

Bk. 31 - Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

SILVER LAKE ROAD

(Fairchild Ave)

From: Rel "D" To Rice Creek Rd.

Road Acc't. No. 20

Date Filed: 4/40

File

Plan Survey
Fairchild Ave.
Silver Lake Rd.
Between Co Rd "D" and
Rice Creek Rd.

R.O.P.
H.W.
A.M.
L.G. } Party

Completed

Index:

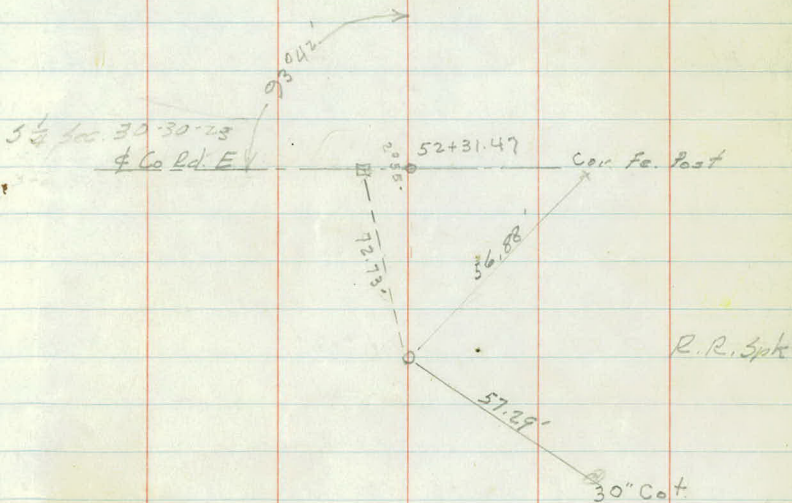
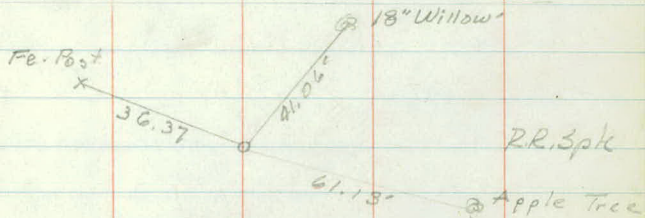
Transit Notes -	Sht #1 to 7
Topography -	" 8 to 34
Bench Levels -	35 to 38
Cross-Sections -	39 to 78
Bridge Infor. as of 1955.	Page 33 1/2

Sta.	Pt.	Lt.	Et.
26+15.64	P.O.T.		E Silver Lake Rd.
13+07.00	P.O.T.		E Sunset Lane
4+19.9	P.O.T.		Base Line for 500 Line Tracks
0+00	P.O.T.		

Sta Pt Lt Lt

+31.20	P.T.	1° 16'	$\Delta = 2^{\circ} 32'$
58		1° 07'	$D = 1^{\circ}$
+50		0° 52'	$T = 126.69$
57+04.56	P.I.	2° 32'	$L = 253.33$
57		0° 37'	$R = 5729.65$
+50		0° 22'	
56		0° 07'	
55+77.87	P.C.	0° 00'	

131.47	P.T.	1° 28'	$\Delta = 2^{\circ} 55'$
52		1° 09'	$D = 2^{\circ}$
51+58.57	P.I.	2° 55'	$T = 72.93$
+50		0° 39'	$L = 145.83$
51		0° 09'	$R = 2864.93$
50+85.64	P.C.	0° 00'	



Sta Pt Lt $\angle$ Rt.

$0^{\circ}03'$ 11°

91+29.0 P.O.T.

6

21 8°

85+22 P.I.

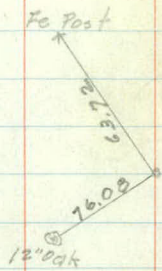
$0^{\circ}18'$ $0^{\circ}12'$

78+60.75 P.O.T.

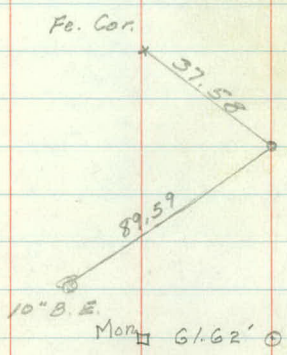
Ctr. $\frac{1}{4}$ Sec. Line E & W.

75+52.80 P.I.

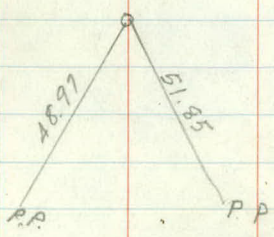
$0^{\circ}32'$ $20^{\circ}12'$



R.R. Spk.



R.R. Spk.



R.R. Spk.

Sta. Pt Lt Rt

$\Delta 22^\circ 51'$

+92.01 P.T.

$11^\circ 25\frac{1}{2}'$ D 20°

+50

$7^\circ 13'$ T = 58.19

108+35.95 P.I.

$22^\circ 51'$ L = 114.25

108

$2^\circ 13'$ R = 287.939

107+77.76 P.C.

0-00

+09.96 P.T.

$12^\circ 13'$

$\Delta 24^\circ 26'$

106

$11^\circ 13'$

D 20°

+50

$6^\circ 13'$

T = 62.34

105+50.13 P.I.

$24^\circ 26'$

L = 122.77

105

$1^\circ 13'$

R = 287.939

+87.79 P.C.

0-00

92139.16 P.O.T.

4 Cemetery Rd

Top Of Windmill Frame

P. R. Spt.

N 4 Cor Sec 30-30-23

2x2 Hub

100'

327.28'
22°51'

100'

2x2 Hub

Top New Brighton
Water Tower

Cor. Fe. Post

17.32

P. R. Spt

58.27

Cor. Fe Post

37.45'

30°00'

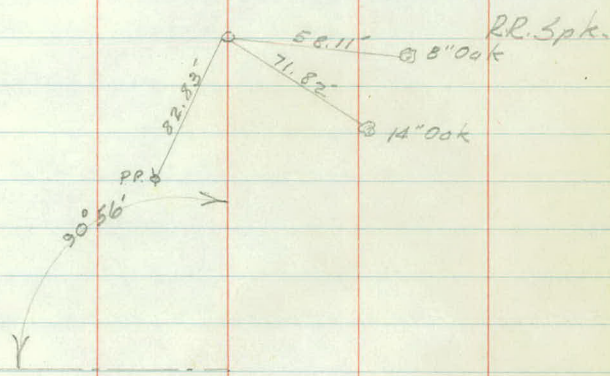
89°44'

Sta. Pt. Lt. Δ Rt.

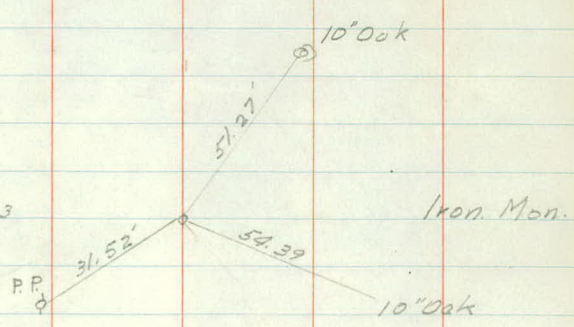
135+50 P.O.T.

131+40.0 P.O.T. $\frac{1}{2}$ Reservoir Rd

131+37.4 P.I. 0° 02'



Ctr. Sec. 19-30-23



Sta. Pt Lt Δ Rt

170+87.7 P.O.T.

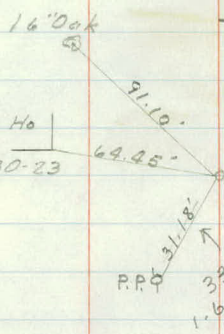
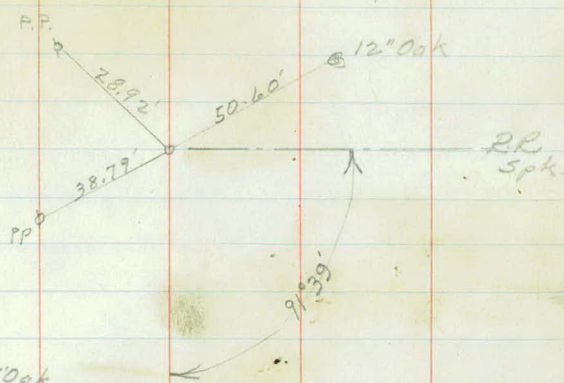
E Rice Creek Road.

157+71.68 P.I.

1° 02'

152+00 P.O.T.

183 1/2

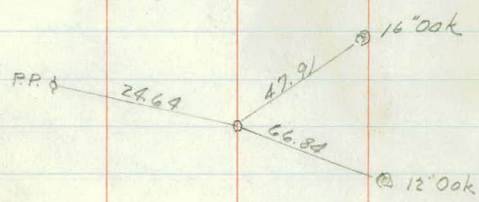


Cor. Ho

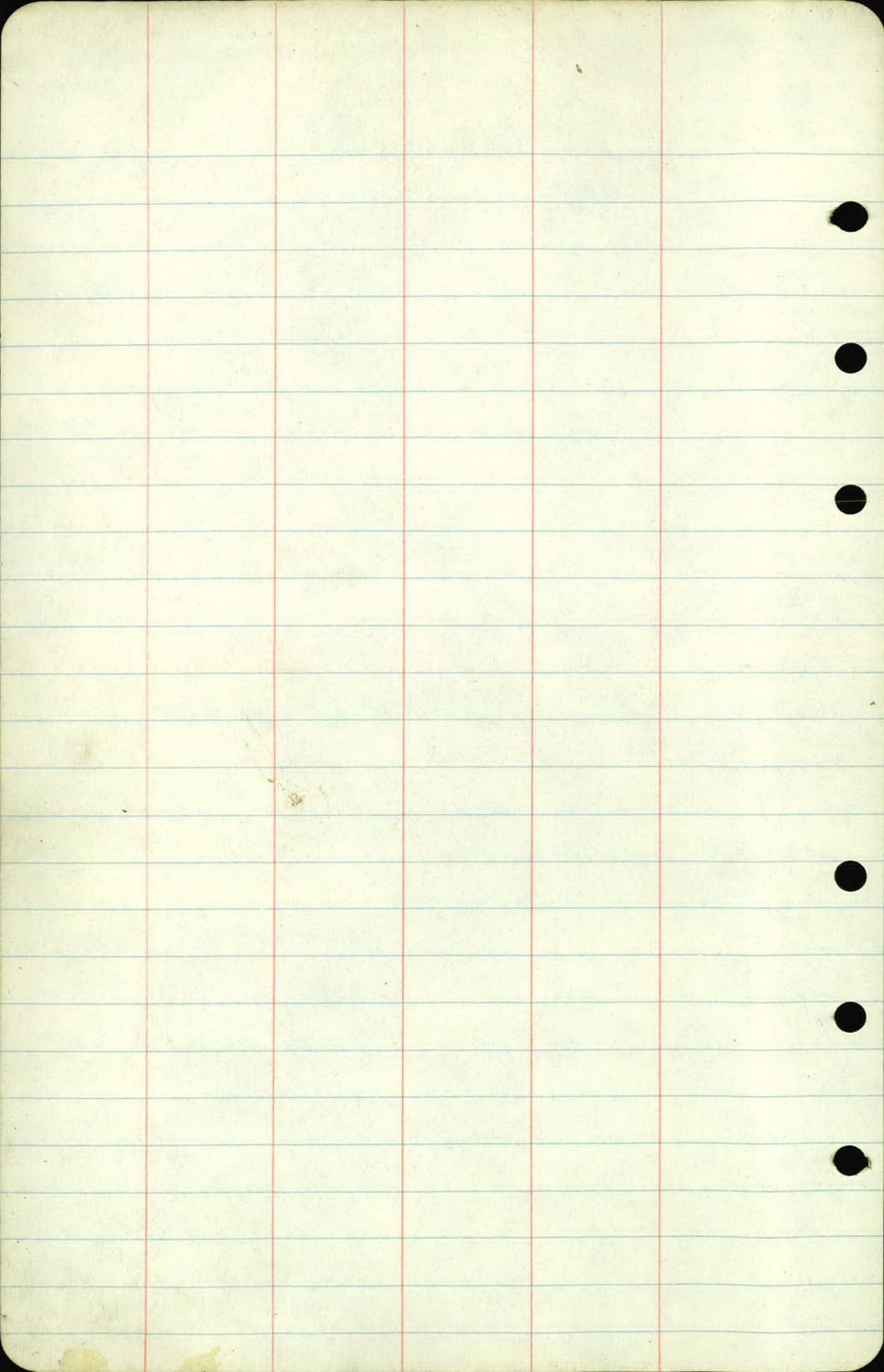
N 1/2 Cor. Sec. 19-30-23

Mon.

33.68
1-6-41



R.R. Spk.



Fairchild Ave.

Artificial Topography

3/2/39

Rd

Handrail 9.3
Wheelguard 8.65

+75.0 Bulkhead

Handrail 8.4
Wheelguard 7.7

4

Handrail 7.8
Wheelguard 7.1

+65.6 Bulkhead Face

Handrail 10"
Wheelguard 9.3

3

7' 8'

2

6' 9'

1

9' 10'

0

Rt. 92 PP 13' (9)

+75 Fe. Cor 42' x x x

+68 T.P. 13'

G.R. 9'

G.R. 9.5'

+65 Beg. G.R. 10'

Uncultivated

Swamp

+756 PP-13'

+450 Swamp-90

+100 Swamp-90

G.R.

+75 Swamp 120'

Swamp

+28 PP-14'

G.R. 12'

+65 Beg. G.R. 12'

Uncultivated

+97 PP-14'

18" x 62' CM

+32 N. End Culv. 20'

+30 T.P. 33'

+45 Rd-9'

+28 Rad Pt 16'

+15 Rad Pt 32'

+42 Rd-9'

+22 Rad Pt 19'

+11 Rad Pt 32'

Co. Rd. D
24' Black top

Note: See Additional Sheet for more complete information on 500 Line Bridge

Page 34

11

11' 9'

10

9' 9'

9

11' 9'

8

10' 6'

36'

+ 32' 24" x 68' G.M. X Drain 32'

7

10' 6'

6

9' 6'

5

9' 7'

+65 Ent.

Yard

+83 Fe Cor. 24' (10)

+65 Ent.

+08 Ent.

+91 Fe Cor. 20'

+92 P.P. 14'

Fe - 20'

Scattered Oaks

Uncultivated

Fe 22'

+90 Fe A - 22'

+79 End G.R. 12'

+78 Fe A 15'

Uncultivated

G.R. - 12 Fe. 14'

Yard

+67 P.P. - 14'

+43 End Row Tr. 33'

+10 Beg. Row Tr. 31'

+97 Ent.

+81 End G.R. 8'

+57-12" Oak 28'

+44-12" Oak 33'

+35 P.P. 14'

+07-9" P.P. 23'
G.R.

+32 C.B. - 36'

+15 Fe A - 15'

G.R. - 12 Fe A - 31'

Pump

+07 2-24" Oak 21'
G.R. - 8'

Fe 30'

G.R. 11

Scattered Oaks

Uncultivated

+56 P.P. - 12'

G.R. - 8'

G.R. - 11

G.R. - 9'

8' 11'

18

8' 10'

17

8' 11'

16

9' 11'

15

9' 10'

14

9' 10'

13

11' 11'

12

12' 8'

+69 30" Cot - 29
+42 18" Oak - 24

+43 - 24" Cot - 27

+56 - 30" Cot - 24

+76 - 30" Cot - 27

+40 - 24" Maple - 22

+92 - 24" Oak - 25
+82 - 15" Oak - 25

+34 G.P. - 23
+66 - Fe Cor - 33

+18 Bay Fe - 33

Cultivated

+60 Fe Cor - 27
+98 P.P. - 16
+92 Fe Cor - 27
+89 Ent.
12"x20" C.M. - 15
Yard
Cult.

+87 X Fe. 33
+58 P.P. - 15
+40 Ent.
12"x20" C.M. - 16
+12 - 12" Oak - 21

+63 - 2-12" Oak - 21-11
+56 Twin 12" Oak 24
+12 P.P. 15

+56 X Fe. - 33
+44 - 12" Oak - 24
+40 - 12" Oak - 25
+29 - Ent

+36 P.P. 15
+18
+66 - 12"x38" C.M. - 18
Sunset Lane
+88
+75 Fe Cor - 24
+51 - 12" Oak - 22
+44 6" Oak - 20

+19 P.P. - 14
Fe 24
Scattered Oaks Yard

8' 12"

25

9' 12"

24

16'

+ 97 - ^{9'}12" x ^{11'}32' CM x Drain 16'

23

8' 11"

22

8' 11"

21

8' 12"

20

8' 12"

There is a Cult. here
buried on purpose

19

8' 11"

+82- Cor. Orch. 46

Orchard

+16- P.P. - 19'

+79-24" Cot 23'

+82- Cor. Orch. 47

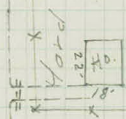
+62 Ent
12"x20' C.M. - 20'

Cultivated

+69- P.P. - 19'

+65 Fe Cor. - 21'

+24- P.P. - 19'



+61 Cor. Ha. - 50'
+58 Ent
15"x20' C.M. - 16
+48 Fe Cor. 22

Cultivated

+80- P.P. - 17'

Cultivated - Berries

+79-22" Cot. 23'
+63-30" Cot. 27'
+58 Ent
12"x20' C.M. 14'

+31 P.P. - 17'

8' 12'

32

8' 12'

31

8' 12'

30

8' 12'

29

8' 12'

28

8' 12'

27

8' 13'

26

8' 12'

End Fe. - 25'

+40 Lake - 28'

+00 Lake - 76' 1/2

+03 Bag G. R. - 11'

Fe 25'

+50 Lake - 150'

Fe. 24'

Fe. - 23'

Fe - 22'

Fe. 21'

+87 Ent.

12"x28' Vit - 14'

+78 - 12" Oak - 23'

+46 Fe Cor. 21'

Silver Lake Rd

Cult

+61 - P.P. 26'

+98 Ent.
12"x28' Vit - 18'

+31 P.P. - 25'

+09 P.P. 24'

+81 - Ent.

+76 Fe. Cor. 27'

+26 - P.P. - 24'

+55 P.P. 21'

+49 Fe Cor. 26'

+42 12" BE - 22'

+25 6" BE - 25'

Scattered Oaks

Scattered Oaks

Cultivated

8' 13'

39

9' 13'

38

8' 12'

37

9' 14'

36

8' 14'

35

8' 13'

34

7' 13'

17'

+ 36 - 12" x 34' G.M. X Drain 17'

33

8' 12'

+75 Swamp 16'-35'

+57 End 12' Cul. 23'

+52 Cor. Pier 31'

+10 Ent.

+00 Rge Tie Ent.

+01 Cor. Pier 31'

+97 End 12' Cul. 29'

+66 Swamp 30'

+24 Fe. Cor. 33'

+79-P.P.-26'

+29-P.P.-26'

+69-P.P.-25'

+19-PP-26'

500 Hared Oaks

Cultivated

+44 End G.R.-9'

+25 Lake 30'

G.R.-9

+90 Lake 20'

Silver Lake

+00 Lake 16'
End Fe. 25'

8' 12'

46

8' 13'

45

7' 13'

44

7' 13'

43

7' 13'

42

8' 12'

41

8' 12'

40

8' 13'

hatched
Ducks

+90 Pot hole 20-60

+50 Pot hole -40'



+80 Swamp 20'

Swamp 16'

+73-T.P. 30'

Evolution Army Cool Corps - Etc.

Swamp.



+55-P.P. -29'

Fe. 35'

+62 Swamp 34'

+100 P.P. 28-Fe 35'

Fe 35'

+148-P.P. -27'

Swamp 30'

Fe 34'

+192 PP-26'

+100 Swamp 30'

Fe. 34'

+35-P.P. -27'

Swamp.

10' 11'

53

9' 12'

52

8 8

51

9 10'

50

8 13

49

8' 10'

48

7' 12'

47

8' 12'

Fe - 46

196 - P.P. 26

16

Cultivated

Yard

+64 Fe Cor. 38'

+16 G.R. - 22
+08 - G.R. - 13'
+70 G.R. 11

Co. Rd.

+70 - 15" x 32 CM 29
+90 Ent.
+58 X Fe 43
+56 - P.P. 36
+19 Eng. 15" Culv 35'
+20 G.R. - 24'
+13 G.R. 14
+03 Fe Cor. 33'
+02 P.P. - 27'
+98 G.R. 11

G.R. 9

+85 End Swamp - 44 - 100'

Pasture

G.R. 13
+90 P.P. 30'

G.R. 9

Fe. 35' G.R. 13

+61 Swamp 35'
+60 P.P. 29'

Swamp

+88 Beg. G.R. 13'

+10 Swamp - 16'

+12 Swamp - 34'
+11 P.P. 29'
Fe 34'

+77 Beg. G.R. - 10'

+83 Ent

Swamp

10 9

60

9 9

59

11' 9'

58

12' 10'

21'

135-24"x42" CM X Drain 21'

57

12' 9'

56

10' 9'

55

10' 11'

54

10' 11'

Fe. 33

Fe 20

(17)

+45 Bag. Pot hole - 39

+45 P.P. 20'

Fe. 34'

Fe 20

+22 Ent
 +16 Bag Tie Fe
 +12 Fe Cor. 19'

+78 P.P. - 17'

+131 Fe Cor. 18'

Fe. 33'

+05 P.P. 15'

Fe. 30

Fe. 19'

+73 End 15" Culv. 22'

+60 Fe Cor. 30'

+49 Ent.

+38 Fe. Cor. 53'

+14 End 15" Culv. 22'
 Fe. 52

+39 P.P. 20'
 +39 Bag Fe. 20'

Fe. 46'

11 11

20'

+67 18" x 40' Vit X Drain 20'

67

11 10

66

9' 11'

23'

+92-12" x 40' Vit X Drain 19'
Poor Cond.

65

12' 9'

64

12 8'

63

12' 8'

62

12' 8'

61

10 9

Fe 31

Fe 21

(18)

Fe 29'

Fe 20'
+91 P.P. 19

Fe 31'

Fe 20'

+46 X Fe. 33'

+44 X Fe. 15' 22'
+32 P.P. 18

Fe 33'

Fe 13'

+81 20' Lot 19'

Fe 35

Fe 13'
+92 P.P. 18

Fe 36'

Fe 17'

Fe 33'

Fe 21

+82 Ent

+44 P.P. - 19'

+40 End Pothole - 54

+53 X Fe. 23

Fe 34'

Fe 20'

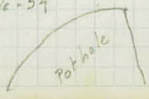
Uncultivated

Scattered Oaks

Scattered Oaks

Cultivated

Post-hole



12 8

74

12 8

73

11 9'

72

10 9'

71

10 12

70

11 11

69

10 9

68

11 11

+91 Ent.
+80 Fe Cor. 31'

Fe. - 31'

Fe 23
+84 PP 19

Orchard

+78 Fe Cor. 31'
+72 Ent.
15"x18" CM - 18"
+66 Fe Cor. 31'

Fe 23'
+83 PP - 19'

Fe. 32'

+76 End G.R. 13'

+84 Ent.
+75 Fe Cor. 22'
+76-12"x42 CM 17'
+66 Ent.
+46 End G.R. 14'
+30 PP - 19'

+10 End 12" Vit. - 84'
GR - 13' Fe 32'

GR-14- Fe 23'

+73-End 12" Vit 25'

+38 New End 68'
24 1963

Fe 22

Fe 32'
+93 Bag G.R. 13'
+84-18" Dot - 27'

+48 Bag G.R. 14'
+47 PP - 19'

Fe 33

+17 x Fe. 19'
Fe 19

+45 Ent

+13 PP - 20
Fe 21

Fe 31

Uncultivated

Cultivated

Disturbed Outlets

10 8

81 10 10

80 9' 11

19 157' 12" x 32' C.M. x Drain 13'

79 10' 10'

78 11 9

77 10 10

76 10' 9'

75 12. 2

Fe. 27

+80 X Fe. 27 x x x

+79 End Fe. 24'

Fe 27

+11 P.P. - M
Fe 24'

Fe. 27'

Fe 23'

+75 PP 17'

Uncultivated

+02 Beg. Fe 22
+92 Ent.
+82 X Fe. 21

+60 Fe Cor 27'-32 x x x

+60 Fe Cor 20

Cultivated

+07 PP 19'

Cultivated

Fe 30

Fe 22

+67 PP - 19'

+08 X Fe 31' x x x

Fe. 23'

+12 PP 30'
+01 Fe Cor - 31 x x x

+03 PP - 18'
Fe 23'

11 11

88

11 11

87

10' 9'

86

9' 9'

85

10 10

84

11 10

83

11 11

82

10 8

Fe 28'

(21)

+64-12" Oak-32'

+36-12" Oak-28'

Fe 27'

+54-12" Oak-26'

Cultivated

+28 X Fe-28'

+58 Fe Cor. 27'

+22 Ent.

+12 Fe. Cor. 28 X.

Cultivated

+78 PP-25

+78 Fe Cor. 27

+64 Ent.

10" x 18" CM. 14'

+56 Rgc tie Ent.

+54 Fe Cor. 27

Fe 27

+32 PP-19'

11 10

95

11 10

94

11 12'

93

10' 12'

92

11' 11'

91

11 10

90

11 10

89

11 11

Fe 31

Brush 35 (22)

Fe 32

Fe. 32'

Fe. 32'

FE. 32'

+71 Ent.

+25 X Fe. 33' x x x

Fe. 31'

+60-12" Oak-33' x

+22 14" Oak-31' x

+04 12" Oak 30 x

Fe 29 x

+87 12" Oak 29 x

+60-14" Oak 31 x

+46 12" Oak 30 x

+40 X Fe. x x x

Fe 28' x

Scattered Oaks

Cultivated

Cultivated

Bag Brush-36'

Cemetery Rd- 26 Gravel

10 9

102

12 10

101

12 10

100

12 9

99

11' 10'

19'

+86-12"x36' C.M. X Drain 17'

98

10 10

97

9' 11'

96

11 10

Fe 31'

Fe 31'

Fe 31'

Fe 30

Fe 30

Fe 30

+60 Pot hole - 20

+100 Swamp 27-80
Fe 31

+20 Beg Pot hole - 20'

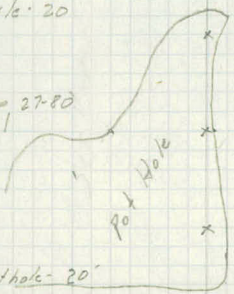
Fe 31

Wooded - Oak's

Cultivated

+85 Ent

Brush 36



11 11

109

7' 12'

+50 8' 12'

108

6 11

19'

+67-12"x34' C.M. X Drain 15'

107

11 8

106

12' 8'

+50 15' 9'

105

15' 7'

26'

+90-12"x46' C.M. X Drain 20'

104

8 12

103

10 9

Cultivated

Uncultivated

+ 21 Fe Cor. 26'
+ 10 Rgc tie Fe.

+ 65 Fe 21'

Fe. 31

Fe 31

Fe 31

Uncultivated

Wooded

Cultivated

+ 90 Ent.

+ 73 Fe Cor. 38'

+ 30 End Pot Hole - 40

Pot hole

Pot Hole 31'

+ 65 Bag Pot hole - 40'

+ 00 Bag Fe - 35'
End Brush - 35'

10 11

116 21'

+ 09-12" x 40' C.M.
10 11

19'

115

10-10'

114

10" 10'

113

9' 12'

112

9' 11'

111

10 10

26'

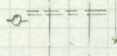
+ 85-12" x 48' C.M. X Drain

22'

110

11 11

+183 P.P. 28'



+73 Bag. Fe. 22'

Cultivated

+28 P.P. 27'



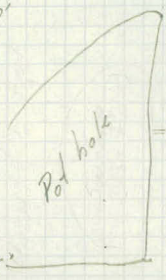
Yard

+96 Ent.



Cultivated

+47 End P.H. 20'



+15 Bag. P.H. 25'

10 10

123

10 10

122

10 10

131

10' 10'

120

10' 10'

119

10 10

118

9 11

117

11 10

Fe. 23'

Scattered Oaks

+52 Fe. Cor. 27'

+91 P.B. 28'

Cultivated

Yard

+20 Ent.

+138 P.B. 28'

Cultivated

Cultivated

+48 End Fe. 23

Fe. 22'

10 11

130

10' 11'

129

9' 11'

126 + 90
1101

128

10 11

127

24

10 10
+ 90-12" x 48 CM. X Drain 24'
SKOW - + 93-22" Rt

126

9 11

125

10' 10

124

10 10

Cultivated

Timber

Fe. 30

Fe. 25

+90 Swamp 25

+90 Swamp 25

Swamp 15'

+100 Swamp - 23'

Fe. 23

+78 PP-28

Swamp

Swamp - 24'

Fe. 23'

+75 Beg Swamp - 23'

Swamp - 23-200

Fe 23

Swamp - 46-100

Fe 22'

+33 PP 28'

Fe 21

Swamp

10 10

137

9 11

136

10' 11

135

10' 12'

134

9' 11'

133

9' 12'

132

9' 12'

131

10 11

+39 PP. - 28'

+83 Fe. Cor. - 31'

Fe 31'

Fe. 32'

Timber

Fe. 33'

+95-12" Willow 32'

+70 PP. - 28'

+75 Ent.

+41-8" Oak 30'

Fe 33'

Fe 34

Fe. 33'

Uncultivated

Timber

Reservoir Rd.

+21 PP-78

+38 X Fe - 31'

Fe 29

9 11

144

9 11

143

10 11

+ 66' 15" x 56' C.M.

142

9 11

18'

+ 40' - 18" x 40' L.M. x Drain

22'

141

9 11

140

10 10

139

10 10

138

10 10

Fe. 21
Swamp 19

Fe 17
Swamp 20

(29)

Swamp 20
Fe - 19

Swamp 20
Fe 17

+40 T.P. 19'

Swamp 21
Fe 21

Swamp 25'
Fe 18'

+60 Beg. Swamp 28'
+60 End 15" CM 28'

+73 End 15" CM 28'

Fe 18

Swamp 31
Fe 19

+65 T.P. 20
+62 P.P. 27

+40 Swamp 18

Swamp 18
Fe 20

Swamp 23-100'
Fe 18

Fe. 20
Swamp 23

+88 T.P. 20'

Beg. Swamp 26-40

+30 Beg Swamp 20'

+70 Fe. Cor - 20'

Fe 22

+25 Ent
12" x 30' CM - 15'

+46 Fe Cor. 27'

+22 P.P. - 28'
+12 Ent
15" x 24' CM 14'

151

10' 10

150

10 10

149

9 11

148

10' 11

147

10' 11'

146

9' 10'

145

+128 X Fe. 31' X

Fe 30.

+143 P.P. 23'

+75 Ent.
12" x 20' CM. 15'

Cultivated

+95 End Orch. 31'

+69 P.P. 25'

Orchard

+10 Ba. Orch. 31'
+09 Fe. Cor. - 33'

Fe. 31'

Fe. 36

Fe. 38'
+91 T.P. - 21

Fe 31'

Fe. 31

Wooded

+19 Ent.
12" x 20' CM. 16'
Fe 30

+50 Cor Swamp 50

+30 Swamp 26
+28 PP - 26
+11 T.P. - 19

+47 Fe Cor - 16'
+38 End Swamp 50

158

9 11

157

9 10

156

9 11

155

9 11

154

9 11

153

10 11

152

10 11

+83 PP-16.

+30 Ent.

+76 Cor. Ho 65'
+71 Ent.
18" x 24" - 15'

+44 PP-16'

+22 X Fe. - 25'

+105 P.P. 18'

+75 PP-19.

+61 Ent.

12" x 20" CP - 15'

+28 PP - 20'

+07 Ent.

12" x 18" CM - 24'

+95 End Orch. 40'

+12 PP 21'

Beg Orch. - 39'

Yard.

Uncult.

Yard.

Yard.

Orchard

Brush

Colt.

Beg. Brush - 30' - 68'
End Timber - 30'

Timber 34'

Timber 35'

Beg. Timber 27'
Swamp 80'

+40 Swamp 22' - 42'

Swamp 29'

Swamp 28' - 100'

+85 Fe. Cor 27'

Fe - 30'

165

10 11

164

9 11

20 . +70 15" x 40' C.M. X Dr. 20'.

163

10 11

162

10 10

161

10 10'

160

10 10

159

9 10

Fe. 26 •

Timber 28. (32)

+49 PP-18 •

Fe. 22 •

Fe. 18 •

+82 PP-17 •

+50 End Swamp 31 •

Swamp 31 •

Fe. 19 •

+70 Beg. Fe. 18 •

+17 PP-17 •
Swamp 29 •

Swamp 32 •

+50 PP-17 •

Swamp 26 •

+50 Swamp 28 •

Swamp 100 •

Timber

+01 G.P. - 15 •
Swamp 37 •

Swamp 30 •

Swamp 29-125 •

+50 Beg. Swamp 39 •

Swamp

25

+68-15-52 CM X Drain

27

170

10 10

169

11 10

168

10 10

167

10 10

166

10 10

Rice Creek Rd 20 Blockers

+75 Rd. Pt. 31.

+75 Rad. Pt. 38.

+53 PP 21.

+50 Rad. Pt. N.

+50 Rad. Pt. N.

+27 End Timber 30.

+96 PP. 20.

Timber 25.

Timber - 23.

+07 PP -18.
End Fc. 26.

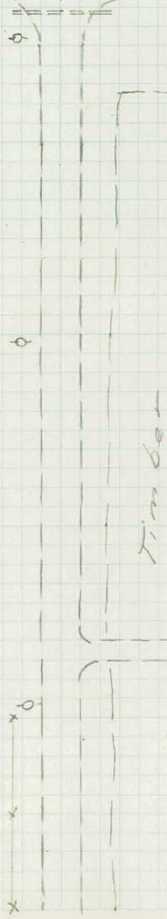
+35 Ent.

Timber 26.

Fc 26.

Timber - 28.

Uncultivated



New Deck Oct. 13, 1955

Stringers 8"x16" (11 or 12 Rows)

Sway Braces are 3" Thick

New Side braces are 6"x12"

Bent #1 8- 8"x16" Blocking
4- 12"x12"x3'2" Col
12"x12"x18" Cap
12"x12"x18" Mud Sill
8"x16"x18" Plank Backing

Bent #9 1- 12"x12"x2'2" Col.
12"x12"x18" Cap
12"x12"x18" Mud Sill
Backing 8"x16" Plank
9- 8"x16" Blocking

Bent #8 8"x16" Backing Plank added

Bent #2 6- 10"x16" Blocking

Clearance 21.9 Rail to Stringers

additions of
Corrections of Page 3A
P.K.

1940 Additional Information On Soo Line Bridge

34

15 Rows
Deck 3'x10"
Stringers 6"x6"-17'
Mid sill 12"x12"
Cap 12"x12"
T Bents

Bent #1

3+65.6

3+86

4+02

4+06

4+23.5

4+41.5

4+44.2

4+59

4+75.0

3-6"x12" Braces
4-6"x12" Braces



12 Stringers

6"x16" Backing Plank
1-22'
2-26'
2-26'
12"x12"x18" Cap
4-12"x12"x2'-10" Stringer
2-6"x16"x18"

Bent #2

4-12"x12"x11'-3" Col.
2-12"x12"x24" Mid Sill
2-2"x10"x24'-6" Sweep Br.
1-12"x12"x20" Cap

Bent #3

1-12"x12"x20" Cap
4-16" Piling
2-2"x12"x38'-4" Sweep Br.

Bent #4

1-12"x12"x20" Cap
4-16" Piling
2-2"x12"x38'-4" Sweep Br.

Bent #5

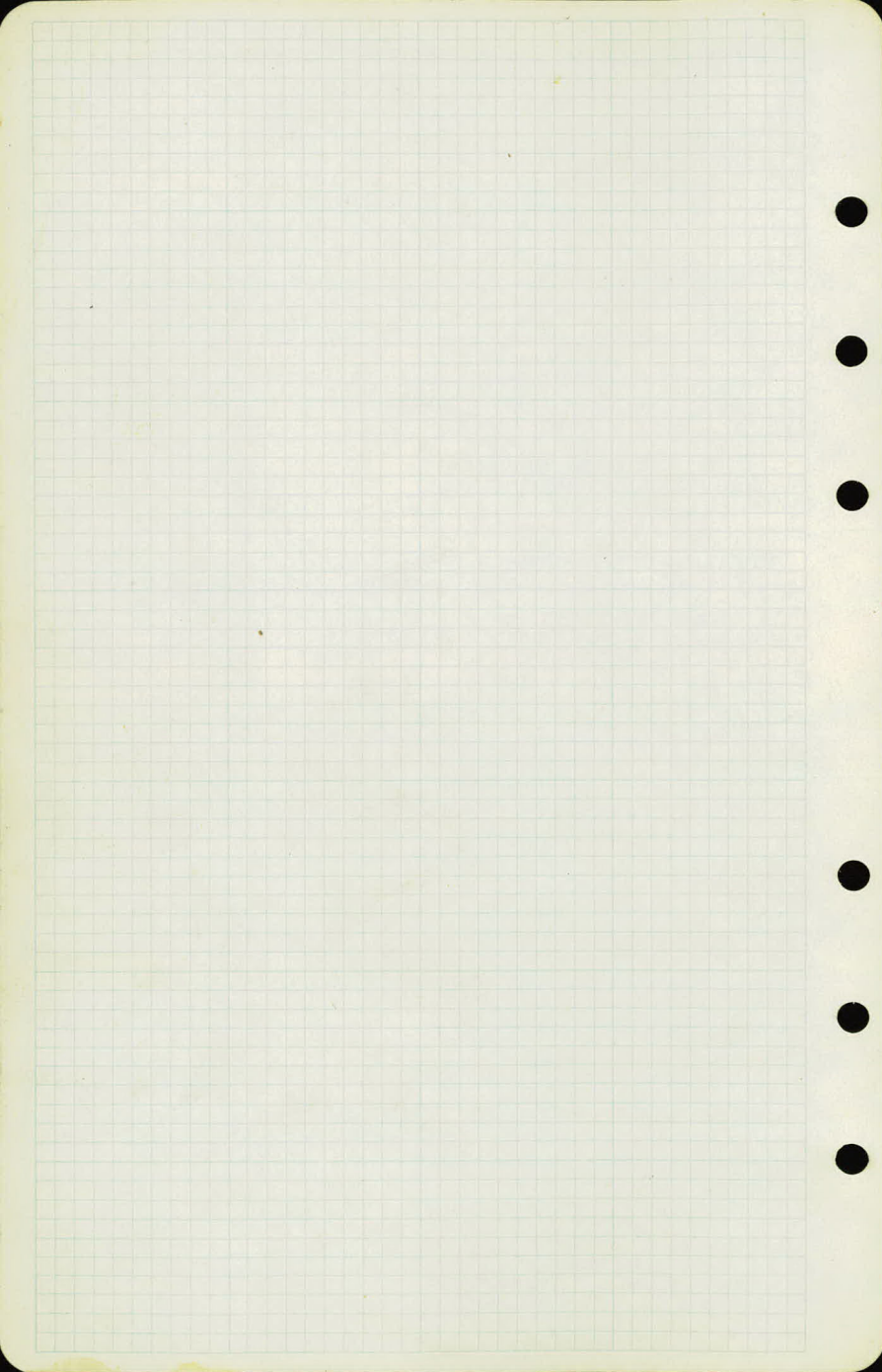
1-12"x12"x20" Cap
4-16" Piling
1-2"x12"x30" Sweep Br.

Bents 6 and 7
Same as Bent 4

Bent #8

12"x12"x20" Cap
4-12"x12"x10" Col.
2-2"x10"x24" Sweep Br.
1-12"x12"x23'-6" Piling
7-12"x12" Backing

Bent 9 & Butthead
Same as Bent 8



Bench Levels

Fairchild Ave.

Co Rd "D" to Rice Creek Rd.

Pt	+	π	-	Elev
B.M.	11.52	970.77		959.25
T.P.	0.45	960.70	10.52	960.25
T.P.	4.35	958.51	6.54	954.16
B.M.	0.18	953.09	5.60	952.91
T.P.	2.76	946.11	9.74	943.35
T.P.	7.72	947.27	6.56	939.55
B.M.	2.86		2.86	944.41
T.P.	4.36	947.83	3.80	943.47
B.M.	7.74	947.53	8.04	939.79
T.P.	1.59	941.80	7.32	940.21
B.M.	5.94		5.94	935.86
T.P.	5.70	940.55	6.95	934.85
T.P.	7.46	946.67	1.34	939.21
T.P.	13.76	959.73	0.70	945.97
B.M.	3.96		3.96	955.77
T.P.	12.28	971.77	0.24	959.49
T.P.	11.43	982.94	0.26	971.51
T.P.	7.51	986.29	4.16	978.78
T.P.	1.70	981.53	6.46	979.83
T.P.	1.22	969.12	13.65	967.88
B.M.	5.35		5.35	963.75
T.P.	6.62	965.14	10.58	958.52
T.P.	11.68	976.45	0.37	964.77
T.P.	10.57	986.62	0.40	976.05
T.P.	3.00	987.96	1.66	984.96

Fairchild E.D.

Top L Iron Base E. Pier Tower N.E. Cor

Spike in P.P. 14' Rt Sta. 13+35

Spike in 14" Oak 24' Lt Sta. 26+79

Spike in P.P. 26' Rt Sta. 32+61

Spike in P.P. 27' Rt Sta. 40+35

Spike in Fe Cor. 33' Rt. Sta. 52+03

Spike in 15" Oak 70 Rt. Sta. 65+93

PI	+	π	-	Elev.
		987.96		
T.P.	8.36	989.18	7.14	980.82.
B.M.	3.31		3.31	985.87.
T.P.	10.22	996.36	3.04	986.14.
T.P.	5.50	998.26	3.60	992.76.
T.P.	0.14	986.63	11.77	986.49.
T.P.	3.72	978.77	11.58	975.05.
T.P.	1.46	974.85	5.38	973.39.
T.P.	0.37	963.89	11.33	963.52.
B.M.	5.97		5.97	957.92.
T.P.	5.68	954.26	10.31	953.58.
T.P.	0.10	944.15	10.21	944.05.
T.P.	0.91	936.82	8.24	935.91.
T.P.	5.73	935.24	7.31	929.51.
B.M.	5.69		5.69	929.55.
T.P.	2.32	933.88	3.68	931.56.
T.P.	1.64	927.40	8.32	925.56.
T.P.	8.65	931.89	3.96	923.24.
T.P.	10.01	940.04	1.86	930.03.
T.P.	6.64	945.69	0.99	939.05.
T.P.	1.99	938.16	9.52	936.17.
B.M.	0.51	930.39	8.28	929.88.
T.P.	9.31	938.23	1.97	928.92.
T.P.	1.59	944.48	1.34	936.89.
T.P.	2.64	941.73	5.39	939.09.

Spike in P.P. 25' Lt. Sta. 82+75

Spike in 12" Oak 24' Lt. Sta. 105+62

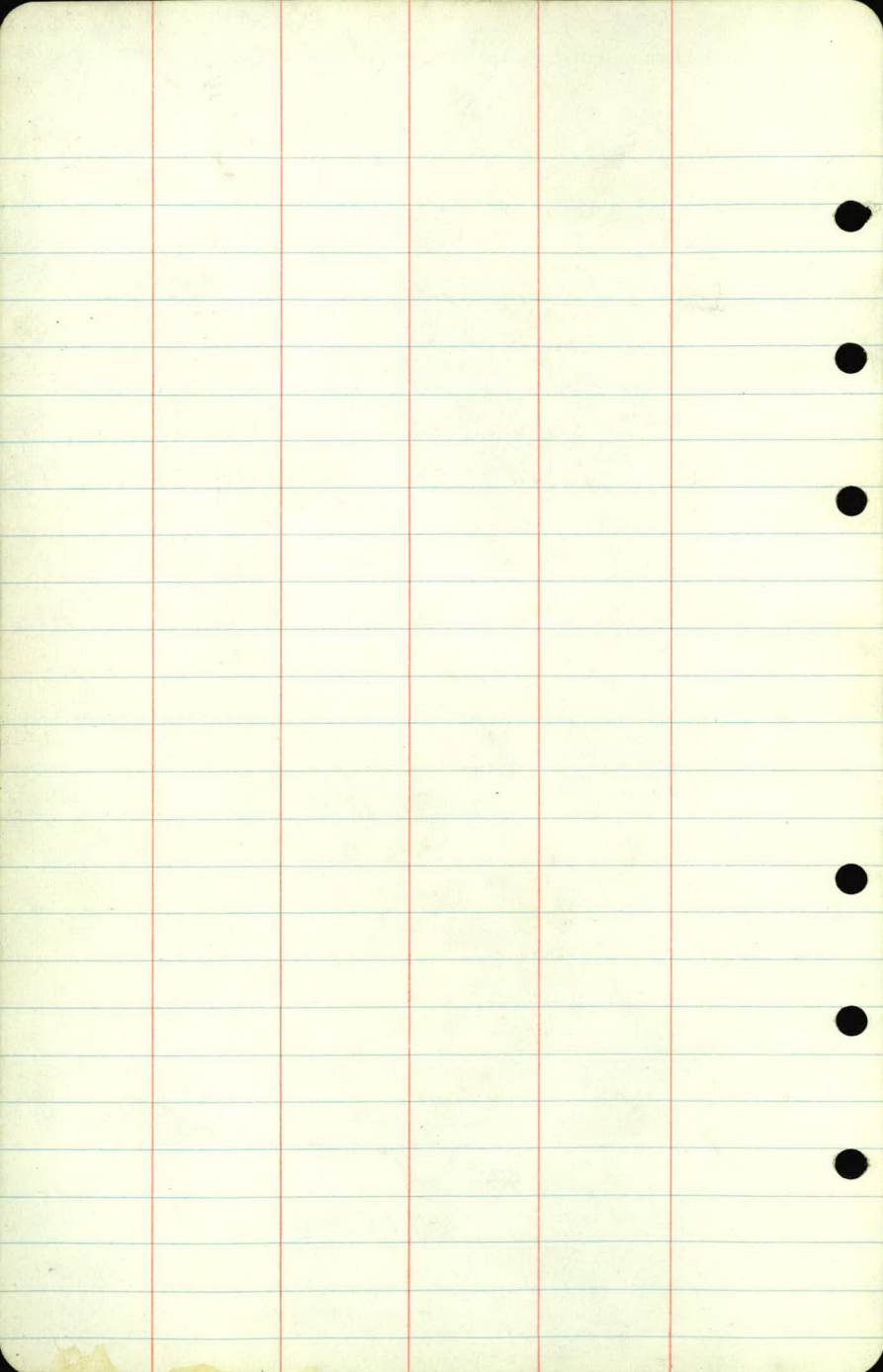
Spike in P.P. 28' Lt. Sta. 118+36
110 213
8+23

Spike in P.P. 27' Lt. Sta. 141+61
110 213
31 48

Pf	+	π	-	Elev
		941.73		
T.P.	116	932.24	10.65	931.08
B.M.	5.08	932.24	5.08	927.16
T.P.	0.17	920.58	11.83	920.41
T.P.	4.62	920.30	4.90	915.68
T.P.	2.27	916.06	6.51	913.79
B.M.			3.99	912.07

Top S.E. Cor. Conc. Step Rail 60' Lt. Sta. 157+80
100 13
47-67

Spike in P.P. N.W. Cor. Fairchild & Rice Cr. Rd.



Cross Sections

Fairchild Ave.

Co. Rd. "D" to Rice Creek Rd.

Sta.	+	π	-	Elev.
B.M.	13.07	972.32		959.25
T.P.	9.27	978.53	3.06	969.26
0+00			5.3	73.2
+15				
+18			6.3	72.2
+23			6.7	71.8
+50			8.6	69.9
1			10.6	68.2 67.9
+50			11.7	66.8
2			12.4	66.1
+50			12.8	65.7
3			13.0	65.5
+10			12.8	65.7
+66			11.2	67.3
4			9.9	69.6

Top Angle Iron Base E. Pier - NE Cor Fairchild & "D"

$$\frac{6.3}{50} \quad 5.3 \quad \frac{4.8}{50}$$

$$\frac{7.1}{50} \quad \frac{7.0}{27} \quad 6.3 \quad \frac{6.7}{26} \quad \frac{5.5}{50}$$

$$\frac{8.8}{50} \quad \frac{8.7}{27} \quad \frac{7.3}{19} \quad 6.7 \quad \frac{7.3}{18} \quad \frac{8.9}{20-22} \quad \frac{6.5}{26} \quad \frac{5.4}{33} \quad \frac{4.8}{50}$$

$$\frac{8.8}{50} \quad \frac{9.8}{27} \quad \frac{10.1}{23-20} \quad \frac{8.6}{15} \quad 8.6 \quad \frac{8.9}{12} \quad \frac{9.1}{19} \quad \frac{9.8}{21-22} \quad \frac{8.5}{26} \quad \frac{6.6}{33} \quad \frac{4.9}{50}$$

$$\frac{10.0}{50} \quad \frac{10.5}{43} \quad \frac{11.8}{25} \quad \frac{11.9}{19} \quad \frac{10.9}{14} \quad 10.6 \quad \frac{10.8}{13} \quad \frac{12.9}{16} \quad \frac{12.5}{27} \quad \frac{8.3}{35} \quad \frac{8.6}{50}$$

$$\frac{12.9}{50} \quad \frac{13.5}{39} \quad \frac{14.0}{30} \quad \frac{14.3}{19} \quad \frac{12.6}{10} \quad 11.7 \quad \frac{12.1}{14} \quad \frac{12.6}{18} \quad \frac{13.5}{23} \quad \frac{13.4}{30} \quad \frac{13.3}{39} \quad \frac{12.3}{50}$$

$$\frac{17.3}{50} \quad \frac{17.7}{40} \quad \frac{18.2}{34} \quad \frac{18.8}{26} \quad \frac{18.2}{21} \quad \frac{12.6}{10} \quad 12.4 \quad \frac{12.7}{12} \quad \frac{18.0}{21-26} \quad \frac{18.0}{30} \quad \frac{18.3}{50}$$

$$\frac{13.7}{10} \quad 12.8 \quad \frac{13.2}{11}$$

$$\frac{13.4}{10} \quad 13.0 \quad \frac{13.1}{11} \quad \frac{14.5}{27}$$

$$\frac{13.2}{10} \quad 12.8 \quad \frac{12.8}{11} \quad \frac{13.6}{14} \quad \frac{14.2}{27}$$

$$\frac{12.1}{15} \quad 11.2 \quad \frac{11.3}{16}$$

Sta + π - Elev

978.53

+4+43

8.7

69.8

+75

10.7

67.8

T.P. 512 970.74 12.91 965.62

T.P. 0.38 958.38 12.74 958.00

T.P. 9.19 954.73 12.84 945.54

2+50

+11.0 65.7

3

+10.8 65.5

+10

+11.0 65.7

+66

+12.0 67.3

4+05

8.1

46.5

+11.5

8.25

46.48

+16.8

8.53

46.30

+29.5

8.73

46.00

+34.8

8.94

45.79

+40

9.2

45.50

+75

+13.1 47.8

5

+11.3 66.0

(11.0)

$$\begin{array}{r} 0.5 \\ 37 \\ \hline \end{array} \quad \begin{array}{r} 0.0 \\ 50 \\ \hline \end{array}$$

(10.8)

$$\begin{array}{r} 5.8 \\ 50 \\ \hline \end{array} \quad \begin{array}{r} 5.9 \\ 68 \\ \hline \end{array}$$

(11.0)

$$\begin{array}{r} 8.0 \\ 60 \\ \hline \end{array} \quad \begin{array}{r} 8.3 \\ 75 \\ \hline \end{array}$$

(12.6)

$$\begin{array}{r} 5.3 \\ 44 \\ \hline \end{array} \quad \begin{array}{r} 5.6 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 8.6 \\ 50 \\ \hline \end{array} \quad \begin{array}{r} 8.2 \\ 21 \\ \hline \end{array} \quad \begin{array}{r} 8.3 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} 9.3 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 9.1 \\ 50 \\ \hline \end{array}$$

9.2

$$\begin{array}{r} 9.8 \\ 50 \\ \hline \end{array}$$

(13.1)

$$\begin{array}{r} 6.6 \\ 44 \\ \hline \end{array} \quad \begin{array}{r} 7.1 \\ 51 \\ \hline \end{array}$$

(11.3)

$$\begin{array}{r} 6.5 \\ 42 \\ \hline \end{array} \quad \begin{array}{r} 7.8 \\ 52 \\ \hline \end{array}$$

Sta.	+	π	-	Elev.
		954.73 [✓]	951	
5+50				+07.6 62.3
6				+04.1 58.8
+50				+01.0 55.7
T.P.	10.66	956.20 [✓]	919	945.54 [✓]
2+50				+09.5 [✓] 65.7
3				+09.3 65.5
+10				+09.5 [✓] 65.7
+66				+11.1 67.3
4+75				+11.0 67.8
5				+09.8 66.0
+50				+06.1 62.3
6				+02.6 58.8
+50				-00.5 55.7
T.P.	12.18	968.38 [✓]	0.00	956.20 [✓]

(7.6)

 $\frac{4.4}{36}$ $\frac{7.2}{44}$ $\frac{7.9}{55}$

(4.1)

 $\frac{4.7}{34}$ $\frac{7.2}{44}$ $\frac{7.1}{55}$

(01.0)

 $\frac{12.4}{40}$ $\frac{14.0}{50}$
 $\frac{0.5}{50}$ $\frac{0.0}{41}$ $\frac{0.0}{29}$ $\frac{+0.3}{23}$

(09.5)

 $\frac{2.9}{50}$ $\frac{4.4}{40}$ $\frac{4.2}{34}$ $\frac{3.3}{31}$

(09.3)

 $\frac{5.6}{50}$ $\frac{5.2}{44}$ $\frac{5.3}{37}$

(09.5)

 $\frac{9.6}{50}$ $\frac{9.2}{46}$

(11.1)

 $\frac{11.6}{65}$ $\frac{10.4}{55}$ $\frac{7.7}{43}$

(11.6)

 $\frac{12.0}{59}$ $\frac{10.9}{53}$ $\frac{8.5}{41}$

(9.8)

 $\frac{12.3}{52}$ $\frac{11.5}{46}$ $\frac{9.0}{37}$

(6.1)

 $\frac{12.8}{50}$ $\frac{12.2}{38}$ $\frac{11.3}{33}$

(2.6)

 $\frac{16.1}{50}$ $\frac{14.8}{33}$

(00.5)

Sta	T	π	-	Elev.
		968.38 ✓		660 659
5			2.4	
	+50		6.1	62.3.
6			9.6	58.8.
	+50		12.7	55.7.
T.P.	2.43	957.65 ✓	13.16	955.22 ✓
7			4.1	53.4.
	+34		4.7	53.0.
	+84		5.0	52.7.
8			5.1	52.6.
	+22		5.0	52.7.
	+50		5.2	52.5.
9			5.4	52.3.
	+60		5.5	52.2.

$$\frac{2.6}{12} \quad 2.4 \quad \frac{2.4}{9} \quad \frac{3.0}{12}$$

$$\frac{6.3}{12} \quad 6.1 \quad \frac{6.2}{12}$$

$$\frac{10.0}{13} \quad 9.6 \quad \frac{9.5}{12}$$

$$\frac{13.0}{13} \quad 12.7 \quad \frac{12.9}{10}$$

$$\frac{17.1}{50} \quad \frac{18.3}{38} \quad \frac{17.1}{32} \quad \frac{4.2}{13} \quad 4.1 \quad \frac{4.5}{8} \quad \frac{18.1}{30} \quad \frac{19.0}{47} \quad \frac{19.3}{60}$$

$$\frac{17.3}{50} \quad \left(\frac{F.L.}{19.3} \right) \quad \frac{37}{29} \quad \frac{4.8}{11} \quad 4.7 \quad \frac{4.9}{9} \quad \frac{18.0}{30} \quad \left(\frac{F.L.}{20.1} \right) \quad \frac{18.6}{50}$$

$$\frac{7.0}{50} \quad \frac{5.2}{11} \quad 5.5 \quad \frac{5.2}{10} \quad \frac{18.6}{30} \quad \frac{19.0}{50} \quad \text{Note - Section on Left Hand Dumps}$$

$$\frac{7.0}{50} \quad \frac{5.2}{11} \quad 5.1 \quad \frac{5.2}{9} \quad \frac{15.4}{29} \quad \frac{16.1}{30}$$

$$\frac{5.9}{50} \quad \frac{6.0}{28} \quad \frac{6.1}{18} \quad \frac{5.1}{12} \quad 5.0 \quad \frac{5.1}{9} \quad \frac{11.6}{20} \quad \frac{11.7}{30} \quad \frac{11.6}{50}$$

$$\frac{6.3}{50} \quad \frac{6.9}{32} \quad \frac{7.5}{26} \quad \frac{6.4}{16} \quad \frac{5.3}{13} \quad \frac{5.2}{9} \quad \frac{8.6}{14} \quad \frac{9.7}{20} \quad \frac{6.2}{29} \quad \frac{7.0}{50}$$

$$\frac{6.5}{50} \quad \frac{7.1}{25} \quad \frac{6.7}{22} \quad \frac{5.2}{16} \quad 5.4 \quad \frac{5.6}{8} \quad \frac{6.5}{14} \quad \frac{7.2}{29} \quad \frac{7.0}{50}$$

$$\frac{5.6}{50} \quad \frac{6.2}{31} \quad \frac{6.7}{24} \quad \frac{6.8}{21} \quad \frac{5.6}{16} \quad 5.5 \quad \frac{5.6}{13} \quad \frac{7.8}{18} \quad \frac{7.8}{17} \quad \frac{7.2}{32} \quad \frac{9.2}{50}$$

Sta	+	π	-	Elev.
		959.65 ✓		
+75		c	5.4	52.3.
10			5.3	52.4.
+50			5.1	52.6.
11			4.3	53.4.
T.P.	722	961.28 ✓	3.59	954.02 ✓
+50			7.8	53.5.
12			8.2	53.1.
+50			8.3	53.0.
+76			8.4	52.9.
+83			8.4	52.9.
+87			8.4	52.9.
+92			8.4	52.9.
13+07			8.8	52.5.

$$\begin{array}{r} 5.3 \quad 6.7 \quad 7.0 \quad 5.8 \quad 5.7 \quad 7.2 \quad 7.9 \quad 5.1 \quad 5.4 \quad 7.9 \\ 50 \quad 23 \quad 16 \quad 12 \quad 5.4 \quad 11 \quad 14 \quad 22 \quad 31 \quad 35 \quad 50 \end{array}$$

$$\begin{array}{r} 4.9 \quad 6.4 \quad 6.6 \quad 5.7 \quad 6.0 \quad 7.0 \quad 7.2 \quad 4.6 \quad 7.0 \\ 50 \quad 24 \quad 19 \quad 17 \quad 14 \quad 5.3 \quad 12 \quad 16 \quad 21 \quad 31 \quad 50 \end{array}$$

$$\begin{array}{r} 4.2 \quad 5.3 \quad 5.7 \quad 6.0 \quad 5.2 \quad 5.8 \quad 6.9 \quad 6.1 \quad 4.9 \quad 8.8 \quad 11.7 \\ 50 \quad 27 \quad 20 \quad 17 \quad 13 \quad 5.1 \quad 13 \quad 17 \quad 21 \quad 26 \quad 38 \quad 50 \end{array}$$

$$\begin{array}{r} 3.3 \\ 50 \end{array}$$

$$43 \quad \begin{array}{r} 4.8 \quad 4.9 \quad 4.7 \quad 1.8 \quad 2.3 \quad 7.2 \\ 10 \quad 16 \quad 19 \quad 26 \quad 34 \quad 50 \end{array}$$

$$\begin{array}{r} 6.1 \quad 6.5 \quad 7.1 \quad 7.5 \quad 8.1 \quad 6.7 \quad 3.3 \quad 3.3 \quad 4.2 \\ 50 \quad 34 \quad 22 \quad 19 \quad 7.8 \quad 17 \quad 24 \quad 27 \quad 40 \quad 50 \end{array}$$

$$\begin{array}{r} 6.3 \quad 7.2 \quad 8.0 \quad 8.2 \quad 8.2 \quad 4.9 \quad 3.7 \quad 3.8 \\ 50 \quad 21 \quad 18 \quad 15 \quad 8.2 \quad 7.0 \quad 15 \quad 24 \quad 50 \end{array}$$

$$\begin{array}{r} 4.3 \quad 5.6 \quad 7.0 \quad 8.7 \quad 8.5 \quad 8.3 \quad 6.9 \quad 6.3 \quad 4.1 \\ 50 \quad 30 \quad 22 \quad 16 \quad 13 \quad 8.3 \quad 11 \quad 17 \quad 25 \quad 50 \end{array}$$

$$\begin{array}{r} 4.5 \quad 4.7 \quad 5.8 \quad 7.9 \quad 9.2 \quad 8.7 \quad 8.8 \quad 7.9 \quad 7.3 \quad 5.1 \\ 50 \quad 30 \quad 25 \quad 19 \quad 16 \quad 13 \quad 8.4 \quad 13 \quad 18 \quad 26 \quad 50 \end{array}$$

$$\begin{array}{r} 4.5 \quad 4.8 \quad 5.7 \quad 7.8 \quad 9.3 \quad 8.7 \quad 9.4 \quad 9.6 \quad 9.6 \quad 7.7 \\ 50 \quad 29 \quad 26 \quad 20 \quad 16 \quad 13 \quad 8.4 \quad 14 \quad 21 \quad 33 \quad 50 \end{array}$$

$$\begin{array}{r} 4.4 \quad 4.7 \quad 5.8 \quad 7.9 \quad 9.2 \quad 8.7 \quad 9.2 \quad 9.7 \quad 9.7 \quad 9.9 \\ 50 \quad 30 \quad 25 \quad 19 \quad 16 \quad 13 \quad 8.4 \quad 16 \quad 23 \quad 32 \quad 50 \end{array}$$

$$\begin{array}{r} 4.6 \quad 4.9 \quad 5.7 \quad 8.0 \quad 9.2 \quad 8.7 \\ 50 \quad 31 \quad 26 \quad 20 \quad 16 \quad 13 \quad 8.4 \end{array}$$

$$\begin{array}{r} 8.6 \quad 8.1 \\ 23 \quad 50 \end{array}$$

$$\begin{array}{r} 4.2 \quad 5.8 \quad 7.1 \quad 8.7 \quad 9.8 \quad 9.1 \quad 9.1 \quad 8.8 \\ 50 \quad 33 \quad 27 \quad 19 \quad 16 \quad 15 \quad 12 \quad 9 \end{array}$$

$$\begin{array}{r} 7.9 \\ 50 \end{array} \text{ \& Sunset Blvd}$$

Sta	+	↑	-	Elev.
		961.28		
13+20			9.0	52.3
+24			9.0	52.3
+28			9.1	52.2
+34			9.3	52.0
+50			9.6	51.7
B.M.	2.05	954.96	8.36	952.92 (952.91)
14			4.3	50.7
+50			5.4	49.6
15			6.6	48.4
+50			7.7	47.3
16			8.5	46.5
+50			9.4	45.6
17			10.0	45.0

$\frac{4.9}{50} \frac{6.1}{40} \frac{7.2}{30} \frac{8.3}{26} \frac{9.1}{20} \frac{10.3}{16-15} \frac{9.3}{11} \frac{9.1}{12} \frac{9.0}{24} \frac{8.3}{50}$

$\frac{4.9}{50} \frac{7.2}{30} \frac{8.2}{26} \frac{9.0}{20} \frac{10.3}{16-17} \frac{9.3}{10} \frac{9.0}{12} \frac{9.8}{15} \frac{9.4}{50}$

$\frac{4.8}{50} \frac{6.1}{40} \frac{8.3}{26} \frac{9.2}{20} \frac{10.3}{16-15} \frac{9.3}{11} \frac{9.1}{12} \frac{9.5}{16} \frac{9.8}{30} \frac{9.5}{50}$

$\frac{5.7}{50} \frac{6.2}{41} \frac{8.1}{28} \frac{9.0}{20} \frac{10.0}{17-16} \frac{9.5}{13} \frac{9.6}{12} \frac{10.0}{17} \frac{8.2}{29} \frac{6.2}{50}$

$\frac{5.8}{50} \frac{7.0}{36} \frac{9.0}{23} \frac{9.3}{19} \frac{10.4}{16-15} \frac{10.1}{13} \frac{9.6}{12} \frac{10.0}{18} \frac{9.3}{31} \frac{8.4}{31} \frac{6.4}{50}$

Spike in PP 14' Rt 5 to 9.13 + 35

$\frac{0.8}{50} \frac{1.6}{32} \frac{2.4}{24} \frac{3.7}{19} \frac{4.7}{14} \frac{4.5}{12} \frac{4.7}{43} \frac{4.5}{16} \frac{3.6}{22} \frac{1.6}{32} \frac{1.6}{50}$

$\frac{3.2}{50} \frac{2.9}{31} \frac{3.7}{23} \frac{3.9}{18} \frac{5.5}{16} \frac{5.9}{11} \frac{5.5}{54} \frac{6.0}{13} \frac{6.3}{17} \frac{6.4}{24} \frac{4.5}{50}$

$\frac{5.4}{50} \frac{5.9}{23} \frac{5.7}{19} \frac{7.3}{16} \frac{7.0}{12} \frac{6.7}{7} \frac{7.1}{6.4} \frac{8.2}{12} \frac{7.4}{15-17} \frac{7.8}{19} \frac{7.5}{32} \frac{7.5}{50}$

$\frac{6.5}{50} \frac{6.9}{39} \frac{6.2}{29} \frac{7.2}{23} \frac{6.8}{17} \frac{8.2}{16} \frac{8.1}{12} \frac{8.3}{7.7} \frac{9.4}{12} \frac{8.4}{16-17} \frac{8.9}{20} \frac{8.6}{33} \frac{8.6}{50}$

$\frac{7.0}{50} \frac{7.7}{40} \frac{7.2}{30} \frac{8.3}{21} \frac{9.5}{16-14} \frac{8.8}{11} \frac{8.6}{8} \frac{9.0}{8.5} \frac{10.3}{13} \frac{9.5}{16-18} \frac{9.5}{21} \frac{9.2}{33} \frac{9.2}{50}$

$\frac{8.0}{50} \frac{8.7}{31} \frac{8.8}{20} \frac{10.1}{16-14} \frac{9.6}{12} \frac{9.3}{10} \frac{9.4}{9.4} \frac{10.5}{13} \frac{10.1}{17-19} \frac{10.2}{21} \frac{9.6}{33} \frac{9.6}{50}$

$\frac{7.9}{50} \frac{9.7}{23} \frac{9.0}{18} \frac{10.8}{16-14} \frac{10.0}{10} \frac{9.9}{5} \frac{10.3}{10.0} \frac{11.2}{13} \frac{10.9}{15-16} \frac{11.2}{20} \frac{10.9}{32} \frac{10.9}{50}$

Sta	+	π	-	Elev
		954.96		
17+50			10.5	445.
18			11.4	436.
T.P.	1.90	946.71	10.15	944.81.
+50			3.8	429.
19			4.3	42.4.
+50			4.7	42.0.
+71			5.0	41.7.
20			5.0	41.7.
+50			5.4	41.3.
21			5.5	41.2.
+50			5.7	41.0.
22			6.2	40.5.
+50			6.6	40.1.

$\frac{9.1}{50}$	$\frac{9.9}{28}$	$\frac{10.6}{19}$	$\frac{11.1}{14-13}$	$\frac{10.8}{11}$	$\frac{10.9}{10.5}$	$\frac{11.8}{12}$	$\frac{11.6}{15.16}$	$\frac{11.6}{19}$	$\frac{11.6}{31}$	$\frac{10.9}{50}$
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$\frac{10.1}{50}$	$\frac{10.7}{37}$	$\frac{11.4}{23}$	$\frac{11.4}{17}$	$\frac{12.0}{13}$	$\frac{11.2}{9}$	$\frac{11.4}{11.4}$	$\frac{11.5}{12}$	$\frac{11.8}{16}$	$\frac{11.2}{27}$	$\frac{11.0}{50}$
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$\frac{2.9}{50}$ $\frac{3.6}{31}$ $\frac{4.2}{22}$ $\frac{4.5}{16}$ $\frac{4.2}{12}$ $\frac{4.0}{12}$ $\frac{4.7}{15}$ $\frac{4.0}{17}$ $\frac{3.9}{22}$ $\frac{3.9}{26}$ $\frac{2.4}{50}$

<u>8.4</u>	<u>3.5</u>	<u>4.5</u>	<u>4.3</u>	<u>4.7</u>	<u>4.6</u>	<u>4.9</u>	<u>5.4</u>	<u>5.0</u>	<u>4.9</u>	<u>4.5</u>	<u>4.1</u>		
50	39	28	21	13	9	4	3	12	15	18	29	37	50

$\frac{3.6}{50}$	$\frac{4.2}{26}$	$\frac{4.7}{17}$	$\frac{5.0}{9}$	$\frac{5.3}{14}$	$\frac{5.8}{18}$	$\frac{6.1}{22}$	$\frac{6.3}{27}$	$\frac{5.6}{36}$	$\frac{5.5}{50}$
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$\frac{3.3}{50}$	$\frac{4.8}{22}$	$\frac{5.2}{77}$	$\frac{6.0}{14}$	$\frac{5.3}{12}$	$\frac{5.0}{11}$	5.0	$\frac{5.6}{14}$	$\frac{6.2}{16}$	$\frac{6.3}{21}$	$\frac{6.5}{25}$	$\frac{6.5}{28}$	$\frac{5.9}{50}$
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$\frac{2.3}{.50}$	$\frac{2.9}{4}$	$\frac{3.4}{29}$	$\frac{5.7}{24}$	$\frac{5.8}{20}$	$\frac{5.4}{14}$	$\frac{5.5}{T3}$	$\frac{6.3}{16}$	$\frac{6.6}{19}$	$\frac{6.7}{21}$	$\frac{6.8}{27}$	$\frac{6.2}{50}$
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<u>2.5</u>	<u>4.0</u>	<u>5.8</u>	<u>5.8</u>	<u>5.8</u>	<u>5.6</u>	<u>5.5</u>		<u>5.9</u>	<u>7.1</u>	<u>7.1</u>	<u>7.1</u>	<u>7.3</u>
50	28	25	21	16	12	9	3.4	15	19	24	31	50

3.7	4.2	4.2	6.0	6.1	5.6	5.3	6.1	7.2	7.3	7.5	8.0
50	31	27	21	15	11	7	5.6	13	17	23	30

$\frac{4.4}{.50} \frac{4.7}{29} \frac{5.9}{22} \frac{6.2}{16} \frac{6.2}{18-11} \frac{5.8}{10} 5.7 \frac{6.3}{14} \frac{7.2}{21} \frac{7.6}{34} \frac{8.2}{50}$

$\frac{5.0}{50}$	$\frac{5.3}{25}$	$\frac{6.8}{20}$	$\frac{6.7}{14}$	$\frac{6.2}{8}$		$\frac{6.6}{12}$	$\frac{7.8}{16}$	$\frac{7.6}{22}$	$\frac{7.7}{50}$
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$\frac{5.8}{50}$	$\frac{6.1}{33}$	$\frac{7.0}{23}$	$\frac{7.4}{18}$	$\frac{7.3}{15}$	$\frac{6.7}{11}$	6.6	$\frac{6.9}{12}$	$\frac{8.0}{17}$	$\frac{8.0}{22}$	$\frac{8.3}{29}$	$\frac{8.5}{50}$
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Sta	+	π	-	Elev
		946.71		
23+00			6.9	39.8
+50			7.2	39.5
T.P.	7.53	947.07	7.17	939.54
+97			7.6	39.5
24+50			7.5	39.6
25			7.2	39.9
+50			6.4	40.7
+90			5.5	41.6
+95			5.4	41.7
26			5.2	41.9
+16			5.1	42.0
+30			5.0	42.1
+35			5.0	42.1

5.5 6.6 7.7 7.6 7.1 7.3 9.1 9.5 9.3 9.6
50 29 19 14 11 13 18 24 33 50

7.6 8.2 8.7 8.6 8.6 8.2 7.7 7.7 10.2 10.3 10.5 10.7
50 42 29 23 18 15 14 12 18 23 35 50

FL. FL.
9.2 9.6 9.6 10.0 10.3 8.1 8.2 10.9 11.2 12.0 11.2 11.5
50 34 21 18 18 14 13 16 16 20 26 50

9.3 9.4 8.8 9.4 7.8 7.8 8.9 10.1 10.2 10.3
50 32 22 18 12 7.5 12 18 20 27 50

9.0 9.4 9.4 7.9 8.0 7.5 7.6 10.6 10.3 10.3
50 32 25 17 13 10 7.2 13 20-24 28 50

7.7 8.6 8.6 8.8 6.7 6.9 8.7 10.2 9.8 10.0
50 31 22 17 11 6.4 12 16 19-21 26 50

5.3 6.4 6.7 6.4 6.3 5.9 8.6 8.3 9.3 9.0
50 33 28 21 14 5.5 13 19-18 26 45 50

6.8 7.1 6.1 5.7 8.4 8.2 9.2
50 33 19 13 19-20 26 50

5.6 5.8 5.7 7.8 8.0 8.2 8.3
50 33 5.2 13 18-20 30 40 50

4 Silver L. Ed. 4.9 5.4 6.8 6.2 7.12
50 13 18-20 22 50

4.7 4.8 5.3 5.9 6.0 6.3
50 33 5.0 14 19 35 50

6.5 6.4 5.6 5.2 5.7 5.4 5.7 5.3
50 33 22 5.0 13 17 21 30 50

Sta	+	Σ	-	Elev.
		947.07		
26+42			4.9	42.2
B.M.			2.64	944.43
+68			4.7	42.4
T.P.	8.19	953.20	2.06	945.01
27			10.4	42.8
+50			9.9	43.3
28			9.7	43.5
+50			9.5	43.7
29			9.1	44.1
+29			9.1	44.1
+61			9.3	43.9
T.P.	3.97	947.14	10.03	943.17
30			3.8	43.3
+29			4.2	42.9
+65			4.7	42.4

$\frac{4.3}{50}$ $\frac{5.1}{22}$ $\frac{5.7}{14}$ 4.9 $\frac{5.2}{13}$ $\frac{5.4}{16}$ $\frac{5.2}{20}$ $\frac{4.2}{50}$

spike in 14" Oak 24' Lt Sta 26+79

$\frac{5.3}{50}$ $\frac{4.6}{33}$ $\frac{4.1}{16}$ $\frac{5.0}{13}$ $\frac{5.0}{10}$ 4.7 $\frac{5.0}{14}$ $\frac{5.1}{18}$ $\frac{3.4}{22}$ $\frac{2.8}{27}$ $\frac{0.0}{50}$

$\frac{11.4}{50}$ $\frac{9.7}{34}$ $\frac{9.3}{25}$ $\frac{8.1}{20}$ $\frac{11.1}{15}$ $\frac{11.2}{12}$ $\frac{10.6}{10}$ 10.4 $\frac{10.8}{13}$ $\frac{10.7}{19}$ $\frac{5.6}{29}$ $\frac{2.9}{50}$

$\frac{12.3}{50}$ $\frac{11.3}{36}$ $\frac{10.6}{30}$ $\frac{9.3}{22}$ $\frac{9.1}{19}$ $\frac{10.8}{13.11}$ $\frac{10.2}{8}$ 9.9 $\frac{10.2}{14}$ $\frac{10.4}{17}$ $\frac{9.8}{19}$ $\frac{4.3}{31}$ $\frac{2.6}{50}$

$\frac{10.5}{50}$ $\frac{9.6}{31}$ $\frac{8.4}{21}$ $\frac{11.0}{14}$ $\frac{10.2}{12}$ 9.7 $\frac{10.1}{13}$ $\frac{9.9}{16}$ $\frac{6.3}{29}$ $\frac{6.4}{50}$

$\frac{9.3}{50}$ $\frac{8.7}{31}$ $\frac{8.3}{26}$ $\frac{7.9}{22}$ $\frac{9.5}{16}$ $\frac{10.2}{14.12}$ $\frac{9.5}{10}$ 9.5 $\frac{9.8}{16}$ $\frac{5.1}{29}$ $\frac{5.5}{50}$

$\frac{6.6}{50}$ $\frac{6.4}{39}$ $\frac{7.0}{25}$ $\frac{7.1}{20}$ $\frac{9.0}{16}$ $\frac{9.7}{14}$ $\frac{9.1}{13}$ 9.1 $\frac{9.7}{13}$ $\frac{10.5}{17}$ $\frac{5.7}{28}$ $\frac{4.8}{37}$ $\frac{4.6}{50}$

$\frac{8.3}{50}$ $\frac{7.3}{34}$ $\frac{6.8}{25}$ $\frac{6.7}{22}$ $\frac{7.7}{18}$ $\frac{9.6}{15}$ $\frac{9.4}{9}$ 9.1 $\frac{9.2}{14}$ $\frac{10.1}{17.19}$ $\frac{6.0}{28}$ $\frac{4.8}{38}$ $\frac{4.3}{50}$

$\frac{11.8}{50}$ $\frac{11.4}{41}$ $\frac{10.8}{31}$ $\frac{9.6}{23}$ $\frac{9.4}{22}$ $\frac{9.5}{17}$ $\frac{10.1}{13}$ $\frac{9.5}{11}$ 9.3 $\frac{9.6}{14}$ $\frac{9.6}{18}$ $\frac{9.1}{23}$ $\frac{9.3}{29}$ $\frac{9.3}{50}$

$\frac{8.7}{50}$ $\frac{8.2}{46}$ $\frac{7.1}{38}$ $\frac{6.4}{30}$ $\frac{5.9}{22}$ $\frac{5.5}{18.15}$ $\frac{4.4}{12}$ $\frac{3.1}{8}$ $\frac{4.0}{14}$ $\frac{4.0}{20}$ $\frac{4.0}{24}$ $\frac{4.6}{30}$ $\frac{3.6}{50}$

$\frac{9.1}{50}$ $\frac{8.3}{40}$ $\frac{7.5}{30}$ $\frac{6.5}{23}$ $\frac{6.2}{18}$ $\frac{4.7}{11}$ $\frac{4.4}{4.2}$ $\frac{4.8}{13}$ $\frac{4.9}{17}$ $\frac{2.2}{27}$ $\frac{1.8}{33}$ $\frac{1.8}{50}$

$\frac{8.9}{50}$ $\frac{7.5}{39}$ $\frac{7.5}{26}$ $\frac{7.1}{23}$ $\frac{7.0}{19}$ $\frac{6.5}{15}$ $\frac{5.2}{11}$ 4.7 $\frac{5.1}{15}$ $\frac{6.0}{19}$ $\frac{5.6}{23}$ $\frac{4.6}{30}$ $\frac{3.6}{50}$

Sta + K - Elev

947.14

31 5.1 420.

+50 5.6 41.5.

32 6.5 40.6.

B.M. 7.34 939.80. 939.79

+50 7.6 39.5.

33 8.2 38.9.

+37 Culv. 8.5 38.6.

34 8.1 39.0.

+50 7.4 39.7.

T.P. 12.32 954.35. 5.11 942.03.

35 13.6 40.8.

+43 12.6 41.8.

36 11.3 43.1.

+50 10.9 43.5.

47 14
39 79
7 35

49

8.2 7.9 6.8 6.7 6.1 5.9 5.4 5.9 6.2 5.9 5.2 4.5
50 45 50 25 20 15 12 5 14 17 19 22 26 50

9.2 8.3 7.4 6.4 6.7 5.8 5.9 6.1 6.5 5.8 4.6 3.3
50 37 27 18 16 15 11 5.6 13 18 17 20 24 31 50

13.8 12.6 11.6 11.2 6.7 6.4 5.7
50 37 26 20 9 16 50

3pike in PP. 26' RT 50. 32+61

15.2 14.8 14.0 7.8 8.0 8.9 9.1 9.1 6.5
50 27 19 9 7.6 16 19 21 26 33 50

15.2 15.2 14.9 8.6 8.8 9.8 10.1 9.8
50 26 17 9 8.2 15 19 35 50

15.2 15.2 15.2 15.2 14.1 8.9 9.0 14.4 11.7 10.8 10.5 10.2
50 32 24 17 17 8 8.5 16 17 18 23 40 50

15.2 15.0 15.0 8.5 8.7 10.3 9.9 9.6 10.7
50 33 19 9 8.1 13 17 22 29 50

10.7 10.4 10.1 7.8 7.8 8.7 9.4 9.1 10.2
50 35 17 7 7.4 13 16 17-18 28 50

12.2 11.4 12.8 14.9 14.0 14.2 15.0 14.6 14.6
50 36 22 17-15 10 13.6 12 17 32 50

6.7 5.7 8.3 13.2 13.6 13.0 13.5 14.4 13.4 12.4 12.3
50 33 24 16 13 8 12.6 14 19 25 33 50

4.6 4.1 7.4 10.2 11.9 11.6 11.9 12.6 11.0 10.1 8.9
50 30 23 17 13 9 11.3 14 18-19 26 34 50

4.7 3.8 7.3 10.2 11.2 11.0 11.5 12.6 12.1 9.4 7.4
50 30 32 18 12 8 10.9 14 18 23 31 50

54

+

 π

-

Elev

954.35 ✓

37

11.5

42.9.

+50

12.8

41.6.

38

14.4

40.0. ✓

T.P.

2.33

943.99. ✓

12.69

941.66. ✓

+50

5.4

38.6.

39

6.4

37.6. ✓

+60

7.4

36.6.

40

8.0

36.0. ✓

B.M.

8.13

935.86. ✓

(935.86)

+50

8.5

35.5. ✓

41

8.8

35.2. ✓

+50

9.0

35.0. ✓

42

9.0

35.0. ✓

T.P.

5.74

940.60. ✓

9.13

934.86. ✓

+50

5.6

35.0. ✓

$\frac{5.2}{50}$ $\frac{4.9}{30}$ $\frac{9.3}{22}$ $\frac{11.9}{17}$ $\frac{11.8}{11}$ $\frac{12.1}{11.5}$ $\frac{13.4}{13}$ $\frac{13.1}{18}$ $\frac{10.7}{25}$ $\frac{8.8}{32}$ $\frac{8.8}{50}$

$\frac{6.4}{50}$ $\frac{8.1}{30}$ $\frac{11.5}{23}$ $\frac{13.4}{19}$ $\frac{13.6}{15}$ $\frac{13.0}{7}$ $\frac{13.4}{15}$ $\frac{13.8}{18}$ $\frac{14.2}{24}$ $\frac{12.5}{32}$ $\frac{12.4}{50}$

$\frac{11.6}{50}$ $\frac{12.3}{39}$ $\frac{15.1}{31}$ $\frac{14.9}{10}$ $\frac{14.4}{14}$ $\frac{14.9}{14}$ $\frac{16.1}{18}$ $\frac{16.0}{23}$ $\frac{15.1}{31}$ $\frac{14.9}{50}$

$\frac{3.8}{50}$ $\frac{4.9}{32}$ $\frac{6.9}{26}$ $\frac{7.2}{21}$ $\frac{6.3}{16}$ $\frac{5.6}{11}$ $\frac{5.4}{15}$ $\frac{6.8}{19}$ $\frac{6.7}{24}$ $\frac{6.7}{32}$ $\frac{6.6}{45}$ $\frac{6.3}{50}$

$\frac{5.5}{50}$ $\frac{6.1}{39}$ $\frac{6.8}{30}$ $\frac{7.5}{25}$ $\frac{6.6}{11}$ $\frac{6.4}{6.4}$ $\frac{7.0}{9}$ $\frac{8.0}{15}$ $\frac{7.2}{21}$ $\frac{8.0}{26}$ $\frac{7.7}{33}$ $\frac{7.7}{50}$

$\frac{10.4}{50}$ $\frac{11.0}{30}$ $\frac{9.8}{22}$ $\frac{9.2}{16}$ $\frac{7.9}{8}$ $\frac{7.4}{7.4}$ $\frac{7.4}{7}$ $\frac{7.9}{15}$ $\frac{10.1}{20}$ $\frac{10.2}{23}$ $\frac{11.4}{33}$ $\frac{11.4}{50}$

$\frac{11.6}{50}$ $\frac{11.9}{34}$ $\frac{12.0}{19}$ $\frac{11.1}{14}$ $\frac{8.6}{10}$ $\frac{8.2}{8.0}$ $\frac{10.2}{15}$ $\frac{11.7}{20}$ $\frac{11.7}{33}$ $\frac{11.7}{50}$

Spike in P.P. 27' Rt. Sta. 40 + 35

$\frac{11.7}{50}$ $\frac{12.4}{33}$ $\frac{12.3}{23}$ $\frac{11.8}{16}$ $\frac{9.2}{11}$ $\frac{8.8}{8.5}$ $\frac{10.4}{14}$ $\frac{10.7}{19}$ $\frac{11.9}{21}$ $\frac{11.7}{33}$ $\frac{11.7}{50}$

$\frac{11.7}{50}$ $\frac{11.8}{40}$ $\frac{11.9}{24}$ $\frac{12.0}{17}$ $\frac{9.4}{10}$ $\frac{8.8}{8.8}$ $\frac{9.3}{15}$ $\frac{9.8}{18}$ $\frac{9.9}{24}$ $\frac{11.5}{28}$ $\frac{11.9}{33}$ $\frac{11.6}{50}$

$\frac{11.8}{50}$ $\frac{12.1}{27}$ $\frac{11.8}{21}$ $\frac{11.7}{17}$ $\frac{9.5}{11}$ $\frac{9.0}{9.0}$ $\frac{9.6}{15}$ $\frac{10.6}{18}$ $\frac{10.9}{21}$ $\frac{10.2}{24}$ $\frac{11.4}{28}$ $\frac{12.0}{34}$ $\frac{12.0}{50}$

$\frac{11.7}{50}$ $\frac{11.7}{33}$ $\frac{11.8}{21}$ $\frac{11.6}{14}$ $\frac{9.4}{10}$ $\frac{9.0}{9.0}$ $\frac{9.7}{14}$ $\frac{10.6}{17}$ $\frac{10.4}{21}$ $\frac{10.1}{24}$ $\frac{12.1}{34}$ $\frac{11.6}{50}$

$\frac{8.5}{50}$ $\frac{8.5}{39}$ $\frac{8.5}{28}$ $\frac{8.5}{20}$ $\frac{8.2}{15}$ $\frac{6.4}{12}$ $\frac{5.6}{5.6}$ $\frac{6.3}{14}$ $\frac{7.0}{16}$ $\frac{7.3}{18}$ $\frac{6.8}{22}$ $\frac{6.3}{24}$ $\frac{8.8}{31}$ $\frac{8.8}{50}$

Sta	+	π	-	Elev.
		940.60		
43			5.2	35.4
+50			5.0	35.6
44			4.8	35.8
T.P.	7.05	942.37	5.28	935.32
+50			6.4	36.0
45			6.2	36.2
+50			5.6	36.8
46			4.4	38.0
+50			3.2	39.2
47			2.3	40.1
+50			1.8	40.6
T.P.	13.06	955.38	0.05	942.32
46+50				(16.2) 39.2
47				(15.3) 40.1

$\frac{8.1}{50}$ $\frac{8.1}{33}$ $\frac{8.7}{30-26}$ $\frac{8.9}{17}$ $\frac{5.9}{11}$ $\frac{5.8}{5.2}$ $\frac{6.6}{15}$ $\frac{6.5}{19}$ $\frac{5.9}{2.2}$ $\frac{8.9}{2.1}$ $\frac{8.9}{3.34}$ $\frac{8.9}{50}$

$\frac{8.1}{50}$ $\frac{8.1}{35}$ $\frac{8.5}{31}$ $\frac{7.6}{20}$ $\frac{7.8}{15}$ $\frac{5.6}{11}$ $\frac{5.8}{5.0}$ $\frac{6.5}{15}$ $\frac{6.6}{17}$ $\frac{6.6}{2.1}$ $\frac{6.6}{2.4}$ $\frac{8.1}{2.9}$ $\frac{8.8}{3.4}$ $\frac{8.9}{50}$

$\frac{7.5}{50}$ $\frac{7.4}{40}$ $\frac{7.7}{32}$ $\frac{8.1}{23}$ $\frac{8.2}{16}$ $\frac{5.7}{10}$ $\frac{5.4}{4.8}$ $\frac{6.4}{16}$ $\frac{7.0}{19}$ $\frac{7.0}{2.3}$ $\frac{8.4}{2.7}$ $\frac{8.9}{3.1}$ $\frac{8.8}{3.4}$ $\frac{8.8}{50}$

Spike in P.D. R+ Sta 50

$\frac{9.0}{50}$ $\frac{9.4}{36}$ $\frac{9.8}{28}$ $\frac{9.9}{20}$ $\frac{9.6}{14}$ $\frac{7.2}{11}$ $\frac{7.0}{6.4}$ $\frac{8.1}{16}$ $\frac{8.3}{18}$ $\frac{9.4}{26}$ $\frac{10.1}{29}$ $\frac{10.3}{34}$ $\frac{10.3}{50}$

$\frac{9.9}{50}$ $\frac{10.1}{45}$ $\frac{10.2}{31}$ $\frac{10.3}{22}$ $\frac{10.0}{16}$ $\frac{6.8}{11}$ $\frac{6.7}{6.2}$ $\frac{8.2}{15}$ $\frac{8.5}{19}$ $\frac{7.6}{2.3}$ $\frac{10.2}{2.8}$ $\frac{10.2}{3.4}$ $\frac{10.2}{50}$

$\frac{10.0}{50}$ $\frac{10.0}{32}$ $\frac{9.9}{25}$ $\frac{9.5}{18}$ $\frac{7.5}{15}$ $\frac{6.1}{12}$ $\frac{6.3}{5.6}$ $\frac{7.9}{16}$ $\frac{7.9}{18}$ $\frac{7.6}{22}$ $\frac{9.8}{27}$ $\frac{10.2}{34}$ $\frac{10.2}{50}$

$\frac{9.8}{50}$ $\frac{9.4}{41}$ $\frac{9.0}{28}$ $\frac{9.0}{21}$ $\frac{8.1}{18}$ $\frac{5.1}{11}$ $\frac{4.8}{4.4}$ $\frac{6.8}{15}$ $\frac{6.0}{2.2}$ $\frac{5.5}{2.4}$ $\frac{5.5}{2.7}$ $\frac{6.0}{3.2}$ $\frac{5.9}{3.6}$ $\frac{5.9}{50}$

$\frac{5.8}{50}$ $\frac{5.0}{38}$ $\frac{4.8}{28}$ $\frac{3.7}{19}$ $\frac{5.3}{15}$ $\frac{3.9}{11}$ $\frac{3.7}{3.2}$ $\frac{5.6}{15}$ $\frac{5.4}{21}$ $\frac{5.4}{2.4}$

$\frac{2.8}{19}$ $\frac{3.9}{15}$ $\frac{2.8}{14}$ $\frac{2.8}{11}$ $\frac{2.8}{2.3}$ $\frac{4.4}{15}$ $\frac{4.5}{18}$ $\frac{4.0}{2.0}$ $\frac{4.0}{2.3}$

$\frac{2.6}{19}$ $\frac{3.6}{16}$ $\frac{3.5}{13}$ $\frac{2.2}{10}$ $\frac{2.2}{1.8}$ $\frac{3.9}{15}$ $\frac{4.0}{19}$ $\frac{2.6}{2.2}$ $\frac{2.6}{2.6}$

+ 16.2

$\frac{1.8}{34}$ $\frac{9.9}{40}$ $\frac{6.0}{51}$ $\frac{5.9}{60}$ $\frac{5.4}{75}$

$\frac{5.9}{75}$ $\frac{5.5}{41}$ $\frac{6.8}{38}$ $\frac{8.7}{29}$

15.3

$\frac{8.7}{34}$ $\frac{1.5}{51}$ $\frac{0.4}{75}$

Sta.	+	π	-	Elev.	
		955.38			
47+50				(148)	40.6
T.P.	8.00	950.32	13.06	942.32	
+84			9.2	41.1	
48					
48+00			9.0	41.3	
+50			8.7	41.6	
49			7.9	42.4	
+50			6.9	43.4	
50			5.3	45.0	
+50			3.1	47.2	
51			0.6	49.7	
+50				+02.1	52.4
+95				+05.4	55.7
T.P.	13.44	963.54	0.22	950.10	
51+50			11.1	52.4	

$\frac{10.3}{50} \frac{10.7}{63} \frac{9.5}{50} \frac{9.1}{31}$

148

$\frac{10.6}{37} \frac{10.6}{58} \frac{10.1}{75}$

$\frac{7.0}{50} \frac{7.3}{40} \frac{8.6}{27} \frac{10.5}{21} \frac{12.2}{18} \frac{11.9}{13} \frac{9.5}{9} \frac{9.2}{9.2} \frac{9.7}{15} \frac{10.7}{20} \frac{10.6}{31} \frac{9.7}{39} \frac{9.9}{50}$

$\frac{8.1}{50} \frac{8.9}{36} \frac{9.5}{32} \frac{11.8}{22} \frac{12.2}{18} \frac{9.3}{9} \frac{9.0}{9.0} \frac{9.7}{15} \frac{10.7}{20} \frac{10.6}{31} \frac{10.3}{35} \frac{11.0}{50}$

$\frac{10.4}{50} \frac{11.2}{35} \frac{11.7}{29} \frac{11.9}{21} \frac{12.1}{16} \frac{11.0}{13} \frac{9.1}{10} \frac{8.7}{8.7} \frac{9.4}{15} \frac{11.2}{22} \frac{11.6}{27} \frac{12.2}{35} \frac{12.2}{50}$

$\frac{11.8}{50} \frac{12.2}{37} \frac{12.2}{27} \frac{11.9}{18} \frac{8.4}{10} \frac{8.3}{7.9} \frac{11.0}{13} \frac{11.1}{20} \frac{11.7}{26} \frac{12.2}{35} \frac{12.2}{50}$

$\frac{12.1}{50} \frac{12.7}{32} \frac{12.5}{26} \frac{12.1}{20} \frac{7.3}{10} \frac{7.4}{6.9} \frac{10.8}{13} \frac{11.1}{20} \frac{11.8}{26} \frac{12.1}{34} \frac{12.1}{50}$

$\frac{12.0}{50} \frac{12.3}{29} \frac{11.7}{20} \frac{5.6}{11} \frac{5.3}{5.3} \frac{5.5}{11} \frac{10.3}{19} \frac{10.6}{25} \frac{11.0}{35} \frac{11.6}{50}$

$\frac{11.6}{50} \frac{11.4}{32} \frac{10.9}{33} \frac{3.3}{11} \frac{3.1}{3.1} \frac{3.4}{12} \frac{8.7}{22} \frac{9.0}{29} \frac{9.0}{34} \frac{9.9}{50}$

$\frac{11.4}{50} \frac{11.2}{35} \frac{10.9}{28} \frac{0.8}{11} \frac{0.6}{0.6} \frac{5.7}{12} \frac{6.9}{21} \frac{6.9}{26} \frac{6.7}{29} \frac{5.9}{34} \frac{5.9}{50}$

$\frac{10.0}{50} \frac{9.1}{38} \frac{8.3}{27} \frac{2.1}{2.1} \frac{2.9}{22} \frac{3.4}{31} \frac{3.5}{34} \frac{4.3}{50}$

$\frac{6.0}{50} \frac{4.5}{31} \frac{3.8}{27} \frac{5.4}{5.4}$

$\frac{11.5}{11} \frac{11.2}{12}$

Sta	+	π	-	Elev
		963.54		
51+95			7.8	55.7
B.M.	1169	967.46	7.75	955.79
				955.77
52+20			9.4	58.1
+31			8.3	59.2
+47			7.1	60.4
+52			6.6	60.9
+63			6.1	61.4
53+10			2.4	65.1
T.P.	12.35	979.22	0.59	966.87
+36			12.5	66.7
54			9.6	70.6
+33			6.9	72.3
+87			4.1	75.1
55+36			1.8	77.4
T.P.	11.97	990.80	0.39	998.83

$\frac{8.0}{11}$	7.8	$\frac{10.5}{12}$	$\frac{11.1}{21}$	$\frac{11.2}{25}$	$\frac{11.2}{29}$	$\frac{11.2}{34}$	$\frac{10.8}{41}$	$\frac{11.2}{50}$
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Spike in Fe. Cor. 33' Rt. Sta 52+03

$\frac{9.4}{50}$	$\frac{9.3}{25}$	9.4	$\frac{9.5}{16}$	$\frac{9.1}{50}$
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$\frac{9.1}{50}$	8.3	$\frac{8.4}{50}$	$\frac{1}{2}$ Cor. Rd E.
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$\frac{7.9}{50}$	$\frac{8.2}{25}$	7.1	$\frac{7.3}{24}$	$\frac{8.4}{50}$
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$\frac{8.1}{50}$	$\frac{8.5}{33}$	$\frac{7.6}{26}$	$\frac{6.9}{7}$	6.6	$\frac{6.9}{20}$	$\frac{7.3}{29}$	$\frac{8.0}{31}$	$\frac{8.9}{50}$
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$\frac{8.6}{50}$	$\frac{8.4}{26}$	$\frac{7.7}{24}$	$\frac{6.3}{6}$	6.1	$\frac{6.3}{17}$	$\frac{5.9}{27}$	$\frac{6.8}{30}$	$\frac{5.2}{32}$	$\frac{5.0}{33}$	$\frac{3.4}{41}$	$\frac{3.1}{47}$	$\frac{3.1}{50}$
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$\frac{2.7}{50}$	$\frac{2.5}{41}$	$\frac{1.1}{26}$	$\frac{2.4}{21}$	$\frac{3.4}{18}$	$\frac{5.2}{18}$	$\frac{3.2}{16}$	$\frac{2.8}{14}$	$\frac{2.5}{8}$	$\frac{2.2}{2.4}$	$\frac{2.5}{11}$	$\frac{2.2}{21}$	$\frac{3.2}{26}$	$\frac{2.9}{27}$	$\frac{2.1}{29}$	$\frac{1.4}{31}$	$\frac{1.4}{50}$
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$\frac{7.5}{50}$	$\frac{8.3}{32}$	$\frac{11.7}{25}$	$\frac{12.6}{20}$	$\frac{14.0}{17}$	$\frac{15.7}{17}$	$\frac{13.3}{15}$	$\frac{12.9}{13}$	$\frac{12.5}{9}$	$\frac{12.6}{12.5}$	$\frac{12.3}{11}$	$\frac{12.8}{17}$	$\frac{14.8}{21}$	$\frac{13.3}{23}$	$\frac{7.0}{25}$	$\frac{8.2}{26}$	$\frac{8.2}{39}$	$\frac{8.2}{50}$
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$\frac{3.8}{35}$	$\frac{10.1}{16}$	$\frac{11.4}{16}$	$\frac{9.8}{14}$	$\frac{9.1}{11}$	8.6	$\frac{9.0}{10}$	$\frac{8.9}{17}$	$\frac{8.4}{21}$	$\frac{0.2}{33}$
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$\frac{2.0}{35}$	$\frac{3.6}{27}$	$\frac{4.4}{22}$	$\frac{7.3}{15}$	$\frac{8.0}{15}$	$\frac{7.5}{14}$	$\frac{7.2}{10}$	6.9	$\frac{7.3}{13}$	$\frac{7.5}{16}$	$\frac{9.0}{18}$	$\frac{6.0}{20}$
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$\frac{1.0}{30}$	$\frac{1.5}{28}$	$\frac{3.5}{34}$	$\frac{5.7}{22}$	$\frac{4.6}{16}$	$\frac{4.4}{10}$	4.1	$\frac{4.5}{10}$	$\frac{4.5}{14}$	$\frac{4.0}{15}$	$\frac{2.9}{19}$
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$\frac{0.9}{16}$	$\frac{1.6}{10}$	1.8	$\frac{1.9}{11}$	$\frac{2.2}{13}$	$\frac{1.6}{15}$	$\frac{1.2}{15}$	$\frac{1.7}{16}$	$\frac{0.9}{21}$
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Sta	+	π	-	Elev
		990.80		
54				(20.2) 70.6
+33				(18.5) 72.3
+87				(15.7) 75.1
55+36				(13.4) 77.4
+73			12.2	78.6
56			11.8	79.0
+50			11.9	78.9
T.P.	5.50	984.33	11.97	978.83
57			5.3	79.0
+36			5.2	79.1
58			4.7	79.6
+40			4.2	80.1
59			3.6	80.7

$$\frac{15.1}{75} \quad \frac{11.9}{50} \quad \frac{11.2}{41}$$

20.2

$$\frac{14.2}{50} \quad \frac{20.8}{75}$$

$$\frac{14.0}{75} \quad \frac{11.3}{50} \quad \frac{10.7}{41}$$

18.5

$$\frac{9.0}{31} \quad \frac{10.1}{50} \quad \frac{12.1}{65} \quad \frac{14.9}{75}$$

$$\frac{5.5}{75} \quad \frac{4.3}{47} \quad \frac{9.7}{40}$$

15.7

$$\frac{10.3}{23} \quad \frac{8.2}{29} \quad \frac{7.7}{39} \quad \frac{6.9}{50} \quad \frac{6.8}{75}$$

$$\frac{5.4}{75} \quad \frac{7.0}{50} \quad \frac{9.0}{44} \quad \frac{11.2}{33} \quad \frac{12.5}{21}$$

13.4

$$\frac{9.7}{21} \quad \frac{8.0}{25} \quad \frac{5.4}{30} \quad \frac{3.4}{50} \quad \frac{3.0}{68} \quad \frac{3.9}{75}$$

$$\frac{13.9}{50} \quad \frac{13.6}{28} \quad \frac{14.7}{24} \quad \frac{17.4}{23-21} \quad \frac{16.0}{20} \quad \frac{12.8}{76}$$

$$\frac{12.2}{122} \quad \frac{12.6}{11} \quad \frac{12.4}{13-14} \quad \frac{12.4}{15}$$

$$\frac{10.0}{19} \quad \frac{7.3}{25} \quad \frac{5.1}{37} \quad \frac{4.1}{50} \quad \frac{1.8}{64} \quad \frac{1.7}{75}$$

$$\frac{14.7}{50} \quad \frac{14.5}{31} \quad \frac{15.1}{24} \quad \frac{17.2}{23-19} \quad \frac{15.7}{18} \quad \frac{12.7}{12}$$

$$\frac{12.2}{118} \quad \frac{12.6}{11} \quad \frac{12.4}{13-14} \quad \frac{12.1}{15} \quad \frac{11.6}{19} \quad \frac{9.4}{30} \quad \frac{4.7}{50} \quad \frac{2.7}{65} \quad \frac{1.0}{75}$$

$$\frac{15.4}{50} \quad \frac{15.1}{31} \quad \frac{16.0}{25} \quad \frac{17.3}{24-21} \quad \frac{15.4}{19} \quad \frac{11.7}{12} \quad 11.9$$

$$\frac{12.1}{12} \quad \frac{14.1}{16} \quad \frac{14.0}{21} \quad \frac{12.6}{23} \quad \frac{10.2}{40} \quad \frac{7.0}{50} \quad \frac{4.4}{65} \quad \frac{1.0}{75}$$

$$\frac{9.3}{50} \quad \frac{9.0}{33} \quad \frac{9.2}{28} \quad \frac{10.5}{26-23} \quad \frac{9.5}{20} \quad \frac{8.4}{17} \quad \frac{6.2}{13} \quad \frac{5.8}{11} \quad 5.3$$

$$\frac{5.7}{11} \quad \frac{9.0}{15} \quad \frac{9.4}{20} \quad \frac{8.6}{24} \quad \frac{5.7}{30} \quad \frac{5.2}{39} \quad \frac{9.7}{50} \quad \frac{3.0}{60} \quad \frac{5.8}{75}$$

$$\frac{5.8}{50} \quad \frac{9.2}{45} \quad \frac{9.2}{35} \quad \frac{8.9}{29} \quad \frac{10.4}{26} \quad \frac{10.9}{21} \quad \frac{8.7}{20} \quad \frac{7.7}{17} \quad \frac{6.1}{14} \quad 5.2$$

$$\frac{6.0}{5.2} \quad \frac{10.7}{12} \quad \frac{10.0}{17} \quad \frac{9.8}{25} \quad \frac{8.5}{29} \quad \frac{6.7}{31} \quad \frac{5.0}{38} \quad \frac{3.4}{50} \quad \frac{1.0}{60} \quad \frac{5.0}{75}$$

$$\frac{9.9}{50} \quad \frac{9.5}{33} \quad \frac{9.4}{29} \quad \frac{9.3}{24} \quad \frac{8.7}{21} \quad \frac{5.9}{14} \quad \frac{5.3}{9} \quad 4.7$$

$$\frac{5.2}{12} \quad \frac{8.2}{16-19} \quad \frac{8.0}{22} \quad \frac{7.0}{26} \quad \frac{6.0}{28} \quad \frac{5.2}{32} \quad \frac{3.3}{39} \quad \frac{1.4}{50} \quad \frac{0.0}{60} \quad \frac{0.0}{75}$$

$$\frac{9.0}{50} \quad \frac{9.0}{34} \quad \frac{8.2}{22} \quad \frac{7.7}{19} \quad \frac{5.1}{13}$$

$$\frac{4.2}{9} \quad \frac{4.5}{13} \quad \frac{4.7}{17} \quad \frac{4.1}{21} \quad \frac{3.4}{29} \quad \frac{2.5}{38} \quad \frac{2.0}{50} \quad \frac{3.5}{75}$$

$$\frac{6.1}{50} \quad \frac{5.8}{39} \quad \frac{4.4}{31} \quad \frac{2.9}{23} \quad \frac{2.8}{20} \quad \frac{4.5}{17-15} \quad \frac{3.9}{12}$$

$$\frac{3.6}{3.6} \quad \frac{3.8}{11} \quad \frac{3.9}{15} \quad \frac{2.9}{18} \quad \frac{3.1}{24} \quad \frac{1.3}{36} \quad \frac{0.2}{50}$$

Sta	+	π	-	Elev
		984.33 ✓		
59+50			3.1	81.2
60			2.7	81.6 ✓
T.P.	9.63	991.28 ✓	2.68	981.65 ✓
+35			9.5	81.8
61			9.7	81.6
T.P.	7.36	994.02 ✓	4.62	986.66 ✓
+43			12.7	81.3
62			14.4	79.6
+55				(16.5) 77.5
+88				(18.0) 23.0 76.0
63+13				(19.2) 24.2 74.8
+50				(21.0) 26.0 73.0
64				(23.3) 70.7 ✓
T.P.	15.6	982.51 ✓	13.07	980.95 ✓
+2+55			5.0	77.5

0.0 +1.3 +1.0 +1.6 2.9 4.1 3.5 3.2 3.6 3.7 2.5 2.6 2.8 2.2
50 34 28 23 18 15 13 10 3.1 10 13-16 18 20 35 50

1.0 +0.7 +2.0 0.2 0.5 2.9 2.8 3.3 3.1 1.6 +0.3 +0.3
50 38 28 24 19 15 9 2.7 11 17 20 42 50

14.5 14.5 11.1 9.0 9.0 9.5 10.3 9.6 9.9 10.0 10.3 7.9 6.6 5.1 4.4
50 46 35 27 19 17 15.14 12 9.5 10 13 16-17 21 29 42 50

Note - Ctr of Pot hole - (15.3)

12.1 10.6 11.1 11.7 11.6 10.1 9.8 9.9 9.6 6.5 5.5 5.6
50 38 27 20 18 13 8 13 16 21 24 50

Fe Pot & Lt Sta 62

13.4 13.7 13.5 12.0 12.8 12.8 12.8 13.2 12.6 8.5 7.7 7.7 8.0
50 43 33 19 16 14 12.7 9 11-14 16 21 27 40 50

8.0 8.6 8.1 8.9 12.4 14.2 14.8 14.6 14.6 14.7 12.7 11.4 11.6 11.7
50 39 33 27 23 20 17 14.4 7 9-12 17 19 34 50

3.0 4.9 5.8 7.0
55 75 54 42 40

(16.5)

11.2 16.6
19 50

2.5 3.3 5.9 6.7
55 75 62 41 37

(23.0)

2.8 5.4 10.0 11.9
60 75 54 36 32

(24.2)

4.4 8.5 13.4
75 55 36

(26.0)

10.6 10.8 13.6 15.6
75 64 41 33

(23.3)

3.1 5.1 5.2 6.0 5.4 5.3 5.5 3.7
25 21 18 14-16 12 5.0 12 13-14 16

Sta	+	π	-	Elev
		982.51		
62+88			6.5	76.0 71.0
63+13			7.7	74.8 69.8
+50			9.5	73.0 68.0
T.P.	2.05	972.66	11.90	970.61
64			2.0	70.7
+33			3.7	69.0
+60			4.9	67.8
65			6.6	66.1
+43			8.1	64.6
B.M.	4.38	968.13	8.91	963.75
+67			4.3	63.8
66+04			5.4	62.7
+25			6.2	61.9
+58			7.3	60.8
T.P.	4.14	963.77	8.50	959.63

963.75

5.5 6.7 7.7 6.9 6.6 7.1 4.1 6.9 9.0
22 19 18-17 14 6.5 8 10-11 15 35 50

5.4 7.4 8.6 8.1 7.7 8.0 8.0 10.0 12.3 15.3
23 19 18-16 15 13 7.7 10 12 17 26 50

4.6 9.8 10.4 9.6 9.6 9.7 9.8 11.2 13.1 15.7
27 18 17-16 14 13 9.5 9 12 16 25 50

1.6 2.9 2.3 2.1 2.3 2.4 2.7 2.9 6.8 8.2
18 17-16 14 12 2.0 8 9 14 16 33 50

+2.2 +1.8 0.0 1.4 3.4 4.0 3.9 3.7 4.1 4.3 5.7 7.3 8.8
50 33 26 24 20 18-17 15 13 3.7 10 13 16 27 50

2.7 5.7 6.5 5.5 5.1 5.1 11.3 13.8 14.8 14.5
50 33 23-21 18 9 4.9 8 19 27 44 55

7.9 9.7 9.0 8.8 6.9 7.0 14.2 15.0 15.5 15.1
50 33 23 21-20 14 6.6 10 22 27 39 50

FL FL
13.0 12.0 12.1 12.9 13.2 8.7 9.9 16.2 15.3 17.0 17.6 19.0
50 32 26 23 22 14 8.1 12 19 17 27 37 50

Spike in 15" Oak 70" dt 1-4 6.5 + 9.3
standing water 9.0 8.9 7.9 7.1 6.4 4.5 5.0 6.4 9.1 11.1 12.0 11.7 10.9
75 50 28 23 19 15 4.3 10 14 18 22 28 37 50

1.9 4.0 4.9 5.0 5.2 5.9 5.5 6.0 6.8 6.7 4.3 3.4 3.3
50 32 24 17 14 12 10 5.4 12 18-20 21 29 32 50

2.6 2.6 3.5 4.0 6.1 6.3 6.5 6.2 5.6 6.9 2.1
50 40 30 22 16-14 11 6.2 12 18 22 33 50

2.3 2.3
+3.8 +3.2 +2.3 4.9 7.6 7.5 7.3 7.4 7.0 6.7 1.2 2.8
50 38 30 2.0 16-14 11 7.3 10 13 19 22 33 50

Sta	+	X	-	Elev
		963.77.		
67			4.0	59.8.
+31			4.7	59.1.
+66			5.1	58.7.
T.P.	5.74	964.33.	5.18	958.59.
68			5.6	58.7.
+48			5.5	58.8.
69			5.0	59.3.
+36			4.6	59.7.
+78			4.1	60.2.
70			3.7	60.6.
+40			2.9	61.4.
+71			2.1	62.2.
71			1.0	63.3.

1.0 3.7 4.5 6.2 6.4 5.8 4.4 4.3 5.5 6.7 7.4 8.3
50 34 29 23 19 15 11 40 7 15 19 23 50

7.0 8.4 8.7 8.5 7.6 5.1 5.3 13.1 13.9 15.7
50 34 28 21 16 9 47 10 24 27 50

7.8 8.3 7.4 11.3 11.6 5.4 5.2 12.5 2.6 17.2 16.9 17.5
50 34 26 20 20 10 11 20 22 24 35 50

Spikes PP- 38+1 21
5.9 6.7 7.1 7.8 8.9 8.0 6.4 6.0 6.1 7.3 9.1 11.3 13.3 14.9
50 36 31 28 23-20 17 15 12 5.6 12 16 20 25 37 50

0.4 1.5 2.0 3.0 6.3 5.8 5.6 5.9 6.3 7.1 7.3 7.0 8.0 9.5
50 40 32 20 20-17 16 11 55 12 16 19 22 27 40 50

5.0 5.1 5.4 5.5 4.6 3.8 5.8
18 12 5.0 12 15-17 20 31 50

4.5 5.1 4.9 4.9 5.2 5.3 4.7 4.8 4.5 7.2
19 17 15 11 4.6 13 16-18 21 25 33 50

3.8 5.2 5.5 5.2 4.4 4.7 7.0 7.2 11.7 12.3 12.9
32 24 21-17 16 10 4.1 15 19 24 34 4 50

4.1 5.4 5.4 5.8 5.8 3.8 4.1 4.7 7.0 7.1 11.9 12.6
50 45 33 27 19 12 3.7 13 16 20 23 35 50

5.8 6.7 7.2 7.2 7.1 3.2 3.7 8.9 11.9 12.8 13.2 13.1
50 42 31 26 22 14 2.9 15 22 27 34 40 50

Drainage

(13.8)
200

7.4 10.3 9.3 8.4 2.6 2.2 2.5 2.8 7.8 13.6 14.0 13.2 (13.6)
50 41 33 24 15 13 2.1 10 14 21 30 36 50

Drainage

(13.6)
100

(14.2)
84

10.3 10.1 8.5 7.2 1.5 1.1 1.6 6.3 10.5 11.1 11.7 (14.0)
50 40 32 24 15 12 1.0 14 20 29 36 50

F.L.

30.2

Sta + π - Elev

964.33 ✓

71+35

+0.6

64.9 ✓

T.P.

11.10

975.01 ✓

642

963.91 ✓

69

(15.7) ✓

59.3

69

(15.3) ✓

59.7

+36

+78

(14.8) ✓

60.2

T.P.

13.30

984.47 ✓

3.84

971.17 ✓

72

15.2

69.3

+50

12.2

72.3

73

9.0

75.5

+50

5.7

78.8

T.P.

11.89

992.63 ✓

3.73

980.74 ✓

74

11.6

81.0

+50

9.4

83.2

75

7.6

85.0

+58

7.6

85.0

<u>8.5</u>	<u>7.3</u>	<u>5.8</u>	<u>4.9</u>	<u>3.1</u>	<u>0.0</u>	<u>+0.3</u>	<u>2.9</u>	<u>6.5</u>	<u>6.8</u>	<u>7.8</u>
50	38	32	25	20	13	10.6	15	20	27	36

Top Post

<u>3.8</u>	<u>6.2</u>	<u>7.0</u>	<u>7.9</u>	(15.7)
75	86	44	31	

<u>5.8</u>	<u>7.1</u>	<u>8.2</u>	(15.3)
75	42	30	

<u>13.0</u>	(14.8)
50	

<u>13.8</u>	<u>12.0</u>	<u>11.7</u>	<u>16.1</u>	<u>15.6</u>	<u>15.4</u>	<u>16.4</u>	<u>15.1</u>	<u>14.0</u>	<u>13.2</u>	<u>12.2</u>
50	32	24	18-17	12	15.2	12	15-16	19	25	36

<u>8.0</u>	<u>7.8</u>	<u>7.3</u>	<u>7.2</u>	<u>12.0</u>	<u>12.6</u>	<u>12.5</u>	<u>12.3</u>	<u>13.0</u>	<u>9.6</u>	<u>8.6</u>	<u>7.3</u>	<u>6.1</u>
50	35	32	25	18	17-16	13	12.2	11	13-14	21	25	36

<u>4.3</u>	<u>3.0</u>	<u>7.0</u>	<u>10.0</u>	<u>9.3</u>	<u>9.2</u>	<u>9.4</u>	<u>4.1</u>	<u>5.2</u>	<u>4.6</u>	<u>3.8</u>	<u>3.4</u>
50	28	21	18-17	14	9.0	9	11-13	17	22	25	38

<u>2.3</u>	<u>1.1</u>	<u>1.7</u>	<u>5.1</u>	<u>6.9</u>	<u>6.2</u>	<u>5.9</u>	<u>6.0</u>	<u>1.5</u>	<u>+0.0</u>	<u>+0.8</u>	<u>+2.5</u>
50	32	27	20	17-16	14	5.7	9	11-12	22	30	35

<u>4.1</u>	<u>4.6</u>	<u>4.6</u>	<u>8.8</u>	<u>12.4</u>	<u>12.0</u>	<u>11.7</u>	<u>11.7</u>	<u>9.4</u>	<u>7.6</u>	<u>6.4</u>	<u>5.7</u>	<u>4.6</u>
50	39	28	23	18-17	16	11.6	10	13	17	21	25	31

<u>6.0</u>	<u>6.0</u>	<u>5.2</u>	<u>9.2</u>	<u>9.5</u>	<u>9.3</u>	<u>9.4</u>	<u>5.4</u>	<u>4.4</u>	<u>4.0</u>	<u>4.6</u>	<u>4.2</u>
50	39	30	21	16	9.4	9	12-13	17	23	27	31

<u>3.6</u>	<u>3.9</u>	<u>4.1</u>	<u>6.6</u>	<u>7.6</u>	<u>7.8</u>	<u>7.7</u>	<u>5.7</u>	<u>4.4</u>	<u>4.7</u>	<u>5.1</u>	<u>5.7</u>
50	45	35	29	13	7.6	8	13	17	22	28	33

<u>4.2</u>	<u>3.8</u>	<u>8.2</u>	<u>7.8</u>	<u>2.8</u>	<u>7.8</u>	<u>6.0</u>	<u>5.8</u>	<u>6.0</u>	<u>6.9</u>
50	30	17-18	12	7.6	9	16	22	26	31

Sta + π - Elev.

992.63

76 7.9 84.7.

+50 8.3 84.3.

77 8.6 84.0.

+50 9.2 83.4.

T.P. 7.26 990.64. 9.25 983.38.

7.8 8.6 82.0.

+50 9.4 81.2.

79 9.6 81.0.

+57 9.5 81.1.

80 9.2 81.4.

+50 8.8 81.8.

81 8.3 82.3.

+50 8.0 82.6.

$\frac{6.4}{50}$ $\frac{6.4}{41}$ $\frac{6.3}{30}$ $\frac{6.4}{25}$ $\frac{9.0}{21-20}$ $\frac{7.7}{11}$ $\frac{8.1}{9}$ $\frac{8.0}{13}$ $\frac{8.0}{17}$ $\frac{6.9}{22}$ $\frac{6.7}{25}$ $\frac{7.2}{39}$ $\frac{7.7}{50}$

$\frac{7.9}{50}$ $\frac{8.3}{30}$ $\frac{8.8}{23}$ $\frac{9.5}{20-19}$ $\frac{8.3}{12}$ $\frac{8.6}{9}$ $\frac{8.9}{14}$ $\frac{9.6}{23}$ $\frac{9.7}{27}$ $\frac{8.6}{31}$ $\frac{9.1}{50}$

$\frac{10.0}{50}$ $\frac{9.9}{31}$ $\frac{10.1}{25}$ $\frac{10.7}{22-20}$ $\frac{9.4}{18}$ $\frac{8.7}{10}$ $\frac{9.0}{12}$ $\frac{9.9}{16}$ $\frac{9.8}{21}$ $\frac{9.6}{25}$ $\frac{9.9}{50}$

Low Spot

$\frac{11.5}{75}$ $\frac{10.8}{50}$ $\frac{10.9}{30}$ $\frac{9.8}{25}$ $\frac{10.8}{23}$ $\frac{10.9}{20-19}$ $\frac{9.5}{13}$ $\frac{9.8}{14}$ $\frac{10.0}{21}$ $\frac{9.3}{26}$ $\frac{9.2}{35}$ $\frac{8.0}{50}$

$\frac{7.7}{50}$ $\frac{8.2}{30}$ $\frac{9.6}{23}$ $\frac{9.5}{20-18}$ $\frac{8.7}{14}$ $\frac{8.6}{11}$ $\frac{9.0}{14-10}$ $\frac{9.1}{14-10}$ $\frac{7.6}{23}$ $\frac{7.8}{32}$ $\frac{7.4}{50}$

$\frac{10.7}{50}$ $\frac{9.0}{33}$ $\frac{9.0}{26}$ $\frac{10.5}{23-21}$ $\frac{10.2}{19}$ $\frac{10.0}{14}$ $\frac{7.7}{11}$ $\frac{9.9}{17-21}$ $\frac{9.6}{25}$ $\frac{7.5}{37}$ $\frac{7.3}{50}$

$\frac{11.4}{50}$ $\frac{11.2}{28}$ $\frac{11.8}{23}$ $\frac{11.7}{19}$ $\frac{10.8}{15}$ $\frac{10.0}{12}$ $\frac{9.8}{12}$ $\frac{10.7}{16-19}$ $\frac{10.6}{22}$ $\frac{10.4}{27}$ $\frac{10.4}{50}$

F.L.

F.L.

$\frac{12.0}{50}$ $\frac{11.9}{36}$ $\frac{11.9}{27}$ $\frac{11.8}{21-19}$ $\frac{12.2}{18}$ $\frac{10.2}{12}$ $\frac{10.0}{9.5}$ $\frac{11.6}{18}$ $\frac{11.1}{16}$ $\frac{11.0}{21}$ $\frac{10.6}{23}$ $\frac{10.6}{50}$

$\frac{11.8}{50}$ $\frac{11.8}{38}$ $\frac{11.7}{28}$ $\frac{11.9}{24}$ $\frac{11.8}{19}$ $\frac{11.6}{17}$ $\frac{10.2}{15}$ $\frac{9.4}{9.2}$ $\frac{11.0}{14}$ $\frac{10.1}{18-23}$ $\frac{10.1}{24}$ $\frac{10.1}{50}$

$\frac{11.0}{50}$ $\frac{11.0}{40}$ $\frac{10.8}{30}$ $\frac{10.7}{23}$ $\frac{10.6}{20-18}$ $\frac{9.4}{12}$ $\frac{9.5}{8.8}$ $\frac{10.5}{15}$ $\frac{10.6}{20-22}$ $\frac{9.3}{26}$ $\frac{8.2}{32}$ $\frac{8.2}{50}$

$\frac{9.1}{50}$ $\frac{9.2}{27}$ $\frac{8.7}{20}$ $\frac{8.9}{16}$ $\frac{9.1}{11}$ $\frac{8.4}{8.3}$ $\frac{8.9}{12-15}$ $\frac{10.0}{18-21}$ $\frac{9.5}{22}$ $\frac{9.5}{28}$ $\frac{6.7}{35}$ $\frac{6.1}{44}$ $\frac{6.2}{50}$

$\frac{8.6}{50}$ $\frac{9.0}{37}$ $\frac{9.5}{29}$ $\frac{9.5}{24}$ $\frac{8.8}{18}$ $\frac{8.4}{13}$ $\frac{7.8}{8.0}$ $\frac{8.2}{10}$ $\frac{9.2}{17}$ $\frac{7.1}{25}$ $\frac{6.6}{29}$ $\frac{5.6}{36}$ $\frac{4.4}{50}$

Sta	f	π	-	Elev.
		990.64		
82			7.6	83.0
+48			7.1	83.5
B.M.	5.70	991.51	468	985.96
83			7.3	84.3
+50			6.5	85.1
84			6.0	85.6
+50			5.6	86.0
85			5.0	86.6
+50			4.2	87.4
86			3.2	88.4
+50			1.7	89.9
T.P.	6.87	997.57	0.87	990.70
87			6.3	91.3
+60			5.3	92.3

985.87

8.0 9.2 9.3 9.3 9.0 8.1 7.3 7.8 7.4 6.6 6.5 6.1 5.7 3.3
50 27 22 20 19-17 13 7.6 10 14-17 18 21 25 29 35 50

6.8 6.8 6.6 6.7 7.0 6.9 7.7 6.6 6.0 4.3 3.7
50 27 23 18 13 7.1 10 14-15 17 26 42 50

Spike in P.P. 25 Lt Sta 82 + 75

6.9 6.9 6.7 2.5 5.3 7.6 7.2 7.7 6.6 5.4 6.0 6.1 4.8
50 27 20 18 16-15 11 7.3 10 13-14 17 23 30 40 50

6.3 6.2 6.2 6.9 7.0 6.5 7.0 5.5 5.2 5.1 5.2 4.6 4.7
50 28 22 17 12 6.5 8 13-16 17 22 28 32 39 50

7.4 7.0 7.0 7.2 6.4 5.9 6.2 5.9 4.1 2.5 2.4 3.3
50 27 21 18-17 11 6.0 7 12-14 15 19 28 37 50

9.0 8.8 8.6 7.8 6.4 5.3 5.7 6.3 4.6 4.1 3.5 3.3 3.9
50 32 23 18 14 5.6 7 13 14-16 18 24 36 45 50

8.4 7.8 7.4 7.5 5.5 5.0 5.3 6.3 6.2 6.1 5.9
50 34 28 23 18 5.0 6 13 17 22 36 50

7.1 7.1 6.9 6.4 6.2 5.2 4.7 6.8 7.7 7.7 7.1
50 36 28 24 19 14 4.2 12 16 25 35 50

6.6 5.8 5.3 3.8 3.6 5.2 6.2 6.7 6.2 5.6
50 29 20 14 3.2 12 17 20 24 37 50

4.2 2.5 2.4 3.0 1.9 1.7 2.5 3.9 3.4
50 28 23 19-18 14 1.7 10 15 29 50

7.7 4.9 5.7 7.5 6.4 6.6 6.7 5.7 7.4 8.8
50 26 19 17-15 14 6.3 14 17 18 39 50

6.3 4.1 4.7 5.9 5.5 5.1 5.8 3.5 3.0 4.8
50 27 18 16-15 12 5.3 9 12-14 18 40 50

Sta + π - Elev.

997.57

88 5.1 92.5.

+50 5.0 92.4.

89 4.8 92.8.

+50 4.6 93.0.

90 4.5 93.1.

+50 4.3 93.3.

T.P. 6.65 1003.35 0.87 996.70.

91 + 11 9.8 93.6.

+65 10.3 93.1.

92 10.7 92.7.

+21 11.1 92.3.

+25 11.3 92.1.

+40 11.7 91.7.

$\frac{6.1}{50}$ $\frac{4.3}{35}$ $\frac{3.7}{27}$ $\frac{4.5}{20}$ $\frac{5.3}{18}$ $\frac{5.3}{13}$ 5.1 $\frac{5.1}{11}$ $\frac{5.5}{13-14}$ $\frac{4.0}{17}$ $\frac{5.1}{37}$ $\frac{5.4}{50}$

$\frac{5.6}{50}$ $\frac{5.0}{29}$ $\frac{5.4}{19}$ $\frac{5.4}{16}$ 5.0 $\frac{5.8}{10}$ $\frac{5.5}{14}$ $\frac{5.6}{24}$ $\frac{5.9}{35}$ $\frac{6.2}{50}$

$\frac{5.2}{50}$ $\frac{4.8}{45}$ $\frac{4.9}{26}$ $\frac{5.0}{20}$ $\frac{5.1}{15}$ $\frac{5.0}{13}$ 4.8 $\frac{4.6}{10}$ $\frac{5.0}{12}$ $\frac{4.4}{15}$ $\frac{4.7}{25}$ $\frac{6.3}{50}$

$\frac{3.5}{50}$ $\frac{2.4}{34}$ $\frac{3.3}{28}$ $\frac{4.2}{23}$ $\frac{4.9}{18}$ $\frac{4.5}{16}$ 4.6 $\frac{4.8}{9}$ $\frac{4.9}{13}$ $\frac{4.6}{20}$ $\frac{5.6}{50}$

$\frac{3.7}{50}$ $\frac{4.1}{35}$ $\frac{4.6}{29}$ $\frac{4.8}{25}$ $\frac{4.9}{21}$ $\frac{4.6}{16-15}$ $\frac{4.7}{13}$ 4.5 $\frac{4.5}{10}$ $\frac{5.0}{12}$ $\frac{6.0}{26}$ $\frac{7.0}{50}$

$\frac{1.3}{50}$ $\frac{2.2}{42}$ $\frac{1.7}{34}$ $\frac{3.0}{29}$ $\frac{3.3}{25}$ $\frac{4.5}{18}$ $\frac{4.4}{12}$ 4.3 $\frac{4.5}{9}$ $\frac{4.9}{12}$ $\frac{7.9}{35}$ $\frac{10.0}{50}$

Sph 12" 10.4 - Lt. 3.1, 91
 $\frac{1.3}{75}$ $\frac{2.0}{50}$ $\frac{2.9}{40}$ $\frac{2.9}{31}$ $\frac{9.5}{23}$ $\frac{9.8}{16-14}$ $\frac{10.0}{12}$ 9.8 $\frac{10.2}{12}$ $\frac{11.5}{17}$ $\frac{13.1}{38}$ $\frac{13.8}{45}$ $\frac{13.9}{50}$

$\frac{8.1}{50}$ $\frac{9.1}{29}$ $\frac{9.6}{22}$ $\frac{10.1}{15}$ $\frac{10.2}{12}$ 10.3 $\frac{10.8}{13}$ $\frac{12.7}{19}$ $\frac{13.7}{23}$ $\frac{14.1}{38}$ $\frac{15.3}{50}$

ss. $\frac{6.5}{50}$ $\frac{5.0}{40}$ $\frac{4.8}{28}$ $\frac{10.7}{21}$ $\frac{10.7}{15}$ $\frac{10.7}{9}$ 10.7 $\frac{11.2}{14}$ $\frac{12.2}{20}$ $\frac{14.8}{29}$ $\frac{16.5}{50}$

ss. $\frac{4.0}{50}$ $\frac{3.1}{31}$ $\frac{11.3}{21}$ $\frac{11.3}{18}$ $\frac{11.2}{13}$ 11.1 $\frac{11.8}{15}$ $\frac{12.8}{23}$ $\frac{15.3}{43}$ $\frac{17.5}{50}$

$\frac{4.2}{50}$ $\frac{3.7}{30}$ $\frac{11.5}{21}$ $\frac{11.5}{16}$ $\frac{11.6}{13}$ 11.3 $\frac{12.1}{14}$ $\frac{14.5}{37}$ $\frac{16.2}{50}$

ss. $\frac{4.5}{50}$ $\frac{4.0}{30}$ $\frac{11.9}{21}$ $\frac{11.8}{13}$ $\frac{11.8}{12}$ 11.7 $\frac{13.0}{18}$ $\frac{15.9}{50}$ Cemetery Rd.

Sta.	+	π	-	Elev.
		1003.35		
92 + 56			12.2	91.2.
+ 60			12.4	91.0.
+ 89			13.8	89.6.
T.P.	3.32	993.09.	13.58	989.77.
93 + 25			5.7	87.4.
94			10.2	82.9.
T.P.	2.84	985.22.	10.71	982.38.
+ 32			4.3	80.9.
95			6.9	78.3.
+ 50			8.3	76.9.
96			9.6	75.6.
T.P.	4.23	979.67.	9.78	975.44.
+ 33			4.5	75.2.
97			5.0	74.7.
+ 54			5.1	74.6.

4

5.5 5.5 4.7 12.5 12.7 12.6 12.9 14.9 16.1
50 30 20 15 11 12.2 14 36 50

6.0 5.2 12.7 12.9 12.7 13.7 14.5 16.8 17.5
50 30 21 16 11 12.4 21 34 45 50

7.5 6.3 14.1 14.3 14.1 14.1 15.7 15.7 15.0
50 30 20 16 11 13.8 15 21 27 50

2.4 3.2 2.3 2.2 6.0 6.0 5.4 6.3 8.0 7.3 2.6 1.6 3.0
50 42 32 26 20 18 13 5.7 13 19 22 37 44 50

14.3 16.3 16.1 16.0 10.7 10.7 12.5 12.5 12.8 13.7 15.4
50 38 31 23 14 10.2 14 19 22 28 42 50

3.5 6.5 8.8 10.1 10.1 4.4 4.9 7.6 7.6 8.6 10.9 11.7
50 39 31 23 14 4.3 13 17 19 32 40 50

5.3 8.3 10.4 10.5 7.2 7.7 11.3 11.6 11.5 11.2
50 38 25 20 14 6.9 13 21 26 34 50

9.5 12.0 13.4 12.8 8.9 9.2 12.1 12.8 13.1 13.1 13.2
50 32 24 22 19 13 8.3 14 20 24 31 39 50

10.0 13.0 14.0 13.7 13.3 10.2 10.4 12.4 13.1 13.5 13.5 13.2
50 33 27 23 19 14 9.6 15 20 26 36 40 50

Drainage

10.6 9.7 9.1 9.3 9.3 9.5 9.1 6.3 4.9 5.1 6.8 7.4 7.7 6.5 5.4
125 75 50 40 31 26 20 16 13 4.5 15 19 36 33 38 50

9.8 9.9 9.6 8.9 8.5 7.9 5.7 5.4 6.0 5.2 4.7 4.3 4.0
50 45 34 29 24 20 13 5.0 14 16 18 22 31 41 50

6.8 8.3 9.0 9.3 8.8 5.8 5.5 6.9 6.8 4.7 2.5 2.7
50 40 30 24 18 13 5.1 12 16 19 24 45 50

Sta	+	π	-	Elev
		979.67		
98			5.3	74.4.
+28			5.4	74.3.
+84			5.8	73.9.
T.P.	9.08	982.89.	5.86	973.81.
99+22			9.0	73.9.
+62			8.8	74.1.
100			8.7	74.2.
+50			9.0	73.9.
101			9.8	73.1.
+50			11.0	71.9.
102			12.3	70.6.
+69			15.1	67.8.
T.P.	0.42	970.64.	12.67	970.22.
103			4.6	66.0.
B.M	7.16	965.08.	12.65	957.99. (957.92)

$\frac{1.3}{50}$ $\frac{3.4}{30}$ $\frac{3.8}{21}$ $\frac{6.4}{18}$ $\frac{6.3}{15}$ $\frac{5.6}{13}$ 5.3 $\frac{5.7}{12}$ $\frac{6.0}{15}$ $\frac{6.3}{17}$ $\frac{3.0}{22}$ $\frac{3.5}{30}$ $\frac{3.0}{37}$ $\frac{3.0}{50}$

$\frac{2.8}{50}$ $\frac{3.4}{36}$ $\frac{3.3}{22}$ $\frac{6.4}{18}$ $\frac{6.3}{16}$ $\frac{5.6}{13}$ 5.4 $\frac{6.2}{12}$ $\frac{7.1}{16}$ $\frac{7.1}{17}$ $\frac{4.5}{21}$ $\frac{5.5}{31}$ $\frac{2.4}{50}$

FL.

FL.

$\frac{13.2}{75}$ $\frac{9.4}{50}$ $\frac{8.9}{36}$ $\frac{9.0}{30}$ $\frac{8.9}{24}$ $\left(\frac{9.1}{19}\right)$ $\frac{9.0}{19}$ $\frac{7.9}{18}$ $\frac{6.4}{14}$ 5.8 $\frac{6.4}{15}$ $\frac{8.7}{16}$ $\left(\frac{8.7}{16}\right)$ $\frac{8.6}{20}$ $\frac{8.3}{21}$ $\frac{8.9}{32}$ $\frac{7.3}{41}$ $\frac{6.4}{50}$

$\frac{10.7}{50}$ $\frac{10.5}{32}$ $\frac{10.6}{26}$ $\frac{10.7}{21-19}$ $\frac{9.6}{15}$ 9.0 $\frac{9.5}{13}$ $\frac{10.6}{18}$ $\frac{10.9}{31}$ $\frac{10.7}{50}$

$\frac{8.1}{50}$ $\frac{8.4}{31}$ $\frac{8.7}{26}$ $\frac{8.7}{19}$ $\frac{9.6}{17-16}$ $\frac{9.4}{13}$ 8.8 $\frac{9.5}{13}$ $\frac{9.7}{14-15}$ $\frac{8.0}{18}$ $\frac{7.4}{21}$ $\frac{7.4}{34}$ $\frac{8.0}{50}$

$\frac{8.7}{50}$ $\frac{8.1}{30}$ $\frac{8.0}{19}$ $\frac{9.5}{17-16}$ $\frac{9.1}{13}$ 8.7 $\frac{9.6}{11}$ $\frac{9.4}{14}$ $\frac{5.9}{18}$ $\frac{5.3}{33}$ $\frac{4.7}{50}$

$\frac{7.6}{50}$ $\frac{7.0}{30}$ $\frac{6.8}{21}$ $\frac{9.5}{18}$ $\frac{9.8}{16}$ $\frac{9.4}{13}$ 9.0 $\frac{9.3}{10}$ $\frac{9.7}{12}$ $\frac{9.7}{14}$ $\frac{5.6}{20}$ $\frac{5.0}{28}$ $\frac{4.5}{50}$

$\frac{7.4}{50}$ $\frac{7.4}{31}$ $\frac{7.7}{23}$ $\frac{9.9}{19}$ $\frac{10.3}{17-16}$ $\frac{10.2}{14}$ 9.2 $\frac{10.1}{11}$ $\frac{10.8}{14-16}$ $\frac{7.0}{22}$ $\frac{7.0}{31}$ $\frac{6.7}{50}$

$\frac{9.0}{50}$ $\frac{8.8}{31}$ $\frac{7.0}{23}$ $\frac{11.8}{18-17}$ $\frac{11.4}{14}$ 11.0 $\frac{11.3}{12}$ $\frac{12.1}{16}$ $\frac{9.5}{20}$ $\frac{9.3}{32}$ $\frac{9.0}{36}$ $\frac{8.6}{39}$ $\frac{8.1}{50}$

$\frac{8.2}{50}$ $\frac{8.1}{31}$ $\frac{8.1}{24}$ $\frac{12.9}{15-14}$ $\frac{12.6}{11}$ 12.3 $\frac{12.8}{11}$ $\frac{13.3}{13-14}$ $\frac{9.8}{20}$ $\frac{10.0}{30}$ $\frac{9.4}{50}$

$\frac{10.1}{50}$ $\frac{10.1}{31}$ $\frac{10.0}{26}$ $\frac{15.5}{17-15}$ $\frac{15.7}{11}$ 15.1 $\frac{15.5}{10}$ $\frac{15.9}{12-13}$ $\frac{14.7}{15}$ $\frac{12.9}{19}$ $\frac{11.5}{21}$ $\frac{10.7}{26}$ $\frac{10.9}{39}$ $\frac{11.8}{50}$

$\frac{1.9}{50}$ $\frac{1.7}{31}$ $\frac{1.8}{24}$ $\frac{4.6}{21}$ $\frac{3.6}{15-14}$ $\frac{5.1}{12}$ 4.6 $\frac{4.8}{9}$ $\frac{5.2}{11-13}$ $\frac{2.1}{19}$ $\frac{1.6}{26}$ $\frac{0.8}{48}$ $\frac{1.9}{50}$

Spike in 12" Oak 24' Lt 105+62

Sta	+	π	-	Elev.
		965.08		
103+54			1.8	63.3.
104			3.8	61.3.
+50			6.1	59.0.
+92			7.5	57.6.
105+37			8.6	56.5.
+60			9.3	55.8.
106			10.7	54.4.
+63			13.1	52.0.
T.P.	3.42	955.50.	13.20	951.88.✓
107			4.8	50.5.
+65			7.3	48.0.
108			8.5	46.8.
+50			10.1	45.2.

$$\begin{array}{cccccc} \frac{4.3}{50} & \frac{5.0}{36} & \frac{4.8}{29} & \frac{4.7}{25} & \frac{3.1}{20} & \frac{2.3}{16} \\ & & & & 1.8 & \frac{2.7}{10} & \frac{5.3}{14} & \frac{6.2}{23} & \frac{7.2}{34} & \frac{6.7}{44} & \frac{6.6}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{4.7}{50} & \frac{4.8}{31} & \frac{5.2}{23} & \frac{4.3}{20} & \frac{4.3}{16} & 3.8 \\ & & & & & \frac{4.5}{10} & \frac{7.3}{16} & \frac{8.1}{20} & \frac{8.1}{27} & \frac{8.1}{39} & \frac{8.0}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{8.3}{50} & \frac{8.6}{42} & \frac{8.4}{30} & \frac{8.9}{26} & \frac{9.0}{23} & \frac{6.6}{18} \\ & & & & & 6.1 & \frac{6.6}{9} & \frac{10.1}{14} & \frac{10.6}{22} & \frac{11.6}{32} & \frac{12.2}{50} \end{array}$$

$$\begin{array}{cccccc} & & & \text{F.L.} & & \text{F.L.} \\ \frac{12.7}{50} & \frac{13.5}{36} & \frac{13.5}{28} & \left(\frac{13.5}{28} \right) & \frac{8.2}{17} & \frac{8.0}{7.5} & \frac{12.8}{15} & \left(\frac{14.2}{20} \right) & \frac{14.0}{20} & \frac{14.5}{27} & \frac{15.2}{35} & \frac{15.8}{50} & \frac{16.4}{75} \end{array}$$

$$\begin{array}{cccccc} \frac{9.0}{50} & \frac{10.0}{35} & \frac{10.2}{26} & \frac{10.9}{22} & \frac{9.7}{19} & \frac{9.0}{9} & \frac{12.7}{18} & \frac{13.5}{26} & \frac{14.2}{42} & \frac{14.5}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{7.8}{50} & \frac{9.6}{29} & \frac{9.5}{23} & \frac{10.1}{18} & \frac{10.2}{14} & 9.3 \\ & & & & & \frac{9.3}{8} & \frac{9.8}{14} & \frac{11.2}{21} & \frac{11.3}{30} & \frac{11.1}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{7.2}{50} & \frac{7.3}{44} & \frac{8.1}{22} & \frac{11.7}{17} & \frac{11.4}{15} & 10.7 \\ & & & & & \frac{10.8}{9} & \frac{11.1}{11} & \frac{11.9}{14} & \frac{10.8}{16} & \frac{10.4}{19} & \frac{10.4}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{9.5}{50} & \frac{9.0}{23} & \frac{14.0}{15} & \frac{13.8}{14} & \frac{13.8}{12} & 12.1 \\ & & & & & \frac{13.5}{12} & \frac{14.4}{14} & \frac{13.1}{16} & \frac{10.7}{19} & \frac{12.4}{23} & \frac{13.5}{37} & \frac{13.5}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{3.0}{50} & \frac{3.0}{23} & \frac{5.7}{18} & \frac{5.4}{16} & \frac{5.4}{12} & 4.8 \\ & & & & & \frac{5.5}{13} & \frac{6.1}{15} & \frac{4.3}{15} & \frac{3.8}{16} & \frac{5.6}{19} & \frac{5.9}{23} & \frac{5.9}{43} & \frac{5.9}{50} \end{array}$$

$$\begin{array}{cccccc} & & & \text{F.L.} & & \text{F.L.} \\ \frac{11.4}{70} & \frac{11.7}{60} & \frac{11.7}{50} & \frac{11.6}{19} & \left(\frac{12.4}{19} \right) & \frac{8.3}{13} & 7.3 & \frac{8.2}{13} & \left(\frac{10.5}{10} \right) & \frac{10.4}{16} & \frac{9.4}{18} & \frac{9.6}{19} & \frac{9.6}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{10.8}{50} & \frac{11.1}{35} & \frac{11.0}{27} & \frac{9.8}{15} & \frac{8.7}{11} & 8.5 \\ & & & & & \frac{9.5}{15} & \frac{9.8}{17} & \frac{9.3}{19} & \frac{10.4}{20} & \frac{10.9}{39} & \frac{11.0}{50} & \frac{11.0}{60} \end{array}$$

$$\begin{array}{cccccc} \frac{9.9}{50} & \frac{9.8}{35} & \frac{9.6}{21} & \frac{11.3}{19} & \frac{11.4}{14} & \frac{10.0}{11} & 10.1 \\ & & & & & \frac{11.1}{15} & \frac{11.1}{16} & \frac{8.2}{18} & \frac{8.0}{24} & \frac{8.0}{33} & \frac{8.0}{50} \end{array}$$

Sta	+	π ✓	—	Elev.
		955.30		
109			11.7	43.6.
+74			13.7	41.6.
T.P.	2.38	944.34 ✓	13.34	941.96 ✓
110+14			4.1	40.2.
+26			4.6	39.7.
+84			6.2	38.1.
111+36			7.1	37.2.
112			8.0	36.3.
+71			9.1	35.2.
113			9.7	34.6.
+50			10.6	33.7.
T.P.	0.70	934.60 ✓	10.44	933.90 ✓
114			1.9	32.7.
+50			2.8	31.8.

$\frac{8.2}{50}$ $\frac{9.2}{23}$ $\frac{13.0}{16-14}$ $\frac{12.1}{13}$ $\frac{12.0}{9}$ 11.7 $\frac{12.5}{14}$ $\frac{12.9}{16}$ $\frac{13.6}{17-19}$ $\frac{8.9}{27}$ $\frac{10.0}{50}$

$\frac{12.3}{50}$ $\frac{11.2}{23}$ $\frac{14.9}{16-14}$ $\frac{14.0}{12}$ $\frac{14.0}{8}$ 13.7 $\frac{14.1}{11}$ $\frac{14.5}{15}$ $\frac{13.6}{22}$ $\frac{7.6}{31}$ $\frac{8.5}{50}$

$\frac{12.4}{50}$ $\frac{8.8}{35}$ $\frac{8.7}{25}$ $\frac{7.7}{17}$ $\frac{4.7}{12}$ 4.1 $\frac{4.6}{11}$ $\frac{5.1}{15}$ $\frac{5.3}{18}$ $\frac{2.9}{22}$ $\frac{1.8}{44}$ $\frac{1.8}{50}$

$\frac{15.4}{50}$ $\frac{13.6}{31}$ $\frac{12.6}{24}$ $\frac{5.4}{11}$ 4.6 $\frac{5.1}{12}$ $\frac{6.4}{16-18}$ $\frac{5.5}{21}$ $\frac{4.4}{26}$ $\frac{4.4}{31}$ $\frac{3.0}{50}$

Water Too Deep to obtain further readings

F.L.

F.L.

$\frac{14.7}{26}$ $\frac{15.2}{27}$ $\frac{6.8}{12}$ 6.2 $\frac{7.0}{12}$ $\frac{7.3}{18}$ $\frac{10.9}{22}$ $\frac{11.3}{22-23}$ $\frac{8.8}{28}$ $\frac{8.2}{39}$ $\frac{6.7}{50}$

$\frac{14.0}{50}$ $\frac{13.5}{30}$ $\frac{14.0}{21}$ $\frac{7.6}{10}$ 7.1 $\frac{7.6}{12}$ $\frac{8.8}{17}$ $\frac{9.1}{25}$ $\frac{8.4}{28}$ $\frac{7.5}{39}$ $\frac{6.3}{50}$

$\frac{5.2}{50}$ $\frac{7.5}{18}$ $\frac{8.2}{8}$ 8.0 $\frac{8.4}{13}$ $\frac{9.2}{15-17}$ $\frac{3.9}{28}$ $\frac{4.6}{50}$

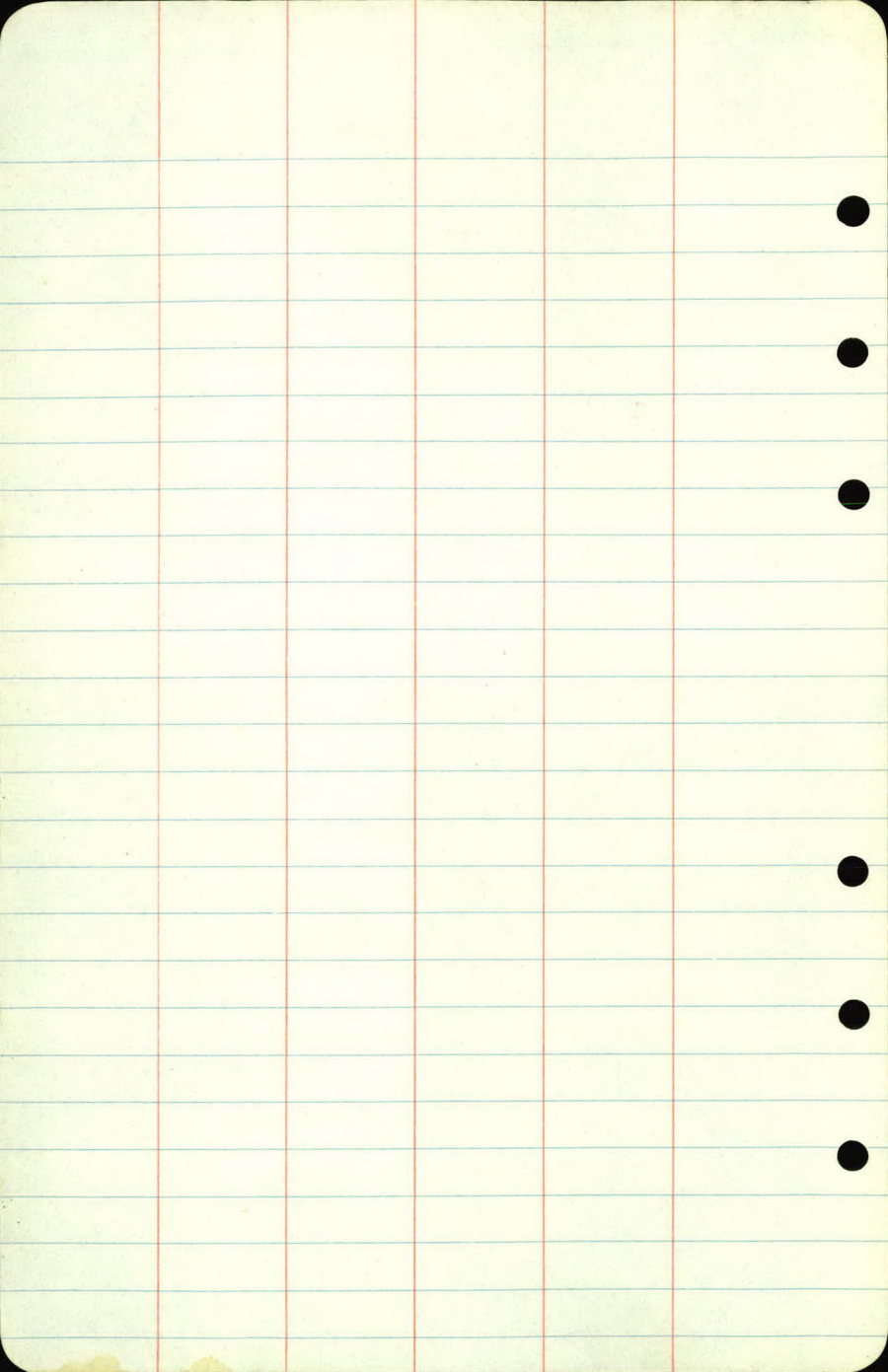
$\frac{1.1}{50}$ $\frac{1.2}{37}$ $\frac{2.0}{30}$ $\frac{10.1}{19}$ $\frac{10.4}{16-15}$ $\frac{2.5}{11}$ 9.1 $\frac{9.6}{13}$ $\frac{10.3}{16-18}$ $\frac{10.1}{19}$ $\frac{3.3}{30}$ $\frac{4.6}{50}$

$\frac{4.0}{50}$ $\frac{3.0}{30}$ $\frac{10.5}{21}$ $\frac{10.9}{15-14}$ $\frac{9.8}{11}$ 9.7 $\frac{10.1}{12}$ $\frac{10.2}{15}$ $\frac{9.1}{20}$ $\frac{2.6}{29}$ $\frac{3.9}{50}$

$\frac{10.6}{50}$ $\frac{9.4}{25}$ $\frac{12.2}{20}$ $\frac{12.2}{15}$ $\frac{10.8}{11}$ 10.6 $\frac{10.9}{11}$ $\frac{11.1}{14}$ $\frac{9.1}{20}$ $\frac{5.0}{26}$ $\frac{5.5}{50}$

$\frac{4.8}{50}$ $\frac{3.3}{23}$ $\frac{3.1}{15-14}$ $\frac{2.2}{11}$ 1.9 $\frac{2.1}{10}$ $\frac{2.5}{14}$ $\frac{2.9}{15-17}$ $\frac{0.0}{23}$ $\frac{+1.5}{50}$

$\frac{7.7}{50}$ $\frac{7.3}{25}$ $\frac{6.5}{18}$ $\frac{3.5}{11}$ 2.8 $\frac{3.6}{13}$ $\frac{4.5}{15-17}$ $\frac{3.9}{20}$ $\frac{2.6}{50}$



Sta	+	π	-	Elev.
		93460		
115			37	30.9
+50			43	30.3
116 + 08			49	29.7
+50			49	29.7
117			50	29.6
+50			52	29.4
118			52	29.4
+50			51	29.5
B.M.	12.00	941.55	5.07	929.53
119			11.7	29.9
+50			11.5	30.1
120			11.0	30.6
+46			10.4	31.2

929.55

$\frac{10.1}{50} \frac{9.6}{27} \frac{8.7}{19} \frac{4.1}{11} \quad 3.7 \quad \frac{4.0}{11} \frac{6.5}{17} \frac{6.2}{22} \frac{5.4}{50}$

$\frac{10.7}{50} \frac{10.6}{30} \frac{11.1}{22} \frac{7.1}{16} \frac{4.8}{12} \quad 4.3 \quad \frac{4.7}{12} \frac{8.3}{17} \frac{8.5}{24} \frac{8.5}{32} \frac{7.7}{50}$

F.L. ← Drain F.L.
 $\frac{10.8}{50} \frac{11.6}{22} \frac{10.9}{22} \frac{5.3}{11} \quad 4.9 \quad \frac{5.6}{11} \frac{10.9}{19} \frac{11.1}{19} \frac{10.4}{25} \frac{10.1}{50}$

$\frac{10.5}{50} \frac{10.3}{30} \frac{10.2}{22} \frac{5.4}{12} \quad 4.9 \quad \frac{5.6}{13} \frac{9.6}{20} \frac{10.2}{23} \frac{10.2}{36} \frac{10.1}{50}$

$\frac{10.1}{50} \frac{9.7}{22} \frac{9.2}{18} \frac{5.6}{12} \quad 5.0 \quad \frac{5.7}{12} \frac{9.1}{17} \frac{9.3}{24} \frac{9.3}{37} \frac{9.2}{50}$

$\frac{8.7}{50} \frac{8.7}{29} \frac{8.1}{18} \frac{5.5}{12} \quad 5.2 \quad \frac{5.9}{13} \frac{8.2}{17} \frac{8.6}{26} \frac{8.2}{38} \frac{8.1}{50}$

$\frac{8.2}{50} \frac{8.2}{22} \frac{8.0}{16} \frac{5.8}{12} \quad 5.2 \quad \frac{5.7}{13} \frac{7.4}{16} \frac{7.7}{19} \frac{6.9}{34} \frac{5.9}{50}$

$\frac{8.3}{50} \frac{7.4}{34} \frac{7.3}{19} \frac{7.5}{17-15} \frac{5.6}{12} \quad 5.1 \quad \frac{5.4}{12} \frac{5.8}{13} \frac{5.6}{18} \frac{5.5}{29} \frac{3.7}{50}$

B.M. - Spike in RP 28' Lt 5th 118+36
 $\frac{14.1}{50} \frac{12.6}{25} \frac{12.0}{19} \frac{13.5}{16-14} \frac{11.9}{12} \quad 11.7 \quad \frac{12.0}{11} \frac{12.0}{17} \frac{11.0}{21} \frac{9.8}{50}$

$\frac{13.0}{50} \frac{11.7}{32} \frac{11.5}{21} \frac{13.4}{18-16} \frac{11.8}{12} \quad 11.5 \quad \frac{11.8}{12} \frac{12.0}{14-16} \frac{9.4}{21} \frac{6.9}{50}$

$\frac{11.0}{50} \frac{9.1}{23} \frac{12.8}{17-15} \frac{11.2}{12} \quad 11.0 \quad \frac{11.2}{12} \frac{11.5}{15} \frac{7.8}{23} \frac{6.7}{33} \frac{4.0}{50}$

$\frac{9.6}{50} \frac{8.6}{38} \frac{7.9}{26} \frac{12.6}{18-14} \frac{10.9}{11} \quad 10.4 \quad \frac{10.9}{13} \frac{11.0}{17-19} \frac{8.9}{22} \frac{8.3}{32} \frac{7.1}{50}$

Sta	+	π	-	Elev.
		941.55 [✓]		
121			10.1	31.5 [✓]
+50			10.0	31.6 [✓]
122			10.2	31.4 [✓]
+33			10.9	30.7 [✓]
123			11.8	29.8 [✓]
+65			13.8	27.8 [✓]
T.P.	2.39	932.15 [✓]	11.79	929.76 [✓]
124			5.1	27.1 [✓]
+50			6.0	26.2 [✓]
125			7.0	25.2 [✓]
T.P.	4.04	927.88 [✓]	8.31	923.84 [✓]
+50			3.8	24.1 [✓]
126			4.3	23.6 [✓]
+40			4.7	23.2 [✓]

<u>7.0</u>	<u>5.2</u>	<u>11.8</u>	<u>10.4</u>		<u>10.6</u>	<u>10.8</u>	<u>4.6</u>	<u>4.7</u>
50	26	17-14	12	10.1	12	15	26	50

<u>6.0</u>	<u>5.1</u>	<u>10.9</u>	<u>11.7</u>	<u>10.6</u>		<u>10.5</u>	<u>10.6</u>	<u>2.7</u>	<u>2.4</u>	<u>3.8</u>
50	27	18	15-14	11	10.0	12	16	28	45	50

<u>9.0</u>	<u>7.1</u>	<u>12.3</u>	<u>10.8</u>		<u>10.8</u>	<u>11.0</u>	<u>5.6</u>	<u>5.5</u>	<u>6.7</u>	<u>7.0</u>
50	23	16-14	12	10.2	12	13-14	24	44	47	50

<u>10.4</u>	<u>8.6</u>	<u>12.0</u>	<u>12.5</u>	<u>11.3</u>		<u>11.6</u>	<u>11.8</u>	<u>9.4</u>	<u>8.7</u>	<u>9.1</u>	<u>9.4</u>
50	22	17	16-15	13	10.9	12	16-17	22	42	45	50

<u>3.4</u>	<u>3.2</u>	<u>12.7</u>	<u>13.2</u>	<u>12.5</u>		<u>12.4</u>	<u>12.6</u>	<u>6.6</u>	<u>7.0</u>	<u>7.8</u>	<u>8.0</u>	<u>10.4</u>
50	29	18	16-14	12	11.8	11	14	23	33	35	42	50

<u>9.1</u>	<u>10.8</u>	<u>14.9</u>	<u>14.2</u>		<u>14.0</u>	<u>14.6</u>	<u>14.2</u>	<u>11.3</u>	<u>11.7</u>	<u>13.7</u>
50	24	17-14	13	13.8	10	11	14	19	41	50

Top Spike 5 to 123

<u>2.0</u>	<u>1.9</u>	<u>6.4</u>	<u>5.9</u>	<u>5.6</u>		<u>5.5</u>	<u>5.7</u>	<u>1.8</u>	<u>2.4</u>	<u>4.9</u>
50	25	18-14	13	10	5.1	12	13-15	20	41	50

<u>10.0</u>	<u>5.8</u>	<u>4.6</u>	<u>7.5</u>	<u>7.4</u>	<u>6.8</u>	<u>6.6</u>	<u>7.0</u>	<u>6.8</u>	<u>3.7</u>	<u>3.2</u>	<u>4.4</u>
50	24	23	17	15	12	6.0	11	13-15	16	21	41

<u>16.0</u>	<u>13.4</u>	<u>12.6</u>	<u>7.8</u>		<u>7.5</u>	<u>7.8</u>	<u>6.0</u>	<u>6.9</u>	<u>6.1</u>	<u>8.3</u>
50	33	23	12	7.0	11	14-15	19	26	39	50

<u>12.1</u>	<u>12.1</u>	<u>11.5</u>	<u>9.8</u>	<u>4.4</u>		<u>4.3</u>	<u>6.0</u>	<u>6.3</u>	<u>7.8</u>
100	50	34	23	12	3.8	12	17	33	50

<u>12.0</u>	<u>4.4</u>	<u>4.9</u>			<u>4.9</u>	<u>8.3</u>	<u>7.4</u>	<u>8.9</u>
50	21	11	4.3		12	18	32	50

<u>12.0</u>	<u>11.7</u>	<u>11.3</u>	<u>5.1</u>		<u>5.1</u>	<u>9.6</u>	<u>9.9</u>	<u>8.0</u>	<u>7.3</u>
50	29	21	10	4.7	13	21	26	37	50

Sta

+

K

-

Elev.

927.88 ✓

126+90

5.0

22.9 ✓

127+50

4.8

23.1 ✓

128

4.3

23.6 ✓

+50

3.5

24.4 ✓

129

2.6

25.3 ✓

+50

0.9

27.0 ✓

T.P.

10.79

937.71 ✓

0.96

926.92 ✓

130

9.2

28.5 ✓

+50

7.8

29.9 ✓

131+18

5.8

31.9 ✓

+30

5.5

32.2 ✓

+40

5.3

32.4 ✓

+48

5.0

32.7 ✓

$$\begin{array}{ccccccc}
 & & & \text{F.L.} & & & \\
 \frac{12.1}{75} & \frac{12.1}{50} & \frac{11.7}{21} & \frac{12.7}{24} \frac{5.4}{11} & \frac{5.5}{12} \frac{13.0}{22} & \text{F.L.} & \frac{13.0}{24} \frac{12.4}{50} \frac{12.1}{100} \frac{12.6}{150}
 \end{array}$$

$$\frac{12.1}{50} \frac{11.6}{23} \frac{5.2}{12} \frac{5.4}{12} \frac{12.3}{50} \frac{12.4}{50}$$

$$\frac{12.1}{50} \frac{11.6}{24} \frac{4.8}{12} \frac{5.1}{12} \frac{12.3}{25} \frac{12.5}{50}$$

$$\frac{12.0}{50} \frac{12.0}{34} \frac{11.6}{25} \frac{4.0}{12} \frac{4.2}{12} \frac{12.3}{25} \frac{12.4}{50}$$

$$\frac{11.7}{50} \frac{11.4}{35} \frac{10.0}{23} \frac{3.2}{12} \frac{3.4}{13} \frac{11.0}{25} \frac{11.6}{30}$$

$$\frac{4.6}{50} \frac{4.8}{28} \frac{4.0}{18} \frac{1.4}{13} \frac{1.6}{13} \frac{6.3}{21} \frac{6.5}{27} \frac{8.3}{50}$$

$$\frac{5.5}{50} \frac{5.4}{26} \frac{10.8}{18-14} \frac{9.5}{11} \frac{9.7}{11} \frac{10.8}{17-18} \frac{9.1}{22} \frac{10.7}{33} \frac{13.4}{50}$$

$$\frac{5.6}{50} \frac{4.0}{35} \frac{3.7}{23} \frac{9.4}{17} \frac{9.4}{13} \frac{8.3}{11} \frac{8.3}{11} \frac{8.9}{15} \frac{4.0}{24} \frac{4.7}{33} \frac{5.8}{50}$$

$$\frac{11.1}{50} \frac{6.7}{34} \frac{7.4}{13} \frac{6.1}{11} \frac{6.4}{58} \frac{2.0}{15-18} \frac{4.2}{23} \frac{5.2}{50}$$

$$\frac{7.9}{50} \frac{6.3}{23} \frac{5.6}{8} \frac{6.1}{13} \frac{6.7}{16-18} \frac{3.9}{23} \frac{4.8}{50}$$

$$\text{E Reservoir} \frac{7.7}{50} \frac{6.3}{29} \frac{5.5}{9} \frac{5.9}{15} \frac{6.2}{17} \frac{3.9}{24} \frac{5.2}{50}$$

$$\frac{7.7}{50} \frac{5.9}{23} \frac{5.2}{9} \frac{5.8}{50} \frac{5.9}{17} \frac{3.9}{22} \frac{4.0}{27} \frac{5.5}{50}$$

Sta	+	π	-	Elev
		937.78		
131	+57		4.7	33.0
	+75		4.1	33.6
132			3.3	34.4
T.P.	11.74	947.67	1.78	935.93
	+50		11.7	36.0
133			10.3	37.4
	+30		9.4	38.3
	+70		8.4	39.3
134			7.6	40.1
	+28		6.9	40.8
	+54		6.3	41.4
135			5.6	42.1
	+42		5.1	42.6
T.P.	16.03	954.12	4.58	943.09

$$\begin{array}{r} 9.4 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 34 \end{array} \quad \begin{array}{r} 6.6 \\ 26 \end{array} \quad \begin{array}{r} 5.6 \\ 22 \end{array} \quad \begin{array}{r} 5.0 \\ 8 \end{array} \quad 4.7 \quad \begin{array}{r} 4.8 \\ 12 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 5.6 \\ 17 \end{array} \quad \begin{array}{r} 3.5 \\ 22 \end{array} \quad \begin{array}{r} 4.1 \\ 50 \end{array}$$

$$\begin{array}{r} 5.4 \\ 50 \end{array} \quad \begin{array}{r} 3.3 \\ 35 \end{array} \quad \begin{array}{r} 6.6 \\ 28 \end{array} \quad \begin{array}{r} 6.5 \\ 24 \end{array} \quad \begin{array}{r} 6.1 \\ 20 \end{array} \quad \begin{array}{r} 4.8 \\ 15 \end{array} \quad \begin{array}{r} 4.6 \\ 11 \end{array} \quad \begin{array}{r} 4.4 \\ 8 \end{array} \quad 4.1 \quad \begin{array}{r} 4.2 \\ 11 \end{array} \quad \begin{array}{r} 4.8 \\ 15 \end{array} \quad \begin{array}{r} 5.0 \\ 17 \end{array} \quad \begin{array}{r} 2.9 \\ 22 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 1.1 \\ 27 \end{array} \quad \begin{array}{r} 4.0 \\ 22 \end{array} \quad \begin{array}{r} 5.0 \\ 15 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 3.7 \\ 11 \end{array} \quad 3.3 \quad \begin{array}{r} 3.5 \\ 9 \end{array} \quad \begin{array}{r} 4.0 \\ 14 \end{array} \quad \begin{array}{r} 4.2 \\ 17 \end{array} \quad \begin{array}{r} 1.4 \\ 23 \end{array} \quad \begin{array}{r} 1.8 \\ 31 \end{array} \quad \begin{array}{r} 2.9 \\ 50 \end{array}$$

$$\begin{array}{r} 12.7 \\ 50 \end{array} \quad \begin{array}{r} 8.8 \\ 30 \end{array} \quad \begin{array}{r} 8.1 \\ 23 \end{array} \quad \begin{array}{r} 13.0 \\ 16-13 \end{array} \quad \begin{array}{r} 12.0 \\ 10 \end{array} \quad 11.7 \quad \begin{array}{r} 12.1 \\ 11 \end{array} \quad \begin{array}{r} 12.3 \\ 14 \end{array} \quad \begin{array}{r} 10.3 \\ 22 \end{array} \quad \begin{array}{r} 6.7 \\ 26 \end{array} \quad \begin{array}{r} 7.0 \\ 34 \end{array} \quad \begin{array}{r} 7.4 \\ 50 \end{array}$$

$$\begin{array}{r} 12.1 \\ 50 \end{array} \quad \begin{array}{r} 7.6 \\ 28 \end{array} \quad \begin{array}{r} 8.1 \\ 21 \end{array} \quad \begin{array}{r} 11.4 \\ 17-15 \end{array} \quad \begin{array}{r} 10.9 \\ 12 \end{array} \quad \begin{array}{r} 10.6 \\ 10 \end{array} \quad 10.3 \quad \begin{array}{r} 10.4 \\ 11 \end{array} \quad \begin{array}{r} 10.7 \\ 12 \end{array} \quad \begin{array}{r} 10.0 \\ 15 \end{array} \quad \begin{array}{r} 9.2 \\ 19 \end{array} \quad \begin{array}{r} 1.2 \\ 30 \end{array} \quad \begin{array}{r} 0.0 \\ 43 \end{array} \quad \begin{array}{r} +1.0 \\ 50 \end{array} \quad \begin{array}{r} +1.5 \\ 75 \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \end{array} \quad \begin{array}{r} 11.4 \\ 34 \end{array} \quad \begin{array}{r} 9.4 \\ 20 \end{array} \quad \begin{array}{r} 10.9 \\ 16-15 \end{array} \quad \begin{array}{r} 10.0 \\ 10 \end{array} \quad \begin{array}{r} 9.7 \\ 8 \end{array} \quad 9.4 \quad \begin{array}{r} 9.5 \\ 11 \end{array} \quad \begin{array}{r} 9.9 \\ 12-13 \end{array} \quad \begin{array}{r} 9.0 \\ 15 \end{array} \quad \begin{array}{r} 8.2 \\ 18 \end{array} \quad \begin{array}{r} 1.7 \\ 27 \end{array} \quad \begin{array}{r} 0.5 \\ 42 \end{array} \quad \begin{array}{r} +1.6 \\ 52 \end{array} \quad \begin{array}{r} +2.5 \\ 75 \end{array}$$

$$\begin{array}{r} 14.4 \\ 50 \end{array} \quad \begin{array}{r} 14.2 \\ 43 \end{array} \quad \begin{array}{r} 13.6 \\ 25 \end{array} \quad \begin{array}{r} 11.6 \\ 18 \end{array} \quad \begin{array}{r} 8.9 \\ 11 \end{array} \quad 8.4 \quad \begin{array}{r} 9.0 \\ 13 \end{array} \quad \begin{array}{r} 10.4 \\ 16-18 \end{array} \quad \begin{array}{r} 9.6 \\ 21 \end{array} \quad \begin{array}{r} 8.8 \\ 33 \end{array} \quad \begin{array}{r} 8.0 \\ 42 \end{array} \quad \begin{array}{r} 6.5 \\ 50 \end{array}$$

$$\begin{array}{r} 12.5 \\ 50 \end{array} \quad \begin{array}{r} 11.7 \\ 36 \end{array} \quad \begin{array}{r} 10.5 \\ 20 \end{array} \quad \begin{array}{r} 8.0 \\ 11 \end{array} \quad 7.6 \quad \begin{array}{r} 8.6 \\ 14 \end{array} \quad \begin{array}{r} 11.6 \\ 21 \end{array} \quad \begin{array}{r} 12.1 \\ 24 \end{array} \quad \begin{array}{r} 12.0 \\ 32 \end{array} \quad \begin{array}{r} 11.3 \\ 45 \end{array} \quad \begin{array}{r} 10.5 \\ 50 \end{array}$$

$$\begin{array}{r} 14.0 \\ 50 \end{array} \quad \begin{array}{r} 11.0 \\ 42 \end{array} \quad \begin{array}{r} 10.2 \\ 29 \end{array} \quad \begin{array}{r} 8.5 \\ 17 \end{array} \quad \begin{array}{r} 7.3 \\ 13 \end{array} \quad 6.9 \quad \begin{array}{r} 7.4 \\ 11 \end{array} \quad \begin{array}{r} 7.8 \\ 14 \end{array} \quad \begin{array}{r} 10.6 \\ 20 \end{array} \quad \begin{array}{r} 11.4 \\ 26 \end{array} \quad \begin{array}{r} 10.7 \\ 42 \end{array} \quad \begin{array}{r} 9.7 \\ 50 \end{array}$$

$$\begin{array}{r} 16.2 \\ 50 \end{array} \quad \begin{array}{r} 12.4 \\ 31 \end{array} \quad \begin{array}{r} 10.5 \\ 20 \end{array} \quad \begin{array}{r} 7.0 \\ 13 \end{array} \quad 6.3 \quad 7.0 \quad \begin{array}{r} 9.8 \\ 19 \end{array} \quad \begin{array}{r} 10.8 \\ 23 \end{array} \quad \begin{array}{r} 10.5 \\ 38 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 17.6 \\ 50 \end{array} \quad \begin{array}{r} 14.5 \\ 33 \end{array} \quad \begin{array}{r} 14.0 \\ 24 \end{array} \quad \begin{array}{r} 6.5 \\ 11 \end{array} \quad \begin{array}{r} 6.2 \\ 9 \end{array} \quad 5.6 \quad \begin{array}{r} 5.9 \\ 12 \end{array} \quad \begin{array}{r} 9.6 \\ 18 \end{array} \quad \begin{array}{r} 10.7 \\ 26 \end{array} \quad \begin{array}{r} 11.2 \\ 50 \end{array}$$

$$\begin{array}{r} 13.7 \\ 50 \end{array} \quad \begin{array}{r} 12.6 \\ 33 \end{array} \quad \begin{array}{r} 9.9 \\ 22 \end{array} \quad \begin{array}{r} 5.6 \\ 11 \end{array} \quad 5.1 \quad \begin{array}{r} 5.6 \\ 12 \end{array} \quad \begin{array}{r} 7.2 \\ 16 \end{array} \quad \begin{array}{r} 7.0 \\ 20 \end{array} \quad \begin{array}{r} 8.0 \\ 29 \end{array} \quad \begin{array}{r} 8.3 \\ 33 \end{array} \quad \begin{array}{r} 9.0 \\ 47 \end{array} \quad \begin{array}{r} 10.0 \\ 50 \end{array}$$

34	+	π	-	Elev
		954.12		

136			11.0	43.1
-----	--	--	------	------

+31			11.4	42.7
-----	--	--	------	------

+70			12.6	41.5
-----	--	--	------	------

137			13.7	40.4
-----	--	--	------	------

T.P.	11.26	951.72	13.66	940.46
------	-------	--------	-------	--------

+39			12.6	39.1
-----	--	--	------	------

+79			14.0	37.7
-----	--	--	------	------

138			(14.8)	36.9
-----	--	--	--------	------

+32			(16.1)	35.6
-----	--	--	--------	------

+72			(17.7)	34.0
-----	--	--	--------	------

139			(18.9)	32.8
-----	--	--	--------	------

T.P.	1.65	942.11	11.26	940.46
------	------	--------	-------	--------

138			5.2	36.9
-----	--	--	-----	------

+32			6.5	35.6
-----	--	--	-----	------

$\frac{9.4}{50}$ $\frac{8.2}{40}$ $\frac{6.2}{24}$ $\frac{11.6}{16}$ $\frac{11.8}{13}$ $\frac{11.2}{11}$ 11.0 $\frac{11.3}{11}$ $\frac{11.4}{13}$ $\frac{10.0}{19}$ $\frac{3.3}{30}$ $\frac{4.5}{41}$ $\frac{5.1}{50}$ $\frac{8.1}{75}$

$\frac{4.2}{50}$ $\frac{2.7}{28}$ $\frac{11.0}{18}$ $\frac{11.6}{16}$ $\frac{12.1}{13}$ $\frac{11.7}{12}$ 11.4 $\frac{11.8}{12}$ $\frac{11.2}{14}$ $\frac{9.5}{20}$ $\frac{2.5}{32}$ $\frac{3.6}{50}$ $\frac{6.3}{60}$ $\frac{10.2}{75}$

$\frac{7.7}{50}$ $\frac{7.8}{44}$ $\frac{7.7}{25}$ $\frac{13.0}{18}$ $\frac{13.6}{16}$ $\frac{13.8}{14}$ $\frac{13.0}{12}$ 12.6 $\frac{12.9}{10}$ $\frac{13.3}{11}$ $\frac{11.7}{18}$ $\frac{7.5}{24}$ $\frac{8.0}{30}$ $\frac{7.6}{41}$ $\frac{8.3}{50}$

$\frac{8.0}{50}$ $\frac{8.2}{26}$ $\frac{8.8}{23}$ $\frac{14.4}{16}$ $\frac{14.6}{13}$ $\frac{14.1}{11}$ 13.7 $\frac{13.9}{12}$ $\frac{13.9}{16}$ $\frac{10.9}{21}$ $\frac{11.5}{30}$ $\frac{11.6}{40}$ $\frac{12.8}{50}$

5th 137

$\frac{6.1}{50}$ $\frac{7.1}{23}$ $\frac{13.3}{15}$ $\frac{13.7}{13}$ $\frac{13.0}{11}$ 12.6 $\frac{12.9}{12}$ $\frac{12.7}{15}$ $\frac{11.3}{19}$ $\frac{6.6}{26}$ $\frac{7.0}{36}$ $\frac{6.6}{46}$ $\frac{6.9}{50}$

$\frac{9.7}{50}$ $\frac{8.1}{25}$ $\frac{14.4}{17}$ $\frac{15.1}{14}$ $\frac{14.7}{13}$ 14.0 $\frac{14.6}{11}$ $\frac{13.6}{14}$ $\frac{11.2}{21}$ $\frac{3.9}{29}$ $\frac{3.3}{44}$ $\frac{4.3}{50}$ $\frac{6.4}{60}$ $\frac{6.1}{75}$

$\frac{10.2}{50}$ $\frac{9.5}{24}$

14.8

$\frac{5.7}{29}$ $\frac{5.3}{45}$ $\frac{6.5}{50}$ $\frac{7.4}{60}$ $\frac{6.9}{75}$

$\frac{12.8}{50}$ $\frac{13.2}{29}$ $\frac{12.8}{21}$

16.7

$\frac{14.9}{19}$ $\frac{9.5}{28}$ $\frac{8.2}{50}$

17.7

$\frac{11.5}{26}$ $\frac{9.8}{38}$ $\frac{9.0}{50}$

18.9

$\frac{14.2}{25}$ $\frac{12.7}{38}$ $\frac{11.8}{41}$ $\frac{11.8}{50}$

$\frac{5.1}{19}$ $\frac{5.5}{17}$ $\frac{7.1}{16-15}$ $\frac{5.8}{14}$ $\frac{5.6}{11}$ 5.2 $\frac{5.5}{11}$ $\frac{4.9}{14}$ $\frac{3.4}{20}$

$\frac{7.8}{15}$ $\frac{7.5}{13}$ $\frac{6.8}{11}$ 6.5 $\frac{6.7}{11}$ $\frac{6.7}{14}$ $\frac{5.2}{19}$

4
5.00
49.90

Sta	+	π	-	Elev.
		942.11		
138+72			8.1	340.
139			9.3	328.
T.P.	1.76	933.88	9.99	932.12.
+29			2.3	31.6.
140+50			3.3	30.6.
140			4.8	29.1.
141+50			5.5	28.4.
141			5.8	28.1.
+40			5.6	28.3.
+95			5.4	28.5.
B.M.	1.36	931.24	3.98	929.90. (929.88)
142+32			2.9	28.3.
+62			3.1	28.1.
143			3.6	27.6.

$$\begin{array}{r} 7.1 \\ 50 \end{array} \begin{array}{r} 5.5 \\ 24 \end{array} \begin{array}{r} 5.4 \\ 20 \end{array} \begin{array}{r} 8.8 \\ 17 \end{array} \begin{array}{r} 9.4 \\ 14 \end{array} \begin{array}{r} 9.1 \\ 13 \end{array} \begin{array}{r} 8.5 \\ 11 \end{array} \begin{array}{r} 8.1 \\ 8 \end{array} \begin{array}{r} 8.4 \\ 11 \end{array} \begin{array}{r} 8.5 \\ 12 \end{array} \begin{array}{r} 7.5 \\ 12 \end{array} \begin{array}{r} 6.2 \\ 20 \end{array}$$

$$\begin{array}{r} 10.5 \\ 50 \end{array} \begin{array}{r} 10.5 \\ 37 \end{array} \begin{array}{r} 10.6 \\ 27 \end{array} \begin{array}{r} 9.2 \\ 19 \end{array} \begin{array}{r} 10.5 \\ 17 \end{array} \begin{array}{r} 9.8 \\ 13 \end{array} \begin{array}{r} 9.3 \\ 11 \end{array} \begin{array}{r} 9.4 \\ 15 \end{array} \begin{array}{r} 10.0 \\ 18 \end{array} \begin{array}{r} 8.7 \\ 18 \end{array}$$

$$\begin{array}{r} 10.4 \\ 50 \end{array} \begin{array}{r} 8.9 \\ 28 \end{array} \begin{array}{r} 3.2 \\ 14 \end{array} \begin{array}{r} 2.9 \\ 9 \end{array} \begin{array}{r} 2.4 \\ 11 \end{array} \begin{array}{r} 2.3 \\ 20 \end{array} \begin{array}{r} 1.8 \\ 35 \end{array} \begin{array}{r} 1.3 \\ 50 \end{array}$$

$$\begin{array}{r} 11.3 \\ 50 \end{array} \begin{array}{r} 11.0 \\ 27 \end{array} \begin{array}{r} 8.5 \\ 22 \end{array} \begin{array}{r} 3.7 \\ 11 \end{array} \begin{array}{r} 4.0 \\ 14 \end{array} \begin{array}{r} 7.3 \\ 19 \end{array} \begin{array}{r} 7.2 \\ 24 \end{array} \begin{array}{r} 8.1 \\ 33 \end{array} \begin{array}{r} 3.0 \\ 39 \end{array} \begin{array}{r} 2.2 \\ 50 \end{array}$$

$$\begin{array}{r} 14.4 \\ 50 \end{array} \begin{array}{r} 11.3 \\ 21 \end{array} \begin{array}{r} 10.2 \\ 19 \end{array} \begin{array}{r} 5.5 \\ 11 \end{array} \begin{array}{r} 5.3 \\ 14 \end{array} \begin{array}{r} 10.5 \\ 24 \end{array} \begin{array}{r} 11.9 \\ 30 \end{array} \begin{array}{r} 11.6 \\ 45 \end{array} \begin{array}{r} 10.9 \\ 50 \end{array}$$

$$\begin{array}{r} 14.3 \\ 50 \end{array} \begin{array}{r} 12.5 \\ 20 \end{array} \begin{array}{r} 11.3 \\ 18 \end{array} \begin{array}{r} 6.0 \\ 11 \end{array} \begin{array}{r} 5.9 \\ 17 \end{array} \begin{array}{r} 11.8 \\ 22 \end{array} \begin{array}{r} 12.5 \\ 28 \end{array} \begin{array}{r} 12.5 \\ 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \end{array} \begin{array}{r} 12.6 \\ 24 \end{array} \begin{array}{r} 11.3 \\ 18 \end{array} \begin{array}{r} 6.1 \\ 10 \end{array} \begin{array}{r} 6.5 \\ 12 \end{array} \begin{array}{r} 13.2 \\ 23 \end{array} \begin{array}{r} 14.4 \\ 50 \end{array}$$

$$\begin{array}{r} 10.9 \\ 50 \end{array} \begin{array}{r} 10.5 \\ 33 \end{array} \begin{array}{r} 11.2 \\ 19 \end{array} \begin{array}{r} \text{F.L.} \\ 10.9 \\ 19 \end{array} \begin{array}{r} 6.1 \\ 10 \end{array} \begin{array}{r} 5.6 \\ 12 \end{array} \begin{array}{r} 6.4 \\ 22 \end{array} \begin{array}{r} 11.7 \\ 22 \end{array} \begin{array}{r} \text{F.L.} \\ 11.3 \\ 22 \end{array} \begin{array}{r} 13.1 \\ 25 \end{array} \begin{array}{r} 13.6 \\ 50 \end{array}$$

$$\begin{array}{r} 2.4 \\ 50 \end{array} \begin{array}{r} 0.9 \\ 30 \end{array} \begin{array}{r} 6.4 \\ 24 \end{array} \begin{array}{r} 7.5 \\ 20 \end{array} \begin{array}{r} 8.0 \\ 17 \end{array} \begin{array}{r} 5.7 \\ 11 \end{array} \begin{array}{r} 5.4 \\ 12 \end{array} \begin{array}{r} 5.7 \\ 12 \end{array} \begin{array}{r} 8.1 \\ 19 \end{array} \begin{array}{r} 9.6 \\ 24 \end{array} \begin{array}{r} 11.9 \\ 33 \end{array} \begin{array}{r} 12.6 \\ 50 \end{array}$$

Spike in P.P. 27' Lt Sta. 141 + 61

$$\begin{array}{r} 5.9 \\ 50 \end{array} \begin{array}{r} 4.8 \\ 23 \end{array} \begin{array}{r} 4.5 \\ 18 \end{array} \begin{array}{r} 3.2 \\ 12 \end{array} \begin{array}{r} 2.9 \\ 14 \end{array} \begin{array}{r} 3.8 \\ 15 \end{array} \begin{array}{r} 10.1 \\ 27 \end{array} \begin{array}{r} 11.6 \\ 50 \end{array}$$

$$\begin{array}{r} 10.2 \\ 50 \end{array} \begin{array}{r} 9.2 \\ 29 \end{array} \begin{array}{r} \text{F.L.} \\ 9.1 \\ 29 \end{array} \begin{array}{r} 7.8 \\ 21 \end{array} \begin{array}{r} 3.4 \\ 12 \end{array} \begin{array}{r} 3.1 \\ 15 \end{array} \begin{array}{r} 3.8 \\ 15 \end{array} \begin{array}{r} \text{F.L.} \\ 8.8 \\ 29 \end{array} \begin{array}{r} 11.2 \\ 29 \end{array} \begin{array}{r} 11.7 \\ 50 \end{array}$$

$$\begin{array}{r} 12.7 \\ 50 \end{array} \begin{array}{r} 8.5 \\ 20 \end{array} \begin{array}{r} 4.5 \\ 13 \end{array} \begin{array}{r} 3.6 \\ 12 \end{array} \begin{array}{r} 4.0 \\ 12 \end{array} \begin{array}{r} 4.5 \\ 16 \end{array} \begin{array}{r} 10.6 \\ 26 \end{array} \begin{array}{r} 11.7 \\ 50 \end{array}$$

Sta	+	π	-	Elev
		931.24		
143+50			4.9	26.3
144			5.5	25.7
T.P.	4.36	933.28	2.32	928.92
+50			7.6	25.7
145			6.7	26.6
+65			4.7	28.6
T.P.	12.76	945.83	0.21	933.07
146			16.2	29.6
+50			14.7	31.1
147			13.0	32.8
+41			11.8	34.0
148			10.2	35.6
T.P.	13.28	950.07	9.04	936.79
+50			13.2	36.9
149			12.2	37.9

$$\begin{array}{r} 12.9 \\ 50 \end{array} \quad \begin{array}{r} 8.8 \\ 21 \end{array} \quad \begin{array}{r} 5.8 \\ 16 \end{array} \quad \begin{array}{r} 5.3 \\ 11 \end{array} \quad 4.9 \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad 12.1 \quad \begin{array}{r} 11.9 \\ 24 \end{array} \quad \begin{array}{r} 12.1 \\ 50 \end{array}$$

$$\begin{array}{r} 11.8 \\ 50 \end{array} \quad \begin{array}{r} 9.4 \\ 19 \end{array} \quad \begin{array}{r} 5.9 \\ 11 \end{array} \quad 5.5 \quad \begin{array}{r} 6.5 \\ 12 \end{array} \quad \begin{array}{r} 9.8 \\ 18 \end{array} \quad \begin{array}{r} 10.0 \\ 25 \end{array} \quad \begin{array}{r} 12.3 \\ 50 \end{array}$$

Pc Cor.

$$\begin{array}{r} 13.3 \\ 50 \end{array} \quad \begin{array}{r} 13.3 \\ 23 \end{array} \quad \begin{array}{r} 12.0 \\ 20 \end{array} \quad \begin{array}{r} 8.1 \\ 13 \end{array} \quad 7.6 \quad \begin{array}{r} 8.4 \\ 15 \end{array} \quad \begin{array}{r} 12.1 \\ 20 \end{array} \quad \begin{array}{r} 13.4 \\ 22 \end{array} \quad \begin{array}{r} 13.4 \\ 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \end{array} \quad \begin{array}{r} 12.6 \\ 25 \end{array} \quad \begin{array}{r} 12.3 \\ 21 \end{array} \quad \begin{array}{r} 11.2 \\ 19 \end{array} \quad \begin{array}{r} 7.3 \\ 4 \end{array} \quad \begin{array}{r} 7.0 \\ 9 \end{array} \quad 6.7 \quad \begin{array}{r} 7.4 \\ 15 \end{array} \quad \begin{array}{r} 12.1 \\ 21 \end{array} \quad \begin{array}{r} 13.3 \\ 28 \end{array} \quad \begin{array}{r} 13.3 \\ 50 \end{array}$$

$$\begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 8.8 \\ 31 \end{array} \quad \begin{array}{r} 7.9 \\ 25 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 4.5 \\ 12 \end{array} \quad 4.7 \quad \begin{array}{r} 5.2 \\ 12 \end{array} \quad \begin{array}{r} 6.6 \\ 17 \end{array} \quad \begin{array}{r} 6.0 \\ 20 \end{array} \quad \begin{array}{r} 7.6 \\ 25 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array}$$

$$\begin{array}{r} 9.6 \\ 50 \end{array} \quad \begin{array}{r} 10.2 \\ 37 \end{array} \quad \begin{array}{r} 10.6 \\ 28 \end{array} \quad \begin{array}{r} 13.5 \\ 23 \end{array} \quad \begin{array}{r} 17.1 \\ 17 \end{array} \quad \begin{array}{r} 16.7 \\ 10 \end{array} \quad 16.2 \quad \begin{array}{r} 16.8 \\ 11 \end{array} \quad \begin{array}{r} 16.8 \\ 18 \end{array} \quad \begin{array}{r} 11.1 \\ 30 \end{array} \quad \begin{array}{r} 12.2 \\ 40 \end{array} \quad \begin{array}{r} 12.2 \\ 50 \end{array}$$

$$\begin{array}{r} 11.0 \\ 75 \end{array} \quad \begin{array}{r} 2.2 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array} \quad \begin{array}{r} 12.6 \\ 22 \end{array} \quad \begin{array}{r} 14.7 \\ 17 \end{array} \quad \begin{array}{r} 15.6 \\ 13 \end{array} \quad \begin{array}{r} 15.0 \\ 9 \end{array} \quad 14.7 \quad \begin{array}{r} 15.0 \\ 13 \end{array} \quad \begin{array}{r} 15.7 \\ 16 \end{array} \quad \begin{array}{r} 15.2 \\ 19 \end{array} \quad \begin{array}{r} 10.6 \\ 27 \end{array} \quad \begin{array}{r} 11.2 \\ 50 \end{array}$$

$$\begin{array}{r} +7.0 \\ 75 \end{array} \quad \begin{array}{r} +3.8 \\ 50 \end{array} \quad \begin{array}{r} +1.5 \\ 34 \end{array} \quad \begin{array}{r} 2.6 \\ 32 \end{array} \quad \begin{array}{r} 13.1 \\ 16 \end{array} \quad \begin{array}{r} 13.7 \\ 11 \end{array} \quad \begin{array}{r} 13.2 \\ 9 \end{array} \quad 13.0 \quad \begin{array}{r} 13.4 \\ 11 \end{array} \quad \begin{array}{r} 14.2 \\ 16 \end{array} \quad \begin{array}{r} 13.1 \\ 20 \end{array} \quad \begin{array}{r} 6.7 \\ 29 \end{array} \quad \begin{array}{r} 7.3 \\ 46 \end{array} \quad \begin{array}{r} 6.9 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 75 \end{array} \quad 4.0$$

$$\begin{array}{r} +3.5 \\ 75 \end{array} \quad \begin{array}{r} +2.5 \\ 50 \end{array} \quad \begin{array}{r} +0.8 \\ 35 \end{array} \quad \begin{array}{r} 12.1 \\ 15 \end{array} \quad \begin{array}{r} 12.0 \\ 10 \end{array} \quad 11.8 \quad \begin{array}{r} 12.4 \\ 13 \end{array} \quad \begin{array}{r} 13.0 \\ 15 \end{array} \quad \begin{array}{r} 12.3 \\ 16 \end{array} \quad \begin{array}{r} 2.2 \\ 20 \end{array} \quad \begin{array}{r} 2.4 \\ 34 \end{array} \quad \begin{array}{r} 1.0 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 75 \end{array} \quad 5.5$$

$$\begin{array}{r} +7.5 \\ 75 \end{array} \quad \begin{array}{r} +2.0 \\ 50 \end{array} \quad \begin{array}{r} 1.0 \\ 39 \end{array} \quad \begin{array}{r} 1.8 \\ 33 \end{array} \quad \begin{array}{r} 10.7 \\ 18 \end{array} \quad \begin{array}{r} 10.7 \\ 9 \end{array} \quad 10.2 \quad \begin{array}{r} 10.6 \\ 13 \end{array} \quad \begin{array}{r} 11.2 \\ 14 \end{array} \quad \begin{array}{r} 10.5 \\ 18 \end{array} \quad \begin{array}{r} +1.0 \\ 35 \end{array} \quad \begin{array}{r} +2.0 \\ 50 \end{array} \quad \begin{array}{r} +3.0 \\ 75 \end{array}$$

$$\begin{array}{r} 0.0 \\ 71 \end{array} \quad \begin{array}{r} 3.0 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 28 \end{array} \quad \begin{array}{r} 13.8 \\ 15 \end{array} \quad \begin{array}{r} 13.6 \\ 9 \end{array} \quad 13.2 \quad \begin{array}{r} 13.6 \\ 13 \end{array} \quad \begin{array}{r} 13.4 \\ 17 \end{array} \quad \begin{array}{r} 12.9 \\ 19 \end{array} \quad \begin{array}{r} 3.8 \\ 31 \end{array} \quad \begin{array}{r} 1.6 \\ 50 \end{array} \quad \begin{array}{r} 0.2 \\ 63 \end{array} \quad \begin{array}{r} +1.4 \\ 75 \end{array}$$

$$\begin{array}{r} 6.9 \\ 50 \end{array} \quad \begin{array}{r} 8.4 \\ 23 \end{array} \quad \begin{array}{r} 12.6 \\ 16 \end{array} \quad \begin{array}{r} 12.8 \\ 13 \end{array} \quad \begin{array}{r} 12.4 \\ 11 \end{array} \quad 12.2 \quad \begin{array}{r} 12.7 \\ 13 \end{array} \quad \begin{array}{r} 12.8 \\ 18 \end{array} \quad \begin{array}{r} 5.4 \\ 31 \end{array} \quad \begin{array}{r} 2.7 \\ 50 \end{array} \quad \begin{array}{r} 0.63 \\ 75 \end{array}$$

Sta	+	π	-	Elev
		950.07		
149+50			11.5	38.6
150			10.8	39.3
+50			10.4	39.7
151			10.4	39.7
+31			10.4	39.7
+75			10.4	39.7
T.P.	4.34	943.80	10.61	939.46 ok
152			4.3	39.5
+48			4.6	39.2
+78			5.3	38.5
153			5.7	38.1
T.P.	3.03	940.11	6.72	937.08
+50			3.0	37.1
154			3.9	36.2

$\frac{7.7}{50}$ $\frac{8.5}{35}$ $\frac{9.1}{23}$ $\frac{12.3}{18}$ $\frac{12.6}{15}$ $\frac{11.9}{13}$ $\frac{11.8}{11.5}$ $\frac{12.6}{12}$ $\frac{11.2}{14-16}$ $\frac{4.5}{22}$ $\frac{3.4}{31}$ $\frac{2.1}{36}$ $\frac{+1.0}{50}$ $\frac{75}{75}$

$\frac{8.8}{50}$ $\frac{8.7}{31}$ $\frac{8.0}{24}$ $\frac{12.0}{18}$ $\frac{12.0}{14}$ $\frac{11.4}{11}$ $\frac{11.3}{13}$ $\frac{11.0}{19}$ $\frac{2.5}{34}$ $\frac{1.1}{50}$ $\frac{+0.3}{75}$

$\frac{8.7}{50}$ $\frac{7.8}{35}$ $\frac{6.3}{25}$ $\frac{11.1}{18}$ $\frac{11.5}{14-15}$ $\frac{10.8}{11}$ $\frac{10.2}{10.4}$ $\frac{10.0}{12}$ $\frac{9.3}{21}$ $\frac{2.7}{31}$ $\frac{5.0}{50}$

$\frac{7.3}{50}$ $\frac{6.0}{38}$ $\frac{5.3}{26}$ $\frac{11.4}{17}$ $\frac{11.8}{16-14}$ $\frac{10.9}{12}$ $\frac{10.8}{10.4}$ $\frac{11.6}{12}$ $\frac{11.0}{14-16}$ $\frac{4.7}{18}$ $\frac{4.7}{31}$ $\frac{5.0}{50}$

$\frac{7.4}{50}$ $\frac{5.3}{25}$ $\frac{11.1}{18}$ $\frac{11.8}{12-14}$ $\frac{10.9}{11}$ $\frac{10.7}{10.4}$ $\frac{11.4}{12}$ $\frac{10.2}{14-15}$ $\frac{5.0}{19}$ $\frac{5.2}{28}$ $\frac{5.2}{50}$

$\frac{9.6}{50}$ $\frac{9.8}{34}$ $\frac{10.8}{26}$ $\frac{10.0}{18}$ $\frac{11.4}{15}$ $\frac{11.7}{14-13}$ $\frac{11.0}{11}$ $\frac{10.9}{10.4}$ $\frac{11.7}{12}$ $\frac{11.3}{15-17}$ $\frac{7.7}{18}$ $\frac{7.9}{24}$ $\frac{7.3}{32}$ $\frac{7.3}{50}$

$\frac{3.1}{50}$ $\frac{3.9}{36}$ $\frac{4.9}{28}$ $\frac{4.8}{18}$ $\frac{5.8}{13-16}$ $\frac{4.8}{10}$ $\frac{4.7}{4.3}$ $\frac{4.9}{12}$ $\frac{2.7}{16}$ $\frac{1.8}{21}$ $\frac{1.8}{50}$

$\frac{1.5}{50}$ $\frac{2.2}{37}$ $\frac{3.8}{23}$ $\frac{3.8}{17}$ $\frac{5.4}{15-13}$ $\frac{5.0}{11}$ $\frac{4.8}{4.6}$ $\frac{5.2}{11}$ $\frac{3.9}{13-15}$ $\frac{4.2}{19}$ $\frac{4.2}{31}$ $\frac{4.2}{50}$

$\frac{8.1}{50}$ $\frac{8.4}{32}$ $\frac{6.4}{20}$ $\frac{5.6}{12}$ $\frac{5.6}{5.3}$ $\frac{6.0}{11}$ $\frac{7.3}{20}$ $\frac{8.0}{25}$ $\frac{8.2}{35}$ $\frac{8.2}{50}$

$\frac{7.9}{50}$ $\frac{9.2}{36}$ $\frac{8.6}{25}$ $\frac{6.3}{19}$ $\frac{6.1}{11}$ $\frac{6.1}{5.7}$ $\frac{7.3}{12}$ $\frac{10.4}{19}$ $\frac{10.7}{26}$ $\frac{10.8}{40}$ $\frac{10.8}{50}$

Rock Lt Sta 153

$\frac{1.0}{50}$ $\frac{2.7}{39}$ $\frac{4.8}{27}$ $\frac{6.0}{24}$ $\frac{6.1}{21}$ $\frac{3.5}{12}$ $\frac{4.0}{3.0}$ $\frac{8.3}{16}$ $\frac{8.7}{26}$ $\frac{8.7}{50}$

$\frac{2.7}{50}$ $\frac{3.6}{44}$ $\frac{4.4}{30}$ $\frac{5.6}{22}$ $\frac{5.9}{20-17}$ $\frac{5.3}{14}$ $\frac{4.3}{12}$ $\frac{5.2}{3.9}$ $\frac{8.2}{16}$ $\frac{8.8}{25}$ $\frac{8.8}{50}$

Sta	+	⌊	-	Elev.
		940.11 ✓		
154 + 43			4.8	35.3 .
155			6.5	33.4 .
+50			8.4	31.7 .
156			10.3	29.8 .
T.P.	9.16	938.98 ✓	10.29	929.82 ✓
+50			10.8	28.2 .
157			12.6	26.4 .
+28			13.6	25.4 .
+50				(14.5) . 24.5
158				(16.3) . 22.7
+50				(18.1) . 20.9
159				(19.8) . 19.2
B.M.	0.86	928.02 ✓	11.78	927.20 ✓ (927.16)
159 + 50			8.5	24.5 .

$\frac{4.0}{50}$ $\frac{4.5}{35}$ $\frac{4.6}{18}$ $\frac{6.0}{16-14}$ $\frac{4.9}{11}$ $\frac{5.6}{4.8}$ $\frac{5.7}{13}$ $\frac{7.0}{18}$ $\frac{8.2}{21}$ $\frac{8.2}{50}$

$\frac{3.8}{50}$ $\frac{5.0}{20}$ $\frac{7.3}{16}$ $\frac{7.3}{12}$ $\frac{7.0}{11}$ $\frac{6.9}{6.5}$ $\frac{7.3}{11}$ $\frac{5.1}{15}$ $\frac{6.5}{20}$ $\frac{6.5}{50}$

$\frac{2.6}{50}$ $\frac{4.8}{22}$ $\frac{9.7}{15-12}$ $\frac{9.0}{11}$ $\frac{9.3}{8.4}$ $\frac{9.4}{13}$ $\frac{5.0}{18}$ $\frac{4.6}{25}$ $\frac{4.6}{50}$

$\frac{3.8}{50}$ $\frac{5.3}{31}$ $\frac{5.1}{27}$ $\frac{11.4}{17-14}$ $\frac{10.9}{12}$ $\frac{10.6}{10.3}$ $\frac{11.2}{11}$ $\frac{10.6}{16}$ $\frac{3.8}{19}$ $\frac{3.3}{28}$ $\frac{3.3}{50}$

$\frac{4.0}{50}$ $\frac{4.7}{26}$ $\frac{12.3}{15-13}$ $\frac{11.9}{12}$ $\frac{11.7}{10}$ $\frac{11.2}{10.8}$ $\frac{10.9}{11}$ $\frac{8.6}{15}$ $\frac{4.6}{23}$ $\frac{4.0}{26}$ $\frac{4.0}{50}$

$\frac{9.4}{50}$ $\frac{7.6}{33}$ $\frac{7.4}{25}$ $\frac{13.9}{17-14}$ $\frac{13.1}{12}$ $\frac{12.9}{9}$ $\frac{13.0}{12.6}$ $\frac{13.3}{11}$ $\frac{12.9}{12}$ $\frac{8.4}{16}$ $\frac{4.3}{24}$ $\frac{4.1}{28}$ $\frac{4.1}{50}$

$\frac{14.2}{50}$ $\frac{14.4}{21}$ $\frac{14.5}{17}$ $\frac{13.8}{10}$ $\frac{13.9}{13.6}$ $\frac{14.4}{11}$ $\frac{14.1}{12}$ $\frac{11.0}{17}$ $\frac{5.0}{24}$ $\frac{4.4}{31}$ $\frac{4.4}{50}$

14.5

$\frac{13.6}{21}$ $\frac{6.2}{31}$ $\frac{5.2}{50}$

16.3

$\frac{7.1}{31}$ $\frac{6.4}{50}$

18.1

$\frac{10.2}{28}$ $\frac{8.7}{50}$

19.8

$\frac{15.0}{24}$ $\frac{12.1}{50}$

Top Conc. Step Rail 66' Lt Sta 157+80

$\frac{3.2}{50}$ $\frac{3.2}{21}$ $\frac{4.9}{15-13}$ $\frac{3.6}{10}$ $\frac{4.0}{3.5}$ $\frac{4.4}{11}$ $\frac{4.4}{13}$

Sta	+	π	-	Elev.
		928.02		
158			5.3	22.7
+50			7.1	20.9
159			8.8	19.2
T.P.	2.11	920.74	9.39	918.63
+50			3.0	17.7
160			4.2	16.5
+50			4.7	16.0
161			5.0	15.7
+50			5.1	15.6
162			5.1	15.6
T.P.	4.10	920.23	4.61	916.13
+50			4.7	15.5
163			4.9	15.3
+70			4.7	15.5

$$\begin{array}{r} 4.2 \quad 4.6 \quad 4.8 \quad 6.0 \quad 5.6 \quad 5.8 \quad 6.3 \quad 5.5 \\ 50 \quad 37 \quad 17 \quad 15 \quad 13 \quad 11 \quad 5.3 \quad 12 \quad 14 \quad 16 \quad 18 \end{array}$$

$$\begin{array}{r} 8.6 \quad 7.4 \quad 6.8 \quad 7.4 \quad 8.0 \quad 7.6 \quad 7.6 \quad 8.0 \\ 50 \quad 41 \quad 26 \quad 14 \quad 9 \quad 8 \quad 7.1 \quad 12 \quad 16 \end{array}$$

$$\begin{array}{r} 16.4 \quad 15.0 \quad 9.7 \quad 7.4 \quad 9.5 \quad 9.6 \\ 50 \quad 28 \quad 14 \quad 8 \quad 8.8 \quad 10 \quad 15 \end{array}$$

$$\begin{array}{r} 10.2 \quad 9.3 \quad 3.7 \quad 3.5 \quad 5.6 \quad 6.0 \quad 6.2 \quad 1.1 \quad 1.2 \\ 50 \quad 26 \quad 11 \quad 3.0 \quad 11 \quad 17 \quad 21 \quad 25 \quad 41 \quad 50 \end{array}$$

$$\begin{array}{r} 11.8 \quad 9.9 \quad 5.5 \quad 5.0 \quad 4.8 \quad 5.7 \quad 8.3 \quad 7.4 \quad 6.4 \\ 50 \quad 28 \quad 19 \quad 12 \quad 4.2 \quad 12 \quad 24 \quad 29 \quad 42 \quad 50 \end{array}$$

$$\begin{array}{r} 12.1 \quad 10.1 \quad 7.4 \quad 6.4 \quad 5.3 \quad 5.3 \quad 6.1 \quad 6.4 \quad 9.1 \quad 8.9 \\ 50 \quad 32 \quad 28 \quad 22 \quad 9 \quad 4.7 \quad 11 \quad 19 \quad 29 \quad 36 \quad 50 \end{array}$$

$$\begin{array}{r} 12.5 \quad 10.8 \quad 7.5 \quad 6.8 \quad 5.8 \quad 5.6 \quad 7.1 \quad 10.0 \quad 9.6 \\ 50 \quad 32 \quad 27 \quad 21 \quad 11 \quad 5.0 \quad 12 \quad 28 \quad 34 \quad 50 \end{array}$$

$$\begin{array}{r} 11.6 \quad 10.9 \quad 6.4 \quad 5.5 \quad 5.8 \quad 6.9 \quad 10.5 \quad 10.7 \\ 50 \quad 32 \quad 22 \quad 12 \quad 5.1 \quad 12 \quad 25 \quad 31 \quad 50 \end{array}$$

$$\begin{array}{r} 12.1 \quad 11.6 \quad 7.4 \quad 6.3 \quad 5.9 \quad 6.9 \quad 10.4 \quad 11.6 \\ 50 \quad 32 \quad 24 \quad 19 \quad 5.1 \quad 13 \quad 22 \quad 30 \quad 50 \end{array}$$

Spike in R.P. 25' L₁ 162 + 20

$$\begin{array}{r} 11.0 \quad 10.3 \quad 6.7 \quad 5.5 \quad 5.4 \quad 5.3 \quad 5.7 \quad 10.4 \quad 11.0 \quad 11.4 \\ 50 \quad 29 \quad 22 \quad 19 \quad 11 \quad 4.7 \quad 12 \quad 19 \quad 28 \quad 36 \quad 50 \end{array}$$

$$\begin{array}{r} 10.4 \quad 9.8 \quad 6.3 \quad 5.7 \quad 5.4 \quad 5.4 \quad 5.9 \quad 10.2 \quad 11.1 \quad 11.4 \\ 50 \quad 32 \quad 24 \quad 20 \quad 10 \quad 4.9 \quad 12 \quad 19 \quad 28 \quad 35 \quad 50 \end{array}$$

$$\begin{array}{r} \text{F.L.} \quad \text{F.L.} \\ 8.3 \quad 8.5 \quad 8.4 \quad (8.7) \quad 5.4 \quad 5.4 \quad (7.9) \quad 10.0 \quad 10.5 \quad 10.9 \\ 50 \quad 30 \quad 21 \quad (21) \quad 14 \quad 4.7 \quad 12 \quad (20) \quad 20 \quad 34 \quad 50 \end{array}$$

Sta + π - Elev.

920.23

164 4.6 15.6

+40 4.6 15.6

165 4.7 15.5

+50 4.9 15.3

166 5.2 15.0

T.P. 4.59 919.32 5.50 914.73

+50 4.8 14.5

167 5.4 13.9

+50 6.2 13.1

168 7.0 12.3

+50 7.6 11.7

169 8.2 11.1

+50 8.9 10.4

$$\begin{array}{r} 7.5 \\ 50 \end{array} \quad \begin{array}{r} 8.00 \\ 17 \end{array} \quad \begin{array}{r} 5.4 \\ 4 \end{array} \quad \begin{array}{r} 5.3 \\ 4 \end{array} \quad \begin{array}{r} 9.1 \\ 24 \end{array} \quad \begin{array}{r} 9.9 \\ 31 \end{array} \quad \begin{array}{r} 10.3 \\ 50 \end{array}$$

$$\begin{array}{r} 2.8 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 33 \end{array} \quad \begin{array}{r} 6.9 \\ 15 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 5.4 \\ 12 \end{array} \quad \begin{array}{r} 8.6 \\ 21 \end{array} \quad \begin{array}{r} 9.7 \\ 50 \end{array}$$

$$\begin{array}{r} 10.5 \\ 50 \end{array} \quad \begin{array}{r} 0.8 \\ 35 \end{array} \quad \begin{array}{r} 2.9 \\ 21 \end{array} \quad \begin{array}{r} 6.1 \\ 16 \end{array} \quad \begin{array}{r} 5.9 \\ 13 \end{array} \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 4.7 \\ 4 \end{array} \quad \begin{array}{r} 5.2 \\ 12 \end{array} \quad \begin{array}{r} 6.7 \\ 17-19 \end{array} \quad \begin{array}{r} 6.4 \\ 20 \end{array} \quad \begin{array}{r} 7.3 \\ 25 \end{array} \quad \begin{array}{r} 8.1 \\ 50 \end{array}$$

$$\begin{array}{r} 0.0 \\ 50 \end{array} \quad \begin{array}{r} 1.4 \\ 23 \end{array} \quad \begin{array}{r} 6.2 \\ 14-16 \end{array} \quad \begin{array}{r} 5.4 \\ 4 \end{array} \quad \begin{array}{r} 5.5 \\ 12 \end{array} \quad \begin{array}{r} 6.3 \\ 15-17 \end{array} \quad \begin{array}{r} 3.1 \\ 23 \end{array} \quad \begin{array}{r} 3.9 \\ 50 \end{array}$$

$$\begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} 2.7 \\ 24 \end{array} \quad \begin{array}{r} 7.3 \\ 18-16 \end{array} \quad \begin{array}{r} 5.8 \\ 11 \end{array} \quad \begin{array}{r} 5.2 \\ 5 \end{array} \quad \begin{array}{r} 5.7 \\ 12 \end{array} \quad \begin{array}{r} 6.7 \\ 14-17 \end{array} \quad \begin{array}{r} 3.1 \\ 23 \end{array} \quad \begin{array}{r} 2.9 \\ 50 \end{array}$$

$$\begin{array}{r} 4.1 \\ 50 \end{array} \quad \begin{array}{r} 4.2 \\ 23 \end{array} \quad \begin{array}{r} 6.8 \\ 18-15 \end{array} \quad \begin{array}{r} 5.3 \\ 11 \end{array} \quad \begin{array}{r} 4.8 \\ 4 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 13-15 \end{array} \quad \begin{array}{r} 4.0 \\ 19 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array}$$

$$\begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 6.2 \\ 19 \end{array} \quad \begin{array}{r} 7.1 \\ 17-14 \end{array} \quad \begin{array}{r} 6.4 \\ 13 \end{array} \quad \begin{array}{r} 5.4 \\ 5 \end{array} \quad \begin{array}{r} 6.0 \\ 12 \end{array} \quad \begin{array}{r} 6.8 \\ 14-16 \end{array} \quad \begin{array}{r} 5.8 \\ 31 \end{array} \quad \begin{array}{r} 4.6 \\ 50 \end{array}$$

$$\begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 24 \end{array} \quad \begin{array}{r} 7.8 \\ 17 \end{array} \quad \begin{array}{r} 7.0 \\ 12 \end{array} \quad \begin{array}{r} 6.6 \\ 9 \end{array} \quad \begin{array}{r} 6.2 \\ 6 \end{array} \quad \begin{array}{r} 7.5 \\ 11 \end{array} \quad \begin{array}{r} 6.7 \\ 14-17 \end{array} \quad \begin{array}{r} 6.2 \\ 21 \end{array} \quad \begin{array}{r} 6.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 22 \end{array} \quad \begin{array}{r} 8.4 \\ 16-14 \end{array} \quad \begin{array}{r} 7.6 \\ 12 \end{array} \quad \begin{array}{r} 7.0 \\ 7 \end{array} \quad \begin{array}{r} 7.7 \\ 12 \end{array} \quad \begin{array}{r} 9.1 \\ 17-17 \end{array} \quad \begin{array}{r} 7.7 \\ 22 \end{array} \quad \begin{array}{r} 8.6 \\ 36 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.1 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 23 \end{array} \quad \begin{array}{r} 9.1 \\ 15-13 \end{array} \quad \begin{array}{r} 8.1 \\ 11 \end{array} \quad \begin{array}{r} 7.6 \\ 7 \end{array} \quad \begin{array}{r} 8.5 \\ 12 \end{array} \quad \begin{array}{r} 9.5 \\ 14-16 \end{array} \quad \begin{array}{r} 6.7 \\ 24 \end{array} \quad \begin{array}{r} 8.0 \\ 37 \end{array} \quad \begin{array}{r} 10.1 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 25 \end{array} \quad \begin{array}{r} 9.9 \\ 17-15 \end{array} \quad \begin{array}{r} 9.1 \\ 12 \end{array} \quad \begin{array}{r} 8.2 \\ 8 \end{array} \quad \begin{array}{r} 8.9 \\ 11 \end{array} \quad \begin{array}{r} 9.9 \\ 14-16 \end{array} \quad \begin{array}{r} 6.2 \\ 25 \end{array} \quad \begin{array}{r} 8.4 \\ 50 \end{array}$$

$$\begin{array}{r} 6.6 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 26 \end{array} \quad \begin{array}{r} 11.0 \\ 18-16 \end{array} \quad \begin{array}{r} 9.5 \\ 12 \end{array} \quad \begin{array}{r} 8.9 \\ 8 \end{array} \quad \begin{array}{r} 9.7 \\ 11 \end{array} \quad \begin{array}{r} 11.2 \\ 14-17 \end{array} \quad \begin{array}{r} 7.7 \\ 25 \end{array} \quad \begin{array}{r} 9.7 \\ 50 \end{array}$$

Sta	+	π	-	Elev.
-----	---	-------	---	-------

919.32

170			9.5	09.8.
-----	--	--	-----	-------

+ 65			10.6	08.7.
------	--	--	------	-------

+ 71			10.6	08.7.
------	--	--	------	-------

+ 76			10.6	08.7.
------	--	--	------	-------

+ 87.7

B. M.

10.7	$\pm$	Rice Creek Rd
------	-------	---------------

7.25		912.07.
------	--	---------

08.6
~~08.8~~

912.07

$\frac{6.0}{50}$	$\frac{6.3}{26}$	$\frac{11.1}{18-16}$	$\frac{10.3}{12}$	9.5	$\frac{10.2}{13}$	$\frac{11.1}{14-16}$	$\frac{8.2}{23}$	$\frac{11.1}{50}$
------------------	------------------	----------------------	-------------------	-----	-------------------	----------------------	------------------	-------------------

$\frac{7.6}{50}$	$\frac{7.6}{31}$	$\frac{11.2}{24}$	$\frac{12.2}{20-22}$	$\frac{10.9}{18}$	$\frac{10.7}{12}$	10.6	$\frac{11.3}{18}$	$\frac{9.5}{22}$	$\frac{11.0}{39}$	$\frac{11.4}{50}$
------------------	------------------	-------------------	----------------------	-------------------	-------------------	------	-------------------	------------------	-------------------	-------------------

		F.L.						F.L.		
$\frac{11.4}{50}$	$\frac{12.3}{25}$	$\frac{11.3}{25}$	$\frac{10.6}{24}$	$\frac{10.8}{16}$	10.5	$\frac{10.8}{12}$	$\frac{11.6}{26}$	$\frac{13.0}{27}$	$\frac{12.7}{27}$	$\frac{13.3}{50}$

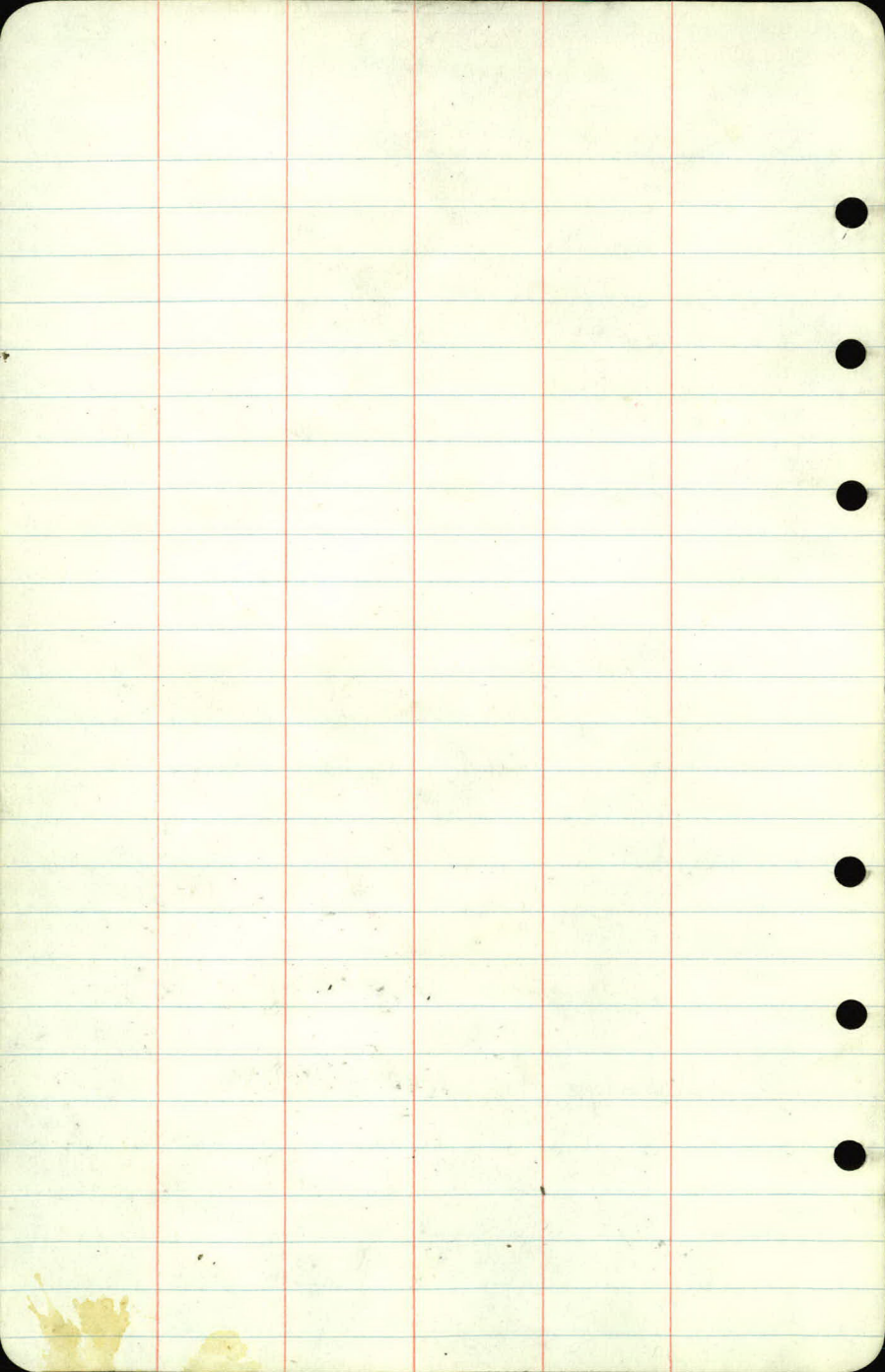
$\frac{10.4}{50}$	$\frac{10.8}{27}$	$\frac{10.7}{14}$	10.6	$\frac{10.9}{16}$	$\frac{11.8}{28}$	$\frac{11.5}{50}$
-------------------	-------------------	-------------------	------	-------------------	-------------------	-------------------

 $\frac{10.1}{50}$

10.7

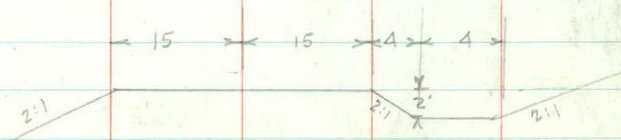
 $\frac{11.0}{50}$

Spike in P.P. N.W. Cor. Rice Creek Rd.



SILVER LAKE ROAD

Slope Stakes



Sta.	T	K	-	Elev.	
B.M.	13.38	972.63		959.25	
0 +23				72.4	0.2
+50				71.6	1.0
1				69.5	3.1
+50				67.3	5.3
2				66.1	6.5
+50				65.6	7.0
3				66.1	6.5
+10				66.2	6.4 *
+66				67.2	5.4
T.P.	3.84	970 ⁵ / ₉	5.98	966.65	
4 +75				67.7	2.8
5				65.9	4.6
T.P.	2.46	962.66	10.29	960.20	
+50				62.4	0.3

Top Angle Iron Base E. Pier of Tower

$$\begin{array}{r} 20 \\ 100.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 0.9 \\ F.07 \end{array}$$

$$\begin{array}{r} 0.8 \\ 100.4 \\ \hline 25.8 \end{array}$$

2.

$$\begin{array}{r} 4.3 \\ F3.3 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 2.8 \\ F1.8 \end{array}$$

$$\begin{array}{r} 2.3 \\ 100.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 6.0 \\ F2.9 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 4.9 \\ F1.8 \end{array}$$

$$\begin{array}{r} 7.2 \\ F4.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 8.6 \\ F3.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ F0.6 \end{array}$$

$$\begin{array}{r} 7.3 \\ F2.0 \\ \hline 19 \end{array}$$

$$\begin{array}{r} 13.1 \\ F6.6 \\ \hline 28.2 \end{array}$$

$$\begin{array}{r} 6.6 \\ F0.1 \end{array}$$

$$\begin{array}{r} 12.6 \\ F5.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 16.6 \\ F9.6 \\ \hline 34.2 \end{array}$$

$$\begin{array}{r} 7.2 \\ F0.2 \end{array}$$

$$\begin{array}{r} 10.5 \\ F3.5 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 20.4 \\ F13.9 \\ \hline 42.8 \end{array}$$

$$\begin{array}{r} 7.2 \\ F0.7 \end{array}$$

$$\begin{array}{r} 8.2 \\ F1.7 \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 26.0 \\ F20.6 \\ \hline 56.2 \end{array}$$

$$\begin{array}{r} 5.5 \\ F0.0 \end{array}$$

$$\begin{array}{r} 23.6 \\ F18.2 \\ \hline 51.4 \end{array}$$

$$\begin{array}{r} 25.4 \\ F23.6 \\ \hline 60.2 \end{array}$$

$$\begin{array}{r} 2.7 \\ F0.0 \end{array}$$

$$\begin{array}{r} 23.3 \\ F20.5 \\ \hline 56.0 \end{array}$$

$$\begin{array}{r} 26.1 \\ F21.5 \\ \hline 58.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ C0.1 \end{array}$$

$$\begin{array}{r} 23.8 \\ F19.2 \\ \hline 53.4 \end{array}$$

$$\begin{array}{r} 18.8 \\ F18.5 \\ \hline 52.0 \end{array}$$

$$\begin{array}{r} 0.1 \\ F.01 \end{array}$$

$$\begin{array}{r} 15.1 \\ F14.8 \\ \hline 44.6 \end{array}$$

Sta.	+	π	-	Elev.	
		962.66			
6				58.9	3.8
	+50			55.8	6.9
7				53.7	9.0
T.P.	460	957.38	9.88	952.78	
	+34			527	4.7
	+84			52.0	5.4
8				52.0	5.6
	+22			52.0	5.4
	+50			52.1	5.3
9				52.1	5.3
	+60			52.2	5.2
	+75			52.2	5.2
10				52.2	5.2

$$\begin{array}{r} 580 \text{ GR24} \\ \hline 15.1 \\ F127 \\ \hline 404 \end{array}$$

$$\begin{array}{r} 19.1 \\ \hline F15.3 \\ \hline 45.6 \end{array}$$

$$\begin{array}{r} 3.9 \\ \hline F0.1 \end{array}$$

$$\begin{array}{r} 7.0 \\ \hline F3.2 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 22.8 \\ \hline F15.9 \\ \hline 46.8 \end{array}$$

$$\begin{array}{r} 620 \text{ GR. 7.7} \\ \hline 7.1 \\ \hline F0.2 \end{array}$$

$$\begin{array}{r} 22.1 \\ \hline F15.2 \\ \hline 45.4 \end{array}$$

$$\begin{array}{r} 18.8 \\ \hline F11.1 \\ \hline 37.2 \end{array}$$

$$\begin{array}{r} 22.6 \\ \hline F13.6 \\ \hline 43.2 \end{array}$$

$$\begin{array}{r} 9.1 \\ \hline F0.1 \end{array}$$

$$\begin{array}{r} 24.5 \\ \hline F15.5 \\ \hline 46.0 \end{array}$$

$$\begin{array}{r} 17.4 \\ \hline F12.7 \\ \hline 40.4 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline C0.3 \end{array}$$

$$\begin{array}{r} 18.3 \\ \hline F13.6 \\ \hline 42.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ \hline DC1.2 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 4.8 \\ \hline C0.6 \end{array}$$

$$\begin{array}{r} 17.8 \\ \hline F12.4 \\ \hline 39.8 \end{array}$$

$$\begin{array}{r} 7.1 \\ \hline DC0.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ \hline C0.6 \end{array}$$

$$\begin{array}{r} 15.8 \\ \hline F10.4 \\ \hline 35.8 \end{array}$$

$$\begin{array}{r} 6.3 \\ \hline DC1.1 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ \hline C0.5 \end{array}$$

$$\begin{array}{r} 11.0 \\ \hline F5.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 6.8 \\ \hline DC0.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline C0.3 \end{array}$$

$$\begin{array}{r} 8.8 \\ \hline F3.5 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 6.8 \\ \hline DC0.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline C0.1 \end{array}$$

$$\begin{array}{r} 7.4 \\ \hline DC0.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 6.7 \\ \hline DC0.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline F0.1 \end{array}$$

$$\begin{array}{r} 7.7 \\ \hline F2.5 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 6.5 \\ \hline DC0.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline F0.1 \end{array}$$

$$\begin{array}{r} 4.6 \\ \hline 00.6 \\ \hline 28.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ \hline DC1.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline F0.0 \end{array}$$

$$\begin{array}{r} 4.3 \\ \hline C0.9 \\ \hline 28.8 \end{array}$$

Sta.	+	π	-	Elev.	
		957.38			
10+50				52.3	5.1
T.P.	5.98	958.40	4.96	952.42	
11				52.3	6.1
+50				52.4	6.0
12				52.4	6.0
+50				52.3	6.1
+76				52.2	6.2
13+07				52.0	6.4
B.M.			5.47	952.93	952.91
+28				51.8	
+34				51.7	
B.M.	2.41	955.32		952.91	
+50				51.5	
14				50.7	
+50				49.8	

Gr Rod

Lt

R

Rt

$$\begin{array}{r} 51 \\ 60.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 49 \\ 60.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ 60.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 47 \\ 61.4 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 5.2 \\ 60.9 \\ \hline \end{array}$$

$$\begin{array}{r} 39 \\ 62.2 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 36 \\ 62.4 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ 61.0 \\ \hline \end{array}$$

$$\begin{array}{r} 17 \\ 64.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 3.9 \\ 62.1 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ 60.7 \\ \hline \end{array}$$

$$\begin{array}{r} 1.2 \\ 64.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 2.6 \\ 63.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ 60.7 \\ \hline \end{array}$$

$$\begin{array}{r} 2.7 \\ 63.6 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 1.3 \\ 64.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ 60.5 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ 62.6 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 3.1 \\ 63.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 6.0 \\ 60.4 \\ \hline \end{array}$$

Spike PP 14' RL 13+35-

3.8

$$31.4' / \frac{1.6}{42.2}$$

$$\frac{38}{00}$$

$$\frac{2.5}{+1.3} / 29.6'$$

4.6

$$33.0' / \frac{1.3}{42.1}$$

$$\frac{48}{-0.2}$$

$$\frac{47}{12.9} / 26.8'$$

5.5

$$31.6' / \frac{3.2}{42.3}$$

$$\frac{59}{-0.4}$$

$$\frac{47}{12.08} / 24.6'$$

Sta.		π	-	Elev.
		955.32		
15				48.9
	+50			48.0
T.P.	3.37	949.69	9.00	946.32
16				47.1
	+50			46.2
17				45.3
	+50			44.4
18				43.5
	+50			42.7
19				42.1
T.P.	2.92	945.11	7.40	942.19
	+50			41.6
1	+71			41.4
20				41.3

11-15-40
K.H.
L.C.
A.M.
L.G.

Gr. Rod.

Lt

R

Rt.

6.4

$$27.2' / \frac{6.3}{10.1}$$

$$\frac{7.1}{-0.7}$$

$$\frac{8.2}{R.02} / 23.4'$$

7.3

$$27.4' / \frac{7.1}{10.2}$$

$$\frac{8.2}{-0.9}$$

$$\frac{9.0}{R.03} / 23.6'$$

2.6

$$26.8' / \frac{2.7}{R.19}$$

$$\frac{3.4}{-0.8}$$

$$\frac{2.7}{R.00} / 23.0'$$

3.5

$$26.8' / \frac{3.6}{R.19}$$

$$\frac{4.1}{-0.6}$$

$$\frac{5.2}{R.03} / 23.6'$$

4.4

$$28.0' / \frac{3.9}{10.5}$$

$$\frac{4.9}{-0.5}$$

$$\frac{5.8}{R.06} / 24.2'$$

5.3

$$28.4' / \frac{4.6}{10.7}$$

$$\frac{5.5}{-0.2}$$

$$\frac{6.4}{R.09} / 24.5'$$

6.2

$$26.8' / \frac{6.3}{R.19}$$

$$\frac{6.2}{0.0}$$

$$\frac{5.9}{10.3} / 27.6'$$

7.0

$$27.0' / \frac{7.0}{10.0}$$

$$\frac{6.8}{10.2}$$

$$\frac{6.8}{10.2} / 27.4'$$

7.6

$$27.2' / \frac{7.5}{10.1}$$

$$\frac{7.4}{10.2}$$

$$\frac{8.1}{R.14} / 25.0' \text{ } \& \text{ } 1.5 / 26.0$$

Nail in T.P. R. 194

3.5

$$28.4' / \frac{2.8}{10.7}$$

$$\frac{3.3}{10.2}$$

$$\frac{4.8}{R.01} / 24.4'$$

3.7

3.8

$$30.6' / \frac{2.0}{11.8}$$

$$\frac{3.6}{10.2}$$

$$\frac{5.4}{R.04} / 23.8'$$

Sta.	+	π	-	Elev.
		945.11		
20 +50				41.1
21				40.9
+50				40.7
22				40.5
+50				40.3
23				40.1
+50				40.0
24				40.0
24 +50				40.3
25				40.7
+50				41.2
T.P.	11.76	952.50	4.37	940.74
+90				41.6

Gr. Rod.	Lt	R	Rt
4.0	$31.2 / \frac{19}{72.1}$	$\frac{39}{70.1}$	$\frac{56}{20.4} / 23.8'$
4.2	$30.0 / \frac{21}{71.5}$	$\frac{41}{70.1}$	$\frac{61}{20.1} / 23.2'$
4.4	$29.2 / \frac{23}{71.1}$	$\frac{43}{70.1}$	$\frac{59}{20.5} / 24.0'$
4.6	$29.0 / \frac{26}{71.0}$	$\frac{48}{70.2}$	$\frac{61}{20.5} / 24.0'$
4.8	$27.0 / \frac{25}{70.0}$	$\frac{51}{70.3}$	$\frac{68}{20.0} / 23.0'$
5.0	$26.4 / \frac{23}{70.17}$	$\frac{55}{70.5}$	$\frac{73}{20.0} / 20.6'$
5.1	$23.4 / \frac{29}{70.2}$	$\frac{59}{70.6}$	$\frac{85}{3.4} / 21.8'$
5.1	$20.6 / \frac{29}{72.8}$	$\frac{57}{70.7}$	$\frac{25}{44} / 23.8'$
4.8	$20.0 / \frac{25}{72.5}$	$\frac{56}{70.8}$	$\frac{83}{35} / 22.0'$
4.4	$19.4 / \frac{26}{72.2}$	$\frac{53}{70.9}$	$\frac{84}{4.8} / 23.0'$
3.9	$21.0 / \frac{29}{73.0}$	$\frac{46}{70.7}$	$\frac{75}{36} / 22.2'$
10.9	$22.2 / \frac{23}{70.6}$	$\frac{11.1}{70.2}$	$\frac{13.9}{30} / 21.0'$

Sta.	+	π	-	Elev.	
		952.50			
26				41.7	
+16				41.9	
+30				42.0	
+45				42.1	
+68				42.4	
B.M.	8.19	952.60	8.19	944.32 944.41	7.44
27				42.7	
B.M.			8.72	945.88	
+50				43.1	
28				43.4	41.4
+50				43.6	11.3 41.3
29				43.6	11.3 41.3
+29				43.5	11.3 41.3
+61				43.4	11.4 41.2

Spec. Dist. Lk. only

4-16-40

Gr Rod Lt R Lt

$$10.4 \quad 26.2' / \frac{108}{21.6} \quad \frac{104}{00} \quad \frac{98}{+106/202'}$$

$$10.1 \quad 26.6' / \frac{103}{21.8} \quad \frac{102}{-0.1} \quad \frac{72}{+229/32.8'}$$

Spike 14" Oak 24' Lt 26 + 79

$$9.9 \quad 29.6' / \frac{86}{11.3} \quad \frac{98}{+0.1} \quad \frac{80}{+359/388'}$$

Spike 14" Oak 24' Lt 26 + 79

$$9.5 \quad 27.2' / \frac{84}{10.1} \quad \frac{95}{+0.2} \quad \frac{31}{+64/39.8'}$$

$$9.2 \quad 28.4' / \frac{85}{10.7} \quad \frac{91}{+0.1} \quad \frac{20}{+5.2/33.4'}$$

$$9.0 \quad 25.6 \quad 30.4' / \frac{79}{10.34} \quad \frac{89}{+0.1} \quad \frac{47}{+43/35.6'}$$

$$9.0 \quad 25.6 \quad 35.0' / \frac{59}{12.54} \quad \frac{86}{+0.4} \quad \frac{41}{+109/36.8'}$$

$$9.1 \quad 25.4 \quad 33.0' / \frac{61}{12.52} \quad \frac{86}{+0.5} \quad \frac{47}{+74.4/35.8'}$$

$$9.2 \quad 25.4 \quad 26.6' / \frac{98}{21.6} \quad \frac{88}{+0.4} \quad \frac{88}{+104/20}$$

Sta.	+	π	-	Elev.	
		952.60			
30				43.2	41.2
T.P.	1.69	946.28	8.01	944.59	
+29				43.0	
+65				42.6	
31				42.2	
+50				41.5	
B.M.					(944.07)
32				40.7	
B.M.	3.66	943.45	6.46	939.82	(939.79)
+50				39.8	
			11.0	932.5	
33				39.1	
+37				38.9	
+50				39.0	
34				39.1	
+50				39.7	
T.P.	14.41	955.08	2.78	940.67	
35				40.6	

11-10-40

G.C. Rod. Lt. E Rt.

9.3 $230' / \frac{113}{R90}$ $\frac{92}{101}$ $\frac{25}{R15} / 26.0'$

Nail in T.P. Rt 30 ft

3.3 $196' / \frac{56}{-2.3}$ $\frac{34}{-01}$ $\frac{10}{+2.3} / 36.0'$

3.7 $202' / \frac{63}{-2.6}$ $\frac{39}{-0.2}$ $\frac{39}{R18} / 26.6'$

4.1 $246' / \frac{58}{R03}$ $\frac{44}{-0.3}$ $\frac{43}{R18} / 26.6'$

4.8 $244' / \frac{61}{R07}$ $\frac{49}{-01}$ $\frac{40}{108} / 28.6'$

Spk in 24" O. Rt. sta 32+00

5.6 $270' / \frac{111}{-5.5}$ $\frac{57}{-01}$

Spk in R.P. 26' Rt. 32+61

3.7 $336' / \frac{12.0}{-8.3}$ $\frac{38}{-01}$ $\frac{54}{R03} / 23.6'$

Elev Silver Lake

12.43
1.21
11.22

4.4 $306' / \frac{152}{-10.9}$ $\frac{48}{-0.4}$ $\frac{62}{R02} / 23.4'$

4.6

4.5 $392' / \frac{156}{-11.1}$ $\frac{50}{-05}$ $\frac{63}{R02} / 23.4'$

4.4 $336' / \frac{12.7}{-8.6}$ $\frac{46}{-0.2}$ $\frac{63}{R03} / 23.6'$

3.8 $216' / \frac{71}{-3.3}$ $\frac{38}{00}$ $\frac{58}{R00} / 22.1'$

14.5 $308' / \frac{126}{-1.9}$ $\frac{146}{-0.1}$ $\frac{16.0}{R05} / 24.0'$

Sta.	+	π	-	Elev.	
		935.08			
35 + 43				41.1	
36				41.6	
+50				41.6	
37				41.2	
+50				40.5	
TP	1.49	943.71	12.86	942.22	
38				39.5	
+50				38.6	
39				37.5	
+60				36.7	
40				36.3	
B.M.	4.08	939.88	7.91	935.80	935.86
+50				36.0	
41				35.9	

Gr Rod Lt. R Rt

14.0 $41.8' / \frac{46}{174}$ $\frac{134}{106}$ $\frac{141}{119} / 26.8'$

13.5 $43.8' / \frac{51}{184}$ $\frac{12.2}{113}$ $\frac{102}{128} / 32.6'$

13.5 $43.6' / \frac{52}{183}$ $\frac{11.9}{116}$ $\frac{96}{139} / 38.0'$

13.9 $42.6' / \frac{41}{178}$ $\frac{12.4}{115}$ $\frac{103}{131} / 33.0'$

14.6 $40.6' / \frac{28}{168}$ $\frac{136}{110}$ $\frac{134}{122} / 31.4'$

Nail in T.P. at 374

4.2 $31.8' / \frac{18}{124}$ $\frac{38}{104}$ $\frac{38}{104} / 27.8'$

5.3 $24.0' / \frac{68}{105}$ $\frac{52}{101}$ $\frac{54}{119} / 26.8'$

6.2 $\frac{62}{00}$ $\frac{76}{106} / 24.2'$

7.0 $20.8' / \frac{99}{129}$ $\frac{76}{106}$ $\frac{101}{131} / 21.2'$

7.4 $26.0' / \frac{124}{150}$ $\frac{83}{109}$ $\frac{101}{127} / 20.4'$

Spike P.P. 27' RL 40 + 35

3.9 $27.2' / \frac{25}{156}$ $\frac{51}{111}$ $\frac{66}{127} / 20.4'$

4.0 $26.0' / \frac{80}{150}$ $\frac{53}{113}$ $\frac{60}{120} / 19.0'$

Sta.		π	-	Elev.
		939.88		
41+50				35.9
42				35.9
+50				35.9
43				35.9
+50				36.0
44				36.1
+50				36.4
45				36.8
+50				37.3
46				37.9
+ 25				
T.P.	14.51	954.39	000	939.88
+25				38.5
+50				
+75				38.9
47				39.2

Gr. Rod	Lt	E	Rt
4.0	$27.0' / \begin{smallmatrix} 95 \\ -5.5 \end{smallmatrix}$	$\frac{5.5}{-1.5}$	$\frac{70}{-3.0} / 21.0'$
4.0	$26.9' / \begin{smallmatrix} 90 \\ -5.0 \end{smallmatrix}$	$\frac{56}{-1.6}$	$\frac{68}{-28} / 20.6'$
4.0	$24.4' / \begin{smallmatrix} 82 \\ -4.2 \end{smallmatrix}$	$\frac{55}{-1.5}$	$\frac{60}{R.90} / 25.0'$
4.0	$25.0' / \begin{smallmatrix} 85 \\ -4.5 \end{smallmatrix}$	$\frac{51}{-1.1}$	$\frac{60}{R.00} / 25.0'$
3.9	$24.4' / \begin{smallmatrix} 81 \\ -4.2 \end{smallmatrix}$	$\frac{40}{-1.0}$	$\frac{59}{R.00} / 26.6'$
3.8	$24.4' / \begin{smallmatrix} 80 \\ -4.2 \end{smallmatrix}$	$\frac{46}{-0.8}$	$\frac{58}{-20} / 19.0'$
3.5	$24.4' / \begin{smallmatrix} 77 \\ -4.2 \end{smallmatrix}$	$\frac{43}{-0.8}$	$\frac{59}{-2.4} / 19.8'$
3.1	$25.6' / \begin{smallmatrix} 7.9 \\ -4.8 \end{smallmatrix}$	$\frac{40}{-0.9}$	$\frac{6.2}{-3.1} / 21.2'$
2.6	$27.8' / \begin{smallmatrix} 85 \\ -5.9 \end{smallmatrix}$	$\frac{33}{-0.7}$	$\frac{55}{-2.9} / 20.8'$
2.0	$25.2' / \begin{smallmatrix} 6.6 \\ -4.6 \end{smallmatrix}$	$\frac{20}{0.0}$	$\frac{4.3}{-2.3} / 19.6'$
16.3 No. 1 F.R. Rd. 4.5 ft	$21.4' / \begin{smallmatrix} 18.3 \\ R.00 \end{smallmatrix}$	$\frac{160}{103}$	$\frac{181}{R.02} / 23.4'$
15.9	$26.0' / \begin{smallmatrix} 14.3 \\ R.16 \end{smallmatrix}$	$\frac{155}{10.4}$	$\frac{98}{16.8} / 39.2'$
15.5	$39.4' / \begin{smallmatrix} 9.3 \\ -4.2 \end{smallmatrix}$	$\frac{15.1}{10.4}$	$\frac{43}{44.2} / 55.4'$
15.2	$48.0' / \begin{smallmatrix} 4.7 \\ -10.5 \end{smallmatrix}$	$\frac{14.7}{10.5}$	$\frac{95}{44.7} / 56.4'$

510.	+	π	-	Elev.
+25		954.39		39.5
47+50				39.8
T.P.	8.32	951.72	10.99	943.40
+84				40.2
48				40.5
+50				41.3
49				42.6
+50				44.4
50				46.6
+50				49.2
51				52.3
T.P.	8.68	958.42	1.98	949.74
+50				55.6
+95				58.4
52+20				58.8
B.M.			2.66	955.76

(955.77)

Gr Rod

Lt

E

Pt

14.9

$$43.2' / \frac{6.5}{18.1}$$

$$\frac{14.3}{+0.6}$$

$$\frac{52}{117} / 50.4'$$

14.6

$$39.4' / \frac{8.4}{14.2}$$

$$\frac{14.0}{+0.6}$$

$$\frac{100}{146} / 36.2'$$

11.5

$$29.8' / \frac{10.1}{11.4}$$

$$\frac{10.9}{+0.6}$$

$$\frac{116}{129} / 26.8'$$

11.2

$$24.0' / \frac{12.7}{12.95}$$

$$\frac{108}{+0.4}$$

$$\frac{122}{151.0} / 25.0'$$

10.4

$$21.8' / \frac{13.8}{-3.4}$$

$$\frac{104}{0.0}$$

$$\frac{125}{-21} / 19.2'$$

9.1

$$46.0' / \frac{14.1}{-5.0}$$

$$\frac{96}{-0.5}$$

$$\frac{125}{-34} / 22.8'$$

7.3

$$29.6' / \frac{14.1}{-6.8}$$

$$\frac{85}{-1.2}$$

$$\frac{128}{-55} / 27.0'$$

5.1

$$33.0' / \frac{14.0}{-8.9}$$

$$\frac{0.7}{-1.6}$$

$$\frac{12.3}{-72} / 30.4'$$

2.5

$$33.0' / \frac{13.2}{-10.8}$$

$$\frac{4.5}{-2.0}$$

$$\frac{10.5}{-8.0} / 32.0'$$

+0.6

$$33.0' / \frac{12.7}{-13.3}$$

$$\frac{0.0}{-2.6}$$

$$\frac{8.2}{-8.8} / 33.0'$$

2.8

$$33.0' / \frac{17.1}{-14.3}$$

$$\frac{0.0}{-3.2}$$

$$\frac{11.7}{-8.9} / 33.0'$$

0.0

$$33.0' / \frac{12.3}{-12.3}$$

$$\frac{2.7}{-2.7}$$

$$\frac{5.9}{-5.9} / 27.8'$$

Spike Fe. Cor. 32' Rt. 52+03

Sta	+	π	-	Grade
B.M.	15.35	971.12		(955.77)
52	+63			59.5
53				62.2
T.P.	13.03	980.20	395	967.17
	+36			63.9
	+65			65.8
54				68.1
T.P.	12.86	987.29	577	974.43
	+33			70.2
	+87			73.1
55	+16			74.7
	+36			75.3
	+73			76.6
56				77.3

$$\begin{array}{r} 12.46 \\ 2.87 \\ \hline 15.33 \end{array}$$

$$\begin{array}{r} 35 \\ 60 \\ \hline 210 \\ 210 \\ \hline 420 \end{array}$$

Cor. Rod Lt. R Pt.

Spt. in Fg. Cor. 32 Pt. Sta. 52+03

$$\begin{array}{r} 11.6 \quad 26.8' / \frac{11.7}{15.19} \quad \frac{95}{+21} \quad \frac{102}{+1.2} / 27.4 \end{array}$$

$$\begin{array}{r} 8.9 \quad 31.8' / \frac{6.5}{12.4} \quad \frac{69}{+20} \quad \frac{63}{+26} / 32.2' \end{array}$$

$$\begin{array}{r} 14.3 \quad 39.0' / \frac{10.3}{16.0} \quad \frac{136}{+2.7} \quad \frac{8.3}{+8.0} / 43.0' \end{array}$$

$$\begin{array}{r} 14.4 \quad 45.8' / \frac{15.9}{18.4} \quad \frac{119}{+2.5} \quad \frac{7.5}{+6.9} / 40.8' \end{array}$$

$$\begin{array}{r} 12.1 \quad 49.2' / \frac{10}{11.0} \quad \frac{98}{+2.3} \quad \frac{34}{+8.7} / 44.4' \end{array}$$

$$\begin{array}{r} 17.1 \quad 44.6' / \frac{1.3}{1.8} \quad \frac{15.9}{+2.1} \quad \frac{6.5}{+0.6} / 48.2' \end{array}$$

$$\begin{array}{r} 14.2 \quad 53.0' / \frac{1.2}{11.0} \quad \frac{12.3}{+1.9} \quad \frac{34}{+0.8} / 48.6' \end{array}$$

$$\begin{array}{r} 12.6 \quad 52.0' / \frac{21}{12.5} \end{array}$$

$$\begin{array}{r} 12.0 \quad 37.4' / \frac{4.8}{15.2} \quad \frac{99}{+2.1} \quad \frac{21}{+1.8} / 50.8' \end{array}$$

$$\begin{array}{r} 10.7 \quad \quad \frac{88}{+1.9} \quad \frac{26}{+0.1} / 47.2' \end{array}$$

$$\begin{array}{r} 10.0 \quad 21.8' / \frac{13.4}{1.4} \quad \frac{86}{+1.4} \quad \frac{38}{+6.2} / 39.4' \end{array}$$

Sta	+	Σ	-	Grade
		987.29		
56	+50			71.4
57				70.9
	+36			79.2
	+65			79.3
58				79.5
T.P.	6.81	985.92	8.18	79.11
	+40			79.8
59				80.1
	+50			80.4
60				80.7
T.P.	9.45	991.01	4.36	81.56
	+35			81.0
61				81.3

Gr. Rod

Lt.

R.

Rt.

8.9

$$23.0' / \frac{13.9}{-4.0}$$

$$\frac{86}{+0.3}$$

$$\frac{81}{+0.9} / 28.6'$$

8.4

$$25.2' / \frac{13.5}{-5.1}$$

$$\frac{86}{-0.2}$$

$$\frac{12.2}{-3.8} / 22.6'$$

8.1

$$25.8' / \frac{12.5}{-5.4}$$

$$\frac{86}{-0.5}$$

$$\frac{13.2}{-5.1} / 25.2'$$

8.0

$$25.6' / \frac{13.3}{-5.3}$$

$$\frac{8.8}{-0.4}$$

$$\frac{12.8}{-4.8} / 24.6'$$

7.8

$$24.2' / \frac{12.4}{-4.6}$$

$$\frac{8.0}{-0.2}$$

$$\frac{11.3}{-3.5} / 22.0'$$

6.1

$$23.0' / \frac{10.1}{-4.0}$$

$$\frac{6.1}{0.0}$$

$$\frac{1.3}{+4.8} / 36.6'$$

5.8

$$28.0' / \frac{5.3}{+0.5}$$

$$\frac{5.3}{+0.5}$$

$$\frac{1.6}{+4.2} / 35.4'$$

5.5

$$36.6' / \frac{0.7}{+4.8}$$

$$\frac{4.9}{+0.6}$$

$$\frac{4.6}{+0.9} / 28.8'$$

5.2

$$36.0' / \frac{0.7}{+4.5}$$

$$\frac{4.4}{+0.5}$$

$$\frac{1.9}{+3.3} / 33.0'$$

10.0

$$29.2' / \frac{8.9}{+1.1}$$

$$\frac{9.3}{+0.7}$$

$$\frac{5.9}{+4.1} / 33.0'$$

9.7

$$28.0' / \frac{11.1}{+0.5}$$

$$\frac{9.4}{+0.3}$$

$$\frac{5.1}{+4.6} / 33.0'$$

Sta	+	π	-	Grade
		991.01		
61	+43			80.6
62				79.3
	+55			77.3
T.P.	1.03	978.40	13.64	977.37
	+88			75.9
63	+13			74.9
	+50			73.3
64				71.2
T.P.				
	+33			69.9
T.P.	1.73	969.90	10.23	968.17
	+60			68.7
65				67.1
	+43			65.3

Gr. Rod

Lt

R

Rt.

10.4

$$278' / \frac{100}{10.4}$$

$$\frac{97}{-0.7}$$

$$\frac{48}{+56} / 33.0'$$

11.7

$$390' / \frac{57}{12.0}$$

$$\frac{112}{+0.3}$$

$$\frac{86}{+31} / 33.0'$$

13.7

$$49.8' / \frac{2.3}{+11.4}$$

$$\frac{13.6}{+0.1}$$

$$\frac{97}{+40} / 33.0'$$

2.5

$$55.6' / \frac{2.3}{+14.3}$$

$$\frac{2.3}{0.0}$$

$$\frac{2.0}{+0.5} / 28.0'$$

3.5

$$55.2' / \frac{2.3}{+14.1}$$

$$\frac{3.8}{-0.3}$$

$$\frac{7.7}{-4.2} / 23.4'$$

5.1

$$48.0' / \frac{2.3}{+10.5}$$

$$\frac{5.6}{-0.5}$$

$$\frac{8.3}{-3.4} / 21.8'$$

7.2

$$47.0' / \frac{2.3}{+10.0}$$

$$\frac{8.0}{-0.8}$$

$$\frac{10.2}{-3.0} / 24.0'$$

8.5

$$35.6' / \frac{4.2}{-4.3}$$

$$\frac{9.5}{-1.0}$$

$$\frac{12.5}{-4.0} / 23.0'$$

1.2

$$23.0' / \frac{3.2}{+10.0}$$

$$\frac{2.3}{-1.1}$$

$$\frac{11.7}{-15.5} / 38.0'$$

2.8

$$22.2' / \frac{4.4}{-3.6}$$

$$\frac{4.0}{-1.2}$$

$$\frac{12.6}{-9.8} / 36.6'$$

4.6

$$25.0' / \frac{9.6}{-5.0}$$

$$\frac{5.6}{-1.0}$$

$$\frac{15.4}{-10.8} / 38.6'$$

Sta.	+	π	-	Grade	
		969.90			
65	+67			64.3	
B.M.	6.25	970.00	6.25	963.65	963.75
66	+00			63.0	
	+25			62.3	
	+44			61.7	
	+58			61.4	
T.P.	3.64	963.62	10.02	959.98	
67				60.6	
	+31			60.1	
	+66			59.4	
68				59.2	
	+48			59.1	
69				59.4	
	+36			59.8	

Gr. Rod

Lt

Rt

Rt

5.6

$$21.6' / \frac{89}{-3.3}$$

$$\frac{63}{-0.7}$$

$$\frac{14.3}{-8.7} / 34.4'$$

Spt. in 15" O. 70' Rt. 65+93

7.0

$$28.0' / \frac{6.5}{-10.5}$$

$$\frac{7.3}{-0.3}$$

$$\frac{8.4}{-6.6} / 24.2'$$

7.7

$$31.0' / \frac{3.7}{-2.0}$$

$$\frac{8.1}{-0.4}$$

$$\frac{3.9}{-4.8} / 36.6'$$

8.3

$$42.0' / \frac{0.8}{-7.5}$$

$$\frac{7.3}{-0.3}$$

$$\frac{8.4}{-6.6} / 24.2'$$

8.6

$$44.2' / \frac{0.0}{-1.6}$$

$$\frac{9.1}{-0.5}$$

$$\frac{3.1}{-5.5} / 38.0'$$

3.0

$$23.0' / \frac{5.0}{-2.0}$$

$$\frac{4.0}{-1.0}$$

$$\frac{7.1}{-4.1} / 24.2'$$

3.5

$$26.6' / \frac{8.8}{-5.3}$$

$$\frac{4.7}{-7.2}$$

$$\frac{14.5}{-11.0} / 39.0'$$

4.2

$$26.6' / \frac{9.5}{-5.3}$$

$$\frac{5.1}{-0.9}$$

$$\frac{18.0}{-13.8} / 44.6'$$

4.4

$$23.0' / \frac{7.9}{-2.5}$$

$$\frac{5.0}{-0.6}$$

$$\frac{12.1}{-7.7} / 32.4'$$

4.5

$$33.4' / \frac{1.3}{-13.2}$$

$$\frac{4.8}{-0.3}$$

$$\frac{6.5}{-10.0} / 23.0'$$

4.2

$$43.0' / \frac{13.8}{-8.0}$$

$$\frac{4.4}{-0.2}$$

$$\frac{3.2}{-1.0} / 29.0'$$

3.8

$$41.8' / \frac{13.6}{-7.7}$$

$$\frac{4.0}{-0.2}$$

$$\frac{3.9}{-11.9} / 26.8'$$

Sta	+	π	-	Grade
		963.62		
69	+78			60.7
70				61.1
T.P.	1.22	964.10	0.74	962.88
	+40			62.2
	+71			63.2
71				64.3
	+35			65.8
T.P.	12.13	975.01	1.22	962.88
	+470			67.5
72				69.0
T.P.	9.44	983.31	1.14	983.81
	+50			71.8
73				74.8
T.P.	8.96	989.96	2.31	981.00
	+50			77.8

Gr. Rod

Lt

\$

Rt

2.9

$$23.8' / \frac{43}{12.3}$$

$$\frac{35}{-0.6}$$

$$\frac{10.0}{-71.9} / 31.2$$

2.5

$$20.2' / \frac{51}{-2.6}$$

$$\frac{31}{-0.6}$$

$$\frac{11.1}{-8.8} / 34.2'$$

Top G.R. Post Rt

1.9

$$26.2' / \frac{20}{-5.1}$$

$$\frac{28}{-0.9}$$

$$\frac{13.5}{-11.6} / 40.2'$$

0.9

$$34.8' / \frac{19.8}{-8.9}$$

$$\frac{1.9}{-1.0}$$

$$\frac{12.8}{-11.7} / 40.8'$$

+0.2

$$34.6' / \frac{8.6}{-8.8}$$

$$\frac{0.9}{-1.1}$$

$$\frac{11.4}{-11.6} / 40.2'$$

+1.7

$$34.2' / \frac{34.2}{-7.1}$$

$$\frac{6.5}{-8.2} / 33.4'$$

7.5

$$24.6' / \frac{8.7}{-8.8}$$

$$\frac{7.9}{-0.4}$$

$$\frac{9.5}{-20.1} / 21.2'$$

6.0

$$33.4' / \frac{3.8}{-13.2}$$

$$\frac{6.0}{0.0}$$

$$\frac{3.0}{-1.0} / 29.0'$$

Top F.G. Post Rt 5/2 72+0.4

11.5

$$36.2' / \frac{6.8}{-4.6}$$

$$\frac{11.2}{+0.3}$$

$$\frac{6.3}{-15.2} / 37.4'$$

8.5

$$39.0' / \frac{3.5}{-10.0}$$

$$\frac{8.0}{+0.5}$$

$$\frac{2.9}{-15.6} / 38.2'$$

R. L

$$35.4' / \frac{8.0}{-4.2}$$

$$\frac{11.9}{+0.5}$$

$$\frac{5.1}{-17.1} / 41.2'$$

Ditch Gr
Lt

Sta	+	π	-	Grade		
		989.96				
74				80.3		
	+50			82.2		
					Gr. Red	Gr
75				83.6	7.9	82.1
	+58			84.4	7.9	82.1
76				84.5	8.0	82.0
	+50			84.3	8.0	82.0
77				83.9	8.1	81.9
	+50			83.6		
78				83.2		
T.P.	4.73	988.03	6.66	982.30		
	+50			82.9		
79				82.5		

Gr. Bod

Lt.

E

Rt.

7.7

$$42.6' / \frac{1.9}{+7.8}$$

$$\frac{9.0}{+9.7}$$

$$\frac{2.5}{+7.2} / 41.4'$$

7.8

$$36.4' / \frac{3.1}{+4.7}$$

$$\frac{6.8}{+1.0}$$

$$\frac{2.3}{+5.5} / 38.0'$$

6.4

52.0

$$35.0' / \frac{1.4}{+12.65}$$

$$\frac{5.4}{+1.0}$$

$$\frac{2.5}{+3.9} / 34.8'$$

5.6

59.6

$$36.8' / \frac{1.3}{+12.66}$$

$$\frac{5.0}{+0.6}$$

$$\frac{3.6}{+2.0} / 31.0'$$

5.8

24.0

$$32.6' / \frac{3.7}{+12.43}$$

$$\frac{5.3}{+0.2}$$

$$\frac{5.0}{+0.5} / 28.0'$$

5.7

29.6

$$28.0' / \frac{5.8}{+12.2}$$

$$\frac{5.7}{0.0}$$

$$\frac{6.9}{+0.8} / 24.6'$$

6.1

$$24.0' / \frac{7.6}{+12.05}$$

$$\frac{6.3}{-0.2}$$

$$\frac{7.2}{+0.9} / 24.8'$$

6.4

$$22.0' / \frac{8.4}{+12.00}$$

$$\frac{7.0}{-0.6}$$

$$\frac{6.6}{+1.8} / 26.6'$$

6.8

$$23.0' / \frac{8.8}{+12.00}$$

$$\frac{7.9}{-1.1}$$

$$\frac{6.9}{+1.9} / 26.8'$$

5.1

$$20.0' / \frac{7.6}{-2.5}$$

$$\frac{7.0}{-1.9}$$

$$\frac{7.1}{+1.0} / 23.0'$$

5.5

$$22.4' / \frac{9.2}{-3.7}$$

$$\frac{7.5}{-2.0}$$

$$\frac{8.5}{+3.0} / 21.0'$$

Sfo.	+	π	-	Grade	
		988.03			
79	+50			82.2	
80				82.0	
	+50			82.0	
81				82.4	
	+50			83.0	
82				83.8	
	+48			84.5	
R.M.	7.72	993.59	2.14	985.89	985.87
83				85.3	
	+50			86.0	
84				86.8	
	+50			87.5	

Gr. Rod.

Lt

4

Rt.

5.8

$$22.8 / \frac{9.1}{-3.9}$$

$$\frac{7.3}{-1.5}$$

$$\frac{8.9}{-3.1} / 21.2'$$

6.0

$$21.2 / \frac{9.1}{-3.1}$$

$$\frac{7.2}{-1.2}$$

$$\frac{8.6}{-2.6} / 20.2'$$

6.0

$$19.0 / \frac{8.0}{-2.0}$$

$$\frac{6.6}{-0.6}$$

$$\frac{8.0}{-2.0} / 19.0'$$

5.6

$$25.0 / \frac{6.6}{-1.0}$$

$$\frac{6.1}{-0.5}$$

$$\frac{7.6}{-0.0} / 23.0'$$

5.0

$$23.0 / \frac{7.0}{-10.0}$$

$$\frac{5.6}{-0.6}$$

$$\frac{6.8}{-0.0} / 23.4'$$

4.2

$$20.0 / \frac{6.7}{-2.5}$$

$$\frac{5.2}{-1.0}$$

$$\frac{3.7}{-0.5} / 28.0'$$

3.5

$$25.0 / \frac{4.5}{-10.0}$$

$$\frac{4.6}{-1.1}$$

$$\frac{3.2}{-0.3} / 27.6'$$

Spl. 1 in PR 25 Lt 82125

8.3

$$25.4 / \frac{9.1}{-8.1.2}$$

$$\frac{9.4}{-1.1}$$

$$\frac{8.0}{-0.3} / 27.6'$$

7.4

$$25.4 / \frac{8.4}{-8.1.2}$$

$$\frac{8.6}{-1.0}$$

$$\frac{7.3}{-0.3} / 27.6'$$

6.8

$$19.4 / \frac{9.0}{-2.2}$$

$$\frac{8.1}{-1.3}$$

$$\frac{4.5}{-2.3} / 31.6'$$

6.1

$$25.8 / \frac{11.0}{-4.9}$$

$$\frac{7.7}{-1.6}$$

$$\frac{6.1}{-0.0} / 27.0'$$

Sta	+	π	-	Grade
		993.59		
85				88.3
	+50			89.0
86				89.8
	+50			90.5
87				91.2
T.P.	6.21	997.40	2.40	991.19
	+60			91.9
88				92.2
	+50			92.5
89				92.7
T.P.	5.26	998.01	4.65	992.75
	+50			93.0
90				93.2

Gr. Rod

Lt.

R.

Rt.

5.3

$$246' / \frac{196}{-4.3}$$

$$\frac{72}{-1.9}$$

$$\frac{85}{-3.2} / 22.8'$$

4.6

$$242' / \frac{87}{-4.1}$$

$$\frac{6.5}{-1.9}$$

$$\frac{98}{-5.0} / 26.4'$$

3.8

$$249' / \frac{75}{-4.0}$$

$$\frac{5.3}{-1.5}$$

$$\frac{92}{-5.5} / 27.0'$$

3.1

$$254' / \frac{39}{-4.2}$$

$$\frac{3.8}{-0.7}$$

$$\frac{5.3}{-2.2} / 19.4'$$

2.4

$$288' / \frac{1.5}{+0.9}$$

$$\frac{2.4}{0.0}$$

$$\frac{2.6}{-2.18} / 26.6'$$

5.5

$$284' / \frac{4.8}{+0.1}$$

$$\frac{5.3}{+0.2}$$

$$\frac{4.3}{+1.2} / 29.4'$$

5.2

$$30.4' / \frac{35}{+1.7}$$

$$\frac{5.0}{+0.2}$$

$$\frac{4.5}{+0.7} / 28.4'$$

4.9

$$27.6' / \frac{4.6}{+0.3}$$

$$\frac{4.9}{+0.0}$$

$$\frac{5.1}{-1.2} / 25.4'$$

4.7

$$27.8' / \frac{4.5}{+0.2}$$

$$\frac{4.7}{0.0}$$

$$\frac{4.3}{+0.4} / 27.8'$$

R 519.89 + 100

5.0

$$30.2' / \frac{3.4}{+1.6}$$

$$\frac{5.1}{-0.1}$$

$$\frac{5.3}{-1.5} / 26.0'$$

4.8

$$26.0' / \frac{5.3}{-1.5}$$

$$\frac{4.0}{-0.1}$$

$$\frac{4.3}{-2.0.5} / 24.0'$$

Sta.	+	π	-	Grade
		998.01		
90	+50			93.5
T.P.	11.05	1004.50	4.56	993.46
91				93.7
	+11			93.8
	+65			93.4
92				92.7
	+21			92.2
	+40			91.5
	+60			90.7
	+89			89.3
T.P.	2.76	993.53	13.73	990.77
93	+25			87.4
	+60			85.4
T.P.	0.32	982.09	10.76	982.77

Gr. Rod

LH

R

Rt.

4.5

$$29.4 / \frac{3.3}{41.2}$$

$$\frac{4.8}{-0.3}$$

$$\frac{4.3}{220/22.6'}$$

4 sta. 91

10.8

$$\frac{5.1}{55.7}$$

$$38.4$$

$$\frac{11.0}{FD.2}$$

$$\frac{12.1}{DCD.2}$$

$$23.4$$

10.7

$$\frac{4.1}{66.6}$$

$$40.2$$

$$\frac{11.0}{FD.3}$$

$$\frac{13.0}{F2.3}$$

$$19.6$$

11.1

$$\frac{10.7}{60.4}$$

$$27.8$$

$$\frac{11.4}{FD.3}$$

$$\frac{13.2}{F2.1}$$

$$19.2$$

11.8

$$\frac{6.3}{55.5}$$

$$38.0$$

$$\frac{11.9}{FD.1}$$

X

12.3

$$\frac{4.8}{71.5}$$

$$42.0$$

$$\frac{12.4}{FD.1}$$

X

13.0

$$\frac{5.2}{77.8}$$

$$42.6$$

$$\frac{13.0}{FD.0}$$

X

13.8

$$\frac{6.9}{66.9}$$

$$40.8$$

$$\frac{13.7}{CD.1}$$

X

15.2

$$\frac{8.1}{66.8}$$

$$40.6$$

$$\frac{15.1}{CD.1}$$

X

6.1

$$\frac{3.7}{61.4}$$

$$31.8$$

$$\frac{6.1}{FD.0}$$

$$\frac{7.3}{DCD.8}$$

$$24.6$$

8.1

$$\frac{9.8}{DC1.1}$$

$$25.2$$

$$\frac{8.3}{FD.2}$$

$$\frac{6.1}{CD.1}$$

$$30.4$$

Sta	+	x	-	Grade
-----	---	---	---	-------

983.09

94				83.2
----	--	--	--	------

+32				81.6
-----	--	--	--	------

+65				79.8
-----	--	--	--	------

95				78.6
----	--	--	--	------

+50				77.0
-----	--	--	--	------

96				75.7
----	--	--	--	------

T.P.	369	979.07	7.71	975.38
------	-----	--------	------	--------

+33				75.2
-----	--	--	--	------

+65				74.8
-----	--	--	--	------

97				74.6
----	--	--	--	------

+54				74.4
-----	--	--	--	------

98				74.3
----	--	--	--	------

Gr. Rod

LH

R

RH

+0.1

$$\begin{array}{r} 6.4 \\ F6.3 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 0.3 \\ F0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 2.3 \\ F2.1 \\ \hline 19.8 \end{array}$$

1.5

$$\begin{array}{r} 8.0 \\ F6.5 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 2.1 \\ F0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ F4.0 \\ \hline 23.0 \end{array}$$

3.3

$$\begin{array}{r} 7.8 \\ F4.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 3.6 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.3 \\ F5.2 \\ \hline 25.4 \end{array}$$

4.5

$$\begin{array}{r} 8.3 \\ F3.8 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 5.0 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 9.5 \\ F5.0 \\ \hline 25.0 \end{array}$$

6.1

$$\begin{array}{r} 11.1 \\ F5.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 6.4 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 11.2 \\ F5.1 \\ \hline 25.2 \end{array}$$

7.4

$$\begin{array}{r} 11.7 \\ F4.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 7.6 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 10.4 \\ F3.0 \\ \hline 21.0 \end{array}$$

3.9

$$\begin{array}{r} 8.9 \\ F5.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ F2.3 \\ \hline 19.6 \end{array}$$

4.3

$$\begin{array}{r} 8.5 \\ F4.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 4.4 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ F1.5 \\ \hline 22.0 \end{array}$$

4.5

$$\begin{array}{r} 7.4 \\ F2.9 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ F0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 4.2 \\ C0.3 \\ \hline 27.6 \end{array}$$

4.7

$$\begin{array}{r} 8.4 \\ F3.7 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 4.6 \\ C0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.3 \\ C0.5 \\ \hline 28.0 \end{array}$$

4.8

$$\begin{array}{r} 2.9 \\ C1.9 \\ \hline 30.8 \end{array}$$

$$\begin{array}{r} 4.8 \\ C0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C1.9 \\ \hline 30.8 \end{array}$$

Sta	+	π	-	Grade
		979.67		
98	+28			74.2
	+84			74.1
99				74.0
T.P.	6.93	978.89	7.11	971.96
	+22			73.9
	+62			73.8
100				73.7
	+50			73.4
101				72.6
	+50			71.4
102				69.7
	+69			67.1
103				66.0
	0.92	966.18	13.63	965.26

Gr. Rod

L_t

R

R_f

4.9

$$\begin{array}{r} 2.8 \\ C2.1 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.4 \\ C0.5 \\ \hline 28.0 \end{array}$$

5.0

$$\begin{array}{r} 7.8 \\ F2.8 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 7.8 \\ F2.8 \\ \hline 20.2 \end{array}$$

5.1

$$\begin{array}{r} 7.1 \\ R.T. F2.0 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.7 \\ F2.6 \\ \hline 20.2 \end{array}$$

Top R.T. 64 99

5.0

$$\begin{array}{r} 4.7 \\ C0.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 2.0 \\ C0.0 \\ \hline 23.2 \end{array}$$

5.1

$$\begin{array}{r} 4.6 \\ C0.5 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 3.2 \\ C1.9 \\ \hline 30.8 \end{array}$$

5.2

$$\begin{array}{r} 4.3 \\ C0.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 4.9 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 1.4 \\ C3.8 \\ \hline 34.6 \end{array}$$

5.5

$$\begin{array}{r} 3.3 \\ C2.2 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 5.2 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 0.9 \\ C4.6 \\ \hline 33.2 \end{array}$$

6.3

$$\begin{array}{r} 3.7 \\ C2.6 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 5.8 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 2.8 \\ C3.5 \\ \hline 33.2 \end{array}$$

7.5

$$\begin{array}{r} 4.6 \\ C2.9 \\ \hline 32.5 \end{array}$$

$$\begin{array}{r} 7.0 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ C2.3 \\ \hline 31.2 \end{array}$$

9.2

$$\begin{array}{r} 4.0 \\ C5.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ C0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ C3.0 \\ \hline 33.0 \end{array}$$

11.9

$$\begin{array}{r} 6.1 \\ C5.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.3 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ C4.8 \\ \hline 33.0 \end{array}$$

12.9

$$\begin{array}{r} 10.3 \\ C2.6 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 12.8 \\ C8.1 \\ \hline \end{array}$$

$$\begin{array}{r} 10.3 \\ C2.6 \\ \hline 32.2 \end{array}$$

966.18²

103+54

64.0

104

62.2

+50

60.4

+92

58.8

T.P.

2.92

959.52

9.58

956.60

105+37

57.1

B.M.

957.92

+60

56.2

106'

54.8

+63

52.4

107

51.0

T.P.

2.68

952.82

9.38

950.14

+65

48.6

108

47.3

+25

46.3

2.2

$$\frac{4.2}{8.75 \times 100} = \frac{2.9}{23.0}$$

$$\frac{2.9}{F0.7}$$

$$\frac{7.6}{F5.4} = \frac{2.6}{25.8}$$

4.0

$$\frac{6.0}{8.75 \times 100} = \frac{5.0}{23.0}$$

$$\frac{5.0}{F1.0}$$

$$\frac{9.3}{65.3} = \frac{2.6}{25.6}$$

W. 1.0

5.2
5.8
8.80.6
0.6

$$\frac{10.0}{F3.6} = \frac{2.2}{23.2}$$

$$\frac{7.1}{F1.3}$$

$$\frac{12.0}{F6.8} = \frac{2.8}{28.5}$$

W. 1.7

6.6
7.4
8.5

" 0.8

$$\frac{14.5}{F6.9} = \frac{2.8}{28.7}$$

$$\frac{8.6}{F1.2}$$

$$\frac{15.6}{F9.9} = \frac{3.2}{32.0}$$

F. C. R.

W. 3.0

1.2
2.41.5
1.2

$$\frac{6.6}{D5.3} = \frac{2.8}{28.6}$$

$$\frac{3.1}{F0.7}$$

$$\frac{8.2}{F1.0} = \frac{2.9}{29.0}$$

Spike 12 Oak 24 Lt. 105 + 62 (Out)

W. 3.0

3.9
2.1
3.3
4.81.5
1.2

$$\frac{3.9}{C0.9} = \frac{3.1}{31.8}$$

$$\frac{3.7}{F0.4}$$

$$\frac{5.5}{F3.4} = \frac{2.1}{21.8}$$

W. 1.7

3.9
4.7
5.8

" 0.8

$$\frac{2.2}{C3.2} = \frac{3.3}{33.0}$$

$$\frac{5.1}{F0.4}$$

$$\frac{4.9}{DC1.0} = \frac{2.5}{25.0}$$

W. 1.0

6.5
7.1
7.70.6
0.6

$$\frac{3.2}{C4.5} = \frac{3.3}{33.0}$$

$$\frac{7.5}{F0.4}$$

$$\frac{5.2}{C1.3} = \frac{2.9}{29.0}$$

$$\frac{6.9}{C1.0} = \frac{2.9}{29.0}$$

$$\frac{9.1}{F0.6}$$

$$\frac{8.2}{C0.9} = \frac{9.1}{8.5} = \frac{7.9}{7.9}$$

W. 1.0

$$\frac{8.6}{F5.2} = \frac{2.5}{25.0}$$

$$\frac{4.8}{F0.6}$$

$$\frac{7.1}{DC0.2} = \frac{5.3}{4.2} = \frac{3.4}{3.4}$$

W. 1.7

$$\frac{8.5}{F4.1} = \frac{2.3}{23.0}$$

$$\frac{6.0}{F0.5}$$

$$\frac{7.3}{DC1.7} = \frac{7.0}{5.5} = \frac{1.5}{4.8} = \frac{1.2}{1.2}$$

W. 3.0

$$\frac{7.3}{DC0.0} = \frac{2.3}{23.0}$$

$$\frac{6.7}{F0.2}$$

$$\frac{6.8}{C6.2} = \frac{8.0}{6.5} = \frac{1.5}{8.3} = \frac{1.2}{1.2}$$

W. 3.0

952.82

108 +50

45.4

+75

44.5

109

43.6

+74

41.3

T.P.

1.65

943.51

1096

941.86

110 +14

40.2

+26

39.9

+84

38.5

111 +36

37.5

112

36.4

+71

35.2

113

34.7

+50

33.9

T.P.

1.14

934.81

9.84

933.67

$$\begin{array}{r} 22 \\ 121.0 \\ \hline 250 \end{array} \quad \begin{array}{r} 75 \\ FO.1 \end{array} \quad \begin{array}{r} 5.5 \\ C3.4 \\ \hline 330 \end{array} \quad \begin{array}{r} 89 \\ 74 \\ \hline 6.2 \end{array} \quad \begin{array}{r} 1.5 \\ 1.2 \end{array} \quad W. 3.0$$

$$\begin{array}{r} 64 \\ 10.7 \\ \hline 280 \end{array} \quad \begin{array}{r} 82 \\ CO.1 \end{array} \quad \begin{array}{r} 5.2 \\ C4.6 \\ \hline 330 \end{array} \quad \begin{array}{r} 78 \\ 8.3 \\ \hline 7.1 \end{array} \quad \begin{array}{r} 1.5 \\ 1.2 \end{array} \quad W. 3.0$$

$$\begin{array}{r} 68 \\ 11.6 \\ \hline 30.2 \end{array} \quad \begin{array}{r} 92 \\ CO.0 \end{array} \quad \begin{array}{r} 6.2 \\ C4.1 \\ \hline 36.9 \end{array} \quad \begin{array}{r} 103 \\ 9.2 \\ \hline 8.4 \end{array} \quad \begin{array}{r} 1.1 \\ 0.8 \end{array} \quad W. 7.7$$

$$\begin{array}{r} 108 \\ CO.2 \\ \hline 27.8 \end{array} \quad \begin{array}{r} 114 \\ CO.1 \end{array} \quad \begin{array}{r} 5.7 \\ C6.1 \\ \hline 39.2 \end{array} \quad \begin{array}{r} 48 \\ 1.5 \\ \hline 4.2 \end{array} \quad \begin{array}{r} 0.3 \\ 0.3 \end{array}$$

3.3

$$\begin{array}{r} 76 \\ F4.3 \\ \hline 23.6 \end{array} \quad \begin{array}{r} 3.4 \\ FO.1 \end{array} \quad \begin{array}{r} 1.5 \\ C1.8 \\ \hline 300 \end{array}$$

3.6

$$\begin{array}{r} 131 \\ F5.5 \\ \hline 34.2 \end{array} \quad \begin{array}{r} 3.8 \\ FO.2 \end{array} \quad \begin{array}{r} 3.6 \\ C0.0 \\ \hline 270 \end{array}$$

5.0

$$\begin{array}{r} 162 \\ F11.2 \\ \hline 37.4 \end{array} \quad \begin{array}{r} 5.5 \\ FO.5 \end{array} \quad \begin{array}{r} 8.7 \\ F3.7 \\ \hline 22.6 \end{array}$$

6.0

$$\begin{array}{r} 131 \\ F7.1 \\ \hline 29.2 \end{array} \quad \begin{array}{r} 6.3 \\ FO.3 \end{array} \quad \begin{array}{r} 8.0 \\ B5.0 CO.0 \\ \hline 230 \end{array}$$

7.1

$$\begin{array}{r} 57 \\ C1.4 \\ \hline 29.8 \end{array} \quad \begin{array}{r} 7.1 \\ FO.0 \end{array} \quad \begin{array}{r} 3.6 \\ C3.7 \\ \hline 34.4 \end{array}$$

8.3

$$\begin{array}{r} 0.0 \\ C8.3 \\ \hline 43.6 \end{array} \quad \begin{array}{r} 8.2 \\ CO.1 \end{array} \quad \begin{array}{r} 3.0 \\ C5.3 \\ \hline 37.6 \end{array}$$

8.8

$$\begin{array}{r} 2.3 \\ C6.5 \\ \hline 400 \end{array} \quad \begin{array}{r} 87 \\ CO.1 \end{array} \quad \begin{array}{r} 2.3 \\ C6.5 \\ \hline 400 \end{array}$$

9.6

$$\begin{array}{r} 91.5 \\ C0.5 \\ \hline 580 \end{array} \quad \begin{array}{r} 98 \\ FO.2 \end{array} \quad \begin{array}{r} 4.6 \\ C5.0 \\ \hline 370 \end{array}$$

934.81

114

33.0

+50

32.1

115

31.4

+50

30.7

B.M.

5.06

934.61

5.15

929.66

929.55

116+08

30.1

+50

29.8

117

29.6

+50

29.5

118

29.5

B.M.

929.55

+50

29.6

119

30.0

+50

30.4

11.31

941.82

4.10

930.51

1.8

$$\begin{array}{r} 3.4 \\ \text{DCD.4} \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 21 \\ \hline \text{FO.3} \end{array}$$

$$\begin{array}{r} 01 \\ \hline \text{CT.7} \\ \hline 30.4 \end{array}$$

2.7

$$\begin{array}{r} 7.1 \\ \hline \text{F4.7} \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 3.1 \\ \hline \text{FO.4} \end{array}$$

$$\begin{array}{r} 41 \\ \hline \text{RO.6} \\ \hline 24.3 \end{array}$$

3.4

$$\begin{array}{r} 10.0 \\ \hline \text{F6.6} \\ \hline 28.2 \end{array}$$

$$\begin{array}{r} 3.9 \\ \hline \text{FO.5} \end{array}$$

$$\begin{array}{r} 65 \\ \hline \text{F2.1} \\ \hline 21.2 \end{array}$$

4.1

$$\begin{array}{r} 10.8 \\ \hline \text{F6.7} \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 45 \\ \hline \text{FO.4} \end{array}$$

$$\begin{array}{r} 82 \\ \hline \text{F4.7} \\ \hline 24.4 \end{array}$$

4.5

$$\begin{array}{r} 11.2 \\ \hline \text{F6.7} \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline \text{FO.5} \end{array}$$

$$\begin{array}{r} 10.1 \\ \hline \text{F5.6} \\ \hline 26.2 \end{array}$$

4.8

$$\begin{array}{r} 10.6 \\ \hline \text{F5.8} \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline \text{FO.3} \end{array}$$

$$\begin{array}{r} 10.3 \\ \hline \text{F5.5} \\ \hline 26.0 \end{array}$$

5.0

$$\begin{array}{r} 10.2 \\ \hline \text{F5.2} \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline \text{FO.2} \end{array}$$

$$\begin{array}{r} 9.6 \\ \hline \text{F4.0} \\ \hline 23.8 \end{array}$$

5.1

$$\begin{array}{r} 8.7 \\ \hline \text{F3.6} \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline \text{FO.2} \end{array}$$

$$\begin{array}{r} 8.6 \\ \hline \text{F3.5} \\ \hline 22.0 \end{array}$$

5.1

$$\begin{array}{r} 8.2 \\ \hline \text{F3.1} \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ \hline \text{FO.3} \end{array}$$

$$\begin{array}{r} 7.3 \\ \hline \text{F2.2} \\ \hline 19.4 \end{array}$$

Spk PP 2866 118-37

5.0

$$\begin{array}{r} 7.0 \\ \hline \text{F2.0} \\ \hline 19.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline \text{FO.2} \end{array}$$

$$\begin{array}{r} 5.7 \\ \hline \text{DC.1.3} \\ \hline 25.6 \end{array}$$

4.6

$$\begin{array}{r} 5.6 \\ \hline \text{DC1.0} \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ \hline \text{FO.3} \end{array}$$

$$\begin{array}{r} 3.7 \\ \hline \text{CO.9} \\ \hline 28.8 \end{array}$$

4.2

$$\begin{array}{r} 4.9 \\ \hline \text{DC1.9} \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 4.6 \\ \hline \text{FO.4} \end{array}$$

$$\begin{array}{r} 1.2 \\ \hline \text{C3.0} \\ \hline 33.0 \end{array}$$

941.82

120

30.9

+46

31.4

121

31.7

+50

31.7

122

31.3

+33

30.8

123

29.5

+65

28.3

124

27.6

T.P.

2.55

931.01

13.36

928.46

+50

26.7

125

25.7

T.P.

3.68

928.58

6.11

924.90

25

+50

24.8

10.9

$$\begin{array}{r} 7.9 \\ \overline{C1.0} \\ 29^\circ \end{array}$$

$$\begin{array}{r} 11.3 \\ \overline{F0.4} \end{array}$$

$$\begin{array}{r} 6.6 \\ \overline{C4.3} \\ 35.6 \end{array}$$

10.6

$$\begin{array}{r} 8.9 \\ \overline{C1.5} \\ 30^\circ \end{array}$$

$$\begin{array}{r} 10.7 \\ \overline{F0.3} \end{array}$$

$$\begin{array}{r} 8.5 \\ \overline{C1.9} \\ 30.8 \end{array}$$

10.1

$$\begin{array}{r} 6.2 \\ \overline{C3.9} \\ 34.8 \end{array}$$

$$\begin{array}{r} 10.3 \\ \overline{F0.2} \end{array}$$

$$\begin{array}{r} 4.3 \\ \overline{C5.8} \\ 38.6 \end{array}$$

10.1

$$\begin{array}{r} 5.2 \\ \overline{C4.9} \\ 36.8 \end{array}$$

$$\begin{array}{r} 10.3 \\ \overline{F0.2} \end{array}$$

$$\begin{array}{r} 2.6 \\ \overline{C7.5} \\ 42^\circ \end{array}$$

10.5

$$\begin{array}{r} 7.5 \\ \overline{C3.0} \\ 33^\circ \end{array}$$

$$\begin{array}{r} 10.7 \\ \overline{F0.2} \end{array}$$

$$\begin{array}{r} 6.3 \\ \overline{C4.2} \\ 35.4 \end{array}$$

11.0

$$\begin{array}{r} 8.8 \\ \overline{C2.2} \\ 31.4 \end{array}$$

$$\begin{array}{r} 11.2 \\ \overline{F0.2} \end{array}$$

$$\begin{array}{r} 9.5 \\ \overline{C1.5} \\ 30^\circ \end{array}$$

12.3

$$\begin{array}{r} 3.3 \\ \overline{C9.0} \\ 45^\circ \end{array}$$

$$\begin{array}{r} 12.2 \\ \overline{C0.1} \end{array}$$

$$\begin{array}{r} 8.0 \\ \overline{C4.3} \\ 35.6 \end{array}$$

13.5

$$\begin{array}{r} 9.5 \\ \overline{C4.0} \\ 35^\circ \end{array}$$

$$\begin{array}{r} 14.0 \\ \overline{F0.5} \end{array}$$

$$\begin{array}{r} 11.4 \\ \overline{C2.1} \\ 31.2 \end{array}$$

14.2

$$\begin{array}{r} 11.5 \\ \overline{C2.7} \\ 32.2 \end{array}$$

$$\begin{array}{r} 14.9 \\ \overline{F0.7} \end{array}$$

$$\begin{array}{r} 12.5 \\ \overline{C1.7} \\ 30.4 \end{array}$$

4.3

$$\begin{array}{r} 4.7 \\ \overline{D61.6} \\ 26.2 \end{array}$$

$$\begin{array}{r} 5.1 \\ \overline{F0.8} \end{array}$$

$$\begin{array}{r} 2.7 \\ \overline{C1.6} \\ 30.2 \end{array}$$

5.3

$$\begin{array}{r} 11.9 \\ \overline{F6.6} \\ 28.2 \end{array}$$

$$\begin{array}{r} 6.1 \\ \overline{F0.8} \end{array}$$

$$\begin{array}{r} 5.4 \\ \overline{D61.9} \\ 26.2 \end{array}$$

3.6

$$\begin{array}{r} 12.3 \\ \overline{F8.5} \\ 32.2 \end{array}$$

$$\begin{array}{r} 4.7 \\ \overline{F0.9} \end{array}$$

$$\begin{array}{r} 6.4 \\ \overline{F2.6} \\ 20.2 \end{array}$$

928.58⁶

126 24.0

+40 23.6

+90 23.3

127+50 23.6

128 23.8

+50 24.6

129 25.6

+50 27.0

T.P. 11.96 939.42 1.12 927.46

130 28.5

+50 30.0

131+18 32.0

+30 32.4

X

4.6

$$\begin{array}{r} 13.7 \\ F9.1 \\ \hline 33.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ F0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 8.8 \\ F4.2 \\ \hline 23.2 \end{array}$$

5.0

$$\begin{array}{r} 13.7 \\ F8.7 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ F.0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 10.9 \\ F5.9 \\ \hline 26.8 \end{array}$$

5.5

$$\begin{array}{r} 13.5 \\ F8.2 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 5.8 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 13.2 \\ F7.9 \\ \hline 30.8 \end{array}$$

5.2

$$\begin{array}{r} 13.8 \\ F8.6 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 5.7 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 13.7 \\ F8.5 \\ \hline 32.2 \end{array}$$

4.8

$$\begin{array}{r} 13.9 \\ F9.1 \\ \hline 33.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ F0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 14.1 \\ F9.3 \\ \hline 33.6 \end{array}$$

4.0

$$\begin{array}{r} 14.0 \\ F10.0 \\ \hline 35.2 \end{array}$$

$$\begin{array}{r} 4.5 \\ F.0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 14.6 \\ F10.6 \\ \hline 36.2 \end{array}$$

3.0

$$\begin{array}{r} 13.5 \\ F9.5 \\ \hline 34.2 \end{array}$$

$$\begin{array}{r} 3.5 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 12.5 \\ F9.5 \\ \hline 34.2 \end{array}$$

1.6

$$\begin{array}{r} 5.1 \\ F3.5 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 2.2 \\ F0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 7.1 \\ F5.5 \\ \hline 26.2 \end{array}$$

10.9

$$\begin{array}{r} 6.8 \\ C4.1 \\ \hline 35.2 \end{array}$$

$$\begin{array}{r} 11.1 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 16.3 \\ DC1.6 \\ \hline 26.2 \end{array}$$

9.6

$$\begin{array}{r} 5.6 \\ C3.8 \\ \hline 34.6 \end{array}$$

$$\begin{array}{r} 9.7 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ C3.2 \\ \hline 33.2 \end{array}$$

7.6

$$\begin{array}{r} 7.6 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ C1.4 \\ \hline 29.8 \end{array}$$

7.6

939.42

131 +40

32.7

T.P.

11.05

950.38

009

939.33

+57

50.2
33.2

475

33.7

132

34.5

+50

36.0

133

37.5

+30

38.4

+70

39.6

134

40.5

+28

41.3

1

+54

41.8

135

42.4

6.6
16.6
15.7

6.7

X

$$\begin{array}{r} 6.9 \\ \hline F0.2 \end{array}$$

$$\begin{array}{r} 57 \\ \hline C1.0 \\ \hline 79 \end{array}$$

17.2

V

$$\begin{array}{r} 17 \\ \hline X \end{array}$$

$$\begin{array}{r} 17 \\ \hline X \end{array}$$

16.7

X

$$\begin{array}{r} 16.9 \\ \hline F0.2 \end{array}$$

$$\begin{array}{r} 160 \\ \hline C0.71 \\ \hline 28 \end{array}$$

15.9

$$\begin{array}{r} 140 \\ \hline C1.9 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 16.1 \\ \hline F0.2 \end{array}$$

$$\begin{array}{r} 140 \\ \hline C1.9 \\ \hline 30 \end{array}$$

14.4

$$\begin{array}{r} 11.9 \\ \hline C2.5 \\ \hline 32 \end{array}$$

$$\begin{array}{r} 14.7 \\ \hline F0.3 \end{array}$$

$$\begin{array}{r} 94 \\ \hline C50 \\ \hline 370 \end{array}$$

12.9

$$\begin{array}{r} 11.3 \\ \hline C1.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 13.0 \\ \hline F0.1 \end{array}$$

$$\begin{array}{r} 29 \\ \hline C10.0 \\ \hline 47 \end{array}$$

12.0

$$\begin{array}{r} 12.5 \\ \hline C1.5 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 12.3 \\ \hline F0.3 \end{array}$$

$$\begin{array}{r} 2.5 \\ \hline C9.5 \\ \hline 46 \end{array}$$

10.8

$$\begin{array}{r} 16.6 \\ \hline F5.8 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 11.3 \\ \hline F0.5 \end{array}$$

$$\begin{array}{r} 124 \\ \hline C0.1 \\ \hline 23.8 \end{array}$$

9.9

$$\begin{array}{r} 13.4 \\ \hline F3.5 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 10.5 \\ \hline F0.6 \end{array}$$

$$\begin{array}{r} 146 \\ \hline C4.7 \\ \hline 24 \end{array}$$

9.1

$$\begin{array}{r} 11.7 \\ \hline F2.6 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 9.8 \\ \hline F0.7 \end{array}$$

$$\begin{array}{r} 160 \\ \hline F4.9 \\ \hline 24 \end{array}$$

8.6

$$\begin{array}{r} 13.3 \\ \hline F4.7 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 9.2 \\ \hline F0.6 \end{array}$$

$$\begin{array}{r} 148 \\ \hline F6.2 \\ \hline 27 \end{array}$$

8.0

$$\begin{array}{r} 16.7 \\ \hline F8.7 \\ \hline 32.4 \end{array}$$

$$\begin{array}{r} 8.6 \\ \hline F0.4 \end{array}$$

$$\begin{array}{r} 13.3 \\ \hline F5.3 \\ \hline 25 \end{array}$$

950.38

135+42

42.6

T.P

5.23

953.09

2.52

947.86

136

42.2

+31

41.7

+70

40.8

137

39.9

+39

38.6

+76

37.2

138

36.5

+52

35.4

+72

34.0

T.P

5.84

940.27

11.98

941.11

139

33.1

T.P

1.42

932.63

9.06

931.21

+29

32.1

T.P

7.6	$\begin{array}{r} 13.6 \\ F5.8 \\ \hline 26.6 \end{array}$	$\begin{array}{r} 7.9 \\ F0.3 \\ \hline \end{array}$	$\begin{array}{r} 9.7 \\ F2.1 \\ \hline 19.2 \end{array}$
Fe P ₂ R ₁ +75			
10.9	$\begin{array}{r} 6.9 \\ C4.0 \\ \hline 35.2 \end{array}$	$\begin{array}{r} 10.1 \\ C0.8 \\ \hline \end{array}$	$\begin{array}{r} 3.4 \\ C7.5 \\ \hline 42.0 \end{array}$
11.4	$\begin{array}{r} 2.6 \\ C8.8 \\ \hline 44.5 \end{array}$	$\begin{array}{r} 10.4 \\ C1.0 \\ \hline \end{array}$	$\begin{array}{r} 1.9 \\ C9.5 \\ \hline 46.3 \end{array}$
12.3	$\begin{array}{r} 6.6 \\ C3.7 \\ \hline 38.4 \end{array}$	$\begin{array}{r} 1.7 \\ C0.6 \\ \hline \end{array}$	$\begin{array}{r} 6.6 \\ C5.7 \\ \hline 38.4 \end{array}$
13.2	$\begin{array}{r} 7.0 \\ C6.2 \\ \hline 39.6 \end{array}$	$\begin{array}{r} 12.7 \\ C0.5 \\ \hline \end{array}$	$\begin{array}{r} 10.6 \\ C2.6 \\ \hline 32.2 \end{array}$
14.5	$\begin{array}{r} 8.1 \\ C2.1 \\ \hline 39.8 \end{array}$	$\begin{array}{r} 14.1 \\ C0.4 \\ \hline \end{array}$	$\begin{array}{r} 8.2 \\ C6.3 \\ \hline 39.6 \end{array}$
15.9	$\begin{array}{r} 10.1 \\ C5.8 \\ \hline 38.6 \end{array}$	$\begin{array}{r} 15.4 \\ C0.5 \\ \hline \end{array}$	$\begin{array}{r} 5.3 \\ C10.6 \\ \hline 48.2 \end{array}$
16.6		$\begin{array}{r} 16.4 \\ C0.2 \\ \hline \end{array}$	$\begin{array}{r} 7.5 \\ C9.1 \\ \hline 45.2 \end{array}$
17.7		$\begin{array}{r} 17.7 \\ C0.0 \\ \hline \end{array}$	$\begin{array}{r} 9.9 \\ C9.8 \\ \hline 42.6 \end{array}$
19.1	$\begin{array}{r} 16.8 \\ C2.3 \\ \hline 31.6 \end{array}$	$\begin{array}{r} 19.2 \\ F0.1 \\ \hline \end{array}$	$\begin{array}{r} 10.8 \\ C8.3 \\ \hline 43.5 \end{array}$
7.2	$\begin{array}{r} 8.6 \\ C0.6 \\ \hline 24.2 \end{array}$	$\begin{array}{r} 7.6 \\ F0.4 \\ \hline \end{array}$	$\begin{array}{r} 10.3 \\ C7.5 \\ \hline 42.2 \end{array}$
0.5	$\begin{array}{r} 6.3 \\ F3.8 \\ \hline 26.6 \end{array}$	$\begin{array}{r} 6.1 \\ F0.6 \\ \hline \end{array}$	$\begin{array}{r} 11.1 \\ C6.4 \\ \hline 25.8 \end{array}$

932.63

139 + 50

31.4 ✓

146

29.9

+ 50

28.8

141

28.2

140

28.0

BM

2.83

932.71

2.83

929.88

929.80

+ 95

28.0

142 + 32

28.0

+ 62

28.0

143

28.0

BM

1.16

931.04

2.83

929.88

+ 50

28.0

144

28.0

+ 50

28.0

$$\begin{array}{r}
 11.9 \\
 \underline{F9.1} \\
 34
 \end{array}
 \qquad
 \begin{array}{r}
 2.1 \\
 \underline{F0.9} \\
 34
 \end{array}
 \qquad
 \begin{array}{r}
 6.1 \\
 \underline{F4.9} \\
 24
 \end{array}$$

$$\begin{array}{r}
 12.7 \\
 \underline{F10.0} \\
 35
 \end{array}
 \qquad
 \begin{array}{r}
 3.6 \\
 \underline{F0.9} \\
 35
 \end{array}
 \qquad
 \begin{array}{r}
 10.8 \\
 \underline{F8.1} \\
 31.2
 \end{array}$$

$$\begin{array}{r}
 12.6 \\
 \underline{F8.8} \\
 32
 \end{array}
 \qquad
 \begin{array}{r}
 4.4 \\
 \underline{F0.6} \\
 32
 \end{array}
 \qquad
 \begin{array}{r}
 13.1 \\
 \underline{F9.3} \\
 33.6
 \end{array}$$

$$\begin{array}{r}
 11.8 \\
 \underline{F7.4} \\
 29
 \end{array}
 \qquad
 \begin{array}{r}
 4.2 \\
 \underline{F0.3} \\
 29
 \end{array}
 \qquad
 \begin{array}{r}
 12.8 \\
 \underline{F8.4} \\
 31.8
 \end{array}$$

$$\begin{array}{r}
 9.3 \\
 \underline{F4.7} \\
 24
 \end{array}
 \qquad
 \begin{array}{r}
 4.6 \\
 \underline{F0.0} \\
 24
 \end{array}
 \qquad
 \begin{array}{r}
 11.9 \\
 \underline{F7.3} \\
 29
 \end{array}$$

Spk PR 27' LT 141 x 60

$$\begin{array}{r}
 0.1 \\
 \underline{C4.6} \\
 36
 \end{array}
 \qquad
 \begin{array}{r}
 1.3 \\
 \underline{C0.4} \\
 36
 \end{array}
 \qquad
 \begin{array}{r}
 6.9 \\
 \underline{F2.2} \\
 19
 \end{array}$$

$$\begin{array}{r}
 5.4 \\
 \underline{C1.3} \\
 25
 \end{array}
 \qquad
 \begin{array}{r}
 4.5 \\
 \underline{C0.2} \\
 25
 \end{array}
 \qquad
 \begin{array}{r}
 10.9 \\
 \underline{F6.2} \\
 27
 \end{array}$$

$$\begin{array}{r}
 10.2 \\
 \underline{F5.5} \\
 26
 \end{array}
 \qquad
 \begin{array}{r}
 4.6 \\
 \underline{C0.1} \\
 26
 \end{array}
 \qquad
 \begin{array}{r}
 12.8 \\
 \underline{F8.1} \\
 31
 \end{array}$$

$$\begin{array}{r}
 13.7 \\
 \underline{F9.0} \\
 33
 \end{array}
 \qquad
 \begin{array}{r}
 5.3 \\
 \underline{F0.6} \\
 33
 \end{array}
 \qquad
 \begin{array}{r}
 12.9 \\
 \underline{F8.2} \\
 31.4
 \end{array}$$

$$\begin{array}{r}
 12.6 \\
 \underline{F9.6} \\
 34
 \end{array}
 \qquad
 \begin{array}{r}
 4.9 \\
 \underline{F1.9} \\
 34
 \end{array}
 \qquad
 \begin{array}{r}
 12.0 \\
 \underline{F9.0} \\
 33
 \end{array}$$

$$\begin{array}{r}
 10.7 \\
 \underline{F7.7} \\
 30
 \end{array}
 \qquad
 \begin{array}{r}
 5.6 \\
 \underline{F2.6} \\
 30
 \end{array}
 \qquad
 \begin{array}{r}
 4.1 \\
 \underline{F8.1} \\
 31
 \end{array}$$

$$\begin{array}{r}
 11.7 \\
 \underline{F8.7} \\
 32
 \end{array}
 \qquad
 \begin{array}{r}
 5.5 \\
 \underline{F2.5} \\
 32
 \end{array}
 \qquad
 \begin{array}{r}
 12.6 \\
 \underline{F9.6} \\
 34
 \end{array}$$

931.04

145-

28.3

+65

29.1

T.P.

13.75

942.60

2.19

928.85

146

29.9

+50

31.3

T.P.

9.96

951.41

1.15

941.45

147

32.9

+41

34.3

148

36.1

+50

37.3

149

38.3

T.P.

7.56

949.65

9.32

942.09

+50

38.9

150

39.3

+50

39.4

2.7

$$\begin{array}{r} 12.1 \\ F9.4 \\ \hline 33.8 \end{array}$$

$$\begin{array}{r} 4.6 \\ F1.9 \\ \hline \end{array}$$

$$\begin{array}{r} 12.3 \\ F9.6 \\ \hline 34.2 \end{array}$$

7.7

$$\begin{array}{r} 5.3 \\ F3.6 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 2.4 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 4.9 \\ F2.0 \\ \hline 21.2 \end{array}$$

12.7

$$\begin{array}{r} 6.7 \\ C6.0 \\ \hline 39.0 \end{array}$$

$$\begin{array}{r} 13.0 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.4 \\ C7.3 \\ \hline 35.2 \end{array}$$

11.3

$$\begin{array}{r} 1.4 \\ C15.4 \\ \hline 37.8 \end{array}$$

$$\begin{array}{r} 11.4 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 7.4 \\ C3.9 \\ \hline 34.8 \end{array}$$

18.5

$$\begin{array}{r} 2.7 \\ C15.8 \\ \hline 58.5 \end{array}$$

$$\begin{array}{r} 18.5 \\ F0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 12.6 \\ C5.9 \\ \hline 38.8 \end{array}$$

17.1

$$\begin{array}{r} 0.7 \\ C10.4 \\ \hline 59.8 \end{array}$$

$$\begin{array}{r} 17.3 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.9 \\ C9.2 \\ \hline 45.1 \end{array}$$

15.3

$$\begin{array}{r} 3.7 \\ C17.6 \\ \hline 50.2 \end{array}$$

$$\begin{array}{r} 15.8 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 3.6 \\ C11.7 \\ \hline 50.4 \end{array}$$

14.1

$$\begin{array}{r} 4.5 \\ C9.6 \\ \hline 46.2 \end{array}$$

$$\begin{array}{r} 14.6 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C11.2 \\ \hline 49.4 \end{array}$$

13.1

$$\begin{array}{r} 8.6 \\ C6.5 \\ \hline 36.0 \end{array}$$

$$\begin{array}{r} 13.4 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ C8.4 \\ \hline 43.8 \end{array}$$

10.8

$$\begin{array}{r} 8.3 \\ C2.5 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 10.9 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 2.1 \\ C8.7 \\ \hline 44.4 \end{array}$$

10.4

$$\begin{array}{r} 8.2 \\ C2.2 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 10.2 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 0.8 \\ C7.6 \\ \hline 46.2 \end{array}$$

10.3

$$\begin{array}{r} 6.9 \\ C3.4 \\ \hline 33.8 \end{array}$$

$$\begin{array}{r} 9.9 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 2.3 \\ C8.0 \\ \hline 43.0 \end{array}$$

949.65⁷

151

39.3

+31

39.3

+25

39.2

152

39.2

T.P. 2.66 942.05 10.26 939.39

+40 39.1

+78

39.0

153

38.8

+50

38.1

154

37.0

+43

35.6

T.P. 3.91 940.82 5.14 936.91

155

33.6

+50

31.8

10.4

$$\begin{array}{r} 5.4 \\ C5.0 \\ \hline 37^{\circ} \end{array}$$

$$\begin{array}{r} 9.9 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 38 \\ C6.6 \\ \hline 40.2 \end{array}$$

10.4

$$\begin{array}{r} 5.7 \\ C4.7 \\ \hline 36.4 \end{array}$$

$$\begin{array}{r} 10.0 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 45 \\ C5.9 \\ \hline 38.8 \end{array}$$

10.5

$$\begin{array}{r} 9.9 \\ C0.6 \\ \hline 28^{\circ} \end{array}$$

$$\begin{array}{r} 10.1 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 7.2 \\ C3.3 \\ \hline 33.5 \end{array}$$

10.5

$$\begin{array}{r} 10.3 \\ C0.2 \\ \hline 27^{\circ} \end{array}$$

$$\begin{array}{r} 10.1 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 8.5 \\ C2.0 \\ \hline 31^{\circ} \end{array}$$

30

$$\begin{array}{r} 1.2 \\ C1.8 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 2.9 \\ C0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 2.2 \\ C0.8 \\ \hline 28.6 \end{array}$$

3.1

$$\begin{array}{r} 4.9 \\ C50.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 3.5 \\ F0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ C50.0 \\ \hline 23.0 \end{array}$$

3.3

$$\begin{array}{r} 4.9 \\ C0.4 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 4.0 \\ F0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 8.4 \\ F5.1 \\ \hline 25.2 \end{array}$$

40

$$\begin{array}{r} 8.2 \\ F4.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 5.0 \\ F1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 10.3 \\ F6.3 \\ \hline 27.6 \end{array}$$

51

$$\begin{array}{r} 7.7 \\ F2.6 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 5.8 \\ F0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 10.2 \\ F5.2 \\ \hline 25.4 \end{array}$$

6.5

$$\begin{array}{r} 6.9 \\ C7.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 6.8 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.3 \\ C50.2 \\ \hline 23.4 \end{array}$$

P.R. L.I. 155

7.2

$$\begin{array}{r} 5.2 \\ C2.0 \\ \hline 31^{\circ} \end{array}$$

$$\begin{array}{r} 7.3 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ C0.8 \\ \hline 28.6 \end{array}$$

9.0

$$\begin{array}{r} 4.9 \\ C4.1 \\ \hline 35.2 \end{array}$$

$$\begin{array}{r} 9.1 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ C3.4 \\ \hline 33.5 \end{array}$$

94082

156 30.0

+50 28.2

157 26.4

+28 25.4

B.M. 927.16

+50 24.6

158 22.8

+50 21.0

B.M. 0.50 927.66 13.58 927.24 (927.16)

159 19.4

T.P. 1.47 920.41 8.72 918.94

+50 18.0

160 17.0

T.P. 3.22 920.25 3.38 917.03

+50 16.2

161 15.8

10.8

$$\begin{array}{r} 5.1 \\ C5.7 \\ \hline 38.2 \end{array}$$

$$\begin{array}{r} 11.0 \\ \hline F0.2 \end{array}$$

$$\begin{array}{r} 6.1 \\ C6.7 \\ \hline 40.4 \end{array}$$

12.6

$$\begin{array}{r} 6.0 \\ C6.6 \\ \hline 40.2 \end{array}$$

$$\begin{array}{r} 12.6 \\ \hline F6.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ C6.4 \\ \hline 39.8 \end{array}$$

14.4

$$\begin{array}{r} 10.1 \\ C4.3 \\ \hline 35.5 \end{array}$$

$$\begin{array}{r} 14.5 \\ \hline F0.1 \end{array}$$

$$\begin{array}{r} 5.6 \\ C8.8 \\ \hline 44.6 \end{array}$$

15.4

$$\begin{array}{r} 15.8 \\ C6.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 15.4 \\ \hline F0.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ C8.8 \\ \hline 44.6 \end{array}$$

J.E. Cor. Conc Step 60' Lt. 15-7-80

16.2

$$\begin{array}{r} 16.2 \\ C0.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 16.2 \\ \hline F0.0 \end{array}$$

$$\begin{array}{r} 21 \\ C9.1 \\ \hline 45.2 \end{array}$$

18.0

$$\begin{array}{r} 17.3 \\ C0.7 \\ \hline 28.1 \end{array}$$

$$\begin{array}{r} 18.0 \\ \hline F0.0 \end{array}$$

$$\begin{array}{r} 8.4 \\ C9.6 \\ \hline 46.2 \end{array}$$

19.8

$$\begin{array}{r} 19.8 \\ C0.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 20.0 \\ \hline F0.2 \end{array}$$

$$\begin{array}{r} 10.8 \\ C9.0 \\ \hline 45.2 \end{array}$$

0.3

$$\begin{array}{r} 14.2 \\ F5.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 8.7 \\ \hline F0.4 \end{array}$$

$$\begin{array}{r} 1.5 \\ C6.8 \\ \hline 40.6 \end{array}$$

2.4

$$\begin{array}{r} 2.4 \\ F7.0 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 2.9 \\ \hline F0.5 \end{array}$$

$$\begin{array}{r} 5.6 \\ F9.2 \\ \hline 21.4 \end{array}$$

3.4

$$\begin{array}{r} 7.7 \\ F6.3 \\ \hline 27.5 \end{array}$$

$$\begin{array}{r} 3.8 \\ \hline F0.4 \end{array}$$

$$\begin{array}{r} 5.0 \\ F1.6 \\ \hline 18.2 \end{array}$$

T.P. Lt. 160 + 50

4.1

$$\begin{array}{r} 5.6 \\ F1.5 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 4.3 \\ \hline F0.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ F1.3 \\ \hline 17.5 \end{array}$$

4.5

$$\begin{array}{r} 4.1 \\ F1.6 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline F0.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ F1.2 \\ \hline 17.4 \end{array}$$

920.25³

161 +50

15.6

162

15.6

+50

15.6

163

15.6

+70

15.6

164

15.6

+40

15.6

165

15.6

T.P. 3.79 919.30 4.74 915.51

+50

15.5

166

15.2

+50

14.6

167

14.1

4.7

$$\begin{array}{r} 5.4 \\ F0.7 \\ \hline 16.4 \end{array}$$

$$\begin{array}{r} 4.7 \\ F0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ F1.0 \\ \hline 17.2 \end{array}$$

4.7

$$\begin{array}{r} 5.7 \\ F1.0 \\ \hline 17.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ F0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.7 \\ F1.0 \\ \hline 17.0 \end{array}$$

4.7

$$\begin{array}{r} 5.8 \\ F0.5 \\ \hline 16.2 \end{array}$$

$$\begin{array}{r} 4.7 \\ F0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ F0.7 \\ \hline 16.4 \end{array}$$

4.7

$$\begin{array}{r} 5.5 \\ F0.8 \\ \hline 16.5 \end{array}$$

$$\begin{array}{r} 4.9 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.7 \\ F1.0 \\ \hline 17.0 \end{array}$$

4.7

$$\begin{array}{r} 8.2 \\ F3.5 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 9.9 \\ F5.2 \\ \hline 25.4 \end{array}$$

4.7

$$\begin{array}{r} 8.1 \\ F3.4 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ F0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 9.5 \\ F4.8 \\ \hline 24.6 \end{array}$$

4.7

$$\begin{array}{r} 5.4 \\ F1.3 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 8.8 \\ F4.1 \\ \hline 23.2 \end{array}$$

4.7

$$\begin{array}{r} 0.8 \\ C3.7 \\ \hline 34.8 \end{array}$$

$$\begin{array}{r} 4.8 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ F0.3 \\ \hline 23.6 \end{array}$$

3.8

$$\begin{array}{r} 10.3 \\ C4.1 \\ \hline 35.2 \end{array}$$

$$\begin{array}{r} 4.0 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 2.6 \\ C1.2 \\ \hline 29.4 \end{array}$$

4.1

$$\begin{array}{r} 1.5 \\ C2.6 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 4.2 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 2.6 \\ C1.7 \\ \hline 30.4 \end{array}$$

4.7

$$\begin{array}{r} 3.8 \\ C0.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 4.8 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.1 \\ C0.6 \\ \hline 28.2 \end{array}$$

5.2

$$\begin{array}{r} 6.1 \\ F1.1 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 5.3 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ DC1.2 \\ \hline 25.4 \end{array}$$

919.30

167+50

13.4

B.M.

6.47

918.34

7.15

912.15

912.07

168

12.6

+50

11.9

169

11.2

+50

10.4

170

09.7

+65

08.7

6.47

+71

08.6

B.M.

912.07

5.9

$$\begin{array}{r} 76 \\ DC03 \\ \hline 236 \end{array}$$

$$\begin{array}{r} 6.2 \\ FO.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ DC1.8 \\ \hline 26.6 \end{array}$$

5.9

$$\begin{array}{r} 46 \\ C1.3 \\ \hline 296 \end{array}$$

$$\begin{array}{r} 6.3 \\ FO.4 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ DC0.9 \\ \hline 24.8 \end{array}$$

6.6

$$\begin{array}{r} 3.3 \\ C3.3 \\ \hline 336 \end{array}$$

$$\begin{array}{r} 7.1 \\ FO.5 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ CO.0 \\ \hline 27.8 \end{array}$$

7.3

$$\begin{array}{r} 44 \\ C2.9 \\ \hline 32.8 \end{array}$$

$$\begin{array}{r} 7.6 \\ FO.3 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ C1.0 \\ \hline 29.8 \end{array}$$

8.1

$$\begin{array}{r} 5.5 \\ C2.6 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 8.3 \\ FO.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.1 \\ C1.0 \\ \hline 29.2 \end{array}$$

8.8

$$\begin{array}{r} 5.4 \\ C3.4 \\ \hline 33.8 \end{array}$$

$$\begin{array}{r} 9.0 \\ FO.2 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ CO.6 \\ \hline 28.2 \end{array}$$

9.8

$$\begin{array}{r} 6.5 \\ C2.3 \\ \hline 33.6 \end{array}$$

$$\begin{array}{r} 9.7 \\ FO.1 \\ \hline \end{array}$$

$$\begin{array}{r} 9.2 \\ CO.6 \\ \hline 28.2 \end{array}$$

9.9

Sph. P.P. N.W. Cor. Rice Creek Rd

$$\begin{array}{r} 686 \overline{) 610912} \\ \underline{686} \\ 223 \\ \underline{223} \\ 000 \end{array}$$

68	79	0912
89	2	

$$\begin{array}{r} 1736 \\ 1664 \\ \hline 72 \end{array}$$

$$\begin{array}{r} 10.83 \\ \times 117.36889 \\ \hline \end{array}$$

57925
Slope Stakes

for Special Ditch

Silver Lake Rd.

Lt. only Sta. to Sta.

21

27.1

5.2

5.2

57+36

10.0

57

10.2

56+50

10.5

56

10.8

55+73

11.0

55+36

11.2

B.M.

95672
=====

144
24.0
174

30.2



$$\begin{array}{r} 8.8 \\ S.D. 21.2 \\ \hline 32.8 \end{array}$$

$$\begin{array}{r} 9.7 \\ 60.3 \\ \hline 75.8 \end{array}$$

$$\begin{array}{r} 8.9 \\ S.D. 1.3 \\ \hline 32.4 \end{array}$$

$$\begin{array}{r} 9.9 \\ S.D. 0.3 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 8.9 \\ S.D. 1.6 \\ \hline 30.8 \end{array}$$

$$\begin{array}{r} 10.2 \\ S.D. 0.3 \\ \hline 23.0 \end{array}$$

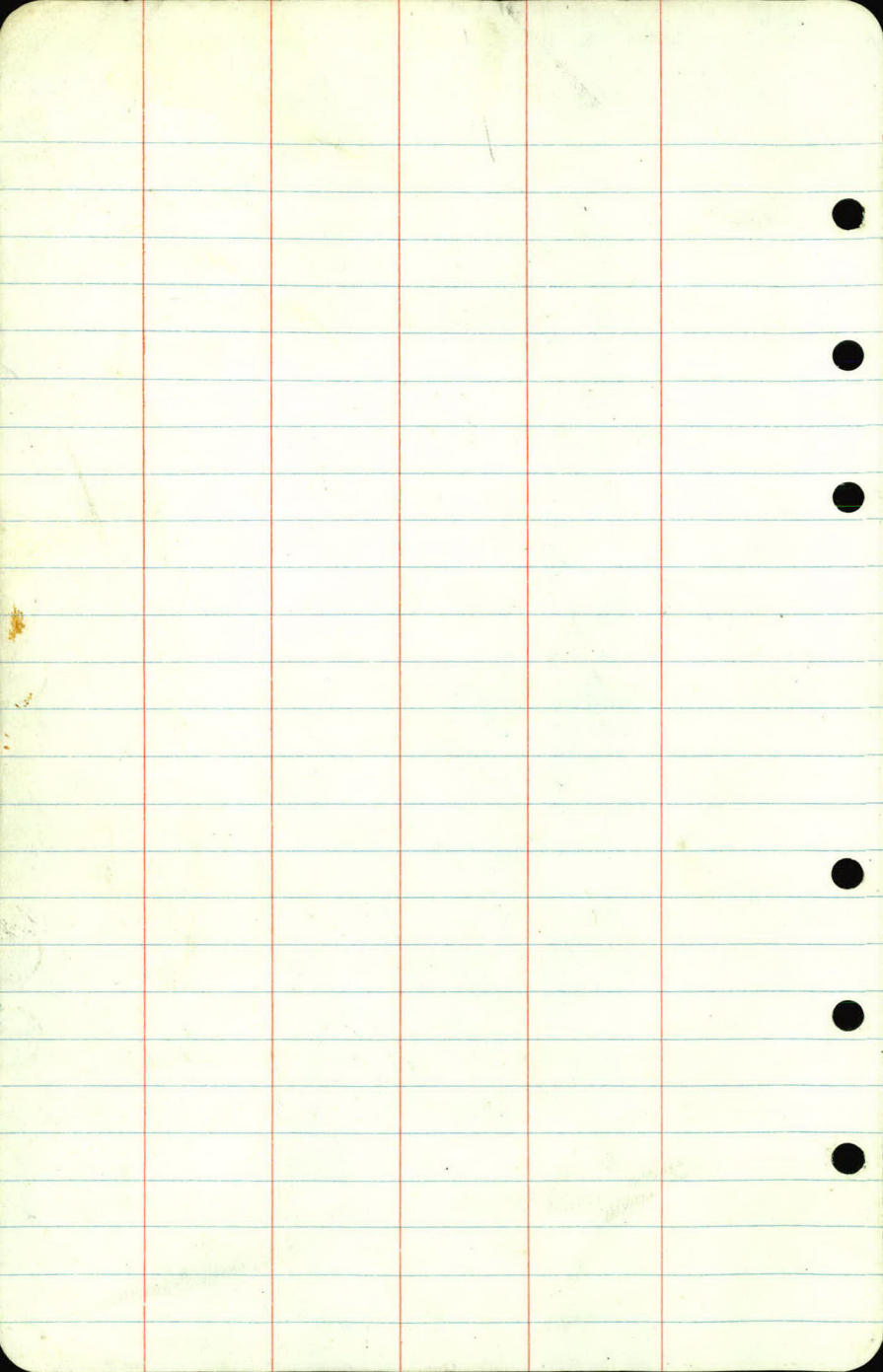
$$\begin{array}{r} 7.7 \\ S.D. 3.1 \\ \hline 33.6 \end{array}$$

$$\begin{array}{r} 10.0 \\ S.D. 0.8 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 7.0 \\ S.D. 4.0 \\ \hline 35.4 \end{array}$$

$$\begin{array}{r} 1.5 \\ S.D. 69.7 \\ \hline 44.2 \end{array}$$

Spike Fe. Cor. at first Curve.



Nail in 8" Oak

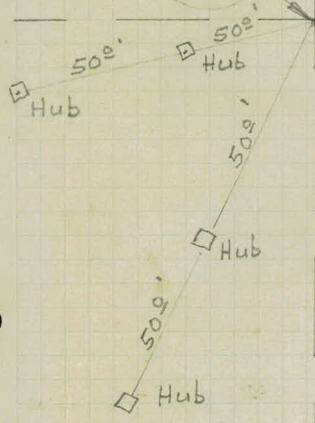
SILVER.

LAKE ROAD.

2x2 Hub
1.3' down

Nail in Cor Fence
Post,

1/4 Cor.



TH #100

Nail in 15" Oak

Nail in 15" Oak

Nail in 12" Oak

