

BK. 136 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

E & Ditch.....Survey

Also x-sections Co. Rd. "D" No.

EDGERTON ST......

From La bore Rd...... To Centerville Rd.

Road Acc't. No.

Date Filed 12-9-47

File

Reid 11-29-47 WTS

Edgerton St.

Land and Ditch Profiles

La Bore Rd. to Centerville Rd.

Same Data as 1944 Plan Survey

32 Pages

Sta.	+	π	-	Elev.
B.M.	3.92	913.32		<u>909.40</u>

127				96.89.
-----	--	--	--	--------

+45				98.15.
-----	--	--	--	--------

+55				
-----	--	--	--	--

128				99.94.
-----	--	--	--	--------

+50				01.65
-----	--	--	--	-------

129				03.09
-----	--	--	--	-------

+50				04.46
-----	--	--	--	-------

130				05.68
-----	--	--	--	-------

K.A. 11-24-47
A.M.
M.B.

2

Ditch L

E

Ditch R

16.43

96.45

1517

16.87

F.L. N. End 18" CM.

96.52

16.80

F.L. N. End 15" CM

98.22

15.1

19.38

98.32

15.0

99.92

13.4

11.67

00.72

12.6

01.42

11.9

10.23

02.22

11.1

03.02

10.3

8.86

03.52

9.8

04.72

8.6

7.64

04.92

8.4

Sta.	+	π	-	Elev.
------	---	-------	---	-------

913.32

130 +50

06.93

+67

+87

131

08.01

+50

09.21

+58

+78

+87

Ditch L

E

Ditch R

✓

05.42

7.9

639

05.52

7.8

✓

05.88 ✓

7.44

FL. 15" CM.

06.39 ✓

6.93

FL. 15" CM.

✓

06.82

6.5

531

07.02

6.3

✓

✓

07.52

5.8

411

06.94

6.38

FL. 15" CM.

✓

0.2 dirt in culv.

6.31 07.01

FL. 15" CM.

✓

07.16 ✓

6.16

FL. 15" CM.

Sta	+	π	-	Elev
		91332		

132				10.01
-----	--	--	--	-------

+07				
-----	--	--	--	--

+50				10.61
-----	--	--	--	-------

+64				
-----	--	--	--	--

+84				
-----	--	--	--	--

+86				
-----	--	--	--	--

133				10.85
-----	--	--	--	-------

+06				
-----	--	--	--	--

Ditch L

2

Ditch R

07.22

331

6.1

✓

0.4 dirt

07.18 ✓

6.14

FL. 15' CM.

07.42

5.9

271

07.22

6.1

✓

06.82

6.50

FL. 15' CM.

✓

0.6 dirt

07.12

6.20

FL. 15' CM.

✓

6.20

07.34 ✓

598

FL. 15' CM.

07.22

0.4 dirt

2.47

6.1

✓

07.30 ✓

6.02

FL. 15' CM.

Sta.	+	π	-	Elev
		913.32		

133	+50			10.99
-----	-----	--	--	-------

	+62			
--	-----	--	--	--

	+82			
--	-----	--	--	--

	+86			
--	-----	--	--	--

	+88			
--	-----	--	--	--

134				11.06
-----	--	--	--	-------

	+08			
--	-----	--	--	--

	+06			
--	-----	--	--	--

T.P.	537	916.43	2.26	911.06
------	-----	--------	------	--------

Ditch L

E

Ditch R

✓
07.42
5.9

233

07.32

6.0

✓
07.1 231

07.12

6.20

FL. 15 CM.

0.4' dirt

5.92

07.40

5.92

FL. 15 CM.

0.7' dirt

07.48

5.84

FL. 12" CONC.

5.71

07.52 ✓

5.80

FL. 15 CM.

0.8' dirt

5.89

226

0.5' dirt

07.43 ✓

5.89

FL. 15 CM.

0.3' dirt

07.61

2.

5.71

FL. 15 CM.

Sto	+	π	-	Elev
		916.43		

134 +50

11.13

+85

+90

135

11.23

+05

+10

+50

11.25

+75

Ditch L

E

Ditch R

✓

08.33

8.1

5.30

07.53

8.9

✓

07.46

8.97

FL. 15' CM.

✓

Culv.

07.51 ✓

8.92
FL. 15' CM.

0.6' dirt

5.20

Culv. full of dirt

07.61

8.82

FL. 15' CM.

✓

07.47 ✓

8.96
FL. 15' CM.

✓

07.73

8.7

5.18

07.43

9.0

✓

✓

07.73

8.7

Sta	+	π	-	Elev
-----	---	-------	---	------

916.43

136

11.21

+15

+50

11.16

+61

+81

137

11.10

+09

+29

Ditch L E Ditch R

+97-Eat.- cannot find culv.

07.53

522

89

✓

✓

08.23

82

✓

08.13

83

527

07.34

909

FL 15' CM.

✓

0.4' dirt

9.04

FL 15' CM.

07.39

714

12.04

✓

533

07.73

87

✓

07.78 ✓

8.65

FL 15' CM.

culv full dirt

07.66 ✓

877

FL 15' CM.

0.6' dirt

Sta. + π - Elev.

91643

11.57

2.56

137 +50

11.04

+89

138 +50

11.01

+09

+50

11.01

+87

+94

139

10.91

Ditch L

±

Ditch R

✓ 08.23

8.2

539

08.13

8.9

✓

07.74 ✓

8.69

FL 15' G.M.

08.68

7.75

FL 15' G.M. ✓

0.4' dirt

5.42

0.9' dirt

07.73 ✓

8.70

FL 15' G.M.

07.39

9.04

FL 15' G.M. ✓

✓ 07.93

8.5

5.42

07.53

8.9

✓

07.90

8.53

FL 15' G.M. ✓

07.71 ✓

8.72

FL 15' G.M.

8.76

8.42

0.5' dirt

0.3' dirt

5.52

Sta	+	π	-	Elev
		916.43		

139 +07

+14

T.P.	7.30	916.28	7.45	908.98
------	------	--------	------	--------

B.M.			4.70	911.58 (911.57)
------	--	--	------	-----------------

+50				10.96
-----	--	--	--	-------

+88

140				11.03
-----	--	--	--	-------

+08

+27

+47

TP = 745

9

Ditch L

4

Ditch R

07.67

8.76
FL. 15" CM.

08.01

8.42
FL. 15" CM.

Boat Sph in 30" Tw. Coll. 19' L Sta. 139+65

✓ 08.18

8.1

532

8.6

07.68

07.80

8.48
FL. 15" CM.

525

8.58
FL. 15" CM.
0.5' dirt

07.70

8.58
FL. 15" CM.

07.89

8.39
FL. 15" CM.

0.3' dirt

07.82

8.46
FL. 15" CM.

Sta. + π - Elev.
9/6.28

140 +50

11.20

+88

141

11.18

+08

+12

+22 +37
2.

+50

11.22

142 +00

11.15

16.28
7.87
8.41

7.11

10

Ditch L

4

Ditch R

08.08 ✓

5.08

8.2

08.0 ✓

8.28
FL. 15 CM.

0.4' dirt

5.10

07.88 ✓

8.40
FL. 15 CM.

07.66

8.62
FL. 15 CM.
0.9' dirt ✓

07.72

8.56
FL. 15 CM.
Full dirt

08.18 ✓

8.1

5.06

08.08 ✓

8.2

08.06 ✓

8.22
FL. 15 CM.

5.13

0.3' dirt

Sta.	+	π	-	Elev.
		916.28		

142 +20

11.04

+66

+86

+90

143

11.06

+10

+50

10.99

+86

Ditch L

4

Ditch R

07.86 ✓

842
FL 15' GM.

$$450 = 5.24$$

07.86

8.42 ✓
FL 15' GM.

0.4 dirt

8.36
FL 15' GM.

07.92 ✓

07.58 ✓

870
FL 15' GM.
0.6

$$5.22$$

07.60 ✓

8.68
FL 15' GM.
0.2 dirt

07.68 ✓

8.6

$$5.29$$

07.78

8.5 ✓

07.25 ✓

9.03
FL 15' GM.

07.65 ✓

8.69
FL 15' GM.

Sta	+	π	-	Elev.
		916.28		

144				10.88
-----	--	--	--	-------

+06				
-----	--	--	--	--

+50				10.90
-----	--	--	--	-------

+83				
-----	--	--	--	--

145				10.86
-----	--	--	--	-------

+23				
-----	--	--	--	--

+50				10.90
-----	--	--	--	-------

T.P.	4.48	915.36	5.40	910.88
------	------	--------	------	--------

+66				
-----	--	--	--	--

Ditch L

4

Ditch R

0.5' dirt ✓

540

0.7' dirt

07.21 ✓

9.07

FL. 156M.

07.89

839

FL. 156M. ✓

07.38 ✓

8.9

538

07.98

8.3 ✓

07.26 ✓

9.02

FL. 156M.

0.9' dirt

Road to West

542

07.22 ✓

9.06

FL. 156M.

0.4' dirt

06.98 ✓

9.3

538

07.68

8.6 ✓

07.46

790

FL. 156M. ✓

Sta	+	π	-	Elev
		915.36		

145 +96

146 +00

10.85

+06

+16

+50

10.82

+86

147

10.58

+06

Ditch L

E

Ditch R

06.77 ✓

859
FL. 15" C.M.

0.6' dirt

451

870
FL. 15" C.M.

0.6' dirt ✓

07.26

810 ✓
FL. 15" C.M.

06.74

862 ✓
FL. 15" C.M.

07.56 ✓

7.8

454

06.96

8.4 ✓

06.48 ✓

888
FL. 15" C.M.
0.7' dirt

06.93

843 ✓
FL. 15" C.M.

478

0.2' dirt

06.18 ✓

913
FL. 15" C.M.
1.0' dirt

06.60

876 ✓
FL. 15" C.M.

Sta	+	π	-	Elev.
-----	---	-------	---	-------

915.36

147 +50

10.45

+98

148

10.26

+18

+50

10.29

+59

+79

+86

Ditch L

4

Ditch R

06.76 ✓

8.6

491

06.26

9.1 ✓

05.64

9.72 ✓

FL. 15' C.M.

05' dirt

510

05.72

9.64

FL. 15' C.M.

Full dirt ✓

05.66 ✓

9.7

507

05.46

9.9 ✓

✓ 05.34

10.02

FL. 15' C.M.

✓ 03' dirt

05.59

9.77

FL. 15' C.M.

05.67 ✓

9.69

FL. 15' C.M.

Sta.	+	π	-	Elev.
		915.36		

149				10.19
-----	--	--	--	-------

+16	+06 v.			
-----	-----------	--	--	--

+50				10.14
-----	--	--	--	-------

+61				
-----	--	--	--	--

+81				
-----	--	--	--	--

+87				
-----	--	--	--	--

150				10.30
-----	--	--	--	-------

+07				
-----	--	--	--	--

~~FR~~

Ditch L

E

Ditch R

517

04' dirt

05.61

9.75

FL. 15" C.M.

✓

522

05.86

9.5

✓

05.96

✓

9.40

FL. 15" C.M.

04' dirt.

✓

9.31

06.05

FL. 15" C.M.

06.26

9.1 - Ground

05.75

✓

9.61

FL. 15" C.M.

506

06.66

8.7 - Ground

P

05.56

✓

9.80

FL. 15" C.M.

Sta.	+	π	-	Elev.
		915.36		

150	+37			
-----	-----	--	--	--

	+57			
--	-----	--	--	--

	+50			
--	-----	--	--	--

				10.37
--	--	--	--	-------

	+85			
--	-----	--	--	--

151	+88			
-----	-----	--	--	--

151	+05			
-----	-----	--	--	--

				10.36
--	--	--	--	-------

	+05			
--	-----	--	--	--

	+08			
--	-----	--	--	--

Ditch L

E

Ditch R

✓ 05.52
9.84
FL. 15" C.M.

✓ 05' dirt
05.57
9.79
FL. 15" C.M.

4.99

05.96

9.4

05.33
1003
FL. 15" C.M.

✓ 05.54
9.82
FL. 15" C.M.

0.9' dirt

500

9.88
FL. 15" C.M.

0.7' dirt

05.48
9.88
FL. 15" C.M.

✓ 05.71
9.65

Sta.	+	π	-	Elev.
		915.36		

151	+50			10.27
-----	-----	--	--	-------

+87

152				10.07
-----	--	--	--	-------

+07

T.P.	5.05	915.12	5.29	910.07
------	------	--------	------	--------

	+50			10.01
--	-----	--	--	-------

+90

153				10.00
-----	--	--	--	-------

+10

Ditch L

E

Ditch R

07.06 ✓

8.9

509

06.46

89 ✓

✓ 05.60

9.76

FL. 15" C.M.

0.3' dirt

05.26

10.10 ✓

FL. 15" C.M.

0.5' dirt

5.29

✓ 05.38

9.98

FL. 15" C.M.

0.8' dirt

0.

10.02

FL. 15" C.M.

0.5' dirt ✓

05.34

05.62 ✓

9.6

511

05.72 ✓

9.4

05.17 ✓

9.95

FL. 15" C.M.

FL. 15" C.M.

✓ 05.24

9.88

FL. 15" C.M.

0.6' dirt

512

0.6' dirt

05.28 ✓

9.84

FL. 15" C.M.

82
512
.9

Sta.	+	π	-	Elev.
------	---	-------	---	-------

915.12

153 +20

+50

10.05

+87

154

10.05

+07

+50

10.07

155

09.96

+20

Ditch L

E

Ditch R

05.40

972

FL 15' CM.

0.9' dirt.

06.72

8.4 ✓

507

05.52

9.6 ✓

05.39

9.73

FL 15' CM.

06.92 ✓

8.2

507

0.5' dirt

05.14

9.98 ✓

FL 15' CM.

06.72 ✓

8.4

505

05.32

9.8 ✓

05.72 ✓

9.4

516

05.10 ✓

10.02

FL 15' CM.

0.5' dirt.

10.16

FL 15' CM.

04.96 ✓

Sta.	+	π	-	Elev.
------	---	-------	---	-------

915.12

135 +50

09.97

+83

156

09.84

+03

+08

+18

+50

09.74

+80

Ditch L

E

Ditch R

05.52

9.6 ✓

515

05.32

9.8 ✓

05.17

9.95 ✓

FL. 15% M.

04' dirt

05.82 ✓

9.3

528

05.19

9.93 ✓

FL. 15% M.

07' dirt

04.90

10.22

FL. 15% M.

0.5 dirt

04.87

10.25 ✓

FL. 15% M.

0.8' dirt

05.12 ✓

10.0

538

05.32

9.8 ✓

04.74 ✓

10.38

FL. 15% M.

07' dirt

Sta.	+	π	-	Elev.
------	---	-------	---	-------

91512

157

09.61

+50

09.51

+66

+86

158

09.51

+09

+29

+40

Ditch L

E

Ditch R

✓ 04.92
10.20
FL. 15'CM.
0.5'dirt

551

05.02

101

05.12 ✓

10.0

561

04.92

10.2

04.77

10.35

FL. 15'CM.

0.4'dirt

10.31

FL. 15'CM.

04.81

05.192 ✓

9.2

561

04.90

10.22

FL. 15'CM.

0.6'dirt

04.73

10.39

FL. 15'CM.

1.0'dirt

04.64

10.48

FL. 15'CM.

0.6'dirt

Sta.	+	π	-	Elev
		915.12		

158 +50

09.45

+60

159

09.28

B.M.

509

914.27

595

909.17

(909.18)

+12

+42

+50

09.23

+82

11-24-47

21

Ditch L

E

Ditch R

567

04.92

10.2

✓

✓ 04.64
10.48
FL. 15' G.M.
0.7' dirt

05.02 ✓
10.1

584

04.72

10.4

✓

Top Moot at "D" & Edgerton

✓ 04.59
9.68
FL. 15' G.M.

0.2' dirt

✓ 04.47
9.80
FL. 15' G.M.

04.77 ✓
9.5

504

04.67

9.6

✓

✓ 04.57
9.70
FL. 15' G.M.

Sta.	+	π	-	Elev.
------	---	-------	---	-------

914.27

160				09.20
-----	--	--	--	-------

+12

+14

+50

09.19

+73

+72

161				09.03
-----	--	--	--	-------

+02

Ditch L

4

Ditch R

ol'dirt

507

04.77

95

✓

✓ 04.50
9.77
FL 15°C.M.

04.86

✓

9.41
FL 18" Vit

04.27 ✓

10.0

508

04.41

9.86

FL 18" Cong.

✓

✓ 04.07
10.20
FL 18°C.M.

178 = 113 02.97

524

02.77

11.5

✓

✓ 04.07
10.20
FL 18°C.M.
0.3'dirt

Sta + N - Elev
91427

161 +40

08.97

B.M.

509 909.13

11-25-46

23

Ditch L

±

Ditch R

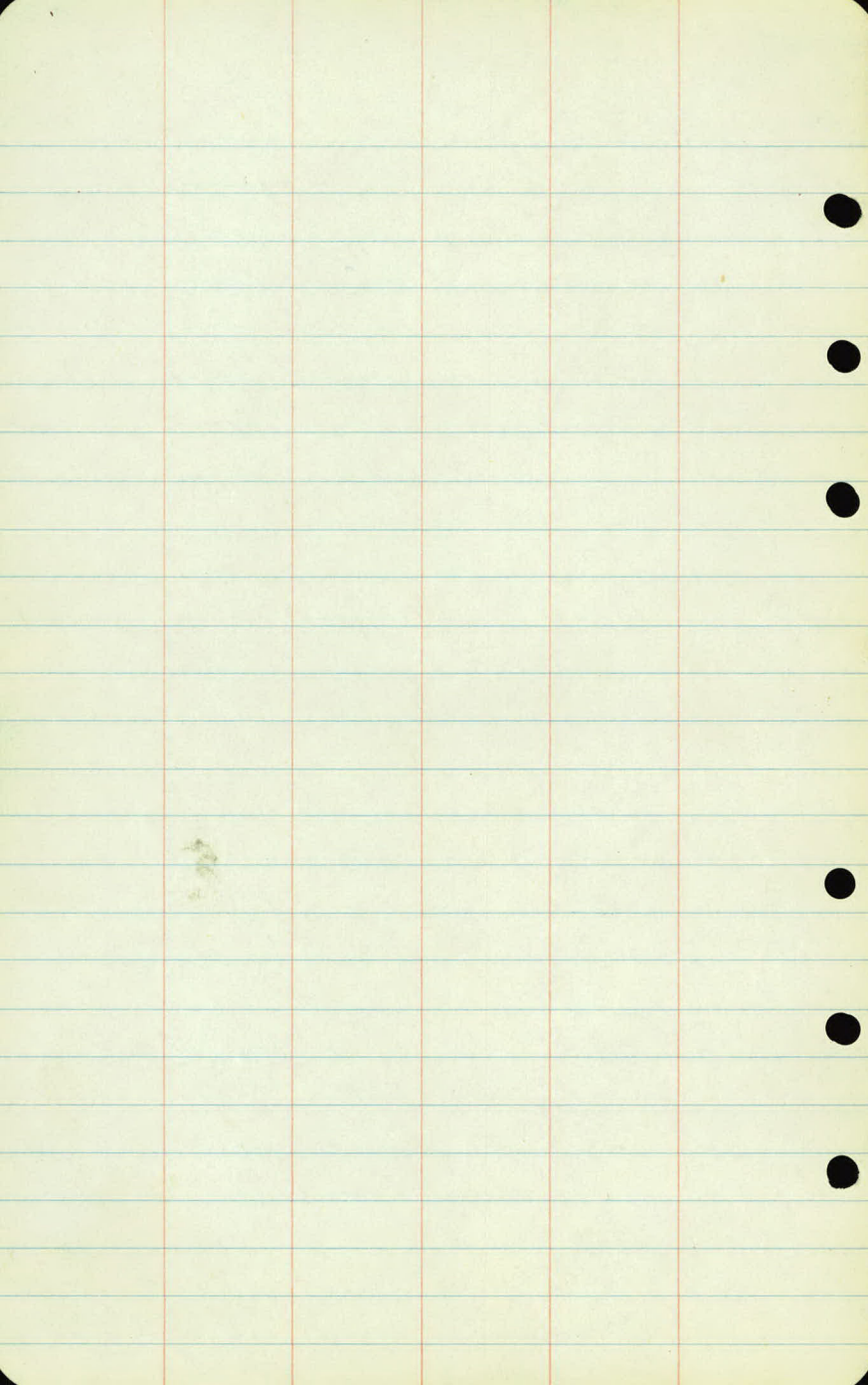
03.67 ✓

10.6

530

02.37

11.9 ✓



EDGERTON ST

X Sections

Co. Ed. D" - North

9- Pages

11-1-46

K.A.

A.M.

M.B.

Rec'd 11/2/46 WB

Sta	+	π	-	Elev
B.M.	4.60	913.78		909.18

160 + 72 @ Ditch from East				09.14
----------------------------	--	--	--	-------

161 + 66 at Manse X Drain + Ditch to East				
--	--	--	--	--

162				08.89
-----	--	--	--	-------

163				08.95
-----	--	--	--	-------

+07	} Ent. - 21" Vlt. CUM. FL.			
+20				

164				09.05
-----	--	--	--	-------

R.A.
A.M.
M.B.

11-1-46

25

Top Mount of Co. Rd. "D"

01.8 ✓
02.4 ✓
01.9 ✓
464 477 52 114 112 109 107 106
10 17 29 100 200 300 400
F.L. H.W. Floor Broken H.W. F.L.
12.9 12.3 11.6 11.7 12.0 50 48 10 49 52 56 11.9 11.7 11.6 108 86
200 100 50 22 16 16 10 C.W. 10 16 16.5 16.5 21 28 35 45
Floor
12.8 13.3 14.2
300 400 500
99.6

03.4 ✓
04.7 ✓
6.9 6.4 104 8.3 56 50 48 9.50 57 7.5 9.1 6.2 6.0 6.9 6.9
50 28 25 23 21 15 10 10 16 19 21 23 28 34 40 50

04.5 ✓
04.9 ✓
6.4 6.5 7.8 9.3 5.9 5.1 5.0 4.8 3.50 5.6 7.8 8.9 6.7 5.7 5.7 6.7 6.5
50 30 27 25 23 16 11 10 10 15 19 20 22 25 28 33 39 50

0.3' dirt

03.98 ✓
9.8
23 ✓

04.03 ✓
9.75
23 ✓

04.9 ✓

05.6 ✓

Yard 5.3 6.1 6.6 8.9 5.8 4.9 4.8 4.73 4.8 5.0 8.2 5.1 5.7 6.4 6.1
46 42 27 24 22 19 15 10 10 13 20 22 29 31 33 39 50

Sta + π - Elev.
913.78

164+04 } Ent. - FL. 21" Vit. Culv.
+16 }

+39 } Road - FL. 18" C.M.
+68 }

+54 } Ent. - FL. 21" Vit. Culv.
+66 }

165 09.33

166 09.48

L

E

R

03.86 ✓

9.92 05' dirt

20

03.98 ✓

9.80 Full dirt

20

04.78 ✓

9.00

23

03' dirt

04.83 ✓

8.95

23

03.95 ✓

9.83 0.7' dirt

21

04.23 ✓

9.55 Full dirt

21

05.1 ✓

05.5 ✓

5.6 5.2 7.6 87 53 47 45 4.45 46 4.9 74 82 83 53 56
 50 30 25 24-22 17 12 10 10 14 20 22 25 30 50

06.0 ✓

05.6 ✓

4.9 5.3 5.8 7.8 4.7 4.3
 50 36 27 23-20 16 10

4.30 4.4 4.7 8.2 4.7 5.5
 10 14 20 24 30 50

Sta.	+	π	-	Elev.
		913.78		

166 +04	}	Ent. - F.L. 18" C.M.
+24		

167				09.59
T.P.	4.74	914.37	4.15	909.63

+90		09.67
-----	--	-------

+95	}	Ent. F.L. 12" C.M.
168 +15		

+07 Hand ditch from East.

168 +07	}	Ent. - F.L. 12" C.M.
+25		

0.4' dirt

8.43

22

05.44 ✓

6.34

22

05.7 ✓

4.9 4.9 3.1 4.5 4.2 4.9 4.3 4.8 7.6 7.6 5.1 4.7 5.5
 50 29 24 21 15 10 10 15 21-25 28 37 50

06.3 ✓

4.9 5.4 8.1 50 4.8 4.7 4.8 5.1 7.5 5.5 5.6
 50 27 24 21 16 10 10 15 21-24 30 50

05.47 ✓

8.9

23.5

0.4' dirt

05.62 ✓

8.75

24.5

06.6

7.3 7.1 7.8 7.5 7.6 7.5
 33 50 100 200 300 400

06.32 ✓

8.05

23

06.30

8.07

23

0.3' dirt

Sta. + π - Elev.

914.37

168+33

09.72

169

09.79

170

09.76

+58 Low spot Lt.

09.82

171

171

09.90

+58 Beg. 3" Iron Irrigation pipe - 47' Rt.

+61

Ent. - FL 110" C.M.

+79

+80 = Δ in Irrigation pipe 37' Rt. Goes due West 450' $\pm$
(Const. ditch to Lh. of +80) to pump Ho.

4.5 5.1 7.5 8.7 7.2 5.3 4.7 4.6 5.4 7.5 3.8 5.8 5.6
 50 33 27 25-23 22 16 10 10 16 21-26 30 50

5.6 5.0 8.1 7.4 5.0 4.7 4.5 8 4.1 5.4 8.0 5.9 5.8
 50 31 26-24 22 17 10 10 14 21-25 29 50

6.7 6.7 7.1 7.6 7.6 5.2 4.6 4.6 4.8 5.1 7.9 5.7 6.3 6.0
 50 35 23 22-21 16 10 10 15 21-25 33-36 40

6.1 6.4 6.9 7.1 7.4 7.0 5.1 4.7 4.55
 150 100 50 32 25 22 15 10

6.0 6.5 6.9 8.2 9.4 Drains West
 200 300 400 500 600 5.5

6.8 7.0 7.3 7.1 4.8 4.5 4.7 4.6 5.2 8.0 7.8 5.6 5.6 6.2 4.1
 50 26 23.5 22 16 10 10 15 22 28 32 35 38 50

Full dirt

8.52
 26

7.43
 25'

0.5' dirt

8.42
 26

7.23
 25'

no dirt

Sta.	+	π	-	Elev
		914.37		

172				10.09
-----	--	--	--	-------

173				10.09
-----	--	--	--	-------

+67
 } ENT-F.L. 10" CM.
 +85

174				10.16
-----	--	--	--	-------

175				10.26
-----	--	--	--	-------

T.P.	5.15	915.41	4.11	910.26
------	------	--------	------	--------

176				10.23
-----	--	--	--	-------

177				10.54
-----	--	--	--	-------

6.4 6.3 6.8 7.8 4.8 4.4 4.2 4.3 5.4 6.5 7.9 5.8 6.0
 50 34 29 27-24 16 10 10 12 17 22-27 30 30

6.8 7.0 6.7 8.4 4.8 4.3 4.2 8.4 5.0 6.6 7.8 4.9 5.9 6.3
 50 34 34 31 28-25 16 10 10 14 19 22-25 27 37 50

0.4' dirt

8.23
 26

7.51 0.2' dirt
 24'

0.2' dirt

8.05
 26

7.35 0.3' dirt
 24'

6.2 6.3 7.7 4.8 4.3 4.2 4.3 4.9 7.1 7.4 6.1 6.2
 50 30 27-24 15 10 10 14 20 27 30 50

0.7.0

0.7.2

5.4 5.6 7.4 4.7 4.2 4.1 4.3 4.9 7.1 7.2 6.0 5.9
 50 30 27-23 16 10 10 16 22 27 30 50

0.7.1

0.6.8

6.7 6.9 8.3 5.9 5.3 5.1 8.5 2.5 9 8.6 6.6 6.8
 50 30 27-24 17 10 10 15 22-26 29 50

0.7.5

0.7.7

6.7 6.6 6.6 7.9 5.4 5.0 4.8 7.5 0.5 7.7 6.4 5.7 6.4
 50 34 29 25-23 17 10 10 16 21-26 28 35 50

Sta. + π - Elev.
91541

177+08

Ent. FL 10" C.M.

+22- ϕ Ent. Lt. No. Culv.

+44

178

10.47

179

10.73

+70

FL
Ent-10" C.M.

+86

+71

FL
Ent-10" C.M.

+89

L

E

R

07.21

8.2
Ditch

07.4

6.5	6.8	7.2	8.0	5.3	5.0	4.9	4.5	1.5	4	8.0	7.3	6.7	6.8
50	36	29	26-22	14	10			10	15	21-24	27	32	50

08.2

6.1	6.7	7.2	7.2	5.8	4.7
50	33	24	21	18	10

4.6	8.4	7.5	2.7	9	6.8	6.6
10	16	22-26	29	50		

07.5

07.51

7.90
23.5
ai'dirt

07.23

8.18
23.5
Full dirt.

07.4

07.59

7.82
25'
ai'dirt

07.79

7.62
25'
ai'dirt

07.91

ai'dirt

7.50
23.5

08.08

ai'dirt

7.33
23.5

Sta.	+	π	-	Elev
		915.41		

180				10.94
-----	--	--	--	-------

181				11.11
-----	--	--	--	-------

182				11.62
-----	--	--	--	-------

+50				11.87
-----	--	--	--	-------

+66	} Ent. FL. 12" CAT.			
+86				

+94	High pt. on E = 324	12.17
-----	---------------------	-------

183	Ent. lt. no culv.	12.14
-----	-------------------	-------

L

E

R

6.0 5.8 6.9 5.7 4.7 4.5 4.4 7.9 5.9 5.6 7.5 6.5 6.4
 50 29 25-20 17 15 10 10 14 18 21-25 29 ~~50~~ 50

5.9 5.7 6.6 6.6 4.9 4.4 4.3 4.3 4.3 4.3 4.5 5.1 7.3 6.2 6.5
 50 29 26 21 17 13 10 10 13 16 21 25 27 50

4.1 4.4 5.1 5.4 3.9 3.6 3.8 3.7 9.4 0.4 0.6 6.1 6.1 5.7 5.7 6.2
 50 34 25 19 15 12 10 10 14 21 23 25 30 50

6.0 6.5 6.2
 200 150 100
 Low spot

2.2 3.8 3.0 3.6 2.3 5.4 3.6 3.5 5.2 5.6 5.2 5.8
 50 22 17 10 10 15 19 24 27 50

buried 5.54
 21'

buried 5.32
 21'

23 31 33 327
 53 28 10

34 3.5 5.1 4.9 4.6
 10 13 19 22 27 50

Sta.	+	x	-	Elev.
		915.41		

183	+25		3.35	12.06
-----	-----	--	------	-------

	+50		3.65	11.76
--	-----	--	------	-------

	+75		4.15	11.26
--	-----	--	------	-------

184			4.82	10.59
-----	--	--	------	-------

	+25		5.62	09.79
--	-----	--	------	-------

	+50		6.60	08.81
--	-----	--	------	-------

185			9.10	06.31
-----	--	--	------	-------

T.P.	1.18	904.44	12.15	903.26
------	------	--------	-------	--------

B.M.	7.43	895.95	15.92	888.52
------	------	--------	-------	--------

T.P.	13.63	906.32	3.26	892.69
------	-------	--------	------	--------

T.P.	12.04	918.23	0.13	906.19
------	-------	--------	------	--------

(888.48)

L

E

R

B.M. - 89738 = New B.M. on sec. cor. Iron at Mississippi + Edgerton

This B.M. no good as it settles

Top + E.N. End of N. ctr. Pier at Underpass

H.I. = 918.23

10.18

928.21

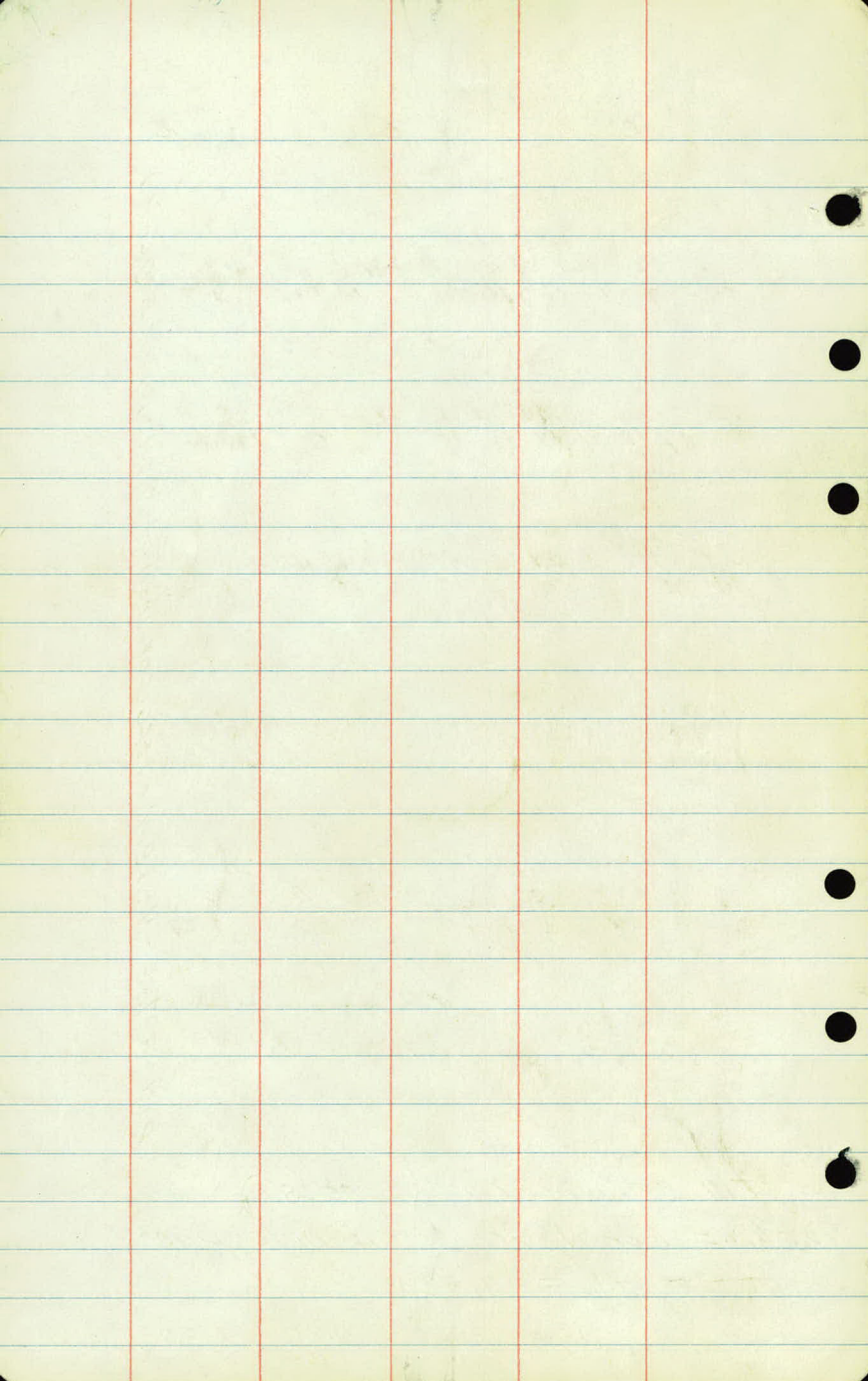
0.20

918.03

0.65

927.56

(927.49)



Ditch Profile

Edgerton St

Co. Rd "D" South

Raise all elevations 0.23

HAW

AM

LC

M.B

5-28-51

Rec'd. 20.
5-29-51

Sta	+	Δ	-	Elev
B.M	5.27	914.22		908.95

160+71 No End 18" Conc Under "D"

24 months

+15 So End 18" V.t

160

+50

159

+50

1 tra 15" No End Culv

+09

L

R +

Top Mon & Co Rd'D

03.97
10.25

04.68
954

04.6
96

04.5
97

04.6
96

04.7
95

04.54
968

04.72
950

Sta + Δ - Elev
91422

158

+85 15" X 20' CM No

+65

+50

157

+50

+29

15"

+09

\$Ditch

04.7

9.5

04.49

9.73

04.55

9.67

04.7

9.5

04.8

9.4

04.9

9.3

04.64

9.58

04.66

9.56

Sta + π - Elev
914.22
914.21

156+04 15"X20 CM No End

+84 15"X20 CM

+50

156+20 15"X20 CM No End

155 15" 50 E

+50

+07 15"X

153+87

£
Ditch
04.92
930

04.92
930

05.1
91

04.70
9.52

04.92
930

05.4
86
Ground

05.1
91

04.94
928

05.13
909

Sta + ~~914.22~~ - Elev
 914.21

153+58

153+09

15" x 20' CM No End

152+89

15" x 20' CM So End ~~909.64~~

TP

5.36

~~915.00~~
914.99

4.58

909.43

+50

+07

15" x 20' CM No End

151+87

15" x 20' CM So End

+50

+07

15" x 20' CM No End

+

£ Ditch

05.2

90

✓

05.05

917

Inv

✓

04.97

925

Inv

✓

05.4

96

✓

05.17

983

Inv

✓

05.04

996

Inv

✓

05.5

95

✓

05.26

974

✓

Sta + Δ - Elev
915.00
914.99

150+87 15" X 20' CM So End

+50

+07 15" X 20' CM No End

149+87 15" CM So End

+50

+07 15" X 20' CM No End

148+87 15" X CM So End

+50

2
Ditch

05.17

983 ✓

05.6

94 ✓

05.4

960 ✓

05.59

941 ✓

05.7

93 ✓

05.42

958 ✓

05.50

950 ✓

05.2

98 ✓

Sta + Δ - Elev
913.00
914.79

148+18 15" X 20' CM No

147+98

+50

+08 15" X 20' CM No End

146+88

+50

+07 15" X 40' CM No End Head
Double Drive

145+67 15" X 40' 50 End

2
Ditch
05.25 ✓
9.75

05.44
956 ✓

06.1
8.9 ✓

06.32 ✓
868

06.67 ✓
833

06.7 ✓
83

06.93 ✓

Conc Headwall

807

07.15 ✓
7.85

Sta + Δ - Elev
 915.00
 914.99

145+50

145

T.P

557

915.67

915.66

490

910.10

910.09

+50

44+06

15" x 20' CM No End

43+86

15"

143+50

+18

15" x 20' CM No End

42+98

15" x

So End

£

Ditch

07.5 ✓
75

07.4 ✓
76

Nail Pole # 2930

07.5 ✓
82

07.70
797

07.49 ✓
818

07.6 ✓
81

07.84 ✓
783

07.74
793

Sta

+

915.67
915.65

142+86

15" x 20' CM. No End

+66

15"

50 End

+50

142

+50

+32

15" x 20' CM

15" x 20' CM No End

+12

50 End

141

2

Ditch

07.74

793

07.6

809? 809

07.9

78

07.1

80

07.7

80

07.50

817

692
123
111

07.46

821

07.4

83

Sta + Δ - Elev
915.67
915.66

140+50

+08

15" X 20' CM No

139+88

S. End

+50

139+08

15" X 20' CM No End

138+88

S. End

+50

+09

15" X 20 CM

✱

Ditch

07.4

8.3

07.46

8.21

07.57

8.10

07.5

8.2

07.47

8.20

07.47

8.20

07.5

8.2

07.12

8.55

Sta + Δ - Elev

915.67
915.66

137+89

So End

+50

915.80

00 910.67

T.P

5.13

915.79

5.00

910.66

+15

15" x 20' CM No End

136+95

So End

+82

15" x 20' CM No End

+62

So End

+50

136

2

Ditch

07.24

843

07.3

84

07.41

840

07.48

832

07.15

865

07.15

865

07.2

86

07.5

83

Sta + Δ - Elev

915.80
915.77

135+60

+05

15" x 20' CM No End

134+85

+50

+06

12" x 20' Conc No End

133+86

So End

+82

15" x 20' CM No End

+62

So End

2

Ditch

07.1

87

07.20

860

07.25

855

07.2

86

07.35

845

07.24

856

07.12

868

06.92

888

Sta + Δ - Elev

~~915.80~~
915.79

+50

133

+84

15" x 20' CM No End

+64

50 End

+50

132

+79

15" x 20' CM

+59

5

2

Ditch

07.3

85

07.0

88

06.88

892

06.64

795

916

07.1

87

07.0

88

06.77

903

06.72

908

Sta	+	Σ	-	Elev
-----	---	----------	---	------

915.80
915.79

131 + 52

131

B.M

664

909.16

909.15

909.40

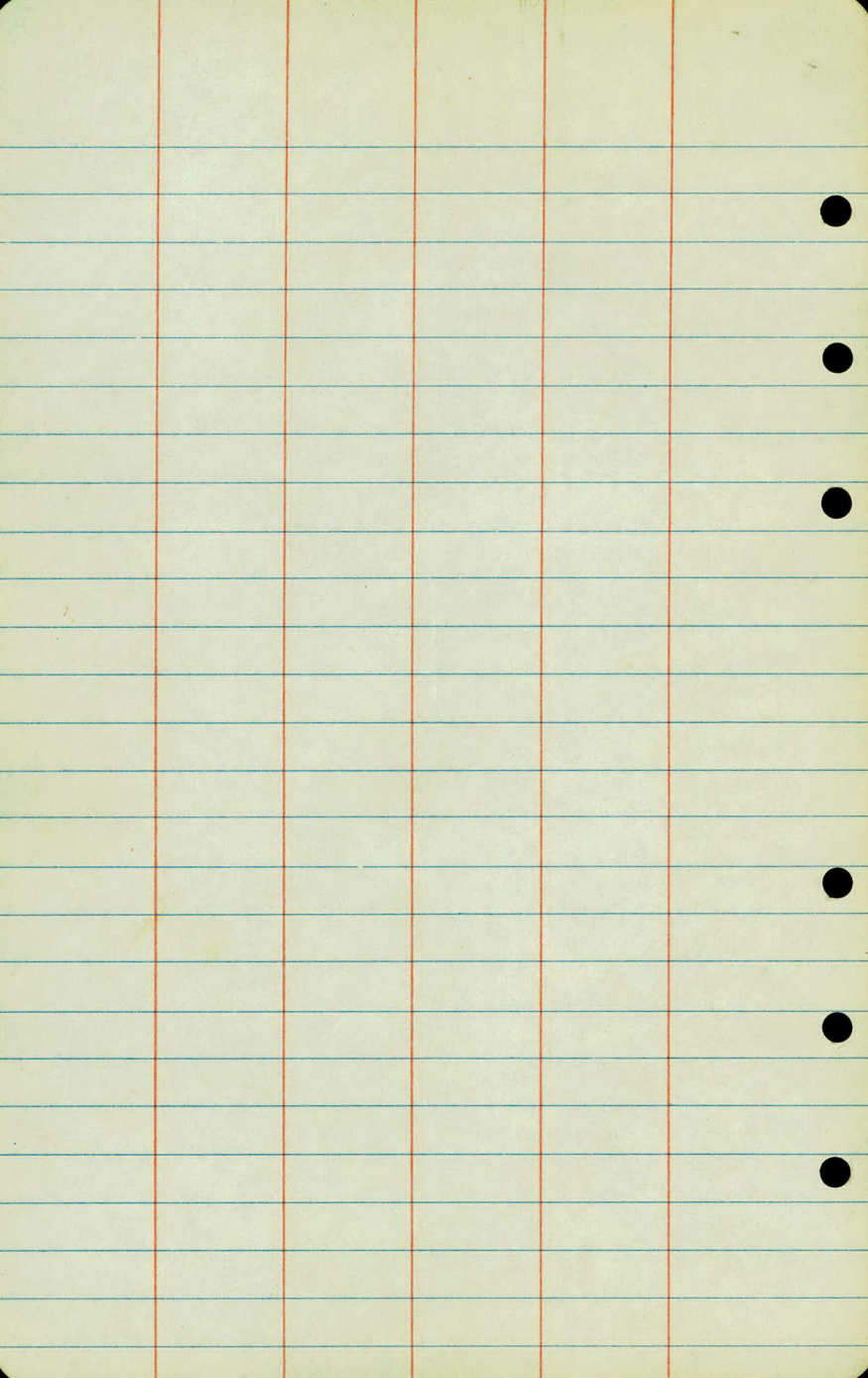
~~2~~
Ditch
06.9

8.9

06.6
9.2

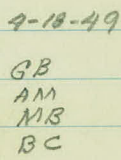
TOP Sta 131+62.4

+ .22 Higher Equation to B.M.
Elev in BM Book



1

● ● ●



Sta	+	∇	-	Elev.
-----	---	---	---	-------

B.M.	4.69	913.87		909.18
------	------	--------	--	--------

1			11.5	02.4
---	--	--	------	------

2			9.56	04.31
---	--	--	------	-------

3			11.6	02.3
---	--	--	------	------

4				
0+00			8.97	04.9

+10			9.2	04.7
-----	--	--	-----	------

+20			9.1	04.8
-----	--	--	-----	------

+30			9.1	04.8
-----	--	--	-----	------

+40			9.2	04.7
-----	--	--	-----	------

+50			9.2	04.7
-----	--	--	-----	------

+60			9.3	04.6
-----	--	--	-----	------

+70			9.1	04.8
-----	--	--	-----	------

+80			9.2	04.7
-----	--	--	-----	------

+90			9.0	04.9
-----	--	--	-----	------

1 + 00			8.9	05.0
--------	--	--	-----	------

+10			8.9	05.0
-----	--	--	-----	------

+20			9.1	04.8
-----	--	--	-----	------

+30			9.1	04.8
-----	--	--	-----	------

+40			9.2	04.7
-----	--	--	-----	------

+50			9.2	04.7
-----	--	--	-----	------

+60			9.0	04.9
-----	--	--	-----	------

+70			8.7	05.2
-----	--	--	-----	------

+80			8.3	05.6
-----	--	--	-----	------

Top Mont Edgerton & Co. Rd "D"

Ditch @ Nend culvert under Co. Rd. D.

N inv. 18" conc. under. Co. Rd D.

Ditch @ X Culvert 100' N int. Edgerton & D.

14v. 18" YCP Under Co. Rd D.

Ditch Profile

10		10
11		11
12		12
13		13
14		14
15		15
16		16
17		17
18		18
19		19
20		20
21		21
22		22
23		23
24		24
25		25
26		26
27		27
28		28
29		29
30		30
31		31
32		32
33		33
34		34
35		35
36		36
37		37
38		38
39		39
40		40
41		41
42		42
43		43
44		44
45		45
46		46
47		47
48		48
49		49
50		50
51		51
52		52
53		53
54		54
55		55
56		56
57		57
58		58
59		59
60		60
61		61
62		62
63		63
64		64
65		65
66		66
67		67
68		68
69		69
70		70
71		71
72		72
73		73
74		74
75		75
76		76
77		77
78		78
79		79
80		80
81		81
82		82
83		83
84		84
85		85
86		86
87		87
88		88
89		89
90		90
91		91
92		92
93		93
94		94
95		95
96		96
97		97
98		98
99		99
100		100

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		913.87		
--	--	--------	--	--

+ 85				
------	--	--	--	--

			7.18	04.69.
--	--	--	------	--------

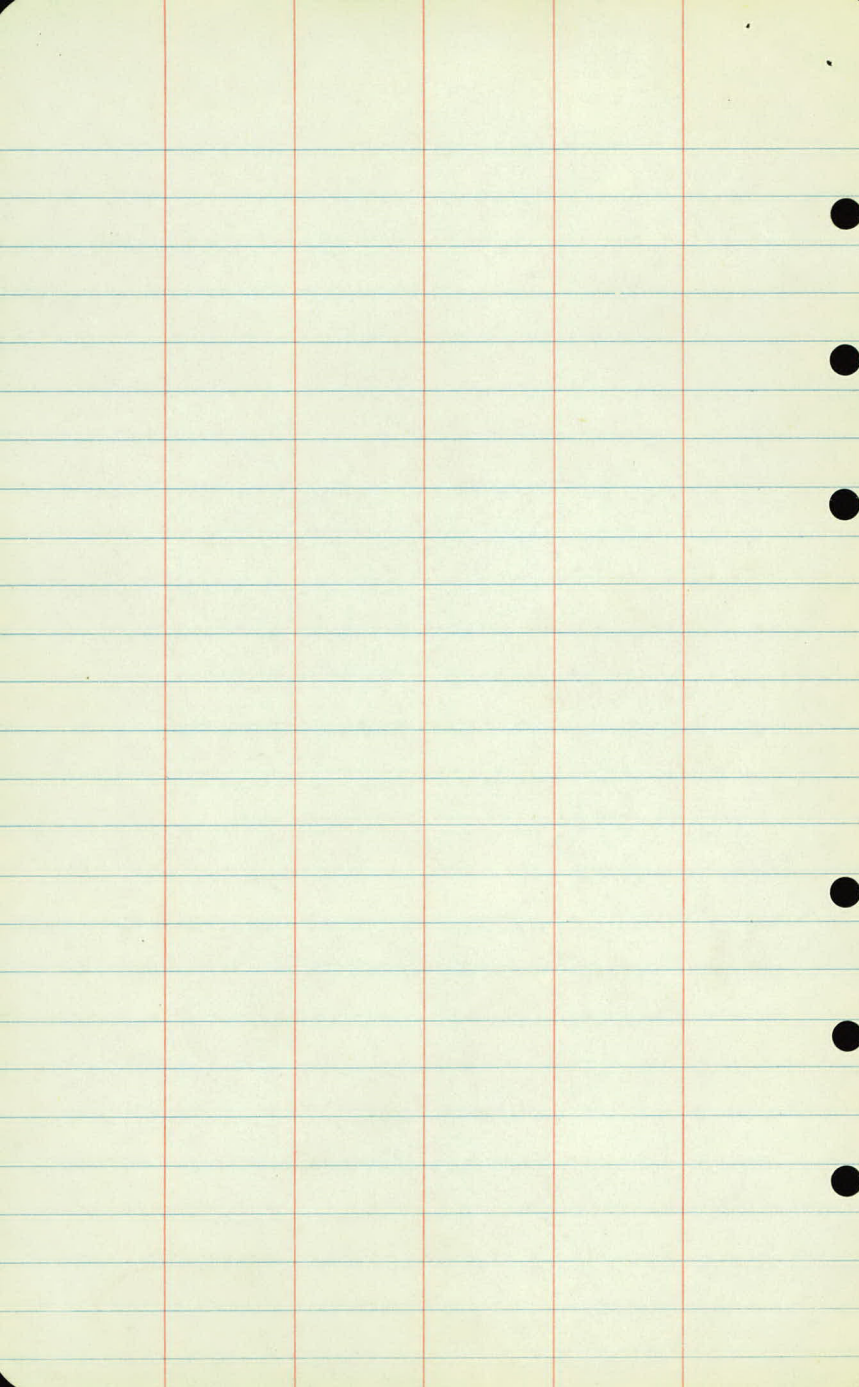
2 + 06				
--------	--	--	--	--

			8.92	04.95.
--	--	--	------	--------

BM				
----	--	--	--	--

				909.18
			4.69	908.18

N inv. 15 "cm ent. culv.
S inv. " " " "



Additional

East Ditch Profile

Edgerton St. S. of Co. Rd. D

Sta	+	π	-	Elev
BM	4.23	913.91		909.18
2 + 06			8.52	04.89
+ 19			8.4	05.0
+ 29			8.70	04.71
+ 49			8.65	04.76
+ 75			8.4	05.0
3 + 00			8.4	05.0
+ 25			8.3	05.1
+ 50			8.2	05.2
+ 75			8.2	05.2
+ 87			8.50	04.91
4 + 07			8.51	04.90
+ 12			8.35	05.06
+ 32			8.30	05.11
+ 50			8.2	05.2
+ 75			8.1	05.3
+ 94			7.8	05.6
+ 96			8.46	04.95
5 + 16			8.30	05.11
+ 35			8.1	05.3
+ 50			8.3	05.1
+ 75			8.1	05.3
6 + 00			8.3	05.1

4-19-49 5
AM - Warm - Clear
GB MB
AM BC

Top Mont "D" & Edgerton.

Send 15" cm
ditch
Nend 15" cm } invert. Elev.
Send 15" cm
ditch
"
"

inv. Nend 15" cm }
" Send 15" cm }
" Nend 15" cm }
Send 15" cm }
ditch
"
"

inv 15" cm Nend }
inv 15" cm Send }
ditch
"
"
"

Sta	+	Δ	-	Elev
		913.41		
6 + 09			8.28	05.13
+ 29			8.05	05.36
+ 50			7.95	05.46
+ 75			8.0	05.4
7 + 00			7.8	05.6
+ 08			8.12	05.29
+ 28			8.19	05.22
+ 50			7.9	05.5
+ 75			7.7	05.7
8 + 00			7.8	05.6
+ 09			8.08	05.33
+ 29			8.12	05.29
+ 50			7.8	05.6
+ 75			7.8	05.6
9 + 00			7.7	05.7
+ 09			7.85	05.56
+ 29			8.08	05.33
+ 33			7.3	06.1
+ 50			7.8	05.6
+ 75			7.4	05.8
10 + 00			7.4	06.0
+ 10			7.80	05.61
+ 30			7.66	05.75
B.M			4.22	909.18 908.19

FL N end 15" cm.

FL S " 15" cm

ditch

"

"

FL 15" cm N end

" " " S end.

ditch

"

"

FL 15" cm N end

FL 15" cm S end.

ditch

"

"

FL 15" cm N end

FL " " S end

ditch

"

"

"

FL 15" cm N end (plugged).

FL " " S end.

Note. Ditch and culverts N end cleaned.
But are not plugged.

Top Mont. Edgerton & "D"

Sta + π - Elev.

Edgerton + A2

Topog for
signals

Worked up ^{4/11/54}
HAW

£

$$1+26 \frac{PP}{19.9}$$

$$1+19 \frac{PP}{28.8}$$

$$0+50.5 \frac{PP}{28.2}$$

Note: Blacktop Fill From
Beg. & End of Road to Steps

$$+11 \frac{Beg. Rad.}{45} +17 \frac{End. Rad.}{10}$$

$$0+29 \frac{PP}{127}$$

0+00

$$-19 \frac{Pl. On Rad.}{20} -12 \frac{Beg. Rad.}{34} -32 \frac{End Rad.}{10}$$

$$+11 \frac{Beg. Rad.}{40} +34 \frac{End Rad.}{10}$$

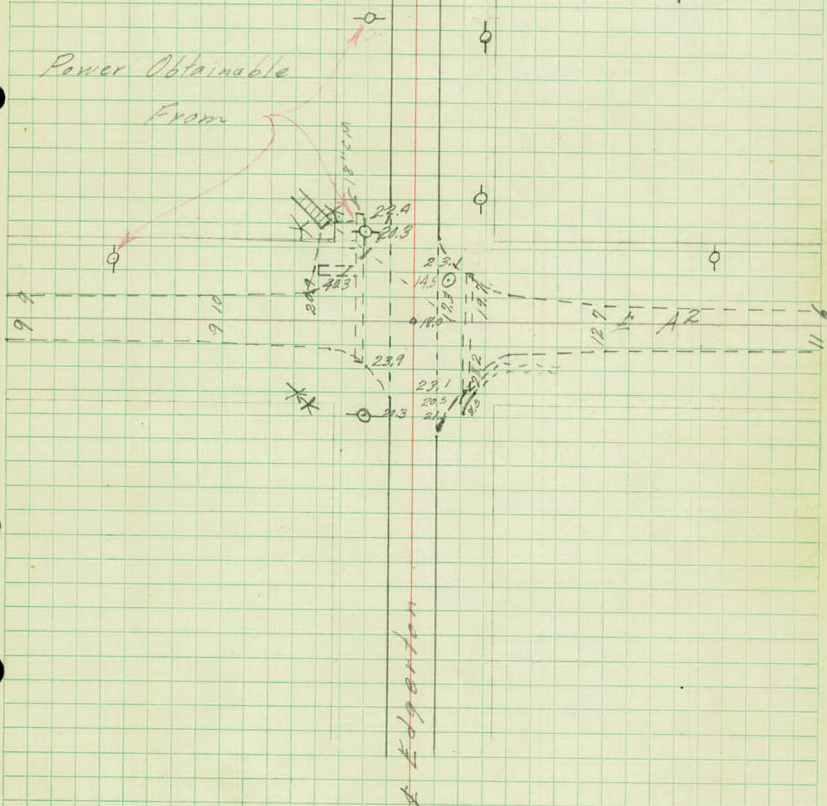
$$-13 \frac{Beg. Rad.}{40} -48 \frac{End Rad.}{10}$$

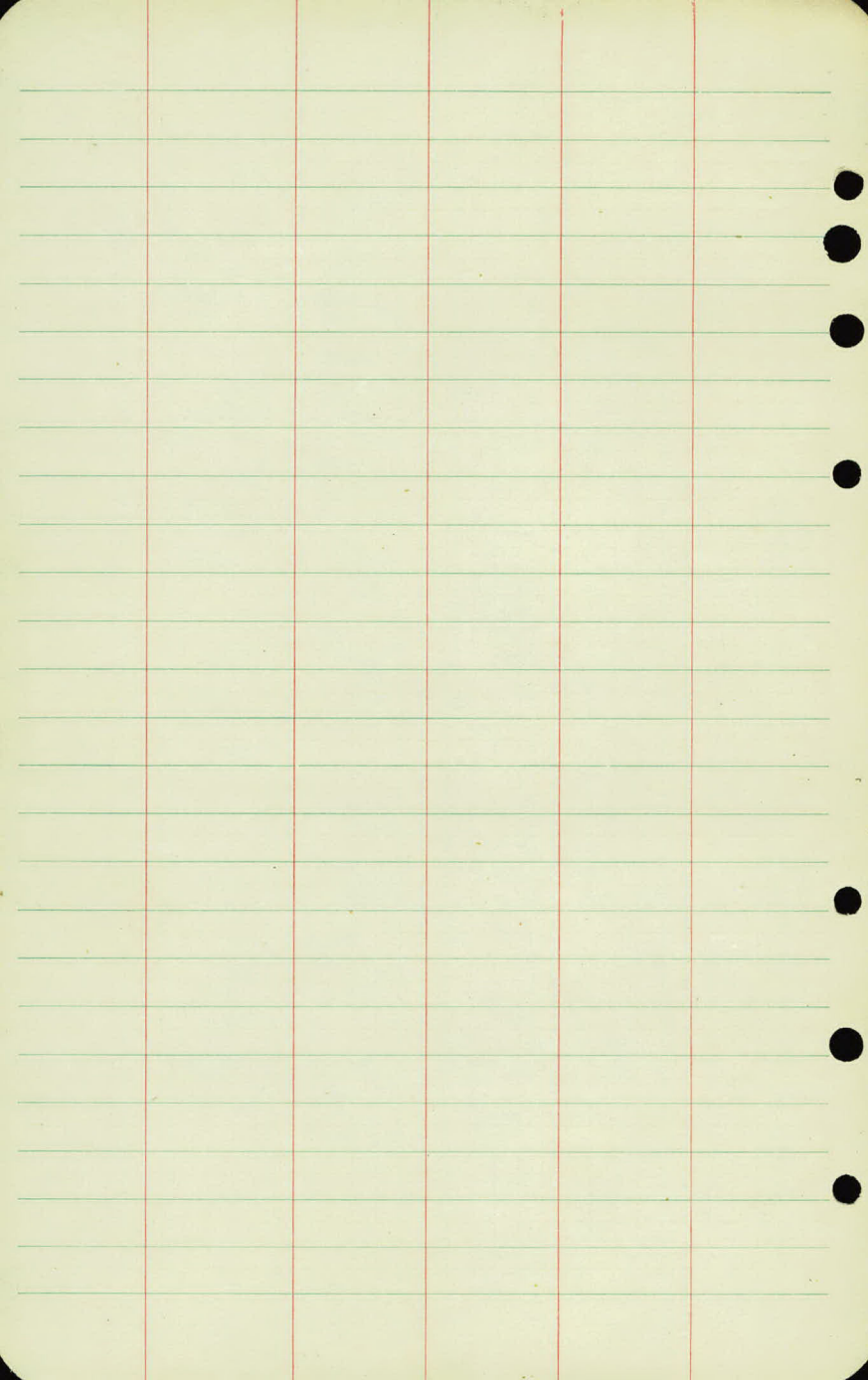
Edgerton & AR

Topog for Signals



Power Obtainable
From





Larpenleur & Hamline
topog for
signals

$$+48 \frac{\text{End Rad}}{14}$$

$$+12 \frac{\text{Beg Rad}}{51}$$

0+00

$$-31 \frac{\text{Sign}}{30}$$

$$-40 \frac{\text{Mail Box}}{25}$$

$$-29 \frac{\text{Edge of Bl Top}}{105}$$

$$-29 \frac{\text{Pl. On Rad}}{34}$$

$$-81 \frac{\text{Beg. Vert. 6'}}{27'}$$

$$-54 \frac{\text{Beg. Rad}}{18}$$

17

F.L. 3.1 Below 2

24
102

183' x Drain
18" S.C.P.

26 Larpentour Ave

185 - 105 Ent

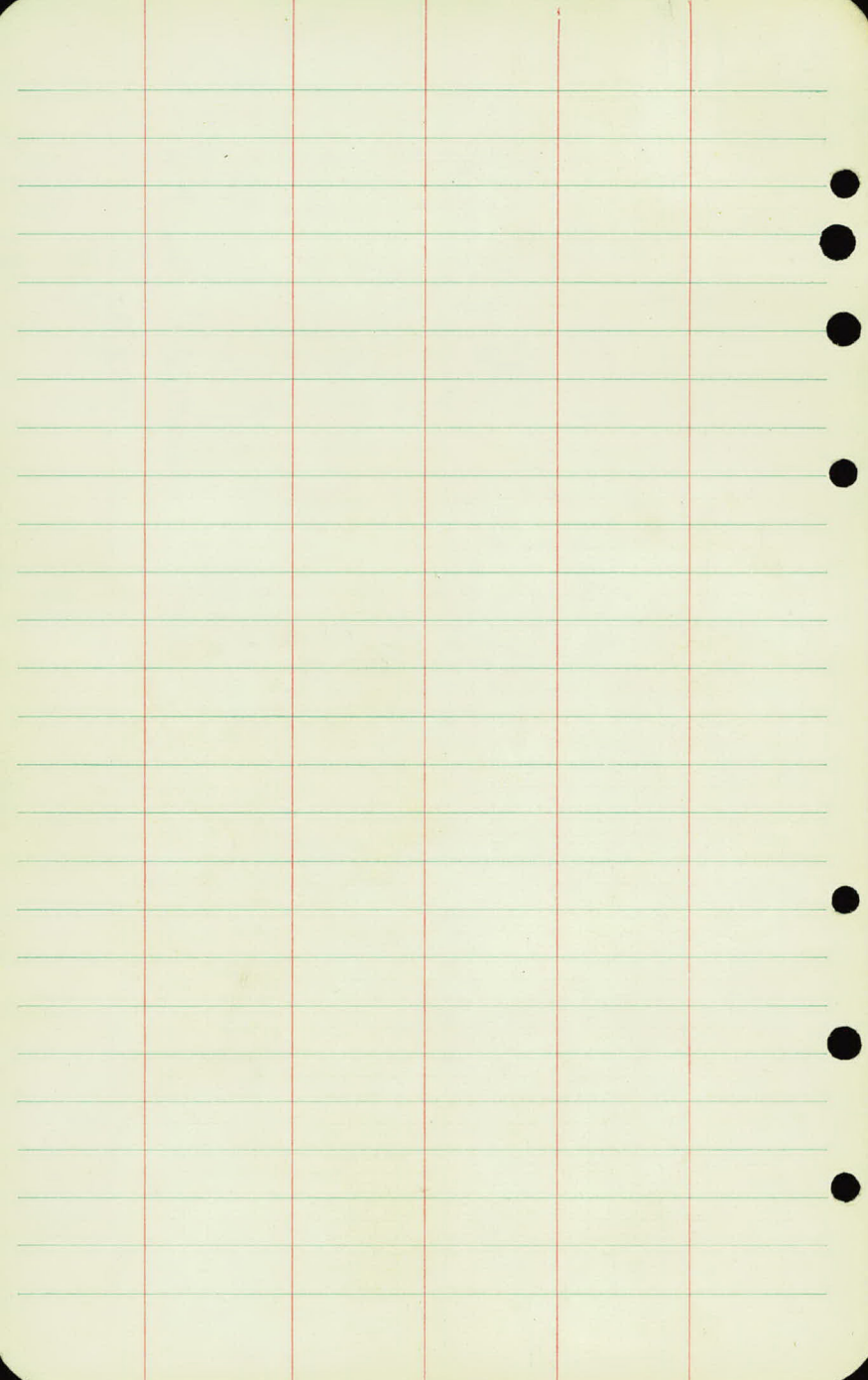
FL 2.6 Below &
Top Exposed
Beyond 13' from &

194-43 Ent.

Harvie Ave

Alley

14 17



FK
AM
LC
MMo

Jan 26, 1954
Cold 10°

2

x-sections

Sta + x - Elev

0+100 E of Edgerton + AR

0+50 On AR

0+45 ON-EDGERTON

£

3

15.35 14.7 14.3 15.5 15.5

14 29 30 33

1.0 5.2 9.1 10.8 13.2

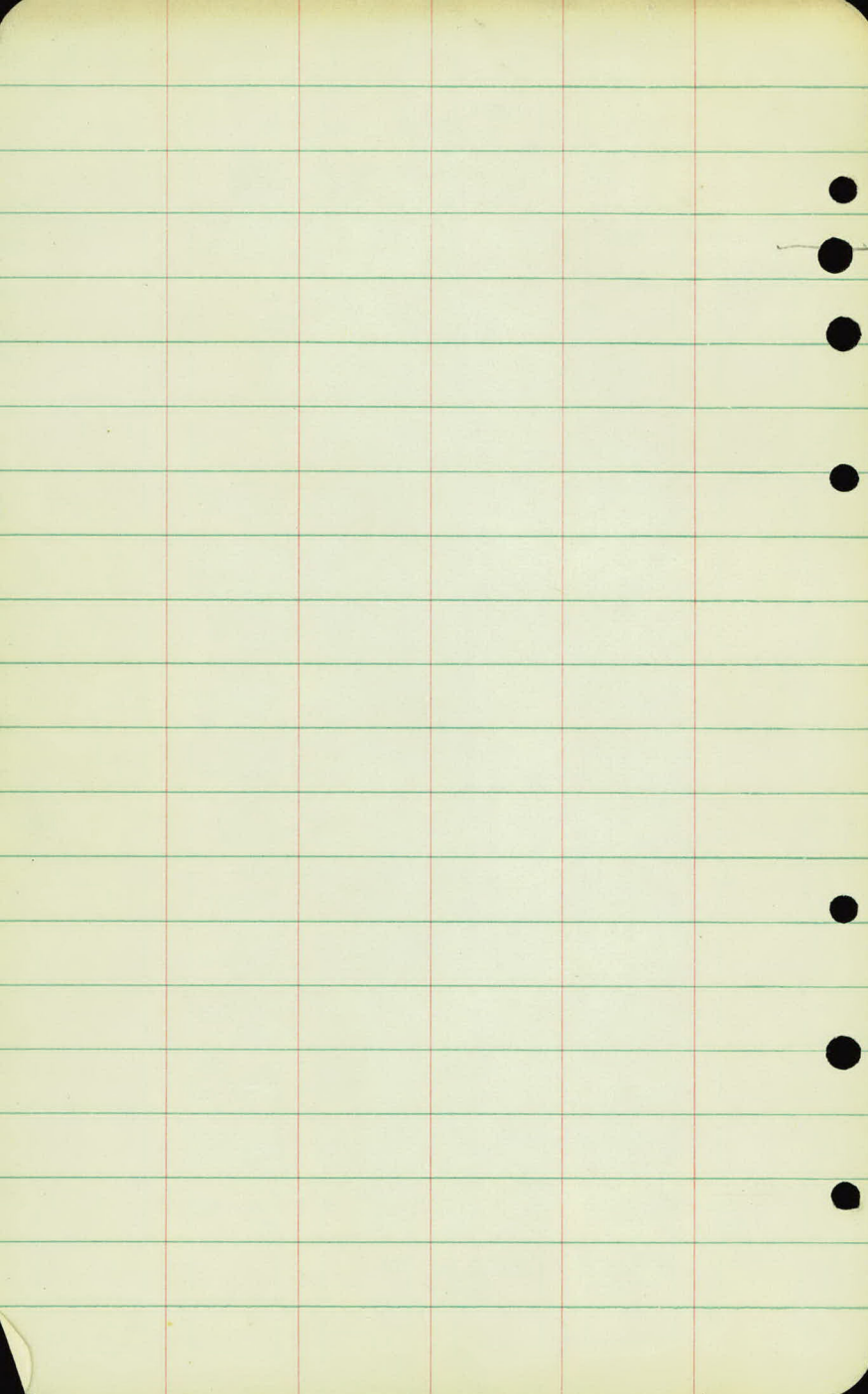
67 61.52 12 35

1.2 4.8 10.0 14.4 14.1 13.6

41 36 25 17 9

13.2 13.1 13.3 14.7 11.7 9.5 5.0 1.2

10 18 19-20 25 32 41 50



Edgerton

Ditch Stakes
Co-RD-D-NORTH

Sta	+	π	-	Elev
B.M	499	914.17		909.18

162 + 0.0

+5.0

162

163

+5.0

+5.0

164

164

+5.0

+5.0

165

+5.0

Ele	Gr	LT	Ele	Gr	RT
					Rod

Top Mon Edgerton YD 150 + 1.2

03.3	10.87	BT 887/c20	035	10.67	BT 767/c30
------	-------	------------	-----	-------	------------

03.6	10.57	BT 857/c20	036	10.57	BT 757/c30
------	-------	------------	-----	-------	------------

03.9	10.27	BT 827/c20	03.7	10.47	BT 747/c30
------	-------	------------	------	-------	------------

04.2	9.97	BT 797/c20	038	10.37	BT 737/c30
------	------	------------	-----	-------	------------

04.5	9.67	BT 767/c20	039	10.27	BT 727/c30
------	------	------------	-----	-------	------------

			04.0	10.17	BT 717/c30
--	--	--	------	-------	------------

04.88	9.77	BT 717/c20	04.5	9.67	BT 667/c30
-------	------	------------	------	------	------------

04.95	9.27	BT 717/c20	04.8	9.37	BT 637/c30
-------	------	------------	------	------	------------

5th

+

X

-

914.17

166

+50

167

TP 7.48 914 63 7.02 907.15

+50

168

+50

169

+50

Elev	Rod	Lt.	Elev	Gr. Rd	Rt
------	-----	-----	------	--------	----

05.3	887	B.T. 687 C.20	049	927	B.T. 687 C.30
------	-----	------------------	-----	-----	------------------

05.1	9.07	B.T. 707 C.20	05.0	9.17	B.T. 617 C.30
------	------	------------------	------	------	------------------

05.18	899	699 C.20	05.1	907	
-------	-----	-------------	------	-----	--

Top stake sta 167 Lt.

05.25	9.38	B.T. 738 C.20	05.2	9.43	B.T. 643 C.30
-------	------	------------------	------	------	------------------

05.33	9.30	B.T. 730 C.20	05.3	9.33	B.T. 633 C.30
-------	------	------------------	------	------	------------------

05.40	9.23	B.T. 723 C.20	05.4	9.23	B.T. 623 C.30
-------	------	------------------	------	------	------------------

05.48	9.15	B.T. 715 C.20	05.5	9.13	B.T. 613 C.30
-------	------	------------------	------	------	------------------

05.55	9.08	B.T. 708 C.20	05.6	9.03	B.T. 603 C.30
-------	------	------------------	------	------	------------------

5/9 + π - Elev

914.63

170

+50

171

+50

172

+50

173

+50

+

T. P

5.17

915.19

4.61

9 10.02

Elev	G. Rod	Lt	Elev	G. Rod	Lt
05.63	9.0	$\frac{B.T. 7.0}{C.20}$	05.7	8.93	$\frac{B.T. 5.93}{C.30}$
05.70	8.93	$\frac{B.T. 6.93}{C.20}$	05.8	8.83	$\frac{B.T. 5.83}{C.30}$
05.78	8.85	$\frac{B.T. 6.85}{C.20}$	05.9	8.75	$\frac{B.T. 5.75}{C.30}$
05.85	8.78	$\frac{B.T. 6.78}{C.20}$	06.0	8.63	$\frac{B.T. 5.63}{C.30}$
05.97	8.66	$\frac{B.T. 6.66}{C.20}$	06.1	8.53	$\frac{B.T. 5.53}{C.30}$
06.02	8.61	$\frac{B.T. 6.61}{C.20}$	06.2	8.43	$\frac{B.T. 5.43}{C.30}$
06.07	8.56	$\frac{B.T. 6.56}{C.20}$	06.3	8.33	$\frac{B.T. 6.33}{C.20}$
06.12	8.51	$\frac{B.T. 6.51}{C.20}$	06.4	8.23	$\frac{B.T. 6.23}{C.20}$

Sta + π - Elev

915.19

174

+50

175

+50

176

+50

177

+50

179 +71

Elev Gr Rod Lt

Elev Gr Rod Lt

063L

8.83

 $\frac{B.T. 6.83}{c.20}$

06.5

8.69

 $\frac{B.T. 6.69}{c.20}$

0649

8.70

 $\frac{B.T. 6.70}{c.20}$

06.6

8.59

 $\frac{B.T. 6.59}{c.20}$

0663

8.56

 $\frac{B.T. 6.56}{c.20}$

06.7

8.49

 $\frac{B.T. 6.49}{c.20}$

0676

8.43

 $\frac{B.T. 6.43}{c.20}$

06.8

8.39

 $\frac{B.T. 6.39}{c.20}$

06.9

8.29

 $\frac{B.T. 6.29}{c.20}$

06.9

8.29

 $\frac{B.T. 6.29}{c.20}$

07.03

8.16

 $\frac{B.T. 7.16}{c.10}$

07.0

8.19

 $\frac{B.T. 6.19}{c.20}$

07.17

8.02

 $\frac{B.T. 7.02}{c.10}$

07.1

8.09

 $\frac{B.T. 7.09}{c.10}$

07.30

7.89

 $\frac{B.T. 6.89}{c.10}$

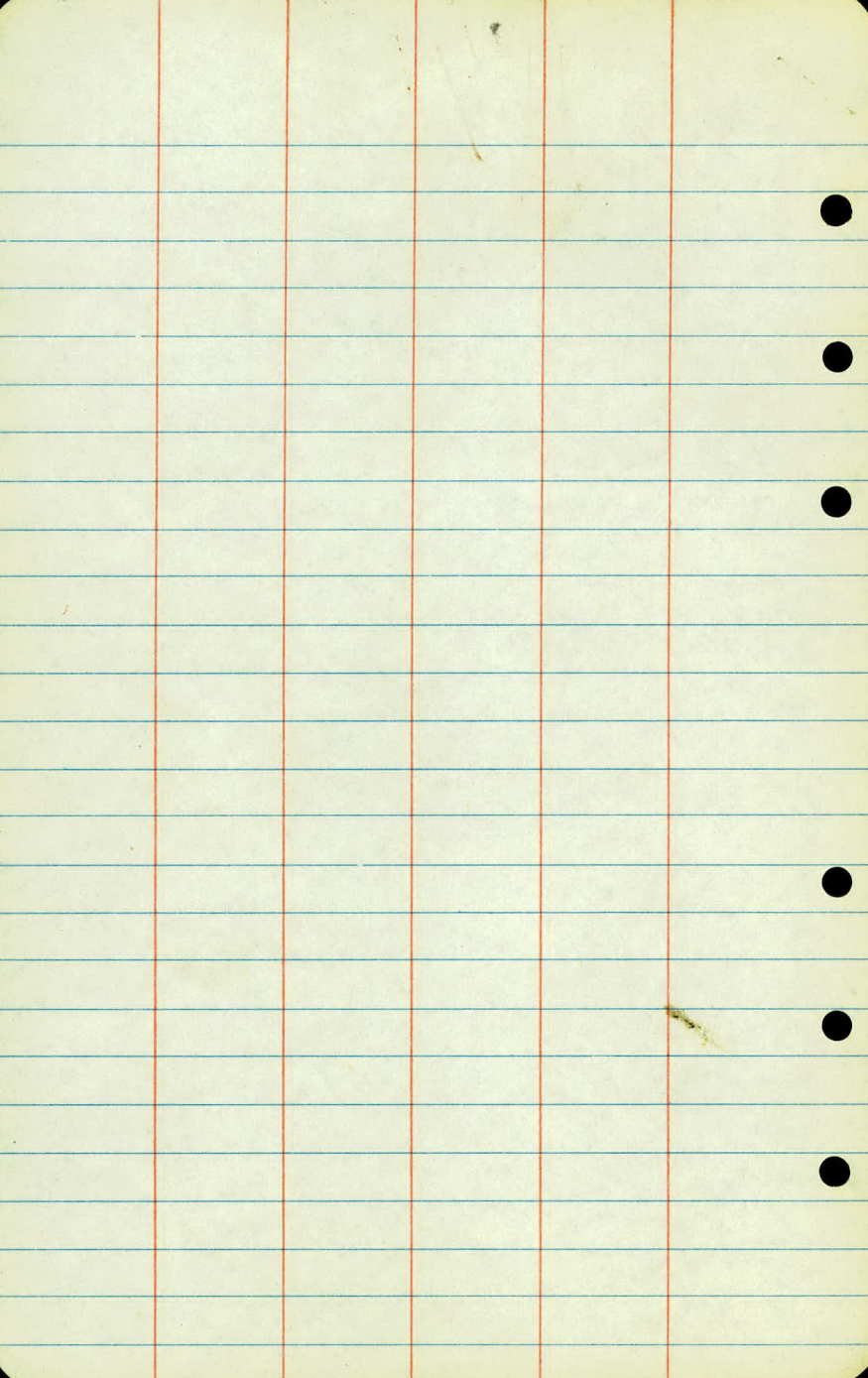
07.2

7.99

 $\frac{B.T. 6.99}{c.10}$

07.91

7.28



Edgerton St.
Ditch Levels
Bt. sta. 157+66 to
160+14.6

Sta.	+	π	-	Elev.
B.M.	334	912.52		909.18

Elev. Nex Bas. floor 8.97 04.15

W.S. in basement. = 0.9' deep

		Gr. = 7.35	05.17	.
157 + 66		In. = 7.68	04.84	.

15" X 20" C.M.

+86		Gr. = 7.15	05.37	.
		In. = 7.75	04.77	.

158		7.5	05.0	.
-----	--	-----	------	---

+10		Gr. = 7.1	05.42	.
		In. = 7.55	04.97	.

15" X 20" C.M.

+30		Gr. = 7.0	05.52	.
		In. = 7.81	04.71	.

+40		7.25	05.27	.
-----	--	------	-------	---

+50		7.7	04.8	.
-----	--	-----	------	---

Top Mont. @ "D" Edgerly St

$$\begin{array}{r} 6.53 \\ 1.63 \\ \hline 4.90 \\ 3.47 \\ \hline 8.37 \end{array}$$

sto.	+	π	-	E/ev.
		912.52		

158 +60

7.6 04.9

+70

7.7 04.8

+80

7.8 04.7

+90

7.8 04.7

159

7.5 05.0

+10

7.4 05.1

+20

7.5 05.0

+30

7.7 04.8

+40

7.75 04.77

Pipe line King $\pm$

Sta.

+

π

912.52

159 +50

7.65 04.87

+60

7.7 04.8

+70

7.85 04.67

+80

7.80 04.72

+90

7.75 04.77

W.S.

7.43 05.09

160

7.70 04.82

+10

7.5 05.0

+19.6 F.L. 18" V.F.

7.63 04.89

X Drain under Co. Rd. "D"

+72.5 F.L. 18" Conc.

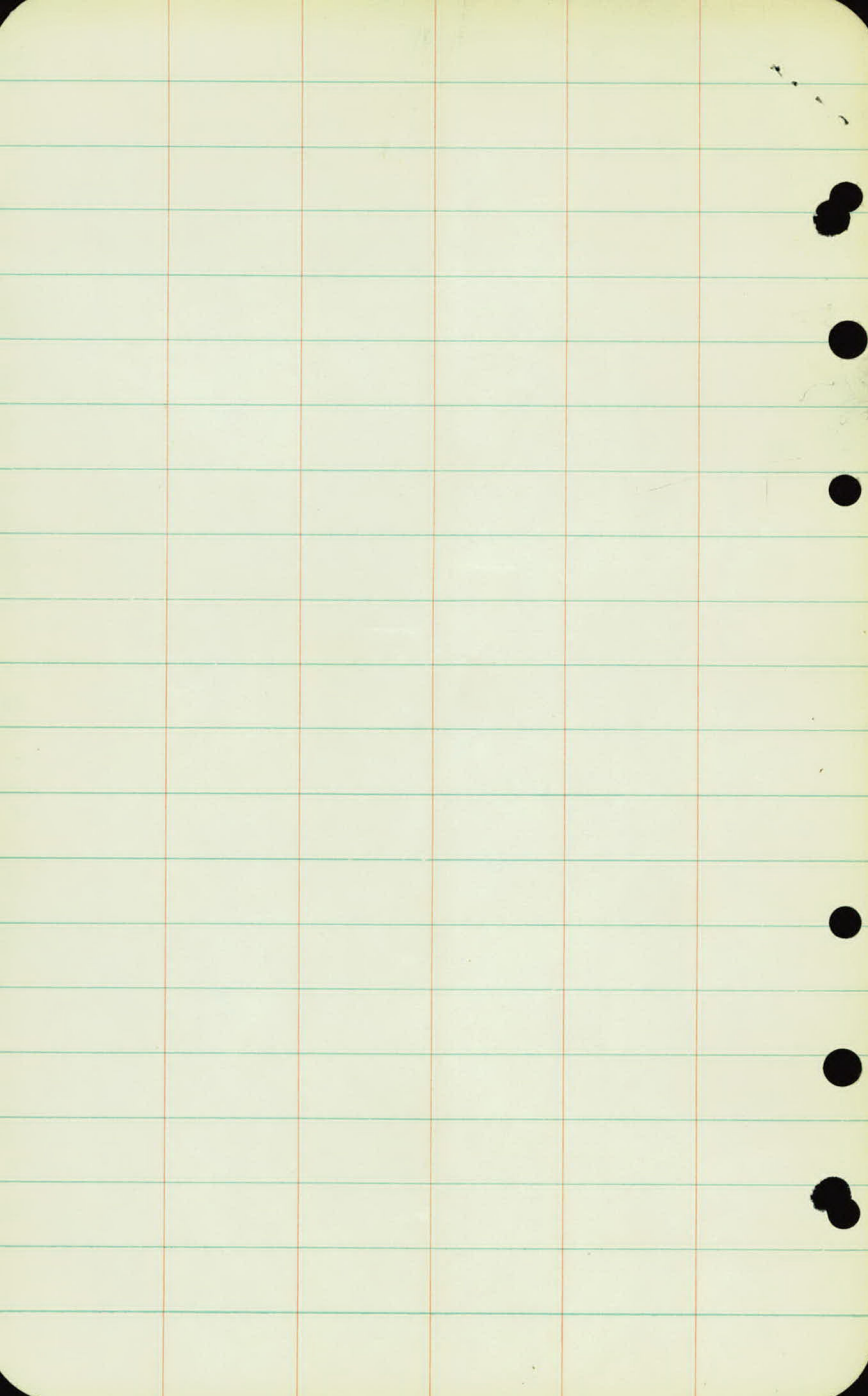
8.41 04.11

in ditch

9.5 03.0

9.85 02.67

E. End Mono. Colv.



FK
PL
RR
OP
DF

June 30, 1959

1

Edgerton & Labor e

Black Top Location

3 pages

Obj

Az Stadia

Pt at CTR. of EGERTON 400' SOUTH of CTR.

Sect. 5-29-22

to CTR. Sec 5-29-22 0°00' 400'

(NORTH)

EDGE of Blacktop SHOULDER 89° 12' ✓

140° 24' ✓

144° 33' ✓

144° 15" 45' ✓

136° 54' ✓

128° 30" 60' ✓

120° 30" 69' ✓

113° 05' 74' ✓

102° 20" 82' ✓

91° 40" 100' ✓

84° 40" 118' ✓

79° 10" 149' ✓

76° 45" 180' ✓

June 30, 1959

2

EDGE of RUBBLE gutter:

<u>AZ</u>	<u>STADIA</u>	
77° 15"	149'	✓
79° 35"	130'	✓
83° 15"	114'	✓
88° 20"	99'	✓
94° 35"	86'	✓
107° 50"	72'	✓

END of gutter at Culvert:

114° 20"	71'	✓
----------	-----	---

EDGE of BLACKTOP: (South Side)

99° 50"	123'	✓
109° 20"	106'	✓
120°	99'	✓
132° 10"	96'	✓
142° 05"	100'	✓
150°	105'	✓
157°	111'	✓
164° 15"	123'	✓

③

[continued]

AZ STADIA

EDGE of BLACKTOP:
(SOUTHSIDE)

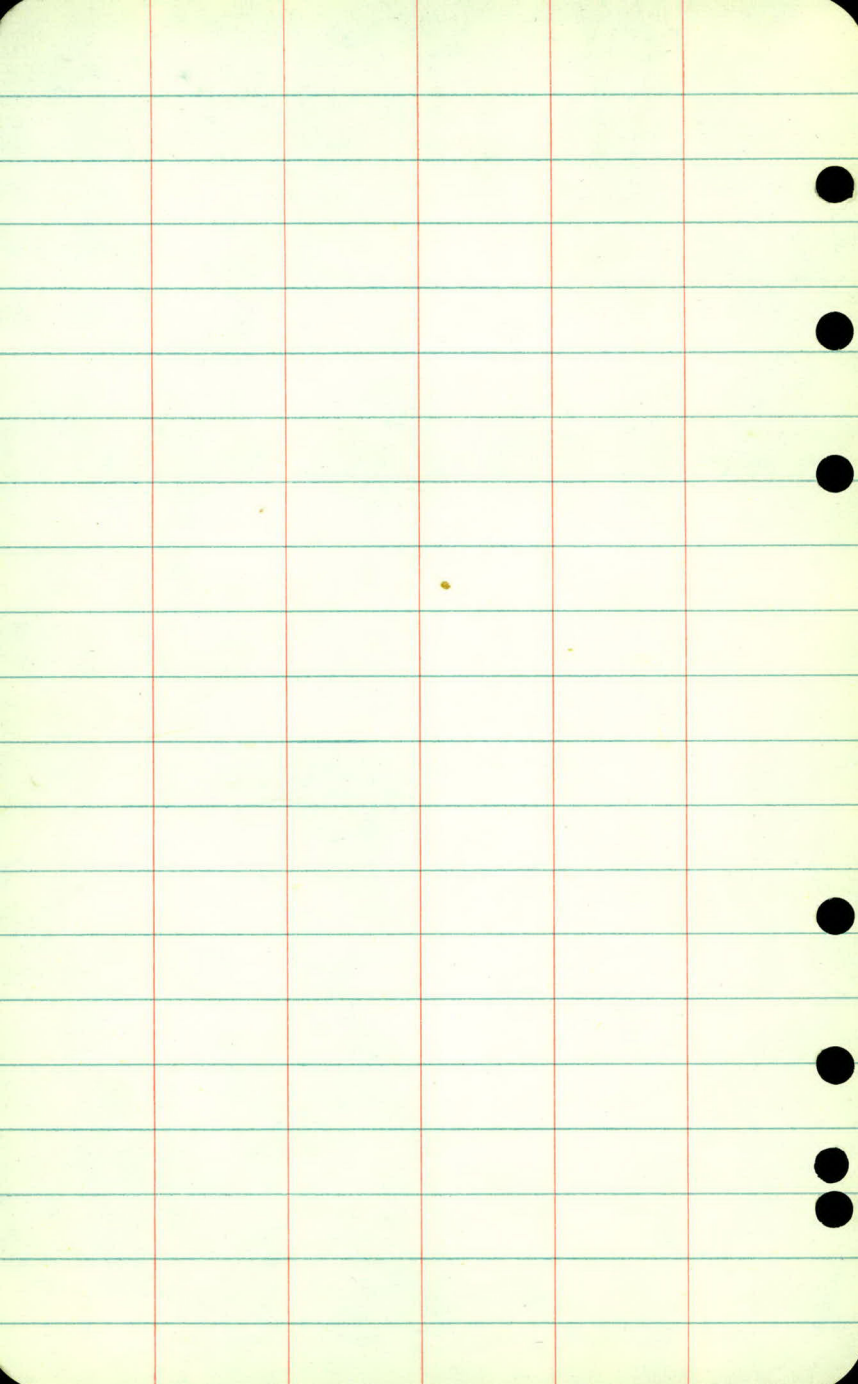
169° 133' ✓

171°30' 144' ✓

172°40' 155' ✓

June 30, 1959

3



1
Edgerton St

La Bore to Co Rd "D"

Ditch Profiles

16 pages

Rec. 12/20/57

Sta + π - Elev

BM 4.91 914.09

(909.18)

160 + 41.22 = C.F.D."

+ 14

+ 13

160 } Ent

159 + 83

+ 50

+ 45

} Ent

+ 12

159

+ 50

FK
RG
KP
CW

14
K
4
8

14

±

RT

Dec 23, 1957

2

Top Meat at Co Rd "D"

9.12
FL 18" SCP

4.47
9.62
FL 15" CM

10.16

9.52
FL 15" CM

9.3

9.57
FL 15" CM

9.47
FL 15" CM

9.1

9.2

8.5

9.4

Sta + π - Elev

914.09

158
+ 30

Ent

+ 10

+ 18

158

Ent

+ 87

+ 79

Ent

+ 67

+ 50

2

Dec 23, 1957

3

Lt

Rt

4.78

9.31

FL 15" CM

9.11

FL 15" CM

9.09

FL 15" CM

9.2

9.31

FL 15" CM

8.69

FL 15" CM

4.63

9.26

FL 15" CM

8.8

8.9

Sta + π - Elev

914.09

157+43

} Ent

+23

157+01

} Ent

+81

+50

+30

+10

Dec. 23, 1957

4

LT

RT

8.87
FL 15"CM

8.73
FL 15"CM

S

4.99

9.10
FL 15"CM

8.8

9.30
FL 15"CM

8.6

8.6

9.20
FL 15"CM

4.91

9.18
FL 15"CM

Sta + π - Elev

914.09

156 + 06

156

} Ent

+ 86

TP

5.05

915.09

4.05

910.04

+ 50

+ 23

} Ent

+ 03

155

+ 50

2 Dec 23, 1957

5

24

B+

8.96
FL15"CM

8.6

5.14
8.95
FL15"CM

96

94

5.03
10.06
FL15"CM

5.21
9.88
FL15"CM

9.5

9.7

9.2

9.7

Sta + π - Elev

915.09

154+23

+16

Ent

+05

154

Ent

+88

+50

+09

153+24

11

Dec 23, 1957
L RT 6

836

9.61
FL 15"CM

9.75
FL 15"CM

9.72

2.0

5.12
9.67
FL 15"CM

8.9

2.5

5.34
9.75
FL 15"CM

5.53

9.56
FL 15"CM

Sta + π - Elev

915.09

152+94

+89

+50

+08

152

Ents

905.1

151+88

+50

TP 4.85 913.40 4.54 910.55

Dec 23, 1957

14

RT

7

5.29

9.80

FL 15"CM

5.29

9.80

FL 15"CM

0.03

9.2

9.2

5.37

9.72

FL 15"CM

5.40

9.69

FL 15"CM

10.08

5.30

9.39

FL 15"CM

5.41

9.68

FL 15"CM

8.9

9.2

sta 151 &

Sta + π - Elev

915.40

151 + 08

151

Ents

149 + 89

+ 58

+ 50

Ent

+ 33

+ 09

150

Ent

+ 89

+ 83

Ent

+ 63

± Dec 23, 1957

14

FL

8

5.49

9.95
FL 15"CM

9.95
FL 15"CM

5.14

9.83
FL 15"CM

9.96
FL 15"CM

9.78
FL 15"CM

9.5

9.98
FL 15"CM

5.47

9.73
FL 15"CM

9.2

5.83

9.57
FL 15"CM

3.85

9.55
FL 15"SCP

9.63
FL 15"SCP

Sta + π - Elev

915.40

148+50

+07

149

+87

Ent

+81

+61

905.7

+30

+18

148

47+98

Dec 23, 1957

Lt.

£

Rt

9

9.2

9.2

9.73
FL 15" CM

9.4

5.75

9.65
FL 15" CM

9.61
FL 15" CM

5.42
9.98
FL 15" CM

9.2

9.6

05.52

9.88
FL 15" CM

9.3

905.48
9.92
FL 15" CM

12.5
72

Sta	+	π	-	Elev
-----	---	-------	---	------

		915.40		
--	--	--------	--	--

147+50				
--------	--	--	--	--

TP	6.86	914.74	7.52	907.88
----	------	--------	------	--------

BM	5.55	914.69	5.55	909.21 (909.14)
----	------	--------	------	-----------------

+07				
-----	--	--	--	--

+86				
-----	--	--	--	--

+50				
-----	--	--	--	--

+16				
-----	--	--	--	--

+06				
-----	--	--	--	--

FK 12
KP X
GW 4

Dec 23, 1957
Dec 26, 1957
Cold 18° clear RT 10

16.8

8.6

9.0

Top 5 End Culvert Fe Ent Lt Sta 146?

Spike in PP RT Sta 149+50

8.45
FL 15" CM

7.20
1.25

8.11
FL 15" CM

8.11
FL 15" CM

7.77
FL 15" CM

7.9

7.5

✓

7.90
FL 15" CM

6.65

129 7.49
FL 15" CM

Sta + π - Elev

914.69

145 + 96

+ 67

+ 50

+ 24

145

+ 83

Dec 26, 1957

11

14

84

7.88
FL 15" CM 6.63

5.98 7.23
FL 15" CM

6.8

7.4

7.38
FL 15" CM

6.9

7.30
FL 15" CM

Sta	+	π	-	Elev
-----	---	-------	---	------

Sta	+	π	-	Elev
		914.69		

Sta	+	π	-	Elev
144+50				

Sta	+	π	-	Elev
+08				

Sta	+	π	-	Elev
144				

Sta	+	π	-	Elev
+87				

Sta	+	π	-	Elev
+50				

Sta	+	π	-	Elev
+19				

Sta	+	π	-	Elev
+10				

21

± Dec 26, 1957

ft

12

7.2

6.8

7.37
FL 15" CM

6.75
FL 15" CM

7.33
FL 15" CM

6.98
FL 15" CM

6.7

6.6

6.61
FL 15" CM

*

7.00
FL 15" CM

Sta + π - Elev

914.69

143

+99

+90

+81

+84

+67

+64

Dec 26, 1959

13

Lt

Rt

11.28

3.41

6.91
FL 15" CM

*

7.11
FL 15" CM

6.71
FL 15" CM

6.89
FL 15" CM

5.79
FL 15" CM

6.87
FL 15" CM

Sta

+

π

-

Elev

9/14.69

142+50

+ 20

142

+ 50

+ 33

+ 13

Dec 26, 1957 1A

Lt

Rt

6.5

6.4

*

5.56

6.81
FL15"CM

5.32

6.57
FL15"CM

6.6

6.2

6.5

6.89
FL15"CM

5.64

6.97

5.72

Sta	+	π	-	Elev
-----	---	-------	---	------

		914.69		
--	--	--------	--	--

141+09				
--------	--	--	--	--

141				
-----	--	--	--	--

289				
-----	--	--	--	--

+51				
-----	--	--	--	--

+25				
-----	--	--	--	--

+23				
-----	--	--	--	--

LT

Dec 26, 1957

15

RT

550

6.75
FL 15" CM

6.7

539

6.62
FL 15" CM

561

6.86
FL 15" CM

6.7

6.83
FL 15" CM

558

6.99
FL 15" CM

570

Sta + π - Elev

9/4.69

140

+ 8'9

+ 50

Dec 26, 1957

16

17

BT

6.7

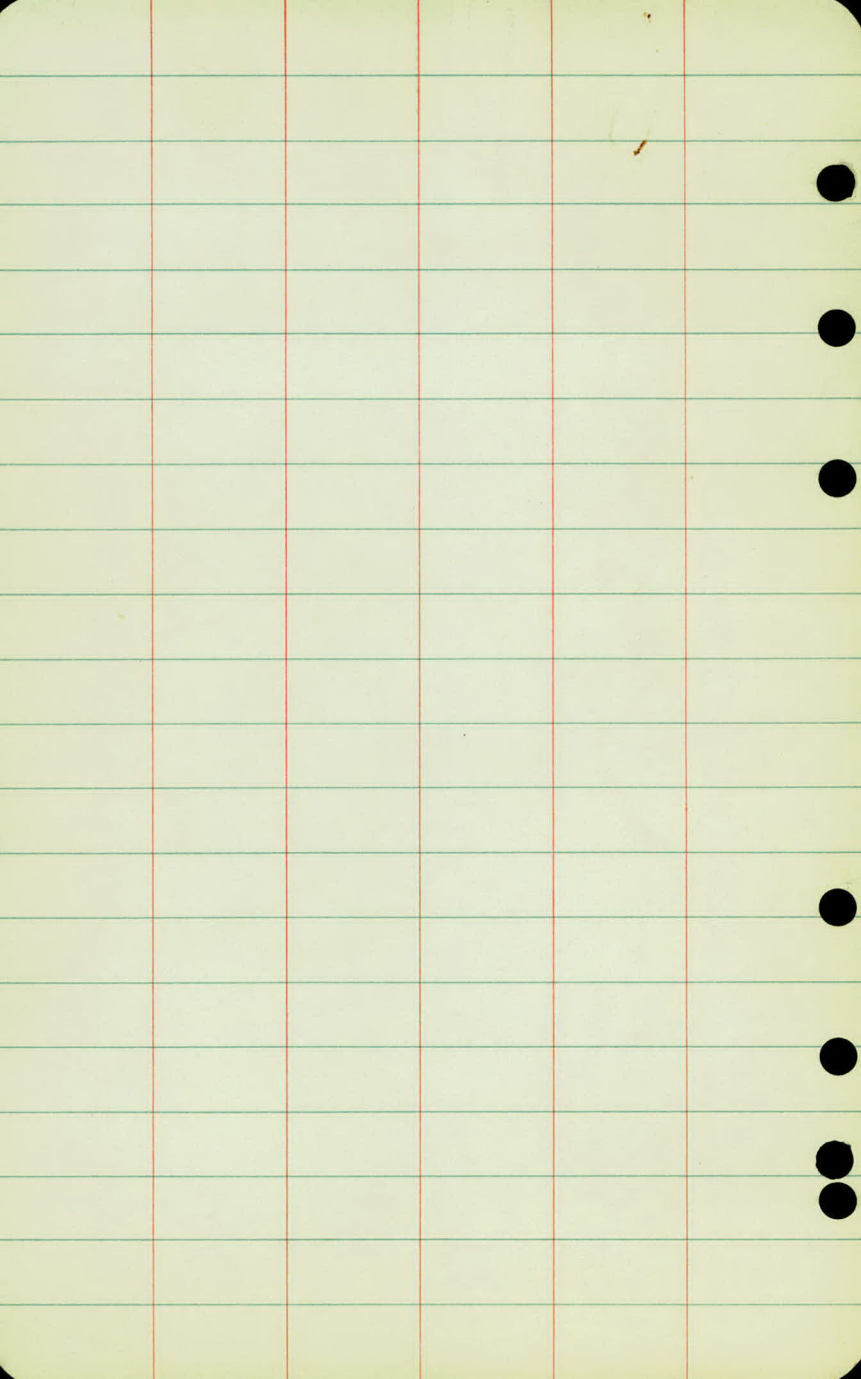
3.45

4.76
FL 15 CM

551

6.5

7.0



Easement Drainage
on Edgerton
Near Laborre Rd

1 Aug 1952

Widera
Moeschter
Clark
Barnes

- 9.1 grade

Sta P.G.R

0 edge pavement 1.95 1.95

0+00 33' from #
6.2

+ 17 7.8 15.5

+ 42 10.0

+ 67 12.3

+ 92 14.6

102 15.5

Con. of Sec. 5.

$$\begin{array}{r} 2630.55 \\ - 1898.75 \\ \hline 731.80 \end{array}$$

731.8'

-170'

Drain. casement.

10'

2630.55 = Meas.

2630.18 = Rec.

--- 1898.75' ---

Edgerton St.

90° 08'

5/4 Cor.
Sec. 5

C 3.0

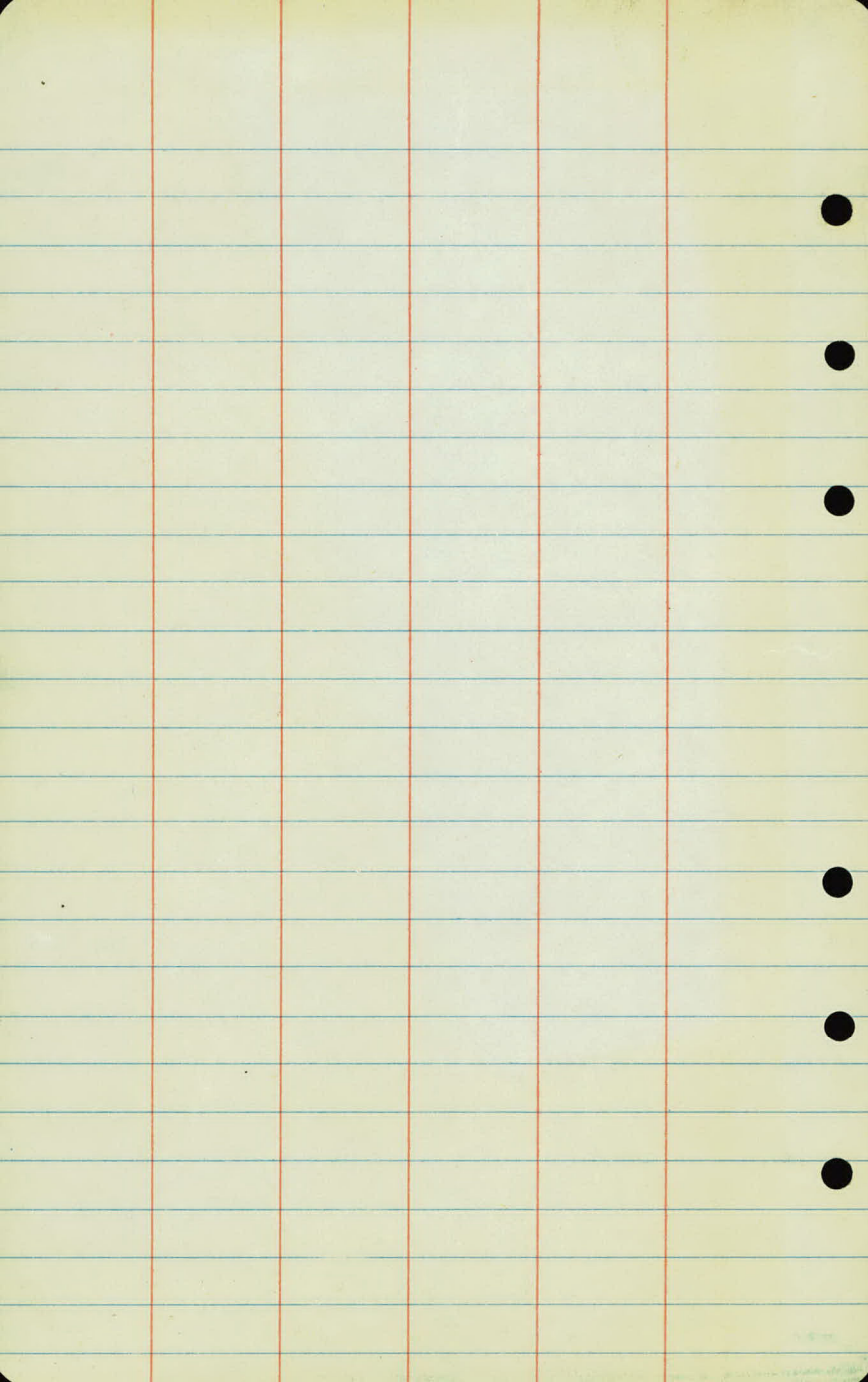
C 3.0

C 3.0

C 3.5

C 2.0

Grade



346-261

1

$$\frac{15.5}{2.0} = 7.75$$

$$\frac{3.8}{2.0} = 1.9$$

$$\begin{array}{r} 108 \\ 102 \overline{) 113} \\ \underline{102} \\ 11 \end{array}$$

Profile

$$\frac{11.3}{1.17} = 9.65$$

$$0400 \quad 6.2 = 6.30$$

$$+17 \quad 7.8 = 6.30$$

$$+42 \quad 10.0 = 6.30$$

$$+67 \quad 12.3 = 6.35$$

$$+92 \quad 14.6 = 6.20$$

$$1402 \quad 15.5$$

$$\frac{14.25}{15.5}$$

$$\begin{array}{r} 6.2 \\ 3.8 \\ \hline 10.0 \\ 6.2 \\ 6.1 \\ \hline 12.3 \\ 8.4 \\ 6.2 \\ \hline 14.6 \\ 6.2 \\ 9.8 \\ \hline 15.5 \end{array}$$

$$4.2$$

$$4.75$$

$$8.9$$

$$4.2$$

$$7.6$$

$$11.8$$

$$4.2$$

$$10.2$$

$$14.4$$

$$11.2$$

$$4.2$$

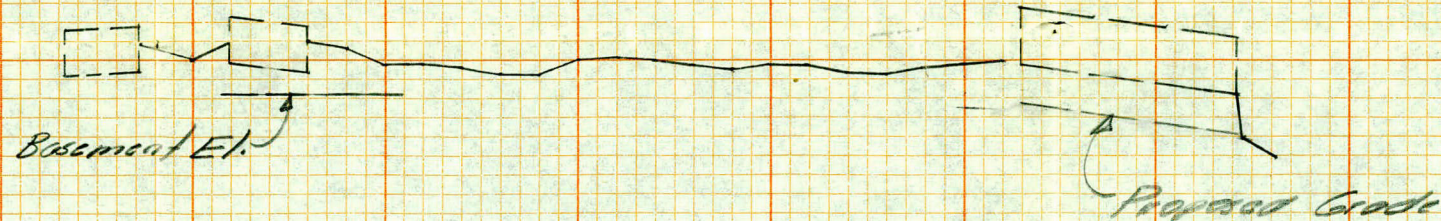
$$15.4$$

910

905

900

EDGERTON ST.



Ditch Profile
EDGERTON ST.
South of Co. Rd "D"

Edgerton + AR
Topic for
Signal Locations

Everton 75

FK
MB
BF

July 13, 1973

1

EDGERTON STREET
at

Co. Rd. "D"

L

Q

R

+14 $\frac{\text{Unusef Field}}{\text{Entrance-Dirt}}$

2

Shoulder Road
18 12 12

Shoulder
16

+93 $\frac{\text{10' Ent}}{\text{Gravel}}$

+66 $\frac{\text{PP}}{29}$

+47 $\frac{\text{14' Ent}}{\text{C. Rock}}$

1

Shoulder Road Shoulder
15 12 12 13

+77 $\frac{\text{10' Ent}}{\text{C Rock}}$

+62 $\frac{\text{PP}}{32}$

+53 $\frac{\text{10' Ent}}{\text{C Rock}}$

0

Shoulder Road
14 12 12

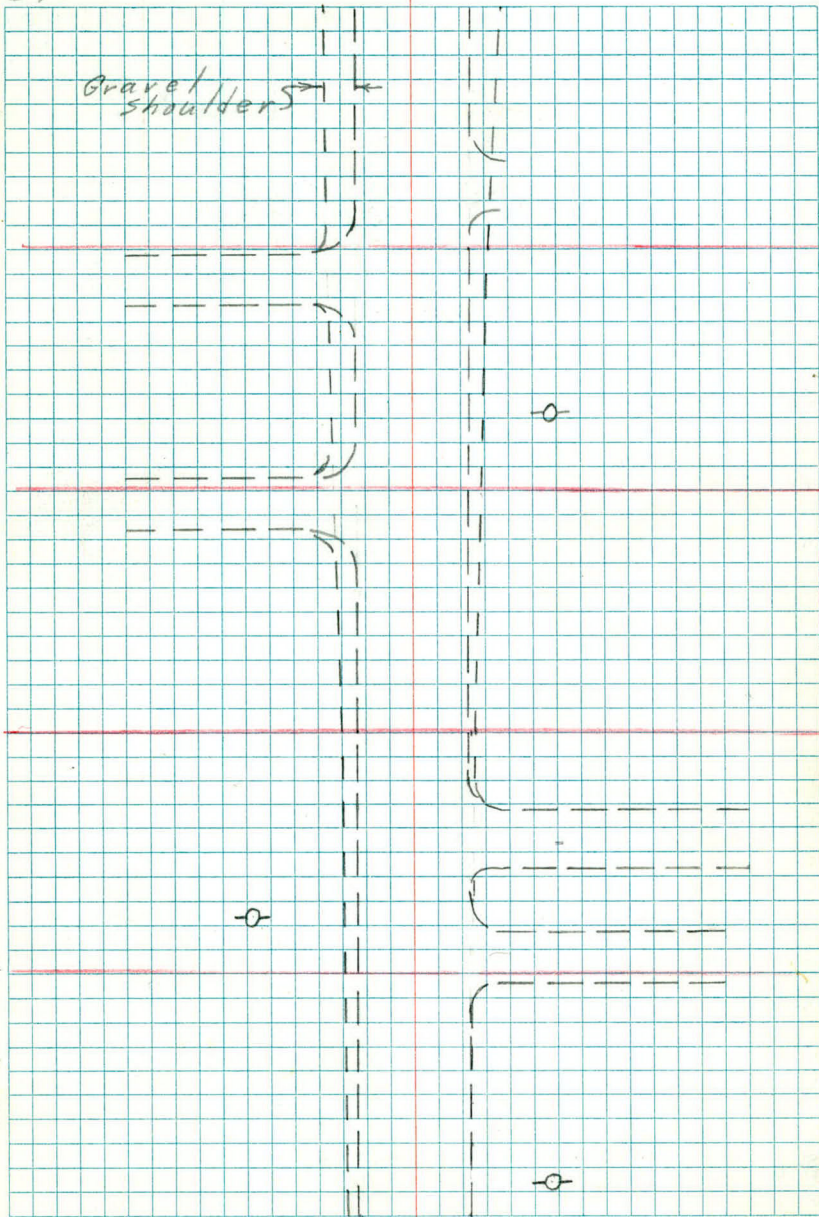
+07 $\frac{\text{PP}}{29}$
Shoulder
12

FK
MB
BF

July 13, 1973

2

Gravel
shoulders



5 = Section Corner Road
19 23

+94 BGR
22

+80 Road
27

+99 BGR
28

+80 POR
24

+61 POR
45

+57 Cor Bit
59

+61 Cor Bit
84

+61 POR
38

+53 Cor Bit
87

+44 Cor Bit
119

+53 Cor Bit
118

+24 Edge Road
182

+35 End GR
175

+20 ER
64

+13 BGR
50

4

Shoulder
35

Road
26 30

GR
27

+97 PP
53

+78 GR Road
19 22

+72 BR
13

+40 GR Rd
19 22

+40 Road Shoulder
19 19

+08 MH
22

+02 EGR
21

3

Show Road
19 13 21

+68 12' Ent
Gravel

+67 PP
39

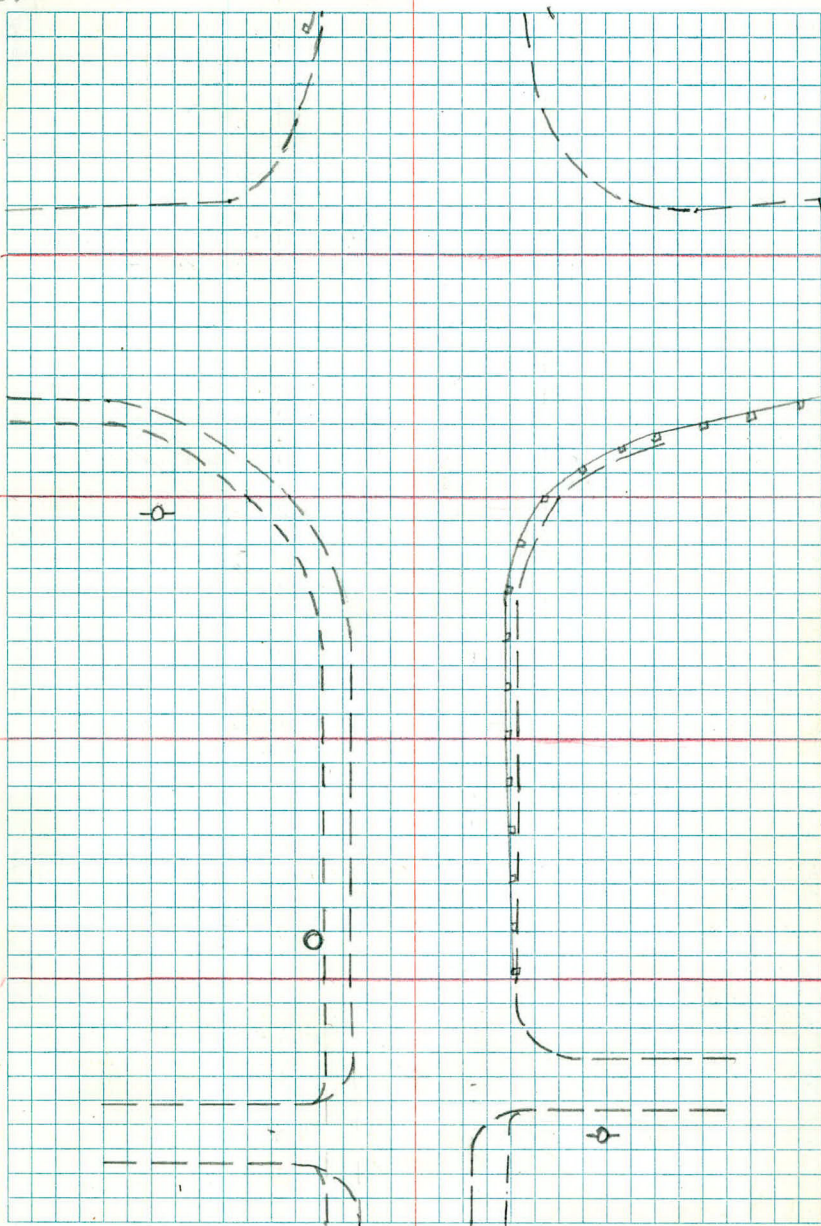
+78 10' Ent
Gravel

+50 PP
48

FK
MB
BF

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3



GR
19
X

199 Bridge
22

198 Curb
14
X

195 GR
13
X

193 Curb
14
X

193 Bridge
18

166 B Curb
14
X

166 GR
15
X

166 Curb
14
X

GR
20

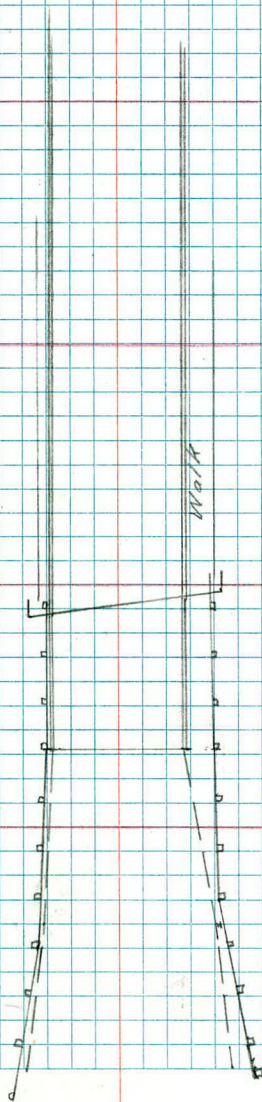
165.5 B Bridge Approach
Panel
X

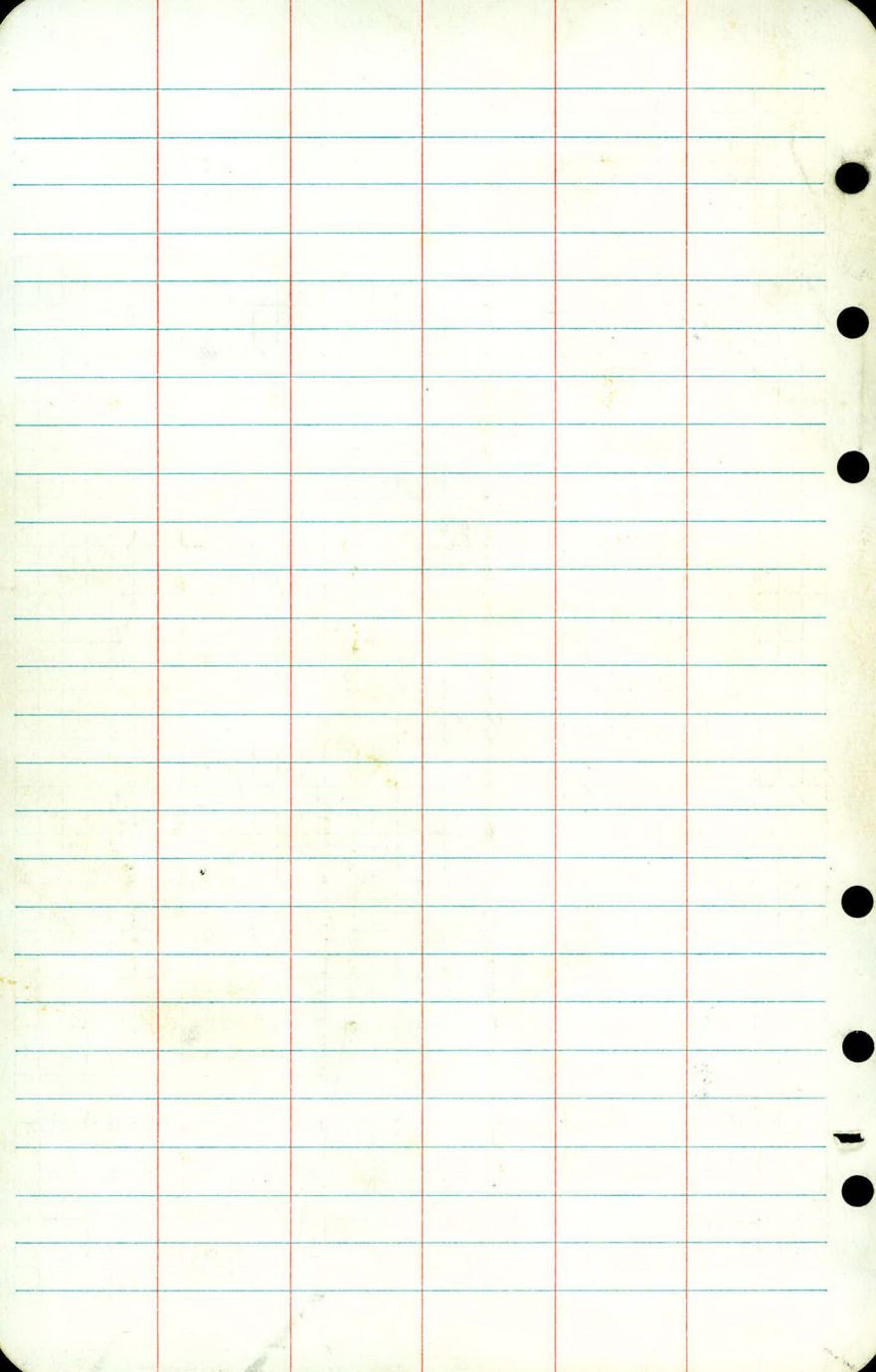
GR Road
130 17 16 21 GR
22
X X X X

FK
MB
BF

July 13, 1973

4





W.S.
K.6
G.A.

10-20-75
CLEARING

CROSS SECTIONS

EDGERTON

STA. 3 → STA 4+80

CORD "D"

STA. 8+50 → STA 11+50

STA	+	π	-	ELEV.
BM	25	102.50		(100.00)
8+50				
✓				
✓				
9+00				
+ 50				
10+50				
11+50				
11+50				

W.S
K6
G.A

LT

E

RT

10-20-75
CLEAR: 65.2

INTERSECTION OF EDGERTON : CORNO "D"

96.8	97.1	96.8	88.7	90.6	91.3
5.1	5.4	5.7	13.8	11.9	11.2
	12	18	49	61	75

98.2	97.8	97.2	89.2	90.9	91.4
4.3	4.7	5.3	13.3	11.6	11.1
	12	21	50	65	75

99.0	98.6	98.2	89.1	89.1
3.5	3.9	4.3	13.4	13.4
	15	25	56	80

99.1	98.3	97.9	89.8	89.3
3.4	4.2	4.6	12.7	13.2
	20	25	51	70

98.3	97.9	97.6	89.4	91.9
4.2	4.6	4.9	13.1	10.6
	12	23	44	54

97.4	97.0	96.7	89.7	91.0
5.1	5.5	5.8	12.8	11.5
	12	21	43	50

STA

+

π

-

ELEV.

102.50

3+00

+50

4+00

W.S
K.G
G.A

LT

⊥

RT

10-20-75 3
CLEM: 65°

93.8	89.3	96.0	96.2	96.4	95.6	92.0	92.4	92.1
8.7	13.2	6.5	6.3	6.1	6.9	10.5	10.1	10.4
58	41	20	12		19	34	42	52

91.6	89.0	96.9	97.4	97.6	97.2	96.6	89.3	92.1
10.9	13.5	5.6	5.1	4.9	5.3	5.9	13.2	10.4
66	46	23	12		21	26	46	58

97.1	98.1	98.6	99.1	98.3	97.5	93.8	93.0
5.4	4.4	3.9	3.4	4.2	5.0	8.7	9.5
74	47	25		29	40	65	90

