

Bk. 26 - Dr 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Drainage _____ Survey

_____ Larpenteur Avenue 2000' So. _____

From _____ Myrtle Ave _____ To _____ East County Line _____

Road Acc't. No. _____

Date Filed _____ 10/39 _____

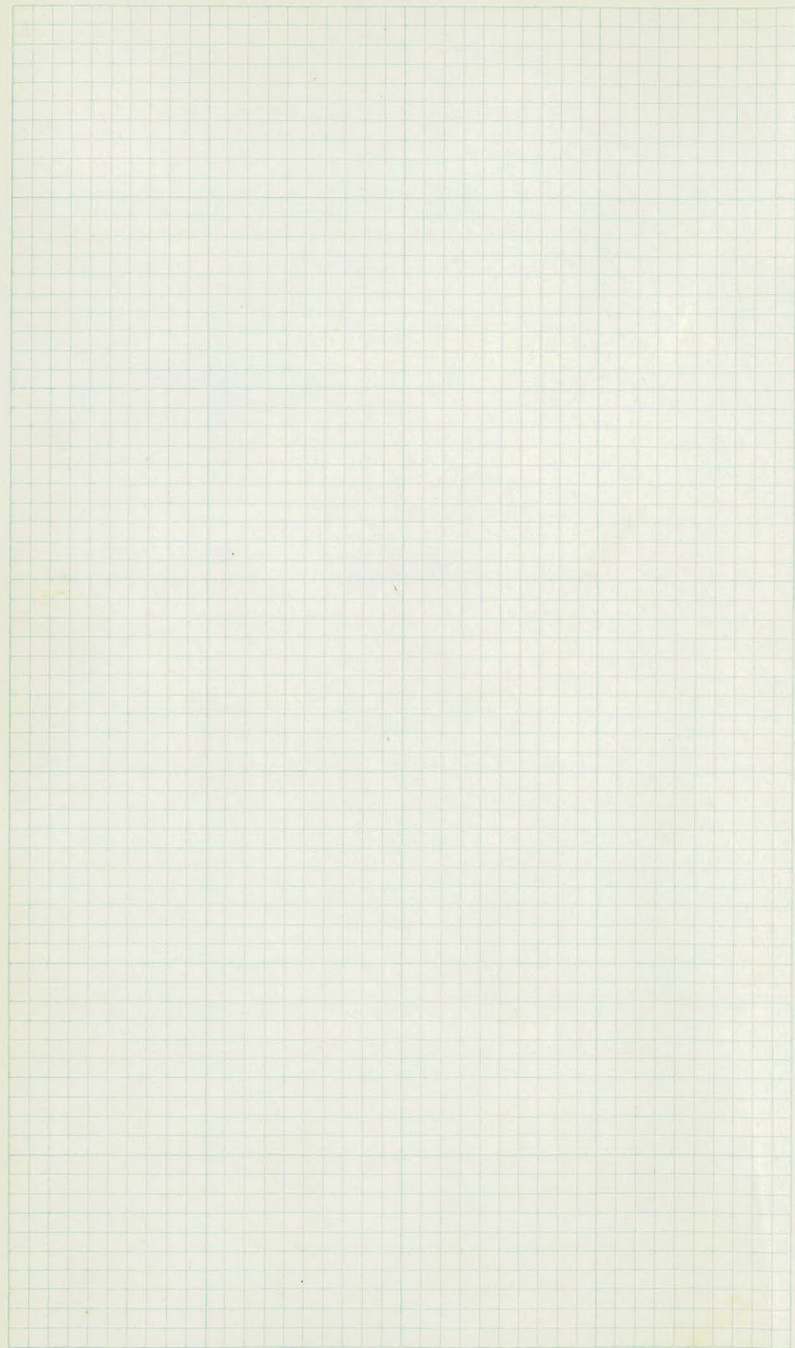
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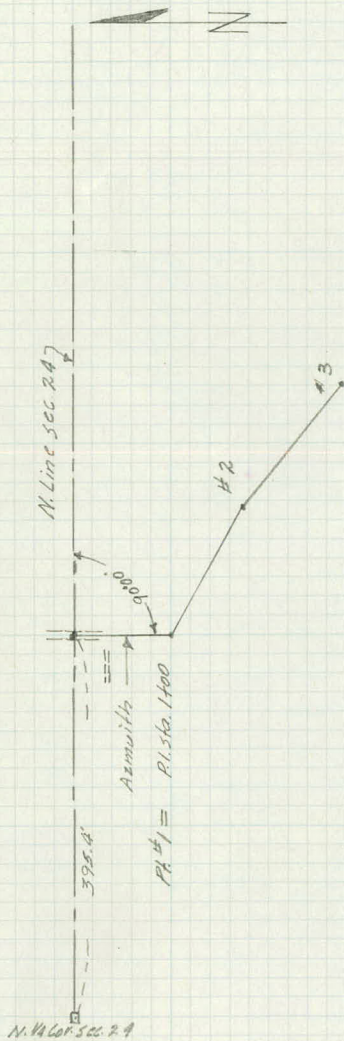
Book 26 Dr 16

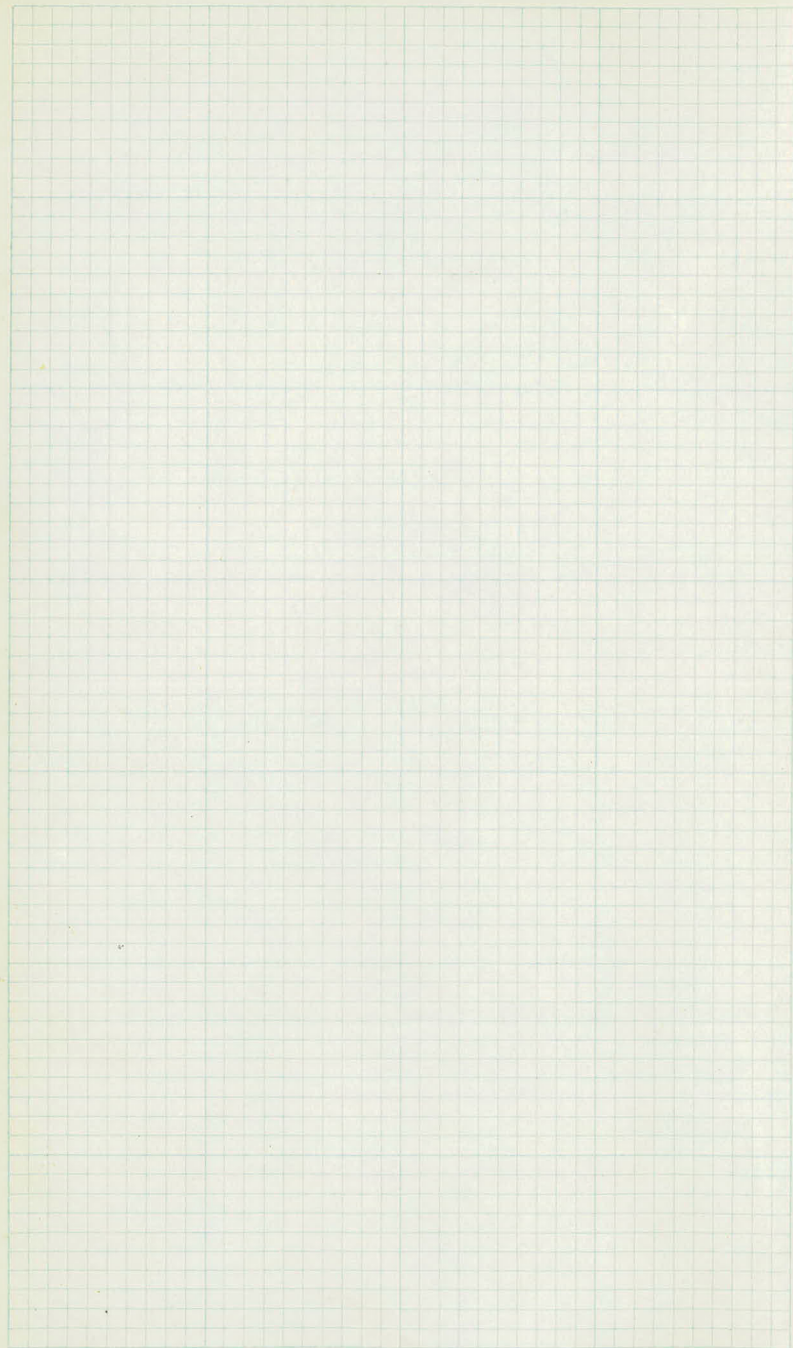
Alignment

Drainage Study
Harpenteur Ave. 2000' so
betw Myrtle Ave & East Co Line

Put on Hardshell
Oct 21-1939
H.C. & W.B.







stadia levels

and

Topography

Azimuth is South.

90° to N. line sec 24

Sta	Azimuth	Dist	Red.	Elev
B.M.	0.08	1002.53		(1002.45)
0 -18			9.0	93.53
01 00				96.73
419				95.9
432	S. End 18" G.M.			91.61
438				91.7
1 +00				
T.P.	4.87	996.58	10.82	991.71
#1	0°00'			
#2	311°36'	264'		
T.P.	3.38	992.21	7.75	988.83
	125°15'	2.24'	2.0	90.2 ✓
	133°42'	202'	5.3	86.9 ✓
	143°57'	186'	5.8	86.4 ✓
	168°57'	172'	4.9	87.3 ✓
Edge Swamp	160°38'	180'	2.9	89.3 ✓
	138°50'	115'	7.9	84.3 ✓
	120°46'	162'	7.0	83.2 ✓
Edge Swamp	116°34'	180'	8.9	83.3 ✓

Description

Top Mant. N. V. Cor. Sec. 24

N. End 18" C.M. G.M.

		97.3	96.73	96.5					
		$\frac{52}{50}$	$\frac{58}{50}$	$\frac{60}{50}$					
		96.6	95.9	96.2					
		$\frac{59}{50}$	$\frac{66}{50}$	$\frac{63}{50}$					
		94.8	93.2	91.61	94.9	95.5	95.0	93.5	93.7
		$\frac{77}{50}$	$\frac{78}{25}$	$\frac{10.92}{C.M.}$	$\frac{76}{9}$	$\frac{70}{31}$	$\frac{15}{23}$	$\frac{90}{28}$	$\frac{85}{22}$
									$\frac{75}{24}$
									$\frac{72}{50}$
	94.0	93.4	92.3	91.3	91.7	92.43	15" C.M. Ent. G.M.	95.0	95.3
	$\frac{85}{50}$	$\frac{91}{37}$	$\frac{102}{21}$	$\frac{11.2}{11}$	$\frac{10.8}{12}$	$\frac{10.10}{12}$	$\frac{7.5}{12}$	$\frac{7.2}{32}$	$\frac{9.22}{32}$
									93.31
88.7	87.5	88.0	88.3	88.9	91.4	95.6			
$\frac{138}{150}$	$\frac{150}{100}$	$\frac{145}{50}$	$\frac{142}{26}$	$\frac{136}{21}$	$\frac{111}{16}$	$\frac{6.9}{16}$			

Sta.	Azimuth	Dist	Red	Elev
		992.21		
	112°46'	198'	56	86.6 ✓
	93°38'	235'	51	87.1 ✓
Edge Swamp	94°29'	220'	94	82.8 ✓
	97°47'	166'	96	82.6 ✓
	100°32'	128'	10.2	82.0 ✓
Edge Swamp	106°36'	72	8.7	83.5 ✓
	117°04'	52	5.8	86.4 ✓
	53°35'	10'	5.5	86.7 ✓
Edge Swamp	34°54'	20'	8.8	83.4 ✓
	27°00'	40'	96	82.6 ✓
	26°10'	53'	10.1	82.1 ✓
	226°50'	53'	6.5	85.7 ✓
Edge Swamp	306°02'	55'	9.2	83.0 ✓
	341°47'	72'	10.9	81.3 ✓
Elev. Water			8.75	83.46 ✓
	297°41'	109'	6.3	85.9 ✓
Edge Swamp	302°03'	110'	8.7	83.5 ✓
	306°49'	188'	6.1	86.1 ✓
Edge Swamp	309°09'	183'	9.5	82.7 ✓
	317°47'	172'	10.7	81.5 ✓
	324°09'	264'	6.8	85.4 ✓
Edge Swamp	324°29'	263'	8.8	83.4 ✓
	328°54'	242'	10.6	81.6 ✓
	331°03'	231'	10.6	81.6 ✓

Description

Sta	Bearing	Dist	Red.	Elev.
		992.21		
T.P.	3.52	992.35	9.38	988.83 ✓
	83°41'	255'	8.6	86.8 ✓
Edge Swamp	83°41'	267'	8.4	84.0 ✓
Swamp	79°45'	190'	9.0	83.4 ✓
	77°18'	310'	4.1	88.3 ✓
Edge	75°09'	285'	5.7	86.7 ✓
Edge Swamp	74°08'	275'	7.8	84.6 ✓
Swamp	71°10'	247	8.5	83.9 ✓
Top Bank	61°07'	315'	5.2	87.2 ✓
Swamp	66°35'	210'	8.5	83.9 ✓
Edge Swamp	60°41'	302'	8.1	84.3 ✓
Top	53°29'	368'	1.9	90.5 ✓
Swamp	51°35'	210'	9.0	83.4 ✓
Edge	50°55'	330'	8.1	84.3 ✓
Top	43°00'	364'	3.9	88.5 ✓
Swamp	50°02'	280'	8.9	83.5 ✓
"	43°32'	324'	8.1	84.3 ✓
"	50°13'	260'	8.6	83.8 ✓
"	43°24'	290'	9.1	83.3 ✓
Top	32°17'	346'	5.9	86.5 ✓
"	23°06'	342'	5.7	86.7 ✓
Swamp	32°15'	336'	8.4	84.0 ✓
Edge	23°36'	330'	9.1	83.3 ✓
Top	13°25'	340'	6.6	85.8 ✓

Description

Sta	Azimuth	Dist	Rod	Elev
Top		992.35		
Top	5° 32'	340'	5.6	86.8 ✓
Swamp	32° 02'	282'	9.1	83.3 ✓
"	23° 34'	300'	10.5	81.9 ✓
Edge	13° 00'	320'	8.4	84.0 ✓
"	4° 20'	330'	8.8	83.6 ✓
Top	353° 51'	365'	6.8	85.6 ✓
Edge	353° 51'	353'	9.3	83.1 ✓
Swamp	12° 39'	193'	8.9	83.5 ✓
"	2° 21'	290	10.4	82.0 ✓
Edge	353° 24'	355'	9.3	83.1 ✓
Top	346° 51'	374'	7.5	84.9 ✓
Swamp	353° 01'	335'	10.8	81.6 ✓
"	340° 49'	219'	10.4	82.0 ✓
"	353° 25'	325'	11.3	81.1 ✓
"	346° 33'	340'	10.7	81.7 ✓
Top	341° 30'	389'	7.2	85.2 ✓
Edge	341° 30'	375'	9.0	83.4 ✓
Swamp	341° 46'	355'	9.8	82.6 ✓
Top	333° 05'	340'	7.7	84.7 ✓
Edge	333° 05'	320'	9.1	83.3 ✓
Swamp	333° 29'	300'	10.5	81.9 ✓
pt. # 3	322° 29'	356'		
T.P.	2.06	989.44	4.97	987.38 ✓
Ridge	119° 49'	26'	3.2	86.2 ✓

Description

Sta	Azimuth	Dist.	Rod	Elev.
		989.44		
Ridge	75°10'	30'	5.7	83.7 ✓
"	60°23'	38'	6.3	83.1 ✓
"	44°13'	60'	5.8	83.6 ✓
"	38°47'	81'	6.5	82.9 ✓
"	33°58'	102'	5.9	83.5 ✓
"	11°33'	130'	6.0	83.4 ✓
Top	2°30'	180'	4.9	84.5 ✓
Top Bank	355°06'	128'	8.0	81.4 ✓
"	353°07'	170'	8.0	81.4 ✓
Edge	354°36'	124'	8.9	80.5 ✓
"	352°16'	167'	9.0	80.4 ✓
Top	347°32'	230'	6.7	82.7 ✓
"	337°14'	253'	5.3	84.1 ✓
Edge	345°25'	283'	8.8	80.6 ✓
Swamp	339°44'	137'	8.6	80.8 ✓
Edge	334°48'	232'	7.6	81.8 ✓
Swamp	333°16'	164'	8.6	80.8 ✓
"	332°26'	215'	9.3	80.1 ✓
"	332°10'	141'	10.7	78.7 ✓
"	330°04'	160'	9.6	79.8 ✓
Top	323°35'	275'	5.3	84.1 ✓
Edge	320°00'	255'	7.6	81.8 ✓
Swamp	317°42'	205'	9.0	80.4 ✓
"	319°50'	165'	8.8	80.6 ✓

Description

Sta.	Azimuth	Dist	Rod	Elev
		989.44		
Swamp	314°12'	151'	9.0	80.4 ✓
Top	313°58'	300'	5.5	83.9 ✓
Edge	311°08'	274'	8.0	81.4 ✓
Swamp	305°13'	245'	9.8	79.6 ✓
"	291°14'	204'	9.2	80.2 ✓
"	288°05'	150'	9.2	80.2 ✓
Top	305°15'	332'	5.0	84.4 ✓
Swamp	297°40'	280'	10.2	79.2 ✓
"	284°00'	270'	10.4	79.0 ✓
"	271°40'	170'	8.8	80.6 ✓
Edge	302°50'	315'	7.3	82.1 ✓
Swamp	300°43'	290'	10.3	79.1 ✓
"	295°15'	291'	11.4	78.0 ✓
Edge	280°33'	360'	9.8	79.6 ✓
Swamp	274°44'	257'	8.3	81.1 ✓
"	268°51'	302'	9.1	80.3 ✓
Top	264°09'	276'	8.9	80.5 ✓
Swamp	264°50'	273'	9.9	79.5 ✓
Gr Ditch	257°19'	258'	9.7	79.5 ✓
Bank	257°19'	264'	8.4	81.0 ✓
Bank	255°30'	250'	8.8	80.6 ✓
Swamp	261°51'	219'	9.9	79.5 ✓
Bank	250°10'	185'	7.4	82.0 ✓
Swamp	257°51'	180'	9.6	79.9 ✓

Description

Sta.	Azimuth	Dist	Red	Elev.
		989.44		
Swamp	271°32'	157	8.9	80.5 ✓
Top	245°54'	150	6.5	82.9 ✓
Swamp	247°04'	138	8.7	80.7 ✓
Top	241°07'	129	7.6	81.8 ✓
Swamp	242°31'	127	8.8	80.6 ✓
Swamp	271°30'	106	8.8	80.6 ✓
Top	243°54'	89	8.4	81.0 ✓
Swamp	240°14'	90	9.8	79.6 ✓
Top	269°11'	35	7.2	82.2 ✓
Swamp	273°24'	47	9.0	80.4 ✓
A #4	299°15'	380		
T.P.	5.12	987.51	7.05	982.39
B.M.			4.83	982.68
Edge	183°09'	18	6.4	81.1 ✓
Swamp	171°58'	120	7.7	79.8 ✓
"	193°53'	50	8.5	79.0 ✓
Edge	225°58'	28	8.0	79.5 ✓
"	204°20'	137	7.0	80.5 ✓
Swamp	167°07'	208	8.0	79.5 ✓
Top	208°32'	144	5.5	82.0 ✓
Edge	180°16'	218	7.0	80.5 ✓
"	202°13'	220	6.3	81.2 ✓
Top	205°42'	219	4.8	82.7 ✓
Edge	218°48'	98	7.6	79.9 ✓

description

Top Rock 5th 4

Sta.	Azimuth	Dist.	Pod.	Elev.
		987.51		
Swamp	244°12'	70'	8.2	79.3 ✓
Top	230°30'	122'	4.3	83.2 ✓
Edge	245°33'	83'	7.9	79.6 ✓
Top	245°33'	98'	5.4	82.1 ✓
"	273°22'	147'	5.7	81.8 ✓
Edge	273°22'	128'	7.0	80.5 ✓
Swamp	273°22'	92'	8.1	79.4 ✓
Top	273°22'	15'	6.8	80.7 ✓
Edge	273°22'	22'	7.9	79.6 ✓
Swamp	273°22'	51'	8.4	79.1 ✓
B.M.	480	987.48		982.68
Top	356°35'	102'	5.1	82.4 ✓
Edge	346°00'	107'	8.2	79.3 ✓
Swamp	313°23'	150'	7.7	79.8 ✓
Top	347°02'	160'	6.6	80.9 ✓
Edge	345°10'	162'	8.2	79.3 ✓
Swamp	340°00'	169'	8.6	78.9 ✓
"	313°22'	225'	7.8	79.7 ✓
Top	347°30'	221'	6.9	80.6 ✓
Edge	344°27'	230'	9.4	78.1
Swamp	324°16'	252'	8.1	79.4
Top	249°45'	270'	7.8	79.7
Edge	349°11'	260'	9.0	78.5
Swamp	328°40'	298'	8.4	79.1

Description

Top Rock 5th 4.

sta	azimuth	dist	Red.	Elev.
		987.48		
Top	349°05'	325'	7.7	79.8 ✓
Edge	348°26'	330'	8.5	79.0 ✓
Swamp	345°02'	336'	9.0	78.5 ✓
"	333°08'	350'	8.9	78.6 ✓
Top	347°06'	380'	7.2	80.3 ✓
Top Ditch ^{8'}	346°30'	382'	8.9	78.6 ✓
In Ditch	345°15'	380'	11.7	75.8 ✓
Top Water			9.05	78.43
Swamp	336°47'	393'	9.1	78.4 ✓
Beginning Ditch	346°35'	360'	9.5	78.0 ✓
Top Ditch	343°45'	372'	10.8	76.7 ✓
Top Ditch	343°30'	370'	8.5	79.0 ✓
Top Bank	346°11'	420'	7.4	80.1 ✓
Swamp	345°37'	425'	9.1	78.4 ✓
Ditch	344°40'	425'	11.4 4.11	83.4 ✓
In Ditch	343°13'	420'	11.7	75.8 ✓
Top Ditch	343°13'	420'	8.9	78.6 ✓
Top Bank	344°17'	465'	8.3	79.2 ✓
End Ditch	343°23'	473'	9.5	78.0 ✓
Top "	342°46'	464'	8.6	78.9 ✓
Swamp	337°34'	405'	9.2	78.3 ✓
"	333°05'	464'	8.8	78.7 ✓
# 5	345°26'	500'		
T.P	4.87	986.62	5.73	981.75 ✓

$$\begin{array}{r} 87.5 \\ 11.4 \\ \hline 76.1 \end{array}$$

Description

Sta.	Azimuth	Dist ↓ 986.62	Red.	Elev
Top	307°41'	35'	8.6	78.0 ✓
Edge	305°00'	37'	9.1	77.5 ✓
Swamp	297°13'	41'	9.9	76.7 ✓
"	263°00'	124'	8.3	78.3 ✓
"	274°18'	92'	8.9	77.7 ✓
Top	05°53'	78'	8.3	78.3 ✓
Edge	01°02'	83'	9.4	77.2 ✓
Swamp	345°04'	80'	9.3	77.3 ✓
"	337°12'	83'	10.9	75.7 ✓
"	307°24'	127'	9.1	77.5 ✓
"	297°04'	180'	8.8	77.8 ✓
"	291°16'	225'	9.3	77.3 ✓
Top Bank 6" Pitch	287°25'	280'	8.7	77.9 ✓
Bottom Pitch	287°25'	282'	11.1	75.5 ✓
Edge Bank Top	286°47'	287'	9.1	77.5 ✓
Swamp	282°25'	350'	9.4	77.2 ✓
"	280°00'	444'	8.9	77.7 ✓
Edge Swamp	279°00'	550'	8.6	78.0 ✓
Top Bank	279°00'	540'	6.4	80.2 ✓
" "	272°35'	540'	5.7	80.9 ✓
Edge Swamp	272°35'	537'	6.9	79.7 ✓
Swamp	272°35'	460'	8.7	77.9 ✓
Top Bank	266°05'	340'	5.9	80.7 ✓
Swamp	273°24'	378'	9.3	77.3 ✓

description

Sta.	Azimuth	Dist.	Red.	Elev.
		986.62		
Edge Swamp	266°10'	324'	8.8	77.8 ✓
Top Ditch	273°25'	292'	8.8	77.8 ✓
In Ditch	273°25'	290'	11.9	74.7 ✓
Top Ditch	273°25'	280'	8.3	78.3 ✓
" "	260°41'	315'	9.1	77.5 ✓
In Ditch	260°41'	313'	11.1	75.5 ✓
Top Ditch	260°41'	320'	9.2	77.4 ✓
Top Bank	247°39'	330'	6.2	80.4 ✓
Edge Swamp	247°27'	330'	8.4	78.2 ✓
Swamp	257°05'	248'	8.3	78.3 ✓
"	240°07'	310'	9.3	77.3 ✓
"	242°30'	265'	8.4	78.2 ✓
Top Bank	237°31'	370'	4.6	82.0 ✓
Edge Swamp	236°42'	360'	7.2	79.4 ✓
Swamp	231°44'	310'	8.1	78.5 ✓
"	225°00'	275'	7.6	79.0 ✓
Top Bank	229°40'	424'	3.9	82.7 ✓
Edge Swamp	227°07'	410'	7.8	78.8 ✓
Swamp	212°28'	310'	8.2	78.4 ✓
"	225°31'	412'	9.1	77.5 ✓
"	218°24'	350'	7.8	78.8 ✓
Top Bank	228°05'	490'	4.3	82.3 ✓
Swamp	209°00'	370'	7.9	78.7 ✓
Edge Swamp	225°00'	500'	7.5	79.1 ✓

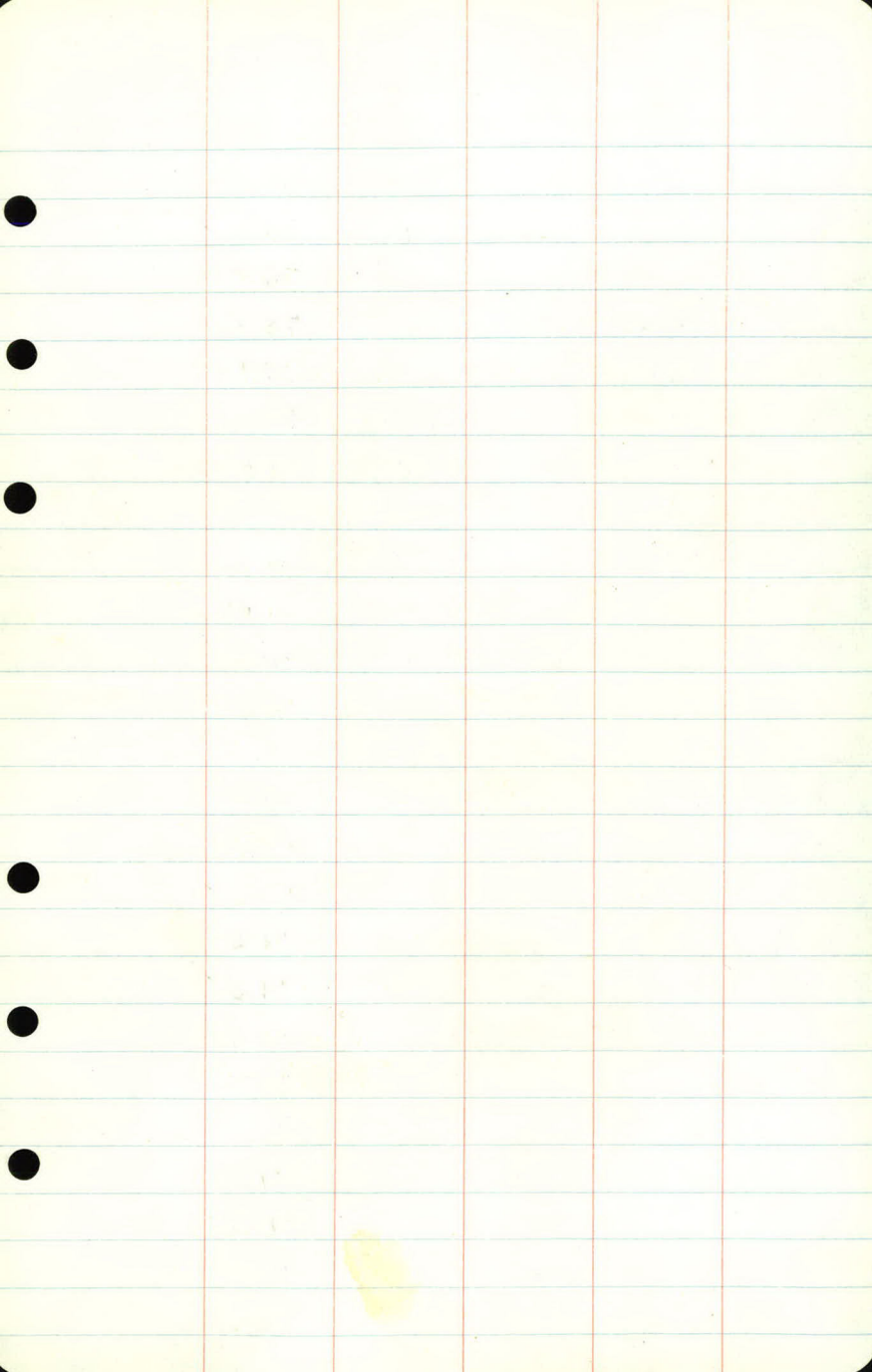
Description

470
981.73
986.45

Sta.	Azimuth	Dist.	Red.	Elev.
		986.62		
Swamp	214°40'	410'	8.0	78.6 ✓
"	223°47'	480'	8.1	78.5 ✓
"	208°05'	440'	8.0	78.6 ✓
Top Bank	226°35'	544'	5.6	81.0 ✓
Edge Swamp	223°40'	543'	6.8	79.8 ✓
Top Bank	207°00'	490'	6.1	80.5 ✓
Edge Swamp	207°00'	488'	7.2	79.4 ✓
" "	220°45'	525'	7.5	79.1 ✓
" "	198°43'	460'	7.9	78.7 ✓
Top Bank	194°42'	450'	6.0	80.6 ✓
Edge Swamp	190°42'	450'	7.6	79.0 ✓
Swamp	190°00'	440'	8.1	78.5 ✓
Δ #6	5°47'	278'		✓
T.P.	3.72	986.45	3.89	982.73
Δ #7	32°30'	1160'	7.2	79.3
T.P.			12.20	74.3
Ditch	34°05'	800'	15.2	71.3 ✓
"	36°20'	520'	12.2	74.3 ✓
"	36°20'	380'	13.5	73.0 ✓
"	33°47'	290'	11.5	75.0 ✓
"	30°45'	270'	14.3	72.2 ✓
"	16°30'	200'	13.1	73.4 ✓
"	27°05'	220'	11.8	74.7 ✓
"	5°30'	180'	13.7	72.8 ✓

Description

Sta	Azimuth	Dist.	Red	Elev.
Swamp	12°50'	210'	10.5	76.0 ✓
Ditch	357°30'	160'	13.5	73.0 ✓
Swamp	344°00'	250'	11.1	75.4 ✓
Pitch	338°30'	140'	12.9	73.6 ✓
Swamp	333°30'	270'	11.6	74.9 ✓
Ditch	312°00'	120'	13.4	73.1 ✓
Swamp	330°00'	280'	10.9	75.9 ✓
Ditch	285°30'	120'	13.2	73.3 ✓
Swamp	343°30'	380'	10.6	75.9 ✓
Ditch	261°00'	180'	13.0	73.5 ✓
"	248°00'	240'	13.0	73.5 ✓
"	241°15'	300'	12.0	74.5 ✓
Swamp	236°15'	270'	9.3	77.2 ✓
"	345°00'	360'	11.4	75.1 ✓
"	230°00'	217'	9.0	77.5 ✓
"	348°30'	380'	11.9	74.6 ✓
"	224°00'	180'	9.6	76.9 ✓
"	346°00'	480'	8.3	78.2 ✓
"	207°30'	160'	10.1	76.4 ✓
"	348°15'	460'	11.0	75.5 ✓
"	295°00'	35'	11.3	75.2 ✓
"	291°35'	70'	10.4	76.1 ✓
"	290°45'	130'	9.8	76.7 ✓
"	291°30'	190'	9.7	76.8 ✓
"	291°30'	260'	9.4	77.1 ✓



Pt.	Azimuth	Dist	Rod	Elev	
		986.45			
Swamp	291°25'	320'	9.0	77.5 ✓	
"	354°45'	100'	11.7	74.8 ✓	
"	12°30'	130'	11.1	75.4 ✓	
"	23°35'	170'	11.4	75.1 ✓	
"	31°00'	215'	11.8	74.7 ✓	
"	42°15'	270'	12.1	74.4 ✓	
T.P.	8.05	982.30 ✓	12.20	974.25 ✓	
Δ #7					
Flow Line West culv.	96°13'	20'	11.05	71.25 ✓	36" culv.
Flow Line East culv.	104°15'	15'	11.00	71.30 ✓	
Ditch	132°00'	13'	11.7	70.6 ✓	
Swamp	143°15'	20'	10.2	72.1 ✓	
"	153°15'	60'	9.9	72.4 ✓	
"	160°10'	120'	9.6	72.7 ✓	
Ditch	239°10'	100'	10.7	71.6 ✓	
Swamp	163°15'	170'	10.3	72.0 ✓	
"	172°30'	170'	10.7	71.6 ✓	
"	201°00'	150'	9.7	72.6 ✓	
"	187°45'	190'	10.4	71.9 ✓	
"	202°25'	210'	10.6	71.7 ✓	
"	205°15'	230'	11.2	71.1 ✓	
"	216°00'	210'	10.7	71.6 ✓	
"	208°15'	240'	11.0	71.3 ✓	
"	226°30'	200'	9.7	72.6 ✓	

1.55

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1.55

1.55

1.55

1.55

Pt.	Az.	Dist.	Rod	Elev.
		982.30		
Swamp	211°45'	240'	12.0	70.3 ✓
"	220°00'	290'	8.4	73.9 ✓
"	234°30'	220'	10.2	72.1 ✓
"	231°45'	300'	10.5	71.8 ✓
"	236°00'	300'	11.5	70.8 ✓
"	206°00'	320'	9.3	73.0 ✓
"	200°00'	360'	10.1	72.2 ✓
Ditch	239°20'	400'	12.5	69.8 ✓
"	110°15'	20'	11.8	70.5 ✓
"	77°45'	65'	11.8	70.5 ✓
"	67°45'	220'	10.4	71.9 ✓
"	72°15'	100'	11.5	70.8 ✓
T.P.	6.83	986.25 ✓	2.88	979.42 ✓
Δ #8 N. Track	47°45'	58'	} Double Tracks 15.7%	
No. Ry. Track	245°15'			
Flow Line W. Culv.	} 2.36" x 78" C.M. Rt. Angles to track bed		15.50	70.75
Flow Line E. Culv.			15.56	70.69

6/16/39

Larpenteur Ave.

Myrtle - 800' East

Slope Stakes



19

Sta.	+	π	-	Elev.	Ditch Lt.
------	---	-------	---	-------	-----------

B.M.	10.12	10 12.57 10 20.73		1002.45	
0				17.5	

+50				16.5	
-----	--	--	--	------	--

1				16.0	12.0
---	--	--	--	------	------

+50				15.7	11.85
-----	--	--	--	------	-------

2				15.5	11.7
---	--	--	--	------	------

+50				15.2	11.55
-----	--	--	--	------	-------

3				15.0	11.4
---	--	--	--	------	------

+50				14.7	11.25
-----	--	--	--	------	-------

4				14.5	11.1
---	--	--	--	------	------

+50				14.2	10.95
-----	--	--	--	------	-------

5				14.0	10.8 ₁₅
---	--	--	--	------	--------------------

+50				13.7	10.65
-----	--	--	--	------	-------

T.P.	5.61	10 19.11	7.23	1013.50	
------	------	----------	------	---------	--

6.16 1018.46 0.27 1012.30 ✓
 7.10 1020.73 4.83 1013.63 ✓

G.R. D.G.R.

£

Top Mon S.W. Cor. Sta 16 + 46.7

3.2

$\frac{3.2}{15}$

4.2

$\frac{4.2}{15}$

$\frac{4.2}{15}$

4.7

8.7 $\frac{4.0}{DC 1.3}$ $\frac{4.7}{15}$
 29.6

$\frac{4.7}{15}$

5.0

8.9 $\frac{3.9}{DC 1.0}$ $\frac{5.0}{15}$
 28.8

$\frac{5.0}{15}$

5.2

9.0 $\frac{3.8}{DC 1.3}$ $\frac{5.2}{15}$
 29.2

$\frac{5.2}{15}$

26.6

5.5

9.1 $\frac{3.6}{SDC 1.3}$ $\frac{4.5}{Down 1.0}$
 29.8 15

$\frac{4.5}{Down 1.0}$
 15

26.2

5.7

9.3 $\frac{3.6}{SDC 6.7}$ $\frac{4.7}{Down 1.0}$
 33 15

$\frac{4.7}{Down 1.0}$
 15

33

6.0

9.4 $\frac{3.4}{SDC 2.8}$ $\frac{5.0}{Down 1.0}$
 31.4 15

$\frac{5.0}{Down 1.0}$
 15

25.8

6.2

9.6 $\frac{3.4}{SDC 0.2}$ $\frac{6.2}{15}$
 26.2

$\frac{6.2}{15}$

25.8

6.5

9.7 $\frac{3.2}{SDC 0.4}$ $\frac{6.5}{15}$
 26.2

$\frac{6.5}{15}$

25.4

6.7

9.9 $\frac{3.2}{SDC 1.0}$ $\frac{6.7}{15}$
 27.4

$\frac{6.7}{15}$

25.4

7.0

10.0 $\frac{3.0}{SDC 0.9}$ $\frac{7.0}{15}$
 26.8

$\frac{7.0}{15}$

25.0

£

Sta	+	π	-	Elev.	Sp. Ditch Lt
-----	---	---	---	-------	--------------

1019.11

6

13.5

10.5

+50

13.2

10.35

7

13.0

10.2

+50

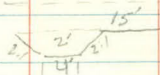
12.7

10.05

8

12.4

09.9



B.M.

4.98

1007.43

1002.45

15

15+50

16

+50

17

+50

18

+50

19

+50

19.0
24.8
4.8

G/R

SDGR

4

5.6

8.6

(3.0)

8.0
SDC 0.6
26.2

5.6
15

5.6
15

25.0

5.9

8.7

(2.8)

5.4
SDC 3.3
31.2

4.9
Down 1.0
15

4.9
Cut 1.0
15

24.6

6.1

8.9

(2.8)

3.4
SDC 5.5
33

5.1
Cut 1.0
15

5.1
Down 1.0
15

24.6

6.4

9.0

(2.6)

9.0
SDC 0.0
27.0

6.4
15

6.4
15

24.6

6.7

9.2

(2.5)

6.7
15

6.7
15

24.0

4

Top S.W. Cor Mon Sta. 14 + 46.7

4.5

6.3
DC 2.2
23.4

7.0
DC 0.1
23.2

5.1

6.7
DC 0.4
23.8

5.0

5.9
DC 1.1
25.2

5.2

6.8
DC 0.4
23.8
8.3
DC 0.2
23.4

6.5

8.7
DC 1.5
42.0
10.3
DC 0.9
24.8

8.2

10.0
DC 0.4
23.4

9.2

10.7
DC 0.5
24.0

9.7

11.2
DC 0.5
24.0

10.0

11.0
DC 1.0
25.0

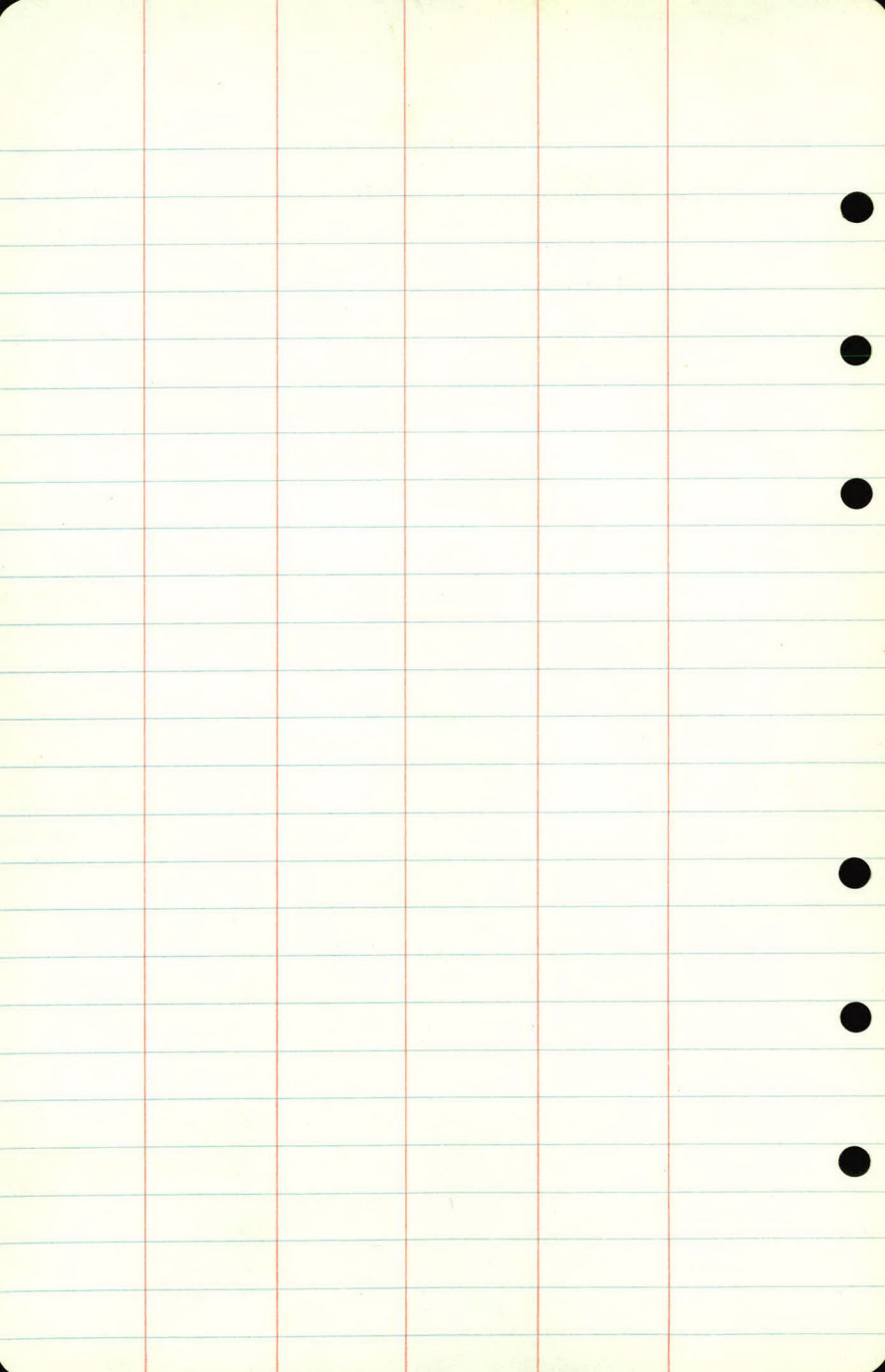
10.4

11.4
DC 1.0
25.0

10.7
DC 1.3
25.6

12.2
DC 0.2
25.4

4



8/26/39

Blue Tops

LARPEUR AVE.

MYRTLE AVE

800 EAST

S/a	t	π	-	Elev.	G.R.
B.M.	12.80	1015.25		1002.45	
	4.11	1019.36 ⁴	0.00	1015.25	
0				17.5	1.9
+50				16.5	2.9
1				16.0	3.4
+50				15.7	3.7
2				15.5	3.9
+50				15.2	4.2
3				15.0	4.4
+50				14.7	4.7
4				14.5	4.9
+50				14.2	5.2
5				14.0	5.4

L £ R

Top Mon. SW. Cor. Sta 16+46.

$$\frac{1.9}{15}$$

$$\frac{2.9}{15}$$

$$\frac{3.4}{15}$$

$$\frac{3.7}{15}$$

$$\frac{3.9}{15}$$

$$\frac{4.2}{15}$$

$$\frac{4.4}{15}$$

$$\frac{4.7}{15}$$

$$\frac{4.9}{15}$$

$$\frac{6.2}{15}$$

$$\frac{5.4}{15}$$

$$\frac{2.7}{15}$$

$$\frac{3.4}{15}$$

$$\frac{3.7}{15}$$

$$\frac{3.9}{15}$$

$$\frac{4.2}{15}$$

$$\frac{4.4}{15}$$

$$\frac{4.7}{15}$$

$$\frac{4.9}{15}$$

$$\frac{5.2}{15}$$

$$\frac{5.4}{15}$$

Sta	+	π	-	Elev.	G.R.
		1019.36 [↓]			

5+50				13.7	5.7
------	--	--	--	------	-----

6				13.5	5.9
---	--	--	--	------	-----

+50				13.2	6.2
-----	--	--	--	------	-----

+70				13.1	6.3
-----	--	--	--	------	-----

7				13.0	6.4
---	--	--	--	------	-----

+50				12.7	6.7
-----	--	--	--	------	-----

8				12.4	7.0
---	--	--	--	------	-----

$$\frac{5.7}{15}$$

$$\frac{5.7}{15}$$

$$\frac{5.9}{15}$$

$$\frac{5.9}{15}$$

$$\frac{6.2}{15}$$

$$\frac{6.2}{15}$$

$$\frac{6.4}{15}$$

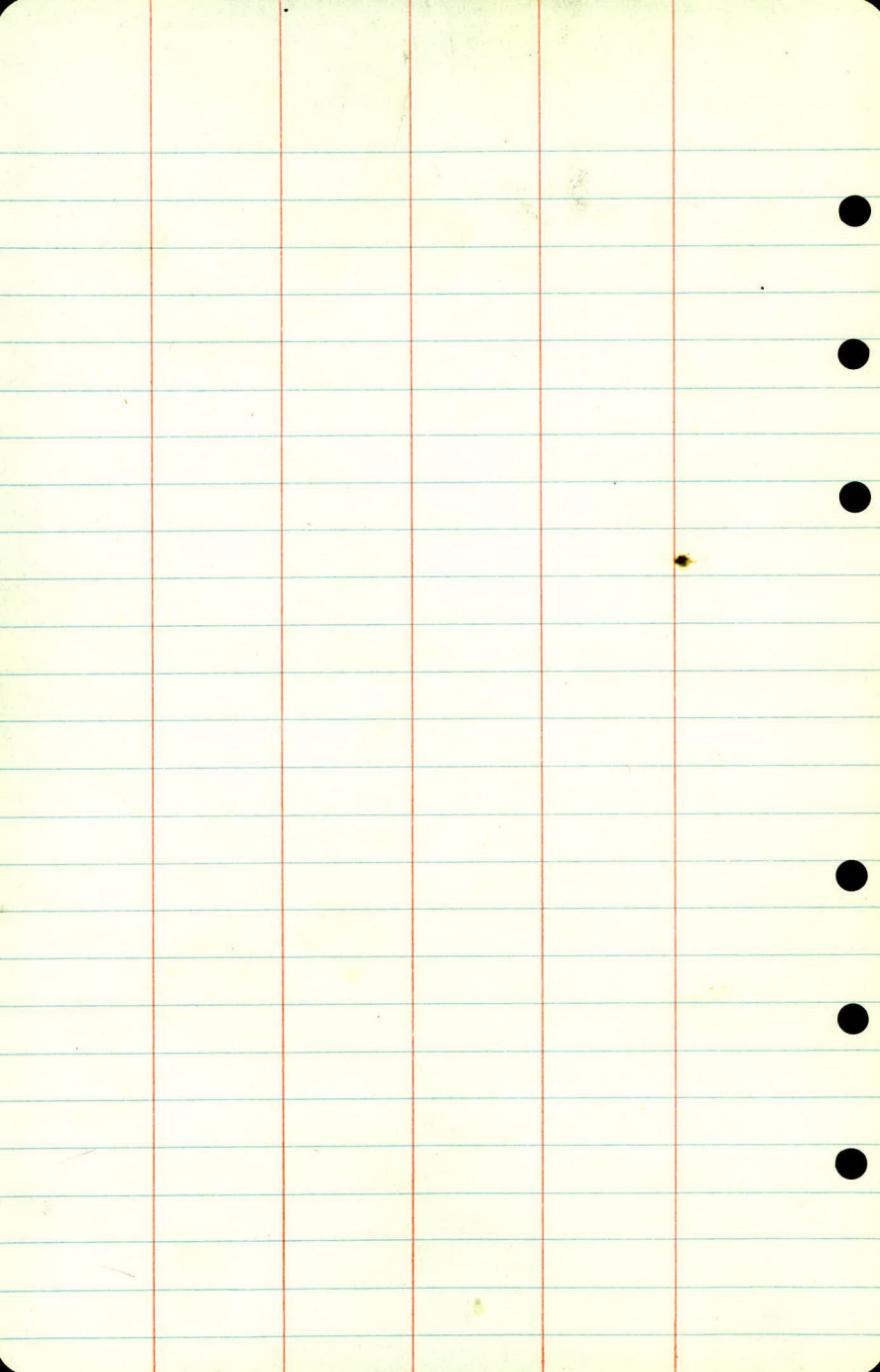
$$\frac{6.4}{15}$$

$$\frac{6.7}{15}$$

$$\frac{6.7}{15}$$

$$\frac{7.0}{15}$$

$$\frac{7.0}{15}$$



Larp. Ave.

Myrtle St. East

slope stakes rt. side

Sta.	+	π	-	Grade
B.M.	14.0	1016.95		(1002.45)
T.P.	9.95	1021.05	9.85	1011.60
1				16.0
	15.0			15.7
2				15.5
	15.0			15.3
3				15.0
	15.0			14.7
T.P.	3.64	918.56	6.13	914.92
4				14.5
	15.0			14.3
5				14.0
	15.0			13.7
6				13.5

Gr. Rod.

L.

Rt.

Top North. S.W. Cor. Sta. 16 + 46.7

51

 $\frac{21}{400/19.3}$

54

 $\frac{73}{401/23.2}$

56

 $\frac{17}{419/30.8}$

58

 $\frac{4.7}{41.1/29.2}$

61

 $\frac{46}{41.5/30.0}$

64

 $\frac{52}{41.2/28.4}$

71

 $\frac{61}{40.0/21.4}$

73

 $\frac{63}{40.0/19.0}$

76

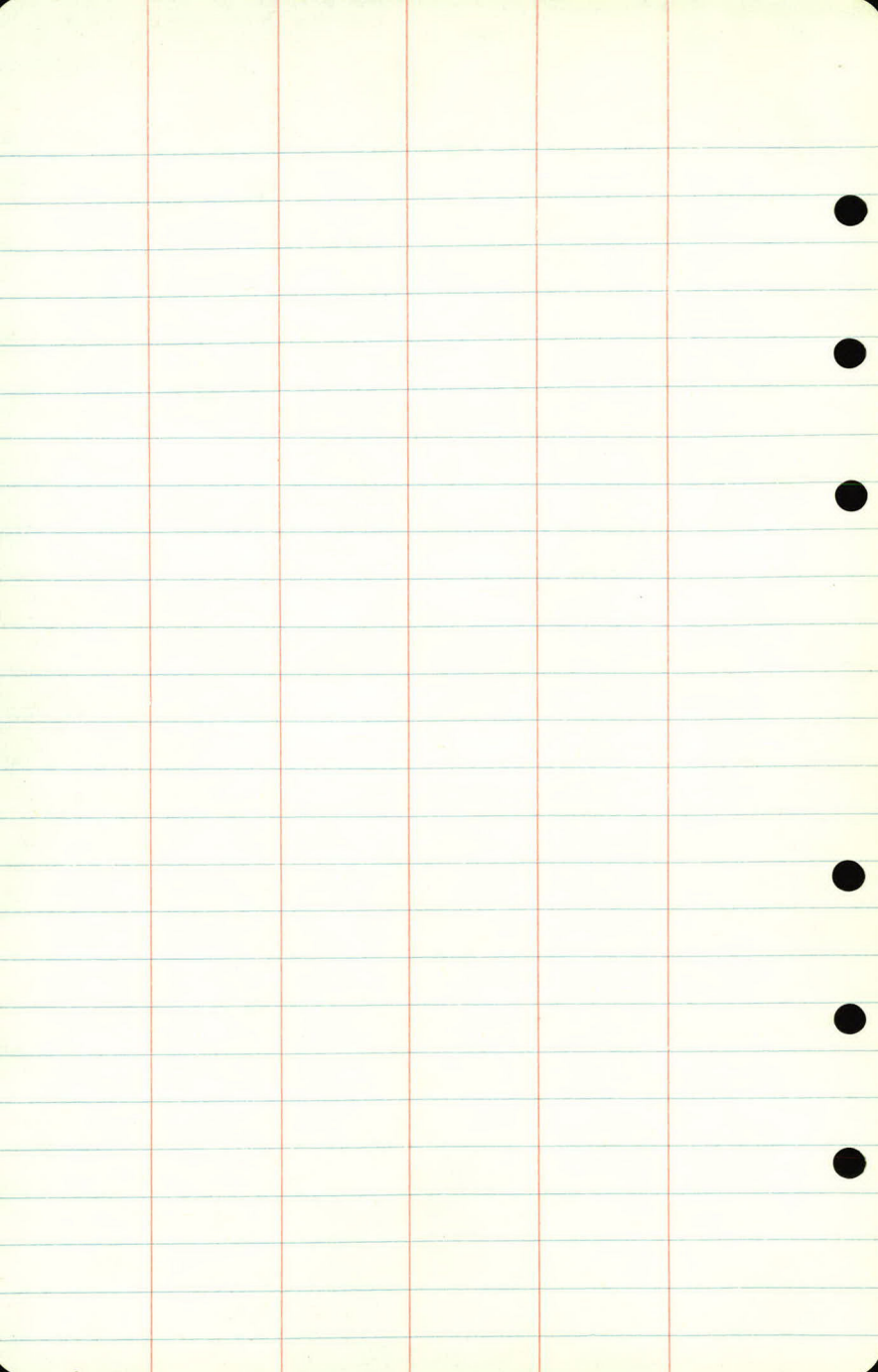
 $\frac{64}{38/18.6}$

79

 $\frac{63}{38.5/17.6}$

81

 $\frac{55}{38.7/16.4}$



Slope stakes

Larp Ave.

9100 to -

5th

+

T

-

E/CV

9 + 60

10

150

11

150

12

150

13

150

14

ξ = grade.

Lt.

ξ

Rt.

$$22.0 / \frac{67}{20.00}$$

$$\underline{49}$$

$$24.6 / \frac{59}{20.08}$$

$$\underline{47}$$

$$24.8 / \frac{60}{20.09}$$

$$\underline{49}$$

$$24.6 / \frac{65}{20.08}$$

$$\underline{53}$$

$$23.5 / \frac{81}{20.03}$$

$$\underline{69}$$

$$23.6 / \frac{94}{20.03}$$

$$\underline{77}$$

$$23.4 / \frac{106}{20.02}$$

$$\underline{88}$$

$$23.6 / \frac{118}{20.03}$$

$$\underline{101}$$

$$23.0 / \frac{136}{20.00}$$

$$\underline{116}$$

