

Bk. 15 - Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ LONG LAKE ROAD _____

From S.T.H. No 8 _____ To Co. Rd "F" _____

Road Acc't. No. 12 _____

Date Filed 6-26-39

File _____

①
Plan Survey

Long Lake Rd.

St. H. 8 to Co. Rd. F.

6-8-37

R. O. Pesse } Party
H. Wilke }
A. Moeckler }

Index

Alignment 1-2

Topography 3-6

Cross Sections 7-11

of Cemetery Rd. 12-13

Sta	Pt.	Lt.	Angle	Rt.
-----	-----	-----	-------	-----

20+29.82	P.O.T.		£	Co. Rd F
----------	--------	--	---	----------

See Co Rd F Notes
for Alignment of F'

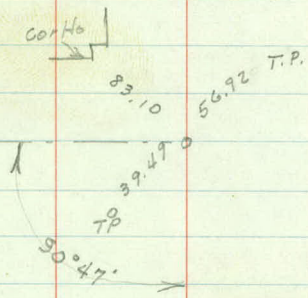
11+00	P.O.T.			
-------	--------	--	--	--

7+13.5	P.O.T.		£	Cemetery Rd.
--------	--------	--	---	--------------

0+00				Edge Pavement.
------	--	--	--	----------------

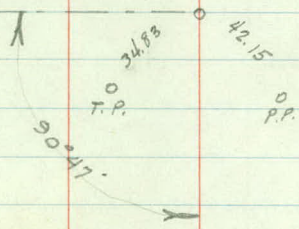
E

Cor Ho

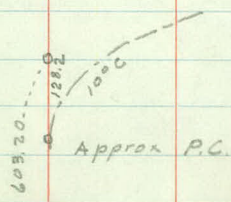


Mon.

Spike

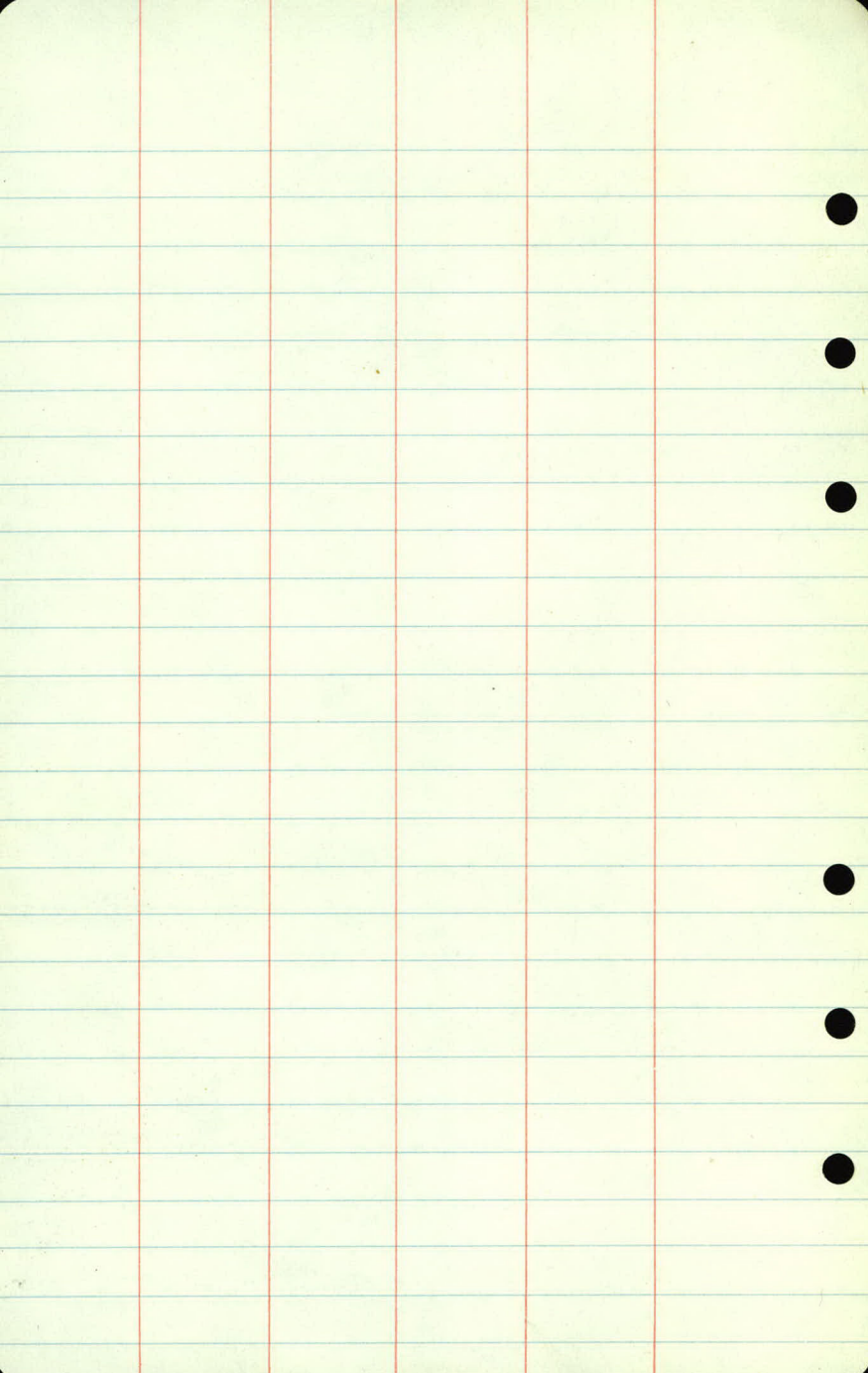


Bolt Spike



Spike

Ctr. Sec. 29



Long Lake Rd

Topography

STH B to Co Rd F

6

8 12

5

8 11

4

9 10

3

9 11

2

10 12

1

8 12-34

+61 4 20' D.H. Rd Lt.

0

7'

+100 End Rad 33

+84 T.P 20

+80 Rd Pt 10

+89 Hyd 37
+82 PP 28

+28 T.P. 19

Cultivated

Uncultivated

+52 PP 28

+75 T.P. 22

+99 PP 28

+31 Ent

+72 Rge tie Ent
+65 PP. 28

+20 T.P. 27'

+30 Ent 50' 28

Cultivated

Uncultivated

+34 PP 29'

+89 T.P. 34'

8 12

13

8 13

12

7 12

11

7 13

10

7 13

9

8 13

8

8 13

7

13

+85 Ent

+23 Ent.
+14 T.P. 21

+82-2" Elm. 26
+60 Cor. Ho 52'
+60-2" Elm 26

+38 Ent.
12"x20 CM. 15'

+75 Ent.
12"x22 CM. 16'

+55 T.P. 21

+37 End Hedge 25
+25 Cor. Ho. 51

+109 Lilac Hedge 25

+80 Orchard 22

+27 Orchard. 26

+06 T.P. 21

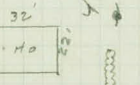
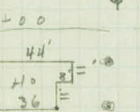
+49 T.P. 21

+91 S.E. Cor. Ho
68'

+57 Rad. 11
+29 Rad. Pl. 41

+14-24"x42" 40'

Cultivated



Orchard

Uncultivated

+50



Q

Q

Q

Q

Wooded - Oaks - Brush

+27 P.P. - 28

+73 P.P. - 27

+37

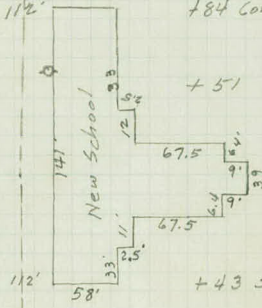
Uncultivated

+19 P.P. - 28'

+67 Ent.

+84 Cor. School 112'

+51 P.P. 28



+43 S.W. Cor. Sch. 112'

20

13 45

+ 75

7 28

+ 50

5 21

+ 25

7 16

19

9 13

18

9 12

17

8 12

16

9 12

15

9 12

14

8 12

+17 End Rad 35
 +05 T.P. 33
 +97 T.P. 23

+17 End Rad. 60

+36 Cor. Garage 36

20
 Gar.

+00 T.P. 22'

+50 End Fe 47
 +44 P.P. 28

+25 Fe. 37

Fe 37'

+83 T.P. 21

Fe 34

+89 P.P. 28

Fe 30

+77 Fe. Cor 32

+46 T.P. - 21

+35 P.P. 28

+82 T.P. 21

+78 P.P. 28

Cultivated

Wooded Oak. Brush

Co. Rd F.



Cross Sections

LONG LAKE ROAD

STH '8' To Co. Rd. F.

Sta	+	π	-	Elev.
B.M.	5.39	912.15		906.76
T.P.	10.68	922.18	0.65	911.50.
0+00			6.6	15.57
+50			7.0	15.2
1			8.1	14.1
+50			8.6	13.6
2			9.2	13.0
+50			10.2	12.0
3			11.3	10.9
T.P.	2.28	912.52	11.94	910.24
+50			2.9	09.6
4			4.1	08.4
+50			4.8	07.7
5			5.0	07.5
+50			4.8	07.7

Top Spike 32' S.E. Sta 7+13.5

3.4 3.0 7.8 8.9 8.3 6.9 8.75 8.8 8.3 9.0
50 36 27 21 15 8 6.61 29 30 38 50

5.8 6.6 7.0 6.81 9.10 8.9 8.5
50 41 18 7.0 15 45 46 50

3.7 3.4 7.1 7.9 8.3 8.1 7.1 6.91 8.01
50 36 28 13 8 8.1 19 32 38 50

4.6 4.1 9.1 9.1 8.7 9.1 8.6 8.7
50 35 26 19 15 8.6 12 18 50

5.8 5.5 9.7 10.2 9.1 9.4 9.8 9.1 9.5 9.9
50 35 27 21 14 10 9.2 13 16 22 50

8.8 8.0 11.4 11.1 10.2 10.6 10.8 10.8 10.7
50 33 27 20 16 10 10.2 13 40 50

11.4 10.9 13.0 12.7 11.6 12.0 11.5 11.5 12.1
50 33 28 20 17 11.3 12 17 34 50

6.9 6.4 4.4 3.5 3.5 4.4 5.8 6.2
50 33 16 13 2.9 13 17 38 50

9.4 8.5 4.7 4.6 9.4 9.4 8.9 10.1
50 20 13 7.1 14 20 31 34 50

11.0 10.8 5.4 5.5 12.4 10.9 11.1
50 22 12 4.8 12 26-31 34 50

10.0 9.5 5.5 5.8 10.0 11.0 10.1 10.8
50 21 11 5.0 14 22 33 36 50

6.7 6.7 8.6 5.2 5.6 10.8 8.4 9.6
50 29 24 18 13 4.8 15 22-30 36 50

Sta + π - Elev

912.52

6 4.5 08.0

+50 4.3 08.2

+92 4.0 08.5

7 3.9 08.6

+26 3.7 08.8

+33 3.7 08.8

+50 3.6 08.9

Water table S.W. Cor. School

B.M. 8.11 914.87 5.77 906.75 906.76

8 5.4 09.5

+50 4.7 10.2

9 4.3 10.6

Water Table N.W. Cor. School

+50 3.9 11.0

T.P. 5.17 916.24 3.80 911.07

$$\begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 6.2 \\ 29 \end{array} \quad \begin{array}{r} 9.5 \\ 22-18 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 4.5 \\ 4.5 \end{array} \quad \begin{array}{r} 5.3 \\ 16 \end{array} \quad \begin{array}{r} 9.6 \\ 23 \end{array} \quad \begin{array}{r} 10.5 \\ 29 \end{array} \quad \begin{array}{r} 8.1 \\ 34 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 30 \end{array} \quad \begin{array}{r} 9.6 \\ 24-18 \end{array} \quad \begin{array}{r} 4.8 \\ 10 \end{array} \quad \begin{array}{r} 4.3 \\ 4.3 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 11.9 \\ 26-30 \end{array} \quad \begin{array}{r} 8.3 \\ 35 \end{array} \quad \begin{array}{r} 8.5 \\ 50 \end{array}$$

$$\begin{array}{r} 6.8 \\ 50 \end{array} \quad \begin{array}{r} 7.1 \\ 32 \end{array} \quad \begin{array}{r} 3.8 \\ 21 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 4.0 \\ 4.0 \end{array} \quad \begin{array}{r} 4.5 \\ 14 \end{array} \quad \begin{array}{r} 6.7 \\ 30 \end{array} \quad \begin{array}{r} 7.3 \\ 50 \end{array}$$

$$\begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 3.9 \\ 3.9 \end{array} \quad \begin{array}{r} 4.6 \\ 14 \end{array} \quad \begin{array}{r} 6.3 \\ 24 \end{array} \quad \begin{array}{r} 6.9 \\ 50 \end{array}$$

$$\begin{array}{r} 3.7 \\ 50 \end{array} \quad \begin{array}{r} 3.7 \\ 3.7 \end{array} \quad \begin{array}{r} 4.3 \\ 14 \end{array} \quad \begin{array}{r} 6.3 \\ 24 \end{array} \quad \begin{array}{r} 7.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 39 \end{array} \quad \begin{array}{r} 3.7 \\ 32 \end{array} \quad \begin{array}{r} 3.7 \\ 3.7 \end{array} \quad \begin{array}{r} 4.3 \\ 14 \end{array} \quad \begin{array}{r} 6.3 \\ 24 \end{array} \quad \begin{array}{r} 7.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.6 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 27 \end{array} \quad \begin{array}{r} 5.6 \\ 19 \end{array} \quad \begin{array}{r} 4.0 \\ 13 \end{array} \quad \begin{array}{r} 3.6 \\ 3.6 \end{array} \quad \begin{array}{r} 3.8 \\ 14 \end{array} \quad \begin{array}{r} 6.2 \\ 28 \end{array} \quad \begin{array}{r} 6.8 \\ 50 \end{array}$$

$$6.04 \quad 906.48$$

Top Spike 32' S.E. 7+13.5

3.84

$$\text{Water Table House} \quad \begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 25 \end{array} \quad \begin{array}{r} 7.8 \\ 20-16 \end{array} \quad \begin{array}{r} 5.8 \\ 10 \end{array} \quad \begin{array}{r} 5.4 \\ 5.4 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 7.0 \\ 19 \end{array} \quad \begin{array}{r} 8.8 \\ 35 \end{array} \quad \begin{array}{r} 8.9 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 22 \end{array} \quad \begin{array}{r} 7.0 \\ 18-14 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 4.7 \\ 4.7 \end{array} \quad \begin{array}{r} 5.1 \\ 16 \end{array} \quad \begin{array}{r} 6.5 \\ 20 \end{array} \quad \begin{array}{r} 7.0 \\ 34 \end{array} \quad \begin{array}{r} 7.8 \\ 42 \end{array} \quad \begin{array}{r} 8.8 \\ 50 \end{array}$$

$$\begin{array}{r} 3.5 \\ 50 \end{array} \quad \begin{array}{r} 4.1 \\ 35 \end{array} \quad \begin{array}{r} 5.8 \\ 29 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \end{array} \quad \begin{array}{r} 4.6 \\ 10 \end{array} \quad \begin{array}{r} 4.3 \\ 4.3 \end{array} \quad \begin{array}{r} 4.8 \\ 16 \end{array} \quad \begin{array}{r} 5.9 \\ 27 \end{array} \quad \begin{array}{r} 8.8 \\ 34 \end{array} \quad \begin{array}{r} 9.6 \\ 50 \end{array}$$

8.66

$$\begin{array}{r} 0.3 \\ 50 \end{array} \quad \begin{array}{r} 0.7 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 24 \end{array} \quad \begin{array}{r} 6.0 \\ 15 \end{array} \quad \begin{array}{r} 4.5 \\ 10 \end{array} \quad \begin{array}{r} 3.9 \\ 3.9 \end{array} \quad \begin{array}{r} 4.5 \\ 17 \end{array} \quad \begin{array}{r} 6.8 \\ 24 \end{array} \quad \begin{array}{r} 7.0 \\ 31 \end{array} \quad \begin{array}{r} 8.2 \\ 50 \end{array}$$

Sta	+	π	-	Elev.
		916.24		
10			5.0	11.2
+50			5.0	11.2
11			5.4	10.8
+50			5.8	10.4
12			6.4	09.8
+50			7.3	08.9
T.P.	1.48	909.49	8.23	908.01
13			1.6	07.9
+50			2.8	06.7
14			4.2	05.3
+50			5.5	04.0
15			7.0	02.5
+50			8.6	00.9

$$\begin{array}{cccccccc} \frac{0.5}{50} & \frac{1.0}{24} & \frac{5.6}{15} & & \frac{5.4}{16} & \frac{6.6}{20.23} & \frac{5.6}{30} & \frac{7.1}{30} \end{array}$$

$$\begin{array}{cccccccc} \frac{40.1}{50} & \frac{1.6}{25} & \frac{5.3}{16} & & \frac{5.8}{20} & \frac{3.4}{28} & \frac{4.6}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{3.3}{50} & \frac{3.9}{23} & \frac{5.8}{15} & & \frac{5.8}{16} & \frac{5.1}{22} & \frac{3.2}{29} & \frac{4.5}{50} \end{array}$$

$$\begin{array}{cccccccccc} \frac{6.0}{50} & \frac{5.3}{20} & \frac{6.4}{15} & & \frac{6.1}{14} & \frac{5.9}{17} & \frac{5.9}{24} & \frac{4.1}{30} & \frac{5.1}{50} \end{array}$$

$$\begin{array}{cccccccccc} \frac{6.7}{50} & \frac{6.6}{26} & \frac{6.9}{19} & \frac{7.8}{17.15} & \frac{6.6}{12} & & \frac{6.8}{13} & \frac{6.0}{21} & \frac{4.3}{22} & \frac{6.3}{36} & \frac{6.8}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{8.8}{50} & \frac{8.4}{18} & \frac{9.0}{17.14} & \frac{7.7}{11} & & \frac{7.9}{15} & \frac{7.8}{22} & \frac{6.6}{26} & \frac{6.8}{50} \end{array}$$

SE Cor Bottom Steps Lt 12460

$$\begin{array}{cccccccc} \frac{3.2}{50} & \frac{2.6}{18} & \frac{2.8}{16.15} & \frac{1.9}{12} & & \frac{1.9}{12} & \frac{1.2}{21} & \frac{0.1}{22} & \frac{0.0}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{5.4}{50} & \frac{4.3}{38} & \frac{3.9}{24} & \frac{3.9}{16} & \frac{3.2}{14} & & \frac{3.3}{13} & \frac{0.6}{25} & \frac{1.0}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{6.2}{50} & \frac{4.9}{20} & \frac{4.5}{12} & & \frac{4.5}{16} & \frac{3.1}{23} & \frac{3.6}{32} & \frac{4.3}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{6.6}{50} & \frac{5.9}{38} & \frac{5.0}{20} & \frac{6.6}{15} & \frac{5.9}{12} & & \frac{6.0}{18} & \frac{5.8}{25} & \frac{6.7}{41} & \frac{7.2}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{9.2}{50} & \frac{6.7}{21} & \frac{8.2}{16} & \frac{7.4}{12} & & \frac{7.6}{17} & \frac{7.2}{25} & \frac{8.7}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{13.2}{50} & \frac{9.2}{19} & \frac{9.2}{12} & & \frac{9.2}{15} & \frac{8.4}{21} & \frac{10.3}{50} \end{array}$$

Sta.	+	+	-	Elev.
		909.49		
16			10.2	99.3
T.P.	2.23	900.47	11.25	898.24
+50			2.7	97.8
17			4.3	96.2
+50			5.7	94.8
18			7.0	93.5
+50			8.4	92.1
19			9.8	90.7
+50			11.2	89.3
20			12.6	87.9
+29			13.3	87.2
B.M.			13.31	887.16
T.P.	10.64	910.79	0.32	900.15
T.P.	4.47	915.03	0.23	910.56
B.M.			8.21	906.82
				906.76

$$\begin{array}{r} 16.7 \\ \hline 50 \end{array} \quad \begin{array}{r} 13.1 \\ \hline 21 \end{array} \quad \begin{array}{r} 10.8 \\ \hline 12 \end{array} \quad 10.2 \quad \begin{array}{r} 10.8 \\ \hline 19 \end{array} \quad \begin{array}{r} 10.1 \\ \hline 25 \end{array} \quad \begin{array}{r} 10.7 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 10.9 \\ \hline 50 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 23 \end{array} \quad \begin{array}{r} 3.3 \\ \hline 11 \end{array} \quad 2.7 \quad \begin{array}{r} 3.1 \\ \hline 18 \end{array} \quad \begin{array}{r} 2.7 \\ \hline 22 \end{array} \quad \begin{array}{r} 1.4 \\ \hline 40 \end{array} \quad \begin{array}{r} 1.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 12.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 7.8 \\ \hline 20 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 12 \end{array} \quad 4.3 \quad \begin{array}{r} 4.6 \\ \hline 16 \end{array} \quad \begin{array}{r} 4.1 \\ \hline 27 \end{array} \quad \begin{array}{r} 3.0 \\ \hline 24 \end{array} \quad \begin{array}{r} 1.7 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 13.4 \\ \hline 50 \end{array} \quad \begin{array}{r} 11.1 \\ \hline 32 \end{array} \quad \begin{array}{r} 7.3 \\ \hline 16 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 13 \end{array} \quad 5.7 \quad \begin{array}{r} 6.2 \\ \hline 15 \end{array} \quad \begin{array}{r} 3.4 \\ \hline 25 \end{array} \quad \begin{array}{r} 1.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 13.7 \\ \hline 50 \end{array} \quad \begin{array}{r} 11.3 \\ \hline 28 \end{array} \quad \begin{array}{r} 8.8 \\ \hline 16 \end{array} \quad \begin{array}{r} 7.6 \\ \hline 12 \end{array} \quad 7.0 \quad \begin{array}{r} 7.6 \\ \hline 20 \end{array} \quad \begin{array}{r} 2.7 \\ \hline 32 \end{array} \quad \begin{array}{r} 1.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 13.7 \\ \hline 50 \end{array} \quad \begin{array}{r} 10.7 \\ \hline 24 \end{array} \quad \begin{array}{r} 8.6 \\ \hline 16 \end{array} \quad 8.4 \quad \begin{array}{r} 9.0 \\ \hline 16 \end{array} \quad \begin{array}{r} 7.3 \\ \hline 25 \end{array} \quad \begin{array}{r} 3.2 \\ \hline 34 \end{array} \quad \begin{array}{r} 1.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 14.7 \\ \hline 50 \end{array} \quad \begin{array}{r} 12.2 \\ \hline 27 \end{array} \quad \begin{array}{r} 10.6 \\ \hline 22 \end{array} \quad 9.8 \quad \begin{array}{r} 10.3 \\ \hline 24 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 34 \end{array} \quad \begin{array}{r} 3.3 \\ \hline 50 \end{array}$$

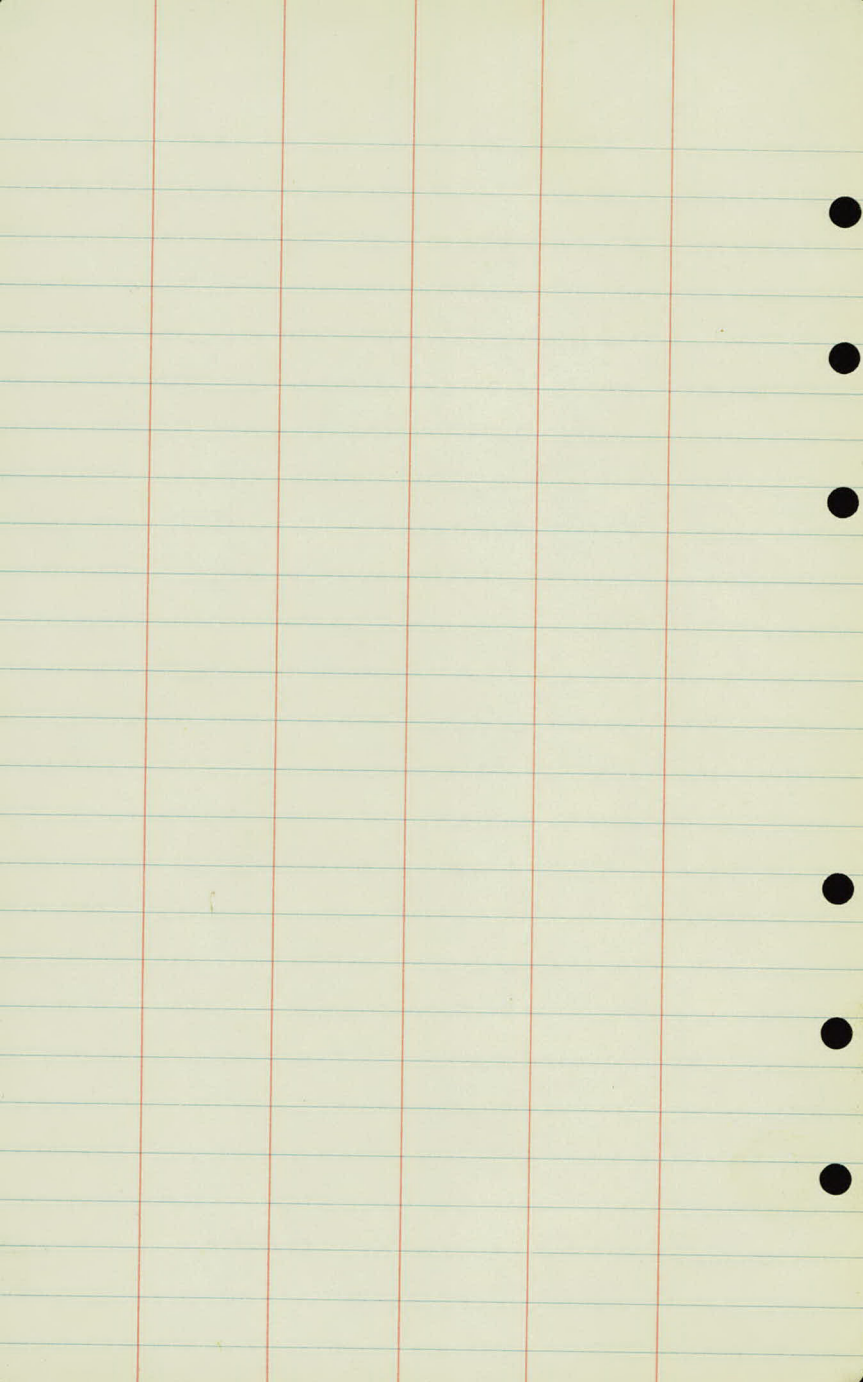
$$\begin{array}{r} 12.7 \\ \hline 50 \end{array} \quad \begin{array}{r} 12.7 \\ \hline 36 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 10 \end{array} \quad 4.2 \quad \begin{array}{r} 11.9 \\ \hline 30 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 40 \end{array} \quad \begin{array}{r} 9.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 13.6 \\ \hline 50 \end{array} \quad \begin{array}{r} 13.0 \\ \hline 21 \end{array} \quad \begin{array}{r} 14.0 \\ \hline 15 \end{array} \quad \begin{array}{r} 13.4 \\ \hline 10 \end{array} \quad 12.6 \quad \begin{array}{r} 12.6 \\ \hline 21 \end{array} \quad \begin{array}{r} 13.0 \\ \hline 37 \end{array} \quad \begin{array}{r} 13.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 14.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 13.6 \\ \hline 30 \end{array} \quad 13.3 \quad \begin{array}{r} 13.3 \\ \hline 50 \end{array}$$

Top Mon Long Lake Rd. Co Rd F.

Top Spike 32' S.E Sta. 7+13.5



Approach Survey for
Long Lake Rd.
of Cemetery Rd.

Sta	+	Δ	-	Elev.
B.M.	8.41	915.17		906.76
0+00 = 7+13.5 (Long Lake Rd) 6.4				08.8
+50			6.0	09.2
1			5.3	09.9
+50			4.9	10.3
2			4.6	10.6
+50			4.2	11.0
3			3.7	11.5
+50			3.3	11.9
4			2.8	12.4
+50			1.9	13.3
5			0.7	14.5
B.M.	8.41			906.76
				906.76

Spike in PP 32 SE. Sta 7+13.5

$$\begin{array}{r} \underline{9.1} \quad \underline{9.4} \quad \underline{6.3} \quad \underline{6.4} \quad \underline{8.7} \quad \underline{7.5} \quad \underline{6.9} \\ 50 \quad 21 \quad 13 \quad 13 \quad 18 \quad 22 \quad 50 \end{array}$$

$$\begin{array}{r} \underline{6.8} \quad \underline{7.0} \quad \underline{8.0} \quad \underline{5.5} \quad \underline{5.6} \quad \underline{7.2} \quad \underline{6.2} \quad \underline{6.1} \\ 50 \quad 29 \quad 26-20 \quad 14 \quad 13 \quad 18-22 \quad 25 \quad 50 \end{array}$$

$$\begin{array}{r} \underline{5.3} \quad \underline{5.1} \quad \underline{7.0} \quad \underline{5.2} \quad \underline{5.0} \quad \underline{6.8} \quad \underline{5.2} \quad \underline{5.5} \\ 50 \quad 27 \quad 21-18 \quad 13 \quad 13 \quad 18-22 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} \underline{4.9} \quad \underline{4.4} \quad \underline{6.8} \quad \underline{4.7} \quad \underline{4.8} \quad \underline{6.5} \quad \underline{5.2} \quad \underline{5.0} \\ 50 \quad 28 \quad 22-18 \quad 13 \quad 13 \quad 18-22 \quad 27 \quad 50 \end{array}$$

$$\begin{array}{r} \underline{3.5} \quad \underline{3.6} \quad \underline{6.4} \quad \underline{4.4} \quad \underline{4.6} \quad \underline{6.4} \quad \underline{5.3} \quad \underline{6.0} \quad \underline{6.8} \\ 50 \quad 29 \quad 22-18 \quad 13 \quad 13 \quad 19-23 \quad 26 \quad 35 \quad 50 \end{array}$$

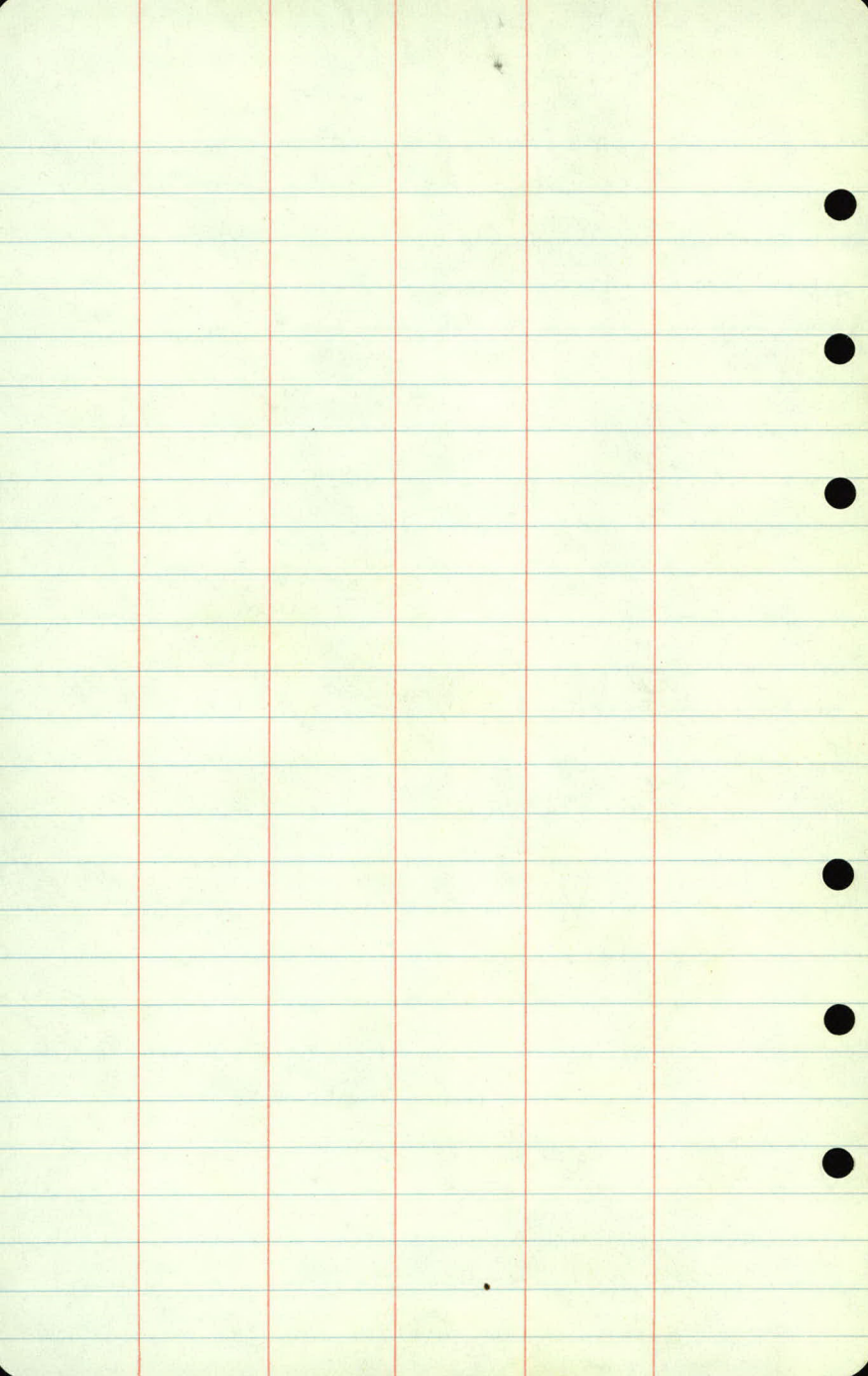
$$\begin{array}{r} \underline{2.6} \quad \underline{3.1} \quad \underline{5.4} \quad \underline{4.2} \quad \underline{4.0} \quad \underline{5.9} \quad \underline{4.8} \quad \underline{6.1} \quad \underline{6.3} \\ 50 \quad 29 \quad 22-18 \quad 13 \quad 13 \quad 18-22 \quad 25 \quad 41 \quad 50 \end{array}$$

$$\begin{array}{r} \underline{3.5} \quad \underline{3.5} \quad \underline{5.5} \quad \underline{3.7} \quad \underline{3.7} \quad \underline{5.5} \quad \underline{4.2} \quad \underline{4.6} \\ 50 \quad 27 \quad 24-20 \quad 15 \quad 13 \quad 17-21 \quad 23 \quad 50 \end{array}$$

$$\begin{array}{r} \underline{3.4} \quad \underline{3.9} \quad \underline{4.8} \quad \underline{3.1} \quad \underline{3.1} \quad \underline{5.3} \quad \underline{4.5} \quad \underline{4.6} \\ 50 \quad 25 \quad 22-18 \quad 14 \quad 13 \quad 17-20 \quad 24 \quad 50 \end{array}$$

$$\begin{array}{r} \underline{4.8} \quad \underline{4.6} \quad \underline{2.2} \quad \underline{2.3} \quad \underline{5.0} \quad \underline{5.1} \\ 50 \quad 18 \quad 13 \quad 13 \quad 20 \quad 50 \end{array}$$

$$\begin{array}{r} \underline{4.2} \quad \underline{4.0} \quad \underline{1.1} \quad \underline{1.1} \quad \underline{3.8} \quad \underline{4.4} \\ 50 \quad 22 \quad 14 \quad 13 \quad 21 \quad 50 \end{array}$$



Staking Notes

Ditch

Long Lake Rd. Near Co. Rd. "F"

3 Pages

Sta.	+	A	-	Grade.	
B.M.	1.90	889.49			887.59
0	100	S. End Cully.		77.5	
	+48	N. FL. Cully.		77.3	
	+60			77.3	
1				77.1	
	+50			76.9	
2				76.7	
	+20			76.6	
	+40			76.5	
3				76.3	
	+50			76.1	
I.P.	0.93	882.29	8.13	881.36	
4				75.9	

Cor. Road. Lt. R. Rd.

Top Road Co. Rd. "F" & Long Lake Rd.

12.0

12.2

12.2

$$7.2 / \frac{9.1}{13.1}$$

$$\frac{9.7}{12.5} / 4.0$$

12.4

$$4.4 / \frac{10.7}{11.7}$$

$$\frac{10.5}{11.7} / 4.8$$

12.4

$$5.6 / \frac{10.3}{12.3}$$

$$\frac{10.3}{12.3} / 5.6$$

12.8

$$\frac{.04}{.20} / .280$$

12.9

$$5.6 / \frac{10.6}{12.3}$$

$$\frac{10.4}{12.5} / 4.0$$

13.0

$$6.4 / \frac{10.3}{12.7}$$

$$\frac{11.0}{12.0} / 5.0$$

13.2

$$6.4 / \frac{10.5}{12.7}$$

$$\frac{10.8}{12.4} / 5.8$$

13.4

$$6.2 / \frac{10.8}{12.6}$$

$$\frac{11.0}{12.4} / 5.8$$

6.4

$$6.0 / \frac{3.9}{12.5}$$

$$\frac{4.1}{12.3} / 5.6$$

Sta.	+	T	-	Grade
------	---	---	---	-------

852.29

4	150		757	757
---	-----	--	-----	-----

463	71	75.6
-----	----	------

5				75.5
---	--	--	--	------

125				75.4
-----	--	--	--	------

+ 36 Approach Ditch to Lake

T.P.	640	882.46	623	876.06
------	-----	--------	-----	--------

Flow Line Cuts. 8.5

450				8.4
-----	--	--	--	-----

6				88
---	--	--	--	----

150				9.0
-----	--	--	--	-----

7				9.2
---	--	--	--	-----

150				94
-----	--	--	--	----

$$\frac{4.7}{2} / \frac{4}{8}$$

Gr. Rod.

Lt.

R

Rt.

6.6

6.7

$$4.4 / \frac{50}{4.7}$$

$$\frac{51}{4.6} / 4.2$$

6.8

$$4.2 / \frac{52}{4.6}$$

$$\frac{52}{4.6} / 4.2$$

6.9

$$50 / \frac{4.9}{4.0}$$

$$\frac{51}{4.9} / 4.8$$

Top 24" Cong. Calc

$$4.6 / \frac{50}{4.6}$$

$$\frac{50}{4.6} / 4.6$$

$$4.7 / \frac{51}{4.7}$$

$$\frac{48}{4.0} / 5.0$$

$$4.8 / \frac{5.2}{4.8}$$

$$\frac{48}{4.2} / 5.2$$

$$4.6 / \frac{5.6}{4.6}$$

$$\frac{58}{4.4} / 4.4$$

$$3.8 / \frac{6.6}{4.8}$$

$$\frac{61}{4.3} / 4.3$$

882.46

7 +77 2 Drives 9 Flow Line Culv. 9.5

8 9.6

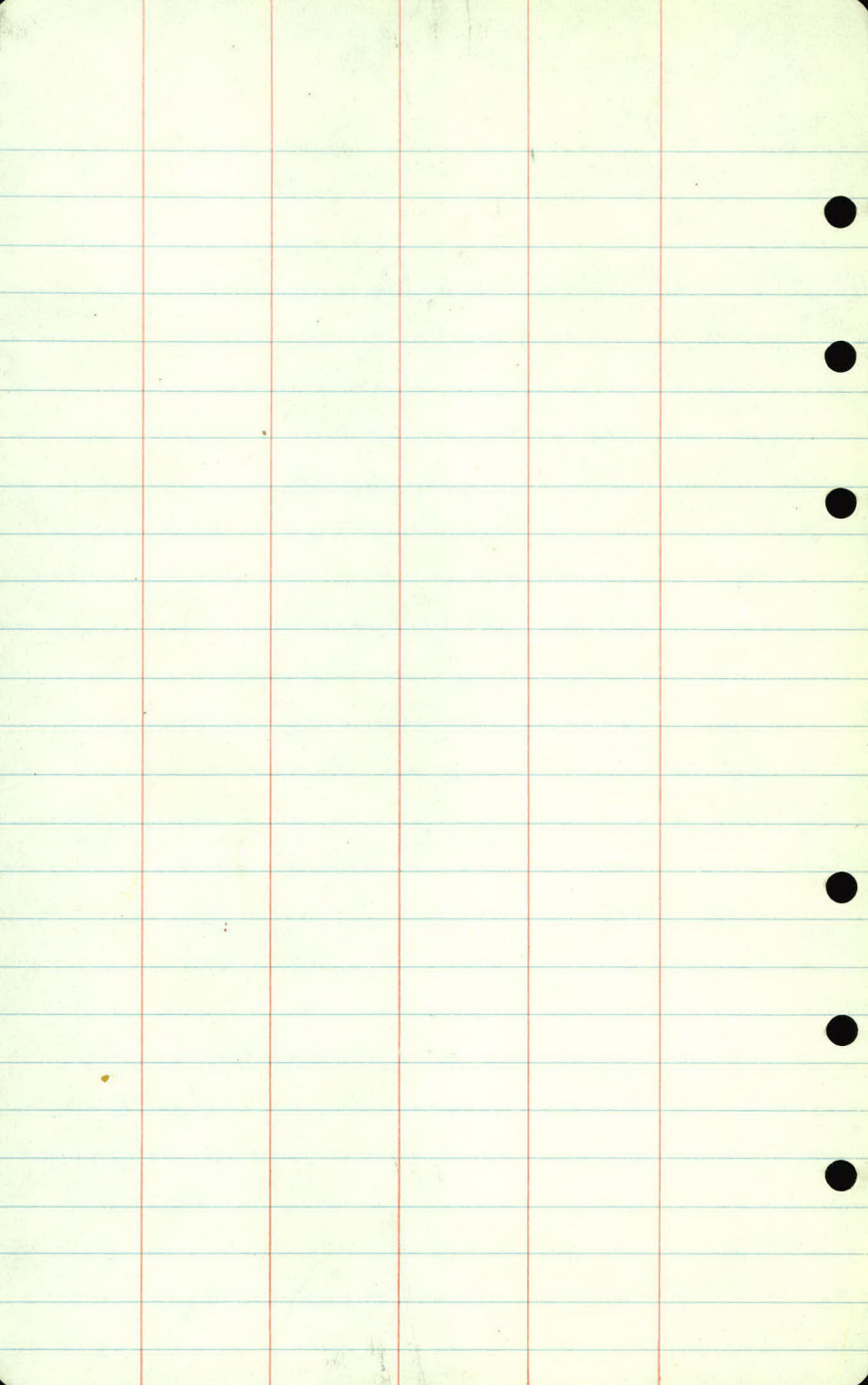
125 9.7

FL. oldGulr

(87)

$$\begin{array}{r} 71 \\ 25 \overline{) 175} \\ \underline{175} \\ 0 \end{array}$$

$$\begin{array}{r} 68 \\ 128 \overline{) 8656} \\ \underline{768} \\ 976 \\ \underline{976} \\ 0 \end{array}$$



①
Slope Stakes
Long Lake Rd.

S.T.H. #8 to Co. Rd. "F"

staked - 9-26-39. 53 sheets.

Party:

R.R.

A.M.

L.G.

C.F.

Sta	+	⌵	-	Elev
B.M.	11.55	918.31		906.76 (906.76)
0+00				15.3
+50				14.6
1				13.9
+50				13.2
2				12.5
50				11.8
3				11.1
50				10.4
4				09.7
T.P.	4.23	912.59	9.95	908.36
+50				09.0
5				08.3
+50				
+50				07.6

Top Spike 32'S.E Sta 7+14

3.0

3.7

4.4

$$\begin{array}{r} 0.5 \\ C3.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.2 \\ C0.2 \\ \hline \end{array}$$

5.1

$$\begin{array}{r} 1.2 \\ C3.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ C0.3 \\ \hline 27.6 \end{array}$$

5.8

$$\begin{array}{r} 2.0 \\ C3.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ DC1.9 \\ \hline 26.8 \end{array}$$

6.5

$$\begin{array}{r} 7.7 \\ DC0.8 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 6.3 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.1 \\ DC1.4 \\ \hline 25.8 \end{array}$$

7.2

$$\begin{array}{r} 9.2 \\ DC0.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 7.5 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 7.6 \\ DC1.6 \\ \hline 26.2 \end{array}$$

7.9

$$\begin{array}{r} 10.5 \\ F2.6 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 8.7 \\ F0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 10.4 \\ F2.5 \\ \hline 20 \end{array}$$

8.6

$$\begin{array}{r} 14.9 \\ F6.3 \\ \hline 27.6 \end{array}$$

$$\begin{array}{r} 9.8 \\ F1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 15.2 \\ F6.6 \\ \hline 28.2 \end{array}$$

3.6

$$\begin{array}{r} 10.7 \\ F7.1 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ F1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 12.0 \\ F8.4 \\ \hline 31.3 \end{array}$$

4.3

$$\begin{array}{r} 10.0 \\ F5.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 5.1 \\ F0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ FG.4 \\ \hline 27.8 \end{array}$$

5.0

$$\begin{array}{r} 7.6 \\ F2.6 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ C0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ F5.7 \\ \hline 26.4 \end{array}$$

Sta	+	π	-	Elev.	Spec. Ditch
		912.57 ⁶			
6				06.9	
	+50			06.2	02.65
	+92			05.7	2.94
7				05.6	3.00
	+26			05.5	3.18
	+33			05.4	3.23
	+50			05.4	3.35
8				05.4	03.7
T.P	5.52	915.59 ⁶	2.50	910.07	
	+50			05.7	
9				06.3	
	+50			07.1	
10				08.0	

5.7	$\begin{array}{r} 9.6 \\ F 3.9 \\ \hline 22.8 \end{array}$	$\begin{array}{r} 4.6 \\ C 1.1 \\ \hline \end{array}$	$\begin{array}{r} 9.7 \\ F 4.0 \\ \hline 23.0 \end{array}$	
6.4	$\begin{array}{r} 10.1 \\ F 3.7 \\ \hline 22.4 \end{array}$	$\begin{array}{r} 4.3 \\ C 2.1 \\ \hline \end{array}$	$\begin{array}{r} 4.4 \\ C 2.0 \\ \hline 15 \end{array}$	$\begin{array}{r} 7.92 \\ C 2.0 \\ \hline 35 \end{array}$
6.9	$\begin{array}{r} 6.9 \\ C 0.0 \\ \hline 33 \end{array}$	$\begin{array}{r} 4.0 \\ C 2.9 \\ \hline \end{array}$	$\begin{array}{r} 4.9 \\ C 2.0 \\ \hline 15 \end{array}$	$\begin{array}{r} 7.63 \\ C 2.0 \\ \hline 35 \end{array}$
7.0		$\begin{array}{r} 4.0 \\ C 3.0 \\ \hline \end{array}$	$\begin{array}{r} 5.0 \\ C 2.0 \\ \hline 15 \end{array}$	$\begin{array}{r} 6.57 \\ C 3.0 \\ \hline 35 \end{array}$
7.1		$\begin{array}{r} 3.8 \\ C 3.3 \\ \hline \end{array}$	$\begin{array}{r} 4.1 \\ C 3.0 \\ \hline 15 \end{array}$	$\begin{array}{r} 6.39 \\ C 3.0 \\ \hline 35 \end{array}$
7.2		$\begin{array}{r} 3.8 \\ C 3.4 \\ \hline \end{array}$	$\begin{array}{r} 4.2 \\ C 3.0 \\ \hline 15 \end{array}$	$\begin{array}{r} 6.34 \\ C 3.0 \\ \hline 35 \end{array}$
7.2	$\begin{array}{r} 5.0 \\ C 2.2 \\ \hline 31.4 \end{array}$	$\begin{array}{r} 3.7 \\ C 3.5 \\ \hline \end{array}$	$\begin{array}{r} 4.2 \\ C 3.0 \\ \hline 15 \end{array}$	$\begin{array}{r} 6.22 \\ C 3.0 \\ \hline 35 \end{array}$
7.2	$\begin{array}{r} 4.2 \\ C 3.0 \\ \hline 33 \end{array}$	$\begin{array}{r} 3.1 \\ C 4.1 \\ \hline \end{array}$	$\begin{array}{r} 3.2 \\ C 4.0 \\ \hline 15 \end{array}$	$\begin{array}{r} 5.9 \\ C 3.0 \\ \hline 35 \end{array}$
9.9	$\begin{array}{r} 6.9 \\ C 3.0 \\ \hline 33.0 \end{array}$	$\begin{array}{r} 5.5 \\ C 4.4 \\ \hline \end{array}$		$\begin{array}{r} 8.9 \text{ Tot} \\ C 3.0 \\ \hline 35 \end{array}$
9.3	$\begin{array}{r} 5.4 \\ C 3.9 \\ \hline 33 \end{array}$	$\begin{array}{r} 5.0 \\ C 4.3 \\ \hline \end{array}$		$\begin{array}{r} 8.3 \text{ Tot} \\ C 3.0 \\ \hline 35 \end{array}$
8.5	$\begin{array}{r} 1.3 \\ C 7.2 \\ \hline 33 \end{array}$	$\begin{array}{r} 4.6 \\ C 3.9 \\ \hline \end{array}$		$\begin{array}{r} 7.5 \text{ Tot} \\ C 3.0 \\ \hline 35 \end{array}$
7.6	$\begin{array}{r} 10.6 \\ C 7.8 \\ \hline 33.0 \end{array}$	$\begin{array}{r} 4.3 \\ C 3.3 \\ \hline \end{array}$	$\begin{array}{r} 5.0 \\ C 2.6 \\ \hline 32.2 \end{array}$	

Sta	+	π	-	Elev.
-----	---	-------	---	-------

915.59

10 + 50

08.5

11

08.9

T.P. 2.51

913.38⁴ 4.72

910.87

+50

08.9

12

08.7

+50

08.2

13

07.4

+50

06.3

14

+50

15

T.P. 2.53

904.40 11.51

901.87

+50

16

Elev. 8" Below

$$\begin{array}{r}
 7.1 \\
 \hline
 62.0 \\
 C 7.1 \\
 \hline
 33
 \end{array}
 \qquad
 \begin{array}{r}
 4.3 \\
 \hline
 C 2.8
 \end{array}
 \qquad
 \begin{array}{r}
 3.5 \\
 \hline
 C 3.8 \\
 \hline
 33.0
 \end{array}$$

$$\begin{array}{r}
 6.7 \\
 \hline
 3.1 \\
 C 3.6 \\
 \hline
 33.0
 \end{array}
 \qquad
 \begin{array}{r}
 4.7 \\
 \hline
 C 2.0
 \end{array}
 \qquad
 \begin{array}{r}
 2.8 \\
 \hline
 C 3.9 \\
 \hline
 33.0
 \end{array}$$

$$\begin{array}{r}
 4.5 \\
 \hline
 2.5 \\
 C 2.0 \\
 \hline
 31.0
 \end{array}
 \qquad
 \begin{array}{r}
 3.0 \\
 \hline
 C 1.5
 \end{array}
 \qquad
 \begin{array}{r}
 1.7 \\
 \hline
 C 2.8 \\
 \hline
 32.6
 \end{array}$$

$$\begin{array}{r}
 4.7 \\
 \hline
 3.7 \\
 C 1.0 \\
 \hline
 29.0
 \end{array}
 \qquad
 \begin{array}{r}
 3.6 \\
 \hline
 C 1.1
 \end{array}
 \qquad
 \begin{array}{r}
 2.6 \\
 \hline
 C 2.1 \\
 \hline
 31.2
 \end{array}$$

$$\begin{array}{r}
 5.2 \\
 \hline
 5.6 \\
 C 1.6 \\
 \hline
 26.2
 \end{array}
 \qquad
 \begin{array}{r}
 4.4 \\
 \hline
 C 0.8
 \end{array}
 \qquad
 \begin{array}{r}
 3.7 \\
 \hline
 C 1.5 \\
 \hline
 30.0
 \end{array}$$

$$\begin{array}{r}
 6.0 \\
 \hline
 6.6 \\
 C 1.4 \\
 \hline
 25.8
 \end{array}
 \qquad
 \begin{array}{r}
 5.5 \\
 \hline
 C 0.5
 \end{array}
 \qquad
 \begin{array}{r}
 3.6 \\
 \hline
 C 2.4 \\
 \hline
 31.8
 \end{array}$$

$$\begin{array}{r}
 7.1 \\
 \hline
 7.9 \\
 C 1.2 \\
 \hline
 25.4
 \end{array}
 \qquad
 \begin{array}{r}
 6.7 \\
 \hline
 C 0.4
 \end{array}
 \qquad
 \begin{array}{r}
 4.4 \\
 \hline
 C 2.7 \\
 \hline
 32.4
 \end{array}$$

$$\begin{array}{r}
 8.1 \\
 \hline
 9.4 \\
 C 1.7 \\
 \hline
 24.4
 \end{array}
 \qquad
 \begin{array}{r}
 7.9 \\
 \hline
 C 0.2
 \end{array}
 \qquad
 \begin{array}{r}
 7.5 \\
 \hline
 C 0.6 \\
 \hline
 28.2
 \end{array}$$

$$\begin{array}{r}
 9.6 \\
 \hline
 10.4 \\
 C 1.2 \\
 \hline
 25.4
 \end{array}
 \qquad
 \begin{array}{r}
 9.4 \\
 \hline
 C 0.2
 \end{array}
 \qquad
 \begin{array}{r}
 9.3 \\
 \hline
 C 0.3 \\
 \hline
 27.6
 \end{array}$$

$$\begin{array}{r}
 11.1 \\
 \hline
 11.1 \\
 C 0.0 \\
 \hline
 27.0
 \end{array}
 \qquad
 \begin{array}{r}
 10.9 \\
 \hline
 C 0.2
 \end{array}
 \qquad
 \begin{array}{r}
 10.9 \\
 \hline
 C 0.2 \\
 \hline
 27.4
 \end{array}$$

$$\begin{array}{r}
 3.7 \\
 \hline
 5.1 \\
 C 0.6 \\
 \hline
 24.2
 \end{array}
 \qquad
 \begin{array}{r}
 3.5 \\
 \hline
 C 0.2
 \end{array}
 \qquad
 \begin{array}{r}
 3.7 \\
 \hline
 C 0.0 \\
 \hline
 27.0
 \end{array}$$

$$\begin{array}{r}
 5.4 \\
 \hline
 7.1 \\
 C 1.7 \\
 \hline
 18.4
 \end{array}
 \qquad
 \begin{array}{r}
 5.2 \\
 \hline
 C 0.2
 \end{array}
 \qquad
 \begin{array}{r}
 5.0 \\
 \hline
 C 0.4 \\
 \hline
 27.8
 \end{array}$$

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		904.40		
--	--	--------	--	--

16+50				
-------	--	--	--	--

17				
----	--	--	--	--

+50				
-----	--	--	--	--

18				
----	--	--	--	--

T.P.	2.94	895.27	12.07	892.33
------	------	--------	-------	--------

+50				
-----	--	--	--	--

19				
----	--	--	--	--

+50				
-----	--	--	--	--

20				
----	--	--	--	--

+29				
-----	--	--	--	--

				887.16
--	--	--	--	--------

B.M.				
------	--	--	--	--

			8.15	
--	--	--	------	--

				887.12
--	--	--	--	--------

G. R.

6.8

$$\begin{array}{r} 10.3 \\ F3.5 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ C0.6 \\ \hline 28.2 \end{array}$$

8.3

$$\begin{array}{r} 12.2 \\ F3.9 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 8.1 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ C1.9 \\ \hline 30.8 \end{array}$$

9.7

$$\begin{array}{r} 12.4 \\ F2.7 \\ \hline 20.4 \end{array}$$

$$\begin{array}{r} 9.5 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ C3.2 \\ \hline 32.0 \end{array}$$

11.2

$$\begin{array}{r} 13.2 \\ F2.0 \\ \hline 19.0 \end{array}$$

$$\begin{array}{r} 11.0 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ C4.8 \\ \hline 33 \end{array}$$

3.4

$$\begin{array}{r} 5.2 \\ C0.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 3.2 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} +3.3 \\ C6.5 \\ \hline 33 \end{array}$$

4.8

$$\begin{array}{r} 6.1 \\ C0.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 4.6 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} +0.4 \\ C5.2 \\ \hline 33.0 \end{array}$$

6.2

$$\begin{array}{r} 7.0 \\ C01.2 \\ \hline 25.4 \end{array}$$

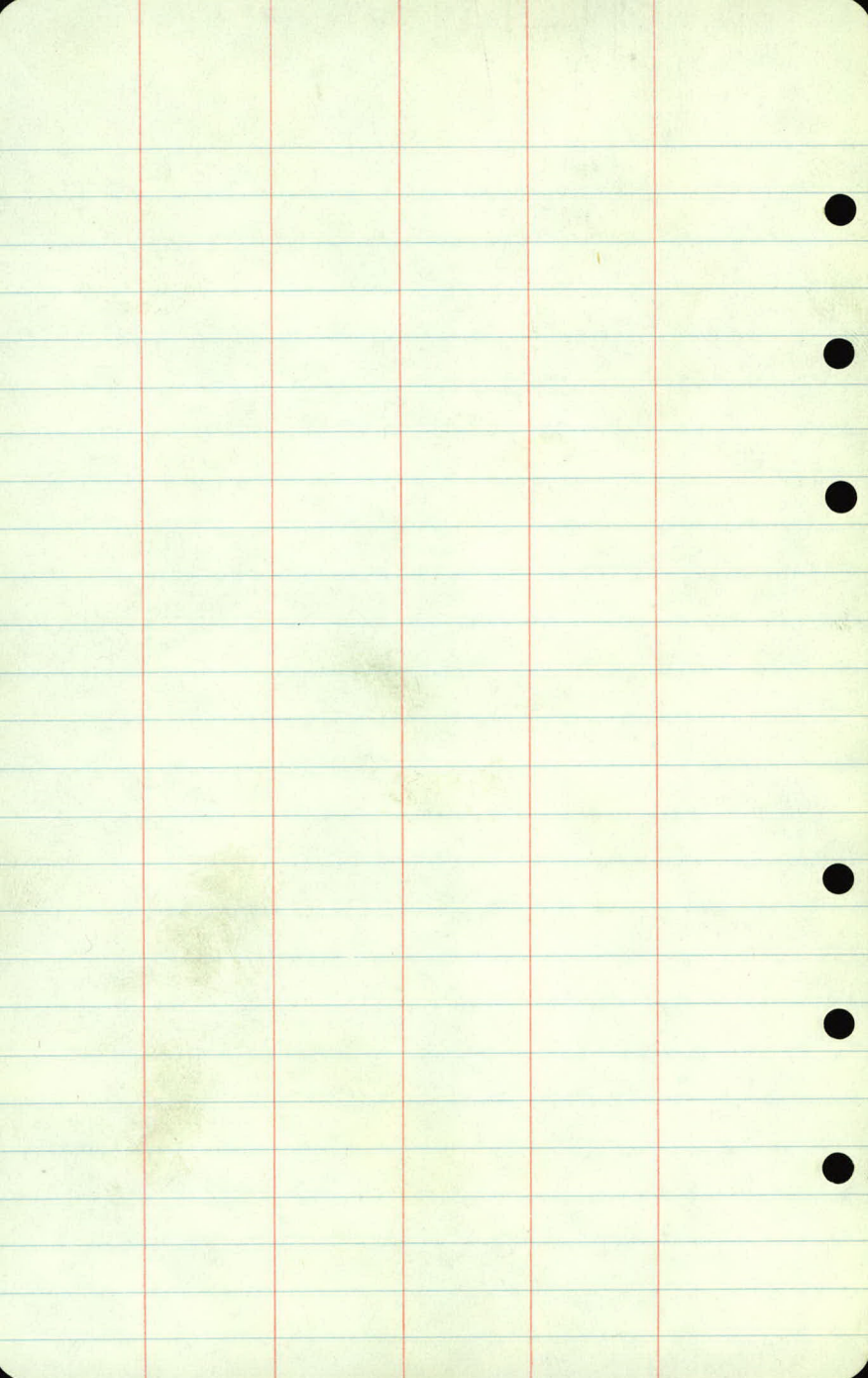
$$\begin{array}{r} 6.0 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ C01.7 \\ \hline 26.4 \end{array}$$

7.6

$$\begin{array}{r} 7.4 \\ C0.2 \\ \hline \end{array}$$

Top Mon. 5/9 20 + 29.82



Long Lake Rd.

S. T. H. = 8

to Front St.

Blue Tops & Slope Stakes
for Grade Change

5 1/2 / 40

Sta.	t	π	-	Elev
B.M.	9.90	897.06		887.16
T.P.	10.27	907.05	0.28	896.78
T.P.	6.68	913.14	0.59	906.46
B.M.	8.79	915.27	6.66	906.48

1100

150

+50			14.6	0.7
-----	--	--	------	-----

1			13.9	1.4
---	--	--	------	-----

+50			13.2	2.1 ✓
-----	--	--	------	-------

2			12.5	2.8
---	--	--	------	-----

+50			11.8	3.5
-----	--	--	------	-----

3			11.1	4.2
---	--	--	------	-----

+50			10.4	4.9
-----	--	--	------	-----

4			09.7	5.6
---	--	--	------	-----

+50			09.0	6.3
-----	--	--	------	-----

5			08.3	7.0
---	--	--	------	-----

Top Mon 20 + 29.82 f

(Now)
Spike in P.P. S.E. of Cemetery Road Int.

$$\frac{2.1}{15}$$

$$\frac{2.1}{15}$$

$$\frac{2.8}{15}$$

$$\frac{2.8}{15}$$

$$\frac{3.5}{15}$$

$$\frac{3.5}{15}$$

$$\frac{4.2}{15}$$

$$\frac{4.2}{15}$$

$$\frac{4.9}{15}$$

$$\frac{4.9}{15}$$

$$\frac{5.6}{15}$$

$$\frac{5.6}{15}$$

$$\frac{6.3}{15}$$

$$\frac{6.3}{15}$$

$$\frac{7.0}{15}$$

$$\frac{7.0}{15}$$

Sta.	+	π	-	Elev.	
		915.27			
5+50				07.6	7.7
6				06.9	8.4
T.P.	5.61	912.41	8.47	* 906.80	
+50				06.2	02.65
7				05.6	03.0
+50				05.4	03.35
8				* 05.4	03.7
+50				05.7	
9				06.3	
+50				07.1	
10				08.0	
T.P.	5.27	913.92	3.76	* 908.65 *	
+50				08.3	
11				08.6	

35' R.H.

Ditch Drop 2' at 35'

Grode Change

$$\frac{7.7}{15}$$

$$\frac{7.7}{15}$$

$$\frac{8.4}{15}$$

$$\frac{8.4}{15}$$

$$6.2 \quad 9.76$$

$$\frac{6.2}{15}$$

$$\frac{6.2}{15} \quad \frac{9.76}{35}$$

$$6.8 \quad 9.41$$

$$\frac{6.8}{15}$$

$$\frac{6.8}{15} \quad \frac{9.41}{35}$$

$$7.0 \quad 9.06$$

$$\frac{7.0}{15}$$

$$\frac{7.0}{15} \quad \frac{9.06}{35}$$

$$7.0 \quad 8.71$$

$$\frac{7.0}{15}$$

$$\frac{7.0}{15} \quad \frac{8.71}{35}$$

$$6.7$$

$$\frac{6.7}{15}$$

$$\frac{6.7}{15} \quad \frac{8.7}{35}$$

$$6.1$$

$$\frac{6.1}{15}$$

$$\frac{6.1}{15} \quad \frac{8.1}{35}$$

$$5.3$$

$$\frac{5.3}{15}$$

$$\frac{5.3}{15} \quad \frac{7.8}{35}$$

$$4.4$$

$$\frac{4.4}{15}$$

$$\frac{4.4}{15} \quad \frac{1.8}{2.6} \quad \frac{2.2}{32.2}$$

$$5.6$$

$$\frac{5.6}{15}$$

$$\frac{5.6}{15} \quad \frac{1.6}{4.0} \quad \frac{33.0}{33.0}$$

$$5.3$$

$$\frac{5.3}{15}$$

$$\frac{5.3}{15} \quad \frac{1.2}{4.1} \quad \frac{33.0}{33.0}$$

Sta.	+	Δ	-	Elev.
		913.92		
11	+50			08.5
12				08.1
	+50			07.4
13				06.8
	+50			06.0
14				05.1
+50	3"	Below Present $\frac{1}{2}$ Grade		

5.4

$$\frac{5.4}{15}$$

$$\frac{5.4}{15}$$

$$\frac{2.4}{33.0}$$

5.8

$$\frac{5.8}{15}$$

$$\frac{5.8}{15}$$

$$\frac{3.0}{31.6}$$

6.5

$$\frac{6.1}{27.8}$$

$$\frac{6.5}{15}$$

$$\frac{6.5}{15}$$

$$\frac{4.3}{31.4}$$

7.1

$$\frac{7.1}{27.0}$$

$$\frac{7.1}{15}$$

$$\frac{7.1}{15}$$

$$\frac{4.2}{32.8}$$

7.9

$$\frac{8.5}{25.8}$$

$$\frac{7.9}{15}$$

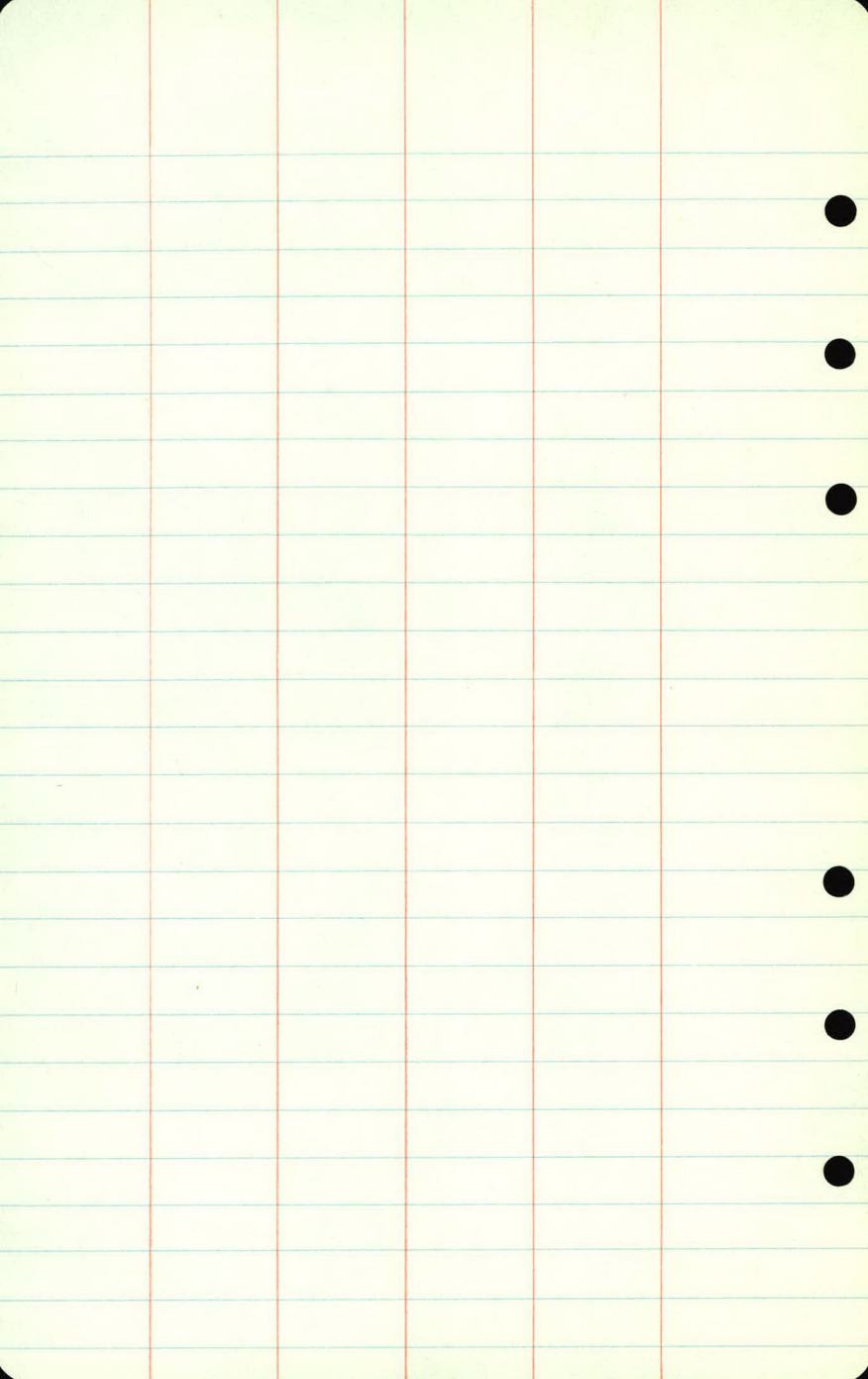
$$\frac{7.9}{15}$$

$$\frac{4.9}{33.0}$$

8.8

$$\frac{8.8}{15}$$

$$\frac{8.8}{15}$$



CEMETARY ROAD

Blue tops & Slope Stakes
for Grade Change

Sta	+	π	-	Elev.
0+00				05.6
+50				06.1
1				06.5
+50				07.3
2				08.5
+50				10.0
3				11.2
+50				11.9
4				12.4