Uncult.



+89-GP-21'

+94-110 Fc-33'

+91-T.P.-

+52-Δ 10 Fc-19'

187

11'

9'

+44-T.P.-

+40-Δ 10 Fc-21'

+52-Δ 10 Fc-31'

+30-Low 20' Paplora-33'

+20-Ent. 12" X 23' Vit-29'

+10-Low Rd Vlt-33'

186

11'

9'

+53-T.P.-

185

11'

9'

+65-R 12" X 54' Vit. Fc-23'

30' 24'

+27-T.P.-

184

10'

9'

183

10'

9'

+52-Ent. Cule-24'

15" X 48' Vit.

+92-Ent. Suld-24'

+90-T.P.-

+23-Ent-12" X 24' Vit-
25'
30'

182

10'

9'

+63-T.P.-

181

10'

9'

Cult.

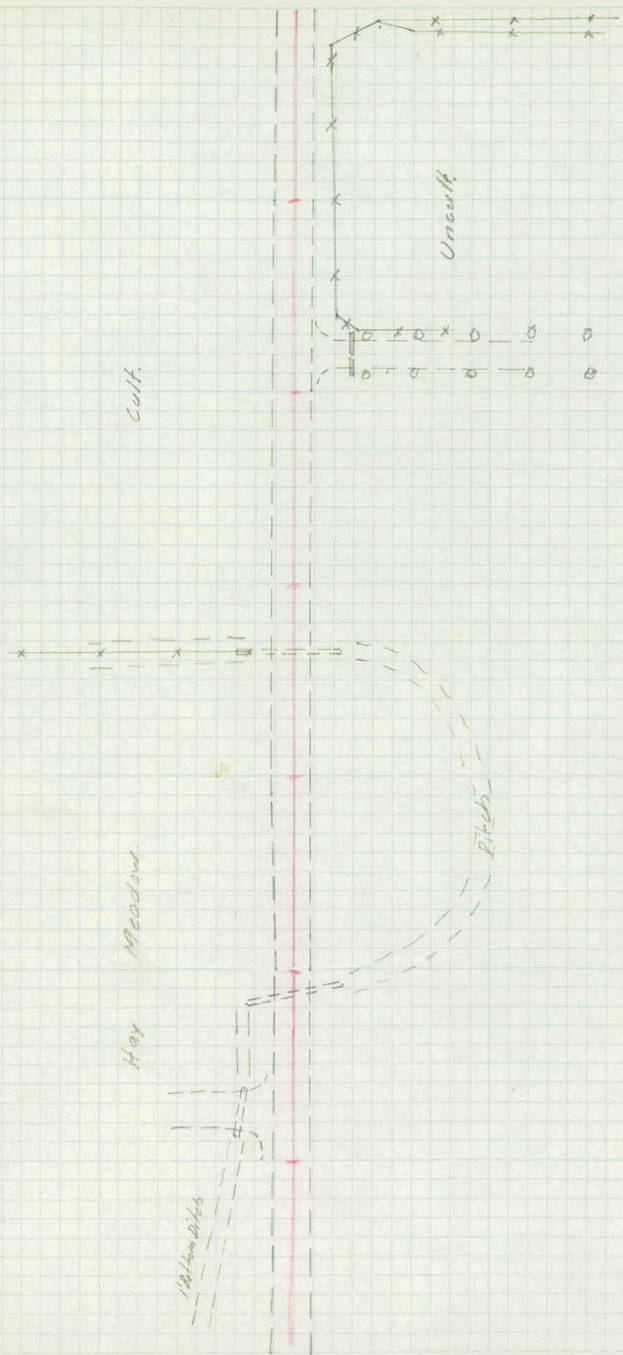
Uncult.

Hay Meadow.

Hay

Wetlands

Pitch



+62-Ent.

+46-T.P.-

+42-Cor Pines -50'

194

11'

10'

+77-P.P.-28'

+76-Ent-

+63-Low R.R. Elders -33'

+15-T.P.-

+10-Cor. Pine Grove -49'

193

10'

10'

+97-Ent.

+86-60a Nursery -37'

192

10'

9'

Nursery -34'

+89-T.P.-

+29-Cor Nurseries -42'

+18-Ent.

191

10'

9'

+52-T.P.-

190

10'

9'

+52-End Low Cadets -34'

+30-T.P.-

189

10'

9'

+17-Hop. Low Cadets -36'

+02-Ent -12" x 20' L.M. - 26'

188

10'

9'

Cult.

Vine Yard

Heavy Pines

O/P Pines

105-T.P.-

145 & 30' X 38' C.M.

34' 24'

201 Fc. 19'

10'

8'

175 & Rd. - 15' X 20' C.M. - 25'

125-T.P.-

200 Fc. 21'

9'

9'

199 Fc. 21'

10'

10'

180-T.P.-

198

10'

9'

195- Δ 10 Fc. 23'

180-10' Coll. - 10' Fc. 24'

150-Ent. - 10' W. C.M. - 21'

184-15' Tw. Coll. - 23'

166-Ent. 10' X 10' C.M. - 21'

131-T.P. - 29'

198-30' Coll. - 37'

124-29' Coll. - 37'

197 Fc. 36'

11'

9'

198-10' Coll. - 30'

172-20' Coll. - 37'

120-20' Coll. - 38'

100- Fc. 40' - 42'

196

10'

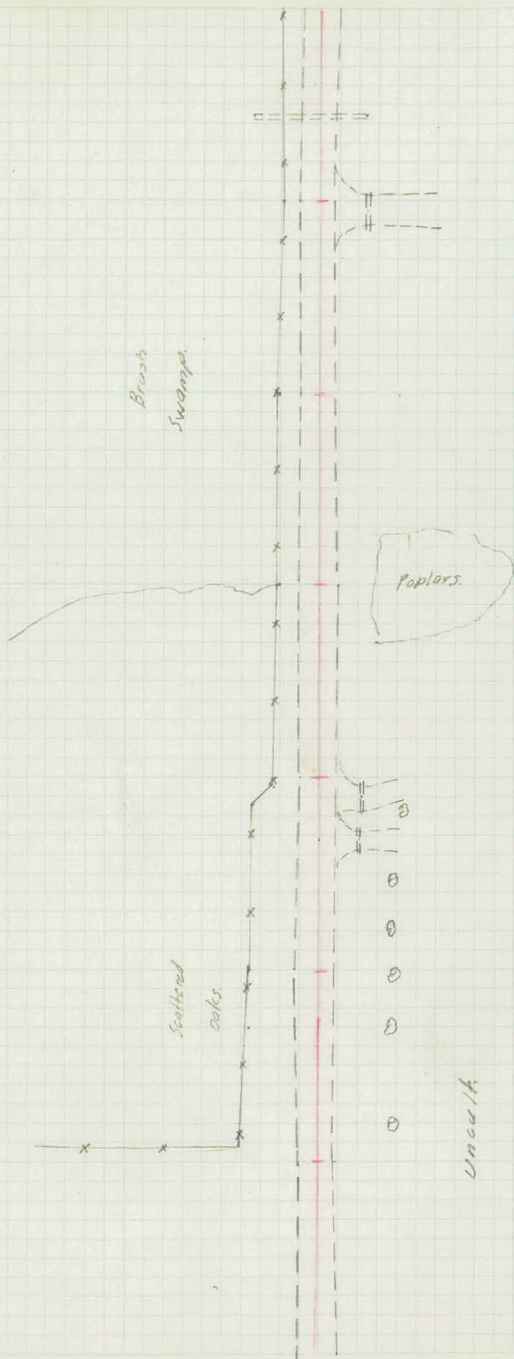
8'

195-T.P.-

195

10'

10'



+80-SEnd 26' CAT-32'

+60-T.P-34'
13' +50

208

8'

11'

+20-T.P-29'

207 Fe-21'

8'

11'

206

8'

11'

+81-T.P-

205 Fe-21'

9'

11'

+42-T.P-

204 Fe-21'

9'

11'

+80-End-24' X 20' CAT-25'

203 Fe-21'

9'

10'

+64-T.P-

202

9'

10'

Waste land

Cult.

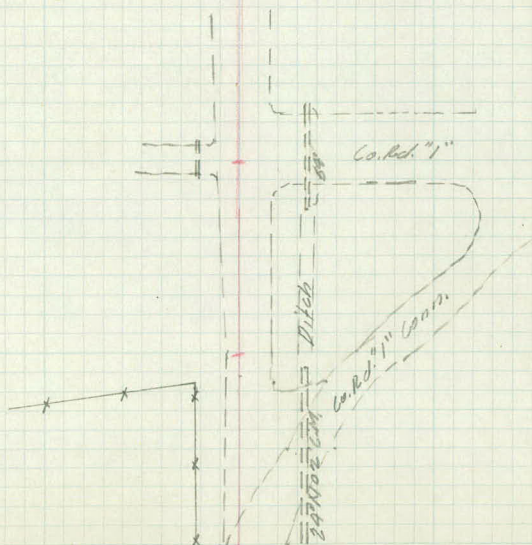


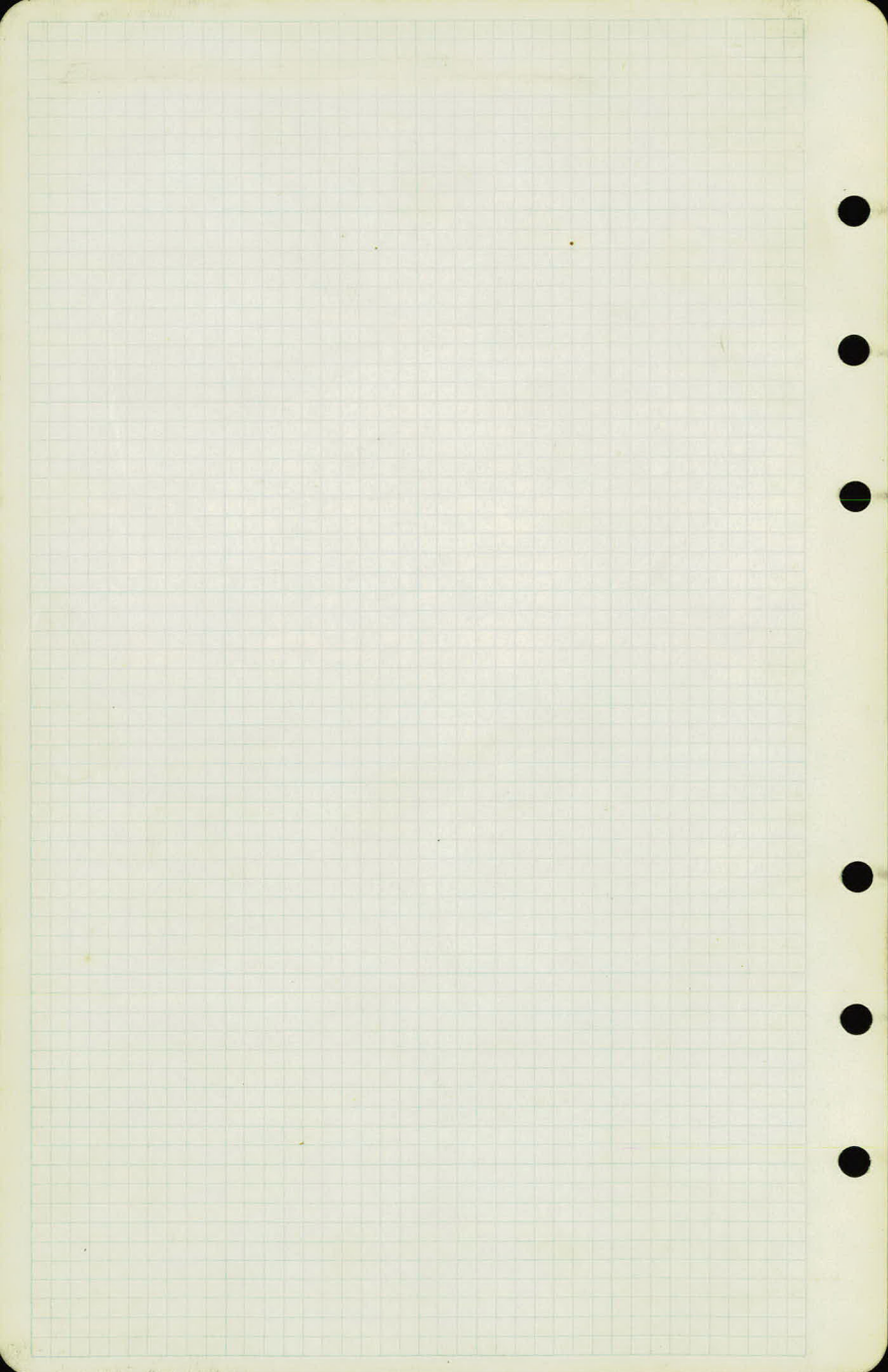
+75. S. End 20°C. M-35'
+68. T. p-38'

17'-45' + 85'

25' 49' 450

25'





Topog -
Lexington Ave

8-5-41
HAW
A.M.
L.G.

218

11'

14'

217

11'

14'

216

11'

14'

215

10'

15'

214

10'

15'

213

10'

16'

212

10'

15'

211

+73 P.P. 28'

Fc 33'

+18 Sta. 40'

Fc 32'

Wooded Pasture

+60 Oak 44'

+32 Oak 42'

+29 Oak 42'

Fc 32

+23 P.P. 28'

Fc 32 Trees 50'

+78 P.P. 27'

+90 Fc Cor. 32'
+ Beg Woods 50'

Fc 34'

+51 P.P. 28'

Uncultivated

Pasture

Fc 34'

+00 P.P. 28'

Fc 35'

+45 E. Rad. 18'

+35 F.C. Cor. 35'

+27 G.P. 38'

+15 Beg Rad 47'

+02 24" X 52" C.M.
Co Rd I

+02 Ent. 12" X 20" C.I.P.

225

12'

13'

224

11'

14'

223

11'

14'

222

11

14

221

12'

13'

220

11'

14'

219

11'

14'

218

11

14'

Fc 36'

+78 P.P. 28'
+20 Fc Cor 38'
+20 6" Birch 42'

Brush &
Pasture

+38 P.P. 28'

+02 P.P. 28'

+63 P.P. 27'

+17 P.P. 28'

Uncultivated

Woods & Pasture

Fc 38'

+20 Fc Cor 32 End Woods
Fc 33' Treeline 75'

+41 6" Oak 42'
+39 16" Oak 34'

Fc 33' Treeline 75'

+55 End Pothole 33'

Trees 100'
Fc 33' Pot Hole 33' 60'

+35 Beg Pot Hole 35'

Fc 33' Trees 100'

+32 6" Oak 40'

+26 10" Birch 38'

Fc 33' Trees 50'

+50 Gr. 3 Oaks 45'

+32 Sto. 41'

Fc 33'

+19 Oak 42'

Fc 33

232

13'

14'

231

13'

14'

230

13'

14'

229

13'

13'

228

13'

14'

227

13'

13'

226

11'

14'

225

12

13'

+97 P.P. 28'
 +70 Ent 44'
 +50 Rqctic Ent.
 +35 10" Oak Fc Cor 33'
 +21 Rqctic Fc.
 +23 6" Oak 20'
 Fc 28'

+44 P.P. 27'
 +32 Ent Brush 80-150'
 Fc 26 Brush 30'

+50 Brush 75'

+00 Brush 100'
 +00 P.P. 28' Fc 28'

Fc. 29' Brush 35'-150'

+59 P.P. 27'

Fc 30' Brush 40'

+60 Brush 40'
 +48 Stu 21'
 +17 P.P. 28'
 Fc 36' Brush 100'

Fc 36'

+85 6" Birch 34'
 +74 Ent
 +62 15" Oak 42'
 +52 Fc Cor 35'

Fc 35' Pothole ^{End} 35'-40'

Fc 32' Pothole 32'-125'

Fc 32' Pothole 32'-150'

Fc. 32' Pothole 32'-158'

+33 Pothole 34'-130'
 Fc 33 Beg Pothole 62'

+78 Fc Cor 33'
 +72 Rqctic Fc.
 +59 Stu 35'

Fc 37'

+94 10" Oak 28'
 +85 6" Oak 35'

Fc 38'

Brush

Pothole

Hayfield

238

237

15'

14'

236

11'

15'

235

12'

15'

234

12'

14'

233

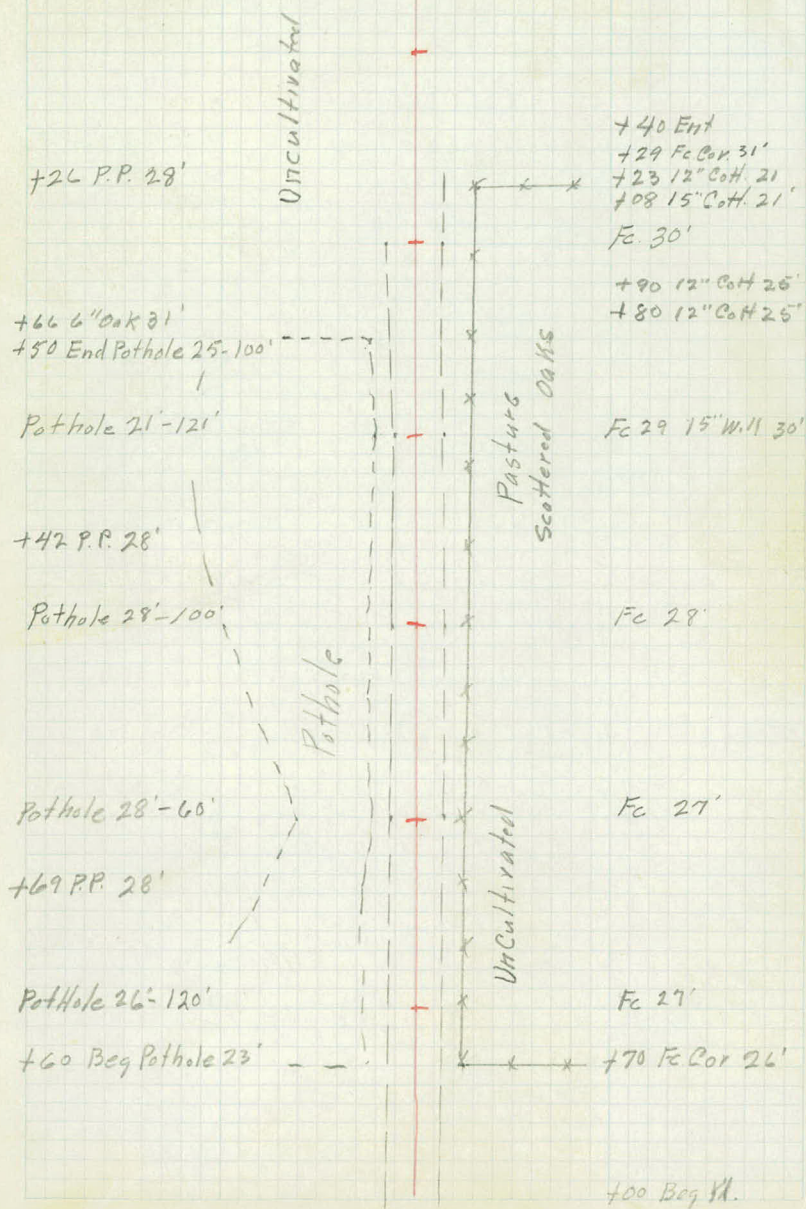
13'

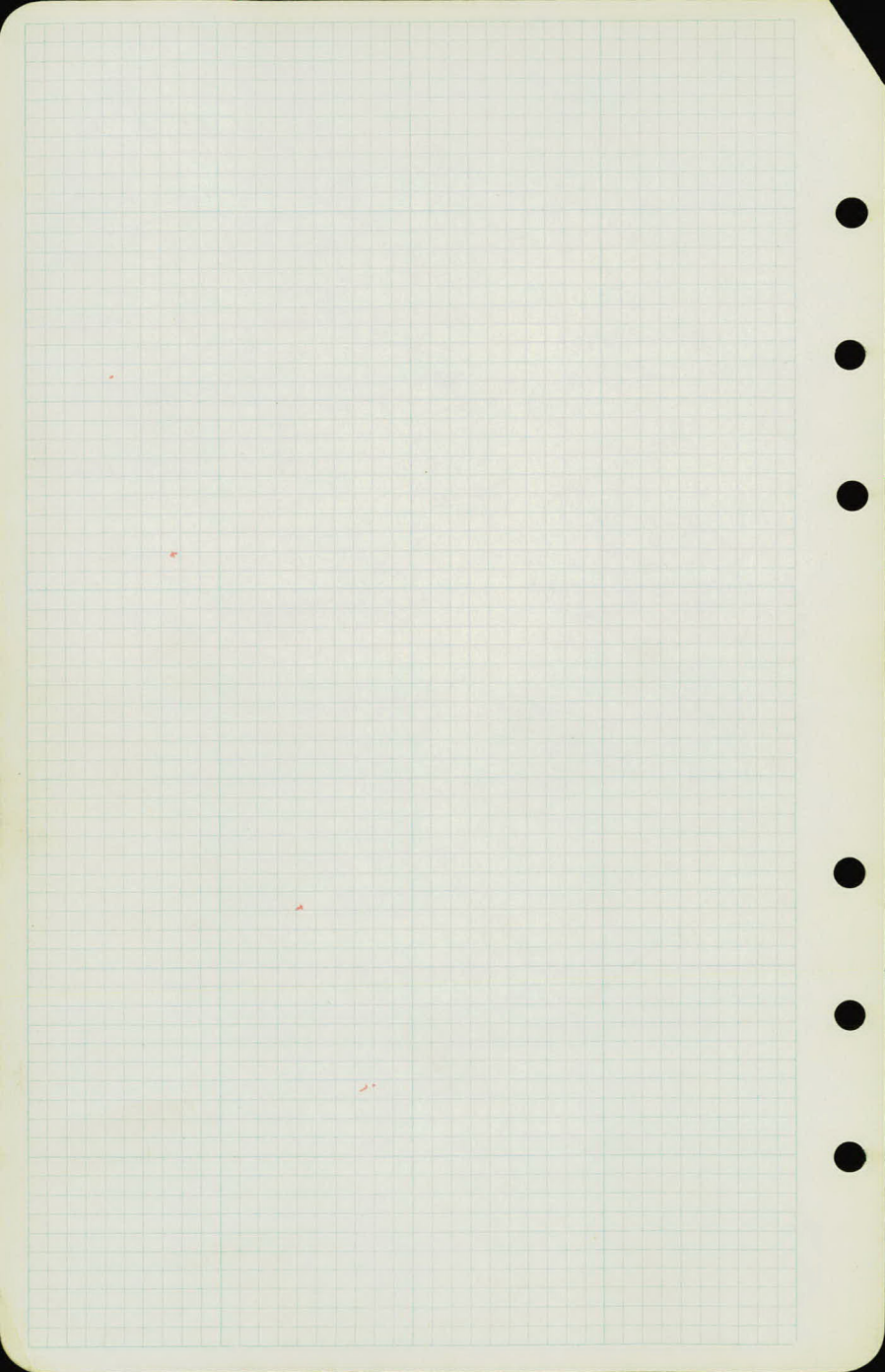
13'

232

13

14'





Bench Levels

Sta.	+	-	-	Elev.
B.M.	1.32	947.63		946.31
T.P.	1.99	936.92	12.70	934.93
T.P.	4.50	936.94	4.48	932.44
B.M.			2.55	934.39
T.P.	3.33	935.85	4.42	932.52
T.P.	8.39	941.29	3.15	932.70
B.M.			4.12	937.17
T.P.	6.54	943.61	4.22	937.07
T.P.	4.96	945.81	2.76	940.85
B.M.	8.09	949.43	4.47	941.34
T.P.	7.15	954.88	1.70	947.73
T.P.	12.92	966.41	1.39	959.49
B.M.	11.47	976.48	1.40	965.01
T.P.	13.65	989.55	0.58	975.90
T.P.	13.47	1002.90	0.12	989.43
T.P.	9.71	1011.97	0.64	1002.26
B.M.			4.79	1007.18
T.P.	2.79	1008.64	6.12	1005.88
T.P.	0.15	995.59	13.20	995.44
T.P.	0.06	982.58	13.07	982.52
T.P.	1.50	970.44	13.64	968.94
B.M.	3.96	965.02	7.38	961.06
T.P.	5.52	967.38	3.16	961.86
T.P.	4.79	966.37	5.80	961.58
B.M.			5.80	960.57

Descriptions

Top Mont. Max & Co. Rd "E"

Spk in 2d Elm 33' Dt. 5/9. 17+28

Top Mont. Maxington & Kowalski Rd.

Spk. in T.P. Rt 39+68

Top Mont. Maxington & Co. Rd "F"

Spk. in T.P. Rt. 67+98

Spk. in Co. Rd. 15' Lt. 5/9. 79+95 ✓

Spk. in T.P. Rt. 92+87

Sta	+	π	-	Elev.
		966.37		
T.P.	1.23	962.41.	5.19	961.18.
T.P.	3.60	956.67.	9.34	953.07.
B.M.	0.52	951.86.	5.33	951.34.
T.P.	0.88	942.88.	9.86	942.00.
T.P.	0.30	930.89.	12.29	930.59.
T.P.	0.35	918.50.	12.74	918.15.
T.P.	0.50	906.40.	12.60	906.90.
B.M.	2.05	899.85.	8.60	897.80.
T.P.	4.73	898.73.	5.85	894.00.
B.M.	6.11	899.08.	5.76	892.97.
T.P.	9.42	906.82.	1.68	897.40.
T.P.	9.14	913.65.	2.31	904.51.
B.M.	6.46	913.60.	6.51	907.14.
T.P.	7.50	914.27.	6.83	906.77.
T.P.	8.92	923.01.	0.18	914.09.
B.M.	2.91	920.74.	5.18	917.83.
T.P.	5.12	917.84.	8.02	912.74.
B.M.	4.75	914.20.	8.39	909.45.
T.P.	0.00	904.27.	9.93	904.27.
B.M.	8.20	903.27.	9.20	895.07.
T.P.	5.39	906.84.	1.82	901.43.
T.P.	0.03	897.59.	9.28	897.56.
B.M.			4.72	892.87.
T.P.	5.09	897.46.	5.22	892.37.
B.M.			5.23	892.23.

Description

Top Mont. Lexington 8" S.T.H. #96

Spk. in T.P. Lt. sta. 120+18

Top Mont. Lexington 8" S.T.H. #96

Spk. in P.P. Lt. sta. 146+44

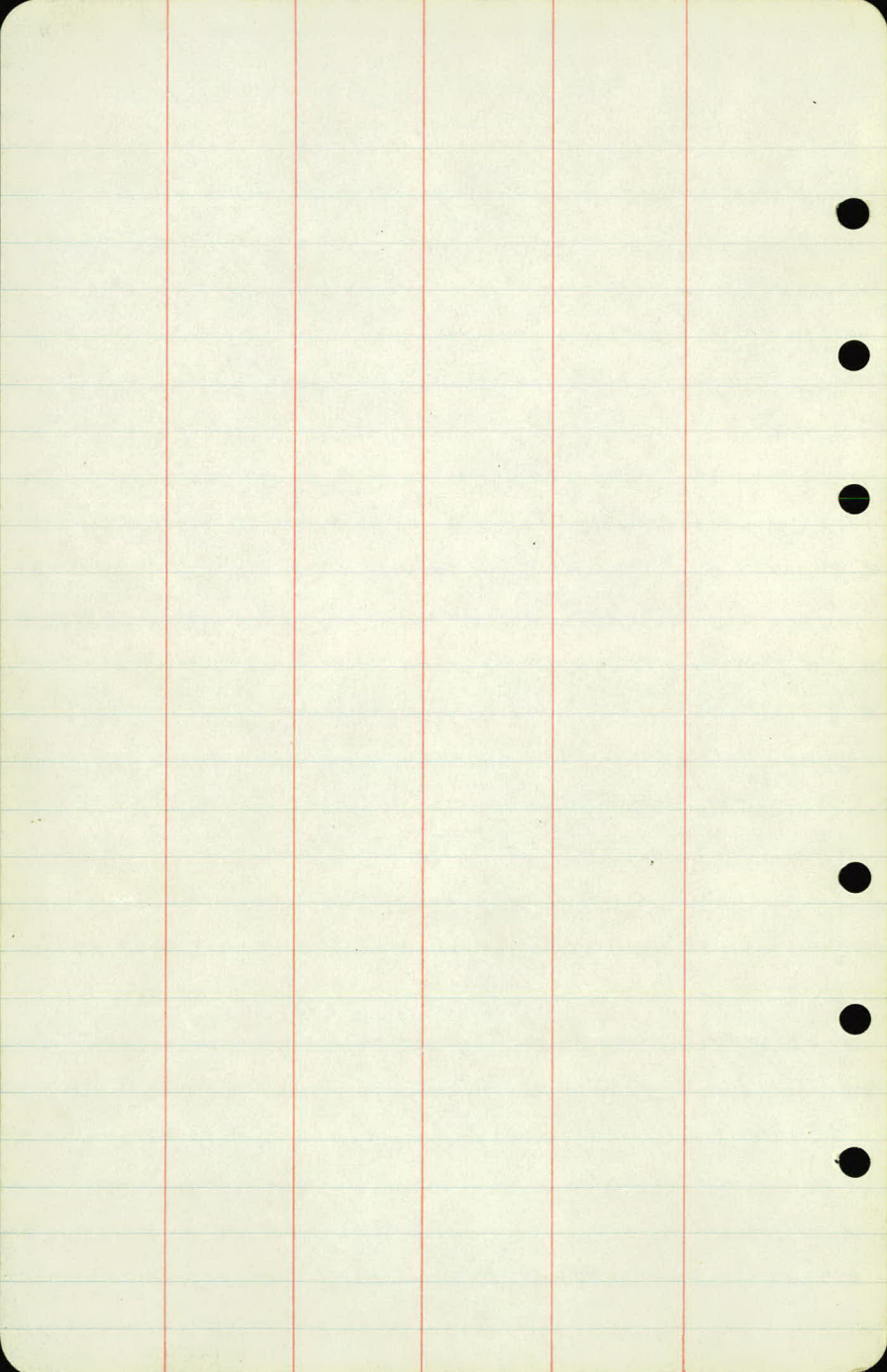
Top Mont. sta. 138+23.6

Spk. in P.P. Lt. sta. 171+44

Top Mont. 184+63.02

Spk. in T.P. Rt. sta. 198+88

Spk. in P.P. Lt. sta. 210+68



Berch levels

8-5-41

HAW
AM
LG

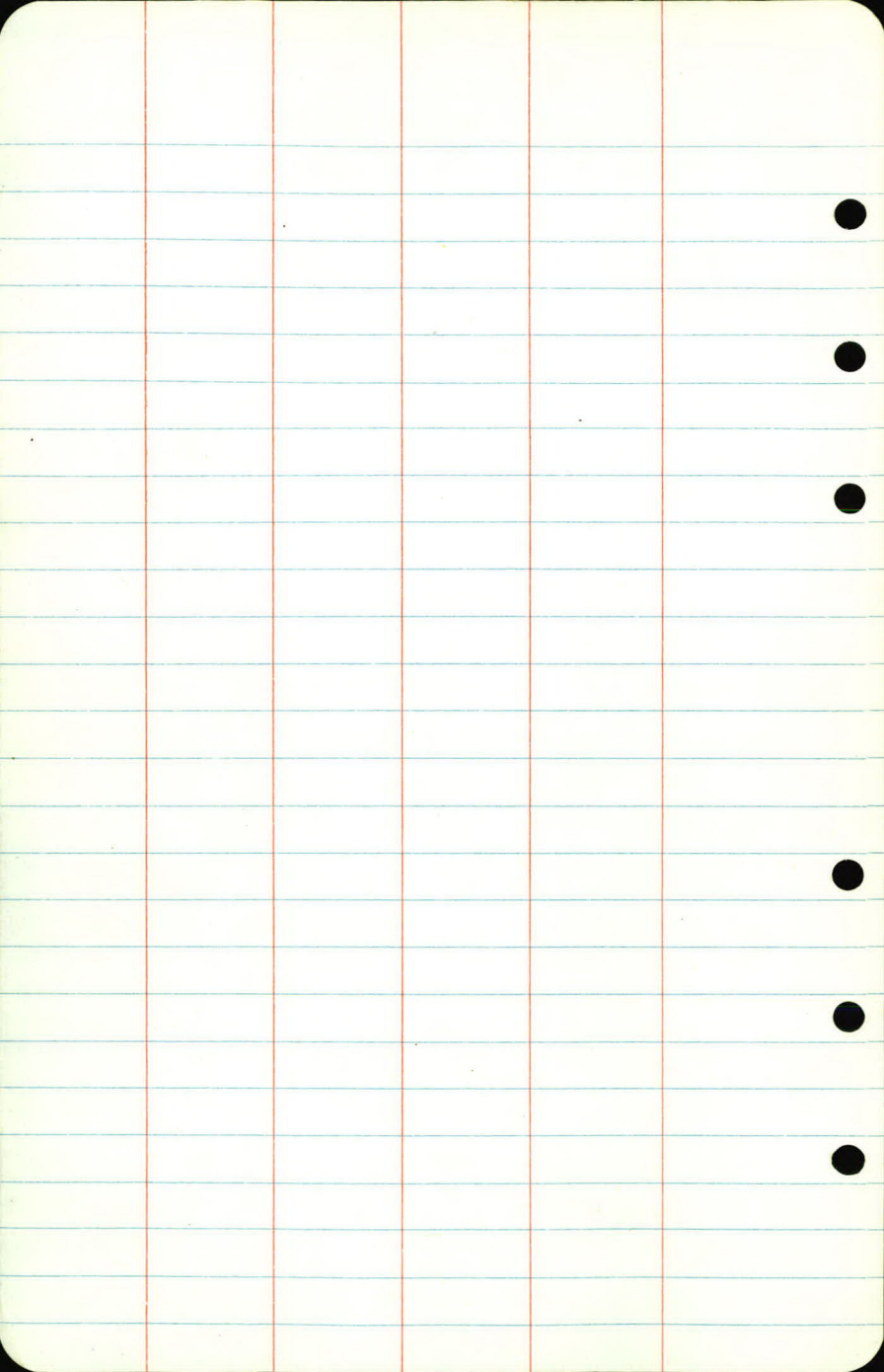
Sta	+	π	-	Elev
B.M.	5.54	898.42.		892.88.
	5.15	897.25.	6.32	892.10.
	4.34	896.84.	4.75	892.50.
B.M.	5.64	897.92.	4.56	892.28.
	9.62	905.49.	2.05	895.87.
	3.41	904.23.	4.67	900.82.
B.M.	2.35	904.23.	2.35	901.88.
	2.18	899.30.	7.11	897.12.
	5.14	900.98.	3.46	895.84.
B.M.			1.86	899.12.

SAGE
Spk in T.P. 28' Rt Sta 198+68

Spk in T.P. 28' Lt Sta 210+68

Spk in 15" Oak 90' Rt Sta 223+00

Spk in 15" Catl. 21' Rt Sta 237+25



x sections

Void. pages 43-50

see revised sections

Sta	+	T	-	Elev.
B.M.	2.04	945.35		946.31
0	+00			46.31
	+22			45.8
	+25			45.8
	+50			45.4
1				44.8
	+50			44.4
	+80			44.0
2				43.8
	+26			43.7
+47	Top Manhole			
+58				43.7

11/25/38
L.A.
L.B.H.
L.C.
M.C.

44

Lt.

4

Rt.

Top Most Lexington + Co. Rd. E"

$$\frac{28}{50} \quad \frac{213}{135} \quad \frac{204}{135} \quad \frac{205}{135} \quad \frac{18}{50}$$

$$\frac{35}{59} \quad \frac{32}{50}$$

$$\frac{26}{19} \quad \frac{26}{50} \quad \frac{29}{50}$$

8620

$$\frac{41}{50} \quad \frac{45}{58} \quad \frac{45}{57} \quad \frac{30}{50} \quad \frac{29}{13} \quad \frac{26}{12} \quad \frac{26}{23} \quad \frac{29}{50} \quad \frac{32}{50}$$

$$\frac{48}{59} \quad \frac{52}{24} \quad \frac{32}{15}$$

$$\frac{30}{7} \quad \frac{32}{23} \quad \frac{37}{50} \quad \frac{38}{50}$$

$$\frac{70}{50} \quad \frac{77}{23} \quad \frac{41}{15} \quad \frac{39}{8} \quad \frac{36}{12} \quad \frac{39}{12} \quad \frac{44}{22} \quad \frac{41}{40}$$

$$\frac{72}{50} \quad \frac{93}{55} \quad \frac{89}{23} \quad \frac{49}{15} \quad \frac{14}{8} \quad \frac{40}{10} \quad \frac{43}{16} \quad \frac{46}{35} \quad \frac{47}{35}$$

$$\frac{105}{50} \quad \frac{27}{22} \quad \frac{56}{16} \quad \frac{48}{7} \quad \frac{44}{10} \quad \frac{47}{13} \quad \frac{49}{33} \quad \frac{47}{33}$$

$$\frac{94}{50} \quad \frac{95}{37} \quad \frac{83}{21} \quad \frac{57}{16} \quad \frac{49}{10} \quad \frac{46}{10} \quad \frac{50}{12} \quad \frac{50}{30}$$

$$\frac{88}{50} \quad \frac{78}{35} \quad \frac{68}{20} \quad \frac{51}{16} \quad \frac{49}{8} \quad \frac{47}{10} \quad \frac{49}{35} \quad \frac{51}{35}$$

51

43.3

$$\frac{78}{50} \quad \frac{89}{41} \quad \frac{65}{22} \quad \frac{51}{16} \quad \frac{49}{7} \quad \frac{47}{10} \quad \frac{50}{37} \quad \frac{50}{50} \quad \frac{51}{50}$$

Sta	+	-	Elev.
-----	---	---	-------

948.35

So. Rail / Spur Track

2	+84		43.8
---	-----	--	------

+99.3	Top So. Rail		43.67
-------	--------------	--	-------

+99.4	Top No. Rail		43.68
-------	--------------	--	-------

2	+99.9	Top So. Rail	43.60
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+14.9	Top No. Rail		43.60
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+38			42.4
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4	+70		40.9
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4			40.1
---	--	--	------

T.R.	0.23	940.30	8.28	940.07
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+41			39.0
-----	--	--	------

5			37.3
---	--	--	------

Lt

A

Rt

43.22

5.13

$$\frac{12.3}{50} \quad \frac{58}{29} \quad \frac{51}{16} \quad \frac{48}{9} \quad \frac{46}{8} \quad \frac{49}{8} \quad \frac{53}{20} \quad \frac{51}{50}$$

$$\frac{56}{50} \quad \frac{53}{16} \quad \frac{48}{12} \quad \frac{46.8}{}$$

467475

$$\frac{475}{10} \quad \frac{49}{15} \quad \frac{5.3}{15} \quad \frac{6.1}{50}$$

$$\frac{14.8}{50} \quad \frac{13.2}{27} \quad \frac{70}{16} \quad \frac{64}{10} \quad \frac{60}{9} \quad \frac{69}{9} \quad \frac{72}{16} \quad \frac{11.8}{26} \quad \frac{12.0}{50}$$

$$\frac{156}{50} \quad \frac{152}{29} \quad \frac{8.9}{17} \quad \frac{79}{9} \quad \frac{75}{8} \quad \frac{7.8}{8} \quad \frac{8.2}{16} \quad \frac{18.5}{29} \quad \frac{13.5}{50}$$

$$\frac{15.2}{50} \quad \frac{14.8}{31} \quad \frac{13.0}{22} \quad \frac{9.2}{16} \quad \frac{8.7}{9} \quad \frac{8.3}{8} \quad \frac{8.5}{16} \quad \frac{9.1}{26} \quad \frac{12.3}{25} \quad \frac{12.7}{50}$$

$$\frac{4.9}{50} \quad \frac{2.9}{20} \quad \frac{2.0}{16} \quad \frac{1.7}{9} \quad \frac{1.8}{8} \quad \frac{1.7}{16} \quad \frac{1.5}{25} \quad \frac{4.8}{25} \quad \frac{5.6}{50}$$

$$\frac{100}{50} \quad \frac{90}{16} \quad \frac{7.7}{22} \quad \frac{4.1}{16} \quad \frac{3.4}{9} \quad \frac{30}{9} \quad \frac{3.5}{17} \quad \frac{40}{17} \quad \frac{7.9}{27} \quad \frac{8.2}{50}$$

Sta	t	A	-	Elev.
		940.30		
5	+50			33.8
6				34.0
	+50			32.7
7				31.9
	+50			31.7
8				31.9
T.P.	502	936.90	842	931.28
	+50			32.3
9				32.5
	+50			32.2
10				31.9
	+50			31.9

Lt

L

Rt

$$\begin{array}{cccccc} \frac{111}{50} & \frac{109}{36} & \frac{101}{22} & \frac{94}{15} & \frac{50}{70} & \frac{45}{11} \end{array} \quad \begin{array}{ccc} \frac{50}{11} & \frac{60}{17} & \frac{102}{26} & \frac{103}{30} \end{array}$$

$$\begin{array}{cccccc} \frac{124}{50} & \frac{122}{31} & \frac{113}{22} & \frac{77}{16} & \frac{68}{10} & \frac{63}{9} & \frac{67}{16} & \frac{74}{25} & \frac{118}{50} & \frac{117}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{122}{50} & \frac{124}{26} & \frac{120}{22} & \frac{91}{15} & \frac{81}{10} & \frac{76}{10} & \frac{81}{17} & \frac{91}{17} & \frac{122}{26} & \frac{132}{27} & \frac{126}{28} & \frac{128}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{121}{50} & \frac{134}{26} & \frac{131}{23} & \frac{131}{22} & \frac{95}{15} & \frac{88}{10} & \frac{84}{9} & \frac{88}{9} & \frac{96}{17} & \frac{135}{25} & \frac{132}{27} & \frac{125}{28} & \frac{124}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{122}{50} & \frac{119}{25} & \frac{130}{23} & \frac{130}{21} & \frac{97}{16} & \frac{90}{9} & \frac{86}{9} & \frac{90}{9} & \frac{93}{15} & \frac{101}{16} & \frac{132}{25} & \frac{132}{27} & \frac{123}{28} & \frac{131}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{123}{50} & \frac{121}{26} & \frac{133}{23} & \frac{133}{21} & \frac{97}{16} & \frac{90}{10} & \frac{84}{9} & \frac{88}{9} & \frac{92}{17} & \frac{115}{21} & \frac{131}{25} & \frac{131}{27} & \frac{123}{28} & \frac{120}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{87}{50} & \frac{90}{25} & \frac{100}{23} & \frac{100}{22} & \frac{60}{16} & \frac{50}{8} & \frac{46}{8} & \frac{49}{16} & \frac{56}{25} & \frac{77}{27} & \frac{93}{27} & \frac{87}{28} & \frac{83}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{90}{50} & \frac{88}{26} & \frac{94}{23} & \frac{94}{22} & \frac{52}{16} & \frac{49}{10} & \frac{44}{9} & \frac{48}{9} & \frac{51}{17} & \frac{96}{26} & \frac{96}{26} & \frac{86}{27} & \frac{79}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{91}{50} & \frac{99}{25} & \frac{100}{24} & \frac{100}{22} & \frac{56}{16} & \frac{50}{9} & \frac{47}{8} & \frac{47}{17} & \frac{53}{25} & \frac{98}{27} & \frac{98}{27} & \frac{87}{28} & \frac{81}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{93}{50} & \frac{92}{25} & \frac{103}{23} & \frac{103}{21} & \frac{62}{17} & \frac{55}{11} & \frac{50}{9} & \frac{52}{9} & \frac{55}{16} & \frac{100}{25} & \frac{100}{27} & \frac{87}{28} & \frac{85}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{92}{50} & \frac{93}{25} & \frac{102}{24} & \frac{102}{22} & \frac{62}{17} & \frac{55}{10} & \frac{50}{8} & \frac{52}{8} & \frac{54}{14} & \frac{101}{25} & \frac{101}{27} & \frac{92}{28} & \frac{86}{50} \end{array}$$

Sta	+	π	-	Elev.
		936.90		
11				31.9
	+50			32.2
12				32.4
	+50			32.4
13				32.0
T.P.	6.01	938.00	4.91	931.99
	+50			31.8
14				31.7
	+50			31.9
	+61	Flow Line to End Culv.		
	+76	Flow Line to End Culv.		
15				31.9

Lt

x

Rt

$$\begin{array}{r} 94 \quad 97 \quad 94 \quad 58 \quad 58 \quad 50 \quad 52 \quad 57 \quad 101 \quad 101 \quad 92 \quad 85 \\ 50 \quad 27 \quad 22 \quad 17 \quad 9 \quad 9 \quad 16 \quad 25 \quad 27 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} 100 \quad 105 \quad 92 \quad 56 \quad 51 \quad 47 \quad 51 \quad 54 \quad 99 \quad 99 \quad 88 \quad 81 \\ 50 \quad 27 \quad 22 \quad 16 \quad 10 \quad - \quad 9 \quad 16 \quad 24 \quad 27 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} 95 \quad 97 \quad 90 \quad 55 \quad 49 \quad 45 \quad 48 \quad 52 \quad 97 \quad 27 \quad 18 \quad 18 \\ 50 \quad 27 \quad 22 \quad 16 \quad 11 \quad 9 \quad 16 \quad 25 \quad 27 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} 97 \quad 98 \quad 88 \quad 52 \quad 47 \quad 45 \quad 49 \quad 55 \quad 101 \quad 101 \quad 93 \quad 91 \\ 50 \quad 29 \quad 24 \quad 17 \quad 9 \quad - \quad 9 \quad 16 \quad 25 \quad 27 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} (93) \\ 99 \quad 99 \quad 105 \quad 97 \quad 92 \quad 60 \quad 54 \quad 49 \quad 53 \quad 58 \quad 107 \quad 107 \quad 99 \quad 96 \\ 50 \quad 29 \quad 26 \quad 25 \quad 22 \quad 16 \quad 11 \quad 9 \quad 16 \quad 25 \quad 27 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} 109 \quad 110 \quad 117 \quad 117 \quad 106 \quad 73 \quad 67 \quad 62 \quad 66 \quad 71 \quad 118 \quad 119 \quad 110 \quad 108 \\ 50 \quad 31 \quad 27 \quad 25 \quad 24 \quad 17 \quad 11 \quad - \quad 8 \quad 16 \quad 25 \quad 27 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} 146 \quad 110 \quad 117 \quad 117 \quad 107 \quad 76 \quad 68 \quad 63 \quad 65 \quad 70 \quad 117 \quad 117 \quad 108 \quad 104 \\ 50 \quad 29 \quad 27 \quad 25 \quad 23 \quad 17 \quad 11 \quad - \quad 9 \quad 17 \quad 26 \quad 28 \quad 29 \quad 50 \end{array}$$

$$\begin{array}{r} 108 \quad 108 \quad 118 \quad 118 \quad 103 \quad 68 \quad 65 \quad 61 \quad 65 \quad 71 \quad 114 \quad 114 \quad 106 \quad 99 \\ 50 \quad 31 \quad 27 \quad 24 \quad 20 \quad 19 \quad 9 \quad - \quad 8 \quad 17 \quad 25 \quad 27 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} 11.4 \\ 26.60 \end{array}$$

$$\begin{array}{r} 11.47 \\ 26.53 \end{array}$$

$$\begin{array}{r} 107 \quad 108 \quad 117 \quad 117 \quad 108 \quad 71 \quad 65 \quad 61 \quad 65 \quad 66 \quad 112 \quad 112 \quad 106 \quad 99 \\ 50 \quad 29 \quad 26 \quad 23 \quad 22 \quad 15 \quad 9 \quad - \quad 9 \quad 16 \quad 26 \quad 28 \quad 29 \quad 50 \end{array}$$

Sta	+	π	-	Elev	
		98800			
15	+08	E. Culv.			
15	+50			32.1	
16				32.3	
	+50			32.8	
	+80			33.0	
17				33.0	
	+50			33.0	
B.M.			363	934.37	(934.37)
	+80			32.7	
18				32.6	
	+50			32.2	
19				31.8	
T.P.	4.41	936.22	6.19	931.81	

LH

K

RH

12.43

25.57

11.2

26.38

$$\frac{10.6}{50} \frac{10.6}{28} \frac{11.9}{27} \frac{11.9}{24} \frac{10.1}{23} \frac{6.6}{13} \frac{6.8}{9} \quad \frac{5.9}{9} \frac{6.3}{7} \frac{6.9}{7} \frac{10.9}{23} \frac{10.5}{50}$$

$$\frac{10.0}{50} \frac{10.1}{28} \frac{11.9}{27} \frac{11.9}{25} \frac{10.1}{24} \frac{6.8}{16} \frac{6.1}{10} \quad \frac{6.1}{9} \quad \frac{7.0}{18} \frac{10.0}{24} \frac{9.9}{33} \frac{9.8}{50}$$

$$\frac{8.2}{50} \frac{7.9}{30} \frac{11.0}{26} \frac{11.0}{24} \frac{9.2}{23} \frac{6.3}{17} \frac{5.5}{10} \quad \frac{5.2}{9} \frac{5.6}{8} \frac{6.1}{15} \frac{7.2}{22} \frac{9.5}{24} \frac{7.5}{26} \frac{8.1}{28} \frac{7.0}{50}$$

$$\frac{3.5}{50} \frac{5.3}{31} \frac{10.8}{28} \frac{10.8}{26} \frac{9.1}{23} \frac{5.8}{16} \frac{5.3}{10} \quad \frac{5.0}{9} \frac{5.4}{16} \frac{5.4}{23} \frac{8.9}{25} \frac{5.2}{30} \frac{4.6}{50}$$

$$\frac{5.4}{50} \frac{4.8}{30} \frac{11.0}{25} \frac{11.0}{23} \frac{8.9}{23} \frac{5.7}{15} \frac{5.3}{10} \quad \frac{5.0}{8} \frac{5.2}{19} \frac{5.5}{22} \frac{7.7}{25} \frac{7.7}{29} \frac{4.9}{30} \frac{4.0}{50}$$

$$\frac{7.0}{50} \frac{6.2}{30} \frac{11.1}{25} \frac{11.1}{23} \frac{8.6}{23} \frac{5.9}{17} \frac{5.4}{10} \quad \frac{5.4}{9} \frac{5.3}{15} \frac{8.7}{22} \frac{8.7}{25} \frac{4.5}{31} \frac{5.0}{50}$$

Spk. in 2.0' Elev 28' 21' 17' 28'

$$\frac{9.2}{50} \frac{8.1}{29} \frac{11.0}{27} \frac{11.0}{25} \frac{9.8}{24} \frac{6.0}{16} \frac{5.7}{9} \quad \frac{5.2}{8} \frac{5.7}{15} \frac{5.9}{21} \frac{7.0}{24} \frac{9.6}{26} \frac{9.6}{28} \frac{8.2}{37} \frac{7.4}{50}$$

$$\frac{10.2}{50} \frac{9.2}{29} \frac{9.9}{27} \frac{11.4}{27} \frac{11.4}{25} \frac{10.2}{23} \frac{6.0}{14} \frac{5.9}{9} \quad \frac{5.9}{8} \frac{5.7}{16} \frac{9.7}{24} \frac{7.7}{26} \frac{8.9}{27} \frac{8.1}{50}$$

$$\frac{10.7}{50} \frac{10.6}{28} \frac{11.6}{27} \frac{11.6}{25} \frac{10.5}{23} \frac{6.7}{15} \frac{6.4}{12} \quad \frac{5.8}{8} \frac{6.0}{16} \frac{6.4}{24} \frac{9.8}{26} \frac{7.5}{26} \frac{8.8}{50}$$

$$\frac{10.6}{50} \frac{9.9}{28} \frac{12.0}{26} \frac{12.0}{24} \frac{10.6}{23} \frac{7.0}{15} \frac{6.6}{10} \quad \frac{6.2}{8} \frac{6.5}{16} \frac{6.8}{25} \frac{10.0}{26} \frac{7.8}{26} \frac{8.8}{50}$$

Sta.

+

x

-

Elev.

936.22

19 +50

31.5

20

31.1

+50

30.9

21

30.9

+50

31.0

+85 Flow Line at End Culv.

22

31.4

+35 Flow Line at End Culv.

+50

32.0

23

32.7

+50

33.4

14.

2.

21.

$$\begin{array}{r} 87 \quad 84 \quad 100 \quad 100 \quad 90 \quad 52 \quad 50 \quad 47 \quad 50 \quad 58 \quad 86 \quad 75 \\ 50 \quad 50 \quad 27 \quad 29 \quad 22 \quad 15 \quad 10 \quad \frac{51}{8} \quad \frac{54}{17} \quad 25 \quad 50 \end{array}$$

$$\begin{array}{r} 88 \quad 86 \quad 102 \quad 102 \quad 95 \quad 88 \quad 59 \quad 57 \quad 51 \quad 54 \quad 57 \quad 90 \quad 86 \\ 50 \quad 29 \quad 26 \quad 24 \quad 23 \quad 20 \quad 15 \quad 9 \quad \frac{51}{9} \quad \frac{54}{16} \quad 23 \quad 50 \end{array}$$

$$\begin{array}{r} 84 \quad 87 \quad 80 \quad 101 \quad 101 \quad 91 \quad 65 \quad 59 \quad 53 \quad 57 \quad 62 \quad 83 \quad 87 \quad 86 \\ 50 \quad 58 \quad 29 \quad 26 \quad 24 \quad 23 \quad 19 \quad 12 \quad \frac{53}{11} \quad \frac{57}{15} \quad 23 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 84 \quad 80 \quad 102 \quad 102 \quad 90 \quad 90 \quad 60 \quad 53 \quad 57 \quad 60 \quad 92 \quad 97 \\ 50 \quad 28 \quad 26 \quad 24 \quad 23 \quad 20 \quad 14 \quad \frac{53}{9} \quad \frac{57}{18} \quad 24 \quad 50 \end{array}$$

$$\begin{array}{r} 86 \quad 80 \quad 90 \quad 105 \quad 105 \quad 91 \quad 81 \quad 61 \quad 57 \quad 52 \quad 55 \quad 56 \quad 90 \quad 87 \quad 87 \\ 50 \quad 29 \quad 27 \quad 27 \quad 25 \quad 25 \quad 20 \quad 17 \quad 12 \quad \frac{52}{9} \quad \frac{55}{18} \quad 23 \quad 34 \quad 50 \end{array}$$

$$\begin{array}{r} 10.98 \\ 25.24 \end{array}$$

$$\begin{array}{r} 88 \quad 87 \quad 88 \quad 57 \quad 59 \quad 48 \quad 52 \quad 62 \quad 87 \quad 86 \\ 50 \quad 29 \quad 23 \quad 17 \quad 11 \quad 10 \quad 19 \quad 23 \quad 50 \end{array}$$

$$\begin{array}{r} 10.96 \\ 25.24 \end{array}$$

$$\begin{array}{r} 84 \quad 90 \quad 82 \quad 48 \quad 47 \quad 42 \quad 45 \quad 51 \quad 81 \quad 29 \\ 50 \quad 30 \quad 24 \quad 14 \quad 11 \quad \frac{42}{9} \quad \frac{45}{17} \quad 23 \quad 50 \end{array}$$

$$\begin{array}{r} 65 \quad 69 \quad 70 \quad 42 \quad 39 \quad 35 \quad 39 \quad 44 \quad 81 \quad 84 \\ 50 \quad 31 \quad 25 \quad 16 \quad 10 \quad \frac{35}{10} \quad \frac{39}{17} \quad 23 \quad 50 \end{array}$$

$$\begin{array}{r} 57 \quad 55 \quad 57 \quad 39 \quad 29 \quad 28 \quad 32 \quad 34 \quad 67 \quad 77 \\ 50 \quad 26 \quad 22 \quad 16 \quad 10 \quad \frac{28}{9} \quad \frac{32}{16} \quad 23 \quad 50 \end{array}$$

Sta.	T	T	-	Elev.
		724.22		
24				34.1'
T.P.	11.09	945.24	2.07	934.16
+50				34.8'
				35.2'
25				35.5'
+40				36.0
26				36.7
+29				37.0
+36				37.1
+60				37.2
27				37.2
+50				37.0'

44

46

48

$$\frac{53}{50} \quad \frac{43}{25} \quad \frac{32}{20} \quad \frac{23}{15} \quad \frac{22}{8} \quad \frac{21}{9} \quad \frac{24}{9} \quad \frac{24}{17} \quad \frac{51}{23} \quad \frac{55}{50}$$

$$\frac{126}{50} \quad \frac{129}{33} \quad \frac{127}{19} \quad \frac{108}{14} \quad \frac{106}{9} \quad \frac{104}{9} \quad \frac{106}{8} \quad \frac{108}{18} \quad \frac{132}{24} \quad \frac{131}{50}$$

$$\frac{141}{50} \quad \frac{141}{30} \quad \frac{132}{21} \quad \frac{104}{16} \quad \frac{102}{10} \quad \frac{100}{8} \quad \frac{103}{8} \quad \frac{101}{19} \quad \frac{116}{22} \quad \frac{108}{50}$$

$$\frac{139}{50} \quad \frac{133}{29} \quad \frac{126}{21} \quad \frac{102}{16} \quad \frac{100}{10} \quad \frac{97}{9} \quad \frac{100}{8} \quad \frac{100}{18} \quad \frac{110}{21} \quad \frac{110}{24} \quad \frac{96}{28} \quad \frac{85}{50}$$

$$\frac{122}{50} \quad \frac{103}{32} \quad \frac{101}{26} \quad \frac{109}{24} \quad \frac{108}{17} \quad \frac{96}{14} \quad \frac{95}{10} \quad \frac{92}{9} \quad \frac{95}{9} \quad \frac{94}{18} \quad \frac{102}{21} \quad \frac{95}{28} \quad \frac{61}{33} \quad \frac{92}{50}$$

$$\frac{86}{50} \quad \frac{69}{26} \quad \frac{95}{22} \quad \frac{96}{17} \quad \frac{90}{14} \quad \frac{88}{10} \quad \frac{85}{9} \quad \frac{87}{8} \quad \frac{88}{17} \quad \frac{97}{20} \quad \frac{77}{31} \quad \frac{25}{38} \quad \frac{0.9}{50}$$

$$\frac{78}{50} \quad \frac{69}{27} \quad \frac{83}{22} \quad \frac{89}{16}$$

$$\frac{82}{9} \quad \frac{83}{9} \quad \frac{85}{20} \quad \frac{75}{31} \quad \frac{33}{39} \quad \frac{19}{50}$$

$$\frac{81}{50} \quad \frac{84}{29} \quad \frac{82}{11} \quad \frac{51}{9} \quad \frac{81}{8} \quad \frac{80}{20} \quad \frac{73}{30} \quad \frac{46}{35} \quad \frac{25}{50}$$

$$\frac{80}{50} \quad \frac{81}{15}$$

$$\frac{80}{8} \quad \frac{81}{16} \quad \frac{81}{18} \quad \frac{72}{27} \quad \frac{83}{27} \quad \frac{38}{34} \quad \frac{30}{50}$$

$$\frac{108}{50} \quad \frac{102}{23} \quad \frac{85}{16} \quad \frac{85}{11} \quad \frac{80}{8} \quad \frac{82}{16} \quad \frac{85}{19} \quad \frac{98}{27} \quad \frac{94}{31} \quad \frac{62}{30} \quad \frac{51}{50}$$

$$\frac{133}{50} \quad \frac{132}{27} \quad \frac{92}{17} \quad \frac{88}{12} \quad \frac{82}{9} \quad \frac{84}{16} \quad \frac{84}{18} \quad \frac{113}{22} \quad \frac{100}{40} \quad \frac{96}{50}$$

Sta.	T	π	-	Elev.	
		745.24			
28				37.0	
B.M.	6.24	745.41	8.07	937.17	(937.17)
	+50			37.3	
29				37.5	
	+50			37.8	
30				37.9	
	+50			38.4	
31				39.0	
	+50			39.5	
32				40.0	
	+50			40.2	
33				40.6	
T.P.	5.54	745.90	3.05	940.36	

12/5/33
K.R.
L.C.
L.R.H.
M.C.G.

51

Lt.

R.

St.

$\frac{14.4}{56}$ $\frac{139}{26}$ $\frac{91}{16}$ $\frac{89}{12}$ $\frac{82}{-}$ $\frac{55}{9}$ $\frac{5.8}{16}$ $\frac{128}{24}$ $\frac{126}{30}$.

Tap. Mand. Kavarston & Kawakuli Rd.

$\frac{12.7}{50}$ $\frac{121}{25}$ $\frac{73}{16}$ $\frac{67}{10}$ $\frac{61}{-}$ $\frac{14}{9}$ $\frac{6.8}{15}$ $\frac{115}{32}$ $\frac{119}{50}$

$\frac{12.8}{50}$ $\frac{124}{25}$ $\frac{71}{15}$ $\frac{6.5}{11}$

$\frac{5.9}{-}$ $\frac{6.2}{8}$ $\frac{4.6}{16}$ $\frac{110}{23}$ $\frac{109}{50}$

$\frac{13.5}{50}$ $\frac{14.2}{41}$ $\frac{124}{39}$ $\frac{11.8}{28}$ $\frac{6.8}{18}$ $\frac{6.2}{11}$ $\frac{5.6}{-}$ $\frac{6.9}{9}$ $\frac{6.1}{15}$ $\frac{9.8}{23}$ $\frac{8.1}{50}$

$\frac{12.2}{50}$ $\frac{10.6}{26}$ $\frac{6.6}{16}$ $\frac{6.1}{10}$ $\frac{5.5}{-}$ $\frac{5.7}{8}$ $\frac{6.1}{16}$ $\frac{8.3}{20}$ $\frac{7.7}{34}$ $\frac{6.2}{40}$ $\frac{6.0}{50}$

$\frac{11.3}{50}$ $\frac{9.8}{29}$ $\frac{6.3}{20}$ $\frac{5.6}{10}$ $\frac{5.0}{-}$ $\frac{5.2}{9}$ $\frac{5.4}{14}$ $\frac{6.4}{17}$ $\frac{5.9}{34}$ $\frac{5.5}{50}$

$\frac{10.7}{50}$ $\frac{10.0}{29}$ $\frac{5.5}{19}$ $\frac{4.8}{10}$ $\frac{4.4}{-}$ $\frac{4.6}{9}$ $\frac{4.7}{15}$ $\frac{5.5}{18}$ $\frac{5.1}{42}$ $\frac{5.8}{50}$

$\frac{8.8}{50}$ $\frac{5.1}{26}$ $\frac{6.0}{24}$ $\frac{5.8}{20}$ $\frac{4.3}{18}$ $\frac{4.1}{11}$ $\frac{3.9}{-}$ $\frac{4.1}{9}$ $\frac{4.2}{16}$ $\frac{5.2}{18}$ $\frac{4.7}{32}$ $\frac{6.7}{50}$

$\frac{5.0}{50}$ $\frac{2.5}{31}$ $\frac{5.4}{27}$ $\frac{5.9}{18}$ $\frac{3.7}{14}$ $\frac{3.8}{10}$ $\frac{3.4}{-}$ $\frac{3.6}{9}$ $\frac{3.6}{15}$ $\frac{5.0}{18}$ $\frac{4.8}{32}$ $\frac{6.6}{50}$

$\frac{4.1}{50}$ $\frac{2.2}{32}$ $\frac{5.0}{28}$ $\frac{5.0}{17}$ $\frac{3.5}{14}$ $\frac{3.4}{10}$ $\frac{3.2}{-}$ $\frac{3.6}{10}$ $\frac{3.8}{16}$ $\frac{5.6}{20}$ $\frac{6.6}{50}$

$\frac{5.2}{50}$ $\frac{4.8}{38}$ $\frac{2.2}{33}$ $\frac{5.0}{27}$ $\frac{4.8}{18}$ $\frac{5.8}{15}$ $\frac{3.2}{11}$ $\frac{3.0}{-}$ $\frac{3.3}{10}$ $\frac{3.6}{16}$ $\frac{5.3}{20}$ $\frac{4.5}{35}$ $\frac{6.4}{50}$

Sta

+

A

-

Elev.

745.90

33 +21

40.5'

+60

40.6'

14

40.8'

+50

40.9'

35

40.8'

+50

40.9'

36

40.7'

+50

40.7'

+56

+2

40.9'

17

LH

4

RH

$$\frac{7.2}{50} \quad \frac{61}{39} \quad \frac{73}{25} \quad \frac{71}{18} \quad \frac{57}{13} \quad \frac{56}{10} \quad \frac{54}{10} \quad \frac{57}{10} \quad \frac{59}{14} \quad \frac{73}{18} \quad \frac{73}{35} \quad \frac{86}{50}$$

$$\frac{43}{50} \quad \frac{23}{30} \quad \frac{67}{22} \quad \frac{66}{16} \quad \frac{58}{16} \quad \frac{58}{9} \quad \frac{53}{10} \quad \frac{55}{10} \quad \frac{57}{14} \quad \frac{72}{19} \quad \frac{67}{35} \quad \frac{78}{50}$$

$$\frac{08}{50} \quad \frac{+26}{31} \quad \frac{42}{23} \quad \frac{60}{17} \quad \frac{54}{13} \quad \frac{52}{9} \quad \frac{51}{10} \quad \frac{58}{10} \quad \frac{57}{15} \quad \frac{76}{21} \quad \frac{73}{27} \quad \frac{82}{50}$$

$$\frac{+12}{50} \quad \frac{+28}{32} \quad \frac{41}{22} \quad \frac{53}{14} \quad \frac{52}{11} \quad \frac{50}{10} \quad \frac{54}{10} \quad \frac{56}{15} \quad \frac{80}{20} \quad \frac{92}{50}$$

$$\frac{+06}{50} \quad \frac{129}{33} \quad \frac{46}{23} \quad \frac{59}{16} \quad \frac{53}{11} \quad \frac{51}{10} \quad \frac{53}{16} \quad \frac{57}{16} \quad \frac{86}{23} \quad \frac{98}{50}$$

$$\frac{+20}{50} \quad \frac{413}{35} \quad \frac{57}{26} \quad \frac{64}{17} \quad \frac{51}{14} \quad \frac{50}{10} \quad \frac{50}{10} \quad \frac{54}{10} \quad \frac{58}{17} \quad \frac{94}{23} \quad \frac{102}{50}$$

$$\frac{64}{50} \quad \frac{78}{29} \quad \frac{83}{19} \quad \frac{55}{15} \quad \frac{54}{10} \quad \frac{52}{10} \quad \frac{55}{10} \quad \frac{58}{16} \quad \frac{101}{23} \quad \frac{112}{50}$$

$$\frac{71}{50} \quad \frac{83}{41} \quad \frac{80}{30} \quad \frac{84}{20} \quad \frac{59}{16} \quad \frac{55}{10} \quad \frac{52}{10} \quad \frac{55}{10} \quad \frac{57}{15} \quad \frac{99}{23} \quad \frac{110}{50}$$

1252
F.L. Calc. 33.38

1075
F.L. Calc. 35.15

$$\frac{96}{50} \quad \frac{93}{23} \quad \frac{57}{16} \quad \frac{54}{10} \quad \frac{50}{9} \quad \frac{52}{15} \quad \frac{54}{15} \quad \frac{95}{23} \quad \frac{105}{32} \quad \frac{93}{35} \quad \frac{98}{50}$$

Sta.	+	π	-	Elev.
		945.90		
37	+50			41.0
38				41.1
T.P.	6.83	946.01	4.72	941.18
	+50			41.3
39				41.8
	+50			42.2
B.M.			6.68	941.33
40				42.6
	+50			42.9
41				43.3
	+50			43.8
42				44.3
	+50			45.0

(941.34)

Lt.

A

Rt.

$$\frac{100}{30} \frac{94}{24} \frac{54}{13} \frac{52}{9} \quad \frac{49}{9} \frac{49}{9} \frac{48}{14} \frac{90}{22} \frac{101}{32} \frac{86}{34} \frac{85}{50}$$

$$\frac{96}{50} \frac{81}{34} \frac{82}{20} \frac{57}{15} \frac{52}{10} \frac{48}{9} \quad \frac{49}{9} \frac{48}{16} \frac{93}{25} \frac{93}{31} \frac{79}{33} \frac{74}{50}$$

$$\frac{96}{50} \frac{84}{26} \frac{93}{29} \frac{88}{17} \frac{70}{14} \frac{70}{10} \frac{67}{8} \frac{67}{20} \frac{74}{24} \frac{109}{28} \frac{59}{35} \frac{65}{50}$$

$$\frac{92}{50} \frac{74}{27} \frac{82}{25} \frac{81}{19} \frac{69}{15} \frac{64}{11} \frac{62}{8} \frac{62}{9} \frac{66}{19} \frac{106}{27} \frac{51}{34} \frac{65}{50}$$

$$\frac{73}{50} \frac{74}{32} \frac{83}{28} \frac{83}{20} \frac{61}{15} \frac{60}{10} \frac{58}{9} \quad \frac{58}{8} \frac{62}{20} \frac{103}{26} \frac{60}{33} \frac{65}{50}$$

Spk. in T.R. Rd 3948

$$\frac{16}{50} \frac{49}{31} \frac{74}{27} \frac{79}{21} \frac{57}{16} \frac{55}{10} \frac{54}{9} \frac{56}{9} \frac{59}{17} \frac{78}{20} \frac{80}{33} \frac{103}{36} \frac{82}{39} \frac{89}{50}$$

$$\frac{55}{50} \frac{74}{26} \frac{89}{25} \frac{89}{23} \frac{56}{16} \frac{53}{11} \frac{41}{9} \quad \frac{59}{9} \frac{58}{15} \frac{98}{23} \frac{107}{50}$$

$$\frac{79}{50} \frac{82}{45} \frac{89}{24} \frac{60}{18} \frac{49}{11} \frac{47}{9} \frac{49}{9} \frac{54}{15} \frac{96}{23} \frac{105}{50}$$

$$\frac{56}{50} \frac{69}{36} \frac{79}{28} \frac{68}{20} \frac{48}{15} \frac{44}{10} \frac{42}{9} \quad \frac{46}{9} \frac{52}{16} \frac{100}{28} \frac{106}{50}$$

$$\frac{11}{50} \frac{22}{46} \frac{50}{40} \frac{52}{29} \frac{66}{27} \frac{64}{22} \frac{40}{16} \frac{39}{10} \frac{37}{9} \frac{39}{9} \frac{46}{16} \frac{93}{24} \frac{100}{50}$$

$$\frac{439}{50} \frac{44}{93} \frac{50}{25} \frac{50}{19} \frac{33}{18} \frac{31}{10} \frac{30}{9} \quad \frac{32}{9} \frac{37}{18} \frac{81}{24} \frac{90}{50}$$

Sta.	+	X	-	Elev.
		948.01		
43				45.7'
T.P.	7.12	952.87.	2.26	945.75.
+30				46.2'
+70				46.6'
44				46.9'
+50				47.5'
45				47.7'
+50				48.0'
46				48.4'
T.P.	8.67	957.09.	4.45	948.42.
+50				49.0'
47				49.3'
+50				49.8'

Lt.

A.

Rt.

$$\frac{13.9}{50} \quad \frac{13.7}{33} \quad \frac{3.9}{24} \quad \frac{4.0}{18} \quad \frac{2.4}{14} \quad \frac{2.4}{11} \quad \frac{2.3}{9} \quad \frac{2.4}{15} \quad \frac{2.8}{21} \quad \frac{5.8}{21} \quad \frac{8.1}{50}$$

$$\frac{11}{50} \quad \frac{1.7}{35} \quad \frac{8.6}{25} \quad \frac{9.0}{19} \quad \frac{6.9}{14} \quad \frac{7.0}{10} \quad \frac{6.7}{9} \quad \frac{6.9}{14} \quad \frac{7.1}{20} \quad \frac{8.4}{33} \quad \frac{9.2}{43} \quad \frac{11.3}{50} \quad \frac{11.7}{50}$$

$$\frac{4.3}{50} \quad \frac{4.0}{39} \quad \frac{5.1}{31} \quad \frac{8.5}{26} \quad \frac{8.4}{18} \quad \frac{6.4}{13} \quad \frac{6.4}{11} \quad \frac{6.3}{15} \quad \frac{6.4}{19} \quad \frac{7.7}{27} \quad \frac{8.0}{33} \quad \frac{3.1}{33} \quad \frac{4.8}{50}$$

$$\frac{5.6}{50} \quad \frac{5.3}{28} \quad \frac{8.2}{24} \quad \frac{7.8}{18} \quad \frac{6.1}{14} \quad \frac{6.2}{11} \quad \frac{6.0}{9} \quad \frac{6.1}{7} \quad \frac{6.2}{15} \quad \frac{7.6}{19} \quad \frac{7.8}{27} \quad \frac{4.4}{32} \quad \frac{4.9}{50}$$

$$\frac{4.5}{50} \quad \frac{4.6}{29} \quad \frac{7.3}{25} \quad \frac{7.4}{17} \quad \frac{5.6}{14} \quad \frac{5.6}{11} \quad \frac{5.4}{9} \quad \frac{5.6}{14} \quad \frac{5.7}{18} \quad \frac{7.2}{18} \quad \frac{7.3}{28} \quad \frac{5.7}{31} \quad \frac{7.1}{50}$$

$$\frac{6.5}{50} \quad \frac{5.9}{27} \quad \frac{7.5}{25} \quad \frac{7.3}{18} \quad \frac{5.3}{14}$$

$$\frac{5.2}{9} \quad \frac{5.3}{13} \quad \frac{5.4}{16} \quad \frac{6.6}{16} \quad \frac{8.2}{36} \quad \frac{8.4}{50}$$

$$\frac{5.9}{50} \quad \frac{4.0}{29} \quad \frac{6.5}{25} \quad \frac{6.6}{18} \quad \frac{5.1}{15} \quad \frac{5.2}{12} \quad \frac{4.9}{6} \quad \frac{5.2}{6} \quad \frac{5.2}{13} \quad \frac{6.2}{24} \quad \frac{7.3}{24} \quad \frac{7.2}{50}$$

$$\frac{5.0}{50} \quad \frac{4.5}{29} \quad \frac{6.5}{25} \quad \frac{6.5}{19} \quad \frac{5.2}{16} \quad \frac{4.8}{13} \quad \frac{4.5}{6} \quad \frac{4.7}{12} \quad \frac{4.8}{12} \quad \frac{5.3}{27} \quad \frac{5.0}{50}$$

2.46

$$\frac{10.2}{50} \quad \frac{10.6}{28} \quad \frac{11.8}{22} \quad \frac{8.7}{16} \quad \frac{8.4}{11} \quad \frac{8.1}{6} \quad \frac{8.3}{12} \quad \frac{8.5}{16} \quad \frac{10.0}{16} \quad \frac{9.7}{33} \quad \frac{9.0}{50}$$

$$\frac{13.9}{50} \quad \frac{13.3}{25} \quad \frac{8.7}{16} \quad \frac{8.2}{11} \quad \frac{7.8}{7} \quad \frac{7.9}{15} \quad \frac{8.5}{25} \quad \frac{12.8}{25} \quad \frac{13.0}{41} \quad \frac{11.7}{50}$$

$$\frac{13.1}{50} \quad \frac{12.4}{22} \quad \frac{8.0}{14} \quad \frac{7.6}{9}$$

$$\frac{7.8}{7} \quad \frac{7.5}{16} \quad \frac{8.2}{16} \quad \frac{13.4}{26} \quad \frac{13.4}{50}$$

54

+

x

-

Elec

257.09

48

503

+50

511

49

524

T.P.

13.30

945.71

9.68

952.41

+30

534

+60

545

50

558

+38

571

51

589

+50

606

52

623

+50

640

Lt

R

Rt

$$\frac{113}{50} \quad \frac{117}{39} \quad \frac{106}{27} \quad \frac{71}{13} \quad \frac{71}{10} \quad \frac{68}{7} \quad \frac{10}{7} \quad \frac{76}{14} \quad \frac{136}{25} \quad \frac{137}{50}$$

$$\frac{91}{50} \quad \frac{95}{39} \quad \frac{105}{22} \quad \frac{69}{15} \quad \frac{62}{9} \quad \frac{60}{8} \quad \frac{61}{8} \quad \frac{64}{15} \quad \frac{126}{26} \quad \frac{133}{50}$$

$$\frac{85}{50} \quad \frac{73}{35} \quad \frac{70}{21} \quad \frac{49}{14} \quad \frac{48}{10} \quad \frac{47}{8} \quad \frac{49}{8} \quad \frac{53}{16} \quad \frac{97}{24} \quad \frac{103}{35} \quad \frac{106}{50}$$

$$\frac{132}{50} \quad \frac{126}{33} \quad \frac{136}{24} \quad \frac{126}{17} \quad \frac{126}{15} \quad \frac{125}{10} \quad \frac{123}{8} \quad \frac{128}{15} \quad \frac{125}{15} \quad \frac{130}{21} \quad \frac{134}{28} \quad \frac{144}{50}$$

$$\frac{72}{50} \quad \frac{69}{33} \quad \frac{125}{25} \quad \frac{127}{17} \quad \frac{114}{15} \quad \frac{115}{9} \quad \frac{112}{8} \quad \frac{115}{8} \quad \frac{112}{15} \quad \frac{133}{20} \quad \frac{136}{40} \quad \frac{130}{50}$$

$$\frac{14}{50} \quad \frac{18}{33} \quad \frac{28}{24} \quad \frac{110}{17} \quad \frac{100}{15} \quad \frac{103}{10} \quad \frac{97}{9} \quad \frac{102}{9} \quad \frac{102}{16} \quad \frac{123}{20} \quad \frac{125}{38} \quad \frac{106}{50}$$

$$\frac{14}{50} \quad \frac{16}{33} \quad \frac{95}{26} \quad \frac{99}{17} \quad \frac{88}{14} \quad \frac{89}{9} \quad \frac{86}{9} \quad \frac{90}{9} \quad \frac{91}{15} \quad \frac{119}{20} \quad \frac{117}{37} \quad \frac{103}{50}$$

$$\frac{79}{50} \quad \frac{20}{27} \quad \frac{57}{24} \quad \frac{85}{18} \quad \frac{71}{15} \quad \frac{71}{10} \quad \frac{68}{9} \quad \frac{71}{9} \quad \frac{70}{14} \quad \frac{88}{17} \quad \frac{92}{24} \quad \frac{87}{25} \quad \frac{92}{38} \quad \frac{99}{50}$$

$$\frac{103}{50} \quad \frac{85}{30} \quad \frac{75}{20} \quad \frac{55}{15} \quad \frac{54}{10} \quad \frac{51}{8} \quad \frac{54}{8} \quad \frac{51}{14} \quad \frac{68}{17} \quad \frac{69}{23} \quad \frac{48}{25} \quad \frac{46}{36} \quad \frac{56}{50}$$

$$\frac{64}{50} \quad \frac{63}{38} \quad \frac{53}{20} \quad \frac{38}{16} \quad \frac{37}{11} \quad \frac{24}{8} \quad \frac{37}{8} \quad \frac{38}{14} \quad \frac{52}{16} \quad \frac{53}{23} \quad \frac{40}{25} \quad \frac{44}{38} \quad \frac{51}{50}$$

$$\frac{20}{50} \quad \frac{24}{27} \quad \frac{24}{21} \quad \frac{18}{11} \quad \frac{17}{8} \quad \frac{19}{13} \quad \frac{21}{17} \quad \frac{35}{17} \quad \frac{36}{23} \quad \frac{28}{24} \quad \frac{26}{37} \quad \frac{20}{50}$$

Sta. + X - Elev.

965.71

52 +71

64.6

B.M.

1308

978.09

0.75

969.96

965.01

+93

653

?

53

65.5

+24

66.3

54

68.4

+50

69.9

55

71.4

+50

73.2

56

74.8

+50

76.4

T.P.

12.73

990.26

0.56

997.53

57

78.3

Lt.

K.

Rt.

$$\frac{20}{50}$$

$$\frac{14}{22}$$

$$\frac{11}{27}$$

$$\frac{11}{27}$$

$$\frac{67}{50}$$

Top Wind Area, 8" F"

$$\frac{23}{50} \quad \frac{12}{24}$$

$$\frac{0.9}{17}$$

$$\frac{0.5}{17}$$

$$\frac{0.3}{50}$$

$$\frac{156}{50} \quad \frac{148}{58} \quad \frac{13.5}{23} \quad \frac{128}{10} \quad \frac{196}{8} \quad \frac{127}{15} \quad \frac{128}{50}$$

$$\frac{137}{50} \quad \frac{128}{29} \quad \frac{137}{23} \quad \frac{126}{77} \quad \frac{122}{10} \quad \frac{118}{8} \quad \frac{121}{14} \quad \frac{124}{17} \quad \frac{140}{23} \quad \frac{140}{26} \quad \frac{115}{26} \quad \frac{117}{50}$$

$$\frac{143}{50} \quad \frac{134}{23} \quad \frac{106}{17} \quad \frac{101}{10} \quad \frac{97}{9} \quad \frac{100}{9} \quad \frac{102}{12} \quad \frac{121}{17} \quad \frac{117}{25} \quad \frac{114}{50}$$

$$\frac{137}{50} \quad \frac{129}{24} \quad \frac{93}{17} \quad \frac{85}{9} \quad \frac{82}{9} \quad \frac{85}{13} \quad \frac{87}{18} \quad \frac{105}{35} \quad \frac{111}{35} \quad \frac{110}{50}$$

$$\frac{116}{50} \quad \frac{114}{32} \quad \frac{80}{21} \quad \frac{67}{11} \quad \frac{67}{9} \quad \frac{70}{14} \quad \frac{73}{17} \quad \frac{94}{36} \quad \frac{98}{50} \quad \frac{97}{50}$$

$$\frac{83}{50} \quad \frac{84}{38} \quad \frac{65}{20} \quad \frac{53}{16} \quad \frac{52}{10} \quad \frac{49}{9} \quad \frac{52}{16} \quad \frac{57}{21} \quad \frac{77}{39} \quad \frac{84}{50} \quad \frac{81}{50}$$

$$\frac{59}{50} \quad \frac{41}{39} \quad \frac{52}{22} \quad \frac{37}{17} \quad \frac{36}{10} \quad \frac{33}{9} \quad \frac{36}{16} \quad \frac{39}{20} \quad \frac{49}{50} \quad \frac{55}{50}$$

$$\frac{47}{50} \quad \frac{47}{39} \quad \frac{33}{21} \quad \frac{23}{16} \quad \frac{20}{10} \quad \frac{17}{8} \quad \frac{19}{15} \quad \frac{17}{18} \quad \frac{22}{37} \quad \frac{25}{50} \quad \frac{16}{50}$$

$$\frac{155}{50} \quad \frac{135}{21} \quad \frac{123}{17} \quad \frac{123}{10} \quad \frac{120}{8} \quad \frac{122}{15} \quad \frac{123}{18} \quad \frac{133}{25} \quad \frac{133}{29} \quad \frac{115}{29} \quad \frac{101}{50}$$

Sta	+	T	-	Elev
		999.26		
57	+50			80.3
58				82.3
	+50			84.4
59				86.5
T.P.	13.25	999.54	877	786.49
	+50			886
60				90.8
	+50			92.8
61				94.5
T.P.	12.80	1007.04	833	776.21
	+50			96.2
62				97.5
	+50			98.6

LA

4

RT

$\frac{138}{50}$ $\frac{125}{35}$ $\frac{79}{30}$ $\frac{120}{27}$ $\frac{122}{19}$ $\frac{103}{15}$ $\frac{103}{10}$ $\frac{100}{9}$ $\frac{102}{14}$ $\frac{103}{18}$ $\frac{115}{25}$ $\frac{115}{32}$ $\frac{73}{50}$

$\frac{110}{50}$ $\frac{79}{35}$ $\frac{81}{31}$ $\frac{103}{28}$ $\frac{101}{19}$ $\frac{84}{15}$ $\frac{83}{10}$ $\frac{80}{9}$ $\frac{84}{13}$ $\frac{84}{15}$ $\frac{95}{25}$ $\frac{95}{32}$ $\frac{53}{50}$

$\frac{95}{50}$ $\frac{88}{37}$ $\frac{66}{32}$ $\frac{81}{28}$ $\frac{82}{18}$ $\frac{65}{15}$ $\frac{63}{10}$ $\frac{59}{8}$ $\frac{61}{13}$ $\frac{63}{15}$ $\frac{73}{24}$ $\frac{72}{32}$ $\frac{38}{50}$

$\frac{68}{50}$ $\frac{61}{37}$ $\frac{37}{32}$ $\frac{56}{28}$ $\frac{56}{18}$ $\frac{42}{15}$ $\frac{42}{10}$ $\frac{38}{9}$ $\frac{40}{15}$ $\frac{43}{18}$ $\frac{47}{24}$ $\frac{47}{32}$ $\frac{109}{50}$

$\frac{117}{50}$ $\frac{114}{43}$ $\frac{100}{32}$ $\frac{126}{28}$ $\frac{124}{18}$ $\frac{113}{15}$ $\frac{112}{9}$ $\frac{109}{8}$ $\frac{111}{15}$ $\frac{112}{18}$ $\frac{122}{24}$ $\frac{109}{32}$ $\frac{33}{50}$

$\frac{95.0}{45}$ $\frac{96.0}{35}$ $\frac{90.6}{32}$ $\frac{89.1}{25}$ $\frac{90.5}{18}$ $\frac{90.5}{15}$ $\frac{90.8}{10}$ $\frac{90.5}{9}$ $\frac{90.4}{13}$ $\frac{89.5}{15}$ $\frac{90.8}{24}$ $\frac{96.0}{32}$ $\frac{96.6}{50}$

$\frac{99.3}{50}$ $\frac{99.5}{30}$ $\frac{90.8}{22}$ $\frac{92.6}{15}$ $\frac{92.6}{9}$ $\frac{92.8}{8}$ $\frac{92.5}{7}$ $\frac{92.2}{6}$ $\frac{91.1}{5}$ $\frac{92.8}{4}$ $\frac{97.8}{3}$ $\frac{96.4}{2}$

$\frac{99.4}{50}$ $\frac{99.1}{32}$ $\frac{93.8}{22}$ $\frac{92.6}{19}$ $\frac{94.2}{15}$ $\frac{94.2}{10}$ $\frac{94.5}{8}$ $\frac{94.2}{7}$ $\frac{94.1}{6}$ $\frac{92.9}{5}$ $\frac{93.2}{4}$ $\frac{98.1}{3}$ $\frac{97.3}{2}$

$\frac{99.5}{50}$ $\frac{93}{31}$ $\frac{94.1}{21}$ $\frac{95.9}{15}$ $\frac{95.9}{10}$ $\frac{96.2}{8}$ $\frac{96.0}{7}$ $\frac{96.0}{6}$ $\frac{96.0}{5}$ $\frac{94.9}{4}$ $\frac{95.0}{3}$ $\frac{99.4}{2}$ $\frac{98.5}{1}$

$\frac{0.7}{50}$ $\frac{0.8}{32}$ $\frac{96.4}{26}$ $\frac{96.1}{18}$ $\frac{97.3}{14}$ $\frac{97.4}{10}$ $\frac{97.5}{8}$ $\frac{97.3}{7}$ $\frac{97.4}{6}$ $\frac{96.2}{5}$ $\frac{96.4}{4}$ $\frac{99.7}{3}$ $\frac{99.0}{2}$

$\frac{99.5}{50}$ $\frac{0.0}{31}$ $\frac{97.0}{26}$ $\frac{97.1}{19}$ $\frac{98.3}{15}$ $\frac{98.4}{10}$ $\frac{98.6}{8}$ $\frac{98.4}{7}$ $\frac{98.3}{6}$ $\frac{97.1}{5}$ $\frac{97.1}{4}$ $\frac{97.7}{3}$ $\frac{97.0}{2}$

Sta.	+	π	-	Elev.
		1007.01		
63				99.6
	+50		10	00.8
64				01.7
	+50			02.5
65				03.3
I.P.	7.07	1012.63 1012.73	1.95	1008.04 1005.66
	+50			04.4 4.3
66				05.5
	+50			06.6
67				07.7
B.M.	13.07	1020.20 1020.25	5.50	1007.13 1007.22
	+50			08.8
68				08.5

Sta	T	A	-	Elev
		1020.20 1020.25		
68	+50			077
69				066
T.P.	987	1026.16 1026.21	391	1016.34
	+30			057
	+65			045
70				031
	+28			01.8
	+64			00.2
71				98.8
	+50			96.6
72				94.5

Lt

A

Pt

20.2	17.9	17.1	4.8	4.5	6.9	7.4	7.6	7.2	6.7	4.8	4.8	7.0	7.5
$\frac{80}{75}$	$\frac{23}{58}$	$\frac{51}{76}$	$\frac{154}{29}$	$\frac{157}{20}$	$\frac{133}{15}$	$\frac{128}{11}$	$\frac{126}{10}$	$\frac{130}{10}$	$\frac{126}{17}$	$\frac{154}{21}$	$\frac{154}{28}$	$\frac{132}{32}$	$\frac{127}{50}$
22.3	22.0	20.4	5.5	3.7	6.1	6.2	6.5	6.2	6.0	3.8	5.7	12.8	15.3
$\frac{421}{100}$	$\frac{418}{70}$	$\frac{462}{51}$	$\frac{147}{31}$	$\frac{145}{19}$	$\frac{141}{10}$	$\frac{140}{10}$	$\frac{137}{10}$	$\frac{140}{10}$	$\frac{142}{16}$	$\frac{164}{20}$	$\frac{145}{30}$	$\frac{74}{39}$	$\frac{49}{70}$
			22.1	23.2	22.9			19.9		20.1	21.2	21.2	
			$\frac{41}{100}$	$\frac{34}{52}$				$\frac{63}{50}$		$\frac{61}{70}$	$\frac{50}{84}$	$\frac{50}{100}$	
			22.5	23.4	23.7			22.0		21.6	21.7		
			$\frac{37}{100}$	$\frac{38}{100}$	$\frac{25}{59}$			$\frac{42}{53}$		$\frac{46}{70}$	$\frac{45}{100}$		
			22.3	22.9	23.1			19.3		19.0			
			$\frac{39}{100}$	$\frac{33}{75}$	$\frac{23}{53}$			$\frac{67}{52}$		$\frac{72}{74}$	$\frac{55}{100}$		
			21.9	21.9	21.6			15.5		15.6	17.5		
			$\frac{43}{100}$	$\frac{43}{75}$	$\frac{46}{58}$			$\frac{107}{52}$		$\frac{106}{75}$	$\frac{87}{100}$		
			21.6	22.1	21.9			14.7		17.6	18.9		
			$\frac{46}{100}$	$\frac{41}{75}$	$\frac{43}{54}$			$\frac{115}{51}$		$\frac{86}{76}$	$\frac{73}{100}$		
			21.2	22.2	22.5			18.1		18.6	19.9		
			$\frac{50}{100}$	$\frac{40}{77}$	$\frac{37}{55}$			$\frac{81}{51}$		$\frac{76}{84}$	$\frac{63}{100}$		
19.6	19.2	20.1						18.0		17.6	16.9		
$\frac{66}{100}$	$\frac{70}{75}$	$\frac{61}{53}$						$\frac{82}{51}$		$\frac{86}{76}$	$\frac{93}{100}$		

Page 4

Page 61

Page 62

Sta.

+

A

-

Elev.

1026.16
1026.21

72 +50

92.4

73

90.1

T.P.

2.34

1017.21
1017.26

11.29

1014.92

+50

81.7

74

85.3

+35

83.7

+35

+67

82.2

T.P.

2.20

1007.11

12.35

1004.91

74

+35

83.7

T.P.

2.38

996.51

12.98

994.13

+67

82.2

L

L

R

$$\begin{array}{r} 17.4 \\ 8.8 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 17.0 \\ 9.2 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 17.2 \\ 9.0 \\ \hline 34 \end{array}$$

$$\begin{array}{r} 17.6 \\ 8.6 \\ \hline 51 \end{array}$$

$$\begin{array}{r} 15.3 \\ 10.9 \\ \hline 70 \end{array}$$

$$\begin{array}{r} 11.8 \\ 14.4 \\ \hline 100 \end{array}$$

Page 62

$$\begin{array}{r} 16.1 \\ 10.1 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 15.8 \\ 10.4 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 15.5 \\ 10.7 \\ \hline 57 \end{array}$$

$$\begin{array}{r} 15.3 \\ 10.9 \\ \hline 51 \end{array}$$

$$\begin{array}{r} 12.7 \\ 13.5 \\ \hline 70 \end{array}$$

$$\begin{array}{r} 8.1 \\ 18.1 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 16.4 \\ 10.8 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 16.1 \\ 11 \\ \hline 74 \end{array}$$

$$\begin{array}{r} 15.5 \\ 17 \\ \hline 51 \end{array}$$

$$\begin{array}{r} 12.4 \\ 4.8 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 9.4 \\ 7.8 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 5.5 \\ 11.7 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 11.9 \\ 5.3 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 10.0 \\ 7.2 \\ \hline 70 \end{array}$$

$$\begin{array}{r} 8.6 \\ 5.6 \\ \hline 55 \end{array}$$

$$\begin{array}{r} 5.7 \\ 11.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 2.9 \\ 14.3 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 98.7 \\ 18.5 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 8.3 \\ 8.9 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 6.8 \\ 10.4 \\ \hline 76 \end{array}$$

$$\begin{array}{r} 5.7 \\ 11.5 \\ \hline 57 \end{array}$$

$$\begin{array}{r} 4.5 \\ 12.7 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 2.6 \\ 14.6 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 1.2 \\ 16.0 \\ \hline 54 \end{array}$$

$$\begin{array}{r} 99.0 \\ 8.1 \\ \hline 44 \end{array}$$

$$\begin{array}{r} 97.2 \\ 9.9 \\ \hline 70 \end{array}$$

$$\begin{array}{r} 91.5 \\ 15.6 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 92.0 \\ 4.5 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 87.0 \\ 2.5 \\ \hline 70 \end{array}$$

$$\begin{array}{r} 81.7 \\ 14.8 \\ \hline 100 \end{array}$$

Page 62

Sta.	+	π	-	Elev.
		996.31		
75				80.5
+40				78.5
T.P.			13.70	982.81
B.M.	3.18	1010.36 1010.32		1007.18
69 +30				05.7
+65				04.5
70				03.1
+28				01.8
+64				00.2
71				98.8
T.P.	0.66	1001.16 1001.12	7.86	1000.50 1000.46

14 14 14

96.1
92.7
91.7
 $\frac{0.4}{70}$ $\frac{9.8}{53}$ $\frac{9.8}{36}$

Page 63

90.0
87.1
 $\frac{6.8}{70}$ $\frac{9.4}{50}$

Page 63

Top G.R. Post

Spk. in T.R. at

5.9 3.8 3.0 5.1 5.3 5.7 5.4 5.3 3.6 4.0 9.4
 $\frac{45}{35}$ $\frac{46}{28}$ $\frac{74}{19}$ $\frac{5.3}{15}$ $\frac{51}{10}$ $\frac{47.50}{10}$ $\frac{51}{17}$ $\frac{6.8}{21}$ $\frac{6.4}{26}$ $\frac{10}{40}$

3.9 1.8 3.7 4.2 4.5 4.3 4.0 2.3 3.4 5.0
 $\frac{6.5}{33}$ $\frac{8.4}{20}$ $\frac{4.7}{16}$ $\frac{4.2}{10}$ $\frac{5.9}{11}$ $\frac{6.1}{18}$ $\frac{6.9}{21}$ $\frac{8.1}{23}$ $\frac{7.0}{28}$ $\frac{5.4}{36}$

2.8 2.7 2.9 3.1 2.8 2.6 0.9 2.5
 $\frac{7.6}{33}$ $\frac{7.5}{20}$ $\frac{7.7}{16}$ $\frac{7.5}{10}$ $\frac{7.3}{10}$ $\frac{7.6}{16}$ $\frac{7.5}{19}$ $\frac{7.5}{32}$ $\frac{7.9}{32}$

1.6 99.9 1.3 1.6 1.8 1.5 1.2 0.0 1.9
 $\frac{8.8}{32}$ $\frac{10.5}{19}$ $\frac{7.1}{15}$ $\frac{8.8}{10}$ $\frac{8.6}{10}$ $\frac{8.9}{10}$ $\frac{9.2}{16}$ $\frac{10.4}{19}$ $\frac{8.8}{35}$

1.6 98.7 99.8 99.9 0.2 99.9 99.9 98.5 99.8
 $\frac{8.8}{33}$ $\frac{11.7}{19}$ $\frac{10.6}{16}$ $\frac{10.5}{10}$ $\frac{10.2}{10}$ $\frac{10.5}{10}$ $\frac{10.5}{16}$ $\frac{11.9}{19}$ $\frac{10.6}{33}$

1.1 97.7 98.5 98.6 98.8 98.5 98.3 97.2 99.4
 $\frac{9.8}{36}$ $\frac{12.7}{17}$ $\frac{11.9}{14}$ $\frac{11.8}{9}$ $\frac{11.6}{10}$ $\frac{11.9}{10}$ $\frac{12.1}{15}$ $\frac{13.2}{18}$ $\frac{11.0}{32}$

Sta.

+

T

-

Elev.

1001.16

1201.12

71 +50

96.6

72

94.5

+50

92.4

73

90.1

+50

T.P.

-0.03

987.54

987.50

13.59

87.7

987.57

987.53

74

85.3

+35

83.7

+67

82.2

Lt.

K

Rt.

97.7	96.0	96.7	96.6	96.6	96.4	96.4	95.0	96.0
$\frac{35}{31}$	$\frac{52}{15}$	$\frac{45}{16}$	$\frac{46}{9}$	$\frac{46}{8}$	$\frac{48}{14}$	$\frac{48}{17}$	$\frac{62}{28}$	$\frac{52}{28}$

95.7	93.4	94.2	94.3	94.5	94.2	94.0	93.3	95.8
$\frac{55}{32}$	$\frac{72}{20}$	$\frac{70}{18}$	$\frac{69}{10}$	$\frac{67}{9}$	$\frac{70}{15}$	$\frac{72}{15}$	$\frac{79}{17}$	$\frac{54}{34}$

94.3	91.5	92.0	92.4	92.4	92.1	91.9	91.3	93.9
$\frac{69}{34}$	$\frac{91}{20}$	$\frac{92}{18}$	$\frac{88}{9}$	$\frac{88}{8}$	$\frac{91}{14}$	$\frac{93}{14}$	$\frac{99}{16}$	$\frac{73}{33}$

92.3	90.0	89.9	90.1	89.8	89.5	89.1	90.7
$\frac{89}{35}$	$\frac{112}{15}$	$\frac{113}{8}$	$\frac{111}{10}$	$\frac{114}{10}$	$\frac{117}{15}$	$\frac{121}{17}$	$\frac{105}{32}$

90.5	87.6	87.7	87.7	87.3	87.0	86.5
$\frac{107}{34}$	$\frac{136}{15}$	$\frac{135}{9}$	$\frac{135}{9}$	$\frac{139}{9}$	$\frac{142}{16}$	$\frac{127}{31}$

86.8	85.1	85.2	85.3	85.0	84.7	83.7	84.8
$\frac{97}{35}$	$\frac{24}{13}$	$\frac{23}{9}$	$\frac{22}{9}$	$\frac{25}{8}$	$\frac{28}{13}$	$\frac{38}{17}$	$\frac{27}{20}$

84.2	83.5	83.6	83.7	83.2	83.0	82.0	82.6
$\frac{33}{32}$	$\frac{40}{15}$	$\frac{39}{8}$	$\frac{38}{10}$	$\frac{43}{14}$	$\frac{45}{16}$	$\frac{55}{16}$	$\frac{42}{30}$

82.8	81.2	81.9	82.1	82.2	81.8	81.5	79.0	79.4
$\frac{47}{33}$	$\frac{68}{21}$	$\frac{56}{17}$	$\frac{54}{9}$	$\frac{53}{9}$	$\frac{57}{14}$	$\frac{60}{19}$	$\frac{85}{19}$	$\frac{81}{25}$

519

+

T

-

E/cv

987.54
987.50

75

80.5

T.P.

0.14

982.96
982.92

4.72

982.82
982.78

+40

78.5

+70

77.0

76

75.6

T.P.

0.53

974.51
974.47

8.92

973.98
973.94

+50

73.2

77

71.2

+45

69.4

T.P.

3.24

967.33
967.29

10.42

964.09
964.05

78

66.9

80.2	79.7	80.4	80.6	80.5	80.2	79.9	75.2	82.0	77.2
$\frac{7.9}{24}$	$\frac{7.8}{19}$	$\frac{7.1}{16}$	$\frac{6.9}{8}$	$\frac{7.0}{9}$	$\frac{7.3}{12}$	$\frac{7.7}{24}$	$\frac{12.3}{24}$	$\frac{5.5}{32}$	$\frac{10.8}{50}$

Top. C. R. Post.

$$\frac{52}{25} \quad \frac{47}{14} \quad \frac{45}{9} \quad \frac{45}{9} \quad \frac{48}{9} \quad \frac{52}{21} \quad \frac{11.3}{31} \quad \frac{12.1}{44} \quad \frac{13.2}{50}$$
$$\frac{36}{50} \quad \frac{93}{55} \quad \frac{91}{25} \quad \frac{63}{27} \quad \frac{61}{9} \quad \frac{60}{1} \quad \frac{62}{9} \quad \frac{70}{21} \quad \frac{155}{36} \quad \frac{163}{50}$$

				75.6		75.3		74.1		65.0		63.8
11.5	15.6	27	26	24	27	89	180	19.2	50			
50	82	29	9	74	8	27	36	50				

Ten Gr. Post Lt, 77+00

$$\frac{14.4}{70} \quad \frac{13.4}{41} \quad \frac{24}{24} \quad \frac{15}{9} \quad \frac{13}{10} \quad \frac{1.7}{20} \quad \frac{2.6}{36} \quad \frac{12.5}{50} \quad \frac{136}{50}$$

					71.2	70.9	70.3	68.9	62.0
$\frac{186}{70}$	$\frac{185}{50}$	$\frac{164}{40}$	$\frac{45}{21}$	$\frac{37}{9}$	$\frac{33}{9}$	$\frac{36}{9}$	$\frac{42}{23}$	$\frac{106}{33}$	$\frac{125}{50}$

$\frac{208}{70}$	$\frac{200}{55}$	$\frac{180}{45}$	$\frac{59}{20}$	$\frac{53}{9}$	$\frac{51}{9}$	$\frac{54}{22}$	$\frac{60}{22}$	$\frac{122}{31}$	$\frac{166}{50}$
------------------	------------------	------------------	-----------------	----------------	----------------	-----------------	-----------------	------------------	------------------

$$\frac{35}{50} \quad \frac{49}{33} \quad \frac{0.7}{25} \quad \frac{05}{9} \quad \frac{94}{-} \quad \frac{08}{9} \quad \frac{1.7}{21} \quad \frac{184}{47} \quad \frac{21.3}{70}$$

Sta. + T - Elev.

96733
967.29

78 +28

65.7

+60

64.4

79

62.8

+18 E Victoria St.

62.1

+38

61.2

B.M. 2.70 963.76 6.40

910.93
960.89

961.06

+38

61.2

+12

60.2

80

59.5

12/9/37
K.R.
L.B.H.
L.G.
M.D.G.

64

4.

4.

12.

$\frac{3.7}{50}$ $\frac{7.9}{34}$ $\frac{2.1}{22}$ $\frac{1.8}{9}$ $\frac{1.6}{10}$ $\frac{2.0}{10}$ $\frac{2.9}{21}$ $\frac{2.1.9}{49}$ $\frac{24.5}{70}$

$\frac{10.9}{50}$ $\frac{13.1}{38}$ $\frac{4.1}{21}$ $\frac{3.2}{9}$ $\frac{2.9}{10}$ $\frac{3.3}{10}$ $\frac{3.6}{20}$ $\frac{2.1.9}{53}$ $\frac{22.9}{70}$

$\frac{4.2}{70}$ $\frac{20.3}{42}$ $\frac{5.6}{18}$ $\frac{4.5}{9}$

$\frac{4.5}{10}$ $\frac{4.8}{10}$ $\frac{5.0}{50}$

$\frac{5.2}{50}$ $\frac{5.1}{50}$ $\frac{4.8}{100}$

$\frac{6.6}{10}$ $\frac{6.0}{9}$ $\frac{6.1}{12}$ $\frac{6.1}{50}$ $\frac{6.2}{50}$

Spk. 12 G.R. M.L.H. 79-45

40.8

$\frac{28.5}{70}$ $\frac{28.8}{58}$ $\frac{23.0}{70}$

$\frac{28.4}{90}$ $\frac{28.8}{70}$ $\frac{26.7}{50}$ $\frac{4.5}{18}$ $\frac{3.6}{9}$ $\frac{3.6}{11}$ $\frac{3.8}{27}$ $\frac{3.8}{50}$ $\frac{16.8}{70}$

$\frac{29.8}{100}$ $\frac{29.3}{70}$ $\frac{29.3}{52}$ $\frac{4.9}{17}$ $\frac{4.5}{8}$ $\frac{4.3}{11}$ $\frac{4.6}{11}$ $\frac{5.1}{63}$ $\frac{18.3}{14}$ $\frac{18.4}{70}$

Sta.	+	π	-	Elev.
		963.76		
80	+50			58.6
81				58.6
	+50			59.2
82				59.7
T.P.	5.11	967.69	1.23	962.53
	+50			60.2
83				60.8
	+50			61.5
84				61.8
	+50			62.0
85				61.8

lt

q.

rt.

(Fly Water)

$$\frac{330}{100} \quad \frac{338}{70} \quad \frac{278}{50} \quad \frac{52}{17} \quad \frac{55}{8} \quad \frac{52}{-} \quad \frac{53}{10} \quad \frac{59}{23} \quad \frac{178}{41} \quad \frac{194}{50} \quad \frac{185}{70}$$

$$\frac{321}{100} \quad \frac{291}{49} \quad \frac{58}{15} \quad \frac{55}{8} \quad \frac{52}{-} \quad \frac{54}{10} \quad \frac{59}{22} \quad \frac{150}{36} \quad \frac{154}{43} \quad \frac{143}{50}$$

$$\frac{339}{100} \quad \frac{288}{50} \quad \frac{50}{15} \quad \frac{50}{8} \quad \frac{46}{-} \quad \frac{49}{11} \quad \frac{59}{23} \quad \frac{88}{31} \quad \frac{81}{32} \quad \frac{77}{41} \quad \frac{59}{50}$$

$$\frac{184}{50} \quad \frac{141}{33} \quad \frac{46}{17} \quad \frac{43}{7} \quad \frac{41}{-} \quad \frac{42}{11} \quad \frac{46}{21} \quad \frac{56}{24} \quad \frac{50}{30} \quad \frac{12}{39} \quad \frac{04}{50}$$

$$\frac{125}{50} \quad \frac{100}{37} \quad \frac{89}{29} \quad \frac{100}{26} \quad \frac{96}{22} \quad \frac{81}{19} \quad \frac{77}{7} \quad \frac{74}{-} \quad \frac{75}{10} \quad \frac{77}{20} \quad \frac{81}{22} \quad \frac{66}{28} \quad \frac{14}{35} \quad \frac{16}{50}$$

$$\frac{48}{50} \quad \frac{56}{30} \quad \frac{83}{26} \quad \frac{89}{20} \quad \frac{72}{18} \quad \frac{70}{8} \quad \frac{68}{-} \quad \frac{70}{10} \quad \frac{70}{16} \quad \frac{73}{21} \quad \frac{63}{28} \quad \frac{61}{34} \quad \frac{05}{50}$$

$$\frac{34}{50} \quad \frac{47}{35} \quad \frac{49}{30} \quad \frac{78}{26} \quad \frac{77}{21} \quad \frac{65}{18} \quad \frac{63}{9} \quad \frac{61}{-} \quad \frac{63}{10} \quad \frac{68}{18} \quad \frac{74}{21} \quad \frac{61}{28} \quad \frac{22}{34} \quad \frac{27}{38} \quad \frac{20}{50}$$

$$\frac{34}{50} \quad \frac{46}{33} \quad \frac{54}{26} \quad \frac{68}{25} \quad \frac{70}{22} \quad \frac{58}{18} \quad \frac{58}{9} \quad \frac{58}{-} \quad \frac{58}{9} \quad \frac{58}{19} \quad \frac{79}{24} \quad \frac{79}{26} \quad \frac{48}{30} \quad \frac{30}{50}$$

$$\frac{49}{50} \quad \frac{54}{40} \quad \frac{62}{28} \quad \frac{69}{20} \quad \frac{59}{17} \quad \frac{58}{9} \quad \frac{56}{-} \quad \frac{58}{10} \quad \frac{62}{19} \quad \frac{81}{23} \quad \frac{70}{25} \quad \frac{59}{28} \quad \frac{58}{35} \quad \frac{43}{50}$$

$$\frac{44}{50} \quad \frac{47}{40} \quad \frac{56}{29} \quad \frac{64}{26} \quad \frac{67}{21} \quad \frac{61}{18} \quad \frac{60}{9} \quad \frac{58}{-} \quad \frac{60}{10} \quad \frac{63}{19} \quad \frac{82}{22} \quad \frac{72}{24} \quad \frac{73}{25} \quad \frac{59}{50}$$

Sta.	+	π	-	Elev.
		967.64		
P5	+50			62.0
	+85			62.2
P6	+05			62.2
T.P.	3.31	967.14	3.81	963.83
	+50			62.2
57				62.2
	+50			62.4
88				62.6
	+50			62.5
89				62.2
	+50			61.9
90				61.5

Lt.

L.

Rt.

$$\begin{array}{cccccccccccccccc} \frac{51}{50} & \frac{40}{35} & \frac{42}{37} & \frac{66}{24} & \frac{67}{19} & \frac{58}{16} & \frac{58}{10} & \frac{56}{10} & \frac{58}{10} & \frac{62}{16} & \frac{78}{19} & \frac{77}{27} & \frac{81}{38} & \frac{75}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{64}{50} & \frac{57}{28} & \frac{65}{21} & \frac{65}{20} & \frac{59}{17} & \frac{56}{9} & \frac{54}{10} & \frac{57}{10} & \frac{60}{16} & \frac{72}{19} & \frac{81}{32} & \frac{76}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{71}{50} & \frac{57}{35} & \frac{62}{24} & \frac{61}{19} & \frac{57}{15} & \frac{55}{9} & \frac{54}{10} & \frac{57}{10} & \frac{58}{16} & \frac{66}{18} & \frac{65}{21} & \frac{52}{29} & \frac{60}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{73}{50} & \frac{61}{36} & \frac{61}{21} & \frac{54}{15} & \frac{54}{10} & \frac{47}{9} & \frac{51}{22} & \frac{50}{24} & \frac{41}{32} & \frac{23}{32} & \frac{34}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{75}{50} & \frac{66}{24} & \frac{53}{16} & & \frac{52}{10} & & \frac{49}{9} & \frac{50}{20} & \frac{52}{23} & \frac{57}{25} & \frac{48}{33} & \frac{38}{50} & \frac{34}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{62}{50} & \frac{56}{30} & \frac{56}{19} & \frac{48}{16} & \frac{48}{11} & \frac{47}{11} & & & \frac{52}{18} & \frac{58}{21} & \frac{46}{25} & \frac{36}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{57}{50} & \frac{48}{34} & \frac{52}{22} & \frac{54}{20} & \frac{49}{12} & & \frac{45}{10} & \frac{46}{19} & \frac{48}{22} & \frac{58}{29} & \frac{58}{26} & \frac{39}{26} & \frac{28}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{80}{50} & \frac{65}{26} & \frac{51}{17} & \frac{50}{11} & \frac{46}{11} & \frac{48}{8} & \frac{53}{19} & \frac{63}{21} & \frac{60}{23} & \frac{46}{24} & \frac{41}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{84}{50} & \frac{61}{23} & \frac{52}{16} & \frac{51}{10} & & & \frac{47}{9} & \frac{53}{17} & \frac{58}{20} & \frac{75}{20} & \frac{79}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{75}{50} & \frac{67}{42} & \frac{64}{27} & \frac{58}{18} & \frac{55}{12} & & \frac{52}{9} & \frac{56}{16} & \frac{61}{22} & \frac{94}{31} & \frac{94}{33} & \frac{103}{50} & \frac{104}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{72}{50} & \frac{77}{33} & \frac{76}{21} & \frac{63}{17} & \frac{59}{10} & & \frac{56}{9} & \frac{59}{16} & \frac{65}{22} & \frac{92}{45} & \frac{95}{45} & \frac{103}{50} \end{array}$$

Sta.	t	T	-	E/cv.
		967.14		
90	+50			61.5-
91				61.4
	+50			61.4
92				61.2
T.P.	5.23	966.90	5.97	961.17
	+50			61.2
B.M.			5.63	960.57
93				61.3
	+50			61.2
94				61.3
	+50			61.3
T.P.	12.89	974.01	5.23	961.17
95				61.2
	+50			60.8

Lt.

L.

Rt.

$$\frac{81}{50} \quad \frac{87}{36} \quad \frac{84}{23} \quad \frac{65}{18} \quad \frac{60}{10} \quad \frac{56}{10} \quad \frac{59}{17} \quad \frac{59}{23} \quad \frac{93}{50} \quad \frac{94}{50}$$

$$\frac{94}{50} \quad \frac{96}{38} \quad \frac{92}{25} \quad \frac{63}{18} \quad \frac{59}{10} \quad \frac{57}{9} \quad \frac{59}{18} \quad \frac{59}{24} \quad \frac{87}{26} \quad \frac{91}{27} \quad \frac{97}{28} \quad \frac{97}{28} \quad \frac{91}{28} \quad \frac{88}{50}$$

$$\frac{111}{50} \quad \frac{111}{41} \quad \frac{107}{26} \quad \frac{67}{17} \quad \frac{61}{11} \quad \frac{57}{9} \quad \frac{59}{18} \quad \frac{61}{25} \quad \frac{104}{26} \quad \frac{109}{27} \quad \frac{92}{27} \quad \frac{85}{50}$$

$$\frac{113}{50} \quad \frac{110}{29} \quad \frac{73}{17} \quad \frac{62}{10} \quad \frac{59}{10} \quad \frac{62}{18} \quad \frac{63}{18} \quad \frac{91}{23} \quad \frac{84}{50}$$

$$\frac{93}{50} \quad \frac{93}{36} \quad \frac{92}{25} \quad \frac{59}{17} \quad \frac{55}{11} \quad \frac{52}{8} \quad \frac{53}{18} \quad \frac{59}{22} \quad \frac{77}{28} \quad \frac{74}{38} \quad \frac{69}{50}$$

Spk. 10 T.P. 92.877

$$\frac{117}{50} \quad \frac{102}{23} \quad \frac{59}{15} \quad \frac{55}{10} \quad \frac{51}{9} \quad \frac{53}{19} \quad \frac{59}{22} \quad \frac{70}{24} \quad \frac{69}{41} \quad \frac{66}{50}$$

$$\frac{111}{50} \quad \frac{98}{22} \quad \frac{59}{16} \quad \frac{59}{9} \quad \frac{52}{8} \quad \frac{53}{20} \quad \frac{57}{22} \quad \frac{63}{22} \quad \frac{61}{29} \quad \frac{55}{50}$$

$$\frac{100}{50} \quad \frac{90}{39} \quad \frac{82}{23} \quad \frac{60}{18} \quad \frac{5.5}{11} \quad \frac{51}{8} \quad \frac{5.2}{19} \quad \frac{50}{20} \quad \frac{57}{24} \quad \frac{56}{26} \quad \frac{50}{26} \quad \frac{43}{50}$$

$$\frac{75}{50} \quad \frac{70}{36} \quad \frac{64}{28} \quad \frac{70}{26} \quad \frac{69}{27} \quad \frac{58}{19} \quad \frac{54}{11} \quad \frac{51}{7} \quad \frac{51}{14} \quad \frac{52}{16} \quad \frac{57}{23} \quad \frac{59}{27} \quad \frac{29}{27} \quad \frac{18}{50}$$

$$\frac{129}{50} \quad \frac{117}{42} \quad \frac{113}{29} \quad \frac{128}{26} \quad \frac{139}{23} \quad \frac{129}{27} \quad \frac{130}{11} \quad \frac{128}{7} \quad \frac{128}{17} \quad \frac{127}{17} \quad \frac{110}{24} \quad \frac{62}{26} \quad \frac{50}{50}$$

$$\frac{96}{50} \quad \frac{85}{35} \quad \frac{142}{27} \quad \frac{142}{23} \quad \frac{136}{18} \quad \frac{135}{15} \quad \frac{132}{9} \quad \frac{131}{13} \quad \frac{120}{13} \quad \frac{108}{25} \quad \frac{47}{33} \quad \frac{103}{39} \quad \frac{106}{50}$$

Sta. + A - Elev.

97401

96

60.3

+60

59.2

T.P.

1.52

961.84

1369

960.32

97

58.4

+40

57.5

+75

56.8

98

56.2

+50

55.2

99

54.4

+50

53.6

100

53.0

T.P.

3.15

956.20

8.79

953.05

+50

52.8

Lt.

A

Rt.

$$\begin{array}{r} 94 \\ 50 \end{array} \frac{90}{36} \frac{152}{28} \frac{152}{22} \frac{140}{18} \frac{139}{13} \frac{127}{8} \frac{127}{8} \frac{135}{13} \frac{107}{24} \frac{47}{34} \frac{23}{34} \frac{22}{50}$$

$$\begin{array}{r} 100 \\ 50 \end{array} \frac{99}{43} \frac{106}{34} \frac{163}{29} \frac{163}{24} \frac{153}{20} \frac{152}{14} \frac{148}{8} \frac{148}{15} \frac{148}{24} \frac{130}{31} \frac{79}{32} \frac{49}{50}$$

$$\begin{array}{r} 0.2 \\ 50 \end{array} \frac{0.0}{40} \frac{33}{33} \frac{54}{29} \frac{52}{25} \frac{40}{22} \frac{38}{13} \frac{34}{9} \frac{36}{14} \frac{34}{18} \frac{29}{22} \frac{29}{30} \frac{137}{50}$$

$$\begin{array}{r} 56 \\ 50 \end{array} \frac{53}{32} \frac{66}{30} \frac{64}{25} \frac{49}{21} \frac{45}{12} \frac{43}{8} \frac{46}{8} \frac{42}{15} \frac{58}{17} \frac{49}{22} \frac{0.0}{29} \frac{0.5}{34} \frac{0.5}{50}$$

$$\begin{array}{r} 11.2 \\ 50 \end{array} \frac{108}{43} \frac{87}{33} \frac{81}{29} \frac{59}{21} \frac{56}{14} \frac{50}{8} \frac{53}{15} \frac{52}{22} \frac{60}{29} \frac{53}{30} \frac{45}{50}$$

$$\begin{array}{r} 11.7 \\ 50 \end{array} \frac{113}{46} \frac{91}{24} \frac{67}{21} \frac{60}{11} \frac{56}{7} \frac{58}{7} \frac{61}{20} \frac{72}{23} \frac{73}{27} \frac{64}{30} \frac{6.0}{50}$$

$$\begin{array}{r} 11.3 \\ 50 \end{array} \frac{103}{25} \frac{75}{21} \frac{69}{11} \frac{66}{7} \frac{68}{17} \frac{81}{24} \frac{77}{31} \frac{71}{50}$$

$$\begin{array}{r} 12.9 \\ 50 \end{array} \frac{113}{26} \frac{85}{21} \frac{77}{12}$$

$$\begin{array}{r} 74 \\ 7 \end{array} \frac{75}{18} \frac{75}{24} \frac{89}{34} \frac{89}{50} \frac{8.2}{50}$$

$$\begin{array}{r} 140 \\ 50 \end{array} \frac{115}{26} \frac{91}{21} \frac{84}{11} \frac{82}{9} \frac{83}{18} \frac{87}{22} \frac{102}{27} \frac{90}{50} \frac{84}{50}$$

$$\begin{array}{r} 146 \\ 50 \end{array} \frac{125}{36} \frac{95}{22}$$

$$\frac{91}{12}$$

$$\begin{array}{r} 88 \\ 7 \end{array} \frac{90}{18} \frac{93}{34} \frac{83}{50} \frac{77}{50}$$

$$\begin{array}{r} 98 \\ 50 \end{array} \frac{91}{42} \frac{78}{29} \frac{42}{20} \frac{37}{12} \frac{34}{6} \frac{36}{14} \frac{37}{17} \frac{41}{24} \frac{39}{28} \frac{20}{50} \frac{11}{50}$$

Sta	+	π	-	Elev.
		954.20		
101				52.5'
	+50			52.3'
102				52.0'
	+50			51.7'
103				51.4'
	+50			51.3'
	+99			51.2'
104	+04			51.2'
	+50			51.0'
105				51.0'
	+32			51.3'

Lt.

L.

Rt.

$$\begin{array}{r} 99 \ 84 \ 72 \ 43 \ 40 \\ 50 \ 25 \ 25 \ 17 \ 11 \end{array}$$

$$\begin{array}{r} 37 \ 38 \ 40 \ 44 \ 41 \ 14 \ 07 \ +03 \\ 8 \ 16 \ 19 \ 25 \ 29 \ 41 \ 50 \end{array}$$

$$\begin{array}{r} 96 \ 77 \ 47 \ 43 \ 39 \ 40 \ 41 \ 48 \ 46 \ 20 \ 12 \ +10 \\ 50 \ 27 \ 19 \ 12 \ 6 \ 15 \ 17 \ 24 \ 28 \ 39 \ 50 \end{array}$$

$$\begin{array}{r} 88 \ 72 \ 66 \ 49 \ 45 \\ 50 \ 33 \ 24 \ 18 \ 12 \end{array}$$

$$\begin{array}{r} 42 \ 44 \ 45 \ 48 \ 44 \ 24 \ 08 \\ 9 \ 16 \ 18 \ 25 \ 29 \ 50 \end{array}$$

$$\begin{array}{r} 72 \ 87 \ 80 \ 50 \ 48 \ 45 \ 48 \ 48 \ 54 \ 52 \ 28 \ 19 \ 05 \\ 50 \ 38 \ 26 \ 17 \ 12 \ 9 \ 15 \ 18 \ 25 \ 29 \ 41 \ 50 \end{array}$$

$$\begin{array}{r} 80 \ 79 \ 73 \ 53 \ 52 \\ 50 \ 32 \ 23 \ 16 \ 12 \end{array}$$

$$\begin{array}{r} 48 \ 49 \ 50 \ 55 \ 48 \ 27 \ 29 \ 04 \\ 8 \ 16 \ 19 \ 26 \ 30 \ 41 \ 50 \end{array}$$

$$\begin{array}{r} 55 \ 57 \ 72 \ 70 \ 55 \ 52 \ 49 \ 50 \ 51 \ 49 \ 25 \ +04 \\ 50 \ 29 \ 25 \ 23 \ 18 \ 12 \ 8 \ 15 \ 26 \ 29 \ 50 \end{array}$$

$$\begin{array}{r} 58 \ 58 \ 70 \ 68 \ 55 \ 52 \ 50 \ 51 \ 52 \ 09 \ 00 \\ 50 \ 28 \ 25 \ 22 \ 16 \ 12 \ 9 \ 24 \ 32 \ 50 \end{array}$$

$$\begin{array}{r} 61 \ 58 \ 71 \ 69 \ 58 \ 53 \ 50 \ 52 \ 40 \\ 50 \ 29 \ 24 \ 27 \ 19 \ 11 \ 10 \ 50 \end{array}$$

$$\begin{array}{r} 65 \ 62 \ 73 \ 71 \ 57 \ 54 \ 52 \ 52 \ 49 \ 29 \\ 50 \ 30 \ 25 \ 21 \ 18 \ 10 \ 10 \ 25 \ 50 \end{array}$$

$$\begin{array}{r} 75 \ 71 \ 74 \ 74 \ 56 \ 55 \ 52 \ 53 \ 53 \ 39 \\ 50 \ 26 \ 24 \ 23 \ 18 \ 14 \ 11 \ 20 \ 50 \end{array}$$

$$\begin{array}{r} 76 \ 70 \ 57 \ 59 \ 49 \ 49 \ 55 \ 50 \\ 50 \ 38 \ 29 \ 17 \ 10 \ 28 \ 30 \end{array}$$

Sta	+	π	-	Elev.
		956.20		
105	+39			574.
18.92	= R.T.H. #96			513.
B.M.	3.05	959.37.	4.90	951.30. (951.34)
	+75			509.
	+82			50.9.
				50.6.
106				49.6.
	+50			48.7.
107				473.
	+50			45.7.
108				44.2.
T.R	0.70	947.07.	8.02	946.37.
	+50			42.0.
109				

1/4/35
Rain

70

Lt

R

Rt

$\frac{72}{50} \frac{61}{26}$

$\frac{48}{23} \frac{49}{23} \frac{51}{50}$

$\frac{63}{50}$

$\frac{49}{50}$

$\frac{49}{50}$

Top Mont Lexington T.H. #96

$\frac{54}{50} \frac{38}{15} \frac{35}{50} \frac{35}{13} \frac{38}{30} \frac{33}{50}$

$\frac{48}{50} \frac{35}{31} \frac{48}{25} \frac{40}{15} \frac{35}{12} \frac{37}{25} \frac{41}{33} \frac{21}{50} \frac{24}{50}$

$\frac{43}{50} \frac{35}{38} \frac{29}{29} \frac{49}{24} \frac{49}{20} \frac{46}{14} \frac{38}{10} \frac{40}{22} \frac{46}{26} \frac{48}{31} \frac{18}{47} \frac{14}{50} \frac{19}{50}$

$\frac{36}{50} \frac{25}{37} \frac{18}{29} \frac{55}{22} \frac{55}{17} \frac{53}{11} \frac{48}{11} \frac{50}{25} \frac{52}{30} \frac{26}{50} \frac{23}{50}$

$\frac{69}{50} \frac{46}{35} \frac{41}{26} \frac{66}{22} \frac{64}{17} \frac{61}{11} \frac{57}{13} \frac{60}{25} \frac{70}{29} \frac{41}{50} \frac{45}{50}$

$\frac{75}{50} \frac{62}{34} \frac{57}{25} \frac{80}{21} \frac{77}{15} \frac{75}{9} \frac{71}{14} \frac{75}{17} \frac{77}{20} \frac{85}{25} \frac{85}{30} \frac{60}{50} \frac{68}{50}$

$\frac{91}{50} \frac{83}{33} \frac{18}{26} \frac{78}{23} \frac{97}{20} \frac{84}{17} \frac{91}{11} \frac{87}{17} \frac{93}{17} \frac{100}{25} \frac{103}{29} \frac{74}{50} \frac{70}{50}$

$\frac{27}{50} \frac{33}{25} \frac{44}{22} \frac{43}{19} \frac{35}{15} \frac{34}{11} \frac{29}{11} \frac{32}{16} \frac{35}{19} \frac{47}{24} \frac{48}{25} \frac{37}{50} \frac{54}{50}$

$\frac{60}{50} \frac{63}{33} \frac{65}{23} \frac{72}{22} \frac{72}{21} \frac{57}{16} \frac{55}{10} \frac{51}{11} \frac{54}{18} \frac{59}{22} \frac{73}{22} \frac{83}{56} \frac{77}{50}$

Sta	+	π	-	Elev
		947.07		
109	+50			40.1
110				38.4
	+50			36.4
111				34.4
T.P.	1.05	955.42	12.70	954.57
	+50			32.3
	+80			31.2
112				30.6
	+28			29.6
	+95			29.0
113				26.8
	+50			24.8

Lt

L

Rt

$$\frac{110}{50} \quad \frac{106}{36} \quad \frac{99}{22} \quad \frac{75}{14} \quad \frac{73}{8} \quad \frac{70}{12} \quad \frac{73}{17} \quad \frac{75}{23} \quad \frac{100}{34} \quad \frac{103}{50}$$

$$\frac{111}{50} \quad \frac{111}{33} \quad \frac{107}{21} \quad \frac{92}{17} \quad \frac{88}{9} \quad \frac{87}{12} \quad \frac{87}{20} \quad \frac{92}{22} \quad \frac{102}{35} \quad \frac{102}{50}$$

$$\frac{115}{50} \quad \frac{117}{29} \quad \frac{122}{23} \quad \frac{106}{16} \quad \frac{103}{8} \quad \frac{107}{11} \quad \frac{108}{23} \quad \frac{110}{30} \quad \frac{87}{50} \quad \frac{88}{50}$$

$$\frac{99}{50} \quad \frac{113}{29} \quad \frac{141}{23} \quad \frac{139}{19} \quad \frac{152}{14} \quad \frac{131}{9} \quad \frac{127}{10} \quad \frac{129}{18} \quad \frac{133}{22} \quad \frac{131}{27} \quad \frac{100}{50} \quad \frac{96}{50}$$

$$\frac{121}{50} \quad \frac{116}{29} \quad \frac{42}{21} \quad \frac{38}{17} \quad \frac{35}{9} \quad \frac{31}{11} \quad \frac{34}{16} \quad \frac{36}{18} \quad \frac{42}{22} \quad \frac{40}{28} \quad \frac{18}{50} \quad \frac{06}{50}$$

$$\frac{128}{50} \quad \frac{127}{31} \quad \frac{119}{20} \quad \frac{47}{16} \quad \frac{45}{9} \quad \frac{42}{11} \quad \frac{44}{16} \quad \frac{47}{18} \quad \frac{58}{24} \quad \frac{57}{26} \quad \frac{53}{32} \quad \frac{54}{50} \quad \frac{68}{50}$$

$$\frac{11}{50} \quad \frac{18}{28} \quad \frac{53}{21} \quad \frac{53}{10} \quad \frac{48}{16} \quad \frac{58}{18} \quad \frac{66}{23} \quad \frac{64}{26} \quad \frac{59}{30} \quad \frac{58}{35} \quad \frac{70}{45} \quad \frac{74}{50} \quad \frac{80}{50}$$

$$\frac{25}{50} \quad \frac{28}{40} \quad \frac{29}{31} \quad \frac{63}{24} \quad \frac{61}{9} \quad \frac{58}{11} \quad \frac{62}{16} \quad \frac{66}{18} \quad \frac{74}{23} \quad \frac{77}{27} \quad \frac{64}{33} \quad \frac{63}{41} \quad \frac{76}{50} \quad \frac{82}{50}$$

$$\frac{134}{50} \quad \frac{140}{36} \quad \frac{70}{22} \quad \frac{68}{9}$$

$$\frac{64}{10} \quad \frac{68}{16} \quad \frac{73}{10} \quad \frac{83}{18} \quad \frac{78}{24} \quad \frac{68}{27} \quad \frac{65}{37} \quad \frac{82}{50}$$

$$\frac{126}{50} \quad \frac{127}{36} \quad \frac{84}{22} \quad \frac{94}{18} \quad \frac{91}{10} \quad \frac{86}{12} \quad \frac{71}{16} \quad \frac{94}{18} \quad \frac{102}{24} \quad \frac{99}{28} \quad \frac{67}{42} \quad \frac{94}{50} \quad \frac{102}{50}$$

$$\frac{115}{50} \quad \frac{119}{34} \quad \frac{100}{23} \quad \frac{117}{18} \quad \frac{117}{17} \quad \frac{110}{16} \quad \frac{110}{8} \quad \frac{106}{10} \quad \frac{110}{10} \quad \frac{115}{16} \quad \frac{124}{19} \quad \frac{124}{24} \quad \frac{111}{28} \quad \frac{115}{50}$$

Sta.	f	T	-	Elev.
		935.42		
114				22.4
T.P.	0.06	923.60	1188	925.54
+50				20.4
115				18.2
+25				17.1
+75				15.2
T.P.	0.53	913.99	1014	913.46
116				14.2
+50				12.0
117				09.9
+50				07.9
118				06.0
+75				03.1
T.P.	1.69	904.65	1103	902.96

Lt.

L.

Rt.

$$\begin{array}{r} 15 \\ 50 \end{array} \frac{40}{35} \quad \begin{array}{r} 130 \\ 22 \end{array} \frac{141}{19} \frac{141}{18} \quad \begin{array}{r} 136 \\ 17 \end{array} \frac{134}{8} \quad \begin{array}{r} 130 \\ 11 \end{array} \frac{133}{17} \frac{138}{24} \quad \begin{array}{r} 168 \\ 24 \end{array} \frac{173}{25} \quad \begin{array}{r} 178 \\ 50 \end{array}$$

$$\begin{array}{r} +28 \\ 50 \end{array} \quad \begin{array}{r} +28 \\ 30 \end{array} \frac{47}{20} \frac{43}{18} \quad \begin{array}{r} 37 \\ 15 \end{array} \frac{35}{9} \quad \begin{array}{r} 32 \\ 15 \end{array} \frac{39}{22} \frac{76}{33} \frac{81}{50}$$

$$\begin{array}{r} 20 \\ 50 \end{array} \quad \begin{array}{r} 33 \\ 35 \end{array} \frac{73}{27} \frac{71}{22} \quad \begin{array}{r} 59 \\ 19 \end{array} \frac{58}{10} \quad \begin{array}{r} 54 \\ 10 \end{array} \quad \begin{array}{r} 62 \\ 15 \end{array} \frac{114}{27} \frac{123}{33} \frac{127}{50}$$

$$\begin{array}{r} 46 \\ 50 \end{array} \frac{57}{35} \frac{78}{27} \frac{80}{21} \frac{71}{19} \quad \begin{array}{r} 68 \\ 10 \end{array} \quad \begin{array}{r} 65 \\ 15 \end{array} \frac{72}{25} \frac{138}{33} \frac{149}{50} \frac{161}{50}$$

$$\begin{array}{r} 21 \\ 50 \end{array} \frac{34}{37} \frac{110}{26} \frac{110}{23} \quad \begin{array}{r} 93 \\ 18 \end{array} \frac{89}{10} \quad \begin{array}{r} 84 \\ 15 \end{array} \frac{92}{24} \frac{178}{30} \frac{225}{50}$$

$$s.s. \quad \begin{array}{r} +70 \\ 50 \end{array} \quad \begin{array}{r} +55 \\ 36 \end{array} \frac{26}{27} \frac{24}{22} \frac{06}{18} \frac{04}{9} \quad \begin{array}{r} +02 \\ 15 \end{array} \frac{05}{25} \frac{83}{42} \frac{120}{50} \frac{140}{50}$$

$$s.s. \quad \begin{array}{r} +62 \\ 50 \end{array} \quad \begin{array}{r} +50 \\ 40 \end{array} \frac{36}{26} \frac{37}{22} \frac{28}{19} \frac{24}{9} \quad \begin{array}{r} 20 \\ 15 \end{array} \quad \begin{array}{r} 26 \\ 15 \end{array} \frac{94}{27} \frac{116}{39} \frac{145}{50}$$

$$s.s. \quad \begin{array}{r} +48 \\ 50 \end{array} \quad \begin{array}{r} +47 \\ 37 \end{array} \frac{61}{22} \frac{63}{19} \frac{47}{15} \frac{44}{9} \quad \begin{array}{r} 41 \\ 15 \end{array} \frac{46}{25} \frac{104}{33} \frac{123}{50} \frac{159}{50}$$

$$s.s. \quad \begin{array}{r} +24 \\ 50 \end{array} \quad \begin{array}{r} +15 \\ 41 \end{array} \frac{80}{24} \frac{82}{19} \frac{67}{16} \frac{65}{10} \quad \begin{array}{r} 61 \\ 15 \end{array} \quad \begin{array}{r} 65 \\ 15 \end{array} \frac{131}{28} \frac{140}{39} \frac{164}{50}$$

$$s.s. \quad \begin{array}{r} 28 \\ 50 \end{array} \quad \begin{array}{r} 42 \\ 38 \end{array} \frac{96}{28} \frac{96}{23} \frac{86}{18} \frac{84}{9} \quad \begin{array}{r} 80 \\ 15 \end{array} \frac{86}{21} \frac{132}{31} \frac{176}{50}$$

$$\begin{array}{r} 85 \\ 50 \end{array} \frac{114}{34} \frac{120}{29} \frac{119}{20} \quad \begin{array}{r} 112 \\ 10 \end{array} \quad \begin{array}{r} 109 \\ 15 \end{array} \quad \begin{array}{r} 116 \\ 15 \end{array} \frac{160}{21} \frac{178}{32} \frac{190}{50}$$

Sta.	+	T	-	Elev.
		904.65		
118	+83			02.2 ✓
119				02.1 ✓
	+50			00.4 ✓
120				98.7 ✓
R.M.			6.83	897.82 ✓ (897.80)
	+50			96.7 ✓
121				95.4 ✓
	+50			95.0 ✓
122				95.0 ✓
T.P.	5.50	899.95 ✓	1020	894.45 ✓
	+50			95.1 ✓
123				95.1 ✓
	+50			95.3 ✓

Lt.

4.

Rt.

$$\frac{30}{50} \quad \frac{35}{39} \quad \frac{26}{19} \quad \frac{24}{9} \quad \frac{31}{15} \quad \frac{26}{22} \quad \frac{71}{30} \quad \frac{86}{30} \quad \frac{96}{30}$$

$$\frac{40}{50} \quad \frac{41}{35} \quad \frac{37}{22} \quad \frac{30}{17} \quad \frac{30}{10} \quad \frac{26}{15} \quad \frac{31}{15} \quad \frac{77}{24} \quad \frac{86}{33} \quad \frac{99}{50}$$

$$\frac{56}{50} \quad \frac{56}{33} \quad \frac{57}{20} \quad \frac{48}{16} \quad \frac{47}{9} \quad \frac{43}{15} \quad \frac{48}{22} \quad \frac{84}{30} \quad \frac{104}{30} \quad \frac{113}{50}$$

$$\frac{74}{50} \quad \frac{72}{34} \quad \frac{70}{24} \quad \frac{68}{15} \quad \frac{65}{8} \quad \frac{60}{15} \quad \frac{65}{15} \quad \frac{105}{23} \quad \frac{113}{30} \quad \frac{115}{50}$$

Spk. in Tr. Lt. 120+18

$$\frac{101}{50} \quad \frac{101}{32} \quad \frac{101}{20} \quad \frac{89}{14} \quad \frac{85}{8} \quad \frac{80}{11} \quad \frac{82}{18} \quad \frac{88}{22} \quad \frac{101}{23} \quad \frac{105}{33} \quad \frac{111}{50} \quad \frac{115}{50}$$

$$\frac{115}{50} \quad \frac{113}{33} \quad \frac{113}{20} \quad \frac{102}{16} \quad \frac{96}{8} \quad \frac{93}{12} \quad \frac{96}{12} \quad \frac{99}{16} \quad \frac{114}{21} \quad \frac{116}{31} \quad \frac{116}{50}$$

$$\frac{116}{50} \quad \frac{116}{33} \quad \frac{117}{22} \quad \frac{107}{17} \quad \frac{99}{8} \quad \frac{97}{13} \quad \frac{100}{19} \quad \frac{105}{20} \quad \frac{113}{26} \quad \frac{117}{32} \quad \frac{117}{50}$$

$$\frac{116}{50} \quad \frac{116}{33} \quad \frac{116}{21} \quad \frac{103}{16} \quad \frac{99}{8} \quad \frac{97}{13} \quad \frac{101}{17} \quad \frac{104}{20} \quad \frac{117}{20} \quad \frac{116}{30} \quad \frac{117}{50}$$

$$\frac{70}{50} \quad \frac{70}{32} \quad \frac{72}{21} \quad \frac{57}{15} \quad \frac{52}{8} \quad \frac{49}{14} \quad \frac{52}{11} \quad \frac{54}{20} \quad \frac{67}{23} \quad \frac{68}{24} \quad \frac{64}{31} \quad \frac{69}{50}$$

$$\frac{72}{50} \quad \frac{70}{33} \quad \frac{70}{20} \quad \frac{56}{15} \quad \frac{52}{8} \quad \frac{49}{15} \quad \frac{52}{17} \quad \frac{53}{20} \quad \frac{65}{22} \quad \frac{66}{23} \quad \frac{62}{33} \quad \frac{70}{50} \quad \frac{72}{50}$$

$$\frac{71}{50} \quad \frac{71}{33} \quad \frac{70}{21} \quad \frac{53}{14} \quad \frac{50}{9} \quad \frac{47}{14} \quad \frac{51}{17} \quad \frac{53}{19} \quad \frac{64}{21} \quad \frac{64}{22} \quad \frac{58}{32} \quad \frac{70}{50} \quad \frac{71}{50}$$

Sta.	+	π	-	Elev.
		879.95		
124				95.4
	+50			94.9
125				94.1
	+50			93.7
126				93.4
T.P.	5.53	898.75	6.73	888.22
	+50			93.3
127				93.2
	+50			93.1
128				93.3
	+50			93.7
129				93.8

11/12/39

19

K.A.

L.C.

L.H.

M.D.G.

R.F.

L.H.

2

$$\frac{62}{50} \frac{65}{50} \frac{75}{29} \frac{75}{28} \frac{64}{28} \frac{54}{16} \frac{47}{7} \frac{46}{16} \frac{51}{16} \frac{59}{19} \frac{55}{23} \frac{70}{25} \frac{72}{32} \frac{73}{50}$$

$$\frac{72}{50} \frac{71}{33} \frac{69}{20} \frac{59}{15} \frac{54}{8} \frac{51}{14} \frac{54}{17} \frac{56}{19} \frac{61}{20} \frac{56}{27} \frac{72}{50} \frac{73}{50}$$

$$\frac{78}{50} \frac{76}{33} \frac{79}{22} \frac{65}{14} \frac{61}{7} \frac{59}{13} \frac{60}{17} \frac{64}{20} \frac{71}{22} \frac{65}{27} \frac{77}{27} \frac{78}{50}$$

$$\frac{77}{50} \frac{76}{33} \frac{78}{19} \frac{69}{12} \frac{65}{7} \frac{63}{14} \frac{64}{18} \frac{67}{21} \frac{74}{22} \frac{65}{22} \frac{76}{28} \frac{77}{50}$$

$$\frac{83}{50} \frac{80}{33} \frac{83}{17} \frac{71}{11} \frac{68}{7} \frac{66}{13} \frac{68}{18} \frac{70}{21} \frac{73}{24} \frac{68}{29} \frac{77}{29} \frac{76}{50}$$

$$\frac{67}{50} \frac{69}{32} \frac{69}{16} \frac{60}{11} \frac{56}{6} \frac{55}{15} \frac{57}{22} \frac{60}{22} \frac{58}{24} \frac{66}{27} \frac{64}{50}$$

$$\frac{71}{50} \frac{69}{16} \frac{60}{11} \frac{58}{6} \frac{54}{15} \frac{56}{24} \frac{62}{30} \frac{67}{50} \frac{65}{50}$$

$$\frac{71}{50} \frac{71}{15} \frac{63}{12} \frac{59}{7} \frac{57}{14} \frac{57}{24} \frac{62}{26} \frac{69}{50} \frac{69}{50}$$

$$\frac{71}{50} \frac{71}{15} \frac{61}{10} \frac{57}{7} \frac{55}{15} \frac{54}{19} \frac{59}{20} \frac{62}{24} \frac{63}{25} \frac{69}{27} \frac{67}{50}$$

$$\frac{70}{50} \frac{70}{15} \frac{58}{12} \frac{53}{7} \frac{51}{15} \frac{52}{19} \frac{53}{21} \frac{58}{25} \frac{58}{27} \frac{66}{27} \frac{67}{50}$$

$$\frac{67}{50} \frac{67}{15} \frac{58}{12} \frac{54}{7} \frac{50}{15} \frac{51}{19} \frac{53}{20} \frac{61}{22} \frac{55}{23} \frac{55}{27} \frac{70}{29} \frac{66}{50}$$

Sta.	+	π	-	Elev.	
		898.75			
129	+50			93.7	
130				93.3	
	+50			93.0	
131				92.7	
	+50			92.8	
	+70				
	+77			92.9	
	+80			92.9	
	+91			93.0	
132	+03			92.9	
	+07	P.L.N. End 18' G.M.	88		
	+10			92.9	
B.M.	6.11	899.08	3.78	892.97	(892.97)

Lt.

L.

Rt.

$$\begin{array}{cccccccccccc} 70 & 69 & 70 & 58 & 54 & 51 & 53 & 57 & 58 & 70 & 70 \\ 50 & 32 & 14 & 12 & 7 & 16 & 19 & 25 & 28 & 50 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 72 & 72 & 62 & 56 & 55 & 55 & 61 & 64 & 66 & 62 & 64 & 71 & 71 \\ 50 & 15 & 11 & 6 & 16 & 20 & 22 & 24 & 25 & 29 & 30 & 50 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 74 & 74 & 64 & 61 & 58 & 60 & 63 & 69 & 71 & 70 \\ 50 & 14 & 11 & 7 & 15 & 18 & 20 & 30 & 50 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 77 & 74 & 77 & 68 & 63 & 61 & 64 & 65 & 73 & 73 & 63 & 73 & 73 \\ 50 & 53 & 15 & 11 & 6 & 13 & 18 & 20 & 29 & 26 & 31 & 50 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 78 & 74 & 78 & 64 & 62 & 60 & 61 & 63 & 66 & 63 & 66 & 78 & 73 & 70 \\ 50 & 53 & 14 & 11 & 7 & 14 & 18 & 23 & 25 & 30 & 33 & 40 & 50 & 50 \end{array}$$

$$\begin{array}{r} 8.2 \\ \text{F.L.E. End R'Gals.} \end{array} \quad 90.6.$$

$$\begin{array}{cccccccc} 75 & 70 & 76 & 76 & 64 & 62 & 59 & 60 & 67 \\ 50 & 21 & 20 & 16 & 11 & 7 & 19 & 34 & 34 \end{array} \left(\begin{array}{r} \text{F.L. Calc.} \\ 505 \\ 37 \end{array} \right) \begin{array}{r} 66 \\ 38 \\ 50 \end{array} \quad 90.7.$$

$$\begin{array}{cccccccc} 74 & 73 & 71 & 76 & 68 & 64 & 62 & 59 & 57 & 62 \\ 50 & 39 & 25 & 24 & 15 & 11 & 7 & 14 & 50 & 50 \end{array} \quad 90.0$$

$$\begin{array}{cccccccc} 81 & 80 & 75 & 72 & 71 & 62 & 61 & 58 & 58 & 60 \\ 50 & 33 & 22 & 20 & 14 & 10 & 7 & 20 & 50 & 50 \end{array}$$

$$\begin{array}{cccccccc} 75 & 73 & 71 & 69 & 62 & 59 & 59 & 63 \\ 50 & 33 & 14 & 11 & 7 & 16 & 50 & 50 \end{array}$$

$$\begin{array}{cccccccc} 73 & 75 & 74 & 63 & 62 & 59 & 60 & 64 & 88 & 72 \\ 50 & 34 & 15 & 10 & 7 & 17 & 34 & 38 & 50 & 50 \end{array}$$

Top Month L.C. + "62"

Sta

+ .

A

-

Elev.

897.08

132 145

93.0 ✓

133

93.3 .

150

93.9 .

134

94.4 .

150

94.3 .

135

93.9 .

150

93.9 .

136

94.1 .

150

94.6 .

150

Elev. to Culv.

137

95.3 .

Lt

L

Rt

$$\frac{76}{50} \frac{76}{29} \frac{76}{17} \frac{70}{14} \frac{66}{9} \frac{61}{9} \frac{63}{9} \frac{64}{17} \frac{69}{18} \frac{67}{21} \frac{65}{22} \frac{75}{32} \frac{75}{50}$$

$$\frac{80}{50} \frac{80}{33} \frac{79}{17} \frac{64}{13} \frac{61}{9} \frac{58}{11} \frac{60}{16} \frac{63}{18} \frac{68}{31} L.O.$$

$$\frac{76}{50} \frac{74}{28} \frac{74}{16} \frac{59}{13} \frac{58}{9} \frac{52}{12} \frac{54}{16} \frac{58}{18} \frac{62}{19} \frac{65}{25} \frac{70}{27} \frac{74}{32} \frac{74}{50}$$

$$\frac{77}{50} \frac{75}{28} \frac{75}{16} \frac{56}{13} \frac{51}{9} \frac{47}{11} \frac{50}{16} \frac{56}{19} \frac{67}{25} \frac{69}{27} \frac{64}{27} \frac{74}{50}$$

$$\frac{77}{50} \frac{74}{27} \frac{73}{17} \frac{58}{12} \frac{51}{9} \frac{48}{11} \frac{50}{15} \frac{56}{19} \frac{67}{25} \frac{68}{26} \frac{69}{33} \frac{73}{50} \frac{74}{50}$$

$$\frac{74}{50} \frac{76}{28} \frac{76}{16} \frac{64}{13} \frac{57}{9} \frac{52}{11} \frac{53}{18} \frac{59}{21} \frac{63}{28} \frac{65}{33} \frac{72}{33} \frac{70}{50}$$

$$\frac{78}{50} \frac{76}{30} \frac{75}{16} \frac{61}{12} \frac{56}{9} \frac{52}{10} \frac{53}{15} \frac{58}{19} \frac{65}{24} \frac{66}{26} \frac{60}{32} \frac{71}{32} \frac{71}{50}$$

$$\frac{77}{50} \frac{76}{29} \frac{70}{16} \frac{61}{12} \frac{53}{9} \frac{50}{10} \frac{50}{17} \frac{59}{20} \frac{67}{24} \frac{67}{26} \frac{62}{26} \frac{72}{32} L.O.$$

$$\frac{77}{50} \frac{75}{32} \frac{71}{21} \frac{57}{15} \frac{48}{9} \frac{45}{10} \frac{47}{17} \frac{54}{20} \frac{65}{24} \frac{65}{27} \frac{62}{32} \frac{71}{32} \frac{69}{50}$$

$$\frac{56}{905}$$

$$\frac{7.90}{91.2}$$

$$\frac{76}{50} \frac{75}{32} \frac{72}{21} \frac{50}{15} \frac{41}{9} \frac{38}{11} \frac{41}{19} \frac{51}{22} \frac{63}{23} \frac{76}{37} \frac{68}{44} \frac{66}{50}$$

Sta.	+	π	-	Elev.
		899.08		
137	+50			96.2
138				97.4
T.P.	10.44	907.82	1.70	897.37 98.4 99.3
	+50			99.3
139				99.3 00.1
				00.1
	+50			01.0
				01.0
140				02.0
				02.0
	+50			02.9
				02.9
141				03.8
				03.8
	+50			04.5
				04.5
142				99.8
T.P.	8.82	913.29	3.35	909.47 05.3
	+50			05.3

LH

L

RH

$$\frac{77}{50} \frac{76}{21} \frac{41}{15} \frac{33}{9} \frac{29}{11} \frac{31}{19} \frac{40}{21} \frac{51}{27} \frac{51}{33} \frac{56}{50}$$

$$\frac{79}{50} \frac{65}{25} \frac{33}{16} \frac{21}{9} \frac{17}{11} \frac{19}{20} \frac{28}{26} \frac{38}{36} \frac{47}{50}$$

$$\frac{147}{50} \frac{134}{30} \frac{109}{18} \frac{97}{9} \frac{94}{11} \frac{96}{22} \frac{104}{35} \frac{119}{45} \frac{125}{50}$$

$$\frac{127}{50} \frac{119}{34} \frac{114}{23} \frac{100}{17} \frac{88}{9} \frac{85}{4} \frac{87}{26} \frac{97}{39} \frac{105}{50} \frac{99}{50}$$

$$\frac{134}{50} \frac{107}{24} \frac{90}{10} \frac{80}{9} \frac{77}{11} \frac{79}{11} \frac{85}{20} \frac{81}{34} \frac{80}{50}$$

$$\frac{92}{50} \frac{90}{32} \frac{96}{23} \frac{88}{16} \frac{71}{9} \frac{68}{11} \frac{70}{19} \frac{76}{27} \frac{80}{33} \frac{65}{50} \frac{53}{50}$$

$$\frac{91}{50} \frac{84}{38} \frac{88}{29} \frac{82}{21} \frac{67}{14} \frac{61}{9} \frac{58}{11} \frac{60}{16} \frac{64}{22} \frac{72}{39} \frac{20}{34} \frac{47}{41} \frac{42}{50} \frac{29}{50}$$

$$\frac{97}{50} \frac{83}{34} \frac{72}{26} \frac{56}{15} \frac{51}{9} \frac{49}{11} \frac{51}{16} \frac{56}{20} \frac{63}{26} \frac{62}{35} \frac{38}{41} \frac{28}{50} \frac{12}{50}$$

$$\frac{96}{50} \frac{73}{28} \frac{60}{21} \frac{47}{15} \frac{43}{9} \frac{40}{11} \frac{41}{15} \frac{45}{19} \frac{52}{22} \frac{52}{29} \frac{41}{35} \frac{31}{40} \frac{27}{50} \frac{15}{50}$$

$$\frac{92}{50} \frac{71}{31} \frac{58}{25} \frac{44}{17} \frac{36}{9} \frac{33}{12} \frac{36}{19} \frac{41}{29} \frac{41}{36} \frac{16}{46} \frac{08}{50} \frac{02}{50}$$

$$\frac{140}{50} \frac{111}{28} \frac{102}{22} \frac{88}{15} \frac{83}{10} \frac{80}{10} \frac{81}{14} \frac{83}{22} \frac{90}{50} \frac{90}{36} \frac{53}{44} \frac{50}{50} \frac{48}{50}$$

Sta

+

K

-

Elev.

91.3.29

143

06.3.

+35

06.9.

+73

07.6.

+86

07.8.

144

08.0.

+06

08.1.

+50

08.4.

145

08.7.

+50

08.5.

146

08.3.

B.M.

619

91.3.33.

619

907.10.

907.14

+50

07.8.

Lt.

R.

Rt.

$$\begin{array}{cccccccccccccccc} 10.8 & 97 & 94 & 87 & 79 & 73 & 71 & 72 & 75 & 80 & 77 & 30 & 31 & 2.8 \\ 50 & 32 & 27 & 22 & 16 & 9 & & 10 & 15 & 20 & 29 & 36 & 44 & 50 \end{array} \quad |$$

$$\begin{array}{cccccccccccccccc} 96 & 79 & 87 & 85 & 72 & 67 & 64 & 66 & 67 & 66 & 16 & 15 \\ 50 & 33 & 31 & 21 & 14 & 9 & & 10 & 15 & 29 & 36 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 84 & 66 & 83 & 61 & 63 & 61 & 57 & & 58 & & 53 & 20 & 0.0 \\ 50 & 32 & 30 & 22 & 14 & 10 & & & 12 & & 28 & 37 & 50 \end{array}$$

$$\begin{array}{cccc} 55 & 55 & 50 & 2.2 \\ 9 & 25 & 50 & \end{array}$$

$$\begin{array}{cccc} 53 & 54 & 48 & 27 \\ 7 & 21 & 37 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 67 & 52 & 76 & 75 & 59 & 56 & 52 & 53 & 45 & 20 & 10 & 12.9 \\ 50 & 33 & 30 & 22 & 16 & 10 & & 7 & 29 & 36 & 50 & 55 \end{array}$$

$$\begin{array}{cccccccccccccccc} 60 & 43 & 70 & 70 & 55 & 53 & 49 & 51 & 52 & 19 & 16 & 13.2 \\ 50 & 34 & 30 & 21 & 14 & 11 & & 9 & 28 & 35 & 41 & 48 \end{array}$$

$$\begin{array}{cccccccccccccccc} 70 & 44 & 68 & 68 & 54 & 50 & 46 & 48 & 53 & 14 & 13 & 13.6 \\ 50 & 33 & 29 & 21 & 15 & 11 & & 10 & 26 & 34 & 42 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 90 & 64 & 76 & 76 & 56 & 52 & 48 & 50 & 50 & 14 & 0.9 & 10.0 \\ 50 & 32 & 28 & 27 & 16 & 11 & & 10 & 26 & 34 & 45 & 54 \end{array}$$

$$\begin{array}{cccccccccccccccc} 115 & 90 & 86 & 68 & 59 & 50 & 54 & 56 & 46 & 07 & 02 & 12.8 & +30 \\ 50 & 36 & 27 & 20 & 11 & & 9 & 19 & 26 & 33 & 38 & 45 & 50 \end{array}$$

2pk in RPLT 146+49

$$\begin{array}{cccccccccccccccc} 140 & 96 & 68 & 59 & 55 & 56 & 59 & 43 & 39 & 105 & 11.8 \\ 50 & 29 & 22 & 11 & & 9 & 17 & 21 & 28 & 37 & 50 \end{array}$$

Sta	T	K	-	Elev.
		913.33		
147				07.4
+50				06.9
T.P.	6.37	913.15	6.55	906.78
148				06.8
+50				06.7
149				06.7
+50				07.2
150				07.6
+50				08.4
151				09.4
T.P.	11.92	921.23	389	909.31
+50				10.2
152				11.3

14.

4.

24.

$$\frac{154}{50} \quad \frac{120}{30} \quad \frac{75}{21} \quad \frac{65}{11} \quad \frac{59}{9} \quad \frac{61}{9} \quad \frac{6.5}{19} \quad \frac{58}{25} \quad \frac{14}{33} \quad \frac{0.4}{50}$$

$$\frac{162}{50} \quad \frac{133}{29} \quad \frac{76}{19} \quad \frac{67}{11} \quad \frac{64}{9} \quad \frac{65}{18} \quad \frac{70}{27} \quad \frac{6.2}{27} \quad \frac{38}{29} \quad \frac{2.9}{50}$$

25/2 48

$$\frac{154}{50} \quad \frac{127}{26} \quad \frac{76}{18} \quad \frac{67}{10} \quad \frac{64}{8} \quad \frac{65}{19} \quad \frac{67}{22} \quad \frac{72}{27} \quad \frac{58}{27} \quad \frac{42}{50}$$

$$\frac{156}{50} \quad \frac{132}{28} \quad \frac{77}{19} \quad \frac{68}{11} \quad \frac{65}{9} \quad \frac{66}{16} \quad \frac{70}{20} \quad \frac{74}{25} \quad \frac{75}{28} \quad \frac{57}{40} \quad \frac{53}{50}$$

$$\frac{152}{50} \quad \frac{133}{37} \quad \frac{120}{27} \quad \frac{76}{18} \quad \frac{68}{11} \quad \frac{65}{9} \quad \frac{65}{15} \quad \frac{68}{20} \quad \frac{84}{23} \quad \frac{83}{26} \quad \frac{63}{35} \quad \frac{62}{54} \quad \frac{54}{50}$$

$$\frac{157}{50} \quad \frac{135}{27} \quad \frac{73}{18} \quad \frac{64}{11} \quad \frac{60}{9} \quad \frac{61}{15} \quad \frac{63}{20} \quad \frac{73}{23} \quad \frac{74}{27} \quad \frac{60}{27} \quad \frac{57}{37} \quad \frac{55}{50}$$

$$\frac{158}{50} \quad \frac{136}{30} \quad \frac{66}{18} \quad \frac{60}{11} \quad \frac{56}{9} \quad \frac{56}{17} \quad \frac{59}{22} \quad \frac{68}{24} \quad \frac{68}{26} \quad \frac{58}{38} \quad \frac{57}{50} \quad \frac{51}{50}$$

$$\frac{154}{50} \quad \frac{131}{30} \quad \frac{59}{19} \quad \frac{53}{11} \quad \frac{48}{9} \quad \frac{49}{17} \quad \frac{53}{19} \quad \frac{54}{22} \quad \frac{56}{26} \quad \frac{42}{26} \quad \frac{32}{50}$$

$$\frac{115}{50} \quad \frac{86}{28} \quad \frac{51}{21} \quad \frac{42}{11} \quad \frac{38}{9} \quad \frac{40}{16} \quad \frac{43}{25} \quad \frac{41}{28} \quad \frac{26}{28} \quad \frac{12}{43} \quad \frac{0.4}{50}$$

$$\frac{133}{50} \quad \frac{103}{27} \quad \frac{125}{22} \quad \frac{118}{15} \quad \frac{112}{10} \quad \frac{110}{9} \quad \frac{112}{15} \quad \frac{115}{24} \quad \frac{115}{28} \quad \frac{90}{34} \quad \frac{81}{38} \quad \frac{56}{38} \quad \frac{4.9}{50}$$

$$\frac{9.0}{50} \quad \frac{6.8}{28} \quad \frac{11.3}{21} \quad \frac{10.7}{15} \quad \frac{10.2}{10} \quad \frac{9.9}{9} \quad \frac{10.0}{17} \quad \frac{10.5}{26} \quad \frac{100}{30} \quad \frac{70}{35} \quad \frac{63}{39} \quad \frac{36}{50} \quad \frac{3.6}{50}$$

Sta	+	π	-	Elev
		921.13.		
152	+50			12.6
153				14.0
	+50			15.2
154				16.2
	+50			17.0
155				17.7
T.P.	5.45	923.14.	3.54	917.69.
	+50			17.9
156				18.0
	+50			18.0
157				18.0
	+50			17.9

41

42

43

$$\frac{75}{50} \quad \frac{57}{28} \quad \frac{104}{20} \quad \frac{104}{18} \quad \frac{93}{15} \quad \frac{89}{11} \quad \frac{86}{9} \quad \frac{87}{16} \quad \frac{92}{18} \quad \frac{91}{24} \quad \frac{56}{28} \quad \frac{53}{32} \quad \frac{36}{35} \quad \frac{30}{50}$$

$$\frac{36}{50} \quad \frac{33}{23} \quad \frac{95}{19} \quad \frac{78}{14} \quad \frac{74}{11} \quad \frac{72}{9} \quad \frac{73}{17} \quad \frac{74}{19} \quad \frac{82}{22} \quad \frac{81}{28} \quad \frac{43}{28} \quad \frac{23}{50}$$

$$\frac{13}{50} \quad \frac{13}{30} \quad \frac{78}{20} \quad \frac{78}{18} \quad \frac{68}{15} \quad \frac{69}{11} \quad \frac{60}{9} \quad \frac{61}{16} \quad \frac{62}{19} \quad \frac{71}{23} \quad \frac{71}{32} \quad \frac{12}{50}$$

$$\frac{17}{50} \quad \frac{12}{29} \quad \frac{65}{23} \quad \frac{65}{19} \quad \frac{56}{14} \quad \frac{54}{11} \quad \frac{50}{10} \quad \frac{52}{16} \quad \frac{53}{18} \quad \frac{63}{21} \quad \frac{61}{28} \quad \frac{20}{50}$$

$$\frac{25}{50} \quad \frac{33}{40} \quad \frac{33}{28} \quad \frac{53}{23} \quad \frac{58}{19} \quad \frac{53}{17} \quad \frac{46}{10} \quad \frac{42}{10} \quad \frac{44}{16} \quad \frac{43}{18} \quad \frac{57}{22} \quad \frac{55}{26} \quad \frac{29}{50}$$

$$\frac{46}{50} \quad \frac{44}{29} \quad \frac{57}{25} \quad \frac{56}{21} \quad \frac{45}{17} \quad \frac{40}{11} \quad \frac{35}{10} \quad \frac{37}{16} \quad \frac{39}{19} \quad \frac{50}{23} \quad \frac{51}{28} \quad \frac{33}{27} \quad \frac{29}{50}$$

$$\frac{76}{50} \quad \frac{72}{31} \quad \frac{76}{26} \quad \frac{73}{23} \quad \frac{68}{22} \quad \frac{59}{18} \quad \frac{55}{10} \quad \frac{52}{10} \quad \frac{54}{16} \quad \frac{56}{19} \quad \frac{64}{23} \quad \frac{68}{28} \quad \frac{55}{35} \quad \frac{55}{50}$$

$$\frac{24}{50} \quad \frac{91}{40} \quad \frac{85}{27} \quad \frac{81}{22} \quad \frac{61}{18} \quad \frac{55}{10} \quad \frac{51}{9} \quad \frac{52}{17} \quad \frac{54}{21} \quad \frac{67}{32} \quad \frac{66}{32} \quad \frac{58}{50}$$

$$\frac{102}{50} \quad \frac{89}{26} \quad \frac{79}{22} \quad \frac{63}{17} \quad \frac{56}{11} \quad \frac{51}{9} \quad \frac{51}{9} \quad \frac{50}{18} \quad \frac{65}{22} \quad \frac{69}{28} \quad \frac{67}{33} \quad \frac{58}{50}$$

$$\frac{82}{50} \quad \frac{72}{30} \quad \frac{71}{20} \quad \frac{61}{16} \quad \frac{54}{10} \quad \frac{51}{10} \quad \frac{53}{19} \quad \frac{50}{22} \quad \frac{63}{27} \quad \frac{65}{27} \quad \frac{65}{33} \quad \frac{57}{50}$$

$$\frac{67}{50} \quad \frac{60}{25} \quad \frac{69}{23} \quad \frac{69}{19} \quad \frac{63}{18} \quad \frac{56}{10} \quad \frac{52}{10} \quad \frac{53}{25} \quad \frac{57}{25} \quad \frac{54}{50}$$

Sta.	+	X	-	Elev.
		923.14.		
158				17.8.
B.M.			5.35	917.79 .
+50				17.9 .
				717.80
159				18.0 .
+50				18.0 .
160				17.6 .
I.P.	1.80	919.45 .	5.49	917.65 .
+50				17.0 .
161				16.3 .
+50				15.8 .
162				15.1 .
+42				14.5 .
+70				14.0 .

14

4

24

$$\frac{64}{50} \frac{60}{28} \frac{67}{25} \frac{66}{11} \frac{63}{17} \frac{57}{14} \frac{55}{9} \frac{53}{11} \frac{55}{16} \frac{57}{19} \frac{62}{23} \frac{63}{28} \frac{53}{28} \frac{47}{50}$$

Top Mount 168+23.6

$$\frac{58}{50} \frac{58}{29} \frac{63}{21} \frac{41}{17} \frac{54}{14} \frac{54}{9} \frac{52}{10} \frac{54}{15} \frac{56}{18} \frac{64}{25} \frac{66}{29} \frac{45}{49} \frac{53}{49} \frac{45}{50}$$

$$\frac{52}{50} \frac{53}{38} \frac{55}{24} \frac{62}{21} \frac{61}{17} \frac{51}{15} \frac{53}{9} \frac{51}{11} \frac{53}{16} \frac{55}{19} \frac{64}{24} \frac{66}{29} \frac{46}{29} \frac{49}{50}$$

$$\frac{50}{50} \frac{51}{28} \frac{64}{20} \frac{63}{17} \frac{55}{14} \frac{54}{9} \frac{51}{11} \frac{53}{17} \frac{57}{20} \frac{64}{23} \frac{66}{29} \frac{47}{29} \frac{45}{50}$$

$$\frac{52}{50} \frac{55}{29} \frac{67}{21} \frac{68}{17} \frac{56}{11} \frac{57}{9} \frac{55}{11} \frac{56}{16} \frac{62}{23} \frac{70}{25} \frac{70}{27} \frac{47}{27} \frac{52}{50}$$

$$\frac{23}{50} \frac{30}{29} \frac{37}{22} \frac{38}{17} \frac{28}{14} \frac{27}{9} \frac{25}{11} \frac{28}{15} \frac{28}{17} \frac{36}{23} \frac{37}{26} \frac{24}{32} \frac{15}{32} \frac{25}{50}$$

$$\frac{27}{50} \frac{33}{39} \frac{42}{24} \frac{43}{18} \frac{36}{14} \frac{33}{9} \frac{32}{11} \frac{35}{16} \frac{36}{19} \frac{44}{21} \frac{45}{26} \frac{31}{26} \frac{44}{50}$$

$$\frac{29}{50} \frac{36}{36} \frac{44}{28} \frac{50}{21} \frac{47}{16} \frac{39}{14} \frac{39}{9} \frac{37}{11} \frac{40}{15} \frac{42}{19} \frac{53}{22} \frac{52}{27} \frac{40}{27} \frac{64}{50}$$

$$\frac{31}{50} \frac{45}{31} \frac{57}{20} \frac{54}{17} \frac{49}{14} \frac{46}{9} \frac{44}{11} \frac{46}{15} \frac{48}{18} \frac{57}{23} \frac{63}{26} \frac{54}{38} \frac{72}{38} \frac{90}{50}$$

$$\frac{35}{50} \frac{47}{35} \frac{58}{28} \frac{62}{19} \frac{54}{15} \frac{52}{9} \frac{50}{11} \frac{53}{16} \frac{54}{22} \frac{85}{27} \frac{91}{27} \frac{114}{50}$$

$$\frac{48}{50} \frac{59}{37} \frac{70}{27} \frac{72}{20} \frac{59}{15} \frac{57}{9} \frac{55}{11} \frac{58}{16} \frac{58}{26} \frac{111}{33} \frac{119}{33} \frac{137}{50}$$

Sta.	+	π	-	E/CV.
		919.45		
163				13.5.
	+50			13.0.
T.P.	563	918.12.	6.96	912.49.
164				12.7.
	+50			12.8.
165				12.7.
	+50			12.7.
166				12.8.
	+50			12.9.
167				13.0.
	+50			13.1.
168				13.1.

Lt.

L

Lt.

$$\frac{78}{50} \quad \frac{92}{33} \quad \frac{95}{25} \quad \frac{88}{20} \quad \frac{62}{14} \quad \frac{61}{9} \quad \frac{60}{-} \quad \frac{63}{11} \quad \frac{66}{16} \quad \frac{129}{27} \quad \frac{132}{33} \quad \frac{134}{50}$$

$$\frac{110}{50} \quad \frac{120}{36} \quad \frac{118}{28} \quad \frac{106}{20} \quad \frac{69}{14} \quad \frac{66}{9} \quad \frac{65}{-} \quad \frac{67}{11} \quad \frac{72}{20} \quad \frac{113}{27} \quad \frac{117}{31} \quad \frac{118}{42} \quad \frac{113}{50}$$

Nail in T.A.R.L. 113 + 70

$$\frac{116}{50} \quad \frac{100}{21} \quad \frac{58}{14} \quad \frac{56}{9} \quad \frac{54}{-} \quad \frac{56}{10} \quad \frac{60}{19} \quad \frac{54}{25} \quad \frac{80}{38} \quad \frac{74}{50}$$

$$\frac{109}{50} \quad \frac{99}{34} \quad \frac{88}{22} \quad \frac{59}{16} \quad \frac{56}{8} \quad \frac{53}{-} \quad \frac{55}{10} \quad \frac{56}{15} \quad \frac{67}{18} \quad \frac{67}{22} \quad \frac{61}{25} \quad \frac{51}{50}$$

$$\frac{93}{50} \quad \frac{81}{33} \quad \frac{67}{18} \quad \frac{59}{15} \quad \frac{55}{7} \quad \frac{54}{-} \quad \frac{55}{9} \quad \frac{55}{16} \quad \frac{63}{18} \quad \frac{62}{23} \quad \frac{50}{26} \quad \frac{48}{32} \quad \frac{48}{50}$$

$$\frac{75}{50} \quad \frac{64}{34} \quad \frac{63}{18} \quad \frac{53}{14} \quad \frac{55}{8}$$

$$\frac{54}{-} \quad \frac{55}{9} \quad \frac{52}{16} \quad \frac{57}{18} \quad \frac{58}{23} \quad \frac{45}{27} \quad \frac{45}{50}$$

$$\frac{57}{50} \quad \frac{54}{38} \quad \frac{58}{17} \quad \frac{52}{14} \quad \frac{53}{7} \quad \frac{53}{-} \quad \frac{54}{9} \quad \frac{52}{16} \quad \frac{57}{19} \quad \frac{57}{23} \quad \frac{48}{25} \quad \frac{48}{50}$$

$$\frac{49}{50} \quad \frac{52}{34} \quad \frac{58}{16} \quad \frac{52}{14} \quad \frac{53}{9} \quad \frac{52}{-} \quad \frac{53}{10} \quad \frac{54}{16} \quad \frac{60}{19} \quad \frac{60}{23} \quad \frac{53}{25} \quad \frac{51}{35} \quad \frac{52}{50}$$

$$\frac{48}{50} \quad \frac{51}{40} \quad \frac{58}{27} \quad \frac{58}{16} \quad \frac{51}{14} \quad \frac{52}{10} \quad \frac{51}{-} \quad \frac{51}{9} \quad \frac{50}{14} \quad \frac{58}{16} \quad \frac{61}{23} \quad \frac{54}{25} \quad \frac{52}{50}$$

$$\frac{54}{30} \quad \frac{54}{35} \quad \frac{60}{19} \quad \frac{50}{14} \quad \frac{51}{10} \quad \frac{50}{-} \quad \frac{50}{9} \quad \frac{51}{15} \quad \frac{56}{16} \quad \frac{57}{22} \quad \frac{48}{24} \quad \text{L.O.}$$

$$\frac{56}{30} \quad \frac{56}{27} \quad \frac{62}{17} \quad \frac{52}{13} \quad \frac{52}{10} \quad \frac{50}{-} \quad \frac{52}{10} \quad \frac{52}{14} \quad \frac{59}{16} \quad \frac{57}{20} \quad \frac{44}{25} \quad \text{L.O.}$$

Sta.	+	π	-	Elev.
		918.12		
168	+50			12.9.
169				12.6.
T.P.	2.96	918.57.	5.51	912.61.
	+50			12.3.
170				11.9.
	+50			11.5.
171				11.2.
	+50			10.8.
B.M.			615	909.42. (909.44)
172				10.4.
	+50			10.1.
173				09.9.
	+50			09.5.

Lt.

K.

Rt.

$$\frac{67}{50} \frac{62}{29} \frac{64}{16} \frac{57}{14} \frac{56}{10} \frac{52}{10} \frac{54}{15} \frac{55}{17} \frac{40}{22} \frac{57}{26} \frac{40}{26} \text{ L.O.}$$

$$\frac{80}{50} \frac{73}{29} \frac{68}{17} \frac{59}{14} \frac{58}{10} \frac{55}{9} \frac{57}{14} \frac{57}{16} \frac{62}{21} \frac{60}{25} \frac{42}{25} \text{ L.O.}$$

$$\frac{69}{50} \frac{62}{35} \frac{51}{18} \frac{37}{14} \frac{35}{10} \frac{33}{9} \frac{35}{15} \frac{35}{17} \frac{41}{21} \frac{40}{25} \frac{15}{25} \text{ L.O.}$$

$$\frac{85}{30} \frac{71}{32} \frac{62}{20} \frac{40}{15} \frac{39}{9} \frac{37}{9} \frac{37}{14} \frac{39}{16} \frac{45}{21} \frac{47}{24} \frac{39}{24} \frac{19}{20}$$

$$\frac{99}{50} \frac{79}{32} \frac{65}{21} \frac{45}{15} \frac{42}{10} \frac{41}{9} \frac{42}{9} \frac{43}{14} \frac{53}{17} \frac{52}{22} \frac{35}{25} \frac{18}{50}$$

$$\frac{108}{50} \frac{77}{32} \frac{75}{23} \frac{48}{15} \frac{46}{10} \frac{44}{9} \frac{46}{15} \frac{47}{17} \frac{54}{22} \frac{53}{25} \frac{37}{25} \frac{28}{30} \frac{19}{50}$$

$$\frac{115}{50} \frac{87}{28} \frac{78}{20} \frac{55}{14} \frac{52}{10} \frac{48}{10} \frac{50}{10} \frac{48}{16} \frac{51}{19} \frac{48}{24} \frac{35}{30} \frac{29}{50}$$

30k.10 PRL 171144

$$\frac{119}{50} \frac{77}{20} \frac{56}{15} \frac{53}{10} \frac{52}{8} \frac{53}{15} \frac{53}{17} \frac{61}{23} \frac{60}{30} \frac{35}{40} \frac{29}{50} \frac{23}{50}$$

$$\frac{118}{50} \frac{80}{21} \frac{61}{16} \frac{57}{11} \frac{55}{8} \frac{56}{14} \frac{55}{17} \frac{63}{19} \frac{58}{25} \frac{35}{32} \frac{31}{42} \frac{24}{50}$$

$$\frac{120}{50} \frac{80}{20} \frac{64}{17} \frac{61}{11} \frac{57}{8} \frac{58}{15} \frac{57}{18} \frac{65}{25} \frac{61}{30} \frac{40}{30} \frac{33}{42} \frac{27}{50}$$

$$\frac{124}{50} \frac{86}{21} \frac{66}{16} \frac{64}{12} \frac{61}{8} \frac{60}{14} \frac{58}{19} \frac{64}{23} \frac{64}{23} \frac{45}{32} \frac{31}{50}$$

Sta.	+	T	-	Elev.
		915.57		
174				09.1
	+50			08.5
175				07.7
T.P.	3.35	911.05	7.87	907.70
	+50			06.8
176				06.0
	+50			05.2
177				04.3
	+50			03.3
178				02.7
	+50			01.7
179				00.8
T.P.	1.43	902.18	10.30	900.75

Lt

R

Rt

$$\begin{array}{r} 124 \ 86 \ 70 \ 69 \\ 50 \ 21 \ 17 \ 12 \end{array} \quad \begin{array}{r} 65 \ 66 \ 63 \ 71 \ 70 \ 62 \ 40 \ 30 \\ 8 \ 17 \ 19 \ 22 \ 26 \ 31 \ 50 \end{array}$$

$$\begin{array}{r} 130 \ 90 \ 77 \ 75 \ 71 \ 72 \ 74 \ 78 \ 76 \ 66 \ 42 \ 32 \\ 50 \ 20 \ 17 \ 11 \ 8 \ 15 \ 17 \ 22 \ 29 \ 35 \ 50 \end{array}$$

$$\begin{array}{r} 134 \ 99 \ 84 \ 83 \\ 50 \ 22 \ 17 \ 11 \end{array} \quad \begin{array}{r} 79 \ 81 \ 81 \ 84 \ 86 \ 70 \ 47 \ 34 \\ 8 \ 15 \ 17 \ 22 \ 29 \ 33 \ 50 \end{array}$$

$$\begin{array}{r} 102 \ 68 \ 49 \ 47 \ 43 \ 45 \ 44 \ 49 \ 50 \ 37 \ 11 \ 11.0 \\ 50 \ 21 \ 17 \ 12 \ 8 \ 15 \ 17 \ 22 \ 27 \ 32 \ 50 \end{array}$$

$$\begin{array}{r} 114 \ 76 \ 58 \ 55 \ 51 \ 53 \ 52 \ 58 \ 57 \ 40 \ 17 \ 0.3 \\ 50 \ 20 \ 16 \ 11 \ 8 \ 15 \ 17 \ 24 \ 29 \ 33 \ 50 \end{array}$$

$$\begin{array}{r} 127 \ 84 \ 65 \ 63 \ 59 \\ 50 \ 20 \ 15 \ 11 \end{array} \quad \begin{array}{r} 60 \\ 9 \end{array} \quad \begin{array}{r} 46 \ 32 \\ 34 \ 50 \end{array}$$

$$\begin{array}{r} 133 \ 96 \ 73 \ 71 \ 68 \ 69 \ 67 \ 73 \ 72 \ 53 \ 3.7 \\ 50 \ 20 \ 15 \ 12 \ 8 \ 15 \ 18 \ 25 \ 30 \ 50 \end{array}$$

$$\begin{array}{r} 137 \ 102 \ 84 \ 81 \ 78 \ 78 \ 74 \ 86 \ 80 \ 63 \ 53 \\ 50 \ 20 \ 16 \ 11 \ 8 \ 15 \ 18 \ 25 \ 30 \ 50 \end{array}$$

$$\begin{array}{r} 143 \ 108 \ 92 \ 88 \ 84 \ 86 \ 88 \ 100 \ 78 \ 74 \ 5.9 \\ 50 \ 21 \ 16 \ 10 \ 8 \ 15 \ 17 \ 26 \ 32 \ 50 \end{array}$$

$$\begin{array}{r} 146 \ 131 \ 113 \ 99 \ 97 \ 94 \ 95 \ 97 \ 107 \ 110 \ 106 \ 81 \ 6.7 \\ 50 \ 39 \ 22 \ 17 \ 11 \ 8 \ 14 \ 17 \ 21 \ 26 \ 36 \ 50 \end{array}$$

$$\begin{array}{r} 150 \ 124 \ 107 \ 105 \ 103 \ 104 \ 105 \ 115 \ 126 \ 110 \ 90 \ 7.9 \\ 50 \ 30 \ 17 \ 11 \ 8 \ 13 \ 18 \ 22 \ 28 \ 36 \ 50 \end{array}$$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

902.18.

179	+50			99.71
-----	-----	--	--	-------

180				988.
-----	--	--	--	------

	+50			979.
--	-----	--	--	------

181				970.
-----	--	--	--	------

	+50			96.2.
--	-----	--	--	-------

182				95.8.
-----	--	--	--	-------

+12	level in ditch running S.W. of S. End Ent. Culv.			
-----	--	--	--	--

+38

+50

95.5.

+82	F.Line W. End R. Culv.			12.64
-----	------------------------	--	--	-------

+92	F.Line E. End R. Culv.			12.60
-----	------------------------	--	--	-------

T.P.	5.22	900.35	7.05	895.13.
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Lt.

2

Rt.

$$\frac{67}{50} \frac{40}{23} \frac{30}{17} \frac{27}{10} \frac{35}{16} \frac{25}{8} \frac{28}{16} \frac{38}{19} \frac{41}{22} \frac{33}{25} \frac{20}{35} \frac{27}{50}$$

$$\frac{29}{50} \frac{65}{32} \frac{56}{21} \frac{42}{16} \frac{38}{10} \frac{34}{8} \frac{36}{16} \frac{37}{19} \frac{48}{24} \frac{49}{29} \frac{43}{36} \frac{38}{50} \frac{24}{50}$$

$$\frac{27}{50} \frac{83}{34} \frac{73}{21} \frac{45}{15} \frac{46}{10} \frac{43}{9} \frac{45}{17} \frac{48}{22} \frac{60}{26} \frac{60}{30} \frac{56}{30} \frac{42}{50}$$

$$\frac{105}{50} \frac{100}{34} \frac{92}{22} \frac{58}{15} \frac{56}{10} \frac{52}{9} \frac{54}{15} \frac{55}{19} \frac{68}{23} \frac{68}{29} \frac{65}{29} \frac{57}{50}$$

$$\frac{109}{50} \frac{104}{24} \frac{68}{16} \frac{65}{11} \frac{60}{9} \frac{62}{12} \frac{61}{21} \frac{74}{35} \frac{75}{50}$$

$$\frac{108}{50} \frac{113}{37} \frac{118}{37} \frac{118}{36} \frac{113}{36} \frac{104}{22} \frac{71}{19} \frac{68}{10} \frac{64}{9} \frac{67}{15} \frac{68}{20} \frac{91}{23} \frac{92}{28} \frac{86}{50}$$

$$\frac{134}{250} \left(\frac{\Delta}{219} \right) \frac{133}{200} \frac{132}{150} \frac{129}{100} \frac{131}{50} \left(\frac{132}{89.0} \text{ F.Line 50. End} \right)$$

$$\frac{12.5}{89.7} \text{ F.Line N. End Ent. Culv.}$$

$$\frac{106}{50} \frac{108}{25} \frac{122}{25} \frac{122}{24} \frac{128}{24} \frac{78}{19} \frac{72}{10} \frac{67}{8} \frac{70}{14} \frac{72}{20} \frac{98}{23} \frac{101}{33} \frac{101}{40} \frac{105}{40} \frac{109}{50}$$

a sta 183

Sta	+	π	-	Elev.	
		900.35			
183				95.2.	
	+50			95.0.	
184				94.9.	
	+50			95.1.	
	465	4. culv.			
B.M.			531	895.04.	895.09
185				95.4.	
	+50			95.8.	
186				96.4.	
	+50			96.8.	
187				97.2.	
	+50			97.9.	
T.P.	1136	909.49.	222	898.13.	

Lt.

A

Rt.

$$\begin{array}{r} 87 \ 86 \ 79 \ 57 \ 57 \ 52 \ 54 \ 57 \ 82 \ 91 \ 90 \ 89 \\ 50 \ 25 \ 20 \ 16 \ 11 \ 8 \ 14 \ 21 \ 27 \ 29 \ 50 \end{array}$$

$$\begin{array}{r} 91 \ 89 \ 81 \ 61 \ 57 \ 54 \ 56 \ 60 \ 80 \ 87 \ 86 \\ 50 \ 26 \ 21 \ 18 \ 11 \ 9 \ 14 \ 20 \ 31 \ 50 \end{array}$$

$$\begin{array}{r} 90 \ 88 \ 83 \ 60 \ 58 \ 55 \ 56 \ 60 \ 82 \ 87 \ 89 \\ 50 \ 29 \ 24 \ 18 \ 11 \ 9 \ 14 \ 20 \ 27 \ 50 \end{array}$$

$$\begin{array}{r} 88 \ 86 \ 75 \ 63 \ 57 \ 53 \ 55 \ 58 \ 82 \ 88 \ 89 \\ 50 \ 23 \ 23 \ 16 \ 11 \ 9 \ 14 \ 21 \ 25 \ 50 \end{array}$$

1090

FLINE

89.45

1095

FLINE

89.40

Two Man 18416502

$$\begin{array}{r} 88 \ 88 \ 81 \ 60 \ 56 \ 50 \ 53 \ 57 \ 84 \ 89 \ 87 \\ 50 \ 33 \ 26 \ 20 \ 11 \ 9 \ 15 \ 20 \ 26 \ 50 \end{array}$$

$$\begin{array}{r} 88 \ 87 \ 84 \ 53 \ 51 \ 46 \ 46 \ 49 \ 87 \ 91 \ 90 \\ 50 \ 32 \ 26 \ 19 \ 11 \ 9 \ 15 \ 23 \ 27 \ 50 \end{array}$$

$$\begin{array}{r} 92 \ 90 \ 45 \ 44 \ 40 \ 42 \ 47 \ 81 \ 87 \ 89 \\ 50 \ 28 \ 19 \ 11 \ 8 \ 15 \ 22 \ 28 \ 50 \end{array}$$

$$\begin{array}{r} 88 \ 87 \ 79 \ 40 \ 39 \ 36 \ 39 \ 42 \ 67 \ 76 \ 79 \ 78 \\ 50 \ 37 \ 25 \ 17 \ 10 \ 8 \ 15 \ 20 \ 24 \ 33 \ 50 \end{array}$$

$$\begin{array}{r} 79 \ 70 \ 56 \ 34 \ 34 \ 32 \ 32 \ 32 \ 51 \ 57 \ 53 \\ 50 \ 34 \ 25 \ 19 \ 11 \ 8 \ 16 \ 20 \ 29 \ 50 \end{array}$$

$$\begin{array}{r} 45 \ 35 \ 33 \ 27 \ 27 \ 25 \ 26 \ 25 \ 32 \ 38 \ 32 \ 19 \ 17 \\ 50 \ 36 \ 23 \ 18 \ 10 \ 8 \ 18 \ 22 \ 25 \ 26 \ 35 \ 50 \end{array}$$

Sta

+

X

-

Elev

909.49

188

981.

+50

98.5 -

189

989.

+50

994.

190

997.

+50

00.2.

191

00.8.

+50

01.3.

192

01.6.

+50

02.0.

193

02.3.

T.P.

4.35

906.67

7.17

902.32.

Lt.

L.

Rt.

$$\frac{115}{50} \frac{115}{36} \frac{106}{26} \frac{114}{18} \frac{115}{10} \frac{114}{8} \frac{113}{16} \frac{110}{24} \frac{102}{29} \frac{89}{36} \frac{88}{50}$$

$$\frac{106}{50} \frac{108}{38} \frac{101}{27} \frac{110}{22} \frac{114}{11} \frac{110}{8} \frac{111}{14} \frac{108}{28} \frac{111}{34} \frac{81}{50} \frac{76}{50}$$

$$\frac{93}{50} \frac{91}{29} \frac{109}{17} \frac{107}{9} \frac{106}{9} \frac{107}{19} \frac{108}{21} \frac{115}{31} \frac{92}{34} \frac{89}{50} \frac{60}{50}$$

$$\frac{78}{50} \frac{74}{34} \frac{65}{24} \frac{101}{18} \frac{103}{9} \frac{101}{9} \frac{103}{19} \frac{100}{29} \frac{86}{36} \frac{40}{50} \frac{37}{50}$$

$$\frac{59}{50} \frac{58}{33} \frac{50}{24} \frac{95}{17} \frac{99}{9} \frac{98}{10} \frac{99}{12} \frac{96}{21} \frac{95}{30} \frac{70}{37} \frac{28}{50} \frac{26}{50}$$

$$\frac{43}{50} \frac{43}{34} \frac{41}{23} \frac{93}{16} \frac{95}{10} \frac{93}{9} \frac{95}{9} \frac{92}{11} \frac{88}{22} \frac{68}{30} \frac{23}{35} \frac{19}{50}$$

$$\frac{34}{50} \frac{35}{32} \frac{33}{24} \frac{86}{17} \frac{89}{10} \frac{87}{10} \frac{89}{12} \frac{86}{20} \frac{83}{30} \frac{62}{37} \frac{21}{50} \frac{21}{50}$$

$$\frac{28}{50} \frac{35}{37} \frac{34}{25} \frac{83}{18} \frac{83}{9} \frac{82}{9} \frac{84}{15} \frac{82}{18} \frac{92}{22} \frac{92}{31} \frac{61}{35} \frac{39}{50} \frac{49}{50}$$

$$\frac{37}{50} \frac{95}{39} \frac{46}{25} \frac{80}{20} \frac{78}{16} \frac{80}{11} \frac{79}{9} \frac{81}{16} \frac{81}{19} \frac{91}{25} \frac{96}{31} \frac{73}{50} \frac{78}{50}$$

$$\frac{36}{50} \frac{51}{38} \frac{51}{24} \frac{73}{18} \frac{76}{10} \frac{75}{10} \frac{77}{17} \frac{77}{21} \frac{87}{29} \frac{89}{35} \frac{110}{50} \frac{130}{50}$$

$$\frac{41}{50} \frac{56}{40} \frac{64}{22} \frac{77}{19} \frac{73}{14} \frac{73}{9} \frac{72}{9} \frac{75}{18} \frac{75}{22} \frac{86}{37} \frac{91}{50} \frac{111}{50}$$

Sta	+	π	-	Elev.
		906.67.		
193	+50			02.4.
194				02.1.
	+50			01.6.
	161	Ent Rt.		01.4.
	165			01.4.
	174			01.2.
	183			01.0.
	192			00.8.
195	195			99.9. 99.0.
	180			99.4.
196				99.2.
I.P.	3.03	902.18.	752	899.15.

Lt

L

Rt

$$\frac{17}{50} \quad \frac{31}{39} \quad \frac{37}{25} \quad \frac{53}{20} \quad \frac{53}{17} \quad \frac{46}{15} \quad \frac{45}{11} \quad \frac{43}{10} \quad \frac{46}{10} \quad \frac{48}{15} \quad \frac{54}{17} \quad \frac{58}{24} \quad \frac{51}{27} \quad \frac{68}{37} \quad \frac{62}{50}$$

$$\frac{20}{50} \quad \frac{31}{39} \quad \frac{33}{25} \quad \frac{57}{20} \quad \frac{57}{17} \quad \frac{49}{15} \quad \frac{47}{10} \quad \frac{46}{10} \quad \frac{49}{10} \quad \frac{49}{15} \quad \frac{58}{18} \quad \frac{60}{24} \quad \frac{41}{29} \quad \frac{24}{38} \quad \frac{25}{50}$$

$$\frac{04}{50} \quad \frac{09}{44} \quad \frac{15}{26} \quad \frac{50}{20} \quad \frac{52}{10} \quad \frac{51}{9} \quad \frac{53}{26} \quad \frac{50}{33} \quad \frac{06}{30} \quad \frac{10}{50}$$

$$\frac{53}{10}$$

$$\frac{54}{10}$$

$$\frac{19}{33} \quad \frac{00}{50}$$

$$\frac{104}{50} \quad \frac{12}{27} \quad \frac{48}{22} \quad \frac{53}{9} \quad \frac{53}{10} \quad \frac{55}{16} \quad \frac{43}{33} \quad \frac{15}{50}$$

$$\frac{24}{50} \quad \frac{45}{21} \quad \frac{54}{8} \quad \frac{55}{10} \quad \frac{57}{10} \quad \frac{44}{24} \quad \frac{08}{33} \quad \frac{00}{43} \quad \frac{120}{50}$$

$$\frac{22}{50} \quad \frac{38}{33} \quad \frac{58}{9} \quad \frac{57}{11} \quad \frac{58}{24} \quad \frac{50}{33} \quad \frac{115}{50} \quad \frac{125}{50}$$

$$\frac{117}{50} \quad \frac{110}{33} \quad \frac{54}{24} \quad \frac{60}{10} \quad \frac{59}{10} \quad \frac{60}{15} \quad \frac{56}{25} \quad \frac{46}{34} \quad \frac{121}{50} \quad \frac{130}{50}$$

$$\frac{146}{50} \quad \frac{139}{35} \quad \frac{70}{21} \quad \frac{68}{10} \quad \frac{68}{10} \quad \frac{70}{18} \quad \frac{66}{20} \quad \frac{53}{25} \quad \frac{50}{35} \quad \frac{139}{50} \quad \frac{147}{50}$$

$$\frac{157}{50} \quad \frac{151}{38} \quad \frac{71}{21} \quad \frac{77}{18} \quad \frac{72}{13} \quad \frac{73}{10} \quad \frac{73}{10} \quad \frac{74}{18} \quad \frac{71}{22} \quad \frac{63}{35} \quad \frac{143}{50} \quad \frac{151}{50}$$

$$\frac{155}{50} \quad \frac{147}{39} \quad \frac{72}{21} \quad \frac{71}{17} \quad \frac{75}{14} \quad \frac{76}{9} \quad \frac{76}{10} \quad \frac{77}{13} \quad \frac{74}{20} \quad \frac{70}{36} \quad \frac{147}{50} \quad \frac{154}{50}$$

Sta. + K - E/cv.

902.18.

196 +30 987'

+67 981.

197 97.6.

+50 96.7.

+80 96.2.

198 95.8.

B.M. 4.33 897.21. 930 892.88 (892.88)

+25 for profile 95.2.

+50 94.5.

+75 93.9.

199 93.3.

+25 92.5.

Lt.

K.

Rt.

$$\begin{array}{cccccccccccccccc} +8.4 & +8.9 & 17 & 34 & 38 & 36 & 37 & 35 & 37 & 33 & 27 & +9.0 & +9.1 \\ \hline 50 & 36 & 24 & 19 & 17 & 15 & 10 & 9 & 13 & 21 & 35 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} +6.2 & +5.3 & 41 & 48 & 44 & 43 & 41 & 43 & 41 & 25 & +5.3 & +5.8 \\ \hline 50 & 35 & 23 & 17 & 15 & 10 & 9 & 19 & 25 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} +2.6 & +2.2 & 50 & 56 & 47 & 48 & 46 & 49 & 49 & +0.9 & +0.8 \\ \hline 50 & 34 & 23 & 19 & 16 & 10 & 9 & 23 & 30 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 55 & 49 & 64 & 65 & 58 & 57 & 55 & 57 & 58 & 62 & 63 & 46 & 46 \\ \hline 50 & 27 & 23 & 19 & 15 & 11 & 10 & 15 & 20 & 23 & 28 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 70 & 88 & 81 & 61 & 64 & 60 & 64 & 67 & 81 & 80 & 65 & 69 & 84 \\ \hline 50 & 35 & 27 & 18 & 10 & 10 & 18 & 21 & 22 & 24 & 35 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 10.7 & 10.3 & 86 & 69 & 66 & 64 & 70 & 85 & 85 & 78 & 98 & 10.4 \\ \hline 50 & 35 & 25 & 17 & 10 & 10 & 18 & 21 & 23 & 26 & 37 & 50 \end{array}$$

5pk. 10 T.P. Rt. 319. 198+88

20

$$\begin{array}{cccccccccccc} 69 & 58 & 31 & 29 & 27 & 27 & 28 & 54 & 61 & 69 \\ \hline 50 & 23 & 17 & 10 & 9 & 17 & 22 & 34 & 50 \end{array}$$

33

$$\begin{array}{cccccccccccc} 79 & 72 & 42 & 40 & 39 & 39 & 44 & 67 & 73 & 74 \\ \hline 50 & 22 & 16 & 9 & 9 & 16 & 22 & 32 & 50 \end{array}$$

47

Sta

+

T

-

Elev.

897.21

199

+50

91.8

+75

91.0

200

90.6

+25

90.6

+50

91.0

+75

91.5

+85 F Line 15" Ent. Culv.

201

91.8

+85 F Line 15" Ent. Culv.

+10

92.0

+45

F Line & Culv.

1-18-39
K. H.
L. B. H.
L. G.
M. J. G.

Lt.

K.

Bt.

$\frac{74}{50} \frac{86}{22} \frac{60}{16} \frac{53}{9} \frac{54}{9} \frac{56}{9} \frac{68}{20} \frac{100}{27} \frac{93}{40} \frac{96}{50}$

62

$\frac{100}{50} \frac{98}{23} \frac{23}{16} \frac{66}{9} \frac{66}{9} \frac{68}{9} \frac{77}{19} \frac{117}{27} \frac{117}{30} \frac{100}{32} \frac{97}{50}$

66

$\frac{99}{50} \frac{101}{22} \frac{74}{18} \frac{62}{10} \frac{62}{9} \frac{62}{9} \frac{73}{18} \frac{97}{22} \frac{114}{24} \frac{114}{26} \frac{93}{30} \frac{93}{50}$

57

$\frac{11.75}{85.46}$

54

$\frac{10.66}{86.55}$

$\frac{97}{50} \frac{86}{21} \frac{56}{15} \frac{54}{8} \frac{52}{9} \frac{56}{9} \frac{57}{15} \frac{91}{24} \frac{110}{26} \frac{111}{28} \frac{89}{30} \frac{87}{50}$

$\frac{11.15}{8606}$

$\frac{11.3}{85.91}$

203 + 120 + 40

Sta.	+	π	-	Elev.
		897.21		
201	+50			92.1
202				92.3
	+50			92.3
203				92.4
	+20	F. Line S. End 20' Ent. Culv.		
	+40	F. Line N. End Ent. Culv.		
	+50			92.3
204				92.2
T.P.	5.28	897.50	4.99	892.22
	+50			92.2
205				92.1
	+50			92.2

Lt

L

Rt

$$\begin{array}{r} 91 \ 91 \ 83 \ 50 \ 52 \\ 50 \ 26 \ 20 \ 14 \ 9 \end{array} \quad \begin{array}{r} 51 \ 52 \ 58 \ 84 \ 111 \\ 9 \ 16 \ 22 \ 24 \ 27 \end{array} \quad \begin{array}{r} 112 \ 91 \ 80 \ 90 \ 87 \\ 27 \ 29 \ 31 \ 37 \ 50 \end{array}$$

$$\begin{array}{r} 96 \ 94 \ 54 \ 50 \ 49 \\ 50 \ 20 \ 15 \ 9 \ 7 \end{array} \quad \begin{array}{r} 51 \ 58 \ 95 \ 113 \ 113 \\ 10 \ 16 \ 23 \ 24 \ 27 \end{array} \quad \begin{array}{r} 95 \ 85 \ 90 \\ 29 \ 32 \ 50 \end{array}$$

$$\begin{array}{r} 99 \ 99 \ 93 \ 55 \\ 50 \ 39 \ 21 \ 14 \end{array} \quad \begin{array}{r} 50 \\ 7 \end{array} \quad \begin{array}{r} 49 \ 52 \ 87 \ 89 \ 117 \ 117 \ 90 \ 91 \ 89 \\ 11 \ 16 \ 22 \ 25 \ 27 \ 29 \ 35 \ 50 \end{array}$$

$$\begin{array}{r} 100 \ 93 \ 63 \ 53 \ 48 \\ 50 \ 21 \ 17 \ 8 \end{array} \quad \begin{array}{r} 51 \ 55 \ 92 \ 113 \ 113 \\ 12 \ 16 \ 23 \ 25 \ 28 \end{array} \quad \begin{array}{r} 92 \ 84 \ 89 \ 89 \\ 29 \ 31 \ 35 \ 50 \end{array}$$

$$\begin{array}{r} 115 \\ 8606. \end{array}$$

$$\begin{array}{r} 115 \\ 8606. \end{array}$$

$$\begin{array}{r} 101 \ 99 \ 56 \ 52 \\ 50 \ 21 \ 16 \ 9 \end{array}$$

$$\begin{array}{r} 49 \ 51 \ 55 \ 84 \ 112 \ 112 \ 88 \ 92 \ 90 \\ 13 \ 16 \ 22 \ 25 \ 29 \ 30 \ 36 \ 50 \end{array}$$

$$\begin{array}{r} 102 \ 98 \ 59 \ 53 \ 50 \\ 50 \ 21 \ 15 \ 9 \end{array} \quad \begin{array}{r} 53 \\ 11 \end{array} \quad \begin{array}{r} 55 \ 86 \ 112 \ 112 \ 89 \ 89 \ 89 \\ 16 \ 23 \ 27 \ 29 \ 30 \ 36 \ 50 \end{array}$$

$$\begin{array}{r} 103 \ 98 \ 88 \ 60 \ 56 \ 53 \ 58 \ 62 \ 93 \ 114 \ 114 \ 88 \ 93 \ 92 \\ 50 \ 23 \ 19 \ 14 \ 8 \end{array} \quad \begin{array}{r} 12 \ 16 \ 24 \ 26 \ 30 \ 32 \ 37 \ 50 \end{array}$$

$$\begin{array}{r} 103 \ 102 \ 92 \ 65 \ 56 \\ 50 \ 23 \ 20 \ 16 \ 8 \end{array} \quad \begin{array}{r} 54 \ 56 \ 58 \ 80 \ 115 \ 115 \ 88 \ 91 \ 88 \\ 11 \ 16 \ 23 \ 25 \ 27 \ 32 \ 38 \ 50 \end{array}$$

$$\begin{array}{r} 104 \ 96 \ 84 \ 59 \ 55 \ 53 \\ 50 \ 22 \ 20 \ 15 \ 8 \end{array} \quad \begin{array}{r} 56 \ 57 \ 87 \ 114 \ 114 \ 92 \ 89 \ 86 \\ 11 \ 16 \ 25 \ 27 \ 29 \ 31 \ 37 \ 50 \end{array}$$

Sta

+

T

-

Elev.

897.50.

206

92.4.

+50

92.5.

207

92.4.

+50

91.9.

208

91.2.

209

+50

91.5.

T.P.

4.97

896.90.

5.57

891.93.

+80

91.9

91.9.

209

91.9

2

+42

91.9.

+85

91.9.

+92

91.9.

14

4

24

$$\frac{99}{50} \frac{87}{24} \frac{78}{19} \frac{56}{16}$$

$$\frac{53}{7}$$

$$\frac{51}{10} \frac{54}{16} \frac{66}{19} \frac{76}{24} \frac{113}{28} \frac{113}{30} \frac{81}{33} \frac{87}{38} \frac{83}{50}$$

$$\frac{91}{50} \frac{90}{31} \frac{83}{20} \frac{64}{16} \frac{53}{8} \frac{50}{11} \frac{54}{16} \frac{53}{20} \frac{71}{25} \frac{78}{27} \frac{90}{28} \frac{115}{30} \frac{115}{32} \frac{89}{36} \frac{89}{40} \frac{96}{50}$$

$$\frac{88}{50} \frac{86}{29} \frac{84}{22} \frac{54}{16}$$

$$\frac{54}{9}$$

$$\frac{51}{11} \frac{55}{16} \frac{57}{21} \frac{76}{25} \frac{78}{28} \frac{91}{30} \frac{112}{33} \frac{112}{35} \frac{90}{50}$$

$$\frac{85}{50} \frac{85}{21} \frac{61}{17} \frac{59}{9} \frac{56}{8}$$

$$\frac{59}{11}$$

$$\frac{64}{20} \frac{78}{22} \frac{90}{25} \frac{116}{28} \frac{116}{32} \frac{89}{35} \frac{91}{50}$$

$$\frac{85}{50} \frac{83}{22} \frac{70}{18}$$

$$\frac{65}{8}$$

$$\frac{63}{11} \frac{66}{17} \frac{68}{22} \frac{85}{25} \frac{87}{28} \frac{117}{32} \frac{117}{36} \frac{84}{43} \frac{91}{50}$$

$$\frac{81}{50} \frac{82}{36} \frac{84}{20} \frac{64}{16} \frac{60}{8} \frac{60}{13} \frac{64}{20} \frac{67}{22} \frac{75}{25} \frac{80}{28} \frac{91}{30} \frac{111}{33} \frac{111}{36} \frac{84}{43} \frac{86}{50}$$

F. Line 2466m

$$\frac{83}{50} \frac{78}{21} \frac{59}{17}$$

$$\frac{52}{8}$$

$$\frac{50}{20} \frac{59}{26} \frac{62}{29} \frac{80}{30} \frac{105}{31} \frac{105}{36} \frac{107}{39} \frac{81}{50}$$

$$\frac{76}{50} \frac{82}{22} \frac{75}{20} \frac{48}{17} \frac{52}{9} \frac{50}{8}$$

$$\frac{52}{10} \frac{62}{26} \frac{64}{33} \frac{73}{38} \frac{103}{40} \frac{103}{42} \frac{79}{44} \frac{77}{50}$$

$$\frac{78}{50} \frac{80}{38} \frac{80}{22} \frac{75}{19} \frac{63}{17}$$

$$\frac{53}{8}$$

$$\frac{50}{10} \frac{52}{20} \frac{57}{27} \frac{63}{50}$$

$$\frac{77}{50} \frac{76}{31} \frac{72}{17} \frac{58}{12} \frac{53}{8} \frac{50}{8}$$

$$\frac{51}{10}$$

$$\frac{56}{18} \frac{62}{22} \frac{60}{50}$$

F. Line 2466m

$$\frac{77}{50} \frac{76}{33} \frac{74}{18} \frac{64}{16} \frac{59}{12} \frac{54}{7}$$

$$\frac{50}{11} \frac{52}{17} \frac{57}{23} \frac{64}{29} \frac{71}{31} \frac{103}{33} \frac{104}{36} \frac{80}{40} \frac{63}{40} \frac{61}{50}$$

Sta

+

K

-

Elev.

896.90

210

91.9

+43

92.2

175

92.5

185

92.6

211 +01.5

926

B.M.

467

892.23

892.25

Lt.

K.

Rt.

$\frac{78}{50}$ $\frac{77}{35}$ $\frac{75}{19}$ $\frac{62}{16}$ $\frac{54}{8}$ $\frac{50}{-}$ $\frac{53}{13}$ $\frac{58}{18}$ $\frac{76}{29}$ $\frac{103}{32}$ $\frac{103}{34}$ $\frac{82}{36}$ $\frac{64}{40}$ $\frac{61}{50}$

$\frac{73}{50}$ $\frac{72}{20}$ $\frac{57}{15}$ $\frac{51}{9}$ $\frac{47}{-}$ $\frac{50}{12}$ $\frac{55}{18}$ $\frac{60}{28}$ $\frac{81}{31}$ $\frac{102}{33}$ $\frac{102}{35}$ $\frac{82}{37}$ $\frac{61}{40}$ $\frac{61}{50}$

$\frac{55}{50}$ $\frac{56}{27}$ $\frac{58}{18}$ $\frac{52}{14}$ $\frac{48}{9}$ $\frac{44}{-}$ $\frac{47}{18}$ $\frac{55}{28}$ $\frac{83}{32}$ $\frac{99}{34}$ $\frac{100}{35}$ $\frac{99}{36}$ $\frac{81}{37}$ $\frac{59}{41}$ $\frac{56}{50}$

$\frac{47}{50}$ $\frac{51}{29}$ $\frac{54}{20}$ $\frac{48}{16}$ $\frac{45}{9}$ $\frac{43}{-}$ $\frac{44}{12}$ $\frac{47}{23}$ $\frac{51}{35}$ $\frac{54}{50}$

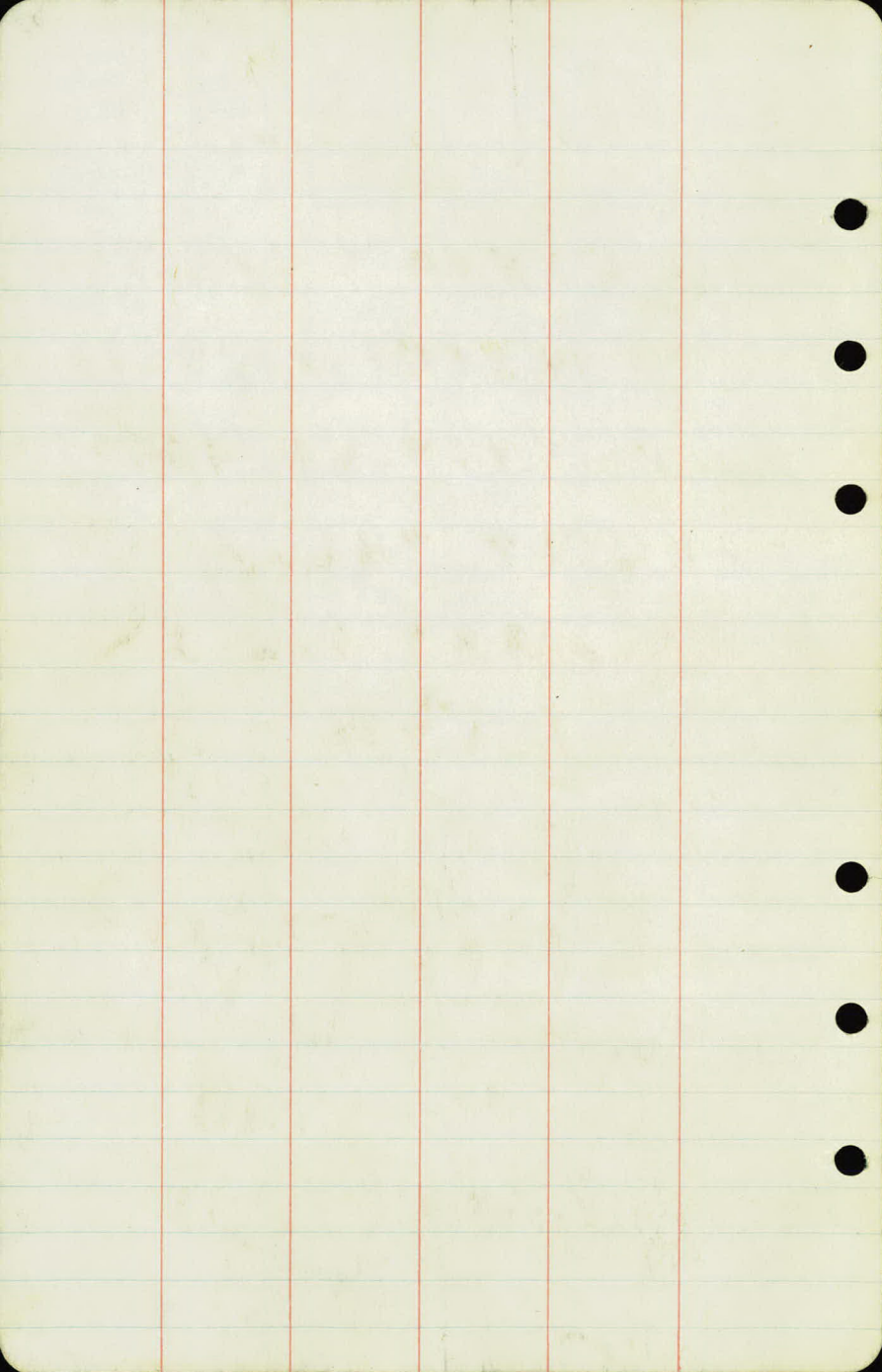
$\frac{37}{50}$ $\frac{42}{28}$ $\frac{44}{12}$ $\frac{41}{-}$ $\frac{42}{11}$ $\frac{44}{25}$ $\frac{45}{50}$

1007

Flinch End 24" Culv.

8683

Folk in T.P.L.A. 2/10/68



Cross Sections

HAW 8-541
1M
LG

Sta	+	π	-	Elev
B.M.	5.49	897.77.		892.28
211+01.50			5.2	92.6
+15			5.1	92.7
+25			5.1	92.7
+30			5.1	92.7
+33			5.1	92.7
+36			5.0	92.8
+58	Top W. Conduit		5.0	92.8
+61			4.9	92.9
212			4.8	93.0
+50			4.8	93.0
213			5.0	92.8
+50			4.8	93.0

LT

L

RT

SpK in T.P. 28' Lt Sta 210+68
 $\frac{4.7}{50}$ $\frac{5.4}{26}$ $\frac{5.3}{11}$ 5.2 $\frac{5.3}{19}$ $\frac{5.5}{50}$

$\frac{4.1}{50}$ $\frac{4.7}{33}$ $\frac{6.0}{27}$ $\frac{6.1}{23-20}$ $\frac{5.5}{18}$ 5.1 $\frac{5.2}{17}$ $\frac{5.9}{35}$ $\frac{6.0}{50}$

$\frac{3.5}{50}$ $\frac{4.2}{31}$ $\frac{6.7}{23-19}$ $\frac{5.1}{17}$ $\frac{5.2}{12}$ 5.1 $\frac{5.1}{13}$ $\frac{6.3}{27}$ $\frac{6.6}{35}$ $\frac{8.1}{42}$ $\frac{8.2}{50}$

$\frac{3.4}{50}$ $\frac{3.7}{31}$ $\frac{6.7}{27-20}$ $\frac{5.3}{16}$ $\frac{5.2}{11}$ 5.1 $\frac{5.2}{15}$ $\frac{6.2}{23}$ $\frac{6.5}{31}$ $\frac{10.6}{35}$ $\frac{10.6}{50}$

$\frac{3.4}{50}$ $\frac{3.7}{31}$ $\frac{6.7}{27-20}$ $\frac{5.3}{16}$ $\frac{5.2}{11}$ 5.1 $\frac{5.2}{15}$ $\frac{6.2}{23}$ $\frac{6.5}{31}$ $\frac{10.6}{35}$ $\frac{10.6}{50}$

$\frac{3.2}{50}$ $\frac{3.4}{32}$ $\frac{6.4}{27}$ $\frac{6.6}{19}$ $\frac{5.4}{17}$ $\frac{5.3}{10}$ 5.0 $\frac{5.3}{16}$ $\frac{6.0}{21}$ $\frac{5.8}{27}$ $\frac{6.6}{34}$ $\frac{8.2}{50}$

$\frac{3.0}{50}$ $\frac{3.4}{31}$ $\frac{6.8}{26-19}$ $\frac{5.4}{17}$ $\frac{5.2}{10}$ 5.0 $\frac{5.1}{12}$ $\frac{5.6}{19}$ $\frac{5.7}{27}$ $\frac{7.0}{30-32}$ $\frac{6.0}{33}$ $\frac{5.2}{50}$

$\frac{3.0}{50}$ $\frac{3.5}{31}$ $\frac{6.8}{25-19}$ $\frac{5.1}{17}$ $\frac{5.2}{12}$ 4.9 $\frac{5.2}{16}$ $\frac{5.7}{27}$ $\frac{6.2}{34}$ $\frac{7.5}{50}$

$\frac{2.5}{50}$ $\frac{2.5}{33}$ $\frac{2.0}{31}$ $\frac{6.2}{25}$ $\frac{6.6}{19}$ $\frac{5.0}{18}$ 4.8 $\frac{5.1}{17}$ $\frac{5.2}{27}$ $\frac{8.2}{34}$ $\frac{8.0}{50}$

$\frac{2.1}{50}$ $\frac{2.6}{33}$ $\frac{6.5}{27}$ $\frac{7.0}{20}$ $\frac{5.3}{17}$ 4.8 $\frac{4.9}{18}$ $\frac{5.6}{23}$ $\frac{7.6}{34}$ $\frac{8.1}{50}$

$\frac{2.9}{50}$ $\frac{4.1}{33}$ $\frac{7.0}{27}$ $\frac{7.2}{20}$ $\frac{5.3}{15}$ 5.0 $\frac{5.3}{19}$ $\frac{6.1}{26}$ $\frac{7.3}{32}$ $\frac{7.7}{34}$ $\frac{7.4}{50}$

$\frac{4.3}{50}$ $\frac{4.8}{33}$ $\frac{6.7}{27}$ $\frac{6.9}{20}$ $\frac{5.0}{16}$ 4.8 $\frac{5.0}{17}$ $\frac{5.4}{22}$ $\frac{6.8}{32}$ $\frac{8.3}{34}$ $\frac{7.7}{50}$

Sta	+	π	-	Elev
		897.77		
214			4.2	93.5
+56			3.4	94.4
T.P.	12.90	908.19	2.48	895.29
+80			13.4	94.8
215			13.1	95.1
+50			12.4	95.8
216			11.7	96.5
+50			10.8	97.4
217			9.7	98.5
+50			8.8	99.4
T.P.	11.47	911.51	8.15	900.04
217				98.5
+50				99.4
218			11.4	00.1

ht

z

ht

$$\frac{4.6}{50} \frac{5.0}{33} \frac{6.6}{28} \frac{6.3}{21} \frac{4.3}{17} \frac{4.4}{11} 4.2 \frac{4.4}{15} \frac{5.3}{27} \frac{7.5}{34} \frac{7.7}{50}$$

$$\frac{3.0}{50} \frac{3.1}{33} \frac{5.2}{27} \frac{5.3}{20} \frac{3.8}{17} \frac{3.6}{11} 3.4 \frac{3.7}{17} \frac{5.6}{23} \frac{5.4}{33} \frac{5.4}{50} 6.0$$

$$\frac{9.7}{75} \frac{10.4}{50} \frac{10.6}{33} \frac{14.7}{23-19} \frac{13.6}{14} 13.4 \frac{13.6}{15} \frac{15.2}{21} \frac{15.7}{33} \frac{14.3}{38} \frac{13.4}{43} \frac{14.0}{50} \frac{15.1}{75}$$

$$\frac{8.7}{75} \frac{9.4}{50} \frac{8.7}{34} \frac{14.3}{25-17} \frac{13.4}{17} 13.1 \frac{13.4}{17} \frac{15.0}{20} \frac{15.0}{32} \frac{12.4}{41} \frac{12.1}{50} \frac{13.7}{75}$$

$$\frac{5.3}{75} \frac{5.4}{43} \frac{4.6}{35} \frac{13.7}{23} \frac{13.7}{18} \frac{12.5}{13} 12.4 \frac{12.7}{16} \frac{14.3}{20} \frac{14.5}{32} \frac{12.3}{43} \frac{8.4}{52} \frac{9.2}{75}$$

$$\frac{2.8}{75} \frac{2.6}{50} \frac{1.6}{42} \frac{12.8}{27} \frac{13.2}{20} \frac{12.0}{18} 11.7 \frac{12.0}{15} \frac{13.5}{20} \frac{13.6}{35} \frac{12.2}{42} \frac{8.8}{50} \frac{8.5}{75}$$

$$\frac{1.7}{75} \frac{1.7}{50} \frac{10.2}{38} \frac{12.4}{29} \frac{12.2}{19} \frac{11.2}{14} 10.8 \frac{11.0}{16} \frac{12.5}{22} \frac{12.6}{32} \frac{11.8}{37} \frac{7.2}{48} \frac{8.9}{75}$$

$$\frac{7.8}{39} \frac{10.9}{31} \frac{11.7}{24} \frac{11.2}{19} \frac{10.0}{15} 9.7 \frac{9.9}{14} \frac{11.2}{20} \frac{11.5}{30} \frac{10.6}{33} \frac{8.7}{42} \frac{5.2}{50} \frac{7.2}{75}$$

$$\frac{8.9}{29} \frac{10.4}{23} \frac{10.4}{18} \frac{9.0}{15} 8.8 \frac{9.1}{15} \frac{10.0}{19} \frac{10.4}{28} \frac{9.1}{34} \frac{5.9}{45} \frac{4.0}{47} \frac{4.1}{50} \frac{5.9}{75}$$

$$\frac{4.1}{75} \frac{3.8}{57} \frac{3.0}{50} (13.0)$$

$$\frac{5.3}{75} \frac{4.0}{47} \frac{3.2}{40} (11.5)$$

$$\frac{6.9}{75} \frac{5.3}{43} \frac{4.1}{34} \frac{11.1}{26} \frac{12.8}{22-18} \frac{11.6}{14} 11.4 \frac{11.7}{14} \frac{12.8}{20} \frac{13.0}{27} \frac{11.9}{35} \frac{7.3}{42} \frac{8.4}{59} \frac{9.6}{75}$$

Sta	+	Σ	-	Elev
		911.51.		
218+50			10.8	00.7
219			10.4	01.1
+50			10.3	01.2
220			10.4	01.1
+50			10.5	01.0
221			10.8	00.7
T.P.	3.57	904.38.	10.70	900.81. 90
B.M	2.19	904.07.	2.50	901.88. 901.88.
+50			3.8	00.3
222			4.3	99.8
+50			4.4	99.7
223			4.5	99.6
+50			5.0	99.1
T.P.	9.50	908.38.	5.19	898.88.
224			9.6	98.8

A

2

Rt.

$\frac{9.0}{75}$ $\frac{7.1}{41}$ $\frac{6.1}{32}$ $\frac{12.4}{23}$ $\frac{12.4}{18}$ $\frac{11.2}{14}$ 10.8 $\frac{11.0}{14}$ $\frac{12.5}{20}$ $\frac{12.5}{26}$ $\frac{0.8}{35}$ $\frac{6.4}{43}$ $\frac{6.7}{54}$ $\frac{8.4}{75}$

$\frac{10.4}{75}$ $\frac{9.7}{59}$ $\frac{9.2}{43}$ $\frac{8.3}{32}$ $\frac{12.1}{24}$ $\frac{10.8}{19}$ $\frac{10.4}{13}$ $\frac{10.6}{14}$ $\frac{12.6}{20}$ $\frac{12.0}{27}$ $\frac{10.5}{35}$ $\frac{6.3}{43}$ $\frac{7.1}{75}$

$\frac{13.0}{75}$ $\frac{11.0}{49}$ $\frac{10.5}{32}$ $\frac{12.4}{29}$ $\frac{12.5}{19}$ $\frac{10.7}{14}$ 10.3 $\frac{10.6}{14}$ $\frac{11.9}{20}$ $\frac{11.9}{27}$ $\frac{10.8}{32}$ $\frac{10.2}{35}$ $\frac{6.1}{44}$ $\frac{6.4}{75}$

$\frac{11.5}{75}$ $\frac{11.8}{55}$ $\frac{11.0}{32}$ $\frac{12.8}{29}$ $\frac{12.7}{20}$ $\frac{10.8}{16}$ 10.4 $\frac{10.6}{14}$ $\frac{12.0}{20}$ $\frac{12.0}{29}$ $\frac{11.8}{35}$ $\frac{8.2}{42}$ $\frac{7.4}{53}$ $\frac{7.7}{75}$

$\frac{10.9}{75}$ $\frac{10.9}{52}$ $\frac{10.8}{33}$ $\frac{13.1}{27}$ $\frac{12.6}{19}$ $\frac{10.9}{13}$ 10.5 $\frac{10.8}{14}$ $\frac{12.0}{20}$ $\frac{12.5}{32}$ $\frac{13.1}{39}$ $\frac{12.5}{55}$ $\frac{10.3}{75}$

$\frac{9.5}{75}$ $\frac{10.1}{50}$ $\frac{10.2}{33}$ $\frac{12.7}{28}$ $\frac{12.4}{19}$ $\frac{11.2}{14}$ 10.8 $\frac{11.0}{14}$ $\frac{11.7}{17}$ $\frac{12.0}{30}$ $\frac{12.9}{34}$ $\frac{13.7}{52}$ $\frac{13.2}{75}$

Spk in 15" Oak 100' Rt 54g 223 100

$\frac{1.8}{75}$ $\frac{2.8}{53}$ $\frac{3.1}{31}$ $\frac{5.7}{25}$ $\frac{4.2}{20}$ $\frac{4.0}{17}$ $\frac{4.0}{13}$ 3.8 $\frac{4.0}{14}$ $\frac{4.7}{25}$ $\frac{6.4}{31}$ $\frac{7.3}{33}$ $\frac{7.0}{55}$ $\frac{5.7}{75}$

$\frac{3.0}{75}$ $\frac{3.6}{54}$ $\frac{3.9}{36}$ $\frac{3.5}{30}$ $\frac{6.2}{25}$ $\frac{4.7}{21}$ $\frac{4.5}{17}$ 4.3 $\frac{4.4}{14}$ $\frac{5.5}{21}$ $\frac{7.0}{27}$ $\frac{8.0}{31}$ $\frac{8.4}{33}$ $\frac{9.4}{45}$ $\frac{8.1}{55}$ $\frac{6.9}{75}$

$\frac{3.3}{75}$ $\frac{3.5}{33}$ $\frac{3.3}{33}$ $\frac{5.9}{26}$ $\frac{5.3}{16}$ $\frac{4.6}{21}$ 4.4 $\frac{4.5}{15}$ $\frac{4.8}{17}$ $\frac{5.9}{25}$ $\frac{6.9}{31}$ $\frac{7.3}{33}$ $\frac{7.0}{54}$ $\frac{5.9}{75}$

$\frac{4.3}{75}$ $\frac{4.3}{53}$ $\frac{4.2}{33}$ $\frac{6.3}{26}$ $\frac{6.1}{19}$ $\frac{4.9}{17}$ $\frac{4.7}{11}$ 4.5 $\frac{4.6}{14}$ $\frac{6.4}{21}$ $\frac{6.5}{26}$ $\frac{6.0}{31}$ $\frac{5.7}{33}$ $\frac{5.3}{55}$ $\frac{3.8}{75}$

$\frac{8.0}{75}$ $\frac{7.4}{51}$ $\frac{6.7}{32}$ $\frac{6.5}{19}$ $\frac{5.4}{17}$ $\frac{5.1}{12}$ 5.0 $\frac{5.0}{16}$ $\frac{6.3}{20}$ $\frac{5.6}{23}$ $\frac{5.7}{30}$ $\frac{3.0}{33}$ $\frac{1.5}{55}$ $\frac{0.3}{75}$

$\frac{15.6}{75}$ $\frac{15.6}{57}$ $\frac{13.1}{39}$ $\frac{12.1}{24}$ $\frac{10.3}{16}$ $\frac{9.8}{11}$ 9.6 $\frac{9.7}{12}$ $\frac{9.9}{17}$ $\frac{10.8}{20}$ $\frac{9.9}{28}$ $\frac{7.8}{34}$ $\frac{5.7}{38}$ $\frac{4.1}{60}$ $\frac{2.8}{75}$

Sta	+	π	-	Elev
		908.38.		
224+50			9.9	98.5
225			10.3	98.1
+22			10.5	97.9
+50			10.8	97.6
226			11.4	98.0
T.P.	3.39	900.51.	11.26	897.12
+50			4.3	96.2
+75			4.7	95.8
227			5.2	95.3
+50			5.9	94.6
228			6.2	94.3
+50			6.2	94.3
229			6.2	94.3
T.P.	6.81	900.94.	6.38	894.13.

LT

X

RT

15.8 15.4 14.4 13.5 12.1 10.1 10.0 11.3 11.0 5.4 4.9 4.0
 75 58 39 31 21 11 99 14 19 27 37 62 75

15.4 13.6 12.1 11.8 12.5 12.4 10.6 10.5 12.0 12.0 9.1 4.3 4.5 3.7
 75 50 36 31 29 20 14 10.3 14 20 26 31 40 60 75

15.4 12.6 11.6 12.7 12.6 10.7 10.7 12.3 12.2 9.8 3.5 4.1 3.8
 75 43 33 30 21 13 10.5 15 20 27 32 41 58 75

15.3 13.5 11.6 13.0 12.8 12.2 11.1 11.0 12.5 12.4 9.7 3.7 4.1 4.0
 75 52 33 29 20 17 13 10.8 15 20 27 33 42 59 75

14.7 13.4 12.6 13.5 13.1 12.2 11.6 11.7 12.9 13.1 5.7 6.7 6.9
 57 40 34 31 21 17 13 11.4 14 18 27 41 55 75
 16.5
 75

9.0 9.0 7.4 6.5 5.3 4.5 4.6 5.3 6.1 6.0 2.4 1.8 2.4
 75 61 37 28 16 13 43 14 19 20 26 35 43 57

9.2 9.0 8.6 7.8 7.2 5.2 5.2 6.5 6.6 4.3 4.6 4.9 5.3
 75 63 44 32 24 16 47 16 19 27 30 34 54 75

9.2 9.2 8.9 8.4 7.6 6.0 5.4 5.5 6.7 7.0 5.4 6.3 7.4 7.4
 75 50 32 29 22 18 13 5.2 14 18 27 29 34 60 75

8.0 8.2 8.6 9.0 8.3 6.3 5.9 6.0 6.6 7.5 7.6 8.1 7.9 7.7
 75 41 30 29 21 16 5.9 13 17 21 30 33 47 60 75

8.4 8.4 8.1 8.3 7.7 6.5 6.5 6.4 7.6 7.6 6.4 7.9 8.1
 75 55 44 28 21 19 14 6.2 14 19 23 26 33 50-75

8.8 8.8 8.4 8.0 6.4 6.4 6.2 6.2 6.5 7.9 7.2 7.5 7.9 7.9
 75 50 30 22 17 13 6.2 13 17 19 30 33 48 75

9.2 8.6 8.3 8.5 6.6 6.4 6.2 6.3 7.8 7.0 7.7 7.9 7.7 8.3
 75 44 28 22 18 13 6.2 15 21 28 31 33 57 75

Sta	+	A	-	Elev
		900.94		
229+50			6.6	94.3
230			6.7	94.2
+50			6.7	94.2
231			6.2	94.7
+50			5.4	95.5
+74			5.2	95.7
+76			5.2	95.7
232			5.0	95.9
+40			4.9	96.0
+70			5.0	95.9
233			5.1	95.8
+50			5.0	95.9

LT

Z

RT

$$\frac{9.0}{75} \frac{9.1}{47} \frac{9.1}{33} \frac{8.4}{22} \frac{7.1}{17} \frac{6.9}{12} 6.6 \frac{6.7}{16} \frac{7.8}{19} \frac{8.3}{26} \frac{6.9}{29} \frac{7.8}{33} \frac{8.3}{50} \frac{8.8}{75}$$

$$\frac{8.7}{75} \frac{8.7}{47} \frac{8.8}{33} \frac{8.3}{25} \frac{7.9}{19} \frac{7.1}{17} 6.7 \frac{7.1}{18} \frac{8.2}{19} \frac{8.0}{26} \frac{7.2}{31} \frac{8.5}{34} \frac{8.7}{60} \frac{8.4}{75}$$

$$\frac{8.5}{75} \frac{8.5}{40} \frac{8.5}{28} \frac{7.7}{19} \frac{7.2}{13} 6.7 \frac{6.8}{15} \frac{7.9}{19} \frac{8.0}{31} \frac{7.6}{34} \frac{8.3}{36} \frac{8.6}{56} \frac{8.6}{75}$$

$$\frac{8.8}{29} \frac{8.3}{22} \frac{6.7}{18} \frac{6.5}{13} 6.2 \frac{6.3}{16} \frac{7.5}{19} \frac{7.6}{31} \frac{7.0}{31} \frac{8.1}{35} \frac{8.0}{52} \frac{7.4}{75}$$

$$\frac{6.2}{75} \frac{5.5}{30} \frac{5.3}{28} \frac{5.8}{23} \frac{5.4}{11} 5.4 \frac{5.5}{13} \frac{6.0}{21} \frac{6.5}{26} \frac{6.5}{31} \frac{3.9}{37} \frac{2.4}{75}$$

$$\frac{4.8}{75} \frac{4.4}{62} \frac{5.1}{59} \frac{5.2}{41} \frac{5.7}{23} \frac{5.2}{13} 5.2 \frac{5.3}{12} \frac{5.0}{23} \frac{4.2}{40} \frac{1.9}{65} \frac{1.0}{75}$$

$$\frac{4.3}{75} \frac{4.7}{50} \frac{3.4}{47} \frac{3.3}{37} \frac{5.0}{32} \frac{5.7}{23} \frac{5.3}{11} 5.2 \frac{5.3}{12} \frac{5.0}{23} \frac{4.2}{40} \frac{1.9}{65} \frac{1.0}{75}$$

$$\frac{2.5}{75} \frac{2.5}{33} \frac{6.3}{25} \frac{6.5}{19} \frac{5.3}{17} 5.0 \frac{5.3}{16} \frac{6.4}{20} \frac{6.2}{31} \frac{5.0}{32} \frac{3.5}{39} \frac{0.5}{75}$$

$$\frac{4.9}{75} \frac{6.4}{64} \frac{6.5}{50} \frac{6.7}{28} \frac{6.4}{19} \frac{5.2}{16} 4.9 \frac{5.2}{17} \frac{6.7}{20} \frac{6.4}{32} \frac{4.4}{36} \frac{3.2}{55} \frac{1.6}{75}$$

$$\frac{7.2}{75} \frac{7.6}{50} \frac{7.4}{27} \frac{7.0}{17} \frac{5.6}{15} 5.0 \frac{5.0}{14} \frac{5.6}{20} \frac{6.0}{23} \frac{6.8}{34} \frac{6.3}{40} \frac{2.5}{75}$$

$$\frac{7.7}{75} \frac{7.7}{53} \frac{7.3}{24} \frac{6.4}{16} \frac{5.4}{15} 5.1 \frac{5.0}{15} \frac{6.3}{23} \frac{5.8}{27} \frac{6.7}{30} \frac{7.2}{38} \frac{6.6}{51} \frac{4.8}{61} \frac{3.1}{75}$$

$$\frac{7.3}{75} \frac{7.8}{53} \frac{7.5}{25} \frac{7.0}{18} \frac{5.3}{14} 5.0 \frac{5.0}{15} \frac{6.3}{21} \frac{6.2}{24} \frac{5.6}{27} \frac{6.2}{29} \frac{7.0}{45} \frac{4.9}{75}$$

Sta	+	π	-	E/kV
		900.94.		

234			4.7	96.2
-----	--	--	-----	------

+50			4.6	96.3
-----	--	--	-----	------

T.P.	5.68	901.89.	4.73	896.21.
------	------	---------	------	---------

235			5.8	96.1
-----	--	--	-----	------

+50			5.8	96.1
-----	--	--	-----	------

236			5.5	96.4
-----	--	--	-----	------

+50			4.8	97.1
-----	--	--	-----	------

237			3.8	98.1
-----	--	--	-----	------

B.M.	5.55	904.67.	2.77	899.12, 899.12
------	------	---------	------	----------------

+38			5.7	99.0
-----	--	--	-----	------

+50			5.6	99.1
-----	--	--	-----	------

238			5.0	99.7
-----	--	--	-----	------

+50			4.2	00.5
-----	--	--	-----	------

239			4.3	00.4
-----	--	--	-----	------

B.M.			5.55	899.12.
------	--	--	------	---------

Lt

L

Rt

$$\frac{7.1}{75} \frac{4.5}{61} \frac{7.8}{42} \frac{7.3}{25} \frac{6.2}{18} \frac{4.9}{15} 47 \frac{4.9}{15} \frac{5.9}{20-25} \frac{5.5}{28} \frac{6.7}{32} \frac{6.1}{58} \frac{5.0}{75}$$

$$\frac{7.5}{75} \frac{7.7}{50} \frac{7.0}{19} \frac{5.1}{14} \quad 46 \frac{5.0}{16} \frac{6.2}{20} \frac{6.2}{24} \frac{5.5}{28} \frac{6.9}{30} \frac{6.9}{47} \frac{6.3}{75}$$

$$\frac{8.0}{75} \frac{8.0}{43} \frac{8.2}{24} \frac{7.4}{17} \frac{6.1}{12} 58 \frac{6.1}{15} \frac{6.8}{21} \frac{6.6}{28} \frac{6.7}{30} \frac{7.1}{35} \frac{7.8}{56} \frac{7.3}{75}$$

$$\frac{8.2}{75} \frac{8.4}{47} \frac{8.4}{27} \frac{8.2}{23} \frac{7.7}{19} \frac{6.4}{16} 5.8 \frac{5.8}{15} \frac{6.8}{22} \frac{7.4}{25} \frac{6.4}{29} \frac{7.7}{35} \frac{7.9}{50} \frac{6.2}{75}$$

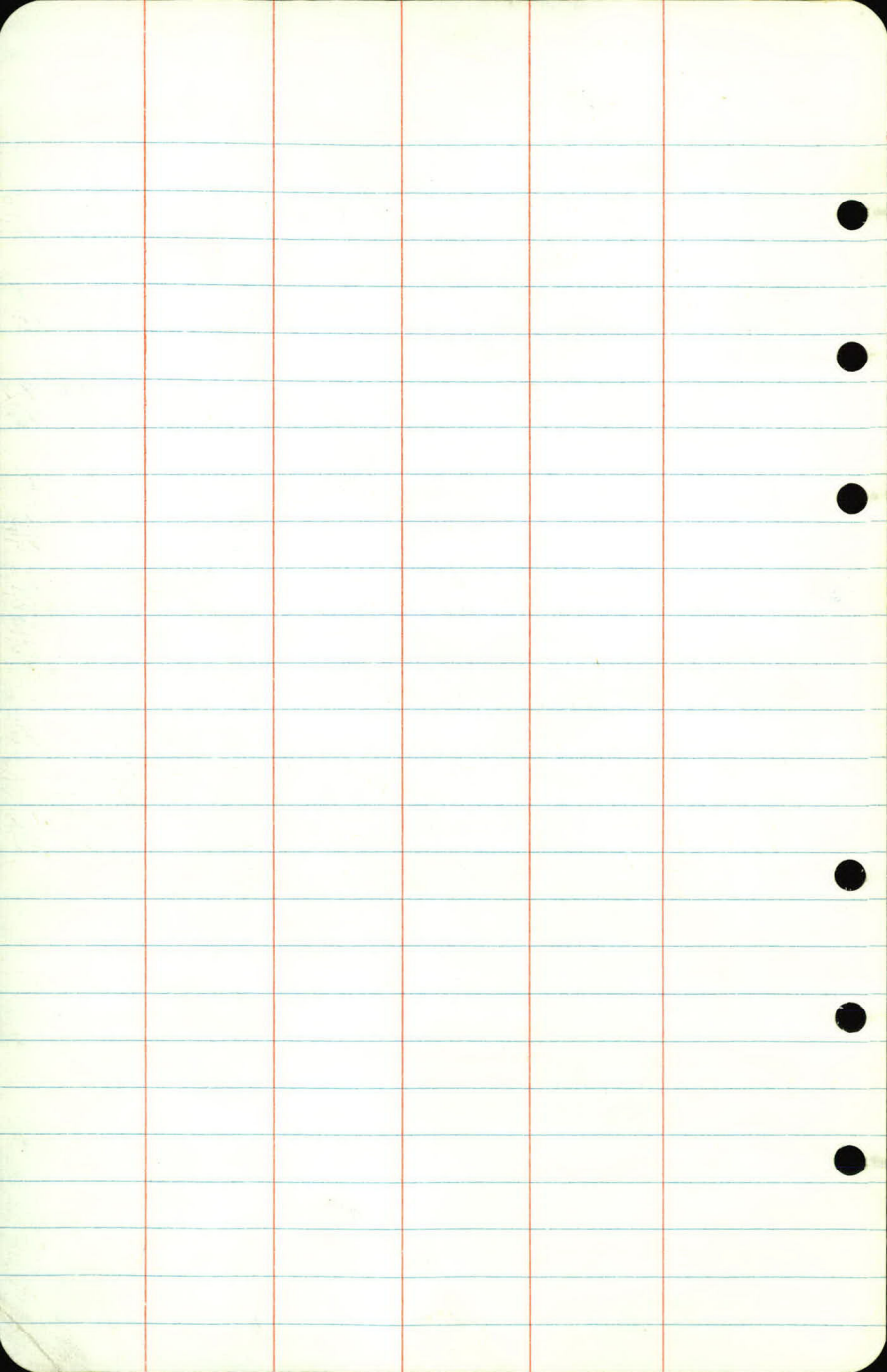
$$\frac{8.3}{75} \frac{8.5}{45} \frac{8.1}{21} \frac{7.0}{18} \frac{6.0}{14} 5.5 \frac{5.6}{16} \frac{6.6}{25} \frac{5.5}{29} \frac{7.0}{36} \frac{8.3}{48} \frac{7.1}{65} \frac{5.0}{75}$$

$$\frac{8.0}{75} \frac{7.8}{50} \frac{7.3}{31} \frac{6.6}{21} \frac{5.5}{14} 4.8 \frac{4.8}{15} \frac{5.3}{20} \frac{6.1}{23-26} \frac{4.5}{29} \frac{4.7}{34} \frac{3.3}{48} \frac{3.6}{56} \frac{4.8}{75}$$

$$\frac{4.0}{75} \frac{3.5}{55} \frac{2.8}{32} \frac{5.2}{25} \frac{5.1}{20} \frac{4.6}{16} 3.8 \frac{3.6}{14} \frac{4.4}{17} \frac{4.1}{24} \frac{3.0}{30} \frac{3.3}{38} \frac{5.3}{44} \frac{5.3}{47} \frac{3.3}{59} \frac{1.9}{59}$$

Spk in 12" C o H. 21' Rt Sta 237 + 25

$$\frac{4.6}{75} \frac{3.4}{50} \frac{2.6}{37} \frac{6.6}{31} \frac{7.4}{27} \frac{7.5}{23} \frac{7.1}{21} 5.7 \frac{5.3}{11} \frac{6.9}{35} \frac{7.6}{67} \frac{7.7}{80}$$



1
Cross Sections

Barrow Pit

Lexington Ave.
at Co. Rd "E"

Mon. Lex. Ave = Sta 10+00

Sta	+	ft	-	Elev.
B.M.	10.43	956.74		946.31

7+80				49.7
------	--	--	--	------

8+00		± Rd		49.4
------	--	------	--	------

8+59				48.4
------	--	--	--	------

8+60				48.4
------	--	--	--	------

9

+60

T.P.	6.79	953.10	10.43	946.31
------	------	--------	-------	--------

9				47.7
---	--	--	--	------

+60

46.8

+70

± Rd Ditch

46.5

B.M.

6.79

946.31

6.0

952.31

9+83

Toe Slope

46.5

9+88

shoulder

46.4

10+00

± Co. Rd. E

46.3

A

Top Mon Lexington E Co Rd "E"

7.00	<u>7.2</u>	<u>5.7</u>	<u>3.7</u>	<u>4.1</u>	<u>4.0</u>	<u>4.8</u>	<u>4.3</u>	<u>3.5</u>	<u>3.5</u>
	14	63	100	150	200	258	300	350	400

<u>7.27</u>	<u>7.4</u>	<u>6.2</u>	<u>4.8</u>	<u>3.9</u>	<u>4.1</u>	<u>4.3</u>	<u>4.1</u>	<u>3.3</u>	<u>3.7</u>
00	14	62	100	150	200	240	300	350	400

<u>8.29</u>	<u>8.4</u>	<u>6.7</u>	<u>5.1</u>	<u>3.7</u>	<u>3.2</u>	<u>3.7</u>	<u>4.0</u>	<u>2.4</u>	<u>2.9</u>	<u>4.6</u>
000	14	62	100	119	152	200	231	300	350	400

<u>8.29</u>	<u>8.4</u>	<u>6.7</u>	<u>5.6</u>	<u>5.3</u>	<u>6.3</u>	<u>5.3</u>	<u>3.2</u>	<u>3.7</u>	<u>4.0</u>	<u>2.4</u>	<u>2.9</u>	<u>4.6</u>
00	15	10	100	132	158	184	185	200	230	300	350	400

9.0

<u>6.7</u>	<u>7.1</u>	<u>3.5</u>	<u>4.0</u>	<u>3.4</u>	<u>2.2</u>	<u>2.8</u>	<u>4.4</u>
121	182	183	200	250	300	352	400

9.9

<u>3.9</u>	<u>4.3</u>	<u>4.5</u>	<u>2.2</u>	<u>2.3</u>
192	248	300	362	400

<u>5.35</u>	<u>5.6</u>	<u>3.7</u>	<u>3.4</u>
00	17	47	69

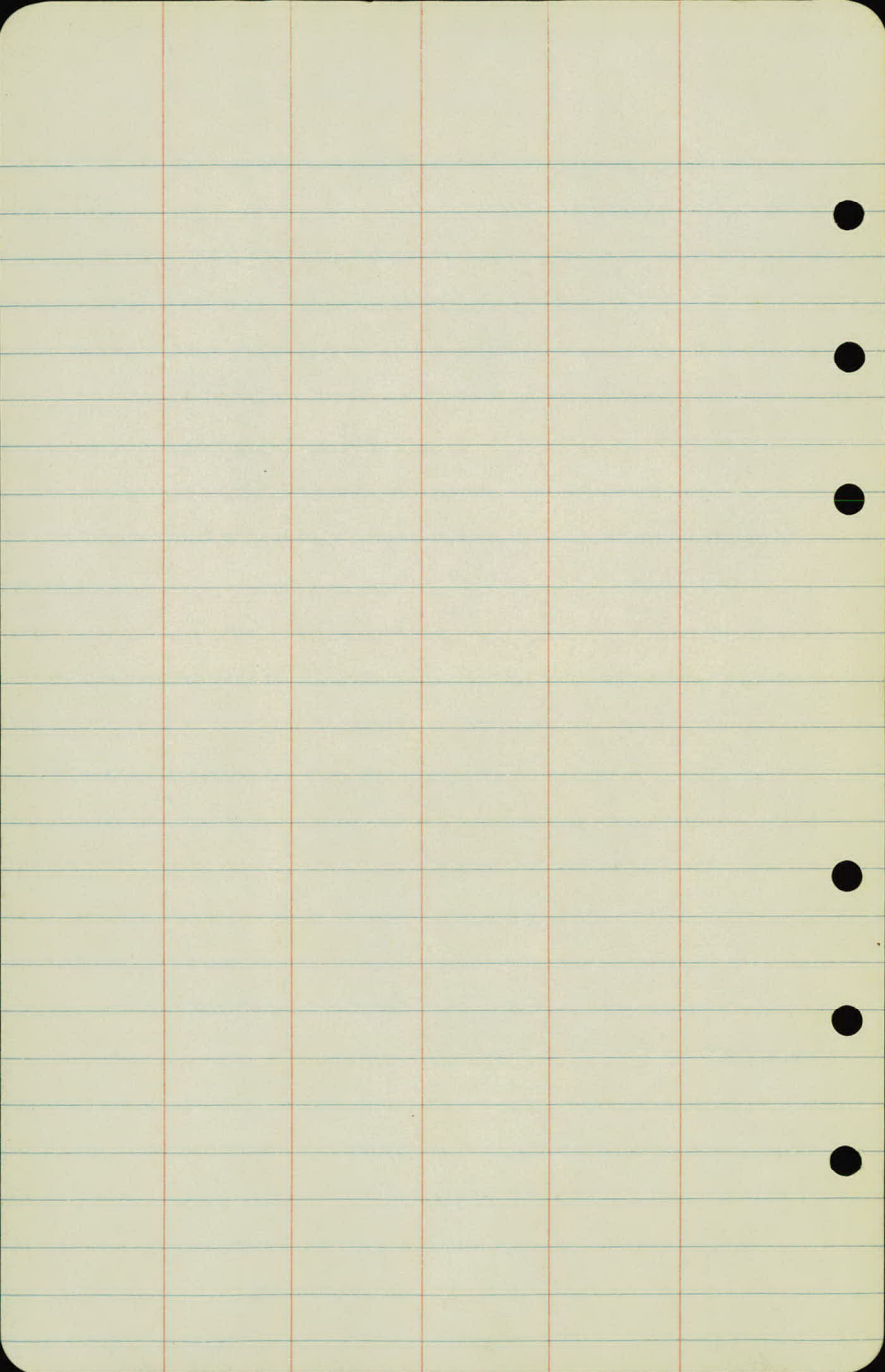
<u>6.28</u>	<u>6.5</u>	<u>5.8</u>	<u>5.6</u>	<u>4.6</u>	<u>4.8</u>
00	16	40	72	100	190

<u>6.60</u>	<u>6.6</u>	<u>6.0</u>	<u>6.2</u>	<u>6.0</u>	<u>6.0</u>	<u>5.2</u>	<u>5.8</u>	<u>5.8</u>
00	28	100	152	200	250	300	350	400

<u>5.8</u>	<u>5.8</u>	<u>5.1</u>	<u>5.5</u>	<u>5.1</u>	<u>4.9</u>
0	25	100	200	300	400

<u>5.9</u>	<u>5.2</u>	<u>4.2</u>	<u>4.0</u>	<u>4.3</u>
0	100	200	300	400

<u>6.0</u>	<u>5.0</u>	<u>3.9</u>	<u>3.7</u>	<u>4.0</u>
0	100	200	300	400



Survey
Co Ditch #12

Lexington Ave West

0+00 = Lexington Sta 22+10
stationing runs west

Pt.

Angle
Lt. Rt.

P.O.T. 5+79.8 End 18" Vlt -

P.1 5+25.3 20°44'

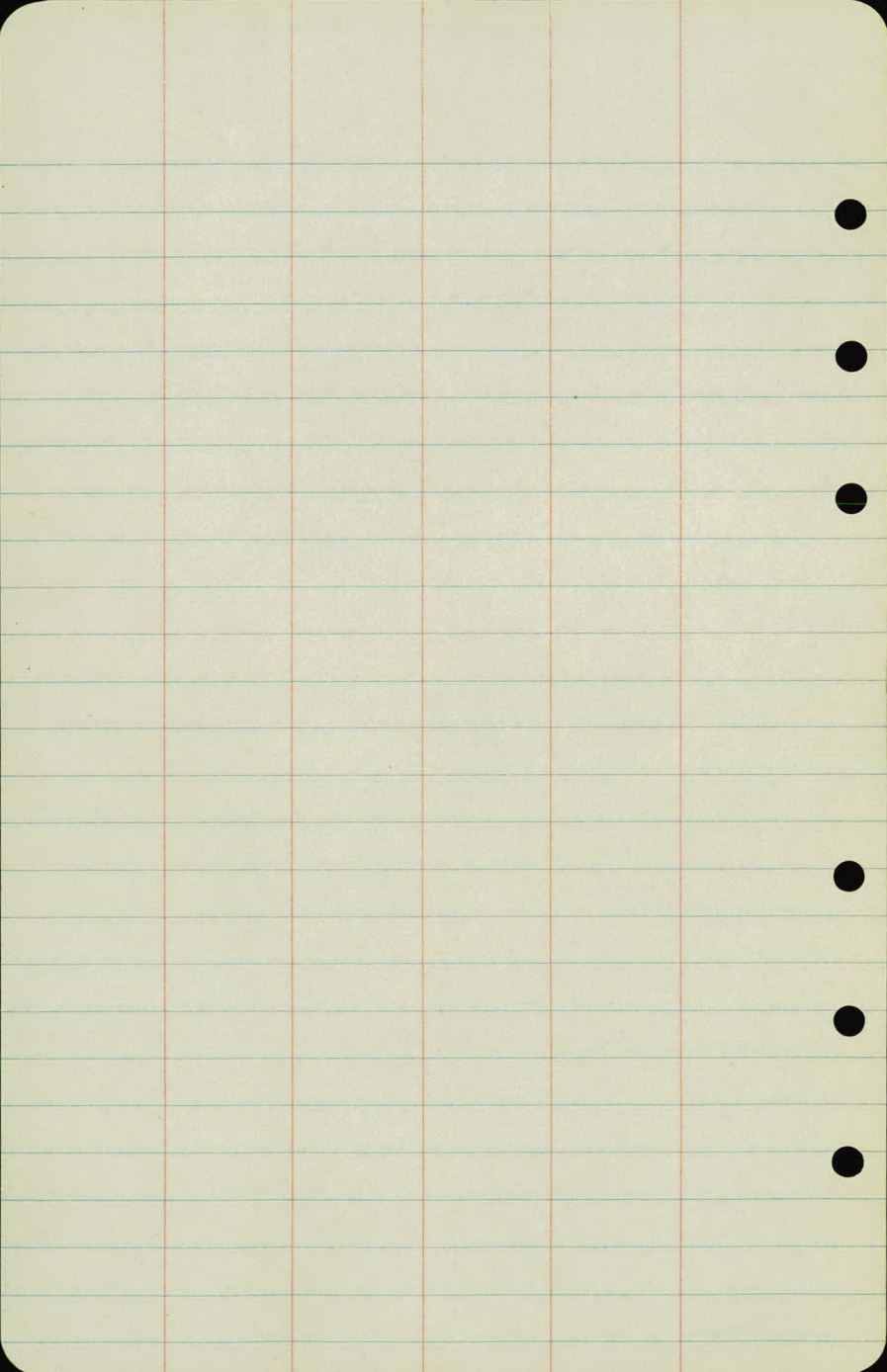
P.1 4+39.4 10°57'

P.1. 3+24.2 9°32'

P.1 2+51.6 2°11'

0+00 = Lexington Sta 22+10 & Lex.

136° 15' →
← Lexington



Profile Levels

Co. Ditch #12'

Lexington West toward Hamline

Pt	+	π	-	Elev
B.M.	1.51	935.90		934.39

0+34	F.L. Culv.	10.70	25.2
------	------------	-------	------

+50		9.9	26.0
-----	--	-----	------

1		10.4	25.5
---	--	------	------

+50		10.4	25.5
-----	--	------	------

2		11.0	24.9
---	--	------	------

+50		10.6	25.3
-----	--	------	------

3		10.8	25.1
---	--	------	------

+50		10.9	25.0
-----	--	------	------

4		10.9	25.0
---	--	------	------

+50		11.1	24.8
-----	--	------	------

5		11.4	24.5
---	--	------	------

+50		11.5	24.4
-----	--	------	------

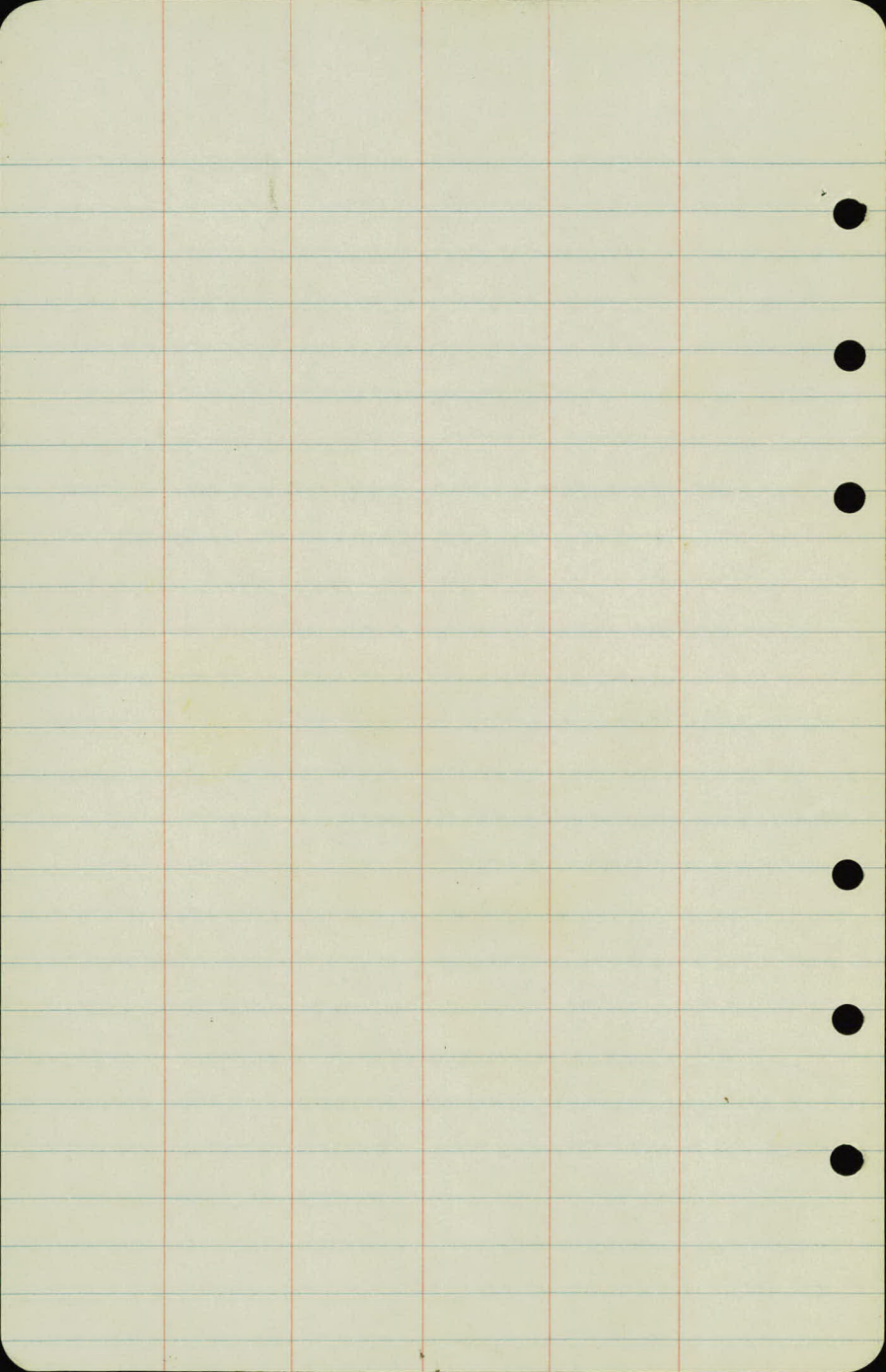
+79.8	F.L. Culv.	11.8	24.1
-------	------------	------	------

B.M.		1.50	934.40
------	--	------	--------

934.39

Spike in 24" Elm 33' Rt Sta 17+28 (Lex.)

Note Brush from 0+75 Sta 2+00



Lexington Ave.

Co. Rd "E" to Koalski Rd.

Slope Stokes.

Sta	+	Σ	-	Elev.	Ditch El
B.M.	2.14	948.45		946.31	
3				43.5	(48.4)
+38				43.4	
+70				43.0	
T.P.	3.23	941.93	9.75	938.70	
4				42.5	
+41				41.5	
5				39.5	
+50				37.5	
6				35.6	(39.3)
T.P.	4.37	937.05	9.25	932.68	
+50				34.1	
7				33.1	26.9
+50				32.6	26.8
8				32.5	26.8

G.R. DGR.

Top Mon.

$$\begin{array}{r} 946.31 \\ + 2.08 \\ \hline 948.39 \\ - 12.34 \\ \hline 936.05 \\ + 3.23 \\ \hline 939.28 \end{array}$$

5.1	$\frac{12.7}{F7.6}$ 31.2	$\frac{6.1}{F1.0}$	$\frac{5.1}{16}$	$\frac{11.7}{F6.6}$ 29.2	(5.0)
-----	-----------------------------	--------------------	------------------	-----------------------------	-------

5.4	$\frac{16.0}{F10.6}$ 37.2	$\frac{7.6}{F2.2}$	$\frac{5.4}{16}$	$\frac{13.6}{F8.2}$ 32.4	(5.4)
-----	------------------------------	--------------------	------------------	-----------------------------	-------

+0.6	$\frac{8.7}{F9.3}$ 34.6	$\frac{1.9}{F2.5}$	$\frac{40.6}{16}$	$\frac{6.2}{F2.8}$ 29.6	(5.9)
------	----------------------------	--------------------	-------------------	----------------------------	-------

0.4	$\frac{4.6}{F4.2}$ 24.4	$\frac{3.0}{F2.6}$	$\frac{0.4}{16}$	$\frac{6.9}{F6.5}$ 29.0	(6.9)
-----	----------------------------	--------------------	------------------	----------------------------	-------

2.4	$\frac{11.0}{F8.6}$ 33.2	$\frac{4.7}{F2.3}$	$\frac{2.4}{16}$	$\frac{9.7}{F7.3}$ 30.6	(8.9)
-----	-----------------------------	--------------------	------------------	----------------------------	-------

4.4	$\frac{12.3}{F7.9}$ 31.8	$\frac{6.1}{F1.7}$	$\frac{4.4}{16}$	$\frac{11.8}{F7.4}$ 30.8	(10.9)
-----	-----------------------------	--------------------	------------------	-----------------------------	--------

6.3	$\frac{13.9}{F7.6}$ 34.2	$\frac{7.9}{F1.6}$	$\frac{6.3}{16}$	$\frac{13.7}{F7.4}$ 30.8	(12.8)
-----	-----------------------------	--------------------	------------------	-----------------------------	--------

3.0	$\frac{9.2}{F6.2}$ 28.4	$\frac{4.4}{F1.4}$	$\frac{4.4}{16}$	$\frac{9.4}{F6.4}$ 28.8	(5.2)
-----	----------------------------	--------------------	------------------	----------------------------	-------

4.0	$\frac{8.7}{DC1.5}$ 33	$\frac{4.0}{16}$	$\frac{5.1}{F1.1}$	$\frac{4.0}{16}$	$\frac{9.3}{DC0.9}$ 33	(6.2)
-----	---------------------------	------------------	--------------------	------------------	---------------------------	-------

4.5	$\frac{8.7}{DC1.6}$ 33	$\frac{4.5}{16}$	$\frac{5.3}{F0.8}$	$\frac{4.5}{16}$	$\frac{9.9}{DC0.4}$ 33	(6.7)
-----	---------------------------	------------------	--------------------	------------------	---------------------------	-------

4.6	$\frac{8.9}{DC1.4}$ 33	$\frac{5.2}{F0.6}$	$\frac{4.6}{16}$	$\frac{9.1}{DC1.2}$ 33	(6.8)
-----	---------------------------	--------------------	------------------	---------------------------	-------

Sta	+	Σ	-	Elev.	Ditch El.
		937.05	(39.3)		
8+50			(6.8)	32.5	26.7
T.P.	5.96	937.19	5.82	931.23	
9			(6.8)	32.5	26.7
+50				32.5	26.6
10				32.5	26.6
+50				32.5	26.5
11				32.5	26.5
+50				32.5	26.4
12				32.5	26.4
+50				32.5	26.3
13				32.5	26.3
+50				32.5	26.2
14				32.5	26.2

G.R. DGR

$$\begin{array}{r} 937.56 \\ -5.20 \\ \hline 932.36 \\ +5.18 \\ \hline 937.54 \end{array}$$

$$\begin{array}{r} 939.28 \\ 6.48 \\ \hline 932.80 \\ +4.85 \\ \hline 937.65 \\ 32.5 \\ \hline 5.2 \end{array}$$

$$\begin{array}{r} 4.6 \quad 10.4 \quad \frac{9.1}{DC 1.3} \quad \frac{4.6}{16} \quad \frac{4.7}{0.1} \quad \frac{4.6}{16} \quad \frac{8.9}{DC 1.5} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.5 \quad \frac{9.6}{DC 0.9} \quad \frac{4.7}{16} \quad \frac{4.7}{FO.0} \quad \frac{4.7}{16} \quad \frac{8.7}{DC 1.8} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.6 \quad \frac{9.9}{DC 0.7} \quad \frac{4.7}{16} \quad \frac{4.9}{FO.2} \quad \frac{4.7}{16} \quad \frac{8.9}{DC 1.7} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.6 \quad \frac{9.4}{DC 1.2} \quad \frac{4.7}{16} \quad \frac{5.3}{FO.6} \quad \frac{4.7}{16} \quad \frac{9.2}{DC 1.4} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.7 \quad \frac{9.5}{DC 1.2} \quad \frac{4.7}{16} \quad \frac{5.3}{FO.6} \quad \frac{4.7}{16} \quad \frac{9.4}{DC 1.3} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.7 \quad \frac{9.3}{1.4} \quad \frac{4.7}{16} \quad \frac{5.3}{FO.6} \quad \frac{4.7}{16} \quad \frac{9.7}{DC 1.0} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.8 \quad \frac{8.9}{DC 1.9} \quad \frac{4.7}{16} \quad \frac{5.0}{FO.3} \quad \frac{4.7}{16} \quad \frac{10.4}{DC 0.4} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.8 \quad \frac{10.0}{DC 0.8} \quad \frac{4.7}{16} \quad \frac{4.7}{FO.0} \quad \frac{4.7}{16} \quad \frac{8.2}{DC 2.4} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.9 \quad \frac{9.9}{DC 1.0} \quad \frac{4.7}{16} \quad \frac{4.7}{FO.0} \quad \frac{4.7}{16} \quad \frac{9.8}{DC 1.1} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 10.9 \quad \frac{10.2}{DC 0.7} \quad \frac{4.7}{16} \quad \frac{5.2}{FO.5} \quad \frac{4.7}{16} \quad \frac{10.4}{DC 0.5} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 11.0 \quad \frac{10.7}{DC 0.3} \quad \frac{4.7}{16} \quad \frac{5.4}{FO.7} \quad \frac{4.7}{16} \quad \frac{10.4}{DC 0.6} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 11.0 \quad \frac{9.8}{DC 1.2} \quad \frac{4.7}{16} \quad \frac{5.5}{FO.8} \quad \frac{4.7}{16} \quad \frac{10.2}{DC 0.8} \\ \hline 33 \end{array}$$

Sta	+	π	-	Elev.	Ditch El.
		937.19			
14+50				32.5	26.1
15				32.5	26.1
+50				32.5	26.0
16 0				32.5	26.0
+50				32.5	25.9
+80				32.5	25.9
17				32.5	25.9
B.M.	2.22	936.61	277	934.32	934.39
+30				32.5	25.8
+80				32.5	25.8
18				32.5	25.8
+50				32.5	25.7
19				32.5	25.7

G. R DGR

$$\begin{array}{r} 4.7 \quad 11.1 \quad \frac{10.2}{\text{DC } 0.9} \quad \frac{4.7}{16} \quad \frac{5.4}{\text{FO.7}} \quad \frac{4.7}{16} \quad \frac{9.5}{\text{DC } 1.6} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 11.1 \quad \frac{10.6}{\text{DC } 0.5} \quad \frac{4.7}{16} \quad \frac{5.2}{\text{FO.5}} \quad \frac{4.7}{16} \quad \frac{9.7}{\text{DC } 1.4} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 11.2 \quad \frac{9.8}{\text{DC } 1.4} \quad \frac{4.7}{16} \quad \frac{5.1}{\text{FO.4}} \quad \frac{4.7}{16} \quad \frac{9.8}{\text{DC } 1.4} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \quad 11.2 \quad \frac{9.6}{\text{DC } 1.6} \quad \frac{4.7}{16} \quad \frac{4.8}{\text{FO.1}} \quad \frac{4.7}{16} \quad \frac{9.8}{\text{DC } 2.2} \\ \hline 34.2 \quad 35.2 \end{array}$$

$$\begin{array}{r} 4.7 \quad 11.3 \quad \frac{7.2}{\text{DC } 4.1} \quad \frac{4.7}{16} \quad \frac{4.3}{\text{CO.4}} \quad \frac{4.7}{16} \quad \frac{6.6}{\text{DC } 4.7} \\ \hline 37.1 \quad 37.7 \end{array}$$

$$\begin{array}{r} 4.7 \quad 11.3 \quad \frac{4.7}{\text{DC } 6.6} \quad \frac{4.7}{16} \quad \frac{4.2}{\text{CO.5}} \quad \frac{4.7}{16} \quad \frac{4.2}{\text{DC } 7.1} \\ \hline 39.2 \quad 40.1 \end{array}$$

$$\begin{array}{r} 4.7 \quad 11.3 \quad \frac{4.3}{\text{DC } 7.0} \quad \frac{4.7}{16} \quad \frac{4.1}{\text{CO.6}} \quad \frac{4.7}{16} \quad \frac{3.3}{\text{DC } 8.0} \\ \hline 40.0 \quad 41.0 \end{array}$$

Spike in 24" Elm 33 RI 5 to 17+28

$$\begin{array}{r} 4.1 \quad 10.8 \quad \frac{5.4}{\text{DC } 5.4} \quad \frac{4.1}{16} \quad \frac{3.7}{\text{CO.4}} \quad \frac{4.1}{16} \quad \frac{2.3}{\text{DC } 7.5} \\ \hline 38.4 \quad 40.5 \end{array}$$

$$\begin{array}{r} 4.1 \quad 10.8 \quad \frac{7.3}{\text{DC } 3.5} \quad \frac{4.1}{16} \quad \frac{4.0}{\text{CO.1}} \quad \frac{4.1}{16} \quad \frac{6.5}{\text{DC } 4.3} \\ \hline 36.5 \quad 37.3 \end{array}$$

$$\begin{array}{r} 4.1 \quad 10.8 \quad \frac{8.3}{\text{DC } 2.5} \quad \frac{4.1}{16} \quad \frac{4.0}{\text{CO.0}} \quad \frac{4.1}{16} \quad \frac{7.5}{\text{DC } 3.3} \\ \hline 35.5 \quad 36.3 \end{array}$$

$$\begin{array}{r} 4.1 \quad 10.9 \quad \frac{9.4}{\text{DC } 1.5} \quad \frac{4.1}{16} \quad \frac{4.4}{\text{FO.3}} \quad \frac{4.1}{16} \quad \frac{7.9}{\text{DC } 3.0} \\ \hline 34.5 \quad 36.0 \end{array}$$

$$\begin{array}{r} 4.1 \quad 10.9 \quad \frac{8.8}{\text{DC } 2.1} \quad \frac{4.1}{16} \quad \frac{4.8}{\text{FO.7}} \quad \frac{4.1}{16} \quad \frac{8.3}{\text{DC } 2.6} \\ \hline 35.1 \quad 35.6 \end{array}$$

Sta	L	K	-	Elev.	Ditch El.
		936.61			
19+50				32.5	25.6
20				32.5	25.6
+50				32.5	25.5
21				32.5	25.5
+50				32.5	25.4
22				32.5	25.4
T.P.	6.06	937.67 ⁷	5.00	931.61	
+50			(49)	32.6	
23				32.9	
+50				33.3	
24				33.9	
B.M.	6.20	943.37	0.50	937.17	
+50					
25					

937.54

28

937.54

40

937.14

G.R. D.G.R.

$$\begin{array}{r} 8.9 \\ \text{DC } 2.1 \\ \hline 35.1 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 5.0 \\ \text{FO.9} \\ \hline 16 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 8.9 \\ \text{DC } 2.1 \\ \hline 35.1 \end{array}$$

$$\begin{array}{r} 9.5 \\ \text{DC } 1.5 \\ \hline 3.2 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 5.4 \\ \text{F1.3} \\ \hline 16 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 7.2 \\ \text{DC } 1.8 \\ \hline 3.3 \end{array}$$

$$\begin{array}{r} 8.7 \\ \text{DC } 2.4 \\ \hline 3.3 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 5.7 \\ \text{F1.6} \\ \hline 16 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 9.0 \\ \text{DC } 2.1 \\ \hline 3.3 \end{array}$$

$$\begin{array}{r} 8.7 \\ \text{DC } 2.4 \\ \hline 3.3 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 5.7 \\ \text{F1.6} \\ \hline 16 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 8.7 \\ \text{DC } 2.4 \\ \hline 3.3 \end{array}$$

$$\begin{array}{r} 8.4 \\ \text{DC } 2.8 \\ \hline 3.3 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 5.3 \\ \text{F1.2} \\ \hline 16 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 8.8 \\ \text{DC } 2.4 \\ \hline 3.3 \end{array}$$

$$\begin{array}{r} 8.9 \\ \text{DC } 2.3 \\ \hline 3.3 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 5.1 \\ \text{F1.0} \\ \hline 16 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 8.9 \\ \text{DC } 2.3 \\ \hline 3.3 \end{array}$$

$$\begin{array}{r} 10.2 \\ \text{F5.1} \\ \hline 26.2 \end{array} \quad \begin{array}{r} 5.6 \\ \text{FO.5} \\ \hline 16 \end{array} \quad \begin{array}{r} 5.1 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 9.7 \\ \text{F4.6} \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 8.3 \\ \text{FO.5} \\ \hline 23.0 \end{array} \quad \begin{array}{r} 5.0 \\ \text{FO.2} \\ \hline 16 \end{array} \quad \begin{array}{r} 4.8 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 9.5 \\ \text{F4.7} \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 6.9 \\ \text{F2.5} \\ \hline 21.0 \end{array} \quad \begin{array}{r} 4.2 \\ \text{CO.2} \\ \hline 16 \end{array} \quad \begin{array}{r} 4.4 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 8.3 \\ \text{F3.9} \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 3.8 \\ \text{CO.2} \\ \hline 21.0 \end{array} \quad \begin{array}{r} 3.6 \\ \text{CO.2} \\ \hline 21.0 \end{array} \quad \begin{array}{r} 6.3 \\ \text{F2.5} \\ \hline 21.0 \end{array}$$

Top Mon. Lex E' Koalski

$$\begin{array}{r} 10.9 \\ \text{F2.3} \\ \hline 20.6 \end{array} \quad \begin{array}{r} 11.0 \\ \text{F2.4} \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 11.0 \\ \text{F3.1} \\ \hline 22.2 \end{array} \quad \begin{array}{r} 7.9 \\ \text{CO.0} \\ \hline 28 \end{array}$$

Sta

+

π

-

Elev.

943.37

25+50

26

+30

G. R

E

^{9.2}
7.2

7.6
DC 1.4
26.8

6.6

5.4
C 1.2
30.4

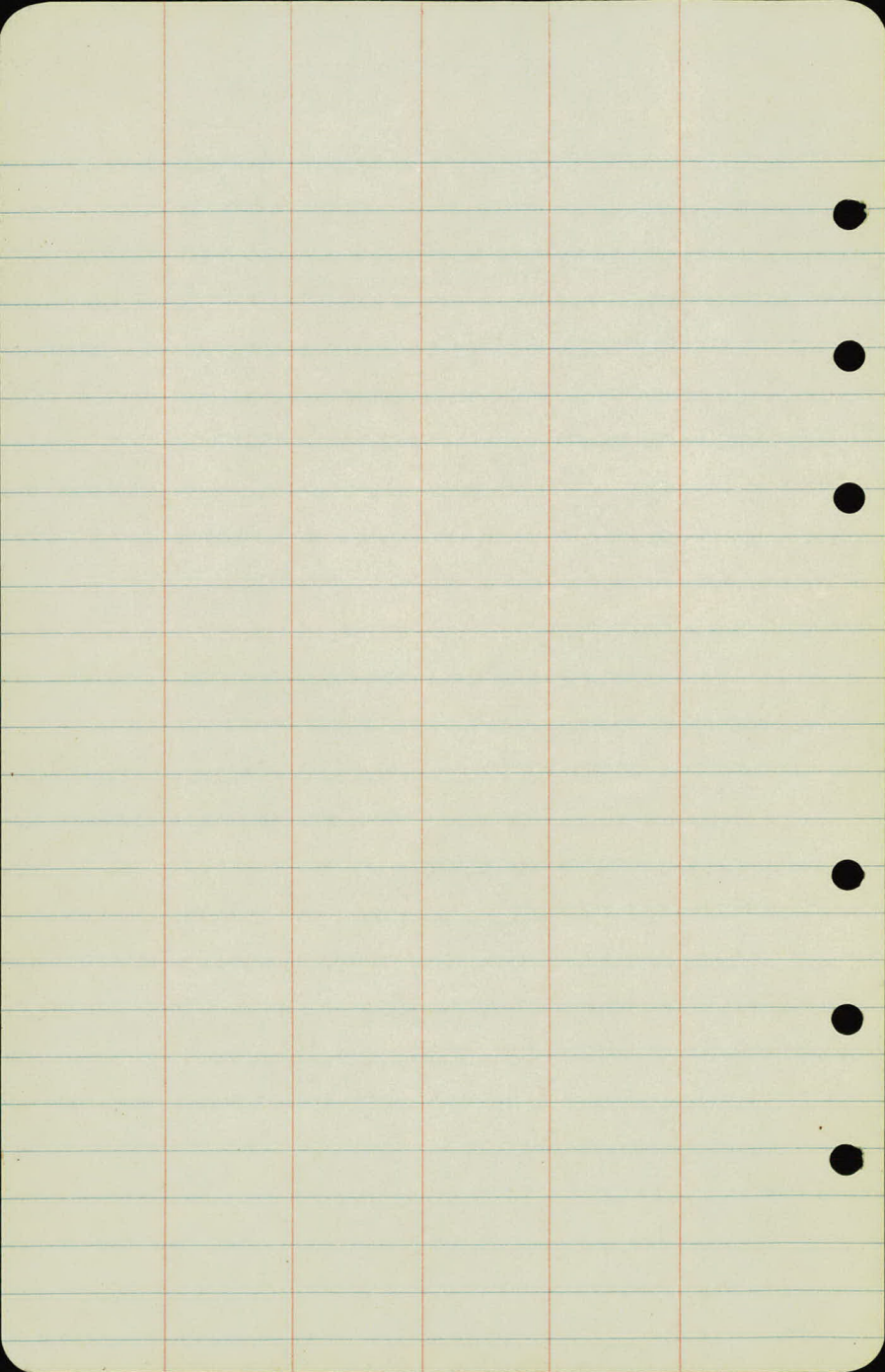
6.3

5.2
C 1.1
30.2

3.5
C 3.7
3.2

6.7
DC 1.9
27.8

3.4
C 2.9
3.3



Borrow Pit

Lexington Ave.

Slope Stakes.

Sta	+	π	-	Elev.
B.M.	11.40	957.71		946.31
8+00				

+60

9

+60

B.M.	8.06	954.37	
8+60			

Top Mon. Lex. and "E"

$$\begin{array}{r} 950.6 \\ \underline{67} \end{array} \quad \begin{array}{r} 6.1 \\ \text{cut } 1.0' \end{array}$$

$$\begin{array}{r} C 2.9 \\ \underline{5.8} \\ 337.8 \end{array}$$

$$\begin{array}{r} C 3.5 \\ \underline{4.2} \\ 333 \end{array}$$

$$\begin{array}{r} 949.6 \\ \underline{110} \end{array} \quad \begin{array}{r} 8.1 \\ \text{B.T.} \end{array}$$

$$\begin{array}{r} C 4.6 \\ \underline{3.6} \\ 935.2 \end{array}$$

$$\begin{array}{r} 949.0 \\ \underline{190} \end{array} \quad \begin{array}{r} 8.7 \\ \text{B.T.} \end{array}$$

$$\begin{array}{r} C 4.2 \\ \underline{4.5} \\ 934.4 \end{array}$$

$$\begin{array}{r} 950.0 \\ \underline{62} \end{array} \quad \begin{array}{r} 4.4 \\ \text{B.T.} \end{array}$$

