

Dr. 16 - Bk. 13

OFFICE OF
RAMSEY

Y ENGINEER
MINN.

Pla. c Survey

BALD EAGLE BLVD. W.

From County Rd. H^E To Co. Rd. "J"

Road Acc't. No. 0

Date Filed: 3-26-27

File

Plan Survey.
Bald Eagle Blvd.

from Co. Rd. H²
to Co. Rd. J

Location Notes

5/9/39 Complete

Party { R. Passc.
H. Wilke
A. Moeschler
L. Goldberg

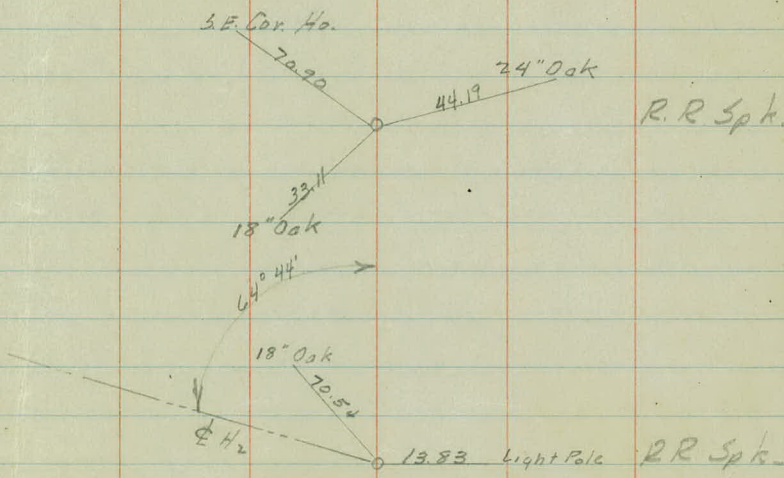
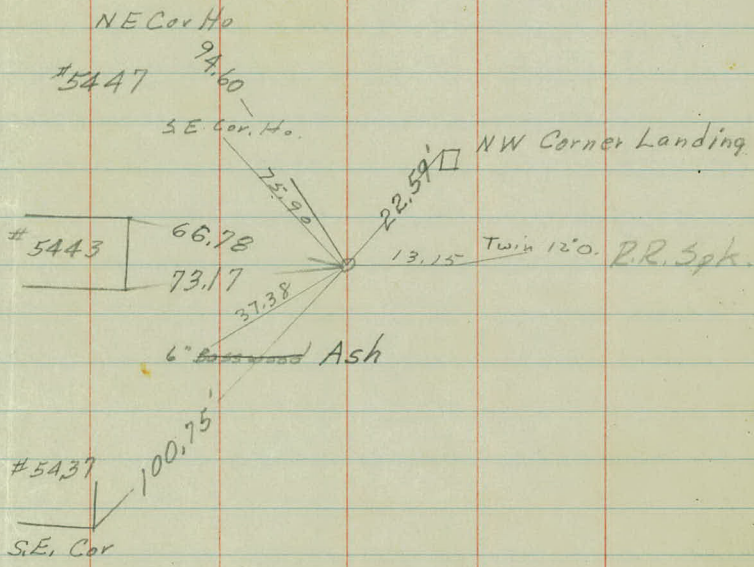
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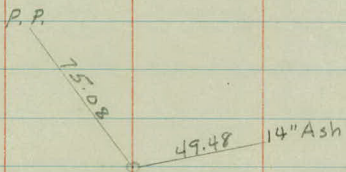
Sta	Pt	Angle	
		Lt	Rt
+42.90	P.T.	$2^{\circ} 29\frac{1}{2}'$	$\Delta = 4^{\circ} 59' \text{ Lt.}$
6		$2^{\circ} 04'$	$D = 2^{\circ}$
+50		$1^{\circ} 34'$	$T = 124.67$
5+18.40	P.I.	$4^{\circ} 59'$	$L = 249.17$
5		$1^{\circ} 04'$	$R = 2864.93$
+50		$0^{\circ} 34'$	$E = 2.5'$
4		$0^{\circ} 04'$	
3+93.73	P.C.	0-00	

+68.86	PT	$5^{\circ} 45\frac{1}{2}'$	$\Delta = 11^{\circ} 31' \text{ Rt.}$
+50		$5^{\circ} 06'$	$D = 7^{\circ}$
2		$3^{\circ} 21'$	$T = 82.59$
1+86.95	P.I.	$11^{\circ} 31'$	$L = 164.52$
+50		$1^{\circ} 36'$	$R = 819.02$
1+04.34	P.C.	$0^{\circ} 00'$	$E = 40$

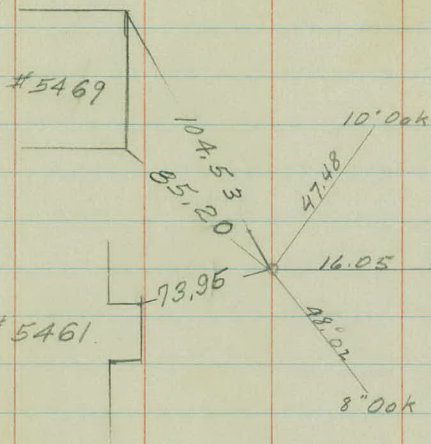
0+00 P.O.T. E Co Rd. H²



Sta	PT	Lt	Angle	Rt	
+50.26	PT.		18° 57'		
+50			18° 55'		$\Delta = 37^{\circ} 54' \text{ Rt.}$
12			15° 40'		$D = 13^{\circ}$
+50			12° 25'		$T = 151.66$
11+10.38	P.I		37° 54'		$L = 291.54$
11			9° 10'		$R = 441.684$
+50			5° 55'		
10			2° 40'		
9+58.72	P.C				
+62.37			4° 33 $\frac{1}{2}$ '		$A = 9^{\circ} 07' \text{ Lt.}$
+50			4° 11'		$D = 6^{\circ}$
8			2° 41'		$T = 76.17$
7+86.60	P.I	9° 07'			$L = 151.94$
+50			1° 11'		$R = 955.37$
7+10.43	PC		0° 00'		$E = 30$



RR Spk.



RR Spk.

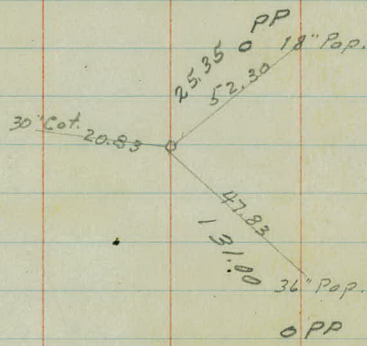
#5461

Sta Pt Lt Angle Rt

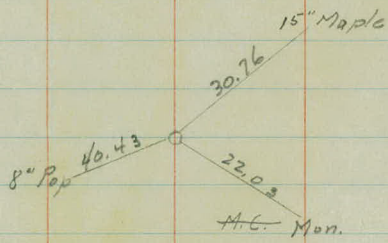
+33.70	P.T.	6°35'	A = 13°10'
23		5°14'	D = 8°
22+51.84	P.I.	13°10'	T = 82.72
+50		3°14'	L = 164.58
22		1°14'	R = 716.779
21+69.12	P.C.		E = 5.0

+56.78	P.T.	10°43½'	A = 21°27' Lt.
+50		10°08'	D = 17°
14 +25		5°53'	T = 64.08
13+94.68	P.I.	21°27'	L = 126.18
+75		1°38'	R = 338.27
+50		0°00'	E = 6.0
13+30.60	P.C.		

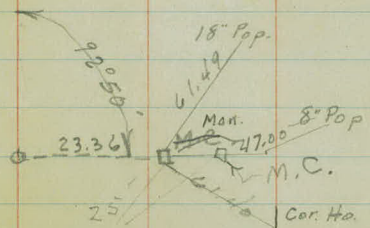
13+80.1 P.O.C. section tie ^{Def.} 4°12'



Bolt Spike

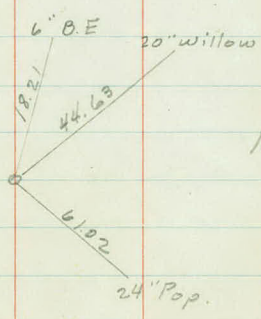


R.R. Spk



Angle

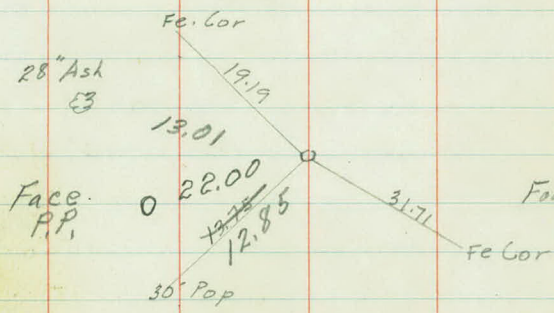
Sta	Pt	Lt	Rt
+53.73	P.T.		$24^{\circ} 23\frac{1}{2}'$
+50			$23^{\circ} 58' \Delta 48^{\circ} 47'$
30			$18^{\circ} 13' D 23^{\circ}$
29+55.35	P.I.	$48^{\circ} 47'$	$T 713.72$
+50			$12^{\circ} 28' L 212.10$
29			$6^{\circ} 43' R 250.793$
+50			$0^{\circ} 58' E = 24.0$
28+41.63	P.C.		
+89.82	P.T.		$19^{\circ} 28'$
+50			$14^{\circ} 29' A 38^{\circ} 56'$
27+15.74	P.I.		$38^{\circ} 56' D 25^{\circ}$
27			$8^{\circ} 14' T 81.65$
+50			$1^{\circ} 59' L 155.73$
26+34.09	P.C.		$R 231.071$
			$E = 14.0$



O.K.
Iron Pipe
~~2x2 Hub~~

28 + 41.63
27 + 89.82
31.81

113.72
81.65
51.81
247.18

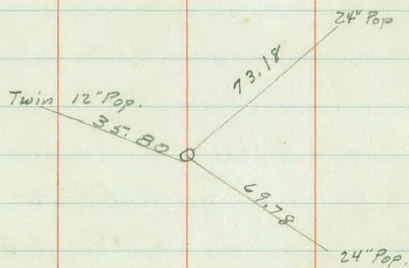
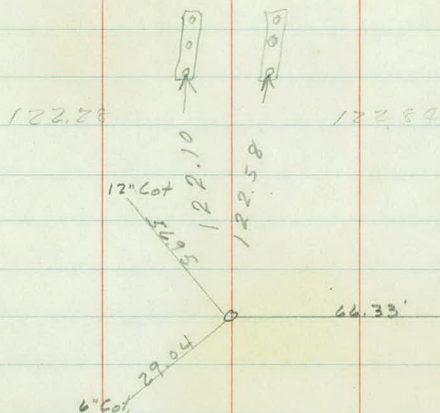


10-69 Jk
O.K.
Bent Spike
2x2 Hub.

Found 5-13-55

Sta.	Pt.	Angle	
		Lt.	Rt.
+06.32	P.T.	18°53'	
41		18°11'	A 37°46'
+50		12°41'	D 22°
40+24.28	P.I.	37°46'	T 89.63 .
40		7°11'	L 171.67 .
+50		1°41'	R 262.042 .
39+34.65	P.C.		E = 15.0

33+90.42	P.T.	9°38'	
+50		7°12½'	
33+11.05	P.I.	19°16'	A = 19°16'
33		4°12½'	D 12°
+50		1°12½'	T 81.19 .
32+29.86	P.C.	0°00'	L 160.555 .
			R 478.339 .
			E = 7.0



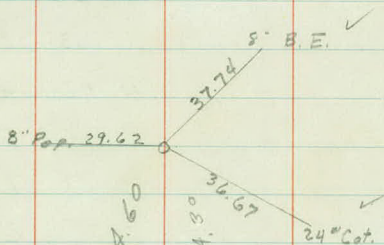
Mosquito

Sta	Pt.	Angle	
		Lt	Rt
+4180	PT		$12^{\circ} 29\frac{1}{2}'$
55			$9^{\circ} 46\frac{1}{2}'$ A $24^{\circ} 59'$
+50			$6^{\circ} 31\frac{1}{2}'$ D 13°
54+47.47	P.I.		$24^{\circ} 59'$ T 97.85 .
54			$3^{\circ} 16\frac{1}{2}'$ L 192.18 .
+50			$0^{\circ} 01\frac{1}{2}'$ R 441.684 .
53+49.62	P.C.		E = 11.0

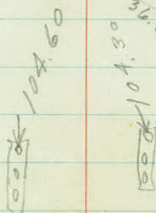
+84.57	P.T.		$2^{\circ} 36'$
+50			$2^{\circ} 15'$ A $5^{\circ} 12'$
43			$1^{\circ} 45'$ D 2°
42+54.66	P.I.	$5^{\circ} 12'$	T 130.09 .
+50			$1^{\circ} 15'$ L 260.0 .
42			$0^{\circ} 45'$ R 2864.93 .
+50			$0^{\circ} 15'$ E = 10 .
41+24.57	P.C.		



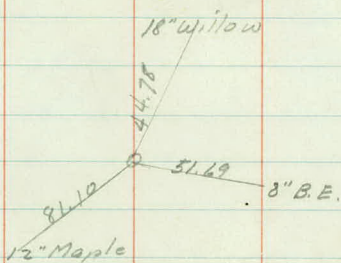
2 x 2 Hub.



Iron
Boat Spike
2 x 2 Hub.



Sta	Pt.	Angle	
		Lt	Rt
+21.50	P.T.		35° 24 $\frac{1}{2}$ '
62			31° 58'
+75			27° 58' Δ 70° 49' Lt.
+50			23° 58' Δ 32°
61+29.15	P.I.	70° 49'	T 128.95
+25			19° 58' L 221.30 ✓
61			15° 58' R 181.398
+75			11° 58' E 40'
+50			7° 58'
+25			3° 58'
60+00.2	P.C.		
+17.69	P.T.		20° 53'
59			19° 23' Δ 41° 46' Rt.
+50			15° 08' Δ 17°
58+01.06	P.I.		41° 46' T 129.06
58			10° 53' L 245.69
+50			6° 38' R 338.273
57			2° 23' E 23'
56+72.0	P.C.		

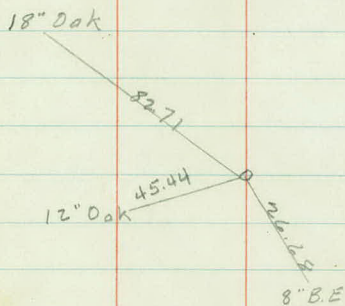


2x2 HWO

107.40

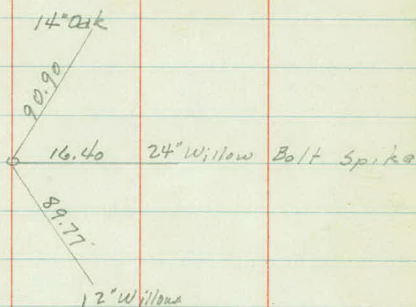
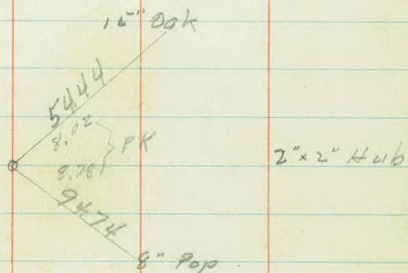
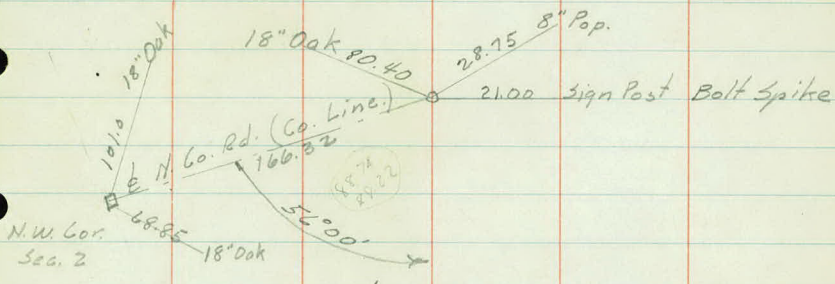
87.50

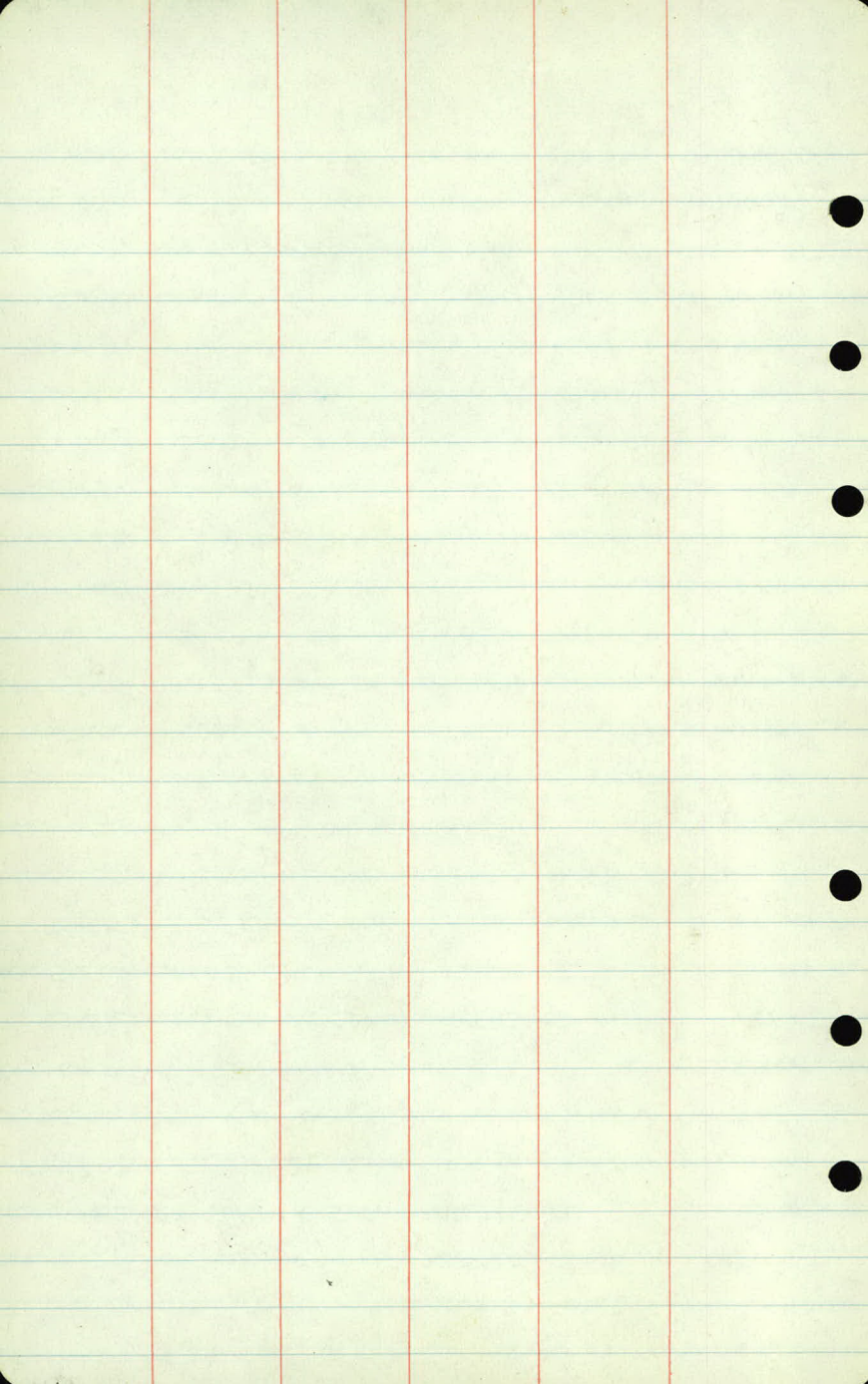
25



2x2 HWO

Sta	Pt.	Lt.	Rt.
74+99.0	P.O.T.		N. Co. Line Rd.
+84.67	P.T.		$\Delta 32^{\circ} 28'$
+50		$16^{\circ} 14'$	$D 20^{\circ}$
72+06.18	P.I.	$12^{\circ} 47'$	$T 83.84$
72		$32^{\circ} 28'$	$L 162.33$
+50		$7^{\circ} 47'$	$R 287.939$
71+22.34	P.C.	$2^{\circ} 47'$	$E = 12'$
		$0^{\circ} 60'$	
66+62.75	P.I.		$0^{\circ} 44'$





Topography

Bald Eagle Blvd W.

10 10

Lake 62.

6

10 11

Lake 62'

5

10' 10'

Lake 59'

4

11 9

Lake 66

3

10' 9'

^L
Lake 68'

2

11' 10'

Lake 72

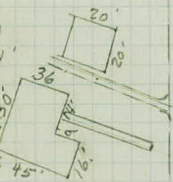
1

12' 11'

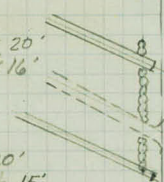
0

Lake 63'

- +29 Cor. Ho. 49
- +07 Cor. Ho. 54
- +89 Ent.
- +84 Rgc tie Ent.
- +67 2' Conc. Walk
- +70 Cor. Ho. 58
- +60 Rgc Tie Walk
- +53 Cor. Ho. 62

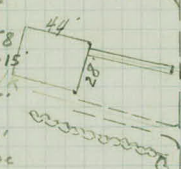


- +87 End Hedge - 20'
- +72 3' Conc. Walk 16'
- +67 Rgc Tie Walk
- +40 Ent.
- +35 Rgc tie Ent.
- +20 Bgg. Hedge 20'
- +18 2' Conc. Walk 15'

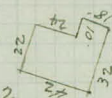


- +69 Ent.
- +63 Rgc tie Ent.

- +42 Cor. Ho. 58
- +28 2' 3' Walk - 15'
- +25 Rgc tie Walk
- +17 Cor. Ho. - 65'
- +94 Drive
- +86 Hedge - 18'
- +82 Rgc tie Hedge



- +57 Cor. Ho. 52



- +25 Cor. Ho. 62

- +96 Ent.
- +90 Rgc tie Ent.

- +62 Rad Pt 14'
- +45 Cor Hedge 35'
- +34 Rad Pt. 51'
- +12 Shldr Xs 2'



Wooded - Oaks - Poplars - Willows

BALD EAGLE LAKE



- +05 2' 3' Conc. Step 14.5'

- +77 End G. R. - 13'

G R 11'

(N 24)

+50-10 10

13

10 10

Lake 116

+50 10 9

12

9 10

Lake 125

+50 10 9

11

9 10

Lake 132

27'

+63-24'x48' CM
+50 8' 10'

21'

10

8 9

Lake 121

+58

9' 10'

9

9' 11

Lake - 90

8

10 10

Lake 68

7

10' 10

Lake 62

+81 Rge. Tie Fe
+79 Fe Cor. 19
+59 12" Pop. 15

+81 Fe. Cor. 35.5

+29 Cor. Ho 51
+07 Cor. Ho. 55
+88 Fe. Cor. 33
+87 4 Willows 27
+75 PP. - 20
+52 Fe Cor. 36
+40 Ent.

+09 12" Ash. 22
+98 Twin Elm. 18
+84 Ent.
+74 Twin Elm. 19
+50 Clump 6 Willows 27

+10 18" Bp. 24
+88 Ent.
+91 Cor. Bldg 41
+75 Rge tie Ent
+72 Cor Bldg 38
+68 Clump 5 Willows 24

+30 Out Ho 30

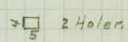
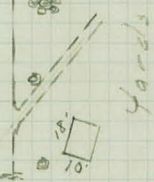
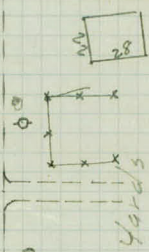
Swamp 75

+77 PP. - 23

+50 Swamp. 68

Swamp. 91

Swamp
Uncultivated



+24 8" Elm. 18

+90 Twin Pop. 14

+37 6" Elm. 16
+34 6" Elm. 16

Yards

PALE EAGLE LAKE

8 9

20

9 9

19

10 9

18

9 9

Lake 278'

17

10 9

16

9 10

15

17' +97 12" + 33' 4" + 9 10

16'

14

10 10

Lake 126

Fe 30

Fe 34
+95 12" Vit-15'
+83 36" Pop-23

+65 14" Pop. 21'

+05 16" Pop. 22
Fe. 30'

+22 30" Pop. 22
+01 30" Pop. 23
Fe. 33
+90 P.P. 18'
+82 26" Pop 23

+60 30" Pop.-21'

+60-30" Pop 23

+33 14" Pop. 22'

+01 12" Pop 22
Fe. 30'

+71 12" Pop-21'

Fe 32'

+30 36" Pop-23

+72 24" Pop 22

Fe 29

+51 30" Pop-22
+48 PP 17'

+80 Ent.

+22 10" Pop 23

Fe 31

+43 30" Pop 23'

+50 Tie to Ent. 50
+45 30" Elm 3
+23 Mt. Ash-29
+22 Fe Cor 31
+18 20" Pop 21'
+16 Δ Fe 41'
+11 PP. 17'

+20 30" Pop 23'

Fe 29

+88 24" Pop 27'
+85 Δ Fe 30'
+93 Δ Fe 31
+62 12" Elm 22
+55 Rgc tie Ent.

+87 30" Pop 23

+21 12" Elm-21'
+00 10" Elm-22
Fe 29

+61 30" Pop 23

+79 12" Elm 21

+39 30" Pop 23

+58 12" Elm 23
+44 PP. 16

+16 30" Pop 23

Fe 28

+98 30" Pop 23

+87 Eind 12" Vit 38

+78 30" Pop 23

+60 8" Elm-20

+56 30" Pop 23

+19 14" Maple-23
+01 PP. 20
Fe 33

+31 30" Pop 23

+00 Fe 28

+01 30" Pop 21

+00 Ditch xs 8

+95 Δ Ditch-28

3' Ditch

Fe 23

240

+50 4 12

27 9 9

+50 9 8

26 8 8

25 9 10

Lake - 323

24 8 9

23 9 9

+50 9 8

22 8' 9'

21 14 +07 12" x 32' Vif (skewed) 32'

8' 9'

Fe. 36

+65 Fe. Cor. 34
+50 Tie Ent. 39'
+29 Fe Cor. 21'
+26 Rge Tie Ent

+00 36" Pop 23
Fe. 31
+98 PP 32
+81 Fe. Cor. 42'
+66 30" Pop 30'
+52 30" Pop 26'
+50 Fe 35

+09 30" Pop 26'
Fe 33

+78 10" Pop 24

+52 6" Pop 23

+28 30" Pop 23'
+08 48" - 24
Fe. 33'

+08 14" Pop 25'
Fe. 31

+33 16" Pop 32

Fe. 31'
+95 14" Pop 23

+56 48" Pop 27'
+50 Fe 35

+24 8" Pop 24

Fe. 31'
+93 12" Pop 23

+52 12" Pop 22'

+26 G.R. - 21.
Fe 30'

Fe 32 (14)
+84 30" Pop 26

+50 Fe 28
+91 - 24" Pop 22

+00 A Fe. - 15'

+94 24" Pop - 12'

+50 Fe 24'

Fe 26

+81 30" Pop 21'

+64 PP - 17'

+27 24" Pop 22
+06 - 24" Pop 22
Fe 28

+68 12" Maple 22

+16 PP 17
+15 18" Elm 23
Fe 30
+94 30" Pop 24

Fe 32'

+65 PP - 14'
+63 8" Pop 21
+50 Fe 31
+47 Ent.
+32 30" Pop 22'
+7
+10 24" Pop 23
Fe. 34

+67 30" Pop 24'
+36 Twin Pop. 26'
+27 30" Pop 23.
+25 Ditch 34
+22 RR 17
+07 Ditch 35
Fe. 34' 24D

Meadow

Hay

Marshy

Yard of Solheim Farms

3' Ditch

8

9

Lake 103

34 7 8 Lake 85

9 9

33 13 6 Lake 73

+50 19 0

32 22'-3' Lake 71

+50 20'-2'

31 15' 2' Lake 83

+50 10' 8'

30 10' 7' Lake 92

+50 10' 7'

29 14' 5' Lake 152

+50 9' 10'

28 5' 13'

25

Fe 27
 +84-4"Will-26
 +77-Twin Will-27
 +72-4"Will-25
 +53-30"Will-25

Swamp

Fe 28
 +86-26"Boss-20
 +84 Fe Coy-32
 +71 Fe x3 E

+50 Fe-37
 +35 8" Twin pop-21

+91 Beg Fe-46

+54-20"Pop-35

Cult

+65-20"Pop-49
 +45-10"Pop-40
 +20-12"Pop-41
 +13-6-12"BE-39-44
 Fe 50

+50-Fe 35

+25 Fe-32

Fe 34

Cult

+50 Fe-38
 +50 24" Oak-40

Fe 45
 +95 20" Oak 50
 +88 20" Oak 50

+59-2"Pop-29
 +50 Fe-44
 +40-2"Pop-30

Fe 36

Standing Water

FC 22 (15)
 +60-6"BE-19
 +51-4-12"Will-13
 +32-4-8"Ash-20

Fe 20
 +89 14"Willow-15

+50 Fe 20
 +43-14"Elm-19
 +25 Twin 8"Will-15
 +16-12"Willow-14
 Fe 19

+62 Twin 6"BE-14
 +50 Fe 15
 +40 12"BE-7

Fe 11

+55 6"BE-3
 +48 Twin 6"BE-8
 +28 12"BE-5

Fe 13
 +90 8"BE-13
 +84 6"Willow-14

+50 Fe-18
 +43-Twin 6"Will-18
 +30-14"Willow-18
 +05-8"Willow-18
 Fe 23

+64 6"BE-20
 +50 Fe 22

+27 Twin 18"Willow-18
 +18 Group 5-18"Willow-18
 Fe 29

+80 A Fence-37

+50 Fe 32
 +48 24"Pop-27
 +27-18"Pop-27
 +05 30"Pop-27
 Fe 32

Brush-Willows-Poplar-Etc.

16 4

Lake 41

+50 Lake 24'

41

15 5

Lake 66

+50 - 11 7

40

8' 7

Lake 123

39

7 9

Lake 128

38

8 9

Lake 128

37

14' +96- 12' ⁹ X 32' ¹⁰ VIT X Culv. Lake 116, 18'

36

9' 10

Lake 110

35 27

8 9

Lake 103

FC 33
 +99-12" Pop 30
 +69-12" Pop 30
 +70 Fe Cor 36
 +69 End G.R. - 18'

+79 Beg Fe - 31
 Note: See Detail Sketch
 on page 22 for Spillway

+21 Beg G.R. - 15
 +16 Fe Cor 36
 +96-12" Pop 30
 +73 8" Pop 27
 +50 Fe 31

+25 Fe Cor - 20

Fe 28
 +98-4" Pop 23
 +68-6" Pop 24

+24-4 Fe - 23
 Fe 24

Fe 27
 +94-6" Pop 23

Fe 24

Fe 27
 +84-4" Pop 22

Fe 26

+31 10" Pop 21

Fe 27

Fe 25

+16 8" Will 14
 +02 Ent.
 Fe 27
 +97-Twin 10" Will - 19

+58-12" Pop 24
 +30-6" Pop 22

Fe 23

+72 6" Pop 22
 +65-Twin Will 19

+42-10" Pop 21

+18-6" Pop 21
 Fe 27

Fe 22



10 9

48 10 10

47 10 9

46 10 10

45 11 10

44 11 10 Lake 120

43 11 10 Lake 76

42 29 16 4 Lake 41

Fe 29

+08-8"Pop 24
Fe 29

+81-4"Pop-25

Fe 29

+10-4"E/m 21

+07-4"E/m 21

Fe 29

+95-4"E/m 23

Fe 29
+92-8"Pop 21

+63-2"Pop 25

+41-2"Pop 25

+17-2"Pop 25

Fe 29

+91-2"Pop 25

+79-2"Pop 25

+63-2"Pop 25

+48-2"Pop 25

+34-2"Pop 25

+20-12"Pop-24

Fe 29

+91-12"Pop-24

+78 Ent.

+53-8"Pop-27

Fe 33

Hay Field

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

Fe 25 (17)

+67 Ent.

+61 Rge Tie Ent

+48-4"Pop 23

Fe 26

+78-12"Pop 23

+55-12"Pop-2

+30 12"Pop 23

Fe 27

+45-4"Pop 23

+19-8"E/m 23

Fe 27

+89-6"Pop 23

+63-4"Pop 24

+36-6"Pop 24

+10-10"Pop 24

Fe 28

+87-6"Pop 24

+63-6"Pop 24

+40-12"Pop 24

+16-8"Pop 24

Fe 28

Fe 30

+58-6"Ash-2

+51-10"Will-2

+43-10"Will-2

+40-18"Pop 30

+38-12"Will-2

+25-6"Ash-2

+02 12"Pop 28

Fe 33

30

9 9

9 9

55 10 10

+50 10 10

54 10 12

+50 10 13

53 10 10

52 10 10

51 10 10

18 + 29- 12" Vit x 33' Vit x Cu/u 15

50 11 9

49 30 1/2 10 9

Fc 19

Fc 22 (18)

Pot hole

+50 Fc 20

+57-8" Pop-18
 +50-Fc-24
 +42-6" Oak 23

+100 Fc 32
 +100 Elm - 30

Wooded

Fc 32

+50 Fc 42

+73-12" Ash 32

+50 Fc 36

Fc 33

Fc 37

+64 4" Oak - 22
 +50 Fc 30

#50 Fc 30

Fc 30

+17-3" Pop 23

Fc 26
 +95- Pop - 23

+72-8" Pop 23

+66-2" Pop 25

+21-6" Pop 26

+30 Ent

+22 12" Pop-22

Fc 30

Fc-26

+96 10" Pop-23

+80 4" Will-26

+71 4" Will-22

+28-8" Pop-26

+46-4" Will-22

+30-4" Willow 22

Fc 29

Fc 26

+96 3" Willow 22

+76-3" Willow 22

+62 10" Pop 26

+34 6" Pop 22

Fc 29

+03 8" Pop 22
 Fc 26

+71 6" Pop-23

Fc 29

Fc 25

30A

11 10

62

11

12

+50

4 - 24

+25

11 - 33

61

12 - 35

+75

3 - 27

+50

5

22

60

11

15

59

9

12

+50

10

10

58

10

10

+50

11

8

57

22

+19- 24" x 36" Vit X Cult.

10

9

14

56

9

9

Fe 15

Fe 20 (19)

+22-12"Will-16

Fe 15

+50 Fe 8

Swamp

+75-Fe 5

+50 Fe 14

Fe 22

+81-6"Pop 25

+59-14"Pop 23

+07-12"Pop-25

Fe 21
+92 4"Pop 28

+77-14"Pop 25

+50 Fe 19

Fe 19

+69-10"Pop 21

+60 Ent
+50 Fe 24

Fe 19

+52 8"Pop 21

+22-6"Pop 21

Fe 19

Hay Field

Swamp

+49 Twin 10"-16"
+36-12"Will-16
+27-12"Will-18

Fe 20

+50 Fe 37
+50 18"Willow 34

+25 Fe 1-49

Fe 5-60

+75 Fe-53

+50 Fe 40

+18-6"Pop 22
Fe-26
+97 6"Pop 21

Fe 24

Fe 22

+17 5"Pop-17
+10 Ent
Fe 20

+66-6"Pop 16
+50 Fe 20
+41-12"Pop 17

Fe 23

+87-5"Pop 20

+60 8"Pop 20

+10-6"Pop-18
Fe 22

69

12

12
+98 R tie Ho

+95 W.C. Ho 79'

68

12

10

+32 R tie Ho

+19 SW Co. Ho 88

67

12

11

66

11

10

65

10

10

64

10

11

63

15'

+03 & Drain

12" x 7

Burried & H. Gr.

Fe 19

Fe 42

(20)

+44 Ent.

Fe 18

124 12" Pop 21

Fe 42

+83 - 12" Will 19

+71 - 12" Will 15

+43 - 12" Will 16

Fe 18

Fe 35

+55 12" Oak 25

+50 12" Oak 25

Fe 17

Fe 26

+62 - Twin Will 18

+51 14" Will 17

+39 12" Will 17

+27 12" Will 18

+20 12" Will 16

+08 12" Will 16

Fe 26

+78 8" Will 18

+74 18" Will 18

+40 - 18" Will 17

Fe 23

Fe 23

Fe 20

30C

Swamp

4-1-70
Heavy Woods+64
244

Swamp

Swamp

Fe 16

+76 12" Will 16

+85 12" Will 16

+32 12" Will 15

+10 12" Will 13

Fe 12

Fe 14

+79 10" Will 15

+69 10" Will 15

+44 10" Will 15

Fe 15

75

74

11 11

73

11 12

+50 11 12

72

13 11

+50 12 12

71

12 12

70

13 13

+20 End Rad. 12

Rad. = 16'

+71 Beg. Rad. 43

+50 End Rad. 41

+36 Beg. Rad. 12

+33 Fe Cor. 31

Fe 36

Fe 39

Fe 23

+76 Ent.

Fe 45

Fe 21

+50 Fe 23

+50 Fe 27

Fe 25

Fe 39

+50 Fe 21

+50 Fe 46

Fe 19

+16 12" P. 25'
+09 14" P. 24'
Fe 45

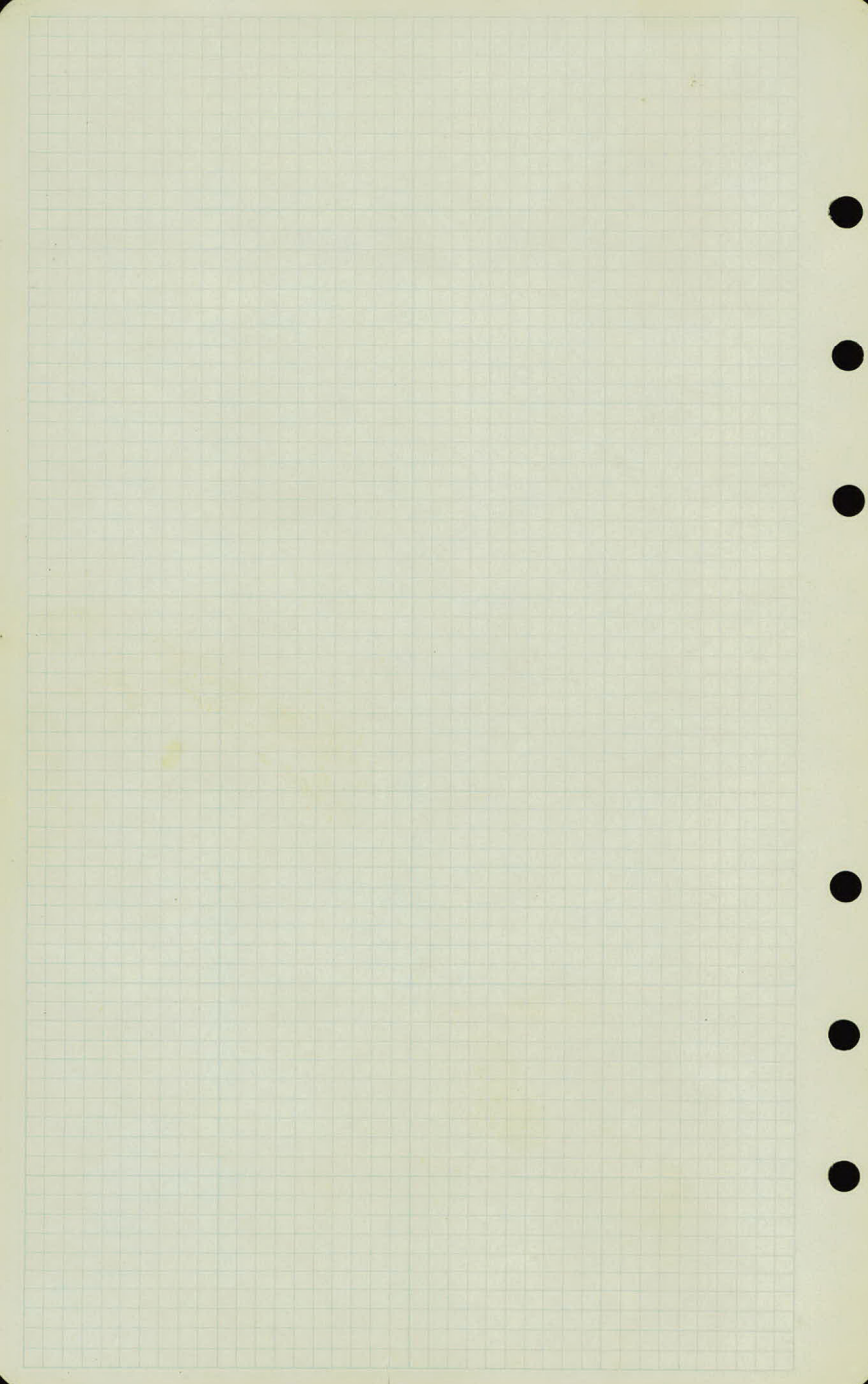
+41-30" Oak 18

Fe 19

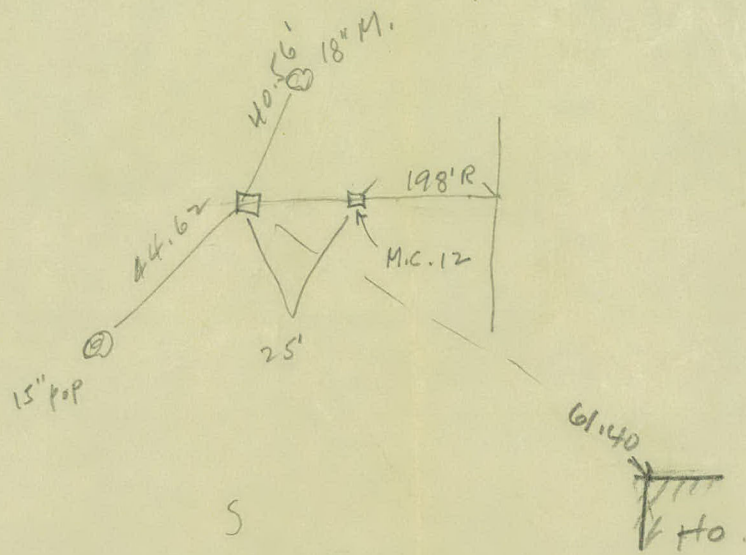
Fe 42

Uncultivated

Wooded

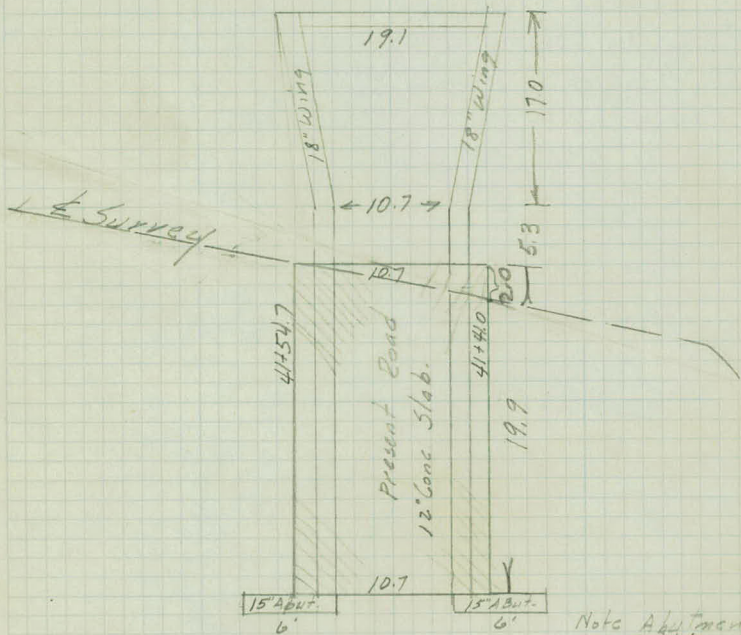


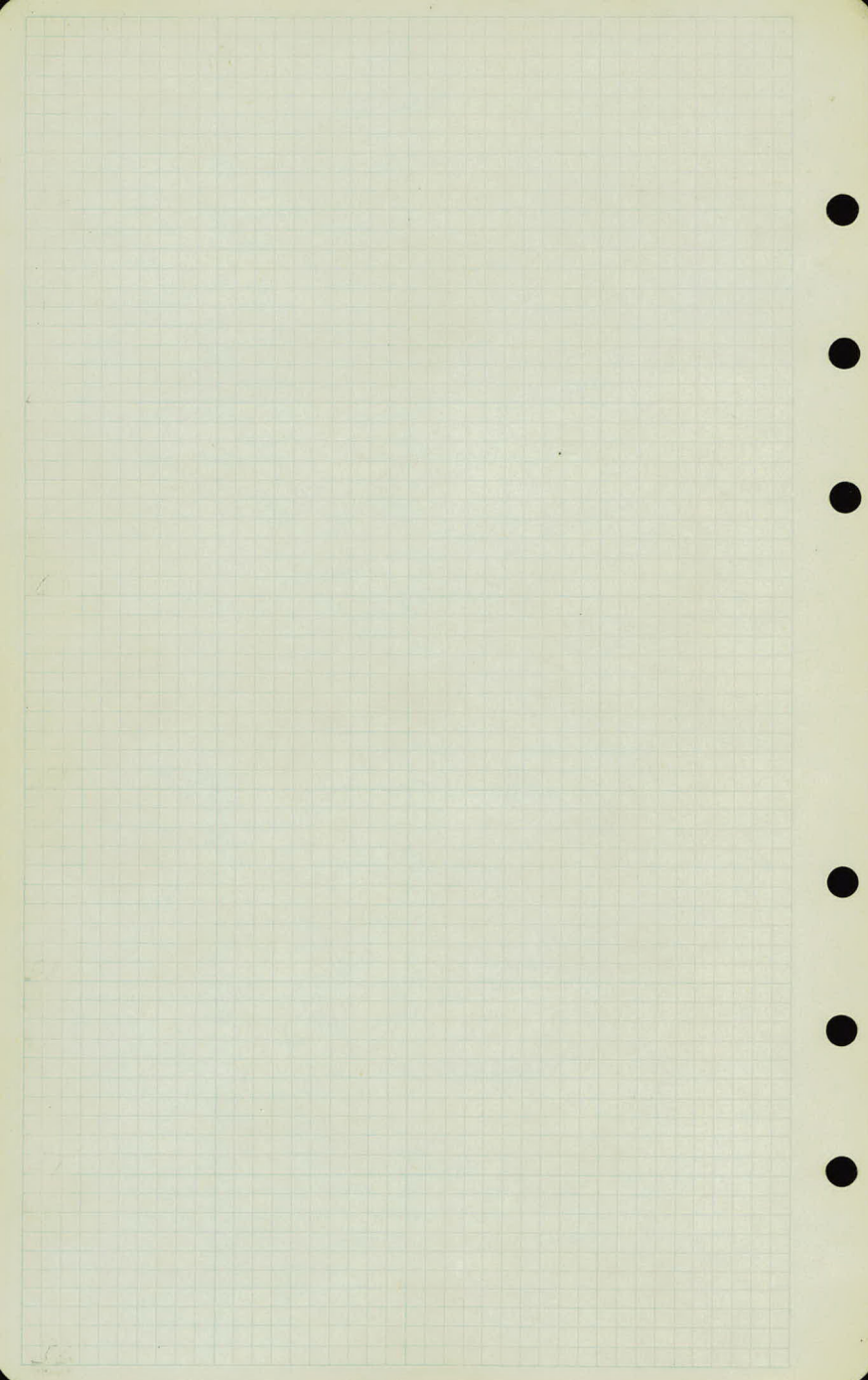
N



S

Detail of Spillway





Bald Eagle Blvd W.

Bench Levels

P/	+	π	-	Elev
B.M.	8.01	918.71.		910.70.
T.P.	4.46	918.76.	4.41	914.30.
T.P.	5.62	920.18.	4.20	914.56.
T.P.	4.36	919.73.	4.81	915.37.
B.M.	4.06	919.73.	4.06	915.67.
T.P.	6.23	919.66.	6.30	913.43.
T.P.	5.90	921.39	4.17	915.49
T.P.	10.00	930.37.	1.02	920.37.
T.P.	3.51	930.55.	3.33	927.04.
B.M.			5.16	925.39.
B.M.	7.89	918.59.		910.70
T.P.	4.38	919.20	3.77	914.82
T.P.	9.29	925.05	3.44	915.76
B.M.	4.35	920.78	8.62	916.43
T.P.	7.33	920.44	7.67	913.11
T.P.	10.58	930.14	0.88	919.56
B.M.			1.30	928.84.

Top S.E. Cor. Spillway 41+41.0

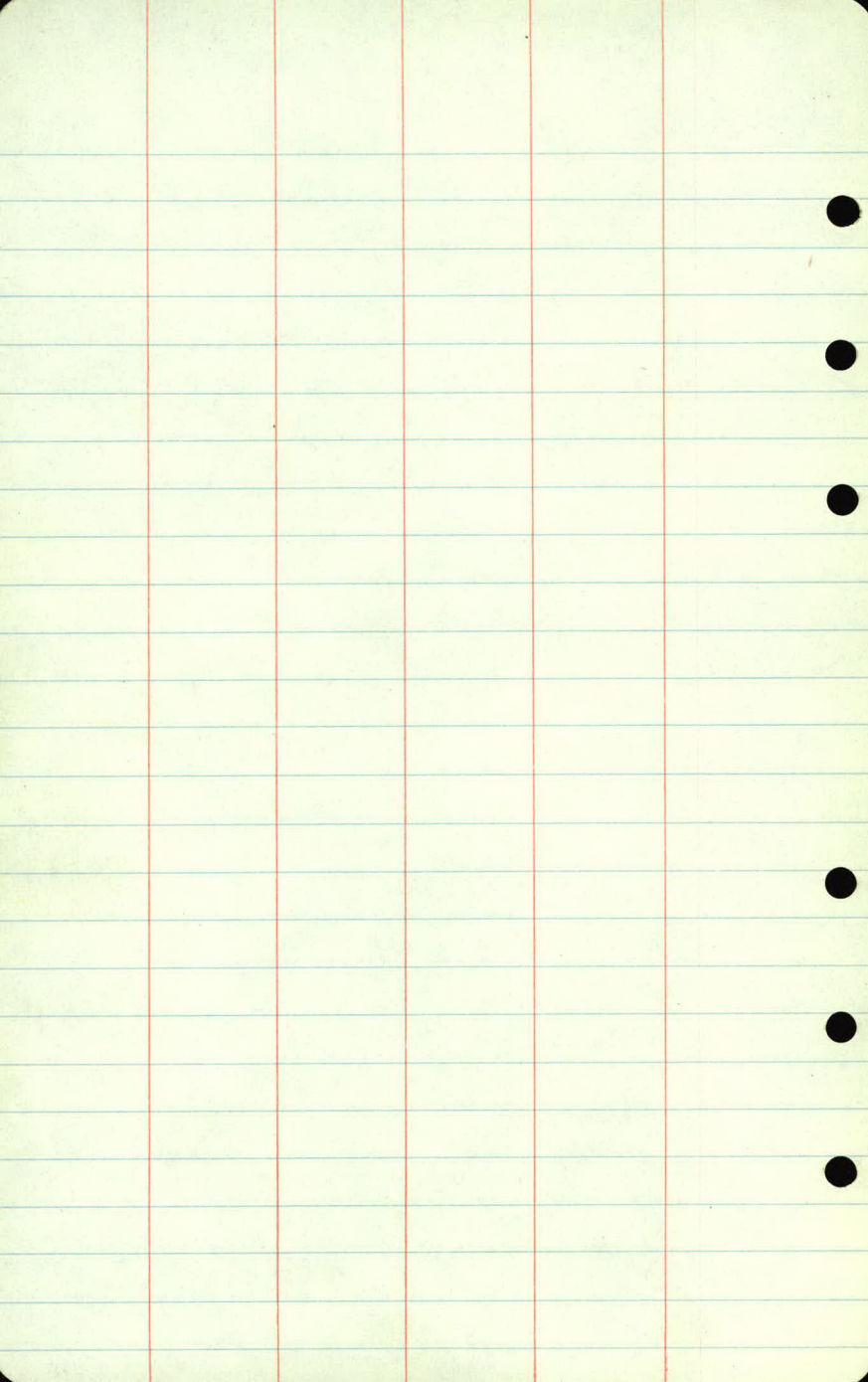
Top Water Table S.W. Cor. Garage 100' Rt 23+00

Spike in 12" Oak 22' Rt Sta 0+35

Top S.E. Cor. Spillway 41+41.0

Spike in 12" Pop 18' Lt 57+70

Spike in 18" Oak S.W. Cor. H. Co. Line E.B. E Blus.



Bald Eagle Blvd. W.

Cross Sections

Sta.	+	π	-	Elev
B.M.	5.16	930.55		925.39
0+00			4.8	25.8
+40			5.1	25.5
+56			5.1	25.5
1			5.0	25.6
+50			4.8	25.8
2			4.6	26.0
+50			4.1	26.5
3			3.6	27.0
+50			3.4	27.2
4			3.2	27.4
T.P.	4.12	931.52.	3.15	927.40.
+50			4.2	27.3
5			4.2	27.3

Spike in 12" Oak 22' Rd 0+35

$\frac{6.5}{50}$ 4.8 $\frac{4.9}{11}$ $\frac{5.6}{14}$ $\frac{15.5}{31}$ $\frac{16.4}{56}$ $\frac{19.7}{63}$

$\frac{7.0}{50}$ $\frac{6.9}{30}$ $\frac{5.9}{16}$ 5.1 $\frac{5.4}{16}$ $\frac{15.4}{35}$ $\frac{16.0}{58}$ $\frac{19.7}{64}$

$\frac{5.4}{50}$ $\frac{5.5}{23}$ $\frac{6.3}{17-15}$ $\frac{5.5}{11}$ 5.1 $\frac{5.4}{13}$ $\frac{6.3}{19}$ $\frac{15.2}{37}$ $\frac{16.0}{61}$ $\frac{19.7}{65}$

$\frac{4.7}{50}$ $\frac{5.4}{24}$ $\frac{5.7}{14}$ $\frac{5.3}{8}$ 5.0 $\frac{5.5}{14}$ $\frac{7.0}{21}$ $\frac{15.3}{37}$ $\frac{16.2}{58}$ $\frac{19.7}{65}$

$\frac{4.3}{50}$ $\frac{5.1}{23}$ $\frac{5.3}{11}$ 4.8 $\frac{5.3}{14}$ $\frac{15.3}{36}$ $\frac{17.3}{57}$ $\frac{19.7}{72}$

$\frac{3.7}{50}$ $\frac{4.4}{23}$ $\frac{4.8}{11}$ 4.6 $\frac{5.2}{20}$ $\frac{15.4}{36}$ $\frac{17.0}{68}$ $\frac{19.7}{72}$

$\frac{3.1}{50}$ $\frac{3.7}{18}$ $\frac{4.5}{12}$ 4.1 $\frac{4.4}{10}$ $\frac{3.7}{13-16}$ $\frac{15.6}{37}$ $\frac{16.6}{69}$ $\frac{19.7}{74}$

$\frac{3.7}{50}$ $\frac{2.8}{20}$ $\frac{3.7}{13}$ 3.6 $\frac{4.1}{17}$ $\frac{15.3}{35}$ $\frac{16.7}{59}$ $\frac{19.7}{67}$

$\frac{1.6}{50}$ $\frac{1.7}{20}$ $\frac{3.6}{14}$ 3.4 $\frac{3.7}{14}$ $\frac{3.9}{16}$ $\frac{15.4}{35}$ $\frac{16.7}{62}$ $\frac{19.7}{67}$

$\frac{1.6}{50}$ $\frac{2.2}{20}$ $\frac{2.9}{17}$ $\frac{3.3}{11}$ 3.2 $\frac{4.0}{15}$ $\frac{15.7}{35}$ $\frac{16.6}{68}$ $\frac{19.7}{70}$

$\frac{2.5}{50}$ $\frac{3.2}{19}$ $\frac{4.3}{9}$ 4.2 $\frac{4.8}{16}$ $\frac{17.1}{36}$ $\frac{17.6}{53}$ $\frac{20.6}{67}$

$\frac{2.7}{50}$ $\frac{3.1}{22}$ $\frac{4.5}{10}$ 4.2 $\frac{4.6}{10}$ $\frac{4.6}{18}$ $\frac{16.2}{36}$ $\frac{17.3}{54}$ $\frac{20.6}{58}$

104

Sta.	+	+	-	Elev
		931.52		
5+50			4.5	27.0
6			5.1	26.4
+50			5.7	25.8
7			5.9	25.6
+50			6.4	25.1
8			7.3	24.20
T.P.	2.82	926.49	7.85	923.67
+50			33	23.2
9			4.0	22.5
+50			5.5	21.0
10			7.0	19.5
+50			8.1	18.4
+ 63		24' culv.	8.4	18.1
T.P.	3.72	921.21	9.00	917.49

$$\begin{array}{r} 2.8 \quad 3.5 \quad 4.8 \\ 50 \quad 22 \quad 11 \end{array} \quad \begin{array}{r} 4.8 \quad 4.4 \quad 16.4 \quad 17.7 \quad 20.6 \\ 11 \quad 20 \quad 39 \quad 58 \quad 63 \end{array}$$

$$\begin{array}{r} 3.5 \quad 4.3 \quad 5.3 \\ 50 \quad 21 \quad 14 \end{array} \quad \begin{array}{r} 5.4 \quad 4.8 \quad 7.5 \quad 16.4 \quad 17.3 \quad 20.6 \\ 12 \quad 16 \quad 25 \quad 37 \quad 58 \quad 61 \end{array}$$

$$\begin{array}{r} 4.3 \quad 4.8 \quad 6.0 \quad 5.8 \\ 50 \quad 21 \quad 18 \quad 11 \end{array} \quad \begin{array}{r} 6.2 \quad 16.8 \quad 17.0 \quad 20.6 \\ 15 \quad 36 \quad 57 \quad 67 \end{array}$$

$$\begin{array}{r} 4.7 \quad 5.0 \quad 6.4 \quad 6.3 \\ 50 \quad 22 \quad 17 \quad 11 \end{array} \quad \begin{array}{r} 6.3 \quad 5.4 \quad 17.2 \quad 17.4 \quad 20.6 \\ 12 \quad 18 \quad 39 \quad 58 \quad 64 \end{array}$$

$$\begin{array}{r} 4.8 \quad 5.9 \quad 7.0 \\ 50 \quad 18 \quad 11 \end{array} \quad \begin{array}{r} 6.4 \quad 6.8 \quad 5.3 \quad 8.4 \quad 17.2 \quad 17.4 \quad 20.6 \\ 11 \quad 20 \quad 25 \quad 32 \quad 60 \quad 68 \end{array}$$

$$\begin{array}{r} 5.1 \quad 7.4 \quad 7.8 \\ 50 \quad 14 \quad 11 \end{array} \quad \begin{array}{r} 7.3 \quad 7.6 \quad 6.0 \quad 18.1 \quad 17.4 \quad 20.6 \\ 12 \quad 19 \quad 39 \quad 64 \quad 72 \end{array}$$

$$\begin{array}{r} 1.3 \quad 2.9 \quad 3.7 \\ 50 \quad 17 \quad 11 \end{array} \quad \begin{array}{r} 3.3 \quad 3.1 \quad 3.3 \quad 12.4 \quad 12.3 \quad 15.6 \\ 15 \quad 17 \quad 20 \quad 35 \quad 75 \quad 78 \end{array}$$

$$\begin{array}{r} 3.2 \quad 3.6 \quad 4.0 \quad 4.7 \\ 50 \quad 31 \quad 17 \quad 11 \end{array} \quad \begin{array}{r} 4.0 \quad 4.4 \quad 12.2 \quad 12.9 \quad 15.6 \\ 17 \quad 28 \quad 86 \quad 93 \end{array}$$

$$\begin{array}{r} 6.8 \quad 6.2 \quad 6.6 \quad 5.8 \\ 50 \quad 23 \quad 20 \quad 9 \end{array} \quad \begin{array}{r} 5.5 \quad 6.0 \quad 11.5 \quad 13.4 \\ 12 \quad 26 \quad 50 \end{array}$$

$$\begin{array}{r} 10.7 \quad 8.5 \quad 7.3 \\ 50 \quad 14 \quad 11 \end{array} \quad \begin{array}{r} 7.0 \quad 7.4 \quad 13.4 \quad 13.8 \\ 13 \quad 34 \quad 50 \end{array}$$

$$\begin{array}{r} 10.6 \quad 10.5 \quad 9.2 \quad 8.2 \\ 50 \quad 26 \quad 16 \quad 11 \end{array} \quad \begin{array}{r} 8.1 \quad 8.8 \quad 7.6 \quad 13.2 \quad 13.8 \\ 11 \quad 15 \quad 25 \quad 50 \end{array}$$

$$\begin{array}{r} 14.7 \quad 15.0 \quad \text{FL.} \\ 50 \quad 28 \quad (15.5) \end{array} \quad \begin{array}{r} 8.6 \quad 9.1 \quad \text{FL.} \\ (28) \quad 12 \quad 8.4 \quad 13 \quad (15.7) \end{array} \quad \begin{array}{r} 5.1 \quad 14.8 \quad 13.6 \\ 22 \quad 29 \quad 50 \end{array}$$

Sta.	+	π	-	Elev.
		921.21		
11			3.7	17.5
+50			4.2	17.0
12			4.6	16.6
+50			5.0	16.2
13			5.2	16.0
+50			5.3	15.9
14			5.3	15.9
+50			5.4	15.8
15 +97	12" Culv		5.7	15.5
15			5.7	15.5
T.P.	4.95	920.20	5.96	915.25
+50			4.8	15.4
16			4.8	15.4

$\frac{9.4}{50}$ $\frac{10.5}{42}$ $\frac{9.6}{26}$ $\frac{4.0}{10}$ 37 $\frac{4.3}{12}$ $\frac{6.4}{79}$ $\frac{8.5}{34}$ $\frac{8.7}{50}$

$\frac{10.2}{50}$ $\frac{8.8}{34}$ $\frac{7.8}{23}$ $\frac{5.6}{15}$ $\frac{4.5}{9}$ 4.2 $\frac{4.8}{12}$ $\frac{7.4}{20}$ $\frac{8.6}{40}$ $\frac{8.8}{50}$

$\frac{8.2}{50}$ $\frac{6.0}{20}$ $\frac{4.8}{10}$ 4.6 $\frac{5.1}{8}$ $\frac{6.1}{15}$ $\frac{8.3}{26}$ $\frac{8.7}{50}$

$\frac{6.1}{50}$ $\frac{5.5}{29}$ $\frac{5.2}{13}$ 50 $\frac{5.1}{9}$ $\frac{5.8}{16}$ $\frac{8.2}{27}$ $\frac{8.7}{50}$

$\frac{4.9}{50}$ $\frac{5.2}{16}$ $\frac{5.8}{13-11}$ 5.2 $\frac{5.6}{15}$ $\frac{8.2}{22}$ $\frac{8.5}{50}$

$\frac{4.0}{50}$ $\frac{5.4}{15}$ $\frac{6.1}{12-10}$ 5.3 $\frac{5.6}{23}$ $\frac{7.7}{31}$ $\frac{8.3}{50}$

$\frac{5.3}{50}$ $\frac{5.3}{31}$ $\frac{4.7}{22}$ $\frac{5.5}{14}$ $\frac{6.1}{10}$ 5.3 $\frac{5.5}{17}$ $\frac{4.9}{20}$ $\frac{4.5}{33}$ $\frac{5.4}{38}$ $\frac{7.4}{45}$ $\frac{7.8}{50}$

$\frac{7.3}{50}$ $\frac{6.6}{27}$ $\frac{6.7}{19}$ $\frac{5.9}{11}$ 5.4 $\frac{5.7}{12}$ $\frac{6.1}{18}$ 5.3 $\frac{5.1}{50}$

$\frac{10.4}{150}$ $\frac{10.2}{125}$ $\frac{9.9}{100}$ $\frac{9.9}{75}$ $\frac{9.8}{50}$ $\frac{9.5}{28}$ $\frac{9.8}{17}$ $\frac{9.7}{17}$ $\frac{4.3}{11}$ 5.7 $\frac{6.4}{13}$ $\frac{9.3}{16}$ $\frac{8.7}{29}$ $\frac{6.9}{42}$ $\frac{5.0}{50}$

$\frac{9.4}{50}$ $\frac{9.2}{27}$ $\frac{8.5}{16}$ $\frac{4.3}{11}$ 5.7 $\frac{6.2}{13}$ $\frac{7.4}{15}$ $\frac{6.9}{16}$ $\frac{6.6}{28}$ $\frac{5.0}{50}$

$\frac{9.0}{50}$ $\frac{7.7}{28}$ $\frac{7.2}{17}$ $\frac{5.4}{11}$ 4.8 $\frac{5.2}{12}$ $\frac{5.6}{19}$ $\frac{4.8}{29}$ $\frac{4.3}{41}$ $\frac{3.1}{50}$

$\frac{8.8}{50}$ $\frac{7.3}{28}$ $\frac{6.6}{17}$ $\frac{5.2}{11}$ 4.8 $\frac{5.1}{11}$ $\frac{4.8}{19}$ $\frac{4.5}{29}$ $\frac{4.2}{50}$

Sta	L	↑	-	Elev.
		920.20		
16+50			4.7	15.5
17			4.8	15.4
+50			5.0	15.2
18			5.7	14.5
+50			7.4	12.8
19			7.7	12.5
+50			8.1	12.1
20			7.8	12.4
+50			7.1	13.1
T.P.	6.04	918.33	7.91	912.29
21			5.0	13.3
+109	12" Cul v.		5.0	13.3
+50			4.9	13.4

$\frac{8.2}{50}$ $\frac{5.7}{28}$ $\frac{5.8}{24}$ $\frac{6.5}{20-17}$ $\frac{5.2}{12}$ 4.7 $\frac{5.0}{11}$ $\frac{4.5}{30}$ $\frac{4.4}{50}$

$\frac{7.4}{50}$ $\frac{5.3}{27}$ $\frac{6.7}{22-19}$ $\frac{5.0}{12}$ 4.8 $\frac{5.2}{9}$ $\frac{5.3}{15}$ $\frac{5.0}{32}$ $\frac{4.6}{50}$

$\frac{5.7}{50}$ $\frac{4.4}{28}$ $\frac{6.5}{23-17}$ $\frac{5.5}{11}$ 5.0 $\frac{5.4}{10}$ $\frac{5.9}{15}$ $\frac{4.7}{27}$ $\frac{5.7}{41}$ $\frac{5.4}{50}$

$\frac{6.0}{50}$ $\frac{7.4}{29}$ $\frac{7.8}{17}$ $\frac{6.2}{11}$ 5.7 $\frac{6.0}{11}$ $\frac{8.4}{16}$ $\frac{8.5}{30}$ $\frac{7.8}{50}$

$\frac{8.4}{50}$ $\frac{9.0}{29}$ $\frac{8.9}{15}$ $\frac{7.5}{12}$ 7.4 $\frac{8.2}{11}$ $\frac{10.4}{15}$ $\frac{10.9}{20}$ $\frac{11.5}{29}$ $\frac{10.1}{43}$ $\frac{9.3}{50}$

$\frac{9.4}{50}$ $\frac{11.2}{29}$ $\frac{10.8}{21}$ $\frac{10.5}{15}$ $\frac{8.0}{11}$ 7.7 $\frac{8.8}{11}$ $\frac{10.8}{14}$ $\frac{11.9}{19}$ $\frac{11.8}{22}$ $\frac{11.0}{31}$ $\frac{10.6}{35}$ $\frac{9.6}{50}$

$\frac{10.5}{50}$ $\frac{11.4}{30}$ $\frac{11.5}{21}$ $\frac{11.0}{15}$ $\frac{8.6}{11}$ 8.1 $\frac{8.5}{11}$ $\frac{10.7}{15}$ $\frac{11.8}{20}$ $\frac{13.0}{28}$ $\frac{12.2}{30}$ $\frac{10.5}{40}$ $\frac{10.4}{50}$

$\frac{9.8}{50}$ $\frac{11.5}{30}$ $\frac{10.8}{14}$ $\frac{8.2}{11}$ 7.8 $\frac{8.3}{8}$ $\frac{8.6}{12}$ $\frac{10.1}{16}$ $\frac{11.5}{23}$ $\frac{12.2}{31}$ $\frac{11.1}{35}$ $\frac{10.0}{50}$

$\frac{9.5}{50}$ $\frac{9.5}{30}$ $\frac{10.4}{27}$ $\frac{9.4}{15}$ $\frac{7.7}{13}$ 7.1 $\frac{7.3}{11}$ $\frac{9.7}{17}$ $\frac{10.0}{23}$ $\frac{9.4}{33}$ $\frac{9.2}{50}$

$\frac{7.7}{50}$ $\frac{8.2}{31}$ $\frac{9.0}{29-28}$ $\frac{7.9}{15}$ $\frac{5.2}{10}$ 5.0 $\frac{4.9}{10}$ $\frac{7.2}{15}$ $\frac{6.4}{33}$ $\frac{6.4}{50}$

Ditch $\frac{8.8}{100}$ $\frac{9.1}{75}$ $\frac{9.0}{50}$ $\frac{9.2}{35}$ $\frac{8.5}{21}$ $\frac{8.1}{13}$ F.L. $\frac{9.0}{12}$ $\frac{5.4}{10}$ 5.0 $\frac{5.0}{13}$ $\frac{8.5}{20}$ $\frac{8.6}{20}$ $\frac{8.2}{26}$ $\frac{7.9}{43}$ Ditch $\frac{8.1}{50}$ $\frac{7.9}{75}$ $\frac{8.6}{100}$

$\frac{7.8}{50}$ $\frac{7.7}{30}$ $\frac{9.1}{28-26}$ $\frac{7.9}{25}$ $\frac{7.9}{16}$ $\frac{5.1}{10}$ 4.9 $\frac{4.9}{12}$ $\frac{7.2}{18}$ $\frac{6.9}{25}$ $\frac{6.9}{34}$ $\frac{6.7}{50}$

Sta	+	π	-	Elev.
		918.33		
22			4.6	13.7
+50			4.4	13.9
23			4.0	14.3
B.M.	4.15	919.82	2.62	915.71
+50			5.2	14.6
24			4.8	15.0
+50			4.8	15.0
25			4.5	15.3
+50			4.7	15.1
26			5.3	14.5
+50			5.0	14.8
27			4.4	15.4
T.P.	4.60	920.22	4.20	915.62
+50			4.0	16.2

915.67

$\frac{8.3}{50}$ $\frac{7.7}{45}$ $\frac{7.7}{31}$ $\frac{9.4}{29}$ $\frac{8.1}{28}$ $\frac{4.8}{17}$ $\frac{4.6}{10}$ $\frac{5.2}{11}$ $\frac{7.1}{17}$ $\frac{6.9}{34}$ $\frac{6.6}{50}$

$\frac{7.9}{50}$ $\frac{8.2}{35}$ $\frac{8.6}{33}$ $\frac{7.8}{32}$ $\frac{4.9}{19}$ $\frac{4.4}{10}$ $\frac{4.9}{11}$ $\frac{7.0}{16}$ $\frac{6.5}{30}$ $\frac{5.5}{50}$

$\frac{7.4}{50}$ $\frac{8.2}{30}$ $\frac{7.9}{17}$ $\frac{4.7}{10}$ $\frac{4.0}{4.0}$ $\frac{4.5}{11}$ $\frac{7.0}{16}$ $\frac{6.2}{32}$ $\frac{5.9}{50}$

s.w.
Top Water table Garage 100' Rt Sta. 23.

$\frac{8.2}{50}$ $\frac{7.9}{31}$ $\frac{7.9}{15}$ $\frac{5.9}{11}$ $\frac{5.2}{5.2}$ $\frac{5.5}{10}$ $\frac{7.7}{16}$ $\frac{7.8}{20}$ $\frac{7.3}{23}$ $\frac{7.7}{31}$ $\frac{7.6}{50}$

$\frac{8.6}{50}$ $\frac{8.2}{31}$ $\frac{7.5}{16}$ $\frac{5.4}{10}$ $\frac{4.8}{4.8}$ $\frac{5.1}{11}$ $\frac{6.3}{15}$ $\frac{6.0}{30}$ $\frac{6.6}{50}$

$\frac{8.9}{50}$ $\frac{8.0}{32}$ $\frac{7.7}{16}$ $\frac{5.1}{10}$ $\frac{4.8}{4.8}$ $\frac{5.3}{11}$ $\frac{6.3}{15}$ $\frac{6.3}{18}$ $\frac{4.9}{21}$ $\frac{4.4}{29}$ $\frac{4.9}{50}$

$\frac{8.6}{50}$ $\frac{7.8}{32}$ $\frac{7.5}{15}$ $\frac{5.2}{10}$ $\frac{4.5}{4.5}$ $\frac{4.9}{10}$ $\frac{5.9}{15}$ $\frac{6.0}{18}$ $\frac{4.9}{28}$ $\frac{3.7}{50}$

$\frac{9.7}{50}$ $\frac{8.7}{32}$ $\frac{8.1}{16}$ $\frac{5.4}{10}$ $\frac{4.7}{4.7}$ $\frac{5.0}{10}$ $\frac{7.1}{17}$ $\frac{7.0}{26}$ $\frac{7.0}{50}$

$\frac{9.3}{50}$ $\frac{10.0}{33}$ $\frac{9.3}{18}$ $\frac{6.0}{11}$ $\frac{5.3}{5.3}$ $\frac{5.4}{10}$ $\frac{7.9}{17}$ $\frac{8.0}{25}$ $\frac{7.7}{50}$

$\frac{7.5}{50}$ $\frac{7.8}{34}$ $\frac{7.7}{16}$ $\frac{5.1}{10}$ $\frac{5.0}{5.0}$ $\frac{5.4}{11}$ $\frac{8.1}{18}$ $\frac{8.3}{24}$ $\frac{8.4}{50}$

$\frac{5.5}{50}$ $\frac{5.4}{29}$ $\frac{5.3}{15}$ $\frac{4.3}{11}$ $\frac{4.4}{4.4}$ $\frac{5.1}{11}$ $\frac{5.4}{15}$ $\frac{7.3}{30}$ $\frac{7.4}{50}$

$\frac{2.0}{50}$ $\frac{2.9}{24}$ $\frac{4.0}{4.0}$ $\frac{4.6}{19}$ $\frac{5.5}{50}$

Sta	+	π	-	Elev.
		920.22		
28			4.6	15.6
+50			4.9	15.3
29			5.2	15.0
+50			5.2	15.0
30			5.4	14.8
+50			5.2	15.0
31			5.4	14.8
+21			5.6	14.6
+44			5.9	14.3
32			6.3	13.9
+50			5.9	14.3
33			5.7	14.5
B.M.			3.65	916.57

$\frac{1.0}{20}$ $\frac{4.8}{19}$ $\frac{5.0}{12}$ $\frac{4.7}{16}$ 4.6 $\frac{4.9}{19}$ $\frac{5.3}{32}$ $\frac{5.8}{50}$

$\frac{4.2}{27}$ $\frac{5.2}{15}$ 4.9 $\frac{5.2}{14}$ $\frac{6.0}{32}$ $\frac{7.5}{39}$ $\frac{8.6}{50}$

$\frac{5.0}{26}$ $\frac{5.6}{15}$ 5.2 $\frac{5.5}{11}$ $\frac{7.8}{23}$ $\frac{8.2}{31}$ $\frac{8.7}{50}$

$\frac{5.5}{26}$ $\frac{5.9}{11}$ 5.2 $\frac{5.4}{11}$ $\frac{7.5}{16}$ $\frac{7.5}{21}$ $\frac{7.3}{30}$ $\frac{7.3}{50}$

$\frac{4.0}{16}$ $\frac{6.0}{11}$ 5.4 $\frac{5.3}{15}$ $\frac{7.9}{22}$ $\frac{7.4}{39}$ $\frac{7.0}{50}$

$\frac{4.9}{17}$ $\frac{5.8}{13}$ 5.2 $\frac{5.2}{14}$ $\frac{6.9}{18}$ $\frac{7.3}{25}$ $\frac{6.6}{50}$

$\frac{4.8}{23}$ $\frac{5.6}{18}$ 5.4 $\frac{5.7}{8}$ $\frac{7.4}{11}$ $\frac{7.8}{19}$ $\frac{7.4}{50}$

$\frac{5.1}{27}$ $\frac{5.6}{21}$ 5.6 $\frac{6.0}{50}$ $\frac{7.7}{8}$ $\frac{8.3}{11}$ $\frac{8.5}{15}$ $\frac{8.0}{50}$

$\frac{2.0}{50}$ $\frac{4.8}{38}$ $\frac{5.5}{33}$ $\frac{5.8}{25}$ $\frac{5.4}{12}$ 5.9 $\frac{6.1}{2}$ $\frac{7.8}{6}$ $\frac{8.0}{9}$ $\frac{8.1}{16}$ $\frac{7.3}{50}$

$\frac{4.8}{50}$ $\frac{6.0}{39}$ $\frac{5.9}{29}$ $\frac{5.5}{12}$ 6.3 $\frac{6.3}{2}$ $\frac{8.0}{5}$ $\frac{8.5}{11}$ $\frac{8.2}{18}$ $\frac{8.2}{50}$

$\frac{0.9}{45}$ $\frac{5.6}{30}$ $\frac{5.9}{26}$ $\frac{5.5}{11}$ 5.9 $\frac{6.3}{5}$ $\frac{8.2}{10}$ $\frac{8.5}{14}$ $\frac{7.9}{28}$ $\frac{7.9}{50}$

$\frac{3.1}{27}$ $\frac{5.4}{19}$ $\frac{6.1}{16}$ 5.7 $\frac{6.2}{12}$ $\frac{7.5}{16}$ $\frac{8.2}{27}$ $\frac{8.2}{50}$

Spikes in 12" Willow - 20' Lt. 33 + 25

Sta	+	π	-	Elev.
		920.22		
T.P.	13.74	933.18	0.78	919.44
28				15.6
	+50			15.3
29				15.0
	+50			15.0
30				14.8
	+50			15.0
31				14.8
	+21			14.6
T.P.	7.44	940.16	0.46	932.72
32 + 50				14.3
33				14.5
	+50			14.6
T.P.	0.21	927.18	13.19	926.97
34 + 75				14.6
B.M.	3.03	919.60	10.63	916.55 (916.57)

£

$$\begin{array}{r} 4.8 \\ 75 \end{array} \quad \begin{array}{r} 8.0 \\ 36 \end{array} \quad (17.6)$$

$$\begin{array}{r} 1.9 \\ 75 \end{array} \quad \begin{array}{r} 4.1 \\ 54 \end{array} \quad \begin{array}{r} 6.6 \\ 40 \end{array} \quad (17.9)$$

$$\begin{array}{r} 1.6 \\ 75 \end{array} \quad \begin{array}{r} 4.1 \\ 51 \end{array} \quad \begin{array}{c} \text{Tree} \\ \begin{array}{r} 7.5 \\ 49 \end{array} \end{array} \quad \begin{array}{r} 7.5 \\ 40 \end{array} \quad (18.2)$$

$$\begin{array}{r} 1.3 \\ 75 \end{array} \quad \begin{array}{r} 3.3 \\ 39 \end{array} \quad \begin{array}{c} \text{Tree} \\ \begin{array}{r} 4.8 \\ 37 \end{array} \end{array} \quad \begin{array}{r} 6.3 \\ 33 \end{array} \quad (18.2)$$

$$\begin{array}{r} 2.2 \\ 75 \end{array} \quad \begin{array}{r} 3.6 \\ 36 \end{array} \quad \begin{array}{r} 4.6 \\ 35 \end{array} \quad \begin{array}{r} 5.5 \\ 30 \end{array} \quad (18.4)$$

$$\begin{array}{r} 1.3 \\ 75 \end{array} \quad \begin{array}{r} 3.8 \\ 34 \end{array} \quad \begin{array}{r} 4.5 \\ 31 \end{array} \quad (18.2)$$

$$+ \begin{array}{r} 0.4 \\ 75 \end{array} \quad \begin{array}{r} 1.0 \\ 50 \end{array} \quad \begin{array}{r} 2.1 \\ 49 \end{array} \quad \begin{array}{r} 2.7 \\ 41 \end{array} \quad (18.4)$$

$$+ \begin{array}{r} 5.0 \\ 75 \end{array} \quad + \begin{array}{r} 3.2 \\ 63 \end{array} \quad + \begin{array}{r} 1.3 \\ 50 \end{array} \quad (18.6)$$

Top Rock Top

$$+ \begin{array}{r} 1.0 \\ 85 \end{array} \quad + \begin{array}{r} 0.4 \\ 73 \end{array} \quad (25.9)$$

$$\begin{array}{r} 5.9 \\ 75 \end{array} \quad \begin{array}{r} 6.6 \\ 66 \end{array} \quad \begin{array}{r} 7.2 \\ 43 \end{array} \quad (25.7)$$

$$\begin{array}{r} 13.7 \\ 45 \end{array} \quad \begin{array}{r} 14.3 \\ 50 \end{array} \quad \begin{array}{r} 14.6 \\ 32 \end{array} \quad (25.6)$$

$$\begin{array}{r} 3.4 \\ 75 \end{array} \quad \begin{array}{r} 4.6 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array} \quad (12.6)$$

Spoke in 12" Willow 20' Lt 33' + 25'

Sta	+	π	-	Elev.
		919.60		
33 + 50			5.0	14.6
34 + 75			5.0	14.6
34			5.0	14.6
+ 50			5.3	14.3
35			5.4	14.2
+ 50			5.3	14.3
36			5.2	14.4
+ 50			5.5	14.1
+ 95	12" Culv.		5.6	14.0
37			5.5	14.1
T.P.	5.13	918.80	5.93	913.67
+ 50			4.6	14.2
38			4.7	14.1

Lt

L

Rt

$\frac{4.0}{24}$ $\frac{5.2}{15}$ $\frac{5.6}{12}$ 5.0 $\frac{5.4}{14}$ $\frac{7.3}{19}$ $\frac{7.8}{26}$ $\frac{7.3}{50}$

$\frac{4.5}{20}$ $\frac{4.9}{14}$ $\frac{5.4}{11}$ 5.0 $\frac{5.4}{13}$ $\frac{6.8}{16-19}$ $\frac{7.5}{25}$ $\frac{7.5}{50}$

$\frac{3.2}{50}$ $\frac{3.2}{28}$ $\frac{4.4}{14}$ $\frac{5.3}{10}$ 5.0 $\frac{5.4}{14}$ $\frac{7.3}{19}$ $\frac{8.1}{29}$ $\frac{7.6}{38}$ $\frac{7.6}{50}$

$\frac{6.5}{50}$ $\frac{6.3}{34}$ $\frac{5.9}{27}$ $\frac{5.5}{14}$ $\frac{5.6}{11}$ 5.3 $\frac{5.9}{13}$ $\frac{7.3}{18}$ $\frac{8.8}{26}$ $\frac{8.8}{31}$ $\frac{9.0}{37}$ $\frac{8.8}{50}$

$\frac{9.3}{50}$ $\frac{8.3}{30}$ $\frac{7.8}{28}$ $\frac{7.3}{15}$ $\frac{5.9}{10}$ 5.4 $\frac{6.0}{11}$ $\frac{7.6}{15}$ $\frac{8.0}{26}$ $\frac{8.8}{33}$ $\frac{8.0}{41}$ $\frac{7.5}{50}$

$\frac{8.6}{50}$ $\frac{7.7}{33}$ $\frac{6.8}{31}$ $\frac{7.0}{26}$ $\frac{6.6}{15}$ $\frac{5.5}{10}$ 5.3 $\frac{5.8}{12}$ $\frac{7.3}{16}$ $\frac{7.4}{23}$ $\frac{7.1}{34}$ $\frac{6.8}{50}$

$\frac{7.7}{50}$ $\frac{8.0}{42}$ $\frac{7.5}{28}$ $\frac{7.1}{21}$ $\frac{5.5}{11}$ 5.2 $\frac{5.8}{12}$ $\frac{7.2}{16}$ $\frac{7.1}{23}$ $\frac{7.2}{50}$

$\frac{8.2}{50}$ $\frac{8.5}{36}$ $\frac{8.5}{26}$ $\frac{8.1}{16}$ $\frac{6.1}{9}$ 5.5 $\frac{6.0}{13}$ $\frac{7.2}{17}$ $\frac{7.3}{24}$ $\frac{8.0}{50}$

FL.
 $\frac{9.1}{50}$ $\frac{9.2}{26}$ $\left(\frac{8.6}{15}\right)$ $\frac{8.5}{16}$ $\frac{6.4}{9}$ 5.6 $\frac{6.0}{16}$ $\frac{8.5}{18}$ $\frac{8.4}{24}$ $\left(\frac{7.2}{17}\right)$ $\frac{9.2}{50}$

$\frac{8.9}{50}$ $\frac{9.0}{26}$ $\frac{8.6}{18}$ $\frac{8.1}{15}$ $\frac{6.4}{9}$ 5.5 $\frac{5.8}{12}$ $\frac{5.8}{20}$ $\frac{7.0}{25}$ $\frac{8.2}{50}$

$\frac{6.3}{50}$ $\frac{6.4}{27}$ $\frac{6.4}{23}$ $\frac{7.4}{20-18}$ $\frac{6.3}{16}$ $\frac{5.4}{10}$ 4.6 $\frac{4.7}{10}$ $\frac{4.5}{16}$ $\frac{6.2}{22-25}$ $\frac{7.1}{50}$

$\frac{4.0}{50}$ $\frac{4.6}{42}$ $\frac{6.0}{27}$ $\frac{6.0}{23}$ $\frac{7.2}{20-18}$ $\frac{6.3}{15}$ $\frac{5.4}{11}$ 4.7 $\frac{4.8}{11}$ $\frac{4.4}{15}$ $\frac{5.7}{21}$ $\frac{5.9}{25}$ $\frac{6.7}{50}$

Sta	+	π	-	Elev
		918.80		
38+50			4.7	14.1
39			4.7	14.1
+50			4.7	14.1
40			5.0	13.8
+50			5.8	13.0
41			6.4	12.4
+41	shldr Ditch		5.3	13.5
+47	E Ditch		5.2	13.6
+55	shldr Ditch		5.4	13.4
Top Slope	5.42	N. Side	Top Wall	6.36
Top Slope	5.35	S. Side	Top Wall	6.16
B.M.	7.99	918.69	8.08	910.72
42.			6.4	12.3
+50			5.7	13.0

$\frac{5.2}{50}$ $\frac{6.3}{27}$ $\frac{6.1}{23}$ $\frac{7.3}{21}$ $\frac{6.7}{19}$ $\frac{6.4}{17}$ $\frac{5.2}{12}$ $\frac{5.2}{9}$ 4.7 $\frac{4.6}{13}$ $\frac{5.9}{21}$ $\frac{6.0}{25}$ $\frac{6.7}{50}$

$\frac{4.1}{50}$ $\frac{6.2}{27}$ $\frac{6.0}{17}$ $\frac{5.2}{9}$ 4.7 $\frac{5.0}{13}$ $\frac{6.4}{20}$ $\frac{6.7}{24}$ $\frac{6.5}{28}$ $\frac{7.1}{31}$ $\frac{6.9}{33}$ $\frac{6.9}{50}$

$\frac{7.2}{50}$ $\frac{6.1}{27}$ $\frac{6.1}{19}$ $\frac{5.1}{13}$ $\frac{4.9}{6}$ 4.7 $\frac{5.4}{15}$ $\frac{6.6}{20}$ $\frac{6.4}{26}$ $\frac{7.1}{31}$ $\frac{7.0}{50}$

$\frac{8.4}{50}$ $\frac{7.3}{27}$ $\frac{6.7}{16}$ $\frac{5.2}{10}$ 5.0 $\frac{5.7}{11}$ $\frac{5.8}{16}$ $\frac{6.7}{20}$ $\frac{6.9}{25}$ $\frac{8.9}{31}$ $\frac{7.2}{50}$

$\frac{8.8}{50}$ $\frac{7.6}{31}$ $\frac{7.3}{21}$ $\frac{5.7}{15}$ 5.8 $\frac{6.3}{9}$ $\frac{7.7}{14}$ $\frac{8.0}{25}$ $\frac{8.4}{29}$ $\frac{8.4}{50}$

$\frac{8.7}{50}$ $\frac{9.3}{33}$ $\frac{9.8}{25}$ $\frac{6.3}{16}$ 6.4 $\frac{6.4}{6}$ $\frac{8.3}{11}$ $\frac{8.4}{24}$ $\frac{8.8}{25}$ $\frac{8.4}{33}$ $\frac{5.7}{40}$ $\frac{4.7}{50}$

$\frac{9.0}{50}$ $\frac{8.5}{25}$ $\frac{5.8}{18}$ $\frac{5.4}{8}$ 5.3 $\frac{6.5}{9}$ $\frac{6.6}{22}$ $\frac{7.8}{25}$

$\frac{10.8}{50}$ $\frac{10.0}{19}$ $\frac{5.6}{19}$ 5.2 $\frac{9.8}{01}$ $\frac{9.9}{22}$ $\frac{7.8}{24}$

$\frac{8.6}{50}$ $\frac{8.8}{21}$ $\frac{6.2}{21}$ 5.4 $\frac{6.4}{16}$ $\frac{7.8}{23}$

13.98

12.44

13.45

12.64

Top Spillway S.E. Cor. Rk Sta 41+40

$\frac{8.0}{50}$ $\frac{8.0}{33}$ $\frac{8.1}{26}$ $\frac{8.5}{22}$ $\frac{7.0}{18}$ 6.4 $\frac{6.7}{6}$ $\frac{7.5}{9}$ $\frac{6.9}{12}$ $\frac{5.0}{32}$ $\frac{7.3}{36}$ $\frac{7.8}{50}$

$\frac{7.5}{50}$ $\frac{6.5}{31}$ $\frac{6.5}{25}$ $\frac{7.3}{21}$ $\frac{6.5}{17}$ $\frac{5.7}{6}$ 5.7 $\frac{5.9}{9}$ $\frac{6.9}{13}$ $\frac{7.7}{30}$ $\frac{2.8}{40}$ $\frac{4.3}{50}$ $\frac{7.3}{60}$

Sta	+	π	-	Elev
		918.69		
43			5.6	13.1
+50			5.2	13.5
44			4.5	14.2
+50			4.2	14.5
45			3.7	15.0
+50			3.4	15.30
T.P.	4.24	919.59	3.34	915.35
46			4.3	15.3
+50			4.4	15.7
47			4.5	15.1
+50			4.6	15.0
48			4.7	14.9
+50			4.8	14.8

<u>8.0</u>	<u>8.0</u>	<u>8.0</u>	<u>6.5</u>		<u>5.2</u>	<u>6.2</u>	<u>6.7</u>	<u>7.5</u>	<u>8.3</u>	<u>8.4</u>
50	28	16	13	5.6	16	21	29	35	42	50

50 28 16 13 5.6 16 21 29 35 42 50

<u>7.4</u>	<u>7.9</u>	<u>7.5</u>	<u>5.8</u>		<u>5.2</u>	<u>4.7</u>	<u>4.5</u>	<u>5.5</u>	<u>4.1</u>
50	28	16	13	5.2	12	19	28	37	50

50 28 16 13 5.2 12 19 28 37 50

<u>8.0</u>	<u>7.5</u>	<u>7.7</u>	<u>5.1</u>		<u>5.2</u>	<u>5.5</u>	<u>4.4</u>	<u>3.4</u>	<u>3.7</u>
50	29	18	12	45	11	18	28	37	50

50 $\frac{1}{29}$ $\frac{1}{18}$ $\frac{1}{12}$ 4.5 $\frac{1}{11}$ $\frac{1}{18}$ $\frac{1}{28}$ $\frac{1}{37}$ $\frac{1}{50}$

$\frac{49}{50}$ $\frac{60}{39}$ $\frac{62}{28}$ $\frac{64}{18}$ $\frac{45}{12}$ 4.2 $\frac{48}{15}$ $\frac{57}{28}$ $\frac{55}{44}$ $\frac{44}{50}$

$\frac{1}{50}$	$\frac{1}{39}$	$\frac{1}{28}$	$\frac{1}{18}$	$\frac{1}{12}$	4.2	$\frac{1}{15}$	$\frac{1}{28}$	$\frac{1}{44}$	$\frac{1}{50}$
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$\frac{1.2}{50}$	$\frac{2.4}{31}$	$\frac{2.4}{25}$	$\frac{4.7}{19-16}$	$\frac{4.2}{14}$	3.7	$\frac{4.5}{13}$	$\frac{4.6}{28}$	$\frac{4.9}{50}$
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50	31	25	19-16	14	3.7	13	28	50
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$$\begin{array}{r} \frac{15.0}{50} + \frac{4.8}{29} = \frac{3.0}{19} \end{array} \quad \begin{array}{r} \frac{4.2}{14} \frac{3.9}{12} = 3.4 \end{array} \quad \begin{array}{r} \frac{4.2}{14} \frac{3.7}{17} \end{array} \quad \begin{array}{r} \frac{3.5}{27} \frac{3.8}{50} \end{array}$$

$\frac{1}{50} \quad \frac{1}{29} \quad \frac{1}{19} \quad \frac{1}{14} \quad \frac{1}{12} \quad 3.4 \quad \frac{1}{14} \quad \frac{1}{17} \quad \frac{1}{27} \quad \frac{1}{50}$

$\frac{+1.9}{50}$ $\frac{+0.8}{41}$ $\frac{+0.5}{29}$ $\frac{50}{17}$ $\frac{48}{14}$ $\frac{4.8}{4.3}$ $\frac{57}{12}$ $\frac{44}{14}$ $\frac{3.8}{21}$ $\frac{4.1}{27}$ $\frac{50}{50}$

50 41 29 17 14 4.3 12 14 21 27 50

<u>2.8</u>	<u>3.5</u>	<u>3.5</u>	<u>5.2</u>	<u>4.6</u>		<u>5.0</u>	<u>5.8</u>	<u>6.3</u>	<u>6.5</u>
50	29	18	14	11	44	12	14	27	50

50 29 18 14 11 4.4 12 14 27 50

47 5.4 5.9 6.2 4.9 5.2 7.2 7.2 7.2
50 28 24 15 11 4.5 11 16 27 50

50 28 24 15 11 4.5 11 16 27 50

$\frac{6.6}{50}$	$\frac{6.9}{28}$	$\frac{7.0}{16}$	$\frac{5.3}{12}$	4.6	$\frac{5.1}{11}$	$\frac{7.4}{16}$	$\frac{7.5}{26}$	$\frac{6.8}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

50 28 16 12 4.6 11 16 26 50

$\frac{7.1}{50}$	$\frac{7.2}{29}$	$\frac{7.4}{17}$	$\frac{5.1}{12}$	$\frac{5.2}{11}$	$\frac{7.2}{16}$	$\frac{7.4}{26}$	$\frac{6.8}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

50 29 17 12 4.7 11 16 26 50

8.0	8.3	7.9	5.2	5.0	6.4	7.3	7.4	6.9
50	29	17	11	12	15	19	26	50

50 $\frac{1}{29}$ $\frac{1}{17}$ $\frac{5.0}{11}$ 4.8 $\frac{5.0}{12}$ $\frac{6.19}{15}$ $\frac{1.5}{19}$ $\frac{1.5}{26}$ 50

Sta	+	π	-	Elev
		919.59		
49			4.7	14.9
+50			5.0	14.6
50			5.1	14.5
+29	12" Culv.		5.0	14.6
+50			5.1	14.5
51			4.9	14.7
+50			4.7	14.9
52			3.8	15.8
T.P.	8.87	924.63	3.83	915.76
+50			7.8	16.8
53			6.8	17.8
+50			5.7	18.9
54			4.9	19.7

$\begin{array}{r} 8.6 \\ \hline 50 \end{array}$
 $\begin{array}{r} 8.3 \\ \hline 29 \end{array}$
 $\begin{array}{r} 8.0 \\ \hline 16 \end{array}$
 $\begin{array}{r} 5.6 \\ \hline 14 \end{array}$
 $\begin{array}{r} 4.9 \\ \hline 11 \end{array}$
 $\begin{array}{r} 7.0 \\ \hline 15 \end{array}$
 $\begin{array}{r} 7.0 \\ \hline 25 \end{array}$
 $\begin{array}{r} 6.9 \\ \hline 50 \end{array}$

$\frac{8.5}{50}$	$\frac{8.4}{29}$	$\frac{8.1}{17}$	$\frac{5.5}{13}$	5.0	$\frac{5.4}{12}$	$\frac{7.3}{16}$	$\frac{7.4}{25}$	$\frac{6.9}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{8.5}{50}$	$\frac{8.5}{29}$	$\frac{8.0}{17}$	$\frac{5.7}{13}$	$\frac{5.1}{5.1}$	$\frac{5.3}{12}$	$\frac{7.1}{15}$	$\frac{7.3}{25}$	$\frac{6.8}{50}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

F.L										
9.6	9.3	9.1	8.8	8.9	8.7	5.5	5.3	7.6	7.4	6.7
100	75	50	29	18	18	13	5.0	12	15	5.0

$\frac{8.4}{50} \quad \frac{9.2}{29} \quad \frac{8.0}{18} \quad \frac{5.4}{13} \quad \frac{5.3}{12} \quad \frac{7.3}{16} \quad \frac{7.5}{25} \quad \frac{6.7}{50}$

$\frac{8.3}{50}$	$\frac{8.3}{29}$	$\frac{8.0}{19}$	$\frac{5.4}{12}$	$\frac{5.2}{12}$	$\frac{7.4}{16}$	$\frac{7.6}{25}$	$\frac{6.6}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

8.2	8.1	7.7	5.3	5.1	7.4	7.6	6.1
50	29	17	12	4.7	12	17	50

$\frac{7.1}{50}$ $\frac{6.6}{29}$ $\frac{6.4}{16}$ $\frac{4.3}{11}$ 38 $\frac{4.2}{11}$ $\frac{5.9}{15}$ $\frac{6.1}{25}$ $\frac{5.2}{50}$

$\frac{9.4}{50}$	$\frac{9.2}{29}$	$\frac{9.2}{14}$	$\frac{8.4}{12}$	$\frac{8.4}{13}$	$\frac{9.1}{16}$	$\frac{8.8}{27}$	$\frac{6.7}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.9}{50}$	$\frac{5.5}{47}$	$\frac{6.5}{29}$	$\frac{6.8}{20}$	$\frac{7.7}{16}$	$\frac{7.2}{10}$	$\frac{7.4}{17}$	$\frac{5.7}{22}$	$\frac{5.1}{26}$	$\frac{2.3}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$+0.5 \quad 2.8 \quad 2.6 \quad 6.5 \quad 6.2 \quad 6.5 \quad 6.8 \quad 1.9$
 $50 \quad 33 \quad 24 \quad 19-12 \quad 10 \quad 5.7 \quad 15 \quad 18.23 \quad 31$

$$\begin{array}{r} 4.9 \\ \hline 18 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 15 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 11 \end{array} \quad 4.9 \quad \begin{array}{r} 5.6 \\ \hline 21 \end{array} \quad \begin{array}{r} 2.3 \\ \hline 28 \end{array}$$

Sta	+	π	-	Elev
		924.63		

54 + 40			4.5	20.1
---------	--	--	-----	------

55			5.1	19.5
----	--	--	-----	------

T.P.	11.35	935.80	0.18	924.45
------	-------	--------	------	--------

53 + 50				18.9
---------	--	--	--	------

54				19.7
----	--	--	--	------

+ 40				20.1
------	--	--	--	------

55				19.5
----	--	--	--	------

T.P.	0.20	924.65	11.35	924.45
------	------	--------	-------	--------

+ 42			6.1	18.2
------	--	--	-----	------

56			7.5	17.2
----	--	--	-----	------

B.M.	4.48	920.91	8.22	916.43
------	------	--------	------	--------

+ 40			4.0	16.9
------	--	--	-----	------

+ 72			4.3	16.6
------	--	--	-----	------

57			4.6	16.3
----	--	--	-----	------

+ 20	24"	Culr.	4.9	16.0
------	-----	-------	-----	------

$$\begin{array}{r} 33 \quad 46 \\ 22 \quad 13 \end{array} \quad \begin{array}{r} 52 \quad 11 \\ 12 \quad 23 \end{array}$$

$$\begin{array}{r} 50 \\ 21 \end{array} \quad \begin{array}{r} 58 \\ 11 \end{array} \quad \begin{array}{r} 52 \\ 17 \end{array} \quad \begin{array}{r} 10 \\ 25 \end{array}$$

$$\textcircled{16.9}$$

$$\begin{array}{r} 11.7 \quad 8.6 \\ 50 \quad 75 \end{array}$$

$$\begin{array}{r} 10 \\ 75 \end{array} \quad \begin{array}{r} 30 \\ 65 \end{array} \quad \begin{array}{r} 60 \\ 50 \end{array} \quad \begin{array}{r} 75 \\ 42 \end{array} \quad \begin{array}{r} 80 \\ 33 \end{array}$$

$$\textcircled{16.1}$$

$$\begin{array}{r} 8.6 \quad 8.2 \quad 6.6 \\ 32 \quad 50 \quad 75 \end{array}$$

$$\begin{array}{r} +1.7 \quad 1.9 \quad 2.5 \\ 75 \quad 55 \quad 39 \end{array}$$

$$\textcircled{15.7}$$

$$\begin{array}{r} 65 \quad 5.9 \quad 8.2 \quad 9.0 \quad 10 \\ 34 \quad 50 \quad 70 \quad 75 \end{array}$$

$$\begin{array}{r} 85 \quad 100 \quad 10.2 \\ 75 \quad 50 \quad 33 \end{array}$$

$$\textcircled{16.3}$$

$$\begin{array}{r} 14.7 \\ 50 \end{array}$$

$$\begin{array}{r} 8.0 \quad 7.0 \quad 6.9 \quad 6.7 \\ 50 \quad 21 \quad 15 \quad 12 \end{array}$$

$$\begin{array}{r} 6.8 \quad 7.9 \quad 8.4 \quad 11.4 \\ 61 \quad 12 \quad 18 \quad 26 \quad 50 \end{array}$$

$$\begin{array}{r} 9.4 \quad 9.2 \quad 7.8 \\ 50 \quad 19 \quad 7 \end{array}$$

$$\begin{array}{r} 8.2 \quad 12.2 \quad 13.0 \\ 9 \quad 18 \quad 50 \end{array}$$

Spike in 12" Pop 18' Lf. 57+70

$$\begin{array}{r} 15 \quad 4.4 \quad 5.1 \quad 5.0 \quad 4.2 \\ 50 \quad 29 \quad 18 \quad 15 \quad 12 \quad 40 \end{array} \quad \begin{array}{r} 4.9 \quad 6.8 \quad 7.3 \quad 9.1 \\ 11 \quad 16 \quad 23 \quad 50 \end{array}$$

$$\begin{array}{r} 6.2 \quad 6.8 \quad 4.4 \\ 50 \quad 18 \quad 11 \end{array}$$

$$\begin{array}{r} 5.3 \quad 7.5 \quad 8.1 \quad 8.9 \\ 11 \quad 16 \quad 24 \quad 50 \end{array}$$

$$\begin{array}{r} 8.0 \quad 8.3 \quad 5.0 \\ 50 \quad 20 \quad 11 \end{array}$$

$$\begin{array}{r} 6.0 \quad 9.0 \quad 9.2 \quad 9.3 \\ 11 \quad 15 \quad 23 \quad 50 \end{array}$$

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$$\begin{array}{r} 8.6 \quad 9.2 \quad 8.7 \quad 5.2 \\ 50 \quad 21 \quad 21 \quad 12 \end{array} \quad \begin{array}{r} 4.9 \quad 6.2 \quad 9.7 \quad 9.0 \quad 9.2 \\ 10 \quad 14 \quad 14 \quad 21 \quad 50 \end{array}$$

Sta	+	Σ	-	Elev
		920.91		
57150			5.0	15.9
58			4.7	16.2
+50			4.7	16.2
+75			4.9	16.0
59			5.1	15.8
+38			4.9	16.0
60			4.9	16.0
T.P.	10.42	927.96	3.37	917.54
58				16.2
+50				16.2
+75				16.0
59				15.8
+38				16.0
T.P.	0.59	918.13	10.42	917.54

$$\begin{array}{r} 5.6 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 39 \end{array} \quad \begin{array}{r} 6.5 \\ 22 \end{array} \quad \begin{array}{r} 4.8 \\ 12 \end{array} \quad 5.0 \quad \begin{array}{r} 6.3 \\ 10 \end{array} \quad \begin{array}{r} 7.9 \\ 13 \end{array} \quad \begin{array}{r} 8.2 \\ 20 \end{array} \quad \begin{array}{r} 9.1 \\ 50 \end{array}$$

$$\begin{array}{r} 3.9 \\ 19 \end{array} \quad \begin{array}{r} 5.0 \\ 15 \end{array} \quad 4.7 \quad \begin{array}{r} 5.9 \\ 12 \end{array} \quad \begin{array}{r} 7.3 \\ 17 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 20 \end{array} \quad 4.7 \quad \begin{array}{r} 5.9 \\ 12 \end{array} \quad \begin{array}{r} 8.1 \\ 17 \end{array} \quad \begin{array}{r} 8.9 \\ 23 \end{array} \quad \begin{array}{r} 8.9 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 28 \end{array} \quad \begin{array}{r} 6.0 \\ 15 \end{array} \quad \begin{array}{r} 5.5 \\ 12 \end{array} \quad 4.9 \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 9.0 \\ 20 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 27 \end{array} \quad \begin{array}{r} 6.7 \\ 22 \end{array} \quad \begin{array}{r} 6.3 \\ 13 \end{array} \quad \begin{array}{r} 5.8 \\ 11 \end{array} \quad 5.1 \quad \begin{array}{r} 6.0 \\ 15 \end{array} \quad \begin{array}{r} 8.8 \\ 22 \end{array} \quad \begin{array}{r} 9.1 \\ 50 \end{array}$$

$$\begin{array}{r} 3.5 \\ 29 \end{array} \quad \begin{array}{r} 5.6 \\ 22 \end{array} \quad \begin{array}{r} 6.1 \\ 16 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad 4.9 \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 8.5 \\ 20 \end{array} \quad \begin{array}{r} 8.9 \\ 50 \end{array}$$

$$\begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 29 \end{array} \quad \begin{array}{r} 6.3 \\ 25 \end{array} \quad \begin{array}{r} 6.3 \\ 16 \end{array} \quad \begin{array}{r} 5.2 \\ 12 \end{array} \quad 4.9 \quad \begin{array}{r} 5.6 \\ 15 \end{array} \quad \begin{array}{r} 6.8 \\ 26 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.9 \\ 25 \end{array} \quad \begin{array}{r} 4.7 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 27 \end{array} \quad (11.8)$$

$$\begin{array}{r} 4.2 \\ 75 \end{array} \quad \begin{array}{r} 3.7 \\ 65 \end{array} \quad \begin{array}{r} 4.6 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 40 \end{array} \quad \begin{array}{r} 7.3 \\ 27 \end{array} \quad (11.8)$$

$$\begin{array}{r} 4.1 \\ 75 \end{array} \quad \begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 8.6 \\ 43 \end{array} \quad \begin{array}{r} 9.8 \\ 33 \end{array} \quad (12.0)$$

$$\begin{array}{r} 3.1 \\ 75 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 7.2 \\ 36 \end{array} \quad (12.2)$$

$$\begin{array}{r} 3.0 \\ 75 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array} \quad \begin{array}{r} 3.2 \\ 37 \end{array} \quad (12.0)$$

Sta	+	π	-	Elev
-----	---	-------	---	------

918.13.

60+50			2.4	15.7
-------	--	--	-----	------

+75			3.5	14.4
-----	--	--	-----	------

+85			5.2	12.9
-----	--	--	-----	------

61			5.8	12.3
----	--	--	-----	------

+38			6.3	11.8
-----	--	--	-----	------

+50			4.4	13.7
-----	--	--	-----	------

62			4.0	14.1
----	--	--	-----	------

+50			5.3	12.8
-----	--	--	-----	------

63			5.6	12.5
----	--	--	-----	------

+50			5.2	12.9
-----	--	--	-----	------

64			5.0	13.1
----	--	--	-----	------

+50			5.3	12.8
-----	--	--	-----	------

$$\begin{array}{r} 60 \\ 50 \end{array} \frac{5.0}{14} \frac{4.7}{11} \frac{2.7}{6} 2.4 \frac{2.1}{9} \frac{2.5}{23} \frac{2.5}{37} \frac{0.4}{42} \frac{2.5}{50}$$

$$\frac{59}{50} \frac{5.1}{4} 3.5 \frac{2.3}{16} \frac{2.4}{27} \frac{3.1}{31} \frac{4.0}{50}$$

$$\frac{6.1}{50} 5.2 \frac{3.7}{4} \frac{2.2}{21} \frac{2.3}{31} \frac{3.6}{37} \frac{3.4}{50}$$

$$\frac{6.1}{50} 5.8 \frac{5.2}{6} \frac{4.0}{9} \frac{2.4}{22} \frac{2.3}{36} \frac{2.0}{50}$$

$$\frac{6.1}{50} 6.3 \frac{3.9}{6} \frac{3.0}{17} \frac{3.5}{30} \frac{6.1}{37} \frac{4.0}{50}$$

$$\frac{6.0}{50} \frac{6.4}{5} 4.4 \frac{3.2}{13} \frac{3.5}{23} \frac{6.4}{31} \frac{6.2}{50}$$

$$\frac{6.3}{50} \frac{6.5}{15} \frac{4.7}{12} 4.0 \frac{4.5}{12} \frac{6.8}{18} \frac{6.7}{50}$$

$$\frac{6.3}{50} \frac{7.9}{15} \frac{5.9}{13} 5.3 \frac{5.7}{9} \frac{8.3}{14} \frac{6.5}{19} \frac{8.2}{50}$$

$$\frac{6.6}{50} \frac{7.3}{14} \frac{5.9}{11} 5.6 \frac{6.0}{11} \frac{7.7}{15} \frac{7.5}{50}$$

$$\frac{6.5}{50} \frac{7.3}{14} \frac{5.6}{12} 5.2 \frac{5.8}{11} \frac{7.8}{14} \frac{7.5}{50}$$

$$\frac{6.5}{50} \frac{7.9}{15} \frac{5.6}{11} 5.0 \frac{5.6}{12} \frac{7.6}{16} \frac{7.4}{23} \frac{6.5}{50}$$

$$\frac{6.5}{50} \frac{7.9}{14} \frac{6.0}{11} 5.3 \frac{5.7}{12} \frac{7.3}{16} \frac{7.1}{23} \frac{6.6}{50}$$

Sta	t	π	-	Ekr
		918.13		
65			5.6	12.5
+50			4.7	13.4
T.P.	7.52	921.40	4.25	913.88
66			7.0	14.4
+50			6.6	14.8
67			5.6	15.8
+50			5.0	16.4
68			4.6	16.8
+50			4.3	17.1
69			3.6	17.8
+50			2.4	19.0
70			1.2	20.2
T.P.	12.41	932.48	1.33	920.07
67 + 50				16.4

$$\begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 9.5 \\ 20 \end{array} \quad \begin{array}{r} 8.9 \\ 14 \end{array} \quad \begin{array}{r} 6.3 \\ 11 \end{array} \quad 5.6 \quad \begin{array}{r} 6.0 \\ 11 \end{array} \quad \begin{array}{r} 7.6 \\ 15 \end{array} \quad \begin{array}{r} 7.7 \\ 23 \end{array} \quad \begin{array}{r} 6.7 \\ 40 \end{array} \quad \begin{array}{r} 6.5 \\ 50 \end{array}$$

$$\begin{array}{r} 6.9 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 18 \end{array} \quad \begin{array}{r} 5.4 \\ 11 \end{array} \quad 4.7 \quad \begin{array}{r} 5.2 \\ 11 \end{array} \quad \begin{array}{r} 7.5 \\ 17 \end{array} \quad \begin{array}{r} 7.5 \\ 25 \end{array} \quad \begin{array}{r} 6.7 \\ 40 \end{array} \quad \begin{array}{r} 6.5 \\ 50 \end{array}$$

$$\begin{array}{r} 10.0 \\ 50 \end{array} \quad \begin{array}{r} 9.8 \\ 20 \end{array} \quad \begin{array}{r} 10.3 \\ 16 \end{array} \quad \begin{array}{r} 7.6 \\ 12 \end{array} \quad 7.0 \quad \begin{array}{r} 7.8 \\ 11 \end{array} \quad \begin{array}{r} 10.5 \\ 19 \end{array} \quad \begin{array}{r} 10.5 \\ 29 \end{array} \quad \begin{array}{r} 10.0 \\ 50 \end{array}$$

$$\begin{array}{r} 9.5 \\ 50 \end{array} \quad \begin{array}{r} 9.6 \\ 19 \end{array} \quad \begin{array}{r} 7.4 \\ 13 \end{array} \quad 6.6 \quad \begin{array}{r} 7.0 \\ 12 \end{array} \quad \begin{array}{r} 8.9 \\ 18 \end{array} \quad \begin{array}{r} 9.1 \\ 29 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 8.9 \\ 50 \end{array} \quad \begin{array}{r} 8.8 \\ 18 \end{array} \quad \begin{array}{r} 6.6 \\ 12 \end{array} \quad 5.6 \quad \begin{array}{r} 5.9 \\ 12 \end{array} \quad \begin{array}{r} 8.4 \\ 19 \end{array} \quad \begin{array}{r} 8.7 \\ 26 \end{array} \quad \begin{array}{r} 7.2 \\ 50 \end{array}$$

$$\begin{array}{r} 8.2 \\ 50 \end{array} \quad \begin{array}{r} 8.3 \\ 17 \end{array} \quad \begin{array}{r} 5.8 \\ 12 \end{array} \quad 5.0 \quad \begin{array}{r} 5.5 \\ 12 \end{array} \quad \begin{array}{r} 6.7 \\ 17 \end{array} \quad \begin{array}{r} 6.2 \\ 26 \end{array}$$

$$\begin{array}{r} 8.5 \\ 50 \end{array} \quad \begin{array}{r} 8.5 \\ 18 \end{array} \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad 4.6 \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 5.9 \\ 15-19 \end{array} \quad \begin{array}{r} 4.7 \\ 25 \end{array} \quad \begin{array}{r} 2.2 \\ 29 \end{array} \quad \begin{array}{r} 0.7 \\ 35 \end{array}$$

$$\begin{array}{r} 8.0 \\ 50 \end{array} \quad \begin{array}{r} 8.2 \\ 18 \end{array} \quad \begin{array}{r} 5.2 \\ 12 \end{array} \quad 4.3 \quad \begin{array}{r} 4.8 \\ 12 \end{array} \quad \begin{array}{r} 5.8 \\ 14 \end{array} \quad \begin{array}{r} 5.2 \\ 28 \end{array} \quad \begin{array}{r} 1.4 \\ 39 \end{array}$$

$$\begin{array}{r} 8.2 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 18 \end{array} \quad \begin{array}{r} 4.6 \\ 12 \end{array} \quad 3.6 \quad \begin{array}{r} 4.1 \\ 12 \end{array} \quad \begin{array}{r} 5.3 \\ 17 \end{array} \quad \begin{array}{r} 4.4 \\ 30 \end{array}$$

$$\begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 5.3 \\ 24 \end{array} \quad \begin{array}{r} 3.2 \\ 13 \end{array} \quad 2.4 \quad \begin{array}{r} 3.1 \\ 14 \end{array} \quad \begin{array}{r} 3.8 \\ 19 \end{array} \quad \begin{array}{r} 1.7 \\ 29 \end{array}$$

$$\begin{array}{r} 1.4 \\ 50 \end{array} \quad \begin{array}{r} 0.0 \\ 37 \end{array} \quad \begin{array}{r} 3.3 \\ 30 \end{array} \quad \begin{array}{r} 2.3 \\ 16 \end{array} \quad 1.2 \quad \begin{array}{r} 1.9 \\ 15 \end{array} \quad \begin{array}{r} 2.2 \\ 23 \end{array} \quad \begin{array}{r} 0.0 \\ 30 \end{array}$$

(161)

$$\begin{array}{r} 15.6 \\ 40 \end{array} \quad \begin{array}{r} 13.8 \\ 50 \end{array}$$

Sta	+	+	-	Elev
		932.48	932.42	
68				16.8
+50				17.1
69				17.8
+50				19.0
70				20.2
+37			11.4	21.0
71			9.9	22.6
+50			8.9	23.6
T.P	6.50	938.03	0.95	931.53
71				22.6
+50				23.6
72			13.4	24.6
+50			12.6	24.4

$$\textcircled{15.7} \quad \frac{10.4}{42} \quad \frac{9.0}{50} \quad \frac{6.2}{75}$$

$$\textcircled{15.4} \quad \frac{9.2}{50} \quad \frac{5.3}{75}$$

$$\textcircled{14.7} \quad \frac{7.7}{38} \quad \frac{8.1}{43} \quad \frac{5.7}{50} \quad \frac{0.7}{75}$$

$$\textcircled{13.5} \quad \frac{3.7}{42} \quad \frac{2.5}{50} \quad \frac{0.4}{75}$$

$$\textcircled{12.3} \quad \frac{4.4}{40} \quad \frac{3.7}{50} \quad \frac{4.7}{75}$$

$$\frac{15.3}{50} \quad \frac{14.5}{27} \quad \frac{13.0}{18} \quad \frac{12.2}{14} \quad 11.4 \quad \frac{12.0}{14} \quad \frac{12.7}{19.2} \quad \frac{12.2}{26} \quad \frac{5.5}{39} \quad \frac{5.0}{50} \quad \frac{3.7}{75}$$

$$\frac{16.0}{50} \quad \frac{13.7}{19} \quad \frac{11.0}{13} \quad 9.9 \quad \frac{10.8}{18} \quad \frac{8.6}{32}$$

$$\frac{15.9}{50} \quad \frac{12.7}{22} \quad \frac{9.8}{16} \quad 8.9 \quad \frac{9.6}{14} \quad \frac{7.7}{22}$$

$$\textcircled{15.4} \quad \frac{2.3}{45} \quad \frac{3.4}{25} \quad \frac{3.9}{75}$$

$$\textcircled{14.4} \quad \frac{5.1}{34} \quad \frac{6.2}{50}$$

$$\frac{15.8}{50} \quad \frac{13.6}{25} \quad \frac{14.5}{23} \quad 13.4 \quad 14.2 \quad \frac{12.4}{18} \quad \frac{8.1}{25} \quad \frac{12.1}{50}$$

$$\frac{16.1}{50} \quad \frac{16.0}{20} \quad \frac{13.5}{12} \quad 12.6 \quad \frac{13.5}{13} \quad \frac{13.0}{15} \quad \frac{10.9}{21} \quad \frac{12.4}{32} \quad \frac{16.4}{50}$$

Sta	+	✕	-	Elev
		938.03		
73			11.9	26.1
T.P.	7.94	934.05	11.92	926.11.
+50			6.9	27.2
74			5.9	28.2
+50			4.4	29.7
+75	1/2 N. Co. Rd		3.8	30.3
+99			3.1	31.0
B.M.			5.17	928.88. 928.84.

$$\begin{array}{r} 19.3 \\ 50 \end{array} \quad \begin{array}{r} 17.8 \\ 40 \end{array} \quad \begin{array}{r} 15.2 \\ 24 \end{array} \quad \begin{array}{r} 12.6 \\ 12 \end{array} \quad 11.9 \quad \begin{array}{r} 12.7 \\ 18 \end{array} \quad \begin{array}{r} 12.3 \\ 20 \end{array} \quad \begin{array}{r} 15.0 \\ 35 \end{array} \quad \begin{array}{r} 14.2 \\ 50 \end{array}$$

$$\begin{array}{r} 8.7 \\ 50 \end{array} \quad \begin{array}{r} 8.2 \\ 40 \end{array} \quad \begin{array}{r} 7.3 \\ 26 \end{array} \quad \begin{array}{r} 8.4 \\ 22 \end{array} \quad \begin{array}{r} 7.5 \\ 18 \end{array} \quad 6.9 \quad \begin{array}{r} 7.3 \\ 13 \end{array} \quad \begin{array}{r} 8.3 \\ 15 \end{array} \quad \begin{array}{r} 8.3 \\ 25 \end{array} \quad \begin{array}{r} 6.1 \\ 50 \end{array}$$

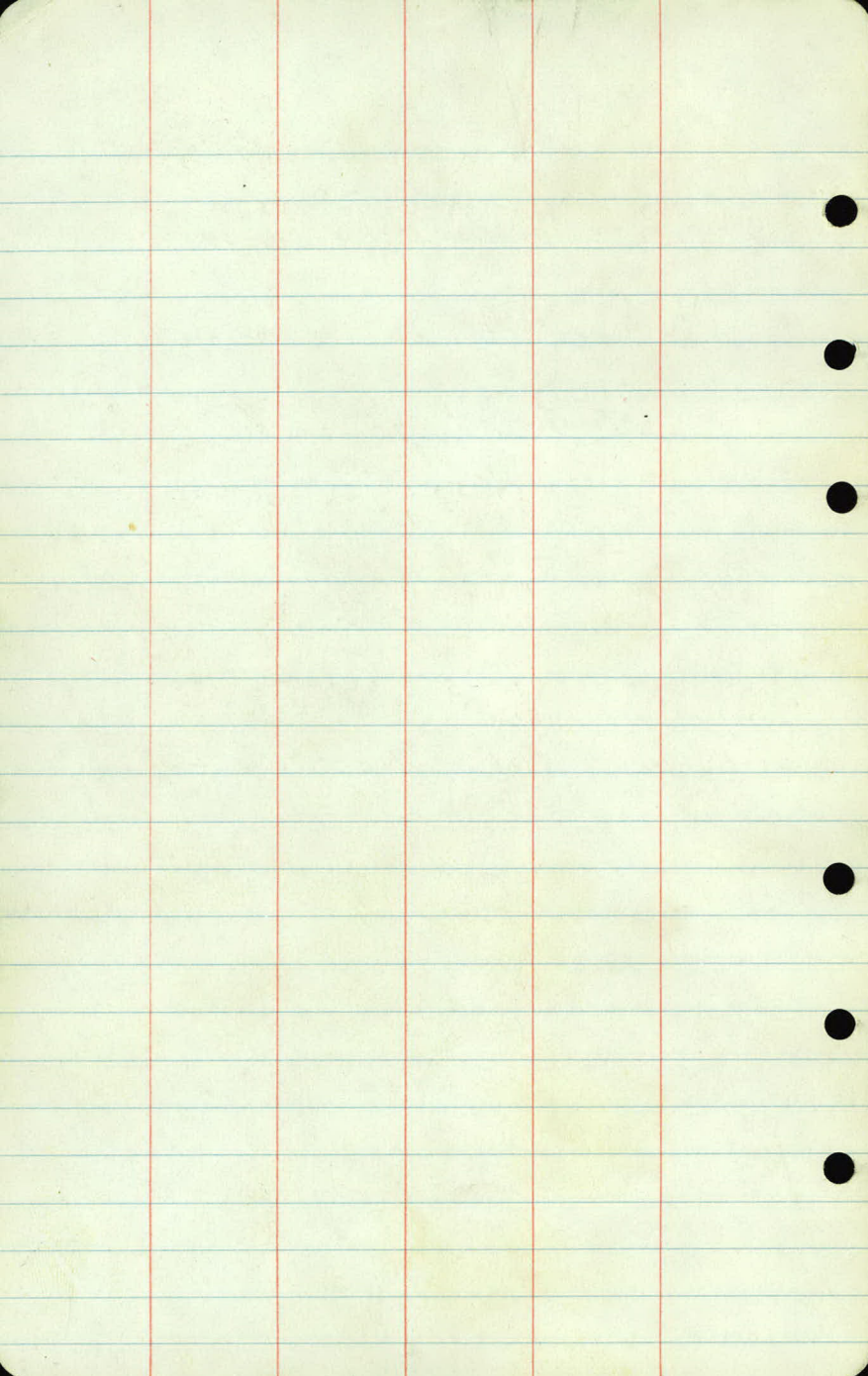
$$\begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 7.3 \\ 31 \end{array} \quad \begin{array}{r} 7.2 \\ 20 \end{array} \quad \begin{array}{r} 6.4 \\ 14 \end{array} \quad 5.9 \quad \begin{array}{r} 6.0 \\ 17 \end{array} \quad \begin{array}{r} 3.7 \\ 20 \end{array} \quad \begin{array}{r} 2.5 \\ 50 \end{array}$$

$$\begin{array}{r} 7.7 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 25 \end{array} \quad \begin{array}{r} 5.3 \\ 11 \end{array} \quad 4.4 \quad \begin{array}{r} 4.6 \\ 20 \end{array} \quad + \begin{array}{r} 1.0 \\ 29 \end{array} \quad + \begin{array}{r} 4.5 \\ 50 \end{array}$$

$$\begin{array}{r} 9.1 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 11 \end{array} \quad 3.8 \quad \begin{array}{r} 3.3 \\ 22 \end{array} \quad + \begin{array}{r} 5.0 \\ 34 \end{array} \quad + \begin{array}{r} 5.0 \\ 40 \end{array} \quad + \begin{array}{r} 7.0 \\ 43 \end{array} \quad + \begin{array}{r} 7.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.7 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 35 \end{array} \quad \begin{array}{r} 5.8 \\ 17 \end{array} \quad 3.1 \quad \begin{array}{r} 3.2 \\ 16 \end{array} \quad \begin{array}{r} 2.2 \\ 22 \end{array} \quad + \begin{array}{r} 7.5 \\ 38 \end{array} \quad + \begin{array}{r} 7.6 \\ 50 \end{array}$$

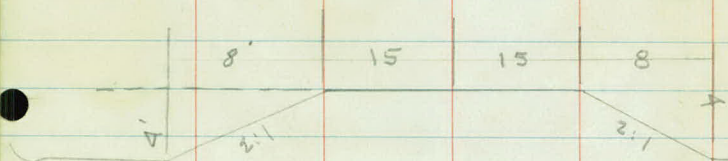
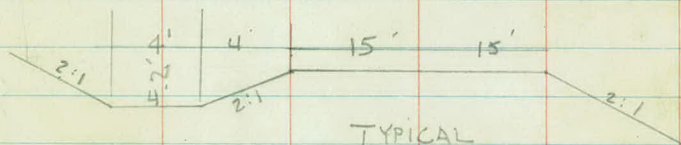
Spike in 18" Oak S.W. Cor H. Co. Line.



Slope stakes

BALD EAGLE BLVD WEST

Party staked 9-19-39
R.O.P.
A.M.
L.G.
C.F.



Spec. Sec. 18+50 to 20+50

Sta.	+	⌒	-	Elev.
B.M.	3.64	919.31		915.67
T.P.	6.44	918.62	7.13	912.18
17				15.3

+50				15.3
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18				15.3
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+50				15.3
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19				15.3
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+50				15.3
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20				15.3
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+50				15.3
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B.M.	2.87	918.54	2.95	915.67
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21				15.3
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+09				15.3
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	3.24	918.91	2.87	915.67
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+50				15.3
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22				15.3
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Spec. Section

E

G.R.

Lt.

Rt.

Top Water table S.W. Cor G.R. 100' Lt 23+00

3.3	$\begin{array}{r} 4.7 \\ 100.4 \\ \hline 23.8 \end{array}$	3.2	$\begin{array}{r} 3.4 \\ 101.9 \\ \hline 24.8 \end{array}$	
5.3				
	$\begin{array}{r} 4.7 \\ 100.6 \\ \hline 24.2 \end{array}$	3.5	$\begin{array}{r} 2.7 \\ 101.4 \\ \hline 27.8 \end{array}$	
	$\begin{array}{r} 6.4 \\ 103.1 \\ \hline 21.2 \end{array}$	4.1	$\begin{array}{r} 7.1 \\ 103.8 \\ \hline 22.6 \end{array}$	
3.3	$\begin{array}{r} 7.3 \\ 101.0 \\ \hline 46.0 \end{array}$	7.3 B.T.	$\begin{array}{r} 5.9 \\ 102.1 \\ \hline \end{array}$	$\begin{array}{r} 7.3 \\ 103.0 \\ \hline 22.0 \end{array}$
7.3				
	$\begin{array}{r} 7.3 \\ 101.0 \\ \hline 72.3 \end{array}$	7.3 B.T.	$\begin{array}{r} 6.4 \\ 103.1 \\ \hline \end{array}$	$\begin{array}{r} 7.3 \\ 103.0 \\ \hline 58.0 \end{array}$
	$\begin{array}{r} 7.6 \\ 101.0 \\ \hline 102.5 \end{array}$	7.3 B.T.	$\begin{array}{r} 6.7 \\ 103.4 \\ \hline \end{array}$	$\begin{array}{r} 7.3 \\ 103.0 \\ \hline 79.0 \end{array}$
	$\begin{array}{r} 8.0 \\ 101.0 \\ \hline 75.2 \end{array}$	7.3 B.T.	$\begin{array}{r} 6.4 \\ 103.1 \\ \hline \end{array}$	$\begin{array}{r} 7.3 \\ 103.0 \\ \hline 126.4 \end{array}$
	$\begin{array}{r} 8.1 \\ 101.0 \\ \hline 100.4 \end{array}$	7.3 B.T.	$\begin{array}{r} 5.6 \\ 102.3 \\ \hline \end{array}$	$\begin{array}{r} 7.3 \\ 103.0 \\ \hline 55.6 \end{array}$
3.2		5.2	7.2	
5.2	$\begin{array}{r} 8.0 \\ 104.8 \\ \hline 24.6 \end{array}$		$\begin{array}{r} 7.5 \\ 104.3 \\ \hline 23.6 \end{array}$	
	$\begin{array}{r} 8.4 \\ 105.1 \\ \hline 25.8 \end{array}$	5.3	5.5	
3.6				
4.0		5.5	4.0	
8.0				
3.6	$\begin{array}{r} 8.6 \\ 105.6 \\ \hline 26.2 \end{array}$	5.0	5.3	
4.2				

E.W. 0.5

E.W. 1.0

Sta	+	π	-	Elev.
		918.94		
22+50				15.3
B.M.				915.67
23				15.3
+50				15.3
24				15.3
+50				15.3
25				15.3
+50				15.3
T.P.	7.37	921.89	43.9	914.52
26				15.3
+50				15.3
27				15.3
+50				15.3
T.P.	3.11	918.11	51.2	915.22
28				15.3

Elevation

G. R.

3.0	8.4	5.0	5.0	4.2	7.1	
3.6	F5.4	F2.0		B.T.	F2.9	
4.2	25.8	15	F1.4	16	21.8	E.W. 1.0

Top Water table S.W. Cor Gor 100' Pt Sta B3100

3.3	8.4	5.3	4.6	4.9	7.4	
3.6	F5.3	F2.0	F1.0	F1.0	F3.5	
3.9	25.6	15		15.5	22.5	E.W. 0.5

3.6	6.7	4.3	6.8
5.6	F3.1	F0.7	F3.2
	21.2		21.4

6.7	3.9	5.2
F3.1	F0.3	DC0.4
21.2		23.8

3.6	6.9	3.8	3.4
	F3.3	F0.2	C0.2
	21.6		27.4

6.8	3.6	4.4
F3.2	F0.0	DC1.2
21.4		25.4

7.6	3.8	6.4
F4.0	F0.2	F2.8
23.0		20.6

7.2	11.5	7.2	7.4	7.2	10.2	P = -0.6
+0.6	F5.3	F1.0	F0.8	B.T.	P3.0	
-0.6	25.6	15		15.3	21.3	E.W. 0.3
-0.4 E.W. 0.3						
6.2						

7.4	9.7	7.0	7.1	7.2	10.4	P = -0.5
+0.8	F3.7	F1.0		B.T.	F3.0	
-0.6 E.W. 2.0	22.4	15	F0.5	17.0	23.0	E.W. 2.0
6.0						

7.5	7.9	5.8	6.5	7.5	8.6	P = -0.9
+0.9	DC0.7	B.T.		B.T.	F1.1	
-0.6 E.W. 3.3	26.0	15.0	C0.1	18.3	20.5	E.W. 3.3
5.8						

7.6	4.3	7.6	5.7	5.6	7.2	P = -1.0
4.0	C1.4	B.T.		F2.0	DC1.4	
-0.9 E.W. 4.0	33.4	15.0	C0.9	19.0	27.8	W = 4.0
5.7						

7.4	3.8	6.0	6.3	6.4	6.9	P = -0.8
+0.8	C10.4	B.T.		C1.0	C0.5	
-0.6 E.W. 2.0	50.2	15.0	C0.3	17.0	26.8	W = 2.0
6.6						

Sta	+	Δ	-	Elev
		921.89		

28+50				15.3
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29				15.2
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T.P.	3.06	919.63	5.32	916.57
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+50				15.1
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30				15.1
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+50				15.0
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31				14.9
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+21				14.9
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T.P.	4.50	919.07	5.06	914.57
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+44				14.8
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32				14.7
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+50				14.7
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33				14.6
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B.M.	2.81	919.38	1.49	916.58
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+50				14.5
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EASEMENT

EASEMENT

916.57

Gr. R.

7.0									
+0.8			+8.1	7.0	6.6	6.4	7.5 P+0.2		
-4.6			C14.7	B.T		B.T	DC.11		
-0.6	EW	2.0	55.2	17.0	F0.0	15.0	25.6		26
6.4									
7.7									
+1.0			+9.1	7.7	7.0	5.8	9.2 P+0.9		
-4.7			C15.8	B.T		B.T	F34		
-0.9	EW	3.8	58.4	18.8	F0.3	15.0	21.8		20
5.8									
5.5									
+1.0			+10.9	4.5		3.8	7.1	P+0.9	
-4.5			C15.4	C2.0	4.9	B.T			
-0.9	EW	4.0	57.8	19.0	F0.4	15	F33		
3.8							21.6		
5.5									
+1.0			+10.2	2.5	4.8	3.6	7.3	P+0.9	
-4.6			C14.7	C3.0		B.T	F37		
-0.9	EW	3.8	56.2	18.8	F0.5	15.0	22.4		
3.6									
5.4									
+0.8			+10.7	4.4		4.0	6.7	P+0.6	
-4.6			C15.3	C1.0	4.7	B.T	F27		
-0.6	EW	2.0	56.4	17.0	F0.1	15.0	20.4		
4.0									
5.8									
+0.4			+13.4	5.1	4.9	4.4	7.2	P+0.3	
-4.7			C18.1	B.T		B.T	F25		
-0.3	EW	0.0	61.6	15.0	F0.2	15.0	20.0		
4.4									
0.0									
4.9			+15.4	5.2		7.6			
0.0			C20.3	F0.3		F2.7			
			67.6			20.4			
4.7									
+0.0									
-4.3			+5.2	4.9	4.0	6.9			
-0.3	EW	0.0	DELS	F0.6	B.T	F2.9			
4.0			25.2		15.0	20.8			
5.1									
+0.7									
-4.4			+4.9	5.3	4.9	7.2			
-0.5	EW	0.5	C0.2	F0.9	F1.0	F3.3			
3.9			25.1		15	21.6			
5.3									
6.0									
-4.4			+5.0	4.9	4.7	7.8			
-0.7	EW	2.1	DC0.5	F0.5	B.T	F4.1			
3.7			23.3		15	23.2			
6.4									
+0.9			+14.2	5.4	4.7	3.8	6.0		
-4.5			C18.7	C1.0		B.T	F2.5		
-0.7	EW	2.0	62.9	17.1	F0.2	15.0	20.0		
3.8									
5.9									
+1.0			+6.9	4.9	4.8	4.1	7.1		
-4.9			C11.8	C1.0		B.T	F3.5		
-0.5	EW	2.0	48.6	17.0	C0.1	15.0	22.0		
4.1									

Spine 12" Willow 20' Ld Sta 53+2.5

Sta	+	π	-	Elev.	L
		919.38			KN M B S A E
33+75				14.5	
34				14.4	
+50				14.3	
35				14.3	
+50				14.2	
36				14.1	
T.P.	3.92	918.83	4.47	914.91	Tree - Rt.
+50				14.0	
+95				13.9	
37				13.9	
+50				13.9	
38				13.8	
+50				13.7	

G. R.

$\begin{array}{r} 5.6 \\ +0.7 \\ 4.9 \\ -0.5 \\ 4.4 \end{array}$ E.W. 1.7 $\begin{array}{r} 1.7 \\ 44.3 \end{array}$ $\begin{array}{r} 4.3 \\ 4.6 \\ 4.8 \\ 4.4 \\ 4.1 \end{array}$ $\begin{array}{r} 4.4 \\ 4.1 \\ 4.1 \\ 4.1 \end{array}$ $\begin{array}{r} 6.8 \\ 2.4 \\ 19.8 \end{array}$ P + 0.5

$\begin{array}{r} 5.8 \\ +0.8 \\ 5.0 \\ -0.6 \\ 4.4 \end{array}$ E.W. 1.2 $\begin{array}{r} 1.2 \\ 30.4 \end{array}$ $\begin{array}{r} 3.1 \\ 3.8 \\ 4.8 \\ 4.4 \\ 3.7 \end{array}$ $\begin{array}{r} 3.8 \\ 4.8 \\ 4.4 \\ 3.7 \\ 3.7 \end{array}$ $\begin{array}{r} 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \\ 7.3 \end{array}$ P + 0.6

$\begin{array}{r} 5.6 \\ +0.5 \\ 5.1 \\ -0.3 \\ 4.8 \end{array}$ E.W. 0.0 $\begin{array}{r} 0.0 \\ 15.0 \end{array}$ $\begin{array}{r} 5.6 \\ 5.6 \\ 5.1 \\ 4.8 \\ 4.8 \end{array}$ $\begin{array}{r} 5.6 \\ 5.6 \\ 5.1 \\ 4.8 \\ 4.8 \end{array}$ $\begin{array}{r} 7.6 \\ 7.6 \\ 7.6 \\ 7.6 \\ 7.6 \end{array}$ P + 0.3

$\begin{array}{r} 0.0 \\ 5.1 \\ 7.1 \end{array}$ $\begin{array}{r} 7.6 \\ 7.6 \\ 7.6 \end{array}$ $\begin{array}{r} 5.3 \\ 5.3 \\ 5.3 \end{array}$ $\begin{array}{r} 7.7 \\ 7.7 \\ 7.7 \end{array}$ P 0.0

$\begin{array}{r} 5.2 \\ 7.2 \end{array}$ $\begin{array}{r} 6.8 \\ 6.8 \\ 6.8 \end{array}$ $\begin{array}{r} 5.0 \\ 5.0 \\ 5.0 \end{array}$ $\begin{array}{r} 7.3 \\ 7.3 \\ 7.3 \end{array}$

$\begin{array}{r} 5.3 \\ 7.3 \end{array}$ $\begin{array}{r} 6.9 \\ 6.9 \\ 6.9 \end{array}$ $\begin{array}{r} 5.0 \\ 5.0 \\ 5.0 \end{array}$ $\begin{array}{r} 6.9 \\ 6.9 \\ 6.9 \end{array}$

$\begin{array}{r} 4.8 \end{array}$ $\begin{array}{r} 7.7 \\ 7.7 \\ 7.7 \end{array}$ $\begin{array}{r} 4.7 \\ 4.7 \\ 4.7 \end{array}$ $\begin{array}{r} 6.5 \\ 6.5 \\ 6.5 \end{array}$

4.9 No Stakes

$\begin{array}{r} 4.9 \end{array}$ $\begin{array}{r} 7.8 \\ 7.8 \\ 7.8 \end{array}$ $\begin{array}{r} 4.9 \\ 4.9 \\ 4.9 \end{array}$ $\begin{array}{r} 6.1 \\ 6.1 \\ 6.1 \end{array}$

$\begin{array}{r} 4.9 \end{array}$ $\begin{array}{r} 7.2 \\ 7.2 \\ 7.2 \end{array}$ $\begin{array}{r} 4.4 \\ 4.4 \\ 4.4 \end{array}$ $\begin{array}{r} 6.1 \\ 6.1 \\ 6.1 \end{array}$

$\begin{array}{r} 0.0 \\ 5.0 \\ 0.0 \end{array}$ $\begin{array}{r} 6.0 \\ 6.0 \\ 6.0 \end{array}$ $\begin{array}{r} 5.0 \\ 5.0 \\ 5.0 \end{array}$ $\begin{array}{r} 4.7 \\ 4.7 \\ 4.7 \end{array}$ $\begin{array}{r} 4.0 \\ 4.0 \\ 4.0 \end{array}$ $\begin{array}{r} 6.0 \\ 6.0 \\ 6.0 \end{array}$

$\begin{array}{r} 5.4 \\ +0.3 \\ 5.1 \\ -0.2 \\ 4.9 \end{array}$ P + 0.2 $\begin{array}{r} 0.2 \\ 25.2 \end{array}$ $\begin{array}{r} 6.2 \\ 6.2 \\ 6.2 \end{array}$ $\begin{array}{r} 4.9 \\ 4.9 \\ 4.9 \end{array}$ $\begin{array}{r} 4.7 \\ 4.7 \\ 4.7 \end{array}$ $\begin{array}{r} 4.4 \\ 4.4 \\ 4.4 \end{array}$ $\begin{array}{r} 6.0 \\ 6.0 \\ 6.0 \end{array}$ P - 0.3

Sta	+	π	-	Elev.	
		918.83			
39				13.6	
T.P.	2.83	918.16 ⁴	3.50	915.33	True 41
+50				13.5	
40				13.5	
+50				13.4	
41				13.3	
B.M.	6.81	917.51	7.41	910.75	910.70
+41				13.23	
+55				13.25 ³	
42				13.5	
T.P.	3.48	918.89 ²	2.10	915.41	
+50				13.7	
43				13.9	
+50				14.1	
44				14.4	

G.R.

5.8									
+0.6									
-5.2									
-0.4	EW 2.3	Ditch -2.4	6.1	4.8	4.7	4.8	4.5	P - 0.6	
4.8			26.0	15	CO.5	15.3	23.5	EW 0.3	
-5.6									
+0.9									
-4.7									
-0.7	EW 2.5	Ditch -2.7	5.4	4.0	4.0	4.6	5.7	P - 0.9	
4.0			27.0	15	CO.7	17.5	25.7	EW 2.5	
5.8									
+1.1									
-4.7									
-0.9	EW 3.7	Ditch -2.9	6.4	3.8	4.4	4.8	6.2	P - 1.1	
3.8			25.4	15	CO.3	18.7	25.6	EW 3.7	
5.8									
+1.0									
-4.8									
-0.8	EW 3.7	Ditch -2.8	4.8	4.0	5.1	5.8	7.2	P - 1.0	
4.0			24.6	15	FO.3	18.7	21.5	EW 3.7	
5.7									
+0.8									
-4.9									
-0.6	EW 1.8		6.4	4.3	5.6	5.7	7.5	P - 0.8	
4.3			17.2	15	FO.7	16.8	20.4	EW 1.8	

S. E. Cor. Spillway

4.2									
4.4									
+0.4									
-0.4									
3.6									
5.6									
+0.4									
-5.2									
-0.4									
4.8									
5.3									
+0.3									
-5.0									
-0.3									
4.7									
5.0									
+0.2									
-4.8									
-0.2									
4.6									
0.0									
4.5									
0.0									

Sta.	+	π	-	Elev.
		918.89		
44 + 50				14.5
45				14.7
+ 50				14.8
T.P.	4.63	919.76 ⁸	3.76	915.13
46				14.9
+ 50				14.9
47				15.0
+ 50				15.0
48				15.1
+ 50				15.1
49				15.2
+ 50				15.2
50				15.3

Easement

G. R.

4.4	$\begin{array}{r} 6.9 \\ F2.5 \\ \hline 20.0 \end{array}$	$\begin{array}{r} 4.5 \\ F0.1 \\ \hline \end{array}$	$\begin{array}{r} 5.7 \\ D0.7 \\ \hline 24.4 \end{array}$
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4.2	$\begin{array}{r} 2.3 \\ C0.9 \\ \hline 28.8 \end{array}$	$\begin{array}{r} 4.0 \\ C0.2 \\ \hline \end{array}$	$\begin{array}{r} 4.9 \\ D0.3 \\ \hline 25.4 \end{array}$
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4.1	$\begin{array}{r} +5.3 \\ C9.4 \\ \hline 45.8 \end{array}$	$\begin{array}{r} 3.6 \\ C0.5 \\ \hline \end{array}$	$\begin{array}{r} 3.7 \\ C0.4 \\ \hline 27.8 \end{array}$
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4.9	$\begin{array}{r} +1.3 \\ C0.2 \\ \hline 30.4 \end{array}$	$\begin{array}{r} 4.6 \\ C0.3 \\ \hline \end{array}$	$\begin{array}{r} 3.9 \\ C1.0 \\ \hline 29 \end{array}$
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4.9	$\begin{array}{r} 3.6 \\ C1.3 \\ \hline 29.6 \end{array}$	$\begin{array}{r} 4.6 \\ C0.3 \\ \hline \end{array}$	$\begin{array}{r} 6.4 \\ D0.5 \\ \hline 24.0 \end{array}$
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4.8	$\begin{array}{r} 5.9 \\ D0.9 \\ \hline 24.8 \end{array}$	$\begin{array}{r} 4.8 \\ C0.0 \\ \hline \end{array}$	$\begin{array}{r} 7.2 \\ F2.4 \\ \hline 19.0 \end{array}$
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4.8	$\begin{array}{r} 7.3 \\ F2.5 \\ \hline 20.0 \end{array}$	$\begin{array}{r} 4.8 \\ C0.0 \\ \hline \end{array}$	$\begin{array}{r} 7.6 \\ F2.8 \\ \hline 20.6 \end{array}$
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4.7	$\begin{array}{r} 7.6 \\ F2.9 \\ \hline 20.8 \end{array}$	$\begin{array}{r} 4.9 \\ F0.2 \\ \hline \end{array}$	$\begin{array}{r} 7.4 \\ F2.7 \\ \hline 20.4 \end{array}$
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4.7	$\begin{array}{r} 8.3 \\ F3.6 \\ \hline 22.2 \end{array}$	$\begin{array}{r} 4.9 \\ F0.2 \\ \hline \end{array}$	$\begin{array}{r} 7.4 \\ F2.7 \\ \hline 20.4 \end{array}$
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4.6	$\begin{array}{r} 8.3 \\ F3.7 \\ \hline 22.4 \end{array}$	$\begin{array}{r} 5.0 \\ F0.4 \\ \hline \end{array}$	$\begin{array}{r} 6.9 \\ F2.3 \\ \hline 19.6 \end{array}$
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4.6	$\begin{array}{r} 8.6 \\ F4.0 \\ \hline 23.0 \end{array}$	$\begin{array}{r} 5.3 \\ F0.7 \\ \hline \end{array}$	$\begin{array}{r} 7.4 \\ F2.8 \\ \hline 20.6 \end{array}$
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4.5	$\begin{array}{r} 8.5 \\ F4.0 \\ \hline 23.0 \end{array}$	$\begin{array}{r} 5.3 \\ F0.8 \\ \hline \end{array}$	$\begin{array}{r} 7.5 \\ F3.0 \\ \hline 21.0 \end{array}$
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G.R.

4.5 $\begin{array}{r} 8.7 \\ F4.2 \\ \hline 23.4 \end{array}$ $\begin{array}{r} 5.2 \\ F0.7 \\ \hline \end{array}$ $\begin{array}{r} 7.4 \\ F2.9 \\ \hline 20.8 \end{array}$

4.4 $\begin{array}{r} 8.2 \\ F3.8 \\ \hline 22.6 \end{array}$ $\begin{array}{r} 5.2 \\ F0.8 \\ \hline \end{array}$ $\begin{array}{r} 7.5 \\ F3.1 \\ \hline 21.2 \end{array}$

4.3 $\begin{array}{r} 8.4 \\ F4.1 \\ \hline 23.2 \end{array}$ $\begin{array}{r} 5.2 \\ F0.9 \\ \hline \end{array}$ $\begin{array}{r} 7.5 \\ F3.2 \\ \hline 21.4 \end{array}$

4.3 $\begin{array}{r} 8.1 \\ F3.8 \\ \hline 22.6 \end{array}$ $\begin{array}{r} 5.0 \\ F0.7 \\ \hline \end{array}$ $\begin{array}{r} 7.3 \\ F3.0 \\ \hline 21.0 \end{array}$

4.2 $\begin{array}{r} 6.8 \\ F2.6 \\ \hline 20.2 \end{array}$ $\begin{array}{r} 3.9 \\ C0.3 \\ \hline \end{array}$ $\begin{array}{r} 6.5 \\ F2.3 \\ \hline 19.6 \end{array}$

4.3 4.3 4.2 2.9 3.2 3.3
+0.0 $\begin{array}{r} 21.9 \\ \hline 26.8 \end{array}$ $\begin{array}{r} 8.7 \\ \hline 15 \end{array}$ $\begin{array}{r} 2.9 \\ C1.3 \\ \hline \end{array}$ $\begin{array}{r} 3.2 \\ C1.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 3.3 \\ C0.9 \\ \hline 28.8 \end{array}$

9.7 *Ditch-2.3*
+0.5 $\begin{array}{r} 6.2 \\ C2.7 \\ \hline 33.6 \end{array}$ $\begin{array}{r} 6.9 \\ C2.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 6.9 \\ C2.3 \\ \hline \end{array}$ $\begin{array}{r} 6.7 \\ C3.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 4.5 \\ C5.2 \\ \hline 35.4 \end{array}$ *Ditch-1.5*
9.2 E.W. 0.0 P-0.5
-0.3 W 0.0

10.0 *Ditch*
+0.8 $\begin{array}{r} 1.6 \\ C7.0 \\ \hline 43.4 \end{array}$ $\begin{array}{r} 6.6 \\ C3.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 5.7 \\ C3.5 \\ \hline \end{array}$ $\begin{array}{r} 6.0 \\ C4.0 \\ \hline 16.3 \end{array}$ $\begin{array}{r} 1.0 \\ C9.0 \\ \hline 43.1 \end{array}$ *Ditch-1.2*
9.2 E.W. 1.3 P-0.8
-0.6 W 1.3

8.6 *Ditch*
10.1 $\begin{array}{r} 6.3 \\ C14.6 \\ \hline 39.4 \end{array}$ $\begin{array}{r} 5.3 \\ C3.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 5.1 \\ C4.0 \\ \hline \end{array}$ $\begin{array}{r} 5.1 \\ C5.0 \\ \hline 17.7 \end{array}$ $\begin{array}{r} +3.1 \\ C13.2 \\ \hline 52.1 \end{array}$ *Ditch-1.0*
+1.0 E.W. 2.7 P-1.0
9.1 W 2.7

-0.8 *Ditch*
8.3 $\begin{array}{r} 10.6 \\ C19.6 \\ \hline 49.8 \end{array}$ $\begin{array}{r} 4.2 \\ C4.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 4.6 \\ C4.5 \\ \hline \end{array}$ $\begin{array}{r} 5.1 \\ C5.0 \\ \hline 17.7 \end{array}$ $\begin{array}{r} +4.5 \\ C14.6 \\ \hline 54.9 \end{array}$ *Ditch-1.0*
10.1 E.W. 2.7 P-1.0
+1.0 W 2.7

9.1 *Ditch*
-9.0 $\begin{array}{r} 10.6 \\ C19.6 \\ \hline 49.4 \end{array}$ $\begin{array}{r} 5.2 \\ C3.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 5.2 \\ C3.8 \\ \hline \end{array}$ $\begin{array}{r} 5.0 \\ C5.0 \\ \hline 17.7 \end{array}$ $\begin{array}{r} -2.7 \\ C7.3 \\ \hline 40.3 \end{array}$ *Ditch*
8.2 E.W. 2.7 P-1.0
10.0 W -2.7

+1.0 *Ditch*
9.0 $\begin{array}{r} 10.6 \\ C19.6 \\ \hline 49.4 \end{array}$ $\begin{array}{r} 5.2 \\ C3.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 5.2 \\ C3.8 \\ \hline \end{array}$ $\begin{array}{r} 5.0 \\ C5.0 \\ \hline 17.7 \end{array}$ $\begin{array}{r} -2.7 \\ C7.3 \\ \hline 40.3 \end{array}$ *Ditch*
-0.8 E.W. 2.7 P-1.0
8.2 W -2.7

7.4 *Ditch*
+0.8 $\begin{array}{r} 5.0 \\ C10 \\ \hline 31.4 \end{array}$ $\begin{array}{r} 4.0 \\ C2.0 \\ \hline 15 \end{array}$ $\begin{array}{r} 3.8 \\ C2.8 \\ \hline \end{array}$ $\begin{array}{r} 4.4 \\ C3.0 \\ \hline 16.3 \end{array}$ $\begin{array}{r} 6.4 \\ C1.0 \\ \hline 27.1 \end{array}$ *Ditch*
6.9 E.W. 1.3 P-0.8
-0.2 W 1.3

Sta	+	+	-	Elev.	
		922.37			
56				15.9	
+40				15.9	
+72				16.0	
B.M.	4.81	921.24	5.86	916.51	916.43
57				16.0	
+20				16.0	
+50				16.0	
B.M.					916.43
58				16.0	
+50				16.0	
59				16.0	
+38				16.0	
	4.50	920.53	5.21	916.03	
60				16.0	
+25				16.0	
+50				16.0	

EASEMENT

G. R.

+0.0
6.5
-0.0 E.W. 0.0

7.7	5.5	5.1	6.5	10.3
DC0.8	C1.0	C1.4	B.T	F3.8
24.6	15	15	15	22.6

7.1
+0.6
6.5
-0.4 E.W. 0.3

5.8	6.1	5.5	7.1	8.8
DC0.6	B.T	C1.0	B.T	F1.5
24.8	15	15.3	18.3	

Pitch 2.4

P-0.6
E.W. 0.2

7.2
+0.8
6.4
-0.6 E.W. 1.6

7.7	5.8	5.7	7.2	9.7
DC0.7	B.T	C0.7	B.T	F2.5
25.6	15	16.6	21.6	

P-0.8
E.W. 1.6

6.2
+1.0
5.2
-0.8 E.W. 2.9

8.9	4.8	5.0	6.2	7.6
F4.1	B.T	C0.2	B.T	F3.4
23.2	15	17.9	24.7	

E.W. 2.9

4.8
6.2
+1.0
5.2
-0.9 E.W. 3.1

9.3	4.3	5.3	6.2	9.5
F5.0	B.T	F0.1	B.T	F3.3
25.0	15	18.1	24.7	

E.W. 3.1

6.2
+1.0
5.2
-0.9 E.W. 3.1

7.1	4.3	5.3	6.2	8.5
DC0.1	B.T	F0.1	B.T	F2.3
24.6	15	18.1	22.7	

E.W. 3.1

Spike in 12" Pop 8' Lt 5' 57 + 70

4.3
+1.0
5.2
-0.9 E.W. 3.1

11.4	4.3	5.0	6.2	8.2
C6.6	B.T	C0.2	B.T	F2.0
43.8	15	18.1	22.1	

E.W. 3.1

6.1
+1.0
5.2
-0.9 E.W. 3.1

10.1	4.3	5.1	6.2	7.0
C5.3	B.T	C0.1	B.T	F2.8
41.2	15	18.1	23.7	

E.W. 3.1

6.1
+0.9
5.2
-0.7 E.W. 2.6

5.9	4.5	5.4	6.1	7.2
DC1.3	B.T	F0.2	B.T	F3.1
27.0	15	17.6	23.8	

E.W. 2.6

4.5
+0.0
5.2
-0.0 E.W. 0.0

3.3	5.2	5.2	5.2	9.0
C8.5	B.T	F0.0	B.T	F3.8
44.0	15.0	15.0	15.0	22.6

5.5
+0.8
4.7
-0.6 E.W. 2.4

5.5	5.5	4.5	6.1	6.1
DC1.2	B.T	C0.2	B.T	DC0.6
26.2	17.4	15	25.4	

Pitch 2.6

5.7
+1.0
4.7
-0.8 E.W. 3.6

6.7	26.2	17.4	4.5	5.6
DC0.0	C1.1	C0.0	C0.2	DC1.1
24.6	18.6	15.2	22.8	

Pitch 2.8

3.9
+1.1
4.7
-0.9 E.W. 4.8

8.0	5.6	4.8	5.0	5.0
F2.2	B.T	F0.1	DC1.7	DC1.7
24.2	19.8		28.2	

Pitch 2.9

Sta.	+	π	-	Elev
		920.53		
60+75				16.0
+85				16.0
61				16.0
T.P.	4.21	918.94	5.80	914.73
+38				16.0
+50				16.0
+75				16.0
62				16.0
+50				16.0
63				16.0
+50				16.0
64				16.0
+50				16.0
65				16.0
T.P.	6.77	919.21	6.50	912.44

G. R.

5.8
+1.1
4.7
-0.9
3.8
E.W. 4.7
82
F2.4
24.5
5.8
B.T.
19.7
5.9
F1.2
4.7
DC0.0
24.8
Ditch
2.9

+1.1
-0.9
E.W. 4.8
No status
Ditch
2.9

5.8
+1.1
4.7
-0.9
3.8
E.W. 4.8
83
F2.5
14.8
5.8
B.T.
19.8
8.2
F3.5
4.4
DC0.3
31.2
Ditch
2.9

4.2
+1.1
3.1
-0.9
2.2
E.W. 4.8
6.9
F2.7
25.2
4.2
B.T.
19.8
6.5
F3.4
3.9
DC1.2
27.2
Ditch
2.9

4.2
+1.1
3.1
-0.9
2.2
E.W. 4.8
6.8
F2.6
25.0
4.2
B.T.
19.8
4.8
F1.7
4.8
DC0.4
25.6
Ditch
2.9

4.1
3.1
-0.8
2.3
E.W. 4.4
4.2
F2.7
24.8
4.1
B.T.
19.4
7.0
4.1
B.T.
18.9
4.5
F1.4
4.9
F1.8
2.2
B.T.
15.0
3.3
F1.0
15.0
7.3
F5.0
25.0

3.7
+0.6
3.1
-0.4
2.7
E.W. 0.4
7.7
F4.0
23.4
5.7
F2.0
15.4
6.2
F3.1
5.7
F3.0
15
8.3
F5.6
26.2

3.4
+0.3
3.1
-0.1
3.0
E.W. 0.0
7.7
F4.3
23.6
6.4
F3.3
8.0
F5.0
25.0

0.0
3.1
-0.0
E.W. 0.0
7.7
F4.6
24.2
6.1
F2.9
7.8
F4.7
24.4

3.1
7.7
F4.6
24.2
5.8
F2.7
7.8
F4.7
24.4

3.1
7.7
F4.8
24.6
6.1
F3.0
8.2
F5.1
25.2

3.1
8.4
F5.3
25.6
6.4
F3.3
7.9
F4.8
24.6

Sta	+	π	-	Elev.
		919.21		
65	+50			16.0
66				16.0
	+50			16.0
67				16.1
	+50			16.4
68				16.8
T.P.	7.56	924.44	2.33	916.88
	+50			17.4
69				18.2
	+50			19.2
70				20.2
	+37			21.0
71				22.3
T.P.	6.15	929.51	1.08	923.36

EASEMENT

G.R.

3.3

7.8
F4.5
24.0

5.7
F2.4

8.1
F4.8
24.6

3.3

7.7
F4.4
23.8

4.8
F1.5

7.9
F4.6
24.2

3.3

7.3
F4.0
23.0

4.4
F1.1

6.9
F3.6
22.2

3.2

7.0
F3.8
22.6

3.4
F0.2

6.4
F3.2
21.4

2.9

6.6
F3.7
22.4

2.8
C0.1

4.0
C0.9
24.8

2.5

6.6
F4.1
22.2

2.4
C0.1

+1.0
C3.5
33

7.2

11.9
F4.7
24.4

7.3
F0.1

8.2
C1.0
25.0

6.4

11.3
F4.9
24.8

6.6
F0.2

8.4
C0.0
23.0

5.4

7.4
F2.0
19.0

5.5
F0.1

3.5
C1.9
30.8

0.0
4.4
0.0

E.W.O.O

6.4
C0.0
23.0

4.3
C0.1

3.9
C0.5
28

3.9

+0.3
3.6
-0.2

E.W.O.O

21.6
2.2

4.3
F0.9
16.8

3.4
B.T
15.0

3.3
C0.3

3.9
B.T
15

4.5
C1.1
24.6

21.6
1.7

E.W.O.O

3.4
3.0

+0.7
2.3
-0.5
1.8

E.W.O.O

6.4
F4.6
24.2

1.8
B.T
15.0

1.8
C0.5

2.0
C1.0
15.6

+11.7
C14.0
52.8

21.6
1.2

E.W.O.O

Sta	+	⌞	-	Elev.	EASEMENT
		929.51			
71+50				23.4	
72				24.4	
+50				25.5	
73				26.5	
+50				27.6	
T.P.	13.56	941.14	1.93	927.58	
74				28.6	
+50				29.7	EASEMENT
+75				30.2	
+99				130.7	
B.M.			12.23	928.91	
					928.84

G.R.

7.2

+1.0

6.2

-0.8

5.4

6.3

+1.1

5.2

-0.9

4.3

5.1

+1.0

4.1

-0.8

3.3

3.8

+0.7

3.1

-0.5

2.6

2.3

+0.3

2.0

-0.2

1.8

+0.0

12.6

-0.0

11.6

11.1

10.6

Spike 18" Oak S.W. Cor. J & Bald Eagle

E.W. 3.2

E.W. 3.4

E.W. 3.2

E.W. 0.6

E.W. 0.0

E.W. 0.0

7.5	5.4	5.9	5.2
<u>F4.1</u>	<u>B.T</u>	<u>C0.3</u>	<u>C2.0</u>
29.2	15		18.2

5.7	4.3	4.7	3.3
<u>F1.5</u>	<u>B.T</u>	<u>C0.5</u>	<u>C3.0</u>
27.8	15.0		18.4

8.3	3.3	4.2	3.1
<u>F5.0</u>	<u>B.T</u>	<u>F0.1</u>	<u>C2.0</u>
25.0	15.0		18.2

6.4	2.6	3.3	3.8
<u>F3.8</u>	<u>B.T</u>	<u>F0.2</u>	<u>B.T</u>
22.6	15		15.6

2.9	1.8	2.4	2.3
<u>F2.1</u>	<u>B.T</u>	<u>F0.4</u>	<u>B.T</u>
25.6	15		15.0

14.0	13.0	9.7
<u>F0.6</u>	<u>F0.4</u>	<u>C2.9</u>
24.2		32.8

11.5	3.4
<u>C0.1</u>	<u>C8.2</u>
	43.4

10.8	0.3
<u>C0.3</u>	<u>C10.8</u>
	48.6

10.1	2.8
<u>C0.0</u>	<u>C7.8</u>
	33.0

11.6
<u>C8.8</u>
43.8

Ditch-1.0
E.W. 3.2

10.7
<u>C3.6</u>
37.2

Ditch-0.9
E.W. 3.4

3.3
<u>C1.8</u>
19.8

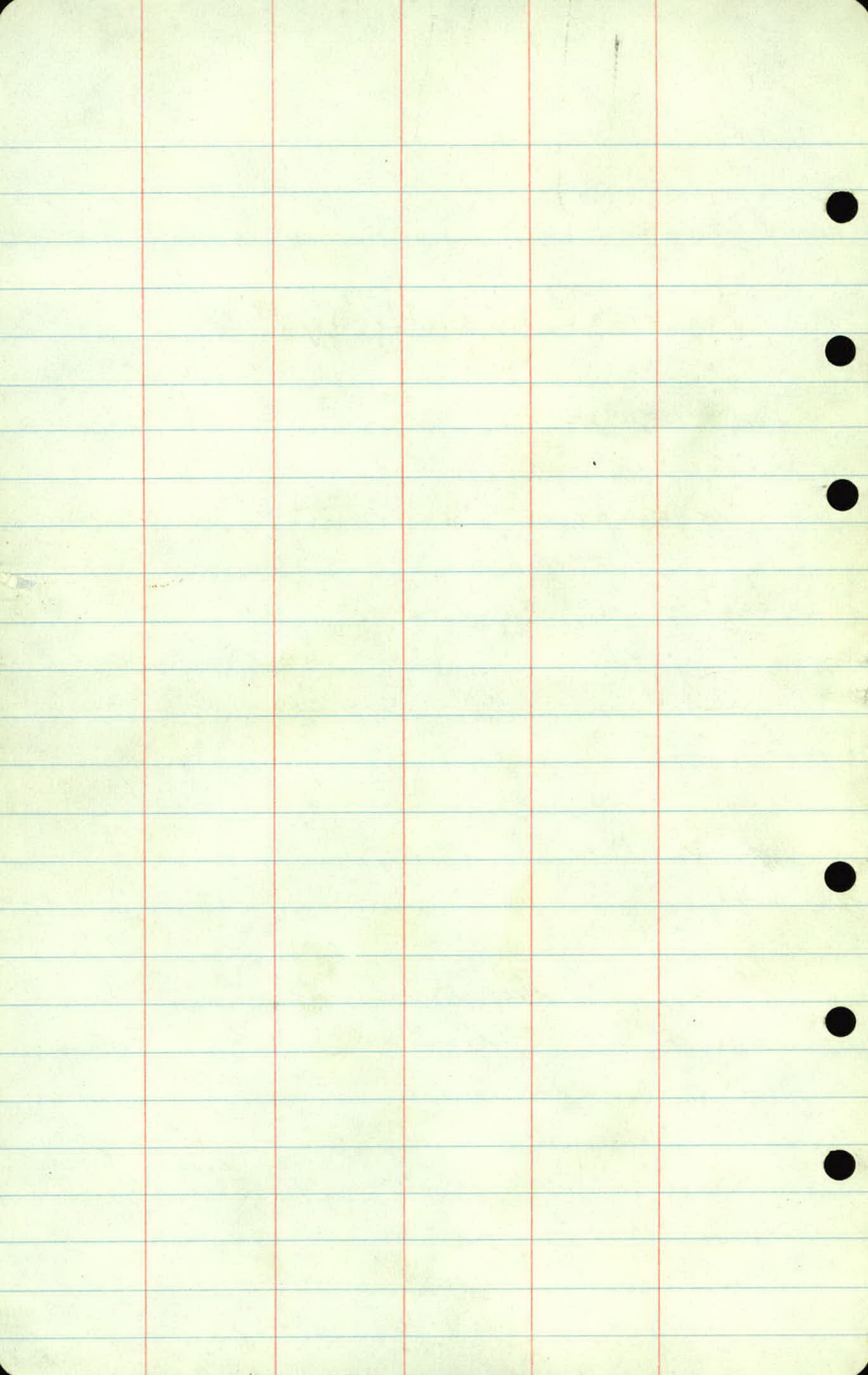
Ditch-1.0
E.W. 3.2

4.6
<u>F0.7</u>
23.6

Ditch-1.3
E.W. 0.6

3.9
<u>F0.1</u>
22.6

Ditch-1.1
E.W. 0.0



Bald Eagle Blvd. W.

Blue Tops

B.M.

4.42

928.84

928.91

74+99

30.7

+50

29.7

74

28.6

T.P.

6.05

933.33

1.67

927.28

1.7

+50

27.6

+0.3
1.4
-0.2
1.2
3.2
+0.7
2.5
-0.5
2.0

73

26.5

+84.67

26.2

5.6
+0.8
2.3
-0.6
2.2
4.5
+1.0
3.5
-0.8
2.7

+50

25.5

72

24.4

5.7
+1.8
4.6
-0.9
3.7

+50

23.4

6.6
+1.0
5.6
-0.8
4.8
7.0
+0.8
6.2
0.6
5.6

+22.41

22.8

71

22.3

7.4
+0.7
6.7
-0.5
6.2
7.7
+0.3
7.4
-0.2
7.2

+50

21.6

928.95

Spike 18" Oak S.W. Cor. J - Bald Eagle

$$\begin{array}{r} 2.6 \\ 2.6 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 2.6 \\ 2.6 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 3.6 \\ 3.6 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 3.6 \\ 3.6 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 4.7 \\ 4.7 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 4.7 \\ 4.7 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 1.2 \\ 1.2 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 1.7 \\ 1.7 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 2.0 \\ 2.0 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 3.2 \\ 3.2 \\ \hline 15.6 \end{array}$$

$$\begin{array}{r} 2.2 \\ 2.2 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 3.6 \\ 3.6 \\ \hline 16.7 \end{array}$$

$$\begin{array}{r} 2.7 \\ 2.7 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 2.5 \\ 2.5 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 3.7 \\ 3.7 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 2.7 \\ 2.7 \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 4.8 \\ 4.8 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 4.6 \\ 4.6 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ 5.6 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 6.0 \\ 6.0 \\ \hline 16.9 \end{array}$$

$$\begin{array}{r} 6.2 \\ 6.2 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 6.4 \\ 6.4 \\ \hline 18.6 \end{array}$$

$$\begin{array}{r} 7.2 \\ 7.2 \\ \hline 15 \end{array}$$

T.P.	8.85	928.95	0.61	920.10
------	------	--------	------	--------

70				20.2
----	--	--	--	------

+50				19.2
-----	--	--	--	------

69				18.2
----	--	--	--	------

+50				17.4
-----	--	--	--	------

68				16.8
----	--	--	--	------

+50				16.4
-----	--	--	--	------

67				16.1
----	--	--	--	------

T.P.	4.54	920.71	4.83	916.17
------	------	--------	------	--------

+50				16.0
-----	--	--	--	------

66				16.0
----	--	--	--	------

+50				16.0
-----	--	--	--	------

65				16.0
----	--	--	--	------

+50				16.0
-----	--	--	--	------

		921.00		
--	--	--------	--	--

0.5

$$\frac{0.5}{15}$$

$$\frac{0.5}{15}$$

1.5

$$\frac{1.5}{15}$$

$$\frac{1.5}{15}$$

2.5

$$\frac{2.5}{15}$$

$$\frac{2.5}{15}$$

3.3

$$\frac{3.3}{15}$$

$$\frac{3.3}{15}$$

3.9

$$\frac{3.9}{15}$$

$$\frac{3.9}{15}$$

4.3

$$\frac{4.3}{15}$$

$$\frac{4.3}{15}$$

4.5

$$\frac{4.5}{15}$$

$$\frac{4.5}{15}$$

5.0

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

5.0

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

5.0

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

64

16.0

+50

16.0

63

16.0

+0.3

-0.1

+50

16.0

+0.6

-0.4

+21.5

16.0

+0.8

-0.6

62

16.0

+1.0

-0.8

+75

16.0

+1.0

-0.8

+50

16.0

+1.1

-0.9

+25

16.0

+1.1

-0.9

61

16.0

+1.1

-0.9

+75

16.0

+1.1

-0.9

+50

16.0

6.1

+1.1

-0.9

4.1

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

$$\frac{5.0}{15}$$

E.W. 0.0

$$\frac{5.3}{15}$$

$$\frac{4.9}{15}$$

E.W. 0.4

$$\frac{5.6}{15.4}$$

$$\frac{4.6}{15}$$

E.W. 2.4

$$\frac{5.8}{17.4}$$

$$\frac{4.4}{15}$$

E.W. 3.9

$$\frac{6.0}{18.9}$$

$$\frac{4.2}{15}$$

E.W. 4.4

$$\frac{6.0}{19.4}$$

$$\frac{4.2}{15}$$

E.W. 4.8

$$\frac{6.1}{19.8}$$

$$\frac{4.1}{15}$$

E.W. 4.8

$$\frac{6.1}{19.8}$$

$$\frac{4.1}{15}$$

E.W. 4.8

$$\frac{6.1}{19.8}$$

$$\frac{4.1}{15}$$

E.W. 4.7

$$\frac{4.1}{15}$$

E.W. 4.8

$$\frac{6.1}{19.8}$$

$$\frac{4.1}{15}$$

60+25			16.0	6.0 +1.0 -0.8 4.2 5.8 +0.8 5.0 -0.6 4.4
-------	--	--	------	---

60	P.C.		16.0	0.0 5.3 0.0
----	------	--	------	-------------------

B.M.	2.29	921.00	918.71	
------	------	--------	--------	--

+350			16.0	5.3 0.0
------	--	--	------	------------

+17.69			16.0	+0.9 -5.3 -0.7
--------	--	--	------	----------------------

59			16.0	+0.9 -5.3 -0.7
----	--	--	------	----------------------

+50			16.0	+1.0 5.3 -0.9
-----	--	--	------	---------------------

58			16.0	+1.0 5.3 -0.9
----	--	--	------	---------------------

+50			16.0	+1.0 5.3 -0.9
-----	--	--	------	---------------------

57			16.0	+1.0 5.3 -0.8
----	--	--	------	---------------------

+72.0			16.0	+0.8 5.3 0.6
-------	--	--	------	--------------------

+50			15.9	+0.6 5.3 -0.4
-----	--	--	------	---------------------

56			15.9	0.0 0.0
----	--	--	------	------------

B.M.	2.63	921.34	918.71	
------	------	--------	--------	--

B.M.			4105	917.29
------	--	--	------	--------

$$\begin{array}{r} \text{E.W. 3.6} \\ 6.0 \\ 18.6 \end{array} \qquad \begin{array}{r} 4.2 \\ 15 \end{array}$$

$$\begin{array}{r} \text{E.W. 2.4} \\ 5.8 \\ 17.4 \end{array} \qquad \begin{array}{r} 4.4 \\ 15 \end{array}$$

$$\begin{array}{r} \text{Spike 6" Oak 50' RA 60+40} \\ \text{E.W. 0.0} \\ 5.0 \\ 15 \end{array} \qquad \begin{array}{r} 5.3 \\ 15.0 \end{array}$$

$$\begin{array}{r} \text{E.W. 2.0} \\ 4.6 \\ 15 \end{array} \qquad \begin{array}{r} 6.2 \\ 17.0 \end{array}$$

$$\begin{array}{r} \text{E.W. 2.6} \\ 4.6 \\ 15 \end{array} \qquad \begin{array}{r} 6.2 \\ 17.6 \end{array}$$

$$\begin{array}{r} \text{E.W. 3.1} \\ 4.4 \\ 15 \end{array} \qquad \begin{array}{r} 6.3 \\ 18.1 \end{array}$$

$$\begin{array}{r} \text{E.W. 3.1} \\ 4.4 \\ 15 \end{array} \qquad \begin{array}{r} 6.3 \\ 18.1 \end{array}$$

$$\begin{array}{r} \text{E.W. 3.1} \\ 4.4 \\ 15 \end{array} \qquad \begin{array}{r} 6.3 \\ 18.1 \end{array}$$

$$\begin{array}{r} \text{E.W. 2.9} \\ 4.5 \\ 15 \end{array} \qquad \begin{array}{r} 6.3 \\ 17.9 \end{array}$$

$$\begin{array}{r} \text{E.W. 1.6} \\ 4.7 \\ 15 \end{array} \qquad \begin{array}{r} 6.1 \\ 16.6 \end{array}$$

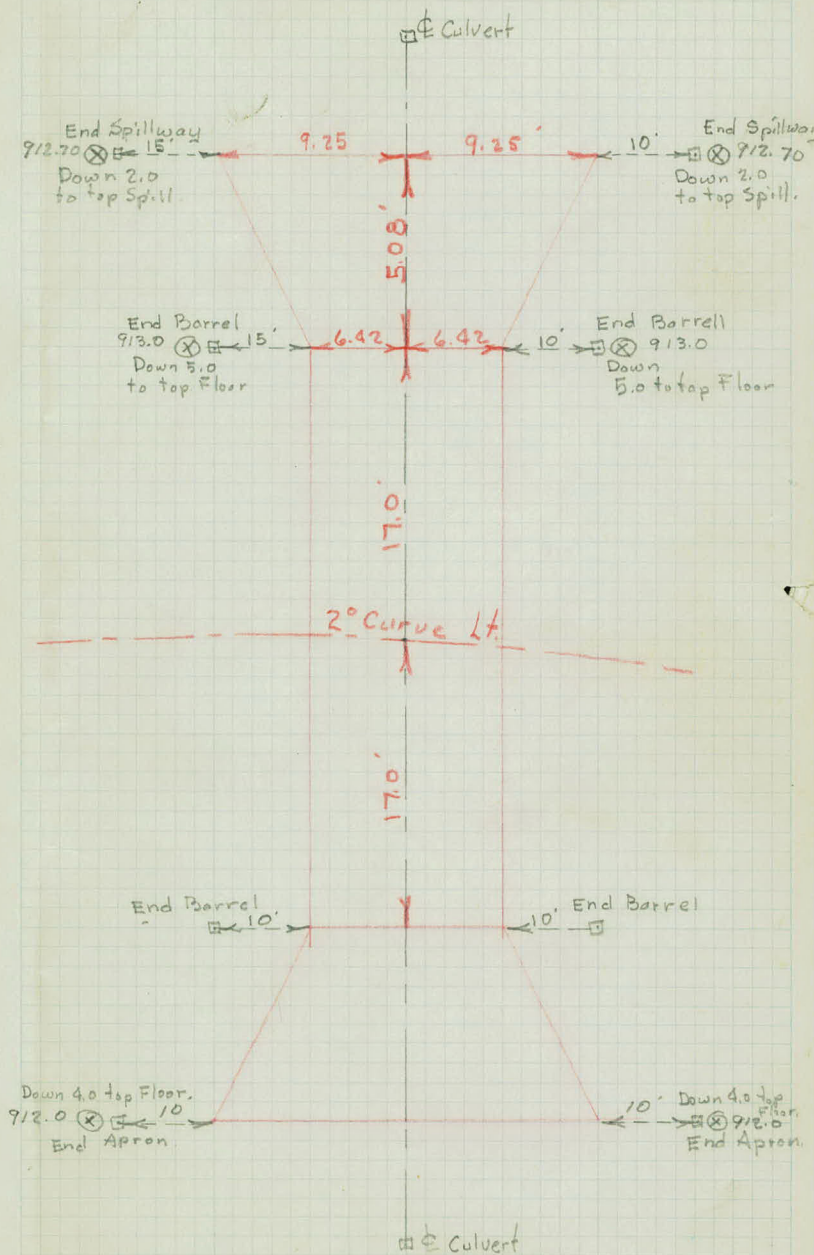
$$\begin{array}{r} \text{E.W. 1.0} \\ 4.0 \\ 15 \end{array}$$

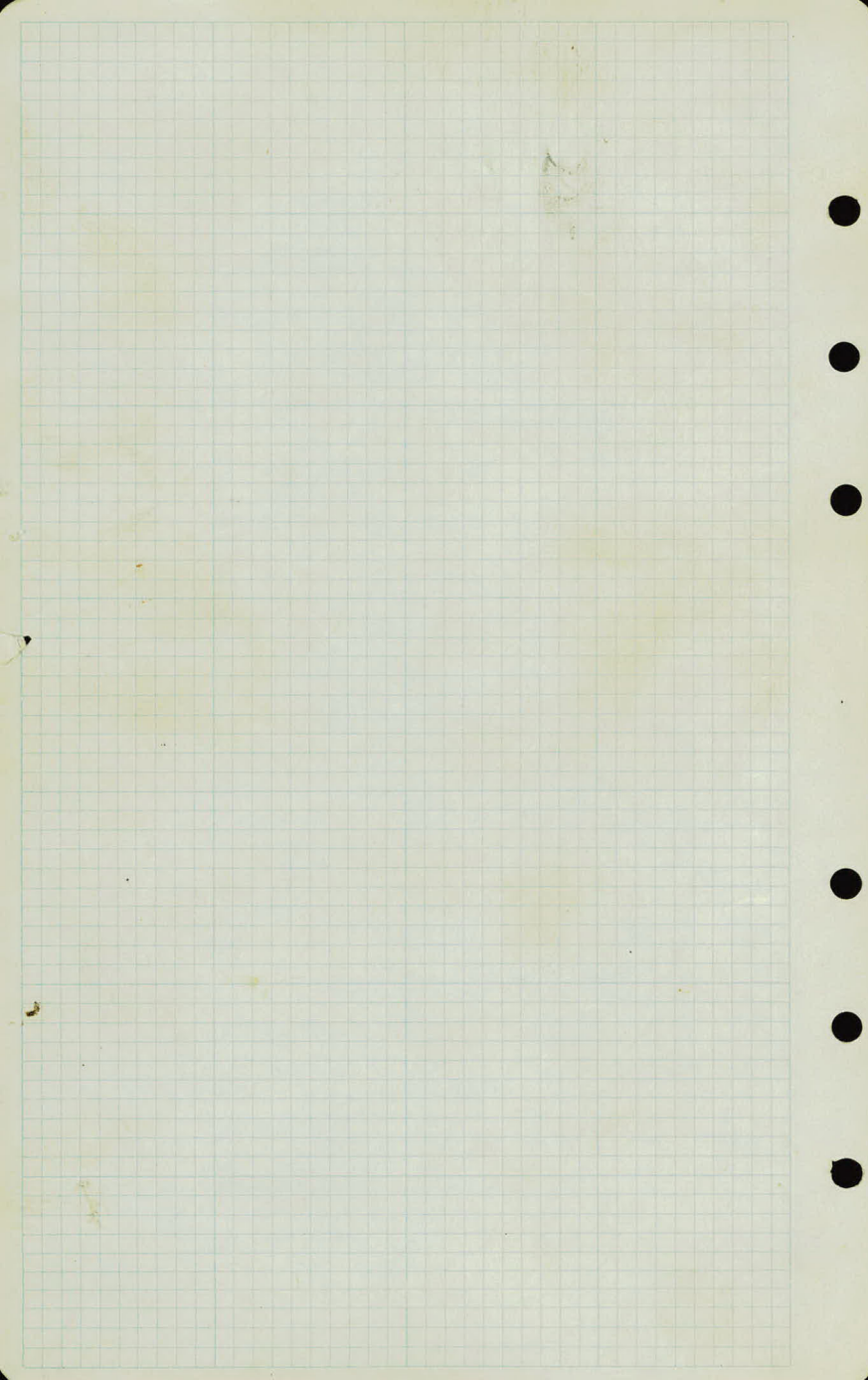
$$\begin{array}{r} \text{E.W. 0.0} \\ 4.0 \\ 15 \end{array}$$

Spike 6" Oak 50' RA 60+40 57+40

Spike 12" Pop 18' LT 56+50

			2.29	918.71
	5.39	921.00	5.50	915.61
T.P	5.18	921.11	7.24	915.93
T.R	0.21	923.17	10.70	922.96
B.M.	4.82	933.66		928.84





Check Levels
of
Bald Eagle Spillway
and
Check of Lake Imp. Datum
against U.S.G.S. Datum

3-22-45

K.A.

G.N.

G.F.

Sta	+	π	-	Elev.
B.M.	3.96	918.47		914.51
Top S End Spillway		7.87		910.60
Top N. End Spillway		7.98		910.49
N.E. Cor. of Headwall		5.10		913.37
S.E. Cor. of Headwall		5.03		913.44
S.W. Cor. of Headwall		4.97		913.50
N.W. Cor. of Headwall		5.05		913.42
Elev. of Otter Lake		6.80		911.67
Elev. of Bald Eagle Lake		6.78		911.69

R.R. Spt. in 8" Pop. No. of Spillway (now 20" Pop.)

Sta	+	π	-	Elev.
B.M.	0.20+	937.42		937.22
	6.88	940.46	3.84	933.58
B.M.	1.77	937.84	4.35	936.11 (936.07)
	0.59	928.82	9.61	928.23
	6.68	927.47	8.035	920.79
			16.28	911.19
B.M.	3.96	924.65	3.96	(920.69)
El. of Bald Eagle Lake			13.45	911.20

Description

This datum from Centerville Rd. ←

Spk in P.P. S.E. Cor. Co. Rd. H 2 & ~~Centerville Rd.~~ ^{Other Lake Rd.}

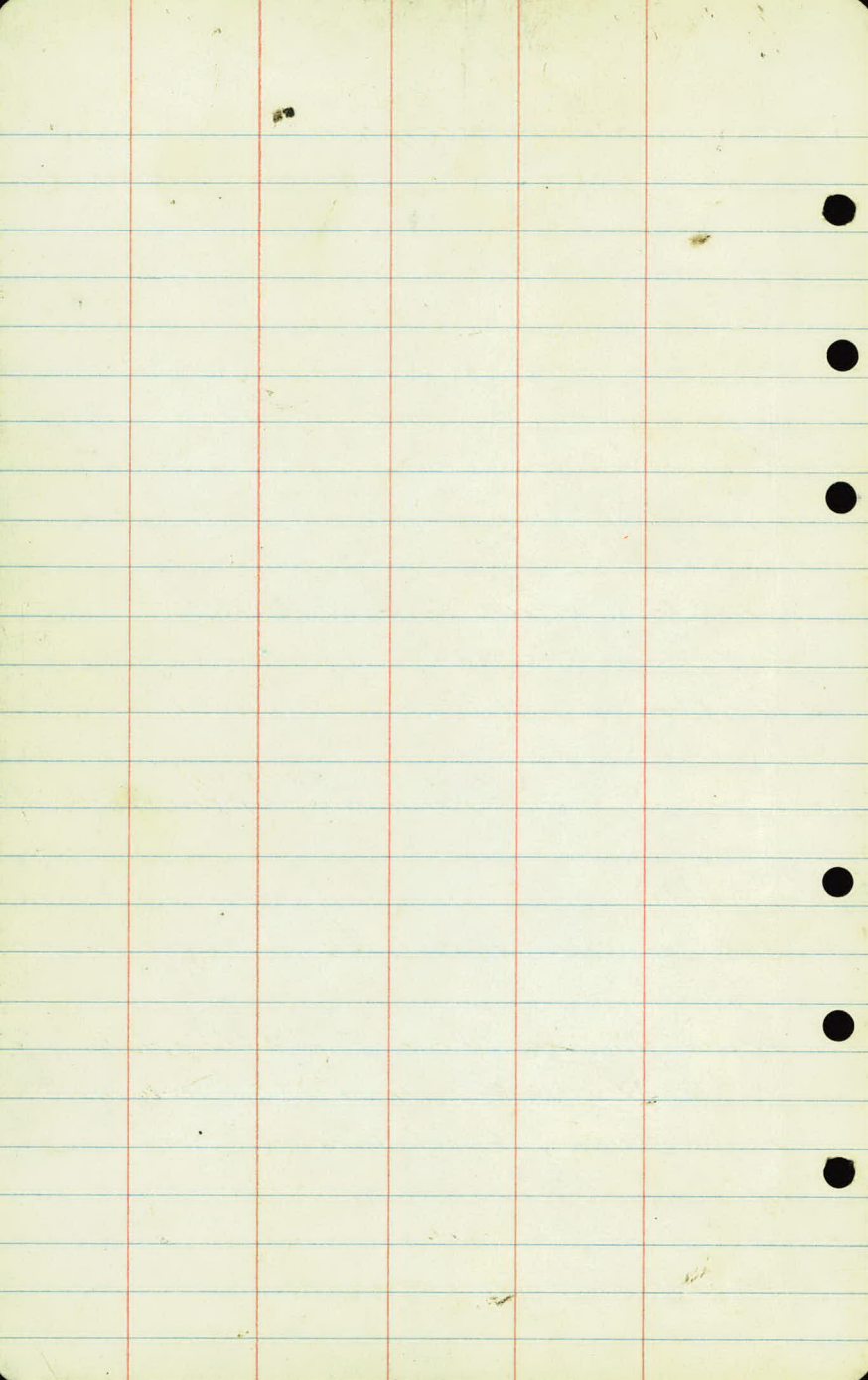
(Co. Rd. H 2 1939 Survey)

Top N.E. Cor. of Conc Base of E Pillar 39' Pt. Sta 4491

Elev. of Bald Eagle Lake. ←

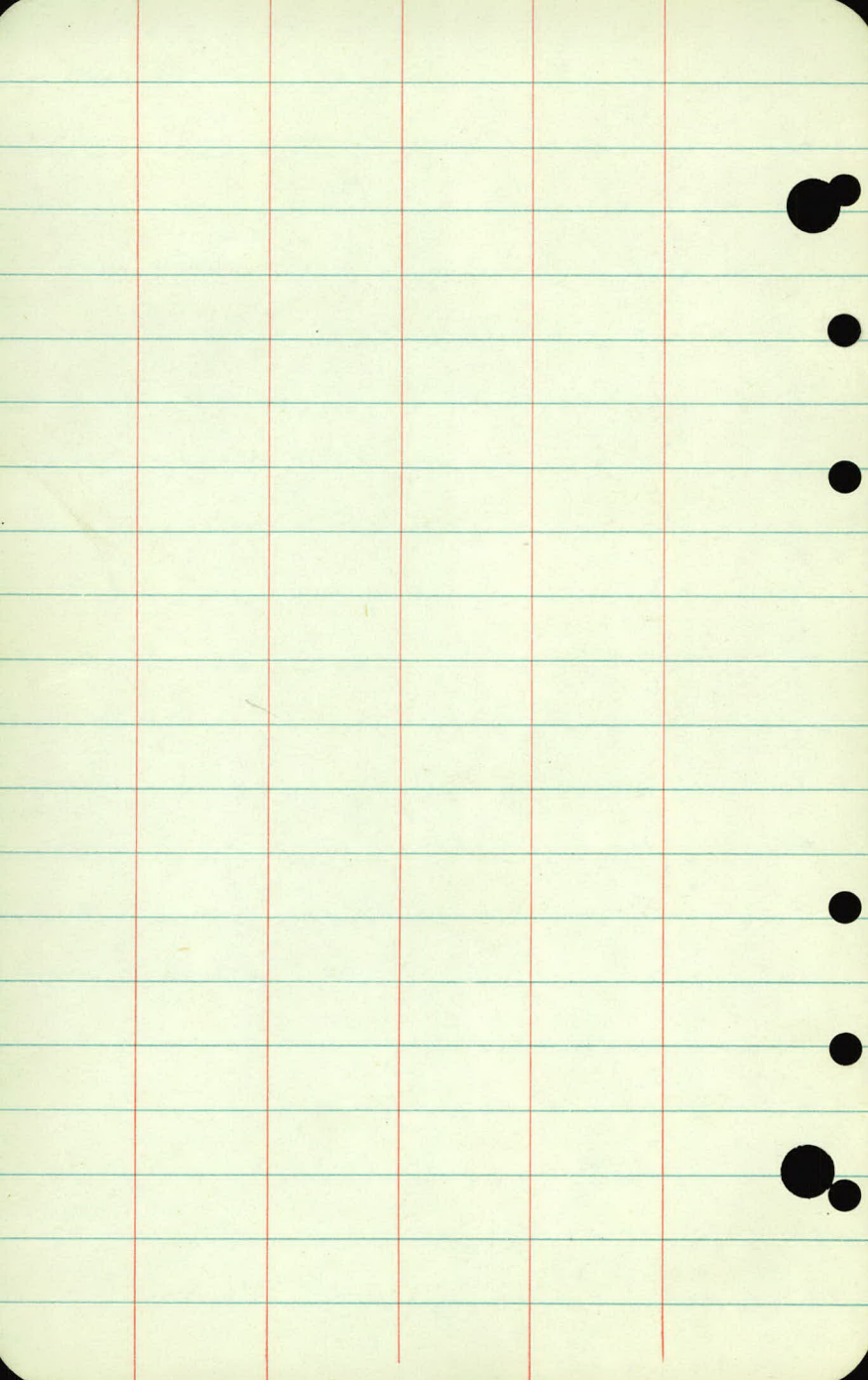
Top of Elbow Pipe at outlet of Bald Eagle Pump Ho.

← This Elev. was run from U.S.G.S. B.M. in
St. Marys School Yard



BALD EAGLE BLVD. WEST

Alinement Change Survey
No actual change
Jk



April 8, 1970

1

New Alinement

Sta 55 to N. Co. Line

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

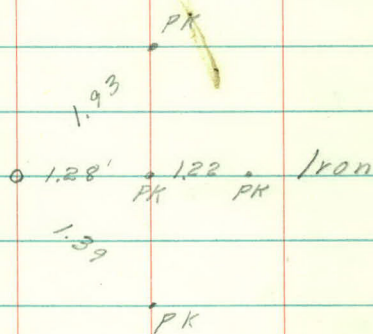
+41.80	P.T.		$\Delta = 24^{\circ} 59'$
55			$\frac{1}{2}\Delta = 12^{\circ} 29' 30''$
+50			$D = 13^{\circ}$
54+47.47	P.I.	$24^{\circ} 59'$	$T = 97.85'$
54			$L = 192.18'$
+50			$R = 441.684'$
53+49.62	P.C.		$E = 11'$

1939 PLAN SURVEY
Stationing

FK
CM

April 8, 1970
Windy

2



Curve
data

R 1145.92'

LT

~~E~~

RT

STA	POINT	ΔL	ΔR	Curve data
-----	-------	------------	------------	------------

$$P.T. = (71+84.19)$$

$$\Delta 24^{\circ} 22.0' R.T.$$

$$D 12^{\circ}$$

$$T 103.08'$$

72+06.12 old P.I. 1934 survey
 $70+88.25 - P.I. =$

$$24^{\circ} 22.0' L 203.06'$$

$$(70+84.21)$$

$$R 477.46'$$

$$P.C. = (69+81.13)$$

$$68+41.68 \quad P.O.T.$$

LT

$\frac{1}{2}$

RT

STA	Point	ALT	ΔRT	curve data
-----	-------	-----	-----	------------

LT

\$

RT

NW Cor Sec. 2

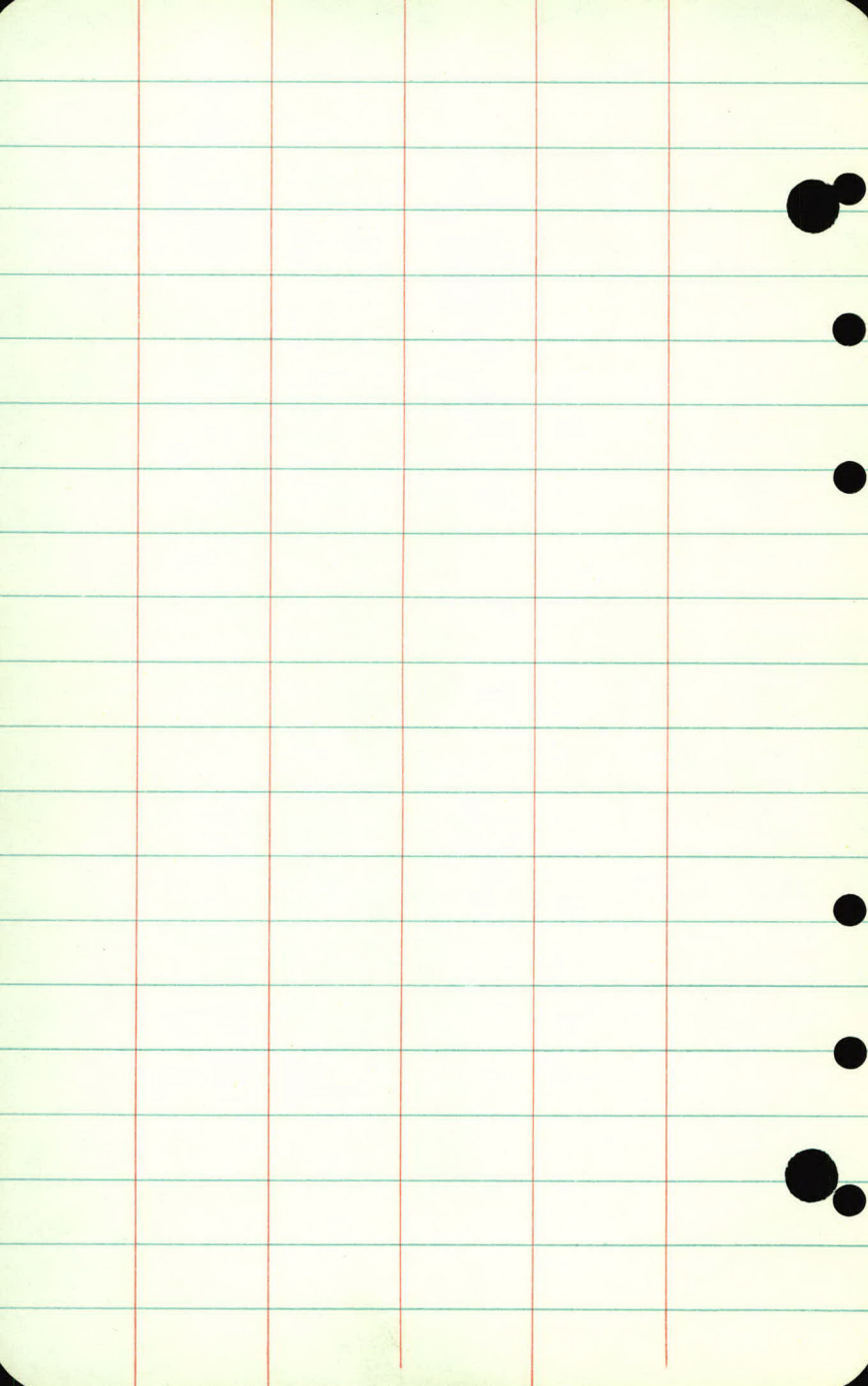
T30N R22W



NORTH
166.32

55° 57.5'

COUNTY LINE RD.



BALD EAGLE BLVD W

NEW ALINEMENT

STA 55 to No. Co. LINE

STA	POINT	ΔL_T	ΔR_T
-----	-------	--------------	--------------

 $54 + 47.47$ P1 $24^{\circ}59.0'$

LT

£

RT

WIC

STA	POINT	ALT	ART
-----	-------	-----	-----

61 + 71.06	PI	19°48.0	5016
------------	----	---------	------

59 + 65.00 POT

LT

E

RT

8" B.E

3N

44.68'

47.04'

IRON

660TT.

3N

Quad 16" Elm

3N

49.42'

28.08'

30" Oak

3N

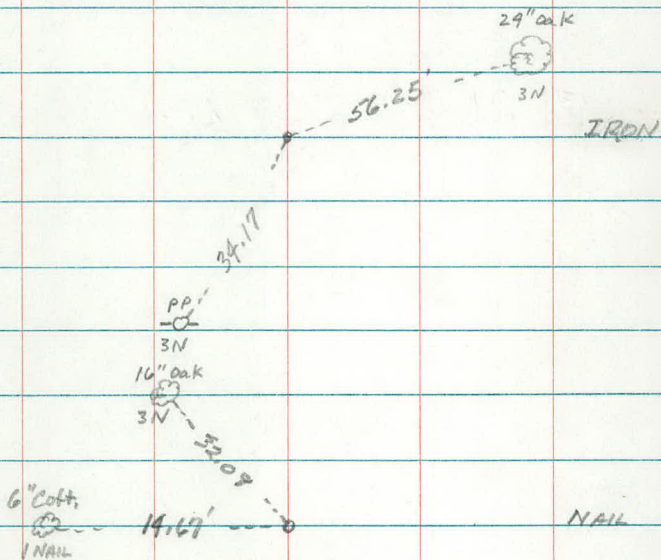
NAIL

STA	POINT	ΔLT	ΔRT
70+88. ²⁵	PI		24°22.0'
68+41. ⁶⁸	POT		

LT

4

RT



STA	POINT	ΔL_T	ΔR_T
73+86.62	PI		

73+86.62 PI = ∇ N. CO. LINE RD

LT

E

RT

SIDE TIE
3N
O
PP

65.72

PK nail

67.08

3N
O
PP

