

BK 27 - Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

KOEHLER RD.

From McMenemy St To Edgerton St

Road Acc't. No. 27

Filed 4/40

File

*At Carterville Rd
Plan 52748*

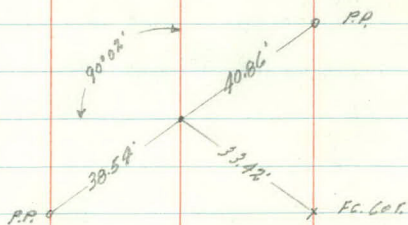
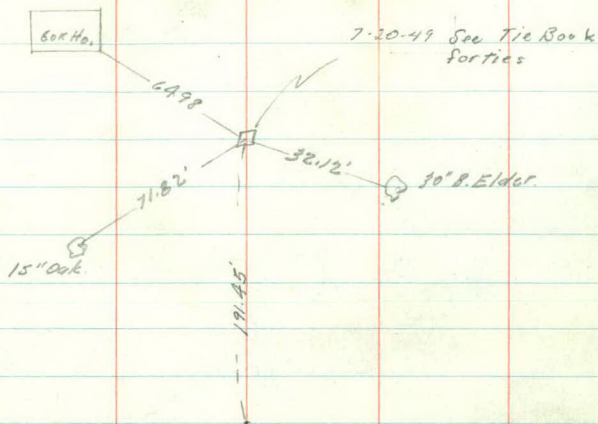
1
Alignment

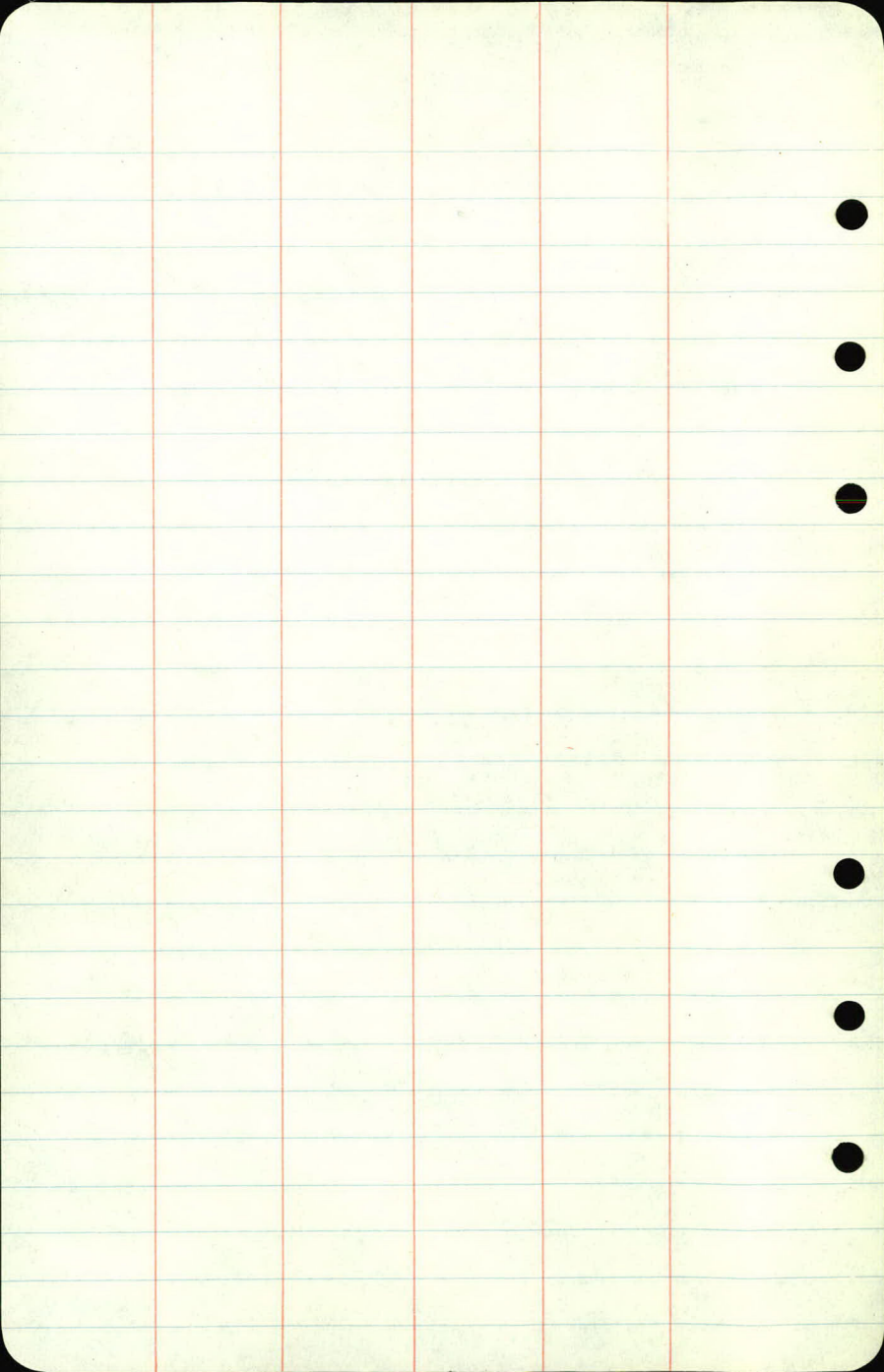
Sta.	Point	Δ Lt.	Δ Rt.
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= P.T. 35+33.22

24	128.70	P.O.T = P.T. 34+03.63	Edgerton, St.
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0	+00	= R. McManamy St.	
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Topography

+53-End 12' C.M.-17'

+60-End 12' C.M.-20'

+A9-15' Top.-20'

+27-Fe Cor.-28'

5

9' 14'

+25-PP-27'

4

8' 15'

Fe-29'

+16-PP-25'

9' 15'

Fe-27'

3

+29-PP-27'

2

12' 13'

Fe-30'

1

14' 11'

Fe-28'

+65- 16'

+31- 29' 8' 131-PP-26'

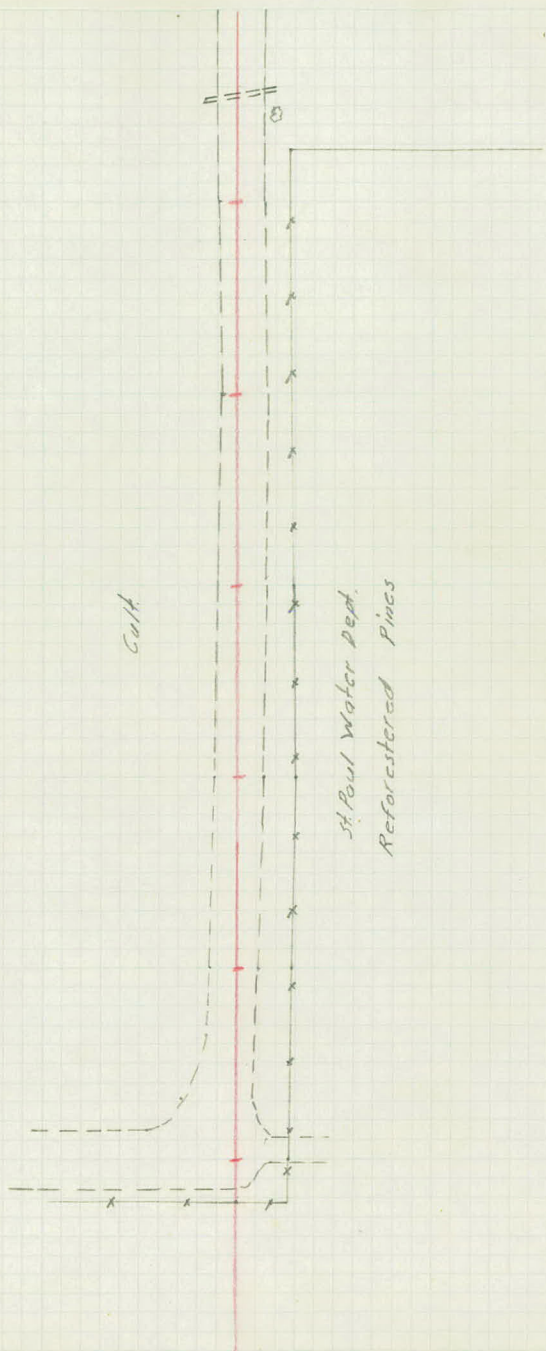
+16-46'

+35-End-

Fe-26'

0 to 0

-15-Shoulder Line-15'



Calk

St. Paul Water Dept.
Reforested Pines

+90-Ent 1st 2

80'x26'x22'

+95-End G.R.-10'

Tic +55-Ent-33'

+98-Retain. Wall-19'-22'

+96-1st of H.W. Retain wall-31'

+95-End 10' G.R.-31'

+90-Cor Conc H.W.-27' End Retain wall-45.5'

Head wall-1' Thick 7' wide

+78-2' B.E.-27' Dike

12

12'

G.R.-10' Fe-24'

+61-8'10"x40' C.M.

19.5'

29.5'

11

12'

G.R. 10'

+11-Bcg. G.R.-10'

+59-Fe Cor-24'

End Cult.

+27-PP-26'

+65-PP-17'

10

10' 12'

+85-Head 40-33'

3.3' outside wall R. next to wall.

+65-Cor Wall-12.5'

+39-6.5' wide Conc steps.

+29-Cor 19.0-52.5'

+31-2nd Co.-28.5'

+17-24' B.E.-21' 17.5'

+16.4-Cor Wall-20.6-12.5'

9

9' 12'

+68-15' B.E.-21'

+48-15' B.E.-21'

+53-Ent.

+26-4' Mortar Ash-19'

+15-End Cult.

8

9' 15'

+25-PP-26'

7

10' 14'

+58-PP-15'

+24-6'2.4"x38' C.M.

18'

20' 24'

6

10' 14'

Calv. in Ch. H. W.
H. W. G. Below Retain Wall

Pasture

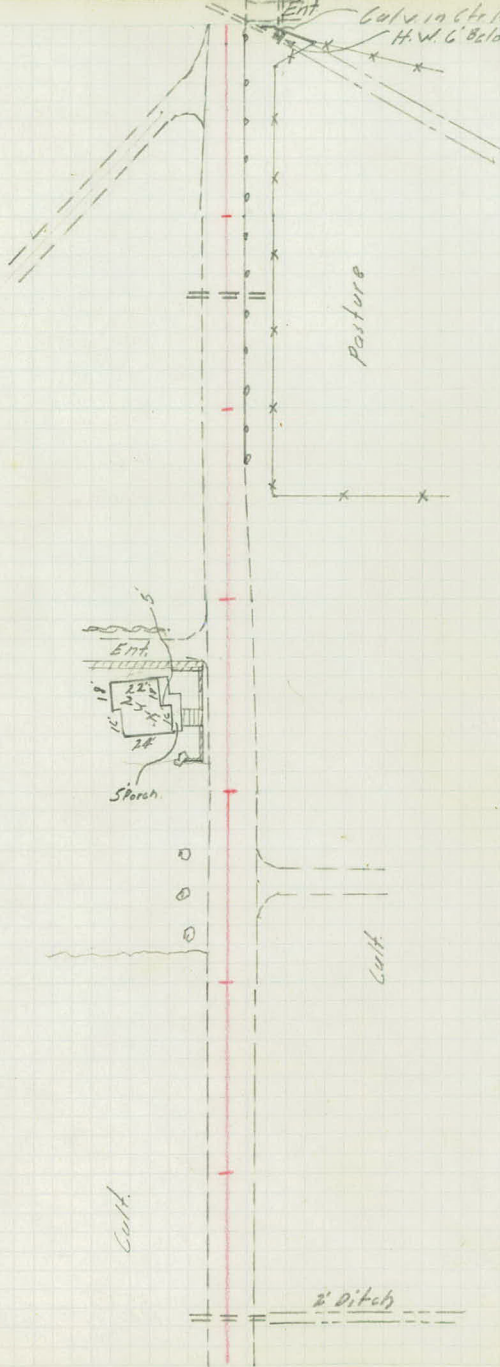
+75 Ent.

Porch

Cult.

Cult.

2' ditch



+51-15" Oak-29'
+46-P.P.-19'

Uncult.
+63-Vine Fc.-36'
Endcult.
+33-P.P.-25'

19 Fc.-32'

12' 11'

+72-20" Oak-5/p-20'

+21-End f- $\frac{12' \times 18' G.M.}{14'}$

18 Fc.-32'

11' 11'

+82-6" Elm-31'
+74-Cor Ho.-56' N.W.
+56-18" B.C.-31'

17 Fc.-32'

11' 11'

+32-P.P.-19'

+30-P.P.-25'

16 Fc.-32'

10' 11'

15 Fc.-33'

11' 11'

+20-10'

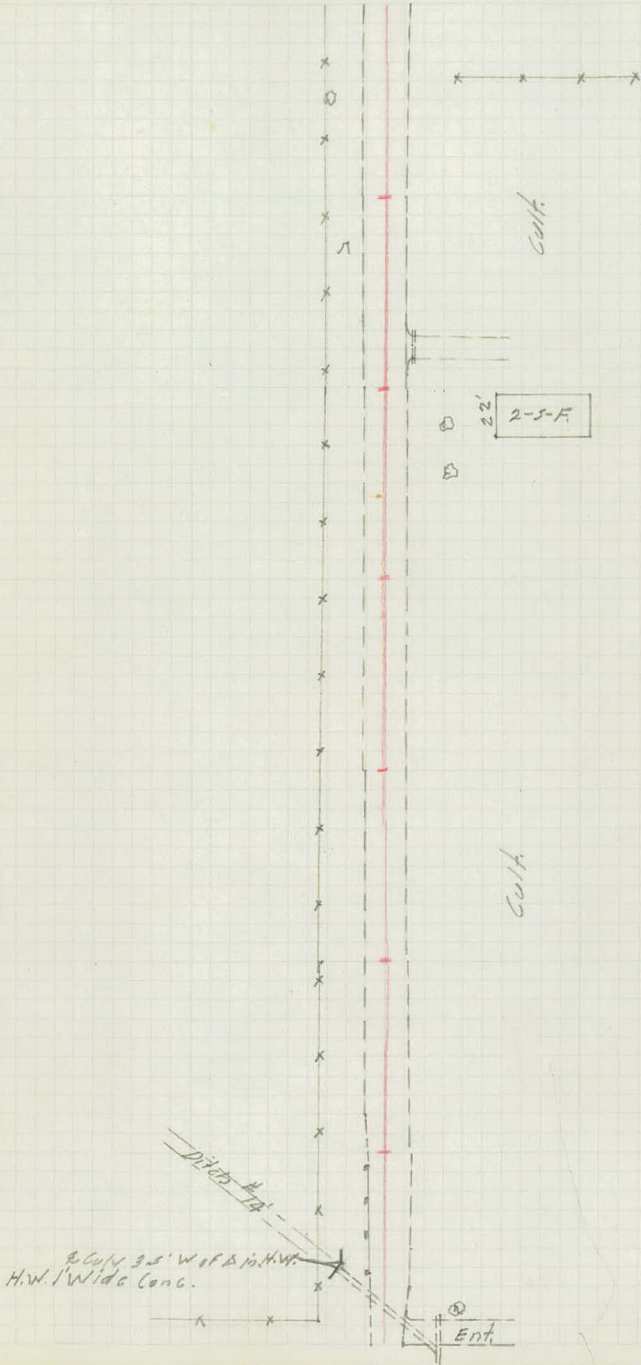
14 +93-End G.R.-9'

9' 13'

+37-BC9 G.R.-8'
+49-End H.W.-22'
+43-Δ 10" H.W.-21'
+35-Cor H.W.-28'
+11-Fc C.B.K.-33'
+07-P.P.-18'

13' +50
8' 13' +30
+27-P.P.-25'
+18-80" Elm-36'
+15-End 10" G.P.P.-29'

13 9' 10'



2 Cult 9.5' W of A in H.W.
H.W. 1' Wide Conc.

24 Fc-32' G.R. 6' G.R. 10'

+84-End 48" 19-43' 1'x7' H.W.

+74-Bcg. G.R. -19'

+30-30" E/m-27' 16'
+22-Bcg. G.R. -5'

23 Fc-32' 8' 16'

+90-Ent-- 15'x20' G.M.
15'

+75-P.P.-19'

+66-Nudge-26'

+34-P.P.-34'

+26-18" S.P.-20'

22 15" B.E.-33' Fc-32' 9' 13'

+90-12" B.E.-32'

+01-Ch 2'x2' A/16r-33'

+95-Ent-- 15'x20' G.M.
22'

+08-Ch 2'x2' A/16r-33'

+66-Bow 1" Poles-36'

+60-Kow 2" Poles-33'

+54-6" Chin & Elm-33'

+15-24" B.E.-28'

2.1 Fc-32' 10' 14'

+00-4" Chin Elm-33'

+28-2" Two Elm-33'

+22-P.P.-50'

+27-4" Elm-32'

2.0 Fc-32' 11 13'



xsections

Sta	+ (2.92)	π	-	Elev	
B.M.	3.59	905.87			(902.28)
T.P.	9.73	909.08	6.52	899.35	
T.P.	4.67	912.02	1.73	907.35	
B.M.			4.81	907.21	
B.M.	8.92	916.13			(907.21)
0	+00			06.2	
	+16			06.7	
	+23			06.9	
	+30			07.0	
	+75			07.2	
1				07.3	
	+45			07.3	
2				06.8	
	+45			06.0	
T.P.	5.34	910.47	11.00	905.13	

Lt 4 Rt.

Top s.w. Cor. Bottom Step Lt 9+37

Spk. in P.R.N. W. Kochler Rd & McManamy St.

$\frac{89}{50}$ $\frac{89}{24}$ $\frac{99}{-}$ $\frac{101}{10}$ $\frac{111}{26}$ $\frac{116}{44}$ $\frac{122}{50}$

$\frac{94}{50}$ $\frac{95}{42}$ $\frac{89}{26}$ $\frac{89}{10}$ $\frac{94}{-}$ $\frac{101}{9}$ $\frac{108}{26}$ $\frac{122}{50}$

$\frac{101}{50}$ $\frac{99}{38}$ $\frac{91}{22}$ $\frac{88}{15}$ $\frac{92}{15}$ $\frac{99}{18}$ $\frac{80}{27}$ $\frac{81}{25}$ $\frac{88}{50}$ $\frac{104}{50}$

$\frac{74}{50}$ $\frac{69}{36}$ $\frac{99}{29}$ $\frac{89}{72}$ $\frac{91}{7}$ $\frac{94}{11}$ $\frac{99}{15}$ $\frac{96}{18}$ $\frac{80}{27}$ $\frac{81}{25}$ $\frac{81}{34}$ $\frac{87}{37}$ $\frac{102}{50}$

$\frac{45}{50}$ $\frac{54}{40}$ $\frac{76}{29}$ $\frac{101}{24}$ $\frac{101}{22}$ $\frac{94}{19}$ $\frac{89}{14}$ $\frac{93}{23}$ $\frac{31}{31}$ $\frac{35}{33}$ $\frac{43}{39}$ $\frac{41}{50}$

$\frac{42}{50}$ $\frac{48}{39}$ $\frac{70}{28}$ $\frac{99}{24}$ $\frac{99}{22}$ $\frac{92}{20}$ $\frac{93}{14}$ $\frac{88}{15}$ $\frac{91}{21}$ $\frac{43}{21}$ $\frac{19}{25}$ $\frac{14}{35}$ $\frac{27}{50}$

$\frac{60}{50}$ $\frac{55}{45}$ $\frac{58}{37}$ $\frac{72}{27}$ $\frac{99}{23}$ $\frac{93}{17}$ $\frac{88}{14}$ $\frac{90}{18}$ $\frac{61}{25}$ $\frac{05}{25}$ $\frac{02}{33}$ $\frac{102}{50}$

$\frac{108}{50}$ $\frac{99}{40}$ $\frac{95}{26}$ $\frac{112}{19}$ $\frac{112}{18}$ $\frac{99}{12}$ $\frac{93}{15}$ $\frac{97}{22}$ $\frac{49}{22}$ $\frac{19}{29}$ $\frac{101}{50}$

$\frac{138}{50}$ $\frac{135}{40}$ $\frac{134}{24}$ $\frac{117}{21}$ $\frac{107}{16}$ $\frac{101}{19}$ $\frac{104}{22}$ $\frac{87}{24}$ $\frac{87}{26}$ $\frac{73}{26}$ $\frac{40}{50}$

Sta. 3

Sta + π - Elev.

910.47,

2 +70 05.7

3 05.2

+50 04.1

4 02.9

+50 01.6

5 00.5

T.P. 4.85 905.04' 10.28 900.19'

+55 99.8

6 99.3

+24 99.2

+62 99.3

7 99.7

Lt.

L

Rt

$$\frac{89}{50} \quad \frac{90}{26} \quad \frac{79}{20} \quad \frac{55}{14} \quad \frac{48}{14} \quad \frac{51}{19} \quad \frac{52}{29} \quad \frac{26}{50} \quad \frac{1.6}{50}$$

$$\frac{96}{50} \quad \frac{94}{26} \quad \frac{82}{16} \quad \frac{59}{11} \quad \frac{53}{17} \quad \frac{58}{22} \quad \frac{65}{24} \quad \frac{48}{32} \quad \frac{41}{50} \quad \frac{29}{50}$$

$$\frac{107}{30} \quad \frac{107}{23} \quad \frac{95}{19} \quad \frac{93}{15} \quad \frac{69}{10} \quad \frac{64}{17} \quad \frac{69}{20} \quad \frac{84}{22} \quad \frac{84}{24} \quad \frac{70}{35} \quad \frac{64}{50} \quad \frac{49}{50}$$

$$\frac{116}{50} \quad \frac{112}{33} \quad \frac{120}{22} \quad \frac{110}{18} \quad \frac{108}{15} \quad \frac{80}{10} \quad \frac{76}{17} \quad \frac{81}{21} \quad \frac{101}{22} \quad \frac{101}{25} \quad \frac{92}{34} \quad \frac{86}{50} \quad \frac{71}{50}$$

$$\frac{128}{50} \quad \frac{126}{31} \quad \frac{132}{22} \quad \frac{123}{16} \quad \frac{93}{11} \quad \frac{89}{17} \quad \frac{94}{20} \quad \frac{114}{22} \quad \frac{114}{26} \quad \frac{106}{50} \quad \frac{93}{50}$$

$$\frac{135}{50} \quad \frac{137}{30} \quad \frac{142}{17} \quad \frac{105}{10} \quad \frac{100}{16} \quad \frac{103}{20} \quad \frac{131}{28} \quad \frac{126}{35} \quad \frac{124}{50} \quad \frac{110}{50}$$

$$\frac{92}{50} \quad \frac{91}{32} \quad \frac{72}{16} \quad \frac{56}{10} \quad \frac{52}{16} \quad \frac{58}{22} \quad \frac{98}{50} \quad \frac{91}{50}$$

$$\frac{95}{50} \quad \frac{100}{27} \quad \frac{94}{17} \quad \frac{62}{11} \quad \frac{57}{15} \quad \frac{62}{22} \quad \frac{104}{33} \quad \frac{95}{50} \quad \frac{103}{50}$$

$$\frac{96}{50} \quad \frac{97}{32} \quad \frac{104}{27} \quad \frac{84}{17} \quad \frac{61}{11} \quad \frac{58}{15} \quad \frac{63}{20} \quad \frac{91}{20.5} \quad \frac{11}{24.7} \quad \frac{101}{24} \quad \frac{107}{50} \quad \frac{112}{100} \quad \frac{114}{150} \quad \frac{113}{200}$$

94.62
94.64
95.94
93.9
94.9
94.3
93.8
93.6

$$\frac{89}{50} \quad \frac{94}{35} \quad \frac{94}{18} \quad \frac{60}{11} \quad \frac{57}{15} \quad \frac{61}{20} \quad \frac{79}{37} \quad \frac{103}{50} \quad \frac{105}{50}$$

$$\frac{89}{50} \quad \frac{93}{23} \quad \frac{66}{20} \quad \frac{54}{12} \quad \frac{53}{15} \quad \frac{60}{20} \quad \frac{88}{35} \quad \frac{95}{50} \quad \frac{95}{50}$$

Sta	+	X	-	Elev.
		90504		
7	+45			00.1
	+82			00.5
8				00.7
	+35			01.0 00.9
T.P.	5.99	90704	3.99	901.03
9				01.5
	+16.4			01.6
	+16.4			01.6
B.M.			4.75	902.29
	+65.5			02.1
	+16.5			
	+80			02.2
10				02.2

Lt

k

Rt

$$\frac{59}{50} \quad \frac{53}{18} \quad \frac{51}{10} \quad \frac{49}{17} \quad \frac{55}{25} \quad \frac{59}{50} \quad \frac{70}{50}$$

$$\frac{32}{50} \quad \frac{34}{26} \quad \frac{40}{13} \quad \frac{47}{9} \quad \frac{45}{18} \quad \frac{51}{26} \quad \frac{56}{25} \quad \frac{64}{50} \quad \frac{70}{50}$$

$$\frac{31}{50} \quad \frac{33}{31} \quad \frac{40}{11} \quad \frac{48}{9} \quad \frac{43}{19} \quad \frac{49}{28} \quad \frac{56}{38} \quad \frac{66}{50} \quad \frac{70}{50}$$

$$\frac{15}{50} \quad \frac{28}{17} \quad \frac{43}{14} \quad \frac{41}{15} \quad \frac{48}{19} \quad \frac{39}{26} \quad \frac{45}{37} \quad \frac{50}{50} \quad \frac{55}{50}$$

$$\frac{27}{50} \quad \frac{21}{28} \quad \frac{24}{19} \quad \frac{36}{17} \quad \frac{58}{9} \quad \frac{55}{14} \quad \frac{57}{21} \quad \frac{55}{38} \quad \frac{54}{50} \quad \frac{57}{50}$$

$$\frac{03}{50} \quad \frac{06}{41} \quad \frac{12}{20} \quad \frac{17}{20} \quad \frac{29}{19} \quad \frac{50}{125} \quad \frac{56}{9} \quad \frac{54}{19} \quad \frac{55}{19} \quad \frac{52}{34} \quad \frac{54}{50}$$

$$\frac{12}{22} \quad \frac{077}{206} \quad \frac{492}{13.2} \quad \frac{143}{12.2} \quad \frac{50}{12.5} \quad \frac{56}{9} \quad \text{5.0}$$

Top S.W. Cor Bottom step Lt 9+37

$$\begin{matrix} \text{9ft Cor} & \text{8ft} \\ \text{Ha} & \text{36} \end{matrix} \quad \frac{072}{19.2} \quad \frac{120}{12.2} \quad \frac{44}{12.5} \quad \frac{48}{10} \quad \frac{49}{12} \quad \frac{52}{15} \quad \frac{47}{20} \quad \frac{51}{37} \quad \frac{50}{50} \quad \frac{54}{50}$$

$$\begin{matrix} \text{S.W.} \\ \text{S.S.} \end{matrix} \quad \frac{071}{42} \quad \frac{3.82}{12.5} \quad \frac{44}{12.5} \quad \frac{48}{10}$$

$$\frac{07}{50} \quad \frac{20}{36} \quad \frac{28}{35} \quad \frac{45}{10} \quad \frac{48}{12} \quad \frac{52}{20} \quad \frac{52}{36} \quad \frac{47}{50} \quad \frac{54}{50}$$

$$\frac{10.9}{50} \quad \frac{10.3}{33} \quad \frac{53}{24} \quad \frac{45}{11} \quad \frac{48}{12} \quad \frac{53}{20} \quad \frac{51}{32} \quad \frac{48}{50} \quad \frac{54}{50}$$

Sta	+	π	-	Elev.
		907.04		
10	+50			021.
	+65			02.0.
11				01.9.
	+25			01.6.
	+61			01.4.
12				01.4.
T.P.	3.45	904.87.	562	901.82.
	+45			01.6.
	+75			01.8.
	+90			01.9.
+93	Flow Line 48" C.M.			
+95	Flow Line 10" C.M. Thru Retain Wall			

Lt

K

Rt

$$\begin{array}{r} +18 \\ 50 \end{array} \begin{array}{r} +10 \\ 34 \end{array} \begin{array}{r} 56 \\ 25 \end{array} \begin{array}{r} 68 \\ 19 \end{array} \begin{array}{r} 67 \\ 15 \end{array} \begin{array}{r} 54 \\ 12 \end{array} \begin{array}{r} 49 \\ 13 \end{array} \begin{array}{r} 51 \\ 15 \end{array} \begin{array}{r} 5.9 \\ 24 \end{array} \begin{array}{r} 6.3 \\ 42 \end{array} \begin{array}{r} 6.5 \\ 50 \end{array}$$

$$\begin{array}{r} +23 \\ 50 \end{array} \begin{array}{r} +12 \\ 34 \end{array} \begin{array}{r} 49 \\ 26 \end{array} \begin{array}{r} 62 \\ 22 \end{array} \begin{array}{r} 66 \\ 16 \end{array} \begin{array}{r} 54 \\ 19 \end{array} \begin{array}{r} 50 \\ 13 \end{array} \begin{array}{r} 51 \\ 22 \end{array} \begin{array}{r} 77 \\ 45 \end{array} \begin{array}{r} 8.3 \\ 50 \end{array} \begin{array}{r} 90 \\ 50 \end{array}$$

$$\begin{array}{r} +23 \\ 50 \end{array} \begin{array}{r} +19 \\ 34 \end{array} \begin{array}{r} 20 \\ 25 \end{array} \begin{array}{r} 6.9 \\ 17 \end{array} \begin{array}{r} 6.9 \\ 15 \end{array} \begin{array}{r} 55 \\ 13 \end{array} \begin{array}{r} 51 \\ 13 \end{array} \begin{array}{r} 5.7 \\ 20 \end{array} \begin{array}{r} 10.5 \\ 26 \end{array} \begin{array}{r} 12.4 \\ 50 \end{array} \begin{array}{r} 12.9 \\ 50 \end{array}$$

$$\begin{array}{r} +28 \\ 50 \end{array} \begin{array}{r} +14 \\ 34 \end{array} \begin{array}{r} 30 \\ 23 \end{array} \begin{array}{r} 7.4 \\ 18 \end{array} \begin{array}{r} 7.4 \\ 16 \end{array} \begin{array}{r} 58 \\ 14 \end{array} \begin{array}{r} 54 \\ 11 \end{array} \begin{array}{r} 5.8 \\ 22 \end{array} \begin{array}{r} 12.5 \\ 25 \end{array} \begin{array}{r} 13.2 \\ 34 \end{array} \begin{array}{r} 130 \\ 50 \end{array} \begin{array}{r} 126 \\ 50 \end{array}$$

$$\begin{array}{r} 5.5 \\ 50 \end{array} \begin{array}{r} 00 \\ 46 \end{array} \begin{array}{r} 1.7 \\ 22 \end{array} \begin{array}{r} 94 \\ 193 \end{array} \begin{array}{r} 101 \\ 193 \end{array} \begin{array}{r} 92.5 \\ 17 \end{array} \begin{array}{r} 87 \\ 14 \end{array} \begin{array}{r} 5.9 \\ 14 \end{array} \begin{array}{r} 56 \\ 11 \end{array} \begin{array}{r} 5.8 \\ 18 \end{array} \begin{array}{r} 10.8 \\ 20.6 \end{array} \begin{array}{r} 11.0 \\ 20.6 \end{array} \begin{array}{r} 11.85 \\ 24 \end{array} \begin{array}{r} 11.5 \\ 33 \end{array} \begin{array}{r} 12.2 \\ 50 \end{array} \begin{array}{r} 103 \\ 50 \end{array}$$

$$\begin{array}{r} 5.5 \\ 50 \end{array} \begin{array}{r} 10 \\ 38 \end{array} \begin{array}{r} 4.0 \\ 21 \end{array} \begin{array}{r} 8.4 \\ 17 \end{array} \begin{array}{r} 8.4 \\ 14 \end{array} \begin{array}{r} 6.0 \\ 14 \end{array} \begin{array}{r} 56 \\ 11 \end{array} \begin{array}{r} 5.8 \\ 19 \end{array} \begin{array}{r} 10.4 \\ 26 \end{array} \begin{array}{r} 11.2 \\ 35 \end{array} \begin{array}{r} 10.8 \\ 50 \end{array} \begin{array}{r} 103 \\ 50 \end{array}$$

K 5/6 12

$$\begin{array}{r} +0.4 \\ 50 \end{array} \begin{array}{r} 0.4 \\ 53 \end{array} \begin{array}{r} 30 \\ 19 \end{array} \begin{array}{r} 3.4 \\ 13 \end{array} \begin{array}{r} 33 \\ 11 \end{array} \begin{array}{r} 3.2 \\ 18 \end{array} \begin{array}{r} 6.6 \\ 27 \end{array} \begin{array}{r} 6.6 \\ 31 \end{array} \begin{array}{r} 6.2 \\ 38 \end{array} \begin{array}{r} 6.6 \\ 50 \end{array} \begin{array}{r} 6.2 \\ 50 \end{array}$$

$$\begin{array}{r} 15 \\ 50 \end{array} \begin{array}{r} 25 \\ 27 \end{array} \begin{array}{r} 23 \\ 24 \end{array} \begin{array}{r} 2.4 \\ 19 \end{array} \begin{array}{r} 3.1 \\ 12 \end{array} \begin{array}{r} 3.1 \\ 12 \end{array} \begin{array}{r} 3.3 \\ 24 \end{array} \begin{array}{r} 5.5 \\ 30 \end{array} \begin{array}{r} 10.6 \\ 41 \end{array} \begin{array}{r} 15.4 \\ 45 \end{array} \begin{array}{r} 17.7 \\ 52 \end{array} \begin{array}{r} 17.7 \\ 52 \end{array}$$

48° 51' 10.6"

$$\begin{array}{r} 25 \\ 50 \end{array} \begin{array}{r} 35 \\ 21 \end{array} \begin{array}{r} 2.9 \\ 13 \end{array}$$

H.W.

(Cor. Retwall)

$$\begin{array}{r} 30.32 \\ 11 \end{array} \begin{array}{r} 4.3 \\ 15 \end{array} \begin{array}{r} 12.40 \\ 27 \end{array} \begin{array}{r} 17.5 \\ 2.8 \end{array} \begin{array}{r} 17.5 \\ 35 \end{array} \begin{array}{r} 13.5 \\ 46 \end{array} \begin{array}{r} 6.0 \\ 46 \end{array} \begin{array}{r} 13.5 \\ 46 \end{array} \begin{array}{r} 8.4 \\ 56 \end{array} \begin{array}{r} 55.10 \\ 55.10 \end{array}$$

18.52

86.35

90.2

95.85

Sta	+	π	-	Elev.
		904.87		
12	+96			02.0
	+98			02.0
13				
13	+12			02.2
	+35			02.7
	+40	Flowline 48" C.M.		
	+43			03.0
	+49			03.0
	+62			03.4
	+83			04.1
T.P.	13.11	917.72	0.26	904.61
14				04.6

LH

K

RH

$$\begin{array}{cccccccccccccccc} & & & & & & & & & & & & & \text{H.W.} & & \text{(Robin)} \\ & & & & & & & & & & & & & \text{Wall} & & \\ \frac{34}{50} & \frac{38}{40} & \frac{39}{19} & \frac{36}{14} & \frac{20}{12} & \frac{29}{12} & \frac{32}{18} & \frac{56}{18} & \frac{114}{26} & \frac{1358}{315} & \frac{171}{315} & \frac{608}{315} & \frac{598}{34} & \frac{7.8}{50} \end{array}$$

same 95 + 98

$$\begin{array}{cccc} \text{Robin} \\ \text{(Wall)} \\ \frac{29}{13} & \frac{35}{19} & \frac{5.56}{26} & \frac{6.39}{50} \end{array}$$

$$\frac{47}{50} \frac{47}{32} \frac{48}{15} \frac{29}{10} \frac{27}{14} \frac{34}{23} \frac{54}{31} \frac{53}{50} \frac{31}{50}$$

$$\begin{array}{cccccccccccccccc} & & & & \text{H.W.} & & & & & & & & & & & \\ \frac{110}{50} & \frac{122}{33} & \frac{142}{30} & \frac{142}{27} & \frac{162}{27} & \frac{125}{27} & \frac{93}{20} & \frac{24}{9} & \frac{22}{14} & \frac{28}{17} & \frac{39}{23} & \frac{44}{26} & \frac{31}{32} & \frac{28}{32} & \frac{23}{50} \end{array}$$

$$\text{by K.A. } \frac{18.15}{14.15} \quad 9072 \quad *$$

$$\begin{array}{cccccccc} & & & & \text{H.W.} & & & \\ \frac{120}{50} & \frac{122}{42} & \frac{173}{29} & \frac{173}{24} & \frac{16.3}{21} & \frac{9.47}{21} & 19 & \text{same 95 + 98} \end{array}$$

$$\begin{array}{cccccccc} & & & & \text{H.W.} & & & \\ \frac{125}{50} & \frac{172}{37} & \frac{172}{30} & \frac{138}{22} & \frac{969}{22} & \frac{969}{21} & \frac{19}{14} & \frac{24}{17} & \frac{89}{24} & \frac{38}{26} & \frac{22}{35} & \frac{23}{35} & \frac{17}{50} \end{array}$$

$$\frac{162}{50} \frac{16.2}{45} \frac{11.8}{32} \frac{99}{21} \frac{1.8}{9} \frac{15}{19} \frac{20}{16} \frac{32}{16} \frac{34}{28} \frac{17}{28} \frac{17}{35} \frac{0.8}{50}$$

$$\frac{11.9}{50} \frac{3.8}{30} \frac{2.5}{15} \frac{11}{12} \frac{0.8}{15} \frac{1.3}{17} \frac{2.3}{17} \frac{2.5}{24} \frac{0.1}{28} \frac{10.1}{33} \frac{10.7}{38} \frac{10.6}{50}$$

$$\frac{192}{50} \frac{160}{42} \frac{146}{32} \frac{130}{16} \frac{140}{14} \frac{135}{12} \frac{131}{14} \frac{135}{16} \frac{142}{22} \frac{144}{25} \frac{11.2}{36} \frac{10.8}{36} \frac{10.8}{50}$$

Sta.	+	π	-	Elev.
		917.72		
14	+40			06.1
	+72			07.3
15				08.3
	+33			09.5
	+74			11.1
16				11.9
	+50			13.1
17				13.9
T.P.	962	923.661	3.68	914.04
	+50			14.4
18				15.1
	+50			15.8

Lt.

K

Lt.

$$\frac{107}{50} \frac{97}{32} \frac{103}{28} \frac{125}{79} \frac{121}{11} \frac{116}{123} \frac{95}{20} \frac{91}{23} \frac{91}{38} \frac{93}{50}$$

$$\frac{115}{50} \frac{115}{32} \frac{107}{15} \frac{107}{12} \frac{104}{14} \frac{108}{18} \frac{93}{23} \frac{91}{33} \frac{90}{50}$$

$$\frac{124}{50} \frac{107}{32} \frac{94}{14} \frac{98}{13} \frac{94}{13} \frac{98}{11} \frac{91}{25} \frac{85}{25} \frac{84}{50}$$

$$\frac{85}{50} \frac{78}{32} \frac{71}{16} \frac{85}{12} \frac{82}{13} \frac{87}{21} \frac{76}{21} \frac{73}{32} \frac{71}{50}$$

$$\frac{70}{50} \frac{68}{32} \frac{55}{16} \frac{70}{13} \frac{66}{14} \frac{70}{18} \frac{59}{25} \frac{53}{25} \frac{49}{50}$$

$$\frac{51}{50} \frac{35}{39} \frac{40}{16} \frac{62}{13} \frac{58}{15} \frac{60}{18} \frac{47}{28} \frac{44}{28} \frac{48}{50}$$

$$\frac{44}{50} \frac{32}{32} \frac{27}{26} \frac{42}{13} \frac{51}{12} \frac{46}{14} \frac{50}{19} \frac{40}{30} \frac{42}{30} \frac{47}{50}$$

$$\frac{31}{50} \frac{32}{46} \frac{26}{37} \frac{26}{32} \frac{23}{17} \frac{43}{13} \frac{38}{12} \frac{41}{20} \frac{43}{35} \frac{46}{35} \frac{48}{50}$$

$$\frac{74}{50} \frac{72}{32} \frac{71}{22} \frac{86}{17} \frac{95}{11} \frac{93}{12} \frac{96}{15} \frac{99}{16} \frac{97}{19} \frac{95}{30} \frac{92}{30} \frac{91}{50}$$

$$\frac{61}{50} \frac{69}{32} \frac{61}{25} \frac{78}{20} \frac{90}{12} \frac{86}{12} \frac{87}{14} \frac{90}{16} \frac{90}{18} \frac{83}{20} \frac{80}{20} \frac{77}{50}$$

$$\frac{48}{50} \frac{44}{32} \frac{45}{25} \frac{83}{12} \frac{77}{12} \frac{80}{19} \frac{74}{19} \frac{69}{34} \frac{70}{50}$$

Sta	+	π	-	Elev
		923.66		
19				16.1
	+60			16.2
	+68			16.3
20				16.3
	+30			16.5
	+58			16.5
21				16.3
	+50			16.3
22				16.3
	+50			16.2
23				16.1
T.P.	0.45	918.58 918.69	5.53	918.13

Lt

x

Rt

$$\frac{39}{50} \frac{39}{42} \frac{32}{32} \frac{32}{29} \frac{63}{23} \frac{80}{15} \frac{76}{12} \frac{79}{12} \frac{73}{19} \frac{71}{27} \frac{68}{50}$$

$$\frac{39}{50} \frac{31}{37} \frac{26}{29} \frac{78}{20} \frac{80}{12} \frac{75}{13} \frac{78}{19} \frac{68}{36} \frac{61}{50}$$

$$\frac{33}{50} \frac{31}{37} \frac{26}{29} \frac{78}{19} \frac{80}{12} \frac{74}{13} \frac{79}{17} \frac{70}{25} \frac{49}{38} \frac{53}{50}$$

$$\frac{35}{50} \frac{32}{37} \frac{27}{36} \frac{31}{31} \frac{89}{21} \frac{90}{16} \frac{77}{12} \frac{74}{13} \frac{79}{17} \frac{79}{25} \frac{46}{45} \frac{50}{50}$$

$$\frac{40}{50} \frac{40}{40} \frac{35}{32} \frac{98}{20} \frac{98}{15} \frac{77}{12} \frac{72}{15} \frac{78}{19} \frac{84}{26} \frac{58}{44} \frac{53}{50}$$

$$\frac{49}{50} \frac{50}{40} \frac{44}{36} \frac{44}{30} \frac{90}{22} \frac{92}{15} \frac{77}{12} \frac{72}{16} \frac{78}{20} \frac{96}{24} \frac{97}{30} \frac{63}{50}$$

$$\frac{66}{50} \frac{68}{44} \frac{61}{37} \frac{63}{28} \frac{92}{21} \frac{95}{16} \frac{78}{11} \frac{74}{15} \frac{77}{19} \frac{107}{24} \frac{113}{30} \frac{82}{38} \frac{89}{50}$$

$$\frac{72}{50} \frac{69}{33} \frac{78}{26} \frac{88}{14} \frac{78}{10} \frac{74}{15} \frac{80}{19} \frac{99}{25} \frac{105}{28} \frac{91}{50}$$

$$\frac{79}{50} \frac{71}{35} \frac{79}{30} \frac{89}{13} \frac{85}{13} \frac{78}{10} \frac{74}{15} \frac{79}{19} \frac{95}{24} \frac{101}{30} \frac{79}{50}$$

$$\frac{90}{50} \frac{83}{31} \frac{84}{16} \frac{78}{11} \frac{75}{16} \frac{80}{21} \frac{98}{25} \frac{100}{32} \frac{71}{50}$$

$$\frac{90}{50} \frac{87}{31} \frac{87}{19} \frac{96}{18} \frac{78}{12} \frac{76}{17} \frac{81}{22} \frac{105}{25} \frac{106}{31} \frac{83}{42} \frac{81}{50}$$

Top G.R. post Lt 2st

Sta.	+	π	-	Elev.
		918.58 918.63		

23	+27			15.8
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	+38			15.7
--	-----	--	--	------

	+51			15.5
--	-----	--	--	------

	+65			15.3
--	-----	--	--	------

	+81			15.1
--	-----	--	--	------

	+87			15.0
--	-----	--	--	------

	+89			
--	-----	--	--	--

+2870	See Edgerton St. for X-section			
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B.M.		2.58		
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916.6

916.05

(916.26)

11/15/39
K.A.
L.C.
M.B.
M.D.G.

16

14

4

24

$\frac{10.7}{50} \frac{40}{32} \frac{40}{21} \frac{48}{18} \frac{34}{13} \frac{28}{7} \frac{28}{17} \frac{33}{23} \frac{52}{27} \frac{54}{27} \frac{41}{29} \frac{34}{37} \frac{32}{50}$

$\frac{125}{50} \frac{98}{30} \frac{7.2}{15} \frac{3.3}{9}$

$\frac{29}{17} \frac{34}{23} \frac{54}{27} \frac{54}{29} \frac{45}{40} \frac{36}{50} \frac{32}{50}$

$\frac{188}{50} \frac{139}{41} \frac{95}{24} \frac{80}{15} \frac{55}{9} \frac{3}{17} \frac{35}{22} \frac{59}{26} \frac{54}{28} \frac{44}{37} \frac{41}{50} \frac{36}{50}$

H.I. 905.47

(49.6)

$\frac{77}{53} \frac{75}{37} \frac{41}{26}$

$\frac{65}{13} \frac{37}{7} \frac{33}{16} \frac{35}{20} \frac{45}{27} \frac{49}{29} \frac{40}{29} \frac{38}{50}$

(H.W.)

$\frac{91}{61} \frac{15.1}{48} \frac{154}{48} \frac{140}{41} \frac{107}{41} \frac{107}{40} \frac{6.5}{28}$

$\frac{96}{10} \frac{5.9}{7} \frac{37}{14} \frac{35}{20} \frac{36}{25} \frac{42}{31} \frac{74}{40} \frac{78}{40} \frac{58}{50} \frac{46}{50}$

H.W.

(49.6)

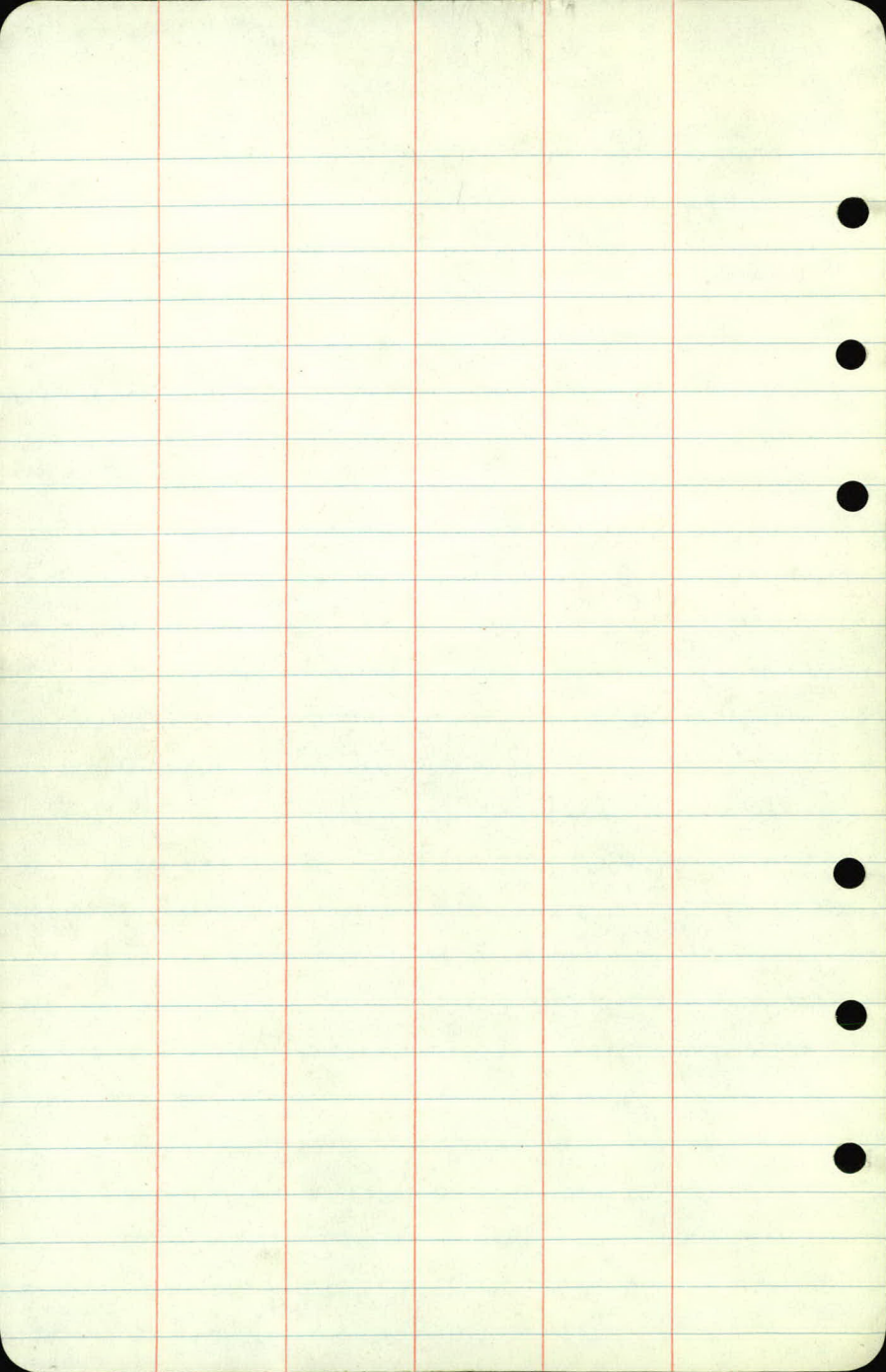
$\frac{81}{54} \frac{131}{45} \frac{110}{45} \frac{119}{44} \frac{99}{33} \frac{51}{25}$

$\frac{68}{11} \frac{37}{6} \frac{36}{14} \frac{36}{20} \frac{48}{25} \frac{85}{32} \frac{95}{41} \frac{76}{41} \frac{54}{50}$

888.60

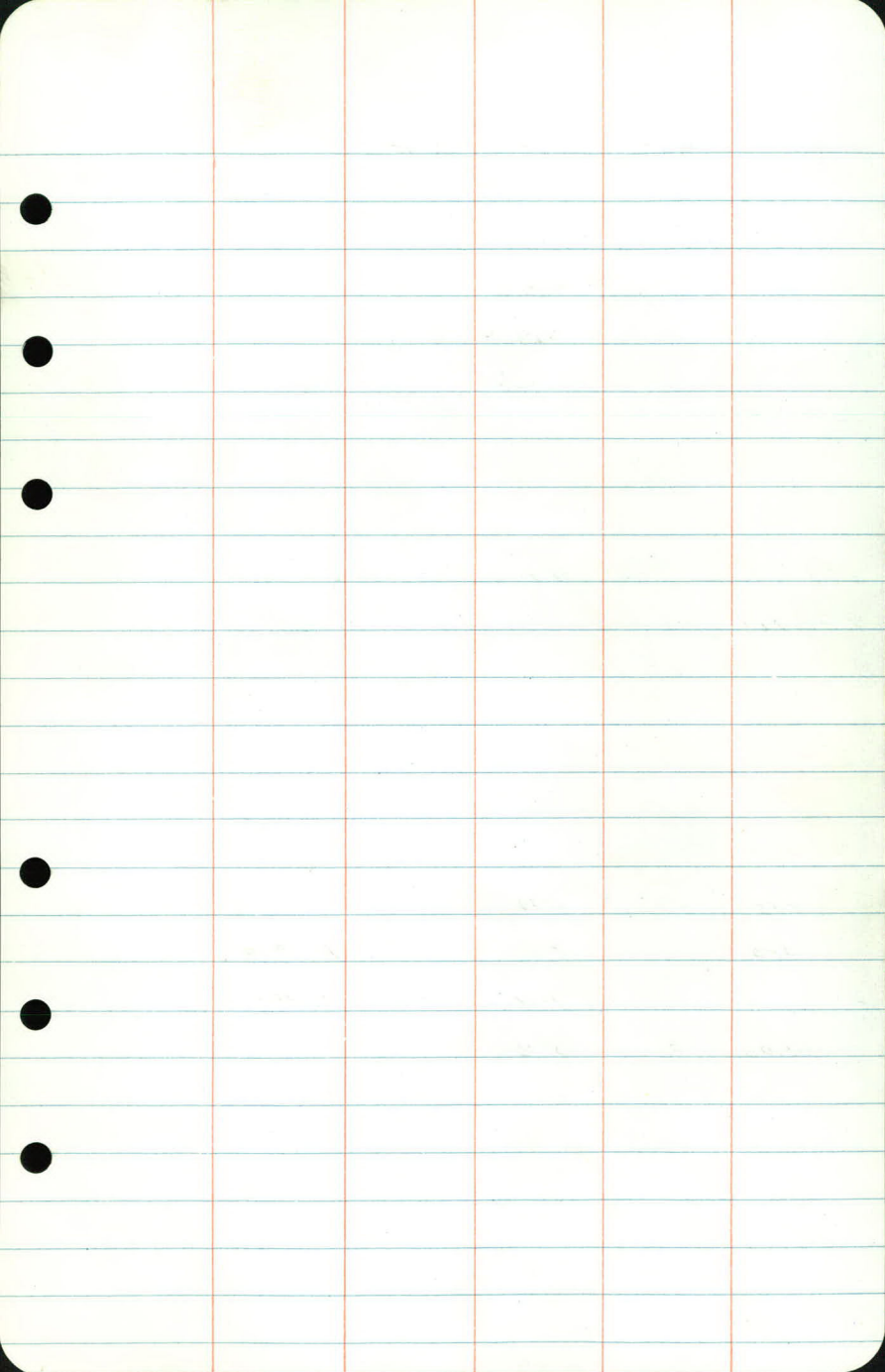
16.83

Top Mont. Keeble Rd. & Edgerfor St.



Alignment
KOHLEB RD.
E. of Edgerton St.

Sta.	Point	ΔL	ΔB
+62.92	P.T.	9°21.0'	
+50		9°01.6'	
6		7°46.6'	
+50		6°31.6'	$\Delta 18°42'$
5		5°16.6'	$D-5°-$
+77.66	P.I.	18°42'	$T-188.74'$
+50		4°01.6'	$L-374.00'$
4		2°46.6'	$B-$
+50		1°31.6'	
3		0°16.6'	
+88.92	P.C.	0°00'	
+28.44	P.T.	10°00'	$\Delta 20°-$
2		7°09.4'	$D-20°-$
+75		4°39.4'	$T-50.78'$
+79.22	P.I.	20°-	$L-100.00'$
+50		2°09.4'	$B-287.94'$
+28.44	P.C.	0°00'	
0	+100 = P.O.T. = P.T. 32+10.05 Edgerton St.		



Sta	Point	ΔL	ΔR
-----	-------	------------	------------

14+35.3	} P.T. - from 7-20-25 Rd. Map Survey.		
9+29.02		P.C. =	

178.75	P.T.	6044'	
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+50		5°35'	
-----	--	-------	--

			A-13°28'
--	--	--	----------

0		3°35'	
---	--	-------	--

			D-8°-
--	--	--	-------

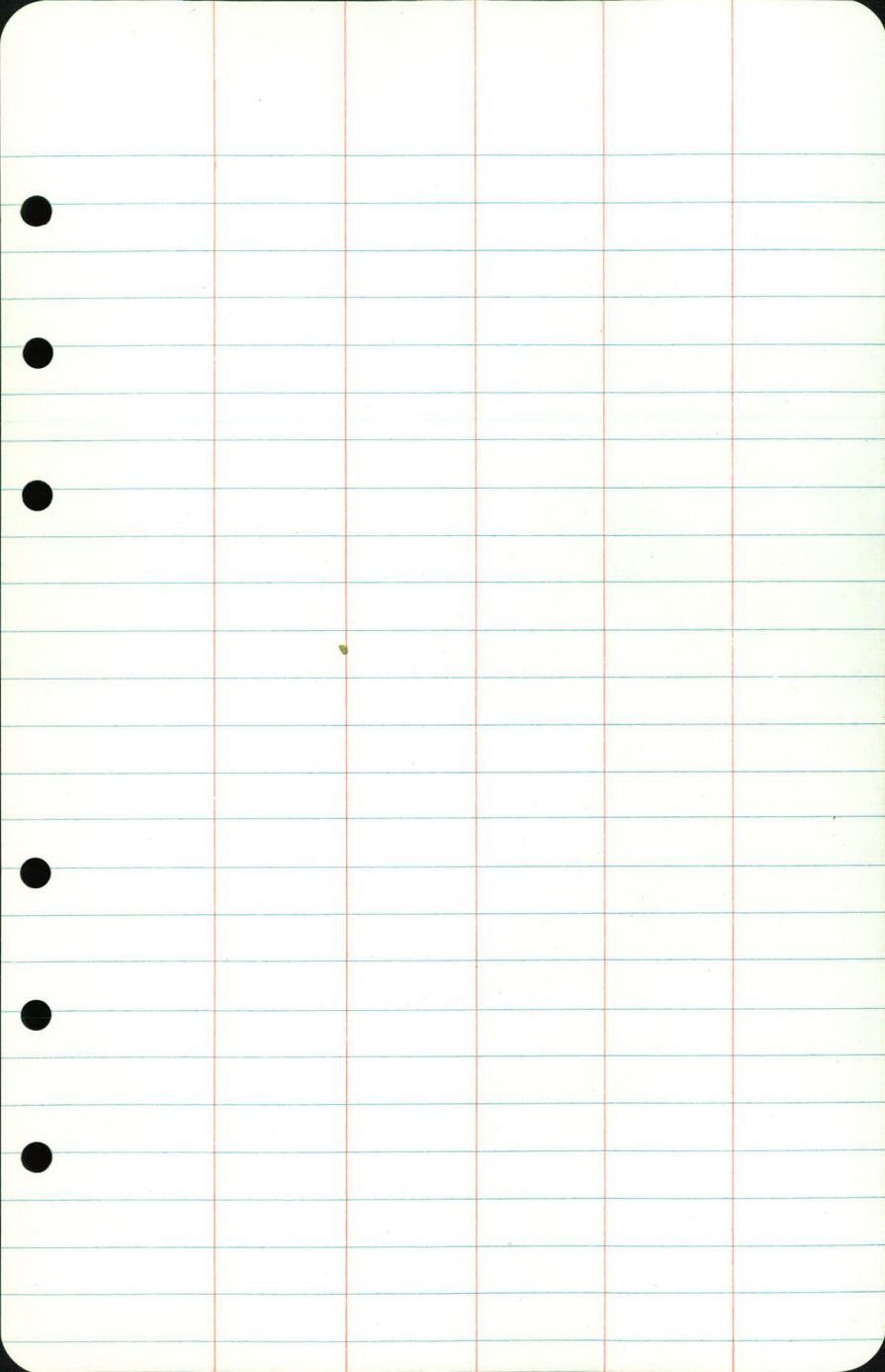
195.05	P.I.	13°28'	
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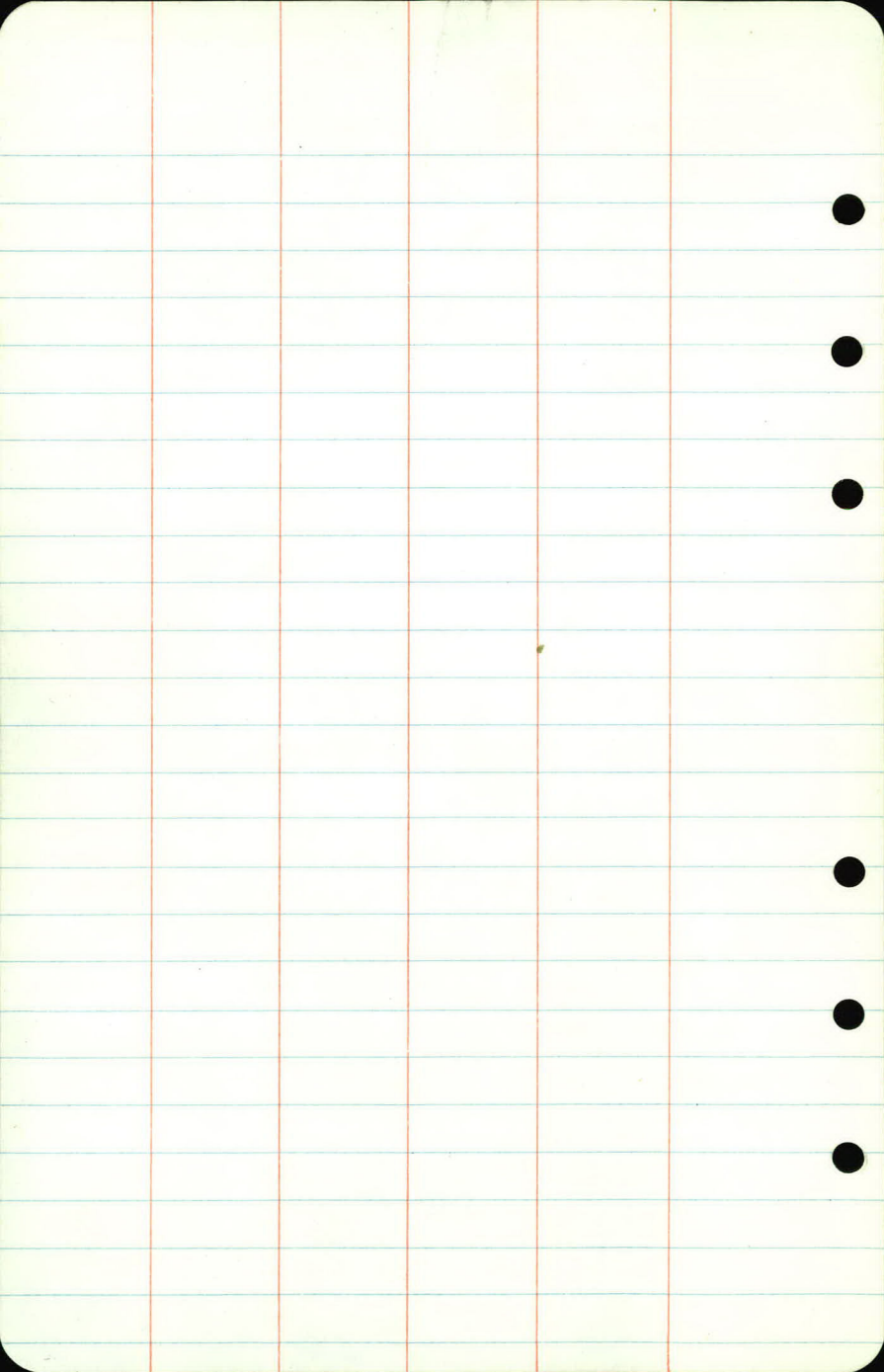
			T-84.63
--	--	--	---------

+50		1°35'	
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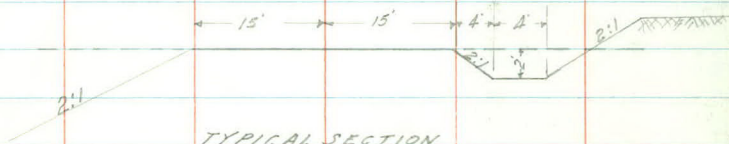
			L-168.33
--	--	--	----------

7 +10.42	P.C.	0°00'	
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Slope stakes
Kohler Rd.



Sta	+	π	-	Grade	
B.M.	12.37	919.58			907.21
0	+00				
	+30			07.1	
	+50			07.1	
1	+75			06.9	
1				06.7	
	+45			06.5	
2				06.1	
	+45			05.5	
B.M.	22.4	909.45	2.24		907.21
	+70			05.2	
3				04.7	
	+50			03.8	

Gr. Rod.

Lt

E

Rt

Spk in P.P. N.W. Cor. Kohler Rd & McManamy St.

12.5

$$\begin{array}{r} 32.0' / 11.0 \\ \hline 41.5 \end{array}$$

$$\begin{array}{r} 12.4 \\ -0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 11.4 \\ +1.1 / 29.2' \end{array}$$

12.5

$$\begin{array}{r} 300' / 11.0 \\ \hline 41.5 \end{array}$$

$$\begin{array}{r} 12.3 \\ +0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 9.5 \\ +30 / 33.0' \end{array}$$

12.7

$$\begin{array}{r} 30.2' / 11.1 \\ \hline 41.6 \end{array}$$

$$\begin{array}{r} 12.2 \\ +0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 12 \\ +48 / 36.6' \end{array}$$

12.9

$$\begin{array}{r} 33.0' / 9.4 \\ \hline 42.5 \end{array}$$

$$\begin{array}{r} 12.1 \\ +0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ +1.1 / 41.2' \end{array}$$

13.1

$$\begin{array}{r} 33.0' / 9.8 \\ \hline 42.3 \end{array}$$

$$\begin{array}{r} 12.1 \\ +1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 3.3 \\ +9.8 / 46.6' \end{array}$$

13.5

$$\begin{array}{r} 28.2' / 12.9 \\ \hline 40.6 \end{array}$$

$$\begin{array}{r} 12.7 \\ +0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ +100 / 47.0' \end{array}$$

14.1

$$\begin{array}{r} 22.6' / 16.1 \\ \hline 42.00 \end{array}$$

$$\begin{array}{r} 19.5 \\ +0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 9.0 \\ +5.1 / 37.2' \end{array}$$

4.3

$$\begin{array}{r} 20.4' / 7.0 \\ \hline -2.7 \end{array}$$

$$\begin{array}{r} 3.7 \\ +0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 2.3 \\ +20 / 31.0' \end{array}$$

4.8

$$\begin{array}{r} 21.2' / 7.9 \\ \hline -3.1 \end{array}$$

$$\begin{array}{r} 4.2 \\ +0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.3 \\ +1.5 / 30.0' \end{array}$$

5.7

$$\begin{array}{r} 23.2' / 7.8 \\ \hline -4.1 \end{array}$$

$$\begin{array}{r} 5.3 \\ +0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ +1.9 / 26.8' \end{array}$$

Sta	+	π	-	Grade
		909.45		
4				02.7
T.P.	2.34	904.58	1.21	902.24
	+50			01.7
5				00.6
	+55			99.7
6				99.3
	+24			99.2
	+62			99.2
7				99.5
T.P.	6.91	905.87	5.62	898.96
	+45			00.0
	+82			00.3
8				00.5

Gr. Rod

LH

E

RH

6.8

$$23.2' / \frac{1.09}{-4.1}$$

$$\frac{46}{+0.2}$$

$$\frac{85}{15.03} / 23.6'$$

Spt in RR Rt 5 ft 4 ft

2.9

$$23.4' / \frac{7.1}{-4.2}$$

$$\frac{30}{-0.1}$$

$$\frac{50}{-2.1} / 19.2'$$

4.0

$$22.6' / \frac{7.8}{-3.8}$$

$$\frac{40}{0.0}$$

$$\frac{72}{-3.2} / 21.4'$$

4.9

$$22.6' / \frac{8.7}{-3.9}$$

$$\frac{47}{+0.2}$$

$$\frac{79}{-4.0} / 23.0'$$

5.3

$$22.4' / \frac{8.0}{-3.7}$$

$$\frac{52}{+0.1}$$

$$\frac{85}{-4.2} / 23.6'$$

5.4

$$23.0' / \frac{9.4}{-4.0}$$

$$\frac{53}{+0.1}$$

$$\frac{97}{-4.3} / 23.6'$$

5.4

$$22.6' / \frac{9.2}{-3.8}$$

$$\frac{52}{+0.2}$$

$$\frac{85}{-4.1} / 23.2'$$

5.1

$$22.2' / \frac{8.7}{-3.6}$$

$$\frac{48}{+0.3}$$

$$\frac{86}{-3.5} / 22.0'$$

Nail in T.P. Rt 7 ft

5.9

$$26.4' / \frac{6.2}{15.7}$$

$$\frac{5.7}{+0.2}$$

$$\frac{66}{15.13} / 25.6'$$

5.6

$$30.2' / \frac{4.2}{11.6}$$

$$\frac{5.3}{+0.3}$$

$$\frac{63}{15.13} / 25.6'$$

5.4

$$29.8' / \frac{4.0}{11.4}$$

$$\frac{5.2}{+0.2}$$

$$\frac{63}{15.09} / 24.8'$$

Sta	+	Σ	-	Grade	Gr. Rod	Gr. Lt	Ditch
		905.87					
8	+3.5			00.9	6.5	21.0	99.4
	+6.5			01.2	5.7	19.0	00.2
9				01.5		17.0	01.0
	+16.5			01.7			
B.M.	4.52	906.80	3.57	902.30		(902.28)	
	+65.5			02.0			
	+80			02.0			
10				02.0			
	+50			02.0			
	+65			01.9			
11				01.7			
	+25			01.5			

Gr. Rod.

Lt.

L

Rt.

5.0

$$28.2 / \frac{2.9}{+2.1}$$

$$\frac{49}{+0.1}$$

$$\frac{52}{+0.8} / 26.6'$$

4.7

$$27.0 / \frac{1.7}{+3.0}$$

$$\frac{47}{0.0}$$

$$\frac{48}{+0.9} / 26.8'$$

4.4

$$25.4 / \frac{0.7}{+3.7}$$

$$\frac{44}{0.0}$$

$$\frac{41}{+0.3} / 27.6'$$

4.2

$$\frac{43}{-0.1}$$

$$\frac{41}{+0.1} / 27.2'$$

Top S.W. Cor. Bottom Step Lt. Sta 9+37

4.8

$$\frac{47}{+0.1}$$

$$\frac{47}{+0.1} / 27.2'$$

4.8

$$33.0 / \frac{0.3}{+4.5}$$

$$\frac{45}{+0.3}$$

$$\frac{46}{+0.2} / 27.4'$$

4.8

$$33.0 / \frac{0.0}{+4.8}$$

$$\frac{46}{+0.2}$$

$$\frac{41}{+0.7} / 24.4'$$

4.9

$$33.0 / \frac{0.1}{+4.8}$$

$$\frac{47}{+0.2}$$

$$\frac{49}{+0.0} / 20.7'$$

5.1

$$33.0 / \frac{0.5}{+4.6}$$

$$\frac{49}{+0.2}$$

$$\frac{12.4}{-7.3} / 29.6'$$

5.3

$$33.0 / \frac{4.8}{+7.1}$$

$$\frac{51}{+0.2}$$

$$\frac{12.8}{-7.5} / 30.0'$$

Sta	+	π	-	Grade	Lt.
		906.80			
11	+61			01.2	
12				01.1	
	+45			01.4	
	+75			01.8	
	+90			01.8	
	+96			02.0	
	+98			02.2	
13				02.2	7.2 ²⁴² 996
	+12			02.5	7.3
	+35			03.1	
	+43			03.3	
	+49			03.5	

Gr. Rod

Lt

K

Rt

5.6

$$22.4' / \frac{2.2}{-3.7}$$

$$\frac{54}{+0.2}$$

$$\frac{116}{-6.0} / 27.0'$$

5.7

$$24.4' / \frac{7.0}{+0.7}$$

$$\frac{54}{+0.3}$$

$$\frac{109}{-5.2} / 25.4'$$

5.4

$$32.8' / \frac{2.5}{+2.9}$$

$$\frac{52}{+0.2}$$

$$\frac{83}{-3.9} / 20.8'$$

5.0

$$27.6' / \frac{4.7}{+0.3}$$

$$\frac{50}{0.0}$$

$$\frac{7.0}{-10.0} / 20.9'$$

5.0

$$\frac{49}{+0.1}$$

$$\frac{12.7}{-7.7} / 22.7'$$

4.8

$$\frac{48}{0.0}$$

$$\frac{10.5}{-5.7} / 20.7'$$

4.6

4.6

$$26.8' / \frac{5.9}{+0.3}$$

$$\frac{48}{-0.2}$$

$$\frac{7.0}{-2.4} / 19.8'$$

4.3

$$25.0' / \frac{2.3}{+0.0}$$

$$\frac{46}{-0.3}$$

$$\frac{6.3}{-2.0} / 19.0'$$

3.7

$$\frac{43}{-0.5}$$

$$\frac{6.0}{-2.3} / 19.6'$$

Sta	+	π	-	Grade
		906.80		
13	+62			03.9
T.P.	12.89	915.28	4.41	902.39
	+83			04.5
14				05.0
	+40			06.2
	+72			07.2
15				08.0
	+33			09.0
	+74			10.2
T.P.	8.93	921.03	3.18	912.10
16				11.0
	+50			12.4
17				13.6

Gr. Rod

L_tL_cR_t

2.9

$$34.4' / \frac{115.0}{-12.1}$$

$$\frac{34}{-0.5}$$

$$\frac{5.3}{-2.4} / 12.1'$$

Nail in R.R. R_t L_t

10.8

$$20.2' / \frac{134}{-2.6}$$

$$\frac{113}{-0.5}$$

$$\frac{12.8}{100.0} / 20.2'$$

10.3

$$24.8' / \frac{114}{10.9}$$

$$\frac{10.8}{-0.5}$$

$$\frac{8.5}{11.7} / 30.4'$$

9.1

$$30.0' / \frac{76}{11.5}$$

$$\frac{92}{-0.1}$$

$$\frac{6.8}{12.3} / 31.6'$$

8.1

$$25.4' / \frac{89}{12.2}$$

$$\frac{80}{10.1}$$

$$\frac{6.7}{11.4} / 29.8'$$

7.3

$$26.2' / \frac{77}{12.6}$$

$$\frac{20}{10.3}$$

$$\frac{6.0}{11.3} / 29.6'$$

6.3

$$29.0' / \frac{53}{11.0}$$

$$\frac{57}{10.6}$$

$$\frac{5.0}{11.3} / 29.6'$$

5.1

$$30.2' / \frac{35}{11.6}$$

$$\frac{42}{10.9}$$

$$\frac{2.5}{10.6} / 32.2'$$

10.0

$$33.0' / \frac{64}{12.6}$$

$$\frac{91}{10.9}$$

$$\frac{7.7}{12.3} / 31.6'$$

8.6

$$31.2' / \frac{6.5}{12.1}$$

$$\frac{79}{10.7}$$

$$\frac{7.4}{11.2} / 29.4'$$

7.4

$$30.2' / \frac{58}{11.6}$$

$$\frac{71}{10.3}$$

$$\frac{7.7}{11.7} / 26.4'$$

Sta.	+	π	-	Grade.
		921.03		
17	+50			14.6
18				15.4
	+50			16.0
19				16.4
	+60			16.6
	+68			16.6
20				16.6
	+30			16.5
	+58			16.4
T.P.	6.28	921.41	5.90	915.13
21				16.3
	+50			16.2

Gr. Rod

Lt.

E

Rt.

$$6.4 \quad 30.8 \frac{14.5}{+1.9} \quad \frac{45}{-0.1} \quad \frac{46}{21.8/26.6'}$$

$$5.6 \quad 31.4 \frac{34}{+2.2} \quad \frac{59}{-0.3} \quad \frac{52}{10.4/27.8'}$$

$$5.0 \quad 33.0 \frac{1.8}{+3.2} \quad \frac{59}{-0.3} \quad \frac{42}{19.8/28.6'}$$

$$4.6 \quad 33.0 \frac{0.6}{+4.0} \quad \frac{50}{-0.4} \quad \frac{42}{10.4/27.8'}$$

$$4.4 \quad 33.0 \frac{4.04}{+4.8} \quad \frac{48}{-0.4} \quad \frac{34}{11.0/29.0'}$$

$$4.4 \quad \quad \frac{47}{-0.3} \quad \frac{25}{19/30.8'}$$

$$4.4 \quad 33.0 \frac{10.1}{+9.5} \quad \frac{47}{-0.3} \quad \frac{19}{12.5/32.0'}$$

$$4.5 \quad 33.0 \frac{1}{+3.4} \quad \frac{47}{-0.2} \quad \frac{24}{12.1/31.2'}$$

$$4.6 \quad 33.0 \frac{1.4}{+3.1} \quad \frac{46}{0.0} \quad \frac{66}{20.0/25.2'}$$

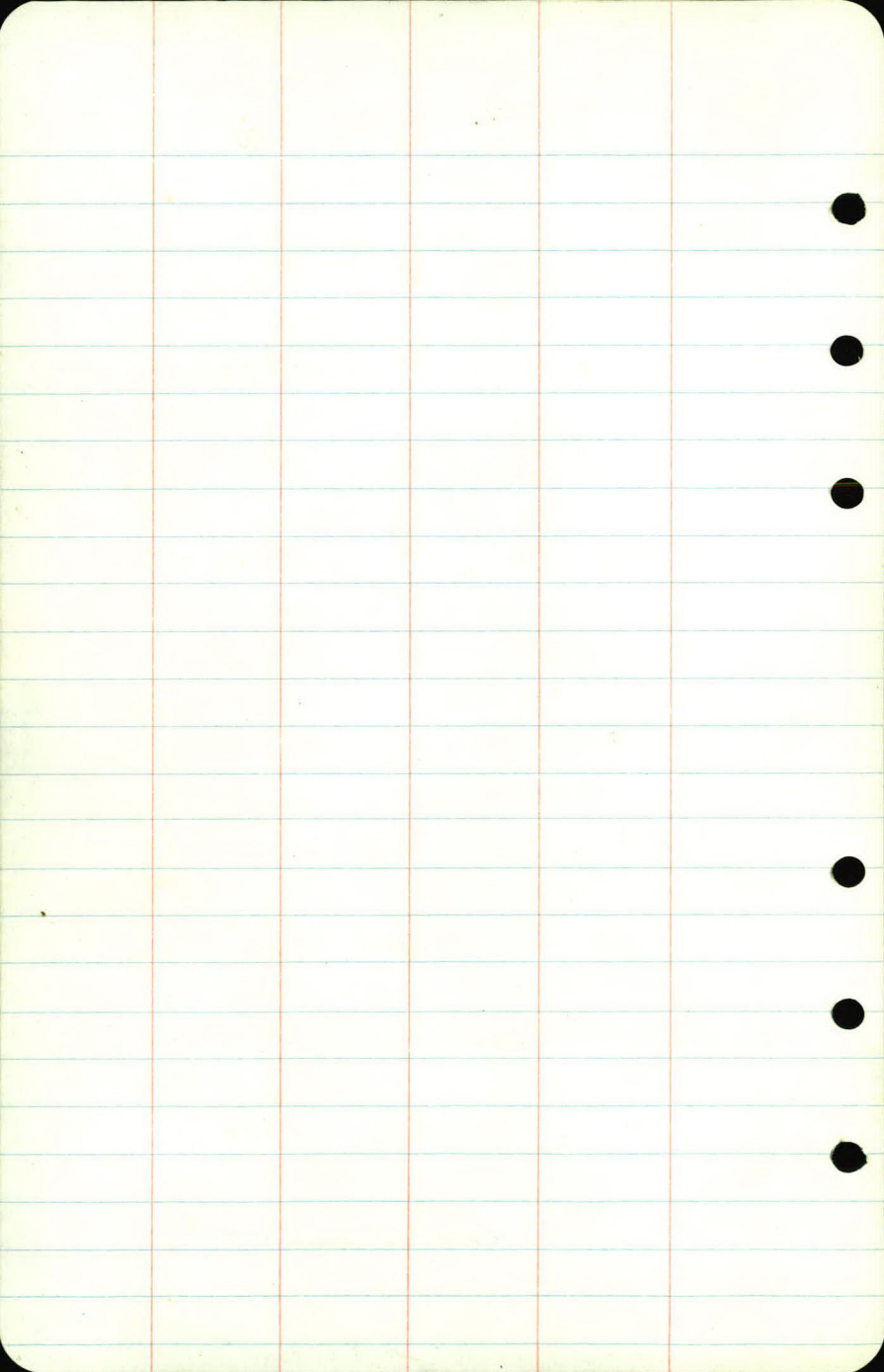
$$5.1 \quad 29.2 \frac{4.0}{+4.1} \quad \frac{51}{0.0} \quad \frac{71}{20.0/27.0'}$$

$$5.2 \quad 25.4 \frac{5.5}{+4.7} \quad \frac{51}{+0.1} \quad \frac{72}{20.0/27.6'}$$

Sta.	+	π	-	Grade
		921.41		
22				161
	+50			16.0
23				15.9
	+27			15.8
	+38			15.7
	+51			15.7
	+65			15.6
	+81			15.5
	+87			15.4
24				15.3
	+28.7			15.2
B.M.			5.40	916.01
				916.06

Gr. Rod	Lt	Supcr Elev	Super Elev	Widening	Pt.
5.3	27.4' / 5.1 +9.2		52 +8.1		7.3 +8.0 / 27.6'
5.4	26.0' / 5.9 +8.5		52 +9.2		7.4 +8.0 / 25.7'
5.5	25.0' / 6.5 +8.0	0.0	54 +8.1		7.5 +8.0 / 27.7'
5.6	25.0' / 6.6 +8.0	0.0	54 +8.0	0.0	7.6 +8.0 / 28.0'
5.7	24.2' / 11.3 -6.1	0.0	53 -8.1	0.0	7.7 +8.0 / 28.0'
5.7	25.5' / 12.6 -7.0	+0.1	60 -8.3	0.0	7.9 +8.0 / 27.5'
5.8	28.2' / 23.9 -17.5	+0.2	62 -8.4	0.1	8.1 +8.0 / 26.4'
5.9		+0.3	63 -8.4	0.2	8.3 +8.0 / 22.1'
6.0		+0.3	64 -8.4	0.1	8.5 +8.0 / 21.6'
6.1	44.1' / 25.7 -19.4	+0.4	65 -8.4	0.3	15.0 -8.0 / 27.8'
6.2	32.5' / 16.4 -11.0	+0.6	67 -8.5	1.9'	23.6' -18.0 / 27.8'

Top Mont. of Kohler Rd. & Edgerton St.



Plan Survey

Kochler Road
Int Centerville Rd
"A" Line

3-6-52

Index

Align 1 to 4

Topog 4 to 7

Bench levels 8 to 10

X Sections 10 to 16

HAW

AM

LC

MB

MM

Rec. 3/7/52
K.A.

16 pages

Sta	Pt	Alt	Dist	Def
-----	----	-----	------	-----

7+54.78	P.1			
---------	-----	--	--	--

725.41	P.7			
--------	-----	--	--	--

			19°41'	
--	--	--	--------	--

6				
---	--	--	--	--

			17°47'	
--	--	--	--------	--

+50				
-----	--	--	--	--

			14°02'	
--	--	--	--------	--

5+00				
------	--	--	--	--

		39°22'		
--	--	--------	--	--

			10°17'	
--	--	--	--------	--

		D 15		
--	--	------	--	--

+50				
-----	--	--	--	--

		T 137.03		
--	--	----------	--	--

			6°32'	
--	--	--	-------	--

		L 262.94		
--	--	----------	--	--

4				
---	--	--	--	--

		R 383.065		
--	--	-----------	--	--

			2°41'	
--	--	--	-------	--

3+62.97	P.C			
---------	-----	--	--	--

			0°00'	
--	--	--	-------	--

SECOV 0 Iron
50029-30-21

PP

Description

G.P.

424'

49.95

52°43'

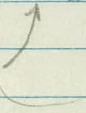
1/13.74

Nail in Parc



20522..

90°00'



P.P.

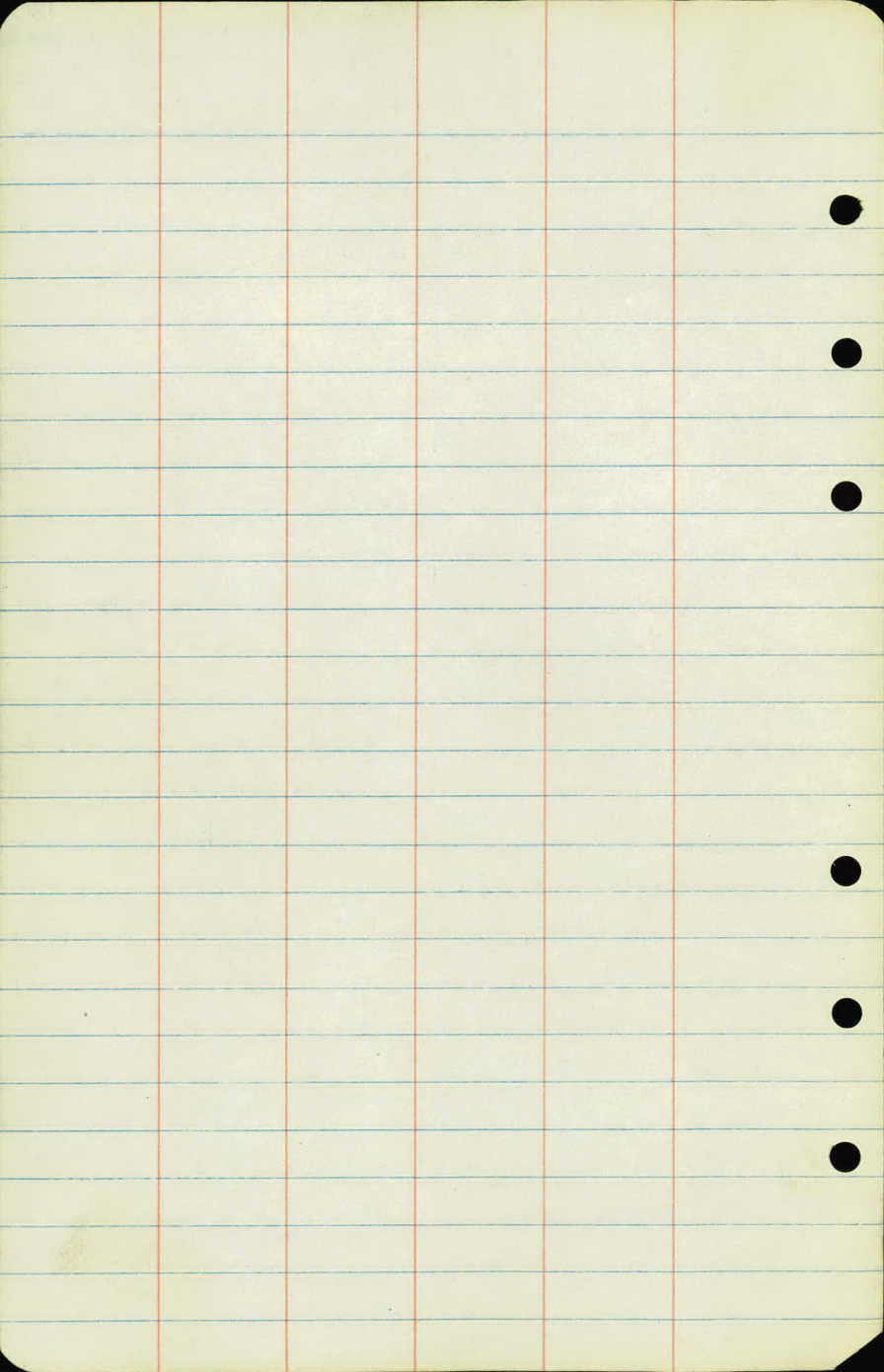
85.55'

65.10'

73.60'

PP

20



Line Revision
Kochler Rd
"B" Loop

Sta.	PT	ALT	ARI
------	----	-----	-----

6+94.80	P.1		90°00'
---------	-----	--	--------

+32.90	PT	15°18'	
--------	----	--------	--

3		12°53'½	
---	--	---------	--

+50		9°08'½	
-----	--	--------	--

2+32.90			Δ 30°36'
---------	--	--	----------

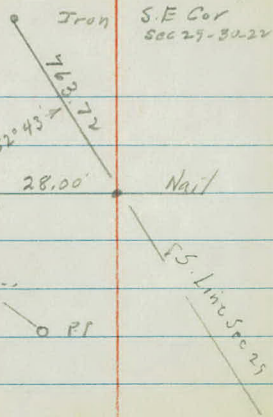
2		5°23'½	D 15°
---	--	--------	-------

+50		1°38'½	T 104.80
-----	--	--------	----------

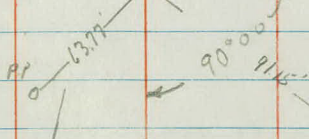
1+28.10	P.C	0°00'	L 204.00
---------	-----	-------	----------

			R 383.065
--	--	--	-----------

Description



Centerville Rd



PI 545400 A
A Line 39°22'

Tri. 15" B.E

41.82'

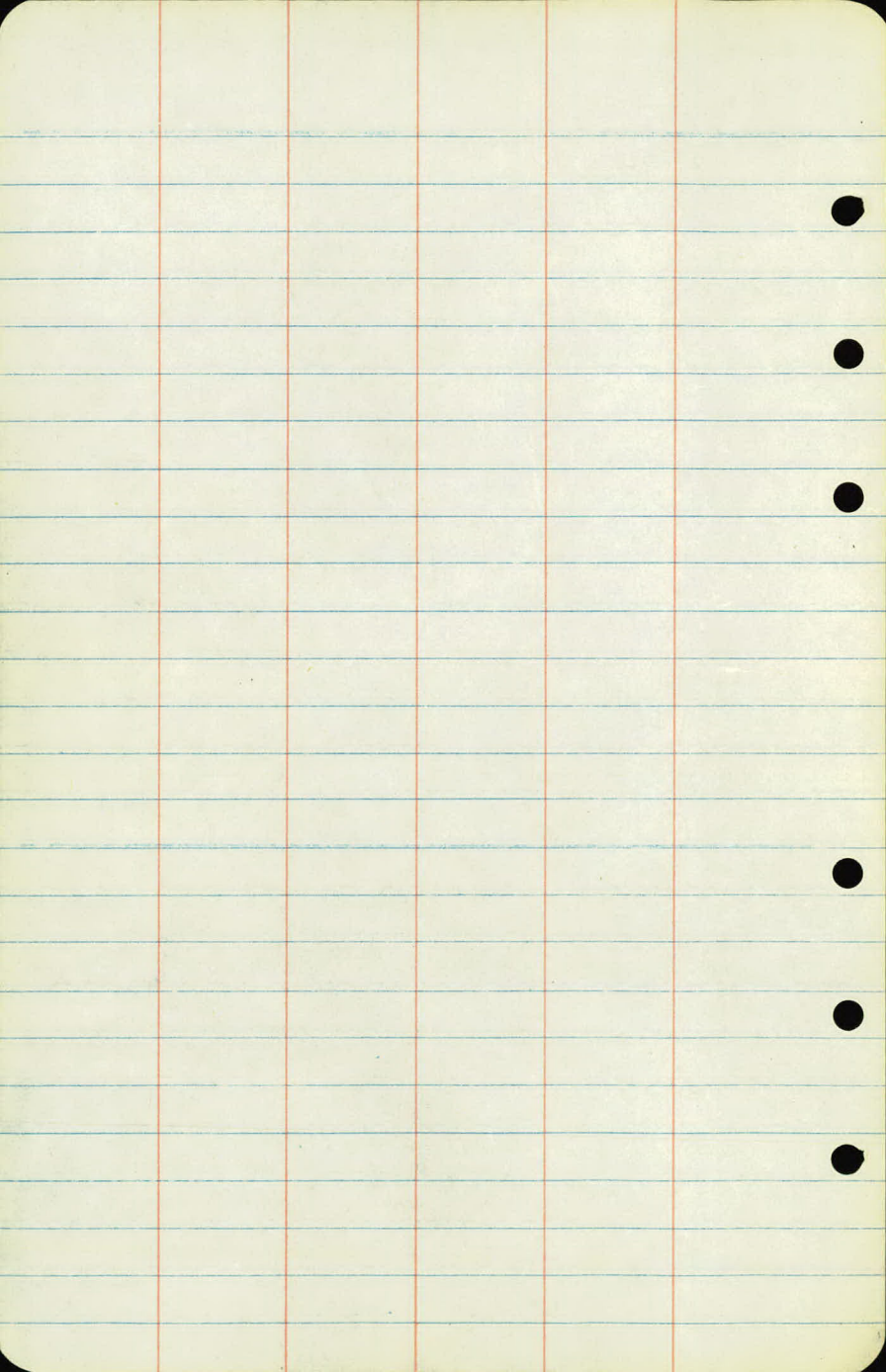
132.75

8°44'

56°46'

15" Oak

PI 1767-25
A & B Lines



TOPOGRAPHY

A Line

Rd

+45 Rad 32

+45 Edge Parr

+45 Rad 39

+20 Rot 10

+20 F. Oak 60

+10 Fe Oak 40

+22 P.P. 27

+20 Beg Rad 11

17' 3'

Fe 28'

33 11

38' 16

+50 Fe 7'

+25 Fe 4'

39-18

Fe 1

36-17

+69 P.P. 17'

Fe 0

28'-8

Fe 7

18' 1

+50 Fe 16

+40 12" Oak 40

+31 G.P. 29

+31 P.P. 16

12' 8

Fe 23

+63 Fe 26

10 10

+21 24" Oak 48'-48"-57

+20 Beg Fe 26

+75 Rye Tix Ent

+66 Ent

+82 P.P. 25

+51 Tr. B.E. 28

+29 8" Lom 26

+19 Oak 45

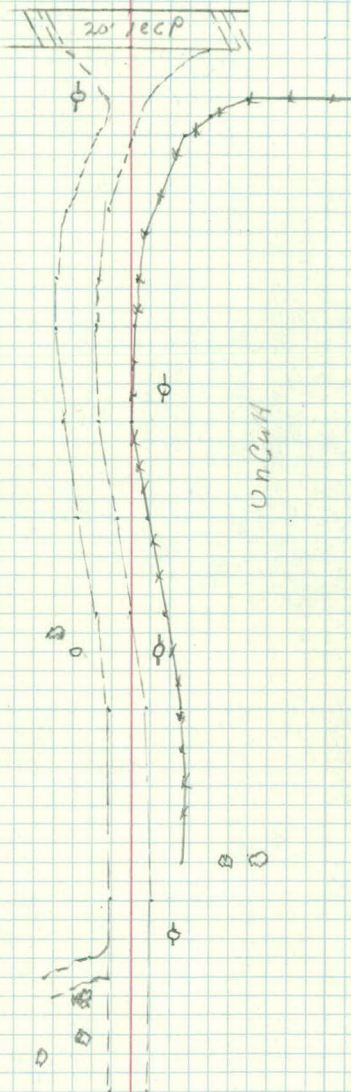
11' 8

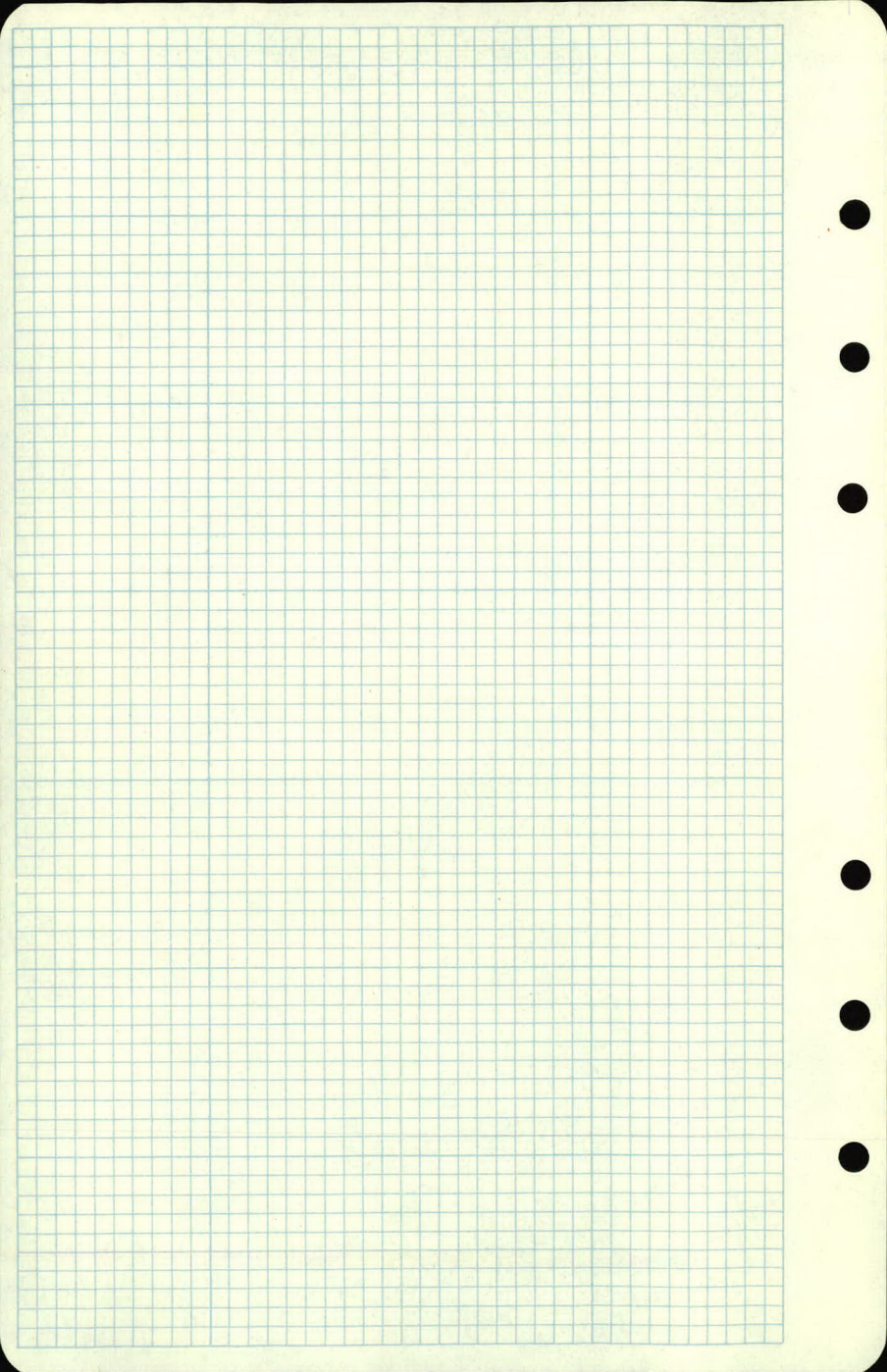
2

1

School Prop

UnCult





TOPOGRAPHY

"B" Line

7

+9480 2 Park

+76 Bay 24" N 66 SCF 225

+62 P.P. 56'

6

5

4

3

+50 43-20

2

21' 1

+77 8" Pop 40

+56 4" Tr 44

+56 Twin Oak 32

+34 P.P. 26

12 8

+19 Rgc. T10 Ent

+09 Oak 29

+07 Ent

1

10 8

+30

10 8

+52 NW Cor Gray 91'

0

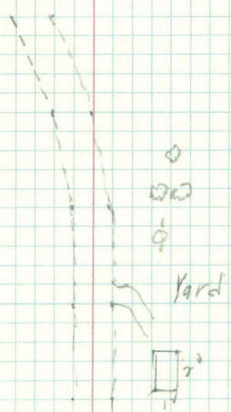
19 19

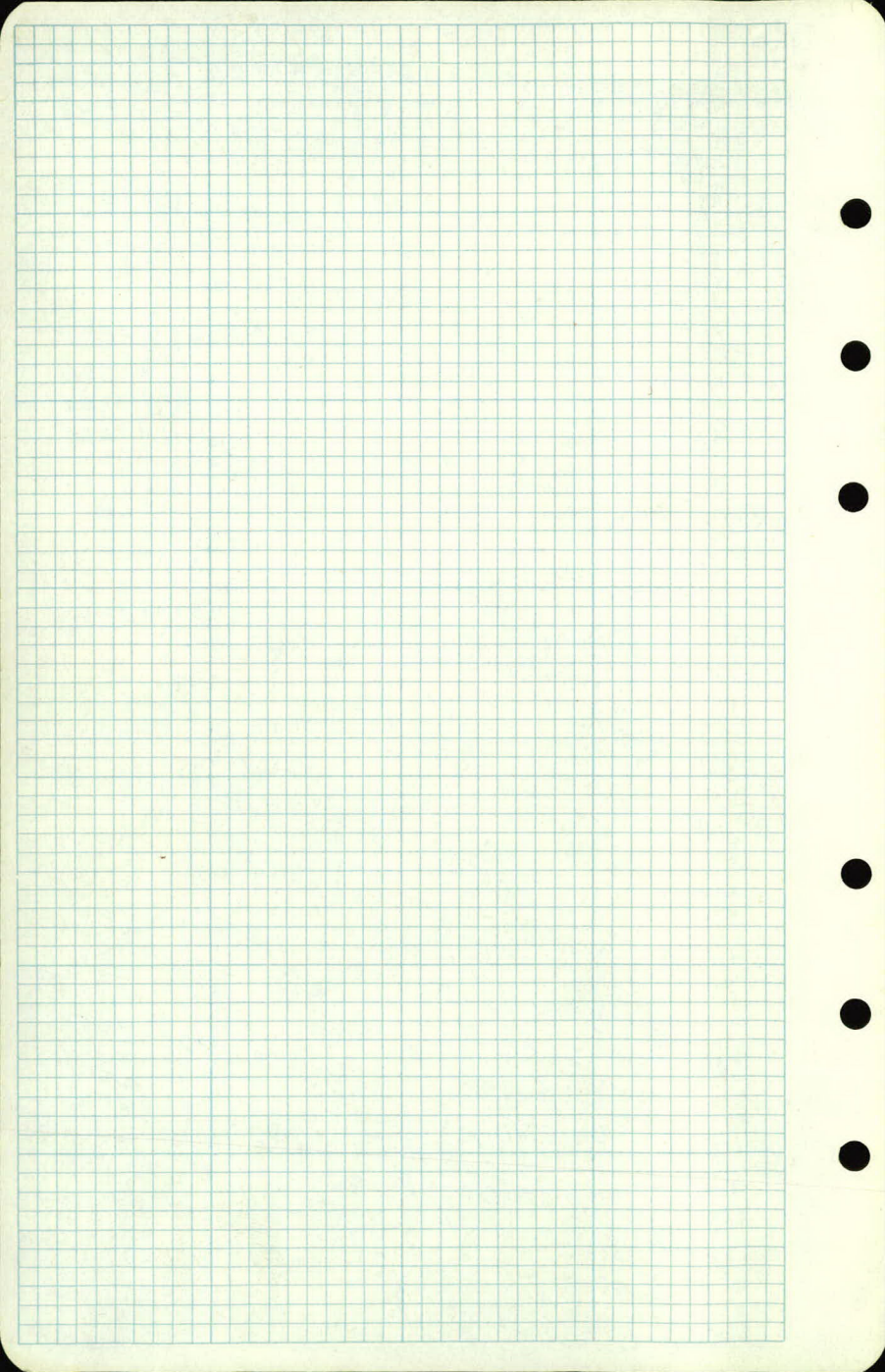
20' 100P 2

2

Uncult

Uncult





Bench Levels

Raise elev. of
X 500. g/levels 9.68 ft.

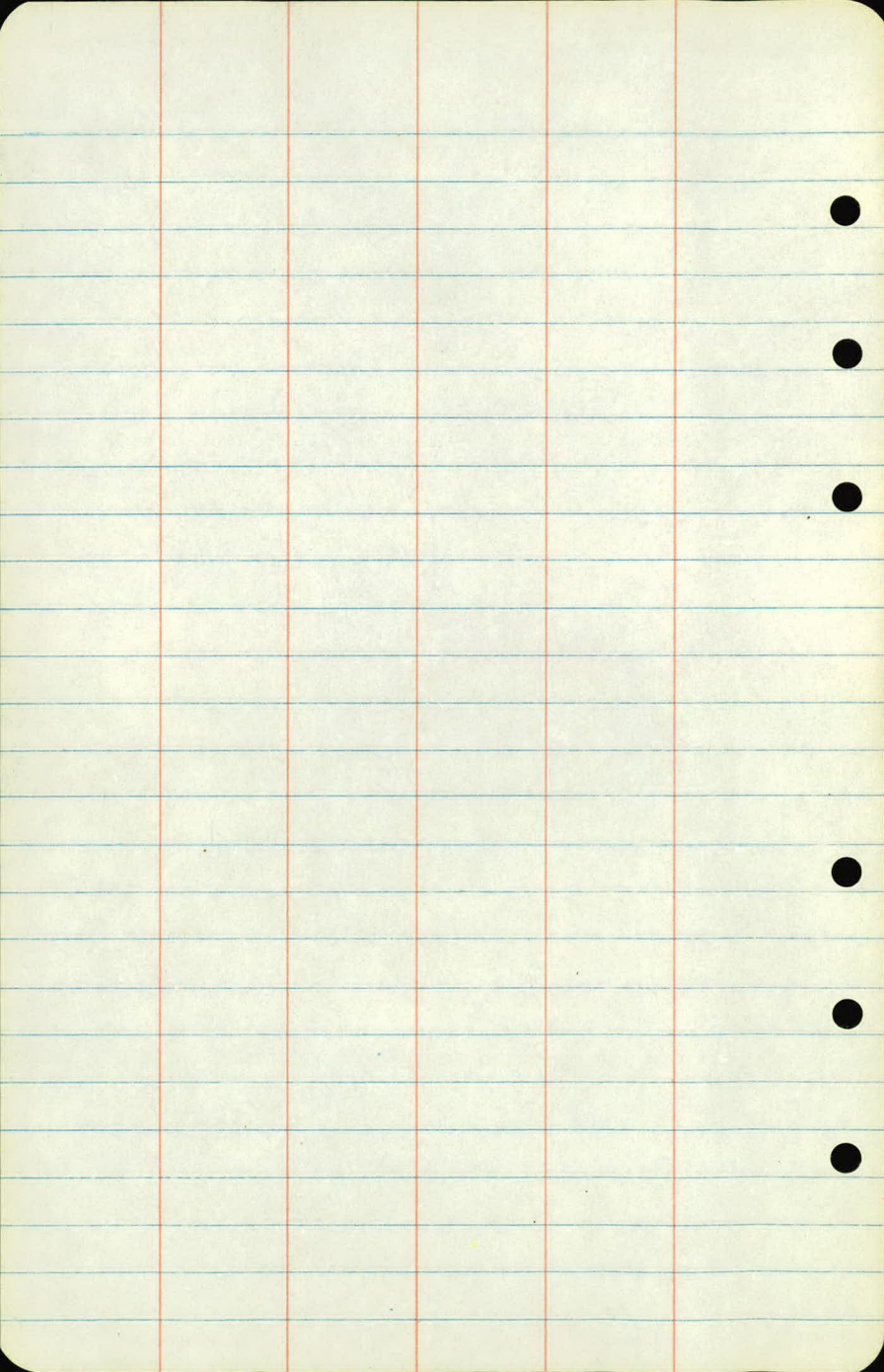
Sta	+	π	-	Elev
B.M	0.75	908.02		907.27
	7.46	910.17	5.25	902.77
	6.01	912.82	3.36	906.81
	2.92	910.86	4.88	909.94
B.M	7.76	910.86	7.76	903.10
B. I.	9.77	916.03	4.60	906.26
B.M			2.43	913.60

Description

Spk in P.P NW Cor Hochler Rd + Edgerly

Spk in 24" G/H 48 R/ Stg 3 + 21 A Line

Spk in P.P NW Cor Hochler Rd + Centerville Rd



X Sections
"A" Line

Sta	+	A	-	Elev
B.M	7.59	910.69		903.10

2+50				05.9
------	--	--	--	------

3				05.7
---	--	--	--	------

+50				05.4
-----	--	--	--	------

4				05.3
---	--	--	--	------

+50				04.6
-----	--	--	--	------

5				03.6
---	--	--	--	------

+50				99.5
-----	--	--	--	------

6				00.6
---	--	--	--	------

Z

RT

Spk in 24" Coll 48' Rt Sta 3+21 ALin

87 80 76 54 51 48 50 56 85 113 122
 50 32 22 14 10 13 19 28 40 50

106 97 87 60 53 50 53 58 94 101 118
 50 35 24 12 11 12 18 25 36 50

99 93 83 59 56 53 58 66 100 130
 50 38 25 15 16 14 21 28 50

97 92 90 58 56 54 59 64 104 113 130
 50 32 24 16 11 10 16 25 36 50

85 91 58 55 54 61 63 72 85 100 111 133
 50 32 26 20 10 2 8 13 16 30 50

82 94 76 51 51 59 63 71 101 106 118 123 140 146
 50 44 39 33 20 9 4 5 10 17 28 43 50

43 40 42 47 62 100 112 114 124 130 137 142
 50 44 38 27 13 5 5 11 20 32 50

2.8 31 39 49 70 95 101 9.8 110 115 118 11.6
 50 42 28 18 6 3 3 15 27 40 50

Sta	+	Δ	-	Elev
		910.69		

6+50				06.1
------	--	--	--	------

T.P.	11.00	919.44	2.25	908.44
------	-------	--------	------	--------

7				10.6
---	--	--	--	------

+2v				12.3
-----	--	--	--	------

+40				14.0
-----	--	--	--	------

+45	Edgr Parc			14.51
-----	-----------	--	--	-------

+55	x Parc			14.60
-----	--------	--	--	-------

B.M.		5.86	913.58	913.60
------	--	------	--------	--------

Lt

R

Rt

20 20 19 22 27 26 46
50 40 33 25 15 5

7.1 7.5 8.4 8.8
8 16 29 50

7.8 83 96 90 87 88 94 12.7 12.2 12.6
50 33 24 17 9 10 16 31 50

7.2 7.8 7.9 7.5 7.1 7.3 7.0 9.5 12.0 8.8 9.4
50 27 15 8 16 18 27 35 43 50

4.6 5.2 5.6 5.3 5.4
50 31 23 11

5.6 5.7 5.7
13 25 50

4.30
50

4.93

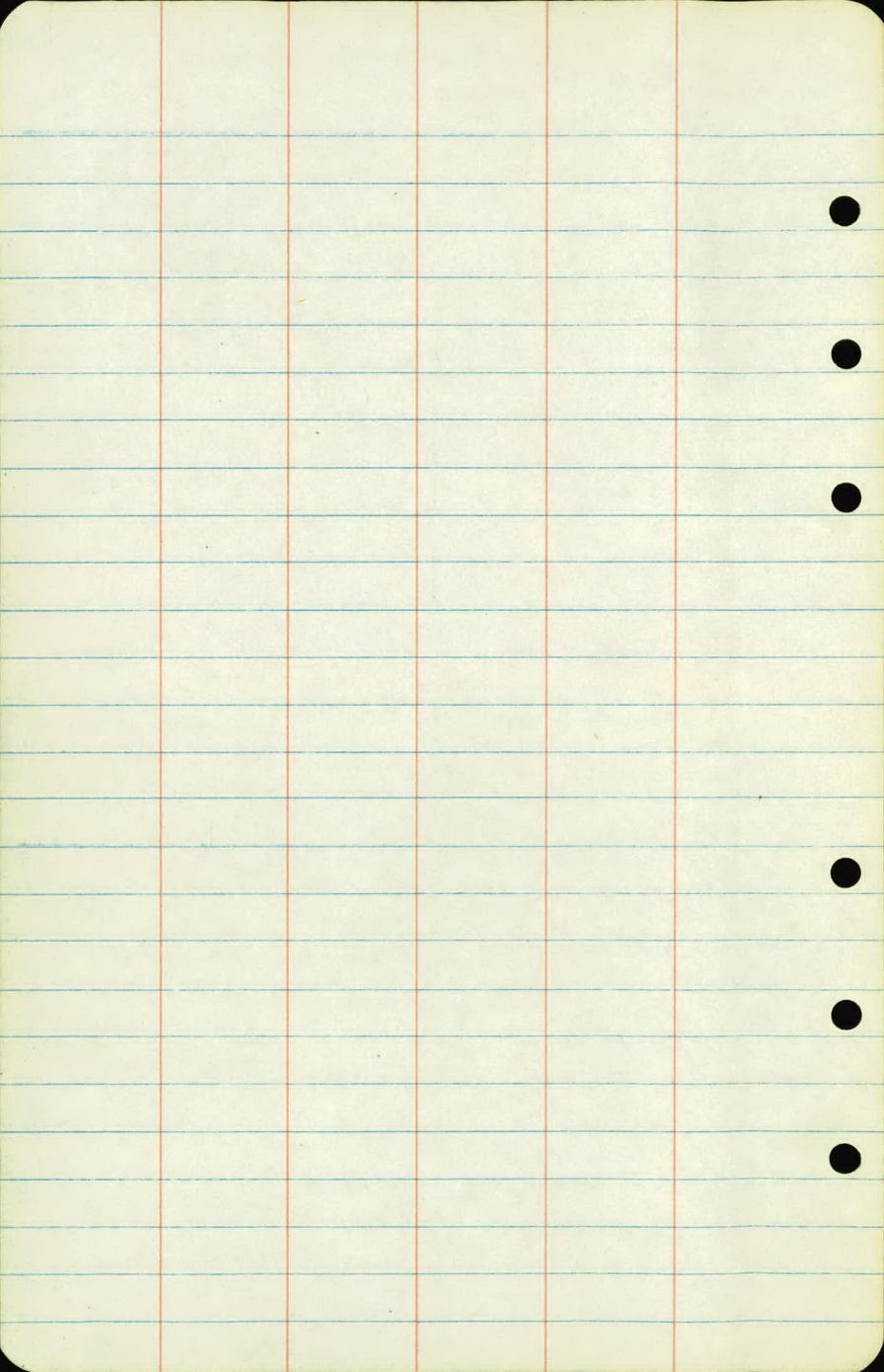
5.47
50

3.52 4.17
100 50

4.84

5.38 5.77
50 100

Spk in PP NW Cor Kochler Rd + Centerville Rd



X sections
Kochler Rd
"B" wing

Sta	+	T	-	Elev
B.M	10.06	913.16		903.10

0+50				08.3
------	--	--	--	------

1				07.8
---	--	--	--	------

+50				07.3
-----	--	--	--	------

2				06.2
---	--	--	--	------

T.P	162	906.17	8.61	904.53
+50				00.6

3				99.1
---	--	--	--	------

+50				92.3
-----	--	--	--	------

4				92.2
---	--	--	--	------

27

2

RT

Spt in 24" CoH 48 Rt Sta 3121 ALIN

121	120	40	47	51	49	5.0	49	35	36	36	16
50	39	26	18	13		12	16	26	36	40	50

5.2	5.3	5.9	5.8
50	31	18	10

5.4	5.4	5.0	5.6	5.3	5.3
7	19	27	42	50	

100	100	95	66	59	5.9	65	73	91	101
50	37	24	15		12	19	26	47	50

10.8	9.8	7.6	7.1	6.8	7.0	7.0	10.6	11.2	12.5	12.5
50	35	28	20	11		5	12	18	33	50

1.6	6.7	0.3	6.5	0.8	5.4	5.6	5.9	6.8	8.4	9.6
50	45	33	22	14	7		9	22	38	50

04	09	1.6	6.1	5.8	6.0	6.5	7.1	8.7	10.9	12.9	13.1
64	50	44	37	30	22	10		15	23	44	50

83	86	107	11.8	12.7	13.9
50	39	26	16	10	

142	142	142
11	28	50

125	140	142
50	28	11

140	142	144	143
	16	35	50

Sta	+	Δ	-	Elev
-----	---	----------	---	------

906.17

4+50

92.2

5

94.6

+50

00.0

6

04.1

T.P

12.70

918.51

0.36

905.81

+50

10.4

+61

11.9

+66

10.1

+71

04.4

L+

L

R+

134
50137
28

140

142
26142
5011.1 48.6
50 2611.4
111.0
3110.5
507.3
506.8
27

6.2

6.9
276.5
503.0
502.7
26

2.1

1.1
240.5
508.6
508.1
20

8.1

8.5
239.1
507.5
507.1
277.0
10

6.6

7.5
167.6
337.4
509.6
508.6
348.8
16

8.4

7.9
157.4
327.3
50

3.1

9.4
5010.5
3410.4
2413.04
24.50
22.5

14.1

9.2
207.7
50

Sta	+	K	-	Elev
-----	---	---	---	------

91851

6 + 7.7

13.0

485

Edge Pav

13.27

194.

± Pav

13.37

BM

492 91359 91360

Lt

Z

Rt

53
50

54
22

55

51
25

52
50

505
50

5.24

5.47
50

465
100

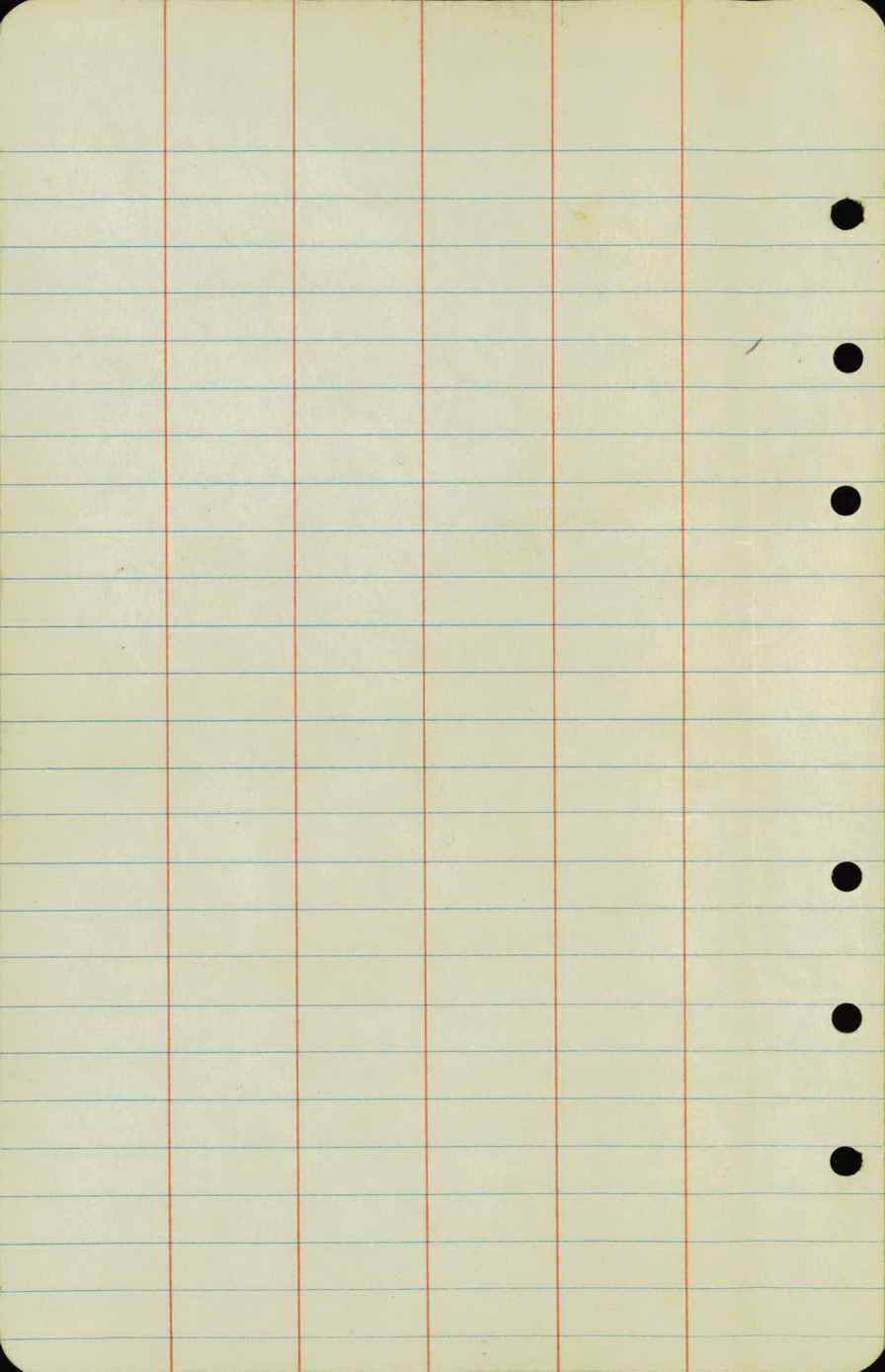
493
50

5.14

5.39
50

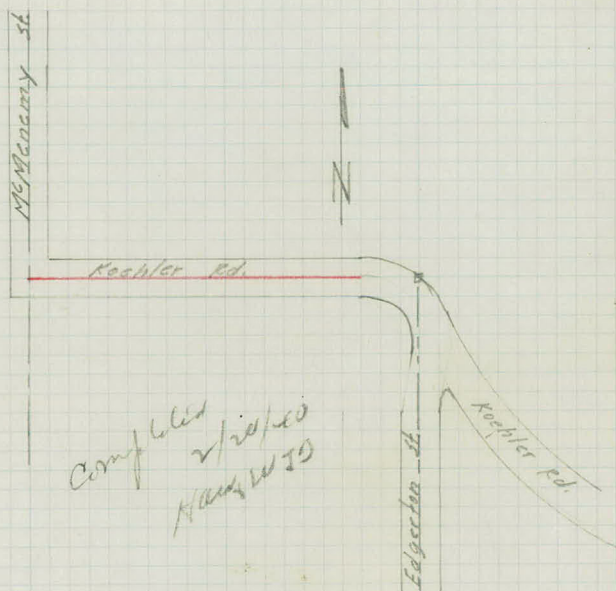
5.58
100

Spk in P.P N.W Cor Koehler Rd & Centerville



PLAN SURVEY
KOEHLER RD.

McMenamy St. to Edgerton St.



INDEX

Align	-1-2
Topog.	-3-7
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