

BK 30 - Dr 16

OFFICE OF COUNTY ENGINEER  
RAMSEY CO. MINN

PLAN

Survey

SNAIL LAKE BLVD.

From Victoria To Hodgson Ave

Road Ac't. No. 29

Date Filed 4/48

File

# Alignment

Snail Lake Blvd.

Victoria St. to Hodgson Rd.

2/13/39

R.P.

H.W.

A.M.

L.G.

Completed

12/1/39

W.S.P. H.W.

## Index

|                       |               |
|-----------------------|---------------|
| Alignment             | Sht. #1 to 8  |
| Topography            | Sht. #9 to 19 |
| Topog of Reiland Lane | #20 to 21     |
| Bench Levels          | 22 to 24      |
| Cross Sections        | 25 to 42      |
| Borrow Pit - Victoria | 43 to 45      |



Sta.      P.I.      Lt. Angle Rt.

|         |      |        |
|---------|------|--------|
| +72.94  | P.T. | 7°35'  |
| +50     |      | 5°52'  |
| 6+22.86 | P.I. | 15°10' |
| 6       |      | 2°07'  |
| 5+71.83 | P.C. | 0°00'  |

$\Delta = 15^{\circ}10'$

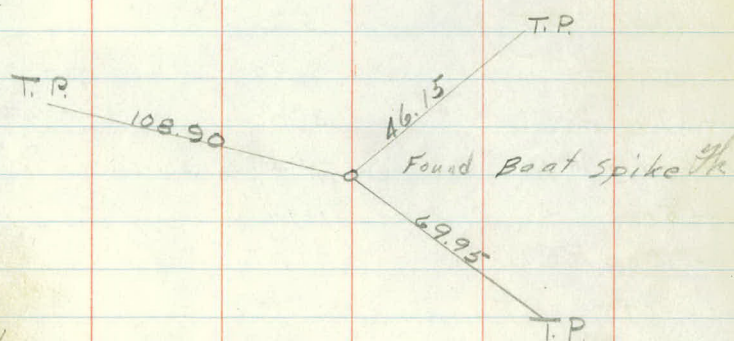
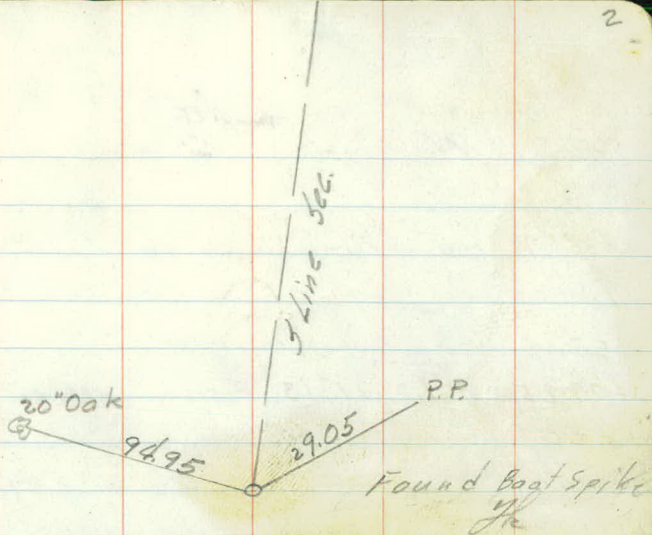
$D = 15^{\circ}$

$T = 51.03$

$L = 101.11$

$R = 383.065$

0-00.58 P.O.T. = 84+95.00 Co. Rd F



Note:  
see Co. Rd. "F" Notes for alignment  
of Victoria St.

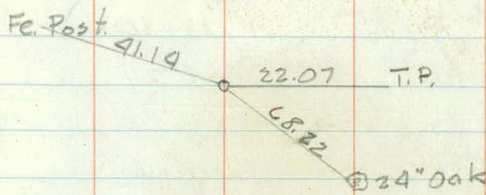
| Sta.    | Pt.  | Lt. Ang/c<br>Rt. |          |
|---------|------|------------------|----------|
| +38.87  | P.T. | 14°37'           |          |
| 19      |      | 12°04'           | Δ 29°13' |
| +50     |      | 8°47'            | D 13°    |
| +29.25  | P.I. | 29°13'           | T 115.12 |
| 18      |      | 5°34'            | L 224.74 |
| +50     |      | 2°19'            | R 491.68 |
| 17+1413 | P.C. | 0°00'            |          |

745.68

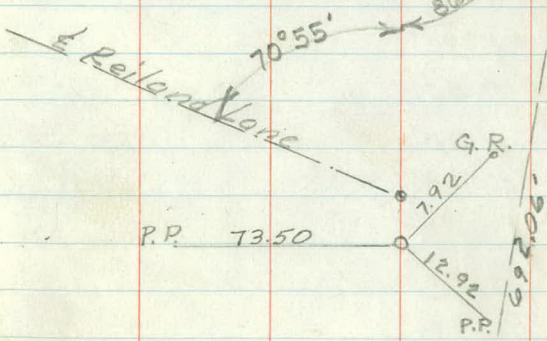
|          |                             |        |            |
|----------|-----------------------------|--------|------------|
| +42.35   | P.T.                        | 5°51'  | Δ - 11°42' |
| 11       |                             | 3°49'  | D - 10°    |
| +89.40   | P.O.C. (E. Ireland<br>lane) | 3°00'  | T - 58.78  |
| 10+8413  | P.I.                        | 11°42' | L 117.00   |
| +50      |                             | 1°14'  | R 573.626  |
| 10+25.35 | P.C.                        | 0°00'  |            |

462.22





498.87



~~E. Pelland Lane~~

| Sta.                                                                                                                                                                                                                                                                                                                                                         | Pt.  | Lt | Angle<br>Rt. |                   |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------|----|--------------|-------------------|
| +47.08                                                                                                                                                                                                                                                                                                                                                       | P.T. |    | 11°45'       |                   |
| 32                                                                                                                                                                                                                                                                                                                                                           |      |    | 9°24'        | $\Delta = 23°30'$ |
| +50                                                                                                                                                                                                                                                                                                                                                          |      |    | 6°54'        | $D = 10°$         |
| +31.42                                                                                                                                                                                                                                                                                                                                                       | P.I. |    | 23°30'       | $T = 119.34$      |
| 31                                                                                                                                                                                                                                                                                                                                                           |      |    | 4°24'        | $L = 235.00$      |
| +50                                                                                                                                                                                                                                                                                                                                                          |      |    | 1°54'        | $R =$             |
| 30+12.08                                                                                                                                                                                                                                                                                                                                                     | P.C. |    | 0°00'        |                   |
| <div style="position: relative; height: 100px;"> <div style="position: absolute; top: 0; left: 0; transform: rotate(-90deg); transform-origin: left top;">636.46</div> <div style="position: absolute; top: 50%; left: 50%; transform: translate(-50%, -50%) rotate(-45deg); font-size: 2em; color: red;">           All future change         </div> </div> |      |    |              |                   |
| +24.94                                                                                                                                                                                                                                                                                                                                                       | P.T. |    | 18°37'       |                   |
| 26                                                                                                                                                                                                                                                                                                                                                           |      |    | 16°45'       | $\Delta = 37°13'$ |
| +50                                                                                                                                                                                                                                                                                                                                                          |      |    | 13°00'       | $D = 15°$         |
| +05.85                                                                                                                                                                                                                                                                                                                                                       | P.I. |    | 37°13'       | $T = 129.98$      |
| 25                                                                                                                                                                                                                                                                                                                                                           |      |    | 9°15'        | $L = 248.11$      |
| +50                                                                                                                                                                                                                                                                                                                                                          |      |    | 5°30'        | $R = 383.065$     |
| 24                                                                                                                                                                                                                                                                                                                                                           |      |    | 1°45'        |                   |
| 23+76.83                                                                                                                                                                                                                                                                                                                                                     | P.C. |    | 0°00'        |                   |

21+02.27 P.O.T.

682.10

Realignment

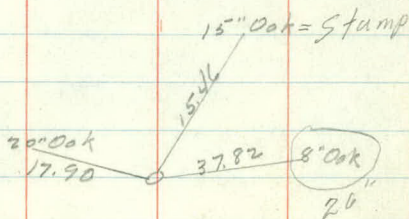
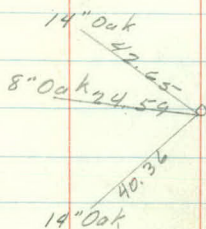
Snail Lake Blvd.

| Sta      | Pt   | LI | Angle   | RT |            |
|----------|------|----|---------|----|------------|
| 170.50   | P.T. |    | 11° 37' | Δ  | 23° 14' RT |
| +50      |      |    | 10° 35' | D  | 10°        |
| 33       |      |    | 8° 05'  | T  | 117.93     |
| 32+56.1  | P.I. |    | 23° 14' | L  | 232.33     |
| +50      |      |    | 5° 35'  | R  | 573.686    |
| 32       |      |    | 3° 05'  |    |            |
| +50      |      |    | 0° 35'  |    |            |
| 31+38.17 | P.C. |    |         |    |            |

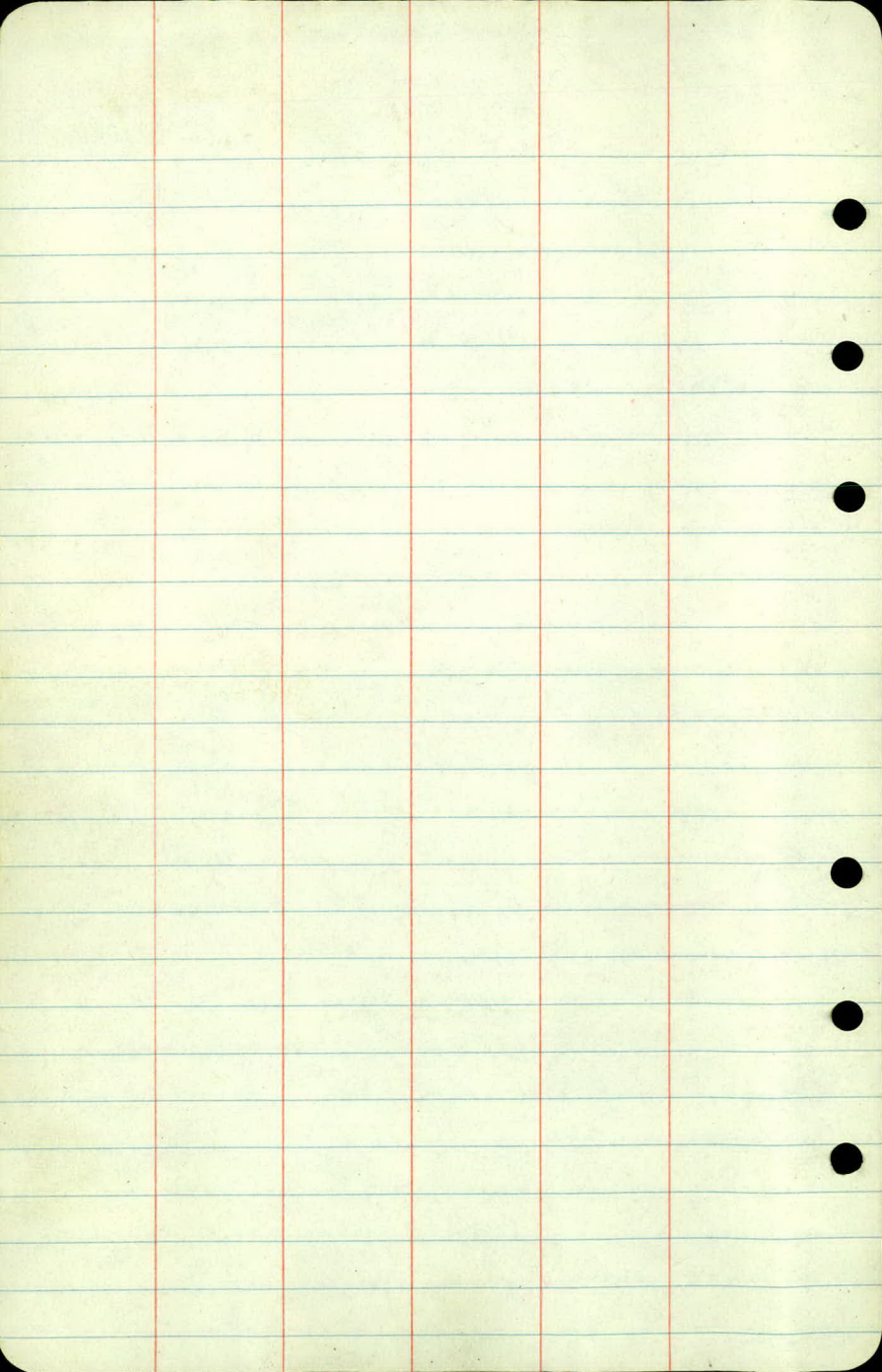
|         |      |         |         |   |            |
|---------|------|---------|---------|---|------------|
| 26+97.2 | P.T. |         | 18° 27' | Δ | 36° 54' LT |
| +50     |      |         | 14° 55' | D | 15°        |
| 26      |      |         | 11° 10' | T | 127.80     |
| 25+79.2 | P.I. | 36° 54' |         | L | 246.00     |
| +50     |      |         | 7° 25'  | R | 383.065    |
| 25      |      |         | 3° 40'  |   |            |
| 24+51.2 | P.C. |         |         |   |            |

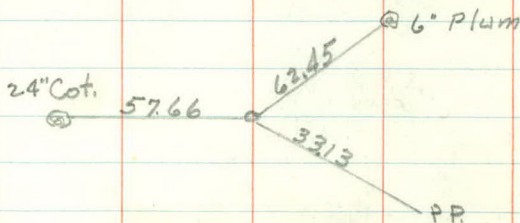
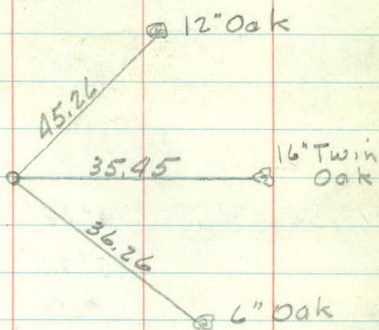
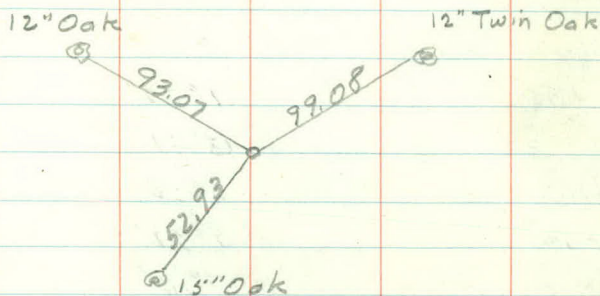


Equation 33+79.03 = P.C. 33+73.77



FIX 8/55





| Sta      | Pt.  | Lt. | Angle | Rt. |                        |
|----------|------|-----|-------|-----|------------------------|
| +89.67   | P.T. |     | 1°11' |     | $\Delta = 2^\circ 22'$ |
| +50      |      |     | 1°02' |     | $D = 1^\circ$          |
| 40       |      |     | 0°47' |     | $T = 118.35$           |
| +71.35   | P.I. |     | 2°22' |     | $L = 236.67$           |
| +50      |      |     | 0°32' |     | $R =$                  |
| 39       |      |     | 0°16' |     |                        |
| 38+53.00 |      |     | 0°00' |     |                        |

505.77

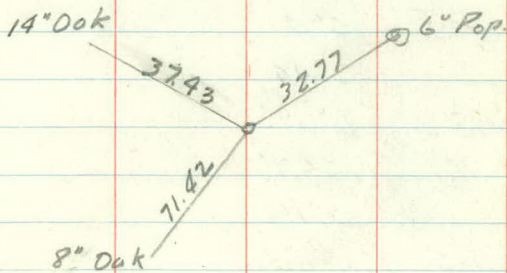
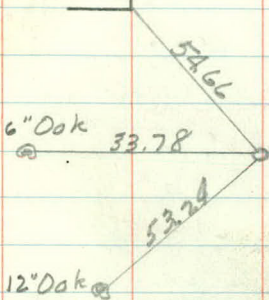
See Line Change  
Pages 8A. + 8B.

|          |      |        |  |  |                         |
|----------|------|--------|--|--|-------------------------|
| +13.58   | P.T. | 14°28' |  |  | $\Delta = 28^\circ 56'$ |
| 36       |      | 13°48' |  |  | $D = 10^\circ$          |
| +50      |      | 11°18' |  |  | $T = 148.00$            |
| 35       |      | 8°48'  |  |  | $L = 289.33$            |
| +72.25   | P.I. | 28°56' |  |  | $R =$                   |
| +50      |      | 6°18'  |  |  |                         |
| 34       |      | 3°48'  |  |  |                         |
| +50      |      | 1°18'  |  |  |                         |
| 33+24.25 | P.C. | 0°00'  |  |  |                         |

344.51



S.E. Cor.  
Bldg.



| Sta | Pt. | Lt. | Angle | Rt. |
|-----|-----|-----|-------|-----|
|-----|-----|-----|-------|-----|

47+54.70 P.O.T.

|          |      |       |
|----------|------|-------|
| +32.21   | P.T. | 0°54' |
| 43       |      | 0°44' |
| +50      |      | 0°29' |
| +43.08   | P.I. | 1°47' |
| 42       |      | 0°14' |
| 41+53.89 | P.C. | 0°00' |

A-1°47'

D-1°

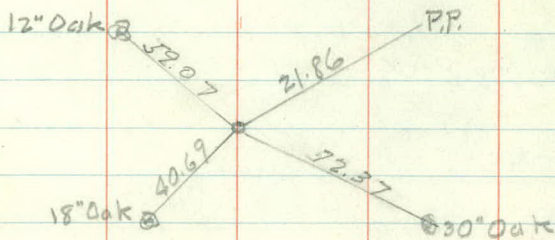
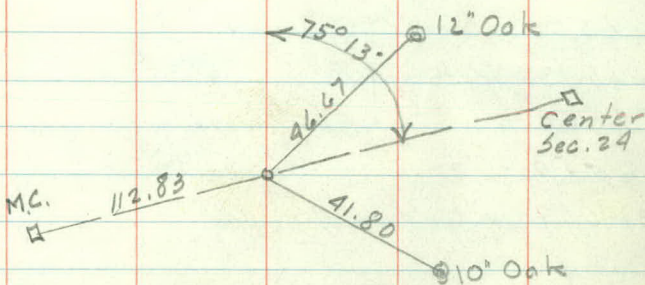
T-89.17

L-178.33

R-

41+60.38

$$\begin{array}{r} 432.69 \\ 80.17 \\ \hline 511.66 \\ 272.80 \\ \hline 784.46 \end{array}$$

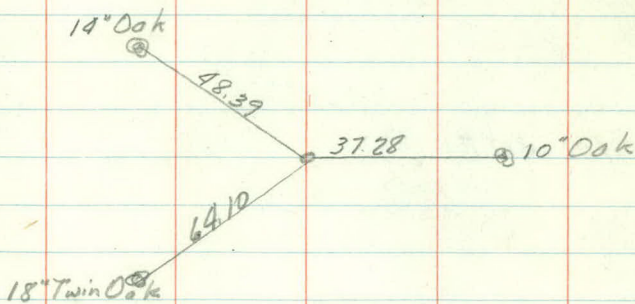
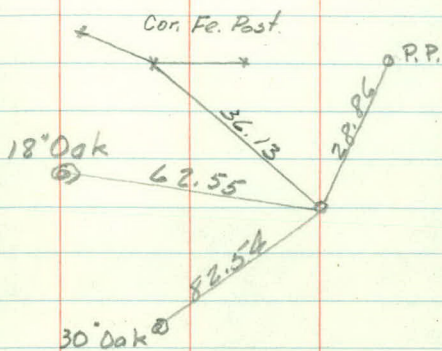


| Sta      | Pt.  | Lt | Angle<br>Rt |                          |
|----------|------|----|-------------|--------------------------|
| +32.61   | P.T. |    | 37°47'      |                          |
| 55       |      |    | 32°04'      | $\Delta = 75^{\circ}33'$ |
| +50      |      |    | 23°19'      | $D = 35^{\circ}$         |
| +45.73   | P.I. |    | 75°33'      | $T = 128.86$             |
| 54       |      |    | 14°34'      | $L = 215.86$             |
| +50      |      |    | 5°44'       | R                        |
| 53+16.75 | P.C. |    | 0°00'       |                          |

50+26.78 P.O.T.

v 272.08

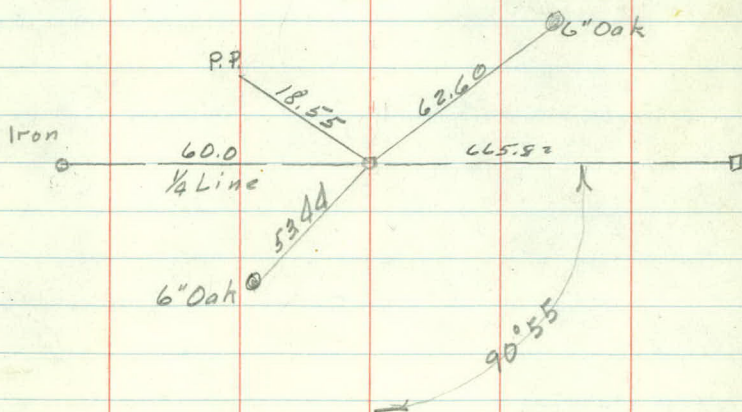
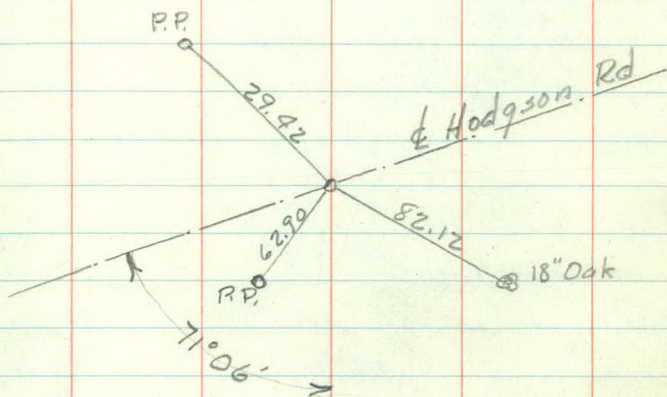


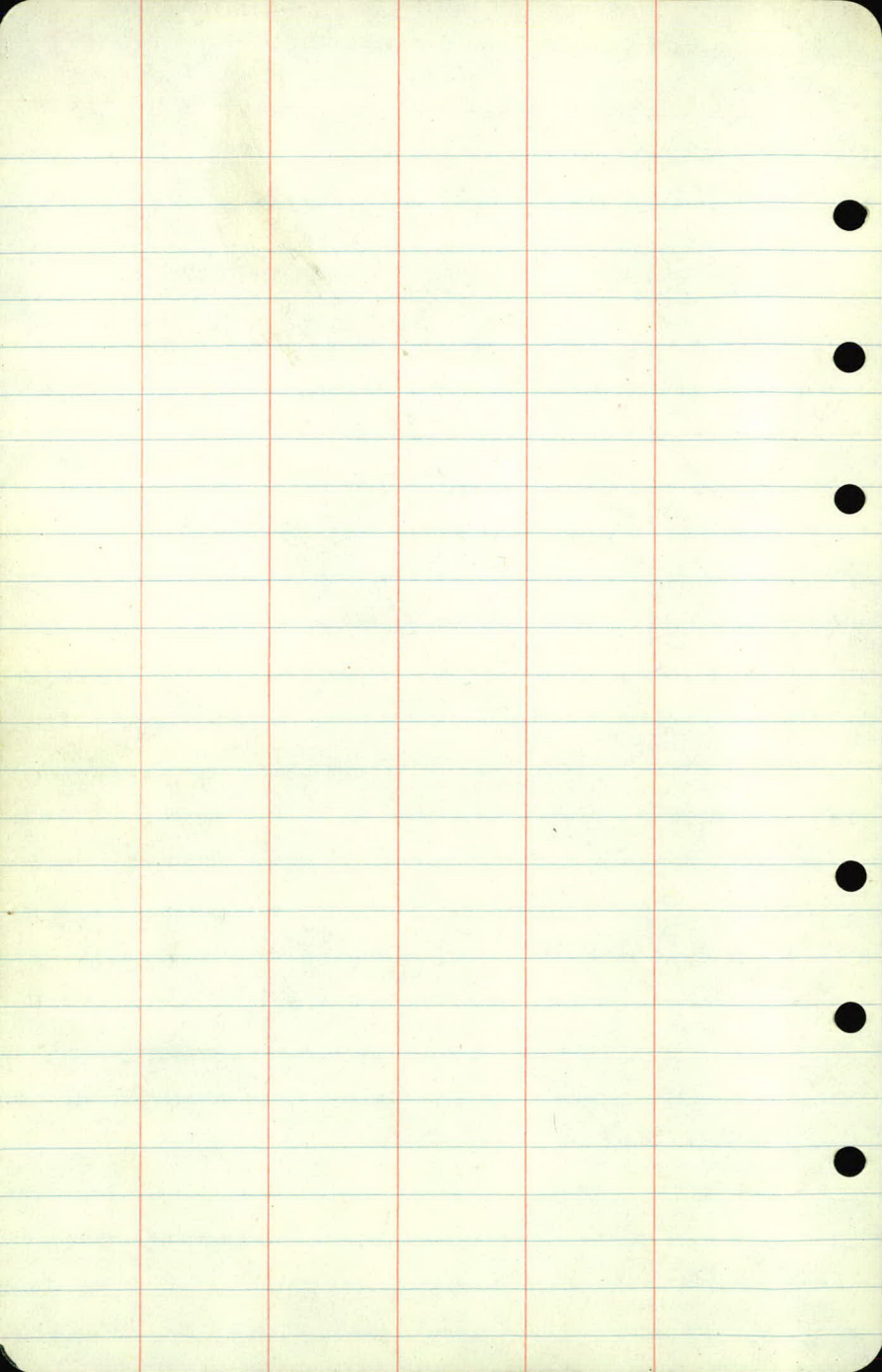


| Sta. | Pt. | Lt. | Angle<br>Rt. |
|------|-----|-----|--------------|
|------|-----|-----|--------------|

65+23.52 P.O.T.

59+91.00 P.O.T.







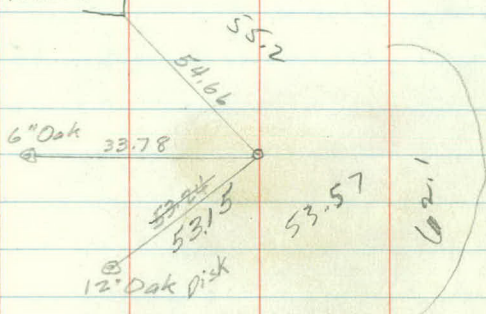
8A.

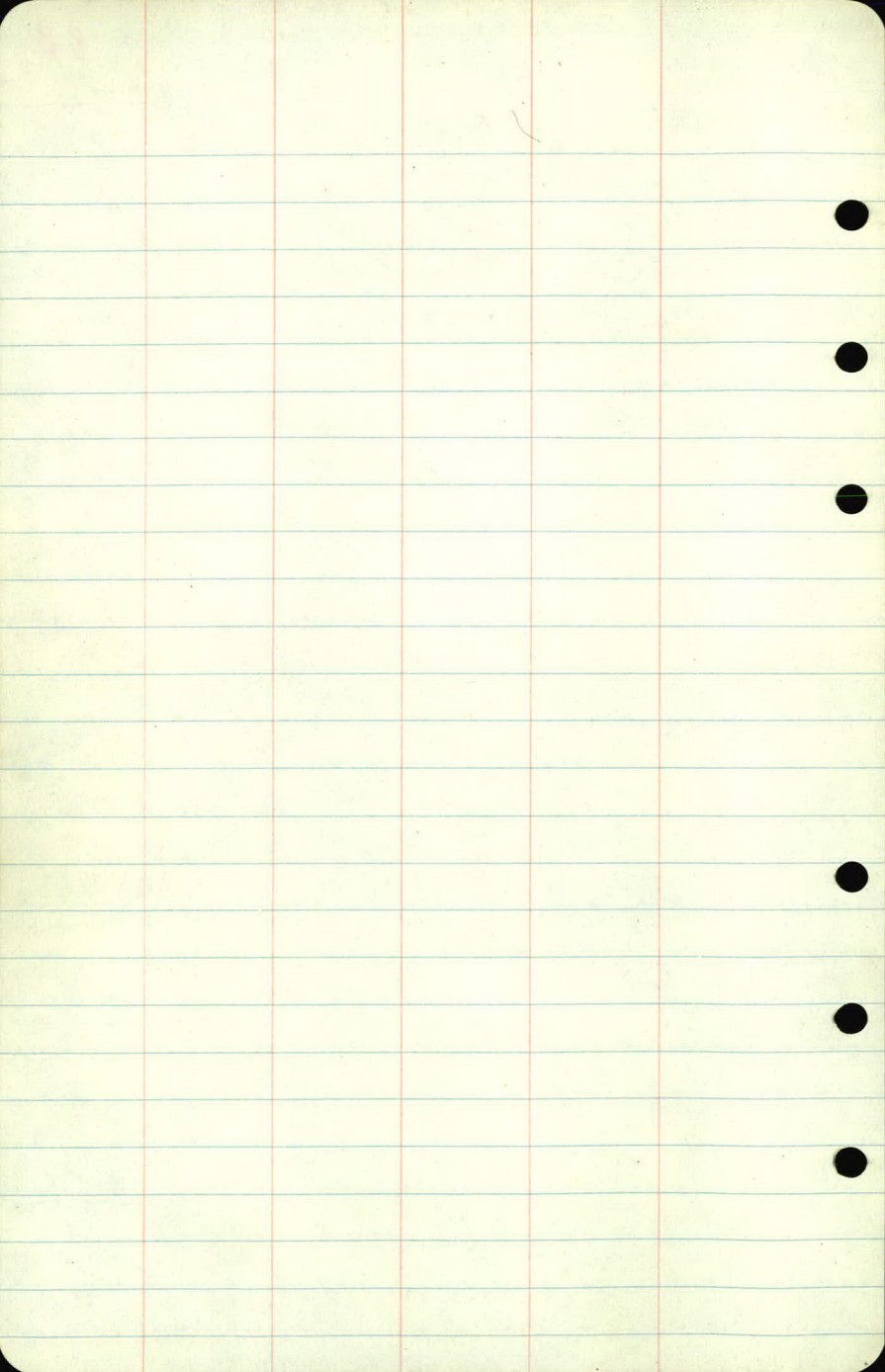
| Sta                                                 | Pt   | Lt      | Δ                          | Rt |
|-----------------------------------------------------|------|---------|----------------------------|----|
| <del>+56.35</del><br><del>+55.80</del>              | P.T. | 3° 34'  |                            |    |
| +50                                                 |      | 3° 30'  |                            |    |
| 41                                                  |      | 3° 00'  | Δ = 7° 08'                 |    |
| +50                                                 |      | 2° 30'  | D = 2°                     |    |
| 40                                                  |      | 2° 00'  | T = 178.57 ✓               |    |
| <del>39 + 78.25</del> ✓<br><del>39 + 77.72</del>    | P.I. | 7° 08'  | L = 356.67 ✓               |    |
| +50                                                 |      | 1° 30'  | R = 2864.93 ✓              |    |
| 39                                                  |      | 1° 00'  |                            |    |
| 38 + 50                                             |      | 0° 30'  |                            |    |
| <del>37 + 99.68</del> ✓<br><del>37 + 99.13</del>    | P.C. | 0° 00'  |                            |    |
| <del>+1041</del><br><del>+10.77</del> ✓             | P.T. | 16° 51' |                            |    |
| 37                                                  |      | 16° 19' |                            |    |
| +50                                                 |      | 13° 49' |                            |    |
| 36                                                  |      | 11° 19' | Δ = <u>33° 41'</u> 33° 42' |    |
| +50                                                 |      | 8° 49'  | D = 10° 10°                |    |
| 35 + 47.52                                          | P.I. | 33° 42' | T = <u>173.94</u> 173.75 ✓ |    |
| 35                                                  |      | 6° 19'  | L = <u>336.83</u> 337.00 ✓ |    |
| +50                                                 |      | 3° 49'  | R = 573.686 ✓              |    |
| 34                                                  |      | 1° 19'  |                            |    |
| <del>33 + 73.58</del> PC<br><del>33 + 73.77</del> ✓ | P.C. | 0° 00'  |                            |    |

EQUATION

$$\text{Sta. } 41+60.35 \checkmark$$

$$\text{Sta. } 41+59.80 = \text{Sta. } 41+53.89 \text{ P.C.}$$

S.E. Cor  
Tavern

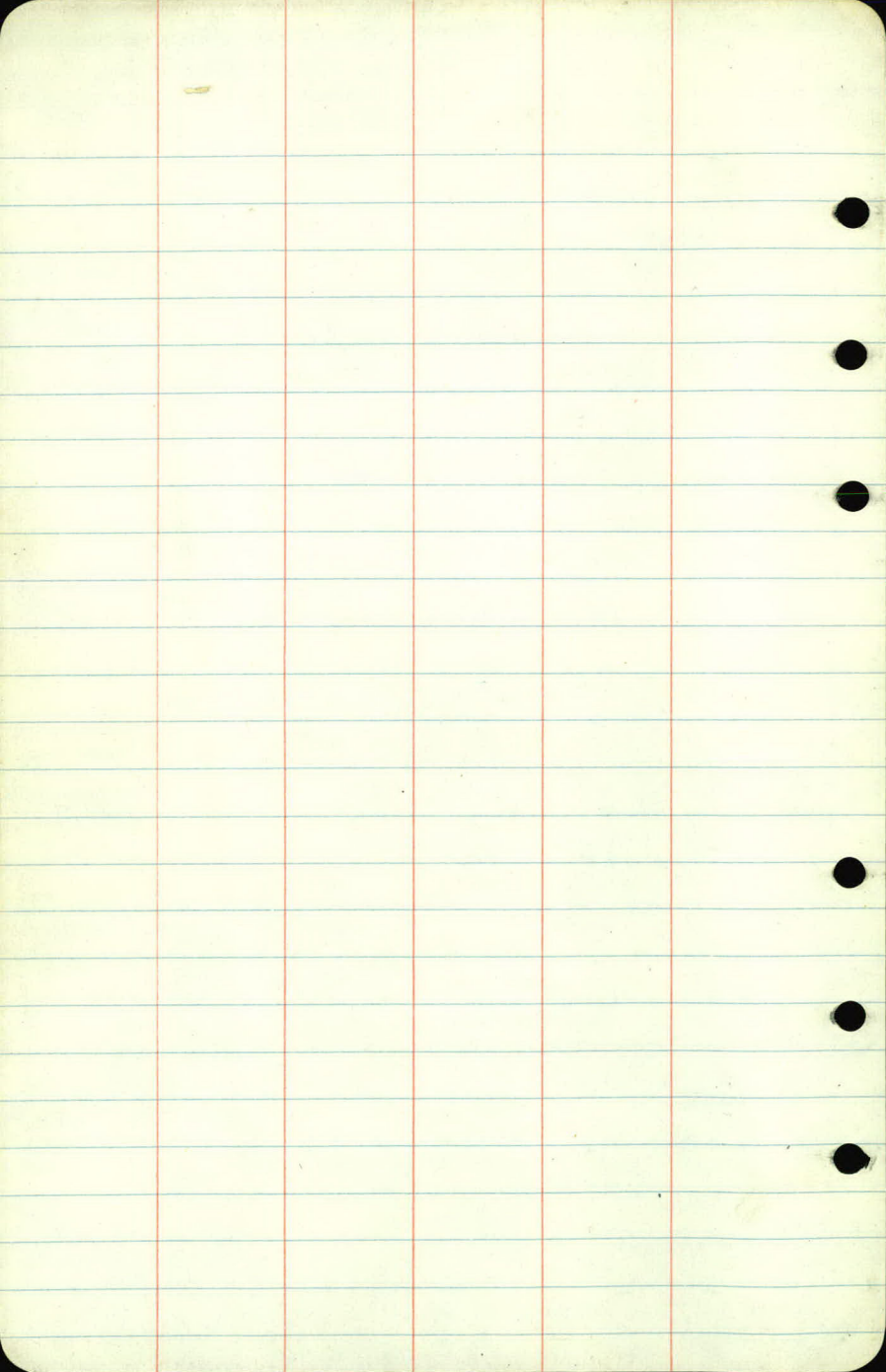




Top Hyd N.W. Cor.  
 East Ave & Minnehaha  
 995.74

1180 N. Lexington  
 Parkway  
 Mrs. Mary G. Reiland

BM 909.01  
 + 7.93  
 H 916.94  
 - 0.54  
 E 916.40  
 918.47  
 H 925.07  
 129  
 E 923.28  
 + 10.05  
 H 933.33  
 B



# Topography

Snail Lake Blvd.

Victoria St. to Hodgson Rd.

16<sup>Rd.</sup> 8'

5

15 6

4

16' 9'

3

13' 10'

2

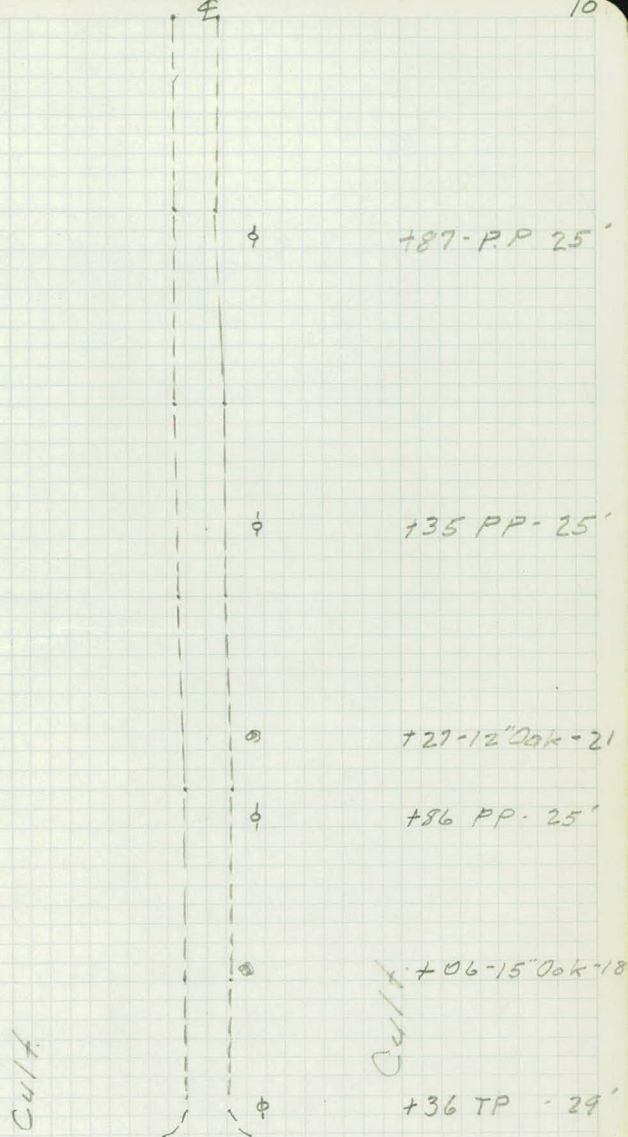
11' 12'

1

11' 11'

0 (00.58)





Victoria Ave.  
(See Co. Rel "F" Notes)

12' 6'

17' 0

12

23' - 6'

+50 28' - 6'

11

32' - 3'

32' 0

10

21' 11'

9

+38 341dr 0.0 -

6' - 29'

+25 20 - 41

8

41' - 22'

+75

19' - 40'

7

4 - 28

0 19' +75

7' 16' +50

19' 11' +25

6

16' 8'

G.R. 13'

G.R. 7 Fe. 14' (11)

+50 G.R. - 18'

+15 G.R. - 23'  
G.R. 3' - 24'

Wooded  
Oak & Willow

Tree Line

+38 G.R. X 56  
+04 PP - 9'  
Fe. - 18'

+50 G.R. 2' & 31'

+28 G.R. - 35'  
+17 G.R. - 50'

Reiland Lane

+90 G.R. 50'  
+85 G.R. 37'

Wooded  
Pot Hole

G.R. 0' - Fe. 25'  
+72 PP - 4'  
+50 Fe. 24'  
+50 G.R. 3'

+50 G.R. 33'

G.R. 22'

+80 Fe. 70'  
+80 End T.L. 70'

Tree Line

+30 A Tree L. 43'  
+00 Fe. 90 A  
Tree Line 42'

Tree Line

+28 PP 30'  
+20 G.R. X 5  
100 Fe. - 42'  
G.R. 30' 6

Uncult

+50 Fe Con 49'

Fe 25' A

Wooded  
Oaks

Tree Line

G.R. 42-21 G.R.

+56 X Fe 10'  
+36 12' O. 23'  
+42 Fe Cor. 11'  
+34 12' O. 4'

+75 PP - 55'  
+75 Beg G.R. - 17'  
+49 Beg G.R. 37'

+17 140-3

Cult

+39 PP - 30'

14' 12'

19

14' 9'

12' 10'

18

12' 11'

11' 10'

17

11' 10'

16

11' 11'

15

10' 12'

14

9' 10'

13

12' - 6'



Fe. 32

12

Fe. 35'

+50 Fe. 31'

+08 Δ Fe. 23

+86 Δ Fe. 21'

+50 Fe 26'

Fe. - 27'

Fe. 26'

Fe. 27

+66 Δ Fe. 26'

+46 Fe Cor. 10'

+46 End. G.R. - 10'

G.R. - 10 - Fe 10

+26 Fe Cor. 12

G.R. 13'

Uncult.

Uncult.

wooded

+40 T.P. - 17'

Uncult.

+12 T.P. - 31'

+96-12" Oak - 30'

+62-12" Oak 28'

+69 P.P. - 18'

+36 T.P. - 18'

+22 End. G.R. - 14'

G.R. 14

Uncult.

+20-18" Oak 24'

+14-12" Oak - 24'

G.R. - 11'

+75-18" Oak - 24'

+82 15" Oak - 24'

+16 Fe Cor - 13'

+02 - P.P. - 14'

G.R. 7' - Fe. 14'

0 - 21'

9' - 28'

26

10' - 30'

9' - 29'

25

4' - 24'

4' 14'

24

12' 11'

23

11' 11'

22

10' 10'

21

13' 12'

20

14' - 12'

G.R. - 1'

G.R. - 22' (13)

Port Hole

+50 Gr. 8'-29'

G.R. 9' - 31'  
+92 - T.P. 37'

+50 G.R. 8'-30'

+39 Beg G.R. 6'  
+39. - G.R. - 31'

+78 T.P. - 35'

+29 End Fe. 14'

+85 - AFe. 45'

Fe 46'

+65 AFe. 42'

Fe - 35  
+90 14' Oak 30

+59 14' Oak 25'  
+40 12' Oak 27'

Fe - 28  
+98 - 15' B.E. 26

Fe 28'

+87 Bag. Row - 18' (15%)  
+74 Rgs to Row Pop  
+66 Ent

+43 Rgs to Ent

Fe 32

Thickly Wooded Oak

Scattered Oaks

Wooded & Brush

Scattered

+18 T.P. 18'

+89 End Fr. Trees  
+73 Stumps - 23'

Fruit Trees - 32'

+74 - T.P. - 18'

+33 - Day Row - 31'  
Fruit trees

+18 Ent

10' 14'

13' 11'

33

14' 11'

32

13' 11'

20' - 2'

31

31' - 8'

47' - 23'

30

66' - 37'

67' - 46'

29

61' - 39'

49' - 28'

28

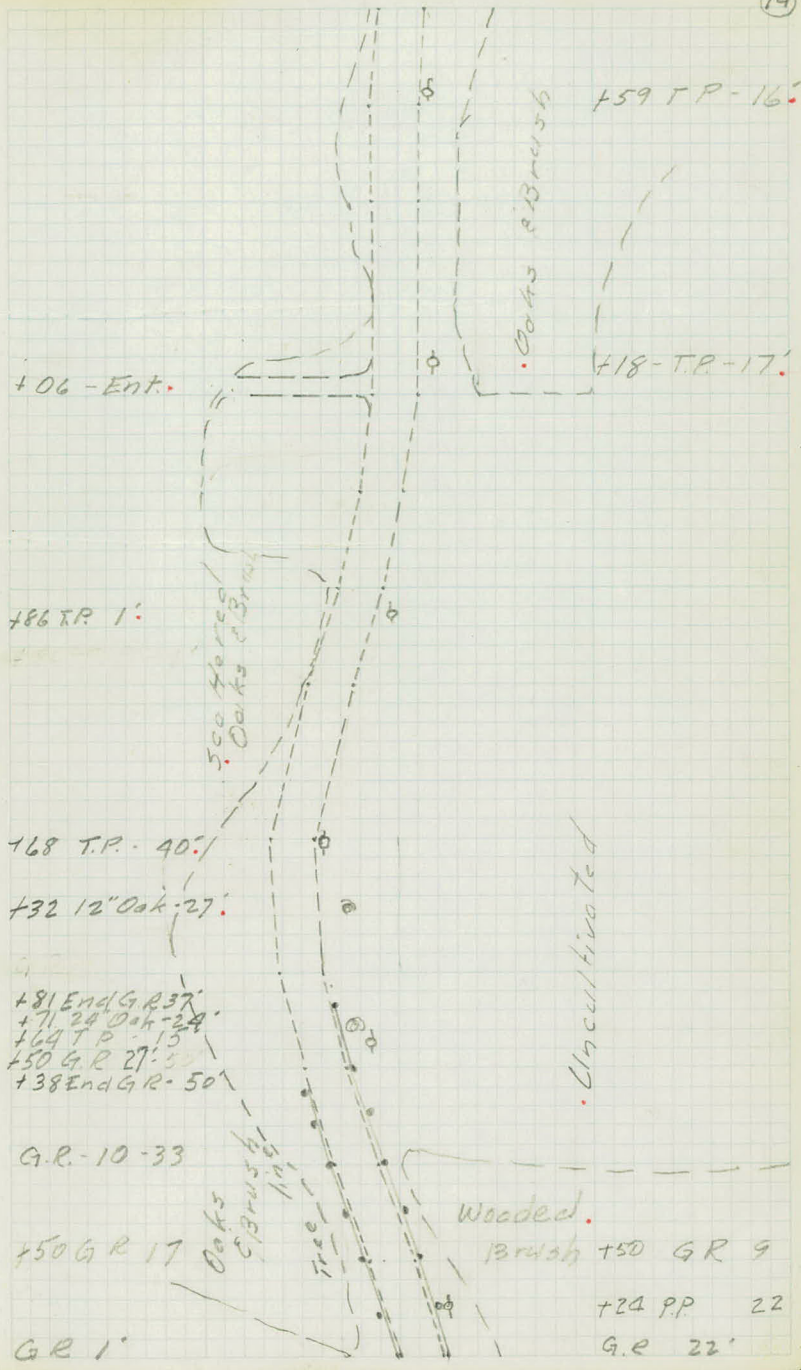
32 - 11

16' 8'

27

0 21'





13' 15'

40

12' 15'

16' 15'

39

17' 11'

38

13' - 13' +537 NW Cr. H. 68.2  
 ON Tan. +27.6 SW Cr. H. 72.9  
 +27.6 P. To S.S. Hat. S.F.

0 - 23'

18.5  
 18.5

Sta 38+00 SW Cr. H.  
 Ho 200' Ht

+50 - 22 - 42

+31 W End - 12' x 46' C. M. - 20'  
 +23 Rgc - 12' x 46'

37

32' 60'

+33 - 45 - 63'

36

37' - 57'

+95 - Fe Ends 68'

22' - 44'

35

4' 29'

6' 21'

34

10' 14'

+99 Cor Bldg 41.

+66-20 Oak-15.

+26 Conc Walk-17.

+02-18 Oak-15.

+02 Cor Bldg 47.

+51 Cor. Ice Ho 73.

79.

+00 T.P. 18. 15.

+89 Cor Ho 82.

+65-4 Walk-28.

Rge Tie Walk-46.

+58 Cor Ho-90.

+41 Cor Ho-94.

+26 Cor Ho-65.

+11 Cor Ho 47.

+92 Cor Ho-103.

+87 T.P. 18.

+83 Cor Ho-103.

+62 Beg Wall-35.

25.

+90-17-G Pole.

+55 Ent.

+30 T.P. 25.

+21 End G.R. 18.

G.R. 23.

+99 End G.R. 1.

+87 24 Oak 2.

+50 G.R. 21-43.

+40 End Fe. 50.

G.R. 37-61.

+87 T.P. 69.

+87 G.R. 43-63.

+33 G.R. 44-64.

G.R. 36-58.

+95 T.P. 63.

+94 Beg G.R. 30.

+83 Ent.

+50 G.R. 45.

G.R. 30.

+82 G.R. 27.

+72 T.P. 29.

Snail Lake

Scattered Oaks - Poplars

G. Brush

Tree lined

Scattered Oaks - Poplars

Picnic Grounds

Uncultivated

10' 10'

47

11' - 9'

46

9 10'

45

9' - 10'

44

11 11

43

12' 11'

42

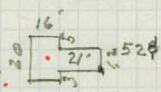
11' - 12'

41

13 - 13

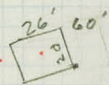


+70 PP-25'  
+57 Cor. Ho. 99.

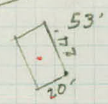


+92 End G.R. 11'

+50 Cor. Ho. 54.



+06 Cor. Ho. 45.  
G.R. 10'



+86 PP-16'

+50 Cor. Ho. 37.

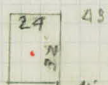


G.R. 10'

+44 Bay G.R. 11'

Lake  
Joa Herod Oak  
Grass

+47 12' Oak 12'  
+33 Drive.  
+16 Rye tie Ent.



+72 Ent.

+48 PP-15.

+82 End G.R. 9'

G.R. 11'

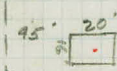
+86 PP-16'

G.R. 11'

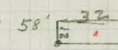
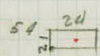
+82 Bay G.R. 10'

+23 PP-15.

End Yard



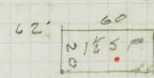
+37 Cor. Ho. 45.  
+25 Ent.



+63 Cor. Ho. 54.  
+58 PP-14'.  
+40 Cor. Ho. 60.

+12 Cor. Ho. 62'.

+89 Ent.



+13 Cor. Ho. 66.

+21 Ent.

+10 End Conc. 46'.

9 10

30'-8'  
+ 25'-4' - 14'  
32'-9'

54

17' 4'

+ 17 11 - 9'

53

10' 12

52

10'-12'

51

12-12

50

11'-10'

49

10' 10'

48

+99-Fe Cor. 37.  
+96-Fe Cor. 22.  
+94 Bay G.R. 16.

+50 Fe 57.  
+33 Fe x 4.  
+25 Ent.  
+25 Fe Δ 4'.

Fe - 2'.  
+92 Rgc Tie Fe.  
+73 Fe<sup>A</sup> Cor 35.

+17 Fe 15'.

+50 Fe 24.  
+46 Ent.  
+25-18 Oak 16.  
Fe 15'.  
+82-24 Oak 16.

Fe - 19'.

+93 Rgc Tie Fe.  
+86 Fe Cor. 25'.

+48 Ent.

+59 Ent.  
+46 Cor. Ho. 42.  
+30 Ent.



Fe 24' (17)

+67-24 Cor. 8.  
+53-2 Pop 3.  
+50 Fe 11.

+89 Fe x 4.

+42 PP 13'.

+17 Fe 16.

+50 Fe 13.

Fe 16'.  
+93 PP 14'.

Fe - 17'.

+47 PP 15'.

+99 Ec Cor. 23'.  
+93 Rgc Tie Fe.

+99 PP 15'.

7' 15"

61

7 12

60

7' 12'

59

7' - 14'

58

8' - 15'

57

7 - 13'

56

18' +25-24' x 52' C.M.

34'  
1' x 3' Hcd wall.

6' - 13'

7' - 12'

+33

55

9 - 10



Fe. 30'.

Fe 42' (18)

+41 P.P. - 17'.

Cult.

+81 Beg. Fe. 32'.

Fe 48'.

+27 Ent.

Yard

+92 P.P. - 19'.

+91 End x Fe. 32'.

Fe. 38'.

Heavily  
wooded.

Thickly wooded

Fe - 36'.

+60 P.P. - 20'.

+60 End Fruit  
Trees. 25'.

Fe 40'.

+87 End G.R. 15'.

+97 End G.R. - 7'.

+60 Beg. Fruit Trees 25'.  
+56 Beg. Fe. 8'.

+15 P.P. - 21'.  
G.R. - 14'.

+50 Beg. Fe - 40'.

3' Ditch.

3' Ditch.

End Orch + 100'.  
G.R. 7'.

+20 Fe. Cor. - 25'.

G.R. - 14 - Fe = 25'.

+77 Fe = G.R.  
+69 A Fe - 16'.  
+68 P.P. - 21'.

Orchard.

Wooded

+33 G.R. 8'.  
+33 Fe. 18'.

+49 Beg G.R. - 14'.  
+33 Fe. - 25'.

Begin Orchard.

Fe - 24'.

67

66

65

64

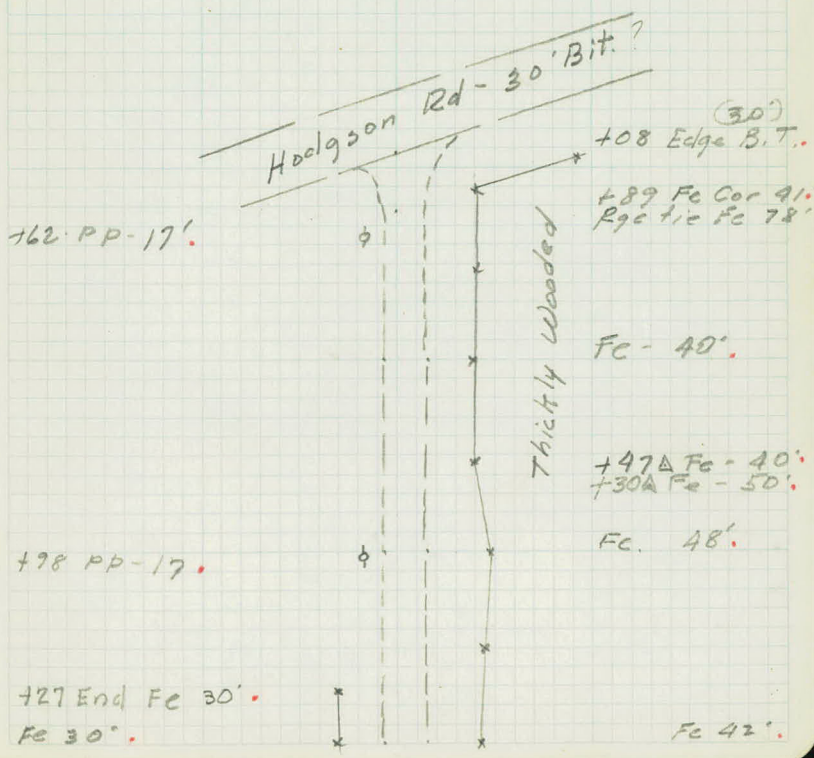
8° 16'

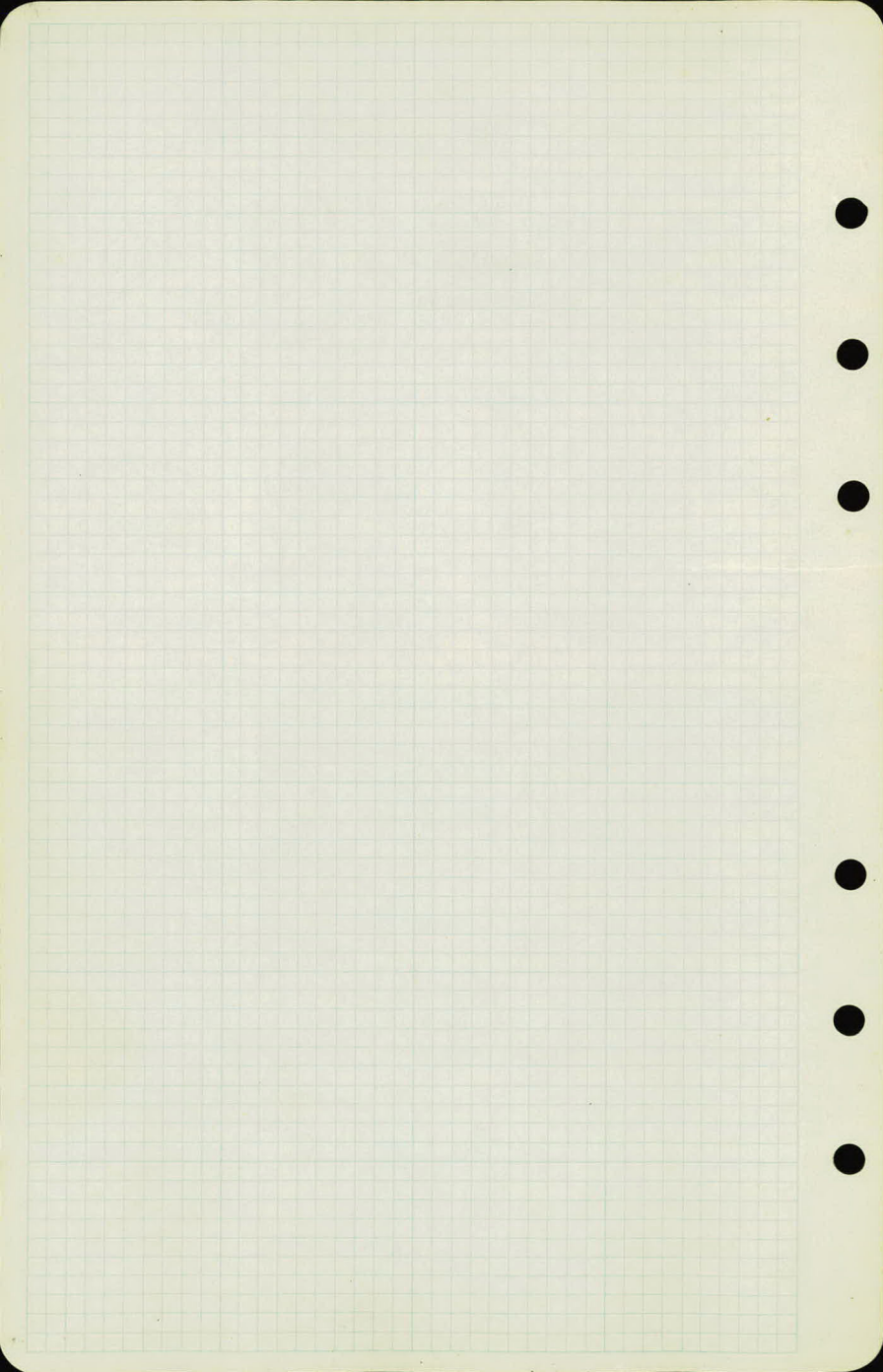
63

7° 15'

62

7° 15'







Topography  
Reiland Lane  
Snail Lake Blvd. to 500' N

5

5' 5'

4

5' 6'

3

5' 5'

2

5' 5'

1

15'

24" x 32" C.M. (426)

17'

6' 6'

0

Fe 17'

Fe 17'

+73 P.P. - 14'

Fe 18'

+73 P.P. - 14'

Fe 18'

+72 End G.R. 9'

+62 Δ Fe 15'

+19 Fe Cor. 15'

Fe Δ 45' G.R. 6

+80 Δ Fe. 83'

+74 P.P. - 13'

+49 G.R. 06'

+33 G.R. 15'

+25 G.R. 33'

Wooded

Wooded - Oaks - Brush

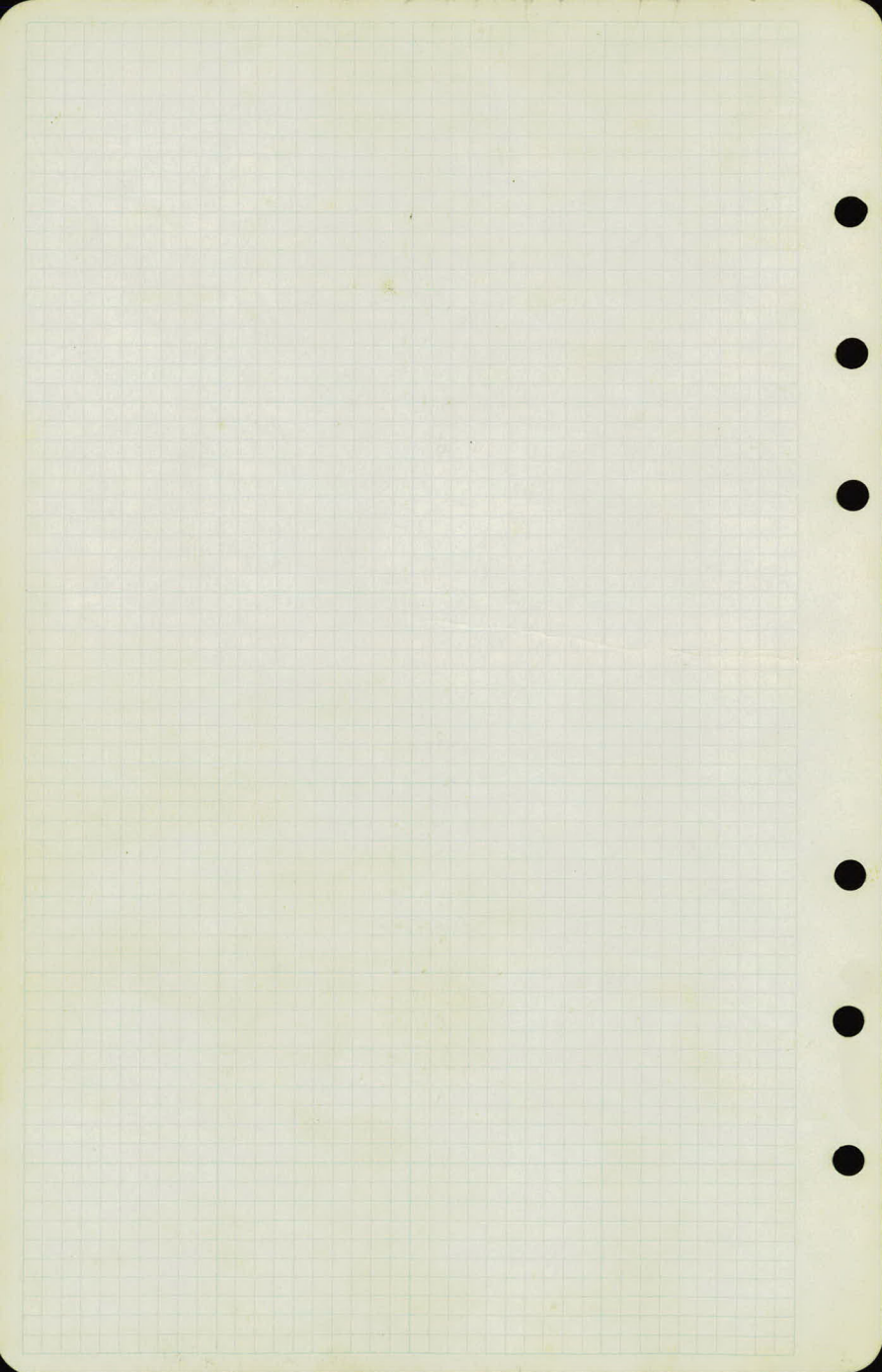
+79 End G.R. 9'

G.R. 6

+54 G.R. - 10'

+43 G.R. - 27'







Bench Levels

Snail Lake Blvd.

| Sta. | +     | -      | Elev.  |
|------|-------|--------|--------|
| B.M. | 1.82  | 982.77 | 980.95 |
|      | 1.86  | 974.32 | 972.46 |
|      | 0.64  | 962.09 | 961.45 |
|      | 0.77  | 951.32 | 950.55 |
| B.M. | 11.74 | 939.58 | 939.58 |
|      | 0.31  | 938.52 | 938.21 |
|      | 0.89  | 927.15 | 926.26 |
|      | 0.07  | 914.02 | 913.95 |
| B.M. | 5.01  | 909.01 | 909.01 |
|      | 10.44 | 923.86 | 913.42 |
|      | 10.68 | 933.94 | 923.26 |
| B.M. | 2.06  | 931.88 | 931.88 |
|      | 0.76  | 928.40 | 927.64 |
|      | 0.76  | 916.88 | 916.12 |
|      | 3.52  | 906.93 | 903.41 |
| B.M. | 2.38  | 904.66 | 902.28 |
|      | 3.38  | 897.80 | 894.42 |
|      | 7.16  | 899.90 | 892.74 |
| B.M. | 3.86  | 899.37 | 895.51 |
|      | 8.19  | 902.59 | 894.40 |
|      | 4.80  | 904.66 | 899.86 |
|      | 8.64  | 907.87 | 899.23 |
| B.M. | 9.20  | 916.82 | 907.62 |
|      | 5.28  | 921.64 | 916.36 |
|      | 0.11  | 915.32 | 915.21 |

Top Bolt Spike. Victoria & Ensl Lake Blvd.

Spike in first G.R. Post 17' Rt. Sta. 17+74

R.R. Spike 15" Oak 30' Rt. Sta. 14+20

Spike in 24" Pop 50' Lt. 21+15

Spike 12" Oak 50' Rt. Sta. 27+50

Spike 8" Pop 30' Rt. Sta. 34+95

Spike 8" Oak 33' Lt. Sta. 47+60

Pf

+

$\pi$

-

Elev.

915.32

8.18

921.34

2.16

913.16

8.43

928.84

0.93

920.41

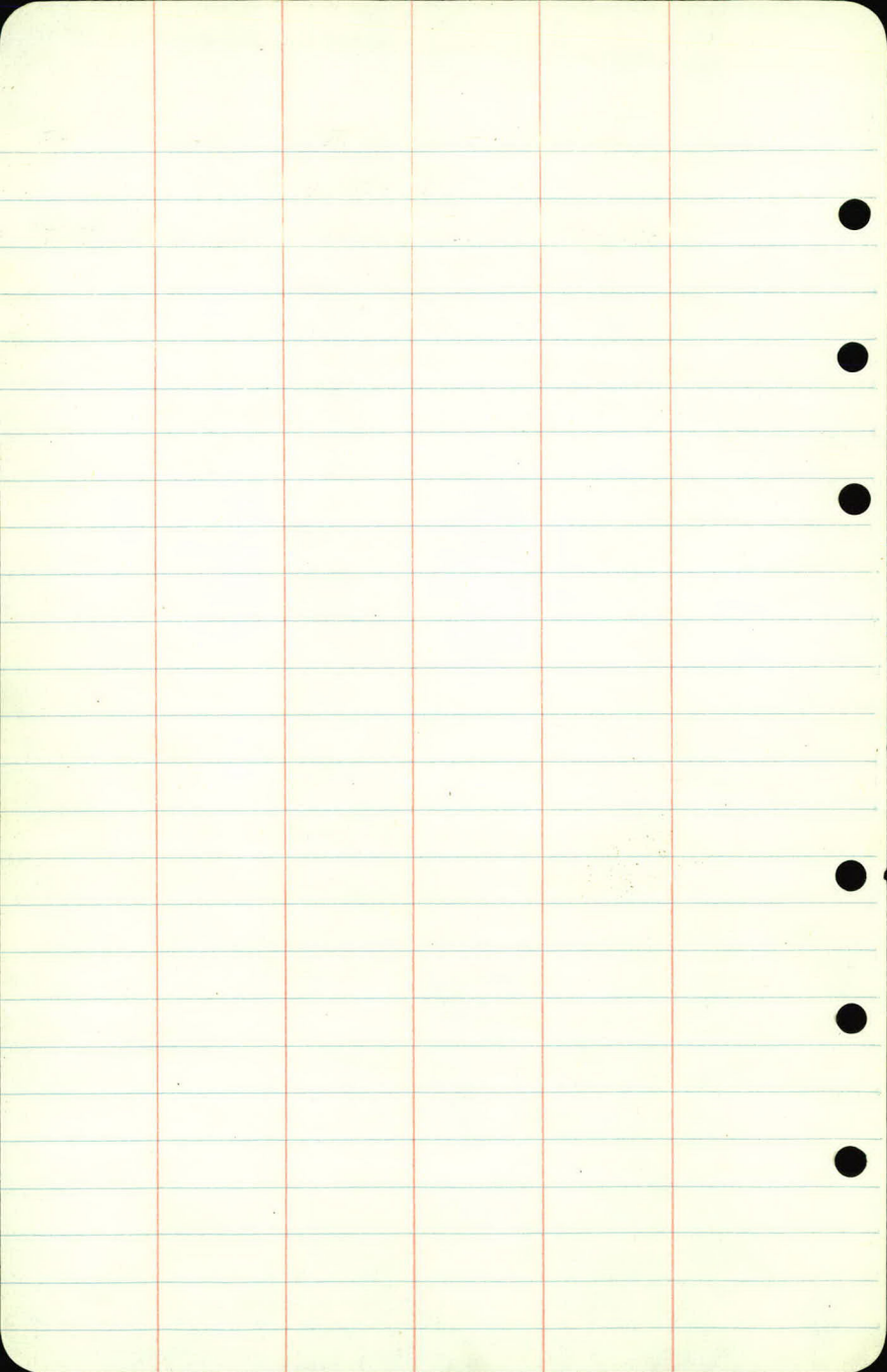
B. M.

3.39

925.45



Spike in P.P. N.E. Cor. Snail Lake Blud & Hodgson



Snail Lake Blvd.

Cross Sections  
first  $\frac{1}{2}$  Mile

| Sta. | +             | ⌒      | -    | Elev.  |
|------|---------------|--------|------|--------|
| B.M. | 1.62          | 982.57 |      | 980.95 |
| 0+00 | ↳ Victoria    |        | 1.6  | 81.0   |
| +18  | Shdr          |        | 2.2  | 80.4   |
| +23  | Toe Shldr     |        | 2.4  | 80.2   |
| +33  | Toe Backslope |        | 2.8  | 79.8   |
| +36  |               |        | 2.9  | 79.7   |
| +50  |               |        | 3.6  | 79.0   |
| 1    |               |        | 5.8  | 76.8   |
| +50  |               |        | 7.8  | 74.8   |
| 2    |               |        | 10.2 | 72.4   |
| +25  |               |        | 11.6 | 71.0   |
| +65  |               |        | 13.6 | 69.0   |
| 3    |               |        |      | 67.2   |



4

Top Spike Sta. 84+95 (Co. Rd. "F" Notes)

$\frac{1.3}{50}$   $\frac{1.6}{24}$   $\frac{1.6}{25}$   $\frac{1.4}{50}$

$\frac{2.3}{50}$   $\frac{2.4}{24}$   $\frac{2.1}{22}$   $\frac{1.7}{26}$   $\frac{1.7}{50}$

$\frac{4.0}{50}$   $\frac{3.7}{22}$   $\frac{2.7}{17}$   $\frac{2.5}{24}$   $\frac{3.4}{20}$   $\frac{3.6}{25}$   $\frac{3.6}{50}$

$\frac{4.0}{50}$   $\frac{4.0}{18}$   $\frac{3.1}{14}$   $\frac{3.0}{13}$   $\frac{4.2}{18}$   $\frac{3.8}{50}$

$\frac{3.7}{50}$   $\frac{4.0}{30}$   $\frac{4.0}{20}$   $\frac{3.4}{14}$   $\frac{3.1}{13}$   $\frac{4.2}{17}$   $\frac{4.2}{21}$   $\frac{3.5}{23}$   $\frac{3.1}{37}$   $\frac{2.3}{50}$

$\frac{4.8}{50}$   $\frac{4.5}{27}$   $\frac{5.1}{23}$   $\frac{4.0}{20}$   $\frac{3.8}{9}$   $\frac{4.7}{13}$   $\frac{4.2}{14}$   $\frac{3.7}{16}$   $\frac{2.9}{33}$   $\frac{2.9}{50}$

$\frac{5.7}{50}$   $\frac{5.7}{31}$   $\frac{5.0}{25}$   $\frac{5.8}{16}$   $\frac{6.3}{15}$   $\frac{6.1}{12}$   $\frac{6.2}{58}$   $\frac{6.3}{10}$   $\frac{5.0}{15}$   $\frac{4.5}{16}$   $\frac{3.9}{32}$   $\frac{3.9}{50}$

$\frac{6.6}{50}$   $\frac{6.4}{29}$   $\frac{6.6}{21}$   $\frac{8.2}{17}$   $\frac{8.3}{13}$   $\frac{8.5}{14}$   $\frac{5.8}{17}$   $\frac{4.9}{33}$   $\frac{3.8}{50}$

$\frac{7.7}{50}$   $\frac{7.6}{32}$   $\frac{7.5}{21}$   $\frac{10.7}{15}$   $\frac{11.2}{15}$   $\frac{6.3}{18}$   $\frac{5.6}{32}$   $\frac{4.7}{50}$

$\frac{8.0}{50}$   $\frac{8.1}{34}$   $\frac{8.3}{21}$   $\frac{12.1}{15}$   $\frac{12.2}{14}$   $\frac{6.6}{20}$   $\frac{6.4}{31}$   $\frac{5.2}{50}$

$\frac{8.0}{50}$   $\frac{8.3}{25}$   $\frac{13.5}{17}$   $\frac{14.4}{16}$   $\frac{14.1}{14}$   $\frac{7.8}{19}$   $\frac{6.8}{11}$   $\frac{6.8}{50}$

$\frac{8.2}{50}$   $\frac{8.6}{30}$   $\frac{10.4}{19}$   $\frac{9.9}{37}$   $\frac{9.8}{50}$   $\frac{9.5}{50}$

4

| Sta. | +     | $\pi$  | -     | Elev.  |
|------|-------|--------|-------|--------|
|      |       | 982.57 |       |        |
| 3+33 |       |        |       | 65.5   |
| +68  |       |        |       | 638    |
| 4    |       |        |       | 621    |
| +32  |       |        |       | 60.2   |
| +80  |       |        |       | 57.2   |
| 5    |       |        |       | 55.9   |
| +40  |       |        |       | 53.3   |
| +72  | P.C.  |        |       | 51.1   |
| T.P. | 0.36  | 970.92 | 12.01 | 970.56 |
| 6    |       |        |       | 49.2   |
| +50  |       |        |       | 45.9   |
| T.P. | 10.66 | 969.14 | 12.44 | 958.48 |
| 3    |       |        | 1.9   | 67.2   |
| +33  |       |        | 3.6   | 65.5   |

$$\begin{array}{r} 5.6 \\ 75 \end{array} \quad \begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 8.2 \\ 30 \end{array} \quad (-17.1) \quad \begin{array}{r} 10.5 \\ 21 \end{array} \quad \begin{array}{r} 11.1 \\ 50 \end{array}$$

$$\begin{array}{r} 2.7 \\ 100 \end{array} \quad \begin{array}{r} 4.2 \\ 75 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array} \quad \begin{array}{r} 5.8 \\ 38 \end{array} \quad (-18.8) \quad \begin{array}{r} 10.9 \\ 25 \end{array} \quad \begin{array}{r} 11.6 \\ 43 \end{array} \quad \begin{array}{r} 11.8 \\ 50 \end{array} \quad \begin{array}{r} 12.3 \\ 75 \end{array}$$

$$\begin{array}{r} 3.7 \\ 100 \end{array} \quad \begin{array}{r} 3.9 \\ 75 \end{array} \quad \begin{array}{r} 3.4 \\ 50 \end{array} \quad \begin{array}{r} 3.4 \\ 43 \end{array} \quad (-20.5) \quad \begin{array}{r} 9.5 \\ 28 \end{array} \quad \begin{array}{r} 10.7 \\ 50 \end{array} \quad \begin{array}{r} 11.6 \\ 75 \end{array} \quad \begin{array}{r} 12.0 \\ 100 \end{array}$$

$$\begin{array}{r} 4.9 \\ 100 \end{array} \quad \begin{array}{r} 4.3 \\ 75 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array} \quad \begin{array}{r} 3.4 \\ 42 \end{array} \quad (-22.4) \quad \begin{array}{r} 6.5 \\ 33 \end{array} \quad \begin{array}{r} 7.8 \\ 50 \end{array} \quad \begin{array}{r} 9.8 \\ 75 \end{array} \quad \begin{array}{r} 10.2 \\ 100 \end{array}$$

$$\begin{array}{r} 7.5 \\ 100 \end{array} \quad \begin{array}{r} 6.7 \\ 75 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array} \quad \begin{array}{r} 6.2 \\ 45 \end{array} \quad (-25.4) \quad \begin{array}{r} 4.4 \\ 36 \end{array} \quad \begin{array}{r} 4.2 \\ 50 \end{array} \quad \begin{array}{r} 4.3 \\ 75 \end{array} \quad \begin{array}{r} 4.5 \\ 100 \end{array}$$

$$\begin{array}{r} 9.4 \\ 100 \end{array} \quad \begin{array}{r} 8.5 \\ 75 \end{array} \quad \begin{array}{r} 7.5 \\ 50 \end{array} \quad \begin{array}{r} 7.5 \\ 45 \end{array} \quad (-26.7) \quad \begin{array}{r} 4.6 \\ 36 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array} \quad \begin{array}{r} 3.9 \\ 75 \end{array} \quad \begin{array}{r} 3.7 \\ 100 \end{array}$$

$$\begin{array}{r} 14.3 \\ 100 \end{array} \quad \begin{array}{r} 12.8 \\ 75 \end{array} \quad \begin{array}{r} 11.2 \\ 50 \end{array} \quad \begin{array}{r} 11.2 \\ 44 \end{array} \quad (-29.3) \quad \begin{array}{r} 8.5 \\ 37 \end{array} \quad \begin{array}{r} 8.3 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 75 \end{array} \quad \begin{array}{r} 7.2 \\ 100 \end{array}$$

$$\begin{array}{r} 17.8 \\ 100 \end{array} \quad \begin{array}{r} 16.5 \\ 75 \end{array} \quad \begin{array}{r} 14.7 \\ 50 \end{array} \quad \begin{array}{r} 14.7 \\ 43 \end{array} \quad (-31.5) \quad \begin{array}{r} 15.0 \\ 34 \end{array} \quad \begin{array}{r} 15.1 \\ 50 \end{array} \quad \begin{array}{r} 14.2 \\ 75 \end{array} \quad \begin{array}{r} 13.2 \\ 100 \end{array}$$

$$\begin{array}{r} 8.5 \\ 100 \end{array} \quad \begin{array}{r} 7.2 \\ 75 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array} \quad \begin{array}{r} 6.2 \\ 38 \end{array} \quad (-21.7) \quad \begin{array}{r} 10.6 \\ 29 \end{array} \quad \begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 11.7 \\ 75 \end{array} \quad \begin{array}{r} 12.5 \\ 100 \end{array}$$

$$\begin{array}{r} 13.5 \\ 100 \end{array} \quad \begin{array}{r} 12.9 \\ 75 \end{array} \quad \begin{array}{r} 13.1 \\ 50 \end{array} \quad \begin{array}{r} 13.6 \\ 27 \end{array} \quad (-25.0)$$

$$\begin{array}{r} 2.4 \\ 17 \end{array} \quad \begin{array}{r} 2.1 \\ 11 \end{array} \quad 1.9 \quad \begin{array}{r} 2.2 \\ 7 \end{array} \quad \begin{array}{r} 2.4 \\ 13 \end{array}$$

$$\begin{array}{r} 4.8 \\ 19 \end{array} \quad \begin{array}{r} 3.7 \\ 9 \end{array} \quad 3.6 \quad \begin{array}{r} 3.9 \\ 7 \end{array} \quad \begin{array}{r} 4.0 \\ 14 \end{array}$$

Sta + K - Elev.

969.14

3+68 5.3 63.8

4 7.0 62.1

+32 8.9 60.2

+80 11.9 57.2

T.P. 2.68 959.08 12.74 956.40

5 3.2 55.9

+40 5.8 53.3

+72 P.C. 8.0 51.1

6 9.9 49.2

+50 13.2 45.9

T.P. 2.70 948.89 12.89 946.19

+73 P.T. 4.6 44.3

B.M. 7.61 947.19 9.30 939.59 (939.58)

7 6.2 41.0

+37 7.6 39.6

|     |     |     |     |   |     |     |
|-----|-----|-----|-----|---|-----|-----|
| 5.2 | 5.4 | 6.1 | 5.3 |   | 5.6 | 5.9 |
| 25  | 19  | 13  | 9   | 5 | 3   | 8   |

|     |     |     |     |   |     |     |     |
|-----|-----|-----|-----|---|-----|-----|-----|
| 5.8 | 7.2 | 7.7 | 7.1 |   | 7.4 | 7.8 | 5.4 |
| 24  | 18  | 12  | 9   | 7 | 0   | 9   | 13  |

|     |      |     |     |     |     |     |
|-----|------|-----|-----|-----|-----|-----|
| 7.5 | 10.0 | 9.0 |     | 9.2 | 9.6 | 7.2 |
| 23  | 12   | 9   | 8.9 | 8   | 11  | 20  |

|      |      |      |      |    |      |      |      |
|------|------|------|------|----|------|------|------|
| 10.5 | 11.7 | 14.0 | 12.0 |    | 12.2 | 12.4 | 11.1 |
| 23   | 18   | 16   | 14   | 11 | 11.9 | 7    | 10   |

|     |     |     |     |     |    |     |     |     |     |
|-----|-----|-----|-----|-----|----|-----|-----|-----|-----|
| 1.5 | 3.2 | 5.7 | 3.8 | 3.2 |    | 3.5 | 4.3 | 3.0 | 0.8 |
| 25  | 19  | 18  | 16  | 15  | 11 | 3.2 | 6   | 9   | 12  |

|     |     |     |     |     |    |     |     |     |     |
|-----|-----|-----|-----|-----|----|-----|-----|-----|-----|
| 5.0 | 6.0 | 7.8 | 6.2 | 5.9 |    | 6.1 | 6.4 | 7.1 | 4.6 |
| 26  | 19  | 18  | 16  | 14  | 11 | 5.8 | 6   | 9   | 11  |

|     |     |     |     |     |     |    |     |     |     |
|-----|-----|-----|-----|-----|-----|----|-----|-----|-----|
| 5.3 | 7.1 | 8.6 | 9.6 | 8.4 | 8.2 |    | 8.2 | 8.4 | 8.9 |
| 27  | 22  | 19  | 18  | 16  | 14  | 11 | 8.0 | 5   | 7   |

|     |     |      |      |     |      |      |     |
|-----|-----|------|------|-----|------|------|-----|
| 7.9 | 7.5 | 10.5 | 10.0 |     | 10.1 | 10.5 | 9.0 |
| 25  | 20  | 13   | 10   | 9.9 | 7    | 14   | 15  |

|      |      |      |      |      |   |      |      |      |     |     |     |     |
|------|------|------|------|------|---|------|------|------|-----|-----|-----|-----|
| 11.6 | 13.6 | 14.7 | 13.6 | 13.3 |   | 13.4 | 13.6 | 11.2 | 8.3 | 8.1 | 8.6 | 9.0 |
| 17   | 13   | 11   | 9    | 8    | 5 | 13.2 | 13   | 21   | 22  | 26  | 29  | 37  |

7 + 3.82 + 4.9  
WFB

|     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 4.9 | 3.8 | 4.8 | 4.8 | 3.6 | 3.9 | 4.9 | 6.5 | 5.2 |     | 4.8 | 5.8 | 5.4 | 1.8 | 3.0 | 4.5 |
| 45  | 32  | 28  | 23  | 18  | 11  | 7   | 6.5 | 4   | 4.6 | 17  | 21  | 26  | 29  | 45  | 50  |

Σ + 5.4 + 6.0  
50 75

Spike in first G.R. Post - 17' Rt Sta. 7 + 74

|     |     |     |     |     |     |   |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|-----|-----|-----|-----|-----|
| 1.0 | 0.3 | 0.1 | 1.1 | 4.2 | 4.3 |   | 6.2 | 5.0 | 4.9 | 5.8 | 6.5 | 5.7 | 4.5 | 6.2 |
| 50  | 33  | 18  | 10  | 7   | 3   | 6 | 2   | 1   | 3   | 17  | 29  | 30  | 31  | 34  |

|     |     |     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 4.5 | 5.1 | 7.0 |     | 8.0 | 8.8 | 7.8 | 7.5 | 8.3 | 9.8 | 8.3 | 7.8 | 8.2 |
| 50  | 37  | 13  | 7.6 | 5   | 6.7 | 11  | 21  | 35  | 36  | 38  | 39  | 42  |



| Sta  | +            | T      | -     | Elev    |
|------|--------------|--------|-------|---------|
|      |              | 947.19 |       |         |
| 7+73 |              |        | 11.3  | 35.9'   |
| T.P. | 2.23         | 936.35 | 13.07 | 934.12' |
| 8    |              |        | 4.6   | 31.9'   |
| +23  |              |        | 8.2   | 28.2'   |
| +55  |              |        | 11.0  | 25.4'   |
| 9    |              |        | 11.8  | 24.6'   |
| T.P. | 1.24         | 927.43 | 10.16 | 926.19' |
| +19  |              |        | 0.3   | 27.1'   |
| +73  |              |        | 3.4   | 24.0'   |
| 10   |              |        | 5.5   | 21.9'   |
| +25  | P.C.         |        | 8.1   | 19.3'   |
| T.P. | 2.47         | 917.54 | 12.36 | 915.07' |
| +50  |              |        | 1.0   | 16.5'   |
| +90  | Reiland Lane |        |       | 14.0'   |
| 11   |              |        | 4.1   | 13.4'   |

$\frac{12.4}{50} \frac{12.3}{24} \frac{11.5}{8} \frac{11.3}{11.3} \frac{10.9}{7} \frac{10.4}{14} \frac{10.4}{28} \frac{11.3}{43} \frac{13.8}{49} \frac{13.2}{61} \frac{15.0}{78}$

$\frac{5.4}{50} \frac{5.0}{22} \frac{4.6}{4.6} \frac{3.8}{15} \frac{1.4}{20} \frac{1.6}{31} \frac{1.8}{43} \frac{5.0}{50} \frac{8.2}{51-53} \frac{5.3}{54} \frac{5.5}{68}$

$\frac{8.4}{50} \frac{8.5}{33} \frac{8.2}{82} \frac{7.5}{12} \frac{3.5}{20} \frac{3.2}{31} \frac{3.5}{44} \frac{7.8}{51} \frac{8.3}{55} \frac{11.3}{58} \frac{8.6}{59} \frac{11.0}{77}$

$\frac{13.3}{50} \frac{12.1}{25} \frac{11.0}{11.0} \frac{10.2}{7} \frac{5.7}{15} \frac{5.0}{28} \frac{5.2}{39} \frac{10.7}{50} \frac{11.1}{52} \frac{14.0}{54-55} \frac{11.0}{56} \frac{12.0}{71}$

$\frac{17.7}{50} \frac{15.2}{21} \frac{11.8}{11.8} \frac{8.3}{7} \frac{8.6}{19} \frac{8.6}{31} \frac{8.6}{37} \frac{13.6}{45} \frac{14.9}{52} \frac{17.3}{56-58} \frac{16.7}{59} \frac{17.5}{69}$

$\frac{10.2}{50} \frac{6.7}{14} \frac{5.2}{8} \frac{0.3}{0.3} \frac{0.0}{14} \frac{0.4}{26} \frac{1.8}{34} \frac{9.2}{46} \frac{14.2}{71}$

$\frac{14.5}{50} \frac{12.8}{29} \frac{3.9}{17} \frac{3.6}{15} \frac{3.4}{3.4} \frac{4.6}{14} \frac{5.4}{22} \frac{12.8}{34}$

$\frac{15.8}{50} \frac{14.8}{39} \frac{5.6}{24} \frac{5.8}{18} \frac{5.5}{5.5} \frac{5.8}{6} \frac{7.1}{16} \frac{14.8}{28}$

$\frac{17.5}{65} \frac{16.9}{51} \frac{8.0}{37} \frac{7.9}{22} \frac{7.6}{11} \frac{8.1}{8.1} \frac{8.7}{10} \frac{19.6}{26}$

$\frac{9.3}{69} \frac{7.9}{53} \frac{40.1}{37} \frac{10.1}{25} \frac{10.2}{12} \frac{1.0}{1.0} \frac{1.2}{6} \frac{13.7}{24}$

$\frac{11.4}{100} \frac{9.6}{150} \frac{7.7}{100} \frac{4.0}{50} \frac{2.4}{30} \frac{3.5}{3.5}$

$\frac{17.1}{70} \frac{16.4}{62} \frac{3.2}{39} \frac{3.0}{18} \frac{4.1}{4.1} \frac{5.3}{6} \frac{17.3}{25}$

| Sta.  | t                       | $\pi$   | -     | Elev            |
|-------|-------------------------|---------|-------|-----------------|
|       |                         | 917.54  | 7.2   |                 |
| 11+42 | PT                      |         | 6.2   | 11.3            |
| 12    |                         |         | 8.2   | 09.3            |
| T.P.  | 3.25                    | 913.94  | 6.88  | 910.66          |
| +19   | Sec. thru 15246' - 74-1 |         |       | 09.6            |
| +50   |                         |         | 4.7   | 09.2            |
| +93   |                         |         | 5.1   | 08.8            |
| 13+00 | See page 29             |         |       |                 |
| 13+21 |                         |         |       |                 |
| 13+35 |                         |         | 5.0   | 08.9            |
| +70   |                         |         | 4.8   | 09.1            |
| 14    |                         |         | 4.6   | 09.3            |
| B.M.  |                         |         | 4.89  | 909.02. 909.01. |
| B.M.  | 1.02                    | 940.60. |       | 939.58.         |
| T.P.  | 0.47                    | 928.65. | 12.42 | 928.18.         |
| T.P.  | 0.54                    | 916.20. | 12.99 | 915.66.         |
| T.P.  | 1.03                    | 903.61. | 13.62 | 902.58.         |
| T.P.  | 2.35                    | 897.74. | 8.22  | 895.39.         |
| 9+73  |                         |         |       | 924.0           |
| 10    |                         |         |       | 921.9           |

45

76 15 CM

31

(29)

19.3 15.4 5.0 5.0 6.9 19.8  
61 50 33 17 6.2 3 23

22.8 22.3 7.3 7.0 7.0 19.3  
60 50 24 13 3 8.2 20

Bot 12+50 RL

(20.3) 18.8 17.5 4.3 3.9 12.5 15.6  
45 50 42 21 11 4.3 14 20

19.8 18.8 5.0 4.7 4.9 12.9  
50 45 17 9 4.7 4 17

17.9 15.8 13.0 5.4 5.1 5.2 12.6 13.9  
50 34 23 14 4 5.1 6 20 50

13.6 11.7 10.6 5.3 5.3 10.9 9.9 9.3  
50 26 21 11 50 10 21-24 30 50

12.0 10.5 5.0 5.3 9.0 8.3 8.1  
50 19 10 4.8 11 19-25 28 50

10.5 9.5 8.8 5.1 4.9 8.1 7.0 7.2  
50 33 16 9 4.6 12 18-23 28 50

Top Spike 15' Oak 30' RT Sta 14+20

Top Spike First G.R. Post. 17' RT 7+74

426.2 +8.0 +6.2 +1.8 4.2 5.3 6.5  
59 64 72 82 122 150

7.70 = 90.04  
W.L. 10-12 39

424.2 4.1 5.5 7.1 8.2  
59 64 70 150



| Sta   | +     | $\pi$  | -    | Elev.  |
|-------|-------|--------|------|--------|
|       |       | 897.74 |      |        |
| 10+25 |       |        |      | 919.3  |
| +50   |       |        |      | 916.5  |
| 11    |       |        |      | 913.4  |
| +42   |       |        |      | 911.3  |
| 12    |       |        |      | 909.3  |
| +19   |       |        |      | 909.6  |
| +50   |       |        |      | 909.2  |
| T.P.  | 9.75  | 904.99 | 2.50 | 895.24 |
| T.P.  | 10.12 | 913.58 | 1.53 | 903.46 |
| B.M.  | 5.16  | 914.17 | 4.57 | 909.01 |
| 13    |       |        | 5.3  | 08.9   |
| +31   |       |        | 5.2  | 09.0   |
| 14    |       |        | 4.9  | 09.3   |
| +33   |       |        | 4.4  | 09.8   |

909.01



$$\begin{array}{r} 4.0 \quad 5.6 \quad 7.4 \quad 8.2 \\ 4216 \quad \underline{50} \quad \underline{58} \quad \underline{100} \quad \underline{150} \end{array}$$

$$\begin{array}{r} 5.4 \quad 6.9 \quad 8.4 \quad 8.5 \\ +188 \quad \underline{42} \quad \underline{70} \quad \underline{120} \quad \underline{150} \end{array}$$

$$\begin{array}{r} 3.5 \quad 5.8 \quad 6.9 \quad 8.6 \quad 8.8 \\ +15.7 \quad \underline{35} \quad \underline{46} \quad \underline{60} \quad \underline{110} \quad \underline{150} \end{array}$$

$$\begin{array}{r} 3.0 \quad 5.0 \quad 6.6 \quad 8.2 \\ +13.6 \quad \underline{30} \quad \underline{43} \quad \underline{57} \quad \underline{100} \end{array}$$

$$\begin{array}{r} 3.1 \quad 5.2 \quad 6.0 \quad 6.4 \\ +11.6 \quad \underline{37} \quad \underline{58} \quad \underline{70} \quad \underline{100} \end{array}$$

$$\begin{array}{r} FL. \\ +11.9 \quad \begin{array}{r} (4.2) \\ 31 \end{array} \quad \begin{array}{r} 2.1 \\ 25 \end{array} \quad \begin{array}{r} 4.2 \\ 51 \end{array} \quad \begin{array}{r} 5.7 \\ 70 \end{array} \quad \begin{array}{r} 6.0 \\ 100 \end{array} \end{array}$$

$$\begin{array}{r} 0.0 \quad 0.2 \quad +0.2 \\ +11.5 \quad \underline{24} \quad \underline{31} \quad \underline{50} \end{array}$$

Top Spike 15" Oak 30' Rt 14+20

$$\begin{array}{r} 18.2 \quad 16.0 \quad 13.3 \quad 5.6 \quad 5.5 \quad 18.1 \quad 13.4 \quad 13.2 \\ \underline{50} \quad \underline{37} \quad \underline{26} \quad \underline{13} \quad \underline{5.3} \quad \underline{8} \quad \underline{20} \quad \underline{32} \quad \underline{50} \end{array}$$

$$\begin{array}{r} 14.1 \quad 11.6 \quad 5.4 \quad 5.5 \quad 8.5 \quad 11.1 \quad 10.6 \quad 9.7 \\ \underline{50} \quad \underline{22} \quad \underline{11} \quad \underline{52} \quad \underline{10} \quad \underline{17} \quad \underline{22} \quad \underline{28} \quad \underline{50} \end{array}$$

$$\begin{array}{r} 10.9 \quad 10.0 \quad 9.2 \quad 5.2 \quad 5.2 \quad 8.3 \quad 7.4 \quad 7.9 \\ \underline{50} \quad \underline{33} \quad \underline{16} \quad \underline{9} \quad \underline{4.9} \quad \underline{12} \quad \underline{19-23} \quad \underline{29} \quad \underline{50} \end{array}$$

$$\begin{array}{r} 8.1 \quad 8.5 \quad 7.3 \quad 7.0 \quad 6.7 \quad 4.8 \quad 4.6 \quad 7.0 \quad 5.5 \quad 5.9 \quad 6.1 \\ \underline{50} \quad \underline{46} \quad \underline{46} \quad \underline{28} \quad \underline{14} \quad \underline{10} \quad \underline{4.4} \quad \underline{13} \quad \underline{16-21} \quad \underline{28} \quad \underline{42} \quad \underline{50} \end{array}$$

| Sta.  | +     | $\pi$   | -    | Elev    |
|-------|-------|---------|------|---------|
|       |       | 914.17. |      |         |
| 14+70 |       |         | 3.5  | 10.7.   |
| 15    |       |         | 2.5  | 11.7.   |
| T.P.  | 11.19 | 922.95. | 2.41 | 911.76. |
| +50   |       |         | 9.3  | 13.7.   |
| 16    |       |         | 7.2  | 15.8.   |
| +50   |       |         | 5.0  | 18.0.   |
| T.P.  | 11.30 | 933.33. | 0.92 | 922.03. |
| 17    |       |         | 12.9 | 20.4.   |
| +14   | P.C.  |         | 12.3 | 21.0.   |
| +50   |       |         | 10.9 | 22.4.   |
| 18    |       |         | 9.4  | 23.9.   |
| +50   |       |         | 7.9  | 25.4.   |
| 19    |       |         | 6.1  | 27.2.   |
| +39   | P.T.  |         | 5.0  | 28.3.   |

|                  |                  |                  |                  |                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| $\frac{6.1}{50}$ | $\frac{4.6}{37}$ | $\frac{4.5}{26}$ | $\frac{5.5}{20}$ | $\frac{3.9}{11}$ | $\frac{3.7}{12}$ | $\frac{5.6}{16}$ | $\frac{3.4}{22}$ | $\frac{3.1}{27}$ | $\frac{3.6}{37}$ | $\frac{5.0}{50}$ |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|

|                  |                  |                  |                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| $\frac{3.5}{50}$ | $\frac{3.0}{39}$ | $\frac{3.0}{27}$ | $\frac{3.7}{23}$ | $\frac{3.0}{11}$ | $\frac{2.8}{14}$ | $\frac{4.9}{20}$ | $\frac{1.3}{23}$ | $\frac{1.5}{30}$ | $\frac{5.0}{50}$ |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|

|                   |                   |                   |                   |                   |                  |                  |                   |                  |                  |                  |
|-------------------|-------------------|-------------------|-------------------|-------------------|------------------|------------------|-------------------|------------------|------------------|------------------|
| $\frac{10.9}{50}$ | $\frac{10.4}{28}$ | $\frac{11.0}{24}$ | $\frac{10.0}{14}$ | $\frac{9.3}{9.3}$ | $\frac{9.6}{11}$ | $\frac{9.6}{17}$ | $\frac{10.8}{20}$ | $\frac{9.0}{26}$ | $\frac{8.4}{42}$ | $\frac{8.1}{50}$ |
|-------------------|-------------------|-------------------|-------------------|-------------------|------------------|------------------|-------------------|------------------|------------------|------------------|

|                  |                  |                  |                  |                  |                  |                  |                   |                 |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|-----------------|------------------|------------------|------------------|------------------|
| $\frac{9.1}{50}$ | $\frac{9.0}{44}$ | $\frac{8.4}{31}$ | $\frac{8.9}{27}$ | $\frac{9.3}{25}$ | $\frac{8.9}{21}$ | $\frac{7.5}{12}$ | $\frac{7.2}{7.2}$ | $\frac{7.4}{9}$ | $\frac{7.3}{16}$ | $\frac{7.9}{19}$ | $\frac{6.6}{24}$ | $\frac{6.0}{50}$ |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|-----------------|------------------|------------------|------------------|------------------|

|                  |                  |                  |                  |                  |                   |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|------------------|
| $\frac{6.9}{50}$ | $\frac{5.7}{31}$ | $\frac{6.3}{26}$ | $\frac{6.0}{18}$ | $\frac{5.2}{14}$ | $\frac{5.0}{5.0}$ | $\frac{5.3}{10}$ | $\frac{5.7}{19}$ | $\frac{4.0}{27}$ | $\frac{2.7}{50}$ |
|------------------|------------------|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|------------------|

|                   |                   |                   |                   |                   |                   |                   |                     |                   |                   |                   |                  |                  |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|---------------------|-------------------|-------------------|-------------------|------------------|------------------|
| $\frac{14.0}{50}$ | $\frac{13.2}{31}$ | $\frac{13.0}{23}$ | $\frac{12.6}{19}$ | $\frac{13.0}{17}$ | $\frac{13.0}{13}$ | $\frac{13.4}{12}$ | $\frac{12.7}{12.7}$ | $\frac{13.2}{12}$ | $\frac{13.8}{19}$ | $\frac{10.7}{22}$ | $\frac{9.8}{32}$ | $\frac{8.8}{50}$ |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|---------------------|-------------------|-------------------|-------------------|------------------|------------------|

|                   |                   |                   |                   |                   |                   |                     |                   |                   |                   |                  |                  |                  |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|---------------------|-------------------|-------------------|-------------------|------------------|------------------|------------------|
| $\frac{13.4}{50}$ | $\frac{12.5}{33}$ | $\frac{11.6}{20}$ | $\frac{12.1}{18}$ | $\frac{12.0}{13}$ | $\frac{13.0}{11}$ | $\frac{12.0}{12.0}$ | $\frac{12.7}{12}$ | $\frac{12.9}{21}$ | $\frac{10.0}{23}$ | $\frac{9.0}{28}$ | $\frac{8.6}{35}$ | $\frac{7.8}{50}$ |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|---------------------|-------------------|-------------------|-------------------|------------------|------------------|------------------|

|                   |                   |                  |                  |                   |                   |                     |                   |                   |                  |                  |                  |                  |
|-------------------|-------------------|------------------|------------------|-------------------|-------------------|---------------------|-------------------|-------------------|------------------|------------------|------------------|------------------|
| $\frac{11.2}{50}$ | $\frac{10.0}{35}$ | $\frac{9.3}{22}$ | $\frac{9.8}{20}$ | $\frac{10.1}{17}$ | $\frac{11.6}{14}$ | $\frac{10.9}{10.9}$ | $\frac{11.3}{12}$ | $\frac{11.1}{20}$ | $\frac{6.6}{23}$ | $\frac{6.0}{30}$ | $\frac{5.4}{42}$ | $\frac{4.7}{50}$ |
|-------------------|-------------------|------------------|------------------|-------------------|-------------------|---------------------|-------------------|-------------------|------------------|------------------|------------------|------------------|

|                  |                  |                  |                   |                   |                  |                  |                  |                  |
|------------------|------------------|------------------|-------------------|-------------------|------------------|------------------|------------------|------------------|
| $\frac{8.0}{50}$ | $\frac{7.4}{38}$ | $\frac{6.4}{22}$ | $\frac{10.0}{12}$ | $\frac{9.4}{9.4}$ | $\frac{9.4}{12}$ | $\frac{9.6}{20}$ | $\frac{5.1}{27}$ | $\frac{4.5}{50}$ |
|------------------|------------------|------------------|-------------------|-------------------|------------------|------------------|------------------|------------------|

|                  |                  |                  |                  |                  |                   |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|
| $\frac{5.9}{50}$ | $\frac{5.3}{33}$ | $\frac{4.9}{24}$ | $\frac{4.8}{21}$ | $\frac{8.4}{12}$ | $\frac{7.9}{7.9}$ | $\frac{8.3}{16}$ | $\frac{4.0}{24}$ | $\frac{3.1}{50}$ |
|------------------|------------------|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|

|                  |                  |                  |                  |                   |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|------------------|
| $\frac{5.7}{50}$ | $\frac{5.1}{36}$ | $\frac{4.3}{22}$ | $\frac{6.7}{17}$ | $\frac{6.1}{6.1}$ | $\frac{6.5}{14}$ | $\frac{3.3}{19}$ | $\frac{3.5}{36}$ | $\frac{3.7}{50}$ |
|------------------|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|------------------|

|                  |                  |                  |                   |                  |                  |                  |
|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|
| $\frac{5.0}{50}$ | $\frac{3.9}{20}$ | $\frac{5.7}{15}$ | $\frac{5.0}{5.0}$ | $\frac{2.7}{20}$ | $\frac{3.9}{33}$ | $\frac{4.8}{50}$ |
|------------------|------------------|------------------|-------------------|------------------|------------------|------------------|

| Sta.  | +    | $\pi$  | -     | Elev.  |
|-------|------|--------|-------|--------|
|       |      | 733.33 |       |        |
| 20    |      |        | 4.2   | 29.1   |
| B.M.  | 4.94 | 936.82 | 1.41  | 931.82 |
| +50   |      |        | 7.6   | 29.2   |
| 21    |      |        | 8.0   | 28.8   |
| +50   |      |        | 8.8   | 28.0   |
| 22    |      |        | 10.4  | 26.4   |
| +50   |      |        | 12.6  | 24.2   |
| 23    |      |        |       | 21.8   |
| +50   |      |        |       | 19.4   |
| 24    |      |        |       | 16.9   |
| T.P.  | 3.44 | 926.89 | 13.37 | 923.45 |
| 23+00 |      |        | 5.1   | 21.8   |
| +50   |      |        | 7.5   | 19.4   |
| 24    |      |        | 10.0  | 16.9   |

$\frac{5.3}{50}$   $\frac{4.6}{33}$   $\frac{4.0}{19}$   $\frac{4.9}{13}$  4.2  $\frac{4.7}{13}$   $\frac{3.6}{19}$   $\frac{5.0}{28}$   $\frac{6.8}{50}$

Spike in 24" Pop. 50' Lt 21+15

$\frac{7.5}{50}$   $\frac{7.2}{39}$   $\frac{7.0}{27}$   $\frac{7.4}{20}$   $\frac{7.9}{15}$   $\frac{8.1}{11}$   $\frac{7.3}{15}$   $\frac{8.4}{25}$   $\frac{9.7}{41}$   $\frac{10.4}{50}$

$\frac{6.6}{50}$   $\frac{6.6}{35}$   $\frac{6.7}{21}$   $\frac{8.1}{17}$   $\frac{8.2}{14}$   $\frac{8.0}{8.0}$   $\frac{8.5}{12}$   $\frac{7.7}{17}$   $\frac{8.3}{29}$   $\frac{9.4}{34}$   $\frac{10.0}{43}$   $\frac{10.9}{50}$

$\frac{4.5}{50}$   $\frac{5.3}{34}$   $\frac{5.7}{25}$   $\frac{9.0}{17}$   $\frac{9.1}{13}$   $\frac{8.8}{8.8}$   $\frac{9.3}{12}$   $\frac{7.8}{18}$   $\frac{8.8}{27}$   $\frac{9.4}{34}$   $\frac{10.8}{50}$

$\frac{3.0}{75}$   $\frac{4.0}{50}$   $\frac{4.5}{27}$   $\frac{9.8}{18}$   $\frac{10.5}{12}$   $\frac{10.4}{10.4}$   $\frac{10.9}{12}$   $\frac{8.7}{19}$   $\frac{9.7}{36}$   $\frac{11.3}{50}$

$\frac{4.6}{75}$   $\frac{4.9}{50}$   $\frac{4.8}{33}$   $\frac{10.4}{20}$   $\frac{12.8}{13}$   $\frac{12.6}{12.6}$   $\frac{13.0}{11}$   $\frac{12.6}{13}$   $\frac{8.9}{19}$   $\frac{9.4}{37}$   $\frac{10.0}{50}$

$\frac{7.1}{100}$   $\frac{6.3}{50}$   $\frac{6.2}{34}$

-15.0

$\frac{6.8}{25}$   $\frac{8.8}{50}$   $\frac{10.7}{75}$

$\frac{10.3}{100}$   $\frac{9.6}{75}$   $\frac{7.1}{50}$   $\frac{9.2}{35}$

-17.4

$\frac{8.5}{27}$   $\frac{9.2}{50}$   $\frac{9.9}{65}$   $\frac{11.4}{75}$

$\frac{14.3}{100}$   $\frac{14.2}{75}$   $\frac{14.0}{50}$   $\frac{13.5}{27}$

-19.9

$\frac{12.1}{29}$   $\frac{11.7}{50}$   $\frac{11.9}{75}$

$\frac{4.6}{20}$   $\frac{5.5}{12}$   $\frac{5.1}{5.1}$   $\frac{5.6}{72}$   $\frac{4.7}{16}$

$\frac{4.5}{27}$   $\frac{6.0}{21}$   $\frac{8.0}{11}$   $\frac{7.5}{7.5}$   $\frac{7.8}{11}$   $\frac{8.1}{12}$   $\frac{7.4}{14}$   $\frac{7.0}{17}$

$\frac{8.5}{19}$   $\frac{10.3}{11}$   $\frac{10.0}{10.0}$   $\frac{10.2}{11}$   $\frac{11.0}{13}$   $\frac{9.5}{18}$



| Sta.  | +    | $\pi$  | -     | Elev.           |
|-------|------|--------|-------|-----------------|
|       |      | 926.89 |       |                 |
| 24+51 | P.C. |        | 12.5  | 14.4            |
| 25    |      |        | 15.1  | 11.8            |
| T.P.  | 1.49 | 915.55 | 12.83 | 914.06          |
| +50   |      |        | 6.7   | 08.9            |
| 26    |      |        | 11.5  | 04.1            |
| T.P.  | 3.95 | 909.44 | 10.06 | 905.49          |
| +25   |      |        | 7.7   | 01.7            |
| +50   |      |        | 11.9  | 97.5            |
| +75   |      |        | 13.3  | 96.1            |
| 27    |      |        | 12.1  | 97.3            |
| +32   |      |        | 9.0   | 00.4            |
| +53   |      |        | 9.0   | 00.4            |
| B.M.  | 2.19 | 904.47 | 7.14  | 902.30 (902.28) |
| +76   |      |        | 7.2   | 97.3            |
| 28    |      |        | 14.5  | 90.0            |

## E. E. Old Roadbed

|                  |                  |                  |                   |                   |      |                   |                   |                   |                  |                  |                  |
|------------------|------------------|------------------|-------------------|-------------------|------|-------------------|-------------------|-------------------|------------------|------------------|------------------|
| $\frac{7.0}{75}$ | $\frac{8.0}{50}$ | $\frac{7.2}{24}$ | $\frac{11.8}{16}$ | $\frac{13.1}{12}$ | 12.5 | $\frac{12.8}{11}$ | $\frac{13.6}{14}$ | $\frac{12.2}{16}$ | $\frac{6.4}{25}$ | $\frac{5.3}{50}$ | $\frac{5.4}{75}$ |
|------------------|------------------|------------------|-------------------|-------------------|------|-------------------|-------------------|-------------------|------------------|------------------|------------------|

|                   |                   |                   |                   |      |                  |                      |                   |                   |
|-------------------|-------------------|-------------------|-------------------|------|------------------|----------------------|-------------------|-------------------|
| $\frac{13.8}{50}$ | $\frac{12.6}{24}$ | $\frac{15.8}{19}$ | $\frac{15.7}{12}$ | 15.1 | $\frac{15.4}{9}$ | $\frac{16.1}{12.14}$ | $\frac{11.6}{18}$ | $\frac{11.7}{50}$ |
|-------------------|-------------------|-------------------|-------------------|------|------------------|----------------------|-------------------|-------------------|

|                  |                  |                  |                  |                  |                  |                  |     |                 |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-----|-----------------|------------------|------------------|------------------|
| $\frac{8.6}{50}$ | $\frac{8.9}{36}$ | $\frac{7.8}{26}$ | $\frac{8.6}{24}$ | $\frac{7.2}{23}$ | $\frac{7.5}{21}$ | $\frac{6.7}{18}$ | 6.7 | $\frac{6.9}{7}$ | $\frac{7.3}{11}$ | $\frac{8.9}{22}$ | $\frac{9.9}{50}$ |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-----|-----------------|------------------|------------------|------------------|

|                   |                   |                   |                  |                  |                 |      |                   |                   |                   |
|-------------------|-------------------|-------------------|------------------|------------------|-----------------|------|-------------------|-------------------|-------------------|
| $\frac{18.6}{50}$ | $\frac{17.9}{43}$ | $\frac{16.9}{38}$ | $\frac{9.9}{26}$ | $\frac{9.3}{16}$ | $\frac{9.2}{9}$ | 11.5 | $\frac{15.1}{12}$ | $\frac{17.6}{27}$ | $\frac{19.4}{50}$ |
|-------------------|-------------------|-------------------|------------------|------------------|-----------------|------|-------------------|-------------------|-------------------|

|                   |                   |                   |                  |                  |                 |     |                  |                   |                   |
|-------------------|-------------------|-------------------|------------------|------------------|-----------------|-----|------------------|-------------------|-------------------|
| $\frac{13.6}{50}$ | $\frac{12.8}{46}$ | $\frac{10.6}{39}$ | $\frac{4.8}{30}$ | $\frac{4.1}{18}$ | $\frac{4.4}{7}$ | 7.7 | $\frac{10.9}{7}$ | $\frac{12.3}{20}$ | $\frac{15.1}{50}$ |
|-------------------|-------------------|-------------------|------------------|------------------|-----------------|-----|------------------|-------------------|-------------------|

|                   |                   |                  |                  |                  |                 |      |                   |                   |                   |
|-------------------|-------------------|------------------|------------------|------------------|-----------------|------|-------------------|-------------------|-------------------|
| $\frac{13.5}{50}$ | $\frac{12.5}{47}$ | $\frac{5.3}{34}$ | $\frac{4.8}{25}$ | $\frac{5.0}{13}$ | $\frac{9.8}{7}$ | 11.9 | $\frac{13.7}{13}$ | $\frac{13.1}{37}$ | $\frac{12.7}{50}$ |
|-------------------|-------------------|------------------|------------------|------------------|-----------------|------|-------------------|-------------------|-------------------|

|                   |                   |                  |                  |                  |                  |                  |      |                  |                   |                   |
|-------------------|-------------------|------------------|------------------|------------------|------------------|------------------|------|------------------|-------------------|-------------------|
| $\frac{17.0}{60}$ | $\frac{16.0}{53}$ | $\frac{6.4}{38}$ | $\frac{5.8}{28}$ | $\frac{5.8}{16}$ | $\frac{11.0}{9}$ | $\frac{12.6}{5}$ | 13.3 | $\frac{13.4}{6}$ | $\frac{11.9}{22}$ | $\frac{10.6}{50}$ |
|-------------------|-------------------|------------------|------------------|------------------|------------------|------------------|------|------------------|-------------------|-------------------|

|                   |                   |                  |                  |                  |                   |                  |      |                   |                  |                  |
|-------------------|-------------------|------------------|------------------|------------------|-------------------|------------------|------|-------------------|------------------|------------------|
| $\frac{19.2}{74}$ | $\frac{16.8}{60}$ | $\frac{7.0}{40}$ | $\frac{6.6}{31}$ | $\frac{6.6}{20}$ | $\frac{11.2}{12}$ | $\frac{12.7}{6}$ | 12.1 | $\frac{10.6}{15}$ | $\frac{8.6}{27}$ | $\frac{6.2}{50}$ |
|-------------------|-------------------|------------------|------------------|------------------|-------------------|------------------|------|-------------------|------------------|------------------|

|                   |                   |                  |                  |                  |                   |     |                 |                  |                  |                  |
|-------------------|-------------------|------------------|------------------|------------------|-------------------|-----|-----------------|------------------|------------------|------------------|
| $\frac{17.3}{67}$ | $\frac{14.9}{59}$ | $\frac{8.1}{48}$ | $\frac{7.7}{37}$ | $\frac{8.0}{25}$ | $\frac{11.3}{16}$ | 9.0 | $\frac{7.8}{7}$ | $\frac{6.5}{22}$ | $\frac{5.0}{38}$ | $\frac{4.6}{50}$ |
|-------------------|-------------------|------------------|------------------|------------------|-------------------|-----|-----------------|------------------|------------------|------------------|

|                   |                   |                  |                  |                  |                   |                  |     |                  |                  |                  |
|-------------------|-------------------|------------------|------------------|------------------|-------------------|------------------|-----|------------------|------------------|------------------|
| $\frac{15.2}{70}$ | $\frac{14.3}{64}$ | $\frac{8.7}{54}$ | $\frac{8.3}{43}$ | $\frac{8.5}{30}$ | $\frac{11.1}{23}$ | $\frac{9.4}{20}$ | 9.0 | $\frac{7.7}{18}$ | $\frac{8.1}{31}$ | $\frac{8.3}{50}$ |
|-------------------|-------------------|------------------|------------------|------------------|-------------------|------------------|-----|------------------|------------------|------------------|

Spike in 12" Oak E 50' Rt. Sta 27+50

|                  |                  |                  |       |                  |                  |     |                  |                   |                   |
|------------------|------------------|------------------|-------|------------------|------------------|-----|------------------|-------------------|-------------------|
| $\frac{9.7}{90}$ | $\frac{9.2}{76}$ | $\frac{5.2}{67}$ | (4.6) | $\frac{5.1}{41}$ | $\frac{8.8}{31}$ | 7.2 | $\frac{8.7}{20}$ | $\frac{12.1}{43}$ | $\frac{14.0}{50}$ |
|------------------|------------------|------------------|-------|------------------|------------------|-----|------------------|-------------------|-------------------|

|                   |                  |                  |                  |                  |                   |                   |                   |      |                   |                   |
|-------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|------|-------------------|-------------------|
| $\frac{10.0}{91}$ | $\frac{9.8}{83}$ | $\frac{5.2}{73}$ | $\frac{4.8}{61}$ | $\frac{5.6}{48}$ | $\frac{10.0}{39}$ | $\frac{11.2}{28}$ | $\frac{13.6}{18}$ | 14.5 | $\frac{16.8}{23}$ | $\frac{18.3}{50}$ |
|-------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|------|-------------------|-------------------|

Sta. +  $\nabla$  - Elev.

904.47

28 + 21

18.5

860

+ 50

20.9

836

T.P.

3.44

898.86

7.55

894.92

29

17.8

80.6

+ 50

17.5

80.9

30

17.9

80.5

+ 50

16.1

82.3

31

14.3

841

+ 38

P.C.

13.1

85.3

+ 76

12.7

85.7

32

10.9

87.5

+ 50

6.1

920

T.P.

8.56

901.60

5.32

893.04

33

1.8

93.8

£  
107 100 62 58 61 89 153 171 195 200  
100 90 82 71 59 50 25 16 18.5 23 50

£  
78 84 70 67 71 122 146 151 174 198 219 228  
100 96 92 80 69 57 50 45 32 19 20.9 16 50

£  
14 0.7 26 23 18 20 90 119 139 155 183 183  
125 114 111 108 93 77 58 42 29 15 17.8 25 50

£  
30 20 36 32 37 25 90 125 152 184 187  
125 118 114 99 88 79 59 41 18 17.5 25 50

£  
44 41 49 45 53 77 98 110 142 170 182 187  
137 125 120 101 87 80 71 62 32 12 17.9 25 50

£  
67 66 58 55 64 101 118 146 153 182 184  
116 106 100 85 74 64 50 12 11 16.1 30 50

£  
96 96 63 60 71 125 137 156 170 171  
90 84 77 65 53 40 23 14.3 22 42 50

£  
76 93 71 65 72 125 135 130 133  
80 71 69 63 50 38 28 15 13.1 27 50

£  
92 73 82 72 66 72 114 126 121 118  
64 56 52 50 48 36 23 14 5 12.7 25 50

£  
74 79 69 64 69 110 107 93 98  
50 40 37 27 14 4 10.9 21 45 50

£  
84 69 63 60 55 65 61 46  
50 45 36 23 14 6.4 5 19 50

£  
115 75 62 61 81 81 77 81 80 60 58 63  
50 46 38 27 23 17 6 78 9 14 18 44 50



| Sta     |           | $\Delta$ | -    | Elev             |
|---------|-----------|----------|------|------------------|
| 33      |           | 901.60   |      |                  |
| 33 + 23 |           |          | 7.3  | 943'             |
| +50     |           |          | 7.0  | 946'             |
| +75     | P.T. - PC |          | 6.8  | 948'             |
| 34      |           |          | 6.4  | 952'             |
| B.M.    | 490       | 900.41   | 6.08 | 895.52' (895.57) |
| +29     |           |          | 4.9  | 955'             |
| +50     |           |          | 4.8  | 956'             |
| +77     |           |          | 4.8  | 956'             |
| 35      |           |          | 5.0  | 954'             |
| +22     |           |          | 5.1  | 953'             |
| +50     |           |          | 5.5  | 949'             |
| +85     |           |          | 5.6  | 948'             |
| 36      |           |          | 10.1 | 903'             |



♂

|    |     |     |     |     |     |     |     |     |     |     |    |
|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|
| 21 | 6.2 | 5.3 | 7.6 | 7.9 | 7.4 | 7.9 | 7.3 | 4.7 | 5.0 | 6.0 | 1  |
| 50 | 43  | 27  | 21  | 16  | 5   | 7.3 | 7   | 17  | 22  | 45  | 50 |

♂

|     |     |     |     |     |     |     |     |     |     |     |     |     |    |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|
| 8.3 | 7.1 | 5.8 | 5.1 | 7.8 | 7.9 | 7.0 | 2.4 | 7.5 | 6.1 | 3.6 | 4.0 | 4.7 |    |
| 50  | 44  | 35  | 25  | 21  | 15  | 4   | 7.0 | 10  | 14  | 22  | 24  | 40  | 50 |

|      |     |     |     |     |     |     |     |     |     |     |     |
|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 10.3 | 7.8 | 6.6 | 5.3 | 7.0 | 7.6 | 2   | 7.2 | 7.0 | 2.4 | 2.5 | 3.2 |
| 50   | 45  | 39  | 27  | 24  | 15  | 6.8 | 70  | 18  | 25  | 43  | 50  |

|      |     |     |     |     |     |      |     |    |
|------|-----|-----|-----|-----|-----|------|-----|----|
| 12.2 | 6.5 | 4.9 | 7.3 | 6.8 | 6.8 | 10.9 | 1.1 |    |
| 50   | 41  | 23  | 15  | 6.4 | 10  | 23   | 33  | 50 |

Spike 8" Pop. 30" Rt 34+95

|      |     |     |     |     |     |     |      |      |    |
|------|-----|-----|-----|-----|-----|-----|------|------|----|
| 11.4 | 5.6 | 4.5 | 5.6 | 5.4 | 5.4 | 3.6 | 12.7 | 43.0 |    |
| 50   | 34  | 24  | 15  | 4.9 | 11  | 22  | 35   | 42   | 50 |

|      |     |     |     |     |     |     |     |     |      |      |    |
|------|-----|-----|-----|-----|-----|-----|-----|-----|------|------|----|
| 11.7 | 6.0 | 5.6 | 4.6 | 5.5 | 5.3 | 5.7 | 5.0 | 2.2 | 12.7 | 44.5 |    |
| 50   | 33  | 25  | 18  | 15  | 4.8 | 11  | 17  | 27  | 37   | 45   | 50 |

|      |      |     |     |     |     |     |     |     |     |    |
|------|------|-----|-----|-----|-----|-----|-----|-----|-----|----|
| 12.8 | 16.3 | 8.8 | 6.0 | 5.5 | 5.1 | 6.4 | 3.1 | 2.5 | 4.0 |    |
| 50   | 36   | 29  | 17  | 11  | 4.8 | 14  | 20  | 27  | 37  | 50 |

♂

|      |      |     |     |     |     |     |     |     |     |    |
|------|------|-----|-----|-----|-----|-----|-----|-----|-----|----|
| 16.2 | 11.3 | 8.5 | 6.7 | 5.7 | 4.7 | 5.1 | 7.1 | 5.9 | 9.6 |    |
| 50   | 31   | 18  | 13  | 9   | 5.0 | 6   | 19  | 26  | 35  | 50 |

♂

|      |      |     |     |     |     |      |      |    |
|------|------|-----|-----|-----|-----|------|------|----|
| 14.4 | 12.0 | 8.3 | 5.9 | 4.7 | 5.0 | 10.5 | 13.5 |    |
| 50   | 30   | 16  | 7   | 5.1 | 10  | 22   | 32   | 50 |

♂

|      |      |      |     |     |     |     |     |      |      |    |
|------|------|------|-----|-----|-----|-----|-----|------|------|----|
| 14.5 | 14.5 | 12.1 | 6.8 | 5.0 | 5.5 | 4.9 | 5.3 | 12.0 | 12.0 |    |
| 50   | 46   | 22   | 10  | 3   | 1   | 5.5 | 16  | 26   | 37   | 50 |

♂

|      |      |      |     |     |     |     |     |      |    |
|------|------|------|-----|-----|-----|-----|-----|------|----|
| 15.7 | 13.7 | 12.0 | 6.9 | 6.0 | 5.1 | 5.4 | 9.9 | 11.9 |    |
| 50   | 27   | 15   | 5   | 5.6 | 6   | 18  | 31  | 43   | 50 |

♂

|      |      |      |     |     |      |      |    |
|------|------|------|-----|-----|------|------|----|
| 15.4 | 13.0 | 5.8  | 5.6 | 5.4 | 12.1 | 14.6 |    |
| 50   | 11   | 10.1 | 8   | 24  | 41   | 50   | 60 |

| Sta.    | +              | $\pi$  | -    | Elev       |
|---------|----------------|--------|------|------------|
|         |                | 900.41 |      |            |
| 36 + 50 |                |        | 13.6 | 86.8       |
| 37      |                |        | 14.0 | 86.4       |
| +37     | 12" x 42" C.M. |        | 12.3 | 88.1       |
| T.P.    | 6.52           | 900.13 | 6.80 | 89.3 61    |
| +63     |                |        | 7.0  | 93.1       |
| 38      | P.C.           |        | 6.1  | 94.0       |
| +50     |                |        | 5.5  | 94.6       |
| 39      |                |        | 4.9  | 95.2       |
|         |                |        |      | +25 Ent 21 |
| +50     |                |        | 3.2  | 96.5       |
| 40      |                |        | 2.7  | 97.4       |
| T.P.    | 7.28           | 904.75 | 2.66 | 97.7 47    |
| +50     |                |        | 6.7  | 98.1       |
| 41      |                |        | 6.0  | 98.8       |
| +58     | PT-P.C.        |        | 5.3  | 99.5       |

$$\begin{array}{r} 15.4 \quad 14.0 \\ \hline 50 \quad 10 \quad 13.6 \end{array} \quad \begin{array}{r} 12.5 \quad 7.2 \\ \hline 11 \quad 20 \end{array} \quad \begin{array}{r} \text{E} \\ 6.3 \quad 6.7 \quad 11.6 \\ \hline 31 \quad 42 \quad 50 \end{array} \quad \begin{array}{r} 15.1 \quad 15.8 \\ \hline 62 \quad 72 \end{array}$$

$$\begin{array}{r} 15.8 \quad 15.0 \\ \hline 50 \quad 14 \quad 14.0 \end{array} \quad \begin{array}{r} 12.6 \quad 12.1 \\ \hline 6 \quad 10 \end{array} \quad \begin{array}{r} \text{E} \\ 7.5 \quad 6.8 \quad 7.2 \\ \hline 17 \quad 27 \quad 43 \end{array} \quad \begin{array}{r} 14.7 \quad 15.4 \\ \hline 50 \quad 55 \quad 65 \end{array}$$

$$\begin{array}{r} 15.5 \quad 14.3 \\ \hline 50 \quad 20 \quad 12.3 \end{array} \quad \begin{array}{r} \text{FL} \quad 7.4 \\ \hline 13.3 \quad 7 \end{array} \quad \begin{array}{r} \text{E} \\ 6.8 \quad 7.1 \quad 12.3 \\ \hline 19 \quad 30 \quad 39 \end{array} \quad \begin{array}{r} \text{FL} \\ 14.0 \quad 14.0 \quad 14.3 \\ \hline 44 \quad 42 \quad 50 \end{array}$$

$$\begin{array}{r} 14.9 \quad 14.0 \quad 12.3 \\ \hline 50 \quad 32 \quad 12 \quad 7.0 \end{array} \quad \begin{array}{r} \text{E} \\ 6.3 \quad 6.8 \quad 12.2 \\ \hline 11 \quad 22 \quad 32 \end{array} \quad \begin{array}{r} 13.6 \quad 11.4 \\ \hline 30 \quad 50 \end{array} \quad \begin{array}{r} \text{New Fill} \\ 11.4 \quad 11.4 \\ \hline 50 \quad 32 \end{array}$$

$$\begin{array}{r} 14.5 \quad 12.0 \quad 6.5 \\ \hline 50 \quad 26 \quad 13.6 \end{array} \quad \begin{array}{r} 6.3 \quad 10.0 \quad 10.4 \\ \hline 11 \quad 18 \quad 23 \end{array} \quad \begin{array}{r} \text{New Fill - run out} \\ 8.9 \quad 8.6 \\ \hline 30 \quad 50 \end{array} \quad \begin{array}{r} \text{at +50} \end{array}$$

$$\begin{array}{r} 13.2 \quad 11.9 \quad 7.5 \\ \hline 50 \quad 46 \quad 3.9 \quad 22 \quad 10 \end{array} \quad \begin{array}{r} \text{E} \\ 6.0 \quad 5.5 \\ \hline 5.5 \quad 6.2 \quad 5.7 \end{array} \quad \begin{array}{r} 5.5 \quad 6.2 \quad 5.7 \\ \hline 5.5 \quad 9 \quad 26 \quad 50 \end{array}$$

Ent. Lt. New Topog.

$$\begin{array}{r} 7.8 \quad 4.8 \quad 4.0 \\ \hline 50 \quad 44 \quad 33 \end{array} \quad \begin{array}{r} 4.7 \quad 4.2 \\ \hline 26 \quad 12 \quad 4.9 \end{array} \quad \begin{array}{r} 4.4 \quad 3.3 \quad 2.8 \quad 2.2 \\ \hline 9 \quad 20 \quad 42 \quad 50 \end{array}$$

$$\begin{array}{r} 4.1 \quad 3.5 \quad 3.8 \quad 3.3 \\ \hline 50 \quad 34 \quad 18 \quad 10 \end{array} \quad \begin{array}{r} 3.6 \quad 4.0 \quad 2.1 \quad 1.3 \\ \hline 10 \quad 18 \quad 50 \end{array}$$

$$\begin{array}{r} 5.0 \quad 3.6 \quad 3.1 \quad 2.7 \\ \hline 50 \quad 38 \quad 17 \quad 6 \end{array} \quad \begin{array}{r} 2.7 \quad 3.2 \quad 2.6 \quad 1.9 \quad 1.4 \quad 0.0 \\ \hline 8 \quad 21 \quad 24 \quad 24 \quad 50 \end{array}$$

$$\begin{array}{r} 9.6 \quad 7.1 \\ \hline 45 \quad 17 \quad 6.7 \end{array} \quad \begin{array}{r} 7.0 \quad 6.5 \quad 5.7 \quad 5.2 \quad 4.2 \quad 3.0 \\ \hline 11 \quad 23 \quad 26 \quad 26 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 4.7 \quad 7.2 \quad 6.3 \\ \hline 41 \quad 16 \quad 9 \quad 6.0 \end{array} \quad \begin{array}{r} 6.3 \quad 5.7 \quad 5.0 \quad 4.3 \quad 2.1 \\ \hline 12 \quad 22 \quad 24 \quad 26 \quad 50 \end{array}$$

$$\begin{array}{r} 12.0 \quad 7.1 \quad 5.6 \\ \hline 50 \quad 18 \quad 9 \quad 5.3 \end{array} \quad \begin{array}{r} 5.7 \quad 5.5 \quad 3.6 \quad 1.1 \\ \hline 13 \quad 15 \quad 19 \quad 50 \end{array}$$

| Sta.  | T    | $\Sigma$ | -    | Elev.   |
|-------|------|----------|------|---------|
|       |      | 904.75.  |      |         |
| 42    |      |          | 4.8  | 00.0.   |
| +50   |      |          | 4.1  | 00.7.   |
| +87   |      |          | 3.8  | 01.0.   |
| 43    |      |          | 3.8  | 01.0.   |
| +32   |      |          | 4.0  | 00.8.   |
| T.P.  | 4.46 | 904.91.  | 4.30 | 900.45. |
| 44    |      |          | 5.2  | 99.7.   |
| +50   |      |          | 6.0  | 98.9.   |
| +76   |      |          | 6.1  | 98.8.   |
| +85   |      |          | 6.1  | 98.8.   |
| +94   |      |          | 6.1  | 98.8.   |
| 45+40 |      |          | 5.8  | 99.1.   |
| 46    |      |          | 5.1  | 99.8.   |

$$\begin{array}{r} 9.7 \ 9.3 \ 6.7 \ 5.5 \\ \hline 50 \ 31 \ 21 \ 12 \end{array} \quad \begin{array}{r} 5.0 \ 4.6 \\ \hline 12 \ 22 \end{array} \quad \begin{array}{r} 1.4 \ 0.8 \\ \hline 32 \ 50 \end{array}$$

$$\begin{array}{r} 11.7 \ 8.3 \ 6.2 \ 4.6 \\ \hline 50 \ 35 \ 24 \ 11 \end{array} \quad \begin{array}{r} 4.7 \ 3.8 \\ \hline 12 \ 25 \end{array} \quad \begin{array}{r} 0.2 \ 0.6 \\ \hline 24 \ 50 \end{array}$$

$$\begin{array}{r} 12.6 \ 9.2 \ 5.4 \ 4.2 \\ \hline 50 \ 41 \ 18 \ 13 \end{array} \quad \begin{array}{r} 3.8 \ 4.5 \ 4.3 \\ \hline 15 \ 25 \ 34 \end{array} \quad \begin{array}{r} 0.3 \ 1.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 13.6 \ 8.7 \ 7.0 \ 4.2 \\ \hline 50 \ 38 \ 32 \ 13 \end{array} \quad \begin{array}{r} 3.8 \ 4.5 \ 4.5 \\ \hline 14 \ 24 \ 35 \end{array} \quad \begin{array}{r} 0.0 \ 0.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 14.4 \ 8.3 \ 6.5 \ 4.3 \\ \hline 50 \ 38 \ 28 \ 16 \end{array} \quad \begin{array}{r} 4.0 \ 4.5 \ 4.3 \\ \hline 15 \ 27 \ 32 \end{array} \quad \begin{array}{r} 3.0 \ 3.0 \\ \hline 50 \end{array}$$

Spike P A 42+ R1

$$\begin{array}{r} 12.1 \ 8.4 \ 7.1 \\ \hline 50 \ 39 \ 33 \end{array} \quad \begin{array}{r} 6.9 \ 5.7 \\ \hline 24 \ 12 \end{array} \quad \begin{array}{r} 5.2 \ 5.7 \ 5.9 \ 5.7 \ 4.1 \ 4.4 \\ \hline 12 \ 16 \ 29 \ 37 \ 50 \end{array}$$

$$\begin{array}{r} 14.0 \ 11.2 \ 10.6 \ 9.9 \ 6.4 \\ \hline 50 \ 37 \ 24 \ 18 \ 11 \end{array} \quad \begin{array}{r} 6.0 \ 6.3 \ 6.1 \\ \hline 12 \ 24 \ 35 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 15.1 \ 12.8 \ 11.4 \ 11.2 \\ \hline 50 \ 41 \ 36 \ 25 \end{array} \quad \begin{array}{r} 10.1 \ 6.4 \\ \hline 19 \ 10 \end{array} \quad \begin{array}{r} 6.1 \ 6.5 \ 6.0 \\ \hline 10 \ 11 \end{array} \quad \begin{array}{r} 6.5 \ 6.5 \ 6.4 \\ \hline 23 \ 32 \ 50 \end{array}$$

$$\begin{array}{r} 14.5 \ 12.6 \ 11.2 \ 11.0 \ 6.4 \\ \hline 50 \ 44 \ 38 \ 19 \ 12 \end{array} \quad \begin{array}{r} 6.1 \ 6.5 \ 6.0 \\ \hline 13 \ 14 \end{array} \quad \begin{array}{r} 6.6 \ 9.3 \ 10.1 \\ \hline 18 \ 26 \ 50 \end{array}$$

$$\begin{array}{r} 14.4 \ 12.6 \ 11.6 \ 11.1 \ 6.4 \\ \hline 50 \ 45 \ 39 \ 20 \ 12 \end{array} \quad \begin{array}{r} 6.1 \ 6.6 \ 10.3 \\ \hline 12 \ 18 \ 33 \end{array} \quad \begin{array}{r} 11.0 \ 11.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 10.7 \ 10.8 \ 6.2 \\ \hline 50 \ 21 \ 13 \end{array} \quad \begin{array}{r} 5.8 \ 6.3 \ 10.6 \\ \hline 12 \ 18 \ 25 \end{array} \quad \begin{array}{r} 13.5 \ 17.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 10.2 \ 9.8 \ 5.5 \\ \hline 50 \ 19 \ 11 \end{array} \quad \begin{array}{r} 5.1 \ 4.8 \ 13.2 \\ \hline 11 \ 23 \ 50 \end{array} \quad \begin{array}{r} 17.3 \\ \hline 50 \end{array}$$



| Sta.  |       | K      | -    | Elek.  |                        |
|-------|-------|--------|------|--------|------------------------|
|       |       | 90491  |      |        |                        |
| 46+40 |       |        | 36   | 01.30  |                        |
|       |       |        |      |        | +90 Ent R <sup>+</sup> |
| 47    |       |        | 16   | 03.31  |                        |
| T.P.  | 10.10 | 914.02 | 0.99 | 903.92 |                        |
| +27   |       |        | 9.6  | 04.4   |                        |
| B.M.  | 6.29  | 913.91 | 6.39 | 907.63 | 907.63                 |
| +60   |       |        | 8.0  | 05.9   |                        |
| 48    |       |        | 6.2  | 07.7   |                        |
| +50   |       |        | 3.3  | 10.6   |                        |
| T.P.  | 9.54  | 921.24 | 2.21 | 911.70 |                        |
| 49    |       |        | 8.4  | 12.8   |                        |
| +38   |       |        | 7.1  | 14.1   |                        |
| 50    |       |        | 5.6  | 15.6   |                        |
| +50   |       |        | 4.5  | 16.7   |                        |
| 51    |       |        | 4.1  | 17.1   |                        |
| +50   |       |        | 4.0  | 17.2   |                        |

$$\begin{array}{r} 93 \\ 50 \end{array} \begin{array}{r} 9.3 \\ 21 \end{array} \begin{array}{r} 4.0 \\ 11 \end{array} \begin{array}{r} 3.8 \\ 11 \end{array} \begin{array}{r} 11.5 \\ 21 \end{array} \begin{array}{r} 13.3 \\ 21 \end{array} \begin{array}{r} 16.0 \\ 50 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array} \begin{array}{r} 4.0 \\ 43 \end{array} \begin{array}{r} 4.6 \\ 20 \end{array} \begin{array}{r} 1.8 \\ 12 \end{array} \begin{array}{r} 1.6 \\ 12 \end{array} \begin{array}{r} 2.0 \\ 12 \end{array} \begin{array}{r} 5.1 \\ 20 \end{array} \begin{array}{r} 7.3 \\ 35 \end{array} \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 10.3 \\ 50 \end{array} \begin{array}{r} 10.3 \\ 24 \end{array} \begin{array}{r} 9.9 \\ 11 \end{array} \begin{array}{r} 9.6 \\ 11 \end{array} \begin{array}{r} 10.0 \\ 11 \end{array} \begin{array}{r} 4.8 \\ 34 \end{array} \begin{array}{r} 13.8 \\ 40 \end{array} \begin{array}{r} 17.9 \\ 50 \end{array}$$

Spike 8" Oak 33' Lt 47+60

$$\begin{array}{r} 2.7 \\ 50 \end{array} \begin{array}{r} 2.0 \\ 22 \end{array} \begin{array}{r} 8.5 \\ 17 \end{array} \begin{array}{r} 8.4 \\ 14 \end{array} \begin{array}{r} 6.9 \\ 16 \end{array} \begin{array}{r} 7.2 \\ 29 \end{array} \begin{array}{r} 9.1 \\ 39 \end{array} \begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 6.0 \\ 50 \end{array} \begin{array}{r} 4.2 \\ 29 \end{array} \begin{array}{r} 4.1 \\ 23 \end{array} \begin{array}{r} 6.4 \\ 17 \end{array} \begin{array}{r} 6.6 \\ 14 \end{array} \begin{array}{r} 5.0 \\ 17 \end{array} \begin{array}{r} 4.8 \\ 23 \end{array} \begin{array}{r} 3.1 \\ 28 \end{array} \begin{array}{r} 4.2 \\ 42 \end{array} \begin{array}{r} 5.1 \\ 50 \end{array}$$

$$\begin{array}{r} 2.0 \\ 42 \end{array} \begin{array}{r} 3.4 \\ 21 \end{array} \begin{array}{r} 4.2 \\ 13 \end{array} \begin{array}{r} 3.3 \\ 3.3 \end{array} \begin{array}{r} 3.6 \\ 16 \end{array} \begin{array}{r} +1.2 \\ 26 \end{array} \begin{array}{r} +1.2 \\ 42 \end{array} \begin{array}{r} +0.5 \\ 50 \end{array}$$

$$\begin{array}{r} 2.6 \\ 50 \end{array} \begin{array}{r} 5.3 \\ 22 \end{array} \begin{array}{r} 8.8 \\ 14 \end{array} \begin{array}{r} 8.4 \\ 8.4 \end{array} \begin{array}{r} 8.6 \\ 14 \end{array} \begin{array}{r} 3.1 \\ 30 \end{array} \begin{array}{r} 3.1 \\ 30 \end{array} \begin{array}{r} 3.6 \\ 50 \end{array}$$

$$\begin{array}{r} 5.6 \\ 50 \end{array} \begin{array}{r} 3.4 \\ 23 \end{array} \begin{array}{r} 7.5 \\ 15 \end{array} \begin{array}{r} 7.1 \\ 7.1 \end{array} \begin{array}{r} 7.4 \\ 14 \end{array} \begin{array}{r} 1.6 \\ 23 \end{array} \begin{array}{r} 1.7 \\ 50 \end{array}$$

$$\begin{array}{r} 4.4 \\ 50 \end{array} \begin{array}{r} 2.1 \\ 22 \end{array} \begin{array}{r} 6.0 \\ 15 \end{array} \begin{array}{r} 5.6 \\ 5.6 \end{array} \begin{array}{r} 6.1 \\ 15 \end{array} \begin{array}{r} 1.6 \\ 21 \end{array} \begin{array}{r} 2.0 \\ 30 \end{array} \begin{array}{r} 3.2 \\ 50 \end{array}$$

$$\begin{array}{r} 2.5 \\ 50 \end{array} \begin{array}{r} 1.5 \\ 21 \end{array} \begin{array}{r} 4.9 \\ 16 \end{array} \begin{array}{r} 4.5 \\ 4.5 \end{array} \begin{array}{r} 5.2 \\ 13 \end{array} \begin{array}{r} 2.9 \\ 18 \end{array} \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 1.7 \\ 50 \end{array} \begin{array}{r} 2.4 \\ 18 \end{array} \begin{array}{r} 4.6 \\ 14 \end{array} \begin{array}{r} 4.1 \\ 4.1 \end{array} \begin{array}{r} 4.7 \\ 14 \end{array} \begin{array}{r} 3.9 \\ 16 \end{array} \begin{array}{r} 5.9 \\ 50 \end{array}$$

$$\begin{array}{r} 3.3 \\ 50 \end{array} \begin{array}{r} 3.2 \\ 18 \end{array} \begin{array}{r} 4.7 \\ 15 \end{array} \begin{array}{r} 4.0 \\ 4.0 \end{array} \begin{array}{r} 4.7 \\ 13 \end{array} \begin{array}{r} 4.5 \\ 15 \end{array} \begin{array}{r} 6.2 \\ 50 \end{array}$$

| Sta. | +    | $\pi$   | -    | Elev.   |
|------|------|---------|------|---------|
|      |      | 921.24  |      |         |
| 52   |      |         | 4.2  | 17.0.   |
| +50  |      |         | 4.4  | 16.8.   |
| 53   |      |         | 4.4  | 16.8.   |
| T.P. | 586  | 922.98. | 4.12 | 917.12. |
| +17  | P.C. |         | 6.2  | 16.8.   |
| +25  |      |         | 6.3  | 16.7.   |
| +50  |      |         | 6.5  | 16.5.   |
| +75  |      |         | 7.6  | 15.4.   |
| +90  |      |         | 5.3  | 17.7.   |
| 54   |      |         | 5.1  | 17.9.   |
| +25  |      |         | 5.0  | 18.0.   |
| +50  |      |         | 8.8  | 14.2.   |
| +75  |      |         | 9.5  | 13.5.   |

|     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|
| 4.0 | 3.8 | 4.6 |     | 5.0 | 4.7 | 7.6 |
| 50  | 15  | 14  | 4.2 | 12  | 15  | 50  |

|     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|
| 3.8 | 4.4 | 4.7 |     | 5.0 | 4.8 | 6.3 |
| 50  | 17  | 14  | 4.4 | 13  | 15  | 50  |

|     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|
| 4.5 | 3.9 | 4.9 |     | 5.2 | 3.9 | 6.3 |
| 50  | 16  | 14  | 4.4 | 13  | 16  | 50  |

Spika P.P

R153+

|     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 6.1 | 5.9 | 5.5 | 6.7 | 6.5 | 6.4 | 6.8 | 5.3 | 5.6 | 6.7 |
| 50  | 33  | 17  | 13  | 9   | 6.2 | 7   | 13  | 16  | 30  |

|     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 6.1 | 5.9 | 5.6 | 6.8 | 6.6 | 6.4 | 6.9 | 5.4 | 5.6 | 6.7 |
| 50  | 33  | 16  | 14  | 10  | 6.3 | 6   | 13  | 16  | 29  |

|     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 6.0 | 5.9 | 5.6 | 7.2 | 6.9 | 6.7 | 6.9 | 5.4 | 5.3 | 6.4 |
| 50  | 37  | 24  | 21  | 15  | 6.5 | 4   | 10  | 12  | 28  |

|     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|
| 6.0 | 6.2 | 7.4 | 7.0 | 7.4 | 5.9 | 5.3 | 5.9 |
| 50  | 34  | 31  | 21  | 7.6 | 4   | 5   | 22  |

4

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 6.2 | 6.0 | 7.5 | 6.9 | 7.0 | 7.7 | 6.5 | 4.8 | 5.7 |
| 50  | 38  | 33  | 24  | 16  | 4   | 3   | 5.3 | 22  |

4

|     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|
| 7.9 | 7.8 | 6.8 | 7.2 | 7.7 | 5.6 | 5.2 | 5.8 |
| 50  | 42  | 27  | 20  | 7   | 4   | 5.1 | 20  |

4

|     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|
| 7.9 | 7.4 | 7.5 | 8.1 | 5.2 | 5.1 | 5.6 |
| 50  | 42  | 22  | 9   | 4   | 5.0 | 11  |

4

|     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 8.9 | 9.6 | 9.5 | 8.6 | 8.1 | 8.2 | 8.0 | 5.1 | 5.3 | 5.6 |
| 52  | 49  | 35  | 32  | 25  | 19  | 8.8 | 5   | 10  | 24  |

4

|      |      |      |      |     |     |     |      |      |     |     |
|------|------|------|------|-----|-----|-----|------|------|-----|-----|
| 10.6 | 10.6 | 11.6 | 11.2 | 9.2 | 9.0 | 9.7 | 10.4 | 6.0  | 5.5 | 6.2 |
| 50   | 39   | 36   | 28   | 17  | 10  | 9.5 | 6    | 8.11 | 19  | 50  |

| Sta. | +        | $\pi$   | -     | Elev    |
|------|----------|---------|-------|---------|
|      |          | 922.98. |       |         |
| 55   |          |         | 9.7   | 13.3.   |
| T.P. | 3.40     | 915.50. | 10.88 | 912.10. |
| +32  | P.T.     |         | 3.5   | 12.0.   |
| +66  |          |         | 4.5   | 11.0.   |
| 56   |          |         | 5.2   | 10.3.   |
| +19  |          |         | 5.6   | 09.9.   |
| +31  | 24" C.M. |         | 5.5   | 10.0.   |
| +39  |          |         | 5.5   | 10.0.   |
| +61  |          |         | 5.5   | 10.0.   |
| 57   |          |         | 5.2   | 10.3.   |
| +50  |          |         | 4.5   | 11.0.   |
| T.P. | 8.41     | 920.17. | 3.74  | 911.76. |
| 58   |          |         | 8.2   | 12.0.   |
| +50  |          |         | 6.6   | 13.6.   |



$\frac{15.4}{50} \frac{14.7}{41} \frac{12.5}{34} \frac{13.0}{28} \frac{12.8}{19} \frac{10.1}{13} \frac{9.7}{9.7} \frac{10.0}{5} \frac{10.7}{13} \frac{11.6}{15.17} \frac{7.8}{24} \frac{7.3}{32} \frac{7.9}{50}$

$\frac{12.0}{50} \frac{11.3}{33} \frac{8.4}{26} \frac{7.6}{16} \frac{4.5}{11} \frac{3.6}{8} \frac{3.5}{3.5} \frac{4.0}{14} \frac{5.9}{19.21} \frac{4.6}{24} \frac{3.3}{36} \frac{2.4}{50}$

$\frac{12.6}{50} \frac{11.3}{29} \frac{9.2}{16} \frac{4.5}{7} \frac{4.5}{4.5} \frac{4.8}{14} \frac{7.8}{21.22} \frac{7.2}{25} \frac{5.9}{35} \frac{5.2}{50}$

$\frac{14.0}{50} \frac{13.2}{27} \frac{11.2}{16} \frac{5.3}{7} \frac{5.2}{5.2} \frac{5.4}{14} \frac{10.2}{24} \frac{11.2}{30} \frac{9.3}{34} \frac{8.4}{50}$

$\frac{17.1}{50} \frac{18.8}{31} \frac{16.1}{20} \frac{5.6}{6} \frac{5.6}{5.6} \frac{6.0}{14} \frac{15.9}{31} \frac{12.5}{33} \frac{12.0}{50}$

FL FL Ditch  
 $\frac{21.1}{50} \frac{21.4}{27} \frac{22.1}{28} \frac{21.9}{28} \frac{16.1}{25} \frac{16.0}{20} \frac{5.9}{7} \frac{5.5}{5.5} \frac{5.7}{14} \frac{15.9}{38} \frac{22.5}{31} \frac{21.2}{31} \frac{21.4}{50}$

$\frac{15.7}{50} \frac{17.4}{39} \frac{16.0}{23} \frac{5.9}{7} \frac{5.5}{5.5} \frac{5.7}{14} \frac{15.4}{31} \frac{16.4}{50}$

$\frac{15.0}{50} \frac{11.8}{20} \frac{5.5}{6} \frac{5.5}{5.5} \frac{5.8}{14} \frac{12.5}{27} \frac{15.1}{50}$

$\frac{11.8}{50} \frac{11.5}{30} \frac{10.1}{16} \frac{5.3}{2} \frac{5.2}{5.2} \frac{5.8}{15} \frac{14.5}{27} \frac{15.2}{50}$

$\frac{5.3}{50} \frac{7.1}{25} \frac{6.8}{13} \frac{4.7}{8} \frac{4.5}{4.5} \frac{4.8}{15} \frac{10.6}{26} \frac{11.8}{38} \frac{12.6}{50}$

$\frac{5.7}{50} \frac{6.9}{27} \frac{9.2}{17} \frac{8.4}{8.2} \frac{8.2}{11} \frac{9.4}{19} \frac{9.7}{25} \frac{12.0}{50}$

$\frac{2.2}{50} \frac{2.8}{32} \frac{5.5}{22} \frac{6.8}{13} \frac{6.6}{6.6} \frac{6.7}{12} \frac{7.3}{20} \frac{6.5}{22} \frac{6.8}{39} \frac{7.7}{50}$

| Sta. | +    | $\pi$   | -    | Elev.   |
|------|------|---------|------|---------|
|      |      | 920.17. |      |         |
| 59   |      |         | 4.8  | 15.4.   |
| T.P. | 7.98 | 926.48. | 1.67 | 918.50. |
| +50  |      |         | 9.6  | 16.9.   |
| 60   |      |         | 8.2  | 18.3.   |
| +50  |      |         | 6.6  | 19.9.   |
| 61   |      |         | 5.4  | 21.1.   |
| +50  |      |         | 4.3  | 22.2.   |
| 62   |      |         | 3.6  | 22.9.   |
| +50  |      |         | 3.1  | 23.4.   |
| T.P. | 6.45 | 929.57. | 3.36 | 923.12. |
| 63   |      |         | 5.7  | 23.9.   |
| +50  |      |         | 5.3  | 24.3.   |
| 64   |      |         | 5.3  | 24.3.   |
| +50  |      |         | 5.2  | 24.4.   |

$\begin{array}{r} 1.3 \\ 50 \end{array}$ 
 $\begin{array}{r} 2.8 \\ 30 \end{array}$ 
 $\begin{array}{r} 3.3 \\ 26.22 \end{array}$ 
 $\begin{array}{r} 2.5 \\ 18 \end{array}$ 
 $\begin{array}{r} 4.9 \\ 13 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 10 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 4.8 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 12 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 18 \end{array}$ 
 $\begin{array}{r} 3.8 \\ 23 \end{array}$ 
 $\begin{array}{r} 3.6 \\ 36 \end{array}$ 
 $\begin{array}{r} 4.0 \\ 50 \end{array}$

$\begin{array}{r} 6.6 \\ 50 \end{array}$ 
 $\begin{array}{r} 8.1 \\ 31 \end{array}$ 
 $\begin{array}{r} 7.5 \\ 18 \end{array}$ 
 $\begin{array}{r} 10.0 \\ 13 \end{array}$ 
 $\begin{array}{r} 10.0 \\ 8 \end{array}$ 
 $\begin{array}{r} 9.6 \\ 9.6 \end{array}$ 
 $\begin{array}{r} 10.0 \\ 18 \end{array}$ 
 $\begin{array}{r} 8.8 \\ 21 \end{array}$ 
 $\begin{array}{r} 8.9 \\ 35 \end{array}$ 
 $\begin{array}{r} 9.2 \\ 50 \end{array}$

$\begin{array}{r} 4.7 \\ 50 \end{array}$ 
 $\begin{array}{r} 5.3 \\ 19 \end{array}$ 
 $\begin{array}{r} 8.4 \\ 12 \end{array}$ 
 $\begin{array}{r} 8.4 \\ 6 \end{array}$ 
 $\begin{array}{r} 8.2 \\ 8.2 \end{array}$ 
 $\begin{array}{r} 8.5 \\ 14 \end{array}$ 
 $\begin{array}{r} 8.5 \\ 19 \end{array}$ 
 $\begin{array}{r} 7.4 \\ 22 \end{array}$ 
 $\begin{array}{r} 7.5 \\ 39 \end{array}$ 
 $\begin{array}{r} 8.0 \\ 50 \end{array}$

$\begin{array}{r} 4.4 \\ 50 \end{array}$ 
 $\begin{array}{r} 4.4 \\ 19 \end{array}$ 
 $\begin{array}{r} 6.4 \\ 12 \end{array}$ 
 $\begin{array}{r} 6.8 \\ 10 \end{array}$ 
 $\begin{array}{r} 6.6 \\ 6.6 \end{array}$ 
 $\begin{array}{r} 7.0 \\ 15 \end{array}$ 
 $\begin{array}{r} 6.8 \\ 19 \end{array}$ 
 $\begin{array}{r} 5.6 \\ 22 \end{array}$ 
 $\begin{array}{r} 5.8 \\ 40 \end{array}$ 
 $\begin{array}{r} 6.1 \\ 50 \end{array}$

$\begin{array}{r} 5.3 \\ 50 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 31 \end{array}$ 
 $\begin{array}{r} 4.6 \\ 17 \end{array}$ 
 $\begin{array}{r} 5.2 \\ 11 \end{array}$ 
 $\begin{array}{r} 5.8 \\ 9 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 5.4 \end{array}$ 
 $\begin{array}{r} 5.7 \\ 15 \end{array}$ 
 $\begin{array}{r} 6.0 \\ 19 \end{array}$ 
 $\begin{array}{r} 4.5 \\ 22 \end{array}$ 
 $\begin{array}{r} 4.0 \\ 28 \end{array}$ 
 $\begin{array}{r} 4.4 \\ 50 \end{array}$

$\begin{array}{r} 5.6 \\ 50 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 29 \end{array}$ 
 $\begin{array}{r} 4.5 \\ 18 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 9 \end{array}$ 
 $\begin{array}{r} 4.3 \\ 4.3 \end{array}$ 
 $\begin{array}{r} 4.6 \\ 16 \end{array}$ 
 $\begin{array}{r} 4.3 \\ 21 \end{array}$ 
 $\begin{array}{r} 4.0 \\ 28 \end{array}$ 
 $\begin{array}{r} 4.0 \\ 50 \end{array}$

$\begin{array}{r} 4.9 \\ 50 \end{array}$ 
 $\begin{array}{r} 4.3 \\ 30 \end{array}$ 
 $\begin{array}{r} 4.4 \\ 23 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 14 \end{array}$ 
 $\begin{array}{r} 4.1 \\ 3.6 \end{array}$ 
 $\begin{array}{r} 4.0 \\ 17 \end{array}$ 
 $\begin{array}{r} 3.9 \\ 24 \end{array}$ 
 $\begin{array}{r} 3.8 \\ 42 \end{array}$ 
 $\begin{array}{r} 4.0 \\ 50 \end{array}$

$\begin{array}{r} 3.4 \\ 50 \end{array}$ 
 $\begin{array}{r} 3.5 \\ 24 \end{array}$ 
 $\begin{array}{r} 3.5 \\ 9 \end{array}$ 
 $\begin{array}{r} 3.1 \\ 3.1 \end{array}$ 
 $\begin{array}{r} 3.8 \\ 18 \end{array}$ 
 $\begin{array}{r} 3.3 \\ 23 \end{array}$ 
 $\begin{array}{r} 3.7 \\ 50 \end{array}$

$\begin{array}{r} 5.4 \\ 50 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 26 \end{array}$ 
 $\begin{array}{r} 3.3 \\ 13 \end{array}$ 
 $\begin{array}{r} 6.1 \\ 9 \end{array}$ 
 $\begin{array}{r} 5.7 \\ 5.7 \end{array}$ 
 $\begin{array}{r} 6.2 \\ 17 \end{array}$ 
 $\begin{array}{r} 5.2 \\ 23 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 37 \end{array}$ 
 $\begin{array}{r} 5.7 \\ 50 \end{array}$

$\begin{array}{r} 4.4 \\ 50 \end{array}$ 
 $\begin{array}{r} 4.5 \\ 31 \end{array}$ 
 $\begin{array}{r} 4.6 \\ 15 \end{array}$ 
 $\begin{array}{r} 5.7 \\ 8 \end{array}$ 
 $\begin{array}{r} 5.3 \\ 5.3 \end{array}$ 
 $\begin{array}{r} 5.6 \\ 18 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 23 \end{array}$ 
 $\begin{array}{r} 4.1 \\ 32 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 40 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 50 \end{array}$

$\begin{array}{r} 5.1 \\ 50 \end{array}$ 
 $\begin{array}{r} 4.9 \\ 33 \end{array}$ 
 $\begin{array}{r} 5.3 \\ 21 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 15 \end{array}$ 
 $\begin{array}{r} 5.6 \\ 9 \end{array}$ 
 $\begin{array}{r} 5.3 \\ 5.3 \end{array}$ 
 $\begin{array}{r} 5.5 \\ 18 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 24 \end{array}$ 
 $\begin{array}{r} 4.3 \\ 41 \end{array}$ 
 $\begin{array}{r} 4.5 \\ 50 \end{array}$

$\begin{array}{r} 6.6 \\ 50 \end{array}$ 
 $\begin{array}{r} 6.1 \\ 21 \end{array}$ 
 $\begin{array}{r} 5.6 \\ 20 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 10 \end{array}$ 
 $\begin{array}{r} 5.7 \\ 9 \end{array}$ 
 $\begin{array}{r} 5.2 \\ 5.2 \end{array}$ 
 $\begin{array}{r} 5.6 \\ 18 \end{array}$ 
 $\begin{array}{r} 4.6 \\ 23 \end{array}$ 
 $\begin{array}{r} 3.8 \\ 32 \end{array}$ 
 $\begin{array}{r} 3.7 \\ 40 \end{array}$ 
 $\begin{array}{r} 4.2 \\ 50 \end{array}$

| Sta     | + | 7      | -    | Elev              |
|---------|---|--------|------|-------------------|
|         |   | 929.57 |      |                   |
| 64 + 79 |   |        | 5.1  | 24.5'             |
| + 93    |   |        | 5.1  | 24.5'             |
| 65 + 07 |   |        | 5.1  | 24.5'             |
| + 23    |   |        | 5.3  | 24.3'             |
| B.M.    |   |        | 4.14 | 925.43' (925.45') |

Lt

X

Rt

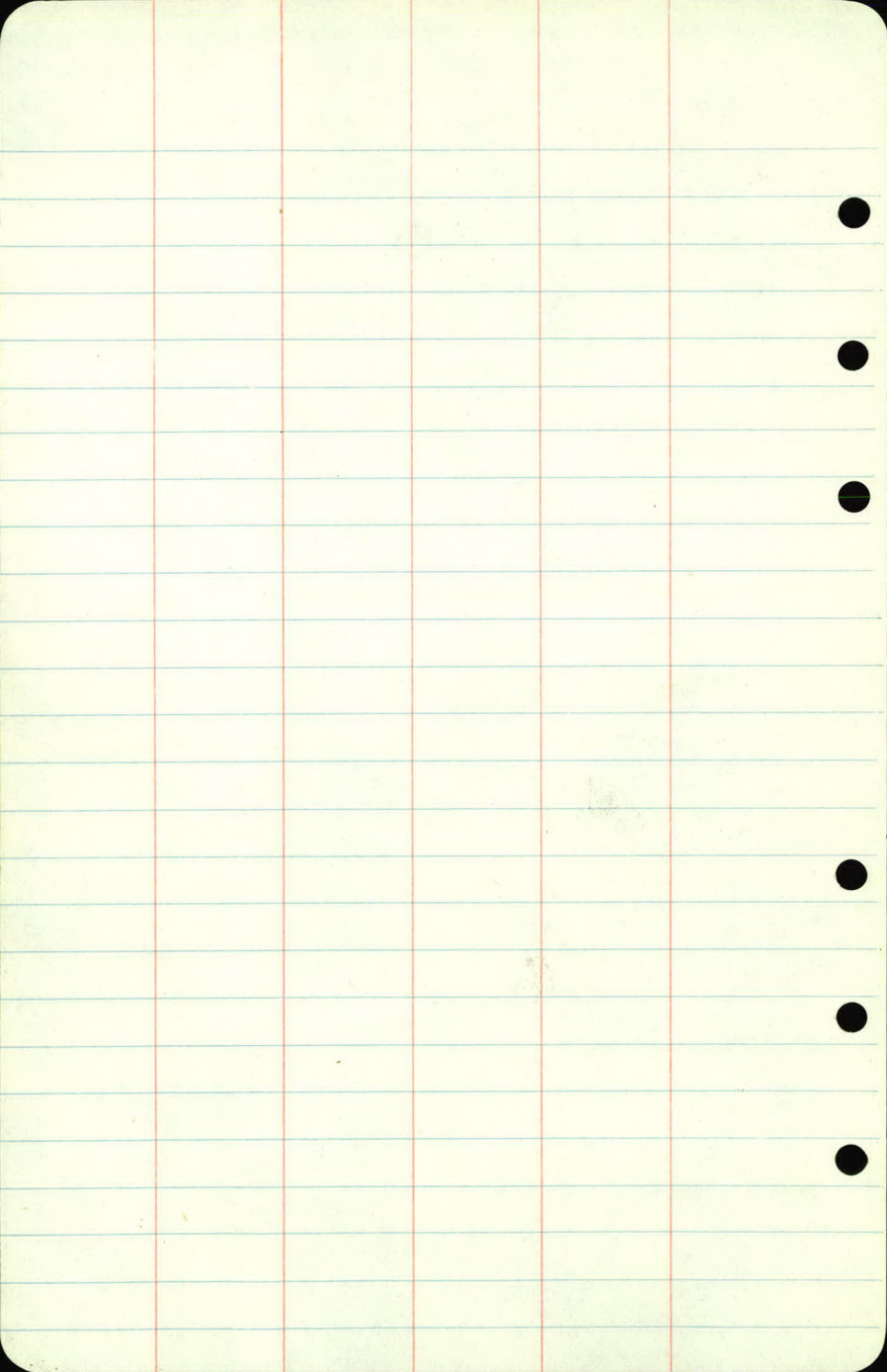
|                  |                  |                  |                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| $\frac{7.3}{50}$ | $\frac{7.1}{38}$ | $\frac{5.8}{31}$ | $\frac{5.3}{18}$ | $\frac{5.6}{15}$ | $\frac{5.1}{51}$ | $\frac{5.6}{18}$ | $\frac{4.9}{20}$ | $\frac{4.8}{30}$ | $\frac{4.3}{50}$ |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|

|                  |                  |                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| $\frac{5.7}{50}$ | $\frac{5.7}{37}$ | $\frac{5.2}{12}$ | $\frac{5.1}{51}$ | $\frac{5.4}{13}$ | $\frac{6.0}{22}$ | $\frac{4.3}{25}$ | $\frac{4.3}{50}$ |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|

|                  |                  |                  |                  |                  |                  |
|------------------|------------------|------------------|------------------|------------------|------------------|
| $\frac{5.2}{50}$ | $\frac{5.5}{51}$ | $\frac{4.2}{16}$ | $\frac{7.5}{29}$ | $\frac{7.3}{37}$ | $\frac{7.3}{50}$ |
|------------------|------------------|------------------|------------------|------------------|------------------|

|                  |                  |                  |
|------------------|------------------|------------------|
| $\frac{5.3}{53}$ | $\frac{5.7}{33}$ | $\frac{6.1}{50}$ |
|------------------|------------------|------------------|





Cross sections of Borrow.

• S. W. Cor. Co. Rd "F" & Victoria

Stationing Runs So. along & Victoria

| Sta. | +             | $\pi$  | -   | Elev.  |
|------|---------------|--------|-----|--------|
| B.M. | 9.91          | 990.86 |     | 980.95 |
| 0+00 | E. C. Rd. "F" |        | 9.9 | 81.0   |
| +25  |               |        | 9.8 | 81.1   |
| +50  |               |        | 9.7 | 81.2   |
| +100 |               |        | 9.2 | 81.7   |
| +50  |               |        | 8.6 | 82.3   |
| +67  |               |        | 8.3 | 82.6   |
| +200 |               |        | 7.8 | 83.1   |
| +38  |               |        | 7.2 | 83.7   |
| +300 |               |        | 6.1 | 84.8   |
| +50  | E. Ent.       |        | 5.4 | 85.5   |

£

# Top Spike & Co. Rd. F. of Victoria

9.9      10.8      11.3      11.1  
50      100      150

FL 12 CM

9.8      10.2      11.8      11.9      10.1      10.3      10.7      13.0      13.5      14.1      13.5  
17      22      31      33      50      67      100      132      133      150

9.7      9.8      11.6      11.9      8.6      9.2      9.7      11.4      12.9  
14      20      28      32      50      70      100      150

9.2      9.6      11.1      11.2      4.5      5.2      6.8      8.1      11.4  
15      20      27      32      50      86      100      150

8.6      9.0      10.6      2.5      2.7      3.7      6.4      11.0  
15      21-26      33      50      75      100      150

8.3      8.8      10.4      2.4      2.8      3.8      6.3      11.3  
17      20-26      33      50      78      100      150

7.8      8.1      9.9      3.1      3.6      4.6      7.5      11.2  
16      20-26      33      50      75      100      150

7.2      7.6      9.3      3.6      4.2      8.4      10.7  
16      21-28      33      50      100      150

6.1      6.5      8.5      8.8      6.4      8.3      11.3      11.4  
16      22      29      33      50      100      115

5.4      5.9      7.4      7.8      6.5      8.9      11.7      11.8  
17      22      30      31      50      81      100

£

| Sta. | s    | K      | - | Elev.  |
|------|------|--------|---|--------|
| B.M. | 9.91 | 990.86 |   | 980.95 |

Note: Contacted John Syka in field - he suggested slope E. side Victoria out approximately 50. ft.

|      |  |     |       |
|------|--|-----|-------|
| 0+50 |  | 9.7 | 81.2. |
|------|--|-----|-------|

|   |  |     |       |
|---|--|-----|-------|
| 1 |  | 9.2 | 81.7. |
|---|--|-----|-------|

|     |  |     |       |
|-----|--|-----|-------|
| +50 |  | 8.6 | 82.3. |
|-----|--|-----|-------|

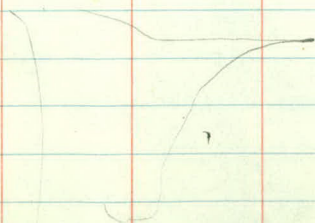
|     |  |     |       |
|-----|--|-----|-------|
| +67 |  | 8.3 | 82.6. |
|-----|--|-----|-------|

|   |  |     |       |
|---|--|-----|-------|
| 2 |  | 7.8 | 83.1. |
|---|--|-----|-------|

|     |  |     |       |
|-----|--|-----|-------|
| +38 |  | 7.2 | 83.7. |
|-----|--|-----|-------|

|   |  |     |       |
|---|--|-----|-------|
| 3 |  | 6.1 | 84.8. |
|---|--|-----|-------|

|     |  |     |       |
|-----|--|-----|-------|
| +50 |  | 5.4 | 85.5. |
|-----|--|-----|-------|





Top Spike & Co. Rd. "F" and Victoria

$$\begin{array}{r} 123 \\ 75 \end{array} \quad \begin{array}{r} 11.7 \\ 50 \end{array} \quad \begin{array}{r} 10.7 \\ 34 \end{array} \quad \begin{array}{r} 12.3 \\ 32 \end{array} \quad \begin{array}{r} 12.1 \\ 22 \end{array} \quad \begin{array}{r} 10.0 \\ 17 \end{array} \quad 9.7$$

$$\begin{array}{r} 10.0 \\ 75 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 34 \end{array} \quad \begin{array}{r} 11.7 \\ 30 \end{array} \quad \begin{array}{r} 11.5 \\ 22 \end{array} \quad \begin{array}{r} 9.8 \\ 17 \end{array} \quad 9.2$$

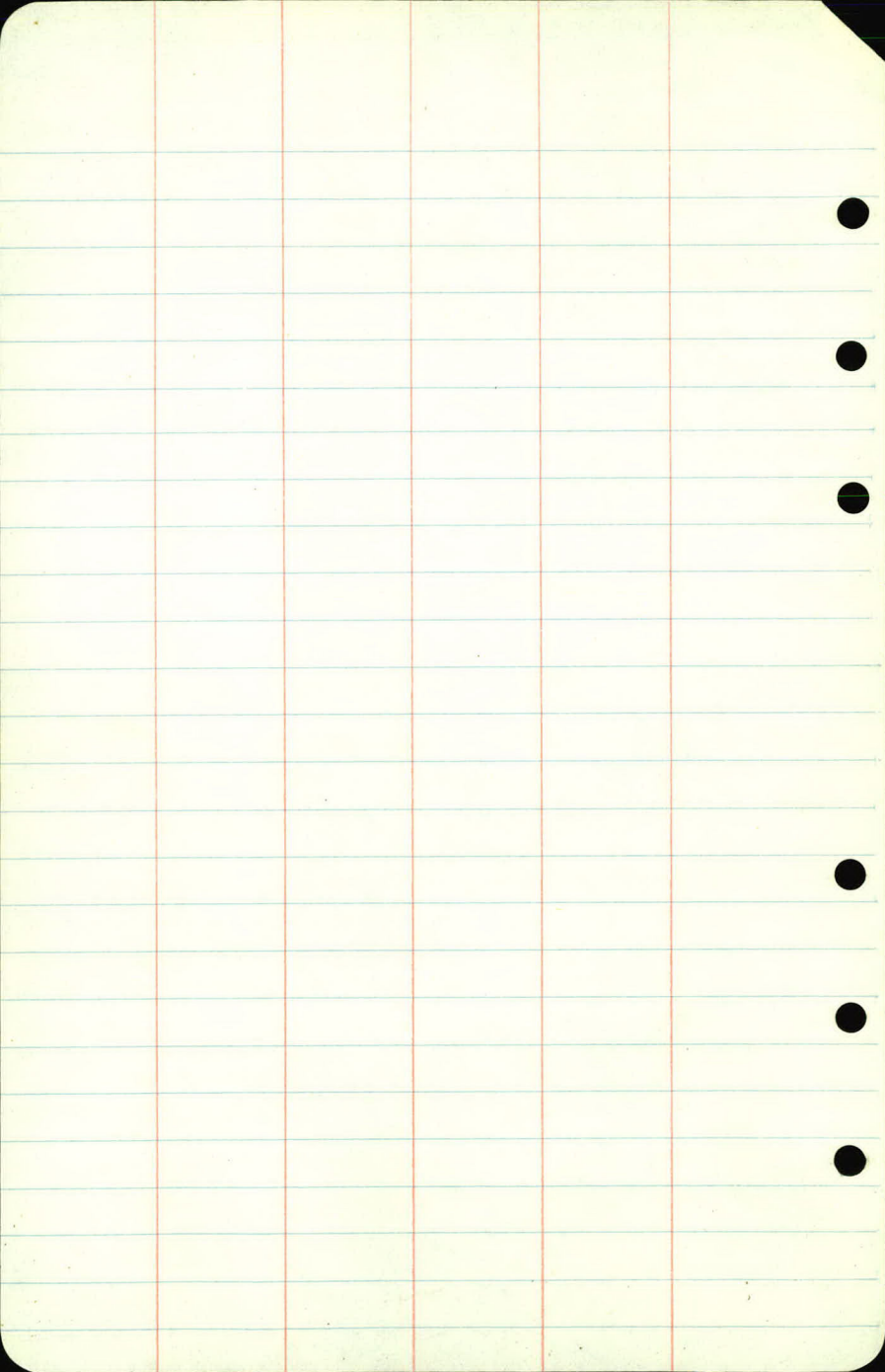
$$\begin{array}{r} 8.5 \\ 75 \end{array} \quad \begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 33 \end{array} \quad \begin{array}{r} 11.0 \\ 28 \end{array} \quad \begin{array}{r} 10.8 \\ 22 \end{array} \quad \begin{array}{r} 8.9 \\ 17 \end{array} \quad 8.6$$

$$\begin{array}{r} 8.3 \\ 75 \end{array} \quad \begin{array}{r} 7.1 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array} \quad \begin{array}{r} 10.5 \\ 29 \end{array} \quad \begin{array}{r} 10.2 \\ 21 \end{array} \quad \begin{array}{r} 8.8 \\ 17 \end{array} \quad 8.3$$

$$\begin{array}{r} 7.9 \\ 75 \end{array} \quad \begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array} \quad \begin{array}{r} 10.0 \\ 28 \end{array} \quad \begin{array}{r} 9.7 \\ 21 \end{array} \quad \begin{array}{r} 8.2 \\ 17 \end{array} \quad 7.8$$

$$\begin{array}{r} 7.7 \\ 75 \end{array} \quad \begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 4.8 \\ 34 \end{array} \quad \begin{array}{r} 9.3 \\ 30 \end{array} \quad \begin{array}{r} 9.3 \\ 22 \end{array} \quad \begin{array}{r} 7.6 \\ 17 \end{array} \quad 7.2$$

$$\begin{array}{r} 7.0 \\ 75 \end{array} \quad \begin{array}{r} 7.7 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 8.9 \\ 29 \end{array} \quad \begin{array}{r} 8.5 \\ 21 \end{array} \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad 6.1$$



SNAIL LAKE BLVD.

Clearing & Grubbing Notes.

Direct Ties.

12

11

10

+95 - 29'  
+76 - 29' - 35'

9

8

+86 - 12' - 36'  
+83 - 12' - 12' - 21' - 26'  
7 +83 - 5'ump 10' - 26'

~~No Trees~~

1

Lt.

Rt.

+18 - 40'-43'  
+07 - 31'

+66 42'  
+55 Twin 29'  
+20 37'  
+10 - 36'

+68 - 36' ←  
+61 45'  
+59 24'-45'  
+52 - 34'-40'  
+43 - 30kts - 29'  
+40 45'  
+36 35'  
+21 36'  
+16 36'  
+00 - 44' ←

+50 6" - 43'  
+46-2-42-44'  
+41-30kts-46'  
+29-12"-40'  
+03 15" 25'  
+02-12" 4.5'  
← +60-12"-27'  
+58-12"-8"-3'-9'  
+54-8"-16'  
+46-6"-30'  
+42-8"-11'  
+42-8-5-15-16-20-35'  
+36-8"-21'  
+33-12"-3'  
+16-15" Dkt 2'

+06-15" Dkt 15'



21

20

X No Trees  
or Brush

18

17

X No Trees  
or Brush

15

14

13

+99 27'

+73 Stump 26'

+52 Stump 39'

+42 - 50'

+00 43'

+91 - 30'

+83 - 19'

+93-2 33'  
+87-3 29'-35'  
+70-Twin Apples 36'  
+54-2- 35'  
+40 - 35'  
+36 - 32'  
+34 - 32'  
+06 Stump 33'

+90-2 Apples 33'  
+77 " 32'  
+47-2 " 32'  
+34 " 32'  
+32 " 32'

X

X

+96 Stump 31'

+65 - 30'

X

X

+30 Stump - 30'  
+22 - 26'  
+16 - 26'

+95 - 25'  
+84 - 25'

+02 - 40'

28

+25 Brush Xs  $\frac{1}{2}$

27

26

+100 Brush Xs  $\frac{1}{2}$

+75 Brush -  $\frac{1}{4}$ 0

25

Begin Brush  
25+00 25' Rt.

24

+50 Brush Lt.  
Begins 32'

23

22

+86 - 70'

+123 - 47'

+67 30'

+54 3'

Brush

+96 .05'  
+80-2 4-38'  
+71 34'  
+61 33'  
+38 43'  
+30 2'

+32 13'  
+09 3'  
+00 Twin 16'

+95 9'  
+87 21'  
+86 13'  
+57 7'

+29 Stump 13'

+02 5'

+86 7'  
+83 36'

+50 16'

+11 40'

+85 33'

+78 Twin 28'

+63 37'

+54 29'

+49 31'

+00-2 46'-48'

+83 50'

+37-2 46'-48'  
+30 Stump 33'  
+26 36'  
+14 Twin 34'  
+08 44'  
+05 39'

+74 - 28'

+62 - 27'

Brush

+75 - 48'

+63 - 41'

+90 Stump 32'

+56 - 29'

+37 - 32'

35

34

33

32

31

30

29



+90 Stump end

+67 6'  
+36 6'  
+26 Stump 18'

+94 32'

+82 28  
+50 37  
+41 26  
+38 25  
+28 Stump 26 44'  
+24 45'  
+21 44'  
+19 43'  
+99 21'

+95 Stump 22  
+88 31  
+62 50

+63 39'  
+40 22'  
+38 33'

+28 Stump 34'

+90 32'  
+78 Stump 41'  
+70 29'  
+67 Stump 32'  
+64 36'  
+47 30'  
+24 45'

+98-2- 51'  
+89 46'  
+68 21'  
+59 25'  
+36 12'  
+20 Stump 23'  
+10-2- 26-28'  
+00 - 48'  
+94 - 44'

+52 - 72'

+18 Stump 70'

BRUSH

42

41

40

39

38

37

36

+68 - 15'

+74 18'

+07 20'

+69 36'  
+63 29'  
+45 43'  
+31 25'

+54 44'  
+37 34'  
+34 34'

+44 17'  
+42 42'  
+41 49'

+97 13'  
+75 45'  
+71 37'  
+55 34'  
+52 37'  
+45 29'  
+39 30'  
+30 22'  
+00 23'

+83 20'

+70 20'

+35 28'

+19 - 1'

51



49  
~~48~~

47



46

45

44

43



51+81 15'



49+69

29'



+03  
+00

29' 31"



|        |         |
|--------|---------|
| +12-2- | 19'-20" |
| +04    | 20      |
| +01    | 21      |
| +85    | 22'     |
| +73    | 22'     |
| +71    | 20'     |
| +65    | 22'     |
| +52    | 20      |
| +46    | 21'     |
| +36    | 19'     |
| +31-   | 17'     |

+74 17'

+72 18'

+58 15'



+80 End Timber 35'

58

+80 Begin Timber 35'

+50 Begin 2" Timber 40'

57

+20 End 2" Timber 25'

56

Apple Orch.

+90 End 35

+88 - 34

55 +81 - 34

54

53

Note 2" Timber  
Begins Lt & Rt.  
at Fe. Cor.  
Approx. 50+00

52

+65 End Orch. 15'  
 +60 " 15'  
 +50 " 34  
 +44 " 32  
 +37 " 32  
 +30 " 31  
 +19 " 32  
 +14 " 31  
 +10 " 31  
 +04 " 30

+96 Orch. 33'  
 +91 " 32'  
 +80 " 33'  
 +77 " 32'  
 +74 " 33'  
 +68 Beg in Orch. 33'  
 +25 " 34  
 +09 Pop 39

+12 · 2 · 27.30

# Apple Orch.

+74 " 34-40.45  
 +63 " 40'  
 +45 " 36  
 +39 " 43  
 +29 " 42  
 +21 " 40  
 +09 " 42  
 +02 " 45

+71 - 9'  
 +58 - 9' 6'  
 +57 - 9' 42'

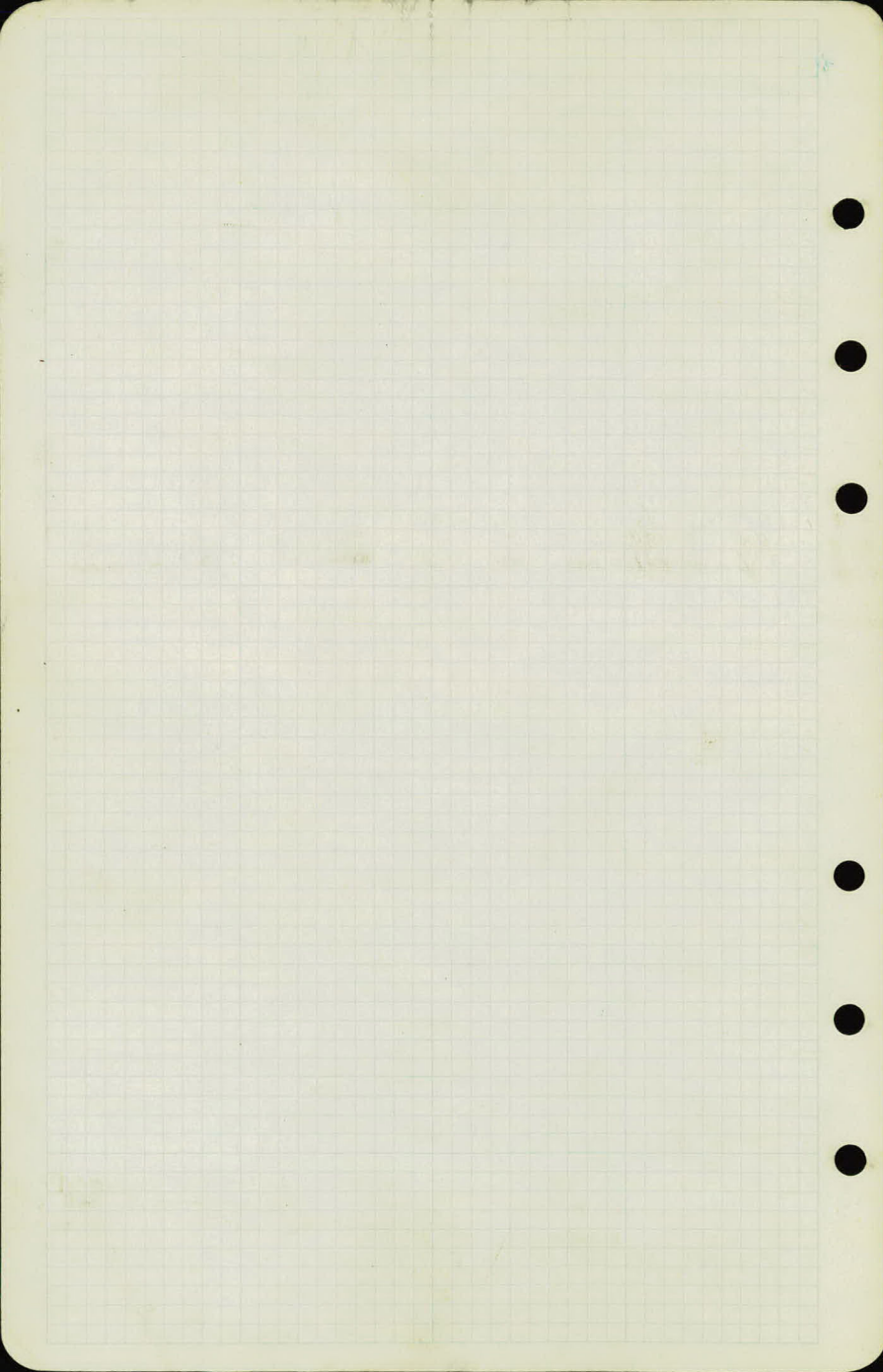
+85 37'  
 +70 43

+49 - 30'

+50 29'  
 +47 47'  
 +46 50'  
 +02 25'  
 +00 42'

+83 37  
 +76-2-28-30  
 +73 Swamp 18

+26 16'



Slope Stake Notes

SNAIL LAKE BLVD.

| Sta.               | +    | $\pi$               | -    | Elev.  | G.R.           |
|--------------------|------|---------------------|------|--------|----------------|
| B.M.               | 1.91 | 982.86 <sup>9</sup> |      | 980.95 |                |
| + 18               |      |                     |      | 80.3   | 2.6            |
| + 23               |      |                     |      | 80.2   | 2 <sup>-</sup> |
| + 33               |      |                     |      | 79.9   |                |
| + 36               |      |                     |      | 79.8   | 3.1            |
| + 50               |      |                     |      | 79.4   | 3.5            |
| 1                  |      |                     |      | 77.3   | 5.6            |
| + 25<br>spec. Sec. |      |                     |      | 76.0   | 6.9            |
| + 50               |      |                     |      | 74.7   | 8.2            |
| 2                  |      |                     |      | 72.2   | 10.7           |
| + 25               |      |                     |      | 70.9   | 12.0           |
| + 65               |      |                     |      | 68.8   | 14.1           |
| 3                  |      |                     |      | 67.1   | 15.6           |
| T.P.               | 7.23 | 980.77              | 7.32 | 973.54 |                |



Top Bolt Spk. E Victoria & Smail Lake Blvd.

$$\begin{array}{r} 6.1 \\ DC 1.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 3.2 \\ FO.1 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ DC 1.1 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ DC 0.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 3.8 \\ FO.3 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ DC 1.1 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ CO.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 6.1 \\ FO.5 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ CO.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ CO.1 \\ \hline 29.0 \end{array}$$

$$\begin{array}{r} 7.3 \\ FO.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.9 \\ CO.2 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 6.8 \\ CO.1 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 8.1 \\ CO.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ CO.9 \\ \hline 32.8 \end{array}$$

$$\begin{array}{r} 8.1 \\ CO.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 10.5 \\ CO.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.7 \\ CO.0 \\ \hline 37.0 \end{array}$$

$$\begin{array}{r} 8.5 \\ CO.3 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 11.9 \\ CO.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ CO.8 \\ \hline 38.6 \end{array}$$

$$\begin{array}{r} 9.0 \\ CO.1 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 13.8 \\ CO.3 \\ \hline \end{array}$$

$$\begin{array}{r} 7.7 \\ CO.1 \\ \hline 37.8 \end{array}$$

$$\begin{array}{r} 8.9 \\ CO.9 \\ \hline 30.8 \end{array}$$

$$\begin{array}{r} 15.7 \\ CO.1 \\ \hline \end{array}$$

$$\begin{array}{r} 9.8 \\ CO.0 \\ \hline 39.0 \end{array}$$

Spk - T.P. - Pl.

| Sta.   | +    | $\pi$<br>8 | -     | Elev.  |                              |
|--------|------|------------|-------|--------|------------------------------|
|        |      | 980.77     |       |        |                              |
| 3 + 33 |      |            |       | 65.4   | 15.4                         |
| + 68   |      |            |       | 63.6   | 17.2                         |
| 4      |      |            |       | 61.8   | 19.0                         |
| + 32   |      |            |       | 60.0   | 20.8                         |
| + 80   |      |            |       | 57.2   | 0.0<br>23.6<br>26.0          |
| 5      |      |            |       | 55.8   | 0.3<br>25.0<br>26.3          |
| + 40   |      |            |       | 53.2   | 28.4<br>29.8<br>28.8<br>26.8 |
| T.P.   | 0.01 | 967.99     | 12.79 | 967.98 | 18.1                         |
| P.C.   |      |            |       |        | 1.1                          |
| + 72   |      |            |       | 51.0   | 17.0<br>1.1<br>15.9          |
|        |      |            |       |        | 17.5<br>1.2<br>18.9          |
| 6      |      |            |       | 49.1   | 1.4<br>20.1<br>20.8          |
| + 50   |      |            |       | 45.6   | 1.2<br>22.4<br>1.4<br>23.6   |
| T.P.   | 0.37 | 955.87     | 12.49 | 955.50 | 10.8                         |
| P.T.   |      |            |       |        | 1.1                          |
| + 73   |      |            |       | 44.0   | 11.9<br>1.1<br>13.0          |
|        |      |            |       |        | 12.9<br>0.8<br>13.7<br>0.8   |
| 7      |      |            |       | 42.2   | 14.5                         |
| T.P.   | 1.91 | 944.60     | 13.18 | 942.69 |                              |

$$\begin{array}{r} 5.8 \\ C 9.2 \\ \hline 34.3 \end{array}$$

$$\begin{array}{r} 15.3 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 9.0 \\ C 6.4 \\ \hline 39.8 \end{array}$$

$$\begin{array}{r} 15.7 \\ C 1.5 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 16.6 \\ C 0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 9.7 \\ C 7.5 \\ \hline 42.0 \end{array}$$

$$\begin{array}{r} 17.9 \\ C 1.1 \\ \hline 22.1 \end{array}$$

$$\begin{array}{r} 18.6 \\ C 0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 8.7 \\ C 10.3 \\ \hline 47.6 \end{array}$$

$$\begin{array}{r} 19.3 \\ C 1.5 \\ \hline 22.7 \end{array}$$

$$\begin{array}{r} 20.5 \\ C 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ C 14.3 \\ \hline 55.6 \end{array}$$

$$\begin{array}{r} 23.1 \\ C 1.5 \\ \hline 22.7 \end{array}$$

$$\begin{array}{r} 23.5 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 2.6 \\ C 26.0 \\ \hline 69.0 \end{array}$$

$$\begin{array}{r} 24.3 \\ C 1.0 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 24.9 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 2.8 \\ C 22.4 \\ \hline 72.8 \end{array}$$

W. 0.0

$$\begin{array}{r} 27.0 \\ C 1.4 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 27.6 \\ C 0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ C 20.6 \\ \hline 68.2 \end{array}$$

E.W. 0.2

$$\begin{array}{r} 14.1 \\ C 4.0 \\ \hline 27.9 \end{array}$$

$$\begin{array}{r} 16.7 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 0.6 \\ C 15.3 \\ \hline 57.6 \end{array}$$

E.W. 1.4

$$\begin{array}{r} 6.8 \\ C 13.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 18.9 \\ C 0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 7.1 \\ C 10.4 \\ \hline 47.8 \end{array}$$

W. 2.5

$$\begin{array}{r} 11.1 \\ C 12.5 \\ \hline 48.0 \end{array}$$

$$\begin{array}{r} 22.1 \\ C 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 16.8 \\ C 4.0 \\ \hline 35.0 \end{array}$$

W. 2.5

$$\begin{array}{r} 4.6 \\ C 8.4 \\ \hline 34.5 \end{array}$$

$$\begin{array}{r} 11.7 \\ C 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ C 2.6 \\ \hline 36.2 \end{array}$$

W. 1.4

$$\begin{array}{r} 10.6 \\ C 3.9 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 14.4 \\ F 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 13.7 \\ C 6.1 \\ \hline 25.4 \end{array}$$

W. 0.2

| Sta.            | +    | $\pi$  | -     | Elev.  |                                                                                         |
|-----------------|------|--------|-------|--------|-----------------------------------------------------------------------------------------|
|                 |      | 944.60 |       |        |                                                                                         |
| 7 + 37          |      |        |       | 39.6   | 0.0<br>0.5<br>0.0                                                                       |
| T.P.<br>End Sec | 0.33 | 939.88 | 5.05  | 939.55 |                                                                                         |
| +45             |      |        |       | 38.9   | 1.0                                                                                     |
| +73             |      |        |       | 37.1   | 2.8                                                                                     |
| 8               |      |        |       | 35.3   | 4.6                                                                                     |
| +23             |      |        |       | 33.7   | 6.2                                                                                     |
| +55             |      |        |       | 31.5   | 8.4                                                                                     |
| T.P.            | 2.10 | 930.03 | 11.95 | 927.93 |                                                                                         |
| 9               |      |        |       | 28.4   | 1.6                                                                                     |
| +19             |      |        |       | 27.0   | 0.0<br>3.0<br>0.5                                                                       |
| +73             |      |        |       | 23.3   | 6.1<br>0.6<br>6.7<br>0.6<br>7.3<br>7.6<br>0.9<br>8.5<br>0.9<br>9.4<br>9.8<br>1.1<br>1.2 |
| 10              |      |        |       | 21.5   | 1.3                                                                                     |
| P.C.<br>+25     |      |        |       | 19.7   | 10.8<br>1.2<br>1.2<br>1.4                                                               |
| +50             |      |        |       | 18.0   | 1.6                                                                                     |
| T.P.            | 1.06 | 919.97 | 11.12 | 918.91 |                                                                                         |



W. 0.0

$$\begin{array}{r} 3.5 \\ C 1.5 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 4.9 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ C 0.2 \\ \hline 27.4 \end{array}$$

$$\begin{array}{r} 1.6 \\ D C 0.4 \\ \hline 19.6 \end{array}$$

$$\begin{array}{r} 0.9 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 0.6 \\ C 0.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ F 2.2 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 4.1 \\ F 1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C 0.0 \\ \hline 2.7 \end{array}$$

$$\begin{array}{r} 9.4 \\ D 4.8 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 8.2 \\ F 3.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ D C 1.8 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 13.4 \\ F 7.2 \\ \hline 29.4 \end{array}$$

$$\begin{array}{r} 11.7 \\ F 5.5 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ D C 1.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 16.4 \\ F 8.0 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 14.7 \\ F 6.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ C 0.2 \\ \hline 27.4 \end{array}$$

$$\begin{array}{r} 9.4 \\ F 7.8 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 5.5 \\ F 3.9 \\ \hline \end{array}$$

$$\begin{array}{r} 12 \\ C 0.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 11.3 \\ F 8.3 \\ \hline 37.6 \end{array}$$

$$\begin{array}{r} 3.5 \\ F 0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 2.7 \\ C 0.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 6.1 \\ G 1.2 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 6.0 \\ C 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 9.3 \\ D C 0.0 \\ \hline 24.6 \end{array}$$

W. 0.0

$$\begin{array}{r} 8.7 \\ D C 0.9 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 8.1 \\ C 0.4 \\ \hline \end{array}$$

W. 2.0

$$\begin{array}{r} 9.8 \\ C 0.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 10.7 \\ C 0.6 \\ \hline \end{array}$$

W. 3.0

$$\begin{array}{r} 11.8 \\ D C 1.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 13.5 \\ F 1.5 \\ \hline \end{array}$$

W. 5.0



20  
919.97

10 + 90

15.5

1.2  
3.5  
1.4

11

14.9

3.9  
1.2  
5.1  
+ 8 1.6

P.T.  
+ 42

12.7

7.3 1.1  
11. 1.3

12

10.6

9.4 0.3  
0.3 0.3

+ 19

10.0

10 0.2 0.2  
2.0 0.4

+ 50

09.4

10.6

+ 93

08.8

11.2

13

08.9

11.1

+ 31

08.8

11.2

+ 35

08.8

11.2

+ 70

09.1

10.9

14

09.7

10.3

B.M.

11.24

920.25

11.00

908.97

909.01

17  
F92

W. 2.9

5.3  
F1.4  
17.8

6.7  
F1.6

W. 5.0

8.6  
F1.3

W. 4.0

11.0  
F1.6

W. 3.0

10.2  
F0.2

W. 2.0

10.8  
F0.2

W. 2.0

W. 2.0

11.1  
C0.1

W. 2.0

W. 2.0

11.1  
C0.0

W. 2.0

W. 2.0

11.0  
C0.2

W. 2.0

W. 2.0

11.0  
C0.2

W. 1.0

W. 1.0

10.8  
C0.1

W. 1.0

W. 1.0

10.6  
F0.3

W. 0.5

W. 0.0

spike 15" Oak. 30' Rt. str. 14120

| Sta.       | +     | $\pi$<br>33.321<br>920.25 | -    | Elev.  |                          |
|------------|-------|---------------------------|------|--------|--------------------------|
| 14 + 33    |       |                           |      | 10.5   | 9.8                      |
| +70        |       |                           |      | 11.7   | 8.6                      |
| 15         |       |                           |      | 12.7   | 7.6                      |
| +50        |       |                           |      | 14.4   | 5.9                      |
| 16         |       |                           |      | 16.1   | 4.2                      |
|            | 12.90 | 933.14                    | 0.01 | 920.24 | 2.14.9                   |
| +50        |       |                           |      | 17.8   | 13.8<br>0.4 15.7         |
| TP         | 13.28 | 946.42                    | 0.07 | 920.38 | 12.7                     |
| 17         |       |                           |      | 19.5   | 13.2<br>1.0 14.6         |
| 9.0<br>+14 |       |                           |      | 20.0   | 12.1<br>13.1<br>1.1 14.2 |
| +50 L      |       |                           |      | 21.2   | 10.7<br>13.2<br>1.4 13.2 |
| B.M.       |       |                           |      |        | 9.2                      |
| 18         |       |                           |      | 22.7   | 11.8<br>10.4<br>1.2 9.2  |
| +50        |       |                           |      | 23.9   | 8.0<br>11.4<br>1.2 8.0   |
| 19         |       |                           |      | 24.8   | 7.1<br>1.4 9.7           |

$$\begin{array}{r} 13.0 \\ F3.2 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 10.4 \\ F0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 13.1 \\ F3.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 11.6 \\ F3.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 7.5 \\ F0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 11.8 \\ F3.2 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 9.7 \\ F2.1 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 8.6 \\ F1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 11.0 \\ F3.4 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 8.0 \\ F2.1 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 6.4 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ DC1.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 6.2 \\ DC0.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ F0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ C0.4 \\ \hline 27.8 \end{array}$$

W. 0.0

$$\begin{array}{r} 10.6 \\ DC0.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 1.8 \\ C0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 13.6 \\ C1.3 \\ \hline 29.0 \end{array}$$

W. 0.9

$$\begin{array}{r} 12.8 \\ C1.8 \\ \hline 31.5 \end{array}$$

$$\begin{array}{r} 12.0 \\ C1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 9.2 \\ C3.5 \\ \hline 34.0 \end{array}$$

W. 1.4

$$\begin{array}{r} 11.9 \\ C2.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.4 \\ C1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.1 \\ C4.0 \\ \hline 35.0 \end{array}$$

W. 2.6

$$\begin{array}{r} 9.6 \\ C5.7 \\ \hline 37.0 \end{array}$$

$$\begin{array}{r} 10.0 \\ C1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ C5.5 \\ \hline 38.0 \end{array}$$

W. 2.9

$$\begin{array}{r} 7.2 \\ C4.6 \\ \hline 39.1 \end{array}$$

$$\begin{array}{r} 8.5 \\ C1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ C5.3 \\ \hline 37.0 \end{array}$$

W. 2.9

$$\begin{array}{r} 5.2 \\ C5.4 \\ \hline 40.7 \end{array}$$

$$\begin{array}{r} 7.0 \\ C1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 2.8 \\ C5.2 \\ \hline 37.4 \end{array}$$

W. 2.8

$$\begin{array}{r} 4.9 \\ C4.8 \\ \hline 39.4 \end{array}$$

$$\begin{array}{r} 5.2 \\ C2.7 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C4.2 \\ \hline 35.4 \end{array}$$

| S. La.          | V    | T      | -     | Elev.  |                            |
|-----------------|------|--------|-------|--------|----------------------------|
|                 |      | 933.14 |       |        | 7.5                        |
| P.T.<br>19 + 39 |      |        |       | 25.2   | 0.4<br>7.9<br>0.6<br>8.5   |
|                 |      |        |       |        | 7.4                        |
| 20              |      |        |       | 25.5   | 0.2<br>7.6<br>0.2<br>7.8   |
| T.P.            | 5.01 | 933.54 | 4.61  | 928.53 |                            |
| +50             |      |        |       | 25.3   | 8.2                        |
| 21              |      |        |       | 24.8   | 8.7                        |
| B.M.            | 6.00 | 937.88 | 1.66  | 931.88 | (931.88) <u>Wong</u>       |
| +50             |      |        |       | 24.0   | 13.9                       |
| 22              |      |        |       | 22.8   | 15.1                       |
| +50             |      |        |       | 21.4   | 16.5                       |
| 23              |      |        |       | 19.5   | 18.4                       |
| T.P.            | 2.28 | 931.26 | 8.90  | 928.98 | 13.8                       |
| +50             |      |        |       | 17.3   | 0.2<br>14.0<br>0.2<br>14.2 |
| 24              |      |        |       | 15.0   | 0.6<br>16.3<br>0.6<br>16.9 |
| P.C.<br>+51     |      |        |       | 12.6   | 1.0<br>18.7<br>14.8        |
| T.P.            | 2.92 | 921.26 | 12.92 | 918.34 | 9.9                        |
| 25              |      |        |       | 10.3   | 1.1<br>21.0<br>1.3<br>22.3 |

15° Curve L



W 1.4

$$\begin{array}{r} 41 \\ C 44 \\ \hline 37.2 \end{array}$$

$$\begin{array}{r} 41 \\ C 3.4 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ C 4.0 \\ \hline 35.0 \end{array}$$

W 0.0

$$\begin{array}{r} 43 \\ C 3.5 \\ \hline 34.0 \end{array}$$

$$\begin{array}{r} 42 \\ C 3.8 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ C 2.6 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 3.8 \\ C 4.4 \\ \hline 35.8 \end{array}$$

$$\begin{array}{r} 4.3 \\ C 3.9 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ 2.4 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 3.3 \\ C 5.4 \\ \hline 37.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ C 4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ C 2.8 \\ \hline 32.6 \end{array}$$

Spike 24" Pop. 50' Lt. Sta. 21 + 15

$$\begin{array}{r} 5.9 \\ C 8.0 \\ \hline 43.0 \end{array}$$

$$\begin{array}{r} 9.9 \\ C 4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 10.3 \\ C 3.6 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ C 10.0 \\ \hline 47.0 \end{array}$$

$$\begin{array}{r} 11.5 \\ C 3.6 \\ \hline \end{array}$$

$$\begin{array}{r} 10.6 \\ C 4.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 6.0 \\ C 10.5 \\ \hline 48.5 \end{array}$$

$$\begin{array}{r} 13.7 \\ C 2.8 \\ \hline \end{array}$$

$$\begin{array}{r} 10.2 \\ C 6.3 \\ \hline 39.4 \end{array}$$

$$\begin{array}{r} 7.3 \\ C 11.1 \\ \hline 49.2 \end{array}$$

$$\begin{array}{r} 16.1 \\ C 2.3 \\ \hline \end{array}$$

$$\begin{array}{r} 9.3 \\ C 9.1 \\ \hline 45.2 \end{array}$$

$$\begin{array}{r} 3.7 \\ C 10.5 \\ \hline 48.0 \end{array}$$

$$\begin{array}{r} 11.9 \\ C 2.1 \\ \hline \end{array}$$

$$\begin{array}{r} 3.3 \\ C 10.5 \\ \hline 48.0 \end{array}$$

W 0.0

$$\begin{array}{r} 8.4 \\ C 8.5 \\ \hline 44.0 \end{array}$$

$$\begin{array}{r} 14.3 \\ C 2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ C 9.3 \\ \hline 45.6 \end{array}$$

W 1.4

$$\begin{array}{r} 12.3 \\ C 7.5 \\ \hline 43.4 \end{array}$$

$$\begin{array}{r} 16.9 \\ C 1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 9.9 \\ C 7.8 \\ \hline 42.6 \end{array}$$

W 2.9

$$\begin{array}{r} 7.6 \\ C 4.7 \\ \hline 39.3 \end{array}$$

$$\begin{array}{r} 9.6 \\ C 1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ C 4.0 \\ \hline 35.0 \end{array}$$

| Sta     |      | $\pi$  | -     | Elev.  |                   |             |
|---------|------|--------|-------|--------|-------------------|-------------|
|         |      | 921.26 |       |        |                   | 11.8        |
| 25 + 50 |      |        |       | 07.9   | 1.2<br>1.5        | 14.9        |
| T.P.    | 0.40 | 911.56 | 10.10 | 911.16 | 1.2<br>6.0<br>1.5 | 4.8         |
| 26      |      |        |       | 05.6   |                   | 7.5         |
| +25     |      |        |       | 04.4   | 7.2<br>1.2<br>1.5 | 6.0<br>8.7  |
| +50     |      |        |       | 03.2   | 8.4<br>1.2<br>1.5 | 7.2<br>9.9  |
| +75     |      |        |       | 02.0   | 9.6<br>1.2<br>1.5 | 8.4<br>11.2 |
| P.T.    |      |        |       | 00.9   | 1.0<br>1.1        | 9.7<br>11.8 |
| 27      |      |        |       |        |                   |             |
| T.P.    | 2.84 | 904.15 | 10.25 | 901.31 |                   |             |
| +32     |      |        |       | 99.3   | 4.9<br>0.8<br>0.8 | 41<br>5.7   |
| B.M.    | 1.87 |        | 1.87  | 902.28 | (902.28)          |             |
| +53     |      |        |       | 98.4   | 0.6<br>580.6      | 5.2<br>6.4  |
| +76     |      |        |       | 97.3   | 6.9<br>0.3        | 6.6<br>7.7  |
| 28      |      |        |       | 96.2   | 8.0<br>0.0        |             |
| T.P.    | 4.54 | 896.60 | 12.09 | 892.06 |                   |             |
| +21     |      |        |       | 95.2   | 1.4               |             |
| +50     |      |        |       | 94.0   | 2.6               |             |

W. 2.9

$$\begin{array}{r} 144 \\ 20.5 \\ \hline 309 \end{array}$$

$$\begin{array}{r} 12.4 \\ 11.0 \\ \hline \end{array}$$

$$\begin{array}{r} 13.8 \\ 20.0 \\ \hline 238 \end{array}$$

W. 0.0

W. 2.9

$$\begin{array}{r} 28 \\ 20.17 \\ \hline 29.3 \end{array}$$

$$\begin{array}{r} 7.6 \\ 11.6 \\ \hline \end{array}$$

$$\begin{array}{r} 18.8 \\ 19.0 \\ \hline 340 \end{array}$$

W. 1.0

W. 2.9

$$\begin{array}{r} 19 \\ 20.8 \\ \hline 31.5 \end{array}$$

$$\begin{array}{r} 9.7 \\ 22.5 \\ \hline \end{array}$$

$$\begin{array}{r} 16.1 \\ 110.1 \\ \hline 372 \end{array}$$

W. 2.0

W. 2.9

$$\begin{array}{r} 28 \\ 22.1 \\ \hline 341 \end{array}$$

$$\begin{array}{r} 13.9 \\ 15.5 \\ \hline \end{array}$$

$$\begin{array}{r} 116.1 \\ 18.9 \\ \hline 34.8 \end{array}$$

W. 2.0

W. 2.5

$$\begin{array}{r} 84 \\ 23.8 \\ \hline 35.1 \end{array}$$

$$\begin{array}{r} 15.5 \\ 15.9 \\ \hline \end{array}$$

$$\begin{array}{r} 143 \\ 16 \\ \hline 282 \end{array}$$

W. 2.0

W. 1.0

W. 1.4

$$\begin{array}{r} 9.3 \\ 22.6 \\ \hline 33.6 \end{array}$$

$$\begin{array}{r} 14.2 \\ 13.5 \\ \hline \end{array}$$

$$\begin{array}{r} 12.9 \\ 13.2 \\ \hline 21.4 \end{array}$$

W. 2.0

W. 0.0

W. 2.0

W. 0.5

$$\begin{array}{r} 2.4 \\ 23.3 \\ \hline 34.1 \end{array}$$

$$\begin{array}{r} 3.8 \\ 11.8 \\ \hline \end{array}$$

$$\begin{array}{r} 10.1 \\ 24.0 \\ \hline 350 \end{array}$$

W. 2.0

Spk 12" Oak 50' Rt. 5/20.27+50

W. 0.0

$$\begin{array}{r} 3.2 \\ 13.2 \\ \hline 33.4 \end{array}$$

$$\begin{array}{r} 3.9 \\ 11.9 \\ \hline \end{array}$$

$$\begin{array}{r} 3.2 \\ 23.2 \\ \hline 310 \end{array}$$

W. 2.0

W. 2.0

W. 2.0

$$\begin{array}{r} 8.2 \\ 12.10 \\ \hline 250 \end{array}$$

$$\begin{array}{r} 7.3 \\ 10.4 \\ \hline \end{array}$$

$$\begin{array}{r} 8.6 \\ 20.0 \\ \hline 230 \end{array}$$

W. 2.0

W. 2.0

$$\begin{array}{r} 10.0 \\ 10.0 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 14.3 \\ 16.3 \\ \hline \end{array}$$

$$\begin{array}{r} 16.8 \\ 18.5 \\ \hline 33.5 \end{array}$$

W. 2.0

W. 1.5

W. 1.0

$$\begin{array}{r} 2.4 \\ 10.0 \\ \hline 240 \end{array}$$

$$\begin{array}{r} 10.5 \\ 19.1 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ 110.3 \\ \hline 37.6 \end{array}$$

W. 2.0

W. 1.0

$$\begin{array}{r} 4.6 \\ 10.0 \\ \hline 240 \end{array}$$

$$\begin{array}{r} 13.0 \\ 110.4 \\ \hline \end{array}$$

$$\begin{array}{r} 15.1 \\ 112.5 \\ \hline 420 \end{array}$$

W. 2.0

| Sta | +           | $\pi$  | -      | Elev |                        |
|-----|-------------|--------|--------|------|------------------------|
|     |             | 896.60 |        |      |                        |
| 29  |             |        |        | 92.4 | 4.2                    |
|     | +50         |        |        | 91.1 | 5.5                    |
| 30  |             |        |        | 90.4 | 6.2                    |
|     | +50         |        |        | 90.0 | 0.3 6.9<br>6.6 0.3 6.3 |
| 31  |             |        |        | 90.2 | 0.6 7.0<br>6.4 0.6 5.8 |
|     | P.C.<br>+38 |        |        | 90.4 | 1.1 7.3<br>6.2 1.1 5.1 |
|     | T.P.        | 6.36   | 898.42 | 454  | 892.06                 |
|     | +76         |        |        | 90.7 | 7.7 1.2 6.5<br>1.4 9.1 |
| 32  |             |        |        | 90.9 | 7.5 1.2 6.3<br>1.4 8.9 |
|     | +50         |        |        | 91.2 | 7.2 1.2 8.6<br>1.4 6.0 |
| 33  |             |        |        | 91.6 | 6.8 1.2 8.2<br>1.4 5.6 |
|     | +23         |        |        | 91.7 | 6.5 1.2 6.9<br>1.4 4.3 |
|     | +50         |        |        | 91.9 | 6.5 0.6 7.0<br>0.7 6.0 |

10° Curve Rk

|       |                                                                       |                                               |                                                       |       |
|-------|-----------------------------------------------------------------------|-----------------------------------------------|-------------------------------------------------------|-------|
| W 1.5 | $\begin{array}{r} 9.2 \\ 10 \overline{) 92.0} \\ 24.5 \end{array}$    | $\begin{array}{r} 15.8 \\ F 11.6 \end{array}$ | $\begin{array}{r} 16.5 \\ F 12.3 \\ 41.6 \end{array}$ | W 2.0 |
| W 2.0 | $\begin{array}{r} 9.5 \\ DC 10 \overline{) 92.0} \\ 25.0 \end{array}$ | $\begin{array}{r} 15.8 \\ F 10.3 \end{array}$ | $\begin{array}{r} 16.8 \\ F 11.3 \\ 39.6 \end{array}$ | W 2.0 |
| W 2.0 | $\begin{array}{r} 10.2 \\ DC 10 \overline{) 210} \\ 25.0 \end{array}$ | $\begin{array}{r} 15.9 \\ F 9.7 \end{array}$  | $\begin{array}{r} 16.5 \\ F 10.3 \\ 37.6 \end{array}$ | W 2.0 |
| W 1.5 | $\begin{array}{r} 9.3 \\ DC 10 \overline{) 10} \\ 24.5 \end{array}$   | $\begin{array}{r} 14.6 \\ F 8.0 \end{array}$  | $\begin{array}{r} 16.5 \\ F 9.6 \\ 35.7 \end{array}$  | W 1.5 |
| W 1.0 | $\begin{array}{r} 8.8 \\ DC 10 \overline{) 1.0} \\ 24 \end{array}$    | $\begin{array}{r} 12.5 \\ F 6.1 \end{array}$  | $\begin{array}{r} 13.8 \\ F 6.8 \\ 30.1 \end{array}$  | W 1.5 |
| W 1.0 | $\begin{array}{r} 8.1 \\ DC 10 \overline{) 10} \\ 24.0 \end{array}$   | $\begin{array}{r} 11.4 \\ F 5.2 \end{array}$  | $\begin{array}{r} 11.3 \\ F 4.0 \\ 25.2 \end{array}$  | W 2.2 |
| W 1.0 | $\begin{array}{r} 6.8 \\ DC 17 \\ 27.4 \end{array}$                   | $\begin{array}{r} 12.7 \\ F 5.0 \end{array}$  | $\begin{array}{r} 12.1 \\ F 3.0 \\ 24.3 \end{array}$  | W 3.3 |
| W 1.0 | $\begin{array}{r} 6.5 \\ DC 18 \\ 27.6 \end{array}$                   | $\begin{array}{r} 10.9 \\ F 3.4 \end{array}$  | $\begin{array}{r} 10.1 \\ DC 0.8 \\ 27.9 \end{array}$ | W 3.3 |
|       | $\begin{array}{r} 6.3 \\ DC 17 \\ 26.4 \end{array}$                   | $\begin{array}{r} 6.1 \\ C 0.9 \end{array}$   | $\begin{array}{r} 5.7 \\ C 2.9 \\ 35.1 \end{array}$   | W 2.3 |
|       | $\begin{array}{r} 2.9 \\ C 2.7 \\ 32.4 \end{array}$                   | $\begin{array}{r} 4.1 \\ C 2.2 \end{array}$   | $\begin{array}{r} 2.7 \\ C 5.5 \\ 40.3 \end{array}$   | W 2.3 |
|       | $\begin{array}{r} 0.9 \\ C 3.4 \\ 33.8 \end{array}$                   | $\begin{array}{r} 4.2 \\ C 2.3 \end{array}$   | $\begin{array}{r} 0.5 \\ C 6.4 \\ 42.1 \end{array}$   | W 2.3 |
| W 0.5 | $\begin{array}{r} 2.7 \\ C 3.3 \\ 34.1 \end{array}$                   | $\begin{array}{r} 3.8 \\ C 2.7 \end{array}$   | $\begin{array}{r} 0.5 \\ C 6.5 \\ 42.0 \end{array}$   | W 2.0 |



898.42

PT.

33 + 75 p.c

92.1 6.3<sup>0.0</sup>  
0.0

34

B.M.

3.24

898.75

2.91

92.3 6.1<sup>0.6</sup>  
0.7 7.6

Hogans!!!

895.51

895.51

1.2 5.1

92.5 6.3<sup>1.4</sup>  
7.7

+29

use 1 1/2:1 B.S.  
on 21.

+50

92.6 6.2<sup>1.2</sup>  
1.4 7.6

+77

92.8 6.0<sup>1.2</sup>  
1.4 7.4

35

93.0 5.8<sup>1.2</sup>  
1.4 7.2

+22 1/2

93.1 5.7<sup>1.2</sup>  
1.4 7.1

+50

93.3 5.5<sup>1.2</sup>  
1.4 6.9

+85

93.6 5.3<sup>1.2</sup>  
1.4 6.6

36

93.7 5.1<sup>1.2</sup>  
1.4 6.5

+50

94.0 4.8<sup>1.2</sup>  
1.4 6.2

PT.

37

94.4 4.4<sup>1.1</sup>  
1.2 5.6

W. 9.8

$$\begin{array}{r} 2.8 \\ C3.5 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 3.5 \\ C2.8 \\ \hline \end{array}$$

$$\begin{array}{r} +1.0 \\ C7.3 \\ \hline 42.1 \end{array}$$

W. 0.5

W. 2.8

$$\begin{array}{r} 2.8 \\ C4.8 \\ \hline 38.6 \end{array}$$

$$\begin{array}{r} 3.2 \\ C2.9 \\ \hline \end{array}$$

$$\begin{array}{r} 1.1 \\ 6.6.5 \\ \hline 40.0 \end{array}$$

Spk 8 Pop 30

$$L4 \quad 34 + 95$$

W. 2.3

$$\begin{array}{r} 4.4 \\ C3.3 \\ \hline 35.9 \end{array}$$

$$\begin{array}{r} 3.8 \\ C3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ C1.3 \\ \hline 28.0 \end{array}$$

W. 2.3

$$\begin{array}{r} 4.9 \\ C2.7 \\ \hline 34.7 \end{array}$$

$$\begin{array}{r} 3.2 \\ C3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C2.1 \\ \hline 29.1 \end{array}$$

W. 2.3

$$\begin{array}{r} 7.1 \\ C0.3 \\ \hline 29.9 \end{array}$$

$$\begin{array}{r} 3.2 \\ C2.8 \\ \hline \end{array}$$

$$\begin{array}{r} 3.4 \\ C2.4 \\ \hline 37.8 \end{array}$$

W. 2.3

$$\begin{array}{r} 8.8 \\ C0.4 \\ \hline 26.1 \end{array}$$

$$\begin{array}{r} 3.3 \\ C2.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ C0.13 \\ \hline 28.6 \end{array}$$

W. 2.3

$$\begin{array}{r} 7.1 \\ B.5 \\ \hline 17.9 \end{array}$$

$$\begin{array}{r} 3.4 \\ C2.3 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ C1.5 \\ \hline 26.0 \end{array}$$

W. 2.3

$$\begin{array}{r} 10.9 \\ F4.0 \\ \hline 25.3 \end{array}$$

$$\begin{array}{r} 3.8 \\ C1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 4.1 \\ C0.2 \\ \hline 27.4 \end{array}$$

W. 2.3

$$\begin{array}{r} 12.7 \\ F6.1 \\ \hline 29.5 \end{array}$$

$$\begin{array}{r} 4.6 \\ C0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ C0.5 \\ \hline 28.0 \end{array}$$

W. 2.3

$$\begin{array}{r} 16.9 \\ F6.2 \\ \hline 29.7 \end{array}$$

$$\begin{array}{r} 8.5 \\ F3.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.3 \\ C0.3 \\ \hline 27.6 \end{array}$$

W. 2.3

$$\begin{array}{r} 13.4 \\ F7.2 \\ \hline 31.7 \end{array}$$

$$\begin{array}{r} 11.7 \\ F7.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ C0.26 \\ \hline 24.2 \end{array}$$

W. 2.0

$$\begin{array}{r} 13.3 \\ F7.7 \\ \hline 32.4 \end{array}$$

$$\begin{array}{r} 12.3 \\ F7.9 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ C0.0 \\ \hline 28.0 \end{array}$$

| Sta.                          |        |        |      | Elev.  |                       |
|-------------------------------|--------|--------|------|--------|-----------------------|
|                               |        | 898.75 |      |        |                       |
| 37 + 37                       | PT     |        |      | 946    | 42 0.8 3.4<br>0.8 5.0 |
| +63                           |        |        |      | 94.8   | 40 0.0<br>0.0         |
| 38                            | PC.    |        |      | 95.1   | 37 0.3 4.0<br>0.3 3.4 |
| +50                           |        |        |      | 95.4   | 34 0.6 4.0<br>0.6 2.8 |
| 39                            |        |        |      | 95.9   | 29 0.3 3.2<br>0.3 2.6 |
| +50                           |        |        |      | 96.5   | 23 0.4 2.7<br>0.0 1.9 |
| B.M.                          |        |        | 3.24 | 895.51 | (895.51)              |
| Work Done<br>No Be Done<br>No | 200 ft |        |      |        |                       |
| B.M.                          | 1300   | 920.62 |      | 907.62 |                       |
| 48 + 00                       |        |        |      | 07.7   | 12.9                  |
| +50                           |        |        |      | 09.7   | 10.9                  |
| 49                            |        |        |      | 11.6   | 9.0                   |
| +38                           |        |        |      | 13.0   | 7.6                   |
| T.P.                          | 8.04   | 922.24 | 6.42 | 914.20 |                       |

W. 1.0

$$\begin{array}{r} 13.5 \\ F 8.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.6 \\ P 7.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ R 0.2 \\ \hline 23.4 \end{array}$$

W. 0.0

$$\begin{array}{r} 13.0 \\ F 9.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ F 1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ R 0.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 11.4 \\ F 8.0 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ F 1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ F 2.5 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 4.1 \\ F 1.3 \\ \hline 12.6 \end{array}$$

$$\begin{array}{r} 4.1 \\ F 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 4.0 \\ C 0.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 2.8 \\ F 0.2 \\ \hline 15.4 \end{array}$$

$$\begin{array}{r} 3.4 \\ F 0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 1.8 \\ C 1.4 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 2.2 \\ F 0.3 \\ \hline 15.6 \end{array}$$

$$\begin{array}{r} 2.3 \\ F 0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 0.4 \\ C 2.3 \\ \hline 29.5 \end{array}$$

Spk. 8" Pop. 30' Rt. Sta 34+95

Spk. 8" Oak 33' Lt. 47+60

$$\begin{array}{r} 10.8 \\ C 2.1 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 12.7 \\ F 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 10.0 \\ C 2.9 \\ \hline 32.8 \end{array}$$

$$\begin{array}{r} 8.9 \\ C 2.0 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 10.1 \\ C 0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ C 5.1 \\ \hline 37.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ C 3.8 \\ \hline 34.6 \end{array}$$

$$\begin{array}{r} 7.8 \\ C 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 2.4 \\ C 6.6 \\ \hline 40.2 \end{array}$$

$$\begin{array}{r} 3.5 \\ C 4.1 \\ \hline 35.2 \end{array}$$

$$\begin{array}{r} 6.4 \\ C 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 1.1 \\ C 6.5 \\ \hline 40.0 \end{array}$$

922.24

50

14.8

7.4

+50

16.0

6.2

51

16.7

5.6

+50

17.2

5.0

52

17.3

4.9

+50

17.2

5.3  
0.3  
5.0  
0.3  
4.7

1'

6.5  
0.9  
5.6  
0.9  
4.7

53

16.6

6.9

P.C.  
+17

16.4

1.1  
5.8  
1.3  
4.5

T.P.

4.39

921.18

545

916.79

6.0  
1.1  
4.9  
1.3  
3.6  
6.5

+25

16.3

1.2  
5.3  
1.6  
3.7  
0.7

+50 R/L  
35.0 R/L

15.9

+75  
Curve

15.6

1.2  
5.5  
1.6  
3.9  
7.0

+90

15.3

1.2  
5.8  
1.6  
4.2



$$\begin{array}{r} 3.5 \\ C 3.9 \\ \hline 34.8 \end{array}$$

$$\begin{array}{r} 6.4 \\ C 1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 2.7 \\ C 2.6 \\ \hline 36.0 \end{array}$$

$$\begin{array}{r} 2.6 \\ C 3.6 \\ \hline 34.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ C 0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 4.3 \\ C 1.9 \\ \hline 30.8 \end{array}$$

$$\begin{array}{r} 5.5 \\ C 0.8 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ C 0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 2.7 \\ C 2.8 \\ \hline 32.6 \end{array}$$

$$\begin{array}{r} 3.7 \\ C 1.3 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ C 0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ C 2.1 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 4.4 \\ C 0.5 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ F 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ D 0.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 5.2 \\ D 1.5 \\ \hline 26.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ F 0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ D 0.9 \\ \hline 24.8 \end{array}$$

W. 0.0

$$\begin{array}{r} 4.8 \\ D 1.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 5.1 \\ C 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ C 1.1 \\ \hline 30.1 \end{array}$$

W. 0.9

$$\begin{array}{r} 4.9 \\ D 1.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 5.5 \\ F 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.9 \\ C 2.0 \\ \hline 33.5 \end{array}$$

W. 2.5

$$\begin{array}{r} 4.0 \\ D 1.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 4.4 \\ C 0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ C 2.1 \\ \hline 34.5 \end{array}$$

W. 3.3

$$\begin{array}{r} 3.7 \\ C 0.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ C 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ C 2.8 \\ \hline 37.5 \end{array}$$

W. 4.9

$$\begin{array}{r} 5.1 \\ F 1.2 \\ \hline 17.4 \end{array}$$

$$\begin{array}{r} 5.4 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ C 3.2 \\ \hline 38.4 \end{array}$$

W. 5.0

$$\begin{array}{r} 5.1 \\ F 0.9 \\ \hline 16.8 \end{array}$$

$$\begin{array}{r} 3.1 \\ C 2.7 \\ \hline \end{array}$$

$$\begin{array}{r} 3.3 \\ C 3.7 \\ \hline 39.4 \end{array}$$

W. 5.0

921.18

54

15.2

1.2

1.6

+25

14.9

1.2 7.1  
6.2  
1.6 4.6

+50

14.5

1.2 7.9  
6.7 1.6 5.1

+75

14.2

1.2 8.2  
7.0 1.6 5.4

T.P.

284

917.40

662

914.56

1.2 4.8  
3.6  
1.6 2.0

55 +100

13.8

P.T  
+32

13.4

1.1 5.1  
4.0  
1.3 2.7

+66

12.9

0.7 5.0  
4.5  
0.8 2.7

56

12.4

0.5 5.5  
5.0  
0.5 4.5

+19

12.2

0.3 5.5  
5.2  
0.3 4.9

1 +31

12.0

5.4

+39

12.0

5.4

+61

11.8

5.6

SKIP

W. 5.0

$$\begin{array}{r} 5.7 \\ F1.1 \\ 17.2 \end{array} \quad \begin{array}{r} 3.2 \\ C3.0 \end{array} \quad \begin{array}{r} 3.1 \\ C4.3 \\ 40.6 \end{array}$$

W 5.0

$$\begin{array}{r} 6.3 \\ F1.2 \\ 17.4 \end{array} \quad \begin{array}{r} 6.7 \\ F0.2 \end{array} \quad \begin{array}{r} 3.3 \\ C4.6 \\ 41.2 \end{array}$$

W 5.0

$$\begin{array}{r} 8.0 \\ F2.6 \\ 20.2 \end{array} \quad \begin{array}{r} 7.6 \\ F0.6 \end{array} \quad \begin{array}{r} 3.3 \\ C4.9 \\ 41.8 \end{array}$$

W. 5.0

W 1.0

$$\begin{array}{r} 7.6 \\ F5.6 \\ 27.2 \end{array} \quad \begin{array}{r} 4.2 \\ F0.6 \end{array} \quad \begin{array}{r} 0.8 \\ C4.0 \\ 39.6 \end{array}$$

W. 4.6

W 2.0

$$\begin{array}{r} 13.2 \\ F10.5 \\ 3.8 \end{array} \quad \begin{array}{r} 5.4 \\ F1.4 \end{array} \quad \begin{array}{r} 5.4 \\ C0.7 \\ 28.9 \end{array}$$

W. 2.5

W 2.0

$$\begin{array}{r} 15.1 \\ F11.4 \\ 39.8 \end{array} \quad \begin{array}{r} 6.3 \\ F1.8 \end{array} \quad \begin{array}{r} 8.7 \\ F3.5 \\ 23.0 \end{array}$$

W. 1.0

W 2.0

$$\begin{array}{r} 16.7 \\ F11.4 \\ 39.8 \end{array} \quad \begin{array}{r} 4.3 \\ F1.9 \end{array} \quad \begin{array}{r} 12.5 \\ F7.0 \\ 30.0 \end{array}$$

W. 1.0

W 3.0

$$\begin{array}{r} 17.3 \\ F11.4 \\ 46.8 \end{array} \quad \begin{array}{r} 7.1 \\ F1.9 \end{array} \quad \begin{array}{r} 15.1 \\ F9.6 \\ 36.2 \end{array}$$

W. 2.0

W 4.0

SKIP

W 3.0

$$\begin{array}{r} 17.1 \\ F11.7 \\ 46.4 \end{array} \quad \begin{array}{r} 7.2 \\ F1.8 \end{array} \quad \begin{array}{r} 16.7 \\ F11.3 \\ 39.6 \end{array}$$

W. 2.0

W 2.0

$$\begin{array}{r} 16.1 \\ F10.5 \\ 38.0 \end{array} \quad \begin{array}{r} 7.3 \\ F1.7 \end{array} \quad \begin{array}{r} 15.8 \\ F10.2 \\ 37.4 \end{array}$$

W. 2.0

| Sta. | +               | $\Delta$ | -    | Elev   |                  |
|------|-----------------|----------|------|--------|------------------|
|      |                 | 917.40   |      |        |                  |
| 57   |                 |          |      | 11.7   | 5.7              |
| +50  |                 |          |      | 12.0   | 5.4              |
| 58   |                 |          |      | 12.5   | 4.9              |
| +50  |                 |          |      | 13.5   | 3.9              |
|      | 9.63            | 923.29   | 3.74 | 913.66 |                  |
| 59   |                 |          |      | 15.8   | 7.5              |
| +50  |                 |          |      | 16.3   | 7.0              |
| 60   |                 |          |      | 17.8   | 5.5              |
| +50  |                 |          |      | 19.3   | 4.0              |
| 61   |                 |          |      | 20.8   | 2.5              |
| T.P. | on B.M.<br>3.63 | 929.08   | 0.37 | 922.92 | B.M.<br>(925.45) |
| +50  |                 |          |      | 22.1   | 7.0              |
| 62   |                 |          |      | 23.1   | 6.0              |
| +50  |                 |          |      | 23.7   | 5.4              |

W 2.0

$$\begin{array}{r} 13.2 \\ F 7.5 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 7.1 \\ F 1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 17.2 \\ F 11.5 \\ \hline 40.0 \end{array}$$

W 2.0

$$\begin{array}{r} 9.1 \\ F 3.7 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 6.4 \\ F 1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 10.6 \\ F 7.2 \\ \hline 30.4 \end{array}$$

W 1.0

$$\begin{array}{r} 4.2 \\ C 0.7 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 5.3 \\ F 0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.9 \\ DC 0.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 40.3 \\ C 4.2 \\ \hline 35.4 \end{array}$$

$$\begin{array}{r} 3.7 \\ C 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ C 0.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ C 1.8 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 7.8 \\ F 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.7 \\ C 2.8 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} 3.6 \\ C 3.4 \\ \hline 33.8 \end{array}$$

$$\begin{array}{r} 6.3 \\ C 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ C 1.6 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 1.5 \\ C 4.0 \\ \hline 35.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ C 0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 4.1 \\ C 1.4 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 1.1 \\ C 2.9 \\ \hline 32.8 \end{array}$$

$$\begin{array}{r} 3.3 \\ C 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 2.3 \\ C 1.7 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 1.6 \\ C 0.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 2.2 \\ C 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 0.9 \\ C 0.6 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 7.4 \\ DC 1.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 6.9 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.7 \\ C 0.3 \\ \hline 27.6 \end{array}$$

$$\begin{array}{r} 6.7 \\ DC 1.1 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ F 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ DC 1.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 6.4 \\ DC 1.2 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 5.7 \\ F 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ DC 1.4 \\ \hline 25.8 \end{array}$$



929.08

63

23.9

5.2

+50

24.0

5.1

64

24.0

5.1

+50

24.1

5.0

+79

24.1

5.0

+93

24.1

5.0

65 +07

24.1

5.0

$$\begin{array}{r} 4.4 \\ 68.8 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} 5.2 \\ 60.0 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ 60.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 3.9 \\ 61.2 \\ \hline 29.4 \end{array}$$

$$\begin{array}{r} 4.8 \\ 60.3 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ 61.4 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 4.6 \\ 60.5 \\ \hline 28.0 \end{array}$$

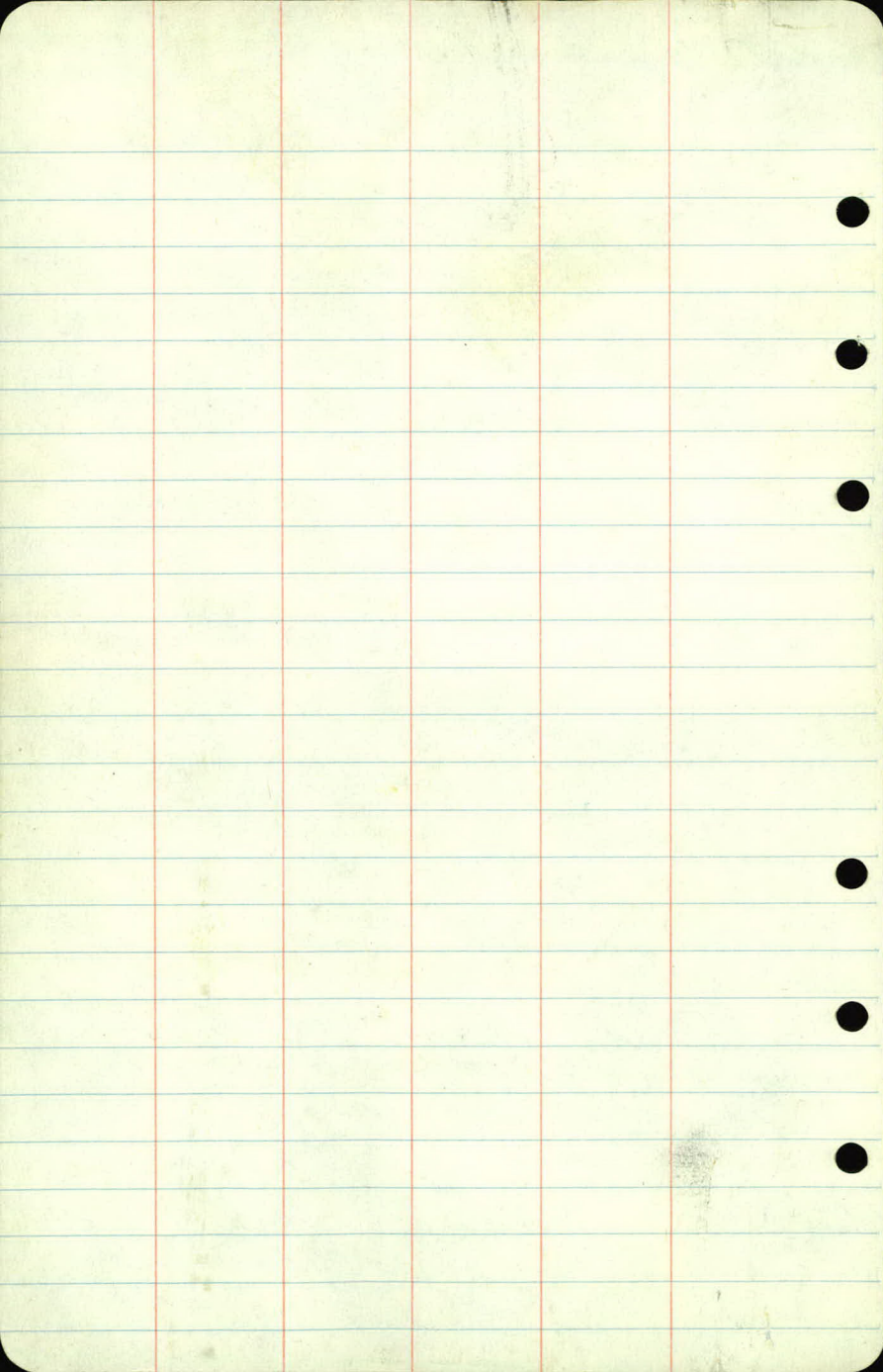
$$\begin{array}{r} 4.8 \\ 60.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.0 \\ 61.1 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ 60.4 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ 60.3 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ 61.1 \\ \hline 29.2 \end{array}$$



Snail Lake Blvd.

Add 1/1. Turns

for Slope Stakes

## Slope Stokes Rt. 10-14

 $\pi$ 

B.M. 0.32 909.33 909.01

0.62 896.97 12.98 896.35

10 921.5 0.9 920.4

+25 19.7 1.3 918.4

+50 18.0 1.6 916.4

11 14.9 1.6 913.3

+42 12.7 1.3 911.4

12 10.6 0.5 910.1

+19 10.0 0.4 909.6

T.P. 11.89 908.24 0.62 896.35

+50 09.4

+93 08.8

13 08.9



$$\begin{array}{r} 6.0 \\ F29.0 \\ \hline 45.0 \end{array}$$

W. 2.0

$$\begin{array}{r} 6.6 \\ F28.0 \\ \hline 74.0 \end{array}$$

W. 3.0

$$\begin{array}{r} 6.6 \\ F26.0 \\ \hline 72.0 \end{array}$$

W. 5.0

$$\begin{array}{r} 6.8 \\ F23.1 \\ \hline 66.2 \end{array}$$

W. 5.0

$$\begin{array}{r} 5.9 \\ F20.3 \\ \hline 59.6 \end{array}$$

W. 4.0

$$\begin{array}{r} 4.0 \\ F17.1 \\ \hline 52.2 \end{array}$$

W. 3.0

$$\begin{array}{r} 3.0 \\ F15.6 \\ \hline 48.2 \end{array}$$

W. 2.0

$$\begin{array}{r} 10.1 \\ F11.3 \\ \hline 39.6 \end{array}$$

W. 2.0

$$\begin{array}{r} 7.7 \\ F8.3 \\ \hline 33.6 \end{array}$$

W. 2.0

$$\begin{array}{r} 7.5 \\ F9.4 \\ \hline 33.4 \end{array}$$

W. 2.0

W.

W. 2.0

W. 2.0

| Sta.    | +    | $\pi$            | -     | Elev   |                |
|---------|------|------------------|-------|--------|----------------|
|         |      | 908.24           |       |        |                |
| 13 + 31 |      |                  |       | 08.8   |                |
| + 35    |      |                  |       | 08.8   |                |
| + 70    |      |                  |       | 09.1   |                |
| 14      |      |                  |       | 09.7   |                |
| B.M.    |      |                  | + 0.8 | 909.04 | 909.01         |
|         |      | Left of 11 to 14 |       |        |                |
| B.M.    | 5.45 | 914.46           |       | 909.01 |                |
| 11      |      |                  |       | 14.9   | 1.2            |
| + 42    |      |                  |       | 12.7   | 1.8<br>1.1 0.7 |
| 12      |      |                  |       | 10.6   | 3.9<br>0.3 3.6 |
| + 19    |      |                  |       | 10.0   | 4.5            |
| + 50    |      |                  |       | 09.4   | 5.1            |
| B.M.    | 48.9 | 913.90           |       | 909.01 |                |
| + 93    |      |                  |       | 08.8   | 5.1            |
| 13      |      |                  |       | 08.9   | 5.0            |

W. 2.0

$$\begin{array}{r} 46 \\ F5.1 \\ \hline 27.2 \end{array}$$

W. 2.0

W. 1.0

$$\begin{array}{r} 46 \\ F5.2 \\ \hline 26.4 \end{array}$$

W. 1.0

W 1.0

$$\begin{array}{r} 3.4 \\ F4.3 \\ \hline 24.6 \end{array}$$

W. 1.0

W00

$$\begin{array}{r} 2.6 \\ F4.1 \\ \hline 23.2 \end{array}$$

W 00

No. Dicks  
Required

$$\begin{array}{r} 1.9 \\ F1.2 \\ \hline 17.4 \end{array}$$

$$\begin{array}{r} 3.8 \\ F0.2 \\ \hline 15.4 \end{array}$$

$$\begin{array}{r} 4.5 \\ B.1 \\ \hline 15 \end{array}$$

W. 1.0

$$\begin{array}{r} 19.3 \\ 14.2 \\ \hline 44.4 \end{array}$$

W. 2.0

$$\begin{array}{r} 16.0 \\ F10.9 \\ \hline 38.8 \end{array}$$

W. 2.0

$$\begin{array}{r} 15.8 \\ F10.6 \\ \hline 38.4 \end{array}$$

9/13.90

13+31

08.8

5.1

135

08.8

5.1

+70

09.1

4.8

14

09.7

4.2

W. 2.0

$$\begin{array}{r} 12.3 \\ F7.4 \\ \hline 31.8 \end{array}$$

W. 1.0

$$\begin{array}{r} 12.3 \\ F7.2 \\ \hline 31.4 \end{array}$$

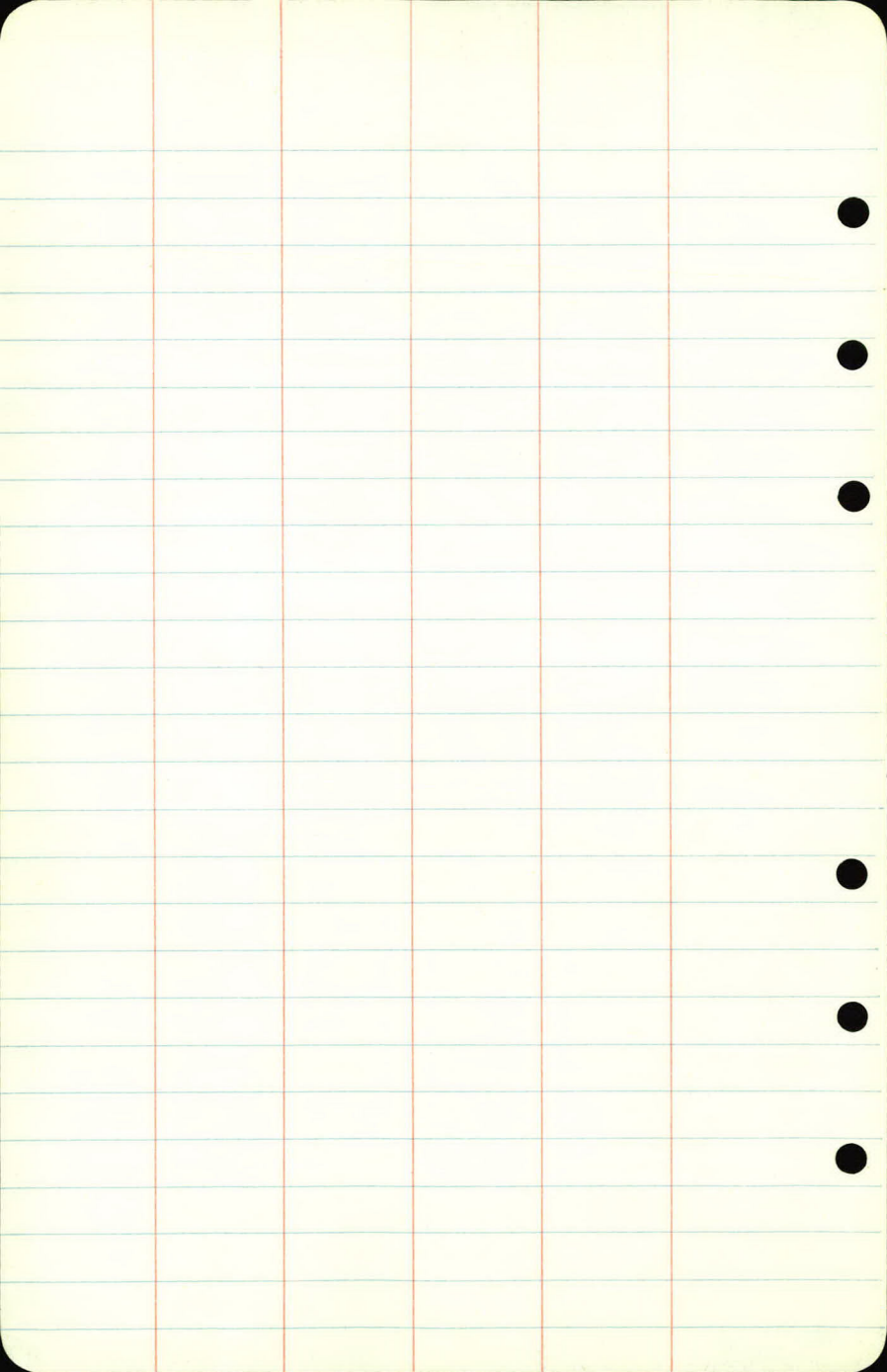
W. 1.0

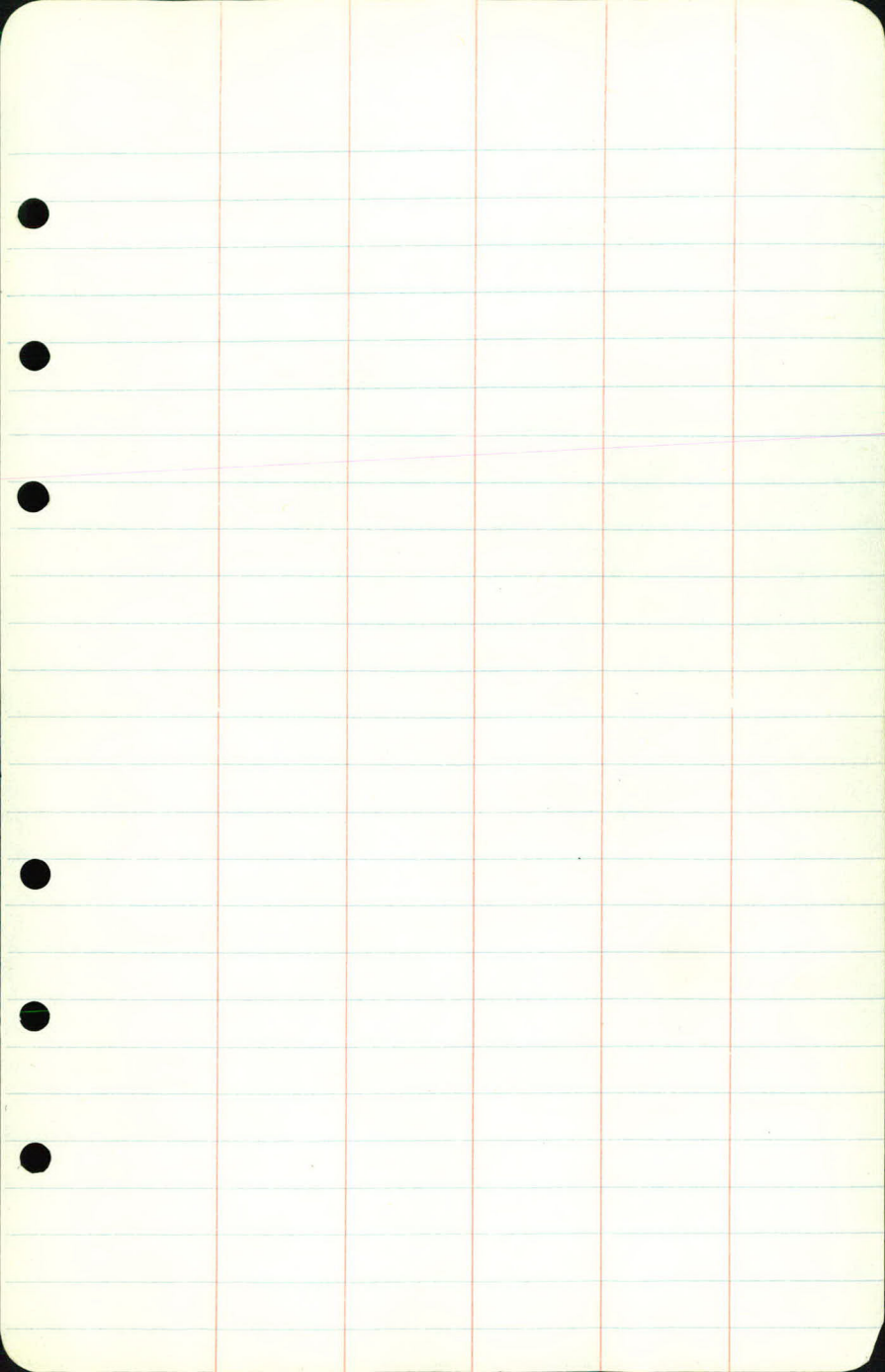
$$\begin{array}{r} 11.3 \\ F6.5 \\ \hline 29.8 \end{array}$$

W. 0.0

$$\begin{array}{r} 9.3 \\ F5.1 \\ \hline 25.2 \end{array}$$







2.13

934.01 931.88

6.49

933.14

7.36

926.65

Slope Stake Notes

Borrow for Snail Lake Blvd.

Rt. and Lt. of Victoria - So. Snail Lake.

| Sta.   | +    | $\pi$  | - | Elev.  |
|--------|------|--------|---|--------|
| B.M.   | 9.36 | 990.31 |   | 980.95 |
| 0 + 50 |      |        |   | 81.2   |

|   |  |  |  |      |
|---|--|--|--|------|
| 1 |  |  |  | 81.7 |
|---|--|--|--|------|

|      |  |  |  |      |
|------|--|--|--|------|
| + 50 |  |  |  | 82.3 |
|------|--|--|--|------|

|        |  |  |  |      |
|--------|--|--|--|------|
| 2 + 67 |  |  |  | 82.6 |
|--------|--|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 2 |  |  |  | 83.1 |
|---|--|--|--|------|

|      |  |  |  |      |
|------|--|--|--|------|
| + 38 |  |  |  | 83.7 |
|------|--|--|--|------|

|   |  |  |  |  |
|---|--|--|--|--|
| 3 |  |  |  |  |
|---|--|--|--|--|



# Top Bolt Spike Victoria of Snail Lake Blvd.

$$\begin{array}{r} 9.1 \\ \underline{60.0} \end{array}$$

$$\begin{array}{r} 9.1 \\ \underline{\phantom{00}} \end{array}$$

$$9.1$$

$$\begin{array}{r} 9.1 \\ \underline{67.0} \\ 33.0 \end{array}$$

$$\begin{array}{r} 9.1 \\ \underline{60.0} \\ 72.0 \end{array}$$

$$\begin{array}{r} 8.6 \\ \underline{60.0} \\ 60.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ \underline{62.0} \\ 34.0 \end{array}$$

$$8.6$$

$$\begin{array}{r} 3.6 \\ \underline{65.0} \\ 33.0 \end{array}$$

$$\begin{array}{r} 8.6 \\ \underline{60.0} \\ 113.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ \underline{60.0} \\ 81.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ \underline{63.0} \\ 33.0 \end{array}$$

$$8.0$$

$$\begin{array}{r} 2.0 \\ \underline{66.0} \\ 34.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ \underline{60.0} \\ 118.0 \end{array}$$

$$\begin{array}{r} 7.7 \\ \underline{60.0} \\ 83.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ \underline{63.0} \\ 33.0 \end{array}$$

$$7.7$$

$$\begin{array}{r} 1.7 \\ \underline{66.0} \\ 35.0 \end{array}$$

$$\begin{array}{r} 7.7 \\ \underline{60.0} \\ 117.0 \end{array}$$

$$\begin{array}{r} 7.2 \\ \underline{60.0} \\ 78.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ \underline{63.0} \\ 33.0 \end{array}$$

$$7.2$$

$$\begin{array}{r} 2.2 \\ \underline{65.0} \\ 35.0 \end{array}$$

$$\begin{array}{r} 7.2 \\ \underline{60.0} \\ 106.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ \underline{60.0} \\ 73.0 \end{array}$$

$$\begin{array}{r} 3.6 \\ \underline{63.0} \\ 34.0 \end{array}$$

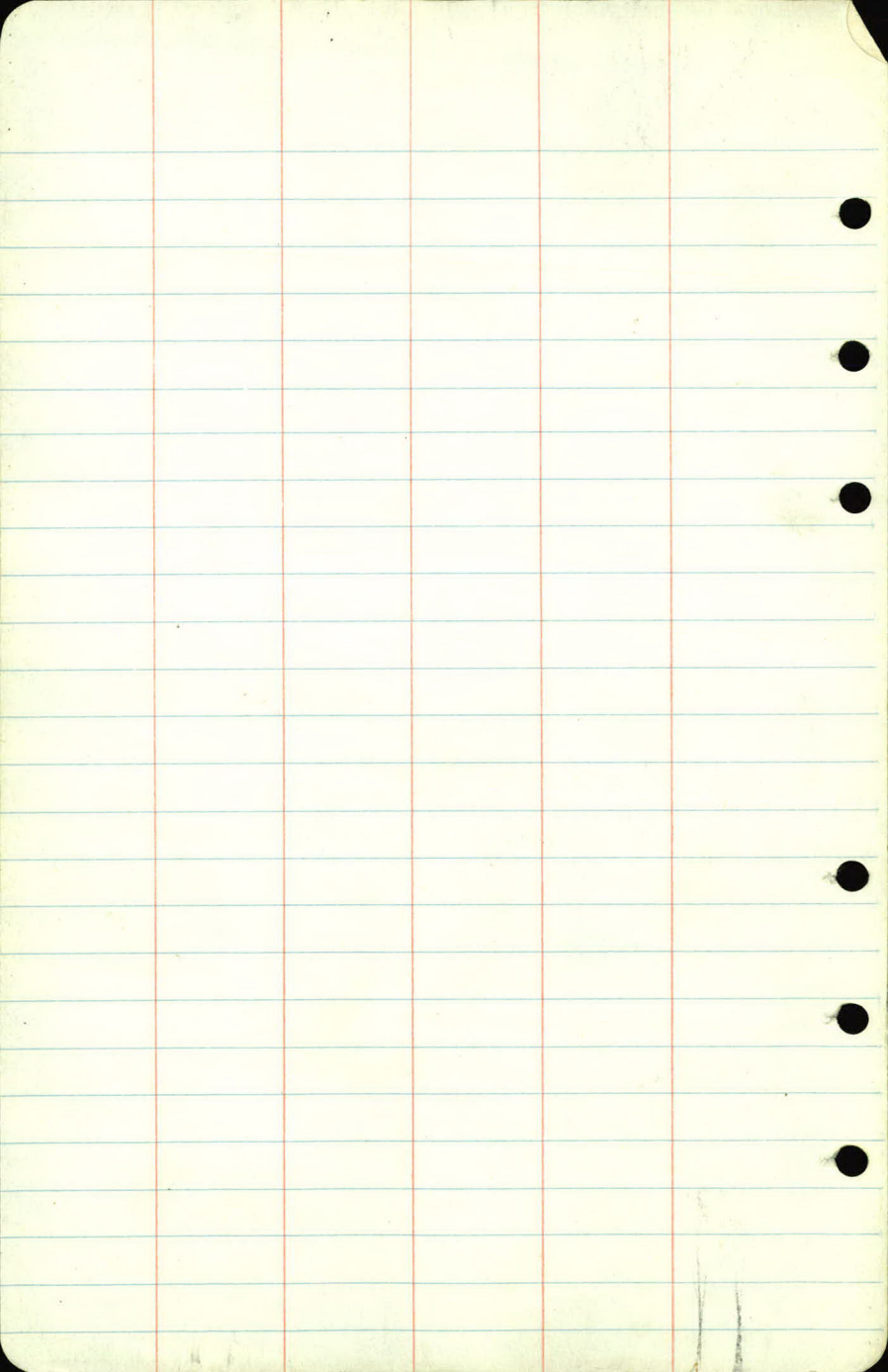
$$6.6$$

$$\begin{array}{r} 2.6 \\ \underline{64.0} \\ 35.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ \underline{60.0} \\ 92.0 \end{array}$$

$$2182 \quad \begin{array}{r} 5.5 \\ \underline{60.0} \end{array}$$

$$2197 \quad \begin{array}{r} 5.5 \\ \underline{60.0} \end{array}$$



Slope Stokes

SNAIL LAKE BLVD.

Sta 44 to 48.

| Sta  | +    | $\Delta$ | -    | Elev.  |
|------|------|----------|------|--------|
| B.M. | 0.97 | 908.59   |      | 907.62 |
| T.P. | 6.26 | 905.05   | 9.80 | 898.79 |

44+00

+50

45

+50

46

+50

47

|      |      |        |      |        |
|------|------|--------|------|--------|
| T.P. | 9.51 | 912.72 | 1.84 | 903.21 |
|------|------|--------|------|--------|

+50

7.3

|      |  |  |      |        |
|------|--|--|------|--------|
| B.M. |  |  | 5.07 | 907.65 |
|------|--|--|------|--------|

Spk 8" Oak 33' Lt. Sta. 47460

$$\begin{array}{r} 7.5 \\ F2.0 \\ \hline 19.0 \end{array} \quad 5.5$$

$$\begin{array}{r} 10.8 \\ F4.6 \\ \hline 21.9 \end{array} \quad 6.2$$

$$\begin{array}{r} 10.3 \\ F4.0 \\ \hline 21.0 \end{array} \quad 6.3 \quad \begin{array}{r} 11.5 \\ F5.2 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 10.7 \\ F4.9 \\ \hline 22.3 \end{array} \quad 5.8 \quad \begin{array}{r} 13.8 \\ F10.0 \\ \hline 35.0 \end{array}$$

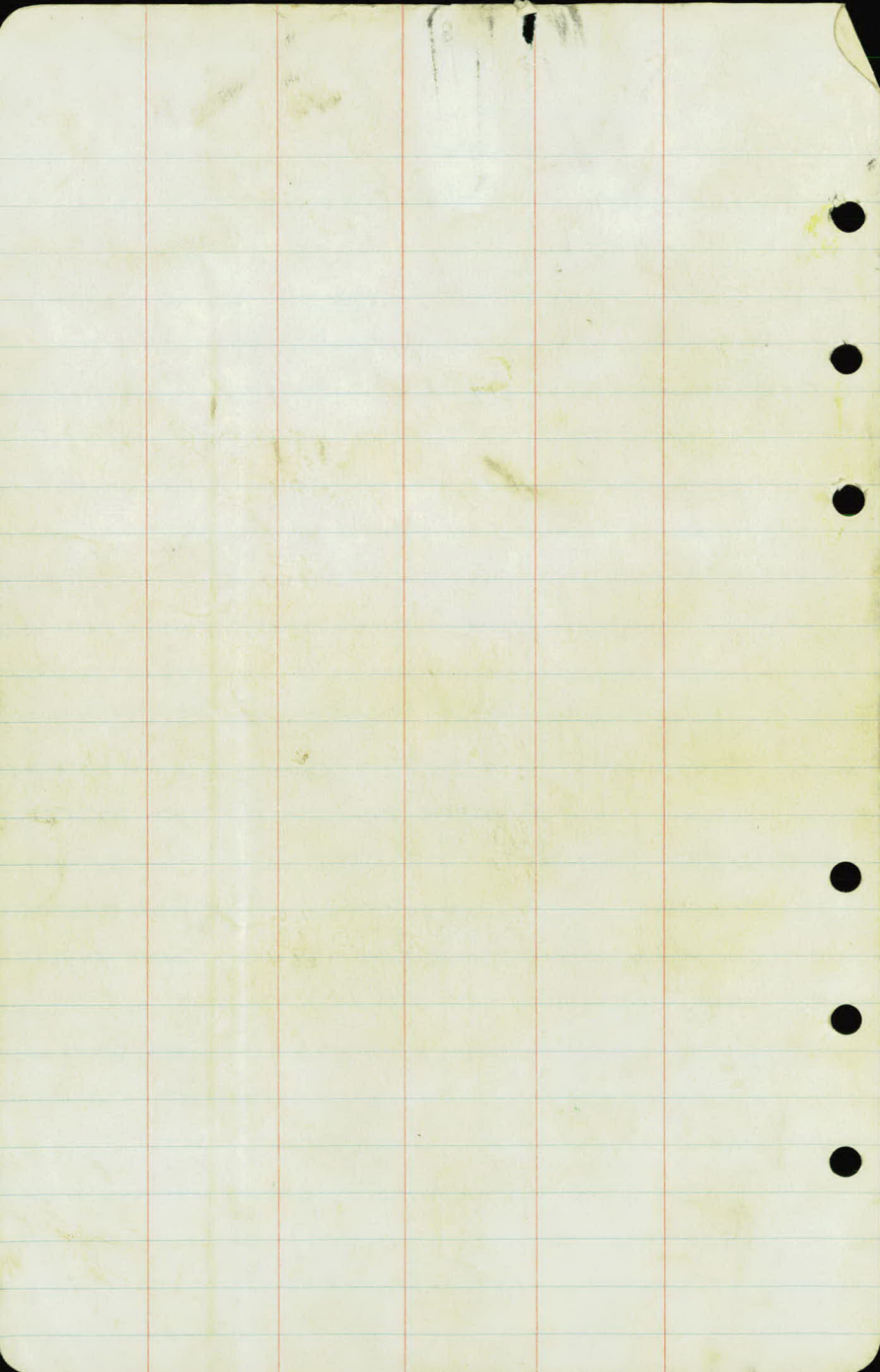
$$\begin{array}{r} 10.1 \\ F4.9 \\ \hline 22.5 \end{array} \quad 5.2 \quad \begin{array}{r} 16.2 \\ F11.0 \\ \hline 37.0 \end{array}$$

$$\begin{array}{r} 9.0 \\ F5.5 \\ \hline 23.2 \end{array} \quad 3.5 \quad \begin{array}{r} 13.5 \\ F10.0 \\ \hline 35.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ F3.0 \\ \hline 19.5 \end{array} \quad 1.8 \quad \begin{array}{r} 5.6 \\ F2.8 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 6.6 \\ 50.7 \\ \hline 28.4 \end{array} \quad 7.3 \quad \begin{array}{r} 7.6 \\ 10.1 \\ \hline 26.4 \end{array}$$





SNAIL LAKE BLVD.

Blue tops  
at C.O.O pts.

|      |      |        |      |        |
|------|------|--------|------|--------|
| B.M. | 1.54 | 982.49 |      | 980.95 |
|      | 1.27 | 975.06 | 9.20 | 973.29 |

|   |  |  |  |      |
|---|--|--|--|------|
| 3 |  |  |  | 67.1 |
|---|--|--|--|------|

|     |      |        |      |        |     |
|-----|------|--------|------|--------|-----|
| +33 |      |        |      | 65.4   | 9.7 |
|     | 2.00 | 967.39 | 9.67 | 965.39 |     |
| +68 |      |        |      | 63.6   | 3.8 |

|   |  |  |  |      |     |
|---|--|--|--|------|-----|
| 4 |  |  |  | 61.8 | 5.6 |
|---|--|--|--|------|-----|

|     |      |        |      |        |     |
|-----|------|--------|------|--------|-----|
| +32 |      |        |      | 60.0   | 7.4 |
|     | 1.91 | 961.92 | 7.38 | 960.01 |     |
| +80 |      |        |      | 57.2   | 4.7 |

|   |  |  |  |      |     |     |     |
|---|--|--|--|------|-----|-----|-----|
| 5 |  |  |  | 55.8 | 6.3 | 5.8 | 6.4 |
|---|--|--|--|------|-----|-----|-----|

|     |  |  |  |      |     |     |     |
|-----|--|--|--|------|-----|-----|-----|
| +40 |  |  |  | 53.2 | 0.8 | 8.7 | 7.9 |
|     |  |  |  |      | 0.8 |     | 9.5 |

|     |  |  |  |      |     |      |      |
|-----|--|--|--|------|-----|------|------|
| +72 |  |  |  | 51.0 | 1.1 | 10.7 | 9.8  |
|     |  |  |  |      | 1.1 |      | 12.0 |

|  |      |        |      |        |  |
|--|------|--------|------|--------|--|
|  | 0.00 | 952.17 | 9.75 | 952.17 |  |
|--|------|--------|------|--------|--|

|   |  |  |  |      |     |     |     |
|---|--|--|--|------|-----|-----|-----|
| 6 |  |  |  | 49.1 | 1.2 | 3.1 | 1.9 |
|   |  |  |  |      | 1.4 |     | 4.5 |

|     |  |  |  |      |     |     |     |
|-----|--|--|--|------|-----|-----|-----|
| +25 |  |  |  | 47.4 | 4.8 | 3.6 |     |
|     |  |  |  |      | 1.4 |     | 6.2 |

$$\overline{20.5}$$

$$\overline{27}$$

$$\overline{20.5}$$

$$\frac{5.7}{27}$$

$$\overline{20.5}$$

$$\frac{3.8}{27}$$

$$\overline{20.5}$$

$$\frac{5.6}{27}$$

$$\overline{20.5}$$

$$\frac{7.4}{27}$$

$$\overline{20.5}$$

$$\frac{27}{\overline{C2.0}} \quad \frac{27}{27}$$

W. 0.0

$$\frac{6.4}{20.5}$$

$$\frac{5.8}{27}$$

W. 0.2

$$\frac{8.5}{20.7}$$

$$\frac{7.9}{27}$$

W. 1.4

$$\frac{12.0}{21.9}$$

$$\frac{9.8}{27}$$

N 2.5

$$\frac{0.5}{\overline{C4.0}} \quad \frac{23.0}{23.0}$$

$$\frac{1.9}{27}$$

W 2.5

$$\frac{5.2}{\overline{C1.0}} \quad \frac{23.0}{23.0}$$

$$\frac{3.6}{27}$$

952.17

6+50

45.6

1.2 5.7  
6.6  
1.4 8.0

+73 PI

44.0

1.1 6.7  
7.8  
1.1 8.9

7

42.2

0.8 9.2  
10.0  
0.8 10.8

B.M.

6.89

915 90

909.01

11

14.9

1.2  
1.0  
1.6 2.6

+42

12.7

1.1  
3.2  
1.1 4.3

12

10.6

0.3  
5.3  
0.3 5.6

+19

10.0

5.9

+56

09.4

6.5

13

08.8

7.1

+35

08.9

7.0

+70

08.8

7.1

14

08.8

7.1



W 25

$$\begin{array}{r} 7.0 \\ 61.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ 61.0 \\ \hline 27 \end{array}$$

W 1.4

$$\begin{array}{r} 7.9 \\ 61.0 \\ \hline 21.9 \end{array}$$

$$\begin{array}{r} 6.7 \\ 27 \end{array}$$

W 0.2

$$\begin{array}{r} 9.8 \\ 61.0 \\ \hline 20.7 \end{array}$$

Spike 15" Oak 30' Rt 1d + 20

$$\begin{array}{r} 2.6 \\ 20 \end{array}$$

W 5.0

$$\begin{array}{r} 4.3 \\ 19 \end{array}$$

W 4.0

$$\begin{array}{r} 5.6 \\ 18 \end{array}$$

W 3.0

$$\begin{array}{r} 5.9 \\ 17 \end{array}$$

W 2.0

$$\begin{array}{r} 6.5 \\ 17 \end{array}$$

W 2.0

$$\begin{array}{r} 7.1 \\ 17 \end{array}$$

W 2.0

$$\begin{array}{r} 7.0 \\ 16 \end{array}$$

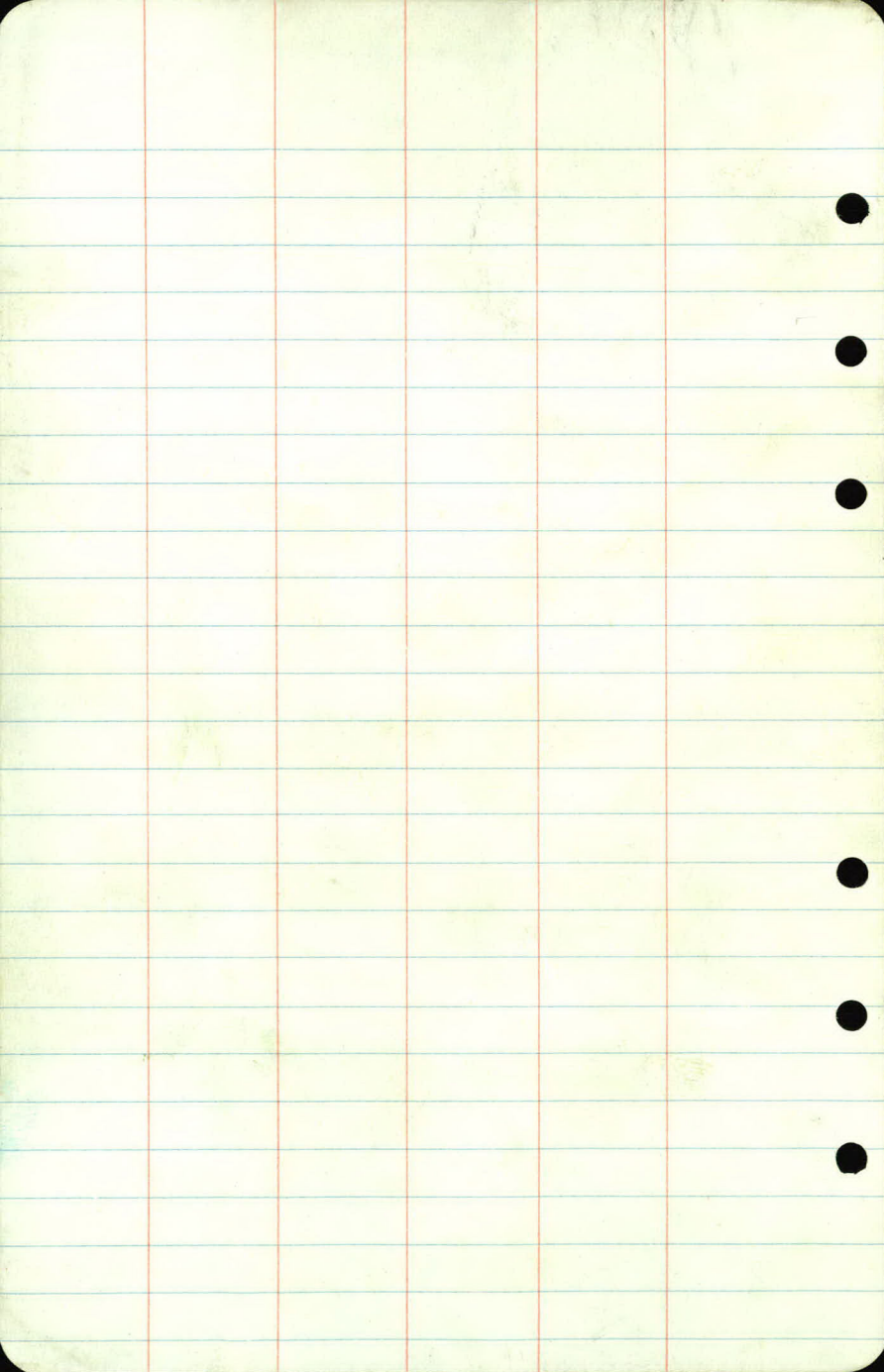
W 1.0

$$\begin{array}{r} 7.1 \\ 15.5 \end{array}$$

W 1.0

$$\begin{array}{r} 7.1 \\ 15 \end{array}$$

W 0.0



SNAIL LAKE BLVD

Grade Change  
Sta. 18+00 to Sta 23+00

|      |      |        |        |      |      |
|------|------|--------|--------|------|------|
| B.M. | 1.95 | 933.83 | 931.88 |      |      |
|      |      |        | 21.~   | 12.6 | 16.4 |
| 18   |      |        |        | 10.2 | 14.0 |
|      |      |        | 22.9   | 1.4  | 9.7  |
|      |      |        |        |      | 12.3 |
| +50  |      |        | 24.6   | 1.2  | 8.0  |
|      |      |        |        | 1.4  | 10.6 |
| 19   |      |        | 26.1   | 1.2  | 6.5  |
|      |      |        |        | 1.4  | 9.1  |
| +39  |      |        |        | 0.6  | 6.4  |
|      |      |        | 26.8   | 1.0  | 7.6  |
|      |      |        |        | 0.6  |      |
| 20   |      |        | 27.4   | 0.2  | 6.2  |
|      |      |        |        | 6.4  | 6.6  |
|      |      |        |        | 2.2  |      |
| +50  |      |        | 27.3   | 6.5  |      |
| 21   |      |        | 26.8   | 7.0  |      |
| +50  |      |        | 25.7   | 8.7  |      |
| 22   |      |        | 24.1   | 9.7  |      |
| +50  |      |        | 22.0   | 11.8 |      |
| 23   |      |        | 19.7   | 14.1 |      |

Spk 24" Pop. 50' Lt. 2/1/15

$$\begin{array}{r} 12.3 \\ 27.9 \\ \hline \end{array} \qquad \begin{array}{r} 9.7 \\ 27 \\ \hline \end{array}$$

W 2.9

$$\begin{array}{r} 10.6 \\ 29.9 \\ \hline \end{array} \qquad \begin{array}{r} 8.0 \\ 27 \\ \hline \end{array}$$

W 2.9

$$\begin{array}{r} 9.1 \\ 29.8 \\ \hline \end{array} \qquad \begin{array}{r} 6.5 \\ 27 \\ \hline \end{array}$$

W 2.8

$$\begin{array}{r} 7.6 \\ 28.4 \\ \hline \end{array} \qquad \begin{array}{r} 6.4 \\ 27 \\ \hline \end{array}$$

W 1.4

$$\begin{array}{r} 6.6 \\ 27 \\ \hline \end{array} \qquad \begin{array}{r} 6.2 \\ 27 \\ \hline \end{array}$$

W 0.0

$$\begin{array}{r} 6.5 \\ 27 \\ \hline \end{array} \qquad \begin{array}{r} 6.5 \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ 27 \\ \hline \end{array} \qquad \begin{array}{r} 7.0 \\ 27 \\ \hline \end{array}$$

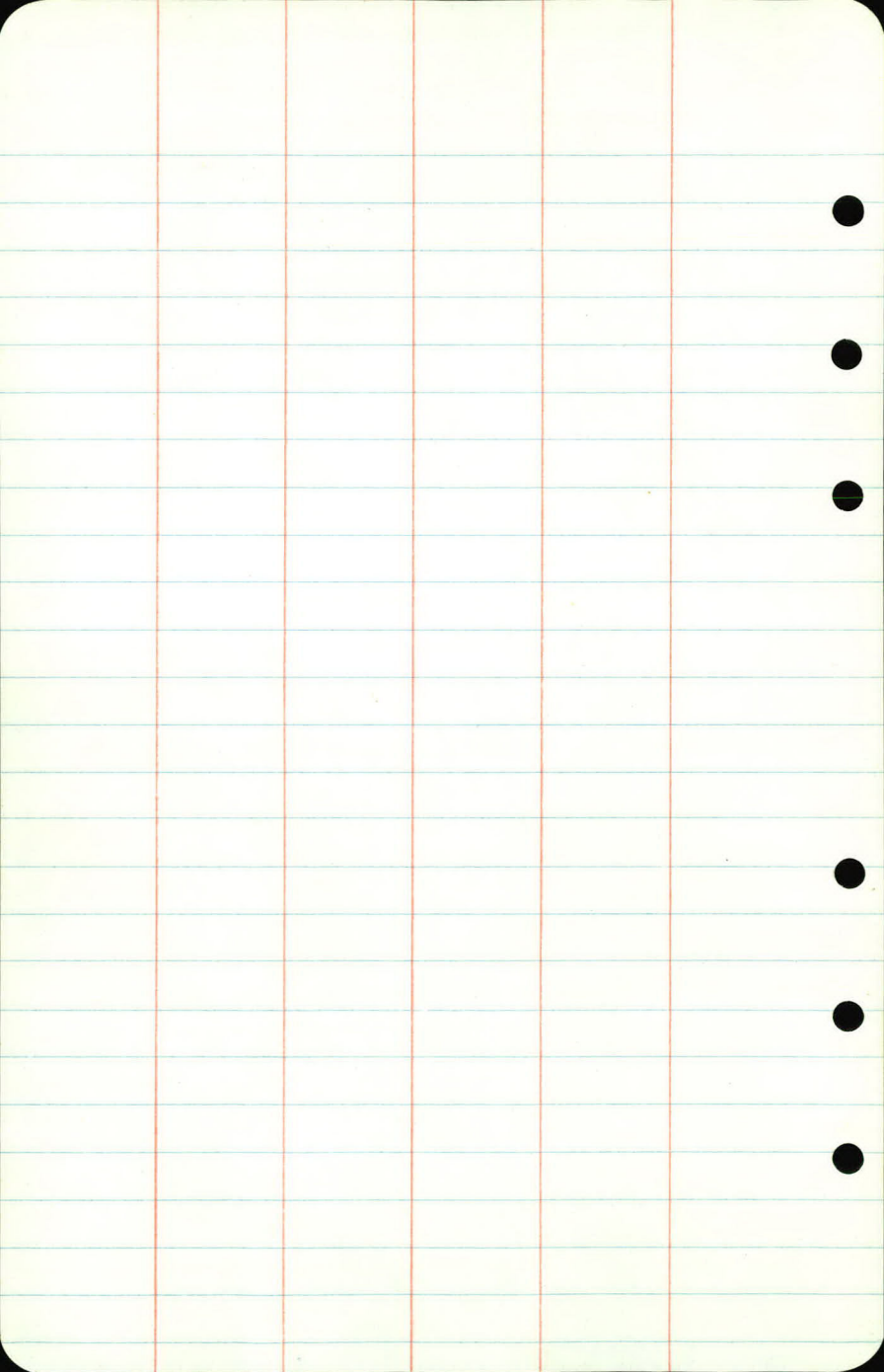
$$\begin{array}{r} 8.1 \\ 27 \\ \hline \end{array} \qquad \begin{array}{r} 8.1 \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} 9.7 \\ 27 \\ \hline \end{array} \qquad \begin{array}{r} 9.7 \\ 27 \\ \hline \end{array}$$

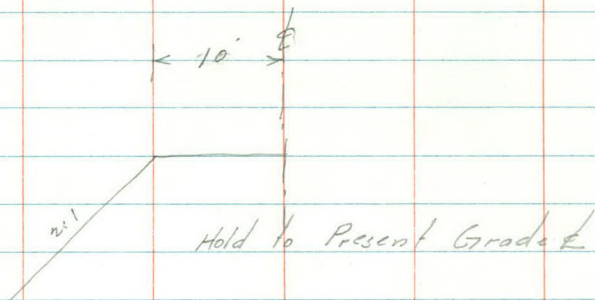
$$\begin{array}{r} 11.8 \\ 27 \\ \hline \end{array} \qquad \begin{array}{r} 11.8 \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} 14.1 \\ 27 \\ \hline \end{array} \qquad \begin{array}{r} 14.1 \\ 27 \\ \hline \end{array}$$





SNAIL LAKE BLVD.  
REILAND LANE



0 + 50

0 + 60

+ 75

1

+ 25

+ 50

+ 85

(Hand Level)

$$\begin{array}{r} 110 \\ F 55 \\ 210 \\ 58 \\ \hline E 58 / 21.6 \end{array}$$

$$\begin{array}{r} 10.7 \\ F 10.7 \\ 31.1 \end{array}$$

$$\begin{array}{r} 6.5 \\ F 6.5 \\ 22.0 \end{array}$$

$$\begin{array}{r} 13.0 \\ F 13.0 \\ 36.8 \end{array}$$

$$\begin{array}{r} 7.8 \\ F 7.8 \\ 25.6 \end{array}$$

$$\begin{array}{r} 13.2 \\ F 13.2 \\ 36.4 \end{array}$$

$$\begin{array}{r} 1.2 \\ F 1.2 \\ 25.0 \end{array}$$

$$\begin{array}{r} 13.2 \\ F 13.2 \\ 36.4 \end{array}$$

24" x 10' Ext.

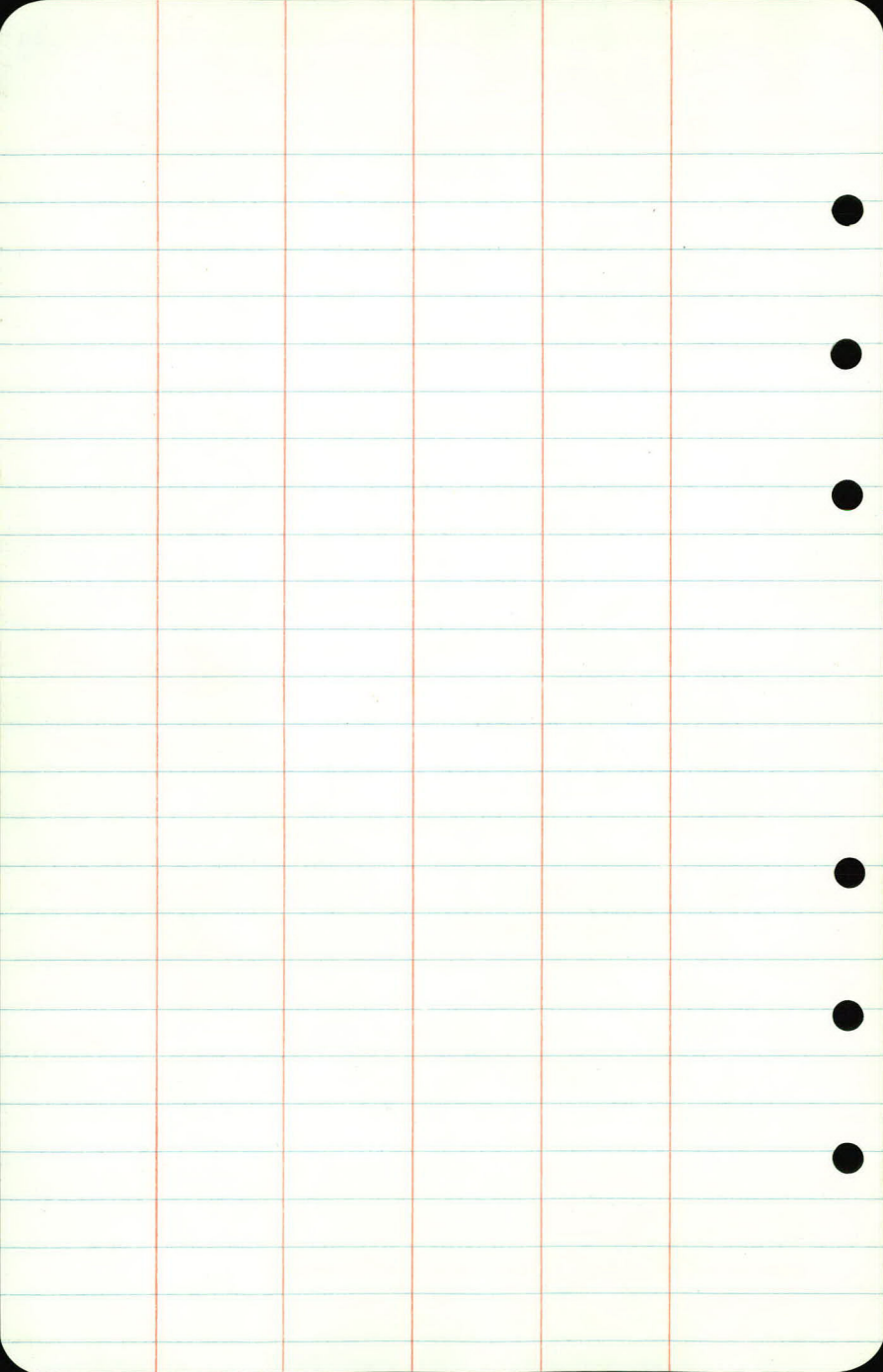
20" x 32' CM

24" x 20' Ext. CM

$$\begin{array}{r} 10.0 \\ F 4.5 \\ 19.0 \end{array}$$

$$\begin{array}{r} 11.7 \\ F 11.7 \\ 33.4 \end{array}$$

$$\begin{array}{r} 5.6 \\ F 5.6 \\ 21.2 \end{array}$$





SNAIL LAKE BLVD.

section change Lt. only

0+00 to 1+50

use special section  
on plans

B.M.

1.94

982.89

980.95

0+36

79.8

3.1

+50

79.4

3.5

1

77.3

5.6

+25

76.0

6.9

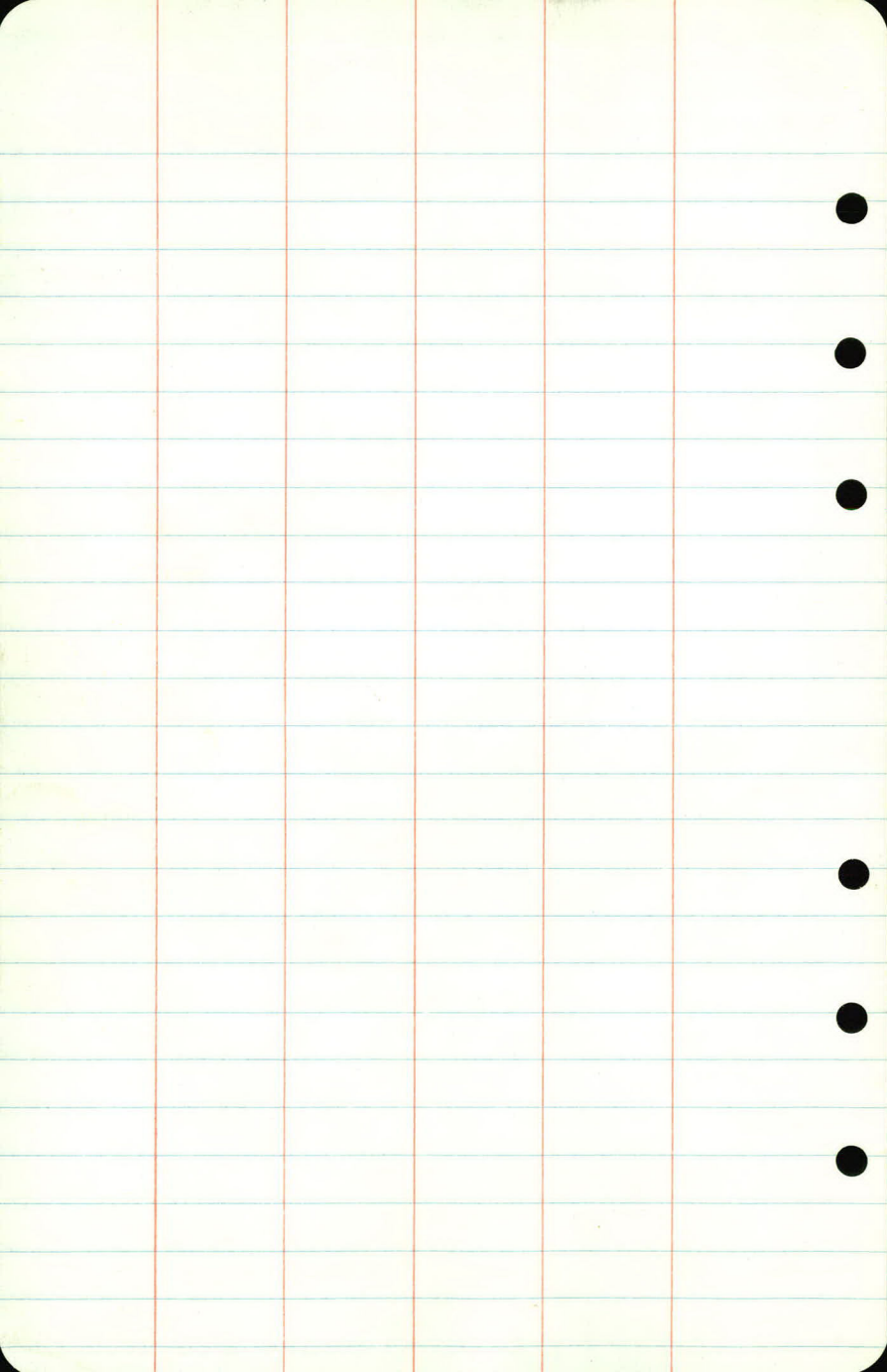
$$\begin{array}{rcl}
 DC\ 0.0 & = & 19 \\
 CO.0 & = & 20.5 \\
 & & 1\frac{1}{2} \text{ to } 1
 \end{array}$$

$$\begin{array}{r}
 41 \\
 DC\ 0.0 \\
 \hline
 19
 \end{array}$$

He Can Do

$$\begin{array}{r}
 61 \\
 DC\ 0.5 \\
 \hline
 19.7
 \end{array}$$

$$\begin{array}{r}
 6.3 \\
 CO.0 \\
 \hline
 21.4
 \end{array}$$



Blue Tops

Small Lake Blvd.

45



| Sta.  | +    | +      | -     | Elev.  |                             |
|-------|------|--------|-------|--------|-----------------------------|
| B.M.  | 1.23 | 933.11 |       | 931.88 |                             |
| T.P.  | 0.73 | 921.57 | 12.27 | 920.84 |                             |
| T.P.  | 0.30 | 909.21 | 12.66 | 908.91 | -1.2 pt on<br>1.3<br>+1.5   |
| 25+50 |      |        |       | 07.9   |                             |
| 26    |      |        |       | 05.6   | -1.2 2.4<br>3.6<br>+1.5     |
| +50   |      |        |       | 03.2   | -1.2<br>6.0<br>+1.5 4.8     |
| 27    |      |        |       | 00.9   | -1.0 8.3 7.0<br>+1.1 9.4    |
| +32   |      |        |       | 99.3   | -0.8 9.9 9.1<br>+0.8 10.7   |
| +53   |      |        |       | 98.4   | -0.6 10.8 10.2<br>+0.6 11.4 |
| +76   |      |        |       | 97.3   | -0.3 11.9 11.6<br>+0.3 12.2 |
| T.P.  | 4.41 | 901.43 | 12.19 | 897.02 |                             |
| 28    |      |        |       | 96.2   | 0.0 5.2<br>0.0              |
| +50   |      |        |       | 94.0   | 7.4                         |
| 29    |      |        |       | 92.4   | 9.0                         |
| +50   |      |        |       | 91.1   | 10.3                        |

3pk 24" Pop 50' Lt 21+15

$$\begin{array}{r} 0.1 \\ 8.7 \\ \hline 15 \end{array}$$

W.O.O

$$\begin{array}{r} 2.6 \\ 8.7 \\ \hline 16 \end{array}$$

W. 1.0

$$\begin{array}{r} 4.3 \\ 8.2 \\ \hline 17.0 \end{array}$$

W. 2.0

E.W. 1.4

$$\begin{array}{r} 9.4 \\ 8.7 \\ \hline 14.4 \end{array}$$

$$\begin{array}{r} 7.0 \\ 8.7 \\ \hline 17.0 \end{array} \quad \begin{array}{r} 10.3 \\ 13.3 \\ \hline 23.6 \end{array}$$

W. 2.0

E.W. 1.0

$$\begin{array}{r} 10.7 \\ 8.7 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 9.1 \\ 8.7 \\ \hline 17.0 \end{array} \quad \begin{array}{r} 4.8 \\ 4.3 \\ \hline 37.6 \end{array}$$

W. 2.0

E.W. 1.0

$$\begin{array}{r} 11.4 \\ 8.7 \\ \hline 16 \end{array}$$

$$\begin{array}{r} 10.2 \\ 8.7 \\ \hline 17.0 \end{array} \quad \begin{array}{r} 8.2 \\ 22.0 \\ \hline 33.0 \end{array}$$

W. 2.0

E.W. 1.0

$$\begin{array}{r} 12.2 \\ 8.7 \\ \hline 16 \end{array}$$

$$\begin{array}{r} 11.6 \\ 8.7 \\ \hline 17.0 \end{array} \quad \begin{array}{r} 13.6 \\ 20.0 \\ \hline 25 \end{array}$$

W 2.0

E.W. 1.0

$$\begin{array}{r} 5.2 \\ 8.7 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ 8.7 \\ \hline 17.0 \end{array}$$

W. 2.0

W. 1.0

$$\begin{array}{r} 7.4 \\ 8.7 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 7.4 \\ 8.7 \\ \hline 17.0 \end{array}$$

W 2.0

W. 1.5

$$\begin{array}{r} 9.0 \\ 8.7 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 9.0 \\ 8.7 \\ \hline 17.0 \end{array}$$

W. 2.0

W. 2.0

$$\begin{array}{r} 10.3 \\ 8.7 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 10.3 \\ 8.7 \\ \hline 17.0 \end{array}$$

W. 2.0

Sta

+

K

-

Elev.

901.43

30

90.4

11.0

+50

90.0

|      |      |      |
|------|------|------|
| -0.3 | 11.4 | 11.7 |
| +0.3 |      | 11.1 |

31

90.2

|      |      |      |
|------|------|------|
| -0.4 | 11.2 | 11.8 |
| +0.6 |      | 10.6 |

+38.17

1055'

90.4

|     |      |      |
|-----|------|------|
| 1.1 | 11.0 | 12.1 |
| 1.1 |      | 9.9  |

+76

305'

90.7

|     |      |      |
|-----|------|------|
| 1.2 |      | 12.1 |
| 1.4 | 10.7 | 9.5  |

32

90.9

|     |      |      |
|-----|------|------|
| 1.2 |      | 11.9 |
| 1.4 | 10.5 | 9.3  |

5055'

+58

91.2

|     |      |      |
|-----|------|------|
| 1.2 |      | 11.6 |
| 1.4 | 10.2 |      |

B.M.

592

895.51

W 2.0

$$\begin{array}{r} 11.0 \\ \underline{8.1} \\ 17 \end{array}$$

$$\begin{array}{r} 11.0 \\ \underline{8.1} \\ 17 \end{array}$$

W. 2.0

W. 2.5

$$\begin{array}{r} 11.1 \\ \underline{8.1} \\ 16.5 \end{array}$$

$$\begin{array}{r} 11.7 \\ \underline{8.1} \\ 17 \end{array}$$

W. 2.0

W. 1.0

$$\begin{array}{r} 10.6 \\ \underline{8.1} \\ 16.0 \end{array}$$

$$\begin{array}{r} 11.8 \\ \underline{8.1} \\ 17 \end{array}$$

W. 2.0

W 1.0

$$\begin{array}{r} 9.9 \\ \underline{8.1} \\ 16.0 \end{array}$$

$$\begin{array}{r} 12.1 \\ \underline{8.1} \\ 17.2 \end{array}$$

W 2.2

$$\begin{array}{r} 9.5 \\ \underline{8.1} \\ 15 \end{array}$$

$$\begin{array}{r} 12.1 \\ \underline{8.1} \\ 18.2 \end{array}$$

W. 3.3

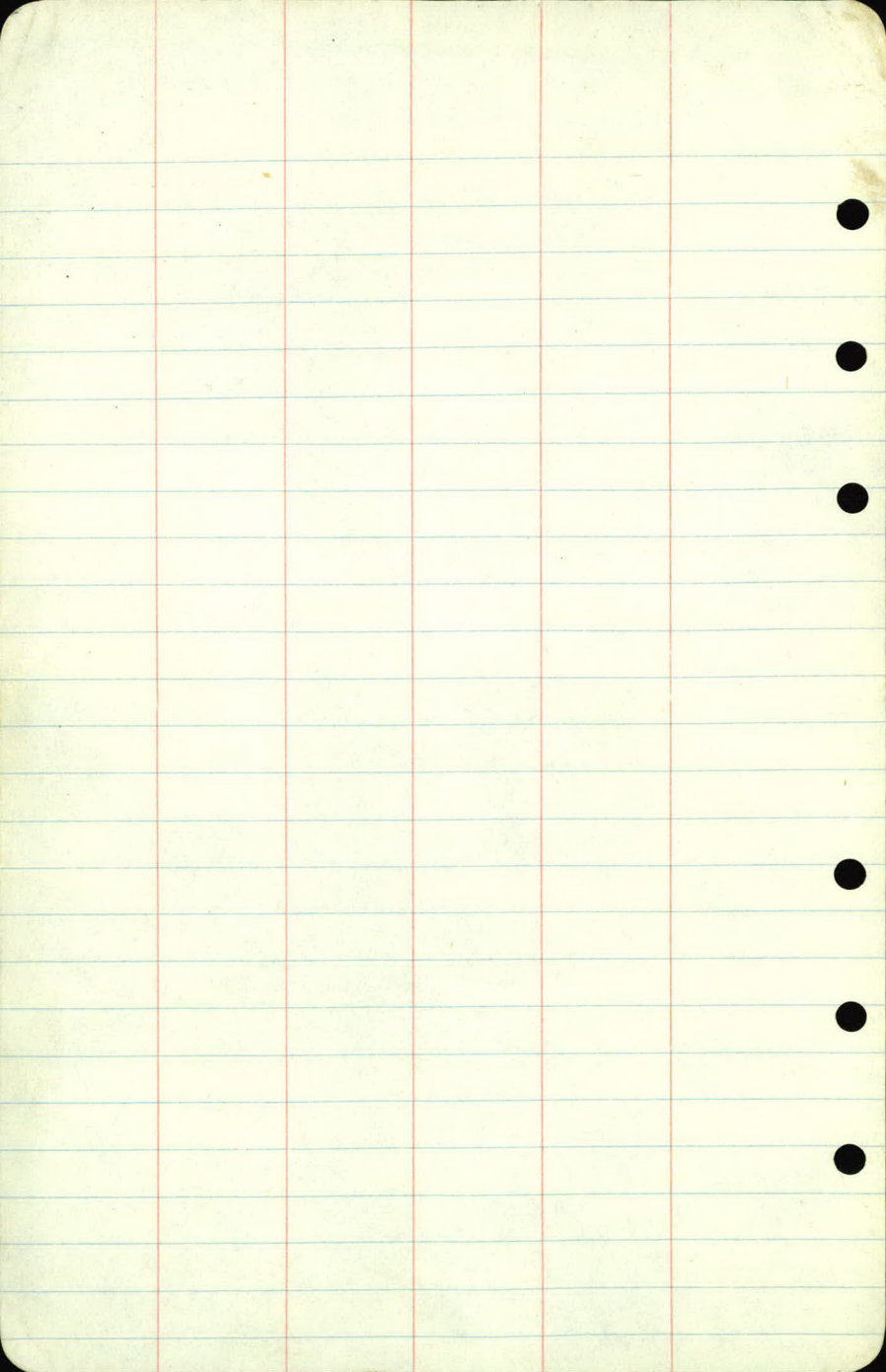
$$\begin{array}{r} 11.9 \\ \underline{8.1} \\ 18.3 \end{array}$$

W. 3.3

$$\begin{array}{r} 11.6 \\ \underline{8.1} \\ 17.3 \end{array}$$

W. 2.3

Spk 4" Pop 30 Rt. 34+95





Snoil Lake Blvd.  
Special Ditch  
at Intersection of Atlantic

| Sta.           | +     | $\pi$               | -    | Elev.       |     |
|----------------|-------|---------------------|------|-------------|-----|
| B. M.          | 10.79 | 918.41              |      | 907.62      |     |
| T. P.          | 4.70  | 921.79 <sup>B</sup> | 1.32 | 917.09      |     |
| T. P.          |       |                     |      |             |     |
| 53 + 50 = 0+00 |       |                     |      | 15.9-0=13.9 | 7.9 |
| +50            |       |                     |      | 13.8        | 8.0 |
| T. P.          | 5.52  | 921.15 <sup>V</sup> | 6.16 | 915.63      |     |
| 1              |       |                     |      | 13.7        | 7.5 |
| +50            |       |                     |      | 13.6        | 7.6 |
| 2              |       |                     |      | 13.5        | 7.7 |
| +50            |       |                     |      | 13.4        | 7.8 |
| 3              |       |                     |      | 13.2        | 8.0 |
| +50            |       |                     |      | 13.0        | 8.2 |
| 4              |       |                     |      | 12.8        | 8.4 |
| +25            |       |                     |      | 12.         |     |

-0.27%

-0.47%

Spk. 8" Oak 33' Lt. 47+60

$$\begin{array}{r} 4.8 \\ C 3.2 \\ \hline 14.4 \end{array}$$

$$\begin{array}{r} (5.7) \\ C 2.3 \\ \hline \end{array}$$

$$(8.7)$$

$$\begin{array}{r} 4.5 \\ C 3.0 \\ \hline 16.0 \end{array}$$

$$5.5$$

$$C 1.7$$

$$7.1$$

$$\begin{array}{r} 4.6 \\ C 3.0 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} (5.1) \\ C 2.5 \\ \hline \end{array}$$

$$(9.0)$$

$$\begin{array}{r} 4.9 \\ C 2.8 \\ \hline 13.6 \end{array}$$

$$\begin{array}{r} (5.3) \\ C 2.4 \\ \hline \end{array}$$

$$(8.8)$$

$$\begin{array}{r} 6.5 \\ C 1.3 \\ \hline 12.6 \end{array}$$

$$\begin{array}{r} (5.8) \\ C 2.0 \\ \hline \end{array}$$

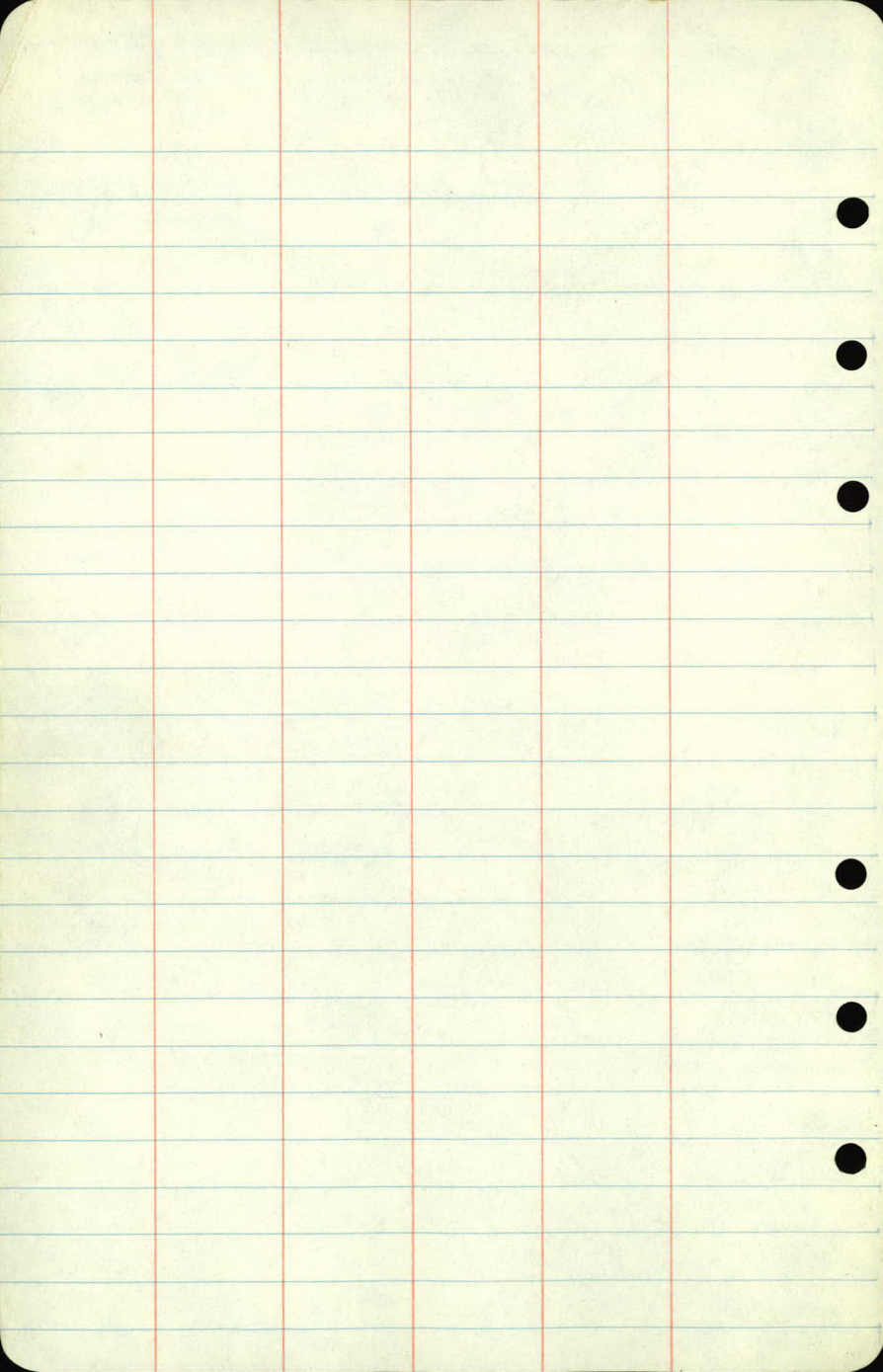
$$(8.0)$$

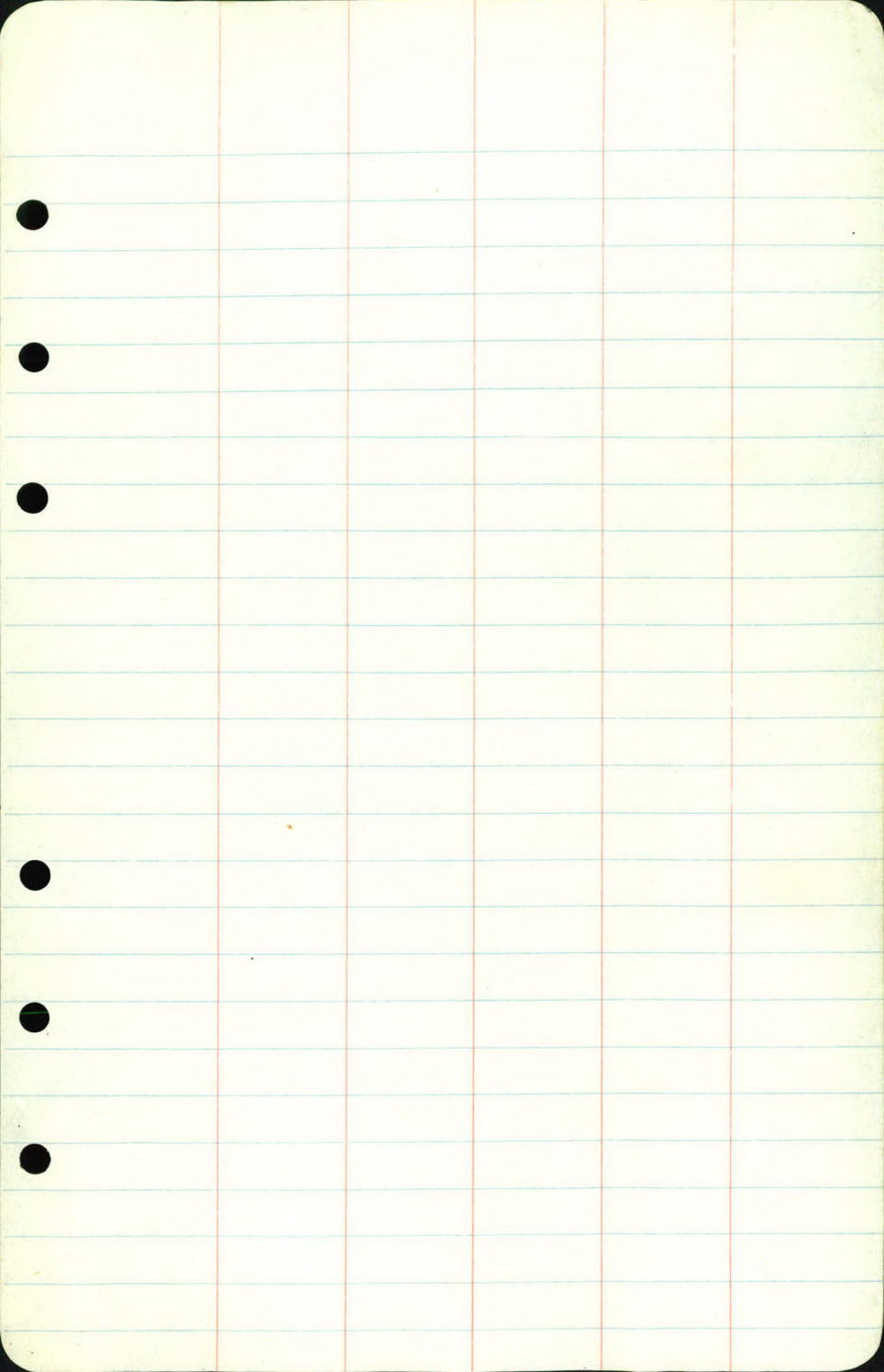
$$\begin{array}{r} 6.0 \\ C 2.0 \\ \hline 14.0 \end{array}$$

$$\begin{array}{r} 3.8 \\ C 4.4 \\ \hline 18.8 \end{array}$$

$$\begin{array}{r} 3.8 \\ C 4.6 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 6.1 \\ C 2.1 \\ \hline 14.8 \end{array}$$







|       |      |        |       |        |      |
|-------|------|--------|-------|--------|------|
| B.M.  | 1.64 | 927.09 |       | 925.45 |      |
| T.P.  | 7.40 | 924.30 | 10.19 | 916.90 |      |
| 58+50 |      |        |       | 13.5   | 10.8 |

|    |  |  |  |      |     |
|----|--|--|--|------|-----|
| 59 |  |  |  | 14.8 | 9.5 |
|----|--|--|--|------|-----|

|     |  |  |  |      |     |
|-----|--|--|--|------|-----|
| +50 |  |  |  | 16.3 | 8.0 |
|-----|--|--|--|------|-----|

|    |  |  |  |      |  |
|----|--|--|--|------|--|
| 60 |  |  |  | 17.8 |  |
|----|--|--|--|------|--|

|     |  |  |  |      |  |
|-----|--|--|--|------|--|
| +50 |  |  |  | 19.3 |  |
|-----|--|--|--|------|--|

|    |  |  |  |      |  |
|----|--|--|--|------|--|
| 61 |  |  |  | 20.8 |  |
|----|--|--|--|------|--|

$$\begin{array}{r} 10.7 \\ 60.1 \end{array}$$

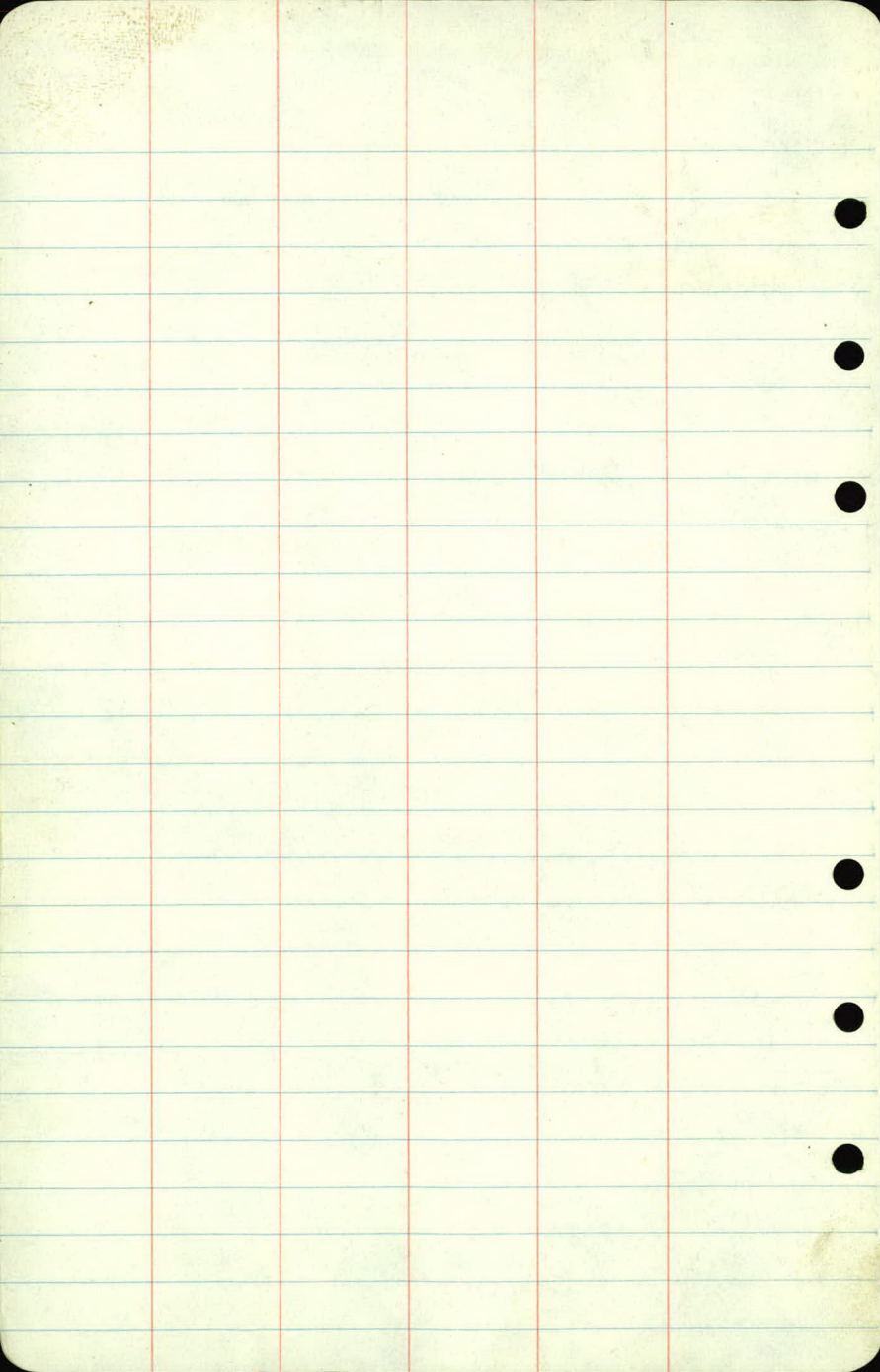
$$\begin{array}{r} 10.4 \\ 60.4 \\ \hline 27.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ 93.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 8.8 \\ 60.7 \end{array}$$

$$\begin{array}{r} 2.7 \\ 1.8 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 7.4 \\ 60.6 \end{array}$$



Snail Lake Blvd.

Add. slope stakes

Sta. 47+50 to Sta. 50

B.M.

7.47

915.09

907.62

48

07.7

7.1

+50

09.7

5.4

49

11.6

3.5

+38

13.0

2.1



$$\begin{array}{r} 2.1 \\ 53.8 \end{array}$$

$$\begin{array}{r} 7.1 \\ 27 \end{array}$$

$$\begin{array}{r} 5.4 \\ 27 \end{array}$$

$$15.1 \left\{ \begin{array}{r} 1.8 \\ 61.7 \\ 52.5 \end{array} \right.$$

$$\begin{array}{r} 3.5 \\ 27 \end{array}$$

$$15.1 \left\{ \begin{array}{r} 0.2 \\ 61.9 \\ 55.5 \end{array} \right.$$

$$\begin{array}{r} 2.1 \\ 27 \end{array}$$

