

BK 25 - Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

CENTERVILLE RD.

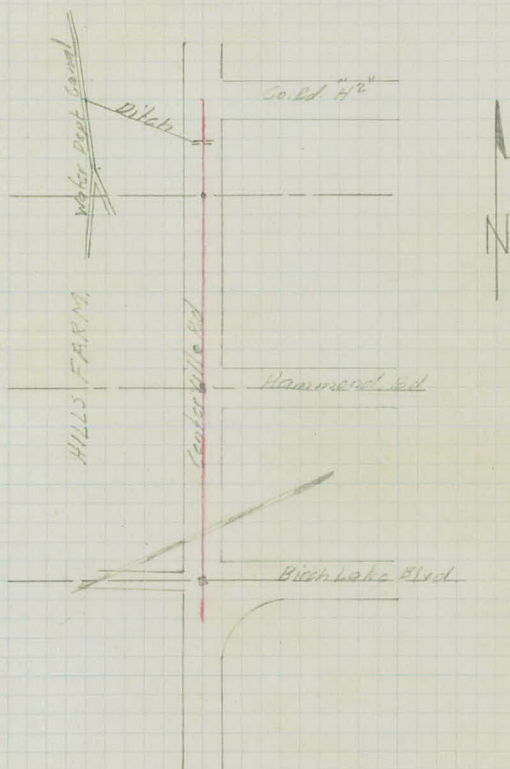
From Birch Lake Blvd N To Co. Rd. H²

Road Acc't. No. 2

Date Filed 10/39

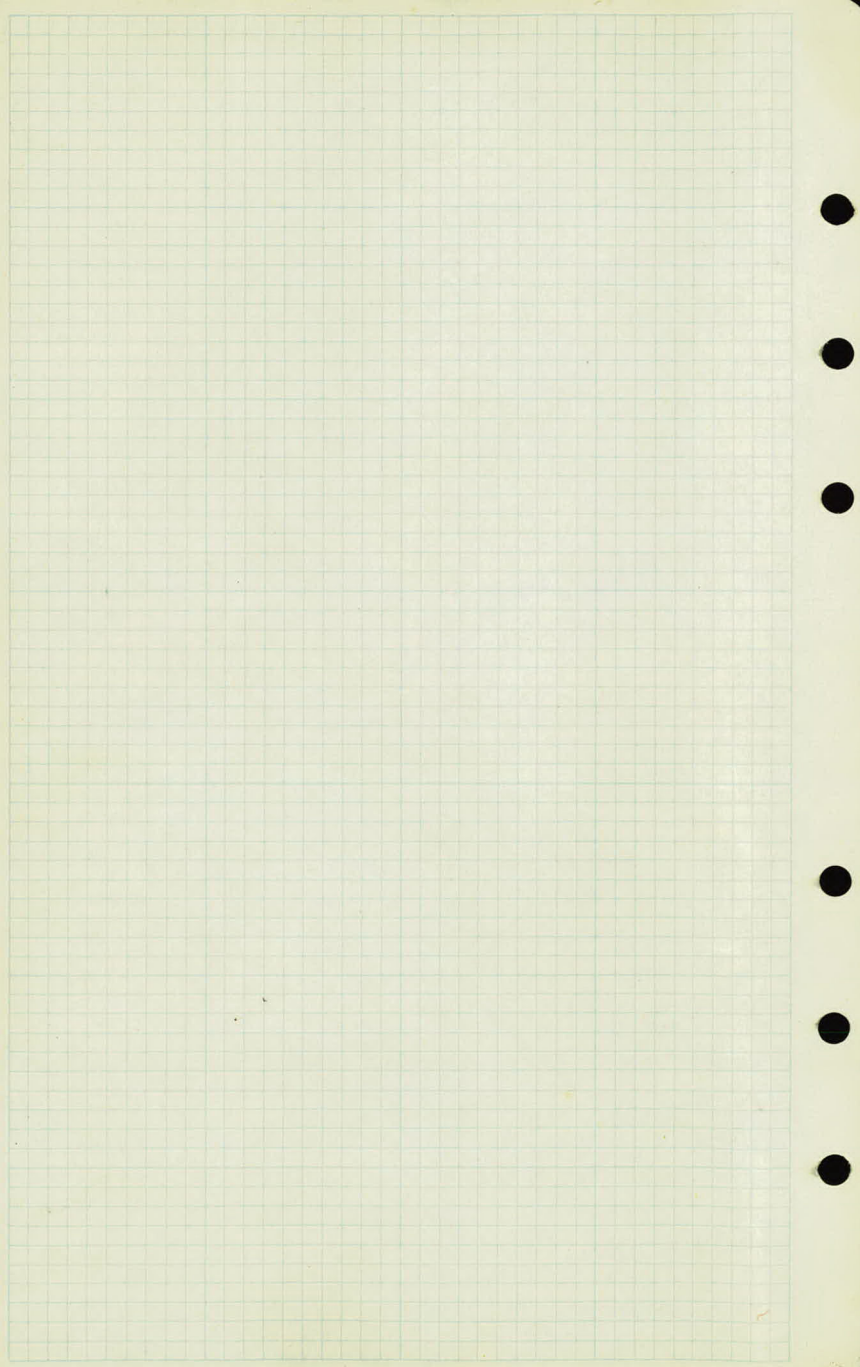
File

PLAN SURVEY
CENTERVILLE RD.
Birch Lake Blvd. to Gold H²



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Alignment

Sta.	Point	ΔL_t	ΔR_t
------	-------	--------------	--------------

26	+49.74	P.I.	$0^{\circ} 03 \frac{1}{2}'$
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3	+06.97	P.O.T.	
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0	+00		
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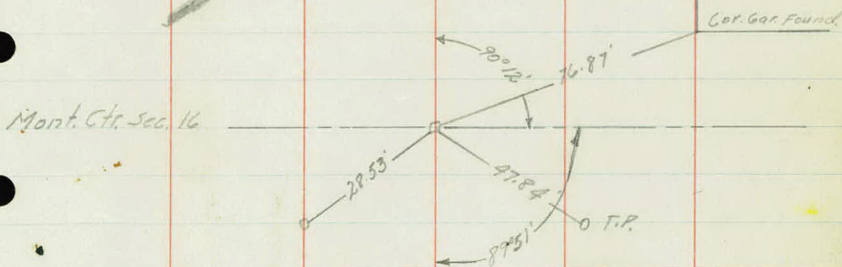
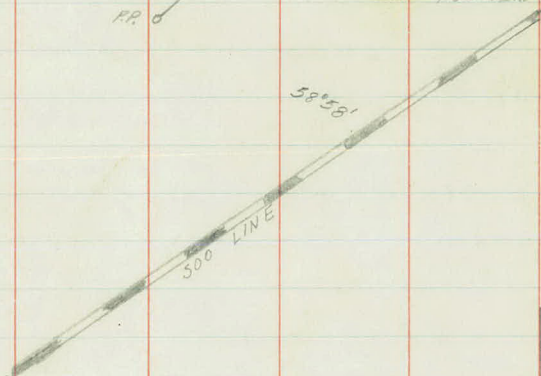
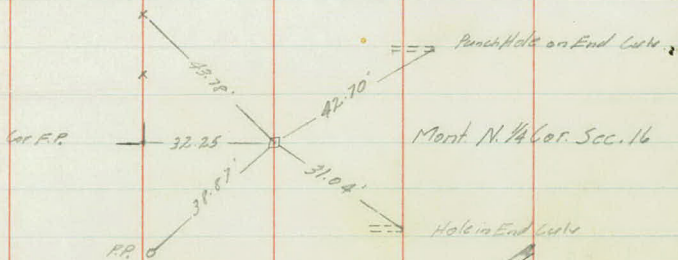
4/21/39

2

K.A.

L.B.H.

L.C.



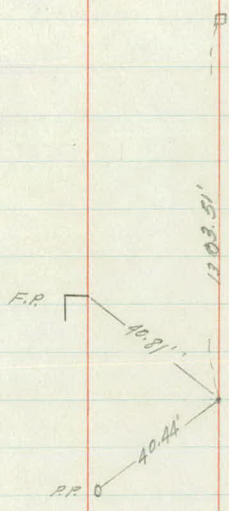
Sta	Point	$\Delta Lt.$	$\Delta Rt.$
-----	-------	--------------	--------------

66 +06.04 P.O.T. = 2 Co. Rd. H²"

52 +81.4

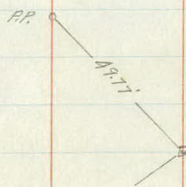
0° 10'

Iron N. 1/4 Cor Sec. 9



1303.51'

1325.6'

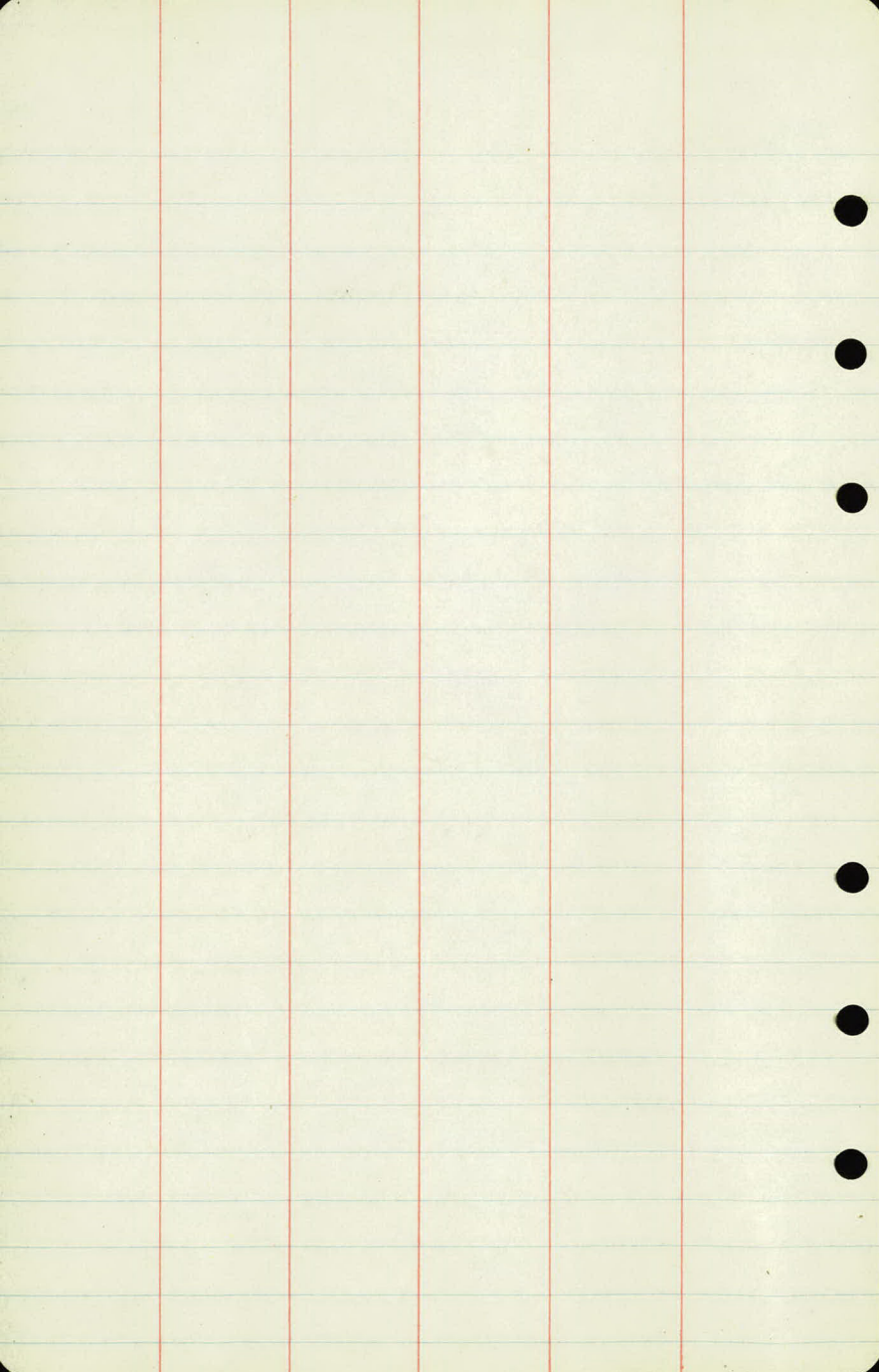


90°00'

Iron Chr. Sec. 9

Borrow Pit Align.

F.P.
Sch. in Conc.



topography

+72-P.P.-28'

+89-End Fe-11'
+77-Div Fe-19'
+69-Range Tr to Fe.

+44-Fe. Cor.-29'
+23-Beg. G.R.-10'

+33-Beg. G.R.-10'

3

8' 8'

+75-End G.R.-10'

+78-Electric Signal-13' 19' to G.R. Battery
+70-Tap 1-49' Fe-59' Box

+44-Tel. G.P.-28'
+38-Fe. Cor.-30'

+52-P.P.-20'
+13-Beg. Fe-39'
+08-End

2

8' 12'

+72-Beg. G.R.-10'
+71-Range Tr to Fe
+68-G.P.-19'
+62-P.P.-23'
+61-Fe. Cor.-28'
+47-G. Mount Fe-30'
+36-End Bow Tr.-21'

+63-T.P.-37'

1

8' 12'

+98-Beg. Now 5 Trs.-21'
+85-Row L. Hags-28'
+76-Killing Bush-26'
+75-L. O. Orchard-30'
+60-8' Maple-20'

+55-Cor. F. H. Sta.-47'
+47-Cor. F. H. Sta.-56'
+50-T.P.-33'
+35-Cor. G.R.-68'

+28-Cor. Orchard-34'
+01-End W. G. Rd.

6/00

-16-C. P. H. Sta.
-19-P.P.-23'
-20-G.R.-24'

-10-1. End of S. Tap
-22-P.P.-28'
-34-T.P.-32'

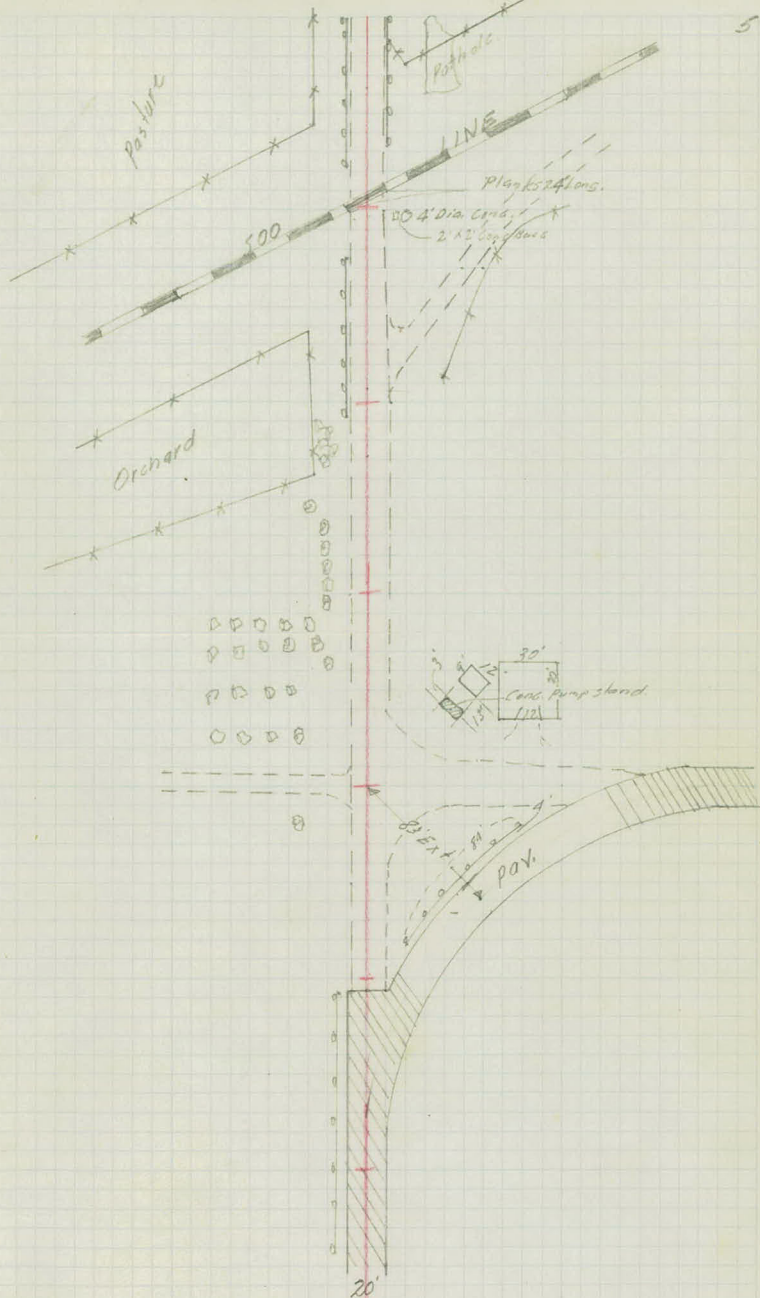
8' 12'

-83-Beg. G.R.-21'

-1/00

-08-End G.R.-14'

+055-End Rev



10 G.R.-9 8' 11' G.R.-11' F.C.-33'
+99-P.R.

9 F.C.-31' G.R.-10' 9' 10' G.R.-11' F.C.-
+89-Range Tie to Ditch
+82-Ditch

8 G.R.-10' 9' 9' G.R.-11'

+57-18" Fur. Oak Reg. F.C.-35'
+93-Deg. G.R.-12'

7 F.C.-31' G.R.-9'

8' 9'

+28-Eng. L. - 8" X 26' V.I. - 26'
+25-End G.R.
G.R.-10'

+77-P.R.-

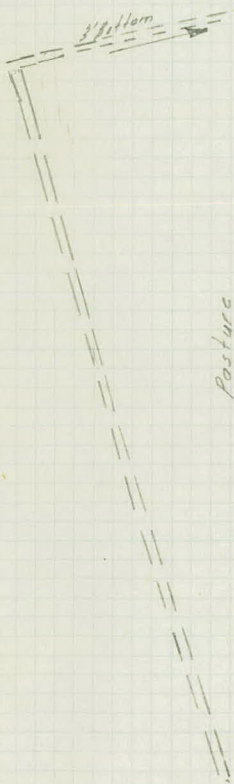
+61-F.C. Cor.-10'

6 9' 9'

5 F.C.-30' G.R.-10' 9' 9' G.R.-10'

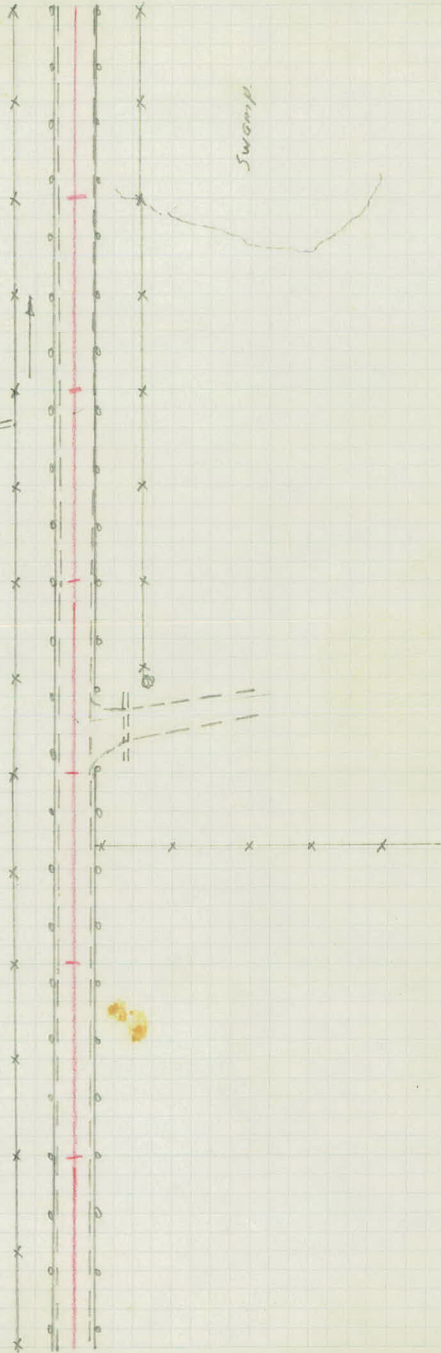
+75-Deg. Ditch - 75'

4 9' 9'



Posture

Swamp



17 G.R.-10' 8' 10' G.R.-12'

+39-PR-

16 G.R.-10' 8' 10' G.R.-12' PG-32'

+57-829 G.R.-

+85-End

+31-End G.R.-10'

15 G.R.-10' 8' 10' G.R.-12'

14 G.R.-10' 8' 9' G.R.-11'

+32-FC Cor-32'

+23-PR-28'

+30-FC Cor-33'

13 G.R.-10' 8' 10' G.R.-11'

+89-Group Whittiers-33'

+57-Group Whittiers

+31-Group Whittiers-33'

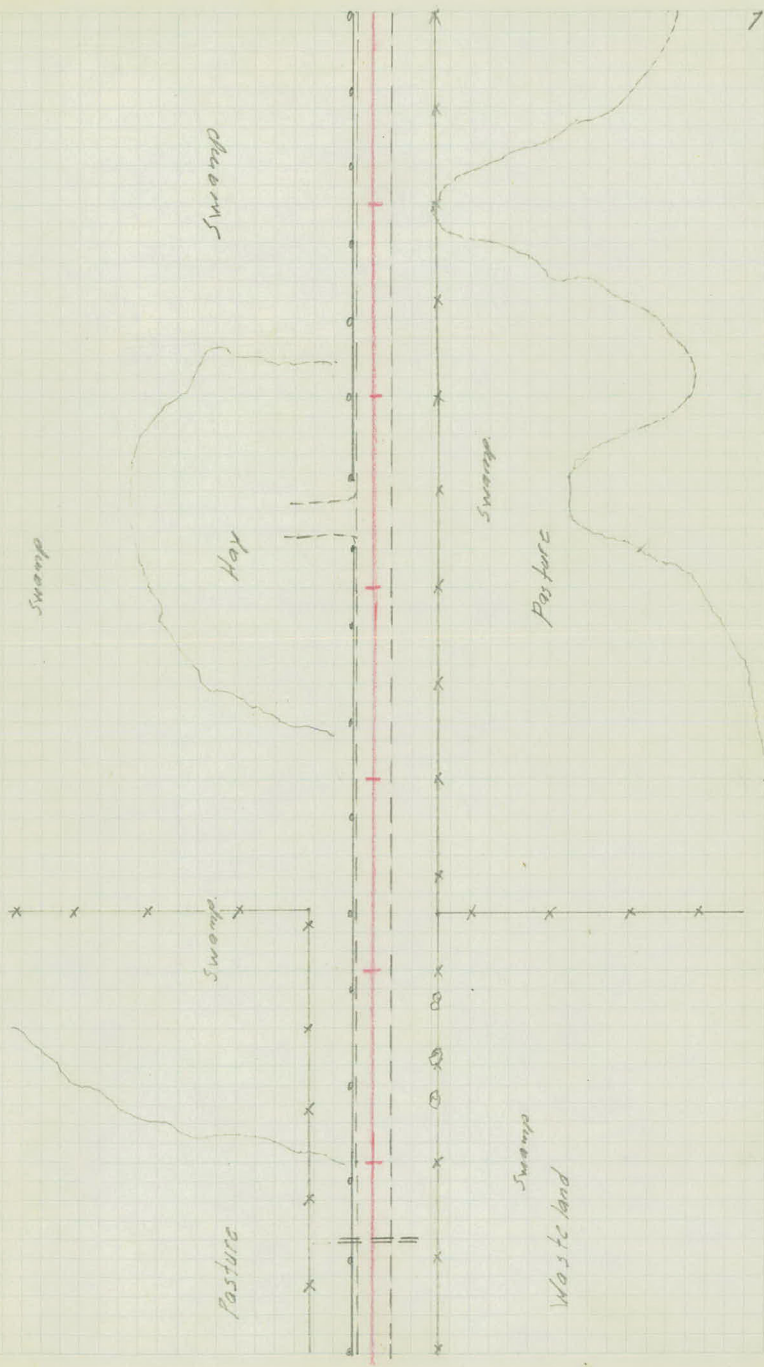
12 G.R.-10' 8' 9' G.R.-11'

+60-E 8" X 45' Vit-

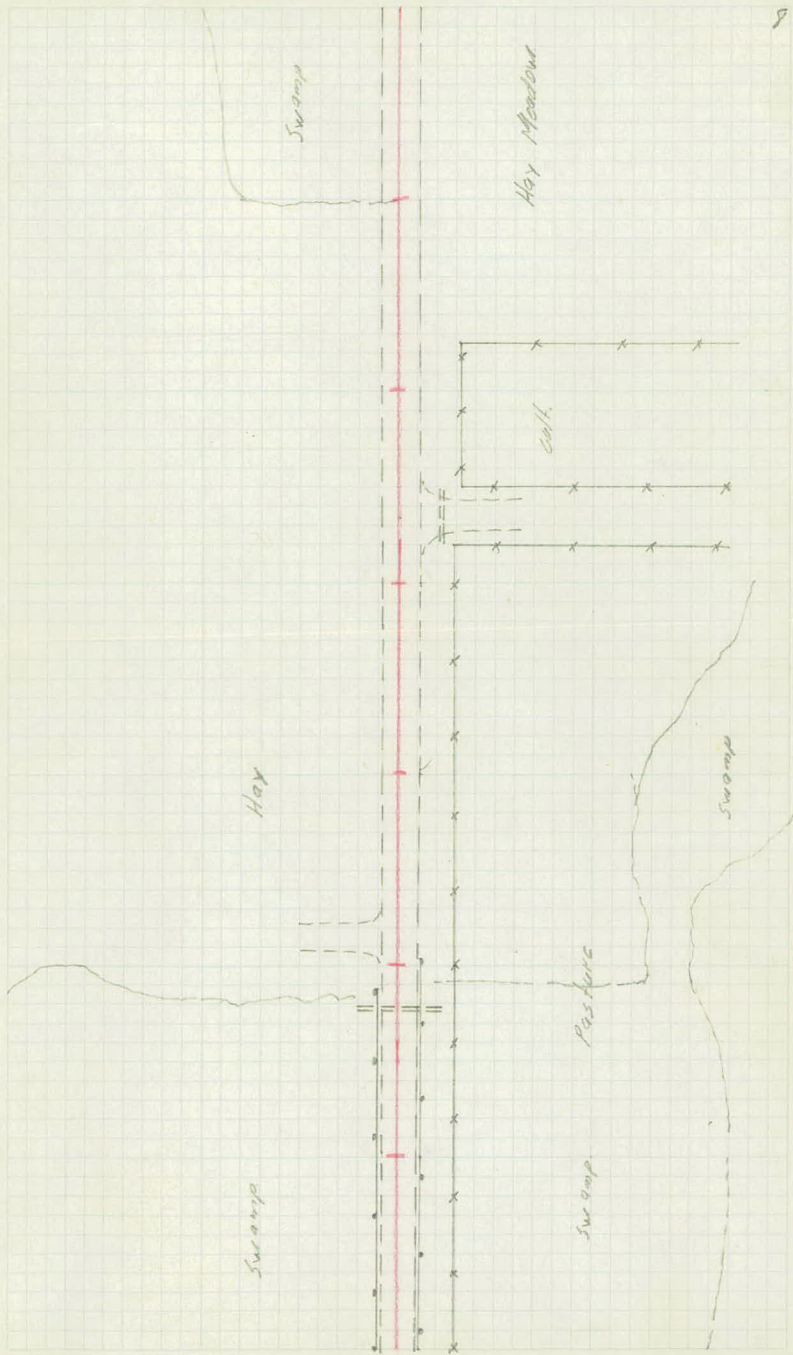
20'

23'

11 G.R.-9' 8' 10' G.R.-11'



24		9'	11'	
23	+95 P.P. - 28'	9'	11'	+86 - F.C. Cor. - 32'
22		8'	11'	+130 - F.C. Cor. - 32' +135 - End 1/2" X 12" C.V. - 2' +120 - F.C. Cor. - 29'
21		8'	11'	
20	+1/4 - Ent - +187 - End G.R. 10' +182 - End 3rd Amp. +175 - P.P. +163 - 12" X 44" Vit.	8'	10'	+103 - End G.R. - 12' F.C. - 30' +190 - End 3rd Amp.
19	G.R. - 10'	8'	10'	G.R. - 12'
18	G.R. - 10'	8'	10'	G.R. - 10'



31 Fe-31.9

11' 9'

30

11' 9'

+15-Fe. Cor. 22'
+22-Ent. 12'x26' ? - 20'

+64-PP-21'

+67-PP.

29

10' 9'

28 Fe-32.5

10' 9'

27

10' 9'

+67-6.5x1.30'x58' C.M.

19'

39'

+50-Fe. Cor. 32'

+50-6. Hammered Ed.

+47-Ent. 24' C.M. - 18'

+35-6. 24'x40' C.M. - Remova - Buried

+23-6. 30'x32' C.M. New

16'

16' 130-Ent. 24' C.M. - 18'

+22-PP-

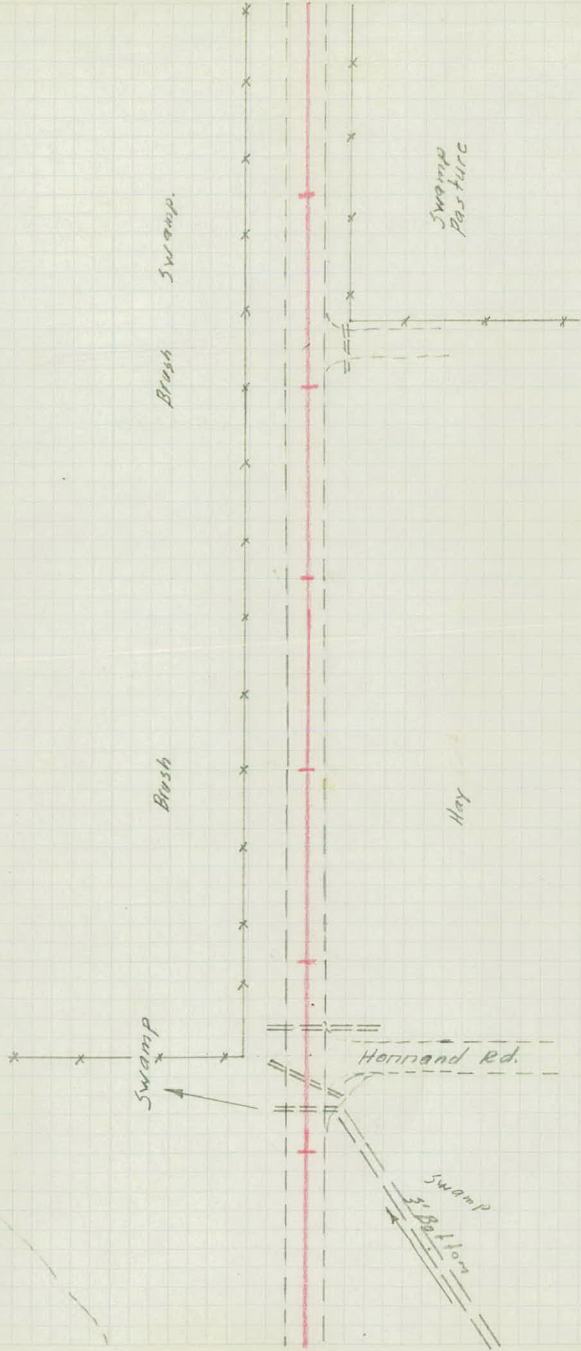
10' 10'

26

+50-PP-63'

25

9' 10'



38 Fe 30.0'

10' 9'

Fe-22'

37

10' 9'

+89-Group S-18" Willows-33'

+77-End 18" C.M. 18'

+79-4 18" X 35' C.M.

+72-Ranger TIC

+70-Fe Cor-21' +75-Ditch

+73-End 18" C.M.-17'

+44-24" Willows-36'

+26-24" Willows-38'

36 Fe 30.5'

10' 9'

35 Fe 31'

10' 10'

34

11' 10'

Fe-21'

33 +13-PP-25'

Fe-31.5'

11' 9'

32

11' 9'

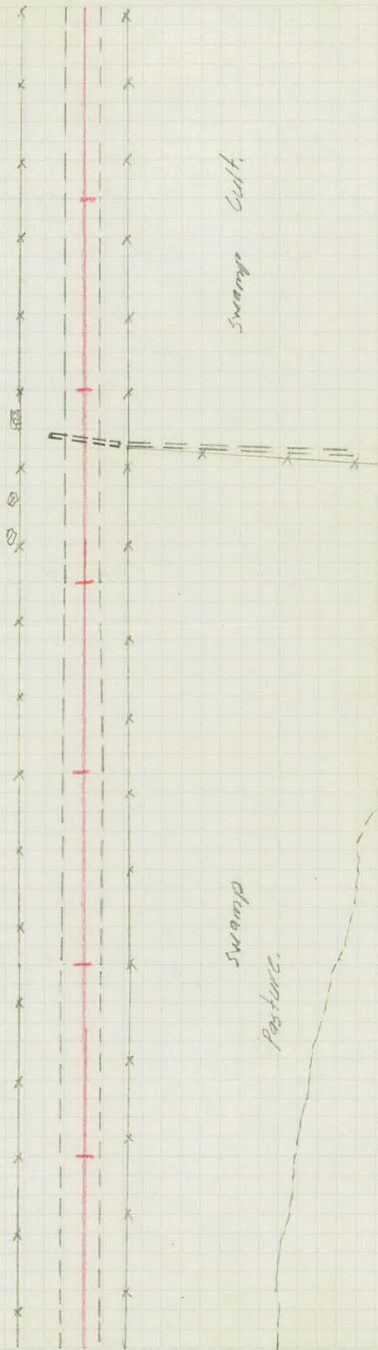
Fe-21'

Swamp
Brush

Swamp
Cult.

Swamp
Brush

Swamp
Pasture.



45 Fc-32.9'

10' 8'

+37-Bos. G.R.-10'

44 +17-Bos. G.R.-12'

10' 8'

+50-P.P.-28'

43 Fc-32.6'

10' 8'

+10-End G.R.-11'

+57-End G.R.-11'

42

9' 9'

+98-36" Willow-36'

41 Fc-31.5'

8' 9'

+67-Bos G.R.-11'

G.R.-11'

40 +06-P.P.
Fc-30.8'

9' 9'

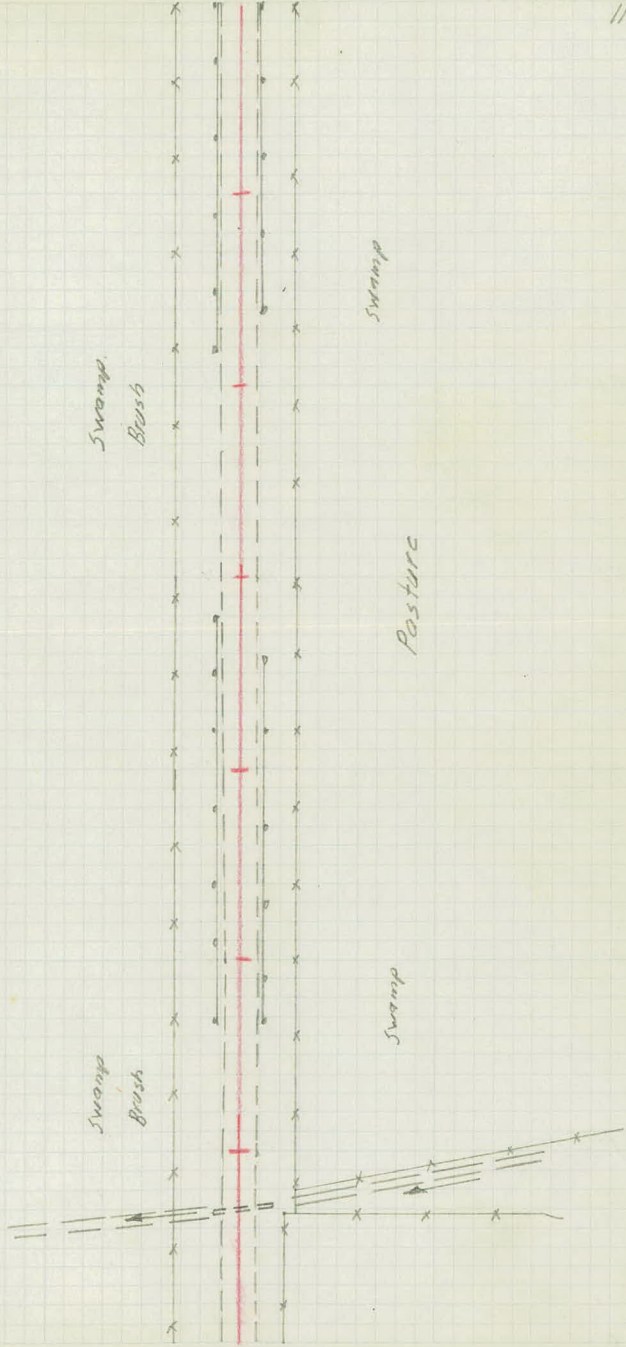
+48-End ^{24"} 36" G.R.-14'

^{24"} 36" 120' M.

+80-Fc Cor-28' pitch
+79-End of 1st Fc
+71-End 30' M. 16'
+61-Fc Cor-22'
+50-Ent

39

10' 9'



#15-End Swamp

52

10' 9'

#65-End Swamp-

51 FC-22.9'

10' 9'

+6

50

+08-PP-29'

10' 9'

49 End G.R.-11' FC-22.9' 9' 8' +02-End G.R.-10'

48

10' 8'

+20-Bos G.R.-11'

47 FC-33.6'

+18-PP-

10' 8'

+23-Bos. G.R.-10'

+03-Ent. 12' X 16' G.M.-19'

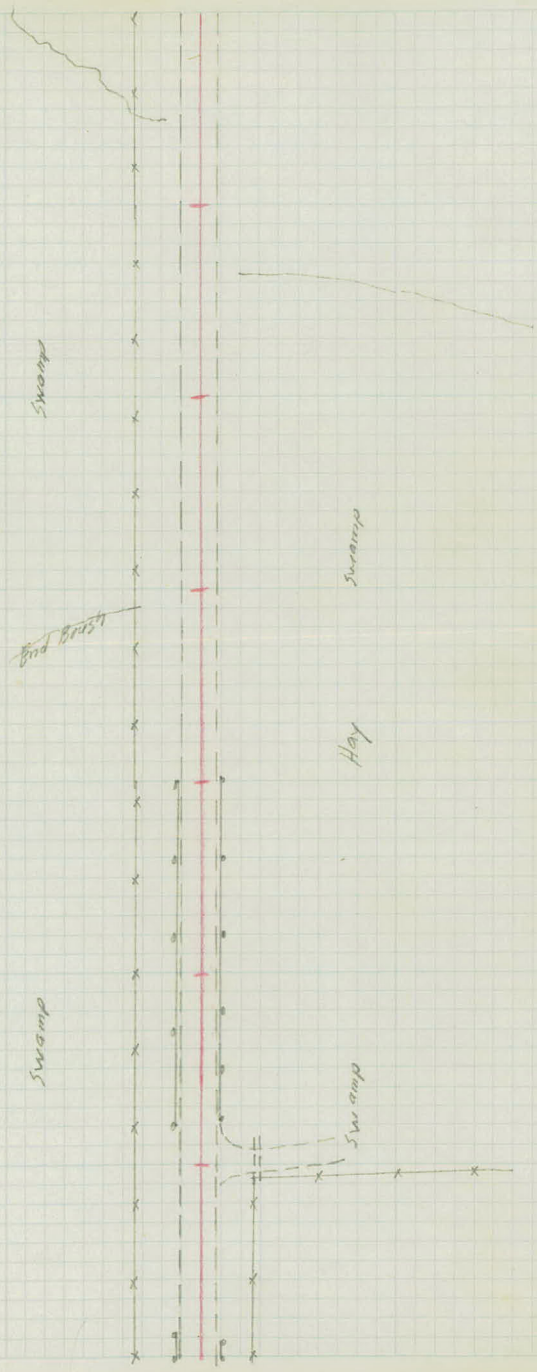
+29-FC GOK-26'
+91-Rising CTIC

46

+14-End G.R.-12'

10' 8'

+08-End G.R.-10'



+90-Range Tie to D/H/6/6

+48-PP-

59 195-Res. G.R.-12' 9' 11' 182-Fc. Cor.-50'
181-Res. G.R.-12'

+54-Range Tie

58 10' 9'

57 Fe-37.0' 10' 9'

+36-PP-29'

56 Fe-33' 10' 9'

55 Res. Brush Fe-33.0' 10' 9' 190-Res. Swamp

54 10' 8'

+22-PP-29'

53 Fe.-13.0' 10' 10'

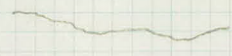
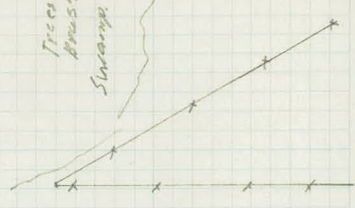
Swamp
Brush

Brush

Swamp

Trees &
Brush
Swamp

Hog Meadow
Swamp



12' 8'

9' 170

180

66 FC-35'

11'

107-Approx. 8' H²⁰

181-P.R.-31'

10' 150

65 FC-35.3'

10' 9'

64 FC-35.7'

10' 9'

180-End G.R.-12'

+41-End Fc.-13'

+37-End G.R.-12'

63 FC-35.7' G.R.-12'

10' 10'

G.R.-12'

164-P.P.-30'

+78-Δ 14 FC-72'

62 -FC-35.0'

9' 11'

+21-End 3' incamp

61 FC-34.5'

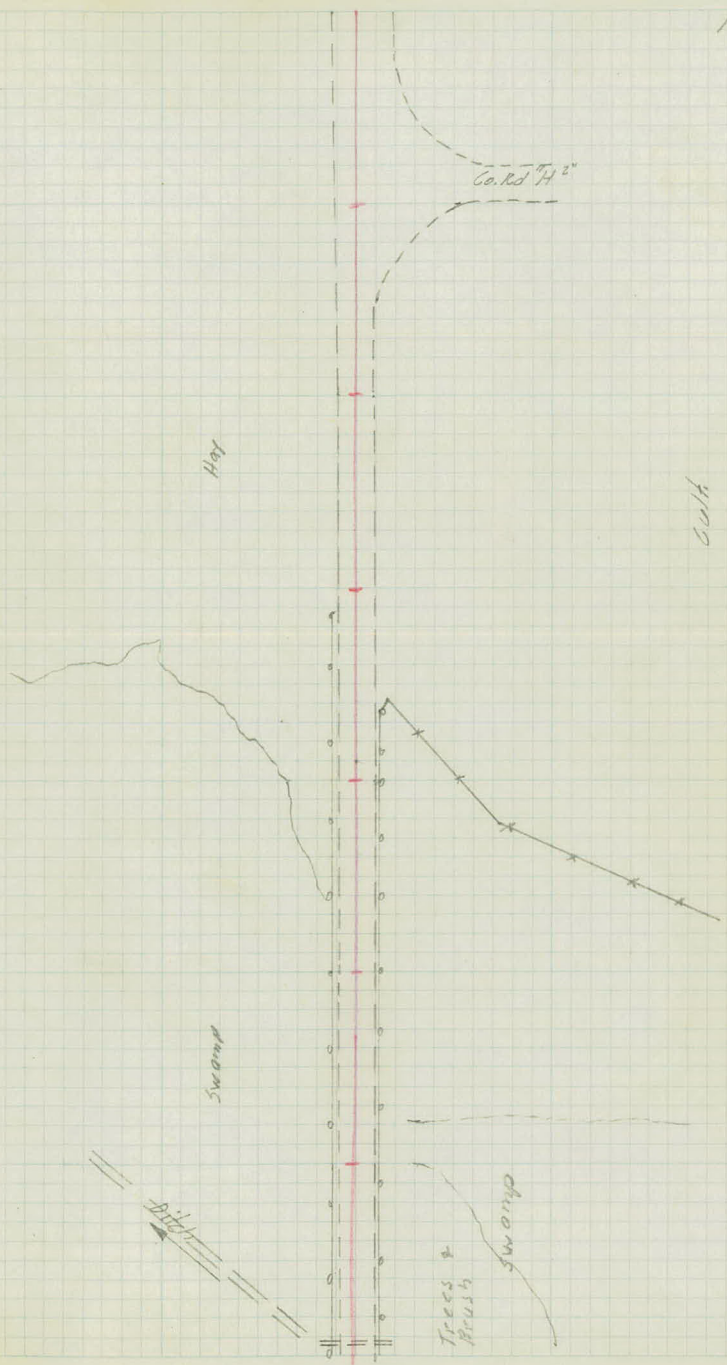
End Brush G.R.-12'

9' 11'

G.R.-12'

60 108-P. Gully 24' X 38' C.M.

19' 19'





Bench Levels

Sta	+	-	Elev.
B.M.	0.20	950.11.	(949.91)
T.P.	0.26	936.88	13.49 936.62
T.P.	0.57	923.87	13.58 923.30
T.P.	4.46	915.20	13.13 910.74
T.P.	4.99	914.86	5.33 909.57
T.P.	2.54	910.88	6.52 908.34
B.M.	4.52	908.85	6.55 904.33
T.P.	4.90	907.47	6.28 902.57
T.P.	6.97	902.23	6.21 901.26
T.P.	40.9	905.48	6.84 901.39
		908.75	No 912
		909.75	OK 4.62
		912.20	901.56
		915.20	907.59
B.M.	4.61	908.74	908.59
		908.74	905.75
T.P.	2.99	908.74	6.45 906.75
		920.38	907.35
T.P.	13.03	921.38	1.39 928.35
		931.06	920.08
T.P.	12.98	922.06	0.30 927.08
			928.10
B.M.			2.96 929.10

Red changes = Corrections done in office
At the time job was drawn up.

Green changes were made Sept 30, 1940
one Foot Error in laterals & Cross sections.
Note - Elev. 928.10 Centerville Rd =
Elev 929.10 Car Rd. H²

Description

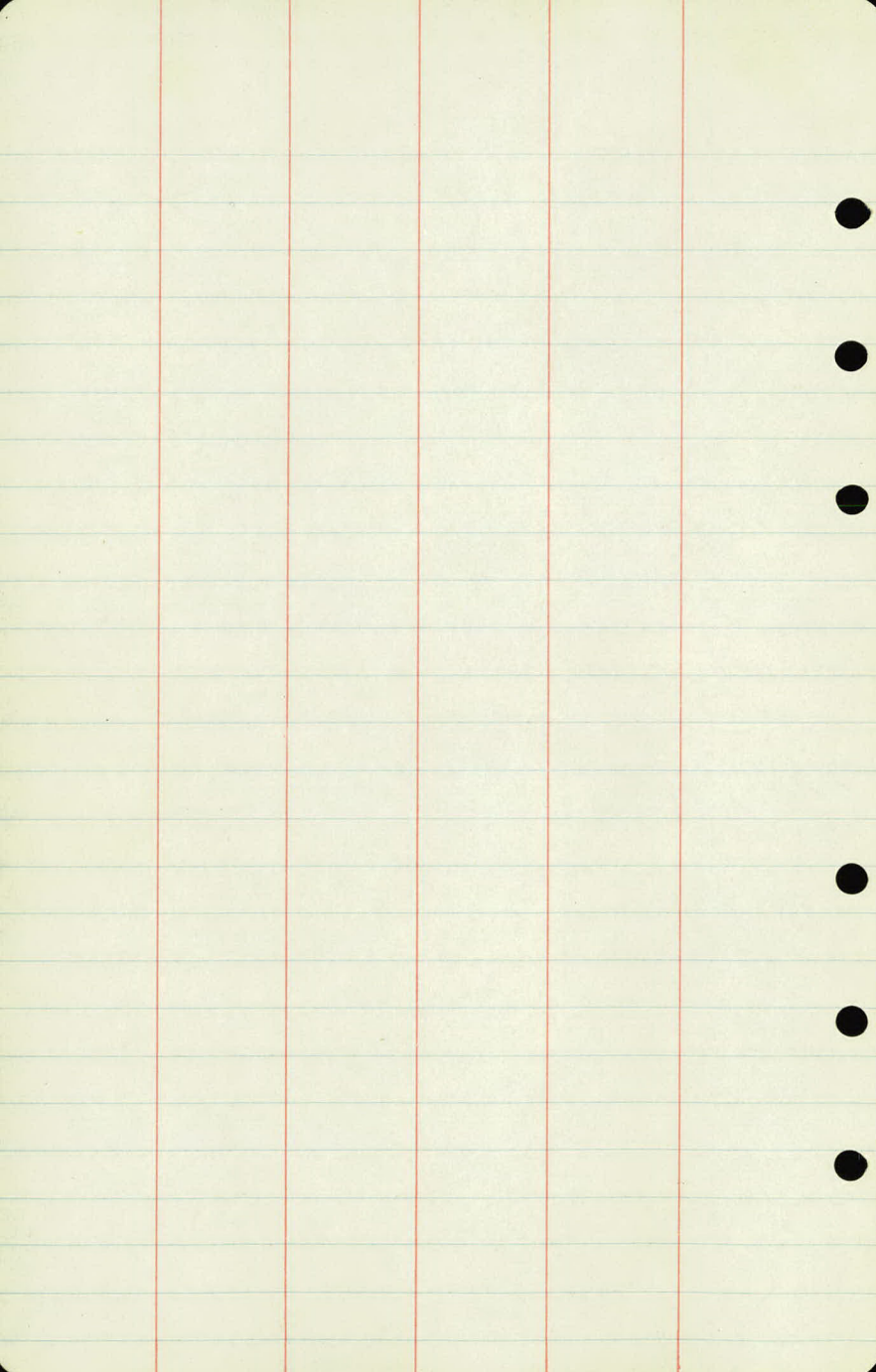
Top Mont. Birch Lake Blvd. N. + Centerville Rd

Top S. End 30' G. M. C. L. 39' Rt. 3/4 26 + 27

Top of Conc. at Base of D. Iron F. Post 33' Lt. 52 + 65

Spike in P.P. Lt. Sta. 65 + 80

These levels are .11' higher than
U.S.G.S. datum.
chk. by L. A. 3-21-45



X Sections

Sta	+	π	-	Elev
B.M.	5.29	955.20		949.91
-34 00			0.18	955.02
+50			1.14	54.06
-7			2.19	53.01
+50			2.60	52.60
-1 +05.5				52.7
- 0 +50				50.7
- 0 +12				50.1
0 +00				50.0
+33				49.4
+64				48.9
+76				48.6

LT

R

RT

Top Mont. Birch Lake Blvd. N + Centerville Rd.

$$\frac{110}{50} \quad \frac{104}{35} \quad \frac{83}{23} \quad \frac{28}{10} \quad \frac{285}{10} \quad \frac{250}{10} \quad \frac{2.54}{10}$$

$$\frac{93}{50} \quad \frac{86}{32} \quad \frac{75}{17} \quad \frac{50}{10}$$

$$\frac{45}{11} \quad \frac{49}{15} \quad \frac{51}{17} \quad \frac{63}{32} \quad \frac{60}{44} \quad \frac{2.0}{44} \quad \frac{2.15}{52.7} \text{ per.}$$

$$\frac{60}{50} \quad \frac{59}{20} \quad \frac{54}{8} \quad \frac{51}{11} \quad \frac{5.1}{43} \quad \frac{46}{78} \quad \frac{2.3}{107.4} \text{ per.}$$

$$\frac{55}{50} \quad \frac{56}{25} \quad \frac{55}{8} \quad \frac{52}{12} \quad \frac{52}{50} \quad \frac{3.6}{100} \quad \frac{1.4}{139.2} \text{ per.}$$

$$\frac{4.6}{50} \quad \frac{52}{20} \quad \frac{6.2}{15} \quad \frac{6.1}{9} \quad \frac{5.8}{11} \quad \frac{6.0}{20} \quad \frac{6.2}{24} \quad \frac{5.5}{50} \quad \frac{40}{69} \quad \frac{3.0}{89} \quad \frac{2.1}{100} \quad \frac{2.0}{100} \quad \left(\frac{2.16}{\text{El. Cons. Floor}} \right)$$

$$\frac{4.6}{50} \quad \frac{52}{20} \quad \frac{6.8}{16} \quad \frac{6.9}{8} \quad \frac{6.3}{11} \quad \frac{6.6}{16} \quad \frac{6.7}{30} \quad \frac{5.5}{50} \quad \frac{3.4}{50}$$

$$\frac{49}{50} \quad \frac{50}{29} \quad \frac{50}{21} \quad \frac{70}{16} \quad \frac{6.6}{8} \quad \frac{6.1}{11} \quad \frac{6.8}{17} \quad \frac{7.3}{18} \quad \frac{6.3}{22} \quad \frac{4.8}{28} \quad \frac{3.1}{30} \quad \frac{2.5}{50}$$

Sta	T	π	-	Elcr.
		955.20		
1			48.2	
	+30		47.4	
	+58		46.7	
T.R	0.75	946.49	9.46	945.24
2			45.7	
	+20		45.3	
	+39		45.1	
	+63		44.5	
	+81		44.2	
3	+09.1		44.06	
	+09.8		43.06	
	+22		43.4	

Lt

K

Rt

$$\begin{array}{r} 64 \ 57 \ 60 \ 77 \ 77 \ 73 \ 72 \ 70 \ 73 \ 77 \ 79 \ 27 \ 16 \\ 50 \ 29 \ 20 \ 15 \ 13 \ 11 \ 8 \ 11 \ 13 \ 23 \ 30 \ 50 \end{array}$$

$$\begin{array}{r} 92 \ 83 \ 71 \ 87 \ 82 \ 79 \ 75 \ 80 \ 82 \ 85 \ 16 \ 12 \\ 50 \ 34 \ 20 \ 16 \ 12 \ 8 \ 11 \ 17 \ 22 \ 34 \ 50 \end{array}$$

$$\begin{array}{r} 120 \ 104 \ 92 \ 87 \ 85 \ 87 \ 88 \ 92 \ 91 \ 75 \ 23 \ 23 \\ 50 \ 37 \ 18 \ 9 \ 11 \ 16 \ 18 \ 24 \ 29 \ 37 \ 50 \end{array}$$

$$\begin{array}{r} 77 \ 42 \ 25 \ 12 \ 10 \ 98 \ 10 \ 14 \ 12 \ 05 \ 04 \ 133 \\ 50 \ 28 \ 14 \ 9 \ 7 \ 11 \ 13 \ 27 \ 21 \ 37 \ 48 \end{array}$$

$$\begin{array}{r} 123 \ 86 \ 65 \ 52 \ 15 \ 12 \ 13 \ 17 \ 18 \ 12 \ 13 \ 127 \\ 50 \ 41 \ 28 \ 18 \ 9 \ 11 \ 13 \ 29 \ 32 \ 42 \ 50 \end{array}$$

$$\begin{array}{r} 143 \ 130 \ 114 \ 18 \ 14 \ 16 \ 29 \ 25 \ 23 \ 20 \ 00 \\ 50 \ 31 \ 23 \ 9 \ 11 \ 14 \ 20 \ 34 \ 46 \ 50 \end{array}$$

$$\begin{array}{r} 64 \ 116 \ 114 \ 25 \ 22 \ 20 \ 22 \ 33 \ 40 \ 38 \ 31 \ 31 \\ 50 \ 34 \ 24 \ 10 \ 8 \ 10 \ 13 \ 20 \ 29 \ 32 \ 50 \end{array}$$

$$\begin{array}{r} 30 \ 30 \ 33 \ 33 \ 24 \ 23 \ 24 \ 36 \ 40 \ 35 \\ 50 \ 39 \ 34 \ 18 \ 8 \ 10 \ 13 \ 46 \ 50 \end{array}$$

Mud Top Rail

$$\begin{array}{r} 73 \ 33 \ 30 \ 26 \ 243 \ 24 \ 40 \ 44 \ 40 \ 35 \\ 50 \ 30 \ 18 \ 12 \ 8 \ 15 \ 35 \ 40 \ 50 \end{array}$$

Top Rail / Mud

$$\begin{array}{r} 120 \ 27 \ 32 \ 26 \ 243 \ 25 \ 30 \ 30 \ 46 \ 41 \ 38 \\ 50 \ 23 \ 14 \ 8 \ 9 \ 10 \ 19 \ 33 \ 40 \ 50 \end{array}$$

$$\begin{array}{r} 14 \ 33 \ 31 \ 33 \ 30 \ 30 \ 39 \ 40 \\ 15 \ 9 \ 8 \ 19 \ 35 \ 45 \ 60 \end{array}$$

Sta.	+	π	-	Elev
		746.49		
3	+31		42.7	
	+63		40.7	
4			38.5	
	+50		36.0	
5			34.2	
I.P.	0.99	935.18	12.30	924.19
3	+32		43.6	
	+31		42.7	
	+63		40.7	
4			38.5	
	+50		36.0	
5			34.2	

Lt

C

Rt

$$\frac{46}{14} \quad \frac{38}{9} \quad \frac{38}{9} \quad \frac{37}{9} \quad \frac{28}{19} \quad \frac{30}{33} \quad \frac{30}{50}$$

$$\frac{58}{15} \quad \frac{59}{9} \quad \frac{58}{9} \quad \frac{60}{9} \quad \frac{63}{15}$$

$$\frac{91}{14} \quad \frac{82}{9} \quad \frac{80}{10} \quad \frac{80}{10} \quad \frac{95}{16}$$

$$\frac{112}{15} \quad \frac{107}{9} \quad \frac{105}{9} \quad \frac{106}{9} \quad \frac{114}{16}$$

$$\frac{128}{14} \quad \frac{124}{9} \quad \frac{123}{10} \quad \frac{123}{10} \quad \frac{128}{16}$$

$$\frac{68}{50} \quad \frac{56}{35}$$

+8.2

$$\frac{73}{50} \quad \frac{73}{35}$$

+7.5

$$\frac{84}{50} \quad \frac{85}{35} \quad \frac{70}{30}$$

+5.5

$$\frac{63}{35} \quad \frac{63}{45} \quad \frac{20}{50}$$

$$\frac{99}{50} \quad \frac{107}{47} \quad \frac{103}{39} \quad \frac{92}{31}$$

+3.3

$$\frac{86}{31} \quad \frac{70}{50}$$

$$\frac{120}{50} \quad \frac{120}{45} \quad \frac{113}{31}$$

+0.8

$$\frac{100}{28} \quad \frac{91}{50}$$

$$\frac{121}{50} \quad \frac{115}{39} \quad \frac{107}{30}$$

-1.0

$$\frac{75}{25} \quad \frac{73}{32} \quad \frac{61}{37} \quad \frac{51}{50}$$

34. + π - E/cv

935.18 .

5 + 40

32.7 .

6

29.9 .

+50

27.9 .

7

26.4 .

T.P.

3.81

926.41

12.58

22.26 .

7.1

19.3 .

7.15

19.26 .

+50

24.7 .

8

22.6 .

+50

20.4 .

9

18.4 .

T.P.

0.74

919.21

7.94

918.47 .

+50

16.8 .

Lt.

K.

Rt.

$\frac{110}{50}$	$\frac{105}{36}$	$\frac{92}{27}$	$\frac{73}{17}$	$\frac{27}{9}$	$\frac{25}{9}$	$\frac{26}{10}$	$\frac{96}{14}$	$\frac{68}{20}$	$\frac{71}{31}$	$\frac{60}{50}$
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$\frac{147}{50}$	$\frac{140}{30}$	$\frac{58}{15}$	$\frac{55}{8}$	$\frac{53}{9}$	$\frac{55}{21}$	$\frac{12.3}{32}$	$\frac{11.7}{50}$	$\frac{99}{50}$
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$\frac{181}{50}$	$\frac{180}{41}$	$\frac{156}{24}$	$\frac{75}{11}$	$\frac{73}{10}$	$\frac{75}{21}$	$\frac{144}{35}$	$\frac{146}{50}$	$\frac{133}{50}$
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$\frac{16.8}{30}$	$\frac{173}{31}$	$\frac{176}{24}$	$\frac{93}{12}$	$\frac{90}{8}$	$\frac{88}{9}$	$\frac{90}{11}$	$\frac{95}{20}$	$\frac{15.3}{39}$	$\frac{15.3}{50}$	$\frac{149}{50}$
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K. 514.8100

S. End Ent. Calc.

N. End Ent. Calc.

$\frac{84}{50}$	$\frac{90}{31}$	$\frac{82}{23}$	$\frac{2.8}{14}$	$\frac{2.0}{8}$	$\frac{17}{9}$	$\frac{19}{17}$	$\frac{30}{24}$	$\frac{70}{27}$	$\frac{6.9}{29}$	$\frac{54}{50}$	$\frac{6.8}{50}$
-----------------	-----------------	-----------------	------------------	-----------------	----------------	-----------------	-----------------	-----------------	------------------	-----------------	------------------

$\frac{93}{50}$	$\frac{99}{31}$	$\frac{104}{28}$	$\frac{100}{23}$	$\frac{44}{13}$	$\frac{40}{8}$	$\frac{38}{9}$	$\frac{39}{15}$	$\frac{5.2}{21}$	$\frac{86}{26}$	$\frac{9.3}{29}$	$\frac{8.3}{31}$	$\frac{74}{50}$	$\frac{8.3}{50}$
-----------------	-----------------	------------------	------------------	-----------------	----------------	----------------	-----------------	------------------	-----------------	------------------	------------------	-----------------	------------------

$\frac{101}{50}$	$\frac{107}{31}$	$\frac{117}{27}$	$\frac{117}{22}$	$\frac{70}{13}$	$\frac{6.2}{8}$	$\frac{60}{9}$	$\frac{6.2}{9}$	$\frac{74}{13}$	$\frac{121}{23}$	$\frac{121}{28}$	$\frac{102}{33}$	$\frac{112}{50}$
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$\frac{104}{50}$	$\frac{115}{31}$	$\frac{130}{28}$	$\frac{132}{20}$	$\frac{9.3}{13}$	$\frac{8.2}{9}$	$\frac{80}{9}$	$\frac{80}{13}$	$\frac{9.3}{18}$	$\frac{118}{22}$	$\frac{147}{30}$	$\frac{148}{34}$	$\frac{12.8}{50}$	$\frac{133}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	----------------	-----------------	------------------	------------------	------------------	------------------	-------------------	------------------

$\frac{35}{50}$	$\frac{40}{34}$	$\frac{75}{30}$	$\frac{89}{23}$	$\frac{79}{21}$	$\frac{33}{14}$	$\frac{26}{9}$	$\frac{24}{10}$	$\frac{26}{13}$	$\frac{35}{21}$	$\frac{9.2}{29}$	$\frac{9.7}{32}$	$\frac{76}{50}$	$\frac{86}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	------------------	------------------	-----------------	-----------------

Sta.	+	π	-	Elev
		919.21		
10	+00			15.4
	+50			14.3
11				13.0
	+50			11.8
12				10.7
T.P.	4.38	915.08	851	910.70
11	+60	4. Calv.		
12	+50			09.5
13				09.4
	+50			10.0
14				10.2
	+50			10.3

41

2

21

$$\frac{49}{50} \frac{58}{35} \frac{71}{31} \frac{93}{29} \frac{99}{21} \frac{52}{14} \frac{40}{9} \frac{38}{9} \frac{40}{9} \frac{50}{12} \frac{111}{22} \frac{113}{29} \frac{95}{32} \frac{100}{50}$$

$$\frac{64}{50} \frac{72}{34} \frac{87}{30} \frac{112}{27} \frac{112}{22} \frac{61}{13} \frac{52}{8} \frac{49}{9} \frac{53}{9} \frac{56}{11} \frac{120}{23} \frac{121}{29} \frac{109}{33} \frac{114}{50}$$

$$\frac{83}{50} \frac{89}{34} \frac{99}{31} \frac{115}{29} \frac{116}{20} \frac{67}{12} \frac{64}{8} \frac{62}{9} \frac{66}{9} \frac{68}{11} \frac{131}{23} \frac{136}{30} \frac{118}{33} \frac{123}{50}$$

$$\frac{104}{50} \frac{106}{35} \frac{115}{31} \frac{124}{28} \frac{125}{21} \frac{78}{11} \frac{78}{8} \frac{74}{9} \frac{78}{9} \frac{84}{12} \frac{135}{22} \frac{137}{29} \frac{126}{31} \frac{127}{50}$$

$$\frac{115}{50} \frac{123}{31} \frac{130}{29} \frac{131}{20} \frac{91}{10} \frac{89}{8}$$

$$\frac{85}{9} \frac{87}{11} \frac{89}{11} \frac{137}{20} \frac{142}{23} \frac{142}{29} \frac{126}{31} \frac{127}{50}$$

05.33

7.15

10.18

04.90

$$\frac{84}{50} \frac{85}{32} \frac{95}{30} \frac{94}{20} \frac{90}{18} \frac{60}{10} \frac{56}{11} \frac{57}{11} \frac{95}{19} \frac{102}{24} \frac{98}{29} \frac{88}{31} \frac{10}{50}$$

$$\frac{84}{50} \frac{87}{32} \frac{94}{29} \frac{95}{20} \frac{87}{19} \frac{81}{14} \frac{60}{11} \frac{57}{11} \frac{69}{12} \frac{60}{17} \frac{87}{22} \frac{110}{26} \frac{110}{30} \frac{100}{32} \frac{92}{50}$$

$$\frac{86}{50} \frac{85}{32} \frac{102}{30} \frac{102}{23} \frac{99}{19} \frac{77}{14} \frac{57}{10} \frac{51}{11} \frac{54}{11} \frac{75}{15} \frac{104}{22} \frac{104}{27} \frac{99}{31} \frac{88}{32} \frac{86}{50}$$

$$\frac{82}{50} \frac{74}{33} \frac{98}{31} \frac{102}{24} \frac{97}{19} \frac{78}{10} \frac{53}{11} \frac{49}{10} \frac{52}{10} \frac{82}{16} \frac{97}{22} \frac{102}{26} \frac{98}{30} \frac{90}{31} \frac{87}{50}$$

$$\frac{64}{30} \frac{59}{33} \frac{97}{27} \frac{97}{23} \frac{89}{19} \frac{53}{10} \frac{48}{11} \frac{52}{11} \frac{85}{18} \frac{100}{21} \frac{100}{29} \frac{88}{31} \frac{87}{50}$$

Sta.	+	π	-	Elev.
		915.08		
15				10.3 .
	+50			10.4 .
16				09.9 .
	+50			09.8 .
17				09.8 .
T.P.	5.15	914.95	5.28	909.80 .
	+50			09.6 .
18				08.9 .
	+50			09.0 .
19				09.6 .
	+50			09.9 .
	+63	to Culv.		

LT

4

21

$$\frac{38}{50} \frac{43}{33} \frac{91}{27} \frac{99}{22} \frac{91}{18} \frac{56}{12} \frac{51}{8} \quad \frac{48}{11} \frac{51}{17} \frac{77}{21} \frac{94}{26} \frac{101}{30} \frac{100}{31} \frac{88}{40} \frac{84}{50} \frac{82}{50}$$

$$\frac{48}{50} \frac{48}{34} \frac{83}{28} \frac{99}{24} \frac{89}{19} \frac{58}{14} \frac{51}{9} \frac{47}{12} \quad \frac{65}{14} \frac{100}{22} \frac{103}{29} \frac{83}{31} \frac{79}{36} \frac{82}{50}$$

$$\frac{76}{50} \frac{76}{34} \frac{100}{31} \frac{105}{26} \frac{103}{20} \frac{79}{17} \frac{63}{12} \frac{55}{9} \quad \frac{52}{11} \frac{55}{16} \frac{76}{21} \frac{105}{29} \frac{105}{31} \frac{91}{50}$$

$$\frac{87}{50} \frac{84}{32} \frac{102}{29} \frac{104}{25} \frac{102}{21} \frac{89}{19} \frac{60}{11} \frac{57}{9} \quad \frac{53}{11} \frac{58}{17} \frac{85}{21} \frac{101}{25} \frac{102}{28} \frac{92}{30} \frac{84}{50}$$

$$\frac{88}{50} \frac{87}{30} \frac{101}{28} \frac{104}{24} \frac{102}{20} \frac{90}{18} \frac{69}{12} \frac{57}{9} \quad \frac{53}{11} \frac{56}{17} \frac{79}{21} \frac{91}{23} \frac{98}{26} \frac{98}{30} \frac{82}{31} \frac{72}{50}$$

2. 17100

$$\frac{84}{50} \frac{86}{30} \frac{100}{27} \frac{98}{20} \frac{57}{10} \frac{54}{12} \frac{58}{22} \frac{91}{29} \frac{98}{30} \frac{89}{50} \frac{86}{50}$$

$$\frac{85}{50} \frac{86}{29} \frac{99}{27} \frac{101}{19} \frac{90}{15} \frac{65}{10} \quad \frac{61}{11} \frac{66}{15} \frac{74}{17} \frac{89}{21} \frac{101}{28} \frac{86}{30} \frac{87}{50}$$

$$\frac{85}{50} \frac{86}{30} \frac{101}{28} \frac{99}{19} \frac{91}{16} \frac{74}{12} \frac{62}{9} \quad \frac{60}{11} \frac{62}{13} \frac{67}{17} \frac{91}{21} \frac{103}{29} \frac{100}{30} \frac{87}{50} \frac{86}{50}$$

$$\frac{84}{50} \frac{86}{30} \frac{100}{28} \frac{89}{20} \frac{84}{18} \frac{64}{13} \frac{57}{9} \quad \frac{54}{12} \frac{58}{15} \frac{69}{20} \frac{87}{21} \frac{100}{29} \frac{99}{30} \frac{85}{50} \frac{87}{50}$$

$$\frac{85}{50} \frac{83}{30} \frac{99}{28} \frac{99}{19} \frac{63}{13} \frac{55}{10}$$

$$\frac{51}{12} \frac{56}{19} \frac{89}{23} \frac{101}{28} \frac{101}{30} \frac{85}{50} \frac{86}{50}$$

1026

04.69

10.1

0495

Sta	+	π	-	Elev.
		91495		
19	+78			10.2
20				10.2
	+33			10.2
	+76			10.0
21				09.9
	+62			09.4
22				09.6
	} +35 Ent & Culv.			
	+50			08.4
	+75			08.2

Lt.

L.

Rt.

$$\begin{array}{cccccccc} 83 & 84 & 94 & 96 & 55 & 48 & 53 & 92 \\ 50 & 31 & 27 & 19 & 11 & & 12 & 22 \end{array} \quad \begin{array}{cccccc} 101 & 101 & 82 & 83 & & \\ 23 & 27 & 30 & 50 & & \end{array}$$

$$\begin{array}{cccccc} 61 & 61 & 88 & 87 & 53 & \\ 50 & 32 & 28 & 18 & 11 & \end{array}$$

$$\begin{array}{cccccc} 48 & 50 & 90 & 100 & 100 & 88 \\ 12 & 19 & 21 & 22 & 24 & 30 \end{array} \quad \begin{array}{cc} 67 & 67 \\ 50 & 50 \end{array}$$

$$\begin{array}{cccccccc} 35 & 46 & 80 & 75 & 56 & 51 & 48 & 53 \\ 50 & 29 & 23 & 15 & 12 & 8 & 12 & 16 \end{array} \quad \begin{array}{cccccc} 87 & 97 & 97 & 87 & 75 & 73 \\ 20 & 21 & 22 & 23 & 25 & 27 \end{array} \quad \begin{array}{cc} 56 & 45 \\ 29 & 34 \end{array} \quad \begin{array}{c} 48 \\ 50 \end{array}$$

$$\begin{array}{cccccc} 07 & 31 & 79 & 77 & 54 & \\ 50 & 28 & 22 & 15 & 10 & \end{array}$$

$$\begin{array}{cccccc} 50 & 56 & 82 & 97 & 97 & 85 \\ 12 & 18 & 20 & 21 & 23 & 26 \end{array} \quad \begin{array}{cc} 78 & 55 \\ 29 & 34 \end{array} \quad \begin{array}{c} 44 \\ 50 \end{array}$$

$$\begin{array}{cccccc} 08 & 15 & 28 & 76 & 75 & 55 \\ 50 & 36 & 28 & 21 & 15 & 11 \end{array} \quad \begin{array}{cccccc} 58 & 89 & 97 & 96 & 83 & 76 \\ 13 & 19 & 20 & 22 & 23 & 26 \end{array} \quad \begin{array}{cc} 54 & 43 \\ 29 & 33 \end{array} \quad \begin{array}{c} 53 \\ 50 \end{array}$$

$$\begin{array}{cccccc} 17 & 21 & 30 & 46 & 71 & 57 \\ 50 & 37 & 27 & 21 & 15 & 11 \end{array}$$

$$\begin{array}{cccccc} 56 & 57 & 68 & 97 & 97 & 80 \\ 12 & 17 & 19 & 21 & 22 & \end{array} \quad \begin{array}{cc} 46 & 35 \\ 28 & 33 \end{array} \quad \begin{array}{c} 37 \\ 50 \end{array}$$

$$\begin{array}{cccccc} 21 & 32 & 48 & 70 & 71 & 63 \\ 50 & 35 & 26 & 22 & 15 & 11 \end{array} \quad \begin{array}{c} 58 \\ 50 \end{array}$$

$$\begin{array}{cccccc} 61 & 75 & 99 & 100 & 58 & 49 \\ 13 & 18 & 20 & 21 & 25 & 28 \end{array} \quad \begin{array}{c} 49 \\ 50 \end{array}$$

S. End. Ent. Culv. Rt.

10.35

904.60

N. End. Ent. Culv. Rt.

10.65

904.30

$$\begin{array}{cccccc} 27 & 41 & 56 & 77 & 80 & 69 \\ 50 & 37 & 26 & 22 & 14 & 70 \end{array}$$

$$\begin{array}{cccccc} 04 & 68 & 87 & 102 & 103 & 75 \\ 12 & 19 & 20 & 22 & 25 & 50 \end{array} \quad \begin{array}{c} 72 \\ 50 \end{array}$$

$$\begin{array}{cccccc} 27 & 46 & 55 & 78 & 79 & 73 \\ 50 & 35 & 27 & 23 & 14 & 11 \end{array} \quad \begin{array}{cccccc} 63 & 73 & 87 & 94 & 108 & 108 \\ 13 & 16 & 20 & 21 & 22 & 23 \end{array} \quad \begin{array}{cc} 77 & 63 \\ 28 & 30 \end{array} \quad \begin{array}{c} 64 \\ 50 \end{array}$$

Sta.	T	T	-	Elev.
		914.95		
23				07.9
I.P.	2.67	910.56	2.06	907.89
+50				07.3
+85				06.9
24	+10			06.6
+50				06.2
25				06.2
+24				06.2
+50				06.0
26				05.6
+23	E. Culv.			
+31				05.5

44

天

24

[illegible]

$\frac{26}{50} \quad \frac{29}{31} \quad \frac{38}{24} \quad \frac{45}{22} \quad \frac{45}{14} \quad \frac{37}{11} \quad \frac{33}{11} \quad \frac{35}{11} \quad \frac{39}{14} \quad \frac{46}{17} \quad \frac{47}{19} \quad \frac{58}{21} \quad \frac{67}{22} \quad \frac{68}{24} \quad \frac{57}{28} \quad \frac{52}{26} \quad \frac{47}{32} \quad \frac{37}{50}$

$$\begin{array}{r} 39 \\ \hline 50 \end{array} \quad \begin{array}{r} 45 \\ \hline 39 \end{array} \quad \begin{array}{r} 45 \\ \hline 26 \end{array} \quad \begin{array}{r} 48 \\ \hline 18 \end{array} \quad \begin{array}{r} 40 \\ \hline 12 \end{array}$$

37 41 48 59 73 72 59 52 51
12 19 21 22 23 24 26 50

$$\begin{array}{r} 71 \\ \hline 50 \end{array} \quad \begin{array}{r} 70 \\ \hline 35 \end{array} \quad \begin{array}{r} 71 \\ \hline 20 \end{array} \quad \begin{array}{r} 60 \\ \hline 15 \end{array} \quad \begin{array}{r} 46 \\ \hline 12 \end{array} \quad \begin{array}{r} 40 \\ \hline \end{array}$$

$\frac{4.7}{12}$ $\frac{6.4}{16}$ $\frac{6.7}{20}$ $\frac{7.5}{22}$ $\frac{7.5}{23}$ $\frac{6.0}{24}$ $\frac{6.2}{50}$

$$\begin{array}{r} 73 \\ \hline 50 \end{array} \quad \begin{array}{r} 83 \\ \hline 18 \end{array} \quad \begin{array}{r} 49 \\ \hline 12 \end{array}$$
$$\frac{49}{13} \frac{51}{16} \frac{70}{18} \frac{79}{20} \frac{79}{21} \frac{72}{37} \frac{73}{50}$$
$$\begin{array}{r} 76 \\ \hline 50 \end{array} \quad \begin{array}{r} 77 \\ \hline 57 \end{array} \quad \begin{array}{r} 82 \\ \hline 17 \end{array} \quad \begin{array}{r} 51 \\ \hline 12 \end{array} \quad \begin{array}{r} 49 \\ \hline \end{array}$$

$\frac{5.2}{13}$ $\frac{7.5}{19}$ $\frac{8.3}{20}$ $\frac{8.3}{21}$ $\frac{6.9}{22}$ $\frac{7.9}{27}$ $\frac{7.2}{30}$

$\frac{76}{50}$	$\frac{72}{38}$	$\frac{62}{29}$	$\frac{62}{20}$	$\frac{68}{19}$	$\frac{66}{17}$	$\frac{49}{12}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{44}{11}$ $\frac{50}{13}$ $\frac{56}{13}$ $\frac{72}{19}$ $\frac{84}{19}$ $\frac{84}{21}$ $\frac{69}{22}$ $\frac{71}{50}$

$$\begin{array}{r} 79 \\ 50 \end{array} \quad \begin{array}{r} 78 \\ 43 \end{array} \quad \begin{array}{r} 61 \\ 20 \end{array} \quad \begin{array}{r} 66 \\ 19 \end{array} \quad \begin{array}{r} 67 \\ 16 \end{array} \quad \begin{array}{r} 51 \\ 12 \end{array} \quad \begin{array}{r} 46 \\ 12 \end{array}$$

5.2	6.6	7.6	8.5	7.6	7.0	7.3
<u>12</u>	<u>15</u>	<u>19</u>	<u>29</u>	<u>22</u>	<u>38</u>	<u>50</u>

$$\frac{9.0}{50}$$

$\frac{90}{19}$	$\frac{56}{12}$
-----------------	-----------------

50 55 72 80 90 90 75 77 86 86 77 74
 12 15 18 19 20 21 28 30 33 34 50

10.78
899.78

9.81 00.75

9009

$$\frac{97}{50} \quad \frac{70}{17} \quad \frac{58}{12} \quad \frac{51}{11} \quad \frac{53}{9} \quad \frac{57}{13}$$
$$\begin{array}{r} 86 \\ 18 \end{array} \quad \begin{array}{r} 80 \\ 31 \end{array} \quad \begin{array}{r} 75 \\ 50 \end{array}$$

Sta	+	T	-	Elev
		910.56		
26	+36			05.5
	+50			05.2
	+62			05.2
	+66	2. Corly		05.1
B.M.	6.26	910.59	6.26	904.30 (904.33)
	+68			05.0
27				05.0
	+50			05.2
28				05.4
T.P.	2.07	907.52	5.14	905.45
	+50			05.2
29				04.6
	+50			03.6

Lt

L

Rt

Duplicate 100 Lt

5153
1357
2752
5093 94
50 3292
1860
1254
1551
5042
10020

Duplicate 100 Lt

5453
1146
50

900.01

10.555555
1353
38626
40888
4063
5002.18
614

901.0

96
5091
3585
2960
2293
1760
1156
1555
3951
5050

L.O.

95
3592
2974
2386
1862
1256
1157
1562
505780 78 80 48 76 88 88 63 60 54 56 72 67 59
50 50 30 25 20 18 17 12 10 11 11 18 19 50L.O. 84 82 74 75 87 87 77 58 52 55 64 71 71 63 50
35 29 26 21 19 17 15 12 12 13 17 18 21 50

9.28

61 58 57 33 29 23 27 30 44 45 40 35 28
50 32 18 12 10 9 12 16 18 21 37 5063 61 67 69 63 62 39 36 29 33 37 53 54 45 41 36
50 32 27 23 22 18 13 11 9 12 16 19 21 35 50L.O. 72 66 72 68 46 42 39 40 42 58 57 51 47 41
35 28 27 18 14 11 8 12 13 19 20 35 50

Sta.	+	T	-	Elev.
		907.52		
30				03.2
	+50			02.8
31				02.5
	+50			02.4
32				02.5
	+50			02.4
33				02.2
	+50			02.1
34				02.4
I.P.	4.63	906.53	5.62	901.90
	+50			02.4
35				02.0

Lt

L

Rt

$$L.O. \quad \frac{66}{35} \quad \frac{68}{28} \quad \frac{67}{18} \quad \frac{53}{15} \quad \frac{49}{12} \quad \frac{43}{8} \quad \frac{43}{15} \quad \frac{43}{17} \quad \frac{56}{21} \quad \frac{58}{22} \quad \frac{49}{40} \quad \frac{47}{50} \quad \frac{44}{50}$$

$$L.O. \quad \frac{58}{35} \quad \frac{59}{23} \quad \frac{68}{22} \quad \frac{68}{19} \quad \frac{56}{16} \quad \frac{52}{11} \quad \frac{47}{9} \quad \frac{48}{14} \quad \frac{49}{18} \quad \frac{54}{19} \quad \frac{62}{21} \quad \frac{57}{50} \quad \frac{52}{50}$$

$$L.O. \quad \frac{62}{35} \quad \frac{64}{23} \quad \frac{70}{22} \quad \frac{70}{19} \quad \frac{59}{16} \quad \frac{59}{12} \quad \frac{50}{8} \quad \frac{52}{13} \quad \frac{54}{17} \quad \frac{61}{19} \quad \frac{67}{20} \quad \frac{60}{32} \quad \frac{53}{50} \quad \frac{50}{50}$$

$$L.O. \quad \frac{63}{35} \quad \frac{64}{23} \quad \frac{74}{22} \quad \frac{74}{19} \quad \frac{61}{15} \quad \frac{56}{11} \quad \frac{51}{9} \quad \frac{52}{15} \quad \frac{53}{17} \quad \frac{60}{19} \quad \frac{70}{21} \quad \frac{62}{31} \quad \frac{57}{50} \quad \frac{52}{50}$$

$$L.O. \quad \frac{62}{35} \quad \frac{65}{23} \quad \frac{76}{22} \quad \frac{74}{19} \quad \frac{62}{16} \quad \frac{57}{11} \quad \frac{50}{9} \quad \frac{53}{15} \quad \frac{58}{17} \quad \frac{74}{18} \quad \frac{73}{20} \quad \frac{63}{34} \quad \frac{57}{50} \quad \frac{55}{50}$$

$$L.O. \quad \frac{66}{35} \quad \frac{70}{22} \quad \frac{78}{21} \quad \frac{77}{18} \quad \frac{63}{16} \quad \frac{58}{11} \quad \frac{51}{10} \quad \frac{54}{16} \quad \frac{61}{18} \quad \frac{74}{19} \quad \frac{74}{20} \quad \frac{66}{26} \quad \frac{69}{36} \quad \frac{56}{50} \quad \frac{55}{50}$$

$$L.O. \quad \frac{68}{35} \quad \frac{69}{23} \quad \frac{80}{22} \quad \frac{78}{18} \quad \frac{66}{16} \quad \frac{58}{11} \quad \frac{53}{9} \quad \frac{54}{16} \quad \frac{59}{17} \quad \frac{73}{18} \quad \frac{73}{20} \quad \frac{67}{26} \quad \frac{67}{35} \quad \frac{58}{50} \quad \frac{55}{50}$$

$$L.O. \quad \frac{69}{35} \quad \frac{72}{22} \quad \frac{81}{21} \quad \frac{78}{18} \quad \frac{66}{15} \quad \frac{60}{11} \quad \frac{54}{9} \quad \frac{54}{15} \quad \frac{58}{18} \quad \frac{72}{19} \quad \frac{72}{21} \quad \frac{69}{29} \quad \frac{67}{38} \quad \frac{58}{50} \quad \frac{57}{50}$$

$$L.O. \quad \frac{70}{35} \quad \frac{71}{22} \quad \frac{78}{21} \quad \frac{78}{16} \quad \frac{60}{13} \quad \frac{56}{10} \quad \frac{51}{10} \quad \frac{53}{16} \quad \frac{59}{17} \quad \frac{72}{18} \quad \frac{72}{19} \quad \frac{67}{29} \quad \frac{69}{38} \quad \frac{60}{50} \quad \frac{50}{50}$$

$$L.O. \quad \frac{66}{35} \quad \frac{60}{23} \quad \frac{71}{20} \quad \frac{70}{17} \quad \frac{53}{13} \quad \frac{46}{10} \quad \frac{41}{9} \quad \frac{42}{16} \quad \frac{51}{18} \quad \frac{64}{29} \quad \frac{62}{38} \quad \frac{51}{50} \quad \frac{50}{50}$$

$$L.O. \quad \frac{68}{35} \quad \frac{67}{23} \quad \frac{77}{21} \quad \frac{78}{18} \quad \frac{59}{14} \quad \frac{53}{10} \quad \frac{45}{9} \quad \frac{45}{14} \quad \frac{50}{18} \quad \frac{68}{25} \quad \frac{65}{37} \quad \frac{56}{50} \quad \frac{52}{50}$$

Sta.	T	X	-	Elev
------	---	---	---	------

906.53

35	+50			01.5
----	-----	--	--	------

36 00,7

450				00.6
-----	--	--	--	------

†77 For piton & cult. Do Not Use for Plotting X-sections

37			01.5
----	--	--	------

150				01.9
-----	--	--	--	------

38			02.6
----	--	--	------

+50				02.9
-----	--	--	--	------

39				03.3 -
----	--	--	--	--------

450				03.0
-----	--	--	--	------

T.P.	4.18	906.79	392	902.61
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+70 Ditch & Cuts Do Not Use for Plotting X-sections

11

8

21

$$L.O. \quad \frac{77}{35} \quad \frac{76}{23} \quad \frac{84}{22} \quad \frac{83}{19} \quad \frac{61}{15} \quad \frac{57}{10} \quad \frac{50}{9} \quad \frac{50}{9} \quad \frac{54}{14} \quad \frac{72}{18} \quad \frac{71}{26} \quad \frac{57}{38} \quad \frac{55}{50}$$

$$L.O. \quad \frac{83}{35} \quad \frac{86}{27} \quad \frac{96}{26} \quad \frac{94}{19} \quad \frac{71}{15} \quad \frac{64}{10} \quad \frac{58}{9} \quad \frac{57}{14} \quad \frac{63}{17} \quad \frac{77}{19} \quad \frac{77}{19} \quad \frac{72}{23} \quad \frac{74}{35} \quad \frac{59}{50}$$

$$L.O. \quad \frac{88}{35} \quad \frac{94}{28} \quad \frac{102}{25} \quad \frac{94}{27} \quad \frac{86}{16} \quad \frac{70}{13} \quad \frac{66}{10} \quad \frac{59}{9} \quad \frac{58}{15} \quad \frac{61}{18} \quad \frac{84}{19} \quad \frac{84}{20} \quad \frac{75}{26} \quad \frac{74}{34} \quad \frac{61}{50}$$

$$\begin{array}{r} 7.35 \quad 899.18 \\ \hline 898.1 \quad 898.0 \quad 96.31 \quad 897.10 \\ \hline 84 \quad 85 \quad 10.22 \quad 896.01 \\ 200 \quad 100 \quad \text{C.M.V.} \quad \text{C.M.V.} \end{array}$$

Ely, Winter
3/30/39

897.5

$$\frac{70}{500} \quad L.O. \quad \frac{84}{35} \quad \frac{83}{17} \quad \frac{57}{12} \quad \frac{54}{10} \quad \frac{50}{9} \quad \frac{54}{13} \quad \frac{55}{18} \quad \frac{81}{22} \quad \frac{79}{35} \quad \frac{61}{50}$$

$$L.O. \quad \frac{77}{35} \quad \frac{82}{28} \quad \frac{81}{18} \quad \frac{51}{12} \quad \frac{49}{10} \quad \frac{46}{9} \quad \frac{46}{13} \quad \frac{47}{17} \quad \frac{66}{18} \quad \frac{79}{24} \quad \frac{78}{25} \quad \frac{69}{35} \quad \frac{60}{50}$$

$$L.O. \quad \frac{75}{35} \quad \frac{76}{25} \quad \frac{83}{20} \quad \frac{49}{14} \quad \frac{46}{10} \quad \frac{39}{8} \quad \frac{40}{13} \quad \frac{44}{18} \quad \frac{60}{19} \quad \frac{71}{24} \quad \frac{20}{27} \quad \frac{40}{37} \quad \frac{48}{50}$$

$$L.O. \quad \frac{70}{35} \quad \frac{70}{26} \quad \frac{70}{19} \quad \frac{62}{18} \quad \frac{45}{13} \quad \frac{41}{10} \quad \frac{36}{9} \quad \frac{39}{14} \quad \frac{40}{18} \quad \frac{52}{19} \quad \frac{63}{25} \quad \frac{62}{30} \quad \frac{50}{30}$$

$$L.O. \quad \frac{66}{35} \quad \frac{64}{18} \quad \frac{55}{17} \quad \frac{44}{13} \quad \frac{37}{9} \quad \frac{32}{9} \quad \frac{36}{13} \quad \frac{38}{17} \quad \frac{46}{17} \quad \frac{62}{18} \quad \frac{60}{24} \quad \frac{47}{33} \quad \frac{44}{50}$$

$$L.O. \quad \frac{62}{35} \quad \frac{57}{18} \quad \frac{44}{15} \quad \frac{41}{9} \quad \frac{35}{9} \quad \frac{38}{15} \quad \frac{44}{17} \quad \frac{63}{25} \quad \frac{64}{31} \quad \frac{56}{50}$$

98.2 277.8

$$\begin{array}{r} 86 \quad 90 \quad 85 \quad 81 \quad 840 \\ 200 \quad 150 \quad 100 \quad 50 \quad \text{C.M.V.} \end{array}$$

898.39

$$\begin{array}{r} 898.71 \\ 808 \quad 78 \quad 6.8 \\ \text{C.M.V.} \quad 50 \quad 30 \end{array}$$

Sta.	+	X	-	Elev.
		906.79		

40				02.5
----	--	--	--	------

	+50			01.7
--	-----	--	--	------

41				00.9
----	--	--	--	------

	+50			00.8
--	-----	--	--	------

42				01.3
----	--	--	--	------

	+50			01.5
--	-----	--	--	------

43				01.50
----	--	--	--	-------

I.P.	4.45	905.95	5.29	901.50
------	------	--------	------	--------

	+50			01.5
--	-----	--	--	------

44				01.0
----	--	--	--	------

	+50			00.3
--	-----	--	--	------

45				00.5
----	--	--	--	------

L.

L.

R.

$$L.O. \quad \frac{75}{35} \quad \frac{75}{25} \quad \frac{82}{18} \quad \frac{57}{15} \quad \frac{48}{9} \quad \frac{43}{9} \quad \frac{45}{9} \quad \frac{58}{18} \quad \frac{81}{19} \quad \frac{81}{21} \quad \frac{58}{23} \quad \frac{54}{50}$$

$$L.O. \quad \frac{90}{35} \quad \frac{90}{19} \quad \frac{69}{17} \quad \frac{54}{11} \quad \frac{54}{8} \quad \frac{51}{8} \quad \frac{53}{9} \quad \frac{63}{17} \quad \frac{85}{19} \quad \frac{85}{22} \quad \frac{62}{26} \quad \frac{62}{50}$$

$$L.O. \quad \frac{83}{35} \quad \frac{88}{26} \quad \frac{91}{22} \quad \frac{82}{17} \quad \frac{69}{14} \quad \frac{60}{9} \quad \frac{59}{9} \quad \frac{60}{9} \quad \frac{65}{11} \quad \frac{86}{14} \quad \frac{95}{20} \quad \frac{82}{25} \quad \frac{72}{26} \quad \frac{66}{35} \quad \frac{66}{50}$$

$$\frac{76}{3/34/37} \quad L.O. \quad \frac{100}{30} \quad \frac{112}{19} \quad \frac{68}{15} \quad \frac{66}{12} \quad \frac{64}{8} \quad \frac{60}{8} \quad \frac{62}{8} \quad \frac{68}{11} \quad \frac{98}{16} \quad \frac{116}{22} \quad \frac{87}{26} \quad \frac{76}{32} \quad \frac{75}{50}$$

$$L.O. \quad \frac{107}{20} \quad \frac{84}{18} \quad \frac{64}{10} \quad \frac{58}{7} \quad \frac{55}{7} \quad \frac{56}{9} \quad \frac{66}{13} \quad \frac{96}{16} \quad \frac{102}{22} \quad \frac{83}{24} \quad \frac{79}{32} \quad \frac{74}{37} \quad \frac{69}{50}$$

$$L.O. \quad \frac{76}{35} \quad \frac{77}{27} \quad \frac{86}{25} \quad \frac{92}{21} \quad \frac{85}{16} \quad \frac{70}{14} \quad \frac{57}{10} \quad \frac{52}{8} \quad \frac{54}{12} \quad \frac{61}{15} \quad \frac{80}{19} \quad \frac{93}{23} \quad \frac{93}{23} \quad \frac{77}{28} \quad \frac{71}{33} \quad \frac{66}{50}$$

$$L.O. \quad \frac{75}{35} \quad \frac{74}{26} \quad \frac{84}{24} \quad \frac{84}{20} \quad \frac{77}{17} \quad \frac{59}{15} \quad \frac{55}{7} \quad \frac{52}{7} \quad \frac{54}{8} \quad \frac{58}{13} \quad \frac{70}{18} \quad \frac{91}{20} \quad \frac{88}{22} \quad \frac{78}{25} \quad \frac{74}{29} \quad \frac{62}{35} \quad \frac{62}{50}$$

R. 43

$$L.O. \quad \frac{64}{35} \quad \frac{65}{26} \quad \frac{77}{24} \quad \frac{73}{19} \quad \frac{60}{18} \quad \frac{50}{15} \quad \frac{47}{10} \quad \frac{45}{9} \quad \frac{47}{9} \quad \frac{52}{14} \quad \frac{60}{18} \quad \frac{75}{19} \quad \frac{77}{23} \quad \frac{67}{25} \quad \frac{65}{27} \quad \frac{55}{30} \quad \frac{51}{50}$$

$$L.O. \quad \frac{61}{35} \quad \frac{66}{25} \quad \frac{76}{24} \quad \frac{75}{18} \quad \frac{66}{17} \quad \frac{55}{13} \quad \frac{53}{9} \quad \frac{50}{9} \quad \frac{51}{8} \quad \frac{53}{11} \quad \frac{62}{18} \quad \frac{78}{19} \quad \frac{78}{23} \quad \frac{65}{24} \quad \frac{64}{29} \quad \frac{55}{31} \quad \frac{53}{50}$$

$$L.O. \quad \frac{65}{35} \quad \frac{68}{27} \quad \frac{87}{24} \quad \frac{92}{20} \quad \frac{75}{15} \quad \frac{60}{12} \quad \frac{57}{8} \quad \frac{58}{8} \quad \frac{64}{12} \quad \frac{95}{18} \quad \frac{82}{23} \quad \frac{70}{30} \quad \frac{88}{30} \quad \frac{63}{31} \quad \frac{60}{50}$$

$$L.O. \quad \frac{61}{35} \quad \frac{63}{27} \quad \frac{72}{26} \quad \frac{94}{21} \quad \frac{77}{17} \quad \frac{65}{15} \quad \frac{58}{10} \quad \frac{53}{10} \quad \frac{58}{8} \quad \frac{61}{10} \quad \frac{78}{13} \quad \frac{90}{21} \quad \frac{77}{23} \quad \frac{74}{30} \quad \frac{67}{31} \quad \frac{58}{36} \quad \frac{59}{50}$$

Sta	+	T	-	Elev.
-----	---	---	---	-------

905.95'

45	+50			00.8
----	-----	--	--	------

46				00.9
----	--	--	--	------

	+50			01.3
--	-----	--	--	------

	+90			01.3
--	-----	--	--	------

} 103 Ent. Cohn Rd.

47	+15			01.0
----	-----	--	--	------

	+50			01.0
--	-----	--	--	------

48				01.1
----	--	--	--	------

	+50			01.9
--	-----	--	--	------

49				01.9
----	--	--	--	------

T.P.	8.20	910.47	418	901.77
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LT

4

RT

L.O. $\frac{58}{35} \frac{64}{26} \frac{73}{24} \frac{97}{19} \frac{82}{17} \frac{63}{15} \frac{56}{11} \frac{52}{8} \frac{55}{10} \frac{60}{13} \frac{75}{16} \frac{90}{20} \frac{96}{22} \frac{86}{28} \frac{67}{30} \frac{58}{35} \frac{58}{50}$

L.O. $\frac{61}{35} \frac{68}{22} \frac{88}{21} \frac{81}{17} \frac{57}{13} \frac{53}{10} \frac{51}{7} \frac{53}{7} \frac{55}{11} \frac{78}{15} \frac{78}{18} \frac{74}{21} \frac{59}{23} \frac{53}{50}$

L.O. $\frac{57}{35} \frac{65}{21} \frac{77}{20} \frac{79}{18} \frac{60}{17} \frac{51}{12} \frac{47}{7} \frac{49}{10} \frac{50}{17} \frac{58}{18} \frac{68}{20} \frac{46}{22} \frac{42}{50}$

L.O. $\frac{58}{35} \frac{59}{23} \frac{75}{21} \frac{75}{19} \frac{63}{18} \frac{53}{13} \frac{51}{10} \frac{47}{7} \frac{47}{13} \frac{46}{17} \frac{51}{19} \frac{60}{21} \frac{61}{23} \frac{46}{23} \frac{45}{50}$

S. End Calc.

6.22 99.73

N. End Calc.

6.31 99.64

L.O. $\frac{58}{35} \frac{66}{24} \frac{77}{21} \frac{79}{17} \frac{61}{15} \frac{52}{11} \frac{50}{7} \frac{49}{15} \frac{50}{18} \frac{62}{21} \frac{62}{24} \frac{55}{29} \frac{49}{50}$

L.O. $\frac{52}{33} \frac{67}{24} \frac{84}{22} \frac{90}{20} \frac{73}{17} \frac{57}{15} \frac{51}{9} \frac{50}{8} \frac{51}{8} \frac{52}{12} \frac{70}{14} \frac{86}{18} \frac{86}{21} \frac{66}{22} \frac{58}{28} \frac{49}{50}$

L.O. $\frac{61}{35} \frac{70}{32} \frac{101}{30} \frac{90}{23} \frac{70}{17} \frac{52}{12} \frac{49}{8} \frac{51}{12} \frac{58}{15} \frac{75}{15} \frac{87}{21} \frac{63}{22} \frac{54}{28} \frac{48}{50}$

L.O. $\frac{52}{35} \frac{62}{31} \frac{80}{29} \frac{98}{25} \frac{103}{21} \frac{73}{17} \frac{51}{14} \frac{42}{10} \frac{41}{10} \frac{45}{10} \frac{63}{13} \frac{85}{17} \frac{86}{20} \frac{56}{22} \frac{49}{50}$

L.O. $\frac{51}{35} \frac{58}{24} \frac{68}{20} \frac{71}{17} \frac{52}{14} \frac{43}{10} \frac{41}{10} \frac{42}{8} \frac{52}{12} \frac{62}{15} \frac{65}{21} \frac{47}{22} \frac{42}{50}$

Sta	+	Σ	-	Elev.
		910.47		
49	+50			02.9
50				04.0
	+50			04.6
51				04.9
	+57			05.4
52				06.1
B.M.	4.86	912.45 913.45	7 1.85	907.59 908.62 (908.59)
	+36			07.9 06.9
	+70			08.4 07.4
	+80			08.5 07.5
53	+10			08.8 07.8
	+63			08.9 07.9

Lt

4

Rt

$$L.O. \quad \frac{89}{35} \quad \frac{91}{21} \quad \frac{102}{20} \quad \frac{102}{18} \quad \frac{96}{17} \quad \frac{81}{13} \quad \frac{78}{10} \quad \frac{76}{9} \quad \frac{78}{13} \quad \frac{81}{17} \quad \frac{99}{20} \quad \frac{78}{22} \quad \frac{86}{50} \quad \frac{84}{50}$$

$$L.O. \quad \frac{84}{35} \quad \frac{85}{21} \quad \frac{94}{20} \quad \frac{94}{18} \quad \frac{85}{17} \quad \frac{72}{14} \quad \frac{69}{10} \quad \frac{65}{9} \quad \frac{67}{10} \quad \frac{72}{14} \quad \frac{90}{18} \quad \frac{90}{20} \quad \frac{78}{22} \quad \frac{80}{50}$$

$$L.O. \quad \frac{75}{35} \quad \frac{76}{21} \quad \frac{85}{20} \quad \frac{85}{18} \quad \frac{79}{17} \quad \frac{67}{13} \quad \frac{63}{10} \quad \frac{59}{9} \quad \frac{61}{9} \quad \frac{65}{14} \quad \frac{83}{18} \quad \frac{83}{21} \quad \frac{75}{24} \quad \frac{72}{50}$$

$$L.O. \quad \frac{71}{35} \quad \frac{70}{23} \quad \frac{81}{22} \quad \frac{81}{19} \quad \frac{76}{18} \quad \frac{64}{13} \quad \frac{60}{10} \quad \frac{56}{9} \quad \frac{57}{9} \quad \frac{59}{13} \quad \frac{79}{19} \quad \frac{79}{21} \quad \frac{67}{24} \quad \frac{68}{50}$$

$$L.O. \quad \frac{66}{35} \quad \frac{67}{23} \quad \frac{74}{21} \quad \frac{74}{18} \quad \frac{62}{13} \quad \frac{56}{9} \quad \frac{51}{9} \quad \frac{51}{14} \quad \frac{53}{19} \quad \frac{72}{22} \quad \frac{71}{24} \quad \frac{63}{27} \quad \frac{57}{50}$$

$$L.O. \quad \frac{62}{35} \quad \frac{61}{19} \quad \frac{66}{17} \quad \frac{55}{12} \quad \frac{58}{10} \quad \frac{49}{9} \quad \frac{42}{9} \quad \frac{47}{14} \quad \frac{56}{19} \quad \frac{56}{24} \quad \frac{28}{38} \quad \frac{24}{50}$$

Top Conc. at Base of A. 1100 F. Post Lt. 52165

$$L.O. \quad \frac{80}{35} \quad \frac{77}{17} \quad \frac{63}{13} \quad \frac{60}{10} \quad \frac{56}{9} \quad \frac{54}{13} \quad \frac{58}{18} \quad \frac{67}{23} \quad \frac{67}{36} \quad \frac{49}{50}$$

$$\frac{56}{50} \quad \frac{51}{39} \quad \frac{49}{30} \quad \frac{71}{26} \quad \frac{70}{17} \quad \frac{56}{13} \quad \frac{53}{10} \quad \frac{51}{10} \quad \frac{54}{13} \quad \frac{57}{18} \quad \frac{63}{26} \quad \frac{61}{39} \quad \frac{47}{50} \quad \frac{45}{50}$$

$$\frac{49}{30} \quad \frac{48}{41} \quad \frac{39}{31} \quad \frac{67}{27} \quad \frac{67}{16} \quad \frac{55}{13} \quad \frac{52}{10} \quad \frac{50}{9}$$

$$\frac{53}{10} \quad \frac{60}{21} \quad \frac{46}{36} \quad \frac{38}{50}$$

$$\frac{32}{50} \quad \frac{20}{39} \quad \frac{12}{31} \quad \frac{57}{25} \quad \frac{58}{17} \quad \frac{52}{13} \quad \frac{51}{10} \quad \frac{47}{9} \quad \frac{58}{15} \quad \frac{54}{21} \quad \frac{58}{21} \quad \frac{40}{40} \quad \frac{37}{50}$$

$$\frac{53}{30} \quad \frac{48}{42} \quad \frac{46}{29} \quad \frac{65}{26} \quad \frac{65}{18} \quad \frac{54}{13} \quad \frac{49}{10} \quad \frac{46}{9} \quad \frac{47}{10} \quad \frac{53}{15} \quad \frac{52}{23} \quad \frac{42}{36} \quad \frac{34}{50}$$

Sta	+	π	-	Elev.
		912.45		
		913.45		
54				08.7 07.7
	+50			08.4 07.4
55				07.6 06.6
	+50			07.3 06.3
56				07.2 06.2
	+50			06.7 05.7
57				06.7 05.7
I.P.	3.12	908.80 909.80	6.77	905.68 906.68
	+50			06.3 05.3
58				05.9 04.9
	+49			05.2 04.2
59				04.7 03.7

Lt

L

LH

$$\begin{array}{cccccccccccccccc} \frac{76}{50} & \frac{69}{39} & \frac{57}{30} & \frac{64}{24} & \frac{63}{17} & \frac{54}{13} & \frac{53}{10} & \frac{48}{9} & \frac{51}{15} & \frac{52}{18} & \frac{50}{32} & \frac{45}{32} & \frac{34}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{74}{30} & \frac{69}{25} & \frac{63}{21} & \frac{67}{19} & \frac{66}{17} & \frac{58}{14} & \frac{56}{10} & \frac{51}{9} & \frac{55}{9} & \frac{56}{25} & \frac{44}{36} & \frac{43}{50} \end{array}$$

$$\text{L.O. } \begin{array}{cccccccccccccccc} \frac{81}{35} & \frac{81}{27} & \frac{95}{25} & \frac{95}{19} & \frac{68}{13} & \frac{68}{10} & \frac{59}{9} & \frac{63}{9} & \frac{66}{19} & \frac{78}{18} & \frac{73}{50} \end{array}$$

$$\text{L.O. } \begin{array}{cccccccccccccccc} \frac{80}{35} & \frac{84}{26} & \frac{101}{24} & \frac{100}{19} & \frac{71}{14} & \frac{69}{10} & \frac{62}{9} & \frac{65}{9} & \frac{67}{14} & \frac{79}{18} & \frac{80}{31} & \frac{75}{50} \end{array}$$

$$\text{L.O. } \begin{array}{cccccccccccccccc} \frac{81}{35} & \frac{83}{26} & \frac{103}{23} & \frac{103}{19} & \frac{70}{14} & \frac{67}{9} & \frac{62}{9} & \frac{65}{9} & \frac{66}{13} & \frac{77}{18} & \frac{75}{32} & \frac{72}{50} \end{array}$$

$$\text{L.O. } \begin{array}{cccccccccccccccc} \frac{81}{35} & \frac{84}{26} & \frac{104}{23} & \frac{105}{19} & \frac{72}{14} & \frac{69}{9} & \frac{63}{9} & \frac{64}{9} & \frac{67}{14} & \frac{77}{19} & \frac{78}{36} & \frac{75}{50} \end{array}$$

$$\text{L.O. } \begin{array}{cccccccccccccccc} \frac{83}{35} & \frac{84}{26} & \frac{106}{23} & \frac{105}{19} & \frac{78}{15} & \frac{73}{10} & \frac{68}{9} & \frac{69}{10} & \frac{71}{14} & \frac{85}{19} & \frac{80}{32} & \frac{79}{50} \end{array}$$

$$\text{L.O. } \begin{array}{cccccccccccccccc} \frac{48}{35} & \frac{49}{27} & \frac{70}{24} & \frac{69}{20} & \frac{46}{15} & \frac{38}{9} & \frac{25}{9} & \frac{36}{9} & \frac{38}{14} & \frac{46}{19} & \frac{44}{31} & \frac{44}{50} \end{array}$$

$$\text{L.O. } \begin{array}{cccccccccccccccc} \frac{51}{35} & \frac{51}{27} & \frac{73}{23} & \frac{74}{19} & \frac{49}{15} & \frac{93}{9} & \frac{39}{9} & \frac{40}{9} & \frac{44}{15} & \frac{49}{19} & \frac{44}{31} & \frac{44}{50} \end{array}$$

$$\text{L.O. } \begin{array}{cccccccccccccccc} \frac{59}{35} & \frac{62}{28} & \frac{80}{25} & \frac{85}{21} & \frac{80}{19} & \frac{56}{14} & \frac{51}{9} & \frac{46}{9} & \frac{49}{10} & \frac{52}{14} & \frac{61}{19} & \frac{52}{33} & \frac{48}{50} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{66}{50} & \frac{68}{35} & \frac{70}{30} & \frac{97}{25} & \frac{88}{21} & \frac{58}{13} & \frac{54}{8} & \frac{51}{10} & \frac{54}{14} & \frac{58}{19} & \frac{80}{32} & \frac{73}{50} \end{array}$$

Sta	+	Σ	-	Elev.
		908.80 909.80		
+50			03.8	02.8
60			04.3	03.3
+08	& Culv. & Ditch			
+30			04.9	03.9
+65			06.5	05.5
61		921.17	08.3	07.3
T.P.	13.81	922.17	1.44	907.36 908.36
+50			10.9	09.9
62			12.9	11.9
+50			15.1	14.1
63			17.2	16.2
+50			19.6	18.6

LH

R

RH

L.O. $\frac{73}{35} \frac{86}{32} \frac{96}{28} \frac{100}{22} \frac{81}{20} \frac{68}{12} \frac{68}{9} \frac{60}{-} \frac{60}{10} \frac{60}{14} \frac{74}{28} \frac{97}{31} \frac{95}{37} \frac{81}{43} \frac{73}{50}$

L.O. $\frac{72}{35} \frac{81}{30} \frac{100}{28} \frac{96}{27} \frac{84}{21} \frac{60}{13} \frac{57}{9} \frac{55}{-} \frac{57}{10} \frac{59}{14} \frac{66}{23} \frac{85}{27} \frac{101}{30} \frac{100}{38} \frac{88}{40}$ L.O.

901.43

899.7

902.43

900.7

737

91

905

00.75

99.75

El. Water 3/31/59

$\frac{65}{30} \frac{68}{32} \frac{80}{30} \frac{97}{26} \frac{87}{24} \frac{65}{21} \frac{51}{14} \frac{50}{9} \frac{49}{-} \frac{52}{11} \frac{53}{15} \frac{69}{24} \frac{90}{26} \frac{97}{28}$ L.O.

$\frac{51}{30} \frac{50}{34} \frac{56}{28} \frac{78}{25} \frac{78}{23} \frac{43}{18} \frac{32}{11} \frac{33}{7} \frac{33}{-} \frac{36}{11} \frac{39}{15} \frac{60}{27} \frac{86}{30} \frac{97}{32}$ L.O.

$\frac{42}{30} \frac{46}{33} \frac{49}{28} \frac{68}{25} \frac{68}{24} \frac{30}{18} \frac{19}{12} \frac{17}{8} \frac{15}{-} \frac{19}{11} \frac{21}{14} \frac{38}{24} \frac{70}{30} \frac{73}{34} \frac{79}{50}$

$\frac{170}{30} \frac{170}{28} \frac{138}{21} \frac{119}{12} \frac{116}{8} \frac{113}{-} \frac{115}{9} \frac{132}{21} \frac{165}{28} \frac{161}{30}$

L.O. $\frac{170}{35} \frac{118}{24} \frac{102}{15} \frac{96}{8} \frac{93}{-} \frac{94}{10} \frac{111}{21} \frac{152}{32} \frac{157}{50}$

L.O. $\frac{107}{35} \frac{95}{21} \frac{74}{8} \frac{71}{-} \frac{72}{10} \frac{83}{21} \frac{121}{29} \frac{126}{50} \frac{95}{100} \frac{81}{121} \frac{66}{150}$

$\frac{173}{30} \frac{179}{44} \frac{79}{24} \frac{65}{18} \frac{54}{10} \frac{50}{-} \frac{52}{10} \frac{65}{20} \frac{87}{26} \frac{88}{41} \frac{80}{50} \frac{74}{58} \frac{17}{90} \frac{112}{141} \frac{196}{172}$

$\frac{122}{30} \frac{110}{37}$

$\frac{49}{25} \frac{35}{16} \frac{29}{9} \frac{26}{-} \frac{27}{9} \frac{32}{14} \frac{53}{23} \frac{53}{24} \frac{46}{25} \frac{90}{50} \frac{177}{73} \frac{196}{100} \frac{108}{150}$

+ $\frac{112}{181}$

Sta	+	Σ	-	Elcv.	
		921.17 922.17			
63	+85			21.2	20.2
64		932.95		21.8	20.8
T.P.	12.87	933.95	1.09	920.08 921.08	
63	+85			21.2	20.2
64				21.8	20.8
	+30			23.2	22.2
	+65			24.6	23.6
65		935.84		26.0	25.0
B.M.	7.74	936.84	4.84	929.11 <u>929.15</u>	928.10 <u>928.10</u>
	+50			27.5	26.5
	+72			28.4	27.4
	+80			28.6	27.6
	+94.4			29.6	28.6

2" H²

Lt

L

Rt

$$\frac{97}{50} \frac{86}{41} \frac{3.9}{27} \frac{16}{16}$$

$$\frac{13}{10}$$

$$\frac{10}{9} \frac{12}{15} \frac{14}{22}$$

$$\frac{78}{50} \frac{61}{39} \frac{28}{32} \frac{20}{25} \frac{31}{23} \frac{29}{19} \frac{10}{15} \frac{95}{10}$$

$$\frac{04}{9} \frac{0.6}{9} \frac{0.5}{20}$$

(12.8)

$$\frac{66}{36} \frac{48}{50} \frac{+0.5}{100} \frac{+0.3}{150}$$

(12.2)

$$\frac{4.2}{35} \frac{2.6}{50} \frac{+1.2}{100} \frac{+0.8}{150}$$

$$\frac{117}{50} \frac{103}{40}$$

$$\frac{94}{36} \frac{130}{25}$$

$$\frac{132}{21} \frac{118}{19}$$

$$\frac{110}{9}$$

$$\frac{108}{8} \frac{111}{16}$$

$$\frac{113}{34} \frac{52}{50}$$

$$\frac{06}{77} \frac{+2.2}{100}$$

$$\frac{+2.7}{150}$$

$$\frac{127}{150}$$

$$\frac{6068}{50} \frac{72}{40} \frac{98}{27} \frac{107}{26} \frac{141}{23} \frac{105}{22} \frac{98}{15} \frac{98}{11} \frac{94}{8} \frac{97}{15} \frac{100}{18} \frac{88}{25} \frac{83}{50} \frac{20}{80} \frac{119}{100} \frac{+2.7}{150} \frac{+3.8}{150}$$

$$\frac{45}{50} \frac{56}{35} \frac{70}{28} \frac{95}{24} \frac{95}{21} \frac{85}{17} \frac{83}{10} \frac{80}{9} \frac{83}{16} \frac{84}{32} \frac{61}{30} \frac{31}{80} \frac{119}{120} \frac{+5.5}{150} \frac{+6.3}{150}$$

Spike in R.P. Lt 54.65180

$$\frac{51}{50} \frac{65}{36} \frac{15}{29} \frac{110}{23} \frac{110}{20} \frac{86}{16} \frac{94}{10} \frac{93}{9} \frac{98}{15} \frac{100}{50} \frac{62}{65} \frac{47}{88} \frac{03}{130} \frac{+3.3}{150} \frac{-36}{150}$$

$$\frac{44}{50} \frac{63}{35} \frac{102}{25} \frac{101}{21} \frac{94}{17} \frac{88}{11}$$

$$\frac{84}{28} \frac{92}{40} \frac{76}{50} \frac{62}{100} \frac{+1.0}{120} \frac{+2.4}{150}$$

$$\frac{40}{50} \frac{69}{35} \frac{104}{29} \frac{98}{20} \frac{90}{16} \frac{85}{10} \frac{82}{9} \frac{92}{24} \frac{81}{53} \frac{77}{50} \frac{61}{100} \frac{51}{150}$$

$$\frac{37}{50} \frac{52}{35} \frac{96}{27} \frac{97}{25} \frac{92}{22} \frac{78}{16}$$

$$\frac{72}{30} \frac{63}{100} \frac{51}{150}$$

Sta	+	935.84 986.84	-	Elev
66	+24		30.4	29.4
	+43		30.7	29.7
	+70		31.3	30.3
67			32.1	31.1
	+35		32.9	31.9
	+50		33.2	32.2
68			34.3	33.3
	+50		35.8	34.8
69			37.4	36.4
B.M.		774	928.10 929.10	<u>928.10</u> 928.10

Lt

6

Rt

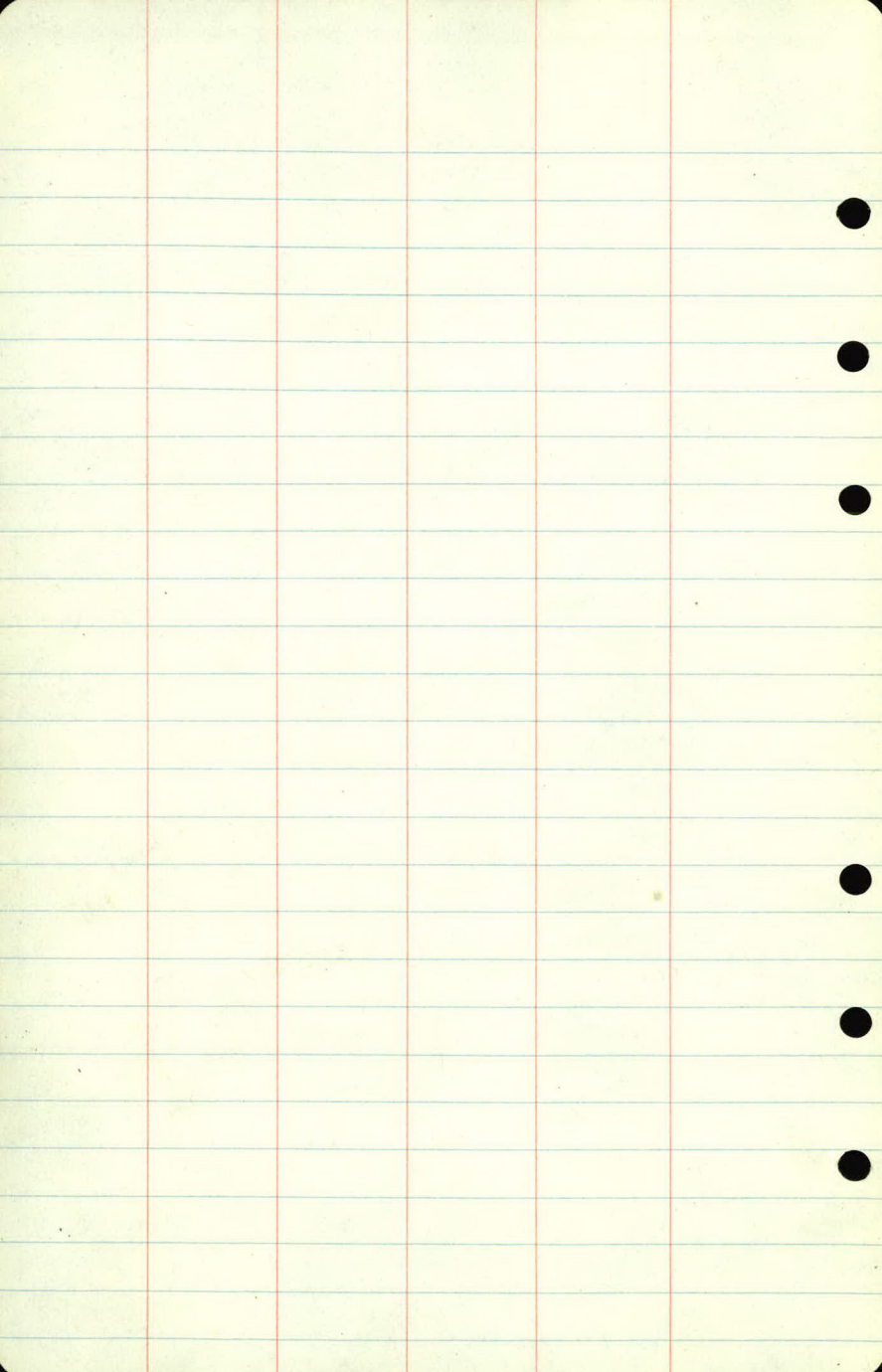
49

$$\frac{72}{38} \quad \frac{69}{50} \quad \frac{58}{100} \quad \frac{51}{150}$$

$$\frac{41}{24} \quad \frac{71}{25} \quad \frac{67}{50} \quad \frac{65}{66} \quad \frac{05}{100} \quad \frac{03}{150} \quad \frac{12}{150}$$

$$\frac{55}{12} \quad \frac{60}{19} \quad \frac{78}{23} \quad \frac{65}{31} \quad \frac{06}{50} \quad \frac{12}{50} \quad \frac{27}{100} \quad \frac{32}{150}$$

$$\frac{47}{8} \quad \frac{50}{13} \quad \frac{59}{17} \quad \frac{70}{21} \quad \frac{70}{27} \quad \frac{27}{50} \quad \frac{32}{100} \quad \frac{51}{100}$$
39 $\frac{41}{8}$ $\frac{50}{17}$ $\frac{50}{21}$ $\frac{67}{50}$ 362510106



X Sections

Borrow Pit.

RA 519 - 62 to 66 + 064

Sta	+	π	-	Elev.
B.M.	9.57	938.67.		929.10

62				12.9
----	--	--	--	------

+50				15.1
-----	--	--	--	------

63				17.2
----	--	--	--	------

I.P.	9.09	945.05	2.71	935.96.
------	------	--------	------	---------

62	+50			12.9
----	-----	--	--	------

64	+50			15.1
----	-----	--	--	------

63	+50			17.2
----	-----	--	--	------

+50				19.6
-----	--	--	--	------

64				21.8
----	--	--	--	------

+30				23.2
-----	--	--	--	------

+65				24.6
-----	--	--	--	------

E

R1

Spike in R.P.Lt. sta 65+80

25.8

29.5	156	197	15.4	101	78	51	25
200	264	300	351	400	475	462	500

23.6

180	156	129	104	99	76	41	0.2
200	253	300	327	360	400	450	500

21.5

116	89	74	8.2	80	69	64	39	0.6
200	239	265	300	316	326	359	400	445

32.2

74	57	36	43	51	50
550	600	610	650	700	750

30.0

52	50	58	55	55
523	567	600	650	700

27.9

45	45	49	48	59
500	550	600	650	700

25.5

121	105	81	90	102	81	68	41	47	51	53	59	69	72
200	245	287	300	322	365	400	475	500	550	600	650	677	700

23.3

98	87	58	55	61	47	34	32	43	48	46	49	67	93
200	230	273	300	334	400	432	474	500	547	581	600	650	700

21.9

52	70	52	49	54	42	37	52	54	59	64
200	229	262	300	331	400	450	500	550	582	600

20.5

60	44	47	62	66	59	47	51	62	80	103
200	245	270	300	329	370	400	450	500	550	600

Sta.	+	π	-	Elev.
		945.05		
65				26.0
	150			27.5
	172			28.4
	180			28.6
66	106.4	2. H ²		29.6
T.P.	375	940.60	8.20	936.85
B.M.			4.08	926.52
T.P.	6.81	935.83	11.58	929.02
B.M.			6.70	922.13

K

Rt.

19.1

$$\frac{39}{200} \quad \frac{35}{230} \quad \frac{43}{263} \quad \frac{66}{300} \quad \frac{73}{330} \quad \frac{67}{368} \quad \frac{60}{400} \quad \frac{63}{450} \quad \frac{73}{500} \quad \frac{83}{533} \quad \frac{118}{573} \quad \frac{129}{600}$$

17.6

$$\frac{56}{200} \quad \frac{46}{247} \quad \frac{63}{300} \quad \frac{69}{350} \quad \frac{80}{400} \quad \frac{86}{450} \quad \frac{103}{500} \quad \frac{128}{550} \quad \frac{145}{600}$$

16.7

$$\frac{57}{200} \quad \frac{52}{250} \quad \frac{42}{272} \quad \frac{51}{300} \quad \frac{64}{332} \quad \frac{74}{373} \quad \frac{79}{400} \quad \frac{88}{450} \quad \frac{96}{480} \quad \frac{108}{500}$$

16.5

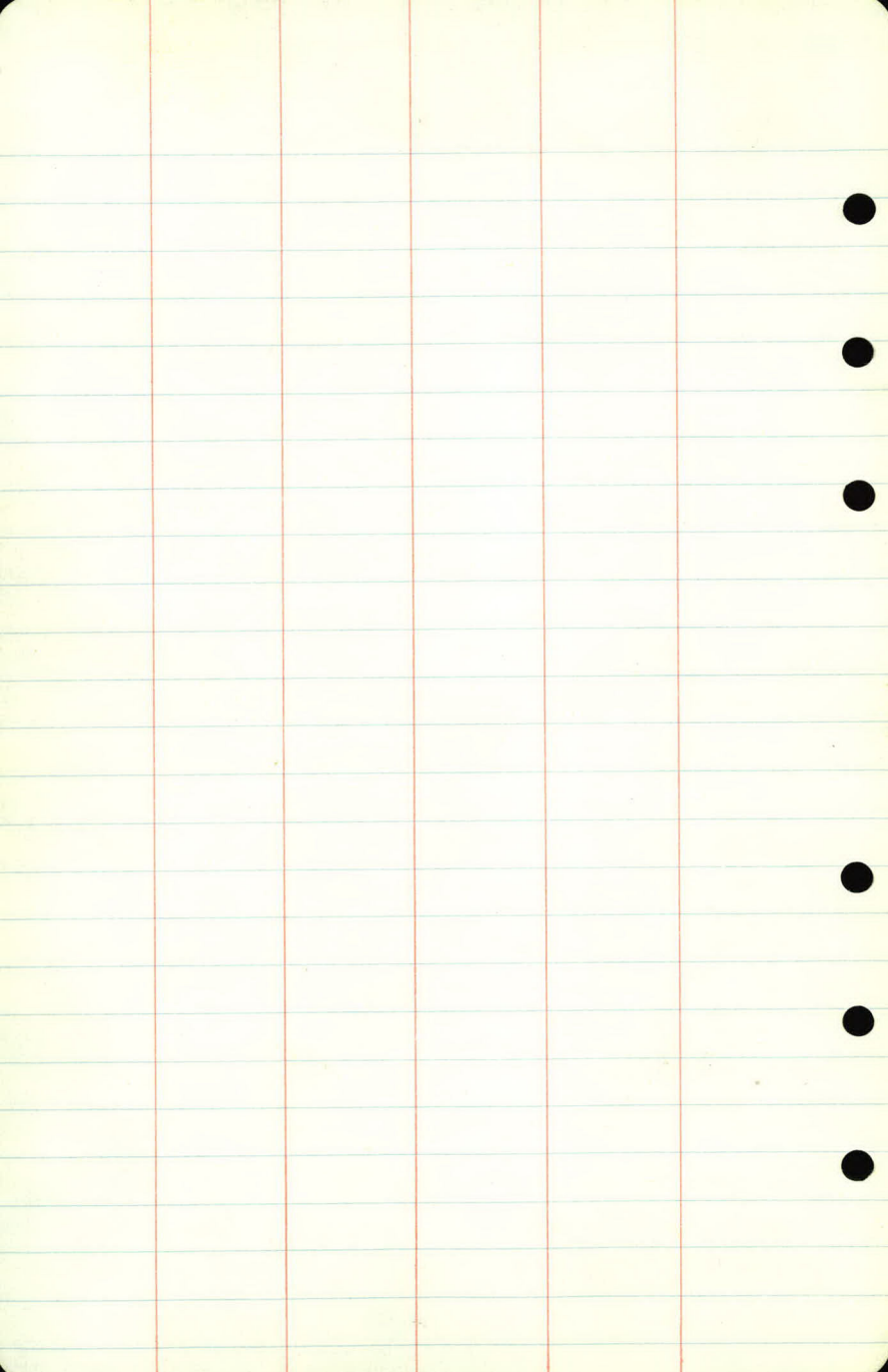
$$\frac{119}{200} \quad \frac{109}{250} \quad \frac{101}{300} \quad \frac{96}{350} \quad \frac{197}{400} \quad \frac{98}{450} \quad \frac{108}{500}$$

15.5

$$\frac{111}{200} \quad \frac{100}{250} \quad \frac{93}{300} \quad \frac{89}{350} \quad \frac{98}{400} \quad \frac{88}{450} \quad \frac{89}{500}$$

Nail in W. side S.W. Cor. Tool Shed.

Spike in P.P.Lt 65150

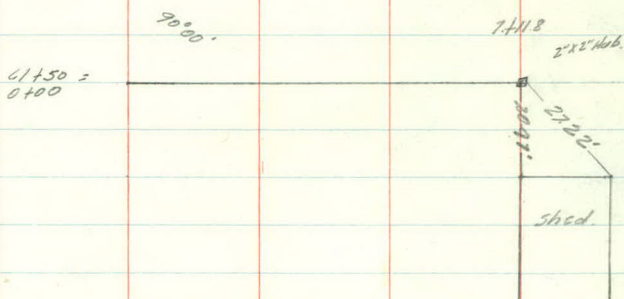
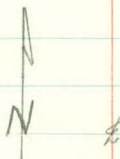


5/15/39
K.A.
L.O.H.
L.G.
A.B.
A.M.
L.G.

39

Xsections

Bures Gravel Pit



Sta.	+	-	Elev.
B.M.	8.20	927.30	929.10
T.P.	0.55	928.32	927.77
T.P.	6.56	926.06	919.50
3	+00		12.5
	+40		15.5
	+50		18.0
	+60		18.3
	+70		15.6
	+89		15.8
4	+1		16.1
	+20		16.3
	+57		17.6
5			20.7
T.P.	6.68	932.93	925.75

Lt

L

Rt

Spike in RR 4465180

$$\frac{70}{50} \quad \frac{113}{20} \quad \frac{136}{28} \quad \frac{172}{50} \quad \frac{185}{50}$$

$$\frac{35}{50} \quad \frac{50}{32} \quad \frac{76}{17} \quad \frac{106}{16} \quad \frac{121}{32} \quad \frac{155}{38} \quad \frac{162}{50} \quad \frac{185}{50}$$

$$\frac{27}{50} \quad \frac{28}{38} \quad \frac{59}{15} \quad \frac{81}{9} \quad \frac{111}{22} \quad \frac{115}{45} \quad \frac{176}{50} \quad \frac{183}{50}$$

$$\frac{17}{50} \quad \frac{18}{39} \quad \frac{21}{29} \quad \frac{51}{12} \quad \frac{78}{16} \quad \frac{109}{9} \quad \frac{112}{29} \quad \frac{127}{36} \quad \frac{153}{42} \quad \frac{175}{50}$$

$$\frac{12}{50} \quad \frac{15}{30} \quad \frac{84}{16} \quad \frac{105}{12} \quad \frac{107}{39} \quad \frac{113}{46} \quad \frac{155}{50} \quad \frac{174}{50}$$

$$\frac{109}{50} \quad \frac{106}{36} \quad \frac{91}{19} \quad \frac{103}{17} \quad \frac{100}{26} \quad \frac{98}{39} \quad \frac{107}{50} \quad \frac{122}{59} \quad \frac{127}{77} \quad \frac{170}{77}$$

$$\frac{123}{50} \quad \frac{116}{39} \quad \frac{79}{23} \quad \frac{100}{14} \quad \frac{95}{20} \quad \frac{57}{37} \quad \frac{95}{50} \quad \frac{112}{68} \quad \frac{128}{91} \quad \frac{164}{91}$$

$$\frac{130}{50} \quad \frac{104}{45} \quad \frac{68}{40} \quad \frac{90}{14} \quad \frac{98}{10} \quad \frac{94}{20} \quad \frac{30}{27} \quad \frac{35}{50} \quad \frac{96}{76} \quad \frac{120}{100} \quad \frac{157}{100}$$

$$\frac{16}{26} \quad \frac{87}{76} \quad \frac{83}{4} \quad \frac{85}{8} \quad \frac{81}{25} \quad \frac{105}{46} \quad \frac{14}{67} \quad \frac{66}{100} \quad \frac{116}{100}$$

$$\frac{10}{31} \quad \frac{66}{26} \quad \frac{59}{12} \quad \frac{52}{19} \quad \frac{23}{28} \quad \frac{86}{28}$$

Sta	+	π	-	Elev
		932.93		

4	+57			17.6
---	-----	--	--	------

5				20.7
---	--	--	--	------

	+50			23.0
--	-----	--	--	------

	+57			23.8
--	-----	--	--	------

6				25.5
---	--	--	--	------

	+23			27.4
--	-----	--	--	------

	+51			26.3
--	-----	--	--	------

T.P.	1327	943.71	1.99	930.44
------	------	--------	------	--------

6				25.5
---	--	--	--	------

	+23			27.4
--	-----	--	--	------

	+51			26.3
--	-----	--	--	------

	+78			40.2
--	-----	--	--	------

11

6

21

$$\frac{119}{50} \quad \frac{113}{33} \quad (14.8)$$

$$\frac{137}{50} \quad \frac{137}{48} \quad (11.7) \quad \frac{15}{29} \quad \frac{40}{50} \quad \frac{47}{58} \quad \frac{40}{67} \quad \frac{95}{81} \quad \frac{125}{100} \quad \frac{174}{135} \quad \frac{207}{150}$$

$$\frac{152}{50} \quad \frac{48}{41} \quad \frac{104}{32} \quad \frac{114}{4} \quad \frac{99}{9} \quad \frac{93}{12} \quad \frac{100}{17} \quad \frac{65}{26} \quad \frac{59}{31} \quad \frac{16}{41} \quad \frac{24}{61} \quad \frac{46}{86} \quad \frac{79}{100} \quad \frac{175}{150}$$

$$\frac{160}{50} \quad \frac{30}{43} \quad \frac{73}{33} \quad \frac{84}{20} \quad \frac{86}{8} \quad \frac{55}{22} \quad \frac{42}{30} \quad \frac{25}{48} \quad \frac{17}{72} \quad \frac{43}{100} \quad \frac{55}{108} \quad \frac{74}{113} \quad \frac{98}{133} \quad \frac{167}{145} \quad \frac{21}{200}$$

$$\frac{44}{28} \quad \frac{45}{8} \quad \frac{0.9}{16} \quad \frac{55}{36}$$

$$\frac{50}{11} \quad \frac{68}{25}$$

$$\frac{35}{10} \quad \frac{61}{8} \quad \frac{78}{14} \quad \frac{100}{21} \quad \frac{95}{35}$$

$$\frac{44}{50} \quad \frac{44}{46} \quad (18.2) \quad \frac{7.9}{40} \quad \frac{84}{50} \quad \frac{123}{62} \quad \frac{157}{100}$$

$$\frac{24}{50} \quad \frac{0.6}{38} \quad \frac{11}{41} \quad \frac{23}{27} \quad (16.3) \quad \frac{7.4}{40} \quad \frac{7.3}{50} \quad \frac{65}{56} \quad \frac{11.6}{76} \quad \frac{14.6}{100}$$

$$\frac{30}{50} \quad \frac{20}{38} \quad \frac{20}{25} \quad (17.4) \quad \frac{6.7}{30} \quad \frac{6.9}{56} \quad \frac{51}{61} \quad \frac{56}{68} \quad \frac{11.0}{84} \quad \frac{134}{100}$$

$$\frac{17}{30} \quad \frac{35}{18} \quad \frac{112}{46} \quad \frac{116}{66} \quad \frac{83}{76} \quad \frac{82}{80} \quad \frac{107}{100} \quad \frac{123}{100}$$

Sta.	t	π_1	-	Elev.	
		943.71			
7				38.10	
B.M.	0.49	937.01	7.20	936.51	936.52
6				25.5	
+23				27.4	
+51				26.3	
+78				40.2	

Lt.

R

Rt.

$$\frac{38}{50} \quad \frac{56}{12} \quad \frac{60}{50} \quad \frac{81}{50} \quad \frac{87}{68} \quad \frac{93}{92} \quad \frac{102}{100}$$

N 91° in W side S.W. Cor Tool shed

(11.5)

$$\frac{11.0}{12.2} \quad \frac{148}{144} \quad \frac{201}{169} \quad \frac{251}{200}$$

(09.6)

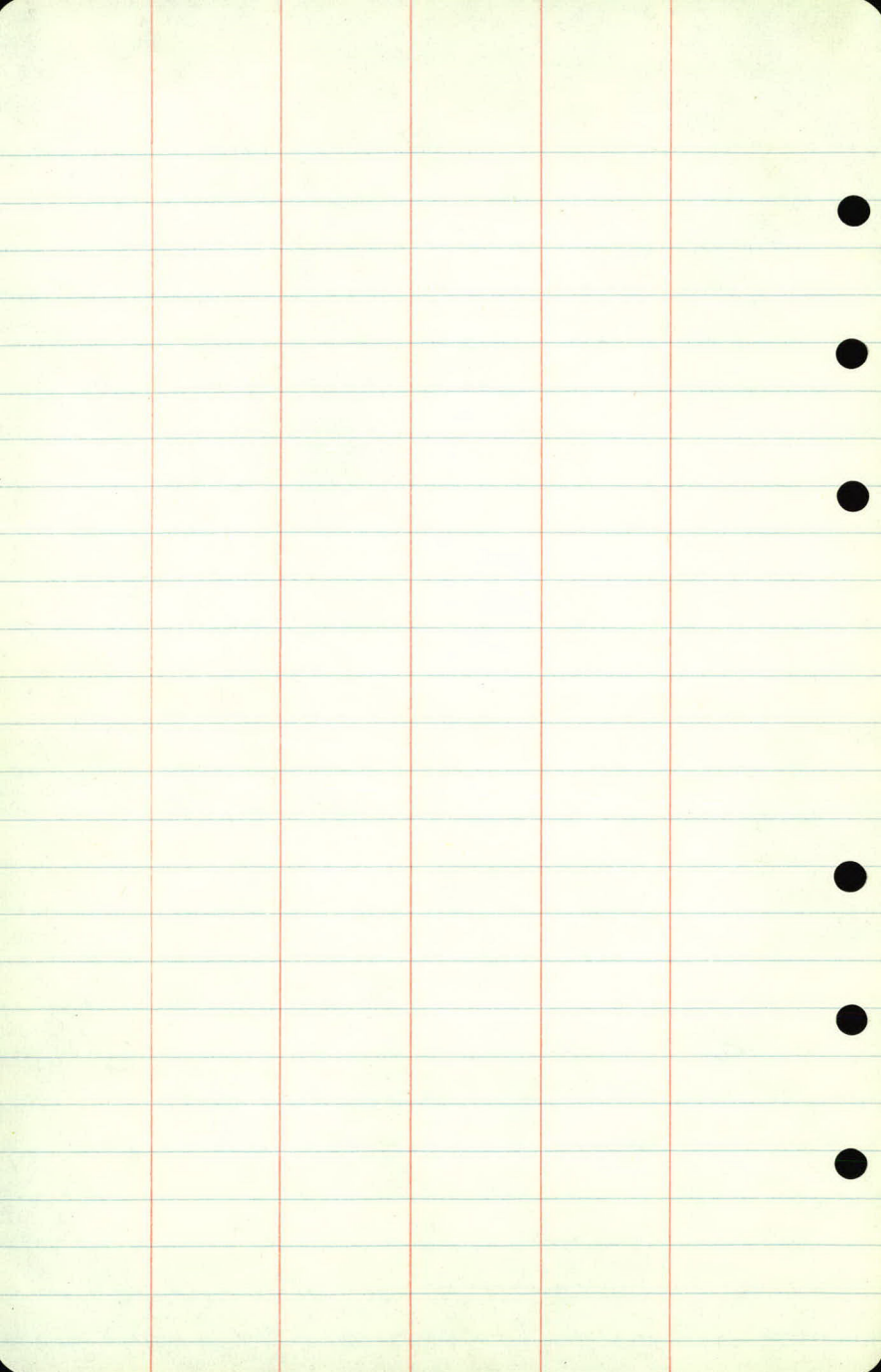
$$\frac{112}{159} \quad \frac{158}{163} \quad \frac{223}{200}$$

(10.7)

$$\frac{12.6}{150} \quad \frac{20.9}{200}$$

+ 3.2

$$\frac{110}{144} \quad \frac{164}{190}$$



Topography
Bures Gravel Pit.

7 H8-Fe Cor-46'

6 Fe-60'

+08-60' Shed-21'
+01-60' Tool Shed-60'

5 Fe-63'

+70-18" Box-60'
+66-12" Box Elder-65'
+38-12" Poplar-54'
+32-24" Poplar-54'

+18-15" stump-48'
+16-12" Poplar-48'

4 Fe-66'

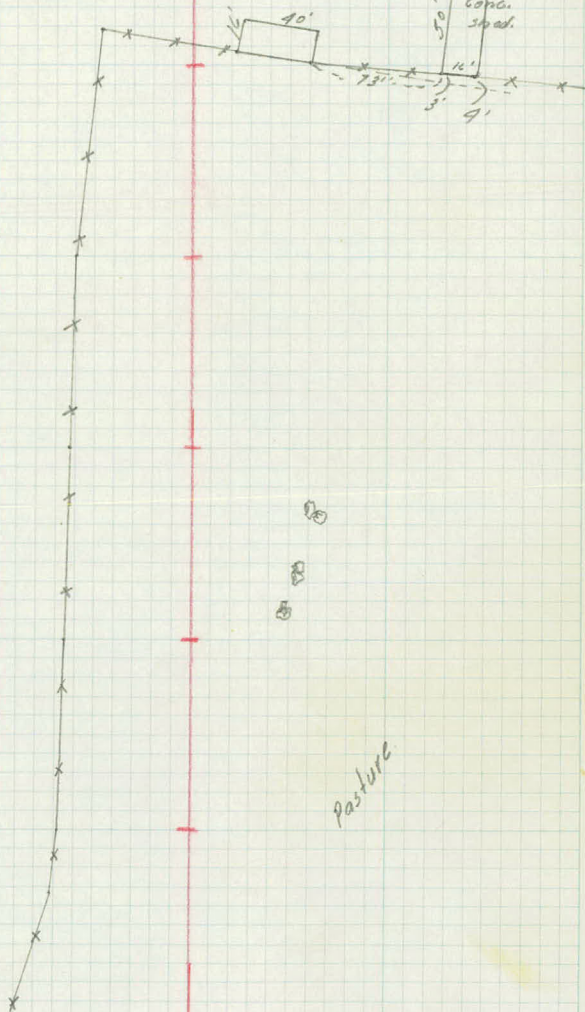
3 Fe-69'

2

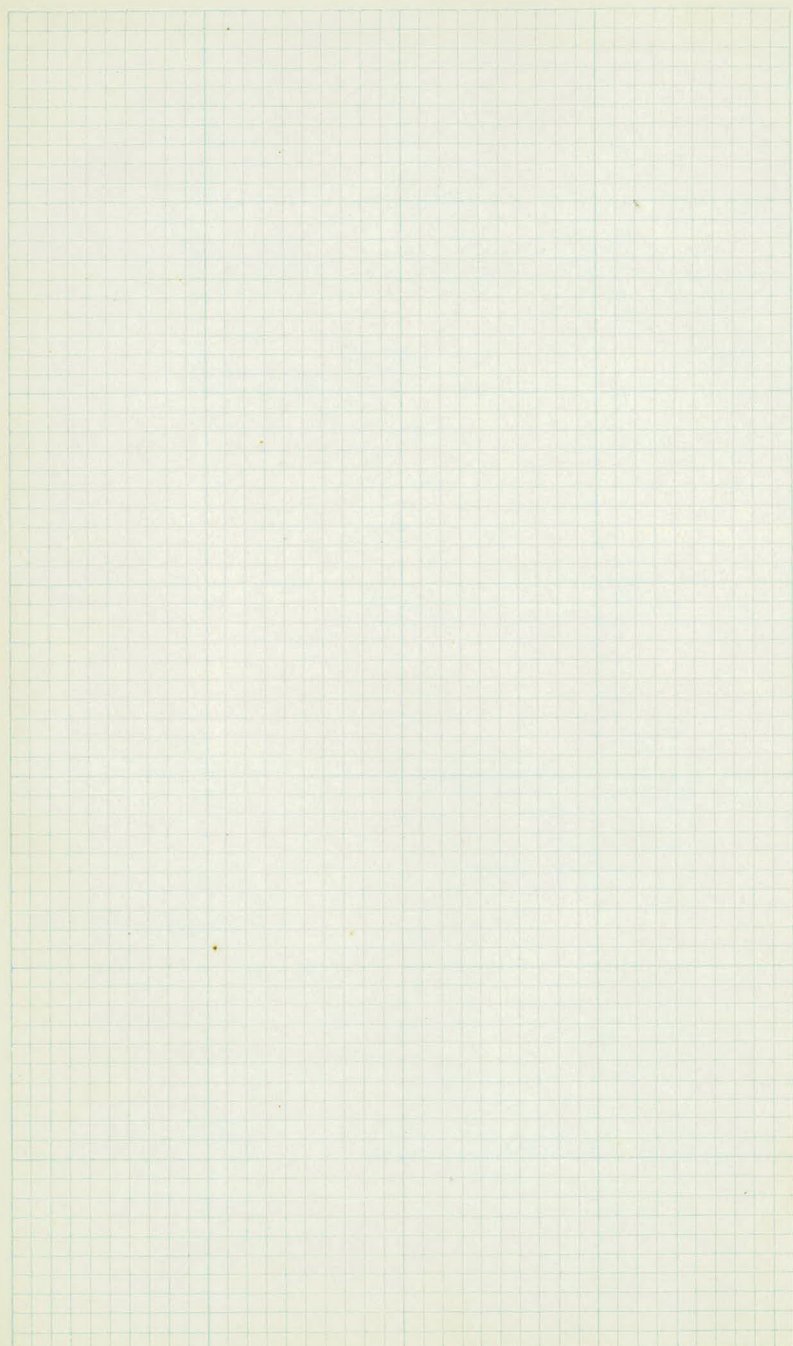
+67-Div Fe-73'

1

cult



Pasture



Borrow pit #5241.4

Xsections

Sta	I	X	-	Elev
B.M.	12.24	920.83		(908.59)
0	+50			09.7
1	+00			14.3
	+28			18.4
	+73			18.0
2				18.3
	+25			18.7
	+50			19.1
3				16.8
	+10 = 0.0			

lt k Rt

Top of Core at Base of A from F.P. Lt 52165

$$\frac{106}{150} \quad \frac{106}{100} \quad \frac{112}{50} \quad \frac{111}{33} \quad \frac{111}{7} \quad \frac{118}{9} \quad \frac{121}{30}$$

$$\frac{118}{150} \quad \frac{90}{100} \quad \frac{79}{50} \quad \frac{65}{6} \quad \frac{63}{13} \quad \frac{106}{33} \quad \frac{110}{33}$$

$$\frac{120}{150} \quad \frac{78}{100} \quad \frac{48}{74} \quad \frac{48}{50} \quad \frac{43}{34} \quad \frac{30}{9} \quad \frac{24}{5} \quad \frac{17}{14} \quad \frac{93}{30} \quad \frac{99}{30}$$

$$\frac{121}{150} \quad \frac{84}{100} \quad \frac{40}{68} \quad \frac{31}{50} \quad \frac{35}{20} \quad \frac{28}{5} \quad \frac{22}{14} \quad \frac{77}{30} \quad \frac{78}{30}$$

$$\frac{92}{100} \quad \frac{50}{6} \quad \frac{46}{50} \quad \frac{25}{5} \quad \frac{17}{15} \quad \frac{70}{30} \quad \frac{65}{30}$$

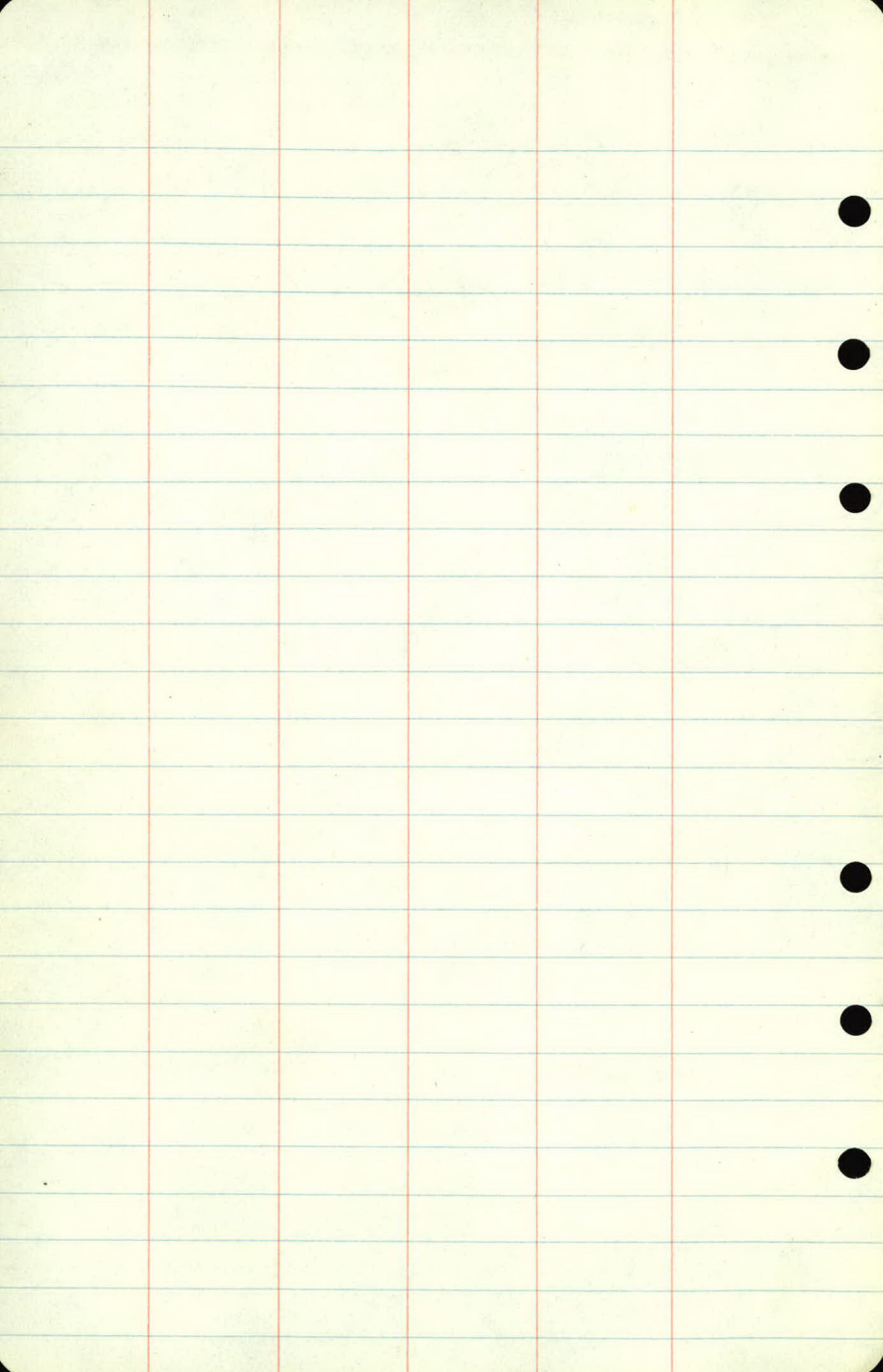
$$\frac{99}{100} \quad \frac{62}{50} \quad \frac{21}{6} \quad \frac{12}{15} \quad \frac{62}{15} \quad \frac{55}{30}$$

$$\frac{97}{50} \quad \frac{40}{22} \quad \frac{17}{5} \quad \frac{83}{14} \quad \frac{55}{30} \quad \frac{47}{30}$$

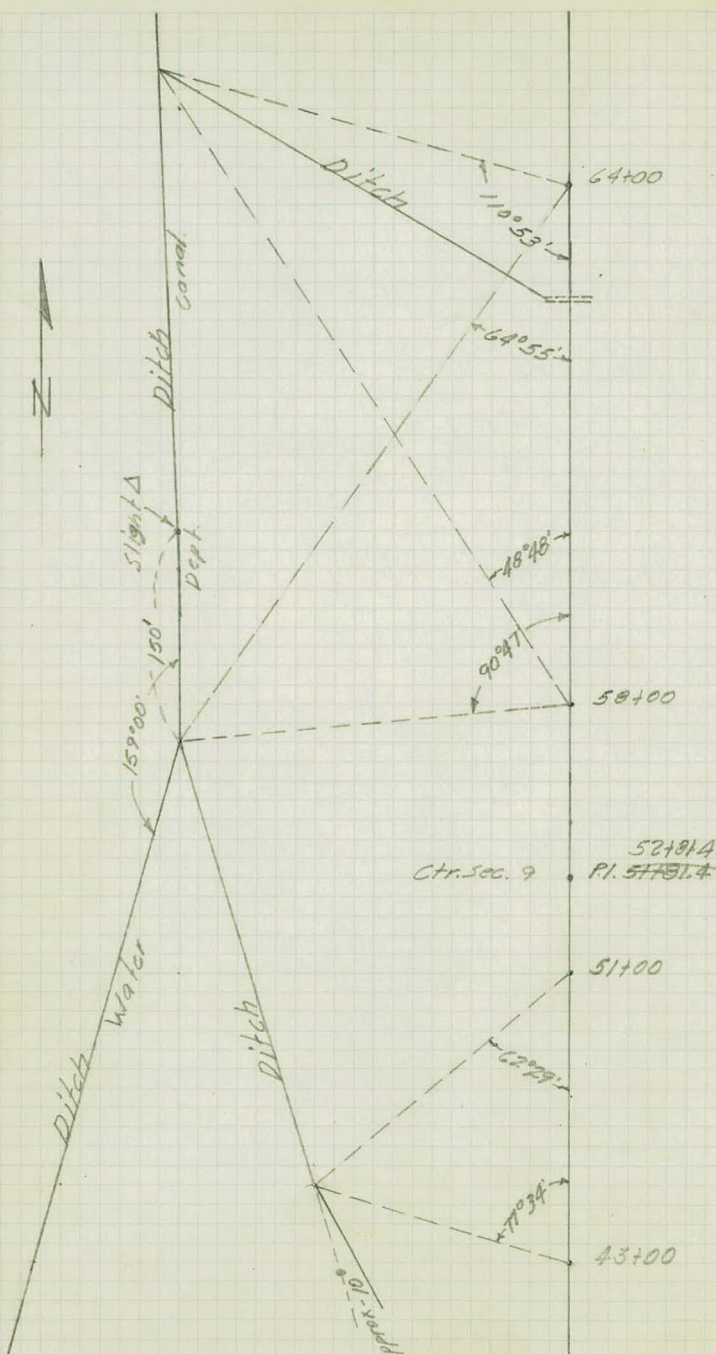
$$\frac{98}{50}$$

$$\frac{40}{6} \quad \frac{24}{12} \quad \frac{45}{12} \quad \frac{40}{30}$$

Hold Grade only to Floor of Low Sheds on Rt.



DITCH
Alignment



Ditch Levels

lt. sta. 60+08

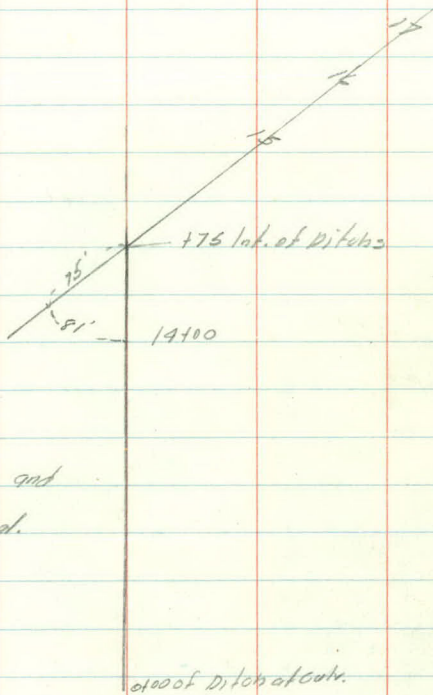
Sta	+	-	Elev.
B.M. = 0+00 W End Culv.	13.65	914.35	(900.7)
1	100	13.6	900.8 (901.8)
2		13.4	01.0
3		13.8	00.6
4		13.6	900.8
175		12.7	901.7
I.P.	425	913.61	4.99 909.36
5		11.9	901.7
6		13.0	900.6
7		13.4	00.2
8		14.0	899.6
9		14.3	899.3
10		14.7	99.9

Flow Line Coll. Lt. Sta. 60108

Clean dead trees out of ditches

#71 - End trees in ditches

Sta.	+	Δ	-	Elev.	Water
		913.61			
11			15.2	98.9	
12			15.8	97.8	
13			16.2	97.4	1.3
14			16.4	97.2	1.1
17.5			17.1	896.5	
15			16.8	96.8	
16			17.8	95.8	2.3
17			17.6	96.0	Running
18			17.2	96.4	
19			17.8	895.8	2.4
T.P.	5.05	908.57	10.09	903.52	
20			12.3	896.4	1.2
				896.3	



Water Dept Canal Runs N.W. and
Sta. continues with Canal.

+40' - 1/2 in Canal Lt.

Clear ditch from here north.

Beg. trees and Brush

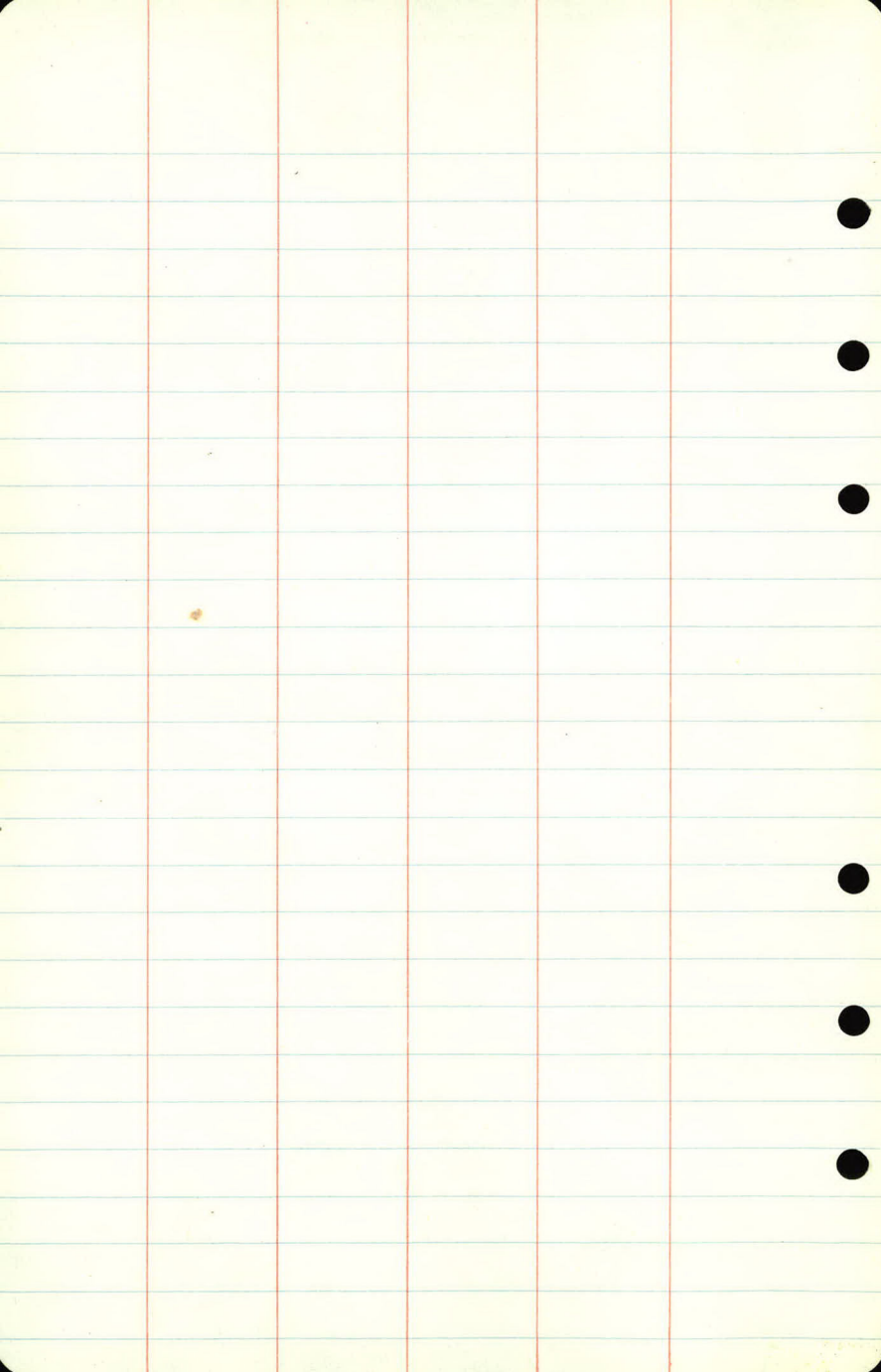
Sta.	+	X	-	Elev.	
		908.57			
21			12.4	96.2	2.1
22			12.4	96.2	2.0
23			12.2	96.4	1.6
24			12.2	96.4	1.6
25			12.1	96.5 96.6	
T.P.	2.10	906.09	4.58	903.29	
+30			9.2	97.0	96.9
26			9.8	96.3	
27			10.4	95.8	95.7
28			10.7	95.4	
29			11.0	95.1	
30			11.0	95.1	
B.M.			3.16	902.93	

Δ Lt.

130 - 2. Rubble Br. - 3' Wide - Wood Deck.

125 Δ Rt.

Top Head Wall S. Mt. Lee Bridge



Levels

Water Dept. Canal Sta. of

Int. of Ditch & Canal. of

Sta. 14+75

Sta	T	X	-	Elev.
T.P.	3.18	906.70		(908.52)

14175
0610 - 60000000

1 100

10.8

96.5

(96.0)

95.9

2

10.5

96.2

3

10.2

96.5

4

10.3

(896.5)

96.4

T.P.

8.31

908.05

6.96

899.74

5

11.6

96.5

6

11.1

897.0

7

10.9

97.2

8

10.7

97.4

+65

10.3

97.8

9

10.0

98.1

10

10.2

97.9

T.P.

3.90

909.03

2.92

905.13

T.P. from 19t

Bog. Cat. clean ditch so.

Sta.	+	-	Elev.
			909.03
B.M.	9.68	909.26	9.45 899.58
10	+10	10.96	898.17 + 898.30
	+10	11.3	980
	+30		
	+30	11.1	998.16
	+59	10.9	78.4
	+63	12.3	97.0
	+81	12.0	97.3
+90 Y in Ditch			
		11.6	97.7
		12.0	97.3
		11.9	97.4

Top N. End Culv. sta. 10+10

Flow Line Culv.

Ground.

Ground.

Flow Line Culv.

Place 36" or Double 36" Culvert.

End clearing ditch

Sta	T	A	-	Elev.
		909.26		
14			11.6	97.7
15			11.7	897.6
16			11.7	97.6
17			12.1	97.2
T.P.	7.83	908.23	8.86	900.40
18			10.9	897.8
19			10.7	98.5 97.5
20			10.8	98.4 97.4
21			10.1	98.1
167			10.0	98.2
189			9.92	898.31
22	10.4		9.60	898.13

Flow Line 18" C.M.

Flow Line 18" C.M.

} Place 36" Culvert

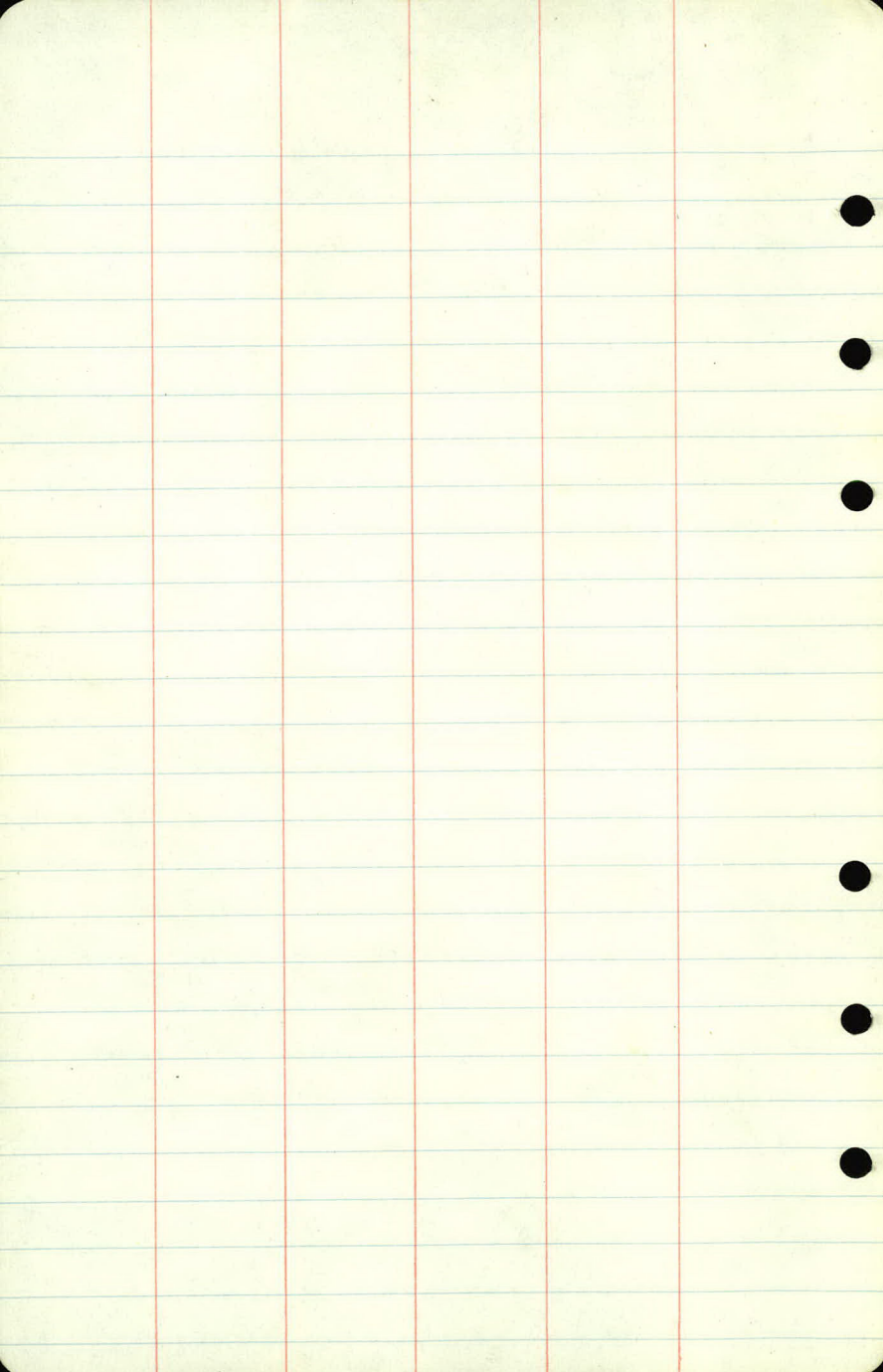
Sta.	T	A	-	Elev.
		908.23		
22	106		10.1	95.1
	130		10.4	97.8
23			10.5	97.7
	167		10.8	97.4
24			10.5	97.7
25			11.0	97.2
26			11.0	97.2
T.P.	975	915.35	2.63	905.60
B.M.			6.84	908.51

908.59

Δ Lt.

26+ = End ditch

Top of Cons. at Base of Δ Iron Ec. Post 33' Lt. 52165



1 Sections

Bures Bottom Pit

Base Line 61+50 Rt.

Sta	+	π	-	FL-0V
B.M	6.29	⁴ 935.39 ✓		⁸ 928.10
31	0.57	² 928.11 ✓	12.85	¹ 928.54 ✓
3+00			11.5	12.5
				14.5
+40				15.5
				16.8
+50				17.8
				17.0
+60				18.0
				14.6
+70				15.6
				14.5
+89				15.5
				15.1
4+00				16.1
				15.2
+20				16.2
				15.7
		927.03		914.71 ✓
T.P.	12.32	928.03 ✓	7.40	915.71 ✓

27

2

R+

2

Nail P.P. L1 Sto 65 100

$$\frac{1.0}{69} \frac{9.7}{9} 10.6 \frac{14.3}{30} \frac{17.2}{100} \frac{18.5}{200} \frac{17.7}{284FC}$$

$$\frac{0.6}{69} \frac{1.2}{50} \frac{2.7}{28} 7.6 \frac{8.8}{6} \frac{9.1}{19} \frac{14.0}{42} \frac{15.9}{100} \frac{18.5}{200} \frac{17.8}{288FC}$$

$$\frac{0.6}{50} \frac{0.8}{35} \frac{3.5}{16} 5.3 \frac{8.1}{10} \frac{8.3}{23} \frac{15.5}{62} \frac{15.9}{100} \frac{18.5}{200} \frac{18.5}{284FC}$$

$$\frac{0.8}{24} 5.1 \frac{7.9}{9} \frac{8.5}{38} \frac{15.2}{64} \frac{15.8}{100} \frac{17.6}{200} \frac{17.8}{284FC}$$

$$\frac{6.7}{9} 7.5 \frac{7.9}{38} \frac{12.6}{51} \frac{15.3}{65} \frac{15.0}{100} \frac{18.2}{200} \frac{18.1}{285FC}$$

$$\frac{7.6}{16} 7.6 \frac{7.3}{24} \frac{9.6}{53} \frac{13.5}{71} \frac{15.7}{100} \frac{17.8}{200} \frac{18.0}{285FC}$$

$$7.0 \frac{7.2}{10} \frac{2.9}{21} \frac{6.6}{37} \frac{9.4}{65} \frac{12.6}{100} \frac{17.4}{200} \frac{18.0}{285FC}$$

$$6.9 \frac{6.6}{8} \frac{0.1}{19} \frac{1.0}{28} \frac{6.5}{47} \frac{8.8}{74} \frac{10.6}{83} \frac{12.9}{100} \frac{17.0}{200} \frac{17.8}{285FC}$$

$$\frac{0.6}{38} \frac{1.0}{21}$$

Sta	+	π	-	Elev
		927.03		
		928.03		

4+20

+57

16.5
~~17.5~~

5+00

933.62

18.2
~~19.2~~
928.15

T.P.

7.47

~~934.62~~

0.88

927.15 ✓

5+00

+50

21.4
~~22.4~~

+87

22.9
~~23.9~~

6+00

24.4
~~25.4~~

+23

26.2
~~27.2~~

+51

25.3
~~26.3~~

937.64 ✓

T.P.

7.30

~~938.64~~

3.28

930.34 ✓
~~931.34~~

B.M

2.15

~~936.49~~
935.49

935.52
~~936.52~~

LT

A

PT

3

$$\frac{1.5}{45} \quad \frac{7.0}{40} \quad \frac{10.1}{22} \quad 11.8$$

$$\begin{array}{r} \frac{1.5}{24} \quad \frac{10.2}{8} \quad 10.5 \quad \frac{10.3}{8} \quad \frac{1.5}{24} \quad \frac{36}{40} \quad \frac{84}{69} \quad \frac{11.3}{80} \quad \frac{15.3}{100} \quad \frac{15.7}{110} \\ \hline \frac{2.0}{289AC} \quad \frac{21.2}{200} \quad \frac{20.2}{148} \\ \hline \frac{8.8}{27} \quad 8.8 \quad \frac{8.8}{12} \quad \frac{5.3}{80} \quad \frac{8.8}{100} \quad \frac{17.3}{148FC} \quad \frac{21.0}{179} \quad \frac{2.0}{200} \end{array}$$

$$15.4 \quad \frac{3.6}{31} \quad \frac{7.1}{56} \quad \frac{6.1}{65}$$

$$\begin{array}{r} 12.8 \quad 12.2 \quad 11.5 \quad 8.5 \quad 6.4 \quad 3.9 \quad 6.9 \quad 8.8 \quad 13.2 \\ \hline \frac{2.8}{28} \quad \frac{1.5}{27} \quad \frac{2.7}{37} \quad \frac{4.4}{44} \quad \frac{8.6}{86} \quad \frac{10.0}{100} \quad \frac{16.3}{163} \\ \hline \frac{1.0}{300} \quad \frac{26.0}{200} \quad \frac{24.0}{186} \quad \frac{21.0}{162FC} \quad \frac{13.7}{137} \\ \hline 9.3 \quad \frac{19.3}{30} \quad \frac{11.4}{13} \quad 10.7 \quad \frac{6.5}{29} \quad \frac{5.2}{40} \quad \frac{4.0}{56} \quad \frac{4.2}{75} \quad \frac{6.2}{100} \quad \frac{7.3}{107} \quad \frac{9.6}{113} \\ \hline \frac{1.0}{300} \quad \frac{27.0}{227} \quad \frac{24.0}{200} \quad \frac{19.4}{168FC} \end{array}$$

$$\begin{array}{r} 6.8 \quad 10.8 \quad 7.6 \quad 6.1 \quad 5.3 \quad 4.9 \quad 3.5 \quad 6.0 \quad 7.5 \\ \hline \frac{2.4}{24} \quad \frac{9.2}{8} \quad \frac{15}{15} \quad \frac{32}{32} \quad \frac{36}{36} \quad \frac{44}{44} \quad \frac{60}{60} \quad \frac{100}{100} \quad \frac{110}{110} \\ \hline \frac{1.0}{300} \quad \frac{33.0}{237} \quad \frac{28.0}{200} \quad \frac{19.0}{170FC} \quad \frac{11.6}{133} \end{array}$$

$$\begin{array}{r} 0.7 \quad 7.4 \quad 9.1 \quad 9.0 \quad 3.6 \quad 3.7 \quad 3.7 \quad 5.6 \quad 7.3 \\ \hline \frac{1.5}{15} \quad \frac{12}{12} \quad \frac{20}{20} \quad \frac{42}{42} \quad \frac{57}{57} \quad \frac{78}{78} \quad \frac{100}{100} \quad \frac{117}{117} \\ \hline \frac{1.0}{300} \quad \frac{33.5}{250} \quad \frac{27.5}{200} \quad \frac{17.5}{174FC} \end{array}$$

$$\frac{5.3}{12} \quad 8.3 \quad \frac{12.4}{17} \quad \frac{11.6}{33}$$

Nail in SW Cor. Tool Shed

Sta	+	Δ	-	Elev
13 M	2.52	938.04 ✓ 939.04		936.52 ✓ 935.52
3+00				

+40

+40

+50

+60

+70

+89

4+00

+20

T.P	7.34	944.46 ✓ 943.46	1.92	937.12 ✓ 936.12
-----	------	-------------------------------	------	-------------------------------

4+00

+20

+57

Lt

2

Nail 117 Tool Speed

$$\begin{array}{r} 0.0 \quad 0.0 \quad 0.2 \quad 2.2 \quad 9.3 \quad 13.5 \\ 300 \quad 273 \quad 231 \quad 200 \quad 144 \quad 100 \end{array}$$

26.5

$$\begin{array}{r} 0.0 \quad 0.0 \quad 3.5 \quad 11.1 \quad 14.0 \\ 300 \quad 256 \quad 200 \quad 100 \quad 70 \end{array}$$

23.5

$$\begin{array}{r} +0.5 \quad 0.0 \quad 3.3 \quad 7.1 \quad 10.7 \quad 13.4 \\ 300 \quad 238 \quad 200 \quad 150 \quad 100 \quad 69 \end{array}$$

21.2

$$\begin{array}{r} +0.5 \quad 0.0 \quad 2.8 \quad 6.8 \quad 10.3 \quad 12.2 \\ 300 \quad 234 \quad 200 \quad 153 \quad 100 \quad 70 \end{array}$$

21.0

$$\begin{array}{r} +0.5 \quad 0.0 \quad 2.7 \quad 5.7 \quad 9.7 \quad 11.4 \quad 12.2 \quad 14.5 \quad 14.6 \\ 300 \quad 236 \quad 200 \quad 160 \quad 100 \quad 70 \quad 64 \quad 44 \quad 30 \end{array}$$

22.4

$$\begin{array}{r} +1.0 \quad +1.0 \quad 0.0 \quad 1.4 \quad 2.8 \quad 8.7 \quad 10.5 \quad 12.5 \\ 300 \quad 252 \quad 223 \quad 200 \quad 179 \quad 100 \quad 67 \quad 36 \end{array}$$

23.5

$$\begin{array}{r} 0.8 \quad 2.2 \quad 7.2 \quad 9.8 \quad 10.2 \quad 11.2 \\ 200 \quad 176 \quad 100 \quad 65 \quad 55 \quad 39 \end{array}$$

22.9

$$\begin{array}{r} 0.2 \quad 2.6 \quad 6.6 \quad 9.6 \quad 9.2 \quad 12.4 \\ 200 \quad 151 \quad 100 \quad 68 \quad 55 \quad 46 \end{array}$$

22.8

$$\begin{array}{r} 3.8 \\ 300 \end{array} \quad \begin{array}{r} 3.9 \\ 250 \end{array}$$

28.4

$$\begin{array}{r} 3.8 \\ 300 \end{array} \quad \begin{array}{r} 3.0 \\ 250 \end{array}$$

28.3

$$\begin{array}{r} 4.9 \quad 2.6 \quad 4.1 \quad 5.3 \quad 9.2 \quad 11.5 \quad 11.1 \\ 300 \quad 250 \quad 200 \quad 162 \quad 100 \quad 58 \quad 33 \end{array}$$

27.0

Sta	+	π	-	Elev
		943.46		
		944.46		

5+00

+50

+87

6

+23

+51

+78

39.3

40.3

+78

7

BM

3.19

938.70

~~939.70~~

7.95

37.2

36.2

935.51

936.51

936.52

935.52

Lt

Z

$$\frac{5.7}{300} \frac{4.1}{257} \frac{3.4}{238} \frac{4.1}{200} \frac{4.2}{130} \frac{5.8}{100} \frac{7.0}{63} \frac{8.3}{50}$$

25.3

$$\frac{7.0}{300} \frac{3.9}{233} \frac{4.6}{200} \frac{4.8}{191} \frac{3.9}{158} \frac{4.7}{100} \frac{5.8}{60} \frac{6.9}{51}$$

22.1

$$\frac{7.9}{300} \frac{4.9}{269} \frac{4.6}{200} \frac{4.2}{158} \frac{5.4}{134} \frac{4.7}{100} \frac{4.9}{60} \frac{6.0}{57}$$

20.6

$$\frac{9.0}{300} \frac{5.0}{256} \frac{4.9}{200} \frac{4.3}{157} \frac{5.5}{137} \frac{5.5}{100} \frac{5.3}{61} \frac{5.3}{47}$$

19.1

$$\frac{10.6}{300} \frac{4.9}{230} \frac{5.5}{200} \frac{4.3}{148} \frac{5.5}{100} \frac{5.0}{71} \frac{3.2}{51} \frac{1.4}{26}$$

17.3

$$\frac{11.4}{300} \frac{5.3}{237} \frac{5.7}{200} \frac{5.7}{176} \frac{4.4}{147} \frac{5.0}{100} \frac{4.8}{75} \frac{4.1}{55} \frac{3.8}{25}$$

18.2

$$\frac{12.3}{300} \frac{7.6}{235} \frac{6.5}{200} \frac{5.2}{154} \frac{5.0}{100} \frac{4.9}{47} 4.2$$

$$\frac{12.3}{300} \frac{10.0}{250} \frac{7.5}{200} \frac{5.3}{152} \frac{4.9}{100} \frac{5.0}{47} 6.3$$

Sta + π - Elev

938.70
~~939.70~~

6+51

+78

7.400

B.M

3.19

935.51

~~936.51~~

2

Rt

13.4

27	30	1.2	1.2	6.6	9.4	130	17.4	20.7	250
50	55	61	66	80	100	132	164	182	200
									314
									250

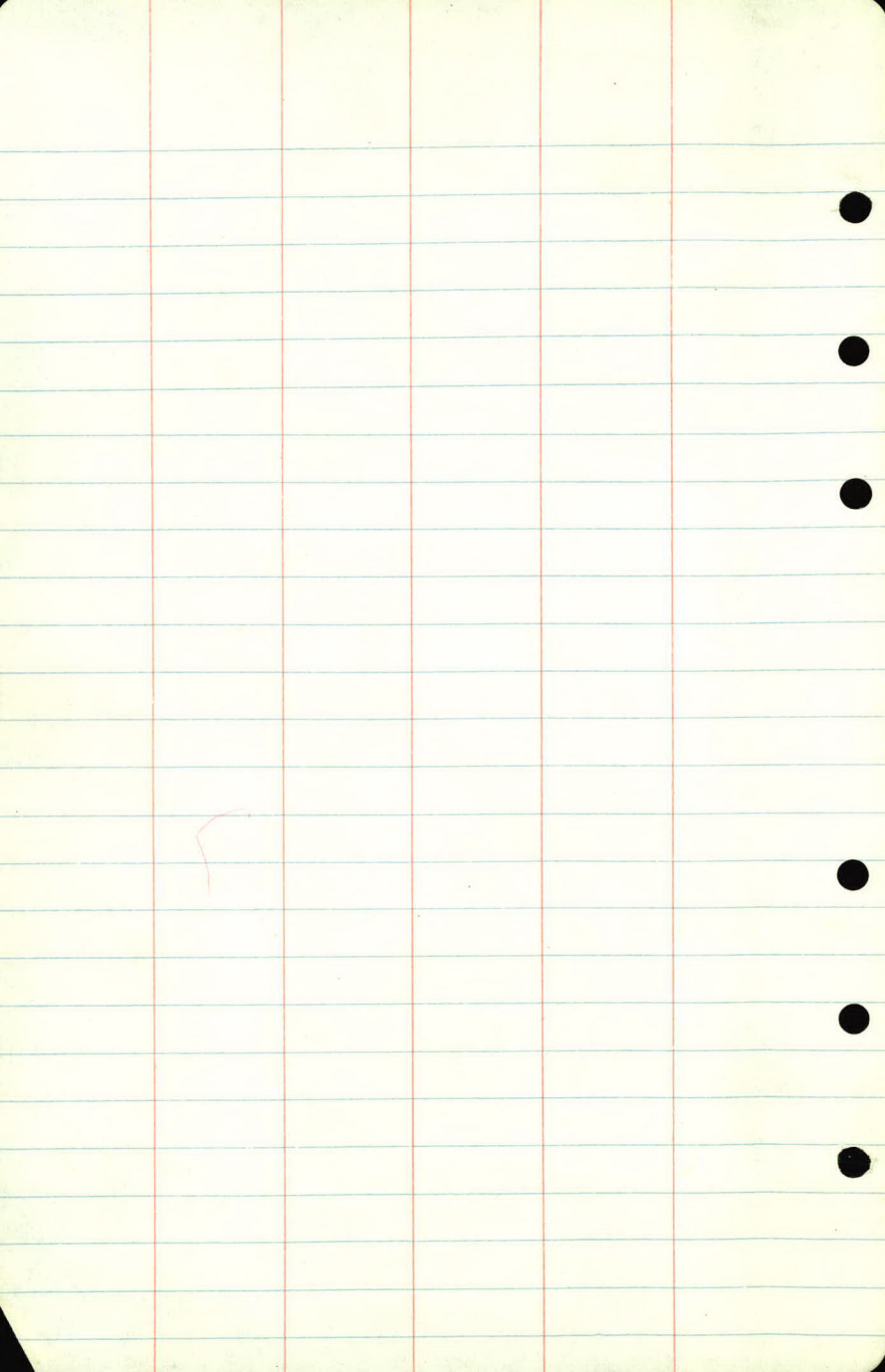
x0.6

7.0	8.4	5.7	6.5	8.3	140	196	22.1	30.0
17	46	72	87	100	146	186	200	259

3.5

1.6	3.4	5.0	7.0	12.7	193	21.1	26.2
10	22	80	100	150	190	200	236

Nail in SE Cor Tool Shrd



Centerville Rd.

Slope stakes

Sta. 3+10 to Sta 19+

Staked at 2:1 Fill Slope.

Sta	+	π	-	Grade	
B.M.	4.89	939.08			934.19

3	+22			43.6	
---	-----	--	--	------	--

	+63			42.4	
--	-----	--	--	------	--

4				407	
T.P.	6.06	934.28	10.86	928.22	

	+50			38.0	
--	-----	--	--	------	--

5				35.3	
---	--	--	--	------	--

	+40			33.1	
--	-----	--	--	------	--

	+70			31.5	
--	-----	--	--	------	--

6				30.3	
---	--	--	--	------	--

T.P.	5.91	927.78	12.41	921.87	
------	------	--------	-------	--------	--

	+50			28.1	
--	-----	--	--	------	--

7				26.2	
---	--	--	--	------	--

B.M.			5.69	922.09	922.06
------	--	--	------	--------	--------

	+50			24.4	
--	-----	--	--	------	--

Gr. Rod Lt k Rt

Top to Red sta. 5400

$$-4.5 \quad 45.4' / \begin{array}{r} 10.7 \\ -15.2 \end{array}$$

$$-3.3 \quad 46.4' / \begin{array}{r} 12.4 \\ -15.7 \end{array}$$

$$\frac{25}{13.1} / 41.2'$$

$$-1.6 \quad 47.4' / \begin{array}{r} 14.6 \\ -16.2 \end{array}$$

$$\frac{12.1}{18.7} / 42.4'$$

$$-3.7 \quad 45.2' / \begin{array}{r} 11.4 \\ -15.1 \end{array}$$

$$\frac{7.9}{17.6} / 38.2'$$

$$-1.0 \quad 32.8' / \begin{array}{r} 10.4 \\ -11.4 \end{array}$$

$$\frac{6.5}{7.5} / 30.0'$$

$$1.2 \quad 30.4' / \begin{array}{r} 8.7 \\ -7.7 \end{array}$$

$$\frac{6.1}{4.9} / 24.8'$$

$$2.8 \quad 30.6' / \begin{array}{r} 10.6 \\ -7.8 \end{array}$$

$$\frac{8.9}{6.1} / 27.2'$$

$$4.0 \quad 33.0' / \begin{array}{r} 13.0 \\ -9.0 \end{array}$$

$$\frac{11.4}{7.4} / 29.8'$$

$$-0.3 \quad 35.2' / \begin{array}{r} 9.8 \\ -10.1 \end{array}$$

$$\frac{7.3}{7.6} / 30.2'$$

$$1.6 \quad 31.8' / \begin{array}{r} 10.0 \\ -8.4 \end{array}$$

$$\frac{8.2}{2.6} / 28.2'$$

Spk. in 24" 0 100 ft. sta 746.5

$$3.4 \quad 28.6' / \begin{array}{r} 10.2 \\ -6.8 \end{array}$$

$$\frac{7.0}{3.4} / 22.2'$$

Sta.	+	π	-	Grade.
		927.78		
8				22.6
+50				20.8
T.P.	4.32	918.87	13.23	914.55
9				19.0
+50				17.2
10				15.5
+50				14.0
11				12.7
+50				11.7
T.P.	3.56	913.99	8.44	910.43
12				10.9
+50				10.3
13				10.0
T.P.	6.16	915.11	5.04	908.95

Gr. Rod

Lt

F

Rt

5.2

$$28.0' \frac{11.7}{-6.5}$$

$$\frac{136}{-55} / 26.0'$$

7.0

$$27.9' \frac{13.0}{-6.0}$$

$$\frac{136}{-66} / 28.2'$$

-0.1

$$26.4' \frac{15.6}{-5.7}$$

$$\frac{72}{-73} / 29.6'$$

1.7

$$27.0' \frac{17.7}{-6.0}$$

$$\frac{80}{-73} / 29.6'$$

3.4

$$27.0' \frac{19.4}{-6.0}$$

$$\frac{108}{-74} / 29.8'$$

4.9

$$26.8' \frac{10.8}{-5.9}$$

$$\frac{121}{-72} / 29.4'$$

6.2

$$25.2' \frac{11.3}{-5.1}$$

$$\frac{132}{-70} / 29.0'$$

7.2

$$24.8' \frac{12.1}{-4.9}$$

$$\frac{135}{-63} / 27.6'$$

3.1

$$24.2' \frac{17}{-4.6}$$

$$\frac{89}{-58} / 26.6'$$

3.7

$$24.6' \frac{8.5}{-4.8}$$

$$\frac{96}{-59} / 26.8'$$

4.0

$$24.9' \frac{8.7}{-4.7}$$

$$\frac{97}{-57} / 26.4'$$

Estg 18400

Sta.	+	π	-	Grade
		915.11		
13	+50			09.8
	+50	Pl. 18" A 48' C. M.	Et + Lt =	905.00
14				09.7
	+50			09.7
15				09.6
	+50			09.6
16				09.5
	+50			09.5
17				09.4
T.P.	3.97	913.46	5.62	909.49
	+50			09.4
18				09.3

Gr. Rod

L

R

R

5.3

$$246' / \frac{101}{-48}$$

$$\frac{103}{-50} / 250'$$

$$24' / \frac{101}{-}$$

$$\frac{101}{-} / 24' \quad 2' \quad 25'$$

5.4

$$244' / \frac{71}{-47}$$

$$\frac{99}{-44} / 23.8'$$

5.4

$$240' / \frac{99}{-45}$$

$$\frac{101}{-47} / 24.4'$$

5.5

$$236' / \frac{98}{-43}$$

$$\frac{100}{-45} / 240'$$

5.5

$$232' / \frac{96}{-41}$$

$$\frac{101}{-46} / 242'$$

5.6

$$246' / \frac{104}{-48}$$

$$\frac{102}{-46} / 242'$$

5.6

$$246' / \frac{104}{-48}$$

$$\frac{104}{-48} / 24.6'$$

5.7

$$242' / \frac{103}{-46}$$

$$\frac{98}{-41} / 23.2'$$

4.1

$$244' / \frac{88}{-47}$$

$$\frac{85}{-43} / 23.6'$$

4.2

$$242' / \frac{88}{-46}$$

$$\frac{89}{-47} / 24.4'$$

sta.	+	π	-	Grade
		913.46		

18	+50			09.3
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19				09.2
----	--	--	--	------

	+50			09.2
--	-----	--	--	------

	+78			09.1
--	-----	--	--	------

20				09.1
----	--	--	--	------

B.M.		5.33	908.13	908.14
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19	+64	1/2 p. 12" X 42' vit Colv.		
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Gr. Red.

Lt

K

Rt

4.2

$$244' \frac{89}{-47}$$

$$\frac{89}{-47} / 24.4$$

4.3

$$238' \frac{87}{-44}$$

$$\frac{87}{-44} / 23.8$$

4.3

$$230' \frac{83}{-40}$$

$$\frac{83}{-40} / 21.8$$

4.4

$$226' \frac{82}{-38}$$

$$\frac{82}{-38} / 21.6$$

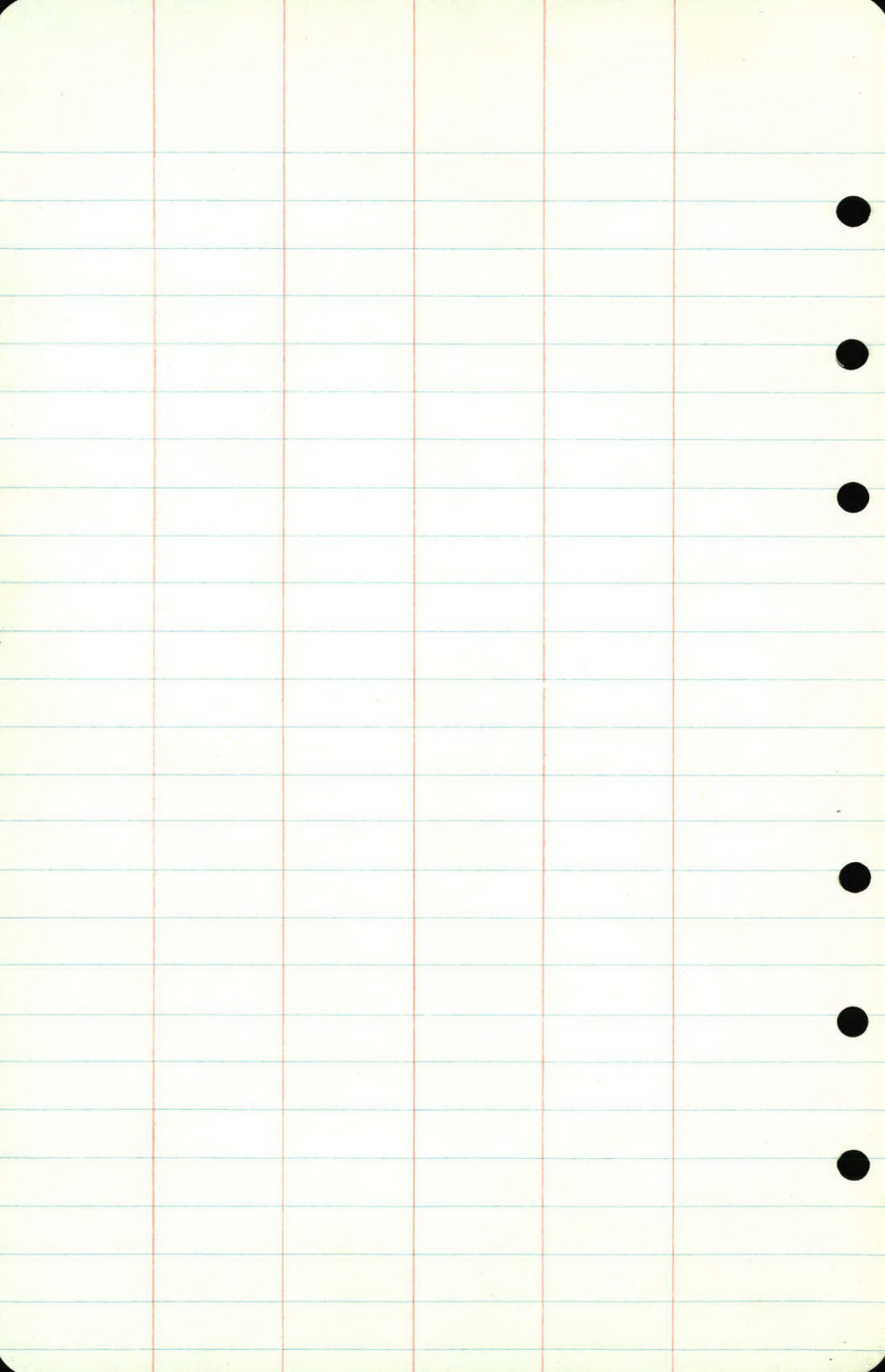
4.4

$$210' \frac{74}{-30}$$

05.0

$$\frac{8.40}{2.0}$$

$$\frac{8.45}{2.2}$$



Slope Stakes
Centerville Rd.

Sta	+	π	-	Grade	
B.M.	0.67	950.58			(949.91)
T.P.	3.28	941.81	12.05	938.53	
3	+10			943.8	
	+22			436	
	+31			43.4	
	+63			42.4	
4				40.7	
	+50			38.0	
T.P.	2.95	937.14	7.62	934.19	
5				35.3	
	+40			33.1	
	+70			31.5	
T.P.	0.58	930.47	7.25	929.89	
6				30.3	
	+50			28.1	

9-11-90
K.R.
L.C.
M.B.

Gr. Rod

Lt.

L

Rt.

Top Mont. & Birch Lake Blvd & Centerville Rd.

-1.8

$$\begin{array}{r} 36.0' / 12.2 \\ \hline 140 \end{array}$$

-1.6

$$\begin{array}{r} 38.1' / 14.2 \\ \hline -15.8 \end{array}$$

$$\begin{array}{r} 11 \\ \hline -2.6 \end{array}$$

-0.6

$$\begin{array}{r} 36.4' / 14.2 \\ \hline -13.6 \end{array}$$

$$\begin{array}{r} 11 \\ \hline -1.7 \end{array}$$

$$\begin{array}{r} 12.5' / 34.7' \\ \hline -13.1 \end{array}$$

1.1

$$\begin{array}{r} 37.4' / 14.0 \\ \hline -14.9 \end{array}$$

$$\begin{array}{r} 33 \\ \hline -2.2 \end{array}$$

$$\begin{array}{r} 15.7' / 36.9' \\ \hline -14.6 \end{array}$$

3.8

$$\begin{array}{r} 37.2' / 18.6 \\ \hline -14.8 \end{array}$$

$$\begin{array}{r} 58 \\ \hline -2.0 \end{array}$$

$$\begin{array}{r} 15.7' / 37.9' \\ \hline -11.9 \end{array}$$

Top & Red sta 5100

1.8

$$\begin{array}{r} 31.5' / 12.8 \\ \hline -11.0 \end{array}$$

$$\begin{array}{r} 30 \\ \hline -1.2 \end{array}$$

$$\begin{array}{r} 58' / 25.5' \\ \hline -7.0 \end{array}$$

4.0

$$\begin{array}{r} 17.6' / 5.7 \\ \hline -1.6 \end{array}$$

$$\begin{array}{r} 45 \\ \hline -0.5 \end{array}$$

$$\begin{array}{r} 91' / 22.7' \\ \hline -5.5 \end{array}$$

5.6

$$\begin{array}{r} 16.4' / 6.5 \\ \hline -0.9 \end{array}$$

$$\begin{array}{r} 59 \\ \hline -0.3 \end{array}$$

$$\begin{array}{r} 11.2' / 23.4' \\ \hline -5.6 \end{array}$$

0.2

$$\begin{array}{r} 21.5' / 4.6 \\ \hline -1.3 \end{array}$$

$$\begin{array}{r} 96 \\ \hline -0.4 \end{array}$$

$$\begin{array}{r} 26' / 26.1' \\ \hline -1.4 \end{array}$$

2.4

$$\begin{array}{r} 29.1' / 11.8 \\ \hline -9.4 \end{array}$$

$$\begin{array}{r} 36 \\ \hline -0.2 \end{array}$$

$$\begin{array}{r} 101' / 26.6' \\ \hline -7.7 \end{array}$$

Sta	+	π	-	Grade
		930.47		
7				26.2
B.M.			8.41	922.06
+50	0.22			24.4
T.P.	0.19	922.75	7.91	922.56
8	41.7			22.6
+50				20.8
9				19.0
+50				17.2
10				15.5
T.P.	0.35	914.62	8.48	914.27
+50				14.0
11				12.7
+50				11.7
12				10.9

G.G. Rod.

Lt

R

Rt.

4.3

$$\frac{282'}{131} / \frac{-88}{-88}$$

$$\frac{42}{101} / \frac{-88}{-88}$$

$$\frac{109}{-66} / \frac{249}{249}$$

Sph. in 24" O. 100' Rt. Sta. 7+6.5

6.1

$$\frac{245'}{12.4} / \frac{-63}{-63}$$

$$\frac{58}{103} / \frac{-63}{-63}$$

$$\frac{81}{-80} / \frac{18.0}{18.0}$$

Sta. 8+00

0.2

$$\frac{245'}{10.5} / \frac{-63}{-63}$$

$$\frac{92}{90} / \frac{-63}{-63}$$

$$\frac{51}{-48} / \frac{22.4}{22.4}$$

2.0

$$\frac{243'}{18.2} / \frac{-62}{-62}$$

$$\frac{24}{-04} / \frac{-62}{-62}$$

$$\frac{86}{-06} / \frac{249}{249}$$

3.8

$$\frac{239'}{19.7} / \frac{-59}{-59}$$

$$\frac{44}{-06} / \frac{-59}{-59}$$

$$\frac{112}{-74} / \frac{20.1}{20.1}$$

5.6

$$\frac{242'}{11.7} / \frac{-61}{-61}$$

$$\frac{00}{-04} / \frac{-61}{-61}$$

$$\frac{132}{-76} / \frac{26.1}{26.1}$$

7.2

$$\frac{242'}{13.3} / \frac{-61}{-61}$$

$$\frac{74}{-02} / \frac{-61}{-61}$$

$$\frac{150}{-78} / \frac{26.1}{26.1}$$

0.6

$$\frac{242'}{16.7} / \frac{-61}{-61}$$

$$\frac{04}{-02} / \frac{-61}{-61}$$

$$\frac{76}{-70} / \frac{25.5}{25.5}$$

Coke STA

1.9

$$\frac{22.9'}{15.9} / \frac{-50}{-50}$$

$$\frac{1.7}{10.2} / \frac{-50}{-50}$$

$$\frac{86}{-47} / \frac{25.1}{25.1}$$

2.9

$$\frac{22.8'}{17.8} / \frac{-49}{-49}$$

$$\frac{30}{-01} / \frac{-49}{-49}$$

$$\frac{91}{-52} / \frac{24.3}{24.3}$$

3.7

$$\frac{22.1'}{18.4} / \frac{-47}{-47}$$

$$\frac{42}{-03} / \frac{-47}{-47}$$

$$\frac{96}{-59} / \frac{23.9}{23.9}$$

Sta	+	π	-	Grade
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$$\begin{array}{r} 914.62 \\ 9.6 \\ \hline 905.0 \end{array}$$

12	+50			10.3
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13				10.0
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Pl. 13" x 44" C.M.

+50	Elev same as slope stake	Bed. Readings	09.8
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14				09.7
----	--	--	--	------

+50				09.7
-----	--	--	--	------

15				09.6
----	--	--	--	------

T.R	3.74	913.91	- 4.45	910.17
-----	------	--------	--------	--------

+50				09.6
-----	--	--	--	------

16				09.5
----	--	--	--	------

+50				09.5
-----	--	--	--	------

17				09.4
----	--	--	--	------

+50				09.4
-----	--	--	--	------

Gr. Rod.

Lt

R

Rt.

4.3

$$\begin{array}{r} 22.4' / 9.2 \\ -4.2 \end{array}$$

$$\begin{array}{r} 54 \\ -11 \end{array}$$

$$\begin{array}{r} 10.1 \\ -5.8 / 23.7 \end{array}$$

4.6

$$\begin{array}{r} 22.2' / 9.4 \\ -4.8 \end{array}$$

$$\begin{array}{r} 56 \\ -10 \end{array}$$

$$\begin{array}{r} 10.3 \\ -5.7 / 23.7 \end{array}$$

4.8

$$\begin{array}{r} 22.2' / 9.6 \\ -4.8 \end{array}$$

$$\begin{array}{r} 50 \\ -0.2 \end{array}$$

$$\begin{array}{r} 9.6 \\ -4.8 / 22.2' \end{array}$$

$$\begin{array}{r} 24.6 \\ 49.2 \end{array} 24'$$

4.9

$$\begin{array}{r} 23.1' / 9.6 \\ -4.7 \end{array}$$

$$\begin{array}{r} 46 \\ 10.3 \end{array}$$

$$\begin{array}{r} 9.8 \\ -4.4 / 21.6' \end{array}$$

4.9

$$\begin{array}{r} 21.3' / 9.1 \\ -4.2 \end{array}$$

$$\begin{array}{r} 4.7 \\ 10.2 \end{array}$$

$$\begin{array}{r} 9.4 \\ -4.5 / 21.8' \end{array}$$

5.0

$$\begin{array}{r} 21.5' / 9.3 \\ -4.3 \end{array}$$

$$\begin{array}{r} 4.4 \\ -0.6 \end{array}$$

$$\begin{array}{r} 9.2 \\ -4.2 / 21.3' \end{array}$$

4.3

$$\begin{array}{r} 20.4' / 9.9 \\ -3.6 \end{array}$$

$$\begin{array}{r} 3.7 \\ 10.6 \end{array}$$

$$\begin{array}{r} 9.3 \\ -4.0 / 21.0' \end{array}$$

4.4

$$\begin{array}{r} 22.1' / 9.1 \\ -4.7 \end{array}$$

$$\begin{array}{r} 4.3 \\ 10.1 \end{array}$$

$$\begin{array}{r} 8.7 \\ -4.3 / 21.5' \end{array}$$

4.4

$$\begin{array}{r} 21.9' / 9.0 \\ -4.6 \end{array}$$

$$\begin{array}{r} 4.5 \\ -0.1 \end{array}$$

$$\begin{array}{r} 9.9 \\ -4.5 / 21.8' \end{array}$$

4.5

$$\begin{array}{r} 21.5' / 8.8 \\ -4.3 \end{array}$$

$$\begin{array}{r} 4.4 \\ 10.1 \end{array}$$

$$\begin{array}{r} 7.9 \\ -3.2 / 20.1' \end{array}$$

4.5

$$\begin{array}{r} 21.9' / 9.1 \\ -4.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ -0.3 \end{array}$$

$$\begin{array}{r} 8.8 \\ -4.3 / 21.5' \end{array}$$

Ditch Rt

Sta	+	π	-	Grade	Gr. Rod.	Grade
		913.91				
18				09.3		
+50				09.3		
19				09.2		
+50				09.2		
+78				09.1		
20				09.1	9.0	04.9
B.M.	4.65	912.79	5.77	908.14		
+33				09.1	7.9	04.9
+76				09.0	8.0	04.8
21				08.9	8.0	04.8
+62				08.6	8.1	04.7
22				08.4	8.1	04.7

8.6

Gr. Rod

Lt

R

Rt

$$4.6 \quad \frac{21.9}{-4.6} \frac{92}{-0.8} \quad \frac{92}{-4.6} \frac{92}{-0.8}$$

$$4.6 \quad \frac{22.1}{-4.7} \frac{93}{-0.7} \quad \frac{91}{-4.5} \frac{91}{-0.7}$$

$$4.7 \quad \frac{21.6}{-4.4} \frac{91}{-0.0} \quad \frac{8.8}{-4.1} \frac{8.8}{-0.2}$$

$$4.7 \quad \frac{20.4}{-3.6} \frac{8.3}{-0.4} \quad \frac{8.2}{-3.5} \frac{8.2}{-0.3}$$

$$4.8 \quad \frac{20.7}{-3.8} \frac{8.6}{-0.7} \quad \frac{7.2}{-2.4} \frac{7.2}{-1.6}$$

$$4.8 \quad \frac{19.7}{-3.1} \frac{7.9}{-0.9} \quad \frac{5.7}{-2.3} \frac{5.7}{-3.0}$$

Spk. in P.P.L.H. Sta. 19+75 28' Lt

$$3.7 \quad \frac{29.0}{-4.0} \frac{2.7}{-0.9} \quad \frac{2.6}{-5.3} \frac{2.6}{-3.0}$$

$$3.8 \quad \frac{33.0}{-3.6} \frac{9.2}{-0.8} \quad \frac{2.5}{-4.5} \frac{2.5}{-3.0}$$

$$3.9 \quad \frac{33.0}{-4.1} \frac{10.2}{-0.7} \quad \frac{2.4}{-4.5} \frac{2.4}{-3.0}$$

$$4.2 \quad \frac{33.0}{-3.6} \frac{10.6}{-0.7} \quad \frac{1.8}{-4.8} \frac{1.8}{-3.0}$$

$$4.4 \quad \frac{33.0}{-3.3} \frac{11}{-0.5} \quad \frac{3.1}{-4.5} \frac{3.1}{-3.0}$$

Ditch Rt

Sta	+	π	-	Grade	Gr. Rod.	Grade
		912.79				
22	+50			08.1	81	04.7
	+75			08.0	82	04.6
23				07.8	82	04.6
	+50			07.5	87	04.1
	+85			07.3	91	03.7
24						03.5
	+10			07.1	94	03.4
	+50			06.9	98	03.0
25				06.6	104	02.4
	+24			06.5	107	02.1
	+50			06.3	109	01.9

Gr. Rod Lt R Rt

4.7 $30.6' / \frac{29}{4.8}$ $\frac{45}{10.2}$ $\frac{54}{42.7 / 31.2}$

4.8

5.0 $30.0' / \frac{35}{4.5}$ $\frac{50}{0.0}$ $\frac{46}{43.6 / 32.6}$

5.3 $26.2' / \frac{57}{4.6}$ $\frac{56}{-0.3}$ $\frac{59}{42.8 / 31.4}$

5.5 $23.0' / \frac{71}{4.04}$ $\frac{61}{-0.6}$ $\frac{78}{41.3 / 28.8'}$

5.7 $22.4' / \frac{94}{3.7}$ $\frac{65}{-0.8}$ $\frac{89}{40.5 / 27.4}$

5.9 $24.8' / \frac{108}{4.9}$ $\frac{70}{-1.1}$ $\frac{98}{40.0 / 26.8'}$

6.2 $23.4' / \frac{104}{4.2}$ $\frac{70}{-0.8}$ $\frac{100}{40.4 / 28.2}$

6.3 $20.0' / \frac{98}{4.5}$ $\frac{71}{-0.8}$ $\frac{91}{41.0 / 29.8'}$

6.5 $19.0' / \frac{85}{4.0}$ $\frac{71}{-0.6}$ $\frac{99}{41.0 / 29.8'}$

Ditch Rt.

Sta	+	π	-	Grade	Gr. Rod. Grade
		912.79			
26				06.0	11.5 ^{28.4} 01.3 v.7
+23					00.8
+31				05.8	
B.M.	5.80	910.05	8.54	904.25	
+36				05.8	
+50				05.7	
+62				05.6	
+68				05.6	Slope stake $\rightarrow$ 904.26
B.M.					<u>904.33</u>
27				05.4	
+50				05.1	
28				04.8	
+50				04.5	
29				04.2	

Gr Rod

Lt

R

Rt

6.8

$$23.4' / \frac{11.0}{-4.2}$$

$$\frac{13}{-97}$$

$$\frac{107}{R.08/30.0'}$$

4.4

$$23.6' / \frac{8.7}{-4.3}$$

$$\frac{52}{-0.8}$$

Top S End 30" C.M. 39' Rt 26+67

4.7

$$21.0' / \frac{7.7}{-3.0}$$

$$\frac{54}{-97}$$

$$\frac{6.0}{R.07/24.4'}$$

5.0

$$24.1' / \frac{2.0}{R.00} \quad 19.8' / \frac{7.4}{-2.4}$$

$$\frac{5.2}{-0.2}$$

$$\frac{6.6}{R.04/23.8'}$$

5.2

$$28.0' / \frac{7.2}{R.00} \quad 19.6' / \frac{7.5}{-2.3}$$

$$\frac{5.0}{+0.2}$$

$$\frac{7.2}{R.16/20.2'}$$

5.5

$$20.4' / \frac{8.2}{-2.7}$$

$$\frac{5.2}{+0.3}$$

$$\frac{6.6}{R.09/24.8'}$$

5.8

$$21.4' / \frac{9.0}{-3.2}$$

$$\frac{5.9}{-0.1}$$

$$\frac{7.3}{R.05/24.0'}$$

Sto	+	π	-	Grade
		910.05		

29	+50			03.9
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30				03.6
T.P.	4.17	906.88	7.34	902.71
	+50			03.3

31				03.2
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	+50			03.0
--	-----	--	--	------

32				03.0
----	--	--	--	------

	+50			↓
--	-----	--	--	---

33				
----	--	--	--	--

	+50			
--	-----	--	--	--

34				
----	--	--	--	--

	+50			↓ 03.0
--	-----	--	--	-----------

Gr. Rod

Lt

Z

Rt.

6.1

$$22.6' / \frac{99}{-58}$$

$$\frac{68}{-0.7}$$

$$\frac{80}{20.1/23.2}$$

6.4

$$21.4' / \frac{96}{-32}$$

$$\frac{74}{-1.0}$$

$$\frac{79}{20.5/24.0}$$

3.6

$$20.8' / \frac{65}{-29}$$

$$\frac{45}{-0.9}$$

$$\frac{54}{20.2/23.4}$$

3.7

$$21.2' / \frac{68}{-3.1}$$

$$\frac{4.7}{-1.0}$$

$$\frac{5.9}{20.3/23.6}$$

3.9

$$21.2' / \frac{70}{-3.1}$$

$$\frac{4.9}{-1.0}$$

$$\frac{5.7}{20.2/23.9}$$

3.9

$$21.2' / \frac{70}{-3.1}$$

$$\frac{4.9}{-1.0}$$

$$\frac{5.8}{20.1/23.2}$$

5.3

3.9

$$21.4' / \frac{21}{-3.2}$$

$$\frac{4.9}{-1.0}$$

$$\frac{6.3}{20.4/19.8}$$

6.7

3.9

$$21.8' / \frac{73}{-3.4}$$

$$\frac{5.0}{-1.1}$$

$$\frac{6.3}{20.4/19.8}$$

6.8

3.9

$$21.6' / \frac{72}{-3.0}$$

$$\frac{5.0}{-1.1}$$

$$\frac{6.6}{20.7/20.4}$$

6.9

3.9

$$21.6' / \frac{72}{-3.3}$$

$$\frac{4.9}{-1.0}$$

$$\frac{6.6}{20.7/20.4}$$

6.9

3.9

$$21.2' / \frac{70}{-3.1}$$

$$\frac{4.9}{-1.0}$$

$$\frac{6.8}{20.7/20.8}$$

6.9

Sta	+	π	-	Grade
		906.88		

35				0.30
T.P.	+ 6.74	907.69	5.93	906.95
+50				

36				
+50				

37				
+50				0.3.0

38				
+50				

39				
+50				

40				0.3.0
T.P.	2.07	905.95	3.81	903.88

Gr. Rod

Lt

2

Rt

3.9

$$\frac{22.4}{-3.7} \frac{7.6}{-3.7}$$

$$\frac{5.2}{-1.3}$$

$$\frac{7.4}{-3.5} \frac{2.4}{22.0}$$

99.4
#5

4.7

$$\frac{23.9}{-1.2} \frac{8.9}{-1.2}$$

$$\frac{6.6}{-1.9}$$

$$\frac{9.0}{-4.3} \frac{9.0}{23.6}$$

4.7

$$\frac{25.8}{-5.4} \frac{10.1}{-5.4}$$

$$\frac{7.3}{-2.6}$$

$$\frac{8.8}{-4.1} \frac{8.8}{23.2}$$

4.7

$$\frac{7.4}{-2.7}$$

$$\frac{8.9}{-4.2} \frac{8.9}{23.4}$$

98.6
9.1

4.7

$$\frac{25.3}{-5.2} \frac{9.9}{-5.2}$$

$$\frac{6.8}{-2.1}$$

$$\frac{9.2}{-4.5} \frac{9.2}{22.0}$$

4.7

$$\frac{25.0}{-5.0} \frac{9.7}{-5.0}$$

$$\frac{6.1}{-1.9}$$

$$\frac{8.9}{-4.0} \frac{8.9}{23.4}$$

4.7

$$\frac{23.6}{-4.3} \frac{9.0}{-4.3}$$

$$\frac{5.5}{-0.8}$$

$$\frac{8.3}{-3.6} \frac{8.3}{22.2}$$

4.7

$$\frac{21.6}{-3.3} \frac{8.0}{-3.3}$$

$$\frac{4.9}{-0.2}$$

$$\frac{7.4}{-2.7} \frac{7.4}{20.4}$$

4.7

$$\frac{20.6}{-2.8} \frac{7.5}{-2.8}$$

$$\frac{4.7}{-0.0}$$

$$\frac{7.3}{-2.6} \frac{7.3}{20.2}$$

4.7

$$\frac{25.6}{-21.3} \frac{5.4}{-21.3}$$

$$\frac{5.1}{-0.4}$$

$$\frac{6.7}{-2.0} \frac{6.7}{22.0}$$

4.7

$$\frac{23.4}{-9.2} \frac{8.8}{-9.2}$$

$$\frac{5.7}{-1.0}$$

$$\frac{8.1}{-3.4} \frac{8.1}{21.8}$$

Top End Gr. Post Rt 40+

Sta	+	π	-	Grade
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905.95

40	+50			03.0
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03.0

Δ

41

+50

42

+50

43

▽
03.0

Δ

+50

44

+50

45

+50

Δ
03.0

Gr. Rod

LH

R

Rt.

2.9

$$24.6' / \frac{77}{-48}$$

$$\frac{46}{-17}$$

$$\frac{6.7}{-38} / 22.6'$$

2.9

$$25.4' / \frac{81}{-5.2}$$

$$\frac{53}{-24}$$

$$\frac{7.3}{-44} / 23.8'$$

2.9

$$27.4' / \frac{91}{-62}$$

$$\frac{54}{-25}$$

$$\frac{7.1}{-4.9} / 24.8'$$

2.9

$$27.0' / \frac{89}{-60}$$

$$\frac{50}{-21}$$

$$\frac{7.4}{-45} / 24.0'$$

2.9

$$25.4' / \frac{81}{-5.2}$$

$$\frac{48}{-19}$$

$$\frac{7.4}{-45} / 24.0'$$

2.9

$$24.6' / \frac{77}{-48}$$

$$\frac{50}{-21}$$

$$\frac{7.4}{-45} / 24.0'$$

2.9

$$25.2' / \frac{75}{-46}$$

$$\frac{51}{-22}$$

$$\frac{7.0}{-41} / 23.2'$$

2.9

$$24.9' / \frac{76}{-47}$$

$$\frac{57}{-28}$$

$$\frac{7.1}{-42} / 23.4'$$

2.9

$$24.2' / \frac{75}{-46}$$

$$\frac{6.0}{-31}$$

$$\frac{7.5}{-46} / 24.2'$$

2.9

$$24.2' / \frac{75}{-46}$$

$$\frac{57}{-28}$$

$$\frac{7.6}{-47} / 24.4'$$

2.9

$$24.2' / \frac{75}{-46}$$

$$\frac{55}{-26}$$

$$\frac{8.3}{-57} / 25.8'$$

Sta + π - Grade

905.95

46

03.0

T.P.

6.50

907.19

5.26

900.69

+50

+90

47

+15

+50

48

+50

03.0

49

03.1

+50

03.4

T.P.

6.01

910.21

3.99

904.20

50

03.8

Gr. Rod.

Lt.

R

Et.

2.9

$$23.2' / \frac{70}{-41}$$

$$\frac{53}{-24}$$

$$\frac{66}{-37} / 22.4$$

4.2

$$21.0' / \frac{72}{-30}$$

$$\frac{66}{-24}$$

$$\frac{71}{-29} / 20.8'$$

4.2

$$21.4' / \frac{74}{-32}$$

$$\frac{64}{-22}$$

$$\frac{73}{-31} / 21.2$$

4.2

4.2

$$23.8' / \frac{81}{-39}$$

$$\frac{64}{-22}$$

$$\frac{72}{-30} / 21.0$$

4.2

$$23.4' / \frac{84}{-42}$$

$$\frac{42}{-23}$$

$$\frac{81}{-39} / 22.8'$$

4.2

$$\frac{63}{-21}$$

$$\frac{7.8}{-36} / 22.2$$

4.2

$$26.6' / \frac{10.0}{-5.8}$$

$$\frac{57}{-15}$$

$$\frac{7.8}{-32} / 21.4'$$

4.1

$$22.8' / \frac{8.0}{-3.9}$$

$$\frac{41}{-14}$$

$$\frac{71}{-30} / 21.0'$$

3.8

$$20.0' / \frac{6.3}{-2.5}$$

$$\frac{34}{-10}$$

$$\frac{56}{-20.2} / 23.4'$$

?

Nail in T.P. Lt 50+

6.4

$$25.0' / \frac{7.4}{-2.10}$$

$$\frac{55}{-10.6}$$

$$\frac{70}{-19.9} / 25.8'$$

Sta	+	π	-	Grade
		910.21		
50	+50			04.5
51				05.3
	+57			06.1
52				06.8
	+36			07.3
B.M.	4.88	913.47	1.62	908.59
	+70			07.8
	+80			07.9
53				08.1
	+30			08.3
	+63			08.5
54				08.5

Gr Rod

Lt

L

Rt

5.7

 $256' / \frac{44}{R13}$ $\frac{53}{+0.4}$ $\frac{43}{R12/25.4}$

4.9

 $248' / \frac{40}{R09}$ $\frac{49}{00}$ $\frac{57}{R12/25.4}$

4.1

 $242' / \frac{35}{R06}$ $\frac{43}{-0.2}$ $\frac{55}{R0.6/24.2}$

3.4

 $240' / \frac{49}{R05}$ $\frac{34}{00}$ $\frac{26}{+0.8/25.6}$

2.9

 $242' / \frac{43}{R06}$ $\frac{26}{+0.3}$ $\frac{32}{R1.7/26.4}$

Top Corng. Based on Iron Fe. Post 33' L + 52 + 55

5.7

 $244' / \frac{70}{R0.7}$ $\frac{52}{+0.7}$ $\frac{61}{R1.6/26.2}$

5.4

 $33.0' / \frac{2.4}{R3.4}$ $\frac{50}{+0.4}$ $\frac{55}{R1.9/26.8}$

5.2

 $33.0' / \frac{2.0}{R3.2}$ $\frac{49}{+0.3}$ $\frac{53}{R1.9/26.8}$

5.0

 $23.8' / \frac{4.6}{R0.4}$ $\frac{48}{+0.1}$ $\frac{51}{R1.9/26.8}$

5.0

 $244' / \frac{63}{R0.7}$ $\frac{49}{+0.1}$ $\frac{47}{+0.3/27.6}$

Sta	+	π	-	Grade
		913.47		
54	+50			08.2
55				07.8
T.P.	3.77	911.17	6.07	907.40
	+50			07.4
56				07.0
	+50			06.6
57				06.2
	+50			05.8
58				05.4
	+44			05.1
T.P.	7.94	912.46	6.65	904.52
59				04.8
	+50			05.1

Gr. Rod

L_t

L

R_t

5.3

$$24.8' / \frac{64}{20.9}$$

$$\frac{52}{10.1}$$

$$\frac{55}{21.8} / 26.6'$$

5.7

$$22.9' / \frac{94}{-9.7}$$

$$\frac{60}{-0.3}$$

$$\frac{77}{10.0} / 19.8'$$

2 slo. 55

3.8

$$23.0' / \frac{88}{-4.0}$$

$$\frac{42}{-0.4}$$

$$\frac{59}{-21} / 19.2'$$

4.2

$$20.8' / \frac{81}{-3.9}$$

$$\frac{43}{-0.1}$$

$$\frac{56}{20.6} / 24.2'$$

4.6

$$22.2' / \frac{82}{-3.6}$$

$$\frac{44}{10.2}$$

$$\frac{59}{20.7} / 24.4'$$

5.0

$$21.8' / \frac{84}{-3.4}$$

$$\frac{48}{10.2}$$

$$\frac{65}{20.5} / 24.0'$$

5.4

$$20.8' / \frac{8.7}{-2.7}$$

$$\frac{52}{10.2}$$

$$\frac{65}{20.9} / 24.6'$$

5.8

$$21.9' / \frac{8.8}{-3.0}$$

$$\frac{56}{10.2}$$

$$\frac{64}{21.4} / 25.8'$$

6.1

$$22.6' / \frac{9.9}{-2.8}$$

$$\frac{6.2}{-0.1}$$

$$\frac{76}{20.5} / 24.0'$$

7.7

$$24.0' / \frac{12.2}{-0.5}$$

$$\frac{7.9}{-0.2}$$

$$\frac{11.6}{-3.9} / 22.8'$$

7.4

$$25.8' / \frac{12.8}{-3.4}$$

$$\frac{8.8}{-1.4}$$

$$\frac{9.3}{-1.7} / 10.8'$$

Sta	+	π	-	Grade
		912.46		
60				05.8
	+30			06.4
	+65			07.3
61				08.4
	+50			10.4
T.P.	13.10	924.12	1.44	911.02
62				12.6
	+50			14.8
63				17.0
	+50			19.2
T.P.	11.15	933.02	2.25	921.87
	+85			20.7
64				21.4

Gr. Rod

L_t

R

R_t

6.7

$$24.0' / \frac{11.2}{-4.5}$$

$$\frac{1.3}{-1.6}$$

$$\frac{84}{-27} / 20.4'$$

6.1

$$24.2' / \frac{10.7}{-4.6}$$

$$\frac{1.1}{-1.6}$$

$$\frac{91}{-30} / 21.0'$$

5.2

$$25.0' / \frac{10.2}{-5.0}$$

$$\frac{0.0}{-0.8}$$

$$\frac{77}{-25} / 20.0'$$

4.1

$$25.4' / \frac{9.4}{-5.3}$$

$$\frac{4.2}{-0.1}$$

$$\frac{54}{-13} / 17.6'$$

2.1

$$17.4' / \frac{8.8}{-7.2}$$

$$\frac{1.6}{+0.5}$$

$$\frac{28}{-0.7} / 10.4'$$

11.5

$$15.0' / \frac{11.8}{8.7}$$

$$\frac{11.2}{+0.3}$$

$$\frac{116}{8.7} / 15.0'$$

9.3

$$15.0' / \frac{8.5}{8.7}$$

$$\frac{8.9}{+0.4}$$

$$\frac{93}{8.7} / 15.0'$$

7.1

$$15.0' / \frac{7.5}{8.7}$$

$$\frac{6.9}{+0.2}$$

$$\frac{73}{8.7} / 15.0'$$

4.9

$$15.0' / \frac{5.15}{8.7}$$

$$\frac{4.5}{+0.4}$$

$$\frac{4.95}{8.7} / 15.0'$$

12.3

$$15.0' / \frac{12.5}{8.7}$$

$$\frac{11.9}{+0.4}$$

$$\frac{43}{18.0} / 48.0'$$

11.6

$$15.0' / \frac{11.65}{8.7}$$

$$\frac{11.2}{+0.4}$$

$$\frac{19}{+10.2} / 47.4'$$

Sta	+	π	-	Grade
		933.02		

64	+30			22.7
----	-----	--	--	------

	+65			24.3
--	-----	--	--	------

65				25.5
----	--	--	--	------

	+50			27.3
--	-----	--	--	------

	+72			28.1
--	-----	--	--	------

	+80			28.2
--	-----	--	--	------

	+95			929.8
--	-----	--	--	-------

B.M.			3.86	929.16
------	--	--	------	--------

929.10

Gr. Rod

Lt.

R.

Rt.

10.3

~~$$\frac{27}{100} / \frac{12.3}{100}$$~~

~~$$\frac{99}{104}$$~~

~~$$\frac{04}{199} / 46.8'$$~~

8.7

~~$$\frac{246}{108} / \frac{99}{108}$$~~

~~$$\frac{84}{103}$$~~

~~$$\frac{43}{144} / 35.8'$$~~

7.5

~~$$\frac{31.9}{12.2} / \frac{53}{12.2}$$~~

~~$$\frac{10}{105}$$~~

~~$$\frac{49}{12.6} / 32.2'$$~~

5.7

~~$$\frac{32.4}{127} / \frac{30}{127}$$~~

~~$$\frac{54}{103}$$~~

~~$$\frac{18}{109} / 28.8'$$~~

4.2

~~$$\frac{28.4}{102} / \frac{60}{102}$$~~

~~$$\frac{39}{103}$$~~

Spk. in R.P. Lt. sta. 65+80

Sta

+

π

-

Grade

Centerville Rd
Slope stakes
Grade Change
sta 50 to sta 65+

Sta.	+	π	-	Grade
B.M.	4.62	912.21		907.59

50	+00			03.7
----	-----	--	--	------

	+50			04.2
--	-----	--	--	------

51				04.8
----	--	--	--	------

	+57			05.5
--	-----	--	--	------

52				06.0
----	--	--	--	------

	+36			06.4
--	-----	--	--	------

	+70			06.8
--	-----	--	--	------

53				07.0
----	--	--	--	------

	+30			07.3
--	-----	--	--	------

	+60			07.4
--	-----	--	--	------

54				07.3
----	--	--	--	------

Gr Rod

Lt

R

Rt

Top Cond Base 32' Lt 52+55

8.5

$$23.0' / \frac{10.5}{R00}$$

$$\frac{88}{-03}$$

$$\frac{98}{R07/24.4'}$$

80

$$24.2' / \frac{9.4}{R06}$$

$$\frac{82}{-02}$$

$$\frac{9.5}{R05/24.0'}$$

74

$$24.0' / \frac{8.9}{R05}$$

$$\frac{79}{-05}$$

$$\frac{8.9}{R05/24.0'}$$

6.7

$$23.0' / \frac{8.7}{R00}$$

$$\frac{72}{-05}$$

$$\frac{8.7}{R01/23.2'}$$

6.2

$$23.4' / \frac{8.0}{R02}$$

$$\frac{64}{-02}$$

$$\frac{5.9}{R03/27.6'}$$

5.8

$$24.0' / \frac{7.3}{R05}$$

$$\frac{56}{+02}$$

$$\frac{6.2}{R1.6/26.2'}$$

5.4

$$24.4' / \frac{6.7}{R07}$$

$$\frac{50}{+0.4}$$

$$\frac{5.9}{R15/26.0'}$$

5.2

$$33.0' / \frac{4.7}{+3.5}$$

$$\frac{4.7}{+05}$$

$$\frac{5.2}{+0.0/27.0'}$$

4.9

$$33.0' / \frac{4.7}{+3.2}$$

$$\frac{4.6}{+03}$$

$$\frac{5.0}{R1.9/26.8'}$$

4.8

$$24.0' / \frac{4.3}{R05}$$

$$\frac{4.6}{+02}$$

$$\frac{4.8}{+0.0/27.0'}$$

4.9

$$23.6' / \frac{6.1}{R08}$$

$$\frac{4.6}{+03}$$

$$\frac{4.5}{+0.4/27.8'}$$

Sta	+	π	-	Grade
		912.21		
54	+50			07.0
55				06.6
I.P.	2.86	909.43	5.64	906.57
	+50			06.2
56				05.9
	+50			05.5
57				05.1
	+50			04.7
58				04.3
	+44			04.0
59				03.7
	+50			04.0

Gr. Rod.

L.F.

E

R.F.

5.2

$$252' \frac{61}{R11}$$

$$\frac{52}{+0.2}$$

$$\frac{53}{R19/26.8}$$

5.6

$$21.8' \frac{90}{-34}$$

$$\frac{58}{-0.2}$$

$$\frac{76}{R20/20.2}$$

3.2

$$22.8' \frac{71}{-39}$$

$$\frac{34}{-0.2}$$

$$\frac{52}{R20/19.0}$$

3.5

$$22.6' \frac{73}{-38}$$

$$\frac{35}{00}$$

$$\frac{49}{R06/24.2}$$

3.9

$$22.2' \frac{75}{-36}$$

$$\frac{36}{+0.3}$$

$$\frac{52}{R07/24.4}$$

4.3

$$21.8' \frac{77}{-34}$$

$$\frac{41}{+0.2}$$

$$\frac{58}{R05/24.0}$$

4.7

$$20.8' \frac{76}{-29}$$

$$\frac{44}{+0.3}$$

$$\frac{58}{R09/24.8}$$

5.1

$$21.0' \frac{81}{-30}$$

$$\frac{49}{+0.2}$$

$$\frac{57}{R14/25.0}$$

5.4

$$22.0' \frac{89}{-35}$$

$$\frac{55}{-0.1}$$

$$\frac{67}{R05/24.0}$$

5.7

$$24.0' \frac{102}{-45}$$

$$\frac{59}{-0.2}$$

$$\frac{76}{-39/22.8}$$

5.4

$$25.8' \frac{128}{-54}$$

$$\frac{67}{-1.3}$$

$$\frac{72}{+8/18.6}$$

Sta	+	π	-	Grade
		909.43		
60				04.6
T.P.	8.24	915.58	2.09	907.34
+30				05.3
+65				06.2
61				07.3
+50				09.3
62				11.5
+50				13.7
T.P.	9.57	924.73	0.42	915.16
63				15.9
+50				18.1
T.P.	11.14	931.97	3.90	920.83
+85				19.7
64				20.3

Gr. Rod

Lt

R

Cl

4.8

$$204' / \frac{25}{-27}$$

$$\frac{6.2}{-1.4}$$

$$\frac{7.2}{-2.4} / 19.8'$$

10.3

$$242' / \frac{14.9}{-4.6}$$

$$\frac{11.8}{-1.5}$$

$$\frac{13.1}{-2.8} / 20.6'$$

9.4

$$250' / \frac{14.4}{-5.0}$$

$$\frac{10.1}{-0.7}$$

$$\frac{11.7}{-2.3} / 19.6'$$

8.3

$$13.6' / \frac{13.6}{-5.3}$$

$$\frac{8.2}{+9.1}$$

$$\frac{9.5}{-1.2} / 17.4'$$

6.3

$$17.2' / \frac{7.4}{-1.1}$$

$$\frac{5.7}{+0.6}$$

$$\frac{7.0}{-0.7} / 24'$$

4.1

$$15.0' / \frac{4.3}{B.T.}$$

$$\frac{3.7}{+0.6}$$

$$\frac{4.1}{B.T.} / 15.0'$$

1.9

$$15.0' / \frac{2.0}{B.T.}$$

$$\frac{1.4}{+0.6}$$

$$\frac{1.8}{B.T.} / 15.0'$$

8.8

$$15.0' / \frac{9.1}{B.T.}$$

$$\frac{8.5}{+0.6}$$

$$\frac{9.0}{B.T.} / 15.0'$$

6.6

$$15.0' / \frac{6.8}{B.T.}$$

$$\frac{6.2}{+0.6}$$

$$\frac{6.6}{B.T.} / 15.0'$$

12.3

$$15.0' / \frac{12.4}{B.T.}$$

$$\frac{11.8}{+0.5}$$

$$\frac{8.3}{+10.0} / 43.0'$$

11.7

$$15.0' / \frac{11.05}{B.T.}$$

$$\frac{11.1}{+0.6}$$

$$\frac{13}{+10.4} / 47.8'$$

Sta.	+	π	-	Grade
		931.97		
64	+30			21.6
	+65			23.1
65				24.5
	+50			26.3
	+80			27.3
B.M.			386	928.11 - (928.10)

Gr. Rod.

Lt.

d.

Rt.

10.4

$$23.4' / \frac{12.2}{40.2}$$

$$\frac{99}{105}$$

$$\frac{04}{109} / 47.0'$$

8.9

$$29.2' / \frac{78}{111}$$

$$\frac{84}{105}$$

$$\frac{42}{147} / 36.4$$

7.5

$$31.4' / \frac{53}{122}$$

$$\frac{70}{105}$$

$$\frac{49}{146} / 32.2'$$

5.7

$$32.4' / \frac{30}{127}$$

$$\frac{54}{103}$$

$$\frac{45}{109} / 28.8'$$

Spt in R.R. Lt. sta. 65180

$$\begin{array}{r} 96.6 \\ 2.95 \\ \hline 99.55 \end{array}$$

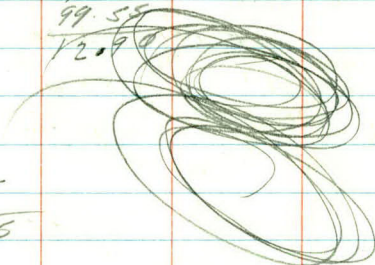
$$\begin{array}{r} 14.75 \\ .2 \\ \hline 2.950 \end{array}$$

New Elev. $\rightarrow$

$$\begin{array}{r} 900.7 \\ 99.55 \\ \hline 1.15 \end{array}$$

$$\begin{array}{r} 12.46 \\ 99.55 \\ \hline 12.46 \end{array}$$

$$\begin{array}{r} 14.75 \\ .03 \\ \hline 4425 \end{array}$$



Ditch

From

W. End of Col. 6008 to 1475 Northwest.

0+00 = 17.7' Lf sta. 6006.5

Note: Levels are 1' higher
than Level Datum.

Sta	+	π	-	Grade
B.M.	8.15	908.85		900.7

0	+00			99.81
---	-----	--	--	-------

	+50			99.70
--	-----	--	--	-------

1				99.59
---	--	--	--	-------

	+50			99.48
--	-----	--	--	-------

2				99.37
---	--	--	--	-------

	+50			99.26
--	-----	--	--	-------

- 0.22%

3				99.15
---	--	--	--	-------

T.P.	5.47	907.60	6.72	902.13
------	------	--------	------	--------

	+50			99.04
--	-----	--	--	-------

4				98.93
---	--	--	--	-------

T.P.	7.59	909.51	5.68	901.92
------	------	--------	------	--------

	+50			98.82
--	-----	--	--	-------

5				98.71
---	--	--	--	-------

Gr. Rod. Lt ^{Stake} Rt Rt
Flow Line W. End Culv. sta 60+08 Old Culv.

9.04
+19 = 908

9.15 7.7' / $\frac{6.1}{+3.1}$ $\frac{9.5}{+3.0}$ $\frac{54}{+58/9.1'}$

9.26 11.7' / $\frac{4.2}{+5.1}$ $\frac{6.28}{+3.0}$ $\frac{39}{+54/12.3'}$

9.37 11.5' / $\frac{4.7}{+5.0}$ $\frac{6.37}{+3.0}$ $\frac{4.10}{+54/12.3'}$

9.48 10.9' / $\frac{4.8}{+4.7}$ $\frac{6.48}{+3.0}$ $\frac{4.9}{+46/10.7'}$

9.59 $\frac{6.59}{+3.0}$ $\frac{5.2}{+44/10.3'}$

9.70 10.3' / $\frac{5.1}{+4.6}$ $\frac{6.70}{+3.0}$ $\frac{5.5}{+42/9.5'}$

Top Blue Top sta 3+00
8.56 10.1' / $\frac{4.3}{+4.3}$ $\frac{5.56}{+3.0}$ $\frac{36}{+50/11.5'}$

8.67 9.7' / $\frac{4.6}{+4.1}$ $\frac{5.67}{+3.0}$ $\frac{33}{+54/12.3'}$

10.69 9.3' / $\frac{5.8}{+3.9}$ $\frac{7.7}{+3.0}$ $\frac{5.0}{+57/12.9'}$

10.80 14.5' / $\frac{4.3}{+4.5}$ $\frac{7.8}{+3.0}$ $\frac{30}{+78/17.1'}$

Sta	+	π	-	Grade
		909.51		
5	+50			98.60
6				98.49
	+50			98.39
7				98.27
	+50			98.16
8				98.05
	+50			97.94
9				97.83
I.P.	4.50	905.29	8.72	900.19
	+50			97.72
10				97.61
	+50			97.50

Gr. Rod

Lt

R
stroke
RT

Rt

10.91

$$95' / \frac{69}{140}$$

$$\frac{82}{127}$$

$$\frac{64}{145/10.5'}$$

11.02

$$75' / \frac{80}{140}$$

$$\frac{802}{130}$$

$$\frac{71}{139/9.3'}$$

11.13

$$79' / \frac{79}{132}$$

$$\frac{813}{130}$$

$$\frac{71}{140/9.3'}$$

11.24

$$79' / \frac{80}{132}$$

$$\frac{824}{130}$$

$$\frac{78}{139/8.3'}$$

11.35

$$101' / \frac{73}{143}$$

$$\frac{835}{130}$$

$$\frac{80}{134/8.3'}$$

11.46

$$99' / \frac{73}{142}$$

$$\frac{846}{130}$$

$$\frac{80}{135/8.5'}$$

11.57

$$99' / \frac{74}{142}$$

$$\frac{857}{130}$$

$$\frac{81}{135/8.5'}$$

11.68

$$97' / \frac{76}{141}$$

$$\frac{868}{130}$$

$$\frac{82}{135/8.5'}$$

7.57

$$93' / \frac{37}{139}$$

$$\frac{457}{130}$$

$$\frac{42}{134/8.3'}$$

7.68

$$79' / \frac{45}{132}$$

$$\frac{468}{130}$$

$$\frac{43}{134/8.3'}$$

7.79

$$81' / \frac{45}{133}$$

$$\frac{479}{130}$$

$$\frac{44}{134/8.3'}$$

Sta.	+	π	-	Grade
		905.29		
11				97.39
	+50			97.28
12				97.17
	+50			97.06
13				96.95
	+50			96.84
14				96.73
	+50			96.62
	+75			96.57
B.M.	2.45	909.15		909.7
Flow Line W. End Culv =				99.81
"	"	E. End Culv.		99.61

9-26-40
K.A.
L.G.
M.B.

Gr. Rod

Lt

L

Rt

7.90

$$6.5' / \frac{54}{12.5}$$

$$\frac{49}{13.0}$$

$$\frac{54}{12.5 / 6.5'}$$

8.01

$$6.5' / \frac{5.5}{12.5}$$

$$\frac{47}{11.3}$$

$$\frac{5.5}{12.5}$$

8.12

$$6.9' / \frac{5.4}{12.7}$$

$$\frac{51.2}{13.0}$$

$$\frac{54}{12.7 / 6.9'}$$

8.23

$$6.1' / \frac{5.9}{12.3}$$

$$\frac{72}{11.0}$$

$$\frac{56}{12.6 / 6.7'}$$

8.3

$$6.9' / \frac{5.6}{12.7}$$

$$\frac{53}{13.0}$$

$$\frac{5.8}{12.4 / 6.3'}$$

8.3

$$4.9' / \frac{6.6}{11.7}$$

$$\frac{77}{10.6}$$

$$\frac{6.2}{12.1 / 5.7'}$$

8.3

$$4.7' / \frac{6.7}{11.6}$$

$$\frac{53}{13.0}$$

$$\frac{6.2}{12.1 / 5.7'}$$

8.3

$$5.1' / \frac{6.5}{11.8}$$

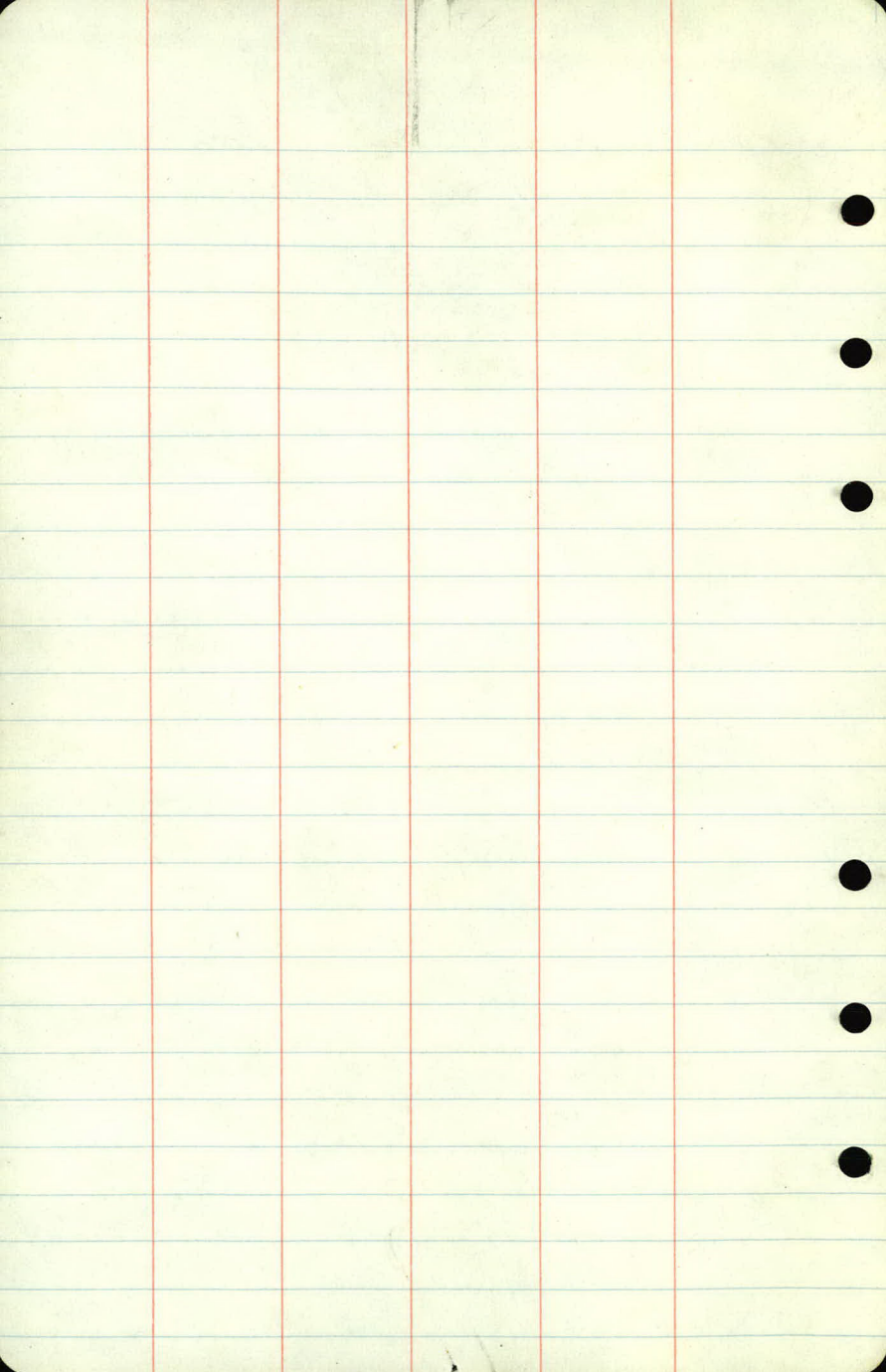
$$\frac{77}{10.6}$$

$$\frac{6.3}{12.0 / 5.5'}$$

8.3

9.34)

9.14



SURVEY
BORROW PIT
on Fischer Prop.

Centerville Rd.

89° 35'

Foresight = L
machine shed.

P.O.T. 47 + 13.0

0+00

Worked up
6/19/41
Haw.

Sta	+	-	Elev
B.M.	10.47	918.06	(907.59)
T.P.	9.25	926.70	0.61 917.45

3 09.1

+50 11.5

+75 12.0

4 12.9

+25 13.8

+50 14.7

+75 15.7

5 16.4

+25 17.1

+50 17.9

6-17-41
K.A.
L.G.
M.B.

Lf

L

Top Conc. Base of Iron P.C. Post 33 Lf Sta 52+55

Note: "L" = approx. limit of borrow pit.

$\frac{17.4}{50}$ $\frac{16.2}{23}$ $\frac{16.4}{8}$ $\frac{18.5}{6}$ $\frac{17.6}{4}$ $\frac{17.6}{}$

$\frac{14.2}{100}$ $\frac{12.1}{70}$ $\frac{12.8}{37}$ $\frac{14.2}{10}$ $\frac{16.4}{6}$ $\frac{15.2}{4}$ $\frac{15.2}{}$

$\frac{11.6}{150}$ $\frac{11.9}{127}$ $\frac{10.0}{100}$ $\frac{8.8}{68}$ $\frac{9.6}{40}$ $\frac{10.9}{21}$ $\frac{11.1}{13}$ $\frac{15.6}{7}$ $\frac{14.7}{5}$ $\frac{14.7}{}$

L
 $\frac{5.4}{250}$ $\frac{8.1}{193}$ $\frac{7.5}{180}$ $\frac{7.4}{150}$ $\frac{7.0}{125}$ $\frac{5.4}{100}$ $\frac{4.3}{75}$ $\frac{4.4}{50}$ $\frac{5.2}{29}$ $\frac{6.6}{17}$ $\frac{6.1}{16}$ $\frac{6.8}{14}$ $\frac{14.4}{6}$ $\frac{13.8}{5}$ $\frac{13.8}{}$

L
 $\frac{3.7}{245}$ $\frac{5.1}{216}$ $\frac{5.6}{200}$ $\frac{5.3}{186}$ $\frac{4.0}{150}$ $\frac{3.9}{125}$ $\frac{3.7}{100}$ $\frac{3.2}{75}$ $\frac{3.0}{50}$ $\frac{3.1}{30}$ $\frac{4.1}{20}$ $\frac{3.4}{17}$ $\frac{5.2}{16}$ $\frac{13.3}{6}$ $\frac{12.9}{}$

L
 $\frac{4.4}{250}$ $\frac{4.8}{220}$ $\frac{4.2}{200}$ $\frac{3.2}{185}$ $\frac{1.6}{154}$ $\frac{2.7}{125}$ $\frac{3.7}{100}$ $\frac{3.7}{50}$ $\frac{3.2}{28}$ $\frac{3.6}{19}$ $\frac{3.0}{16}$ $\frac{4.7}{15}$ $\frac{12.5}{6}$ $\frac{12.0}{}$

L
 $\frac{2.9}{300}$ $\frac{4.7}{270}$ $\frac{4.7}{231}$ $\frac{2.6}{200}$ $\frac{1.0}{171}$ $\frac{1.5}{150}$ $\frac{3.2}{125}$ $\frac{4.6}{100}$ $\frac{4.9}{80}$ $\frac{4.2}{55}$ $\frac{2.8}{30}$ $\frac{2.9}{19}$ $\frac{2.3}{15}$ $\frac{4.1}{14}$ $\frac{11.4}{6}$ $\frac{11.0}{}$

L
 $\frac{4.0}{300}$ $\frac{5.5}{253}$ $\frac{4.2}{225}$ $\frac{2.2}{200}$ $\frac{1.6}{175}$ $\frac{2.7}{151}$ $\frac{4.5}{125}$ $\frac{5.6}{100}$ $\frac{5.4}{75}$ $\frac{4.2}{50}$ $\frac{2.7}{30}$ $\frac{2.3}{18}$ $\frac{1.3}{15}$ $\frac{2.8}{14}$ $\frac{10.8}{6}$ $\frac{10.3}{}$

L
 $\frac{4.0}{300}$ $\frac{5.6}{263}$ $\frac{5.6}{243}$ $\frac{4.8}{225}$ $\frac{3.0}{200}$ $\frac{2.5}{181}$ $\frac{4.1}{150}$ $\frac{5.6}{125}$ $\frac{6.3}{100}$ $\frac{6.2}{75}$ $\frac{5.1}{50}$ $\frac{2.3}{29}$ $\frac{2.8}{17}$ $\frac{1.8}{14}$ $\frac{3.5}{13}$ $\frac{10.0}{6}$ $\frac{9.6}{}$

L
 $\frac{4.8}{266}$ $\frac{5.3}{231}$ $\frac{4.0}{200}$ $\frac{3.4}{175}$ $\frac{4.4}{150}$ $\frac{5.7}{125}$ $\frac{6.3}{100}$ $\frac{6.2}{75}$ $\frac{5.4}{50}$ $\frac{3.8}{29}$ $\frac{3.2}{16}$ $\frac{2.3}{13}$ $\frac{3.2}{12}$ $\frac{9.2}{5}$ $\frac{8.8}{}$

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		926.70	/	
--	--	--------	---	--

6				19.0
---	--	--	--	------

	+30			19.5
--	-----	--	--	------

	+90			19.9
--	-----	--	--	------

B.M.				
------	--	--	--	--

		19.12		
--	--	-------	--	--

			907.58	
--	--	--	--------	--

				907.59
--	--	--	--	--------

Lt

L

L

68	68	60	45	38	26	80	11
100	74	97	26	14	10	5	<u>1</u>

L

74	69	61	44	34	76	7.2
100	65	36	17	5	4	<u>1</u>

$\frac{7.3}{50}$ $\frac{7.3}{31}$ $\frac{7.0}{10}$ $\frac{6.8}{1}$

Top Conc. Base of Iron Pg. post.

11.82
7.3
 19.12

P.P.

0

53.36

Clev. Ave



Co. Rd. "C"

P.P.

0

53.36

Sounding
Centerville Rd
Sta 92+ = H¹²"

12-8-43

HAW

AM

L G

Depth

Sounding #1

Lt Sta 86+00

50th Hammer

Depth

1-8	Push	
8-24	1 Blows per Ft	49 to 50 27 Blows
24 to 28	4 Blows per Ft	50 to 51 34 "
28 to 30	6 Blows per Ft	51 to 52 50 "
30 to 32	6 Blows per Ft	52 to 53 60 "
32 to 33	8 " per Ft	
33 to 34	8 " "	
34 to 35	8 " "	
35 to 36	8 " "	
36 to 37	10 " "	
37 to 38	9 " "	
38 to 39	9 " "	
39 to 40	10 " "	
40 to 41	14 " "	
41 to 42	12 " "	
42 to 43	12	
43 to 44	12	
44 to 45	14	
45 to 46	14	
46 to 47	14	
47 to 48	14	
48 to 49	26	

Sounding #2

Pt Sta 86

50th Hammer

Depth

Blows per Ft.

1 to 4	1 Blow
4 to 8	8 Blows
8 to 12	5 "
12 to 16	10 "
16 to 20'	12 "
20 to 21	3 per Ft
21 to 22	3 " "
22 to 23	3
23 to 24	3
24 to 25	4
25 to 26	4
26 to 27	4
27 to 28	4
28 to 29	5
29 to 30	5
30 to 31	5
31 to 32	5
32 to 33	8
33 to 34	20'

Sounding #3

Lt Sta 85+00

Depth	Blows
1 to 4	4
4 to 8	7
8 to 12	10
12 to 16	15
16 to 17	6 per Ft
17 to 18	6
18 to 19	6
19 to 20	6
20 to 21	8
21 to 22	8
22 to 23	8
23 to 24	8
24 to 25	12

Sounding 4

Rt Sta 87

1 to 4 4

4 to 8 4

8 to 12 4

12 to 16 6

16 to 17 4 per Ft

17 to 18 4

18 to 19 4

19 to 20 4

20 to 21 5

21 to 22 5

22 to 23 5

23 to 24 5

24 to 25 6

25 to 26 5

26 to 27 6

27 to 28 5

28 to 29 6

29 to 30 6

30 to 31 8

31 to 32 7

32 to 33 8

33 to 34 9

34 to 35 10

35 to 36 11

Sounding # 5

Lt 54 75+00

Depth	Blows
1 to 4	2
4 to 8	2
8 to 12	2 per Ft
12 to 16	3 per Ft
16 to 17	4
17 to 18	5
18 to 19	6
19 to 20	7
20 to 21	8
21 to 22	9
22 to 23	10
23 to 24	12

Sounding # 6

Lt 54 70 100

Depth

1 to 4 4 Blows

4 to 8 2

8 to 12 9 Blows

12 to 13 3 Blows per Ft

13 to 14 3 " "

14 to 15 3 " "

15 to 16 3 " "

16 to 17 4 " "

17 to 18 4

18 to 19 5

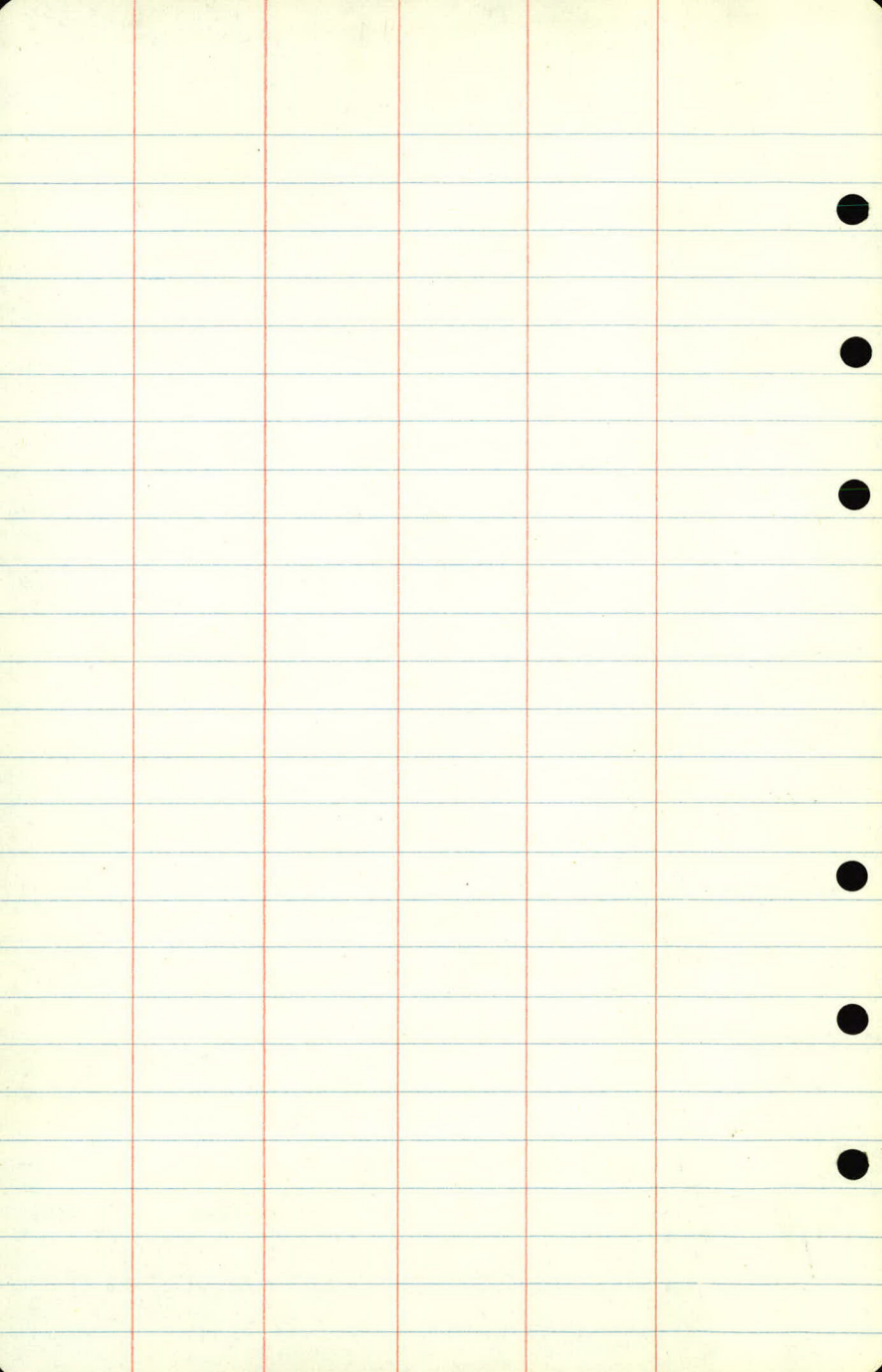
19 to 20 5

20 to 21 10

21 to 22 10

22 to 23 13

23 to 24



1
Levels

Low spot Centerville Rd
To Wilkinson Lake

7-8-42

HAW

AM

L.G.

ASSUMED
ELEV.

	+	+	-	Elev
BM	4.90	904.90		900.00
	4.54	905.48	3.96	900.94
	5.11	905.78	4.81	900.67
	9.07	910.75	4.10	901.68
	2.63	906.75	6.63	904.12
	11.61	917.73	0.63	906.12
	13.67	930.81	0.59	917.14
	10.31	940.41	0.71	930.10
	0.68	931.70	9.39	931.02
	0.90	919.48	13.12	918.58
	3.76	910.81	12.43	907.05
	8.10	917.50	1.41	909.40
	2.58	911.31	8.77	908.73
	9.99	920.47	0.83	910.48
	8.32	928.58	0.21	920.26
	1.70	916.94	13.34	915.24
	0.24	908.29	11.89	905.05
T.P	3.59	904.40	4.48	900.81
W.S.			11.88	892.52

(Top Rd)

W/S 7/8/43

T.LZ

897.28

IN DITCH

BESIDE ROAD.

Top Fe Post

WILKINSON LAKE

