

BK. 129

BK. 29 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

Edgerton Street

From Larpentel r Ave. Go. Koehler Rd.

Also X-Sections Co. Rd. "D" - North

Read Acc. t. No. 1946

Date Filed 2-11-46

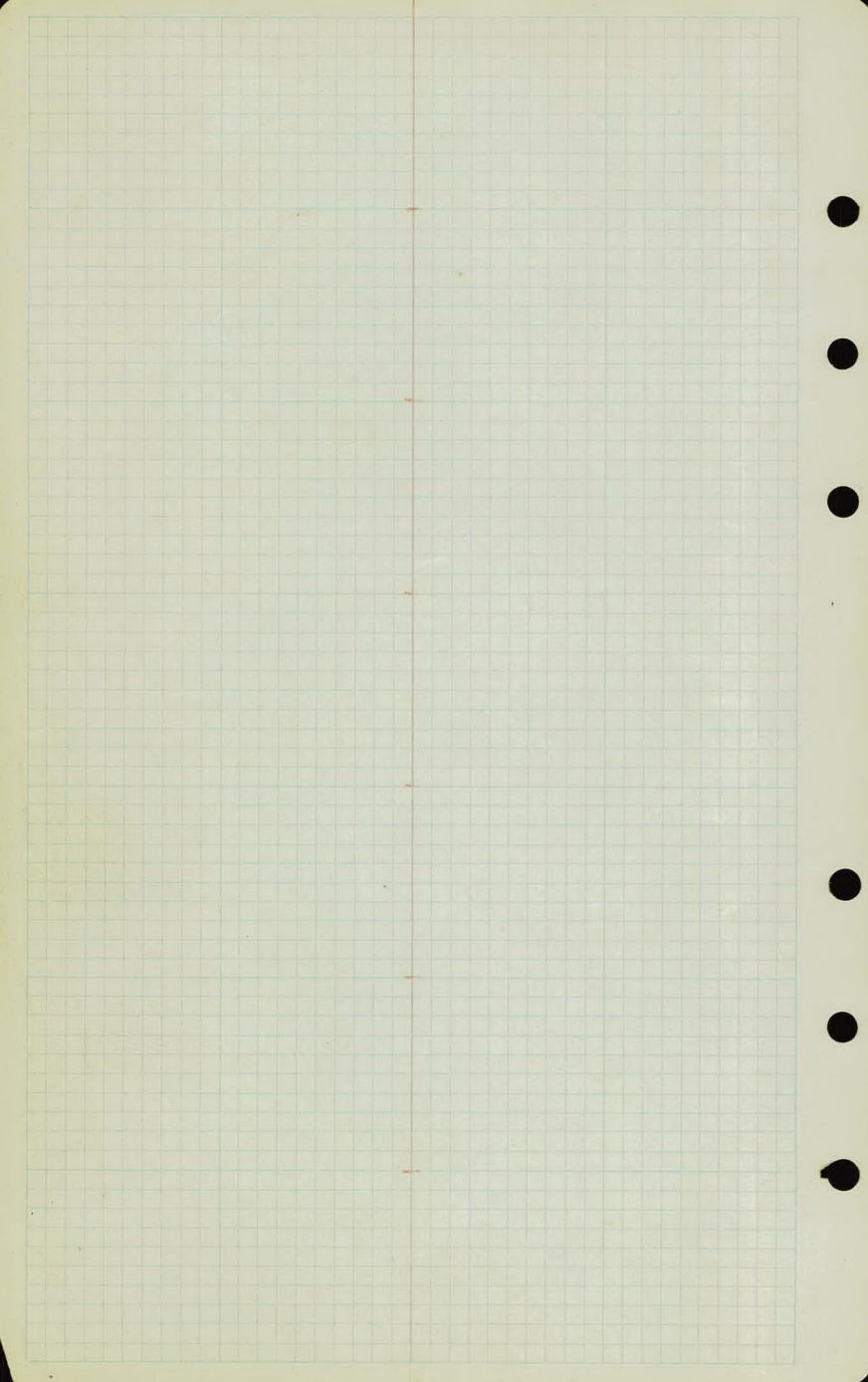
File .

PLAN SURVEY
EDGERTON ST.
Larpenteur Ave to Koehler Rd.

Partially Completed
5-11-44

INDEX

Align - 1-8
Topog. - 9-43
Bench
Levels -
X Sections -



Plan Survey
Edgerton Street

From Carpenter Ave to Kohler Rd

K.A.

~~4-1-44~~

HAW

AM

Index

Pages

LC

Align

1 to

CF

Topog.

L.L.

Bench levels

C.N.

X Sections

Sta

Pt

ΔL

ΔR

26+27⁵⁰

POT

& Co. Rd. "A"

9+65.29

POT

& Sookline RR

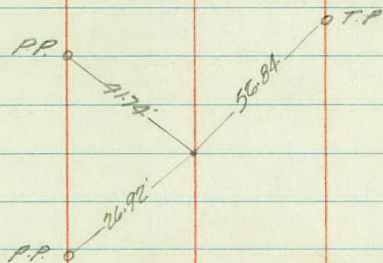
0+00

& Carpenter Ave

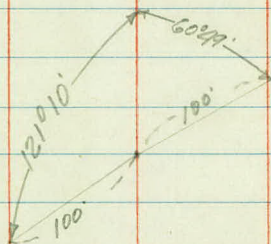
Description

Brass Plug

Chr Sec 17

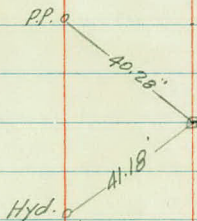


Nail



Stone Mark

Sec 14 Sec 17



Sta	Pt.	Def	$\Delta L +$	$\Delta R +$
-----	-----	-----	--------------	--------------

64+67.85	P.O.T =	E.S.T.H. 36		
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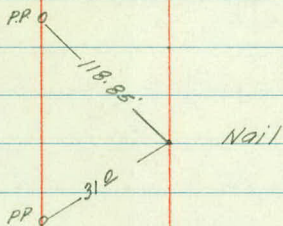
61+66.25	P.O.T			
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52+64.00	P.I.	Co. Rd. "B"		0° 05'
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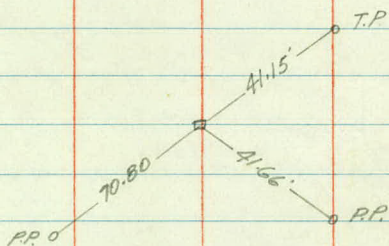
35+49.37	P.O.T.			
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Description

Nail



Mon.



So 1/4 Cor Sec 8

Drill hole



Face N W
Cor Btm Step

Cor Ref Wall



Sta	Pt	Def	Alt	ARt
-----	----	-----	-----	-----

105+32.00	P1		0°20'	
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78+86.94	POT			
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105132
 7418654
 264582

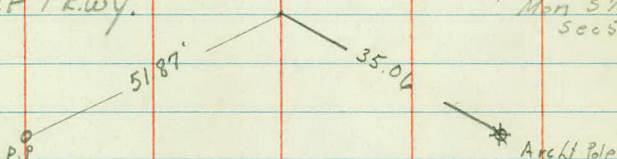
72+31.08	P.O.T	- E Co Rd "B2"		
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67+03.00	P.O.T			
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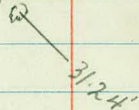
Description

4 Keller Pl.wy.

Mon 5 1/4 Cor
Sec 5



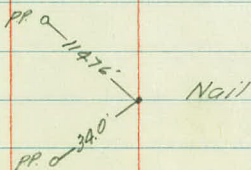
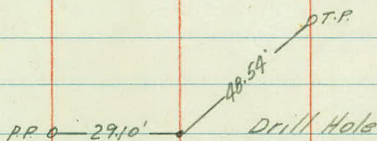
12" Maple



Mon
Str. Sec 8-

24" Cott

18.47'



Sta

R/

ΔL

ΔR

182+67.74

P.O.T

160+41.22

P.I

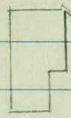
0°37'

131+62.55

P.O.T

Description

NE Cor
Clear Fount



35.90'

61.51

T.P

R.R. Spt

PP

52.86'

G.R. Post

38.05'

Mon Co. R. 1. "D"

No 1/4 Sec 5

39.55'

PP

PP

36.33'

Cent Sec 5

Mon

76.60

N.W.
Cor Fount
#2

Sta

Pt.

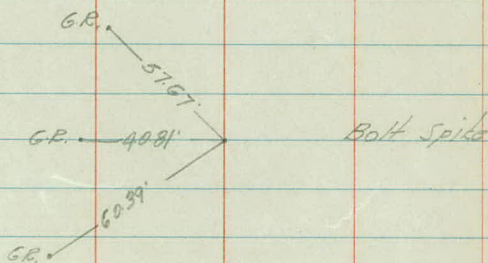
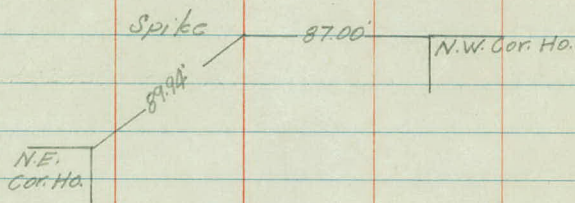
ΔL

ΔR

208+23.92 P.O.T

192+33.97 P.O.T

186+79.06 P.O.T



Ch. Sec. 32

Iron

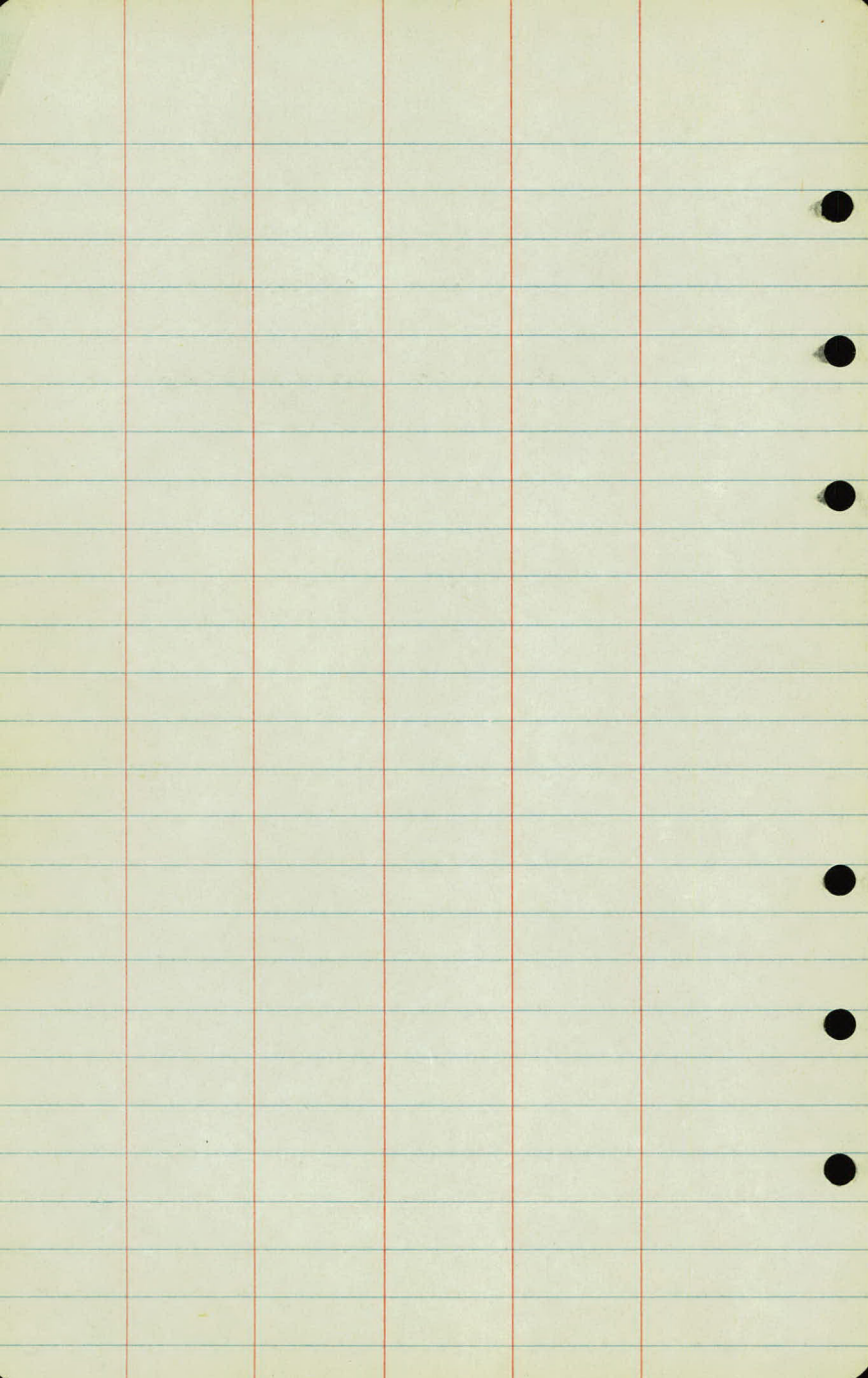
Sta	Point	ΔL	ΔR
15274	P.T.	45°58.5'	
+50		45°37'	
227		42°22'	
		39°07'	Δ -91°57'
		35°52'	
+50		32°37'	D-260-
		3	
2026+29.05	P.L.		T-22997
226		29°22'	
		26°07'	L-353.66
+		22°52'	
+50		19°37'	R-222.27
		16°22'	
225		13°07'	
		9°52'	
+50		6°37'	
		3°22'	
224		0°07'	
223+99.08	P.G.	0°00'	
+11456			
+1462	P.T.		1°03.5'
214			0°59' Δ 2°07'
+50			0°44' D-1°—
213+08.75	P.L.		105.86 T-105.8'
213			0°29' L-211.67
+50			0°14' E-5729.65
212+02.95	P.G.		0°00'
02.89			

Fore Tangz

□
Ment.

2' x 2" Hub.

n Mont.



Topography
Edgerton Str

198-TP-19' Top-40 7 Risers
 181-E 6' Walk Botl-33'
 161-36" Pop-34'
 Conc. Block Wall 2
 149-End Hedge-30' Beg. Wall-33'
 120-Beg. Hedge-34'
 11-E Ent

5
 198-PP-19'
 188-24" Oak.-38'

160-15" Tw. BE-32

4

188-PP-20'

154-18" Tw. Will.-33'
 152-Hedge-30

118-9' Driveway
 110-Fence
 110-End Hedge-34'

3

178-6' Elm-37
 171-E Ent.
 161-PP-20'

139-E 23' Walk-39'
 131-6' Pop-37'
 112-6' Elm-37'
 101-TP-20'

2

194-Bow Tie-37'
 193-Beg. Hedge-33'
 158-H. Pole-20'
 150-H. Pole-20'

1

134-PP-23'
 130-GR-14' Beg
 124-GR-29'
 115-E 18' Rd.-

0400

-04-End 15" CM-21'
 -30-End 5W-26'32'
 -22-PP-22' -30-Par. 10'
 -36-Hyd-19.5'

185-8" Trip. BE-39'

162-Ent 15"X10" CM-21'
 150-End Hedge-34'

140-E 3' Walk Botl-39' 2 Risers

182-Ent 15"X20" CM-21'

193-End Re. 1 Beg Hedge-36'

175-15"X6" CM-21'
 149-Beg. FC-33' Hedge-36'
 147-End 15" CM-21'
 138-Rod-35'
 112-End Rod-32'
 107-Beg. 15" CM-21'

195-TP-21'

140-E Ent-12"X20" CM-22'
 131-Botl. 5' 10" 34.5
 108 Top Step-42' 4' Walk.

180-Shrub-37'
 156-E Ent-15"X24" CM-22'
 146-Shrub-43'
 134-Hedge-40'

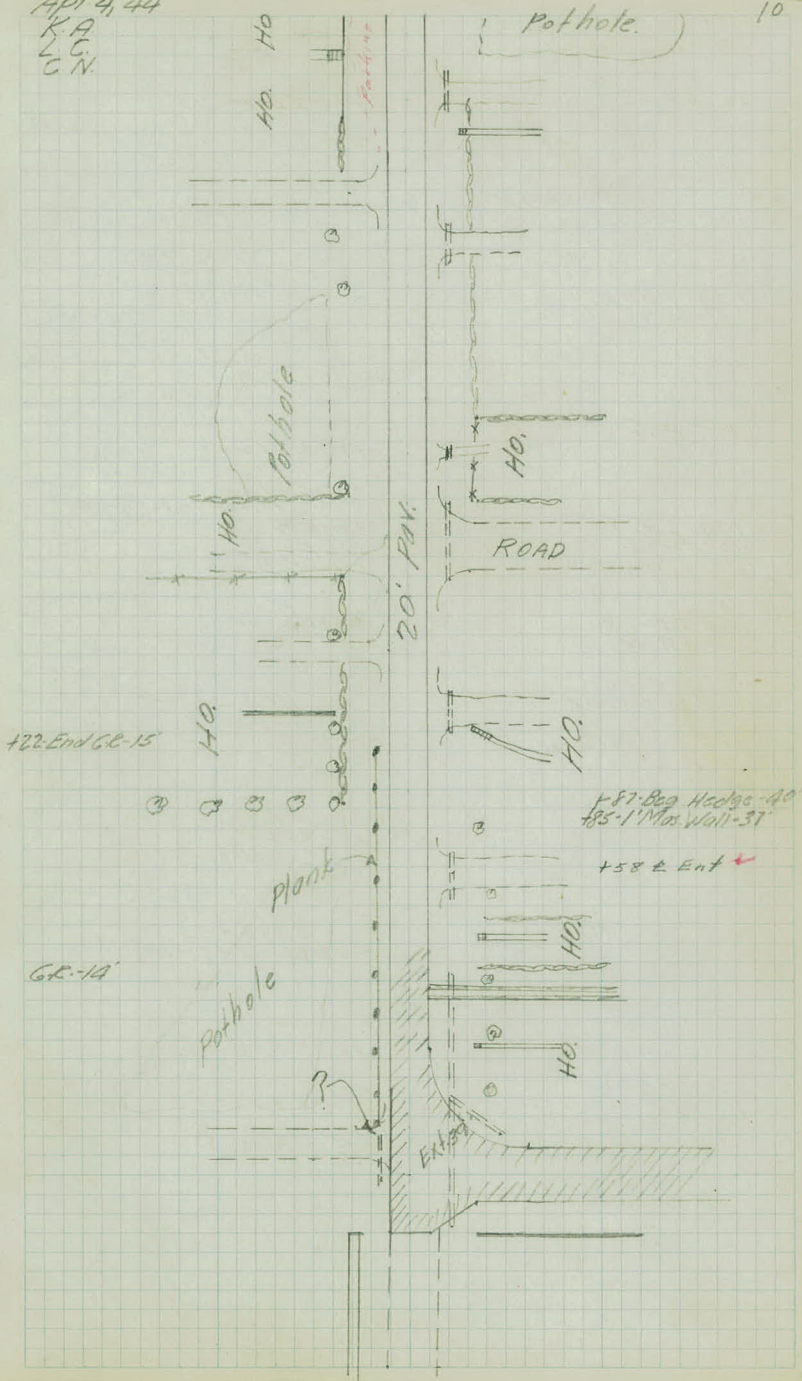
Top-36'
 123-E 3' Walk Botl. 40'
 15"X12" CM-22'
 106-E Hedge-37'
 104-End 15" CM-22'
 15" BE-41'

196-E
 191-E 18" Conc. Drive Lane
 174-18" Maple-42'
 168-End Ent. 11' Top-37' 3 Risers
 166-E 3' Walk Botl. 39'
 144-18' Elm-42'
 120-End 18" Colr-47.5
 113.5-Beg. Rod-63'

-13.5-Div Par-35'
 -27-End 12" CM-21'
 -16-Tel. M. H.-16.5'
 -30-Conc. Block Retain Wall-35.4

Apr 4, 44
K.A.
L.C.
C.N.

10



+98-End G.R.-100'
+87-Cor G.R.-15'

+77-PP-19

12 G.S. Conc. Spillway at End
+98-End 15' Conc. Culv.-25'
+93-12" B.E.-40'
+89-Bog G.R.-15'
+56-5" Tw Elm.-32'
+53-Hyd.-16'
+47-Gate Valve-9'
+46-PP-20'

11

+97-Ent.

+39-Ent
+15-PP-20'
+08-8" Willow-30'

10

+81-T.P.-28'
+68-M.H.-45'
+30-End G.R.-15'
+26-30" Iron Culv.-21'

+25-End 12" C.M.-20' 32" C.M. +7' V.A.

9 PP-20'

+92-End Hedge-3A'
+82-Bog G.R.-15'

8

+25-Ent.-4" Trip Pipe-29'
+04-15" Elm.-34'
+95-24" Walk-31'
+83-12" Elm.-35' S.E. Cor Ho.-58'
+67-PP-20'
+61-10" Tw Elm.-34'
+38-8" B.E.-34'
+13-S.E. Cor Ho.-58'
+26-25" Walk-31'
+14-8" B.E.-34'

7

+90-12" Elm.-34'
+86-Cor Hedge-32'
+65-Ent.

+40-PP-20'
+18-Gas Pump-21'
+09-S.E. Cor Stone-33'
+05-Cor Wall-33'

6

Curb buried from here on
+80-Curb-20.2

+78-Cedar-25'
+67-Shrub-25'
+35-3" Tw Cedar-25'

+99-Shrub-25'
+92-Shrub-25'
+84-6" Walk-20.3'
+74-Shrub-25'
+68-5" Cedar-25'
+53-Telc. M.H.-16'
+47-6" Cedar-25'
+36-Shrub-25'
+27-Shrub-25'
+06-6" Cedar-25'

+93-Bog S.W.
+85-Ent-12" X 26" C.M.-19.5'
+78-End S.W.
+40-Cor Steel Pipe at P.-34'
+34-Bog Curb-30.4'
+35-PP-35'
+21-T.P.-41'

+6529-2 Tracks +90 Bog 4.5' S.W.-29.4-34'

+60-Signal Box-30'
+56-Xing Signal-17.5'
+55-End 18" C.M.-36'
18" X 6" C.M.

39" Culvert. +44-End 18" C.M.-25'
+21-End 10" V.A. Culv. 19'

+86-End 12" C.M. From East-24.5'
+15 X 6" C.M.-21'
+98-2 3' Steps-37-57'

+40-Gate Valve-27'
+15 X 8" C.M.-21'
+02-2 7' Steps-33-48'

+98-5" Elm.-25'
+62-5" Elm.-25'

+25-5" Elm.-34'
+05-8" Elm.-35'

+88-Row Trees-34'

+22-8" Tw B.E.-41'
+04-10" Trip B.E.-40'

ROAD

APR 4, 44
K.A.
L.C.
C.N.

11

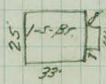
Pothole

Curb-20' Fc-34'

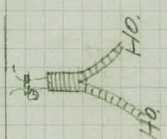
H.O.

H.O.

R/R tracks



5.5' W



H.O.

2' Rubble Gutter
 +85-End Rod-21'
 +71-Beg Rod-44'
 +45-End Rod-15'
 +21-Beg Rod-20'

+69-FC-23'

+79-TP-29'

+56-3" Elm-25'

19 +19-PP-18'

+10-8" Elm-42'

+92-10' Ent

+75-8" Elm-42'

+75-Swamp-40'

+39-FC-18'

+28-3" Elm-25'

18 Swamp-400-200'-40'

+91-PP-19'

+85-3" Elm-25'

+39-3" Elm-25'

17

Swamp-57'

+94-3" Elm-25'

+61-PP-20'

+40-3" Elm-25'

+04-3" Elm-25'

Swamp-60'

+10-15" Willow-37'

+09-Spillway Culv.-16.5'-31'

16 Swamp-200'-37' 12'x16' C.M.

+91-6 Spillway-22'

+60-3" Elm-25'

+28 to 17+10 Settlement Bumps & Patch

+36-PP-20'

+12-3" Elm-25'

15 Beg. Swamp-35' +03-Beg. 2" sloped gutter both sides curb

+77-Beg. Rubble Gutter-17-20.5'

+77-End FC-34'

+65-Beg. G.K. Posts-14'

+68-12" Oak-27'

+64-End SW. 29.5-34'

+29-3 shrubs-25'

+18-Shrub-25'

+22-Ent

+03-End G.K.-15 PP-19'

14

38" of C.M. & vit. Culv.-12" P

+97-SW Cor 37x37 P/lor-33'

+80-NW Cor 37x37 P/lor-33' Ent

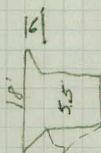
+70-End Curb-20'

+36-8" Tree-31'

+30-8" Tree-31'

+22-Beg. G.K.-130'-15'

13 +08 & Southard Rd 24' Ent



Apr 5, 94

12

G.R.-14'

stop Gutter - 22'
+01 Gutter - 26.1
+82 Gutter - 258
+77 Gutter - 21.7

Gutter - 16 - 21'

G.R.-14'

Swamp

Gutter 165-218'

Pothole.

Gutter - 17 - 22'

Driveway

ROAD

+80-E +top 6' step-50'

+71-End 18" CM-22'

+68-E.C. steps-35'

+65-PP-20'

+71-End 18" CM-24'

+69-PP-20'

26

+79-End Shrub-55-38'

+78-Beg. Shrub-39'

+44-12" PP-40'

+30-5" PP-37'

+18-Beg. rubble gutter 233-195'

+18-Ent-18x20" CM-20'

Not used for drive

+06-24" D.-53'

25

+88-Fe. Cor-58'

+66-Step-+Fe-44'

+58-PP-20'

+38-Beg. Pav.

+25-End Pav.

24

+06-Step-40'

+98-Step-36'

+22 to 25+52 Bumps + Patch

+49-18" Tw. O.-33' +Fe.

+30-24" O.-35'

+13-PP-19'

+12-24" O.-30'

23

+93-18" Oak +Fe-33'

+53-Fe. Cor + 18" D.O.C.-35'

22

+14-Range f/c to Fe.

+94-5" Tw. BE-34'

+84-10" BE-37'

+81-PP-19'

+72-10" Tw. BE-36'

21

+53-PP-20'

20

+78-T.P.-28'

+44-End 18" CM-23'

+45-Tele. MA-145'

+02-End 18" CM-23'

175-Block Top-10'

Rubble H.V.I.

148-End 18" C.M. 40'

138-Block Top-45'

117-Block Top-56'

Block Top-10'

Gutter-252-21.8

165-End Bl Top-10'

195-Block Top-40'

115-Block Top-52'

12" X 11" C.M. 23'

106-End 12" C.M. 24'

101-End 12" C.M. 24'

190-Box Block Top-10'

115 Gutter 27.5-21.0

Gutter-174-21.4'

Block Top Patch

Gutter-174-21.4

Uncult

Pasture

193-End G.R. Posts-14'

G.R.-14'

Cult

Gutter-17.6-21.6

+83-PP-20'

+70-T.P.

Hedge inside of Fe₂

+51-15" Pop-33 Cor Fe-41

+40-E Ent.

+29-18" Pop-34'

+20-8" Trip Pop-35'

+15-8" Tw Pop-35'

+14-10" Pop-36

33 +05 Cor Conc Block Wall-295

+92-E Drive way

+78-E Drive way

+52-4" Elm-37'

+48-PP

+94-Grav 6-8" Pop-34'

+59 10' Conc Ent 33'

+46-T.P.

+16-3' Conc. Still way - 33'-41'

+15-Row 3" Pines - 41

32

+78-PP-20'

31 +15-E 10' wide Hedge - 44'

+09-Ent. $\frac{15" \times 200 \text{ CM}}{22'}$

+98-T.P.

+96-E Hedge - 40'

+89-FC-41'

+50-24" BE-32

+38' 15" Elm 56'

+18-15" Elm-56

30

+93-PP-

+90-T.P-28' +98-15" Elm-56

+83-12" Elm-48'

+76-Ent. - $\frac{12" \times 200 \text{ CM}}{24}$

+58-PP-43'

+57-FC-40'

+19-FC-39'

+20-End Rubble Slope-29-25'

+16-Cor Rubble Slope-39-33'

+12-Cor Rubble Gutter-49-28'

+11-E 18" Stone Slope-49-28'

29

+79-6" Elm End of Row-55'

+53-PP-20

+55-T.P.-28'

28 +15-3" Elm-

+81-A" Elm

+54-PP-20'

+50-4" Elm-

+56-Row 5" Pines - 46'

+46-T.P-29

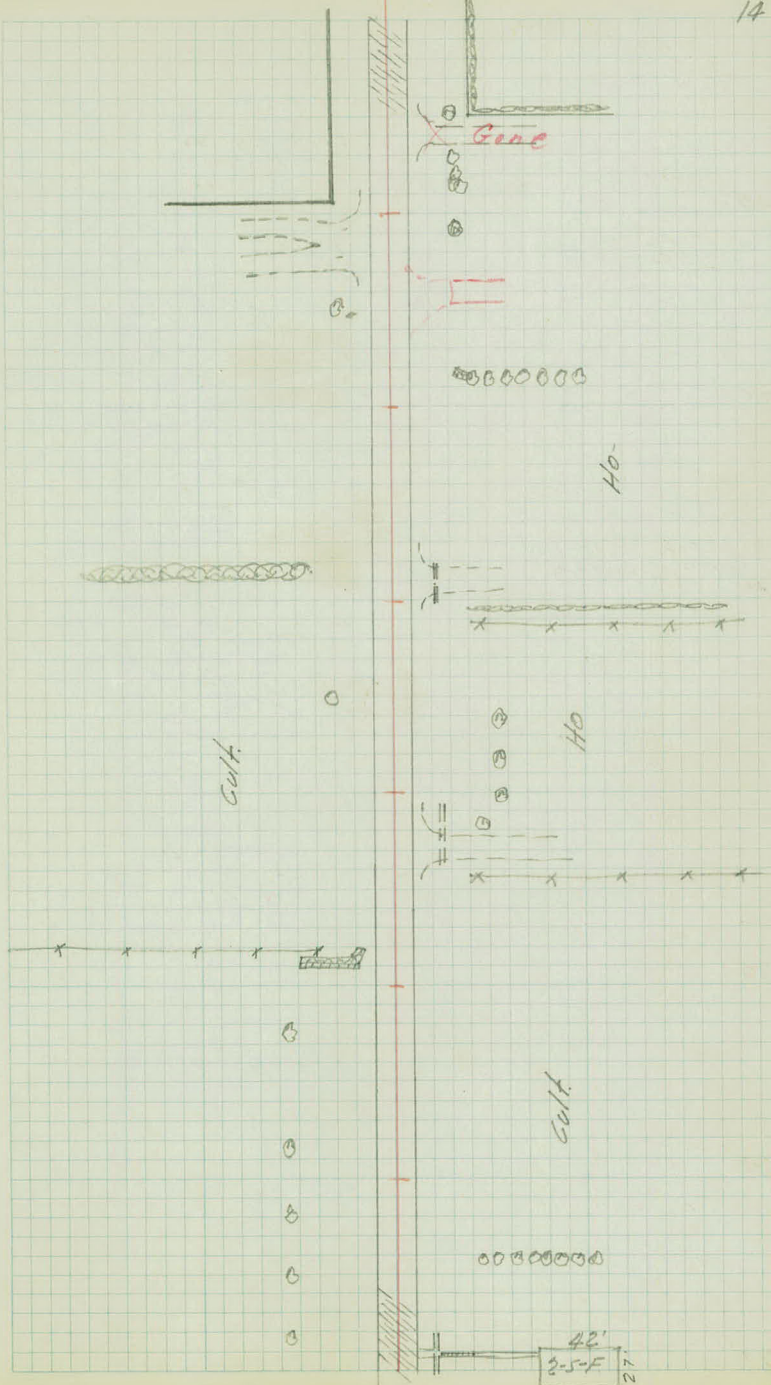
27

+17-Beg Row 5" Elms - 55

+11-NW Cor Ho.-74'

Top - 20' $\frac{18 \times 200 \text{ CM}}{21}$

+08-E 3' Steps. Batt - 244'



+92-Bog Rock Garden-31-25'

+67-Ent 18' ✓

+40-Row 30" B.E. -52'

+24-PP

39

+47-Fc Cor -34'

+26-GP-35'

~~+24-PP~~

39

FC-33

+90-T.P.-

+95-6" Pine -44'

+83-4' Steps -36-22'

+74-6" Elm -45

+50-FC -35'

+20-6" Cedar -42'

+07-8" Cedar -41'

38

+96-PP-

+62-T.P.-28'

+55-Fc Cor -40'

+51 Ent ✓

37

+68-PP

Cult

+47-Group 5" B.E. -36'

+34-T.P.

+32-Row 6" Pines -38'

+28-2' Rubble Wall -33

+21 Ent ✓

+15-Cor Rubble Wall -33'

36

4" x 15" Iron Pine -19'

+48-6' Steps -33-43'

+17-Bog Rubble Wall -33' Hedge

+15-Ent Fc/Hedge -37'

35

+14-PP

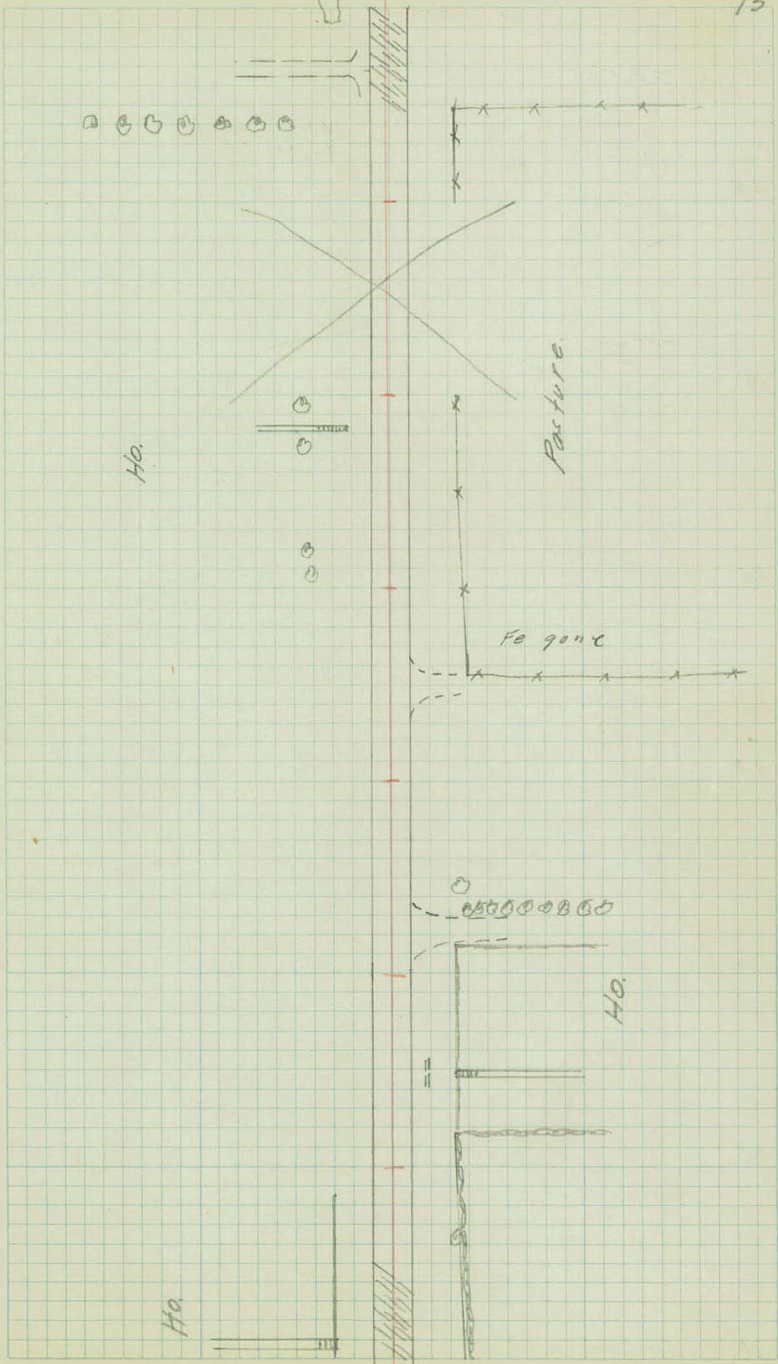
+99-T.P.-

+85-Ent Wall -29-8'

+62-15" Elm -34'

34

+18-6' Steps Top -38.8' 6' wide
Bottom -29.8'



+95-24"0.-35 P.P.-20

+63-Bcg. Fc.-20'

+45-End G.R.-14'

46

+91-Fc.-15

+70-PP-20

+14 Ent ✓

45

+44-PP-

+39-Bcg G.R. Posts-13.6'

+23-Ent

44

+95-51p-38'

+87-Ent

+67-24"0.-37'

+91-Ent Par with 1/2 SW

+19-2'2" Walk 175

+15-PP-

+11-Range to 1st W.

43

42

+85-PP-

41

+62-SW Cor. Cor + Roof Cellar -32.6

+54-PP-20'

+46-End of Septic Tank Drain-26'

+42-Rock Garden-40-31-2.5'

+06 to +07 Bump + Patch

+18 TP-

40 5" Pins-45'

+90-18"0.-37'

+80-12"0.-36'

+49 Ent 33' ✓

+55-TP-28'

+33-18"0.-43'

+22-15"0.-41'

+82 Ent ✓

+82 Range to ✓

+57-Cor Hedge-29'

+26-PP-28'

+14-Cor Hedge-29'

+61-6" Elm-41'

+51-5 Standard Sign Post-26'

Driveway-45'

+50-2 Gas Pump Stand-6.5'

+ SW Cor. Fill Sta-79'

+96-TP-28" to Edge Ent.

+05-Ent.

+88 Bcg Ent Same ✓

+83-Fc.-24 End G.R.-145'

+74-TP-28'

+96-24"0.-

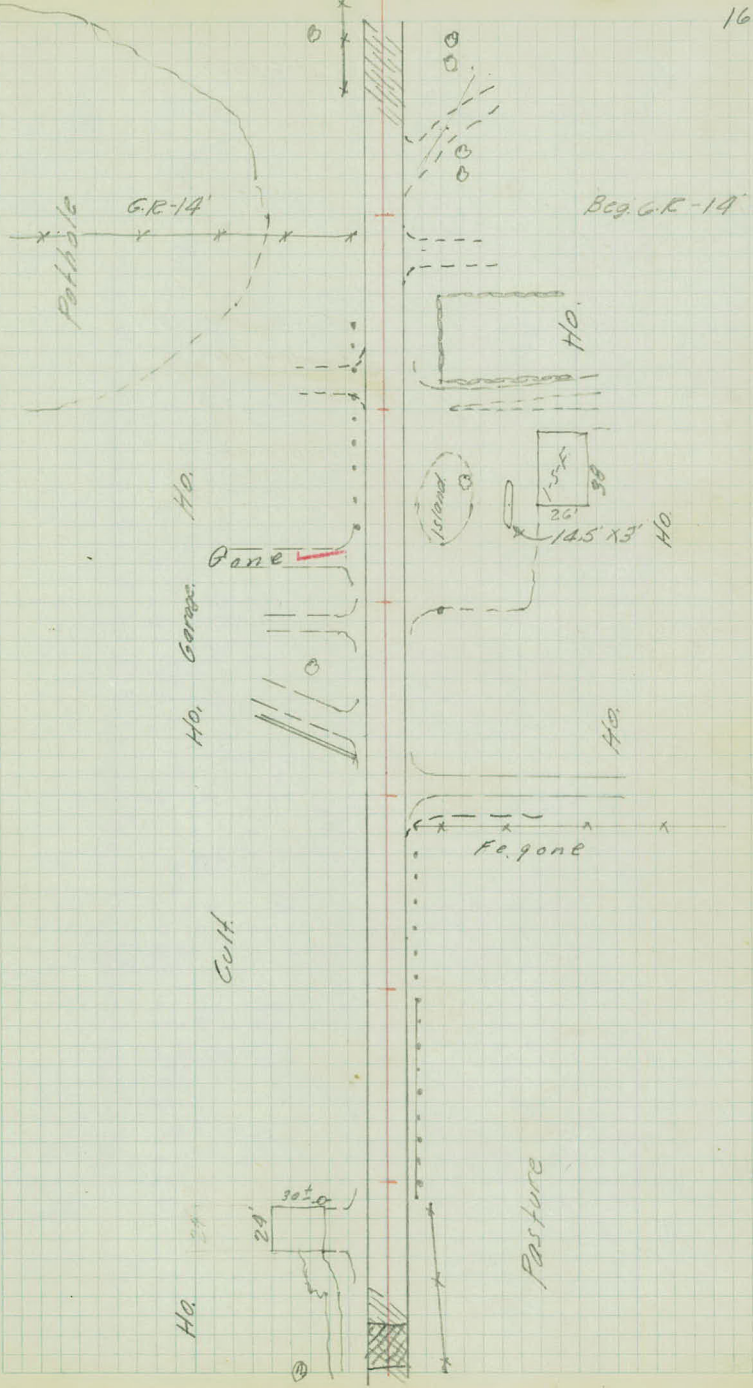
+95-End Plank G.R. + Bcg. G.R. Posts

+47-TP-

+91-Bcg. Plank G.R.-15'

+88-End Fc.-22'

Fc.-30'



+78-PP-19.5

+77-G.P.-19'

+20-G.R.-14.5'
53 Pot hole-31

+83-G.R.-27'

+73-Beg. G.R.-59'

+29-PP-52'
+25-Δ in Fe-67
52 Δ in Fe-34'

+78-PP

+64 to 52 +06 Bump

51 H3-15"O-42'
Fe-26'

+88-30"O-43'
+70-PP-20'

+68 ± 18' Ent

50 Fe-24'

+95 Ent

+53-End G.R.-14'
+44-PP- + Fe-20'

49

48 +20-PP-

+75-Beg. G.R.-14'
+70-End Fe-21'
+64-24"O-40'

47

G.R.-15" Pot hole-28'
+94-T.P.-27.5'
+91-51P-20-28'
+82-G.R.-25'

+74-G.R.-43'

+44-G.R.-52'
+32-PP-26' G.R.-24'

+06-G.R.-13' T.P.-26'

+83-Beg. G.R.-13'

+ Patch
+58-15"O-Fe-Cor-41'
+50-8"O-41'
+44-8"O-39'
+24-24"O-Fe-36'

+98-T.P.-26'
+94-18"O-43'

+56-18"O-35'
+25-Beg. Fe-32'
+22-15"O-34'
+16-T.P.-

+68-15"O-40'
+58-18"O-46'

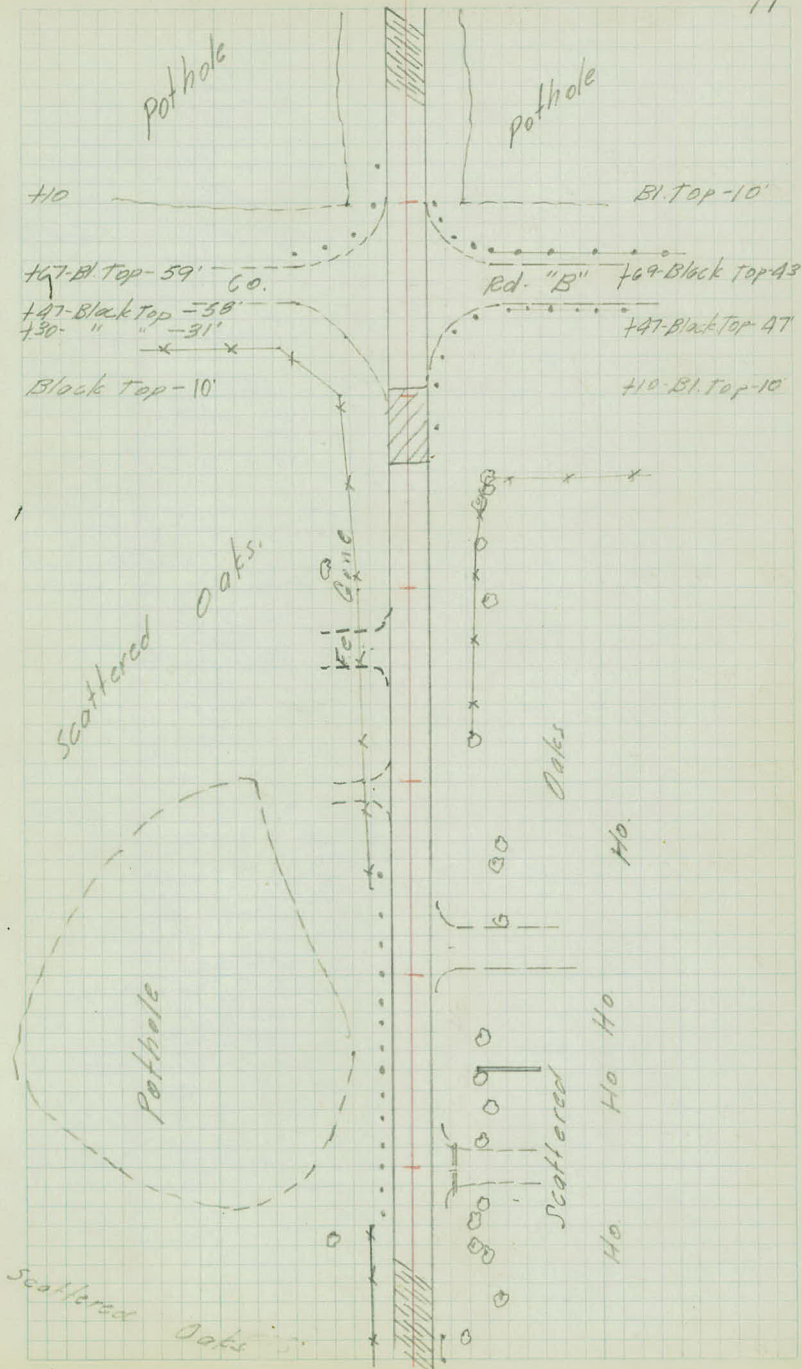
+25-18"O-49'
+22-T.P.-28'
+13-Double Ent.

+68-24"O-38'
+50-± Stone Walk-32'
+47-15"O-36'
+30-18"O-41'
+13-2" Pine-37'

+98-Double Ent- $\frac{15" \times 26" \text{ Gang}}{22"}$

+81-T.P. 2" Pine-36'

+73-15"O-33'
+60-12"O-33'
+55-18"O-40'
+32-15"O-47'
+13-End G.R.-14 12"O-37'



60 +129-PP-30' +127-Beg. New Pav. +115-BI Top-19.5'-30'-51'
BI Top 47 47 +110-BI Top-24'

+150-BI Top-34 34'

59 +103-PP-30'
Ed.-147'-119' BI Top 24' 24.5

+150-BI Top-20' 20'

58 Rd.-98'-71'

+179-PP-30'
+177-Beg. Blk. Top-A Rd.-59'
+169-Rd.-32'-82'
+143-Rd.-60'

+160-Fc-32'
+157-Beg BI Top-19.5

57 Road-20'

Beg. Road 2
+177-End G.R.-14'
+150-PP-

+102-End Cdv. 16.5 } 15" x 26 CM.
+103-End CUN -33'
+190-End G.R.-14'
+160-TP-28' /
+150-G.P.-21' /

56 G.R.-14'

G.R.-13.5'

+150-Pol hole-37'

+161-TP-27.5'

55 +113-PP-20'

+113-PP + Fc. Cor-30' Pol hole-35'
Range 110 to Fc

54

+126-TP-

FC-44

Duplicate
rt. side

ROAD

ROAD

FC-30

pothole

pothole

188-PP-30'

67

66

65

64

63

62

156-PP-

61

B/Top-19-60'-80'



+94-PP-20
+74-15BE-35' +80-15BE-30'
+60-FC Cor-41 FC-66'
+59-15BE-31'
+55-End 24"CM-33'
+35-End 24"CM-29'
+32-FC Cor-34'
+17-Long R15 to FC-
+02-FC Cor-37'

+90 Bag G.R.-19'

+50-End Bl.Top-21'

+46-Catch Basin-21'

74

+86 to 74+15 Bump + Patch

+98-TP-28'

+58-PP-20'

+71-2" Ash-54'

+42-4" Ash-54'

+14-4" Ash-54
Bl.Top-21'

73

+70-TP-29'

+67-Bl.Top-22'

+41-Bl.Top-59'

+31-28" E.C. Rd. B2"

+21-Bl.Top-60'

+26-PP-29'

72 End Bl.Top-18'-10'

Bl.Top-32'

+85-Bl.Top-22'

+65-Catch Basin-21'

+35-Bl.Top-19'

71

Bl.Top-20'

+70-PP-29'

+50-Rd-22'

70

Bl.Top-30'

+70-End New Pav

+29-PP-29

+50-Bl.Top-42

+21-Bl.Top-24'

+17" -20-52'-30

+08-Surface Drain-20.5'

69

~~+39-PP-37'~~

+31-Bl.Top-24'

~~+08-Surface Drain-20.5'~~

+17-Bl.Top-20'-52'

Bl.Top-19'-13'-93'

68

+13-PP-19'

+33-E 2' Both Ditch -50'-22'
+23-24" Maple-39' 30" Maple-46'
+103-25" BE-25'
81

+95-4" BE-28'
+86-4" BE-28'
+33-PP-19'

80

+45-Ent
+14-15" Maple-17'
+105-End GR-12.5
79 +101-PP-18'

+32-30" Cott.-19'

78 G.R.-12.5'

+74-24" BE-22'
+65-PP-19'
+63-E 2.5' Wide Spillway-23'-12'

+46-15" B.E.-37'
+29-15" B.E.-20'
+102-Group 4-12" BEs-29'
77

+59-15" BE-33 +61-12" BE-28'
+56-BCG GR-12.5' 15" BE-32'
+44-2-10" BEs-
+33-15" BE-
+32-10" BE-
+24-15" BE-
+18-Group 3-15" BEs-32'
+105-E Ent.
76 Fe Cor-39'

+52-T.P.-28'

+15-End Gutter-12.5'

+99-E Ent

+64-SW Cor Cor-33'
+58-30" Maple-36'
+48-End Hedge-21'
+37-30" Maple-38'
+28-T.P.-28'
+14-30" Maple-40'

+85-BCG Lilliac Hedge-21'
+68-SW Cor He-36'
+66-E 3' Walk-18' Top steps-17.5'
Bottom-21.5'
+59-51p-25' 24" Maple-32'
+32-End GR-13'

+50 Ent (Small)

+85-T.P.-27'

+57-6 3/2' Wide Spillway-19.5-29'

GR-13.5

+52-T.P.-
+50-End Trees-40-70'

+34-T.P.-27'

GR-13.5 Trees-40-70'

+40-Beg. Trees-40-70'

+105-Group 7-12" BEs-32'
75 Fe-37'

Yard

20
20

20'

21

24' 10"
1 1/2 - 5 - 1/2
10 1/2
10

Gutter - 12.6'

Block Top Spillway
between Pav. & G.R.

3" to 6" Box Elders

Uncult.

Block Top Gutter Inside of G.R.

+93-End Pav. + Bag Black Top-

+54-PP-165'

88 6R-13' Swamp-27'

+83-Bag G.R-17.5'

+90-End 12" CM-28'

+56-E Ent-24'

+96-18" Pop. 40'

+48-End 12" CM-27.5'

+30-15" Pop-55'

+15-PP-19'

+23-Range tic to Ent

87 Brush-41'

Lake-32

+97-T.P.-29'

+65-Lake-34'

+32-Bag GE-152'

+20-G.P.-29 End Brush & Lake-50

Brush-34' Lake-60'

+77-T.P.-28'

+65-18" Elm #3 Brush-35

+30-Bag Brush-31'

86

+84-PP-

+28-Ent

& Ent-39' Brush-55'

+90-Bag Brush

+89-Trans. Pole 28'

+76-Trans. Pole

+38-Cor Ho.-65'

+05-Range tic House.

85

+96-T.P.-28'

+44-PP-19'

84 +11-4-4" B.E.^s-35'

+93-T.P.-27

+40-14-4" B.E.^s-35'

83 +08-PP-

+71-T.P.-

82

Lake

Gervais

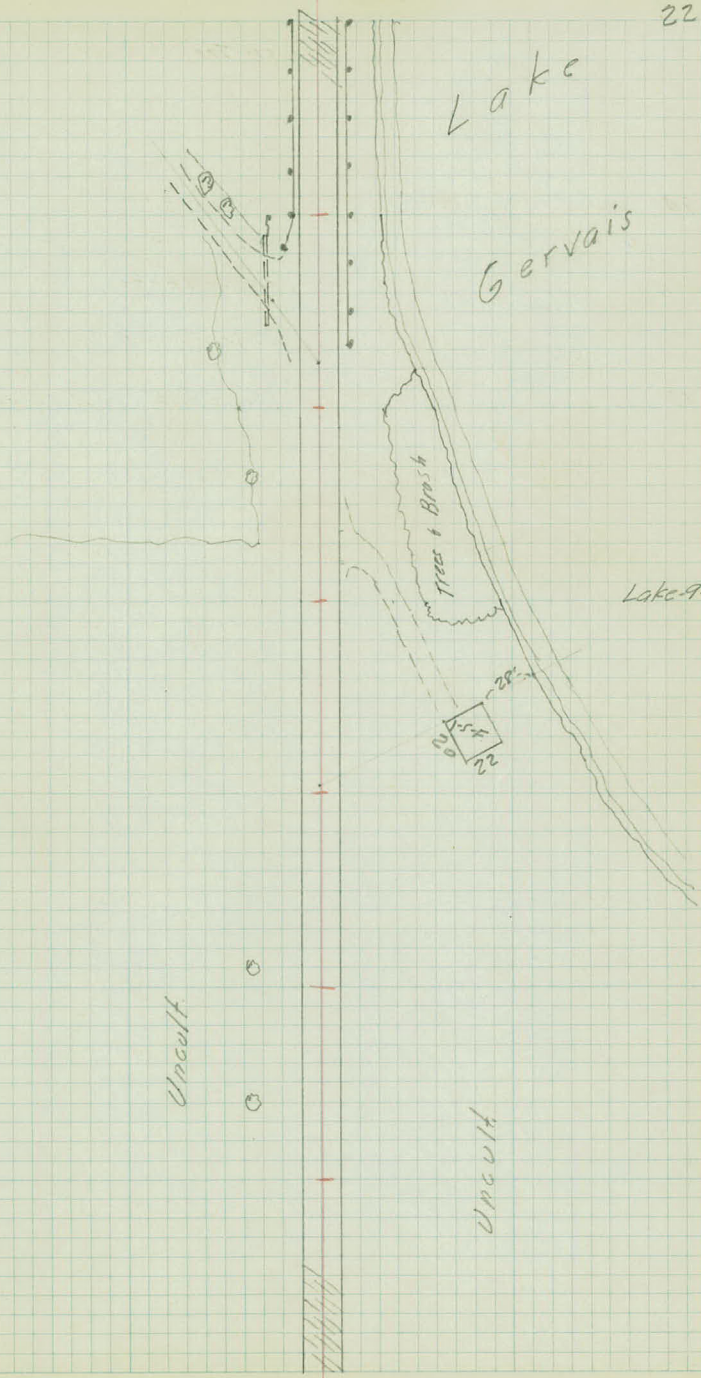
Lake 94'

22
5 ft
28'

Trees & Brush

Uncult.

Uncult.



+58 Ent

94

+95-PP-20

+98-Gr. 3'x3' Riffy -46'
+80-26" Pop-68'
+62-24" B.-42'
+48-Ent. YG+52'
+31-10" O.-40'
+29-T.P.-2P'-8" O.-43'
+25-24" Cott.-66'
+49 E Ent
Lake-72'

+68-30" Cott.-62'
+60-18" Trip. Cott.-61'

+33-18" Elm-60'

93

+02-T.P.-27'
18" Tw. Elm-59' 24" Tw. Willow-69'-

92

Lake

+69-15" O.-45'
+64-12" O.-48'
+61-PP-
+56-8" O.-50'

+55-Lake-65'

+25-End Brush-41'
+19-End G.R.-14'

92

Lake-39'

+25-End Swamp-33'

+26-T.P.-27'

+50-Bog. Brush-33' +45-End B. Top + Bog. Pav.
+50-Lake-31'

+25-PP-16'

+27-End G.R.-14'

91 Swamp-33' G.R.-14.5'

G.R.-14' Lake 28'

+51-T.P.-

90 Swamp-28'

Lake-29'

+89-PP-17' X Drain =
+72-End CM-28'

X 57' CM
+76-End CM-29'

+18-T.P.-

89 Swamp-33' G.R.-14'

G.R.-15'

Unpult.

Lake 70

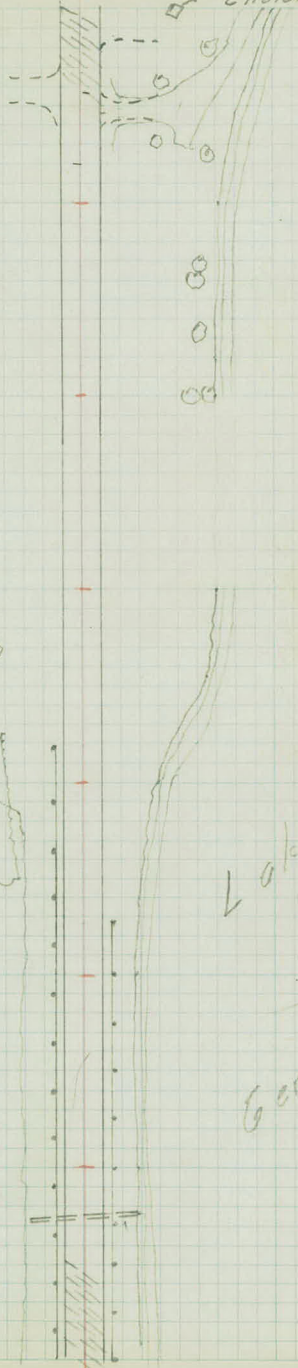
Swamp



Lake

Gervais

Swamp



+82 £

+43-PP-

101

+59 £ Ent

+26-PP-

100

+10 £ Ent

+15-PP-19'

99 Ent 12x22 Conc.
22'

+86 £ Ent

+80-T.P.-28'

+62-24" Pop-42

+99-T.P.-28'

+34-Shrub-20' 15" BE-25'

+30-15" B.E-20

+20-15" B.E-21'

+16-Shrub 25' - SW Cor Ho-33'

+97-Ent-

98

+97-PP-19'

+16-T.P.-28'

+56 £ Ent

+40 £ Ent

97

+12-Ent-

+01-T.P.

+98-E 3' Walk-16'

+60-SW Cor. Ho-80'

+44-24'E 1m-39'

+67-PP-16'

96

+90 to 96 +15 Bump + Patch

+83 Large tie House-

+33-PP-19.5

+62-T.P.-27'

+57-PP-27'

+42-Cor Cottage-70'

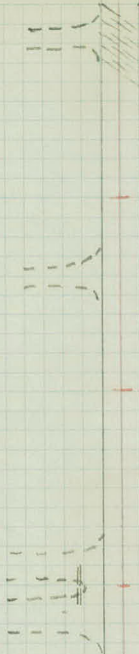
+33-30" Cott-65'

+28-15"-Pop-65'

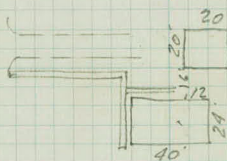
+05-8" O-40

+02 40' £ Ent

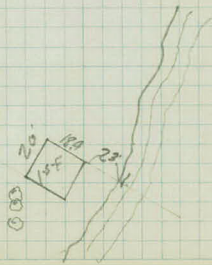
95



8' 1-s-st.
4' 43'



③



+34-TP-28'

108
+92-TP-26'

+91-Ent.

+25-TP

107
+95 Ent Lt.
+71 Range tie
+67-TP-26'

+04-TP-28'

+05-BI Top-10'

106
+90-BI Top-10'
+79-TP-26'
+68-BI Top-23'
+67-TP-44'
+61-G.P.-28'
+46-BI Top-55'

+65-BI Top-28'
+61-G.P.-48'

+52-BI Top-45'

+22-BI Top-40'
+05-PP-40'
105 BI Top-30'

+13-PP-30' +22-BI Top-41'

BI Top-18'

+75-G.P.-25' 30" Elm-40'
+60-BI Top-10'

+70-BI Top-10'
+65-TP-

104
+06-PP-18'

+73 to +84
Bump & Patch

+36-TP-

103

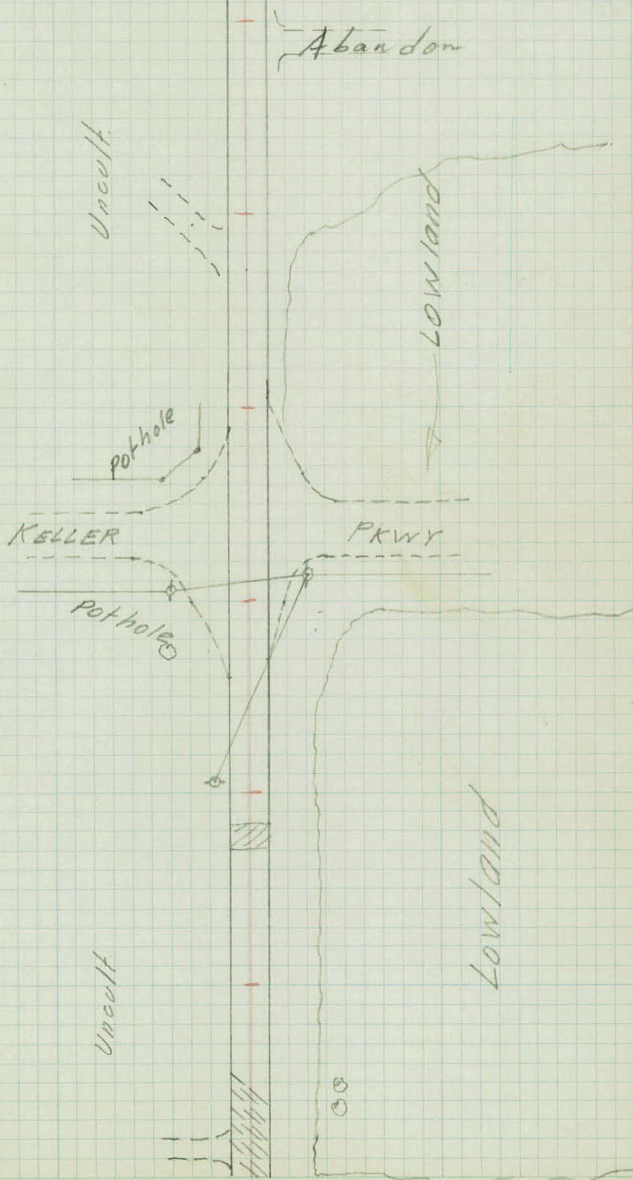
+62-PP-

+14 Ent

102

+46-8" Tw. Bosswood-47'
+37-8" Tw. Linden-48'

+10-TP-



+74-End Culv. 22.5' Ditch -34'

+74-End Culv. -34'

15" x 4' Mos. Box Culv.
18" Wide 4' High

+62-H" Pile -25'30' +72 to 91 Bump & Patch

+40 Range pier
115 Fe. -35' Δ in Ditch -102'

+49-TP-27'

114 +66-Fe Cor -34'

+60-Beg. Swamp -37'

+73-TP-

113 +16-TP-

+45-TP-27'

112 +18-PP-37'

+25 L End
+11-PP-39'

+86-TP-

111

+19-TP-

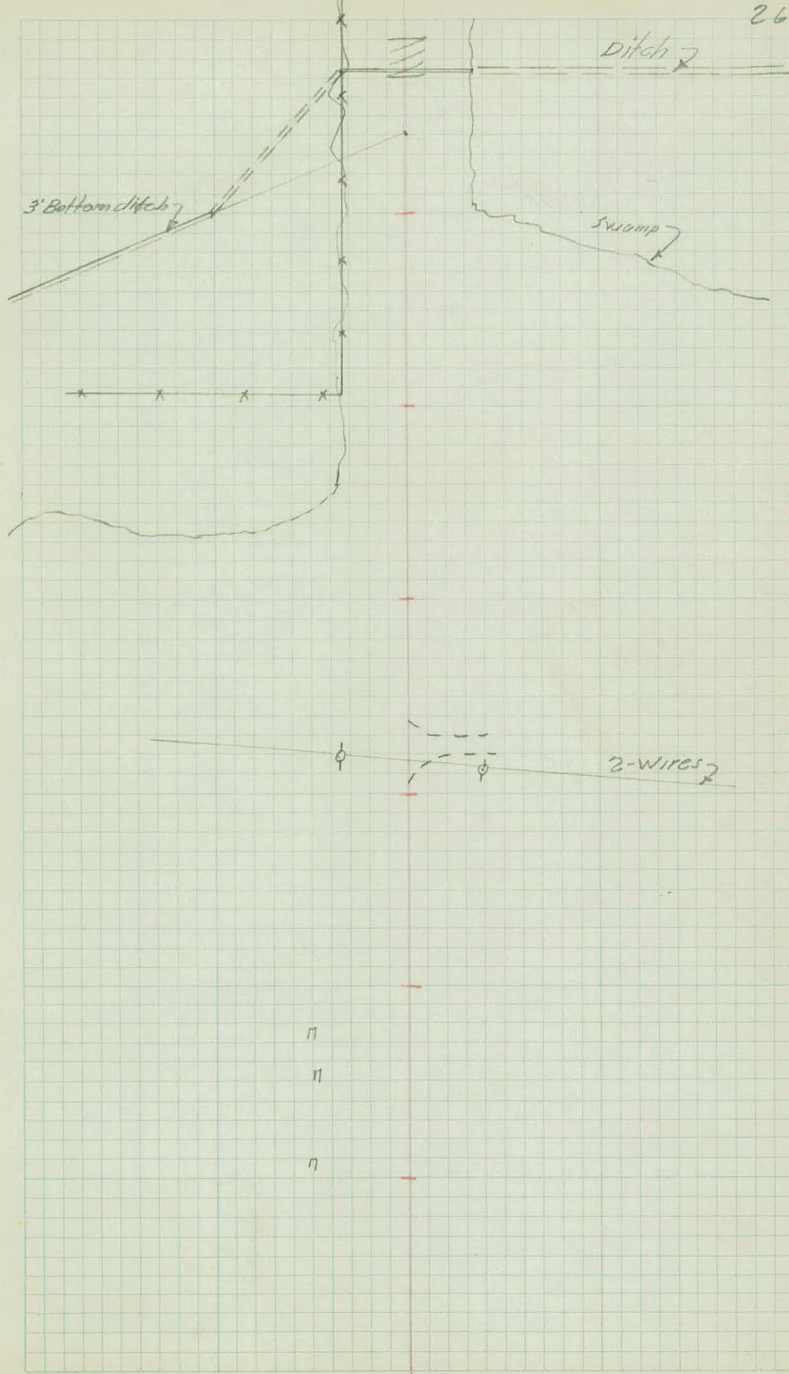
+75-Str. 50'
+57-TP-27'
+52-Str. 47'

110 +08-Str. 50'

+83-TP-

+25-TP-

109



Fe. -32'

+97 $\frac{1}{2}$ Ent

+74-T.P.-

+17-T.P.-
122 Lowland-40

+52-T.P.-28'

+41 $\frac{1}{2}$ Ent

121 Lowland-40

+80-T.P.-

+02 to +37 Patch + Bump

+21-T.P.-

120 Fe-33'

+90-30' O-53'

+55-T.P.-26'

+62 $\frac{1}{2}$ Ent

119

+90-T.P.-

+38-Fe. Cor. 34 Swamp-40
+22-T.P.-

118

+61-T.P.-

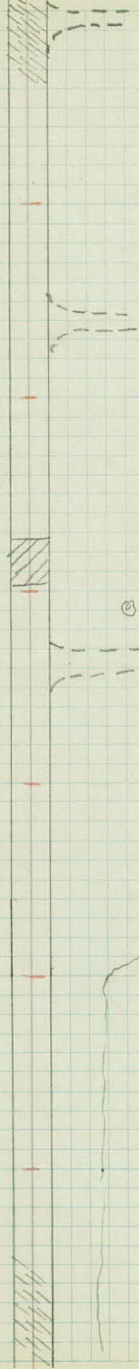
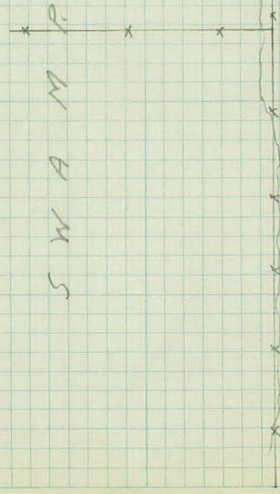
117 T.P.-28

Swamp-36'

+32-T.P.-

116 Fe + Swamp-34'

S W A M P P A S T U R E Lowland



Uncult

③

Lowland

+85-P.T.P.-

129

+47 Δ Ent

+66-P.T.P.-29'

128

+55-End 15" C.M. Side Drain-22'
+38.02-26' Road
+15-End 15" Side Drain-22'
+09-FC Cor-32'

+73-P.P.-29'
+60-BI. Top-100'
+50-BI. Top-10'
+45-End 18" C.M.-16'
+34-End of 15" C.M.-67'
+30-BI. Top-15-73'-106'
+15-BI. Top-37-56'
BI. Top-83'

127

+95 G.P.-24'

+50-BI. Top-38'
+42-T.P.-56'
+24 S.D. F.M.H.-21.5'
+02-T.P.-28'

126

+76 Δ Ent

+90-BI. Top-10'

+86-Ent

+61-End 18 C.M.-25'

+28-T.P.-24'

+10-T.P.-28'

125 FC-31'

+77 Δ Ent

+51-T.P.-25'

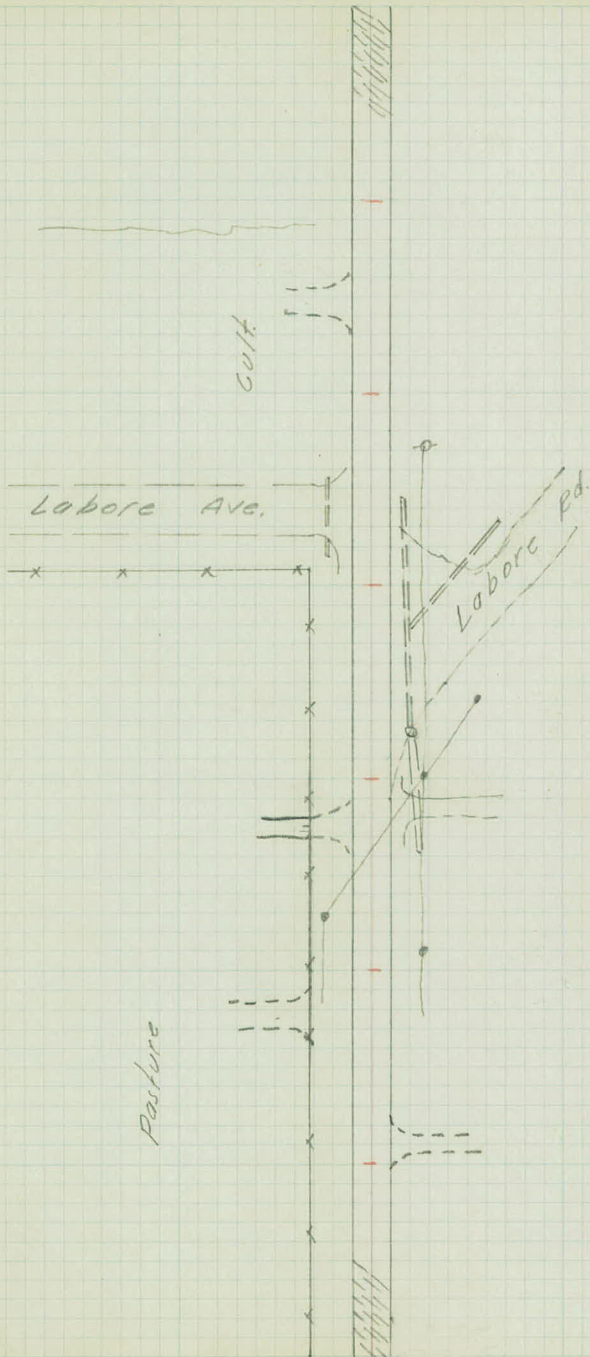
124

+11 Δ Ent

+90-T.P.-

+43-T.P.-

123



500000

+71-Ent $\frac{15" \times 20' CM}{25'}$

136
+97-Ent. Cult.?
+83-Hedge-32'
+85-PP-28'

+86 & Double Ent
+87-PP-28'
+86-Shrub-33'
+72-Shrub-33'
+61-Shrub-33'
+50-Shrub
+41-Shrub
+31-Shrub-33'
+20-Shrub-33'

135 Ent $\frac{15" \times 20' CM}{26'}$

+83-Row Pop-40'
+78-4" Elm-39'

+55-4" Elm-39'

+32-4" Elm-39'

+09-4" Elm-39'

+95-Ent $\frac{15" \times 20' CM}{25'}$

+38-T.P.-

134
+98-Ent $\frac{15" \times 20' CM}{26'}$

+86-PP-29

+84-Row 6" Pop-39' 190-Ent $\frac{10" \times 20' CM}{24'}$
+72-Ent $\frac{15" \times 20' CM}{24'}$

133
+96-Ent $\frac{15" \times 20' CM}{25'}$

+87-P + T.P.-

+74-Ent $\frac{15" \times 20' CM}{25'}$

132 $\frac{15" \times 20' CM}{25'}$

+97-
+83-Row 3" Pop-34'
+86-PP-26'

+67-Ent $\frac{15" \times 20' CM}{25'}$

+35-P + T.P.-29

131

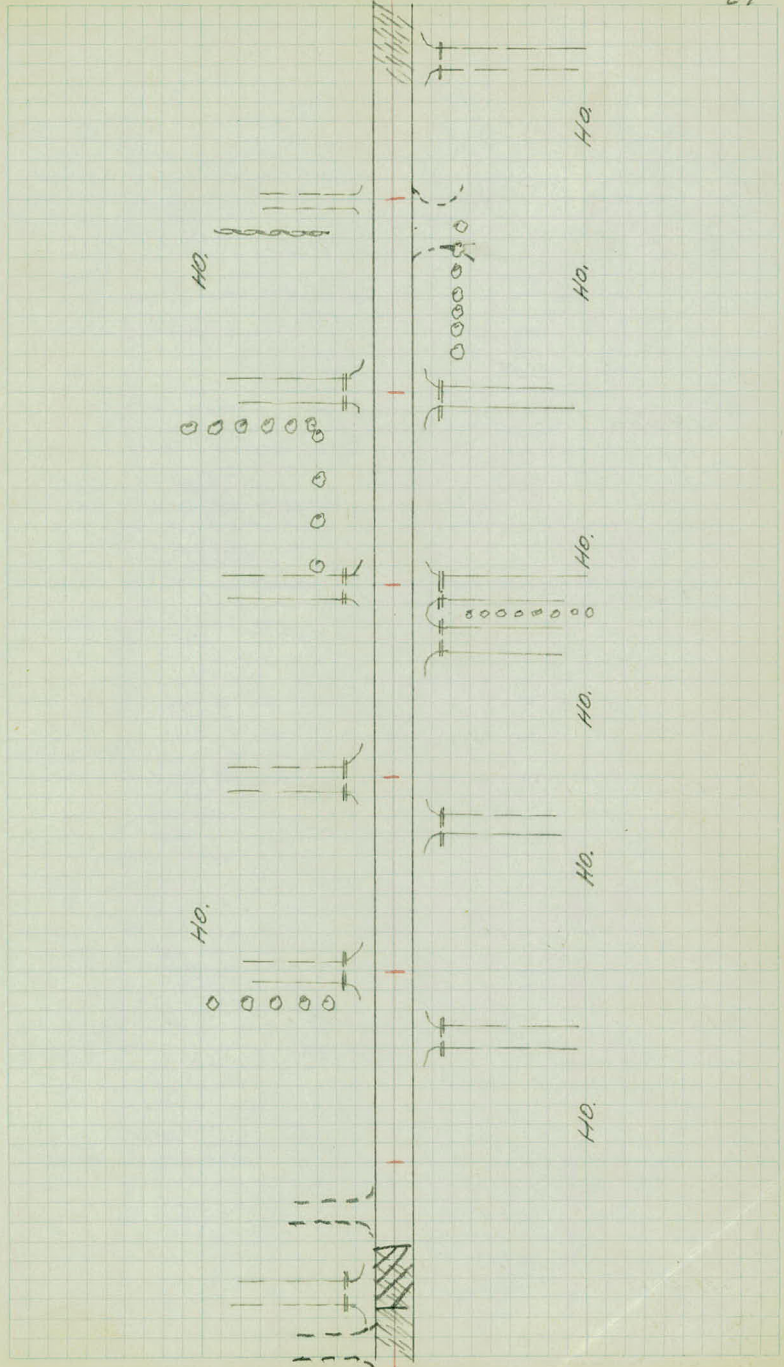
+76 & Ent

+24 to +58 Bump + Patch

+93-Ent $\frac{15" \times 20' CM}{22'}$

+04 & Ent

130



+97-Ent $\frac{15'' \times 20' CM}{26}$

+89-Row Pop-41'
+85-PP-28

+96-Ent-

+37-T+PP-28'

+08 ♀ Ent

143 Ent- $\frac{15'' \times 20' CM}{26}$

+73 ♀ Ent

+76-Ent $\frac{15'' \times 20' CM}{25}$

142 +09-Ent $\frac{15'' \times 20' CM}{26}$

+87-PP-28
+85-Hedge-39

+87-T+PP-

+24-Ent- $\frac{15'' \times 20' CM}{25}$

+92-Row-Pop-2'

141 +91-Ent- $\frac{15'' \times 20' CM}{25}$

+80-6" Elm-39'

+47-6" Elm-39'

+38-Ent- $\frac{15'' \times 20' CM}{26}$

+25-4" Elm-39'

+37-T+PP-

140 +90-6" Elm-39'
+85-PP-28

+98-Ent $\frac{15'' \times 20' CM}{25}$

+59-30" Tw. Catt.-19'

139 +05-Ent- $\frac{15'' \times 20' CM}{25}$

+12-6" Elm-38'

+98-Ent $\frac{15'' \times 20' CM}{25}$

+87-PP+T.P.-28'

138 +12-6" Elm-39'
+98-Ent $\frac{15'' \times 20' CM}{25}$

Ent $\frac{15'' \times 20' CM}{25}$

+33-6" Pop-38'

+36-PP

137 +19 Ent $\frac{15'' \times 20' CM}{25}$

+03 ♀ Ent

0 0 0 0 0 0

Ho.

Ho.

Ho.

Ho.

198-Ent- $\frac{15' \times 20' \text{ C.M.}}{25'}$

+60-4" Elm-40'

147-Ent $\frac{15' \times 20' \text{ C.M.}}{25'}$

+30-4" Elm-40'

150

+86-PP-28'

+69-Ent $\frac{12' \times 20' \text{ C.M.}}{25'}$

149

+87-Row 1" Pop-40'

+67-Ent $\frac{15' \times 20' \text{ C.M.}}{25'}$

148

+92-Row 1" Pop-40'

147

+96-Ent. $\frac{15' \times 20' \text{ C.M.}}{25'}$

146

+86-Ent. $\frac{15' \times 20' \text{ C.M.}}{25'}$

145

+01 E Allen Ave 20' Ent

+82-Hedge-35'

144

+96-Ent $\frac{15' \times 20' \text{ C.M.}}{25'}$

+88-Hedge-48'

+86-P+TP-29'

+84-Cor Hedge-33'

+86-Cor Hedge-34'

+98-Ent $\frac{15' \times 20' \text{ C.M.}}{25'}$

+83

+36-P+TP-

+98-Ent $\frac{15' \times 20' \text{ C.M.}}{25'}$

+07-Ent $\frac{15' \times 20' \text{ C.M.}}{25'}$

+87-P+TP-29'

+97 E Ent

+38-T+PP-

+99-Ent $\frac{15' \times 30' \text{ C.M.}}{25'}$

+77-Ent

+89-Hedge-43'

+86-P+TP-

4-6-94

HO.

HO.

HO.

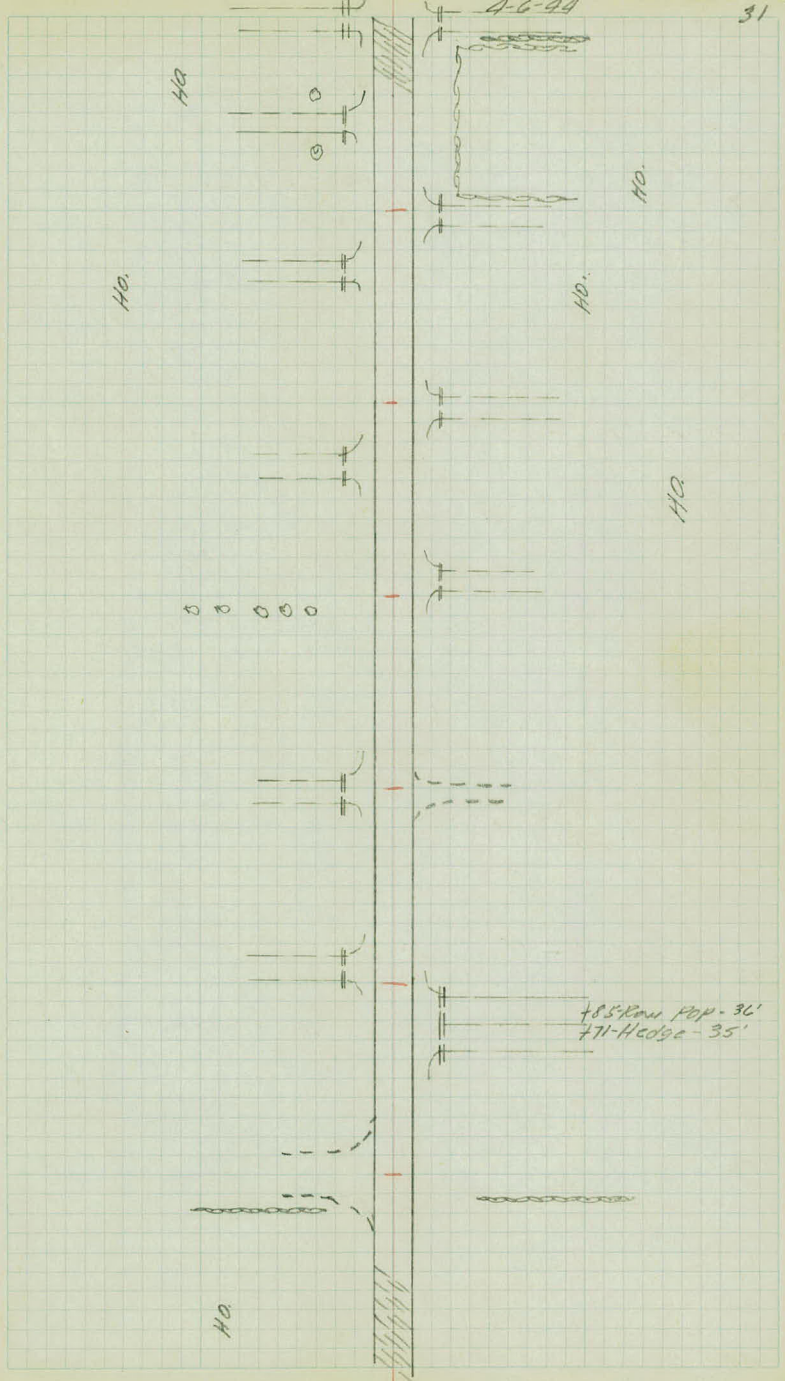
HO.

HO.

3 8 0 0 0

+8.5' Low Pop - 36'
+71' Hedge - 35'

HO.



176-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

157

188-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

108-P.T.P-29'

156

197-PP-29'

119-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

+93 $\pm$ Ent

142-P.T.P-29'

155

110-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

195-Power Line X $\pm$ 3 Wires

+13 $\pm$ Ent

154

199-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

186-P.T.P-30'

153

109-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

198-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

149-Shrub- 189-Co-Shrub-36'

138-Shrub- 172-Shrub-

136-P.T.P- 161-Shrub-

+28-Shrub-

117-Shrub-

106-Pg. Co. Shrub-36'

152

197-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

197-Ent- $\frac{15' \times 20' \text{ CM}}{25'}$

184-Co. Hedge-48'

151

184-Co. Hedge-48'

4-10-41

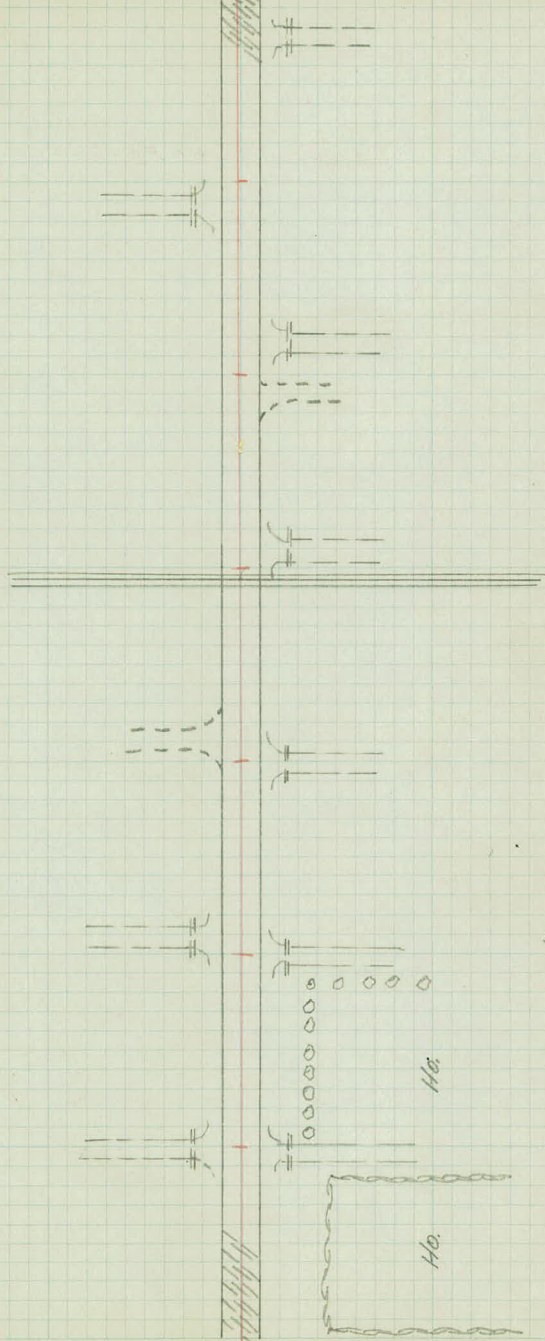
Ho.

Ho.

Ho.

Ho.

Ho.



+71-PP-44

153-2 15' Road $\frac{10'' \times 30' \text{ C.M.}}{22'}$

+59-Ent $\frac{20'' \times 12' \text{ Vit}}{20'}$

+26-8" Elm-35'

+10-Ent $\frac{20'' \times 12' \text{ Vit}}{20'}$

164

+91-T.P.-

+73-3" Elm-35'

+26-3" Elm-35'

+13-Ent $\frac{20'' \times 12' \text{ Vit}}{25'}$

+04-PP-44

163

+75-T.P.-

162

+86-Row 1 Pines-52'

+83-Ent G.R.-143'

+01-1 Pines 52' Row

$\frac{16'' \times 16.2'}{25'}$

+78-T.P.-29'

2 Bottom Dike hole

+66-2 Box Culv.

$32.5' \times 6' \times 6' \text{ Conc. Culv.} - 18'' \times 5.6' \text{ Wing Walls}$

+93-6" Elm-51'

+97-N.E. Cor Ho.-95'

+54 to +75 Cracked Pave.

+29-6" Elm-51'

+04-6" Elm-51'

161

+77-G.R.-143'

+88-Ent $\frac{18'' \times 30' \text{ C.M.}}{26'}$

+73-18" Conc. Culv.-25'

+16-Row 1 Pines-46'

+55-G.R.-45'

+27-Ent G.R. Poles-40'

+14-Box 18" Vit-25'

+12-PP-T.P.-28'

+08-Box G.R. Posts-15'

160

+95-Ent $\frac{15'' \times 30' \text{ C.M.}}{25'}$

+88-N.E. Cor-Ho.-92'

+16 to +20 Bump & Patch

+28-Ent $\frac{15'' \times 30' \text{ C.M.}}{25'}$

159

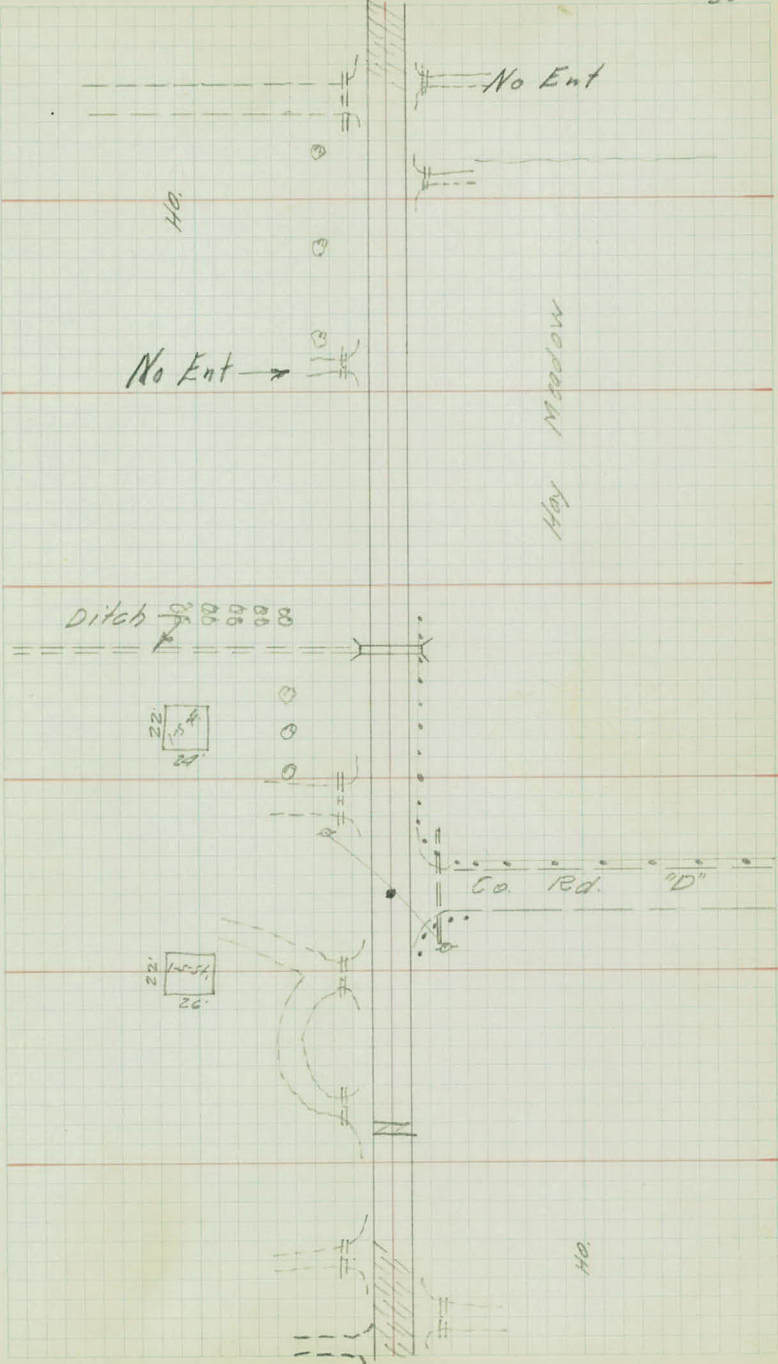
+57-PP-T.P.-

+50-Ent $\frac{15'' \times 20' \text{ C.M.}}{25'}$

+20-Ent $\frac{15'' \times 20' \text{ C.M.}}{25'}$

+06-2 Ent

158



No Ent

No Ent

Hay Meadow

Ditch

Co. Rd. "D"

22' 24'

22' 22'

Ho.

Ho.

169-Ent $\frac{12" \times 18' \text{ CM}}{25'}$

170-Ent $\frac{12" \times 18' \text{ CM}}{24'}$

158-T.P.-27'

171

138-T.P.

170

117-T.P.-

169

172-18" Elm-40'

140-Ho

106-2 1' Bottom ditch

122-3" Elm-40'
105-Ent $\frac{15" \times 20' \text{ CM}}{24'}$

115-Ent $\frac{12" \times 18' \text{ CM}}{23'}$

168

180-P.P.-44'

181-T.P.-

167

157-T.P.-

135-P.P.

166 115-Ent $\frac{15" \times 20' \text{ CM}}{22'}$

166

165 128-T.P.-

Cult.

Cult.

Ho.

Ditch 2

Uncult.

Ho.

a

b

178

+09-T.P.-27'

177
+16-Ent.- $\frac{12'' \times 18' \text{ C.M.}}{25'}$

+25-~~E~~ Double Ent $\frac{12'' \times 38' \text{ C.M.}}{23'}$

+80-T.P.-

176

+51-T.P.-

175

+20-T.P.-

174

+76-Ent $\frac{12'' \times 18' \text{ C.M.}}{26'}$

+76-Ent - $\frac{12'' \times 18' \text{ C.M.}}{23'}$

173

+99-T.P.-

172

cult



cult.

cult



cult

Edge Load - 53'

+70-B1/Top-23'

460-Rd-23'

+53-Epd 15" C.M. - 25'

+90. Rubble Gutter - 16'-22'

420-B1. Top - 41

+11-End 18" Conc. Culv. -49

185 18" X 50' Conc. Culv.

481-TP-25

472-B1. Top - 30' - 69'

+66-End 18" Conc. Culy-25"

469-81 Top-46

+55-Block Top-10'

140-PR-

+52-Bag. Bubble Gutter-18'-24'

+ 41 ϕ Ent

+01 ♀ Ent

184

423-T.P.-

183

+90-N.E. Cor Cor F Chick Coop
264' 2

26.4' 2

f 98-Entf

+43 Ent

177-Ent. - $\frac{12'' \times 206.17}{21'}$

182

496-T.P.-

181

465-T.P.-

180

483-Ent-12" x 18" C + M
73'

177-Ent - $\frac{12'' \times 166 \text{ M.}}{21''}$

438-TP-

179

LT

Z

RT

$\frac{12.9}{50}$ $\frac{11.2}{35}$ $\frac{11.8}{29}$ $\frac{12.1}{26}$ $\frac{11.6}{22}$ $\frac{9.4}{17}$ $\frac{9.2}{14}$ $\frac{9.3}{16}$ 9.2 $\frac{9.3}{10}$ $\frac{9.2}{11}$ $\frac{9.5}{15}$ $\frac{11.4}{20-22}$ $\frac{11.0}{29}$ $\frac{7.8}{26}$ $\frac{9.1}{50}$ $\frac{9.6}{60}$

$\frac{11.2}{50}$ $\frac{10.2}{44}$ $\frac{10.7}{34}$ $\frac{11.9}{27-24}$ 9.1 $\frac{8.9}{16}$ $\frac{8.9}{13}$ $\frac{8.9}{10}$ 8.8 $\frac{8.9}{10}$ $\frac{8.9}{12}$ $\frac{8.8}{14}$ $\frac{9.5}{18}$ $\frac{10.8}{21-24}$ $\frac{10.2}{26}$ $\frac{3.4}{38}$ $\frac{4.0}{52}$

$\frac{10.7}{50}$ $\frac{10.3}{33}$ $\frac{11.1}{27}$ $\frac{10.8}{23}$ $\frac{8.0}{15}$ $\frac{7.9}{10}$ 7.8 $\frac{7.9}{10}$ $\frac{7.9}{14}$ $\frac{8.6}{18}$ $\frac{9.3}{20}$ $\frac{8.5}{22}$ $\frac{0.1}{25}$ $\frac{1.0}{37}$ $\frac{1.0}{50}$

$\frac{15.9}{50}$ $\frac{15.1}{42}$ $\frac{13.2}{34}$ $\frac{12.9}{31}$ $\frac{10.6}{25}$ $\frac{6.8}{16}$ $\frac{6.8}{10}$ 6.7 $\frac{6.8}{10}$ $\frac{6.8}{15}$ $\frac{8.4}{21}$ $\frac{9.1}{28}$ $\frac{1.5}{37}$ $\frac{1.1}{50}$

$\frac{17.7}{60}$ $\frac{15.6}{50}$ $\frac{14.6}{37}$ $\frac{13.8}{33}$ $\frac{5.8}{30}$ $\frac{5.6}{16}$ $\frac{5.6}{10}$ 5.5 $\frac{5.5}{10}$ $\frac{5.6}{14}$ $\frac{7.2}{22}$ $\frac{7.3}{26}$ $\frac{7.0}{30}$ $\frac{3.4}{40}$ $\frac{3.3}{50}$

$\frac{16.5}{60-50}$ $\frac{15.3}{40}$ $\frac{14.1}{34}$ $\frac{13.2}{31}$ $\frac{4.7}{16}$ $\frac{4.5}{12}$ $\frac{4.5}{10}$ 4.3 $\frac{4.4}{10}$ $\frac{4.4}{16}$ $\frac{5.5}{21}$ $\frac{5.9}{26}$ $\frac{4.9}{30}$ $\frac{5.4}{31-35}$ $\frac{4.2}{40}$ $\frac{3.7}{50}$

$\frac{15.8}{60}$ $\frac{15.6}{50}$ $\frac{13.1}{36}$ $\frac{12.6}{33}$ $\frac{12.1}{30}$ $\frac{3.3}{17}$ $\frac{3.1}{11}$ $\frac{3.1}{10}$ 2.8 $\frac{3.0}{10}$ $\frac{2.9}{13}$ $\frac{3.1}{19}$ $\frac{5.6}{25-27}$ $\frac{3.8}{31}$ $\frac{4.5}{37}$ $\frac{4.3}{50}$

$\frac{12.6}{50}$ $\frac{10.0}{34-31}$ 2.1 $\frac{1.5}{16}$ $\frac{1.5}{12}$ $\frac{1.5}{10}$ 1.4 $\frac{1.5}{10}$ $\frac{1.4}{11}$ $\frac{1.7}{16}$ $\frac{3.4}{21-23}$ $\frac{4.8}{24-27}$ $\frac{2.5}{27-31}$ $\frac{3.8}{34}$

$\frac{18.8}{50}$ $\frac{12.2}{35}$ $\frac{16.5}{29}$ $\frac{10.8}{16}$ $\frac{10.6}{10}$ 10.5 $\frac{10.7}{10}$ $\frac{10.6}{11}$ $\frac{10.8}{15}$ $\frac{13.3}{24}$ $\frac{14.5}{25-27}$ $\frac{12.4}{29-30}$ $\frac{13.8}{32}$ $\frac{14.5}{32}$

$\frac{14.0}{50}$ $\frac{14.7}{36}$ $\frac{13.3}{26}$ $\frac{9.2}{17}$ 9.0 8.9 $\frac{9.1}{10}$ $\frac{9.0}{11}$ $\frac{9.3}{16}$ $\frac{13.1}{24}$ $\frac{13.5}{25}$ $\frac{11.8}{30}$ $\frac{13.4}{31}$ $\frac{14.1}{39}$ $\frac{14.1}{50}$

$\frac{11.8}{50}$ $\frac{12.4}{35}$ $\frac{12.6}{31}$ $\frac{11.8}{25}$ $\frac{7.7}{15}$ $\frac{7.4}{10}$ 7.4 $\frac{7.5}{10}$ $\frac{7.5}{11}$ $\frac{7.6}{15}$ $\frac{11.8}{25-27}$ $\frac{10.4}{29-30}$ $\frac{12.7}{38}$ $\frac{13.2}{50}$

$\frac{8.2}{50}$ $\frac{9.5}{38}$ $\frac{10.0}{33}$ $\frac{10.0}{28}$ $\frac{5.9}{16}$ $\frac{5.8}{10}$ 5.8 $\frac{5.9}{10}$ $\frac{6.0}{15}$ $\frac{9.5}{24}$ $\frac{10.2}{25-27}$ $\frac{8.8}{29-30}$ $\frac{11.2}{34}$ $\frac{13.1}{50}$

STA	+	π	-	ELEV
		896.11		
125+50				92.0
+61				92.4
+70				92.7
126				93.7
+07				93.9
T.P.	10.32	905.44	0.99	895.12
126				93.7
+07				93.9
+50				95.3
+75				96.1
127				96.8
+06				97.0
+12				97.1

LT

♀

RT

$\frac{7.6}{50} \frac{7.2}{38} \frac{6.0}{32} \frac{5.5}{24} \frac{5.7}{20} \frac{4.0}{16} \frac{4.0}{16} \frac{4.1}{10} \frac{4.3}{10} \frac{4.6}{16} \frac{7.7}{23} \frac{8.9}{25} \frac{6.5}{27} \frac{8.8}{29} \frac{9.0}{30} \frac{8.8}{34} \frac{9.0}{50}$

$\frac{7.9}{50} \frac{7.1}{44} \frac{6.0}{33} \frac{5.5}{27} \frac{5.2}{21} \frac{3.7}{15} \frac{3.7}{10} \frac{3.7}{10} \frac{3.8}{10} \frac{4.1}{16} \frac{7.3}{24} \frac{8.5}{25} \frac{6.2}{27} \frac{8.4}{29} \frac{7.8}{30} \frac{7.8}{33} \frac{7.8}{50}$

$\frac{6.2}{54-50} \frac{6.5}{39} \frac{4.8}{32} \frac{4.8}{20} \frac{3.4}{15} \frac{3.4}{10} \frac{3.4}{10} \frac{3.5}{10} \frac{3.5}{21} \frac{4.1}{27} \frac{5.0}{39} \frac{5.8}{50}$

$\frac{0.0}{50} \frac{3.0}{45} \frac{3.0}{39} \frac{3.3}{32} \frac{3.5}{26} \frac{4.1}{25} \frac{2.5}{20} \frac{2.4}{15} \frac{2.4}{10} \frac{2.6}{15} \frac{2.4}{20} \frac{3.3}{22} \frac{5.1}{50}$

$\frac{1.4}{41} \frac{2.9}{38} \frac{2.9}{32} \frac{3.2}{25} \frac{3.9}{23} \frac{2.3}{19} \frac{2.2}{15} \frac{2.2}{10} \frac{2.2}{10} \frac{2.4}{16} \frac{1.8}{19} \frac{1.8}{22} \frac{2.0}{27} \frac{2.6}{33} \frac{1.9}{31} \frac{2.0}{50}$

$\frac{2.8}{62} \frac{5.4}{56} \quad (11.7)$

$\frac{3.1}{60} \frac{6.0}{50} \quad (11.5)$

C.L.
LABORE

$\frac{3.0}{60} \frac{3.6}{50} \frac{4.6}{41} \frac{9.6}{33} \frac{10.0}{28} \frac{11.2}{24} \frac{10.3}{20} \frac{10.1}{17} \frac{10.1}{10} \frac{10.2}{10} \frac{9.6}{16} \frac{9.7}{22} \frac{9.6}{31} \frac{10.0}{38} \frac{6.9}{47} \frac{6.2}{50}$

C.L.
LABORE

$\frac{3.0}{60} \frac{3.2}{50} \frac{4.1}{38} \frac{7.7}{34} \frac{7.9}{29} \frac{10.8}{23} \frac{10.7}{19} \frac{9.4}{16} \frac{9.3}{10} \frac{9.3}{10} \frac{9.4}{10} \frac{9.3}{10} \frac{9.4}{10} \frac{9.3}{10} \frac{9.3}{10} \frac{9.3}{10}$

♀
LABORE

$\frac{4.8}{60} \frac{4.6}{50} \frac{4.8}{38} \frac{4.3}{33} \frac{10.1}{24} \frac{9.7}{20} \frac{8.6}{16} \frac{8.6}{10} \frac{8.6}{10} \frac{8.1}{16} \frac{7.2}{29} \frac{6.1}{49} \frac{5.9}{57}$

♀
LABORE

$\frac{4.9}{50} \frac{4.6}{33} \frac{9.7}{23} \frac{8.4}{20} \frac{8.4}{16} \frac{8.4}{10} \frac{8.4}{10} \frac{8.5}{10} \frac{7.7}{16} \frac{7.2}{31} \frac{5.9}{57} \frac{5.5}{66}$

♀
LABORE

$\frac{7.1}{50} \frac{7.3}{31} \frac{9.5}{24} \frac{9.6}{20} \frac{8.3}{17} \frac{8.3}{10} \frac{8.3}{10} \frac{8.3}{10} \frac{8.3}{10} \frac{7.7}{16} \frac{7.4}{30} \frac{6.2}{50} \frac{5.2}{66}$

STA	+	π	-	ELEV
		905.44		
127+17				973
+24				97.5
+37				978
	ϕ	LA BORE RD WEST LT		
+50				982
+54				984
+59				985
128				99.8
+50				01.6
129				03.0
T.P.	8.20	912.61	1.03	904.41
+50				044
130				05.6
+50				069

LT

L

RT

LABORE

$\frac{9.1}{50}$	$\frac{7.4}{23}$	$\frac{8.1}{19}$	$\frac{8.2}{10}$	<u>8.1</u>	$\frac{8.2}{10}$	$\frac{7.9}{14}$	$\frac{7.2}{39}$	$\frac{5.4}{60}$	$\frac{4.9}{72}$
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LABORE

$\frac{7.8}{50}$	$\frac{7.9}{35}$	$\frac{7.9}{25}$	$\frac{8.0}{10}$	<u>7.9</u>	$\frac{8.0}{10}$	$\frac{7.8}{27}$	$\frac{6.9}{39}$	$\frac{5.8}{58}$	$\frac{5.6}{60}$	$\frac{4.3}{75}$
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LABORE

$\frac{6.5}{100}$	$\frac{6.9}{50}$	$\frac{7.3}{27}$	$\frac{7.6}{10}$	<u>7.6</u>	$\frac{7.7}{10}$	$\frac{7.1}{20}$	$\frac{6.2}{36}$	$\frac{4.9}{60}$	$\frac{3.7}{90}$
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$\frac{7.4}{50}$	$\frac{7.4}{26}$	$\frac{7.1}{16}$	$\frac{7.2}{10}$	<u>7.2</u>	$\frac{7.3}{10}$	$\frac{7.2}{14}$	$\frac{8.7}{18-24}$	$\frac{6.2}{28}$	$\frac{5.6}{50}$
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$\frac{8.4}{50}$	$\frac{8.6}{25}$	$\frac{8.6}{21}$	$\frac{7.5}{20}$	$\frac{7.0}{10}$	<u>7.0</u>	$\frac{7.2}{10}$	$\frac{7.0}{13}$	$\frac{8.2}{17}$	$\frac{8.0}{22}$	$\frac{6.0}{30}$	$\frac{5.7}{50}$
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$\frac{6.6}{50}$	$\frac{6.4}{32}$	$\frac{8.7}{25-22}$	$\frac{7.2}{17}$	$\frac{6.9}{10}$	<u>6.9</u>	$\frac{7.0}{10}$	$\frac{7.0}{14}$	$\frac{8.1}{17}$	$\frac{8.0}{21}$	$\frac{6.1}{28}$	$\frac{5.7}{50}$
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$\frac{5.6}{50}$	$\frac{5.4}{34}$	$\frac{7.6}{23-21}$	$\frac{5.6}{17}$	$\frac{5.6}{10}$	<u>5.6</u>	$\frac{5.7}{10}$	$\frac{5.6}{14}$	$\frac{6.8}{17-20}$	$\frac{4.6}{29}$	$\frac{3.7}{50}$
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$\frac{4.2}{50}$	$\frac{3.5}{42-36}$	$\frac{5.3}{26}$	$\frac{5.6}{22}$	$\frac{4.1}{17}$	$\frac{3.8}{10}$	<u>3.8</u>	$\frac{4.0}{10}$	$\frac{4.0}{15}$	$\frac{5.0}{17-20}$	$\frac{2.6}{29}$	$\frac{2.4}{50}$
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$\frac{2.3}{50}$	$\frac{1.8}{39}$	$\frac{3.5}{30}$	$\frac{4.1}{23-20}$	$\frac{2.5}{16}$	$\frac{2.5}{10}$	<u>2.4</u>	$\frac{2.5}{10}$	$\frac{2.6}{16}$	$\frac{3.4}{17}$	$\frac{3.2}{19}$	$\frac{0.2}{28}$	$\frac{0.0}{50}$
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$\frac{6.7}{50}$	$\frac{7.4}{32}$	$\frac{9.6}{24-20}$	$\frac{8.4}{17}$	$\frac{8.3}{10}$	<u>8.2</u>	$\frac{8.3}{10}$	$\frac{8.4}{15}$	$\frac{9.4}{17-19}$	$\frac{5.2}{29}$	$\frac{4.8}{35}$	$\frac{2.7}{39}$	$\frac{2.6}{50}$
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$\frac{4.8}{50}$	$\frac{5.2}{33}$	$\frac{8.4}{24-20}$	$\frac{7.3}{17}$	$\frac{7.0}{10}$	<u>7.0</u>	$\frac{7.1}{10}$	$\frac{7.2}{15}$	$\frac{8.1}{17-19}$	$\frac{7.8}{20}$	$\frac{6.3}{23}$	$\frac{4.1}{33}$	$\frac{4.1}{50}$
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$\frac{3.8}{50}$	$\frac{4.8}{32}$	$\frac{5.7}{28}$	$\frac{7.2}{24-20}$	$\frac{5.9}{16}$	$\frac{5.7}{10}$	<u>5.7</u>	$\frac{5.8}{10}$	$\frac{5.7}{16}$	$\frac{9.6}{17-19}$	$\frac{6.5}{20}$	$\frac{5.3}{23}$	$\frac{3.9}{38}$	$\frac{4.4}{50}$
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STA	+	π	-	ELEV
		912.61.		
131+00				080
+50				09.1
132				09.9
B.M	6.72	916.12.	3.24	909.37. 909.40.
+50				10.3
133				10.8
+50				10.9
134				11.0
+50				11.1
135				11.2
+50				11.2
136				11.2
+50				11.1

L.T

4

R.T

$\frac{3.4}{50}$ $\frac{4.1}{33}$ $\frac{5.8}{23-19}$ $\frac{4.7}{15}$ $\frac{4.7}{10}$ $\frac{4.7}{10}$ $\frac{5.0}{18}$ $\frac{5.7}{20-22}$ $\frac{4.7}{28}$ $\frac{3.4}{50}$

$\frac{3.1}{50}$ $\frac{3.6}{36}$ $\frac{4.4}{26-20}$ $\frac{5.2}{24}$ $\frac{3.8}{16}$ $\frac{3.5}{10}$ $\frac{3.5}{10}$ $\frac{3.6}{16}$ $\frac{4.9}{20}$ $\frac{5.6}{22-25}$ $\frac{3.4}{50}$

$\frac{2.9}{50}$ $\frac{3.1}{28}$ $\frac{5.2}{26-22}$ $\frac{3.0}{17}$ $\frac{2.8}{10}$ $\frac{2.7}{10}$ $\frac{3.1}{16}$ $\frac{5.5}{22-26}$ $\frac{3.5}{30}$ $\frac{3.5}{50}$

HIGH POINT MONT STA 131+62.55

$\frac{6.4}{50}$ $\frac{6.6}{32}$ $\frac{8.8}{27-24}$ $\frac{7.8}{22}$ $\frac{5.8}{13}$ $\frac{5.7}{10}$ $\frac{5.8}{10}$ $\frac{6.1}{17}$ $\frac{7.7}{21}$ $\frac{9.0}{23-26}$ $\frac{6.8}{30}$ $\frac{6.8}{50}$

$\frac{6.3}{50}$ $\frac{6.9}{30}$ $\frac{8.7}{26-23}$ $\frac{7.5}{21}$ $\frac{5.9}{17}$ $\frac{5.3}{12}$ $\frac{5.4}{10}$ $\frac{5.4}{10}$ $\frac{5.5}{13}$ $\frac{7.5}{20}$ $\frac{8.9}{23-26}$ $\frac{7.2}{30}$ $\frac{6.9}{50}$

$\frac{6.3}{50}$ $\frac{6.5}{32}$ $\frac{8.7}{27-24}$ $\frac{7.8}{23}$ $\frac{5.8}{15}$ $\frac{5.2}{10}$ $\frac{5.3}{10}$ $\frac{5.5}{15}$ $\frac{7.9}{22}$ $\frac{8.7}{23}$ $\frac{8.3}{27}$ $\frac{7.0}{30}$ $\frac{6.6}{50}$

$\frac{6.5}{50}$ $\frac{6.5}{32}$ $\frac{8.7}{26-23}$ $\frac{8.3}{22}$ $\frac{5.3}{14}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.6}{17}$ $\frac{8.3}{23}$ $\frac{8.1}{28}$ $\frac{7.2}{30}$ $\frac{6.8}{50}$

$\frac{6.5}{50}$ $\frac{6.2}{32}$ $\frac{8.8}{26-23}$ $\frac{7.6}{20}$ $\frac{6.1}{17}$ $\frac{5.3}{14}$ $\frac{5.1}{10}$ $\frac{5.1}{10}$ $\frac{5.2}{15}$ $\frac{6.0}{18}$ $\frac{7.8}{23}$ $\frac{8.8}{24-27}$ $\frac{6.5}{32}$ $\frac{6.6}{50}$

$\frac{6.7}{50}$ $\frac{6.7}{31}$ $\frac{8.4}{27-23}$ $\frac{5.9}{16}$ $\frac{5.3}{14}$ $\frac{5.1}{10}$ $\frac{5.0}{10}$ $\frac{5.0}{14}$ $\frac{6.7}{20}$ $\frac{8.7}{24-28}$ $\frac{7.1}{30}$ $\frac{6.7}{50}$

$\frac{6.6}{50}$ $\frac{6.8}{31}$ $\frac{8.5}{27-23}$ $\frac{5.8}{17}$ $\frac{5.2}{14}$ $\frac{5.0}{10}$ $\frac{4.9}{10}$ $\frac{5.0}{13}$ $\frac{5.2}{18}$ $\frac{6.6}{22}$ $\frac{8.0}{23}$ $\frac{9.0}{23-26}$ $\frac{7.1}{29}$ $\frac{6.5}{50}$

$\frac{6.6}{50}$ $\frac{7.0}{30}$ $\frac{8.5}{26-23}$ $\frac{6.5}{16}$ $\frac{5.6}{14}$ $\frac{5.1}{12}$ $\frac{5.0}{10}$ $\frac{4.9}{10}$ $\frac{5.0}{15}$ $\frac{5.3}{19}$ $\frac{6.0}{22}$ $\frac{7.3}{23-26}$ $\frac{8.7}{31}$ $\frac{6.8}{50}$

$\frac{6.8}{50}$ $\frac{7.1}{28}$ $\frac{8.4}{26-23}$ $\frac{7.2}{20}$ $\frac{5.7}{16}$ $\frac{5.2}{14}$ $\frac{5.0}{10}$ $\frac{5.0}{10}$ $\frac{5.1}{12}$ $\frac{5.3}{18}$ $\frac{6.1}{22}$ $\frac{7.5}{23-26}$ $\frac{8.6}{30}$ $\frac{7.0}{50}$

STA	+	π	-	ELEV
		916.12		
137				11.1
+50				11.0
138				11.0
+50				11.0
139				10.8
T.P.	5.52	916.28.	5.36	910.76.
B.M	4.73	916.30.	4.73	911.55. 911.57.
+50				11.0
140				11.0
+50				11.2
141				11.2
+50				11.2
142				11.2
+50				11.1

LT

♀

PT

6.9	7.0	8.4	7.2	5.8	5.3	5.1	5.1	5.6	7.5	8.6	6.5	6.5	
50	28	25-23	20	17	14	10	5.0	10	12	22	23-26	31	50

7.4	7.4	8.3	5.9	5.3	5.2	5.2	5.4	5.7	7.6	8.6	6.9	6.6	
50	28	26-22	16	14	10	5.1	10	14	18	23	24-26	30	50

7.0	7.0	8.5	5.9	5.3	5.2	5.2	5.2	6.0	7.9	8.7	8.4	6.8	6.6	
50	28	25-22	16	12	10	5.1	10	14	16	20	22	26	29	50

6.8	7.0	8.2	8.1	6.2	5.6	5.2	5.2	5.6	6.5	8.6	8.7	6.8	6.5	
50	30	26	21	16	14	10	5.1	10	13	17	22	26	30	50

6.8	7.0	8.4	8.3	6.1	5.5	5.4	5.4	5.5	6.4	8.6	6.8	6.1	6.4	
50	30	26	21	16	13	10	5.3	10	15	18	23-26	30	40	50

SPIKE 24" COTTONWOOD 19" LT STA 139+65

7.1	7.1	8.1	8.0	6.8	5.5	5.4	5.3	5.3	5.7	8.5	6.5	6.5	
50	29	26	21	18	14	10	5.3	10	12	16	22-25	29	50

7.2	7.0	8.2	8.2	6.3	5.6	5.4	5.3	5.3	6.2	8.6	7.2	6.2	6.7	
50	30	27	22	18	15	10	5.3	10	12	17	22-25	28	37	50

7.7	6.9	8.4	8.0	5.9	5.4	5.2	5.2	5.5	6.1	7.4	8.4	7.6	7.5	6.8	6.8			
50	32	27	20	16	13	10	5.1	10	14	19	20	22	24	26	28	31	34	50

7.0	6.9	8.1	8.0	6.7	5.5	5.1	5.1	5.2	5.3	6.1	8.5	8.6	7.4	6.7	6.5
50	33	29	22	19	14	10	5.1	10	13	16	21	26	29	34	50

6.5	6.5	8.2	8.2	6.1	5.5	5.2	5.1	5.3	5.8	7.0	8.5	7.3	6.3	6.2	
50	33	28	21	17	14	10	5.1	10	13	16	19	22-25	28	37	50

7.0	7.0	8.0	6.4	5.4	5.2	5.2	5.4	6.5	8.2	8.5	6.9	6.4	
50	31	28-21	17	14	10	5.1	10	13	17	21	25	36	50

7.0	6.5	8.2	8.5	6.3	5.7	5.3	5.3	5.4	6.0	7.8	8.5	8.0	6.9	6.6	
50	35	30	21	16	13	10	5.2	10	13	16	20	24	30	38	50

STA	+	∇	-	ELEV
		916.30.		
143+00				11.1
+50				11.0
144				10.9
+50				10.9
T.P	4.53	915.28.	5.55	910.75.
145				10.9
+50				10.9
146				10.9
+50				10.8
147				10.6
+50				10.5
148				10.3
+50				10.3

LT

4

PT

$\frac{6.9}{50}$ $\frac{7.0}{42}$ $\frac{8.4}{28}$ $\frac{8.4}{21}$ $\frac{5.8}{16}$ $\frac{5.5}{12}$ $\frac{5.3}{10}$ $\frac{5.3}{52}$ $\frac{5.3}{70}$ $\frac{5.3}{15}$ $\frac{8.1}{21}$ $\frac{7.8}{29}$ $\frac{7.1}{33}$ $\frac{6.7}{50}$

$\frac{6.8}{50}$ $\frac{7.2}{40}$ $\frac{8.6}{26}$ $\frac{8.6}{21}$ $\frac{6.2}{16}$ $\frac{5.5}{12}$ $\frac{5.4}{10}$ $\frac{5.4}{53}$ $\frac{6.3}{10}$ $\frac{8.0}{17}$ $\frac{8.2}{21}$ $\frac{7.5}{29}$ $\frac{7.1}{31}$ $\frac{6.4}{34}$ $\frac{6.4}{40}$ $\frac{6.4}{50}$

$\frac{7.0}{50}$ $\frac{7.0}{36}$ $\frac{7.6}{30}$ $\frac{8.7}{28}$ $\frac{8.9}{22}$ $\frac{6.8}{17}$ $\frac{5.8}{13}$ $\frac{5.5}{10}$ $\frac{5.5}{54}$ $\frac{5.3}{10}$ $\frac{7.0}{12}$ $\frac{8.2}{18}$ $\frac{8.4}{21}$ $\frac{7.8}{26}$ $\frac{6.5}{31}$ $\frac{6.5}{37}$ $\frac{6.5}{50}$

$\frac{7.1}{50}$ $\frac{7.4}{31}$ $\frac{8.9}{27}$ $\frac{8.9}{21}$ $\frac{7.5}{18}$ $\frac{5.8}{13}$ $\frac{5.5}{10}$ $\frac{5.4}{54}$ $\frac{5.5}{10}$ $\frac{5.7}{14}$ $\frac{6.6}{17}$ $\frac{8.1}{21}$ $\frac{8.2}{31}$ $\frac{7.0}{34}$ $\frac{6.5}{50}$

$\frac{6.8}{50}$ $\frac{6.2}{31}$ $\frac{8.2}{27}$ $\frac{8.2}{22}$ $\frac{5.4}{16}$ $\frac{4.7}{13}$ $\frac{4.5}{10}$ $\frac{4.4}{44}$ $\frac{4.5}{10}$ $\frac{4.5}{12}$ $\frac{5.5}{17}$ $\frac{7.6}{21}$ $\frac{7.6}{26}$ $\frac{7.2}{30}$ $\frac{5.6}{35}$ $\frac{5.5}{50}$

$\frac{6.6}{50}$ $\frac{5.8}{30}$ $\frac{8.4}{26}$ $\frac{8.2}{21}$ $\frac{5.7}{15}$ $\frac{4.7}{12}$ $\frac{4.5}{10}$ $\frac{4.4}{44}$ $\frac{4.5}{10}$ $\frac{4.6}{12}$ $\frac{5.0}{17}$ $\frac{7.6}{23}$ $\frac{7.4}{28}$ $\frac{7.2}{30}$ $\frac{5.8}{35}$ $\frac{5.5}{50}$

$\frac{7.1}{50}$ $\frac{6.0}{30}$ $\frac{8.4}{26}$ $\frac{8.2}{21}$ $\frac{5.5}{16}$ $\frac{4.7}{13}$ $\frac{4.5}{10}$ $\frac{4.4}{44}$ $\frac{4.5}{10}$ $\frac{4.6}{12}$ $\frac{4.9}{14}$ $\frac{7.7}{21}$ $\frac{7.8}{30}$ $\frac{7.3}{31}$ $\frac{5.7}{35}$ $\frac{5.8}{50}$

$\frac{6.7}{50}$ $\frac{7.0}{30}$ $\frac{8.6}{25}$ $\frac{5.6}{23}$ $\frac{5.6}{15}$ $\frac{4.7}{12}$ $\frac{4.6}{10}$ $\frac{4.5}{45}$ $\frac{4.5}{10}$ $\frac{4.6}{13}$ $\frac{5.3}{16}$ $\frac{8.1}{22}$ $\frac{8.2}{29}$ $\frac{6.4}{32}$ $\frac{6.1}{50}$

$\frac{7.8}{50}$ $\frac{7.8}{33}$ $\frac{9.0}{26}$ $\frac{8.6}{21}$ $\frac{6.2}{16}$ $\frac{5.1}{13}$ $\frac{4.9}{10}$ $\frac{4.7}{47}$ $\frac{4.8}{10}$ $\frac{4.8}{12}$ $\frac{5.8}{17}$ $\frac{8.6}{24}$ $\frac{8.5}{30}$ $\frac{7.5}{33}$ $\frac{7.3}{50}$

$\frac{8.4}{50}$ $\frac{8.5}{25}$ $\frac{8.9}{24}$ $\frac{6.3}{23}$ $\frac{5.3}{16}$ $\frac{5.0}{12}$ $\frac{4.8}{10}$ $\frac{5.0}{70}$ $\frac{5.4}{13}$ $\frac{6.3}{17}$ $\frac{8.8}{23}$ $\frac{9.0}{31}$ $\frac{8.1}{33}$ $\frac{8.0}{50}$

$\frac{8.7}{50}$ $\frac{9.0}{30}$ $\frac{9.6}{27}$ $\frac{9.6}{21}$ $\frac{6.6}{17}$ $\frac{5.5}{13}$ $\frac{5.2}{10}$ $\frac{5.0}{50}$ $\frac{5.3}{10}$ $\frac{5.4}{12}$ $\frac{6.5}{16}$ $\frac{9.3}{23}$ $\frac{9.4}{32}$ $\frac{8.8}{33}$ $\frac{8.2}{50}$

$\frac{8.7}{50}$ $\frac{8.7}{31}$ $\frac{9.6}{28}$ $\frac{9.6}{22}$ $\frac{6.4}{15}$ $\frac{5.5}{12}$ $\frac{5.2}{10}$ $\frac{5.0}{50}$ $\frac{5.2}{10}$ $\frac{5.2}{12}$ $\frac{6.3}{16}$ $\frac{9.1}{23}$ $\frac{9.7}{28}$ $\frac{8.0}{33}$ $\frac{7.7}{50}$

STA	+	π	-	ELEV
		915.28.		
149+00				10.2
+50				10.2
150				10.3
B.M	5.96	915.10.	6.14	909.14.
+50				10.4
151				10.3
+50				10.2
152				10.1
+50				10.0
153				10.0
+50				10.0
154				10.0
+50				10.1

LT

E

RT

<u>8.1</u>	<u>8.0</u>	<u>9.4</u>	<u>9.6</u>	<u>9.1</u>	<u>6.2</u>	<u>5.4</u>	<u>5.2</u>	<u>5.2</u>	<u>5.4</u>	<u>6.1</u>	<u>8.3</u>	<u>9.2</u>	<u>9.3</u>	<u>7.5</u>	<u>6.7</u>	
50	30	26	24	23	16	12	10	5.1	10	14	16	22	23	27	33	50

<u>7.0</u>	<u>6.9</u>	<u>9.3</u>	<u>8.4</u>	<u>6.1</u>	<u>5.4</u>	<u>5.2</u>	<u>5.2</u>	<u>5.3</u>	<u>6.1</u>	<u>8.3</u>	<u>9.3</u>	<u>9.5</u>	<u>7.9</u>	<u>7.0</u>	<u>6.5</u>	
50	33	27-25	24	15	13	10	5.1	10	12	17	22	23-25	26	30	33	50

<u>5.8</u>	<u>6.2</u>	<u>7.5</u>	<u>9.0</u>	<u>9.5</u>	<u>8.2</u>	<u>6.0</u>	<u>5.4</u>	<u>5.1</u>	<u>5.1</u>	<u>5.2</u>	<u>6.1</u>	<u>8.3</u>	<u>9.1</u>	<u>7.6</u>	<u>6.2</u>	<u>6.4</u>	
50	34	31	27	28	22	16	13	10	5.0	10	12	17	22	25-27	30	34	50

SPIKE IN P.P. RT STA 149+50

<u>5.9</u>	<u>5.7</u>	<u>9.1</u>	<u>9.3</u>	<u>8.1</u>	<u>5.6</u>	<u>5.0</u>	<u>4.8</u>	<u>4.7</u>	<u>4.8</u>	<u>4.8</u>	<u>5.5</u>	<u>7.8</u>	<u>9.3</u>	<u>9.0</u>	<u>6.0</u>	<u>5.9</u>
50	34	27	23	22	16	12	10	4.7	10	12	16	22	23	25	23	50

<u>6.1</u>	<u>6.2</u>	<u>9.3</u>	<u>9.4</u>	<u>8.0</u>	<u>5.7</u>	<u>5.0</u>	<u>4.8</u>	<u>4.8</u>	<u>4.9</u>	<u>5.3</u>	<u>8.2</u>	<u>9.5</u>	<u>9.3</u>	<u>6.5</u>	<u>6.0</u>	
50	33	27	23	22	16	12	10	4.8	10	12	15	22	23	27	33	50

<u>6.0</u>	<u>6.5</u>	<u>9.3</u>	<u>9.5</u>	<u>8.2</u>	<u>6.2</u>	<u>5.4</u>	<u>4.9</u>	<u>4.9</u>	<u>4.9</u>	<u>5.0</u>	<u>5.7</u>	<u>8.5</u>	<u>9.5</u>	<u>9.1</u>	<u>6.4</u>	<u>6.0</u>
50	32	26	23	22	17	15	10	4.9	10	12	16	22	23	27	33	50

<u>6.5</u>	<u>6.6</u>	<u>9.2</u>	<u>9.3</u>	<u>7.9</u>	<u>5.4</u>	<u>5.0</u>	<u>5.1</u>	<u>5.3</u>	<u>8.1</u>	<u>9.4</u>	<u>9.0</u>	<u>6.0</u>	<u>5.8</u>	
50	33	26	23	22	12	10	5.0	10	12	22	23	27	34	50

<u>6.7</u>	<u>6.4</u>	<u>9.3</u>	<u>9.6</u>	<u>8.0</u>	<u>5.7</u>	<u>5.4</u>	<u>5.2</u>	<u>5.2</u>	<u>5.3</u>	<u>5.8</u>	<u>8.5</u>	<u>9.6</u>	<u>9.3</u>	<u>6.0</u>	<u>6.0</u>	
50	34	27	23	22	14	12	10	5.1	10	12	15	22	22	26	33	50

<u>6.6</u>	<u>6.6</u>	<u>9.3</u>	<u>9.5</u>	<u>8.6</u>	<u>6.2</u>	<u>5.5</u>	<u>5.2</u>	<u>5.2</u>	<u>5.3</u>	<u>5.9</u>	<u>8.5</u>	<u>9.5</u>	<u>9.5</u>	<u>6.2</u>	<u>6.2</u>	
50	34	27	23	22	16	12	10	5.1	10	12	16	22	23	27	33	50

<u>6.6</u>	<u>6.7</u>	<u>9.4</u>	<u>9.7</u>	<u>8.7</u>	<u>5.8</u>	<u>5.3</u>	<u>5.1</u>	<u>5.1</u>	<u>5.2</u>	<u>5.7</u>	<u>8.7</u>	<u>9.7</u>	<u>9.6</u>	<u>6.7</u>	<u>6.3</u>	
50	33	27	23	22	15	12	10	5.1	10	12	14	22	23	27	33	50

<u>6.6</u>	<u>6.0</u>	<u>9.6</u>	<u>9.9</u>	<u>8.5</u>	<u>5.8</u>	<u>6.2</u>	<u>5.1</u>	<u>5.1</u>	<u>5.1</u>	<u>8.4</u>	<u>10.0</u>	<u>10.4</u>	<u>9.9</u>	<u>6.6</u>	<u>6.7</u>	
50	33	27	23	22	16	13	10	5.1	10	12	22	23	25	27	33	50

<u>6.6</u>	<u>6.2</u>	<u>9.6</u>	<u>9.8</u>	<u>8.5</u>	<u>5.7</u>	<u>5.3</u>	<u>5.1</u>	<u>5.1</u>	<u>5.2</u>	<u>5.7</u>	<u>8.6</u>	<u>9.8</u>	<u>9.7</u>	<u>6.5</u>	<u>6.8</u>	
50	33	26	23	22	15	12	10	5.0	10	12	17	23	24	26	33	50

STA	+	π	-	ELEV	
		915.10			
155+00				10.1	
+50				10.1	
T.P.	5.61	914.44	6.27	908.83 909.83	
156				09.8	
+50				09.7	
157				09.6	
+50				09.5	
158				09.5	
+50				09.4	
159				09.2	
+50				09.2	
160				09.1	
B.M.	5.27	914.45	5.27	909.17	909.18
+14				09.2	

LT

E

RT

$\frac{6.7}{50}$ $\frac{6.5}{34}$ $\frac{9.9}{27}$ $\frac{10.0}{23}$ $\frac{8.6}{22}$ $\frac{6.0}{16}$ $\frac{5.3}{12}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.5}{12}$ $\frac{5.9}{16}$ $\frac{8.5}{22}$ $\frac{9.6}{23}$ $\frac{9.6}{27}$ $\frac{6.9}{33}$ $\frac{6.8}{50}$

$\frac{7.0}{50}$ $\frac{6.4}{34}$ $\frac{9.8}{27}$ $\frac{10.0}{23}$ $\frac{8.4}{22}$ $\frac{5.8}{15}$ $\frac{5.3}{12}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.3}{12}$ $\frac{5.9}{16}$ $\frac{8.6}{22}$ $\frac{9.8}{23}$ $\frac{9.7}{27}$ $\frac{6.9}{33}$ $\frac{6.8}{50}$

$\frac{6.5}{50}$ $\frac{6.3}{34}$ $\frac{8.8}{28}$ $\frac{8.9}{23}$ $\frac{7.7}{22}$ $\frac{5.4}{16}$ $\frac{4.9}{13}$ $\frac{4.7}{10}$ $\frac{4.7}{10}$ $\frac{4.8}{12}$ $\frac{5.3}{16}$ $\frac{8.3}{22}$ $\frac{9.3}{23}$ $\frac{9.3}{26}$ $\frac{6.0}{33}$ $\frac{6.2}{50}$

$\frac{6.7}{50}$ $\frac{6.6}{33}$ $\frac{9.3}{26}$ $\frac{9.3}{23}$ $\frac{7.9}{22}$ $\frac{5.4}{15}$ $\frac{4.9}{13}$ $\frac{4.8}{10}$ $\frac{4.8}{10}$ $\frac{5.0}{12}$ $\frac{5.2}{14}$ $\frac{7.9}{23}$ $\frac{9.3}{25}$ $\frac{6.2}{27}$ $\frac{6.2}{33}$ $\frac{6.2}{50}$

$\frac{6.9}{50}$ $\frac{6.8}{33}$ $\frac{9.0}{28}$ $\frac{9.1}{23}$ $\frac{8.1}{22}$ $\frac{5.2}{15}$ $\frac{5.0}{12}$ $\frac{4.9}{10}$ $\frac{4.9}{10}$ $\frac{4.9}{12}$ $\frac{5.6}{15}$ $\frac{7.7}{19}$ $\frac{8.2}{22}$ $\frac{9.3}{23}$ $\frac{9.2}{27}$ $\frac{6.5}{34}$ $\frac{6.8}{50}$

$\frac{7.0}{50}$ $\frac{7.0}{33}$ $\frac{9.2}{27}$ $\frac{9.2}{23}$ $\frac{8.4}{22}$ $\frac{5.4}{15}$ $\frac{5.1}{12}$ $\frac{5.0}{10}$ $\frac{5.0}{10}$ $\frac{5.2}{12}$ $\frac{5.6}{15}$ $\frac{8.4}{22}$ $\frac{9.6}{23}$ $\frac{9.3}{27}$ $\frac{7.2}{33}$ $\frac{7.4}{50}$

$\frac{7.6}{50}$ $\frac{7.6}{33}$ $\frac{9.4}{27}$ $\frac{9.4}{23}$ $\frac{8.5}{22}$ $\frac{6.1}{16}$ $\frac{5.3}{12}$ $\frac{5.1}{10}$ $\frac{5.1}{10}$ $\frac{5.4}{12}$ $\frac{5.9}{15}$ $\frac{8.8}{22}$ $\frac{9.5}{23}$ $\frac{9.5}{26}$ $\frac{7.6}{33}$ $\frac{7.5}{50}$

$\frac{7.9}{50}$ $\frac{7.8}{33}$ $\frac{9.6}{27}$ $\frac{9.4}{23}$ $\frac{5.8}{14}$ $\frac{5.3}{12}$ $\frac{5.1}{10}$ $\frac{5.1}{10}$ $\frac{5.1}{10}$ $\frac{5.1}{12}$ $\frac{5.6}{15}$ $\frac{9.5}{22}$ $\frac{9.2}{27}$ $\frac{6.6}{34}$ $\frac{6.5}{50}$

$\frac{7.9}{50}$ $\frac{7.5}{33}$ $\frac{9.4}{27}$ $\frac{9.8}{24}$ $\frac{9.1}{22}$ $\frac{6.0}{17}$ $\frac{5.4}{12}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.4}{12}$ $\frac{5.9}{14}$ $\frac{9.5}{22}$ $\frac{9.2}{26}$ $\frac{6.6}{33}$ $\frac{7.1}{50}$

$\frac{5.8}{50}$ $\frac{6.7}{35}$ $\frac{9.7}{27}$ $\frac{9.8}{23}$ $\frac{9.0}{22}$ $\frac{5.9}{15}$ $\frac{5.3}{12}$ $\frac{5.2}{10}$ $\frac{5.3}{10}$ $\frac{5.3}{12}$ $\frac{5.9}{14}$ $\frac{9.7}{23}$ $\frac{9.6}{27}$ $\frac{6.8}{34}$ $\frac{6.8}{50}$

$\frac{6.8}{50}$ $\frac{6.7}{34}$ $\frac{9.6}{27}$ $\frac{9.6}{23}$ $\frac{8.6}{22}$ $\frac{5.8}{15}$ $\frac{5.3}{12}$ $\frac{5.3}{10}$ $\frac{5.3}{10}$ $\frac{5.6}{12}$ $\frac{6.2}{15}$ $\frac{9.5}{22}$ $\frac{9.6}{26}$ $\frac{6.7}{34}$ $\frac{6.9}{50}$

HIGH POINT MONT Co. RD. D

$\frac{6.8}{50}$ $\frac{6.5}{34}$ $\frac{9.7}{27}$ $\frac{9.6}{23}$ $\frac{8.6}{21}$ $\frac{6.1}{15}$ $\frac{5.4}{12}$ $\frac{5.3}{10}$ $\frac{5.4}{10}$ $\frac{5.4}{12}$ $\frac{5.9}{17}$ $\frac{8.7}{22}$ $\frac{9.7}{25}$ $\frac{9.2}{27}$ $\frac{6.0}{35}$ $\frac{6.7}{38}$ $\frac{7.1}{50}$

STA	+	π	-	ELEV
		914.45.		
160+18				09.2
+23				09.2
+27				09.3
+41	Q	Co.Rd.	RT	09.2
+46				09.2
+50				09.2
+56				09.2
+68				09.2
+75				09.2
+84				09.1
161				09.1
+50				09.0
T.P.	5.31	914.04.	5.72	908.73.

LT

4

RT

$\frac{6.8}{50} \frac{6.5}{34} \frac{9.7}{27} \frac{9.6}{23} \frac{8.6}{21} \frac{6.1}{15} \frac{5.4}{12} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{5.5}{16} \frac{5.8}{22} \frac{7.3}{34} \frac{7.7}{40} \frac{7.6}{50}$

$\frac{6.7}{50} \frac{7.3}{37} \frac{9.0}{33} \frac{9.2}{29} \frac{9.8}{26} \frac{9.9}{22} \frac{6.3}{16} \frac{5.5}{13} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{5.5}{16} \frac{5.8}{22} \frac{7.3}{34} \frac{7.7}{40} \frac{7.6}{50}$

DITCH

$\frac{9.0}{50} \frac{9.1}{41} \frac{9.2}{29} \frac{9.8}{26} \frac{10.0}{23} \frac{6.1}{15} \frac{5.4}{12} \frac{5.3}{10}$

$5.3 \frac{5.3}{10} \frac{5.5}{15} \frac{5.5}{34} \frac{5.7}{50}$

$\frac{7.3}{50} \frac{7.2}{34} \frac{9.5}{29} \frac{10.0}{26} \frac{10.2}{22} \frac{6.3}{16} \frac{5.4}{13} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{5.4}{34} \frac{5.5}{50}$

$\frac{7.2}{50} \frac{7.0}{34} \frac{9.8}{29} \frac{10.1}{26} \frac{10.4}{22} \frac{6.3}{15} \frac{5.3}{12} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{5.4}{34} \frac{5.5}{50}$

$\frac{8.2}{50} \frac{8.5}{32} \frac{10.0}{27} \frac{10.5}{21} \frac{9.2}{20} \frac{6.5}{18} \frac{5.4}{12} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{5.4}{34} \frac{5.5}{50}$

$\frac{8.2}{50} \frac{8.5}{32} \frac{10.0}{27} \frac{10.5}{21} \frac{9.2}{20} \frac{6.5}{15} \frac{5.4}{12} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{5.6}{20} \frac{5.8}{30} \frac{5.9}{50}$

$\frac{7.5}{50} \frac{7.6}{38} \frac{10.2}{26} \frac{10.3}{21} \frac{6.6}{15} \frac{5.4}{11} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{5.9}{17} \frac{8.9}{28} \frac{10.9}{32} \frac{12.1}{36} \frac{12.0}{50}$

$\frac{7.5}{50} \frac{7.6}{35} \frac{10.2}{26} \frac{10.3}{21} \frac{6.6}{15} \frac{5.4}{11} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{5.8}{16} \frac{11.1}{25} \frac{12.1}{28} \frac{11.9}{37} \frac{11.8}{50}$

$\frac{7.5}{50} \frac{7.6}{35} \frac{10.2}{26} \frac{10.3}{21} \frac{6.6}{15} \frac{5.4}{11} \frac{5.3}{10}$

$5.3 \frac{5.4}{10} \frac{6.3}{13} \frac{10.6}{24} \frac{12.4}{26-29} \frac{10.6}{33} \frac{7.4}{41} \frac{7.7}{50}$

$\frac{7.1}{50} \frac{7.2}{35} \frac{9.7}{28} \frac{10.3}{23} \frac{8.9}{22} \frac{6.4}{16} \frac{5.6}{12} \frac{5.5}{10}$

$5.4 \frac{5.5}{10} \frac{5.5}{12} \frac{10.7}{25} \frac{11.9}{27-31} \frac{10.5}{33} \frac{7.6}{40} \frac{7.7}{50}$

$\frac{7.5}{50} \frac{7.7}{34} \frac{11.1}{27} \frac{11.1}{24} \frac{9.9}{22} \frac{6.7}{16} \frac{5.7}{12} \frac{5.5}{10}$

$5.5 \frac{5.6}{10} \frac{5.7}{13} \frac{6.4}{16} \frac{10.6}{23} \frac{11.1}{25} \frac{12.1}{28-31} \frac{10.5}{33} \frac{8.2}{39} \frac{8.3}{50}$

STA	+	PK	-	ELEV
		914.04.		
161	+59			089
+63		Φ MONOLITHIC CULVERT		089
+75				090
162				089
+50				089
163				089
+50				090
164				090
+38				09.1
+43				09.1
+50		Φ VADNAIS RD		09.1 LT
+62				09.1

LT

Z

RT

$\frac{85}{50}$ $\frac{85}{32}$ $\frac{105}{26}$ $\frac{105}{22}$ $\frac{60}{15}$ $\frac{53}{12}$ $\frac{51}{10}$ $\frac{5.2}{10}$ $\frac{5.4}{12}$ $\frac{6.2}{15}$ $\frac{9.7}{20}$ $\frac{10.5}{25}$ $\frac{11.6}{27}$ $\frac{11.7}{31}$ $\frac{10.7}{32}$ $\frac{8.1}{40}$ $\frac{8.2}{50}$

DITCH

901.79

F. 901.90

$\frac{12.9}{206}$ $\frac{12.8}{150}$ $\frac{12.8}{100}$ $\frac{12.4}{50}$ $\frac{12.0}{25}$ $\frac{12.25}{17}$ $\frac{5.2}{16}$ $\frac{5.2}{12}$ $\frac{5.1}{10}$ $\frac{5.2}{10}$ $\frac{5.3}{13}$ $\frac{5.9}{16}$ $\frac{12.74}{17}$ $\frac{12.1}{25}$ $\frac{11.5}{27}$ $\frac{11.2}{34}$ $\frac{9.5}{38}$ $\frac{8.7}{50}$

$\frac{7.1}{50}$ $\frac{6.6}{32}$ $\frac{11.6}{26}$ $\frac{14.4}{24}$ $\frac{5.7}{23}$ $\frac{5.4}{15}$ $\frac{5.1}{12}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.2}{12}$ $\frac{5.7}{14}$ $\frac{14.2}{22}$ $\frac{8.2}{24}$ $\frac{7.7}{28}$ $\frac{7.7}{30}$ $\frac{7.2}{50}$

$\frac{7.2}{50}$ $\frac{6.4}{30}$ $\frac{8.7}{26}$ $\frac{10.5}{25}$ $\frac{8.6}{23}$ $\frac{5.9}{22}$ $\frac{5.6}{16}$ $\frac{5.3}{14}$ $\frac{5.3}{12}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.3}{12}$ $\frac{5.9}{15}$ $\frac{9.5}{21}$ $\frac{7.6}{23}$ $\frac{6.3}{24}$ $\frac{7.0}{30}$ $\frac{7.2}{37}$ $\frac{7.2}{50}$

$\frac{7.1}{50}$ $\frac{6.5}{28}$ $\frac{10.0}{24}$ $\frac{8.5}{22}$ $\frac{5.9}{21}$ $\frac{5.4}{17}$ $\frac{5.1}{13}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.4}{12}$ $\frac{5.7}{15}$ $\frac{9.3}{21}$ $\frac{7.5}{23}$ $\frac{6.4}{24}$ $\frac{6.2}{27}$ $\frac{7.1}{32}$ $\frac{7.2}{38}$ $\frac{7.2}{50}$

$\frac{6.5}{50}$ $\frac{6.8}{30}$ $\frac{9.6}{25}$ $\frac{8.2}{22}$ $\frac{5.7}{21}$ $\frac{5.3}{14}$ $\frac{5.2}{12}$ $\frac{5.2}{10}$ $\frac{5.2}{10}$ $\frac{5.2}{12}$ $\frac{6.1}{16}$ $\frac{9.4}{20}$ $\frac{6.9}{22}$ $\frac{6.1}{26}$ $\frac{6.3}{28}$ $\frac{6.8}{32}$ $\frac{6.5}{50}$

$\frac{6.5}{50}$ $\frac{6.9}{29}$ $\frac{9.6}{25}$ $\frac{8.5}{23}$ $\frac{5.7}{21}$ $\frac{5.1}{16}$ $\frac{5.1}{12}$ $\frac{5.1}{10}$ $\frac{5.1}{10}$ $\frac{5.0}{12}$ $\frac{5.3}{14}$ $\frac{9.3}{20}$ $\frac{6.7}{22}$ $\frac{5.8}{25}$ $\frac{5.6}{27}$ $\frac{6.8}{32}$ $\frac{6.5}{39}$ $\frac{6.5}{50}$

$\frac{5.6}{50}$ $\frac{5.7}{46}$ $\frac{6.3}{43}$ $\frac{6.8}{28}$ $\frac{9.5}{25}$ $\frac{5.4}{23}$ $\frac{5.1}{16}$ $\frac{5.1}{12}$ $\frac{5.1}{10}$ $\frac{5.1}{10}$ $\frac{5.2}{12}$ $\frac{5.3}{14}$ $\frac{8.5}{19}$ $\frac{6.6}{23}$ $\frac{5.9}{28}$ $\frac{6.0}{33}$ $\frac{6.5}{35}$ $\frac{6.4}{50}$

$\frac{6.9}{50}$ $\frac{7.5}{26}$ $\frac{9.5}{24}$ $\frac{5.3}{22}$ $\frac{5.0}{15}$ $\frac{5.0}{10}$ $\frac{4.9}{12}$ $\frac{5.3}{14}$ $\frac{8.4}{20}$ $\frac{8.8}{24}$ $\frac{8.5}{27}$ $\frac{5.6}{31}$ $\frac{6.0}{33}$ $\frac{6.4}{35}$ $\frac{6.4}{50}$

$\frac{6.0}{50}$ $\frac{5.8}{27}$ $\frac{5.4}{17}$ $\frac{5.0}{10}$ $\frac{4.9}{10}$ $\frac{4.9}{12}$ $\frac{5.9}{15}$ $\frac{8.4}{20}$ $\frac{8.7}{23}$ $\frac{8.5}{26}$ $\frac{6.8}{31}$ $\frac{6.2}{37}$ $\frac{6.4}{50}$

$\frac{5.7}{50}$ $\frac{5.5}{30}$ $\frac{5.0}{15}$ $\frac{4.9}{10}$ $\frac{4.9}{10}$ $\frac{4.9}{12}$ $\frac{5.9}{15}$ $\frac{8.4}{20}$ $\frac{8.7}{23}$ $\frac{8.5}{26}$ $\frac{6.8}{31}$ $\frac{6.2}{37}$ $\frac{6.4}{50}$

$\frac{6.2}{50}$ $\frac{5.9}{33}$ $\frac{5.4}{20}$ $\frac{5.1}{15}$ $\frac{4.9}{10}$ $\frac{4.9}{10}$ $\frac{4.9}{12}$ $\frac{5.9}{15}$ $\frac{8.3}{20}$ $\frac{8.8}{23}$ $\frac{8.4}{26}$ $\frac{6.8}{31}$ $\frac{6.3}{36}$ $\frac{6.4}{50}$

STA	+	π	-	ELEV
		914.04.		
164+68				09.2
+69				09.2
165				09.2
+50				09.3
166				09.4
+50				09.5
T.P.	5.77	914.84.	4.97	909.07.
167				09.5
+50				09.5
168				09.6
+03				09.6
+06		$\angle$ DITCH RT		09.6
+09				09.6

LT

F.

RT

$\frac{6.6}{50}$ $\frac{6.1}{29}$ $\frac{8.1}{25}$ $\frac{8.9}{24-22}$ $\frac{5.4}{17}$ $\frac{5.1}{12}$ $\frac{4.9}{10}$ 4.8 $\frac{5.0}{10}$ $\frac{4.9}{12}$ $\frac{5.6}{14}$ $\frac{8.2}{20}$ $\frac{8.2}{23}$ $\frac{7.7}{26}$ $\frac{6.1}{30}$ $\frac{6.3}{50}$

$\frac{5.9}{50}$ $\frac{6.4}{29}$ $\frac{8.1}{25}$ $\frac{8.9}{24-22}$ $\frac{5.3}{17}$ $\frac{5.1}{12}$ $\frac{4.9}{10}$ 4.8 $\frac{5.0}{10}$ $\frac{4.9}{12}$ $\frac{5.6}{14}$ $\frac{8.2}{20}$ $\frac{8.2}{23}$ $\frac{7.7}{26}$ $\frac{6.1}{30}$ $\frac{6.3}{50}$

$\frac{5.7}{50}$ $\frac{5.4}{31}$ $\frac{7.9}{25}$ $\frac{9.0}{24-22}$ $\frac{7.9}{21}$ $\frac{5.4}{16}$ $\frac{4.9}{12}$ $\frac{4.8}{10}$ 4.8 $\frac{4.9}{10}$ $\frac{4.9}{12}$ $\frac{5.6}{15}$ $\frac{8.6}{21}$ $\frac{8.6}{26}$ $\frac{5.6}{31}$ $\frac{6.2}{50}$

$\frac{5.5}{50}$ $\frac{5.2}{30}$ $\frac{7.6}{25}$ $\frac{8.8}{24-22}$ $\frac{5.3}{16}$ $\frac{4.9}{12}$ $\frac{4.8}{10}$ 4.7 $\frac{4.8}{10}$ $\frac{4.8}{12}$ $\frac{5.6}{15}$ $\frac{7.9}{20}$ $\frac{8.0}{24}$ $\frac{6.5}{28}$ $\frac{5.2}{31}$ $\frac{5.9}{50}$

$\frac{5.1}{50}$ $\frac{5.9}{28}$ $\frac{8.3}{23-21}$ $\frac{5.0}{16}$ $\frac{4.7}{12}$ $\frac{4.6}{10}$ 4.6 $\frac{4.6}{10}$ $\frac{4.7}{12}$ $\frac{5.1}{14}$ $\frac{8.3}{19}$ $\frac{5.1}{24}$ $\frac{5.9}{30}$ $\frac{5.9}{50}$

$\frac{5.0}{50}$ $\frac{6.2}{26}$ $\frac{8.3}{24-22}$ $\frac{5.0}{17}$ $\frac{4.6}{12}$ $\frac{4.5}{10}$ 4.5 $\frac{4.6}{10}$ $\frac{4.6}{12}$ $\frac{5.3}{16}$ $\frac{7.9}{20-24}$ $\frac{5.2}{31}$ $\frac{5.6}{50}$

$\frac{6.0}{50}$ $\frac{6.0}{29}$ $\frac{7.9}{24}$ $\frac{7.3}{23-21}$ $\frac{5.8}{17}$ $\frac{5.4}{14}$ $\frac{5.3}{10}$ 5.3 $\frac{5.4}{10}$ $\frac{5.4}{12}$ $\frac{6.2}{16}$ $\frac{8.6}{21}$ $\frac{8.9}{23}$ $\frac{8.5}{25}$ $\frac{5.9}{29}$ $\frac{5.6}{37}$ $\frac{6.7}{50}$

$\frac{5.0}{50}$ $\frac{6.4}{29}$ $\frac{8.1}{25}$ $\frac{9.1}{24-22}$ $\frac{5.8}{16}$ $\frac{5.3}{12}$ $\frac{5.3}{10}$ 5.3 $\frac{5.4}{10}$ $\frac{5.4}{13}$ $\frac{5.8}{15}$ $\frac{8.4}{21}$ $\frac{8.7}{24}$ $\frac{5.9}{31-34}$ $\frac{6.5}{50}$

$\frac{5.4}{50}$ $\frac{6.2}{27}$ $\frac{8.7}{25-23}$ $\frac{7.7}{22}$ $\frac{5.6}{17}$ $\frac{5.4}{12}$ $\frac{5.3}{10}$ 5.2 $\frac{5.3}{10}$ $\frac{5.2}{13}$ $\frac{5.7}{16}$ $\frac{8.2}{22-24}$ $\frac{5.7}{29}$ $\frac{5.6}{37}$ $\frac{5.9}{50}$

$\frac{5.4}{50}$ $\frac{6.2}{27}$ $\frac{8.7}{25-23}$ $\frac{7.7}{22}$ $\frac{5.6}{17}$ $\frac{5.4}{12}$ $\frac{5.3}{10}$ 5.2 $\frac{5.3}{10}$ $\frac{5.2}{13}$ $\frac{5.7}{16}$ $\frac{8.2}{22-24}$ $\frac{5.7}{29}$ $\frac{5.6}{37}$ $\frac{5.9}{50}$

$\frac{5.4}{50}$ $\frac{6.2}{27}$ $\frac{8.7}{25-23}$ $\frac{7.7}{22}$ $\frac{5.6}{17}$ $\frac{5.4}{12}$ $\frac{5.3}{10}$ 5.2 $\frac{5.3}{10}$ $\frac{5.3}{12}$ $\frac{5.9}{17}$ $\frac{7.6}{22}$ $\frac{8.2}{23}$ $\frac{8.0}{31}$ $\frac{7.9}{50}$ $\frac{8.4}{100}$ $\frac{8.3}{150}$

$\frac{5.4}{50}$ $\frac{6.2}{27}$ $\frac{8.7}{25-23}$ $\frac{7.7}{22}$ $\frac{5.6}{17}$ $\frac{5.4}{12}$ $\frac{5.3}{10}$ 5.2 $\frac{5.3}{10}$ $\frac{5.3}{12}$ $\frac{5.9}{17}$ $\frac{7.6}{22}$ $\frac{8.2}{23}$ $\frac{5.9}{30}$ $\frac{6.3}{50}$

STA	+	π	-	ELEV
		914.84		
168+50				09.6
169				09.7
+50				09.7
170				09.7
+50				09.8
171				09.9
+50				09.9
+78				10.0
+81	$\angle$	DITCH	RT	09.9
+84				09.9
BM	5.66	915.27	5.23	909.61
172				10.1
+50				10.1

LT

4

RT

$\frac{5.0}{50}$ $\frac{6.0}{31}$ $\frac{8.4}{27}$ $\frac{9.0}{26-24}$ $\frac{8.2}{23}$ $\frac{5.6}{16}$ $\frac{5.3}{14}$ $\frac{5.2}{10}$ $\frac{5.2}{51}$ $\frac{5.2}{10}$ $\frac{5.3}{13}$ $\frac{5.9}{16}$ $\frac{8.4}{20}$ $\frac{8.5}{26}$ $\frac{6.4}{29}$ $\frac{5.9}{50}$

$\frac{6.0}{50}$ $\frac{5.6}{30}$ $\frac{8.2}{26-24}$ $\frac{8.1}{23}$ $\frac{7.6}{21}$ $\frac{5.2}{17}$ $\frac{5.2}{14}$ $\frac{5.2}{10}$ $\frac{5.2}{51}$ $\frac{5.2}{10}$ $\frac{5.2}{12}$ $\frac{6.2}{16}$ $\frac{8.4}{21}$ $\frac{8.3}{26}$ $\frac{6.3}{29}$ $\frac{6.0}{50}$

$\frac{6.2}{50}$ $\frac{6.1}{37}$ $\frac{5.3}{32}$ $\frac{8.5}{26-24}$ $\frac{8.1}{23}$ $\frac{7.9}{21}$ $\frac{5.2}{17}$ $\frac{5.2}{13}$ $\frac{5.2}{10}$ $\frac{5.2}{51}$ $\frac{5.2}{10}$ $\frac{5.2}{13}$ $\frac{5.9}{16}$ $\frac{8.5}{20}$ $\frac{8.4}{25}$ $\frac{6.3}{29}$ $\frac{6.3}{50}$

$\frac{7.2}{50}$ $\frac{7.5}{27}$ $\frac{8.0}{22}$ $\frac{5.8}{17}$ $\frac{5.2}{13}$ $\frac{5.1}{10}$ $\frac{5.2}{51}$ $\frac{5.2}{10}$ $\frac{5.2}{12}$ $\frac{5.8}{16}$ $\frac{8.4}{21-25}$ $\frac{6.5}{31}$ $\frac{6.6}{50}$

$\frac{7.3}{50}$ $\frac{7.2}{31}$ $\frac{7.8}{21}$ $\frac{6.0}{17}$ $\frac{5.1}{13}$ $\frac{5.1}{10}$ $\frac{5.1}{50}$ $\frac{5.1}{10}$ $\frac{5.3}{13}$ $\frac{5.8}{16}$ $\frac{8.1}{21-26}$ $\frac{6.8}{29}$ $\frac{7.2}{50}$

$\frac{7.1}{50}$ $\frac{7.5}{29}$ $\frac{7.5}{21}$ $\frac{5.8}{16}$ $\frac{5.0}{12}$ $\frac{5.0}{10}$ $\frac{4.9}{49}$ $\frac{5.0}{10}$ $\frac{5.0}{12}$ $\frac{5.2}{16}$ $\frac{8.0}{21}$ $\frac{8.4}{24-28}$ $\frac{6.4}{32}$ $\frac{6.6}{50}$

$\frac{6.7}{50}$ $\frac{7.0}{30}$ $\frac{8.3}{27-24}$ $\frac{7.8}{21}$ $\frac{5.6}{16}$ $\frac{5.0}{13}$ $\frac{4.9}{10}$ $\frac{4.9}{49}$ $\frac{5.0}{10}$ $\frac{5.3}{13}$ $\frac{5.8}{16}$ $\frac{8.0}{21}$ $\frac{8.0}{25}$ $\frac{6.2}{31}$ $\frac{6.8}{50}$

$\frac{7.0}{50}$ $\frac{7.1}{29}$ $\frac{8.4}{26}$ $\frac{5.6}{23}$ $\frac{5.1}{17}$ $\frac{4.9}{12}$ $\frac{4.9}{10}$ $\frac{4.9}{48}$ $\frac{5.0}{16}$ $\frac{5.1}{12}$ $\frac{5.6}{16}$ $\frac{7.5}{21}$ $\frac{8.1}{25}$ $\frac{6.2}{30}$ $\frac{6.6}{50}$

$\frac{7.0}{58}$ $\frac{7.1}{29}$ $\frac{8.4}{26-23}$ $\frac{5.6}{17}$ $\frac{5.1}{12}$ $\frac{4.9}{10}$ $\frac{4.9}{49}$ $\frac{5.0}{10}$ $\frac{5.1}{12}$ $\frac{5.6}{16}$ $\frac{7.5}{21}$ $\frac{8.1}{25}$ $\frac{7.8}{29}$ $\frac{7.7}{50}$ $\frac{7.7}{100}$ $\frac{7.5}{150}$

$\frac{7.0}{50}$ $\frac{7.1}{29}$ $\frac{8.4}{26-23}$ $\frac{5.6}{17}$ $\frac{5.1}{12}$ $\frac{4.9}{12}$ $\frac{4.9}{49}$ $\frac{5.0}{10}$ $\frac{5.1}{12}$ $\frac{5.6}{16}$ $\frac{7.5}{21}$ $\frac{8.1}{25}$ $\frac{7.8}{29}$ $\frac{6.3}{31}$ $\frac{6.4}{50}$

SPIKE T.P. RT STA 171+53

$\frac{7.2}{50}$ $\frac{7.3}{32}$ $\frac{8.1}{31-30}$ $\frac{8.8}{28}$ $\frac{8.8}{26}$ $\frac{8.4}{23}$ $\frac{5.9}{17}$ $\frac{5.4}{13}$ $\frac{5.3}{10}$ $\frac{5.2}{51}$ $\frac{5.3}{10}$ $\frac{5.3}{12}$ $\frac{6.1}{15}$ $\frac{8.4}{21}$ $\frac{8.9}{24}$ $\frac{8.5}{27}$ $\frac{6.8}{30}$ $\frac{6.4}{35}$ $\frac{7.0}{50}$

$\frac{7.4}{50}$ $\frac{7.4}{32}$ $\frac{9.3}{29-25}$ $\frac{7.5}{22}$ $\frac{6.0}{18}$ $\frac{5.4}{18}$ $\frac{5.2}{10}$ $\frac{5.2}{51}$ $\frac{5.3}{10}$ $\frac{5.3}{12}$ $\frac{6.3}{16}$ $\frac{8.2}{22}$ $\frac{9.3}{24}$ $\frac{9.0}{28}$ $\frac{7.8}{30}$ $\frac{7.1}{35}$ $\frac{7.4}{50}$

STA	+	π	-	ELEV
		915.27.		
173+00				10.1
+50				10.2
174				10.2
+50				10.2
175				10.3
+50				10.2
176				10.2
+50				10.4
177				10.5
+50				10.5
178				10.5
+50				10.6
T.P	6.57	917.10.	4.74	910.53.

LT

K

RT

6.4

$\frac{7.7}{50}$ $\frac{8.9}{30}$ $\frac{9.2}{29}$ $\frac{9.4}{28}$ $\frac{8.6}{26}$ $\frac{5.9}{23}$ $\frac{5.4}{16}$ $\frac{5.2}{10}$ $\frac{5.3}{5}$ $\frac{5.4}{10}$ $\frac{8.1}{12}$ $\frac{7.0}{16}$ $\frac{8.4}{18}$ $\frac{8.7}{21}$ $\frac{8.7}{22}$ $\frac{7.7}{26}$ $\frac{6.8}{27}$ $\frac{7.3}{37}$ $\frac{7.3}{50}$

$\frac{7.4}{50}$ $\frac{7.4}{33}$ $\frac{9.0}{29}$ $\frac{9.3}{26}$ $\frac{8.9}{23}$ $\frac{7.6}{20}$ $\frac{5.7}{16}$ $\frac{5.4}{13}$ $\frac{5.2}{10}$ $\frac{5.2}{5}$ $\frac{5.3}{10}$ $\frac{5.9}{13}$ $\frac{6.8}{15}$ $\frac{7.6}{17}$ $\frac{8.2}{20}$ $\frac{8.7}{22}$ $\frac{8.6}{24}$ $\frac{7.3}{26}$ $\frac{6.8}{29}$ $\frac{7.0}{35}$ $\frac{7.0}{50}$

$\frac{7.2}{50}$ $\frac{7.3}{29}$ $\frac{8.7}{26}$ $\frac{8.7}{24}$ $\frac{8.2}{21}$ $\frac{6.1}{16}$ $\frac{5.3}{13}$ $\frac{5.2}{10}$ $\frac{5.2}{5}$ $\frac{5.2}{10}$ $\frac{5.3}{12}$ $\frac{6.0}{15}$ $\frac{8.1}{20}$ $\frac{8.3}{24}$ $\frac{8.1}{27}$ $\frac{7.5}{29}$ $\frac{7.1}{32}$ $\frac{7.2}{50}$

$\frac{6.8}{50}$ $\frac{7.1}{29}$ $\frac{8.3}{27}$ $\frac{8.6}{25}$ $\frac{8.2}{22}$ $\frac{6.8}{18}$ $\frac{6.1}{16}$ $\frac{5.3}{13}$ $\frac{5.2}{10}$ $\frac{5.2}{5}$ $\frac{5.4}{10}$ $\frac{6.0}{13}$ $\frac{7.9}{16}$ $\frac{8.3}{21}$ $\frac{8.1}{24}$ $\frac{7.1}{27}$ $\frac{7.0}{29}$ $\frac{7.0}{50}$

$\frac{6.3}{50}$ $\frac{6.5}{30}$ $\frac{8.1}{27}$ $\frac{8.3}{25}$ $\frac{8.1}{23}$ $\frac{6.9}{20}$ $\frac{5.7}{17}$ $\frac{5.3}{13}$ $\frac{5.1}{10}$ $\frac{5.2}{5}$ $\frac{5.4}{10}$ $\frac{5.8}{13}$ $\frac{7.7}{15}$ $\frac{8.2}{20}$ $\frac{7.9}{24}$ $\frac{6.9}{27}$ $\frac{6.9}{30}$ $\frac{6.9}{50}$

$\frac{6.6}{50}$ $\frac{6.5}{30}$ $\frac{8.1}{27}$ $\frac{8.0}{24}$ $\frac{7.7}{22}$ $\frac{6.5}{18}$ $\frac{5.3}{13}$ $\frac{5.2}{10}$ $\frac{5.2}{5}$ $\frac{5.2}{10}$ $\frac{5.4}{13}$ $\frac{5.8}{16}$ $\frac{8.0}{20}$ $\frac{8.1}{22}$ $\frac{7.5}{24}$ $\frac{6.6}{28}$ $\frac{6.7}{50}$

$\frac{6.6}{50}$ $\frac{6.8}{30}$ $\frac{8.1}{27}$ $\frac{8.1}{25}$ $\frac{7.6}{22}$ $\frac{5.8}{17}$ $\frac{5.3}{13}$ $\frac{5.2}{10}$ $\frac{5.1}{5}$ $\frac{5.1}{10}$ $\frac{5.1}{12}$ $\frac{8.1}{15}$ $\frac{8.3}{21}$ $\frac{8.2}{23}$ $\frac{8.2}{26}$ $\frac{6.5}{30}$ $\frac{6.7}{50}$

$\frac{6.7}{50}$ $\frac{7.1}{30}$ $\frac{8.1}{26}$ $\frac{8.2}{24}$ $\frac{8.0}{22}$ $\frac{7.0}{20}$ $\frac{5.3}{14}$ $\frac{5.1}{12}$ $\frac{5.0}{10}$ $\frac{4.9}{5}$ $\frac{5.0}{10}$ $\frac{5.5}{13}$ $\frac{7.8}{16}$ $\frac{8.3}{21}$ $\frac{8.3}{24}$ $\frac{6.7}{26}$ $\frac{6.4}{30}$ $\frac{6.6}{50}$

$\frac{6.5}{50}$ $\frac{6.7}{29}$ $\frac{7.8}{26}$ $\frac{8.1}{25}$ $\frac{7.6}{23}$ $\frac{5.3}{16}$ $\frac{4.9}{13}$ $\frac{4.9}{10}$ $\frac{4.9}{5}$ $\frac{4.9}{10}$ $\frac{5.0}{13}$ $\frac{5.6}{16}$ $\frac{7.4}{21}$ $\frac{7.7}{23}$ $\frac{7.4}{26}$ $\frac{6.2}{28}$ $\frac{5.7}{33}$ $\frac{5.9}{40}$ $\frac{6.4}{50}$

$\frac{6.2}{50}$ $\frac{6.2}{30}$ $\frac{7.7}{27}$ $\frac{7.7}{24}$ $\frac{7.8}{22}$ $\frac{5.8}{17}$ $\frac{5.1}{13}$ $\frac{4.9}{10}$ $\frac{4.9}{5}$ $\frac{4.9}{10}$ $\frac{4.9}{13}$ $\frac{5.6}{16}$ $\frac{7.5}{21}$ $\frac{8.0}{24}$ $\frac{7.8}{27}$ $\frac{7.3}{29}$ $\frac{6.4}{32}$ $\frac{6.5}{50}$

$\frac{6.4}{50}$ $\frac{6.8}{33}$ $\frac{7.2}{28}$ $\frac{7.8}{26}$ $\frac{7.9}{23}$ $\frac{7.5}{20}$ $\frac{5.6}{17}$ $\frac{4.9}{13}$ $\frac{4.9}{10}$ $\frac{4.8}{5}$ $\frac{5.0}{10}$ $\frac{5.9}{13}$ $\frac{7.5}{16}$ $\frac{7.8}{20}$ $\frac{7.8}{24}$ $\frac{6.8}{29}$ $\frac{6.8}{50}$

$\frac{6.4}{50}$ $\frac{6.7}{28}$ $\frac{7.4}{26}$ $\frac{7.6}{23}$ $\frac{7.4}{20}$ $\frac{5.8}{17}$ $\frac{5.0}{13}$ $\frac{4.9}{10}$ $\frac{4.7}{5}$ $\frac{4.8}{10}$ $\frac{4.9}{13}$ $\frac{5.4}{17}$ $\frac{7.2}{22}$ $\frac{7.8}{24}$ $\frac{7.8}{26}$ $\frac{6.7}{30}$ $\frac{6.4}{50}$

STA	+	π	-	ELEV	
		917.10			
179+00				10.7	
+50				10.8	
180				10.9	
+50				10.9	
181				11.1	
+50				11.3	
182				11.6	
+42				11.8	
+62				11.9	
183				12.1	
+36				11.9	
B.M	2.62	914.89	4.78	912.32	912.27
+50				11.7	

LT

C

RT

7.9 8.5 9.1 9.1 8.8 7.1 6.7 6.5 6.4 6.5 6.6 7.1 9.0 9.7 9.5 8.6 8.3
50 29 25 23 22 16 13 10 6.4 10 13 16 20 23 26 29 50

7.9 8.0 8.7 8.8 7.2 6.6 6.4 6.3 6.5 7.2 9.4 9.8 9.7 8.2 8.2
50 30 23 21 16 12 10 6.2 10 13 16 21 23 25 30 50

7.8 7.5 8.9 8.8 7.0 6.4 6.3 6.2 6.4 7.1 9.2 9.2 9.1 8.3 8.1
50 29 25 20 17 13 10 6.2 10 12 16 22 24 26 29 50

7.7 7.8 8.5 8.9 8.7 6.8 6.2 6.2 6.2 6.4 6.9 8.9 9.2 8.3 8.1
50 29 27 24 22 16 12 10 6.2 10 12 16 21 24 27 50

7.5 7.6 8.5 8.3 6.7 6.1 6.1 6.0 6.1 6.2 6.9 9.2 9.0 8.0 8.3
50 28 25 21 16 12 10 6.0 10 12 17 22 25 27 50

6.9 7.2 7.8 7.9 6.4 5.8 5.9 5.8 6.1 6.7 8.9 9.0 8.0 8.1
50 29 25 21 16 12 10 5.8 10 13 17 23 25 29 50

5.9 6.2 7.2 7.2 5.9 5.4 5.6 5.7 5.8 7.0 8.2 8.0 7.6 7.9
50 31 26 20 16 12 10 5.5 10 14 17 22 24 27 50

4.2 5.4 6.1 6.2 5.1 5.4 5.3 5.4 5.3 5.8 6.9 7.4 7.4 7.6
50 25 23 18 14 10 5.3 10 14 17 20 23 31 50

FLOOR
GARAGE

3.6 4.3 4.3 4.9 5.0 5.3 5.3 5.3 6.1 7.1 7.1 6.6 6.4 6.7 7.3
28 28 22 17 12 10 5.2 10 14 16 17 20 23 25 28 32 50

4.6 4.6 4.9 5.1 5.0 5.1 5.1 5.7 6.9 6.9 6.1 6.2
50 33 12 10 5.0 10 12 16 19 22 27 50

4.0 4.5 5.4 5.2 5.3 5.3 5.3 5.8 7.0 7.2 6.1 5.4 5.5
50 31 25 18 10 5.2 10 12 16 18 20 24 29 50

SPIKETP RT STA

T.P. #45

3.1 2.6 3.0 4.1 0.6 1.3 2.8 3.8 5.0 3.5 3.2 3.3 3.3 3.3 3.7 5.2 4.5 3.4 3.0
119 111 100 93 73 50 34 23 21 18 15 12 10 3.2 10 13 16 19 28 34 50

WIK 2.0
121 127
1.3
140

CENTERVILLE

STA	+	∇	-	ELEV
		914.89.		
184+00				10.5
+34				09.4
+44				09.0
+65				08.0
+70				07.8
185				06.2
+24				05.1
+50				03.7
B.M	12.67	914.89.	12.67	902.22.
186				01.3
+40				99.3
+71				97.7
187				(96.2)

LT

Z

RT

Z

CENTERVILLE

3.1 3.8 4.2 3.4 0.7 0.9 1.2 2.1 2.9 5.7 4.4 4.4 4.4 4.5 5.0 5.9 3.2 2.5
 107 94 91 75 60 50 40 31 27 22 19 14 10 4 10 13 17 20 38 48-50

Z

CENTERVILLE

5.0 5.9 6.1 6.3 2.2 2.4 6.8 7.2 5.9 5.6 5.6 5.6 5.6 5.6 6.2 7.0 6.2 3.3 1.9 2.0
 81 67 65 57 46 32 23 21 18 15 13 10 5 5 10 14 18 19-22 26 44 50 60

Z

CENTERVILLE

5.4 6.3 6.6 6.8 6.1 7.0 6.6 7.6 6.4 6.1 6.0 6.0 6.0 6.3 7.5 6.6 2.2 1.8 1.9 1.9
 73 60 58 50 46 32 26 22 19 15 13 10 5 9 10 12 16 20 26 46 50 60 75

6.5 7.2 7.5 8.2 8.3 10.0 7.6 7.4 7.0 6.9 6.9 7.1 8.6 8.2 1.5 1.3 1.7
 60 46 39 36 31 27 25 20 17 10 4 9 10 13 16 21-23 24 47 50 75

CENTERVILLE

6.8 7.5 7.8 7.3 7.2 7.2 7.1 7.3 9.0 8.4 1.7 1.3 1.7
 56 39 27 16 10 7 10 13 16 20-23 24 49 60 75

Z

CENTERVILLE

9.0 9.6 8.8 8.8 8.4 8.7 8.9 8.8 8.6 8.8 8.8 8.9 10.6 10.0 1.8 1.6 1.7
 71 62 52 50 39 25 19 14 10 8 10 12 16 20-22 23 48 60 73

CENTERVILLE

8.9 9.6 4.2 11.4 10.5 10.6 10.2 10.0 7.9 9.8 9.9 9.9 9.9 11.7 11.0 1.3 1.5 1.5
 81 67 54 47 42 39 36 26 13 10 9 8 10 12 16 19-22 23 50 68 85

CENTERVILLE + MISSISSIPPI

10.9 11.2 11.8 11.9 12.1 11.0 11.3 11.2 11.3 11.4 7.5 13.1 12.5 8.7 2.2 1.7 1.6
 80 64 46 32 30 27 17 2 11 12 10 13 17 20-22 27 43 68 73 92

DRILL HOLE & MISSISSIPPI STA 185+83

MISSISSIPPI

13.0 13.9 14.1 13.8 13.6 13.6 13.2 4.4 10.6 10.5 1.1 1.1
 72 42 24 17 18 13.6 10 12 33 54 66 97 100

MISSISSIPPI

7.2 6.1 14.9 15.3 16.7 16.3 15.8 15.7 15.7 15.6 15.7 13.9 10.5 10.4 9.5 8.8 8.6
 80 57 47 31 16 13-15 11 10 15 10 13 17 22 44 48-50 56 66 77
 65
 97

9.9 9.9 7.3 15.6 17.0 17.2 18.0 7.4 17.2 17.3 17.3 13.2 15.3 1.7 1.5 0.9 5.6 7.8
 100 80 53 40 25 16 13-15 11 10 17 10 12 14-15 18 40 42 48 62 84

7.4 7.5
 86-90 100

18.7 4.1 2.2 1.6 2.0 3.3
 41 42 59 84 100

STA	+	π	-	ELEV
-----	---	-------	---	------

914.89.

187+50

(93.7)

188

(91.2)

+50

(88.8)

T.P	4.65	908.04	11.50	903.39.
-----	------	--------	-------	---------

187+00

96.2

+50

(93.7)

188

(91.2)

+50

(88.8)

189

(87.0)

+23

03.54 NOT
 & N.P. TRACKS TOP RAILS RY. ANGLES

+23

(86.2)

T.P	2.56	905.95.	4.65	903.39.
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+57

(86.0)

+81

(86.0)

LT

E

RT

$$(21.2) \quad \frac{3.5}{41} \quad \frac{2.4}{67} \quad \frac{1.6}{100}$$

$$(23.7) \quad \frac{10.0}{35} \quad \frac{5.8}{38} \quad \frac{4.4}{45} \quad \frac{3.0}{63} \quad \frac{2.1}{80} \quad \frac{1.7}{100} \quad \frac{1.0}{100}$$

$$(26.1) \quad \frac{8.8}{39} \quad \frac{7.0}{50} \quad \frac{5.5}{75} \quad \frac{4.0}{100}$$

$$\frac{6.2}{100} \quad \frac{4.6}{70} \quad \frac{3.4}{66} \quad \frac{1.4}{47} \quad \frac{11.4}{33} \quad \frac{12.0}{16} \quad \frac{12.6}{15-13} \quad \frac{12.1}{11} \quad \frac{11.9}{10} \quad \frac{11.8}{10} \quad \frac{11.9}{10} \quad \frac{11.8}{12} \quad \frac{12.1}{14-16} \quad \frac{10.8}{18}$$

$$\frac{8.3}{100} \quad \frac{7.4}{84} \quad \frac{6.3}{59} \quad \frac{4.1}{47} \quad \frac{2.1}{46}$$

$$\frac{R.R.}{R.W.} \quad \frac{6.2}{61} \quad \frac{5.8}{55} \quad \frac{5.4}{54} \quad \frac{5.8}{37}$$

$$\frac{R.R.}{R.W.} \quad \frac{10.1}{53} \quad \frac{9.1}{33} \quad \frac{11.7}{32}$$

$$(14.3)$$

$$(14.8)$$

$$(19.2)$$

$$\frac{7.1}{68} \quad \frac{7.7}{46} \quad \frac{9.0}{37} \quad (21.0) \quad \frac{8.3}{33} \quad \frac{2.9}{41} \quad \frac{6.7}{57} \quad \frac{1.7}{68} \quad \frac{1.2}{95}$$

$$\frac{9.5}{500} \quad \frac{8.7}{400} \quad \frac{7.7}{300} \quad \frac{7.1}{200} \quad \frac{5.8}{100} \quad \frac{4.50}{100} \quad \frac{3.5}{100} \quad \frac{2.4}{200} \quad \frac{1.5}{300} \quad \frac{0.6}{400}$$

$$\frac{9.4}{100} \quad \frac{8.1}{64} \quad \frac{7.6}{36} \quad (21.8) \quad \frac{9.6}{36} \quad \frac{7.4}{68} \quad \frac{2.2}{80} \quad \frac{0.8}{100}$$

$$\text{TOP N. RAIL} \quad (20.0) \quad \frac{7.9}{35} \quad \frac{6.2}{36} \quad \frac{5.1}{42} \quad \frac{4.2}{56} \quad \frac{6.7}{65} \quad \frac{6.0}{77} \quad \frac{3.6}{91} \quad \frac{0.0}{100}$$

$$(20.0) \quad \frac{7.5}{40} \quad \frac{3.8}{112} \quad \frac{2.5}{50} \quad \text{TOP N. RAIL} \quad \frac{1.6}{56}$$

STA	+	π	-	ELEV
		905.95		
190				(86.1)
+40				(86.5)
+74				(87.0)
191				(87.4)
T.P.	0.85	895.62	11.18	894.77
187+50				937
188				91.2
+50				888
189				87.0
B.M	6.38	895.18	6.86	888.76
				888.80
+23	CL. CLEARANCE OF OVERHEAD			13.4
				86.2
+51				86.0
+81				86.0
190				86.1

LT

±

RT

T.O.P.
N. RAIL

(199)

9.5	2.0	5.7	3.9	2.5	2.9	1.8	1.3
40	42	49	53	62	67	70	74

(195)

11.5	9.1	7.6	5.6	2.7	2.8	2.8
43	45	60	78	90	95	100

(190)

11.5	9.5	9.1	7.3	7.2	6.6
44	45	57	71	87	100

(186)

11.3	10.6	11.1	11.0	10.0	8.5
45	49	53	62	87	100

1.2	2.0	2.5	2.0	1.9	1.9	1.9	2.2	1.6
32	17	16-14	12	10	10	12	12-15	16

4.0	4.0	4.5	5.1	4.5	4.5	4.5	4.5	5.0	2.7
25	20	16	15-13	11	10	44	10	11	13-15

5.0	6.5	7.3	7.0	6.9	6.8	6.9	2.1	2.1	4.4
27	18	16-15	13	10	10	10	10	16	20

6.5	8.9	8.7	8.2	8.9	8.7	6.7
20	13	13	12	12	17	22

Top No. END CONC. ETR. LANE OF N.P. UNDER PASS

4.7	5.4	8.9	8.7	9.0	9.2	6.7
27	24	17	13	2.0	13	19

3.4	4.2	4.4	6.1	6.5	9.2	9.2	9.6	5.6	5.0
15	50	33	19	26	20	14	12	13	22

4.5	5.1	5.5	7.0	8.8	9.6	9.4	9.4	9.9	6.9	4.0
75	50	36	27	23	19	15	9.2	14	16-20	24

5.0	5.6	6.8	9.1	9.7	9.4	9.1	9.4	9.5	10.0	7.5	3.8	2.7
75	50	29	23	21-18	15	9.1	14	17	18-21	24-26	32	35

STA	+	π	-	ELEV
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895.18

190+40

86.5

87.0

+74 SECTION C.B 18" C.M. CULVERT RT

87.4

191 SECTION C.B. 18" CM LT 24" CM ON WEST

87.6

+15 SECTION C.B 24" C.M LT 24" CONC ON WEST

+40

88.2

+75

88.9

192

89.7

+34

90.7

+70

91.2

193

91.5

+10

91.5

+24 66' X 30" CONC CULVERT LT

91.6

LT

CL

RT

5.0 6.2 6.9 7.9 14.2 8.8 8.7 8.9 2.0 10.2 8.3 8.1 4.1 3.7
75 50 32 27 22 20 17 13 8.7 14 17 20 22 26 30 35 39

FL

3.4 5.4 7.2 10.5 8.4 8.2 8.6 10.5 10.5 8.1 5.5 4.4
88 56 31 25 21 17 14 8.2 14 24 24 28 30 34 38

F.L. 24"
F.L. 18"

VADNAP BLVD

2.9 3.4 3.9 4.6 4.5 6.7 10.8 10.8 8.3 7.9 8.3 8.7 10.2 7.8 8.7
97 86 80 74 76 71 23 26 24 23 15 7.8 15 24 27 29 32 34

VADNAP

3.3 3.8 4.0 6.7 11.2 11.2 7.1 9.5 7.8 8.7 9.6 10.0 4.9 2.4 0.0
86 74 68 50 50 48 30 24 21 15 7.6 22 30 32 34 42 45 80

VADNAP

4.0 4.9 6.8 6.8 7.6 8.5 9.3 9.3 4.1 2.2
63 51 27 17 7.0 7.7 30 39 43 50 80

VADNAP

4.6 4.4 5.7 6.9 8.1 8.5 8.8 6.6 6.2 5.1
61 41 17 6.3 20 38 50 52 54 59 68 80

4.8 4.3 4.5 5.5 6.2 7.7 7.8 7.4 6.6 4.9
55 41 28 5.5 21 48 57 64 83 100

C.L. CENTERVILLE

6.2 4.7 4.3 4.2 4.0 5.5 5.8 6.2 5.8
51 38 26 15 4.5 20 47 67 82 83

11.8 11.6 11.1 5.9 5.2 4.9 4.0 4.0 4.2 3.2
60 50 46 36 31 24 12 4.0 21 30 100

11.2 12.5 12.1 11.3 5.5 4.5 4.0 3.7 4.1 4.3 4.0
60 44 38 35 27 16 10 3.7 12 32 110 50

12.0 11.8 11.2 5.8 4.7 4.3 3.7 3.8 4.1 4.0 4.4
50 43 36 25 21 12 3.7 12 22 28 50

F.L.
14.45 3.6
33

STA	+	π	-	ELEV
		895.18.		91.6
193+31	26' X 30"	CONC	CHWERT	RT
	+70			91.4
194				91.3
	+50			91.4
195				91.6
	+50			92.0
196				92.3
	+50			92.6
197				92.9
T.P.	7.11	899.81.	2.48	892.70.
	+50			93.3
198				94.0
	+25			94.5

LT

Z

RT

FL

$$\frac{11.9}{47} \quad \frac{11.0}{36} \quad \frac{9.9}{32} \quad \frac{6.5}{26} \quad \frac{5.3}{21} \quad \frac{4.8}{14}$$

$$\frac{3.6}{18} \quad \frac{3.9}{18} \quad \frac{8.9}{27} \quad \frac{14.3}{33} \quad \frac{10.8}{36} \quad \frac{11.2}{50}$$

$$\frac{11.4}{50} \quad \frac{10.1}{30} \quad \frac{4.5}{19} \quad \frac{4.2}{13} \quad \frac{3.8}{9} \quad \frac{4.9}{12} \quad \frac{4.3}{17} \quad \frac{4.6}{25} \quad \frac{8.4}{31} \quad \frac{12.1}{35} \quad \frac{11.6}{37} \quad \frac{10.9}{50} \quad \frac{10.7}{50}$$

$$\frac{11.1}{50} \quad \frac{10.6}{39} \quad \frac{10.0}{29} \quad \frac{4.5}{18} \quad \frac{4.2}{9} \quad \frac{4.8}{9} \quad \frac{4.4}{11} \quad \frac{4.1}{18} \quad \frac{9.1}{27} \quad \frac{11.6}{33} \quad \frac{10.9}{43} \quad \frac{11.5}{45} \quad \frac{11.0}{48} \quad \frac{10.7}{50}$$

$$\frac{11.5}{50} \quad \frac{10.1}{30} \quad \frac{4.8}{20} \quad \frac{4.2}{14} \quad \frac{4.3}{12} \quad \frac{3.8}{9} \quad \frac{4.1}{9} \quad \frac{4.2}{13} \quad \frac{4.0}{18} \quad \frac{7.1}{26} \quad \frac{11.4}{33} \quad \frac{10.8}{35} \quad \frac{10.7}{50}$$

$$\frac{12.0}{50} \quad \frac{10.5}{31} \quad \frac{4.3}{19} \quad \frac{4.0}{13} \quad \frac{3.6}{12} \quad \frac{4.2}{11} \quad \frac{4.3}{18} \quad \frac{9.1}{29} \quad \frac{11.8}{33} \quad \frac{11.9}{36} \quad \frac{12.1}{50}$$

$$\frac{11.1}{50} \quad \frac{11.4}{34} \quad \frac{3.8}{17} \quad \frac{3.6}{12} \quad \frac{3.5}{9} \quad \frac{3.2}{11} \quad \frac{3.7}{17} \quad \frac{4.0}{20} \quad \frac{4.7}{32} \quad \frac{11.6}{36} \quad \frac{12.4}{50} \quad \frac{12.5}{50}$$

$$\frac{10.8}{50} \quad \frac{10.4}{30} \quad \frac{3.9}{18} \quad \frac{3.4}{16} \quad \frac{3.2}{10} \quad \frac{3.2}{11} \quad \frac{3.7}{20} \quad \frac{9.9}{32} \quad \frac{10.9}{35} \quad \frac{11.3}{50}$$

$$\frac{10.2}{50-38} \quad \frac{10.3}{36} \quad \frac{9.1}{29} \quad \frac{4.0}{19} \quad \frac{3.0}{14} \quad \frac{2.8}{10} \quad \frac{3.0}{21} \quad \frac{3.6}{20} \quad \frac{3.8}{24} \quad \frac{9.3}{33} \quad \frac{10.6}{37} \quad \frac{10.5}{50}$$

$$\frac{11.5}{50} \quad \frac{8.9}{31} \quad \frac{2.8}{18} \quad \frac{2.6}{12} \quad \frac{2.3}{23} \quad \frac{2.8}{11} \quad \frac{3.0}{15} \quad \frac{3.8}{19} \quad \frac{9.1}{31} \quad \frac{9.2}{40} \quad \frac{9.6}{42} \quad \frac{9.7}{50}$$

$$\frac{15.5}{50} \quad \frac{14.5}{33} \quad \frac{10.4}{25} \quad \frac{7.5}{18} \quad \frac{7.0}{14} \quad \frac{6.9}{9} \quad \frac{6.5}{11} \quad \frac{7.0}{15} \quad \frac{7.2}{20} \quad \frac{8.6}{28} \quad \frac{12.4}{33} \quad \frac{13.5}{37} \quad \frac{13.6}{50}$$

$$\frac{13.3}{50} \quad \frac{12.7}{33} \quad \frac{6.1}{19} \quad \frac{6.1}{11} \quad \frac{5.8}{10} \quad \frac{6.1}{15} \quad \frac{6.4}{24} \quad \frac{9.3}{31} \quad \frac{10.1}{50} \quad \frac{9.6}{50}$$

$$\frac{12.7}{50} \quad \frac{11.7}{43} \quad \frac{10.3}{29} \quad \frac{6.1}{18} \quad \frac{5.6}{10} \quad \frac{5.3}{10} \quad \frac{5.6}{17} \quad \frac{6.0}{21} \quad \frac{7.3}{26} \quad \frac{7.7}{33} \quad \frac{7.6}{38} \quad \frac{7.5}{50}$$

STA	+	π	-	ELEV
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899.81

198+50

949

+75

954

199

959

+50

972

T.P

984

+85

WATER WORKS SERVICE DRIVE LT

200+00

988

T.P

13.78

912.11

1.48

898.33

+50

00.5

201

02.0

+50

03.5

202

05.4

+50

07.5

203

09.7

T.P

13.64

925.11

0.64

911.47

LT

♀

RT

$$\frac{9.5}{50} \frac{8.3}{35} \frac{7.9}{27} \frac{7.3}{22} \frac{5.8}{18} \frac{5.4}{11}$$

$$49 \frac{5.2}{10} \frac{5.5}{16} \frac{6.4}{18} \frac{6.3}{25} \frac{5.8}{26} \frac{5.2}{31} \frac{5.7}{50}$$

$$\frac{6.4}{50} \frac{5.8}{45} \frac{5.5}{38} \frac{5.7}{29} \frac{6.3}{27} \frac{6.1}{21} \frac{5.0}{18} \frac{4.7}{10} \frac{4.4}{44}$$

$$\frac{4.5}{9} \frac{4.8}{15} \frac{5.9}{18-24} \frac{4.0}{27} \frac{4.4}{33} \frac{4.6}{50}$$

$$\frac{4.4}{50} \frac{3.7}{42} \frac{3.4}{34} \frac{3.7}{28} \frac{5.6}{26-23} \frac{4.3}{19} \frac{4.2}{11} \frac{3.9}{39}$$

$$\frac{4.1}{10} \frac{4.3}{15} \frac{5.0}{18} \frac{5.4}{24} \frac{4.7}{27} \frac{4.0}{34} \frac{3.7}{50}$$

$$\frac{1.8}{50} \frac{1.5}{36} \frac{1.9}{30} \frac{3.7}{26-22} \frac{2.7}{20} \frac{2.9}{14} \frac{2.8}{10} \frac{2.6}{26}$$

$$2 \frac{2.8}{10} \frac{3.2}{16} \frac{4.5}{18-24} \frac{3.3}{33} \frac{3.2}{50}$$

$$\frac{0.5}{50} \frac{0.5}{33} \frac{1.5}{13} \frac{1.4}{14} \frac{1.7}{10} \frac{1.9}{15} \frac{3.2}{19-24} \frac{1.9}{27} \frac{1.8}{50}$$

$$\frac{0.5}{50} \frac{0.6}{33} \frac{2.3}{31-20} \frac{1.0}{15} \frac{1.0}{10} \frac{1.0}{10}$$

$$\frac{1.2}{10} \frac{1.4}{15} \frac{2.8}{18} \frac{2.8}{24} \frac{1.5}{27} \frac{0.5}{33} \frac{1.2}{50}$$

$$\frac{11.3}{50} \frac{11.9}{36} \frac{13.6}{30} \frac{13.5}{19} \frac{12.4}{16} \frac{11.9}{12} \frac{11.6}{11.6}$$

$$\frac{11.9}{10} \frac{12.1}{15} \frac{14.0}{19-24} \frac{12.1}{26} \frac{12.0}{50}$$

$$\frac{10.1}{50} \frac{10.2}{37} \frac{11.8}{31} \frac{11.6}{19} \frac{10.8}{17} \frac{10.5}{12} \frac{10.1}{10.1}$$

$$\frac{10.4}{12} \frac{10.6}{16} \frac{11.7}{18} \frac{11.6}{25} \frac{10.3}{27} \frac{11.1}{50}$$

$$\frac{9.2}{50} \frac{9.0}{37} \frac{9.9}{30} \frac{9.2}{18} \frac{9.1}{16} \frac{8.7}{12} \frac{8.6}{8.6}$$

$$\frac{8.9}{10} \frac{9.2}{16} \frac{10.4}{18} \frac{10.3}{24} \frac{10.0}{27} \frac{10.7}{50}$$

$$\frac{7.3}{50} \frac{7.1}{32} \frac{8.1}{30} \frac{7.7}{23} \frac{7.9}{18} \frac{7.2}{16} \frac{6.8}{12} \frac{6.7}{6.7}$$

$$\frac{7.0}{11} \frac{7.2}{16} \frac{8.4}{19} \frac{8.2}{24} \frac{7.3}{50}$$

$$\frac{5.0}{50} \frac{4.7}{33} \frac{5.4}{30} \frac{5.7}{25} \frac{5.7}{17} \frac{5.1}{16} \frac{4.8}{11} \frac{4.6}{4.6}$$

$$\frac{5.1}{10} \frac{5.6}{17} \frac{5.9}{18} \frac{5.9}{27} \frac{6.8}{32} \frac{7.7}{50}$$

$$\frac{2.0}{50} \frac{2.3}{27} \frac{3.8}{24} \frac{3.8}{17} \frac{3.1}{15} \frac{2.7}{11} \frac{2.4}{2.4}$$

$$\frac{2.8}{11} \frac{3.0}{15} \frac{3.9}{18} \frac{3.8}{27} \frac{5.1}{50}$$

STA	+	π	-	ELEV	
		925.11.			
203+58				12.0	
204				13.9	
+50				15.9	
+66				16.4	
205				17.6	
+50				19.3	
206				21.0	
T.P.	9.59	933.93.	0.77	924.34.	
+50				22.6	
207				24.3	
+50				25.9	
208				27.3	
B.M	6.36	933.85.	6.36	927.57.	927.49.
+50					

LT

E

RT

$\frac{11.4}{50}$
 $\frac{12.2}{30}$
 $\frac{15.0}{24}$
 $\frac{14.8}{19}$
 $\frac{13.8}{14}$
 $\frac{13.4}{9}$
 $\frac{13.1}{13.1}$
 $\frac{13.4}{9}$
 $\frac{13.9}{15}$
 $\frac{15.0}{18}$
 $\frac{15.0}{25}$
 $\frac{14.2}{27}$
 $\frac{15.4}{50}$

$\frac{7.9}{50}$
 $\frac{8.7}{35}$
 $\frac{8.6}{34}$
 $\frac{12.9}{25}$
 $\frac{13.2}{18}$
 $\frac{11.8}{14}$
 $\frac{11.3}{10}$
 11.2
 $\frac{11.5}{10}$
 $\frac{11.9}{15}$
 $\frac{12.8}{19}$
 $\frac{12.8}{24}$
 $\frac{10.7}{30}$
 $\frac{11.9}{50}$

$\frac{4.7}{50}$
 $\frac{5.0}{38}$
 $\frac{6.5}{34}$
 $\frac{9.5}{29}$
 $\frac{11.0}{24}$
 $\frac{11.1}{20}$
 $\frac{10.0}{15}$
 $\frac{9.5}{10}$
 $\frac{9.7}{9.2}$
 $\frac{8.9}{10}$
 $\frac{8.9}{13}$
 $\frac{10.6}{19}$
 $\frac{11.2}{20}$
 $\frac{10.6}{23}$
 $\frac{9.8}{24}$
 $\frac{7.5}{28}$
 $\frac{8.1}{33}$
 $\frac{8.1}{50}$

$\frac{3.5}{50}$
 $\frac{3.9}{38}$
 $\frac{6.2}{34}$
 $\frac{9.0}{29}$
 $\frac{10.5}{25}$
 $\frac{10.1}{21}$
 $\frac{8.3}{16}$
 $\frac{9.0}{12}$
 $\frac{8.9}{8.7}$
 $\frac{9.3}{10}$
 $\frac{10.3}{15}$
 $\frac{10.3}{17}$
 $\frac{10.3}{24}$
 $\frac{9.2}{29}$
 $\frac{5.5}{34}$
 $\frac{5.5}{50}$

$\frac{2.0}{50}$
 $\frac{2.0}{39}$
 $\frac{4.8}{34}$
 $\frac{7.8}{27}$
 $\frac{9.1}{22}$
 $\frac{9.2}{19}$
 $\frac{8.2}{16}$
 $\frac{7.7}{11}$
 $\frac{7.5}{7.5}$
 $\frac{7.7}{10}$
 $\frac{8.0}{13}$
 $\frac{9.0}{17}$
 $\frac{9.0}{22}$
 $\frac{7.8}{28}$
 $\frac{6.3}{32}$
 $\frac{4.3}{33}$
 $\frac{5.0}{50}$

$\frac{1.2}{50}$
 $\frac{1.2}{38}$
 $\frac{3.1}{34}$
 $\frac{5.0}{30}$
 $\frac{7.5}{23}$
 $\frac{7.5}{20}$
 $\frac{6.5}{16}$
 $\frac{6.0}{10}$
 $\frac{6.1}{5.8}$
 $\frac{6.7}{10}$
 $\frac{7.4}{16}$
 $\frac{7.1}{21-23}$
 $\frac{6.0}{24}$
 $\frac{3.5}{29}$
 $\frac{1.9}{33}$
 $\frac{2.4}{34}$
 $\frac{2.4}{50}$

$\frac{0.9}{50}$
 $\frac{0.7}{40}$
 $\frac{0.8}{34}$
 $\frac{3.1}{30}$
 $\frac{5.5}{25}$
 $\frac{6.0}{23}$
 $\frac{4.9}{20}$
 $\frac{4.4}{15}$
 $\frac{4.1}{10}$
 $\frac{4.4}{10}$
 $\frac{4.7}{14}$
 $\frac{5.5}{21}$
 $\frac{5.9}{22}$
 $\frac{5.5}{26}$
 $\frac{3.2}{32}$
 $\frac{1.3}{33}$
 $\frac{1.7}{50}$

$\frac{8.8}{50}$
 $\frac{8.9}{33}$
 $\frac{12.3}{27}$
 $\frac{13.3}{23}$
 $\frac{11.8}{19}$
 $\frac{11.5}{15}$
 $\frac{11.3}{11}$
 $\frac{11.5}{11.3}$
 $\frac{12.0}{10}$
 $\frac{12.8}{15}$
 $\frac{12.9}{18}$
 $\frac{10.4}{24}$
 $\frac{9.4}{30}$
 $\frac{9.7}{32}$
 $\frac{9.7}{50}$

$\frac{6.5}{50}$
 $\frac{7.4}{33}$
 $\frac{8.4}{32}$
 $\frac{9.7}{29}$
 $\frac{10.5}{24}$
 $\frac{10.5}{19}$
 $\frac{9.7}{15}$
 $\frac{9.8}{10}$
 $\frac{9.6}{9.6}$
 $\frac{10.1}{11}$
 $\frac{10.2}{15}$
 $\frac{11.8}{20-23}$
 $\frac{9.7}{29}$
 $\frac{8.8}{30}$
 $\frac{9.0}{50}$

Floor
 HOUSE
 215
 63

$\frac{5.0}{63}$
 $\frac{5.2}{50}$
 $\frac{5.9}{33}$
 $\frac{7.6}{32}$
 $\frac{9.5}{25}$
 $\frac{9.8}{19}$
 $\frac{9.2}{16}$
 $\frac{8.6}{14}$
 $\frac{8.2}{10}$
 $\frac{8.4}{8.0}$
 $\frac{8.7}{11}$
 $\frac{10.2}{14}$
 $\frac{8.9}{20-24}$
 $\frac{7.6}{29}$
 $\frac{7.9}{31}$
 $\frac{7.9}{50}$

$\frac{3.3}{50}$
 $\frac{3.5}{35}$
 $\frac{7.2}{28}$
 $\frac{8.1}{23}$
 $\frac{7.1}{19}$
 $\frac{6.8}{14}$
 $\frac{6.6}{11}$
 $\frac{7.0}{11}$
 $\frac{7.3}{14}$
 $\frac{8.5}{20}$
 $\frac{7.4}{24}$
 $\frac{5.8}{28}$
 $\frac{5.1}{31}$
 $\frac{6.3}{50}$

P.P. RT STA 208+32

$\frac{4.7}{50}$
 $\frac{4.1}{40}$
 $\frac{2.7}{35}$
 $\frac{6.4}{33}$
 $\frac{7.0}{27}$
 $\frac{6.3}{22}$
 $\frac{5.7}{19}$
 $\frac{5.5}{15}$
 $\frac{5.8}{11}$
 $\frac{6.1}{11}$
 $\frac{7.2}{14}$
 $\frac{6.3}{21-25}$
 $\frac{4.6}{27}$
 $\frac{5.1}{31}$
 $\frac{5.1}{50}$

STA	+	π	-	ELEV
		933.85		
209+00				28.8
+50				28.9
210				28.9
+50				28.6
211				28.1
+50				27.6
212				
T.P.	0.93	929.86	4.92	928.93
+50				
213				
+05				
+22				
+50				

See Line Revision

LT

±

RT

$\frac{4.8}{50} \frac{4.6}{43} \frac{4.0}{39} \frac{3.3}{33} \frac{4.4}{30} \frac{6.8}{25} \frac{5.2}{21} \frac{5.4}{15} \frac{5.4}{11} \frac{5.4}{11} \frac{5.7}{16} \frac{6.5}{18} \frac{6.6}{23} \frac{6.1}{28} \frac{4.2}{31} \frac{4.9}{50}$

$\frac{4.8}{50} \frac{4.2}{39} \frac{3.5}{35} \frac{3.3}{32} \frac{6.3}{25} \frac{6.9}{23} \frac{6.4}{20} \frac{5.7}{18} \frac{5.3}{15} \frac{5.3}{11} \frac{5.3}{11} \frac{5.3}{11} \frac{5.7}{17} \frac{6.4}{18} \frac{6.8}{23} \frac{6.2}{26} \frac{4.5}{30} \frac{4.1}{37} \frac{4.8}{50}$

$\frac{4.7}{50} \frac{4.5}{42} \frac{2.7}{35} \frac{2.7}{32} \frac{4.4}{28} \frac{6.4}{25} \frac{6.9}{23} \frac{6.9}{20} \frac{6.5}{17} \frac{5.8}{14} \frac{5.8}{12} \frac{5.8}{11} \frac{5.8}{11} \frac{5.8}{16} \frac{6.7}{19} \frac{7.0}{21} \frac{6.2}{27} \frac{4.6}{29} \frac{4.2}{37} \frac{5.0}{44} \frac{5.2}{50}$

$\frac{4.8}{50} \frac{4.7}{42} \frac{3.3}{35} \frac{6.5}{32} \frac{6.7}{25} \frac{6.0}{22} \frac{5.6}{18} \frac{5.6}{15} \frac{5.6}{12} \frac{5.6}{11} \frac{5.6}{11} \frac{5.6}{11} \frac{5.6}{16} \frac{5.9}{18} \frac{6.8}{21} \frac{7.1}{23} \frac{6.4}{27} \frac{4.5}{29} \frac{4.2}{37} \frac{5.1}{43} \frac{4.8}{50}$

$\frac{5.5}{50} \frac{5.1}{40} \frac{4.3}{35} \frac{5.2}{28} \frac{7.1}{25} \frac{7.4}{23} \frac{6.4}{20} \frac{6.1}{18} \frac{6.1}{15} \frac{6.1}{11} \frac{6.1}{11} \frac{6.1}{11} \frac{6.1}{16} \frac{6.5}{18} \frac{7.3}{21} \frac{7.6}{23} \frac{7.0}{26} \frac{5.3}{28} \frac{5.3}{50}$

$\frac{6.6}{50} \frac{6.2}{41} \frac{4.9}{36} \frac{5.2}{29} \frac{7.8}{25} \frac{8.1}{23} \frac{7.8}{20} \frac{6.6}{18} \frac{6.6}{16} \frac{6.6}{14} \frac{6.6}{12} \frac{6.6}{11} \frac{6.6}{11} \frac{6.6}{16} \frac{7.0}{18} \frac{8.0}{21} \frac{8.3}{23} \frac{7.5}{26} \frac{6.0}{28} \frac{5.6}{37} \frac{6.5}{44} \frac{5.8}{50}$

$\frac{4.3}{50} \frac{7.1}{42} \frac{6.1}{36} \frac{5.9}{28} \frac{8.6}{24} \frac{8.7}{18} \frac{7.8}{15} \frac{7.2}{11} \frac{7.2}{11} \frac{7.2}{11} \frac{7.2}{11} \frac{7.2}{11} \frac{7.2}{11} \frac{7.2}{16} \frac{7.2}{18} \frac{8.2}{21} \frac{7.0}{23} \frac{8.1}{26} \frac{6.7}{28} \frac{6.1}{37} \frac{6.4}{44} \frac{6.9}{50}$

$\frac{3.8}{50} \frac{2.7}{42} \frac{2.8}{37} \frac{5.3}{28} \frac{5.7}{24} \frac{5.3}{21} \frac{5.3}{18} \frac{4.2}{16} \frac{3.9}{11} \frac{3.9}{11} \frac{3.9}{11} \frac{3.9}{11} \frac{3.9}{16} \frac{4.4}{18} \frac{5.4}{21} \frac{5.6}{23} \frac{5.0}{26} \frac{3.2}{28} \frac{3.1}{50}$

$\frac{4.2}{50} \frac{3.6}{29} \frac{5.8}{25} \frac{6.1}{23} \frac{5.1}{18} \frac{4.7}{16} \frac{4.7}{11} \frac{4.7}{11} \frac{4.7}{11} \frac{4.7}{11} \frac{4.7}{16} \frac{4.6}{18} \frac{5.2}{21} \frac{6.0}{23} \frac{6.3}{26} \frac{5.9}{28} \frac{3.3}{30} \frac{3.6}{50}$

$\frac{4.1}{50} \frac{2.7}{29} \frac{5.8}{25} \frac{6.1}{23} \frac{5.1}{18} \frac{4.8}{16} \frac{4.8}{11} \frac{4.8}{11} \frac{4.8}{11} \frac{4.8}{11} \frac{4.8}{16} \frac{4.6}{18} \frac{5.2}{21} \frac{6.0}{23} \frac{6.4}{26} \frac{5.9}{28} \frac{3.3}{30} \frac{3.6}{50}$

$\frac{7.3}{50} \frac{6.2}{29} \frac{6.8}{25} \frac{6.5}{23} \frac{5.7}{18} \frac{5.7}{16} \frac{5.7}{11} \frac{5.7}{11} \frac{5.7}{11} \frac{5.7}{11} \frac{5.7}{16} \frac{5.0}{18} \frac{5.6}{21} \frac{6.4}{23} \frac{6.6}{26} \frac{6.1}{28} \frac{3.9}{30} \frac{3.9}{50}$

$\frac{8.1}{50} \frac{7.1}{32} \frac{6.1}{26} \frac{7.6}{24} \frac{7.3}{22} \frac{6.1}{19} \frac{5.5}{17} \frac{5.5}{10} \frac{5.5}{10} \frac{5.5}{10} \frac{5.5}{10} \frac{5.5}{16} \frac{5.9}{18} \frac{6.8}{21} \frac{7.1}{23} \frac{6.5}{26} \frac{4.9}{29} \frac{5.0}{50}$

STA	+	π	-	ELEV
		929.86		

214+00

+50

215

+50

216

T.P	0.98	920.69	10.15	919.71
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+50

217

+50

218

+50

B.M.

	7.62	913.63	913.07	913.04
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LINE REVISION

EDGERTON

FROM STA 212+02.95 TO KOEHLER RD

STA	+	π	-	ELEV
B.M.	4.86	932.35		927.49

212 + 02.95

+50

213

+05

+22

+50

214

T.P	1.81	925.02	9.14	923.21
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+14.62

+50

215

+50

216

LT

#

RT

SPIKE IN P. POLE RT STA 208

<u>5.9</u>	<u>4.6</u>	<u>4.5</u>	<u>7.1</u>	<u>7.5</u>	<u>7.3</u>	<u>5.8</u>		<u>5.1</u>	<u>6.2</u>	<u>7.3</u>	<u>7.8</u>	<u>5.2</u>	<u>5.2</u>	<u>5.3</u>
50	36	29	25	22-18	16	11	5.4	10	16	19-22	26	28	39	50

<u>6.5</u>	<u>5.1</u>	<u>5.3</u>	<u>7.8</u>	<u>8.2</u>	<u>7.8</u>	<u>6.7</u>	<u>6.5</u>		<u>6.4</u>	<u>6.9</u>	<u>7.9</u>	<u>8.0</u>	<u>7.4</u>	<u>5.7</u>	<u>5.6</u>	<u>5.9</u>
50	37	29	25	21	18	16	13	6.1	11	16	19	22	26	28	36	50

<u>6.5</u>	<u>6.2</u>	<u>8.6</u>	<u>8.9</u>	<u>8.7</u>	<u>7.7</u>	<u>7.4</u>		<u>7.2</u>	<u>7.6</u>	<u>8.4</u>	<u>8.8</u>	<u>8.4</u>	<u>5.8</u>	<u>6.0</u>	<u>6.1</u>
50	30	25	23	19	16	12	6.9	10	16	18	21	24	29	38	50

<u>6.3</u>	<u>6.4</u>	<u>8.4</u>	<u>8.9</u>	<u>8.7</u>	<u>7.8</u>	<u>7.3</u>		<u>7.3</u>	<u>7.6</u>	<u>8.4</u>	<u>8.8</u>	<u>8.4</u>	<u>5.7</u>	<u>6.1</u>	<u>6.1</u>
50	30	26	24	20	17	12	7.0	10	16	18	21	24	29	38	50

<u>9.7</u>	<u>8.6</u>	<u>9.2</u>	<u>9.5</u>	<u>8.4</u>	<u>7.7</u>		<u>7.6</u>	<u>8.1</u>	<u>8.8</u>	<u>9.1</u>	<u>8.7</u>	<u>6.5</u>	<u>6.6</u>	<u>6.7</u>
50	28	25	21	18	11	7.2	10	16	18	21	24	28	40	50

<u>10.2</u>	<u>9.8</u>	<u>9.1</u>	<u>9.9</u>	<u>10.0</u>	<u>9.7</u>	<u>8.1</u>		<u>8.0</u>	<u>8.4</u>	<u>9.3</u>	<u>9.6</u>	<u>9.1</u>	<u>7.5</u>	<u>7.4</u>	<u>7.4</u>
50	36	28	25	23	20	18/14	7.7	10	15	18	20	24	27	36	50

<u>9.7</u>	<u>9.1</u>	<u>10.4</u>	<u>10.5</u>	<u>9.1</u>	<u>8.6</u>		<u>8.7</u>	<u>9.2</u>	<u>10.2</u>	<u>10.5</u>	<u>10.2</u>	<u>8.9</u>	<u>8.8</u>	<u>8.8</u>
50	30	26	22	19	13	8.4	7	10	16	18	22	24	34	50

<u>2.6</u>	<u>1.8</u>	<u>3.3</u>	<u>3.3</u>	<u>3.0</u>	<u>1.9</u>	<u>1.4</u>		<u>1.6</u>	<u>1.8</u>	<u>2.9</u>	<u>3.1</u>	<u>3.0</u>	<u>2.0</u>	<u>1.7</u>
50	34-31	27	24	22	19	14	1.2	7	12	15	18	20	23	50

<u>2.8</u>	<u>2.1</u>	<u>3.4</u>	<u>3.7</u>	<u>3.5</u>	<u>2.4</u>	<u>1.8</u>		<u>2.0</u>	<u>2.4</u>	<u>3.5</u>	<u>3.8</u>	<u>3.6</u>	<u>2.4</u>	<u>2.4</u>
50-44	35-33	30	27	24	22	15	1.7	6	12	14	17	19	22	50

<u>3.0</u>	<u>3.0</u>	<u>2.5</u>	<u>4.2</u>	<u>4.7</u>	<u>4.4</u>	<u>3.1</u>	<u>2.7</u>	<u>2.6</u>		<u>2.8</u>	<u>3.3</u>	<u>4.5</u>	<u>4.8</u>	<u>4.5</u>	<u>3.3</u>	<u>3.8</u>
50	39	35	31	28	26	25	18	9	2.7	4	10	12	15	18	22-30	50

<u>3.9</u>	<u>3.5</u>	<u>5.6</u>	<u>5.8</u>	<u>5.4</u>	<u>4.3</u>	<u>3.7</u>	<u>3.4</u>		<u>3.9</u>	<u>4.3</u>	<u>5.4</u>	<u>5.3</u>	<u>4.2</u>	<u>4.3</u>	<u>4.8</u>	<u>5.6</u>
50	37	32	29	27	24	18	9	3.8	3	9	12	17	21	25	34	50

<u>5.0</u>	<u>4.7</u>	<u>7.3</u>	<u>6.8</u>	<u>6.4</u>	<u>5.3</u>	<u>5.0</u>	<u>4.6</u>		<u>5.4</u>	<u>6.1</u>	<u>6.3</u>	<u>6.0</u>	<u>6.3</u>	<u>7.7</u>
50-41	37	34	31	28	25	22	10	5.0	6	11	16	18	23	50

STA	+	π	-	ELEV
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		925.02		
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216+50				
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217				
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+50				
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T.P.	3.23	919.12	9.13	915.89
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218				
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+50				
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219				
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+50				
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220				
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+50				
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B.M	4.22	917.26	6.04	913.08	913.04
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221					
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+50					
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222					
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LT

2

RT

$\frac{7.0}{50} \frac{6.6}{45} \frac{6.0}{40} \frac{7.9}{36} \frac{8.5}{33} \frac{7.9}{32} \frac{6.5}{27} \frac{6.2}{24} \frac{5.9}{13} \underline{6.3}$

$\frac{6.6}{5} \frac{7.9}{8} \frac{8.8}{21} \frac{9.7}{32} \frac{10.4}{50}$

$\frac{8.4}{50} \frac{7.2}{41} \frac{8.8}{37} \frac{9.4}{35} \frac{8.9}{32} \frac{7.8}{29} \frac{7.5}{25} \frac{7.1}{13} \frac{7.5}{3} \underline{7.7}$

$\frac{8.0}{5} \frac{7.6}{11} \frac{10.3}{19} \frac{11.5}{27} \frac{12.1}{50}$

$\frac{9.6}{50} \frac{8.9}{44} \frac{10.0}{40} \frac{10.0}{35} \frac{9.1}{32} \frac{8.5}{26} \frac{8.2}{16} \frac{8.6}{5} \underline{9.0}$

$\frac{9.3}{3} \frac{12.7}{14} \frac{12.8}{20} \frac{13.2}{25} \frac{13.5}{50}$

$\frac{4.7}{50} \frac{4.1}{46} \frac{4.1}{42} \frac{5.0}{39} \frac{4.9}{37} \frac{4.8}{34} \frac{4.0}{32} \frac{3.5}{21} \frac{3.3}{16} \frac{3.7}{6} \underline{4.3}$

$\frac{4.4}{1} \frac{7.3}{9} \frac{8.0}{14} \frac{8.2}{30} \frac{8.4}{50}$

$\frac{5.5}{50} \frac{4.9}{48} \frac{5.0}{43} \frac{5.7}{40} \frac{5.6}{38} \frac{5.4}{28} \frac{4.8}{25} \frac{4.3}{24} \frac{4.0}{19} \frac{4.3}{8} \underline{5.0}$

$\frac{7.9}{8} \frac{8.0}{14} \frac{8.2}{30} \frac{8.4}{50}$

$\frac{5.5}{50} \frac{5.4}{45} \frac{6.3}{43} \frac{6.4}{41} \frac{6.2}{38} \frac{5.2}{36} \frac{4.9}{30} \frac{4.5}{18} \frac{4.9}{10} \frac{5.2}{2} \underline{6.0}$

$\frac{7.3}{5} \frac{7.5}{18} \frac{7.2}{39} \frac{7.2}{50}$

$\frac{5.5}{50} \frac{5.6}{46} \frac{6.6}{44} \frac{6.7}{41} \frac{6.5}{40} \frac{5.4}{37} \frac{5.0}{31} \frac{4.8}{22} \frac{5.1}{11} \frac{5.4}{4} \underline{6.9}$

$\frac{7.5}{7} \frac{7.5}{20} \frac{6.8}{36} \frac{6.3}{50}$

$\frac{6.3}{50} \frac{6.8}{48} \frac{6.9}{46} \frac{6.8}{43} \frac{5.3}{41} \frac{5.3}{38} \frac{5.0}{34} \frac{4.9}{28} \frac{5.3}{13} \frac{5.9}{6} \frac{7.0}{4} \underline{7.2}$

$\frac{8.0}{5} \frac{8.2}{16} \frac{7.5}{30} \frac{6.5}{50}$

$\frac{6.5}{50} \frac{6.9}{48} \frac{6.9}{47} \frac{6.7}{45} \frac{6.7}{42} \frac{5.3}{39} \frac{5.0}{34} \frac{4.9}{25} \frac{5.4}{14} \frac{6.2}{7} \frac{7.2}{4} \underline{7.5}$

$\frac{6.6}{3} \frac{7.0}{12} \frac{7.5}{30} \frac{7.6}{50}$

SPIKE IN P. POLE RT STA 220+00

$\frac{5.1}{50} \frac{4.6}{43} \frac{3.3}{39} \frac{3.2}{34} \frac{3.3}{25} \frac{3.9}{14} \frac{4.3}{8} \frac{5.9}{4} \frac{6.1}{1} \underline{5.9}$

$\frac{3.2}{6} \frac{3.9}{20} \frac{4.7}{38} \frac{5.2}{50}$

$\frac{5.5}{50} \frac{5.5}{47} \frac{5.0}{45} \frac{3.7}{41} \frac{3.4}{38} \frac{3.5}{28} \frac{4.4}{13} \frac{5.2}{5} \frac{6.1}{3} \underline{6.5}$

$\frac{6.5}{2} \frac{5.3}{5} \frac{5.4}{19} \frac{5.6}{32} \frac{6.0}{50}$

$\frac{4.3}{50} \frac{4.3}{44} \frac{4.9}{41} \frac{4.8}{37} \frac{3.5}{35} \frac{3.7}{26} \frac{3.9}{18} \frac{4.8}{7} \underline{5.4}$

$\frac{6.5}{3} \frac{6.8}{8} \frac{7.5}{16} \frac{7.8}{30} \frac{8.5}{50}$

STA	+	π	-	ELEV
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STA	+	π	-	ELEV
222+35		917.26		

STA	+	π	-	ELEV
222+35		917.26		
+50				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				
223				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				
223				
+50				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				
223				
+50				
+90				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				
223				
+50				
+90				
224				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				
223				
+50				
+90				
224				
+25				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				
223				
+50				
+90				
224				
+25				
+36				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				
223				
+50				
+90				
224				
+25				
+36				
+40				

STA	+	π	-	ELEV
222+35		917.26		
+50				
+64				
+70				
+76				
223				
+50				
+90				
224				
+25				
+36				
+40				

LT

2

R.T

$\frac{2.7}{50} \frac{3.6}{39} \frac{4.8}{36} \frac{5.1}{33} \frac{5.1}{31} \frac{1.3}{28} \frac{3.9}{23} \frac{4.7}{14} \frac{4.7}{2} \frac{4.9}{5} \frac{5.2}{7} \frac{6.3}{10} \frac{6.8}{12} \frac{5.6}{14} \frac{8.2}{24} \frac{8.7}{35} \frac{8.6}{50}$

KOEHLER
RD

$\frac{2.4}{50} \frac{3.9}{32} \frac{5.2}{29} \frac{5.1}{25} \frac{4.3}{22} \frac{4.0}{19} \frac{4.0}{13} \frac{4.8}{5} \frac{5.3}{6} \frac{6.3}{9} \frac{6.6}{15} \frac{5.7}{16} \frac{6.8}{30} \frac{7.4}{42} \frac{7.8}{45} \frac{7.0}{48} \frac{5.4}{56} \frac{5.6}{78}$

KOEHLER
RD

$\frac{2.4}{50} \frac{3.5}{31} \frac{5.0}{28} \frac{5.1}{26} \frac{5.1}{23} \frac{4.3}{22} \frac{4.2}{17} \frac{4.2}{10} \frac{4.7}{3} \frac{5.3}{9} \frac{6.7}{13} \frac{7.0}{16} \frac{6.9}{18} \frac{6.0}{20} \frac{7.0}{29} \frac{7.4}{31} \frac{7.3}{35} \frac{5.7}{45} \frac{5.0}{50}$

FLOOR
HOUSE

KOEHLER
RD

$\frac{0.66}{62} \frac{2.6}{50} \frac{3.6}{30} \frac{5.3}{26} \frac{5.3}{24} \frac{5.2}{22} \frac{4.8}{21} \frac{4.3}{16} \frac{4.2}{8} \frac{4.7}{5} \frac{5.0}{5} \frac{5.4}{18} \frac{7.0}{17} \frac{7.2}{25} \frac{7.1}{33} \frac{5.6}{38} \frac{5.6}{50} \frac{5.1}{64}$

KOEHLER
RD

$\frac{2.8}{50} \frac{3.7}{29} \frac{5.1}{26} \frac{5.4}{24} \frac{5.3}{22} \frac{4.6}{20} \frac{4.4}{15} \frac{4.3}{6} \frac{4.7}{7} \frac{5.1}{7} \frac{5.6}{18} \frac{5.6}{34} \frac{5.6}{47} \frac{5.6}{50} \frac{5.6}{58}$

KOEHLER
RD

$\frac{3.0}{50} \frac{3.9}{35} \frac{4.4}{23} \frac{5.4}{21} \frac{5.4}{19} \frac{5.0}{16} \frac{4.8}{11} \frac{4.7}{5} \frac{5.0}{10} \frac{5.1}{18} \frac{5.4}{38} \frac{5.6}{50}$

KOEHLER
RD

$\frac{6.0}{50} \frac{5.6}{32} \frac{5.7}{14} \frac{6.1}{13} \frac{5.7}{10} \frac{5.5}{8} \frac{5.2}{4} \frac{5.2}{18} \frac{5.3}{30} \frac{6.0}{49} \frac{7.2}{50}$

KOEHLER
RD

$\frac{7.4}{50} \frac{7.4}{36} \frac{6.5}{17} \frac{7.0}{16} \frac{6.4}{14} \frac{5.9}{13} \frac{5.7}{4} \frac{5.7}{1} \frac{5.5}{9} \frac{5.0}{23} \frac{4.9}{23} \frac{5.3}{35} \frac{4.8}{37} \frac{5.1}{47} \frac{6.3}{57}$

KOEHLER
RD

$\frac{8.5}{50} \frac{8.5}{37} \frac{7.6}{22} \frac{6.3}{10} \frac{5.8}{4} \frac{5.7}{1} \frac{4.9}{5} \frac{4.9}{10} \frac{4.9}{21} \frac{5.1}{30} \frac{5.2}{33} \frac{4.7}{36} \frac{5.3}{42} \frac{9.6}{53}$

KOEHLER
RD

$\frac{6.0}{7} \frac{4.7}{5.7} \frac{4.9}{15} \frac{4.2}{29} \frac{5.7}{31} \frac{10.2}{35} \frac{10.2}{45}$

KOEHLER
RD

$\frac{6.0}{8} \frac{5.6}{5.6} \frac{4.6}{15} \frac{4.7}{28} \frac{4.6}{29} \frac{5.0}{32} \frac{8.8}{42}$

KOEHLER
RD

$\frac{6.0}{8} \frac{5.6}{5.6} \frac{4.7}{12} \frac{4.6}{27} \frac{4.4}{29} \frac{4.7}{32} \frac{7.8}{38}$

STA	+	π	-	ELEV
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		917.26		
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224+44				
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+50				
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+65				
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+75				
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B.M	265	91960	0.34	916.92	916.95
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225					
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+15					
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+25					
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+50					
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+75					
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226					
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+25					
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+50					
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NOEHLER
K

$\frac{6.0}{8}$ $\frac{4.7}{5.6}$ $\frac{4.6}{12}$ $\frac{4.4}{27}$ $\frac{4.9}{29}$ $\frac{7.8}{32}$ $\frac{7.8}{38}$

NOEHLER
K

$\frac{6.1}{9}$ $\frac{4.5}{5.4}$ $\frac{4.5}{13}$ $\frac{4.3}{25}$ $\frac{4.0}{28}$ $\frac{3.3}{32}$ $\frac{8.1}{38}$

$\frac{6.0}{11}$ $\frac{4.3}{5.2}$ $\frac{4.0}{13}$ $\frac{3.6}{26}$ $\frac{5.0}{28}$ $\frac{7.9}{32}$ $\frac{7.9}{39}$

$\frac{5.7}{12}$ $\frac{4.2}{5.0}$ $\frac{3.8}{12}$ $\frac{3.4}{25}$ $\frac{5.5}{27}$ $\frac{7.6}{35}$ $\frac{8.2}{40}$ $\frac{6.4}{44}$ $\frac{6.4}{50}$

SPIKE IN P. POLE N.W. COR NOEHLER + EDGERTON

$\frac{10.0}{50}$ $\frac{10.1}{42}$ $\frac{10.1}{28}$ $\frac{10.7}{26-23}$ $\frac{9.6}{16}$ $\frac{7.9}{14}$ $\frac{7.4}{10}$ $\frac{7.4}{7}$ $\frac{6.9}{6.9}$ $\frac{6.0}{16}$ $\frac{5.9}{30}$ $\frac{7.4}{35}$ $\frac{7.8}{40}$ $\frac{7.6}{44}$ $\frac{5.3}{49}$ $\frac{5.3}{60}$

$\frac{8.0}{68}$ $\frac{8.0}{46}$ $\frac{7.2}{31}$ $\frac{6.4}{25}$ $\frac{9.5}{20-17}$ $\frac{7.3}{12}$ $\frac{7.1}{6}$ $\frac{6.7}{6.7}$ $\frac{5.8}{12}$ $\frac{5.9}{33}$ $\frac{7.7}{41}$ $\frac{7.8}{49}$ $\frac{6.2}{52}$ $\frac{4.6}{56}$ $\frac{4.6}{62}$

$\frac{8.1}{76}$ $\frac{5.9}{44}$ $\frac{5.9}{28}$ $\frac{9.2}{21-17}$ $\frac{7.2}{13}$ $\frac{7.2}{7}$ $\frac{6.6}{6.6}$ $\frac{5.8}{14}$ $\frac{5.6}{24}$ $\frac{5.9}{35}$ $\frac{7.7}{45}$ $\frac{7.3}{54}$ $\frac{5.1}{57}$ $\frac{4.8}{72}$

$\frac{8.4}{81}$ $\frac{6.8}{73}$ $\frac{3.5}{65}$ $\frac{5.8}{50}$ $\frac{6.2}{29}$ $\frac{8.9}{23}$ $\frac{8.4}{17}$ $\frac{7.2}{13}$ $\frac{6.7}{5}$ $\frac{6.3}{6.3}$ $\frac{5.1}{20}$ $\frac{5.1}{32}$ $\frac{5.7}{48}$ $\frac{6.7}{56}$ $\frac{6.9}{62}$ $\frac{5.4}{73}$

$\frac{8.9}{77}$ $\frac{7.4}{68}$ $\frac{4.6}{62}$ $\frac{4.3}{59}$ $\frac{5.5}{52}$ $\frac{6.5}{41}$ $\frac{6.4}{30}$ $\frac{8.5}{24}$ $\frac{8.1}{18}$ $\frac{7.3}{16}$ $\frac{6.0}{6.0}$ $\frac{5.2}{12}$ $\frac{5.0}{22}$ $\frac{4.7}{43}$ $\frac{5.2}{64}$ $\frac{5.3}{80}$

EDGERTON

$\frac{9.6}{72}$ $\frac{7.5}{63}$ $\frac{4.2}{55}$ $\frac{6.1}{53}$ $\frac{5.9}{49}$ $\frac{6.5}{43}$ $\frac{8.1}{30}$ $\frac{8.0}{27}$ $\frac{7.0}{19}$ $\frac{6.3}{10}$ $\frac{5.6}{5.6}$ $\frac{5.1}{18}$ $\frac{5.0}{38}$ $\frac{4.7}{48}$ $\frac{4.7}{69}$

$\frac{11.3}{67}$ $\frac{9.0}{63}$ $\frac{8.7}{58}$ $\frac{5.4}{48}$ $\frac{6.7}{46}$ $\frac{6.7}{30}$ $\frac{8.2}{26}$ $\frac{7.7}{20}$ $\frac{7.0}{18}$ $\frac{6.2}{11}$ $\frac{5.3}{5.3}$ $\frac{5.0}{8}$ $\frac{4.9}{16}$ $\frac{6.7}{22}$ $\frac{6.6}{34}$ $\frac{3.9}{40}$ $\frac{3.7}{50}$

$\frac{10.6}{59}$ $\frac{8.2}{47}$ $\frac{5.4}{41}$ $\frac{6.8}{38}$ $\frac{6.6}{34}$ $\frac{8.2}{30}$ $\frac{7.8}{27}$ $\frac{6.7}{22}$ $\frac{6.0}{17}$ $\frac{6.0}{13}$ $\frac{5.1}{5.1}$ $\frac{4.8}{15}$ $\frac{8.2}{22}$ $\frac{7.9}{34}$ $\frac{7.0}{42}$ $\frac{1.4}{58}$ $\frac{0.6}{64}$ $\frac{0.6}{70}$

STA	+	π	-	ELEV
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919.60

226+75

+85

227

+25

+36

+52.74

T.P.	0.45	907.79	12.26	901.34
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224+25

+36

+40

T.P.	6.54	902.01	12.32	895.47
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+44

+50 48" X 113' C.M. CULVERT

+65

LT

Q

RT

$\frac{11.0}{43} \frac{6.7}{37} \frac{6.0}{31} \frac{8.0}{27} \frac{7.4}{23} \frac{6.5}{20} \frac{5.7}{12} \underline{4.8}$ $\frac{4.4}{15} \frac{7.9}{21} \frac{8.1}{25} \frac{6.0}{29} \frac{2.0}{36} \frac{+0.1}{43} \frac{+0.5}{51} \frac{+0.5}{63}$

$\frac{9.5}{39} \frac{7.7}{35} \frac{7.3}{31} \frac{8.4}{28} \frac{8.0}{25} \frac{6.3}{20} \frac{5.7}{12} \underline{4.8}$ $\frac{4.6}{8} \frac{4.3}{14} \frac{7.8}{22} \frac{8.0}{26} \frac{7.1}{30} \frac{2.3}{39} \frac{0.0}{49} \frac{+0.5}{59}$

$\frac{13.2}{43} \frac{15.0}{42} \frac{13.2}{36} \frac{10.4}{34} \frac{7.4}{26} \frac{6.2}{22} \frac{6.3}{20} \frac{5.5}{12} \underline{4.6}$ $\frac{4.2}{14} \frac{6.8}{21} \frac{7.0}{27} \frac{3.1}{38} \frac{2.6}{43} \frac{0.9}{50}$

$\frac{11.1}{31} \frac{6.0}{23} \frac{6.0}{22} \frac{6.7}{21} \frac{5.4}{14} \underline{4.5}$ $\frac{4.4}{9} \frac{4.2}{14} \frac{7.2}{21} \frac{7.3}{28} \frac{4.3}{42} \frac{3.5}{53}$

$\frac{11.3}{33} \frac{6.4}{23} \frac{5.1}{11} \underline{4.4}$ $\frac{4.4}{9} \frac{4.3}{15} \frac{8.0}{22} \frac{6.5}{37} \frac{3.9}{50}$

$\frac{10.3}{31} \frac{10.1}{30} \frac{6.4}{23} \frac{5.2}{15} \underline{4.3}$ $\frac{4.4}{10} \frac{4.2}{15} \frac{10.3}{25} \frac{12.0}{28} \frac{12.3}{33} \frac{8.8}{44} \frac{6.9}{50}$

$\frac{6.8}{68} \frac{7.6}{50} \frac{9.0}{35} \frac{7.3}{25} \frac{5.6}{21}$

$\frac{11.0}{76} \frac{11.2}{63} \frac{11.1}{48} \frac{12.6}{44} \frac{11.4}{42} \frac{8.3}{36} \frac{2.7}{27}$

$\frac{9.2}{92} \frac{11.1}{78} \frac{13.3}{63} \frac{14.0}{50} \frac{14.0}{38} \frac{10.3}{33} \frac{6.6}{23}$

$\frac{9.2}{92} \frac{11.1}{78} \frac{13.3}{63} \frac{14.0}{50} \frac{14.0}{38} \frac{10.3}{33} \frac{6.6}{23}$

$\frac{4.0}{98} \frac{8.6}{80} \frac{10.3}{38} \frac{12.6}{38} \frac{3.6}{29} \frac{2.7}{25}$

Q
DITCH

$\frac{8.4}{100} \frac{10.2}{86} \frac{8.6}{68} \frac{7.3}{56} \frac{6.6}{42} \frac{5.8}{36} \frac{3.7}{33} \frac{2.4}{30} \frac{0.5}{24}$

STA	+	π	-	ELEV
		902.01		

224+75

225

+15

+25

T.P	7.47	905.13	4.35	897.66
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+50

+75

T.P	7.58	902.41	10.30	894.83
-----	------	--------	-------	--------

226

+25

+50

+75

227

+25

LT

¢

RT

$$\begin{array}{r} 9.9 \\ 97 \end{array} \quad \begin{array}{r} 8.3 \\ 87 \end{array} \quad \begin{array}{r} 4.0 \\ 67 \end{array} \quad \begin{array}{r} 4.1 \\ 51 \end{array} \quad \begin{array}{r} 0.5 \\ 28 \end{array} \quad \begin{array}{r} 12.0 \\ 21 \end{array}$$

$$\begin{array}{r} 10.4 \\ 112 \end{array} \quad \begin{array}{r} 8.7 \\ 106 \end{array} \quad \begin{array}{r} 4.8 \\ 99 \end{array} \quad \begin{array}{r} 2.2 \\ 83 \end{array}$$

$$\begin{array}{r} 10.6 \\ 116 \end{array} \quad \begin{array}{r} 8.6 \\ 110 \end{array} \quad \begin{array}{r} 4.8 \\ 105 \end{array} \quad \begin{array}{r} 4.2 \\ 98 \end{array} \quad \begin{array}{r} 2.3 \\ 73 \end{array}$$

$$\begin{array}{r} 10.6 \\ 117 \end{array} \quad \begin{array}{r} 8.6 \\ 110 \end{array} \quad \begin{array}{r} 4.8 \\ 106 \end{array} \quad \begin{array}{r} 4.2 \\ 99 \end{array} \quad \begin{array}{r} 2.3 \\ 94 \end{array}$$

$$\begin{array}{r} 13.5 \\ 120 \end{array} \quad \begin{array}{r} 11.7 \\ 115 \end{array} \quad \begin{array}{r} 7.9 \\ 109 \end{array} \quad \begin{array}{r} 4.3 \\ 99 \end{array}$$

$$\begin{array}{r} 13.7 \\ 121 \end{array} \quad \begin{array}{r} 11.7 \\ 116 \end{array} \quad \begin{array}{r} 7.6 \\ 108 \end{array} \quad \begin{array}{r} 7.5 \\ 103 \end{array} \quad \begin{array}{r} 5.0 \\ 93 \end{array}$$

$$\begin{array}{r} 10.6 \\ 118 \end{array} \quad \begin{array}{r} 9.3 \\ 114 \end{array} \quad \begin{array}{r} 3.8 \\ 104-102 \end{array} \quad \begin{array}{r} 3.5 \\ 99 \end{array} \quad \begin{array}{r} 3.5 \\ 93 \end{array}$$

$$\begin{array}{r} 10.9 \\ 114 \end{array} \quad \begin{array}{r} 9.8 \\ 110 \end{array} \quad \begin{array}{r} 4.2 \\ 99-96 \end{array} \quad \begin{array}{r} 4.4 \\ 94-90 \end{array}$$

$$\begin{array}{r} 11.2 \\ 110 \end{array} \quad \begin{array}{r} 9.8 \\ 104 \end{array} \quad \begin{array}{r} 3.9 \\ 93-89 \end{array} \quad \begin{array}{r} 4.3 \\ 85 \end{array} \quad \begin{array}{r} 4.3 \\ 78 \end{array}$$

$$\begin{array}{r} 11.3 \\ 100 \end{array} \quad \begin{array}{r} 9.7 \\ 94 \end{array} \quad \begin{array}{r} 8.6 \\ 91 \end{array} \quad \begin{array}{r} 5.3 \\ 85 \end{array} \quad \begin{array}{r} 4.7 \\ 80 \end{array} \quad \begin{array}{r} 5.7 \\ 77 \end{array} \quad \begin{array}{r} 5.9 \\ 68 \end{array} \quad \begin{array}{r} 2.2 \\ 62 \end{array}$$

$$\begin{array}{r} 11.0 \\ 85 \end{array} \quad \begin{array}{r} 9.2 \\ 79 \end{array} \quad \begin{array}{r} 6.9 \\ 73 \end{array} \quad \begin{array}{r} 6.1 \\ 65 \end{array} \quad \begin{array}{r} 3.9 \\ 56 \end{array}$$

$$\begin{array}{r} 11.7 \\ 71 \end{array} \quad \begin{array}{r} 9.7 \\ 62 \end{array} \quad \begin{array}{r} 8.4 \\ 60 \end{array} \quad \begin{array}{r} 5.2 \\ 58-55 \end{array} \quad \begin{array}{r} 1.3 \\ 43 \end{array}$$

LAST READINGS TO DITCH

STA	+	π	-	ELEV
		962.41		

227+36	48" X 113' C.M. CULVERT LT			
--------	----------------------------	--	--	--

+32.74

T.P.	12.50	914.81	0.10	962.31
------	-------	--------	------	--------

T.P.	0.77	914.88	0.70	914.11
------	------	--------	------	--------

T.P.	0.42	904.15	11.15	903.73
------	------	--------	-------	--------

224+25

+36 48" X 113' C.M. CULVERT RT

+40

+44

+50

T.P.	11.48	915.21	0.42	903.73
------	-------	--------	------	--------

+65

T.P.	612	919.29	2.04	913.17
------	-----	--------	------	--------

B.M.			229	917.00	916.95
------	--	--	-----	--------	--------

LT

♀

RT

F.L. 88.78

$$\frac{3.6}{89} \frac{7.4}{74} \frac{9.9}{68} \frac{12.3}{61}$$

$$\frac{13.63}{60} \frac{7.5}{60} \frac{2.7}{49}$$

$$\frac{1.8}{78} \frac{4.3}{70} \frac{6.0}{60} \frac{6.9}{58-57} \frac{5.1}{55}$$

$$\frac{4.2}{60} \frac{6.4}{70} \frac{7.5}{75} \frac{5.8}{100}$$

F.L. 100.0

$$\frac{7.9}{63} \frac{14.1}{75} \frac{13.2}{100}$$

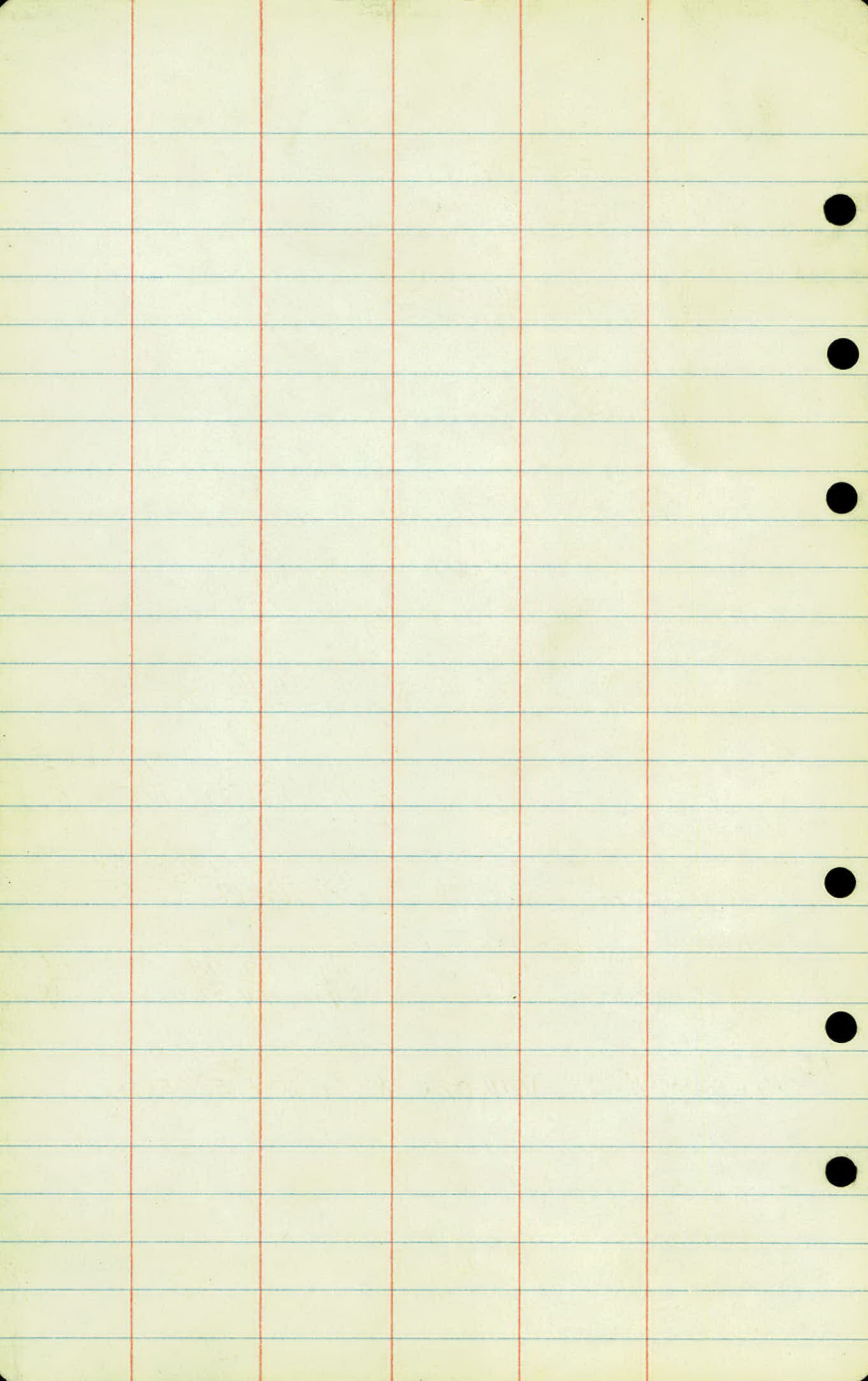
$$\frac{7.5}{63} \frac{9.6}{70} \frac{11.4}{77} \frac{10.7}{87} \frac{9.6}{92} \frac{9.9}{100}$$

$$\frac{8.0}{65} \frac{7.5}{77} \frac{7.1}{87} \frac{6.6}{100}$$

$$\frac{4.3}{57} \frac{6.0}{62} \frac{5.4}{69} \frac{6.0}{87} \frac{5.4}{100}$$

$$\frac{7.1}{42} \frac{7.9}{44} \frac{9.9}{47-49} \frac{9.0}{51} \frac{9.7}{74} \frac{6.0}{100}$$

SPIKE IN P. POLE N.W. COR KOENKER + EDGERTON



Edgerton St.

Stationing Notes

X Drain at sta. 16 + 23

Sta	+	π	-	Elev
BM	0.29	879.42		(879.13)
T.P.	1.58	870.51	10.49	868.93

14.35

Elev. water rt. = 12.14

16 +23

E 15+00			2.84	
FF			2.84	
T.P.	9.85	879.46	0.90	869.61
BM.			0.31	879.15

11-30-44
K. Anker
G. Nadon
G. Fewer

20° Above

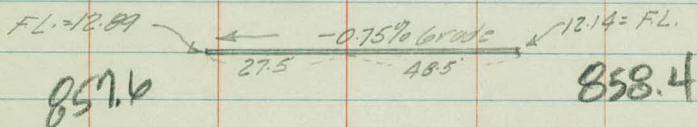
Lt

☒

Bt.

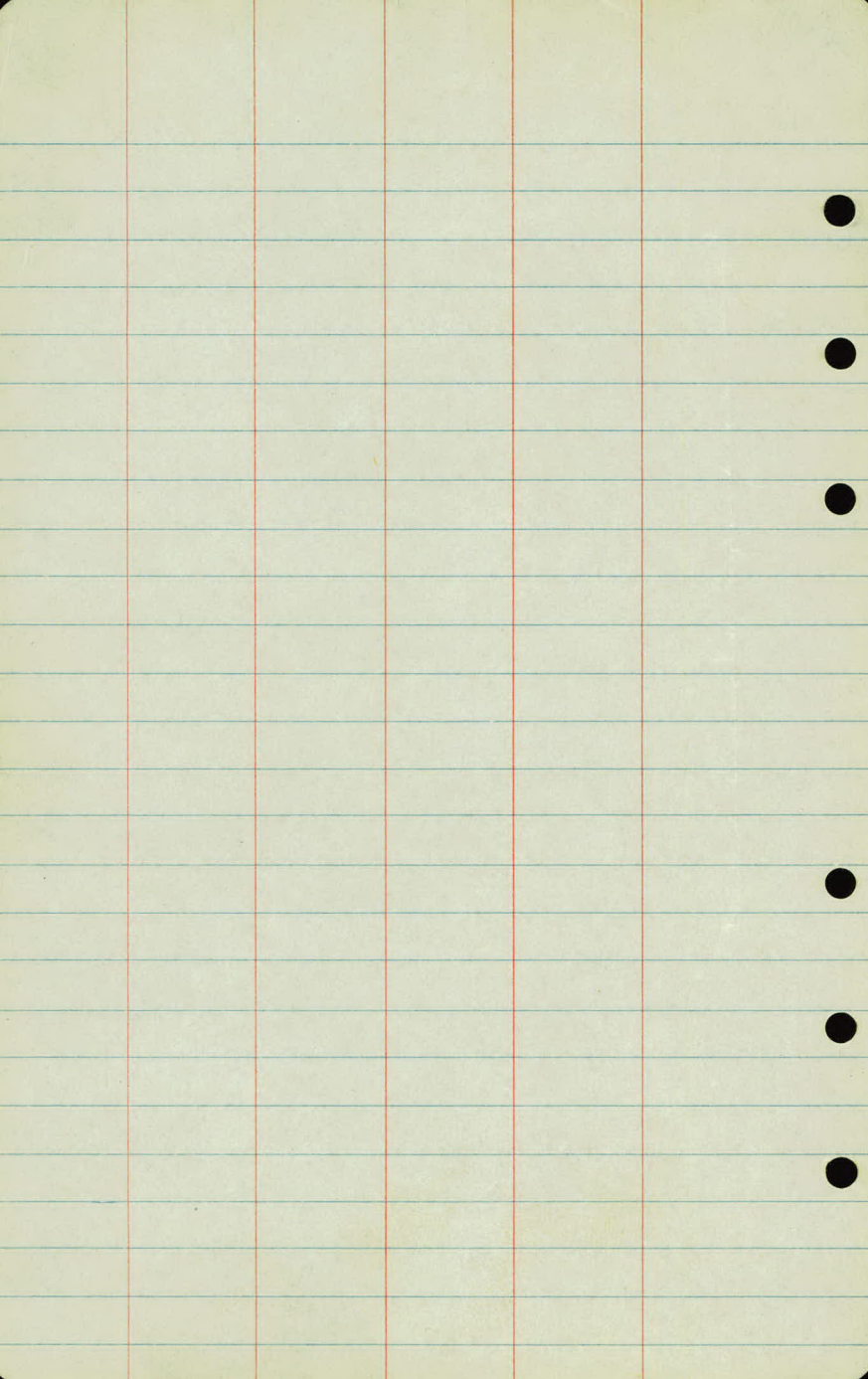
Top Hyd. W. side Edgerton St. & 1100' N. of Carpentier.
(No out)

Top & approx end of tile pipe at S. end of path.



E. Sta. 15+00

Top Hyd.



EDGERTON ST. XDRAIN

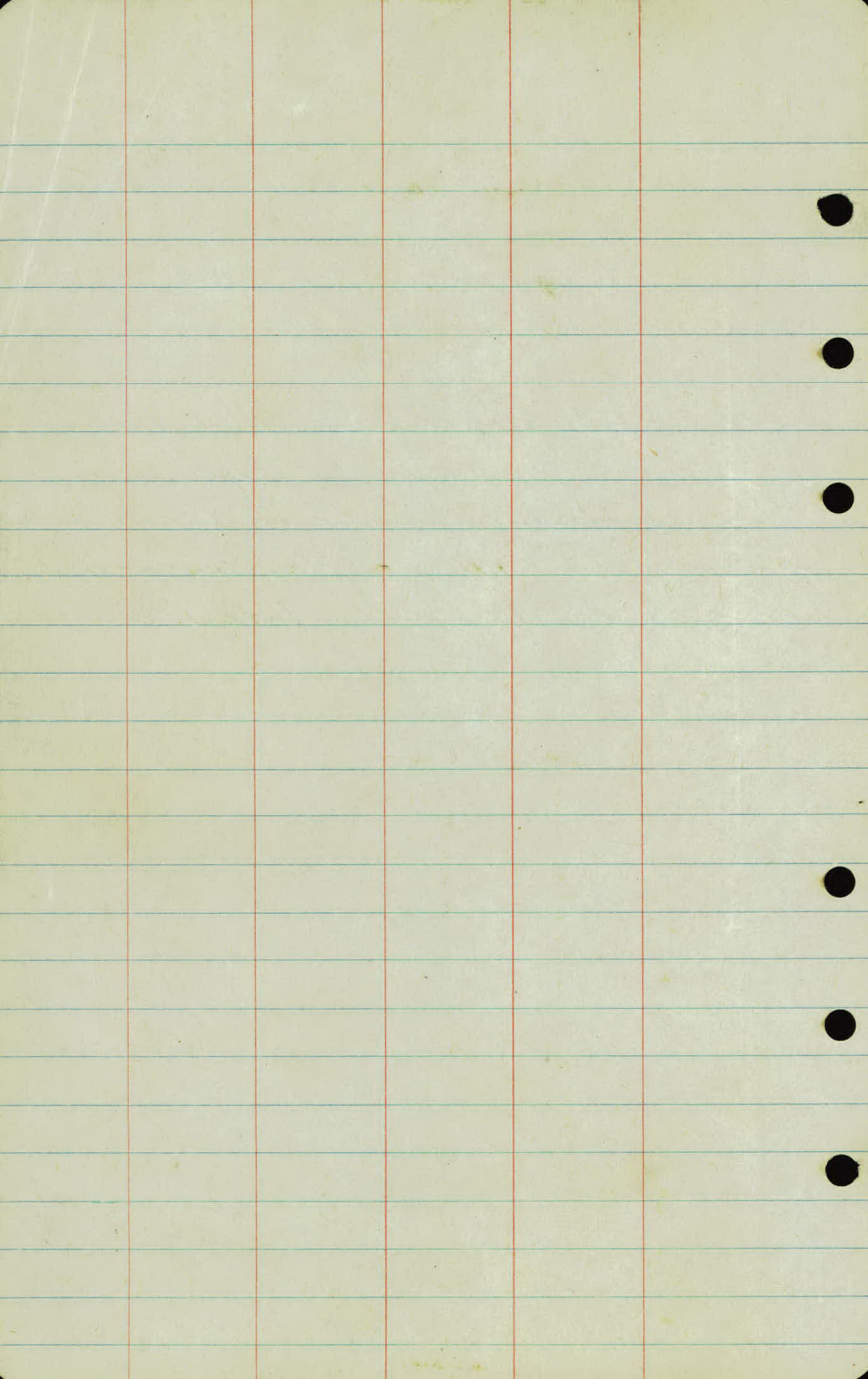
Located at Engineers Station 16+23 at
Forest Cemetery.

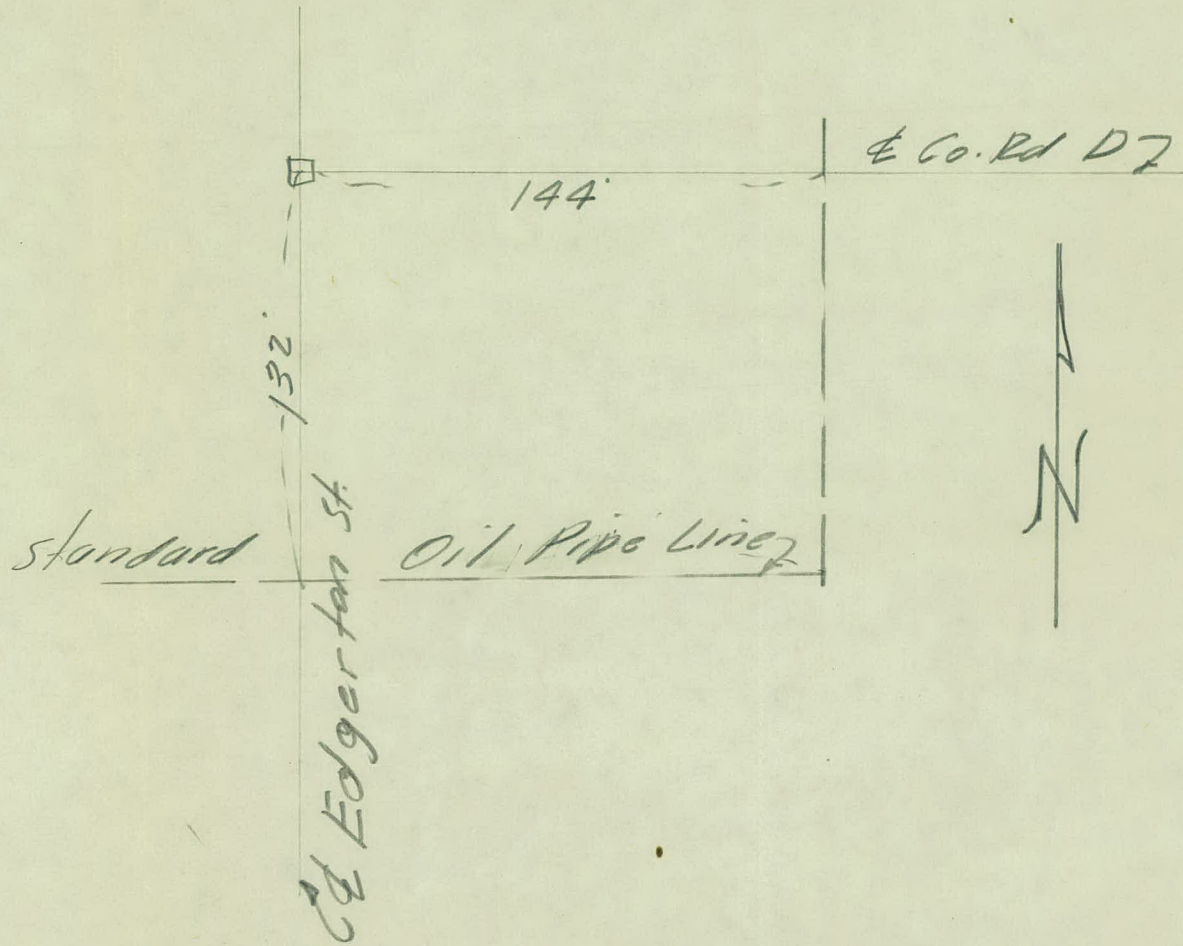
This is to certify that I have
inspected the survey grade stakes showing
the elevation for the inlet of Xdrain
culvert and I am satisfied that they
are set to the grade I desire.

J. W. Eiler
Supt.

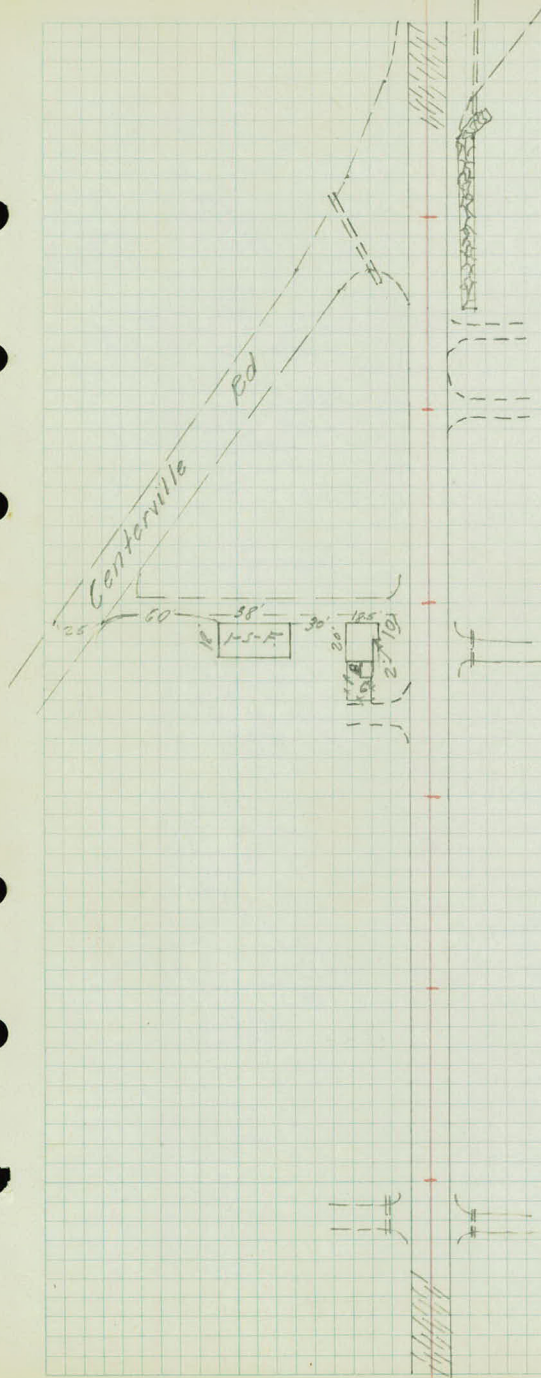
Chas. H. Nadon } witnesses
Chas. A. Fencer }

Nov. 30, 1944





16044122
132.00
15940922



G.R.-22 B.Top-17' B1.Top-47-100' Pav. 115-164'

+50-G.R.-38- B1 Top-30' +50-B1.Top-61. Pav.-92'

+25 End B1.Top + Beg. Pav.-72'

192 G.R.-59'

B1.Top-51'

+65 End 24" Conc. Culv.-95'

+90-Δ in Fe.-64'

+76-T.P.-Fe-59'

+13-61r. 4'x4' C.B.-48' Beg. G.R.-68'

+19-End of Wall-21'

+03-Ctr. 4'x4' C.B.-24.6' 18"x54.5" CM

191 Vadon's Blvd.-110-85'

Fe-46

+95-Face of Beg. of Br. Retain. Wall-215'

+92-Beg. G.R.-15.2'

+90-T.P.-32'

+75-Ctr. 4'x4' C.B.-25'

190

+21-Fe Cor.-44'

+95-T.P.-28'

+62-End of E1x4' 1" Rod.

+47-End of Bent Along Rd.-16.3'

+50-Δ Bent-18.5'

+41-Δ Bent-26'

+32-End of Ctr Bent

+32-End Bent Along Rd.-17.5'

(Black Top Begins Under Bridge)

+23.4-Δ of Tracks

+15-End of Bent-16.4' 2. sets of piling.

+06-Bent-26'

+14.5-Beg Ctr Bent

189) Δ + End of Bent along Rd.-16.8'

+98-Δ End of Bent Btu to Br.-18'

+82-Beg. Ctr. Lane.

+89-T.P.-24'

1" Rod.

+61-Pav 11' 11'

+25-Pav= 10' 10'

188 Gutter-16'

+89-T.P.-

187 Gutter-16'

+80-36" E1m.-52'

+69-T.P.-25'

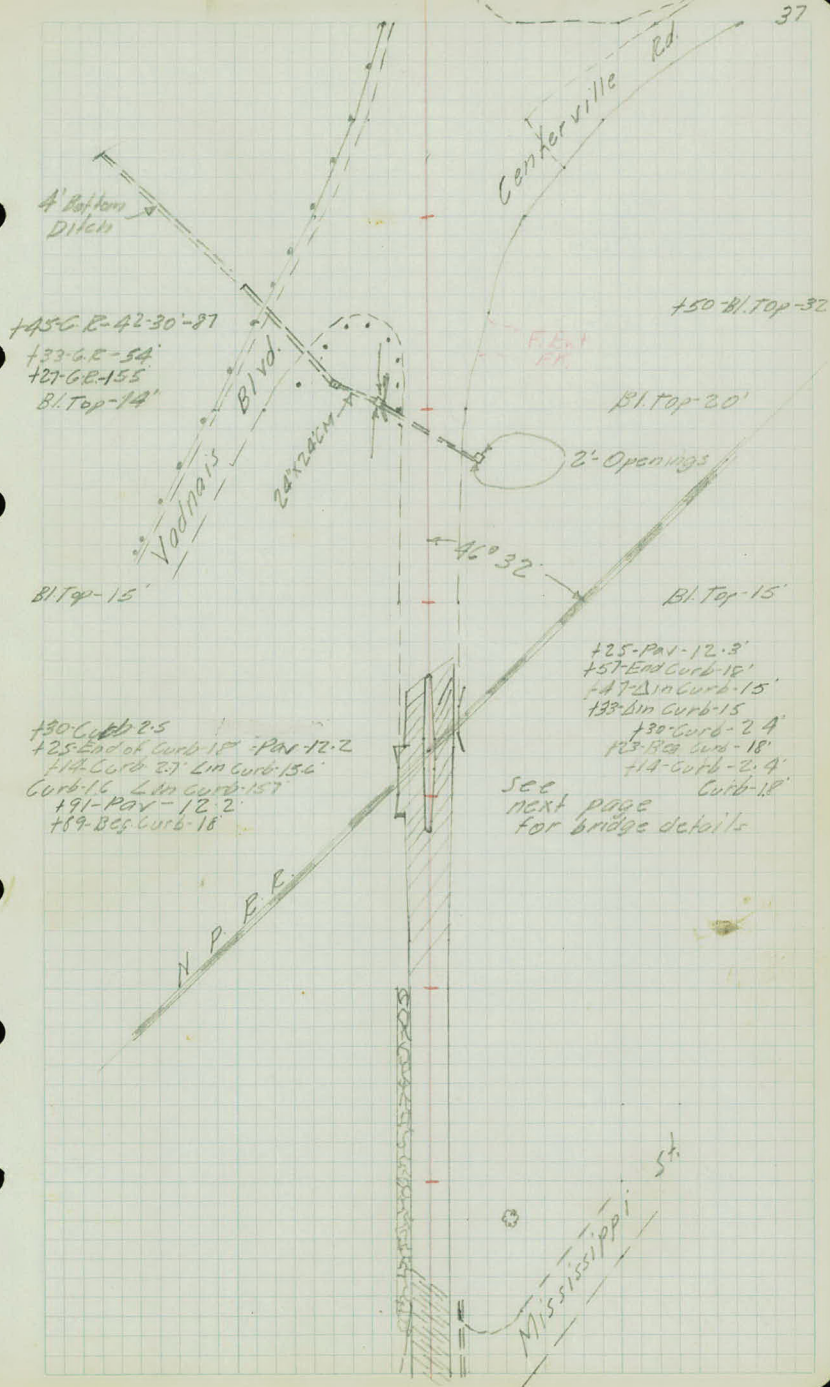
+35-B1 Top-10'

+32-Subsile Gutter 16-10'

+99-End Culv.-14'

+33-Edge Rd.-15'-48'

186



4' Bottom Ditch

Centerville Rd.

+456 B-42-30-87

+33 G.R.-54

+27 G.R.-155

Bl. Top-14'

+50 Bl. Top-32'

Vadnais Blvd.

2x22cm

Flt FR

Bl. Top-30'

2' Openings

Bl. Top-15'

46° 32'

Bl. Top-15'

+130 Curb-2.5

+25 End of Curb-18' Pav-12.2

+14 Curb 27' Lin Curb-136'

Curb-16' Lin Curb-157

+91 Pav-12.2

+89 Beg Curb-18'

+25 Pav-12.3'

+57 End Curb-18'

+47.2 In Curb-15'

+33.2 In Curb-15'

+30 Curb-2.4'

+23 Beg Curb-18'

+14 Curb-2.4'

Curb-18'

see next page for bridge details

N.P.E.R.

Mississippi St.

194 Treas-35 Bl Top

+80-Beg Treas-41'

+50-Ent Lake-135

+33-End G.R.-17'

+21-End 30" Conc. Culv-33'

193

Fc.-32'

+36-Fc. Cor.-35

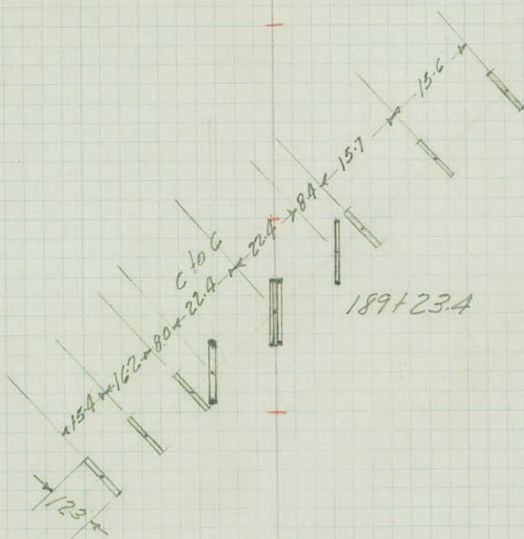
+31-End 30" Conc. Culv.-32'

+30-Bl Top-11'

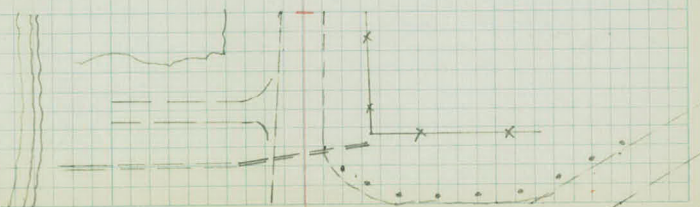
+25-Pav.-164' +20-T.P.-33'

+19-End G.R.-20'

G.R. about 14' from Bl Top



TOP VIEW OF BENTS OF R.R. BRIDGE



12' 10' +92-Ent- $\frac{15" \times 20' \times 17}{21'}$

+67-Fc Cor-27'

+17-Cor Pines-50'

200 Fc-33' 12' 10'

+85-E Road $\frac{18" \times 26' \times 17}{90'}$

199

12' 10'

+17-Ent $\frac{15" \times 20' \times 17}{21'}$

+52-PP-31'

+30-Beg Fc-33'

+22-Fc Cor-32'

198

11' 11'

+81-24" Tw. Cotta-27'

+74-24" Cotta-28'

+29-18" Tw. Willow-27'

197 End Brush + Trees-30' 12' 12' +104-PP-

+50-Ent-

196 Trees + Brush-30' 11' 11'

Fc, 33'

195

11' 11' +14-PP?

+88-trees-30'

+70-Trees-30'

194

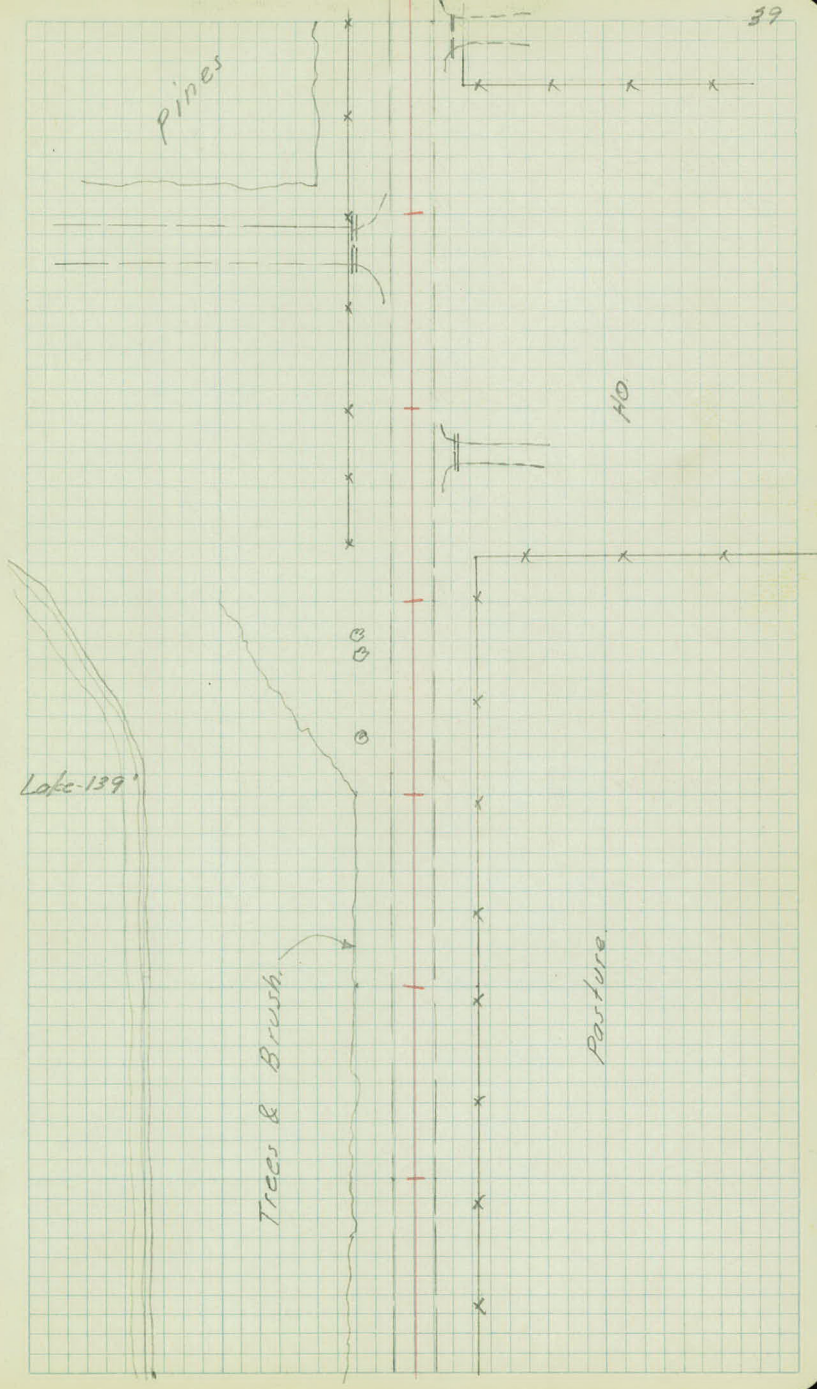
pinet

40

Lake-139'

Trees & Brush

Pasture



+81-4" Elm-35'

+93-SW Cor Ho-85'

+91-12" O.-36'

+75-4" Elm-42'

+36-SE Cor Ho-65'

+51-12" Trip O.-41'

+21-12" O.-35'

+42-Fe Cor-34'

207

10' 11'

+96-Ent-

+77-4" Elm-34'

+51-Fe Cor-35'

+30-Cor Pines-55'

206

11' 11'

Fe-35'

205

11' 10'

+65-Fe Cor-34'

204 Fe-34

11' 10'

+72-Range Tie

+69-Fe Cor-29'

203 Pines-47'

11' 11'

+67-Ent $\frac{15 \times 20 \text{ C.M.}}{21}$

202 Fe-33

11' 10'

Fe-27

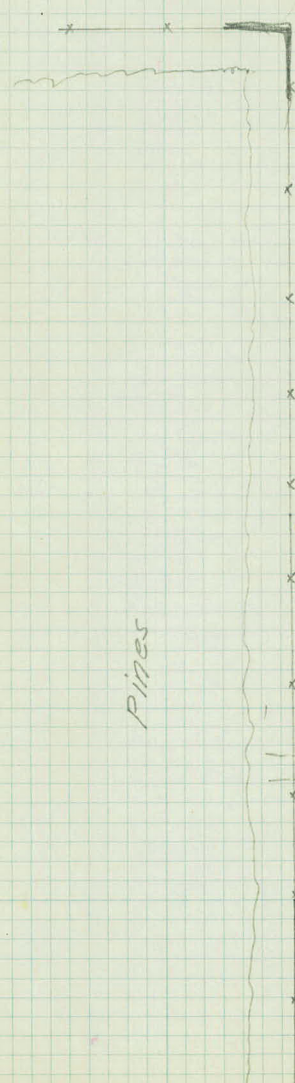
201

4-11-44

15-5-51
30' 24'

40

24'
1-5-51
10' 5' 10'
11'



Pines

Uncult.

Uncult.

+43-PP-23'
+33-S.W. Cor Ho-110'

214 14 7
+96-Ent- $\frac{15' \times 20' \times 11}{19'}$

213 11' 11' Fe-33'

+20-5/p-35'
212 11' 10'

+23-PP-29'
211 11' 10' Fe-33'

+42-5/p-33'
+23-5/p-31'
210 11' 10'

209 11' 10'

+39-Beg. Fe.-33
+32-Ent- $\frac{15' \times 20' \times 11}{21'}$

208 +03-PP-29'

32
1-5-4
22



+50- 35'-12'

Fe-113' Rd-131'-161'

221

35'-14'

Fe-148 Rd-170'-200'

+87-PP-1'

+75-End Fe-5'

220

34'-12'

219

30'-9'

Fe-10'

218

28'-6'

+69-PP-12'

217

23'-2'

Fe-19'

+49-18'BE-22'

216

20'-0

Fe-22'

215

18' 4'

Fe-26'

42

Kepler

Pd.

16' 11' +11-End 48" C.M. - A3'

X Drain 48" X 120' C.M.

1' X 7' H.W. 2
+33-End 48" C.M. - 59' 6R-21' 19' 9'
+45-12" 0-35'
+37-18" 0-38'
+17-18" 0-40' +26-Beg. CR-13'
+104-Beg. CR-21' 21' 8' +08-Ent

227

+58-PP-36'

19' 11' +64-CP-19'
170'-220'

14'-+18'

226 2 Ditch-105'

17' 37'-51'-92'

13' 46'

+18-4-15' B.E.-30'
225 2 Ditch-99' 9' 28'

+86-End G.R.-10.7' X Drain 48" X 113' C.M.
1' X 7' H.W. 2
+51-End 48" C.M.-38' 6R-9' 7' 26' +73-Ent G.R.-26'
+36-End 48" C.M.-73' 1' X 7' H.W. 2

+10-Beg. G.R.-7'
224 +05-5' TW.B.E.-23' 3' 31'
+99-PP-10' +97-Beg. G.R.-35'
+90-PP-11' +78-Ent
+71-5' P-31'

+50. 5' 42'

+41-5' P-32'
+18-5' P-30'
+11-NE Cor Ho-56'
223 +102-15' Maple-29' 12' 56'

+88-15' Elm-31'
+68-15' Maple-34'

+51-Ent 12" X 24" Conc
30'

+50-22-0'

+59-12" B.E.-29' End Fe.
+52-12" B.E.-19'
Fe-41' Rd-61'-88'

222

28'-7'

Fe-81'

Rd-98-124'

C.N.

Ditch

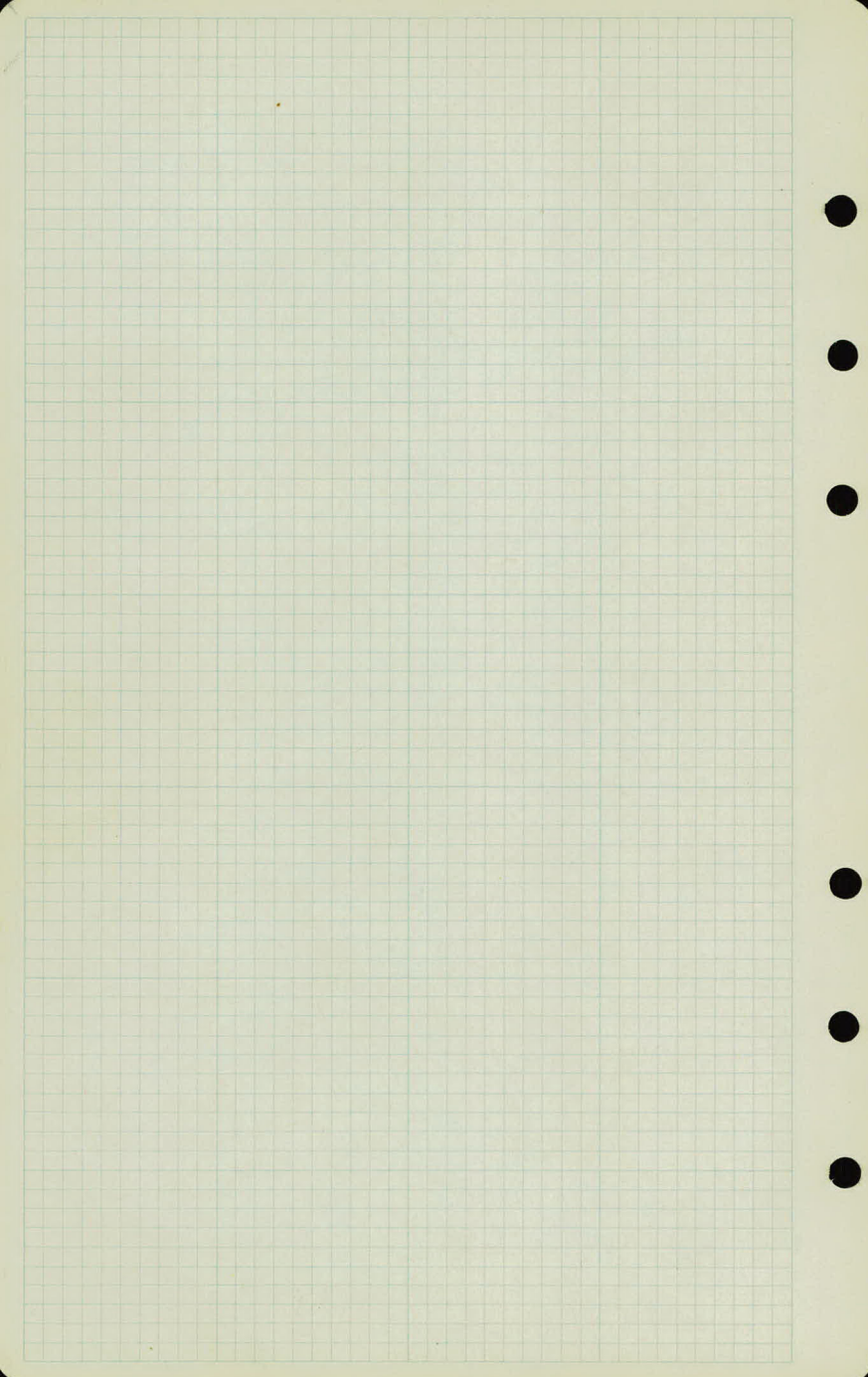
B. rush.

Ditch

22
1/2-5-8
17

+ 89. Lange me to Ho

+77-Rd-28'
+67-Rd-5'-45'



X SECTIONS

EDGERTON ST. - To - KAHLER RD

From Larpenteur Ave. to Koehler Road.

A.M

L.L

C.F

STA	+	π	-	ELEV
B.M	0.24	896.83		896.59

93.0

0+00

2 LARPEUR RT

+15

2 LARPEUR LT

+33

919

+50

91.4

1+00

89.7

+05

89.5

+37

88.5

+41

88.4

+85

86.9

+90

86.7

2+00

86.4

+27

85.7

LT

L

RT.

HYDRANT S.W. COR LAR PENTEUR + EDGERTON

$$\begin{array}{r} 5.3 \quad 4.6 \quad 4.1 \quad 3.9 \quad 3.8 \quad 3.3 \\ 50 \quad 27 \quad 17 \quad 10 \quad 3.8 \quad 50 \end{array}$$

$$\begin{array}{r} 5.1 \quad 4.6 \quad 4.4 \quad 4.3 \quad 4.2 \quad 4.1 \quad 3.6 \\ 50 \quad 28 \quad 10 \quad 4.3 \quad 10 \quad 35 \quad 50 \end{array}$$

$$\begin{array}{r} 5.9 \quad 5.3 \quad 5.0 \quad 4.9 \quad 4.9 \quad 4.9 \quad 3.9 \quad 2.7 \quad 1.8 \\ 50-45 \quad 18 \quad 10 \quad 4.9 \quad 10 \quad 22 \quad 33 \quad 38 \quad 50 \end{array}$$

$$\begin{array}{r} 15.1 \quad 13.5 \quad 7.8 \quad 6.1 \quad 5.3 \quad 5.2 \quad 5.4 \quad 5.5 \quad 4.6 \quad 3.1 \quad 1.6 \\ 64 \quad 50 \quad 33 \quad 19 \quad 14 \quad 10 \quad 5.4 \quad 10 \quad 13 \quad 34 \quad 37 \quad 50 \end{array}$$

$$\begin{array}{r} 17.0 \quad 12.2 \quad 11.0 \quad 7.9 \quad 7.3 \quad 7.3 \quad 7.2 \quad 6.9 \quad 6.3 \quad 4.5 \quad 3.1 \\ 50-45 \quad 32 \quad 23 \quad 17 \quad 14 \quad 10 \quad 7.1 \quad 10 \quad 18 \quad 35 \quad 38 \quad 50 \end{array}$$

$$\begin{array}{r} 17.0 \quad 12.2 \quad 11.0 \quad 7.8 \quad 7.4 \quad 7.3 \quad 7.4 \quad 9.6 \quad 6.9 \quad 6.2 \quad 4.3 \quad 3.2 \\ 50-45 \quad 32 \quad 23 \quad 17 \quad 10 \quad 7.3 \quad 10 \quad 18 \quad 21-23 \quad 27 \quad 34 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 15.8 \quad 12.4 \quad 8.4 \quad 8.5 \quad 8.3 \quad 8.2 \quad 9.7 \quad 7.8 \quad 7.8 \quad 4.9 \quad 4.2 \\ 50-38 \quad 23 \quad 16 \quad 10 \quad 8.3 \quad 10 \quad 17 \quad 21-23 \quad 27 \quad 35 \quad 42 \quad 50 \end{array}$$

$$\begin{array}{r} 15.8 \quad 13.5 \quad 12.8 \quad 8.6 \quad 8.6 \quad 8.5 \quad 8.4 \quad 9.7 \quad 8.0 \quad 8.2 \quad 7.9 \\ 50-38 \quad 30 \quad 24 \quad 16 \quad 10 \quad 8.4 \quad 10 \quad 18 \quad 21-23 \quad 27 \quad 41 \quad 50 \end{array}$$

$$\begin{array}{r} 15.7 \quad 14.4 \quad 9.7 \quad 10.0 \quad 9.9 \quad 9.9 \quad 9.8 \quad 10.6 \quad 9.8 \quad 9.3 \quad 8.9 \\ 50-36 \quad 24 \quad 15 \quad 11 \quad 9.9 \quad 10 \quad 18 \quad 21-23 \quad 26 \quad 37 \quad 50 \end{array}$$

$$\begin{array}{r} 14.6 \quad 15.0 \quad 14.3 \quad 9.9 \quad 10.2 \quad 10.1 \quad 10.1 \quad 10.9 \quad 10.1 \quad 9.9 \quad 7.2 \quad 6.0 \\ 50-34 \quad 32 \quad 24 \quad 15 \quad 10 \quad 10.1 \quad 10 \quad 18 \quad 21-23 \quad 26 \quad 32 \quad 41 \quad 50 \end{array}$$

$$\begin{array}{r} 14.5 \quad 14.5 \quad 10.1 \quad 10.5 \quad 10.4 \quad 10.4 \quad 11.2 \quad 10.2 \quad 10.2 \quad 7.2 \quad 5.8 \\ 50 \quad 26 \quad 14 \quad 10 \quad 10.4 \quad 10 \quad 18 \quad 21-23 \quad 26 \quad 32 \quad 42 \quad 50 \end{array}$$

$$\begin{array}{r} 14.5 \quad 14.5 \quad 13.7 \quad 11.0 \quad 11.3 \quad 11.1 \quad 11.0 \quad 12.1 \quad 10.9 \quad 10.8 \quad 7.1 \quad 6.1 \\ 50 \quad 28 \quad 21 \quad 14 \quad 10 \quad 11.1 \quad 10 \quad 18 \quad 21-23 \quad 26 \quad 32 \quad 45 \quad 50 \end{array}$$

STA	+	π	-	ELEV
		896.83.		
T.P.	1.38	888.48	9.73	887.10.
2+37				85.4
3+00				84.1
+05				84.0
+12				83.9
+25	L PRICE-AVE RT.			83.7
+45				83.4
+56				83.3
4+00				82.7
+50				82.2
5+00				81.6
T.P.	4.27	885.69.	7.06	881.42.
+09				81.6
+48				81.2

LT

K

RT

$$\checkmark \quad \begin{array}{cccccccccccc} \underline{6.1} & \underline{5.5} & \underline{3.2} & \underline{3.1} & \underline{3.3} & \underline{3.1} & \underline{3.1} & \underline{3.9} & \underline{2.9} & \underline{2.2} & \underline{1.4} \\ 50 & 24 & 14 & 11 & 10 & 31 & 10 & 18 & 21 & 23 & 26 & 31 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccccccc} \underline{6.4} & \underline{6.4} & \underline{6.0} & \underline{4.3} & \underline{4.3} & \underline{4.6} & \underline{4.4} & \underline{4.2} & \underline{5.3} & \underline{4.4} & \underline{4.0} & \underline{3.7} \\ 50 & 32 & 22 & 17 & 11 & 10 & 44 & 10 & 17 & 31 & 23 & 24 & 31 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccccccc} \underline{6.6} & \underline{6.1} & \underline{4.7} & \underline{4.4} & \underline{4.6} & \underline{4.5} & \underline{4.5} & \underline{4.3} & \underline{5.5} & \underline{4.4} & \underline{4.2} & \underline{5.3} & \underline{4.4} \\ 50 & 23 & 18 & 11 & 10 & 45 & 10 & 17 & 51 & 23 & 24 & 31 & 35 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{5.9} & \underline{3.5} & \underline{4.5} & \underline{4.6} & \underline{4.8} & \underline{4.6} & \underline{4.6} & \underline{4.4} & \underline{3.6} \\ 50 & 25 & 14 & 11 & 10 & 46 & 10 & 23 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{5.6} & \underline{5.4} & \underline{5.7} & \underline{5.2} & \underline{4.8} & \underline{5.0} & \underline{4.8} & \underline{4.3} & \underline{3.2} \\ 50 & 34 & 32 & 19 & 13 & 10 & 48 & 10 & 27 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{6.0} & \underline{5.8} & \underline{4.9} & \underline{5.2} & \underline{5.1} & \underline{5.1} & \underline{4.6} & \underline{3.5} \\ 50 & 21 & 14 & 10 & 51 & 10 & 31 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{11.0} & \underline{10.3} & \underline{5.6} & \underline{5.1} & \underline{5.3} & \underline{5.3} & \underline{5.0} & \underline{5.9} & \underline{4.7} & \underline{3.7} \\ 50 & 34 & 17 & 14 & 10 & 52 & 10 & 19 & 21 & 23 & 25 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{12.2} & \underline{12.3} & \underline{8.1} & \underline{5.9} & \underline{5.6} & \underline{5.9} & \underline{5.8} & \underline{5.9} & \underline{6.5} & \underline{5.9} & \underline{5.2} & \underline{4.6} \\ 50 & 40 & 26 & 18 & 14 & 10 & 58 & 10 & 18 & 21 & 23 & 24 & 33 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{11.4} & \underline{11.5} & \underline{8.0} & \underline{6.2} & \underline{6.2} & \underline{6.4} & \underline{6.4} & \underline{6.4} & \underline{7.0} & \underline{6.2} & \underline{5.7} & \underline{5.6} \\ 50 & 37 & 24 & 18 & 14 & 10 & 63 & 10 & 17 & 20 & 22 & 26 & 35 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{7.8} & \underline{9.0} & \underline{7.0} & \underline{7.5} & \underline{6.9} & \underline{6.9} & \underline{6.8} & \underline{7.4} & \underline{6.8} & \underline{6.8} & \underline{5.3} & \underline{4.9} \\ 50 & 35 & 22 & 18 & 10 & 69 & 10 & 15 & 20 & 22 & 25 & 37 & 44 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{3.9} & \underline{4.3} & \underline{4.5} & \underline{4.2} & \underline{4.1} & \underline{4.2} & \underline{4.2} & \underline{4.6} & \underline{4.4} & \underline{4.0} & \underline{4.5} & \underline{3.1} \\ 50 & 33 & 18 & 10 & 41 & 10 & 13 & 20 & 22 & 24 & 31 & 37 & 43 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} \underline{2.4} & \underline{3.9} & \underline{4.9} & \underline{3.1} & \underline{4.6} & \underline{4.5} & \underline{4.5} & \underline{5.1} & \underline{4.5} & \underline{4.2} & \underline{4.8} & \underline{2.1} \\ 50 & 33 & 25 & 17 & 10 & 45 & 10 & 17 & 20 & 22 & 25 & 30 & 36 & 41 & 50 \end{array}$$

STA	+	AT	-	ELEV
-----	---	----	---	------

885.69.

5+50				81.2
------	--	--	--	------

+54				81.2
-----	--	--	--	------

+60				81.1
-----	--	--	--	------

+78				80.9
-----	--	--	--	------

+92				80.8
-----	--	--	--	------

6+00				80.7
------	--	--	--	------

+05				80.7
-----	--	--	--	------

+20				80.5
-----	--	--	--	------

+38				80.3
-----	--	--	--	------

+58		80.1		
-----	--	------	--	--

£ KINGSTON ST RT.

+73				79.9
-----	--	--	--	------

+82				79.8
-----	--	--	--	------

LT

L

RT

$$\checkmark \quad \frac{1.3}{54} \quad \frac{2.0}{33} \quad \frac{4.0}{32} \quad \frac{5.0}{24} \quad \frac{5.0}{17} \quad \frac{4.6}{10} \quad \frac{4.5}{10} \quad \frac{4.5}{10} \quad \frac{4.6}{15} \quad \frac{5.0}{20-22} \quad \frac{4.3}{25} \quad \frac{4.3}{30} \quad \frac{4.8}{36} \quad \frac{2.8}{41-50}$$

$$\checkmark \quad \frac{0.8}{50} \quad \frac{2.0}{33} \quad \frac{3.9}{32} \quad \frac{5.2}{20} \quad \frac{4.6}{10} \quad \frac{4.5}{10} \quad \frac{4.6}{15} \quad \frac{5.1}{20-22} \quad \frac{4.3}{25} \quad \frac{4.4}{30} \quad \frac{4.8}{36} \quad \frac{2.9}{41-50}$$

$$\checkmark \quad \frac{0.8}{50} \quad \frac{0.9}{40} \quad \frac{1.8}{34} \quad \frac{4.2}{33} \quad \frac{5.2}{19} \quad \frac{4.7}{10} \quad \frac{4.6}{10} \quad \frac{4.6}{15} \quad \frac{5.3}{20-22} \quad \frac{4.6}{32} \quad \frac{4.9}{50}$$

$$\checkmark \quad \frac{0.6}{50} \quad \frac{0.8}{40} \quad \frac{2.0}{34} \quad \frac{5.1}{33} \quad \frac{5.4}{19} \quad \frac{4.9}{10} \quad \frac{4.8}{10} \quad \frac{4.9}{16} \quad \frac{5.3}{19-21} \quad \frac{4.8}{23} \quad \frac{4.6}{32} \quad \frac{5.2}{39} \quad \frac{5.0}{50}$$

$$\checkmark \quad \frac{0.5}{50} \quad \frac{1.3}{38} \quad \frac{2.3}{34} \quad \frac{5.1}{33} \quad \frac{5.5}{20} \quad \frac{5.1}{10} \quad \frac{4.9}{10} \quad \frac{4.9}{15} \quad \frac{5.0}{19-21} \quad \frac{5.3}{23} \quad \frac{4.9}{32} \quad \frac{4.5}{40} \quad \frac{8.0}{50} \quad \frac{9.2}{50}$$

$$\checkmark \quad \frac{0.5}{50} \quad \frac{1.2}{36} \quad \frac{2.6}{33} \quad \frac{5.2}{32} \quad \frac{5.4}{19} \quad \frac{5.1}{10} \quad \frac{5.0}{10} \quad \frac{5.1}{17} \quad \frac{5.4}{19-21} \quad \frac{4.8}{24} \quad \frac{4.8}{32} \quad \frac{8.4}{41} \quad \frac{8.6}{50}$$

$$\checkmark \quad \frac{5.0}{50} \quad \frac{5.0}{34} \quad \frac{5.4}{33} \quad \frac{5.4}{19} \quad \frac{5.2}{10} \quad \frac{5.0}{10} \quad \frac{5.2}{17} \quad \frac{5.4}{19-21} \quad \frac{5.3}{24} \quad \frac{5.2}{31} \quad \frac{5.6}{42} \quad \frac{6.3}{48} \quad \frac{8.1}{52}$$

FLOOR STORE

$$\checkmark \quad \frac{5.0}{34} \quad \frac{5.5}{33} \quad \frac{5.5}{15} \quad \frac{5.3}{10} \quad \frac{5.3}{10} \quad \frac{5.3}{16} \quad \frac{5.4}{19-21} \quad \frac{4.3}{25} \quad \frac{4.0}{32} \quad \frac{3.3}{37} \quad \frac{4.5}{50}$$

$$\checkmark \quad \frac{6.1}{50} \quad \frac{6.7}{33} \quad \frac{5.9}{16} \quad \frac{5.5}{10} \quad \frac{5.4}{10} \quad \frac{5.2}{13} \quad \frac{4.6}{30} \quad \frac{3.9}{41} \quad \frac{3.6}{50}$$

$$\checkmark \quad \frac{7.1}{50} \quad \frac{7.0}{33} \quad \frac{6.3}{20} \quad \frac{5.7}{10} \quad \frac{5.6}{10} \quad \frac{5.7}{10} \quad \frac{4.6}{14} \quad \frac{3.0}{50}$$

$$\checkmark \quad \frac{7.0}{50} \quad \frac{6.4}{20} \quad \frac{5.9}{10} \quad \frac{5.8}{10} \quad \frac{5.8}{10} \quad \frac{4.4}{37} \quad \frac{4.8}{38-40} \quad \frac{4.0}{43} \quad \frac{3.8}{50}$$

$$\checkmark \quad \frac{6.9}{50} \quad \frac{6.8}{24} \quad \frac{5.9}{10} \quad \frac{5.9}{10} \quad \frac{5.9}{10} \quad \frac{6.1}{18} \quad \frac{5.7}{24} \quad \frac{6.1}{24-28} \quad \frac{5.0}{31} \quad \frac{3.3}{50}$$

STA	+	π	-	ELEV
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885.69.

6+90

79.8

7+00

79.7

+50

79.2

8+00

78.8

+50

78.3

+87

78.1

9+00

77.9

+25

SECTION 10" X 38' VIT X DRAIN

77.8

+32

77.8

+50

77.8

T.P

10.09

895.26.

0.52

885.17.

7+50

79.2

8+00

78.8

LT

✱

RT

$$\checkmark \quad \begin{array}{cccccccccccccccc} 6.1 & 5.6 & 6.3 & 6.5 & 6.0 & 5.9 & 6.1 & 6.2 & 5.0 & 5.1 & 1.5 & 0.8 \\ 50 & 34 & 29 & 16 & 10 & 59 & 10 & 18 & 19-22 & 27 & 34 & 43 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccccccccccc} 6.4 & 6.1 & 6.8 & 6.2 & 6.1 & 6.0 & 5.8 & 6.3 & 5.6 & 5.5 & 0.1 \\ 30 & 33 & 29 & 20 & 10 & 60 & 10 & 17 & 18-23 & 25 & 32 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccccccccccc} 6.1 & 7.4 & 6.9 & 6.6 & 6.5 & 6.4 & 7.4 & 6.3 & 5.7 \\ 35-50 & 28 & 17 & 10 & 65 & 10 & 17 & 21-23 & 25 & 36 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccccccccccc} 7.0 & 7.6 & 7.0 & 6.9 & 6.9 & 7.9 & 6.6 & 6.4 \\ 50-33 & 30 & 10 & 69 & 10 & 18 & 21-22 & 25 & 33 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccccccccccc} 7.3 & 8.4 & 8.4 & 8.0 & 7.5 & 7.4 & 7.4 & 8.2 & 7.9 & 5.9 \\ 50-33 & 32 & 29 & 25 & 10 & 74 & 10 & 18 & 20-23 & 23 & 37 \end{array}$$

F.L. DRAIN

↓

$$\checkmark \quad \begin{array}{cccccccccccccccc} 9.4 & 9.4 & 9.0 & 10.1 & 8.7 & 8.1 & 7.8 & 7.6 & 7.6 & 8.8 & 8.9 & 7.6 & 7.1 \\ 50 & 41 & 34 & 30-23 & 20 & 15 & 10 & 76 & 10 & 19 & 20-23 & 25 & 26 & 34 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccccccccccc} 12.9 & 11.5 & 10.5 & 8.0 & 8.0 & 7.7 & 7.8 & 9.4 & 7.8 & 7.5 \\ 50 & 33 & 24 & 15 & 10 & 78 & 10 & 18 & 21-23 & 25 & 33 \end{array}$$

30" EAST-10RN

12" CM

F.L. 15' 6"

F.L. 15' 6"

F.L. R.R. X DRAIN

$$\checkmark \quad \begin{array}{cccccccccccccccc} 12.32 & 11.4 & 11.8 & 11.0 & 12.0 & 8.2 & 8.0 & 7.9 & 7.8 & 10.0 & 9.8 & 7.9 & 7.6 \\ 20 & 50 & 36 & 24 & 19 & 16 & 10 & 79 & 10 & 18 & 19 & 20-23 & 26 & 32 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccccccccccc} 9.1 & 9.5 & 8.1 & 8.0 & 7.9 & 7.9 & 7.9 & 9.3 & 7.8 & 7.5 \\ 50 & 32 & 16 & 10 & 79 & 10 & 18 & 20-23 & 25 & 36 \end{array}$$

T.P. TOP

N. RAIL S. RAIL

$$\checkmark \quad \begin{array}{cccccccccccccccc} 9.5 & 7.88 & 8.11 & 8.6 & 7.9 & 7.8 & 7.6 & 9.1 & 7.4 & 7.3 \\ 50 & 40 & 28 & 20 & 10 & 79 & 10 & 18 & 27-29 & 42 & 50 \end{array}$$

✓

(16.1)

+7.3

8.8

50

+9.3

6.8

65

✓

(16.5)

+8.6

7.9

50

+11.4

5.1

65

STA + π - ELEV

895.26

8+50

78.3

+87

78.1

9+00

77.9

+25

77.5

+32

77.8

T.P. 0.57 882.68 13.15 882.11

+63

SO. RAIL

7770

+68

NO. RAIL

77.98

+72

CATCH-BASIN R.R. CULV LT

+90

77.9

10+00

77.8

+34

77.7

+45

77.7

LT

Z

RT

✓

(17.0) ✓

+8.3

+9.9

+9.9

8.7

7.1

7.1

50

57

65

✓

(17.2) ✓

+5.4

+5.8

+9.7

+9.8

11.8

11.4

7.5

7.4

45

49

56

65

✓

(17.4) ✓

+5.5

+5.8

+10.0

+10.1

11.9

11.6

7.4

7.3

46

49

56

65

✓

(17.5) ✓

+5.6

+5.9

+9.9

+10.0

11.9

11.6

7.6

7.5

44

49

56

65

✓

(17.5) ✓

+5.8

+6.4

+6.4

11.7

11.1

11.1

46

57

65

4.98

4.70

✓

15"
CON
CURV
N.E.M.A.
CULV

10.4

7.3

C.8

N. RAIL S. RAIL

9.1
5012.29
4512.25
458.1
458.3
295.0
214.6
134.7
105.6
5.64.69
84.78
205.6
334.4
445.9
50

✓

10.5
509.4
347.6
265.1
114.9
104.9
4.94.9
104.8
145.0
194.8
294.70
375.6
4.975.6
50

✓

7.4
506.2
235.2
164.9
105.0
4.95.0
104.9
145.0
184.6
194.5
295.0
4.55.1
50

✓

7.0
506.0
295.1
174.8
125.0
7.05.0
5.05.0
105.4
134.9
204.5
205.9
295.0
50

✓

8.8
507.9
366.6
295.6
195.0
135.0
105.0
5.05.4
104.9
204.9
204.3
294.5
414.5
50

CURB WALK

CURB WALK

STA	+	π	-	ELEV	
		882.68.			
10+80				775	
+85				774	
11+00				772	
+43				76.3	
B.M	3.53	882.66.	3.53	879.15.	879.13.
+66				75.8	
+95				75.0	
12+00				74.9	
T.P	4.39	876.95.	10.10	872.56.	
+15				74.5	
+50				73.7	
+80				72.8	
+95				72.5	
13+00				724	

LT

L

RT

✓ $\frac{9.2}{50}$ $\frac{7.8}{24}$ $\frac{5.9}{19}$ $\frac{5.3}{10}$ $\frac{5.2}{10}$ $\frac{5.3}{10}$ $\frac{5.4}{20}$ $\frac{3.9}{34}$ $\frac{3.4}{50}$

✓ $\frac{7.4}{50}$ $\frac{5.9}{19}$ $\frac{5.3}{10}$ $\frac{5.3}{10}$ $\frac{5.3}{10}$ $\frac{5.4}{20}$ $\frac{4.1}{34}$ $\frac{3.5}{50}$

✓ $\frac{7.0}{50}$ $\frac{6.8}{36}$ $\frac{6.0}{18}$ $\frac{5.6}{10}$ $\frac{5.5}{10}$ $\frac{5.6}{10}$ $\frac{5.8}{20}$ $\frac{5.1}{20}$ $\frac{4.4}{29-34}$ $\frac{3.2}{38}$ $\frac{2.8}{50}$ CURB WALK

✓ $\frac{8.0}{50}$ $\frac{7.2}{33}$ $\frac{7.4}{30-24}$ $\frac{6.7}{19}$ $\frac{6.4}{10}$ $\frac{6.4}{10}$ $\frac{6.6}{20}$ $\frac{6.1}{20}$ $\frac{4.9}{30-34}$ $\frac{2.5}{39}$ $\frac{1.4}{50}$ CURB WALK

HYDRANT LT STA 11+50
✓ $\frac{14.0}{65}$ $\frac{10.2}{50}$ $\frac{7.1}{40}$ $\frac{7.1}{33}$ $\frac{8.8}{28-21}$ $\frac{7.0}{15}$ $\frac{7.0}{10}$ $\frac{6.9}{10}$ $\frac{7.0}{20}$ $\frac{6.9}{20}$ $\frac{6.6}{20}$ $\frac{5.7}{30-34}$ $\frac{1.9}{41}$ $\frac{1.1}{50}$ CURB WALK

✓ $\frac{15.1}{50}$ $\frac{10.7}{35}$ $\frac{10.2}{32}$ $\frac{10.5}{28-24}$ $\frac{7.7}{15}$ $\frac{7.7}{10}$ $\frac{7.7}{10}$ $\frac{7.7}{20}$ $\frac{7.7}{20}$ $\frac{7.2}{20}$ $\frac{6.5}{30-34}$ $\frac{2.2}{42}$ $\frac{1.3}{50}$ CURB

✓ $\frac{15.8}{50}$ $\frac{11.7}{34}$ $\frac{13.1}{29-25}$ $\frac{13.15}{25}$ $\frac{10.4}{22}$ $\frac{7.8}{15}$ $\frac{7.9}{10}$ $\frac{7.8}{10}$ $\frac{7.9}{20}$ $\frac{7.5}{20}$ $\frac{6.8}{30-34}$ $\frac{6.0}{34}$ $\frac{2.6}{42}$ $\frac{2.0}{50}$ NO END IS CONC CURV EL CURB WALK

✓ $\frac{16.7}{60}$ $\frac{14.8}{50}$ $\frac{13.3}{40}$ $\frac{3.5}{32}$ $\frac{2.4}{15}$ $\frac{2.5}{10}$ $\frac{2.5}{10}$ $\frac{2.6}{20}$ $\frac{2.7}{20}$ $\frac{2.4}{20}$ $\frac{1.6}{30-34}$ $\frac{0.8}{35}$ $\frac{1.21}{41}$ $\frac{1.3}{50}$

✓ $\frac{18.1}{60-50}$ $\frac{16.0}{43}$ $\frac{10.0}{27}$ $\frac{4.4}{18}$ $\frac{3.3}{15}$ $\frac{3.4}{10}$ $\frac{3.4}{10}$ $\frac{3.5}{20}$ $\frac{3.7}{20}$ $\frac{3.0}{20}$ $\frac{2.7}{30-34}$ $\frac{1.06}{35}$ $\frac{1.06}{50}$ CURB WALK

✓ $\frac{17.0}{60}$ $\frac{17.3}{50}$ $\frac{14.2}{35}$ $\frac{11.6}{26}$ $\frac{4.3}{15}$ $\frac{4.2}{10}$ $\frac{4.2}{10}$ $\frac{4.6}{18}$ $\frac{4.8}{20}$ $\frac{4.3}{30-34}$ $\frac{3.4}{42}$ $\frac{2.8}{50}$ CURB WALK

✓ $\frac{7.8}{50}$ $\frac{7.6}{35}$ $\frac{4.7}{15}$ $\frac{4.6}{10}$ $\frac{4.5}{10}$ $\frac{4.6}{15}$ $\frac{4.8}{20}$ $\frac{5.2}{20}$ $\frac{4.9}{30}$ $\frac{4.7}{34}$ $\frac{4.6}{41}$ $\frac{4.3}{50}$ CURB WALK

✓ $\frac{9.5}{50}$ $\frac{7.0}{32}$ $\frac{4.8}{16}$ $\frac{4.2}{10}$ $\frac{4.6}{10}$ $\frac{4.7}{10}$ $\frac{5.0}{15}$ $\frac{5.6}{20}$ $\frac{5.3}{30}$ $\frac{4.8}{34}$ $\frac{5.0}{42}$ $\frac{4.8}{50}$ CURB WALK

STA	+	π	-	ELEV
-----	---	-------	---	------

876.95

13+08	Φ	SCOTLAND RD	LT	721
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+21				718
-----	--	--	--	-----

+32				715
-----	--	--	--	-----

+57				709
-----	--	--	--	-----

+71				706
-----	--	--	--	-----

14+00				698
-------	--	--	--	-----

+47				686
-----	--	--	--	-----

T.P	4.55	871.53	9.97	866.98
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+58				684
-----	--	--	--	-----

+72				681
-----	--	--	--	-----

15+00				676
-------	--	--	--	-----

+50				666
-----	--	--	--	-----

+91	Φ	SPILLWAY	RT	661
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LT

Q

RT

CURB WALK

✓ $\frac{12.8}{75} \frac{9.4}{50} \frac{7.5}{36} \frac{5.3}{16} \frac{4.9}{10} \frac{4.9}{10} \frac{5.0}{10} \frac{5.2}{15} \frac{5.7}{20} \frac{5.4}{30} \frac{5.2}{34} \frac{5.5}{40} \frac{5.9}{50}$

CURB WALK

✓ $\frac{10.3}{50} \frac{7.9}{33} \frac{5.6}{15} \frac{5.3}{10} \frac{5.2}{10} \frac{5.3}{10} \frac{5.5}{15} \frac{6.1}{20} \frac{6.1}{30} \frac{5.8}{34} \frac{6.5}{40} \frac{7.3}{50}$

CURB WALK

✓ $\frac{19.7}{65} \frac{17.2}{50} \frac{16.2}{35} \frac{7.2}{18} \frac{5.9}{15} \frac{5.6}{10} \frac{5.5}{10} \frac{5.6}{10} \frac{6.0}{14} \frac{6.4}{20} \frac{6.5}{30} \frac{6.3}{34} \frac{6.7}{40} \frac{7.7}{50}$

CURB WALK

✓ $\frac{19.3}{65} \frac{18.4}{50} \frac{15.8}{35} \frac{7.1}{18} \frac{6.3}{15} \frac{6.1}{10} \frac{6.1}{10} \frac{6.2}{10} \frac{6.5}{14} \frac{7.1}{20} \frac{7.4}{30} \frac{7.2}{34} \frac{7.4}{38} \frac{8.1}{50}$

CURB WALK

✓ $\frac{10.6}{50} \frac{7.2}{35} \frac{7.4}{22} \frac{6.6}{15} \frac{6.5}{10} \frac{6.4}{10} \frac{6.5}{10} \frac{6.8}{14} \frac{7.0}{20} \frac{7.8}{30-34} \frac{8.3}{50}$

WALK

✓ $\frac{9.9}{50} \frac{8.4}{27} \frac{7.5}{14} \frac{7.2}{10} \frac{7.2}{10} \frac{7.2}{10} \frac{7.6}{18} \frac{8.5}{30-34} \frac{8.6}{50}$

WALK

✓ $\frac{11.3}{50} \frac{8.8}{26} \frac{8.7}{15} \frac{8.4}{10} \frac{8.4}{10} \frac{8.4}{10} \frac{8.7}{16} \frac{9.3}{18-20} \frac{9.0}{22} \frac{9.4}{27} \frac{9.5}{33} \frac{9.5}{50}$

WALK

✓ $\frac{12.4}{60} \frac{11.4}{50} \frac{8.2}{33} \frac{7.5}{25} \frac{3.3}{14} \frac{3.1}{10} \frac{3.1}{10} \frac{3.1}{10} \frac{3.5}{16} \frac{4.0}{18-20} \frac{3.8}{22} \frac{3.9}{29} \frac{4.2}{33} \frac{4.2}{50}$

✓ $\frac{13.5}{60} \frac{13.1}{50} \frac{11.6}{32} \frac{5.9}{19} \frac{5.2}{17} \frac{3.7}{14} \frac{3.5}{10} \frac{3.4}{10} \frac{3.5}{10} \frac{3.6}{16} \frac{4.2}{18-20} \frac{3.9}{22} \frac{4.2}{24} \frac{5.4}{50}$

✓ $\frac{16.0}{65} \frac{16.1}{50} \frac{15.1}{37} \frac{12.9}{29} \frac{6.6}{19} \frac{6.0}{18} \frac{4.1}{15} \frac{4.0}{10} \frac{3.9}{10} \frac{3.9}{16} \frac{5.0}{18-20} \frac{3.8}{21} \frac{3.9}{41} \frac{5.6}{50}$

✓ $\frac{19.0}{65} \frac{17.8}{50} \frac{16.2}{32} \frac{12.6}{27} \frac{11.9}{24} \frac{7.5}{20} \frac{6.9}{18} \frac{5.5}{14} \frac{5.1}{10} \frac{5.2}{9} \frac{4.9}{9} \frac{5.2}{9} \frac{5.0}{10} \frac{5.1}{16} \frac{6.3}{18-20} \frac{5.1}{21} \frac{5.1}{31} \frac{6.6}{41} \frac{7.6}{50}$

✓ $\frac{17.8}{70} \frac{17.2}{50} \frac{17.0}{40} \frac{16.2}{34} \frac{7.1}{19} \frac{5.8}{14} \frac{5.8}{10} \frac{5.6}{9} \frac{5.4}{10} \frac{6.1}{10} \frac{7.2}{21} \frac{8.0}{28} \frac{13.5}{50}$

STA + ∇ - ELEV

871.53.

16+00

66.2

+03

12" CM X 12' SPILLWAY LT

66.2

+50

66.3

17+00

66.5

+50

67.4

+76

68.1

18+00

69.0

+50

70.2

19+00

72.5

+50

74.6

+63

75.2

+73

75.7

LT

L

RT

✓ $\frac{17.8}{70} \frac{17.2}{50} \frac{17.1}{45} \frac{15.5}{33} \frac{7.4}{19} \frac{5.8}{14} \frac{5.5}{10} \frac{5.6}{9} \frac{5.3}{5.3} \frac{6.0}{10} \frac{6.3}{16} \frac{7.3}{18.20} \frac{6.6}{21} \frac{6.3}{30} \frac{11.7}{50} \frac{14.2}{58} \frac{15.1}{60}$

FL FL

✓ $\frac{15.5}{35} \frac{7.6}{17} \frac{6.4}{11} \frac{5.7}{10} \frac{5.3}{5.3} \frac{6.0}{10} \frac{6.3}{16} \frac{7.3}{18.20} \frac{6.6}{21} \frac{6.3}{30} \frac{11.7}{50} \frac{14.2}{58} \frac{15.1}{60}$

✓ $\frac{18.2}{60} \frac{18.0}{58} \frac{14.3}{31} \frac{5.4}{16} \frac{5.6}{16} \frac{5.7}{9} \frac{5.6}{5.2} \frac{5.5}{9} \frac{5.7}{10} \frac{6.9}{16} \frac{5.9}{18.20} \frac{6.4}{21} \frac{15.6}{50} \frac{15.3}{58}$

✓ $\frac{20.2}{65} \frac{19.4}{50} \frac{14.3}{32} \frac{4.4}{15} \frac{4.9}{10} \frac{5.0}{9} \frac{5.3}{5.0} \frac{5.2}{9} \frac{5.5}{10} \frac{6.4}{16} \frac{5.3}{18.20} \frac{5.6}{22} \frac{6.1}{27} \frac{15.4}{30} \frac{15.4}{60}$

✓ $\frac{20.2}{65} \frac{18.7}{50} \frac{17.1}{41} \frac{14.8}{33} \frac{5.8}{19} \frac{4.1}{15} \frac{3.9}{10} \frac{4.0}{9} \frac{4.1}{4.1} \frac{4.4}{9} \frac{4.3}{10} \frac{4.4}{16} \frac{5.6}{18.20} \frac{4.4}{22} \frac{4.3}{25} \frac{4.9}{31} \frac{15.3}{63}$

✓ $\frac{18.8}{60} \frac{17.2}{44} \frac{14.9}{33} \frac{5.4}{19} \frac{3.3}{14} \frac{3.2}{10} \frac{3.4}{9} \frac{4}{2.4} \frac{3.6}{9} \frac{3.5}{10} \frac{3.6}{16} \frac{4.5}{18.20} \frac{3.5}{21} \frac{3.3}{24} \frac{4.1}{31} \frac{11.8}{60} \frac{15.3}{77}$

✓ $\frac{17.8}{60} \frac{16.9}{50} \frac{15.5}{39} \frac{8.7}{25} \frac{4.0}{18} \frac{2.6}{13} \frac{2.5}{10} \frac{2.6}{9} \frac{2.5}{2.5} \frac{2.2}{9} \frac{2.6}{10} \frac{2.7}{16} \frac{3.7}{18.20} \frac{2.7}{21} \frac{2.6}{25} \frac{2.7}{30} \frac{7.4}{50}$

✓ $\frac{15.2}{60} \frac{15.1}{43} \frac{12.2}{33} \frac{1.8}{16} \frac{0.7}{10} \frac{0.8}{9} \frac{0.9}{0.9} \frac{1.0}{9} \frac{0.9}{10} \frac{0.9}{16} \frac{1.9}{18.20} \frac{1.0}{21} \frac{0.9}{30} \frac{2.6}{50}$

- $\frac{12.3}{12.3} - \frac{12.0}{12.0} = 11.0$

✓ $\frac{12.4}{60} \frac{12.1}{39} \frac{10.7}{34} + \frac{0.9}{0.9}$

- $\frac{12.3}{12.3} - \frac{12.0}{12.0} = 13.1$

✓ $\frac{9.3}{60} \frac{9.3}{37} + \frac{3.0}{3.0}$

- $\frac{12.1}{12.1} - \frac{11.3}{11.3} = 13.7$

✓ $\frac{8.5}{60} \frac{7.7}{34} + \frac{3.6}{3.6}$

- $\frac{10.6}{10.6} - \frac{10.8}{10.8} = 14.2$

✓ $\frac{6.5}{60} \frac{6.7}{32} + \frac{4.1}{4.1}$

STA	+	π	-	ELEV	
		871.53		(77.0)	
20+00					
T.P.	13.01	883.86	0.68	870.85	
19+00				72.5	
+50				74.6	
+63				75.2	
B.M	10.15	883.86	10.15	873.71	873.71
+73				75.6	
20+00				77.0	
+50				79.6	
21+00				82.1	
T.P.	9.55	893.07	0.34	883.52	
+50				84.6	
22+00				87.1	
+32				88.7	
+50				89.6	

LT 5 2 RT

$$\checkmark \quad \frac{50}{60} \frac{48}{44} \frac{53}{59} \frac{53}{32} + (55)$$

$$\checkmark \quad \frac{11.4}{16} \frac{11.2}{10} \frac{11.4}{9} \frac{11.4}{9} \frac{11.5}{9} \frac{11.3}{10} \frac{11.4}{17} \frac{11.9}{20} \frac{11.4}{26} \frac{11.5}{33} \frac{12.7}{30}$$

$$\checkmark \quad \frac{9.4}{15} \frac{9.2}{10} \frac{9.3}{9} \frac{9.3}{9} \frac{9.2}{10} \frac{9.3}{16} \times \frac{9.2}{21} \frac{9.3}{29} \frac{10.0}{37} \frac{11.1}{46} \frac{13.9}{54}$$

$$\checkmark \quad \frac{8.9}{13} \frac{8.6}{10} \frac{8.8}{9} \frac{8.7}{9} \frac{8.6}{10} \frac{8.5}{16} \times \frac{8.6}{21} \frac{8.7}{29} \frac{10.5}{38} \frac{14.5}{56}$$

$$\checkmark \quad \text{ARC-LITE POLE 15' LT STA 19+50}$$

$$\frac{8.4}{15} \frac{8.1}{10} \frac{8.3}{9} \frac{8.3}{9} \frac{8.3}{10} \frac{8.3}{16} \times \frac{8.4}{21} \frac{8.2}{30} \frac{10.2}{39} \frac{14.4}{57}$$

$$\checkmark \quad \frac{6.9}{15} \frac{6.8}{10} \frac{6.9}{9} \frac{6.9}{9} \frac{6.9}{10} \frac{6.9}{16} \times \frac{6.8}{21} \frac{6.9}{29} \frac{8.9}{39} \frac{12.9}{56} \frac{13.3}{60}$$

$$\checkmark \quad \frac{15.2}{33} \frac{13.7}{40} \frac{12.3}{28} \frac{9.4}{15} \frac{9.3}{10} \frac{9.5}{9} \frac{9.4}{9} \frac{9.3}{10} \frac{9.3}{16} \times \frac{9.3}{21} \frac{9.4}{29} \frac{10.2}{41} \frac{10.8}{56} \frac{10.8}{60}$$

$$\checkmark \quad \frac{7.9}{60} \frac{6.6}{52} \frac{6.6}{44} \frac{6.6}{39} \frac{8.4}{35} \frac{8.4}{31} \frac{11.5}{29} \frac{8.4}{27} \frac{1.9}{15} \frac{1.9}{10} \frac{1.9}{10} \frac{2.0}{16} \frac{2.4}{19} \times \frac{1.7}{22} \frac{1.8}{31} \frac{4.4}{41} \frac{8.3}{58} \frac{8.7}{64}$$

$$\checkmark \quad \frac{8.6}{50} \frac{8.1}{46} \frac{6.4}{43} \frac{13.3}{41} \frac{13.4}{31} \frac{15.6}{26} \frac{8.8}{23} \frac{8.7}{21} \frac{8.5}{15} \frac{8.7}{10} \frac{8.7}{8.5} \frac{8.7}{10} \frac{8.9}{16} \frac{8.9}{18} \times \frac{8.4}{21} \frac{8.4}{30} \frac{14.3}{54} \frac{14.7}{60}$$

$$\checkmark \quad \frac{7.7}{25} \frac{8.8}{20} \frac{6.5}{18} \frac{6.1}{16} \frac{6.0}{10} \frac{6.1}{10} \frac{6.1}{16} \frac{6.3}{18} \times \frac{6.0}{21} \frac{5.9}{30} \frac{9.5}{43} \frac{9.5}{50} \frac{9.0}{60}$$

$$\checkmark \quad \frac{4.4}{24} \frac{5.7}{21} \frac{4.8}{19} \frac{4.5}{18} \frac{4.4}{10} \frac{4.5}{10} \frac{4.5}{16} \frac{4.5}{18} \times \frac{4.3}{22} \frac{4.5}{30} \frac{6.5}{32} \frac{3.6}{34} \frac{2.1}{40} \frac{5.4}{54}$$

$$\checkmark \quad \frac{1.6}{32} \frac{4.4}{25} \frac{3.8}{23} \frac{5.1}{22} \frac{4.1}{20} \frac{3.6}{19} \frac{3.6}{10} \frac{3.7}{10} \frac{3.6}{16} \times \frac{3.2}{22} \frac{3.6}{30} \frac{4.4}{31} \frac{1.2}{33} \frac{0.2}{51} \frac{6.0}{60}$$

STA	+	π	-	ELEV
		893.07		
22+73				90.9
T.P	12.10	904.24	0.93	892.14
22+00				87.1
+32				88.7
+50				89.2
+73				90.9
+80				91.1
23+00				92.1
+50				94.7
24+00				97.1
+50				99.5
25+00				102.1
+10				102.6

LT

A

PT

✓

$$\frac{3.7}{22-20} \frac{2.4}{19} \frac{2.0}{10} \frac{2.2}{2.2} \frac{2.3}{10} \frac{2.4}{16} \frac{2.5}{18} \times \frac{2.2}{22} \frac{2.3}{30} \frac{3.1}{32-34} \frac{1.0}{40} \frac{0.2}{50} \frac{1.0}{60}$$

✓

$$\begin{array}{ccc} \textcircled{+8.2} & \textcircled{+7.9} & \textcircled{+8.4} \\ \frac{8.9}{60} & \frac{9.2}{52} & \frac{8.7}{42} \end{array} \quad \textcircled{17.1}$$

✓

$$\begin{array}{ccc} \textcircled{+5.5} & \textcircled{+6.2} & \textcircled{+5.9} \\ \frac{10.0}{60} & \frac{9.3}{42} \frac{9.6}{40} & \frac{9.9}{34} \end{array} \quad \begin{array}{ccc} \textcircled{+5.6} & \textcircled{+4.4} & \\ \frac{11.1}{30} & & \end{array} \quad \textcircled{15.5}$$

✓

$$\begin{array}{ccc} \textcircled{+3.3} & \textcircled{+3.7} & \\ \frac{11.3}{60} & \frac{10.9}{45} & \end{array} \quad \textcircled{14.6}$$

✓

$$\begin{array}{ccc} \textcircled{+11.8} & \textcircled{+2.3} & \textcircled{+1.2} \\ \frac{11.5}{62} \frac{11.0}{58} & \frac{12.1}{50} & \frac{12.8}{31} \end{array} \quad \textcircled{13.3}$$

$$\frac{11.2}{60} \frac{11.4}{50} \frac{10.5}{28} \frac{13.5}{24} \frac{14.9}{23-21} \frac{13.6}{20} \frac{13.2}{10} \frac{13.2}{10} \frac{13.3}{16} \frac{13.4}{18} \times \frac{13.2}{22} \frac{13.1}{30} \frac{13.9}{32-34} \frac{11.8}{40} \frac{11.9}{50} \frac{12.1}{60}$$

$$\frac{9.8}{60-50} \frac{8.7}{35} \frac{8.5}{28} \frac{12.3}{24} \frac{13.4}{23-21} \frac{12.6}{20} \frac{12.2}{10} \frac{12.1}{10} \frac{12.2}{10} \frac{12.2}{16} \frac{12.3}{18} \times \frac{11.9}{22} \frac{11.8}{29} \frac{12.5}{30} \frac{11.7}{40} \frac{9.8}{50} \frac{8.9}{60}$$

✓

$$\frac{6.6}{60} \frac{5.9}{50} \frac{4.7}{31} \frac{9.5}{23} \frac{11.0}{22-20} \frac{9.8}{19} \frac{9.5}{10} \frac{9.5}{10} \frac{9.5}{16} \frac{9.7}{18} \times \frac{9.3}{22} \frac{9.0}{30} \frac{10.1}{32-34} \frac{9.2}{35} \frac{7.1}{50} \frac{6.7}{60}$$

✓

$$\frac{4.6}{60} \frac{4.0}{50} \frac{0.5}{35} \frac{6.7}{24} \frac{8.9}{23-21} \frac{7.5}{19} \frac{7.1}{10} \frac{7.0}{10} \frac{7.1}{16} \frac{7.2}{18} \times \frac{6.9}{22} \frac{6.5}{30} \frac{7.1}{32-34} \frac{6.6}{35} \frac{5.0}{50} \frac{4.0}{60}$$

✓

$$\frac{4.6}{37} \frac{0.0}{33} \frac{4.4}{23} \frac{5.8}{22-21} \frac{4.9}{19} \frac{4.4}{10} \frac{4.4}{10} \frac{4.4}{16} \frac{4.8}{18} \times \frac{4.4}{22} \frac{4.2}{29} \frac{4.8}{31-32} \frac{4.4}{33} \frac{1.7}{50} \frac{1.1}{60}$$

✓

$$\frac{0.0}{27} \frac{1.8}{23} \frac{3.5}{22-20} \frac{2.3}{18} \frac{1.9}{10} \frac{1.9}{10} \frac{2.4}{16} \frac{2.4}{18} \times \frac{2.0}{22} \frac{1.4}{29} \frac{1.9}{32-33} \frac{1.0}{36} \frac{0.0}{47} \frac{1.0}{60}$$

✓

$$\frac{0.9}{23} \frac{3.1}{22-20} \frac{1.8}{18} \frac{1.3}{10} \frac{1.3}{10} \frac{1.7}{16} \frac{1.8}{18} \times \frac{1.4}{21} \frac{1.0}{30} \frac{1.4}{32-33} \frac{0.5}{35}$$

STA	+	π	-	ELEV
		904.24.		
25+16				02.9
+21				03.2
T.P	11.72	914.61.	1.35	902.89.
24+50				(99.5)
25+00				02.1
+10				(02.6)
+16				(02.9)
+21				(03.2)
+27				03.4
+50				04.6
26+00				07.1
+08				07.5
+15				07.9

LT

E

RT

✓

$$\frac{3.1}{22.21} \quad \frac{1.2}{17} \quad \frac{0.9}{10} \quad \frac{1.3}{10} \quad \frac{1.0}{16} \quad \frac{1.4}{16} \quad \frac{1.5}{18} \times \frac{1.1}{21} \quad \frac{1.0}{22} \quad \frac{0.4}{24} \quad \frac{0.4}{36}$$

✓

$$\frac{0.6}{18} \quad \frac{0.5}{10} \quad 1.0 \quad \frac{0.8}{10} \quad \frac{1.2}{16} \quad \frac{1.2}{18} \times \frac{0.9}{21} \quad \frac{0.5}{30} \quad \frac{0.7}{32} \quad \frac{0.0}{37}$$

✓

$$\frac{7.9}{60} \quad \frac{6.6}{50} \quad \frac{5.7}{41} \quad (15.1)$$

✓

$$\frac{7.0}{60} \quad \frac{0.0}{50} \quad \frac{0.4}{45} \quad \frac{7.6}{35} \quad (12.5) \quad \frac{10.0}{50} \quad \frac{9.0}{60}$$

✓

$$\frac{0.5}{60} \quad \frac{0.5}{50} \quad \frac{5.4}{37} \quad \frac{9.6}{30} \quad (12.0) \quad \frac{9.6}{50} \quad \frac{8.3}{60}$$

✓

$$\frac{4.3}{60} \quad \frac{5.5}{50} \quad \frac{5.8}{30} \quad (11.7) \quad \frac{11.2}{30} \quad \frac{11.6}{31-33} \quad \frac{10.2}{39} \quad \frac{9.2}{50} \quad \frac{8.1}{60}$$

✓

$$\frac{5.6}{60} \quad \frac{5.5}{50} \quad \frac{8.8}{24} \quad \frac{12.4}{23} \quad (11.4) \quad \frac{9.6}{41} \quad \frac{8.4}{53} \quad \frac{7.6}{60}$$

✓

$$\frac{1.2}{60} \quad \frac{2.8}{50} \quad \frac{6.0}{35} \quad \frac{10.5}{23} \quad \frac{12.4}{23-21} \quad \frac{11.1}{19} \quad \frac{10.9}{16} \quad \frac{11.1}{10} \quad \frac{11.1}{16} \quad \frac{11.4}{18} \times \frac{11.0}{22} \quad \frac{10.5}{29} \quad \frac{4.0}{31-33} \quad \frac{8.4}{40} \quad \frac{8.7}{50} \quad \frac{7.5}{60}$$

✓

$$\frac{1.0}{60} \quad \frac{2.2}{50} \quad \frac{9.9}{25} \quad \frac{10.1}{24} \quad \frac{11.0}{23-21} \quad \frac{10.3}{20} \quad \frac{9.8}{10} \quad \frac{10.0}{10} \quad \frac{9.8}{10} \quad \frac{9.9}{16} \quad \frac{10.2}{18} \times \frac{9.7}{22} \quad \frac{9.4}{30} \quad \frac{9.8}{31-33} \quad \frac{8.5}{40} \quad \frac{7.2}{50} \quad \frac{6.5}{60}$$

✓

$$\frac{2.5}{60} \quad \frac{2.8}{50} \quad \frac{4.4}{37} \quad \frac{6.6}{28} \quad \frac{7.8}{28} \quad \frac{8.9}{24-22} \quad \frac{7.6}{20} \quad \frac{7.4}{10} \quad \frac{7.5}{10} \quad \frac{7.3}{10} \quad \frac{7.4}{19} \quad \frac{8.4}{21-24} \quad \frac{6.9}{26} \quad \frac{6.5}{36} \quad \frac{5.0}{50} \quad \frac{4.2}{60}$$

✓

$$\frac{6.0}{60} \quad \frac{6.3}{50} \quad \frac{6.9}{36} \quad \frac{8.0}{26} \quad \frac{8.6}{25-23} \quad \frac{7.2}{21} \quad \frac{7.0}{10} \quad \frac{7.1}{10} \quad \frac{6.9}{10} \quad \frac{6.7}{22} \quad \frac{6.4}{32} \quad \frac{7.0}{34} \quad \frac{6.0}{50} \quad \frac{6.1}{60}$$

✓

$$\frac{5.5}{60} \quad \frac{5.2}{50} \quad \frac{6.0}{33} \quad \frac{6.4}{24} \quad \frac{6.6}{10} \quad \frac{6.7}{10} \quad \frac{6.6}{10} \quad \frac{5.7}{22} \quad \frac{5.0}{50} \quad \frac{4.6}{60}$$

STA	+	π	-	ELEV
		914.61.		
26+28		$\frac{1}{2}$ Co. RD A. v		08.5
B.M	5.53	914.59.	5.53	909.08. 909.06.
+43				09.3
+48				09.6
+50				09.7
+63				10.3
+71				10.7
27+00				12.2
T.P	9.88	924.12.	0.35	914.24.
26+63				(10.3)
+71				(10.7)
27+00				(12.2)
+50				14.5
28+00				16.2

LT

±

RT

✓ $\frac{3.9}{100} \frac{5.0}{50} \frac{5.6}{26} \frac{5.9}{10} \frac{6.08}{10} \frac{5.9}{10} \frac{5.3}{33} \frac{4.3}{50} \frac{2.3}{101}$

P.P. S.W. COR H.2 + ^{Edgerton} ~~ARPEMENTE~~

✓ $\frac{4.7}{60} \frac{5.0}{50} \frac{5.4}{41} \frac{5.3}{32} \frac{5.2}{10} \frac{5.3}{10} \frac{5.2}{10} \frac{4.6}{23} \frac{4.7}{41} \frac{4.2}{50} \frac{4.2}{60}$

✓ $\frac{6.0}{60} \frac{6.1}{50} \frac{6.4}{41} \frac{4.7}{40} \frac{5.2}{23} \frac{4.9}{10} \frac{4.9}{50} \frac{5.4}{10} \frac{6.6}{20} \frac{5.5}{22} \frac{1.8}{24} \frac{1.3}{25} \frac{0.9}{33} \frac{0.9}{50} \frac{0.9}{60}$

✓ $\frac{5.8}{60} \frac{5.9}{50} \frac{5.9}{41} \frac{5.0}{39} \frac{5.0}{22} \frac{4.8}{10} \frac{4.9}{10} \frac{4.8}{10} \frac{5.1}{21} \frac{6.5}{22} \frac{2.5}{24} \frac{0.6}{27} \frac{0.6}{50} \frac{0.6}{60}$

✓ $\frac{0.3}{60} \frac{1.2}{50} \frac{4.4}{37} \frac{4.6}{21} \frac{4.2}{10} \frac{4.3}{10} \frac{4.1}{10} \frac{4.0}{17} \frac{5.6}{19} \frac{1.1}{21} \frac{0.0}{29} \frac{0.0}{34}$

✓ $\frac{0.5}{46} \frac{4.6}{28} \frac{5.9}{25} \frac{4.0}{22} \frac{3.8}{17} \frac{3.7}{10} \frac{3.9}{10} \frac{3.7}{10} \frac{3.9}{17} \frac{5.4}{19} \frac{6.4}{21} \frac{0.5}{27} \frac{0.5}{32}$

✓ $\frac{2.2}{28} \frac{4.3}{25} \frac{2.3}{22} \frac{2.3}{17} \frac{2.3}{10} \frac{2.3}{24} \frac{2.3}{10} \frac{2.3}{16} \frac{4.0}{18} \frac{4.0}{21}$

✓ $\frac{0.2}{13.8} \frac{4.6}{50} \frac{1.2}{60}$

✓ $\frac{0.2}{61} \frac{0.2}{58} \frac{1.2}{13.4} \frac{1.2}{50} \frac{1.2}{60}$

✓ $\frac{0.2}{4.8} \frac{0.2}{5.1} \frac{0.2}{11.9} \frac{1.5}{43} \frac{1.5}{52} \frac{1.5}{60}$

✓ $\frac{2.6}{60} \frac{2.7}{50} \frac{10.1}{28} \frac{11.6}{25} \frac{9.7}{22} \frac{9.6}{16} \frac{9.6}{10} \frac{9.6}{10} \frac{9.6}{15} \frac{10.8}{17} \frac{1.9}{19} \frac{0.7}{26} \frac{0.7}{42} \frac{0.7}{55}$

✓ $\frac{0.0}{60} \frac{0.8}{50} \frac{3.2}{31} \frac{2.9}{21} \frac{8.0}{18} \frac{7.9}{14} \frac{7.9}{10} \frac{7.9}{19} \frac{8.0}{10} \frac{7.9}{15} \frac{9.8}{22} \frac{8.6}{25} \frac{1.8}{28} \frac{1.8}{50} \frac{1.8}{60}$

STA	+	π	-	ELEV
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		924.12		
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28+50				174
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29+00				18.1
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T.P.	6.11	929.48	0.75	923.37
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+15				18.2
-----	--	--	--	------

+19				18.3
-----	--	--	--	------

+50				18.5
-----	--	--	--	------

+55				18.5
-----	--	--	--	------

+66				18.6
-----	--	--	--	------

+71				18.7
-----	--	--	--	------

+80				18.7
-----	--	--	--	------

+87				18.8
-----	--	--	--	------

30+00				18.9
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+50				19.2
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LT

E

RT

$$\checkmark \quad \frac{1.5}{60-50} \quad \frac{7.7}{28} \quad \frac{8.7}{25-27} \quad \frac{6.9}{16} \quad \frac{6.7}{10} \quad \frac{6.7}{10} \quad \frac{6.7}{10} \quad \frac{6.8}{13} \quad \frac{8.7}{17-19} \quad \frac{2.4}{30} \quad \frac{1.9}{50} \quad \frac{0.0}{60}$$

$$\checkmark \quad \frac{1.6}{60-50} \quad \frac{7.1}{28} \quad \frac{8.0}{24-21} \quad \frac{6.0}{15} \quad \frac{6.0}{10} \quad \frac{6.0}{60} \quad \frac{6.0}{10} \quad \frac{6.0}{14} \quad \frac{7.9}{19-21} \quad \frac{2.0}{30} \quad \frac{0.7}{50} \quad \frac{0.0}{53} \quad \frac{0.0}{60}$$

$$\checkmark \quad \frac{7.2}{60-52} \quad \frac{12.4}{30} \quad \frac{6.0}{24-21} \quad \frac{11.2}{15} \quad \frac{11.2}{10} \quad \frac{11.2}{10} \quad \frac{11.2}{10} \quad \frac{11.2}{13} \quad \frac{12.9}{18-20} \quad \frac{7.8}{29} \quad \frac{6.4}{30} \quad \frac{3.3}{60}$$

$$\checkmark \quad \frac{3.9}{60-50} \quad \frac{3.9}{30} \quad \frac{13.0}{23-21} \quad \frac{11.3}{15} \quad \frac{11.1}{10} \quad \frac{11.2}{10} \quad \frac{11.2}{10} \quad \frac{11.2}{14} \quad \frac{12.8}{18-20} \quad \frac{7.6}{28} \quad \frac{6.5}{52} \quad \frac{3.2}{60}$$

$$\checkmark \quad \frac{3.7}{60-50} \quad \frac{3.8}{38} \quad \frac{12.6}{24} \quad \frac{12.3}{18} \quad \frac{11.0}{15} \quad \frac{10.9}{10} \quad \frac{11.0}{10} \quad \frac{11.0}{10} \quad \frac{12.0}{17} \quad \frac{8.4}{19-21} \quad \frac{6.6}{29} \quad \frac{5.9}{35} \quad \frac{3.0}{52} \quad \frac{3.0}{60}$$

$$\checkmark \quad \frac{3.6}{60-50} \quad \frac{3.6}{38} \quad \frac{12.5}{24-18} \quad \frac{10.8}{14} \quad \frac{10.9}{10} \quad \frac{11.0}{10} \quad \frac{10.9}{10} \quad \frac{11.0}{18} \quad \frac{12.1}{20-22} \quad \frac{3.7}{36} \quad \frac{3.5}{50-60}$$

$$\checkmark \quad \frac{3.6}{60-50} \quad \frac{3.6}{38} \quad \frac{12.5}{24-18} \quad \frac{12.1}{17} \quad \frac{10.9}{15} \quad \frac{10.8}{10} \quad \frac{10.9}{10} \quad \frac{10.9}{10} \quad \frac{10.9}{18} \quad \frac{12-1}{20-22} \quad \frac{9.8}{24} \quad \frac{4.2}{37} \quad \frac{3.0}{50-60}$$

$$\checkmark \quad \frac{3.6}{60-50} \quad \frac{3.6}{38} \quad \frac{12.3}{24} \quad \frac{12.0}{17} \quad \frac{10.8}{15} \quad \frac{10.8}{10} \quad \frac{10.8}{10} \quad \frac{10.8}{10} \quad \frac{12-1}{20-22} \quad \frac{9.7}{26} \quad \frac{8.0}{50} \quad \frac{7.0}{60}$$

$$\checkmark \quad \frac{3.6}{60-50} \quad \frac{3.6}{38} \quad \frac{12.0}{24} \quad \frac{12.0}{17} \quad \frac{10.9}{15} \quad \frac{10.7}{10} \quad \frac{10.7}{10} \quad \frac{10.7}{10} \quad \frac{10.7}{18} \quad \frac{13.2}{23-25} \quad \frac{10.1}{26} \quad \frac{8.0}{50} \quad \frac{7.0}{60}$$

$$\checkmark \quad \frac{3.5}{60-50} \quad \frac{3.5}{38} \quad \frac{11.8}{24} \quad \frac{11.9}{17} \quad \frac{10.7}{14} \quad \frac{10.6}{10} \quad \frac{10.7}{10} \quad \frac{10.7}{10} \quad \frac{13.2}{19} \quad \frac{8.7}{23-25} \quad \frac{7.0}{30} \quad \frac{3.6}{38} \quad \frac{3.4}{44} \quad \frac{3.0}{50-60}$$

$$\checkmark \quad \frac{3.2}{50} \quad \frac{3.2}{38} \quad \frac{12.0}{24} \quad \frac{11.9}{18} \quad \frac{10.7}{15} \quad \frac{10.6}{10} \quad \frac{10.6}{10} \quad \frac{10.6}{10} \quad \frac{10.6}{10} \quad \frac{10.5}{17} \quad \frac{12.0}{21-25} \quad \frac{10.7}{26} \quad \frac{4.4}{38} \quad \frac{3.0}{50-60}$$

$$\checkmark \quad \frac{3.0}{50-38} \quad \frac{11.5}{25} \quad \frac{11.4}{18} \quad \frac{10.5}{15} \quad \frac{10.3}{10} \quad \frac{10.3}{10} \quad \frac{10.3}{10} \quad \frac{10.4}{15} \quad \frac{11.3}{18} \quad \frac{11.4}{26} \quad \frac{3.6}{38} \quad \frac{3.0}{45} \quad \frac{2.0}{50-60}$$

STA	+	π	-	ELEV.
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929.48.

30+90				195
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31+00				196
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+18				197
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+24				198
-----	--	--	--	-----

+50				199
-----	--	--	--	-----

32+00				203
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+50				206
-----	--	--	--	-----

+61				207
-----	--	--	--	-----

+69				207
-----	--	--	--	-----

+75				208
-----	--	--	--	-----

33+00				209
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+04				209
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LT

F

RT

$$\checkmark \quad \frac{2.4}{60-50} \quad \frac{2.6}{38} \quad \frac{11.2}{25} \quad \frac{10.3}{19} \quad \frac{10.0}{14} \quad \frac{10.0}{10} \quad \frac{10.0}{10} \quad \frac{10.1}{14} \quad \frac{11.1}{21} \quad \frac{10.3}{22} \quad \frac{2.6}{28} \quad \frac{1.0}{39} \quad \frac{1.0}{50-60}$$

$$\checkmark \quad \frac{2.4}{60} \quad \frac{2.6}{50} \quad \frac{10.4}{38} \quad \frac{10.2}{25} \quad \frac{10.0}{18} \quad \frac{9.9}{16} \quad \frac{9.9}{10} \quad \frac{10.0}{15} \quad \frac{11.0}{22} \quad \frac{10.0}{23} \quad \frac{9.3}{26} \quad \frac{7.8}{36} \quad \frac{7.2}{52} \quad \frac{7.2}{60}$$

$$\checkmark \quad \frac{2.3}{60-50} \quad \frac{2.6}{28} \quad \frac{10.6}{23} \quad \frac{10.1}{18} \quad \frac{9.9}{16} \quad \frac{9.9}{10} \quad \frac{9.8}{10} \quad \frac{9.7}{15} \quad \frac{10.6}{21} \quad \frac{10.0}{23} \quad \frac{9.3}{25} \quad \frac{8.0}{32} \quad \frac{7.4}{50} \quad \frac{7.4}{60}$$

$$\checkmark \quad \frac{3.1}{60-50} \quad \frac{5.9}{35} \quad \frac{10.6}{22} \quad \frac{10.1}{18} \quad \frac{9.9}{16} \quad \frac{9.9}{10} \quad \frac{9.8}{11} \quad \frac{9.9}{15} \quad \frac{10.6}{21} \quad \frac{10.0}{23} \quad \frac{9.8}{25} \quad \frac{5.1}{30} \quad \frac{4.8}{41} \quad \frac{4.6}{50} \quad \frac{4.6}{60}$$

$$\checkmark \quad \frac{3.2}{60-50} \quad \frac{6.2}{34} \quad \frac{10.3}{23} \quad \frac{9.8}{18} \quad \frac{9.6}{15} \quad \frac{9.6}{10} \quad \frac{9.6}{10} \quad \frac{9.7}{15} \quad \frac{10.5}{22} \quad \frac{9.7}{25} \quad \frac{4.9}{30} \quad \frac{4.7}{41} \quad \frac{4.7}{50} \quad \frac{4.7}{60}$$

$$\checkmark \quad \frac{2.9}{60} \quad \frac{3.4}{50} \quad \frac{6.4}{35} \quad \frac{7.8}{33} \quad \frac{9.9}{31} \quad \frac{9.3}{22} \quad \frac{9.3}{19} \quad \frac{9.2}{15} \quad \frac{9.2}{10} \quad \frac{9.3}{15} \quad \frac{9.8}{22} \quad \frac{9.2}{25} \quad \frac{5.0}{30} \quad \frac{4.5}{41} \quad \frac{4.2}{50} \quad \frac{4.2}{60}$$

$$\checkmark \quad \frac{3.3}{60} \quad \frac{3.8}{50} \quad \frac{5.9}{36} \quad \frac{7.1}{35} \quad \frac{9.3}{33} \quad \frac{8.8}{27} \quad \frac{8.9}{21} \quad \frac{8.9}{17} \quad \frac{8.9}{10} \quad \frac{8.9}{89} \quad \frac{8.7}{10} \quad \frac{8.4}{18} \quad \frac{5.2}{33} \quad \frac{3.9}{38} \quad \frac{3.9}{50-60}$$

$$\checkmark \quad \frac{4.8}{60} \quad \frac{4.3}{50} \quad \frac{6.3}{36} \quad \frac{7.1}{35} \quad \frac{7.4}{33} \quad \frac{8.6}{29} \quad \frac{8.8}{17} \quad \frac{8.9}{10} \quad \frac{8.8}{88} \quad \frac{8.9}{10} \quad \frac{8.6}{17} \quad \frac{7.9}{30} \quad \frac{7.3}{50} \quad \frac{6.8}{60}$$

$$\checkmark \quad \frac{7.1}{60} \quad \frac{7.8}{50} \quad \frac{8.3}{34} \quad \frac{8.5}{18} \quad \frac{8.8}{10} \quad \frac{8.8}{8.8} \quad \frac{8.8}{10} \quad \frac{8.6}{16} \quad \frac{7.7}{32} \quad \frac{7.0}{50} \quad \frac{6.3}{60}$$

$$\checkmark \quad \frac{7.1}{60} \quad \frac{7.8}{50} \quad \frac{8.3}{34} \quad \frac{8.5}{18} \quad \frac{8.8}{10} \quad \frac{8.8}{8.8} \quad \frac{8.8}{10} \quad \frac{8.6}{16} \quad \frac{7.7}{32} \quad \frac{7.0}{50} \quad \frac{6.3}{60}$$

$$\checkmark \quad \frac{7.0}{60} \quad \frac{7.2}{50} \quad \frac{8.5}{30} \quad \frac{8.5}{18} \quad \frac{8.6}{10} \quad \frac{8.6}{8.6} \quad \frac{8.6}{10} \quad \frac{8.7}{14} \quad \frac{10.0}{20} \quad \frac{8.4}{21} \quad \frac{3.6}{29} \quad \frac{2.6}{37} \quad \frac{2.5}{45} \quad \frac{2.5}{50-60}$$

$$\checkmark \quad \frac{7.3}{60-50} \quad \frac{8.3}{30} \quad \frac{8.6}{17} \quad \frac{8.6}{10} \quad \frac{8.6}{8.6} \quad \frac{8.7}{10} \quad \frac{10.0}{14} \quad \frac{8.2}{21} \quad \frac{3.4}{29} \quad \frac{2.4}{40} \quad \frac{2.4}{50-60}$$

STA	+	+	-	ELEV
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929.48.

33+06

20.9

+29

21.1

+36

21.1

+46

21.1

+54

21.3

T.P.

9.05

933.76.

4.77

924.71.

34+00

21.7

+50

22.1

35+00

22.6

+50

23.0

36+00

23.3

+13

23.4

+15

23.3

LT

Z

RT

$$\checkmark \quad \frac{4.7}{60-50} \quad \frac{4.9}{31} \quad \frac{8.3}{30} \quad \frac{8.6}{17} \quad \frac{8.6}{16} \quad \frac{8.6}{8.6} \quad \frac{8.7}{11} \quad \frac{10.0}{21-23} \quad \frac{8.2}{29} \quad \frac{3.4}{40} \quad \frac{2.4}{50-60}$$

$$\checkmark \quad \frac{3.1}{60-50} \quad \frac{3.5}{38} \quad \frac{4.8}{21} \quad \frac{8.1}{30} \quad \frac{8.7}{19} \quad \frac{8.5}{15} \quad \frac{8.4}{10} \quad \frac{8.4}{10} \quad \frac{8.6}{14} \quad \frac{9.4}{20-22} \quad \frac{8.6}{29} \quad \frac{2.4}{44} \quad \frac{1.3}{50-60}$$

$$\checkmark \quad \frac{3.1}{60-50} \quad \frac{3.5}{38} \quad \frac{4.8}{31} \quad \frac{8.1}{30} \quad \frac{8.7}{19} \quad \frac{8.5}{15} \quad \frac{8.4}{16} \quad \frac{8.4}{10} \quad \frac{8.6}{15} \quad \frac{9.4}{20-22} \quad \frac{8.8}{27} \quad \frac{8.4}{31} \quad \frac{4.5}{50} \quad \frac{5.6}{60}$$

$$\checkmark \quad \frac{2.6}{60-50} \quad \frac{2.8}{40} \quad \frac{4.6}{31} \quad \frac{8.4}{30} \quad \frac{8.7}{19} \quad \frac{8.5}{15} \quad \frac{8.4}{10} \quad \frac{8.4}{10} \quad \frac{8.6}{15} \quad \frac{9.5}{20-22} \quad \frac{8.8}{27} \quad \frac{8.4}{31} \quad \frac{6.5}{50} \quad \frac{5.6}{60}$$

$$\checkmark \quad \frac{2.6}{60-50} \quad \frac{2.8}{40} \quad \frac{4.6}{31} \quad \frac{8.4}{30} \quad \frac{8.7}{19} \quad \frac{8.5}{15} \quad \frac{8.3}{10} \quad \frac{8.2}{8.2} \quad \frac{8.2}{10} \quad \frac{9.2}{14} \quad \frac{9.0}{20-22} \quad \frac{2.7}{28} \quad \frac{1.7}{38} \quad \frac{1.7}{50-60}$$

$$\checkmark \quad \frac{6.5}{60-50} \quad \frac{6.9}{39} \quad \frac{8.5}{31} \quad \frac{12.3}{30} \quad \frac{12.6}{22} \quad \frac{12.4}{16} \quad \frac{12.1}{10} \quad \frac{12.1}{12.1} \quad \frac{12.2}{10} \quad \frac{12.3}{15} \quad \frac{13.7}{18-21} \quad \frac{12.8}{24} \quad \frac{12.8}{28} \quad \frac{6.9}{36} \quad \frac{6.8}{50-60}$$

$$\checkmark \quad \frac{6.4}{60-50} \quad \frac{6.8}{39} \quad \frac{8.3}{31} \quad \frac{11.7}{30} \quad \frac{12.0}{21} \quad \frac{11.9}{15} \quad \frac{11.7}{10} \quad \frac{11.7}{11.7} \quad \frac{11.8}{10} \quad \frac{12.2}{15} \quad \frac{13.5}{18-21} \quad \frac{12.4}{25} \quad \frac{12.3}{29} \quad \frac{6.8}{36} \quad \frac{6.7}{50-60}$$

$$\checkmark \quad \frac{6.4}{60-50} \quad \frac{6.9}{32} \quad \frac{10.7}{26} \quad \frac{11.7}{23} \quad \frac{11.3}{21} \quad \frac{11.2}{16} \quad \frac{11.2}{10} \quad \frac{11.3}{10} \quad \frac{11.6}{15} \quad \frac{12.4}{18-21} \quad \frac{11.6}{24} \quad \frac{6.6}{37} \quad \frac{6.5}{50-60}$$

$$\checkmark \quad \frac{5.4}{60-50} \quad \frac{6.3}{32} \quad \frac{12.0}{20-24} \quad \frac{10.6}{15} \quad \frac{10.8}{10} \quad \frac{10.8}{10.8} \quad \frac{10.9}{10} \quad \frac{11.8}{19-21} \quad \frac{11.2}{24} \quad \frac{10.7}{33} \quad \frac{8.0}{34} \quad \frac{6.6}{40} \quad \frac{6.2}{50-60}$$

$$\checkmark \quad \frac{4.7}{60-50} \quad \frac{4.8}{40} \quad \frac{6.2}{30} \quad \frac{11.3}{23} \quad \frac{12.0}{18-21} \quad \frac{10.6}{14} \quad \frac{10.6}{10} \quad \frac{10.5}{10.5} \quad \frac{10.5}{10} \quad \frac{10.6}{15} \quad \frac{10.9}{19-21} \quad \frac{10.4}{33} \quad \frac{7.5}{34} \quad \frac{6.9}{36} \quad \frac{6.2}{50-60}$$

$$\checkmark \quad \frac{5.4}{60-50} \quad \frac{5.8}{34} \quad \frac{7.2}{30} \quad \frac{12.1}{19} \quad \frac{10.7}{15} \quad \frac{10.5}{10} \quad \frac{10.4}{10.4} \quad \frac{10.5}{10} \quad \frac{10.1}{33} \quad \frac{7.5}{34} \quad \frac{7.0}{50} \quad \frac{6.7}{60}$$

$$\checkmark \quad \frac{5.4}{60-50} \quad \frac{5.8}{34} \quad \frac{7.2}{30} \quad \frac{12.1}{19} \quad \frac{10.7}{15} \quad \frac{10.5}{10} \quad \frac{10.5}{10.5} \quad \frac{10.5}{10} \quad \frac{10.3}{21} \quad \frac{10.2}{23} \quad \frac{9.4}{50} \quad \frac{8.9}{60}$$

STA	+	π	-	ELEV
		933.76		
36+27				23.3
B.M	8.24	931.53	10.47	923.29
+38				23.4
37+00				23.4
+50				23.3
38+00				22.9
+50				22.4
39+00				21.7
+40				21.0
+47				20.9
+59				20.7
+77				20.2
+88				20.0

LT

Z

RT

✓ $\frac{5.4}{60-50} \frac{6.2}{34} \frac{7.2}{30} \frac{12.1}{19} \frac{10.7}{15} \frac{10.5}{10} \frac{10.5}{10.5} \frac{10.2}{10} \frac{7.4}{21} \frac{8.9}{33} \frac{8.9}{30} \frac{8.9}{60}$

S.W. COR LOWER CONC STP RT STA 35+00

✓ $\frac{3.6}{60-50} \frac{3.9}{34} \frac{8.7}{25} \frac{9.2}{21} \frac{8.4}{18} \frac{8.1}{16} \frac{8.1}{10} \frac{8.1}{10} \frac{8.3}{14} \frac{8.9}{19} \frac{6.2}{23} \frac{1.4}{29} \frac{1.3}{44} \frac{1.3}{58} \frac{1.3}{60}$

✓ $\frac{3.0}{60-50} \frac{3.4}{32} \frac{8.4}{24} \frac{9.5}{21} \frac{8.2}{18} \frac{8.2}{15} \frac{8.1}{10} \frac{8.2}{10} \frac{8.2}{15} \frac{8.2}{20} \frac{7.8}{24} \frac{2.4}{30} \frac{2.8}{39} \frac{2.8}{50} \frac{2.8}{60}$

✓ $\frac{2.4}{60-50} \frac{1.2}{35} \frac{2.2}{33} \frac{3.7}{29} \frac{8.3}{23} \frac{9.2}{20} \frac{8.2}{18} \frac{8.2}{10} \frac{8.2}{10} \frac{8.4}{15} \frac{10.2}{20} \frac{9.0}{22} \frac{1.6}{29} \frac{2.0}{37} \frac{2.0}{50} \frac{2.0}{60}$

✓ $\frac{7.04}{60-50} \frac{0.7}{35} \frac{3.2}{29} \frac{4.0}{27} \frac{8.4}{18} \frac{6.5}{14} \frac{8.6}{10} \frac{8.6}{10} \frac{8.6}{10} \frac{8.6}{15} \frac{8.6}{20} \frac{10.5}{22} \frac{10.1}{29} \frac{3.1}{37} \frac{4.2}{50} \frac{5.0}{60}$

✓ $\frac{0.0}{60-50} \frac{0.6}{37} \frac{1.2}{30} \frac{4.0}{27} \frac{4.6}{27} \frac{8.7}{19} \frac{8.8}{15} \frac{9.1}{10} \frac{9.1}{10} \frac{9.3}{15} \frac{10.7}{22} \frac{7.2}{26} \frac{9.3}{32} \frac{11.0}{50} \frac{11.0}{60}$

✓ $\frac{0.9}{60-50} \frac{1.4}{50} \frac{1.8}{39} \frac{5.2}{32} \frac{5.5}{29} \frac{9.7}{21} \frac{9.6}{17} \frac{9.8}{15} \frac{9.8}{10} \frac{9.8}{10} \frac{9.8}{10} \frac{9.8}{15} \frac{11.7}{20} \frac{12.4}{24} \frac{11.5}{27} \frac{14.0}{31} \frac{15.8}{50} \frac{15.8}{60}$

✓ $\frac{1.6}{60-50} \frac{2.0}{50} \frac{3.0}{42} \frac{5.7}{36} \frac{6.2}{30} \frac{9.9}{22} \frac{10.2}{19} \frac{10.5}{14} \frac{10.5}{10} \frac{10.5}{10} \frac{10.6}{14} \frac{12.5}{19} \frac{13.0}{31} \frac{14.8}{45} \frac{14.7}{50} \frac{14.7}{60}$

✓ $\frac{1.9}{60-50} \frac{2.4}{50} \frac{2.8}{41} \frac{5.9}{33} \frac{6.2}{31} \frac{9.7}{23} \frac{10.4}{13} \frac{10.6}{10} \frac{10.7}{10} \frac{10.9}{15} \frac{12.0}{20} \frac{12.4}{27} \frac{13.5}{34}$

✓ $\frac{7.0}{60-50} \frac{7.5}{50} \frac{9.5}{30} \frac{10.2}{17} \frac{10.3}{14} \frac{10.8}{10} \frac{10.8}{10} \frac{10.9}{10} \frac{11.0}{15} \frac{11.6}{19} \frac{16.3}{33}$

✓ $\frac{2.0}{60-50} \frac{7.9}{50} \frac{8.9}{37} \frac{10.4}{24} \frac{10.9}{15} \frac{11.3}{10} \frac{11.3}{10} \frac{11.4}{10} \frac{11.5}{14} \frac{11.9}{18} \frac{13.1}{21} \frac{17.8}{28} \frac{17.8}{33}$

✓ $\frac{2.2}{60-50} \frac{2.7}{50} \frac{3.5}{44} \frac{5.7}{38} \frac{7.8}{32} \frac{10.4}{26} \frac{11.3}{14} \frac{11.5}{10} \frac{11.5}{10} \frac{11.6}{15} \frac{11.8}{14} \frac{13.1}{20} \frac{14.8}{25}$

STA	+	π	-	ELEV
		931.53		
40+00				197
+50				184
41+00				172
+50				159
42+00				146
+50				133
43+00				120
+22				115
T.P.	0.72	919.38	12.87	918.66
39+47				20.9
+59				20.7
+77				20.2
+88				20.0

LT

♀

♂

$$\begin{array}{r} \checkmark \quad 21.2 \quad 21.7 \quad 21.1 \quad 6.0 \quad 8.3 \quad 9.3 \quad 11.3 \quad 11.3 \quad 11.8 \quad 14.8 \quad 11.9 \quad 12.6 \quad 14.4 \\ \hline 60 \quad 50 \quad 23 \quad 37 \quad 25.3 \quad 27 \quad 25 \quad 17 \quad 14 \quad 1.8 \quad 10 \quad 15 \quad 18 \quad 26 \end{array} \quad (2)$$

$$\checkmark \quad \begin{array}{r} 1.8 \quad 2.4 \quad 2.6 \quad 6.7 \quad 7.4 \quad 9.2 \quad 10.2 \quad 13.0 \quad 13.3 \quad 13.1 \quad 12.1 \quad 13.3 \quad 14.3 \quad 15.0 \\ \hline 60 \quad 50 \quad 42 \quad 37 \quad 34 \quad 32 \quad 29 \quad 26 \quad 17 \quad 10 \quad 13 \quad 10 \quad 15 \quad 21 \quad 25 \end{array}$$

$$\checkmark \quad \begin{array}{r} 1.4 \quad 2.4 \\ \hline 60 \quad 50 \end{array} \quad \frac{2.4}{42} \quad (14.3)$$

$$\checkmark \quad \begin{array}{r} 1.4 \quad 2.6 \quad 3.8 \quad 5.2 \\ \hline 60 \quad 50 \quad 42 \quad 38 \end{array} \quad (15.6)$$

$$\checkmark \quad \begin{array}{r} 7.0 \quad 7.9 \quad 9.8 \\ \hline 60 \quad 55 \quad 41 \end{array} \quad (16.9)$$

$$\checkmark \quad \begin{array}{r} 9.7 \quad 10.2 \quad 10.9 \\ \hline 60 \quad 50 \quad 45 \end{array} \quad (18.2)$$

$$\checkmark \quad \begin{array}{r} 11.2 \quad 12.5 \quad 13.7 \\ \hline 60 \quad 50 \quad 43 \end{array} \quad (19.5)$$

$$\checkmark \quad \begin{array}{r} 12.2 \quad 13.3 \quad 14.1 \\ \hline 60 \quad 50 \quad 43 \end{array} \quad (20.0)$$

$$\checkmark \quad \begin{array}{r} 4.3 \quad 7.6 \\ \hline 47 \quad 60 \end{array} \quad (+1.5)$$

$$\checkmark \quad \begin{array}{r} 5.7 \quad 7.3 \quad 9.8 \\ \hline 41 \quad 50 \quad 60 \end{array} \quad (+1.3)$$

$$\checkmark \quad \begin{array}{r} 7.5 \quad 8.5 \quad 9.4 \quad 10.6 \quad 11.9 \\ \hline 39 \quad 44 \quad 46 \quad 54 \quad 60 \end{array} \quad (+0.8)$$

$$\checkmark \quad \begin{array}{r} 8.0 \quad 9.7 \quad 11.7 \\ \hline 41 \quad 50 \quad 60 \end{array} \quad (+0.6)$$

STA	+	π	-	ELEV
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919.38

40+00

19.7

+50

18.4

41+00

17.2

+50

15.9

42+00

14.6

+50

13.3

43+00

12.0

+22

11.5

+57

10.7

+79

10.3

+89

10.2

44+00

09.9

LT

2

RT

✓

(10.3)

$$\frac{6.3}{32} \frac{8.7}{40} \frac{10.4}{50} \frac{11.9}{60}$$

✓

(-1.0)

$$\frac{3.8}{26} \frac{5.7}{30-32} \frac{8.2}{36} \frac{10.6}{44} \frac{12.0}{50} \frac{12.8}{60}$$

✓

$$\frac{2.4}{22} \frac{2.8}{14} \frac{2.8}{10}$$

$$\frac{2.3}{22} \frac{2.3}{10} \frac{3.6}{14} \frac{5.7}{17} \frac{11.0}{26} \frac{13.4}{28} \frac{14.8}{50} \frac{14.8}{60}$$

✓

$$\frac{3.5}{25} \frac{3.8}{22} \frac{3.3}{20} \frac{3.8}{13} \frac{3.6}{10} \frac{3.6}{15} \frac{6.2}{17-19} \frac{7.2}{22} \frac{7.6}{27} \frac{11.8}{38} \frac{14.0}{50} \frac{14.8}{60}$$

✓

$$\frac{5.4}{28} \frac{5.3}{27} \frac{4.8}{22} \frac{4.7}{18} \frac{4.9}{14} \frac{4.9}{10} \frac{4.8}{10} \frac{5.0}{15} \frac{6.7}{19} \frac{8.2}{22} \frac{9.4}{27} \frac{11.5}{32} \frac{13.1}{39} \frac{14.6}{50} \frac{14.6}{60}$$

✓

$$\frac{6.0}{33} \frac{6.3}{27} \frac{6.9}{25-24} \frac{6.4}{21} \frac{6.2}{15} \frac{6.2}{10} \frac{6.1}{10} \frac{6.2}{10} \frac{6.2}{14} \frac{8.2}{17-18} \frac{10.1}{22} \frac{11.2}{26} \frac{11.7}{29} \frac{13.9}{37} \frac{15.0}{50} \frac{15.7}{60}$$

✓

$$\frac{7.6}{33} \frac{8.0}{28} \frac{7.9}{22} \frac{7.4}{14} \frac{7.4}{10} \frac{7.4}{10} \frac{7.5}{10} \frac{7.8}{15} \frac{10.6}{25} \frac{12.5}{39} \frac{13.1}{50} \frac{13.8}{60}$$

✓

$$\frac{6.0}{38} \frac{7.1}{34} \frac{8.0}{28} \frac{8.8}{25} \frac{7.8}{23} \frac{8.0}{21} \frac{8.0}{14} \frac{8.0}{10} \frac{7.9}{10} \frac{8.0}{10} \frac{8.2}{15} \frac{8.9}{17} \frac{12.6}{22-29} \frac{12.6}{36} \frac{12.6}{50} \frac{12.6}{60}$$

✓

$$\frac{4.3}{60} \frac{7.6}{50} \frac{7.9}{38} \frac{8.3}{23} \frac{8.5}{15} \frac{8.7}{10} \frac{8.7}{10} \frac{8.8}{10} \frac{8.9}{15} \frac{9.4}{17} \frac{13.4}{22} \frac{13.8}{33} \frac{13.8}{50} \frac{13.4}{60}$$

✓

$$\frac{8.7}{60} \frac{9.2}{50} \frac{9.4}{34} \frac{9.2}{21} \frac{9.1}{14} \frac{9.1}{10} \frac{9.1}{10} \frac{9.1}{10} \frac{9.2}{15} \frac{9.7}{18} \frac{12.0}{21} \frac{13.6}{35} \frac{13.3}{50} \frac{12.9}{60}$$

✓

$$\frac{9.1}{60} \frac{9.3}{50} \frac{9.4}{39} \frac{9.2}{24} \frac{9.2}{14} \frac{9.3}{10} \frac{9.2}{10} \frac{9.3}{10} \frac{9.4}{14} \frac{9.4}{19} \frac{10.7}{31} \frac{11.5}{40} \frac{12.6}{48} \frac{12.2}{60}$$

✓

$$\frac{9.3}{60} \frac{9.2}{50} \frac{9.5}{39} \frac{11.3}{35} \frac{10.5}{23} \frac{10.4}{18} \frac{9.4}{15} \frac{9.4}{10} \frac{9.5}{10} \frac{9.6}{15} \frac{10.2}{28} \frac{10.7}{50} \frac{10.8}{60}$$

STA	+	π	-	ELEV
		919.38		
44+30				09.4
+35				09.4
+50				09.2
B.M.	4.61	913.82	10.17	909.21
45+00				09.2
+50				09.0
46+00				08.8
+04				08.8
+50				08.8
47+00				08.8
+50				08.7
+85				08.6
48+00				08.6

LT

L

RT

✓ $\frac{16.7}{60} \frac{12.3}{50} \frac{12.2}{35} \frac{10.0}{15} \frac{10.0}{10} \frac{10.0}{100} \frac{10.0}{10} \frac{10.0}{16} \frac{10.4}{26} \frac{10.5}{50} \frac{10.5}{60}$

✓ $\frac{12.9}{60} \frac{13.8}{57} \frac{12.5}{45} \frac{13.2}{31} \frac{12.7}{21} \frac{10.2}{15} \frac{10.0}{100} \frac{10.0}{10} \frac{10.1}{16} \frac{10.2}{24} \frac{10.3}{42} \frac{10.4}{50} \frac{10.5}{60}$

✓ $\frac{13.6}{60} \frac{14.4}{56} \frac{14.0}{50} \frac{14.3}{37} \frac{14.1}{29} \frac{13.2}{19} \frac{10.2}{14} \frac{10.1}{70} \frac{10.1}{101} \frac{10.1}{10} \frac{10.1}{15} \frac{10.2}{24} \frac{10.4}{44} \frac{10.5}{50} \frac{10.5}{60}$

Top. 50. END CONC PUMP BASE STA 44+50 RT

✓ $\frac{9.6}{60} \frac{10.0}{50} \frac{10.0}{37} \frac{10.1}{27} \frac{9.7}{22} \frac{4.8}{14} \frac{4.7}{70} \frac{4.6}{4.6} \frac{4.7}{10} \frac{4.7}{17} \frac{5.0}{30} \frac{5.3}{50-60}$

✓ $\frac{11.2}{60} \frac{11.1}{50} \frac{11.0}{31} \frac{10.2}{24} \frac{8.1}{18} \frac{5.2}{13} \frac{4.9}{10} \frac{4.8}{4.8} \frac{5.0}{10} \frac{5.1}{15} \frac{5.4}{20} \frac{6.0}{29} \frac{6.0}{50}$

✓ $\frac{11.4}{60} \frac{10.9}{50} \frac{10.5}{36} \frac{9.8}{24} \frac{7.6}{18} \frac{5.3}{12} \frac{5.1}{10} \frac{5.0}{5.0} \frac{5.0}{10} \frac{5.0}{14} \frac{5.2}{18} \frac{6.5}{33} \frac{6.9}{50}$

✓ $\frac{11.3}{60} \frac{10.7}{50} \frac{10.2}{29} \frac{9.1}{22} \frac{7.2}{17} \frac{6.6}{16} \frac{5.2}{13} \frac{5.1}{10} \frac{5.0}{5.0} \frac{5.0}{10} \frac{5.0}{15} \frac{7.4}{26} \frac{7.2}{30} \frac{8.5}{34} \frac{10.2}{50}$

✓ $\frac{8.1}{50} \frac{7.2}{31} \frac{7.4}{25} \frac{7.2}{20} \frac{5.2}{15} \frac{5.1}{10} \frac{5.0}{5.0} \frac{5.0}{10} \frac{5.1}{15} \frac{8.2}{22} \frac{8.7}{28} \frac{7.2}{32} \frac{8.2}{50}$

✓ $\frac{4.1}{50} \frac{3.7}{42} \frac{3.5}{32} \frac{7.0}{25} \frac{5.5}{21} \frac{5.5}{17} \frac{5.2}{10} \frac{5.0}{5.0} \frac{5.1}{10} \frac{5.1}{15} \frac{7.7}{20} \frac{8.0}{25} \frac{3.7}{34} \frac{4.4}{50}$

✓ $\frac{5.6}{50} \frac{5.6}{29} \frac{7.0}{25-23} \frac{6.8}{22} \frac{5.4}{16} \frac{5.2}{10} \frac{5.1}{5.1} \frac{5.1}{10} \frac{5.4}{15} \frac{7.7}{20} \frac{7.6}{24} \frac{3.0}{31} \frac{2.8}{50}$

✓ $\frac{10.8}{50} \frac{10.2}{39} \frac{9.0}{26} \frac{8.1}{23} \frac{5.3}{16} \frac{5.2}{10} \frac{5.2}{5.2} \frac{5.3}{10} \frac{5.5}{14} \frac{7.2}{19} \frac{7.4}{23} \frac{7.0}{25} \frac{5.2}{32} \frac{5.2}{50}$

✓ $\frac{11.2}{50} \frac{10.4}{31} \frac{9.3}{24} \frac{6.4}{19} \frac{5.3}{15} \frac{5.2}{10} \frac{5.2}{5.2} \frac{5.3}{10} \frac{5.8}{14} \frac{7.5}{21} \frac{7.5}{27} \frac{5.9}{33} \frac{5.6}{50}$

STA	+	Δ	—	ELEV
		913.82.		
48+50				085
49+00				085
+50				08.5
50+00				085
T.P.	5.41	915.55.	3.68	910.14.
+50				085
51+00				08.4
+50				08.4
52+00				08.3
+24				08.3
+35				08.3
+44				08.4
+58	±	Co-RD B		08.5

LT

C

RT

$$\checkmark \quad \frac{12.3}{50} \quad \frac{11.3}{23} \quad \frac{10.3}{22} \quad \frac{6.9}{18} \quad \frac{5.4}{17} \quad \frac{5.3}{14} \quad \frac{5.3}{10} \quad \frac{5.4}{10} \quad \frac{5.5}{15} \quad \frac{7.6}{20} \quad \frac{7.7}{25} \quad \frac{7.7}{28} \quad \frac{6.1}{34} \quad \frac{5.6}{50}$$

$$\checkmark \quad \frac{11.2}{50} \quad \frac{9.5}{23} \quad \frac{7.2}{19} \quad \frac{5.3}{18} \quad \frac{5.3}{15} \quad \frac{5.3}{10} \quad \frac{5.3}{10} \quad \frac{5.5}{15} \quad \frac{7.0}{21} \quad \frac{7.1}{29} \quad \frac{5.8}{33} \quad \frac{5.2}{50}$$

$$\checkmark \quad \frac{10.8}{50} \quad \frac{9.1}{28} \quad \frac{7.7}{21} \quad \frac{6.4}{19} \quad \frac{5.5}{18} \quad \frac{5.3}{14} \quad \frac{5.3}{11} \quad \frac{5.3}{10} \quad \frac{5.3}{10} \quad \frac{5.6}{15} \quad \frac{6.9}{19} \quad \frac{6.7}{26} \quad \frac{3.9}{33} \quad \frac{3.1}{50}$$

$$\checkmark \quad \frac{10.3}{50} \quad \frac{9.1}{29} \quad \frac{7.8}{24} \quad \frac{6.1}{18} \quad \frac{5.6}{14} \quad \frac{5.4}{10} \quad \frac{5.3}{10} \quad \frac{5.4}{10} \quad \frac{5.5}{15} \quad \frac{6.5}{19} \quad \frac{6.8}{24} \quad \frac{3.7}{33} \quad \frac{3.0}{50}$$

$$\checkmark \quad \frac{11.1}{50} \quad \frac{10.5}{23} \quad \frac{9.8}{27} \quad \frac{8.9}{23} \quad \frac{7.3}{15} \quad \frac{7.2}{10} \quad \frac{7.1}{10} \quad \frac{7.2}{10} \quad \frac{7.3}{12} \quad \frac{7.8}{16} \quad \frac{8.9}{19} \quad \frac{8.2}{22} \quad \frac{8.5}{27} \quad \frac{3.5}{34} \quad \frac{3.5}{50}$$

$$\checkmark \quad \frac{7.1}{50} \quad \frac{9.5}{40} \quad \frac{8.4}{24} \quad \frac{9.1}{22} \quad \frac{8.0}{20} \quad \frac{7.4}{16} \quad \frac{7.3}{14} \quad \frac{7.3}{12} \quad \frac{7.3}{10} \quad \frac{7.2}{15} \quad \frac{8.6}{21} \quad \frac{8.6}{24} \quad \frac{8.9}{27} \quad \frac{4.1}{34} \quad \frac{3.1}{44} \quad \frac{3.1}{50}$$

$$\checkmark \quad \frac{4.4}{50} \quad \frac{6.4}{28} \quad \frac{9.5}{23} \quad \frac{8.5}{21} \quad \frac{7.5}{17} \quad \frac{7.3}{13} \quad \frac{7.2}{10} \quad \frac{7.2}{10} \quad \frac{7.3}{10} \quad \frac{7.3}{12} \quad \frac{7.6}{15} \quad \frac{9.3}{23} \quad \frac{9.4}{27} \quad \frac{1.7}{29} \quad \frac{2.3}{32} \quad \frac{2.3}{50}$$

$$\checkmark \quad \frac{3.9}{50} \quad \frac{4.3}{33} \quad \frac{5.7}{31} \quad \frac{9.3}{25} \quad \frac{8.4}{22} \quad \frac{7.7}{19} \quad \frac{7.4}{15} \quad \frac{7.4}{10} \quad \frac{7.1}{12} \quad \frac{7.6}{18} \quad \frac{10.2}{25} \quad \frac{10.7}{28} \quad \frac{11.7}{50}$$

$$\checkmark \quad \frac{7.1}{50} \quad \frac{8.9}{46} \quad \frac{8.2}{14} \quad \frac{7.9}{39} \quad \frac{7.9}{31} \quad \frac{7.4}{26} \quad \frac{7.4}{14} \quad \frac{7.3}{10} \quad \frac{7.4}{10} \quad \frac{7.3}{17} \quad \frac{8.2}{29} \quad \frac{10.9}{35} \quad \frac{11.3}{41} \quad \frac{12.7}{50}$$

$$\checkmark \quad \frac{7.9}{58} \quad \frac{8.0}{42} \quad \frac{8.2}{38} \quad \frac{7.4}{19} \quad \frac{7.3}{14} \quad \frac{7.3}{10} \quad \frac{7.3}{10} \quad \frac{7.3}{10} \quad \frac{7.4}{14} \quad \frac{7.6}{22} \quad \frac{7.4}{26} \quad \frac{8.0}{37} \quad \frac{10.2}{50}$$

$$\checkmark \quad \frac{8.1}{50} \quad \frac{7.9}{40} \quad \frac{7.4}{22} \quad \frac{7.2}{16} \quad \frac{7.2}{10} \quad \frac{7.2}{10} \quad \frac{7.3}{10} \quad \frac{7.1}{14} \quad \frac{7.4}{24} \quad \frac{7.5}{34} \quad \frac{7.3}{38} \quad \frac{7.4}{50}$$

$$\checkmark \quad \frac{7.4}{50} \quad \frac{7.3}{30} \quad \frac{7.2}{16} \quad \frac{7.2}{16} \quad \frac{7.1}{10} \quad \frac{7.2}{10} \quad \frac{7.1}{16} \quad \frac{7.2}{24} \quad \frac{7.3}{50}$$

STA	+	π	-	ELEV
		915.55.		
B.M	7.09	915.61.	7.09	908.46. 908.52.
52+78				08.7
				0
+90				0.88
53+00				089
+50				0.99
54+00				108
+50				119
55+00				13.2
+50				146
56+00				160
+50				175
57+00				18.8
T.P	11.50	926.63.	0.48	915.13.

LT

K

RT

Top MT CORD B + EDGERTON

✓ $\frac{8.4}{50} \frac{8.2}{41} \frac{7.9}{22} \frac{7.2}{22} \frac{7.0}{15} \frac{7.0}{10} \frac{6.9}{10} \frac{7.0}{10} \frac{7.1}{18} \frac{7.1}{26} \frac{7.4}{40} \frac{7.6}{50}$

✓ $\frac{8.5}{50} \frac{8.2}{45} \frac{8.2}{32} \frac{7.8}{23} \frac{7.2}{15} \frac{6.9}{10} \frac{6.9}{10} \frac{7.0}{15} \frac{6.7}{18} \frac{7.1}{22} \frac{7.9}{31} \frac{9.2}{37} \frac{10.2}{50}$

✓ $\frac{12.0}{50} \frac{12.1}{43} \frac{8.4}{31} \frac{7.3}{19} \frac{6.9}{13} \frac{6.8}{10} \frac{6.7}{10} \frac{6.8}{14} \frac{7.2}{19} \frac{8.9}{28} \frac{12.3}{35} \frac{13.7}{45} \frac{14.3}{50}$

✓ $\frac{15.2}{40} \frac{13.8}{33} \frac{7.3}{24} \frac{6.5}{20} \frac{5.9}{14} \frac{5.9}{10} \frac{5.2}{10} \frac{6.2}{10} \frac{5.7}{13} \frac{6.2}{19} \frac{12.4}{30} \frac{16.0}{3.6}$

✓ $\frac{15.5}{40} \frac{12.6}{33} \frac{5.8}{22} \frac{5.1}{15} \frac{5.0}{10} \frac{4.8}{10} \frac{4.9}{10} \frac{5.2}{10-11} \frac{4.8}{14} \frac{5.2}{19} \frac{12.4}{20} \frac{12.7}{31} \frac{13.3}{33} \frac{15.4}{38}$

✓ $\frac{15.1}{45} \frac{12.1}{36} \frac{11.9}{29} \frac{4.7}{21} \frac{4.0}{14} \frac{3.9}{10} \frac{3.7}{10} \frac{3.9}{10} \frac{3.9}{12} \frac{3.5}{14} \frac{4.7}{21} \frac{12.7}{32} \frac{15.7}{40}$

✓ $\frac{15.2}{48} \frac{13.0}{39} \frac{11.2}{33} \frac{3.1}{19} \frac{2.7}{14} \frac{2.6}{10} \frac{2.4}{10} \frac{2.6}{10} \frac{2.5}{12} \frac{2.8}{14} \frac{2.8}{20} \frac{12.0}{33} \frac{15.1}{44}$

✓ $\frac{12.3}{50} \frac{11.6}{42} \frac{10.1}{34} \frac{2.0}{20} \frac{1.4}{14} \frac{1.2}{10} \frac{1.0}{10} \frac{1.1}{10} \frac{0.7}{12} \frac{1.0}{14} \frac{10.3}{19} \frac{12.3}{34} \frac{12.3}{50}$

✓ $\frac{7.4}{50} \frac{7.4}{35} \frac{0.2}{22}$

+04

$\frac{8.8}{37} \frac{8.9}{50}$

✓ $\frac{4.6}{50} \frac{3.7}{44} \frac{3.1}{32}$

+19

$\frac{4.4}{34} \frac{5.1}{41} \frac{3.6}{50}$

*

STA	+	π	-	ELEV
		926.63		
56+00				16.0
+50				17.5
57+00				18.8
+50		$\frac{1}{2}$ SUN-RISE DRIVE	20.3 LT	
58+00	SO. ENSTH	H - R.W		21.6
+50				22.9
59+00				24.3
+50				25.6
T.P	9.27	935.82	0.08	926.55
60+00				26.9
+50				28.2
61+00				29.2
+50				30.0

LT

A

RT

✓

$$\frac{10.9}{14} \frac{10.8}{10} \frac{10.6}{10} \frac{10.7}{10} \frac{10.9}{10-12} \frac{10.4}{14} \frac{10.8}{19}$$

✓

$$\frac{10.1}{24} \frac{9.4}{14} \frac{9.2}{10} \frac{9.1}{10} \frac{9.2}{10} \frac{9.4}{14} \frac{9.6}{21}$$

✓

$$\frac{9.6}{50} \frac{9.7}{43} \frac{10.4}{41-38} \frac{8.6}{35} \frac{8.0}{26} \frac{7.9}{14} \frac{8.0}{10} \frac{7.8}{24} \frac{7.9}{10} \frac{8.0}{13} \frac{7.5}{17} \frac{7.4}{23} \frac{8.3}{29} \frac{10.0}{32} \frac{13.2}{39} \frac{14.6}{50}$$

✓

$$\frac{3.8}{50} \frac{4.9}{36} \frac{6.0}{19} \frac{6.5}{10} \frac{6.3}{10} \frac{6.4}{10} \frac{6.7}{19} \frac{6.2}{22} \frac{6.3}{24} \frac{6.9}{29} \frac{8.5}{35} \frac{9.7}{42} \frac{10.2}{50}$$
5.03.72.31.08.97.66.65.8

STA	+	π	-	ELEV	
		935.82'			
62+00				30.4	
+50				30.6	
63+00				30.8	
+50				30.6	
64+00				30.7	
B.M.	3.39	935.76.	3.39	932.43.	932.37.
+50				30.7	
65+00				30.9	
+50				30.7	
66+00				30.6	
+50				30.6	
67+00				30.6	
+50				30.5	

LT

4

RT

5.4

5.2

5.0

5.2

5.1

SPIKE P.P.

LT STA

+

1ST POLE 50.05 ^{OVERHEAD}

5.1

4.9

5.1

5.2

5.2

5.2

5.3

STA	+	Δ	-	ELEV
-----	---	----------	---	------

		935.76		
--	--	--------	--	--

68+00				
-------	--	--	--	--

				30.2
--	--	--	--	------

	+50			
--	-----	--	--	--

				296
--	--	--	--	-----

T.P				
-----	--	--	--	--

	0.61			
--	------	--	--	--

		930.48		
--	--	--------	--	--

			5.89	
--	--	--	------	--

				929.87
--	--	--	--	--------

69+00				
-------	--	--	--	--

				284
--	--	--	--	-----

	+50			
--	-----	--	--	--

				268
--	--	--	--	-----

70+00				
-------	--	--	--	--

				250
--	--	--	--	-----

	+50			
--	-----	--	--	--

				230
--	--	--	--	-----

71+00				
-------	--	--	--	--

				209
--	--	--	--	-----

	+50			
--	-----	--	--	--

				189
--	--	--	--	-----

72+00				
-------	--	--	--	--

				169
--	--	--	--	-----

	+31			
--	-----	--	--	--

				15.7
--	--	--	--	------

	+47			
--	-----	--	--	--

				15.1
--	--	--	--	------

	+58			
--	-----	--	--	--

				14.6
--	--	--	--	------

LT

Q

RT

5.6

6.2

2.1

3.7

5.5

7.5

9.6

11.6

✓ $\frac{6.2}{50} \frac{6.2}{41} \frac{11.9}{27} \frac{13.1}{20} \frac{14.2}{19} \frac{13.8}{15} \frac{13.7}{16} \frac{13.6}{10} \frac{13.7}{10} \frac{13.9}{19} \frac{14.7}{29} \frac{15.6}{31} \frac{15.0}{50} \frac{12.0}{60}$

✓ $\frac{9.4}{50} \frac{8.3}{40} \frac{11.8}{31} \frac{14.1}{19} (148)$

✓ $\frac{11.7}{50} \frac{9.3}{39} \frac{8.5}{34} \frac{8.5}{30} \frac{13.7}{24} (154)$

✓ $\frac{12.9}{50} \frac{10.8}{41} \frac{8.8}{35} \frac{9.9}{30} (159)$

STA + ~~AK~~ - ELEV

930.48

73+00

(129)

T.P. 1.65 918.99. 13.14 917.34.

B.M. 3.31 918.98. 3.31 915.68. 915.67.

72+31 ~~4~~ CORD BZ RT 15.7

+47

15.1

+58

14.6

73+00

12.9

+50

11.0

T.P. 4.38 913.52. 9.84 909.14.

74+00

08.8

+38

07.3

+47

CATCH BASIN

+73

05.9

75+00

04.8

T.P. 0.62 904.99. 9.15 904.37.

+14

04.3

LT

L

RT

✓

$$\frac{14.8}{50} \quad \frac{12.1}{35} \quad \frac{12.6}{30} \quad (17.6)$$

DRILL HOLE L B² + EDGERTON

✓

$$\frac{3.7}{17-15} \quad \frac{3.4}{13} \quad \frac{3.4}{10} \quad \frac{3.3}{3.3} \quad \frac{3.4}{10} \quad \frac{3.5}{16} \quad \frac{3.9}{33} \quad \frac{4.7}{50}$$

✓

$$\frac{2.2}{23} \quad \frac{3.2}{20} \quad \frac{4.4}{18} \quad \frac{4.1}{16} \quad \frac{4.0}{13} \quad \frac{3.9}{50} \quad \frac{4.0}{10} \quad \frac{4.2}{17} \quad \frac{4.2}{21} \quad \frac{4.9}{39} \quad \frac{5.7}{50}$$

✓

$$\frac{3.0}{24} \quad \frac{3.8}{20} \quad \frac{4.9}{16} \quad \frac{4.6}{18} \quad \frac{4.5}{12} \quad \frac{4.5}{10} \quad \frac{4.4}{4.4} \quad \frac{4.5}{10} \quad \frac{4.5}{16} \quad \frac{4.8}{30} \quad \frac{4.6}{34} \quad \frac{3.9}{50}$$

✓

$$\frac{5.4}{23-20} \quad \frac{6.2}{18} \quad \frac{6.9}{16-15} \quad \frac{6.6}{14} \quad \frac{6.3}{13} \quad \frac{6.2}{10} \quad \frac{6.1}{6.1} \quad \frac{6.2}{10} \quad \frac{6.3}{20} \quad \frac{6.1}{22} \quad \frac{4.3}{30} \quad \frac{2.9}{42} \quad \frac{2.1}{50}$$

✓

$$\frac{3.3}{50} \quad \frac{2.9}{42} \quad \frac{2.3}{31} \quad \frac{3.4}{25} \quad \frac{7.6}{21} \quad \frac{8.2}{18} \quad \frac{8.8}{17-15} \quad \frac{8.2}{14} \quad \frac{9.1}{10} \quad \frac{8.0}{8.0} \quad \frac{8.1}{10} \quad \frac{8.3}{20} \quad \frac{7.8}{24} \quad \frac{6.3}{29} \quad \frac{4.4}{42} \quad \frac{3.6}{50}$$

✓

$$\frac{1.8}{50} \quad \frac{1.3}{36} \quad \frac{3.9}{29} \quad \frac{4.5}{19} \quad \frac{7.1}{17-16} \quad \frac{4.9}{15} \quad \frac{4.7}{10} \quad \frac{4.7}{4.7} \quad \frac{5.1}{10} \quad \frac{4.6}{20} \quad \frac{2.2}{22} \quad \frac{1.5}{30} \quad \frac{0.7}{38} \quad \frac{0.7}{50}$$

✓

$$\frac{9.8}{50} \quad \frac{8.1}{39} \quad \frac{8.5}{36} \quad \frac{8.1}{32} \quad \frac{9.6}{30} \quad \frac{7.6}{26} \quad \frac{6.6}{25} \quad \frac{6.4}{14} \quad \frac{6.2}{10} \quad \frac{6.2}{6.2} \quad \frac{7.0}{10} \quad \frac{6.6}{20} \quad \frac{5.7}{26} \quad \frac{4.8}{37} \quad \frac{5.3}{50}$$

$$\begin{array}{l} \text{T.P.} \\ \text{C.B.} \\ \text{O.C.} \end{array} \quad \begin{array}{l} \text{F.L.} \\ 24^{\circ}\text{CM} \\ 21 \end{array} \quad \begin{array}{l} 1.5 \\ 20 \end{array} \quad \begin{array}{l} 12.5 \\ 11 \end{array}$$

✓

$$\frac{11.4}{50} \quad \frac{11.5}{40} \quad \frac{11.1}{37} \quad \frac{8.1}{36} \quad \frac{7.7}{14} \quad \frac{7.7}{10} \quad \frac{7.7}{7.7} \quad \frac{7.6}{10} \quad \frac{7.7}{14} \quad \frac{7.3}{20} \quad \frac{10.1}{30} \quad \frac{10.1}{50}$$

✓

$$\frac{14.9}{50} \quad \frac{14.9}{41} \quad \frac{13.7}{37} \quad \frac{11.4}{29} \quad \frac{9.1}{24} \quad \frac{8.8}{14} \quad \frac{8.8}{10} \quad \frac{8.8}{8.8} \quad \frac{8.8}{10} \quad \frac{8.8}{12} \quad \frac{8.8}{14} \quad \frac{9.3}{23} \quad \frac{10.7}{30} \quad \frac{13.6}{50}$$

✓

$$\frac{8.0}{50} \quad \frac{7.8}{44} \quad \frac{8.1}{40} \quad \frac{7.6}{37} \quad \frac{1.4}{24} \quad \frac{0.8}{14} \quad \frac{0.8}{10} \quad \frac{0.7}{0.7} \quad \frac{0.7}{10} \quad \frac{0.6}{13} \quad \frac{1.4}{16} \quad \frac{2.2}{22} \quad \frac{5.3}{30} \quad \frac{9.3}{42-50}$$

STA	+	Δ	-	ELEV
		904.99		
75+50				02.8
76+00				00.8
+50				898.9
+70				98.1
T.P.	2.97	897.36	10.60	894.39.
75+50				(02.8)
76+00				(00.8)
77+00				96.8
+50				94.9
78+00				92.9
+50				90.9
B.M	792	897.34	792	889.44. 889.42.
79+00				88.8
+30				87.7

LT

Z

RT

$$\checkmark \begin{array}{cccccccccccc} \frac{8.4}{60} & \frac{10.1}{53} & \frac{10.3}{43} & \frac{10.1}{39} & \frac{3.2}{26} & \frac{2.4}{13} & \frac{2.4}{10} & \frac{2.2}{2.2} & \frac{2.3}{10} & \frac{2.4}{11} & \frac{2.3}{13} & \frac{4.9}{18} & \frac{15.5}{38} \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} \frac{10.4}{60} & \frac{12.3}{52} & \frac{12.3}{36} & \frac{5.0}{20} & \frac{4.4}{13} & \frac{4.3}{10} & \frac{4.2}{4.2} & \frac{4.4}{10} & \frac{4.4}{12} & \frac{4.2}{14} & \frac{5.4}{16} \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} \frac{12.8}{60} & \frac{14.2}{50} & \frac{14.2}{36} & \frac{13.4}{33} & \frac{6.7}{21} & \frac{6.1}{13} & \frac{6.2}{10} & \frac{6.2}{6.1} & \frac{6.2}{10} & \frac{6.2}{12} & \frac{6.0}{13} & \frac{6.4}{15} & \frac{9.8}{18} \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} \frac{14.3}{60} & \frac{15.7}{52} & \frac{15.9}{42} & \frac{15.0}{28} & \frac{13.6}{24} & \frac{10.4}{18} & \frac{6.9}{13} & \frac{7.1}{11} & \frac{7.0}{10} & \frac{6.9}{6.9} & \frac{7.0}{10} & \frac{7.1}{12} & \frac{6.8}{13} & \frac{7.8}{16} & \frac{10.1}{18} \end{array}$$

$$\checkmark \begin{array}{ccccccc} (15.4) & \frac{11.7}{42} & \frac{13.2}{50} & \frac{14.4}{68} & \frac{15.5}{93} & \frac{14.9}{100} \end{array}$$

$$\checkmark \begin{array}{ccccccc} (43.4) & \frac{15.7}{43} & \frac{17.1}{50} & \frac{19.2}{65} & \frac{26.0}{100} \end{array}$$

$$\checkmark \begin{array}{ccccccccccc} \frac{9.9}{60} & \frac{9.7}{43} & \frac{8.4}{24} & \frac{0.7}{13} & \frac{0.7}{10} & \frac{0.6}{0.6} & \frac{0.7}{10} & \frac{0.7}{12} & \frac{0.5}{13} & \frac{2.2}{16} \end{array}$$

$$\checkmark \begin{array}{ccccccccccc} \frac{9.3}{60} & \frac{11.0}{50} & \frac{11.1}{37} & \frac{10.7}{26} & \frac{2.6}{13} & \frac{2.6}{10} & \frac{2.5}{2.5} & \frac{2.7}{10} & \frac{2.8}{12} & \frac{2.6}{13} \end{array}$$

$$\checkmark \begin{array}{ccccccccccc} \frac{8.3}{60} & \frac{9.4}{50} & \frac{10.2}{42} & \frac{11.5}{36} & \frac{11.0}{24} & \frac{4.4}{13} & \frac{4.6}{10} & \frac{4.5}{4.5} & \frac{4.7}{10} & \frac{4.8}{11} & \frac{4.6}{13} \end{array}$$

$$\checkmark \begin{array}{ccccccccccc} \frac{6.2}{60} & \frac{8.4}{48} & \frac{10.8}{35} & \frac{11.5}{30} & \frac{11.6}{24} & \frac{6.5}{14} & \frac{6.6}{10} & \frac{6.6}{6.5} & \frac{6.7}{10} & \frac{6.6}{11} \end{array}$$

✓ Top Mont. 4 64. 78+

$$\begin{array}{ccccccccccc} \frac{8.1}{50} & \frac{9.5}{40} & \frac{10.8}{35} & \frac{10.1}{19} & \frac{8.6}{16} & \frac{8.3}{13} & \frac{8.7}{12} & \frac{8.5}{11} & \frac{8.5}{10} & \frac{8.6}{8.5} & \frac{8.5}{10-11} & \frac{8.5}{13} \end{array}$$

$$\checkmark \begin{array}{ccccccccccc} \frac{9.4}{50} & \frac{10.8}{40} & \frac{10.9}{27} & \frac{10.1}{22} & \frac{9.9}{14} & \frac{9.8}{10} & \frac{9.6}{9.6} & \frac{9.7}{10} & \frac{9.7}{11} & \frac{9.6}{13} \end{array}$$

*

STA	+	π	-	ELEV
		897.34.		
79+43				87.2
T.P.	4.02	890.58.	10.78	886.56.
76+50				(98.9)
77+00				(96.8)
+50				(94.9)
78+00				(92.9)
+50				(90.9)
79+00				(88.8)
+30				(87.7)
+43				(87.2)
+59				86.6
+78				(86.0)
T.P.	2.28	887.11.	5.15	884.83.
80+00				85.2

LT

Z

RT

$$\checkmark \quad \frac{10.4}{50} \frac{10.5}{40} \frac{10.4}{27} \frac{10.0}{18} \frac{10.2}{10} \quad 10.1 \quad \frac{10.2}{10} \frac{10.2}{11-12} \frac{10.5}{16}$$

$$\checkmark \quad (+83) \quad \frac{14.4}{46} \quad \frac{17.4}{59} \quad \frac{23.9}{100}$$

$$\checkmark \quad (+62) \quad \frac{21.3}{58} \quad \frac{27.0}{100}$$

$$\checkmark \quad (+43) \quad \frac{17.7}{44} \quad \frac{21.8}{71} \quad \frac{25.2}{100}$$

$$\checkmark \quad (+23) \quad \frac{15.0}{38} \quad \frac{17.3}{56} \quad \frac{19.2}{62} \quad \frac{22.0}{100}$$

$$\checkmark \quad (+02) \quad \frac{11.7}{31} \quad \frac{13.9}{48} \quad \frac{15.3}{75} \quad \frac{19.4}{100}$$

$$\checkmark \quad (1.8) \quad \frac{12.2}{29} \quad \frac{13.5}{50} \quad \frac{14.2}{80}$$

$$\checkmark \quad (2.9) \quad \frac{10.8}{27} \quad \frac{13.1}{50} \quad \frac{13.1}{75}$$

$$\checkmark \quad (34) \quad \frac{5.6}{22} \quad \frac{7.9}{34} \quad \frac{9.8}{60}$$

$$\checkmark \quad \frac{3.9}{50} \quad \frac{4.0}{40} \quad \frac{4.4}{24} \quad \frac{4.2}{16} \quad \frac{4.1}{10} \quad \frac{4.0}{40} \quad \frac{4.1}{10} \quad \frac{4.0}{13} \quad \frac{4.5}{18} \quad \frac{6.7}{26} \quad \frac{8.4}{50}$$

$$\checkmark \quad \frac{5.5}{50} \quad \frac{5.6}{30} \quad \frac{5.3}{18} \quad \frac{4.8}{16} \quad \frac{4.7}{10} \quad \frac{4.6}{10} \quad \frac{4.7}{10} \quad \frac{4.6}{12} \quad \frac{4.8}{15} \quad \frac{7.0}{19} \quad \frac{7.7}{22} \quad \frac{8.6}{35} \quad \text{Floor House} \quad \frac{7.9}{35}$$

$$\checkmark \quad \frac{3.6}{50} \quad \frac{3.4}{37} \quad \frac{2.8}{21} \quad \frac{2.0}{16} \quad \frac{1.9}{13} \quad \frac{2.0}{10} \quad \frac{1.9}{10} \quad \frac{2.0}{10} \quad \frac{1.9}{11-12} \quad \frac{2.0}{14} \quad \frac{4.2}{18} \quad \frac{6.0}{43}$$

STA	+	Δ	-	ELEV	
		887.11			
80+50				83.5	
81+00				81.9	
+22				81.3	
+45				80.5	
82+00				78.8	
+50				77.3	
83+00				75.9	
+50				74.6	
84+00				73.3	
T.P	2.13	876.26	12.98	874.13	
B.M	6.08	876.25	6.08	870.18	870.17
+50				72.2	
85+00				71.0	

LT

Q

RT

$$\checkmark \frac{4.0}{50} \frac{4.4}{30} \frac{5.0}{28} \frac{4.9}{22} \frac{3.9}{16} \frac{3.5}{14} \frac{3.6}{10} \frac{3.6}{10} \frac{3.5}{12} \frac{3.8}{13} \frac{4.0}{16} \frac{5.8}{28} \frac{6.8}{41} \frac{7.9}{50}$$

$$\checkmark \frac{4.7}{50} \frac{4.1}{43} \frac{3.9}{30} \frac{6.0}{26} \frac{5.4}{16} \frac{5.1}{12} \frac{5.2}{10} \frac{5.2}{10} \frac{5.0}{10} \frac{5.5}{13} \frac{8.0}{18} \frac{11.3}{35} \frac{14.0}{60}$$

$$\checkmark \frac{5.1}{50} \frac{3.8}{44} \frac{2.9}{27} \frac{6.5}{21} \frac{5.9}{19} \frac{5.4}{16} \frac{5.9}{12} \frac{5.9}{10} \frac{5.8}{10} \frac{5.9}{10} \frac{5.7}{13} \frac{5.7}{15} \frac{7.0}{22} \frac{11.8}{36} \frac{15.2}{50} \frac{17.0}{60}$$

$$\checkmark \frac{5.3}{60} \frac{4.6}{50} \frac{1.8}{30} \frac{7.2}{27} \frac{6.7}{20} \frac{6.6}{17} \frac{6.6}{14} \frac{6.6}{12} \frac{6.6}{10} \frac{6.6}{10} \frac{6.2}{10} \frac{6.5}{14} \frac{6.8}{16} \frac{8.1}{22} \frac{14.9}{37} \frac{16.7}{46} \frac{18.1}{57} \frac{18.8}{60}$$

$$\checkmark \frac{2.8}{60} \frac{2.6}{50} \frac{2.0}{40} \frac{1.5}{39} \frac{8.4}{21} \frac{8.8}{23} \frac{8.3}{19} \frac{8.4}{12} \frac{8.4}{10} \frac{8.3}{10} \frac{8.4}{10} \frac{8.3}{12} \frac{8.3}{15} \frac{9.6}{21} \frac{14.2}{30} \frac{16.0}{38} \frac{19}{41} \frac{21.1}{50} \frac{21.1}{60}$$

$$\checkmark \frac{0.2}{60} \frac{2.2}{50} \frac{2.2}{39} \frac{2.8}{37} \frac{10.7}{23} \frac{10.1}{25} \frac{9.8}{20} \frac{9.9}{12} \frac{9.9}{10} \frac{9.8}{10} \frac{9.8}{12} \frac{9.8}{14} \frac{15.4}{27} \frac{18.1}{38} \frac{21.0}{50} \frac{22.2}{60}$$

$$\checkmark \frac{2.8}{60} \frac{4.0}{50} \frac{4.7}{40} \frac{5.3}{36} \frac{12.3}{24} \frac{11.6}{22} \frac{11.1}{21} \frac{11.3}{12} \frac{11.3}{10} \frac{11.2}{10} \frac{11.4}{10} \frac{11.2}{12} \frac{11.3}{15} \frac{18.4}{30} \frac{21.4}{45} \frac{23.0}{60}$$

$$\checkmark \frac{2.6}{60} \frac{4.2}{50} \frac{4.6}{43} \frac{6.5}{38} \frac{13.2}{25} \frac{13.2}{27} \frac{12.7}{21} \frac{12.4}{14} \frac{12.6}{12} \frac{12.6}{10} \frac{12.5}{10} \frac{12.6}{10} \frac{12.5}{11} \frac{12.4}{14} \frac{17.0}{23} \frac{18.8}{33} \frac{20.6}{44} \frac{21.7}{47} \frac{22.2}{60}$$

$$\checkmark \frac{5.0}{60} \frac{6.8}{50} \frac{7.2}{40} \frac{8.5}{38} \frac{15.1}{27} \frac{14.3}{29} \frac{13.8}{20} \frac{13.9}{13} \frac{13.9}{10} \frac{13.9}{10} \frac{13.7}{12} \frac{13.7}{15} \frac{16.9}{23} \frac{20.1}{33} \frac{20.8}{40} \frac{22.2}{47} \frac{22.2}{60}$$

SPIKE ARC LITE POLE #A13 LT STA 86+00

$$\checkmark \frac{3.8}{56} \frac{4.1}{38} \frac{5.2}{32} \frac{5.2}{28} \frac{5.4}{60} \frac{4.4}{27} \frac{4.1}{17} \frac{4.2}{11} \frac{4.2}{10} \frac{4.1}{10} \frac{4.2}{10} \frac{4.1}{11} \frac{4.2}{15} \frac{9.3}{24} \frac{11.5}{35} \frac{12.4}{50} \frac{12.3}{60}$$

$$\checkmark \frac{5.5}{50} \frac{6.6}{32} \frac{6.6}{27} \frac{6.2}{22} \frac{5.8}{16} \frac{5.4}{15} \frac{5.5}{10} \frac{5.3}{10} \frac{5.4}{10} \frac{5.3}{11} \frac{5.2}{15} \frac{11.9}{31} \frac{12.8}{42} \frac{12.6}{50} \frac{12.4}{60}$$

STA	+	π	-	ELEV
		876.25.		
85+50				701
86+00				694
+29				692
+50				69.0
87+00				687
T.P	2.56	872.33.	6.48	869.77.
+38				684
+50				682
+87				679
88+00				678
+50				675
89+00				673
+50				668

LT

Q

RT

$$\checkmark \quad \frac{6.2}{50} \quad \frac{6.8}{36} \quad \frac{7.4}{32} \quad \frac{8.0}{25} \quad \frac{6.6}{75} \quad \frac{6.3}{12} \quad \frac{6.3}{10} \quad \frac{6.3}{12} \quad \frac{6.2}{16} \quad \frac{11.1}{26} \quad \frac{12.7}{23} \quad \frac{13.0}{50} \quad \frac{12.8}{60}$$

$$\checkmark \quad \frac{7.7}{50} \quad \frac{9.0}{37} \quad \frac{8.7}{27} \quad \frac{8.6}{22} \quad \frac{7.3}{18} \quad \frac{7.4}{14} \quad \frac{6.9}{10} \quad \frac{6.9}{10} \quad \frac{7.0}{10} \quad \frac{7.1}{13} \quad \frac{11.1}{26} \quad \frac{12.7}{36-38} \quad \frac{12.1}{41} \quad \frac{12.5}{50} \quad \frac{13.2}{60}$$

$$\checkmark \quad \frac{8.2}{50} \quad \frac{9.4}{38} \quad \frac{9.9}{30} \quad \frac{9.6}{25} \quad \frac{7.6}{17} \quad \frac{7.2}{12} \quad \frac{7.2}{10} \quad \frac{7.2}{110} \quad \frac{7.3}{172} \quad \frac{8.6}{630-33} \quad \frac{10.3}{38} \quad \frac{8.8}{45} \quad \frac{9.9}{50} \quad \frac{10.0}{60} \quad \frac{12.0}{60}$$

$$\checkmark \quad \frac{6.7}{60} \quad \frac{8.8}{50} \quad \frac{10.0}{45} \quad \frac{10.2}{31} \quad \frac{9.5}{23} \quad \frac{7.5}{14} \quad \frac{7.3}{11} \quad \frac{7.4}{10} \quad \frac{7.3}{10} \quad \frac{7.3}{12} \quad \frac{7.6}{17} \quad \frac{10.4}{24-26} \quad \frac{9.2}{30} \quad \frac{8.3}{24} \quad \frac{10.1}{50} \quad \frac{16.6}{70} \quad \text{L.R.K.}$$

$$\checkmark \quad \frac{5.2}{50} \quad \frac{9.6}{42} \quad \frac{10.8}{39} \quad \frac{10.8}{31} \quad \frac{10.4}{25} \quad \frac{8.0}{16} \quad \frac{7.8}{10} \quad \frac{7.8}{9} \quad \frac{7.7}{10} \quad \frac{7.2}{12} \quad \frac{8.4}{16} \quad \frac{9.6}{26} \quad \frac{11.6}{34} \quad \frac{14.5}{44} \quad \frac{16.8}{68} \quad \text{L.R.K.}$$

$$\checkmark \quad \frac{1.8}{50} \quad \frac{6.4}{40} \quad \frac{7.0}{33} \quad \frac{9.0}{30-28} \quad \frac{5.6}{23} \quad \frac{4.9}{21} \quad \frac{4.4}{14} \quad \frac{4.1}{10} \quad \frac{3.9}{10} \quad \frac{4.1}{10} \quad \frac{4.2}{14} \quad \frac{4.4}{19} \quad \frac{6.0}{24}$$

$$\checkmark \quad \frac{6.3}{50} \quad \frac{6.7}{44} \quad \frac{5.7}{34} \quad \frac{9.0}{30-28} \quad \frac{5.6}{23} \quad \frac{4.9}{21} \quad \frac{4.4}{17} \quad \frac{4.2}{10} \quad \frac{4.1}{10} \quad \frac{4.2}{10} \quad \frac{4.2}{14} \quad \frac{4.9}{19}$$

$$\checkmark \quad \frac{7.7}{50} \quad \frac{7.9}{41} \quad \frac{9.7}{36} \quad \frac{10.0}{29} \quad \frac{4.3}{22} \quad \frac{4.1}{17} \quad \frac{4.5}{10} \quad \frac{4.4}{10} \quad \frac{4.5}{10} \quad \frac{4.4}{14} \quad \frac{4.8}{20}$$

$$\checkmark \quad \frac{8.2}{54} \quad \frac{11.4}{46} \quad \frac{11.0}{32} \quad \frac{9.9}{28} \quad \frac{4.6}{19} \quad \frac{4.6}{13} \quad \frac{4.6}{10} \quad \frac{4.5}{10} \quad \frac{4.6}{10} \quad \frac{4.6}{14} \quad \frac{5.0}{19}$$

$$\checkmark \quad \frac{4.9}{19} \quad \frac{4.9}{14} \quad \frac{5.0}{10} \quad \frac{4.8}{10} \quad \frac{5.0}{10} \quad \frac{5.0}{14} \quad \frac{5.9}{18}$$

$$\checkmark \quad \frac{5.1}{19} \quad \frac{5.3}{14} \quad \frac{5.3}{10} \quad \frac{5.0}{10} \quad \frac{5.1}{10} \quad \frac{5.0}{15} \quad \frac{5.2}{19}$$

$$\checkmark \quad \frac{5.7}{18} \quad \frac{5.6}{12} \quad \frac{5.6}{10} \quad \frac{5.5}{10} \quad \frac{5.7}{10} \quad \frac{5.5}{14} \quad \frac{5.5}{17}$$

STA + ∇ - ELEV

872.33

667

89+75 SECTION $\frac{1}{2}$ 30" X 56" C.M X DRAIN

90+00

665

+50

662

91+00

666

+50

672

T.P. 5.79 873.70 4.42 867.91

87+38

684

+50

682

+87

679

88+00

678

+50

675

89+00

673

+50

668

LT

2

RT

$$\checkmark \quad \frac{6.0}{17} \quad \frac{6.0}{13} \quad \frac{6.0}{11} \quad \frac{5.8}{10} \quad \frac{5.6}{5.8} \quad \frac{5.8}{10} \quad \frac{5.8}{14} \quad \frac{6.5}{19}$$

$$\checkmark \quad \frac{6.4}{18} \quad \frac{6.2}{14} \quad \frac{6.1}{11} \quad \frac{6.0}{10} \quad \frac{5.8}{5.8} \quad \frac{6.0}{10} \quad \frac{6.1}{13} \quad \frac{5.8}{15} \quad \frac{6.3}{18}$$

$$\checkmark \quad \frac{6.4}{19} \quad \frac{6.3}{14} \quad \frac{6.3}{10} \quad \frac{6.1}{5.8} \quad \frac{6.1}{10} \quad \frac{6.1}{11} \quad \frac{5.9}{14} \quad \frac{5.8}{17}$$

$$\checkmark \quad \frac{6.2}{19} \quad \frac{6.0}{13} \quad \frac{6.0}{10} \quad \frac{5.7}{5.7} \quad \frac{5.7}{10} \quad \frac{5.7}{11} \quad \frac{5.3}{15} \quad \frac{5.4}{18}$$

$$\checkmark \quad \frac{5.6}{19} \quad \frac{5.3}{13} \quad \frac{5.3}{10} \quad \frac{5.1}{5.1} \quad \frac{5.0}{10} \quad \frac{4.9}{13} \quad \frac{5.7}{22}$$

$$\checkmark \quad (5.3) \quad \frac{13.8}{34} \quad \frac{14.8}{41} \quad \frac{17.1}{60}$$

$$\checkmark \quad (5.5) \quad \frac{14.2}{31} \quad \frac{14.9}{36} \quad \frac{17.3}{60}$$

$$\checkmark \quad (5.8) \quad \frac{12.8}{28} \quad \frac{15.2}{33} \quad \frac{17.2}{50}$$

$$\checkmark \quad (5.9) \quad \frac{15.0}{32} \quad \frac{17.5}{50}$$

$$\checkmark \quad \frac{14.7}{30} \quad \frac{14.7}{40} \quad \frac{13.4}{31} \quad (6.2) \quad \frac{13.7}{28} \quad \frac{15.3}{30} \quad \frac{17.5}{50}$$

$$\checkmark \quad \frac{15.4}{50} \quad \frac{15.0}{40} \quad \frac{13.7}{30} \quad (6.4) \quad \frac{14.2}{28} \quad \frac{15.2}{30} \quad \frac{17.7}{50}$$

$$\checkmark \quad \frac{15.2}{54} \quad \frac{14.9}{32} \quad \frac{13.7}{29} \quad (6.9) \quad \frac{13.6}{26} \quad \frac{15.0}{29} \quad \frac{17.5}{50}$$

*

STA + π - ELEV

873.70.

667

89+75 SECTION $\phi 30'' \times 56''$ C.M X DRAIN

90+00

66.5

+50

66.2

91+00

66.6

+50

67.2

92+00

68.4

+20

68.6

+36

68.8

+50

69.0

93+00

69.4

+38

69.8

+61

70.1

LT

4

RT

$$\checkmark \quad \begin{array}{ccccccc} & & & F.L & & & \\ 16.4 & 16.8 & 16.5 & 17.4 & 14.8 & 14.4 & 17.40 & 16.1 & 16.4 \\ 50 & 40 & 27 & 26 & 25 & 27 & 29 & 30 & 50 \end{array} \quad (70)$$

$$\checkmark \quad \begin{array}{ccccccc} 18.0 & 17.7 & 15.3 & 14.4 & 13.9 & 15.1 & 17.7 \\ 50 & 45 & 31 & 28 & 28 & 32 & 50 \end{array} \quad (72)$$

$$\checkmark \quad \begin{array}{ccccccc} 17.8 & 17.3 & 16.4 & 13.8 & 14.0 & 15.1 & 17.7 \\ 50 & 44 & 32 & 29 & 27-29 & 30 & 50 \end{array} \quad (75)$$

$$\checkmark \quad \begin{array}{ccccccc} 16.1 & 16.1 & 15.4 & 14.0 & 12.8 & 13.9 & 15.5 & 17.6 \\ 50 & 43 & 40 & 36 & 28 & 27 & 29 & 30 & 50 \end{array} \quad (71)$$

$$\checkmark \quad \begin{array}{ccccccc} 15.3 & 14.9 & 13.7 & 13.7 & 15.2 & 12.4 \\ 50 & 38 & 31 & 28-30 & 31 & 50 \end{array} \quad (65)$$

$$\checkmark \quad \begin{array}{ccccccccccccccc} 13.5 & 12.8 & 5.9 & 5.5 & 5.6 & 5.3 & 5.4 & 5.5 & 5.4 & 1.43 & 15.4 & 16.3 \\ 50 & 33 & 19 & 12 & 10 & 5.3 & 10 & 13 & 19 & 26 & 37-39 & 40 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccccccccccc} 11.2 & 11.3 & 16.3 & 9.8 & 6.0 & 5.3 & 5.3 & 5.2 & 5.2 & 6.3 & 7.8 & 14.3 & 15.4 & 16.5 \\ 50 & 45 & 33 & 29 & 19 & 14 & 10 & 5.1 & 10 & 14 & 18 & 22 & 42-44 & 46 & 60 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccccccccccc} 5.0 & 4.7 & 4.1 & 4.0 & 4.9 & 4.2 & 5.1 & 5.0 & 4.9 & 5.1 & 7.1 & 8.1 & 10.9 & 11.6 & 13.6 & 15.3 & 16.1 \\ 50 & 43 & 37 & 33 & 29 & 22 & 24 & 14 & 10 & 13 & 20 & 34 & 38 & 44 & 47 & 52 & 60 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccccccccccc} 4.2 & 3.4 & 6.3 & 4.9 & 4.8 & 4.8 & 5.3 & 7.4 & 8.2 & 9.5 & 11.7 & 13.9 & 14.2 \\ 50 & 30 & 24-21 & 15 & 10 & 4.7 & 10 & 11 & 15 & 20 & 29 & 38 & 45 & 52 & 58 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccccccccccc} 3.3 & 3.1 & 5.9 & 6.0 & 4.5 & 4.4 & 4.3 & 4.4 & 4.6 & 6.3 & 7.5 & 8.7 & 9.7 \\ 50 & 31 & 26 & 19 & 15 & 10 & 10 & 16 & 14 & 22 & 28 & 36 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccccccccccc} 2.9 & 2.8 & 5.4 & 4.4 & 3.9 & 3.9 & 3.9 & 4.2 & 6.2 & 7.2 & 9.7 & 10.2 & 9.7 \\ 50 & 30 & 25-20 & 16 & 17 & 10 & 3.9 & 10 & 14 & 22 & 28 & 34 & 42 & 50 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccccccccccc} 2.9 & 2.7 & 5.4 & 5.9 & 3.8 & 3.7 & 4.0 & 4.5 & 6.2 & 4.4 & 8.7 & 9.1 & 9.3 \\ 50 & 29 & 24-21 & 15 & 10 & 3.6 & 10 & 14 & 19 & 23 & 28 & 32 & 41 & 45 & 50 \end{array}$$

STA	+	π	-	ELEV
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873.70.

94+00

70.3

+41

70.6

+50

70.6

+62

70.8

95+00

70.9

T.P.

6.13

877.13.

2.70

871.00.

+50

71.2

96+00

71.1

+50

71.3

97+00

71.4

B.M.

5.47

877.13.

5.47

871.66.

+50

71.8

+73

71.9

98+00

72.0

LT

♀

RT

$$\checkmark \quad \begin{array}{cccccccc} 2.6 & 2.5 & 4.2 & 4.4 & 3.7 & 3.5 & 3.5 & 3.4 \\ 50 & 28 & 24 & 19 & 15 & 12 & 10 & 10 \end{array} \quad \begin{array}{cccccccc} 3.5 & 4.8 & 5.8 & 6.1 & 4.4 & 5.1 & 9.3 & 9.6 \\ 10 & 14 & 20 & 22 & 28 & 32 & 37 & 44 \end{array} \quad \begin{array}{c} 3.1 \\ 50 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} 2.0 & 2.3 & 4.2 & 3.3 & 3.2 & 3.2 & 3.5 & 4.2 \\ 50 & 29 & 22-20 & 15 & 10 & 3.1 & 10 & 11 \end{array} \quad \begin{array}{cccccccc} 5.7 & 6.2 & 5.5 & 6.5 & 8.8 & 9.1 & 5.1 & 5.5 \\ 15 & 24 & 32-34 & 41 & 44 & 5.1 & 5.5 & 5.5 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} 1.8 & 1.8 & 1.8 & 4.1 & 3.4 & 3.2 & 3.1 & 3.1 \\ 50 & 36 & 38 & 22-19 & 15 & 10 & 3.1 & 10 \end{array} \quad \begin{array}{cccccccc} 3.5 & 5.3 & 7.6 & 9.0 & 3.1 & 3.5 & 5.3 & 7.6 \\ 10 & 13 & 24 & 37 & 50 & 10 & 13 & 24 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} 1.9 & 1.7 & 4.1 & 3.2 & 3.1 & 2.9 & 3.0 & 3.6 \\ 50 & 29 & 22-18 & 14 & 10 & 2.9 & 10 & 15 \end{array} \quad \begin{array}{cccccccc} 4.6 & 4.2 & 5.7 & 9.1 & 4.6 & 4.2 & 5.7 & 9.1 \\ 15 & 28 & 37 & 39 & 46 & 50 & 15 & 28 \end{array}$$

$$\checkmark \quad \begin{array}{cccccccc} 1.9 & 1.8 & 3.6 & 3.2 & 2.9 & 2.9 & 2.8 & 2.9 \\ 50 & 27 & 22-19 & 15 & 13 & 10 & 2.8 & 10 \end{array} \quad \begin{array}{cccccccc} 4.0 & 5.4 & 5.4 & 5.4 & 4.7 & 2.3 & 9.4 & 9.4 \\ 10 & 14 & 19 & 23 & 34 & 39 & 42 & 45 \end{array}$$

$$\begin{array}{cccccccc} 5.4 & 4.9 & 6.9 & 6.3 & 6.1 & 6.0 & 6.1 & 6.5 \\ 50 & 25 & 20 & 18 & 15 & 10 & 5.9 & 10 \end{array} \quad \begin{array}{cccccccc} 7.2 & 7.1 & 6.8 & 6.0 & 6.1 & 6.5 & 7.0 & 7.2 \\ 10 & 13 & 16 & 21 & 24 & 36 & 50 & 50 \end{array}$$

$$\begin{array}{cccccccc} 5.7 & 5.3 & 7.1 & 6.6 & 6.3 & 6.0 & 6.2 & 7.9 \\ 50 & 26 & 21-18 & 15 & 10 & 6.0 & 10 & 13 \end{array} \quad \begin{array}{cccccccc} 7.9 & 7.4 & 7.1 & 7.1 & 7.4 & 7.1 & 7.9 & 7.4 \\ 19 & 22 & 27 & 27 & 27 & 27 & 27 & 27 \end{array}$$

$$\begin{array}{cccccccc} 5.5 & 5.7 & 7.5 & 6.8 & 6.3 & 5.8 & 5.9 & 6.0 \\ 50 & 27 & 20-18 & 14 & 10 & 5.8 & 10 & 11 \end{array} \quad \begin{array}{cccccccc} 6.1 & 7.1 & 6.6 & 6.1 & 7.1 & 6.6 & 6.1 & 7.1 \\ 13 & 17 & 50 & 13 & 17 & 50 & 13 & 17 \end{array}$$

$$\begin{array}{cccccccc} 5.3 & 5.3 & 7.0 & 6.2 & 6.0 & 5.7 & 5.9 & 6.2 \\ 50 & 25 & 21-18 & 15 & 10 & 5.7 & 10 & 13 \end{array} \quad \begin{array}{cccccccc} 6.2 & 6.2 & 6.0 & 6.2 & 6.2 & 6.2 & 6.2 & 6.0 \\ 27 & 27 & 50 & 27 & 27 & 27 & 27 & 50 \end{array}$$

SPIKIN P.P. #84 FRONT LINDEN HAME

$$\begin{array}{cccccccc} 5.0 & 4.7 & 5.3 & 6.2 & 5.4 & 5.4 & 5.4 & 5.5 \\ 50 & 29 & 25 & 24-19 & 14 & 10 & 5.3 & 10 \end{array} \quad \begin{array}{cccccccc} 6.2 & 7.2 & 6.7 & 6.5 & 6.2 & 7.2 & 6.7 & 6.5 \\ 12 & 16 & 19 & 35 & 50 & 12 & 16 & 19 \end{array}$$

$$\begin{array}{cccccccc} 4.6 & 4.4 & 5.9 & 5.3 & 5.2 & 5.3 & 5.3 & 5.2 \\ 50 & 28 & 23-21 & 16 & 12 & 10 & 5.2 & 10 \end{array} \quad \begin{array}{cccccccc} 5.5 & 8.1 & 7.9 & 6.4 & 4.8 & 5.5 & 8.1 & 7.9 \\ 15 & 24 & 33 & 44 & 50 & 15 & 24 & 33 \end{array}$$

$$\begin{array}{cccccccc} 4.4 & 4.3 & 5.9 & 5.2 & 5.1 & 5.1 & 5.2 & 5.1 \\ 50 & 28 & 23-21 & 16 & 13 & 10 & 5.1 & 10 \end{array} \quad \begin{array}{cccccccc} 5.4 & 5.9 & 7.3 & 4.6 & 1.8 & 5.4 & 5.9 & 7.3 \\ 15 & 18 & 22 & 24 & 28 & 50 & 15 & 18 \end{array}$$

STA	+	π	-	ELEV
		877.13.		
98+50				72.2
+80				72.3
+87				72.2
99+00				72.2
+07				72.3
+20				72.3
+50				72.3
100+00				72.2
+50				72.0
101+00				71.8
T.P.	4.37	876.30.	5.20	871.93.
+50				71.4
102+00				71.3
B.M	5.27.	877.85.	3.12	872.58. (872.58.

LT

2

RT

$\frac{4.0}{50}$ $\frac{4.1}{28}$ $\frac{6.0}{23}$ $\frac{6.3}{22-19}$ $\frac{4.8}{14}$ $\frac{4.9}{10}$ $\frac{4.9}{10}$ $\frac{4.8}{14}$ $\frac{5.0}{16}$ $\frac{5.7}{21-23}$ $\frac{5.1}{26}$ $\frac{3.2}{33}$ $\frac{3.3}{50}$

$\frac{4.2}{50}$ $\frac{4.3}{27}$ $\frac{5.8}{23-21}$ $\frac{5.0}{16}$ $\frac{4.7}{13}$ $\frac{4.9}{10}$ $\frac{4.8}{10}$ $\frac{4.9}{10}$ $\frac{4.8}{16}$ $\frac{4.8}{22}$ $\frac{2.8}{30}$ $\frac{3.1}{50}$

$\frac{4.2}{50}$ $\frac{4.4}{27}$ $\frac{5.9}{23-21}$ $\frac{4.6}{14}$ $\frac{5.0}{10}$ $\frac{4.9}{10}$ $\frac{5.0}{10}$ $\frac{4.7}{29}$ $\frac{4.3}{35}$ $\frac{4.0}{50}$

$\frac{4.1}{50}$ $\frac{4.2}{27}$ $\frac{5.2}{24-22}$ $\frac{4.8}{14}$ $\frac{4.9}{10}$ $\frac{4.9}{10}$ $\frac{4.9}{10}$ $\frac{4.5}{16}$ $\frac{4.2}{38}$ $\frac{4.2}{50}$

$\frac{4.1}{50}$ $\frac{4.2}{27}$ $\frac{5.2}{24-22}$ $\frac{4.8}{14}$ $\frac{4.9}{10}$ $\frac{4.8}{10}$ $\frac{4.9}{10}$ $\frac{4.7}{14}$ $\frac{4.6}{33}$ $\frac{4.2}{50}$

$\frac{4.0}{50}$ $\frac{4.0}{27}$ $\frac{5.6}{24-22}$ $\frac{5.0}{18}$ $\frac{4.9}{13}$ $\frac{4.9}{10}$ $\frac{4.8}{10}$ $\frac{4.9}{10}$ $\frac{4.8}{15}$ $\frac{4.2}{18}$ $\frac{3.4}{34}$ $\frac{0.8}{34}$

FLOOR
HAUCE

$\frac{4.0}{50}$ $\frac{4.0}{29}$ $\frac{5.8}{23-21}$ $\frac{5.0}{15}$ $\frac{4.8}{12}$ $\frac{4.8}{10}$ $\frac{4.8}{10}$ $\frac{4.9}{10}$ $\frac{4.5}{13}$ $\frac{4.2}{19}$ $\frac{3.0}{33}$ $\frac{3.1}{32}$ $\frac{3.1}{50}$

$\frac{4.0}{50}$ $\frac{3.7}{33}$ $\frac{4.4}{27}$ $\frac{4.2}{21-19}$ $\frac{5.2}{15}$ $\frac{5.0}{10}$ $\frac{4.9}{10}$ $\frac{5.0}{10}$ $\frac{4.9}{15}$ $\frac{5.2}{22}$ $\frac{4.5}{29}$ $\frac{3.7}{40}$ $\frac{3.2}{50}$

*

$\frac{4.0}{50}$ $\frac{4.1}{30}$ $\frac{4.6}{26}$ $\frac{6.2}{23-21}$ $\frac{5.2}{17}$ $\frac{5.0}{12}$ $\frac{5.1}{10}$ $\frac{5.1}{10}$ $\frac{5.1}{12}$ $\frac{5.9}{18}$ $\frac{6.8}{24}$ $\frac{6.9}{29}$ $\frac{5.6}{42}$ $\frac{4.8}{50}$

$\frac{4.3}{50}$ $\frac{4.2}{31}$ $\frac{4.9}{26}$ $\frac{5.9}{23-21}$ $\frac{5.4}{17}$ $\frac{5.3}{11}$ $\frac{5.4}{10}$ $\frac{5.3}{10}$ $\frac{5.3}{10}$ $\frac{5.3}{13}$ $\frac{5.8}{17}$ $\frac{7.8}{23}$ $\frac{7.9}{34}$ $\frac{8.0}{50}$

$\frac{3.3}{50}$ $\frac{3.5}{31}$ $\frac{3.8}{27}$ $\frac{5.6}{21-19}$ $\frac{5.3}{17}$ $\frac{5.1}{13}$ $\frac{5.0}{10}$ $\frac{4.9}{10}$ $\frac{4.8}{11}$ $\frac{5.2}{16}$ $\frac{7.7}{23}$ $\frac{10.8}{32}$ $\frac{11.5}{50}$

$\frac{3.9}{50}$ $\frac{4.2}{30}$ $\frac{5.6}{25}$ $\frac{6.1}{19}$ $\frac{5.6}{17}$ $\frac{5.3}{14}$ $\frac{5.2}{10}$ $\frac{5.0}{10}$ $\frac{5.1}{10}$ $\frac{5.1}{11}$ $\frac{5.4}{16}$ $\frac{7.8}{23}$ $\frac{11.3}{34}$ $\frac{12.4}{50}$

TOP MONT KELLER PKWY + EDGERTON

STA	+	π	-	ELEV
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877.85.

102+50				71.3
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103				71.3
-----	--	--	--	------

+20				71.2
-----	--	--	--	------

+30				71.2
-----	--	--	--	------

+50				71.3
-----	--	--	--	------

104				71.5
-----	--	--	--	------

+50				71.9
-----	--	--	--	------

+80				72.1
-----	--	--	--	------

105				72.2
-----	--	--	--	------

+15				72.4
-----	--	--	--	------

+32				72.6
-----	--	--	--	------

& KERLER PKWY RT

LITTLE CANADIAN LT

+55				72.9
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LT

Q

RT

$\frac{5.8}{50}$ $\frac{6.3}{32}$ $\frac{8.4}{25}$ $\frac{6.9}{28}$ $\frac{6.7}{15}$ $\frac{6.7}{10}$ $\frac{6.6}{10}$ $\frac{6.6}{10}$ $\frac{7.0}{15}$ $\frac{9.5}{22}$ $\frac{13.1}{32}$ $\frac{14.2}{43}$ $\frac{14.3}{50}$

$\frac{6.1}{50}$ $\frac{6.9}{30}$ $\frac{9.0}{24}$ $\frac{7.0}{20}$ $\frac{6.8}{15}$ $\frac{6.6}{10}$ $\frac{6.7}{10}$ $\frac{6.7}{12}$ $\frac{7.1}{16}$ $\frac{9.8}{24}$ $\frac{13.4}{34}$ $\frac{14.9}{50}$

$\frac{6.4}{50}$ $\frac{7.1}{39}$ $\frac{9.9}{25}$ $\frac{7.0}{21}$ $\frac{6.8}{16}$ $\frac{6.7}{10}$ $\frac{6.8}{10}$ $\frac{6.8}{11}$ $\frac{7.2}{17}$ $\frac{12.5}{31}$ $\frac{14.6}{39}$ $\frac{15.7}{50}$

$\frac{11.7}{50}$ $\frac{12.0}{43}$ $\frac{11.8}{32}$ $\frac{10.7}{27}$ $\frac{7.0}{17}$ $\frac{6.8}{12}$ $\frac{6.7}{10}$ $\frac{6.7}{10}$ $\frac{6.7}{11}$ $\frac{7.0}{16}$ $\frac{10.0}{23}$ $\frac{15.1}{38}$ $\frac{16.1}{50}$

$\frac{11.5}{50}$ $\frac{12.2}{37}$ $\frac{11.1}{29}$ $\frac{6.8}{15}$ $\frac{6.6}{11}$ $\frac{6.6}{10}$ $\frac{6.6}{10}$ $\frac{6.7}{10}$ $\frac{6.7}{11}$ $\frac{7.1}{16}$ $\frac{11.9}{28}$ $\frac{15.5}{38}$ $\frac{16.5}{50}$

$\frac{9.8}{50}$ $\frac{11.1}{33}$ $\frac{9.1}{25}$ $\frac{6.5}{17}$ $\frac{6.4}{12}$ $\frac{6.5}{10}$ $\frac{6.4}{10}$ $\frac{6.5}{10}$ $\frac{6.6}{11}$ $\frac{7.0}{16}$ $\frac{10.2}{24}$ $\frac{14.8}{34}$ $\frac{16.6}{50}$

$\frac{8.2}{50}$ $\frac{9.4}{45}$ $\frac{8.3}{40}$ $\frac{7.6}{27}$ $\frac{6.8}{20}$ $\frac{6.0}{11}$ $\frac{6.1}{10}$ $\frac{6.0}{10}$ $\frac{6.1}{10}$ $\frac{6.1}{11}$ $\frac{6.4}{17}$ $\frac{9.1}{23}$ $\frac{12.2}{30}$ $\frac{15.9}{39}$ $\frac{16.4}{50}$

$\frac{10.6}{50}$ $\frac{10.2}{44}$ $\frac{6.8}{40}$ $\frac{7.7}{34}$ $\frac{6.3}{26}$ $\frac{6.0}{19}$ $\frac{6.0}{15}$ $\frac{5.8}{10}$ $\frac{5.8}{10}$ $\frac{5.9}{10}$ $\frac{5.9}{11}$ $\frac{6.0}{18}$ $\frac{9.4}{26}$ $\frac{15.5}{39}$ $\frac{15.8}{50}$

$\frac{9.9}{60}$ $\frac{9.2}{50}$ $\frac{6.2}{37}$ $\frac{5.6}{32}$ $\frac{6.0}{30}$ $\frac{5.7}{18}$ $\frac{5.7}{10}$ $\frac{5.7}{10}$ $\frac{5.8}{13}$ $\frac{5.9}{18}$ $\frac{6.3}{20}$ $\frac{6.1}{28}$ $\frac{6.7}{31}$ $\frac{8.7}{40}$ $\frac{12.7}{50}$

$\frac{5.0}{60}$ $\frac{5.4}{47}$ $\frac{5.7}{44}$ $\frac{5.1}{24}$ $\frac{5.3}{16}$ $\frac{5.4}{10}$ $\frac{5.5}{10}$ $\frac{5.6}{10}$ $\frac{5.6}{11}$ $\frac{6.1}{21}$ $\frac{6.7}{29}$ $\frac{6.4}{31}$ $\frac{7.5}{50}$

$\frac{4.5}{50}$ $\frac{4.8}{30}$ $\frac{5.0}{18}$ $\frac{5.2}{10}$ $\frac{5.3}{5.3}$ $\frac{5.4}{10}$ $\frac{5.7}{22}$ $\frac{6.2}{34}$ $\frac{7.0}{50}$

$\frac{5.0}{50}$ $\frac{4.8}{46}$ $\frac{5.2}{33}$ $\frac{5.7}{30}$ $\frac{5.5}{27}$ $\frac{5.0}{12}$ $\frac{5.0}{10}$ $\frac{5.0}{50}$ $\frac{5.1}{10}$ $\frac{5.1}{11}$ $\frac{5.7}{22}$ $\frac{7.1}{37}$ $\frac{7.0}{42}$ $\frac{7.3}{50}$

STA	+	π	-	ELEV
		877.85.		
105+65				73.1
106				74.1
+18				74.8
+50				75.9
107				77.5
+26				(78.5)
+43				(79.1)
+50				(79.3)
T.P.	12.94	890.15.	0.64	877.21.
107+26				78.5
+43				79.1
+50				79.3
+86				80.3

LT

4

RT

$\frac{8.7}{50}$ $\frac{8.2}{40}$ $\frac{5.6}{29}$ $\frac{5.2}{24}$ $\frac{5.4}{21}$ $\frac{5.1}{16}$ $\frac{4.9}{10}$ 48 $\frac{5.0}{10}$ $\frac{5.0}{12}$ $\frac{5.2}{14}$ $\frac{5.8}{20}$ $\frac{6.5}{29}$ $\frac{6.4}{33}$ $\frac{7.1}{50}$

$\frac{11.7}{50}$ $\frac{11.3}{37}$ $\frac{8.2}{30}$ $\frac{3.9}{20}$ $\frac{3.8}{11}$ $\frac{3.9}{10}$ 3.8 $\frac{4.0}{10}$ $\frac{4.4}{15}$ $\frac{5.4}{24}$ $\frac{6.8}{33}$ $\frac{7.0}{46}$ $\frac{8.2}{52}$ $\frac{13.7}{60}$ $\frac{14.9}{70}$

$\frac{10.0}{50}$ $\frac{9.1}{33}$ $\frac{6.2}{26}$ $\frac{3.3}{19}$ $\frac{3.2}{12}$ $\frac{3.3}{10}$ 3.1 $\frac{3.3}{10}$ $\frac{3.5}{14}$ $\frac{3.9}{19}$ $\frac{6.3}{23}$ $\frac{8.7}{28}$ $\frac{14.4}{41}$ $\frac{15.9}{60}$

$\frac{7.0}{50}$ $\frac{7.7}{36}$ $\frac{6.7}{32}$ $\frac{4.7}{27}$ $\frac{2.7}{22}$ $\frac{2.3}{18}$ $\frac{2.2}{10}$ 2.0 $\frac{2.2}{10}$ $\frac{2.4}{15}$ $\frac{3.7}{19}$ $\frac{7.4}{25}$ $\frac{13.6}{35}$ $\frac{15.5}{50}$ $\frac{15.8}{60}$

$\frac{0.3}{50}$ $\frac{1.4}{35}$ $\frac{1.1}{26}$ $\frac{0.3}{20}$ $\frac{0.5}{11}$ $\frac{0.5}{10}$ 0.4 $\frac{0.8}{10}$ $\frac{1.4}{16}$ $\frac{3.5}{19}$ $\frac{7.2}{24}$ $\frac{9.6}{30}$ $\frac{10.8}{37}$ $\frac{12.0}{42}$ $\frac{13.2}{48}$ $\frac{13.2}{60}$

106 $\frac{3.3}{26}$ $\frac{6.3}{31}$ $\frac{7.5}{38}$ $\frac{8.6}{46}$ $\frac{9.2}{60}$

112 $\frac{4.1}{31}$ $\frac{6.0}{37}$ $\frac{7.3}{47}$ $\frac{8.6}{60}$

114 $\frac{0.7}{27}$ $\frac{1.8}{40}$ $\frac{4.4}{46}$ $\frac{6.2}{53}$ $\frac{7.2}{60}$

$\frac{9.7}{50}$ $\frac{10.6}{39}$ $\frac{12.0}{24}$ $\frac{12.2}{18}$ $\frac{11.9}{14}$ $\frac{11.8}{12}$ $\frac{11.9}{10}$ 11.7 $\frac{11.9}{10}$ $\frac{11.0}{13}$ $\frac{12.2}{17}$ $\frac{12.9}{21}$

$\frac{6.9}{50}$ $\frac{9.0}{27}$ $\frac{11.5}{22}$ $\frac{11.6}{19}$ $\frac{11.2}{14}$ $\frac{11.2}{10}$ 11.1 $\frac{11.2}{10}$ $\frac{11.2}{13}$ $\frac{11.2}{16}$ $\frac{12.8}{20}$ $\frac{13.4}{25}$

$\frac{6.3}{50}$ $\frac{6.4}{39}$ $\frac{8.0}{28}$ $\frac{10.4}{23}$ $\frac{11.2}{19}$ $\frac{11.1}{15}$ $\frac{11.0}{10}$ 10.9 $\frac{11.0}{10}$ $\frac{11.0}{13}$ $\frac{11.3}{16}$ $\frac{11.8}{20}$ $\frac{12.7}{24}$

$\frac{0.8}{60}$ $\frac{2.3}{42}$ $\frac{2.0}{38}$ $\frac{3.1}{29}$ $\frac{8.8}{19}$ $\frac{10.1}{16}$ $\frac{10.0}{10}$ 9.9 $\frac{10.1}{10}$ $\frac{10.1}{12}$ $\frac{10.0}{15}$ $\frac{10.4}{27}$ $\frac{11.2}{35}$ $\frac{13.0}{49}$ $\frac{15.1}{60}$

STA	+	π	-	ELEV
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890.15

108+00

805

+24 ✓

809

+50

814

+55

815

109 ✓

820

+29

824

+60

82.7

T.P 12.02

901.29

0.88

889.27.

108+00

(80.5)

+24

(80.9)

+50

(814)

+55

(81.5)

109

(82.0)

LT

Q

RT

$\frac{0.1}{32}$	$\frac{6.1}{23}$	$\frac{8.3}{19}$	$\frac{9.4}{14}$	$\frac{9.7}{10}$	$\frac{9.7}{9}$	$\frac{9.8}{10}$	$\frac{9.8}{12}$	$\frac{9.7}{15}$	$\frac{9.8}{26}$	$\frac{10.1}{37}$	$\frac{11.8}{60}$
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$\frac{8.6}{16}$	$\frac{8.8}{14}$	$\frac{9.4}{10}$	$\frac{9.3}{9}$	$\frac{9.4}{10}$	$\frac{9.3}{13}$	$\frac{9.4}{21}$	$\frac{9.9}{40}$	$\frac{8.0}{47}$	$\frac{8.3}{52}$	$\frac{8.2}{60}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{7.5}{18}$	$\frac{8.0}{14}$	$\frac{8.9}{13}$	$\frac{8.9}{10}$	$\frac{8.8}{9}$	$\frac{8.9}{10}$	$\frac{8.9}{13}$	$\frac{9.0}{18}$	$\frac{8.7}{19}$	$\frac{8.7}{28}$	$\frac{7.5}{37}$	$\frac{2.9}{45}$	$\frac{3.7}{50}$	$\frac{5.0}{60}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{7.4}{18}$	$\frac{8.2}{15}$	$\frac{8.8}{14}$	$\frac{8.8}{10}$	$\frac{8.7}{9}$	$\frac{8.8}{10}$	$\frac{8.8}{12}$	$\frac{8.7}{16}$	$\frac{8.1}{19}$	$\frac{6.8}{25}$	$\frac{2.4}{34}$	$\frac{4.0}{40}$	$\frac{2.4}{47}$	$\frac{4.0}{60}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.5}{21}$	$\frac{7.8}{13}$	$\frac{8.2}{10}$	$\frac{8.2}{9}$	$\frac{8.3}{10}$	$\frac{8.4}{12}$	$\frac{8.0}{17}$	$\frac{7.4}{22}$	$\frac{7.0}{26}$	$\frac{4.0}{31}$	$\frac{0.8}{32}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{7.0}{18}$	$\frac{7.3}{15}$	$\frac{7.9}{10}$	$\frac{7.8}{9}$	$\frac{8.0}{10}$	$\frac{8.2}{14}$	$\frac{7.6}{19}$	$\frac{7.8}{26}$	$\frac{7.1}{29}$	$\frac{1.6}{37}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.5}{18}$	$\frac{7.0}{14}$	$\frac{7.6}{12}$	$\frac{7.6}{10}$	$\frac{7.5}{9}$	$\frac{7.6}{10}$	$\frac{7.6}{15}$	$\frac{7.4}{20}$	$\frac{7.3}{31}$	$\frac{7.3}{41}$	$\frac{1.2}{47}$
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$\frac{10.3}{75}$	$\frac{10.6}{60}$	$\frac{11.2}{50}$	(20.8)
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$\frac{7.3}{75}$	$\frac{7.6}{60}$	$\frac{8.1}{50}$	$\frac{8.7}{32}$	(20.4)
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$\frac{4.2}{100}$	$\frac{4.5}{75}$	$\frac{4.8}{62}$	$\frac{5.3}{57}$	$\frac{5.6}{50}$	$\frac{5.3}{44}$	$\frac{6.1}{34}$	(19.9)
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$\frac{3.7}{100}$	$\frac{4.0}{75}$	$\frac{4.2}{60}$	$\frac{4.7}{57}$	$\frac{4.9}{50}$	$\frac{5.0}{44}$	$\frac{6.0}{34}$	(19.8)
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(19.3)

$\frac{9.5}{41}$	$\frac{9.3}{55}$	$\frac{10.7}{75}$	$\frac{11.3}{100}$
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STA	+	π	-	ELEV
		901.29		
109+29	✓			(82.4)
+60				(82.7)
+75				(82.9)
110				(83.0)
+07				(83.0)
+25				(83.0)
+55				(82.8)
111+00				(82.4)
T.P	10.05	908.79	2.55	898.74.
109+00				(82.0)
+29				(82.4)
+60				(82.7)
+75				(82.9)

LT

Q

RT

$$(187) \quad \frac{8.5}{40} \quad \frac{8.6}{60} \quad \frac{8.9}{80} \quad \frac{10.1}{100}$$

$$(186) \quad \frac{7.9}{54} \quad \frac{7.9}{75} \quad \frac{8.7}{100}$$

$$(184) \quad \frac{6.9}{56} \quad \frac{7.3}{75} \quad \frac{8.1}{100}$$

$$(183) \quad \frac{5.7}{46} \quad \frac{5.3}{65} \quad \frac{5.7}{75} \quad \frac{7.1}{100}$$

$$(183) \quad \frac{8.2}{37} \quad \frac{5.6}{41} \quad \frac{5.6}{55} \quad \frac{4.2}{63} \quad \frac{4.9}{73} \quad \frac{6.9}{100}$$

$$(183) \quad \frac{5.7}{57} \quad \frac{4.3}{68-73} \quad \frac{5.2}{80} \quad \frac{6.2}{100}$$

$$(185) \quad \frac{3.1}{36} \quad \frac{2.8}{46} \quad \frac{4.8}{56} \quad \frac{4.0}{74} \quad \frac{5.5}{100}$$

$$(187) \quad \frac{7.0}{32} \quad \frac{5.1}{36} \quad \frac{5.8}{50} \quad \frac{5.7}{62} \quad \frac{4.7}{82} \quad \frac{10.0}{100}$$

$$\frac{6.6}{100} \quad \frac{7.1}{75} \quad \frac{7.7}{58} \quad \frac{7.5}{46} \quad \frac{8.1}{42} \quad (26.8)$$

$$\frac{4.1}{100} \quad \frac{4.8}{75} \quad \frac{4.8}{67} \quad \frac{9.2}{47} \quad (26.4)$$

$$\frac{2.7}{100} \quad \frac{3.4}{75} \quad \frac{3.4}{54} \quad \frac{4.5}{45} \quad (26.1)$$

$$\frac{2.4}{100} \quad \frac{2.5}{80} \quad \frac{2.8}{63} \quad \frac{2.5}{44} \quad (25.9)$$

STA	+	π	-	ELEV
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908.79

110+00

(83.0)

+07

(83.0)

+25

(83.0)

+55

(82.8)

111

(82.4)

+50

(81.6)

T.P	0.93	896.98	12.74	896.05
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112

(80.5)

+50

(79.3)

T.P	1.77	886.93	11.82	885.16
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109+75 ✓

82.9

110

83.0

+07 ✓

83.0

+25

83.0

LT

L

RT

$$\frac{1.6}{100} \quad \frac{2.1}{70} \quad \frac{2.7}{47} \quad (258)$$

$$\frac{2.0}{100} \quad \frac{2.3}{79} \quad \frac{2.4}{47} \quad (258)$$

$$\frac{2.1}{100} \quad \frac{2.2}{75} \quad \frac{2.3}{56} \quad \frac{2.0}{48} \quad (258)$$

$$\frac{2.9}{100} \quad \frac{2.6}{70} \quad \frac{2.2}{48} \quad (260)$$

$$\frac{5.6}{100} \quad \frac{5.4}{70} \quad \frac{4.1}{50} \quad \frac{4.7}{45} \quad (264)$$

$$\frac{11.0}{100} \quad \frac{9.9}{75} \quad \frac{9.3}{53} \quad \frac{9.0}{41} \quad (272) \quad \frac{4.3}{35} \quad \frac{4.6}{44} \quad \frac{4.6}{55} \quad \frac{4.2}{72} \quad \frac{14.9}{100}$$

$$\frac{7.9}{100} \quad \frac{6.2}{75} \quad \frac{5.7}{50} \quad \frac{4.0}{3.7} \quad (165) \quad \frac{8.0}{30} \quad \frac{8.0}{42} \quad \frac{11.6}{56} \quad \frac{12.9}{67} \quad \frac{12.4}{80}$$

$$\frac{17.3}{100} \quad \frac{15.8}{75} \quad \frac{14.2}{60} \quad \frac{13.1}{41} \quad \frac{11.9}{38} \quad (177)$$

$$\frac{3.9}{17} \quad \frac{4.0}{15} \quad \frac{4.9}{11} \quad \frac{4.2}{10} \quad \frac{4.0}{10} \quad \frac{4.1}{10} \quad \frac{4.2}{15} \quad \frac{3.7}{19} \quad \frac{3.6}{24} \quad \frac{4.2}{29} \quad \frac{3.8}{37}$$

$$\frac{3.6}{17} \quad \frac{3.6}{14} \quad \frac{3.9}{11} \quad \frac{4.0}{10} \quad \frac{3.9}{10} \quad \frac{4.0}{10} \quad \frac{3.9}{13} \quad \frac{3.7}{17} \quad \frac{3.2}{18} \quad \frac{2.4}{25} \quad \frac{1.1}{28}$$

$$\frac{3.6}{18-16} \quad \frac{3.9}{15} \quad \frac{3.9}{11} \quad \frac{4.0}{10} \quad \frac{3.9}{10} \quad \frac{4.0}{10} \quad \frac{4.0}{13} \quad \frac{3.3}{17} \quad \frac{2.4}{25}$$

$$\frac{3.7}{18-16} \quad \frac{4.0}{15} \quad \frac{4.0}{10} \quad \frac{3.9}{10} \quad \frac{4.0}{10} \quad \frac{3.8}{14} \quad \frac{3.3}{16} \quad \frac{3.0}{25} \quad \frac{1.0}{28} \quad \frac{+1.4}{37}$$

STA	+	π	-	ELEV
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		886.93		
--	--	--------	--	--

110+55				82.8
--------	--	--	--	------

111+00	✓			82.4
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+50				81.6
-----	--	--	--	------

112				80.5
-----	--	--	--	------

+50				79.3
-----	--	--	--	------

+87				78.4
-----	--	--	--	------

113				78.1
-----	--	--	--	------

T.P	0.47	877.80	9.60	877.33
-----	------	--------	------	--------

+14				77.8
-----	--	--	--	------

+25				77.4
-----	--	--	--	------

+50				76.8
-----	--	--	--	------

114				75.3
-----	--	--	--	------

+50				73.9
-----	--	--	--	------

LT

2

RT

$$\frac{3.2}{17-16} \frac{4.0}{15} \frac{4.2}{10} \frac{4.1}{10} \frac{4.0}{11} \frac{3.8}{16} \frac{3.3}{50}$$

$$\frac{3.6}{18-16} \frac{4.4}{15} \frac{4.6}{10} \frac{4.5}{10} \frac{4.5}{12} \frac{4.5}{16} \frac{4.2}{17} \frac{3.7}{19}$$

$$\frac{5.3}{19} \frac{5.4}{15} \frac{5.4}{10} \frac{5.3}{10} \frac{5.4}{11} \frac{5.3}{18} \frac{5.1}{19} \frac{4.2}{21}$$

$$\frac{6.5}{17} \frac{6.5}{12} \frac{6.6}{10} \frac{6.4}{10} \frac{6.5}{12} \frac{6.6}{15-18} \frac{5.7}{19}$$

$$\frac{7.4}{19} \frac{8.0}{16} \frac{7.2}{13} \frac{7.2}{10} \frac{7.6}{10} \frac{7.6}{10} \frac{7.2}{12} \frac{8.2}{15} \frac{7.7}{19} \frac{4.6}{24} \frac{3.4}{27} \frac{3.1}{31} \frac{3.8}{40} \frac{6.4}{50}$$

$$\frac{12.0}{50} \frac{11.5}{48} \frac{10.7}{34} \frac{9.3}{22} \frac{9.6}{19} \frac{8.9}{16} \frac{8.6}{14} \frac{8.6}{10} \frac{8.5}{10} \frac{8.6}{12} \frac{8.2}{16} \frac{9.3}{22} \frac{8.0}{25} \frac{6.6}{31} \frac{6.4}{37} \frac{7.9}{50}$$

$$\frac{15.2}{50} \frac{12.9}{34} \frac{11.4}{30} \frac{10.4}{25} \frac{9.9}{20} \frac{8.9}{16} \frac{8.9}{11} \frac{9.0}{10} \frac{8.8}{10} \frac{8.9}{10} \frac{9.0}{14} \frac{9.6}{18} \frac{10.0}{21} \frac{9.3}{24} \frac{8.4}{31} \frac{8.0}{39} \frac{8.7}{50}$$

$$\frac{7.2}{50} \frac{6.3}{37} \frac{4.1}{29} \frac{2.5}{22} \frac{0.3}{15} \frac{0.2}{10} \frac{0.1}{10} \frac{0.4}{15} \frac{1.3}{19} \frac{1.6}{23} \frac{0.8}{26} \frac{1.1}{50}$$

$$\frac{10.2}{50} \frac{9.5}{44} \frac{8.6}{37} \frac{7.7}{34} \frac{5.6}{27} \frac{3.0}{21} \frac{0.6}{16} \frac{0.6}{10} \frac{0.5}{10} \frac{0.5}{12} \frac{0.2}{16} \frac{1.1}{23} \frac{2.3}{30} \frac{3.3}{58}$$

$$\frac{12.5}{50} \frac{10.6}{35} \frac{6.5}{24} \frac{1.4}{16} \frac{1.2}{12} \frac{1.2}{10} \frac{1.1}{10} \frac{1.1}{10} \frac{1.4}{11} \frac{1.6}{15} \frac{1.7}{19} \frac{4.3}{26} \frac{6.9}{33} \frac{6.3}{38} \frac{6.3}{50}$$

$$\frac{14.8}{50} \frac{13.3}{36} \frac{9.6}{29} \frac{6.6}{22} \frac{2.9}{16} \frac{2.6}{11} \frac{2.7}{10} \frac{2.5}{10} \frac{2.6}{10} \frac{2.6}{11} \frac{3.0}{16} \frac{4.1}{21} \frac{4.5}{24} \frac{10.5}{35} \frac{11.6}{50}$$

$$\frac{15.3}{50} \frac{13.3}{32} \frac{11.6}{28} \frac{3.9}{14} \frac{4.0}{10} \frac{3.9}{10} \frac{4.0}{10} \frac{4.1}{15} \frac{6.6}{23} \frac{13.2}{35} \frac{15.3}{50}$$

STA	+	π	-	ELEV
		877.80		
115+00		1.41 697		730
+50.				72.5
				72.4
+74		STONE BOX CULV X DRAIN 30" X 48'		
116				72.2
T.P	5.74	876.87	6.67	871.13
+50				718
117				715
+50				716
118				719
+50				728
119				742
+38				752
T.P	9.97	885.31	1.53	875.34
B.M	8.68	885.34	8.68	876.63
				876.66

LT

4

RT

<u>16.5</u>	<u>15.5</u>	<u>14.6</u>	<u>5.1</u>	<u>4.9</u>	<u>4.9</u>	<u>5.1</u>	<u>12.7</u>	<u>15.2</u>	<u>15.8</u>	<u>15.5</u>
54	35	32	15	10	48	10	15	31	36	50

<u>16.1</u>	<u>15.7</u>	<u>14.8</u>	<u>14.0</u>	<u>5.9</u>	<u>5.7</u>	<u>5.6</u>	<u>5.4</u>	<u>5.9</u>	<u>12.6</u>	<u>13.5</u>	<u>15.6</u>
50	46	26	21	18	14	10	5.3	10	15	32	50

F.L

F.L 4 DITCH

<u>16.0</u>	<u>15.2</u>	<u>16.2</u>	<u>16.7</u>	<u>16.8</u>	<u>12.6</u>	<u>5.8</u>	<u>5.7</u>	<u>5.6</u>	<u>5.4</u>	<u>5.5</u>	<u>6.0</u>	<u>16.9</u>	<u>18.1</u>	<u>18.0</u>	<u>16.8</u>	<u>17.0</u>
50	46	38	32	30	28	23	16	13	10	5.4	10	14	23	25	30	50

11.1
100

<u>15.7</u>	<u>14.5</u>	<u>13.7</u>	<u>6.3</u>	<u>6.0</u>	<u>5.8</u>	<u>5.6</u>	<u>5.8</u>	<u>6.0</u>	<u>6.4</u>	<u>13.5</u>	<u>14.5</u>	<u>15.7</u>
50	35	31	17	14	10	56	10	12	15	29	31	50

<u>13.5</u>	<u>12.1</u>	<u>6.0</u>	<u>5.5</u>	<u>5.3</u>	<u>5.3</u>	<u>5.9</u>	<u>6.9</u>	<u>12.3</u>	<u>13.0</u>	<u>13.1</u>
50	42	32	18	14	10	5.1	10	16	19	32

<u>13.6</u>	<u>12.8</u>	<u>12.2</u>	<u>6.2</u>	<u>5.6</u>	<u>5.5</u>	<u>5.5</u>	<u>5.7</u>	<u>6.0</u>	<u>11.1</u>	<u>12.6</u>
50	35	21	18	13	10	5.4	10	13	16	31

<u>13.1</u>	<u>12.1</u>	<u>11.2</u>	<u>6.1</u>	<u>5.7</u>	<u>5.6</u>	<u>5.3</u>	<u>5.5</u>	<u>5.6</u>	<u>6.2</u>	<u>10.8</u>	<u>11.5</u>	<u>12.4</u>
50	34	30	15	12	10	5.3	10	13	18	30	37	50

<u>13.4</u>	<u>12.3</u>	<u>11.8</u>	<u>5.4</u>	<u>5.1</u>	<u>5.1</u>	<u>5.4</u>	<u>10.1</u>	<u>11.3</u>	<u>11.8</u>
50	34	30	15	10	5.0	10	15	28	36

<u>13.5</u>	<u>12.4</u>	<u>11.7</u>	<u>5.5</u>	<u>4.7</u>	<u>4.2</u>	<u>4.1</u>	<u>4.1</u>	<u>4.3</u>	<u>7.7</u>	<u>9.9</u>	<u>10.7</u>
50	34	31	18	15	10	4.1	10	16	23	30	50

<u>12.5</u>	<u>12.4</u>	<u>11.4</u>	<u>10.5</u>	<u>3.3</u>	<u>3.0</u>	<u>2.9</u>	<u>2.9</u>	<u>3.1</u>	<u>8.2</u>	<u>8.6</u>	<u>9.6</u>
50	41	35	32	16	13	10	2.7	10	12	15	27

<u>9.2</u>	<u>8.1</u>	<u>7.7</u>	<u>4.1</u>	<u>1.9</u>	<u>1.8</u>	<u>1.7</u>	<u>1.7</u>	<u>1.7</u>	<u>4.0</u>	<u>4.8</u>	<u>5.3</u>
50	36	24	22	14	10	1.7	10	11	17	22	24

SPK.T.P. LT STA 120+80 POLE 2.

STA	+	π	-	ELEV
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885.34

119+80				761
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120				765
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+50				775
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121				786
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+50				798
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122				800
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+50				825
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123				839
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T.P.	12.12	896.11	1.35	883.99
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+50				856
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124				872
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+50				887
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125				903
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