BK 28 - Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

EDGERTON ST.

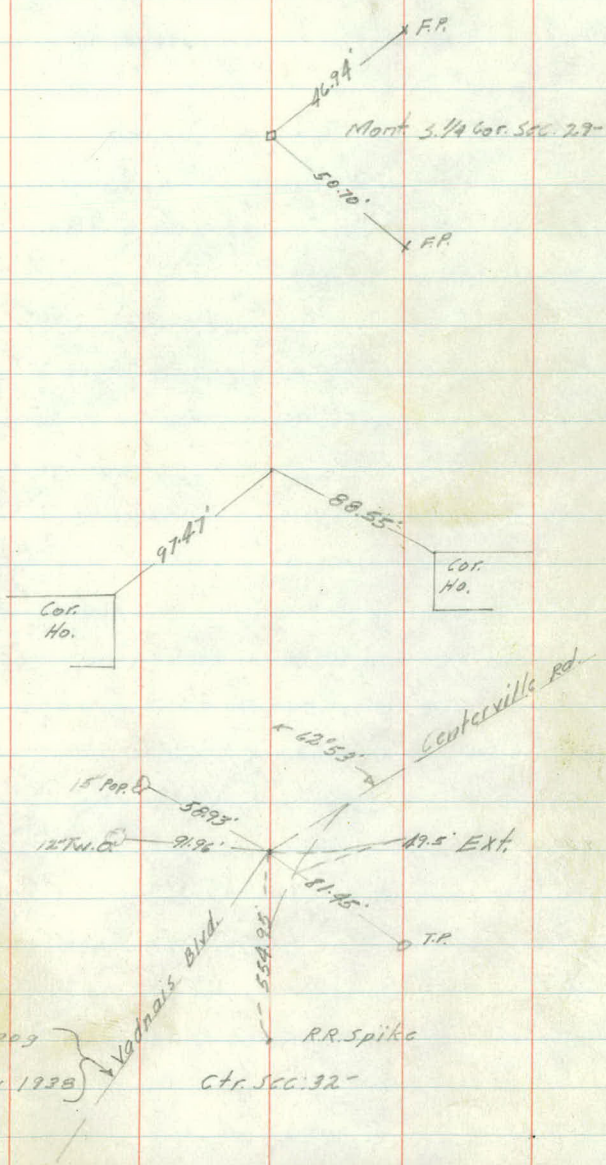
From Centerville Rd. To Kaehler Rd.

Road Acc't. No. 44

Date Filed 4/40 File

Alignment

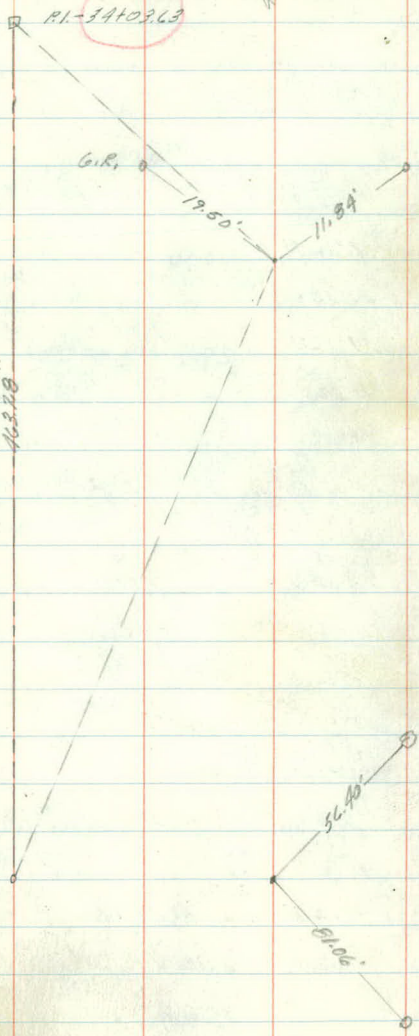
Sta		Point	Δ Lt.	Δ Rt.
20	+746	P.I.		0°18'
16	+00	P.O.T.		
0	+00	= Int. of Centerville Rd. & Vadnais Blvd.		


F.P.
46.94'
Mont. 3.1/4 Cor. Sec. 29-
50.70'
F.P.
97.47'
88.55'
Cor. Ho.
Cor. Ho.
Centerville Rd.
42°53'
15 Pop.
58.93'
12" Tw. Cr.
91.96'
49.5' Ext.
81.45'
T.P.
554.95'
Kadnais Blvd.
For Align & Topog
See Plan Survey 1938
R.R. Spike
Ctr. Sec. 32-

Sta.	Point	Δ Lt	Δ Rt	
32 + 10.05				
	+10.98	P.T.	13°16'	
32			11°52'	Δ - 26°32'
	+75		8°22'	D - 28° - Lt.
31	+63.95	P.I.		T. - 48.73'
	+50		4°52'	L - 94.83'
	+25		1°22'	R - 206.68'
31	+15.22	P.C.	0°00'	
				186.14
	+13.5	P.T.		6°43'
30				6°10.6' Δ 13°26'
	+50			4°10.6' D = 8° - Rt.
29	+30.0	P.I.		T. - 84.42'
29				2°10.6' L. - 167.92'
28	+45.58	P.C.		0°00' R - 716.78'

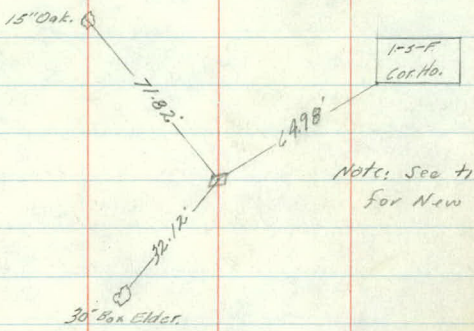
34+02.70

P.I.-34+03.63



Sta.	Point	Δ Lt	Δ Rt.	
℄ 24+28.70 Kochler Rd.				
	+33.22	P.T. =	38°31.5'	
32.29	+25		37°52.8'	
35			34°32.3'	
	+75		31°32.3'	
	+50		28°32.3'	Δ - 77°03'
	+25		25°32.3'	D - 24° - Lt
	+03.63	P.I.		T 191.45
34	02.70		22°32.3'	L - 321.04'
	+75		19°32.3'	R - 240.407
	+50		16°32.3'	
	+25		13°32.3'	
33			10°32.3'	
	+75		7°32.3'	
	+50		4°32.3'	
	+25		1°32.3'	
32	+12.18	P.C.	0°00'	
	+11.25			

88.58
1.49


15" Oak.
71.82'
1-5-P.
Cor No.
64.98'
Note: See tie Book
for New ties 7-20-49
32.12'
30" Box Elder.

Topography

+97-24" Pop - 26' - 29'
+48-24" Stump - 25'
+37-24" Pop - 28'

5 10' 12' Fc - 34'

+95-2-18" willows - 28'

+70-End Brush - 20'

+50-Beg Fc - 34'

4 Brush - 21' 10' 12'

3 Brush - 23' 10' 12' Fc - 34'

Beg - Brush -
+54-End Trees - 29'

2 10' 11'

+43-Beg Scattered Trees - 35'
+17-End

+01-Fc Cor - 34'

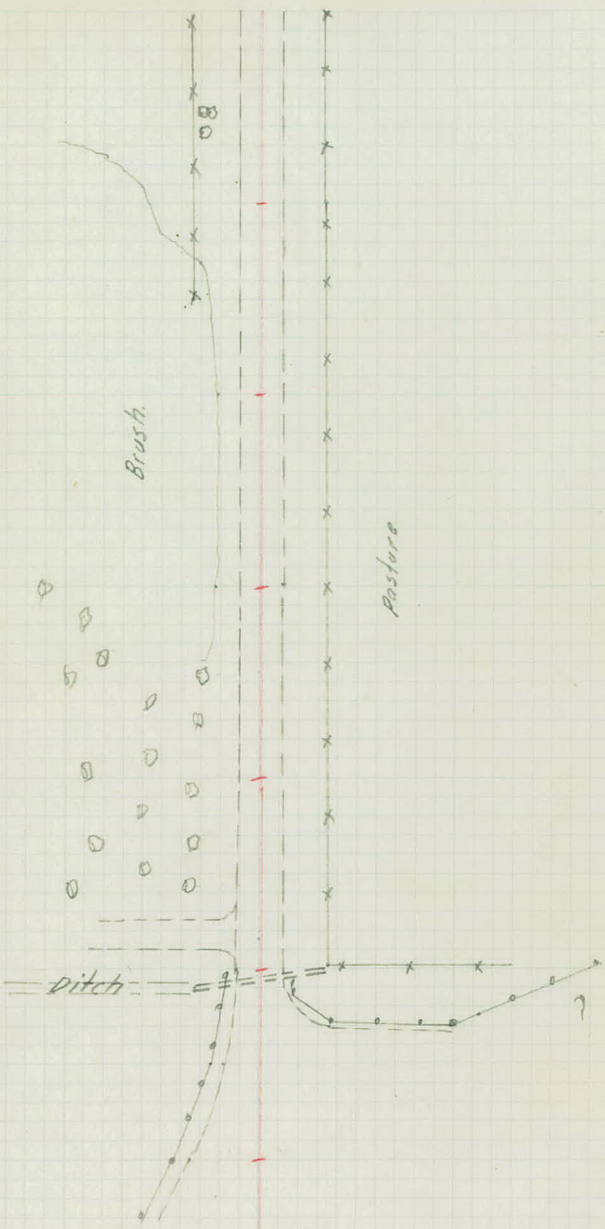
1 12' 13' End 30" Conc Culv - 32'

+92-End G.R - 17'
+30-End 30" Conc Culv - 23'

+92-End G.R - 17'
+75-Δ in G.R - 113'
35' +70-Δ in G.R - 98'

G.R - 25' 17'

0+00 G.R - 44' 36'


Brush
Pasture
ditch

+31-Fc Cor.-21'

12 Fc.-34' 11' 12'

11 11' 12'

10 Fc.-34' 13' 12'

9 11' 12'

8 Fc.-33' 11' 12' End.
+85-Bag Piles

+96-L. Road

7 11' 10'

+37-Fc Cor -31'

6 Fc.-33' 10' 12'

Unrath

19

10' 13'

#59-RP-29'

#109-12" Stump-33'

18

10' 13' FC-33'

17

11' 12'

16

#105-Beg. FC-33'

11' 12'

#96-Ent.
#70-FP.-29'

#59-S.W Cor Ho-85'

#47-3" Elm-35'

#27-N.E Cor Ho-65'
#107-12" Oak-36'

#116-15" Trip. Oak-41'
#109-E.C Cor-39'

15

12' 11'

#88-10" W Oak-35'

#85-Din Fc.-22'

#69-Ent.-30'
#55-Rangetic

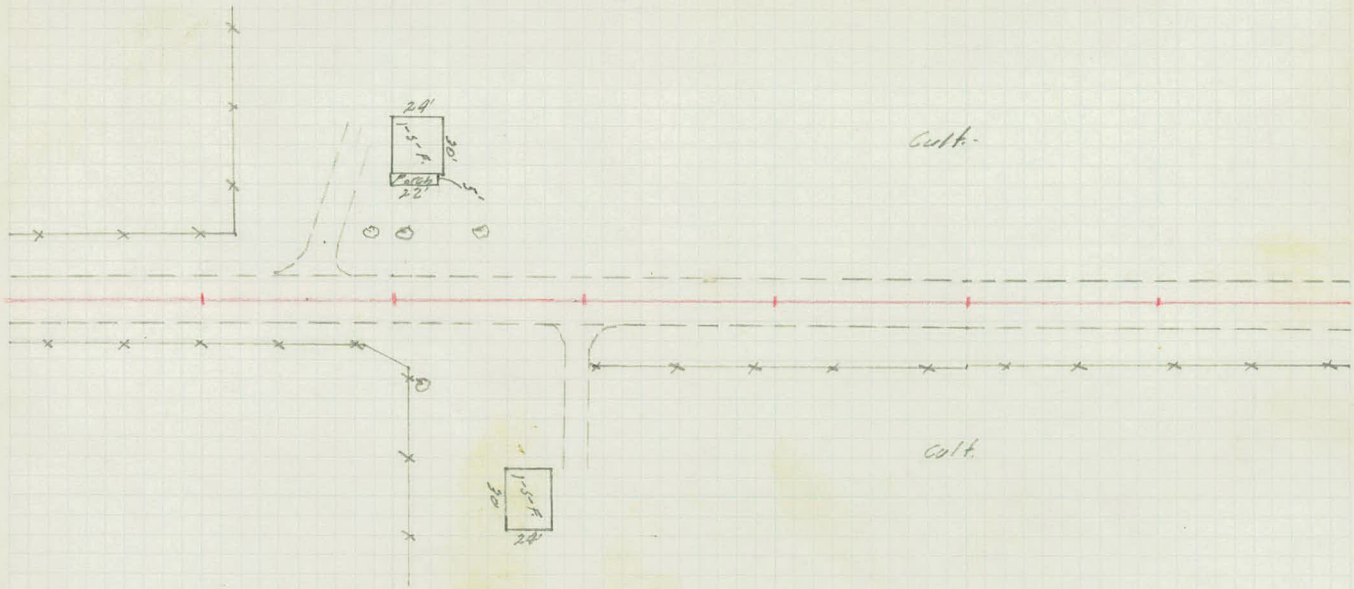
#18-Fc. Cor-34'

14

11' 12' Fc-20'

13

11' 11' Fc.-21'


24'
1-S.F.
30'
Patio
22'
5'
Colt.
Colt.
1-S.F.
24'

26 10' 12'

+34-RP-26'

25 10' 11' Fc-30'

24 10' 12' +14-18" Box Elder-33'

23 11' 12' Fc-32'

22 11' 12' +09-RP-27'
+96-SW Conifer-114'

+63-End

21 10' 12'

20 10' 13' Fc-33'

Curb
Curb
Curb
1-S-A
22'
32'

+71-24" B.Elder-35'

10' 13'

15'-10' -+32'
8' 36'

33 4-15" B.Elders - 36' 5' 26'
+80-End G.R.-4'
+78-24" B.Elder-14'
+70-12" B.Elder-26'

20' +75

G.R. 5'
1'X7' H.W. 48"X113' C.M. +43-End G.R.-15' 1'X7' H.W.
+27-End 48" C.M.-49' G.R. 6' G.R.-13'
+03-End 48" C.M.-62'
32 G.R.-7' G.R. 11'

+75-Beg. G.R.-9'
+68-R.P.-17' +70-Beg. G.R.-15'
+58-R.P.-25'
+46-Hedge 50' 11' 19'
+48-Cor. Hedge-19'
+33-30" Maple-44'

12' 28' +25

31 24" Maple-40' Hedge-21' 11'

+80-24" Maple-33'
+65-12" Maple-30'
+50-10" Elm-29' 25' +53
+33-Δ in Hedge-23' 12' +68-Range Tie
+30-15" Maple-28' +47-Fe. Cor.-23'
+24-Beg. Hedge-58' 11' +41
+26-12" Tw. B.Elder-37'
+10-Δ in Hedge-42'
30 +02-Range Tie 11' 11' Fe.-21'
+94-Beg. Hedge-22'

+80-Group 5-15" B.Elders-24'

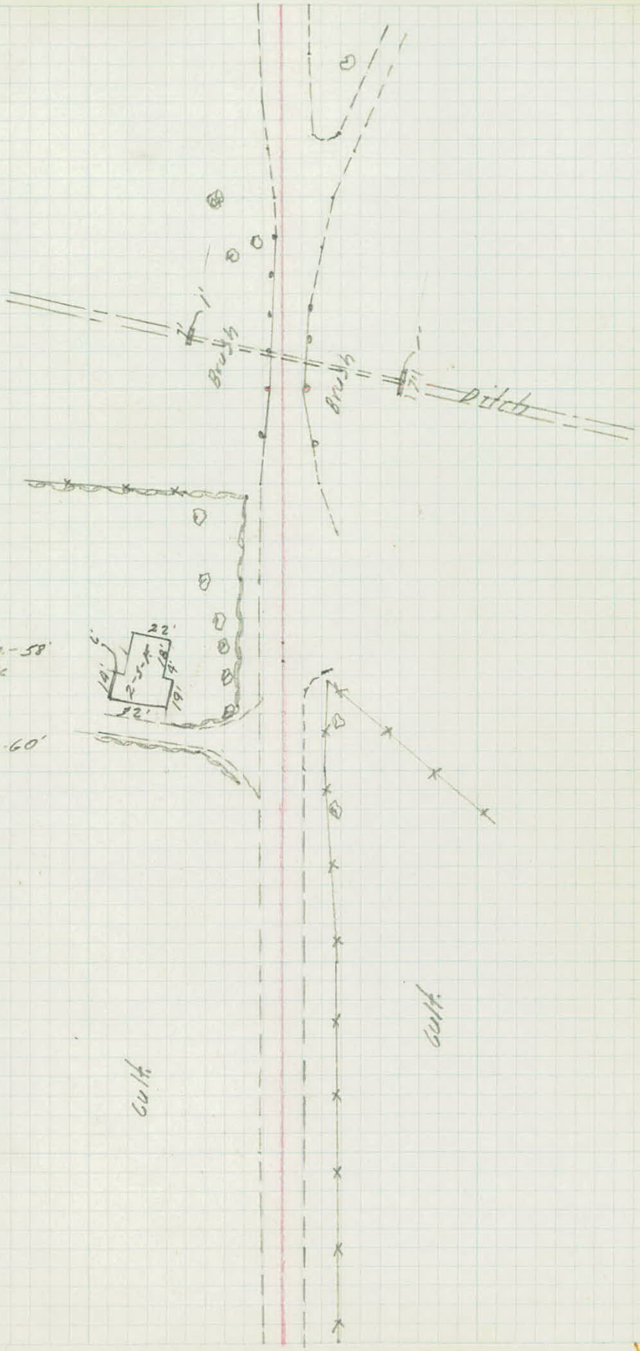
+56-R. Gate
11' 11' Fe.-22'

29 11' 11' Fe.-27'

10' 11' +52-R.P.-24'

28 11' 11'

27 10' 11' Fe.-29'



+68-N.E.Cor.Ho.-58'
+58-Range tie

+32-S.E.Cor.Ho.-60'

+33.22' G.R.-14'
+25-G.R.-14'
+10-End 48"C.M.-59' 1'ST' H.W.
AR"X120'C.M.

G.R-6'
+25- G.R-6' End Wire Mesh Fc.-32'
Fc.-35'
+98-Beg G.R.-6'

35

+74-Beg. G.R.:-14'

8'
13' 10'

+36-RP-23'

13' 11'
12' 12'

+40 G.R-20'

34

Mont. P.I.= 34+03.63

West. East

P.T. 32+10.98 = 0+00

+50

9' 1+00

12' +50

8' +75'

00 25' 2+00

Bench Levels.

Sta.	+	π	−	Elev.	
B.M.	1.16	917.22			(916.06)
T.P.	9.02	921.90	3.34	913.88	
T.P.	9.01	931.52	0.39	922.51	
B.M.			6.46	925.06	
T.P.	0.59	929.16	2.95	928.57	
T.P.	0.29	916.99	12.76	916.70	
T.P.	0.56	904.52	13.03	903.96	
T.P.	3.93	896.39	12.06	892.46	
B.M.			6.05	888.34	

Description

Top Mont Koehler Rd & Edgerton St.

Top Mont. 20+14.6

Top N. End Conc. Str. Long N. End R.R. Bridge & Edgerton St.

Xsections

Sta.	+	℄	−	Elev.
B.M.	7.65	895.99		(888.34)
0 −19				89.9
−36				89.1
−70				87.0
−99	Edge Pav.			85.95
1 −50				84.75
0 +00				90.5
+50				91.2
+79				91.3
	Flow line 30" Conc. Culv.			
1 +00				91.3
+50				91.2
2 +00				91.1

Lt. Q Rt.

Top. N. End Conc. Ctr. Line N. End R.R. Bridge & Edgerton St.

61

69

90

10.04

11.24

Edge Pvt.

Toe Slope → 11.4/60 7.1/50 6.2/44 5.7/36 5.1/17 5.5 6.0/15 6.6/33 6.86/47.8

Toe Slope → 13.5/91 6.6/31 5.6/19 4.8 4.9/14 5.1/30 5.1/30

13.3/50 13.3/34 6.1/24 5.4/15 4.7 5.0/22 5.4/31 5.1/50

80.58 81.03

15.41 14.96

13.3/50 11.8/33 6.7/24 5.4/14 4.7 4.9/13 5.1/18 15.5/31 13.7/35 12.8/50

13.2/50 12.7/31 5.3/18 5.2/12 4.8 5.4/12 5.3/17 13.7/31 12.9/37 12.7/30

14.4/51 12.8/43 11.5/30 5.4/19 5.3/12 4.9 5.3/13 5.4/19 13.3/32 12.5/35 12.3/50

Sta.	+	H	−	Elev.
		895.99		
2 + 50				91.2
3				91.6
+50				92.0
4				92.3
T.P.	8.04	900.51	3.52	892.47
+50				92.4
5				92.7
+50				93.5
6				94.4
+50				95.3
7				96.5
+60				98.4
T.P.	10.93	910.61	0.83	899.68

Lt.					Z			Rt.	
12.9 / 50	12.7 / 32	5.5 / 21	5.2 / 12		4.8	5.3 / 13	5.5 / 20	12.1 / 31	13.0 / 50
12.5 / 50	12.4 / 32	5.0 / 21	4.7 / 12		4.4	5.0 / 13	5.4 / 19	13.0 / 32	13.0 / 50
11.8 / 50	11.7 / 31	4.4 / 19	4.4 / 11		4.0	4.5 / 12	4.6 / 19	12.6 / 33	12.5 / 50
11.4 / 50	10.9 / 30	4.1 / 19	4.0 / 11		3.7	4.1 / 13	4.2 / 20	11.3 / 32	12.1 / 50
160 / 50	151 / 32	89 / 19	82 / 10		81	85 / 12	84 / 19	150 / 33	158 / 50
166 / 50	163 / 35	148 / 30	82 / 19		81 / 11	78 / 12	82 / 20	94 / 32	154 / 50	155 / 50
152 / 50	145 / 34	73 / 19	73 / 11		70	73 / 12	77 / 17	118 / 25	127 / 34	120 / 50
126 / 50	101 / 27	65 / 18	64 / 11		61	63 / 13	66 / 16	78 / 22	79 / 25	75 / 27	75 / 30
60 / 50	55 / 29	77 / 25	77 / 23		56 / 19	57 / 11	52	54 / 12	51 / 28	54 / 50
31 / 50	28 / 30	55 / 25	55 / 23		45 / 19	44 / 11	40	44 / 12	43 / 23	38 / 27	36 / 43	38 / 50
21 / 50	16 / 31	30 / 27	31 / 22		22 / 20	22 / 12	21	25 / 13	26 / 23	22 / 34	23 / 50

Sta	+	HI	−	Elev.
		910.61		
8				99.7
+50				01.1
9				02.7
+50				04.6
10				06.5
+50				08.6
T.P.	12.10	922.15	0.56	910.05
11				10.9
+50				13.2
12				15.0
+33				16.3
	12.08	929.68	4.55	917.60
+70				17.5

Lt. & Rt.

100/50 104/38 119/34 128/29 133/23 115/16 113/11 109/ 113/13 118/23 114/31 113/50

94/50 93/39 103/33 116/28 116/25 97/14 95/ 99/13 102/18 95/23 99/50

78/50 80/34 97/28 98/25 83/14 79/ 83/14 88/20 88/30 91/50

64/50 68/34 72/29 63/15 60/ 65/14 76/18 78/29 86/50

45/30 45/34 59/26 59/23 42/18 41/ 45/14 59/16 61/27 65/50

29/50 17/34 18/24 24/23 15/16 16/13 24/11 20/ 23/14 30/18 36/30 42/50

103/50 105/34 126/18 113/16 117/12 113/ 115/12 113/14 121/22 130/36 137/50

68/50 68/34 67/23 86/18 92/14 90/ 95/12 90/14 91/28 105/50

25/50 38/34 42/24 74/13 72/ 75/12 65/35 66/50

14/20 16/34 18/30 32/25 50/18 65/13 59/ 62/12 26/21 27/35 31/50

66/50 69/34 83/26 109/21 114/17 128/12 122/ 125/12 87/20 90/35 95/50

Sta	+	π	−	Elev.
		929.68		
13				18.5
+50				20.1
14				21.8
+50				23.5
15				25.2
T.P	7.52	934.16	3.04	926.64
+35				26.3
+72				27.4
16				28.1
+50				28.6
17				28.8
+50				28.6

Lt & Rt.

58/50 59/34 70/26 94/21 101/17 117/12 112/— 113/12 107/15 73/20 74/38 80/50

57/50 56/34 57/29 63/21 98/14 96/— 98/12 92/15 64/19 46/50

55/50 51/34 53/31 69/26 70/19 82/13 79/— 83/12 57/19 53/25 58/50

39/50 43/36 40/21 57/16 65/12 62/— 66/12 50/17 51/50

12/50 29/21 49/14 60/12 45/— 48/12 35/20 56/29 39/50

52/50 57/35 64/21 85/13 79/— 83/13 71/19 72/35 78/50

34/50 32/33 41/22 70/12 68/— 73/12 59/19 59/34 66/50

52/50 42/39 30/35 35/22 63/13 61/— 65/14 52/20 59/50

55/50 48/38 38/35 42/20 59/12 56/— 59/13 46/19 45/33 49/50

51/50 49/38 37/35 40/22 48/14 56/12 54/— 58/14 48/19 48/33 L.O.

51/50 44/40 33/34 39/21 50/13 59/12 56/— 59/14 50/19 49/37 55/43 49/50

Sta	+	π	−	Elev.	
		924.16			
18				28.5	
	+50			28.1	
19				27.5	
	+50			26.8	
20				26.2	
	+50			25.5	
	+69			25.3	
B.M.	3.21	928.27	9.10	925.06	(924.06)
21				24.7	
	+50			23.9	
22				23.4	
	+50			22.7	

Lt Q Rt

52/50 48/40 57/36 40/21 52/13 60/12 57/— 60/15 49/20 49/33 48/37 55/44 50/50

57/50 51/42 39/35 45/33 54/14 64/12 61/— 64/15 53/20 53/34 54/39 59/44 53/30

66/50 61/39 52/34 54/25 70/13 67/— 71/15 63/22 62/33 60/38 68/43 61/30

74/50 71/42 57/36 66/25 71/14 78/12 74/— 77/16 70/21 67/36 75/43 68/30

81/50 73/38 66/35 70/26 84/13 80/— 83/14 76/20 74/33 73/36 80/44 73/30

87/50 86/40 75/36 78/29 84/26 89/20 85/14 90/12 87/— 89/14 74/21 77/35 84/43 77/50

83/50 80/35 83/25 85/14 91/13 89/— 92/13 77/21 79/35 85/43 81/50

Top Mont sta 20174L

63/30 56/32 45/22 56/17 32/14 39/12 36/— 38/13 30/17 30/30 33/45 29/50

62/50 52/27 51/21 44/15 47/12 44/— 47/13 42/19 41/38 48/46 44/30

61/30 56/32 53/26 54/21 50/15 49/— 52/13 50/19 56/26 56/30

64/30 62/33 55/28 59/21 55/15 58/13 56/— 60/13 56/17 62/21 64/30 67/30

Sta.	+	I	−	Elev.
		928.27		
23				21.7
+50				20.6
24				19.4
T.P.	1.35	920.73	8.89	919.38
+50				18.2
25				17.0
+50				16.0
26				15.1
+50				14.5
27				14.2
27				
+50				13.9
28				13.8
T. P.	4.79	918.47	7.05	913.68

Lt. R. Rt.

6.6/50 6.7/33 6.1/32 6.3/26 6.4/15 6.9/13 — 6.6 7.1/13 6.9/18 6.9/22 7.3/31 8.1/41 8.1/50

8.3/50 8.3/32 7.9/27 8.3/26 8.3/18 7.7/15 8.0/12 7.7 — 8.3/13 7.6/17 8.6/24 8.8/32 9.8/41 10.1/50

9.5/50 9.7/35 8.8/28 8.9/26 9.0/19 8.4/15 8.9/12 — 8.9 9.4/15 10.9/20 11.8/21 13.1/50

3.1/50 3.1/33 2.4/29 2.7/26 2.3/18 2.0/15 2.7/13 — 2.5 3.0/15 4.3/17 5.7/25 6.6/32 7.3/43 7.5/50

4.4/50 4.3/32 3.6/28 3.9/25 3.6/20 3.2/16 4.0/12 — 3.7 4.1/15 6.9/21 7.8/30 8.8/42 8.7/50

5.9/50 5.9/31 5.2/28 5.4/24 5.3/23 5.4/19 4.9/17 4.9/13 — 4.7 5.2/15 8.8/24 9.2/29 9.4/35 9.9/50

6.7/50 7.0/37 5.8/28 6.4/25 6.0/21 5.8/14 — 5.6 6.0/14 9.4/19 9.7/30 9.7/50

7.3/50 7.6/38 7.0/32 6.7/28 6.8/26 6.4/14 — 6.2 6.6/14 8.6/19 9.3/23 9.1/35 8.9/50

7.8/50 7.8/35 7.5/31 7.0/29 7.6/25 7.0/21 6.9/14 — 4.5 4.8/15 8.6/19 9.2/26 9.3/37 8.7/50

8.1/50 8.0/27 7.4/26 7.0/19 7.3/14 — 6.8 7.2/15 8.8/19 9.4/28 9.9/35 9.0/50

8.4/50 8.4/28 7.8/24 7.4/14 — 6.9 7.2/14 8.7/17 8.3/22 9.0/30 9.5/40 9.3/50

Sta.	+	H	−	Elev.
		918.47		
28	+40			13.8
	+67			13.5
29				13.1
	+50			12.6
30				12.7
	+26			12.7
	+60			12.4
31				12.1
	+25			12.1
	+60			12.2
	+70			12.2
T.P.		0.58	3.82	914.65

Lt. E Rt.

65/50 64/27 60/20 55/18 53/13 47 51/13 54/17 44/20 48/28 53/35 58/50

68/50 68/28 67/21 61/16 57/13 50 54/13 55/18 44/21 46/28 52/38 59/30

67/50 70/29 68/24 70/20 57/14 54 59/12 60/15 55/20 56/28 59/30

55/50 62/33 59/29 63/26 61/21 55/17 58/13 59 68/13 72/15 82/26 86/50

31/50 39/37 48/28 54/13 58 66/14 63/17 67/25 97/35 100/50

33/50 47/32 52/26 55/17 58 65/12 69/36 76/42 81/50

Kochler Rd

39/50 49/29 53/19 59/17 61 66/14 67/50

Kochlerrd

65/50 63/33 65/22 65/13 69 66/30 76/44 94/50

77/50 72/24 70/18 65/16 67/12 69 64/16 68/29 88/35 91/50

87/50 86/36 79/23 80/19 74/14 67/9 63 64/18 67/21 62/23 66/30 89/50

96/50 57/38 76/23 63/21 75/16 66/8 62 64/14 68/19 120/36 134/45 118/50

Sta	+	π	−	Elev.
		915.23		
32				12.1
+03	Flow Line Culv.			
+06				12.1
+22				12.0
+27	Flow Line Culv.			
+32				12.0
+50				12.0
+70				12.2
T.P.	9.99	920.63	4.59	910.64
+81				12.4
33				12.7
+30				13.1

Lt. ℄ Rt.

915.23
4.24 (905.85) H.I. 13.62 (901.61)

915.23
T.P. 0.66 (902.30) H.I. 13.59 (901.64)

℄ +6.2

+9.8

6.0/60 7.1/22 5.8/30 12.5/22 3.3/8 3.1/— 3.2/12 13.0/25 3.3/34 7.4/40 9.2/59 (6.3/59 Inside Edge H.W. Top.)

90.23
12.07

+6.2

+9.8

6.8/60 7.4/44 6.5/31 13.2/22 3.3/8 3.1/— 3.1/12 13.7/25 5.3/31 7.6/40 9.7/62 (6.3/62 Top Inside Edge H.W.)

+6.1

+9.7

(Top Inside Edge H.W. 10.35/48) 7.3/26 3.4/7 3.2/— 3.0/14 11.1/24 3.9/33 3.9/43 2.6/60

+6.1

89.38
16.47

+6.1

(Top Inside Edge H.W. 10.6/47) 8.2/32 5.1/24 3.4/7 3.2/— 2.9/15 13.0/31 11.5/37 9.7/43 9.7/50

+6.1

5.0/50 5.0/41 6.0/34 13.7/22 3.4/7 3.2/— 2.6/15 3.5/23 5.6/29 3.9/35 4.3/50

6.8/50 6.3/34 6.1/23 7.4/21 6.7/10 3.2/50 3.0/— 2.4/9 2.3/19 3.4/25 3.4/34 1.3/40 1.0/50

Top Rock.

10.7/50 10.8/36 9.0/17 8.0/10 8.3/7 8.2/— 7.6/11 7.5/24 8.9/30 8.9/40 6.2/47 6.2/50

7.4/50 6.7/41 7.4/22 7.2/10 8.2/5 7.9/— 7.4/12 7.7/27 8.1/34 9.3/40 9.1/48 5.9/53

7.0/50 7.6/40 6.9/21 6.4/13 8.0/9 7.5/— 7.4/6 7.5/16 6.9/25 6.9/41 6.8/50

Sta.	+	H	−	Elev.	
		92063			
33	+35			13.1	
	+65			13.3	
34				13.6	
	+29			13.8	
	+81			14.3	
T.P.		1.77	918.67	3.73	916.90
	+81			(14.3)	
35	+06			14.6	
	+10	Flow Line 48" C.M.			
	+14			14.7	
	+33.22			14.8	
B.M.				916.09	(916.06)

11/15/39
K.A.
L.C.
M.B.
Md.G.

Lt. | R. | Rt.

71/50 76/42 65/20 69/13 78/10 75/15 75/21 55/27 68/45 67/50

66/50 77/41 77/29 72/19 66/14 76/13 79/12 73/17 72/22 53/32 49/45 50/50 53/50

63/50 81/44 75/38 79/29 69/15 75/14 70/12 70/18 77/27 75/31 83/42 47/50 47/50

98/50 65/40 80/33 75/24 71/15 76/15 68/14 68/20 75/25 98/42 83/58 2.2

118/26 77/17 69/13 63/8 63/12 62/17 82/25 90/38 49/50 30

Hi. = 904.83 +9.5

91/60 62/45 134/30 (20)

+9.8

Top Inside Edge H.W. → 101/57 113/57 105/48 76/40 67/18 46/14 41/9 42/16 50/24 75/29 60/39 51/50 2.7

88.71
16.12
59'

+9.9

101/61.0 109/27 105/45 50/34.0 55/17 46/13 40/7 40/13 51/20 84/25 69/28 65/38 55/50

+10.0

63/63 83/53 76/41 50/34 43/15 39/9 43/15.7 24 15.9/27 119/38 78/50

Top Mont. Kochler Rd. & Edgerton St.

Edgerton St.
slope stakes.

sta	+	T	−	Grade	
B.M.	12.64	901.28			888.64
0 +00					
+50					
+79					

Gr. Rod Lt. & Rt.

Top N. End Conc. Str. Pier Edgerton St. & R.R. Bridge

Sta.	+	π	−	Grade	
1					
	+50				
2					
	+50				
3					
	+50				
4					
	+50				
5					
	+50				
B.M.		12.64	901.28		888.64
6					
	+30				

Gr. Rod.	Lt.	℄	Rt.
			$\frac{6.4}{1.9}$/26.8
6.3	23.0/$\frac{8.3}{0.0}$	$\frac{}{0.0}$	

Sta.	+	H	−	Grade
		901.28		
+60				
7				
+27				
+72				
8				
T.P.	12.91	912.52	1.67	89961
+50				
9				
+50				
T.P.				
10				
T.P.	10.33	921.13	1.72	91080
+50				08.6
T.P.				
11				10.7

Gr. Rod.	Lt.	Rt.	Rt.
5.6	23.0 / 176 / R.00	00	58 / R1.8 / 24.6
4.7	24.2 / 161 / R.06	00	50 / R1.7 / 26.4
3.8	24.8 / 149 / R.09	00	41 / R1.7 / 26.4
2.5	24.8 / 136 / R.09	00	31 / R1.4 / 25.8
1.7	21.8 / 137 / R.00	00	23 / R1.4 / 25.8
11.5	23.6 / 132 / R0.3	0.0	11.2 / R.03 / 27.6
9.8	24.0 / 114 / R.05	00	10.4 / R1.4 / 25.8
8.0	24.6 / 92 / R.08	0.0	87 / R.03 / 23.6
6.1	26.4 / 64 / R1.7	00	75 / R.06 / 24.2
12.6	27.4 / 124 / 10.2	00	135 / R.08 / 24.6
10.4	28.6 / 96 / 10.8	103 / 10.1	11.3 / R1.1 / 25.2

Sta.	+	H	−	Grade	
		921.13			
11 +50				12.5	
BM	10.15	930.47	0.93	920.20	(920.32)
12				14.3	
+33				15.5	
+70				16.8	
13				17.9	
+50				19.7	
14				21.5	
+50				23.2	
15				24.6	
+35				25.5	
T.P.	6.33	932.57	3.23	927.24	
+72				26.3	

1-16-41

Gr. Rod.	Lt.	&	Rt.
8.6	33.2 / 55 / +2.1	8.1 / +0.5	80 / +0.6 / 28.2'
Nail 10 Ft Post 50' Rt. 12+33			
16.2 (6.9)	35.0' / 122 / +4.0	15.6 / +0.6	147 / +1.5 / 30.0'
15.0	37.2' / 99 / +5.1	14.3 / +0.7	110 / +2.0 / 33.0'
13.7	39.4' / 75 / +4.2	13.0 / +0.7	96 / +4.1 / 33.0'
12.6	39.4' / 69 / +5.7	12.1 / +0.6	82 / +4.4 / 33.0'
10.8	39.4' / 66 / +4.2	10.4 / +0.4	72 / +3.6 / 33.0'
9.0	33.0' / 58 / +3.2	8.7 / +0.3	63 / +2.7 / 32.4'
7.3	31.6' / 50 / +2.3	7.1 / +0.2	46 / +1.6 / 30.2'
5.9	32.6' / 31 / +2.8	5.4 / +0.5	44 / +1.5 / 30.0'
5.0	32.8' / 21 / +3.9	4.2 / +0.8	36 / +1.4 / 29.8'
7.3	33.0' / 27 / +4.6	4.2 / +1.1	53 / +2.0 / 31.0'

Sta.	+	T	−	Grade	
		933.57			
16				26.9	
+50				27.6	
17				28.2	
+50				28.5	
18				28.6	
+50				28.4	
19				28.1	
+50				27.5	
20				26.6	
B					
+50				25.7	
B.M.	3.72	928.78	8.55	925.02	(925.06)
+69				25.3	
B.M.					(925.06)

Gr. Rod.	Lt.	℄	Rt.
6.7	33.0'/2.3/+4.4	5.6/+1.1	5.2/+1.5/30.0'
6.0	32.6'/3.2/+2.8	5.0/+1.0	4.0/+2.0/31.0'
5.4	32.6'/3.1/+2.3	4.9/+0.5	4.2/+1.2/29.4'
5.1	31.6'/2.8/+2.3	5.0/+0.1	4.6/+0.6/28.2'
5.0	30.8'/3.1/+1.9	5.1/-0.1	4.3/+0.7/28.4'
5.2	25.6'/3.4/+1.8	5.6/-0.4	4.8/+0.4/27.8'
5.5	28.4'/4.8/+0.7	6.1/-0.6	5.7/+1.8/26.6'
6.1	28.7'/5.5/+0.6	6.8/-0.7	6.3/+1.8/26.6'
7.0	28.2'/6.4/+0.6	7.5/-0.5	6.8/+0.2/27.4'
7.9	28.4'/7.2/+0.7	8.1/-0.2	7.0/+0.9/28.8'
3.5	28.6'/2.7/+0.8	3.6	2.4/+1.1/29.2'

Top Mont sta 20+74.6

Sta.	+	H	−	Grade
		928.78		
21				24.7
21 +50				23.8
T.P.	1.58	925.22	5.14	923.64
22				22.8
+50				21.9
23				20.9
+50				20.0
24				19.0
+50				18.1
25				17.3
+60				16.6
26				16.0
+50				15.5
27				15.1

Gr. Rod	Lt	C	Rt
4.1	25.4 / 54 / 10.07	41 / 0.0	34 / +0.7 / 28.4
5.0	25.8 / 56 / 10.19	49 / +0.1	51 / 10.19 / 26.8
Nail in PP Rt 2 Lt			
2.4	27.6 / 21 / +0.3	18 / +0.6	25 / 10.19 / 26.8
3.3	28.6 / 25 / +0.8	25 / +0.8	30 / +0.3 / 27.6
4.3	29.4 / 31 / +1.2	35 / +0.8	40 / +0.3 / 27.6
5.2	27.4 / 50 / +0.2	47 / +0.5	54 / 10.18 / 24.6
6.2	28.4 / 55 / +0.7	58 / +0.4	64 / 10.1 / 23.2
7.1	27.2 / 70 / +0.1	70 / +0.1	91 / -2.0 / 19.0
7.9	25.8 / 85 / 10.4	82 / -0.3	118 / -3.9 / 22.8
8.6	24.8 / 96 / 10.09	92 / -0.6	135 / -4.9 / 24.8
9.2	23.8 / 108 / 10.04	101 / -0.9	142 / -5.0 / 25.0
9.7	24.3 / 112 / 10.05	107 / -1.0	137 / -4.0 / 23.0
10.1		110 / -0.9	ok.

Sta	+	H	−	Grade	Gr. Rod	Ditch Gr. Lt
B.M.	1.03	917.09			916.06	
27				15.1		13.1
+50				14.8	4.2	12.9
28				14.4	4.4	12.7
+40				14.1	4.6	12.5
+67				13.9	4.7	12.4
29				13.7	4.8	12.3
+50				13.4	5.0	12.1
B.M.	1.01	917.07			916.06	
30				13.0	5.2	11.9
+30				12.8	5.3	11.8
+60	Reversal of Transition			12.7	5.4	11.7
31				12.6	5.6	11.5

Gr. Rod	Lt.	Wide	Super Elev	℄ Super Elev	Wide	Rt.
Top Mont.						
2.0	23.1'/3.7 / R0.3		0.0	(2.9 / -0.9)		5.1 / -3.1 / 21.2'
2.3	24.2'/3.6 / R0.6		+0.1	(3.1 / -0.1) -0.0		5.0 / -2.7 / 20.4'
2.7	24.0'/4.0 / R0.4		+0.4	(3.3 / -0.6) -0.4'	0.0	4.7 / R0.4 / 23.8'
3.0	23.4'/4.6 / R0.0		+0.6	(3.4 / -0.4) -0.6	0.9'	3.5 / +0.1 / 28.1'
3.2	20.2'/5.0 / -2.6		+0.8	(3.7 / -0.5) -0.9	1.6	3.2 / +0.9 / 30.4'
3.4	21.0'/5.5 / -3.0		+0.9	(4.1 / -0.7) -1.0	2.1'	4.2 / +0.2 / 29.5'
3.7	24.2/4.6 / R0.4		+0.9	(4.6 / -0.1) -1.0	2.1'	6.7 / R0.0 / 24.0'
4.1	26.4'/3.5 / R1.8		+0.7	(4.5 / -0.4) -0.8	1.6'	5.6 / R1.3 / 27.0'
4.3	25.6'/3.3 / R2.0		+0.3	(4.5 / 0.2) -0.3	0.7'	5.6 / R1.0 / 25.7'
4.4	24.4'/3.7 / R1.7	0.0	0.0	(4.5 / -0.4) 0.0	0.0	
4.5	24.2'/5.1 / R0.9	1.4'	-0.4'	5.1		

Sta.		+	⊼	−	Grade	Gr. Rod	Ditch Gr. Lt
			917.07				
B.M.		1.05	917.11			916.06	
31	+25				12.5		
	+60				12.7		
	+70	℄=5.5 Rt. Reg. ℄			12.6		
32					12.6		
	+06				12.6		
	+11.25 = P.C.						
	+22	1°17.4			12.7		
	+32	2°29.4' End Transition			12.8		
	+50	4°39'			12.9		
	+70	7°03'			13.0		
	+81	8°22'			13.1		
33		10°39'			13.2		

Gr. Bod		Lt.	Wide.	super Elev.	super Rt.	Wide	Rt.
4.6	1.0	25.7 / 5.7 / 10.7	3.3	-0.8	5.1 / -0.5		
4.4	1.2	25.5 / 6.3 / 10.1	4.3	-1.0	5.0 / -0.6 / +0.9		
4.5	1.6	22.9 / 6.6 / 10.0	4.3	+1.1	4.9 / -0.4 / +0.0		7.6 / -3.1 / 19.7
4.5	1.6	38.2 / 19.2 / -12.6	4.3	-1.1	5.0 / -0.5 / +0.6		23.3 / -19.4 / 42.6
			4.2		+0.8		
4.4		42.7 / 21.2 / 15.8	4.0		5.1 / -0.7 / +0.9		19.5 / -14.1 / 39.2
4.3		45.0 / 22.7 / -17.3	4.0		5.1 / -0.8 / +0.9		14.2 / -10.8 / 31.2
4.2		36.3 / 16.8 / 11.3			5.1 / -0.9		
4.1		22.9 / 7.5 / -2.6			4.9 / -0.8		
4.0		27.0 / 6.1 / 10.05			4.7 / -0.7		
3.9		32.0 / 3.5 / 11.5		-1	4.4 / -0.5		

Sta.	+	H	−	Grade	
B.M.	2.81	918.87			916.06
33 +30				13.5	
+35				13.5	
+65				13.8	
34				14.1	
+29				14.3	
+50				14.5	
+81				14.8	
35				14.9	
+06				15.0	
+14				15.0	
+32.29				15.2	
B.M.					916.06

Gr. Rod.	Lt	Widening	Super Elev	Super Elev	Widening	Rt.
		4.0	-1.1	+0.9		
5.4	31.4' / 5.3 / +1.2		5.8 / -0.4			
5.4						
5.1	29.4' / 6.0 / +0.2		5.5 / -0.4			4.2 / BT. / 19.5
4.8	28.4' / 6.2 / +1.2		5.2 / -0.4			-6.0 / -2.1 / 19.2'
4.5	28.4' / 5.9 / +1.2		5.1 / -0.6			8.1 / -4.5 / 21.8'
4.3	28.6' / 5.6 / +1.3	4.0	-1.1	(4.9 / -0.6) +0.9		7.8 / -4.4 / 21.6'
4.1	38.8' / 17.3 / 13.2	4.0	-0.9	(5.1 / -0.5) +0.8		6.7 / -3.4 / 20.1'
4.0	44.1' / 22.2 / 17.4	3.6'	-0.8	(4.3 / -0.3) +0.7		4.6 / -1.3 / 17.0'
3.9		3.4'	-0.8	+0.7		
3.7	48.8' / 25.0 / -20.4	3.2'	-0.7	4.2 / -0.3 +0.6		8.4 / -5.1 / 22.7'
		1.9'	-0.6	+0.3		

Top Mont Kobler Rd & Edgerton St.

Slope Stakes.

Grade change.

% of present road = % grade as staked.

Sta.	+	π	−	Grade
24				
	+50			
25				
	+50			
26				
	+50			
27				
	+50			
28				

Grade Rod	Lt.	℄	Rt.
1.5	27.6' / 1.2 / +0.3	1.5	3.5 / ℄ 0.0 / 22.2'
2.7			

Sta.	+	∧	−	Grade

Gr. Rod.	Lt.	℄	Rt.

Special Ditch Lt
Sta. 7+00 to 9+16.5

Sta.	+	Δ	−	Elev	
B.M.	4.26				(902.28)
7 +00					
+45					
+92					
8					
+35					
+65					
9					
+16.5					
+65.5					

Ditch Cr. Rod. Lt. ℄

Top S. W. Cor. Bottom Step Lt. Sta. 9+37

6.1	17.9' / 4.2 / Rc 1.9	5.6
6.0	18.8' / 3.2 / Rc 2.8	5.5
5.6	19.8' / 1.8 / Rc 3.8	5.1
		4.9

Elev. Bottom Wall = 5.15 / 5.38

50

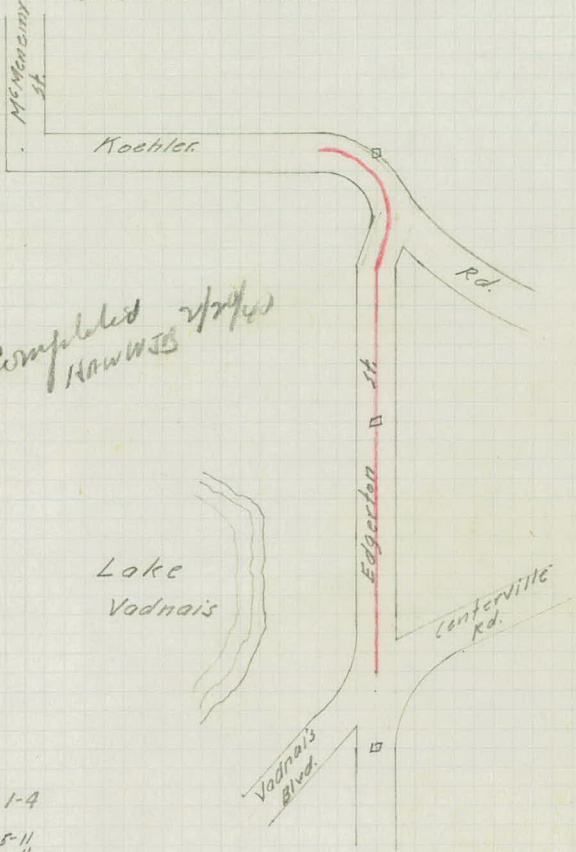
38 3 1 1
10 0 3 7

29 3 0 0
20 7 7 4 6
8 5 5 4

PLAN SURVEY

EDGERTON ST.

Centerville Rd to Koehler Rd.



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