

BK. 128 Dr. 10

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

Keller Parkway

From Edgerton St., Co. Rd. "C"

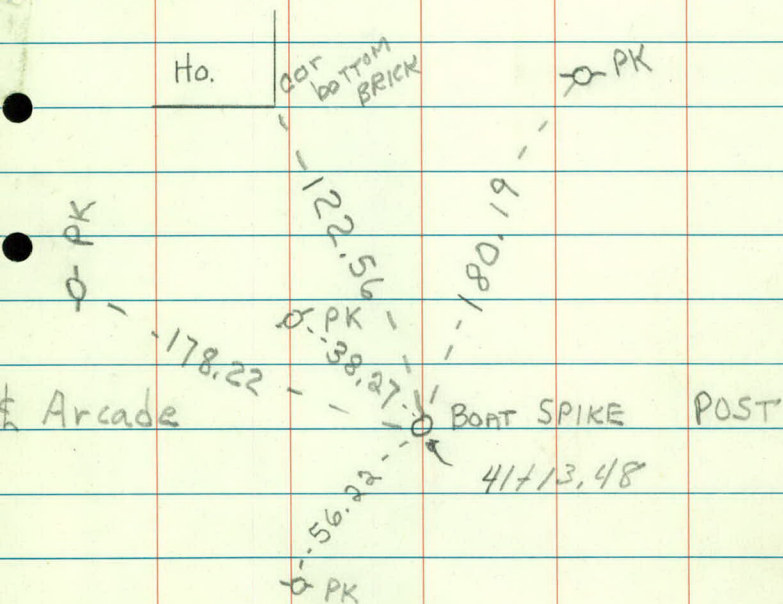
Road Acc't. No.

Date Filed. 2-11-46

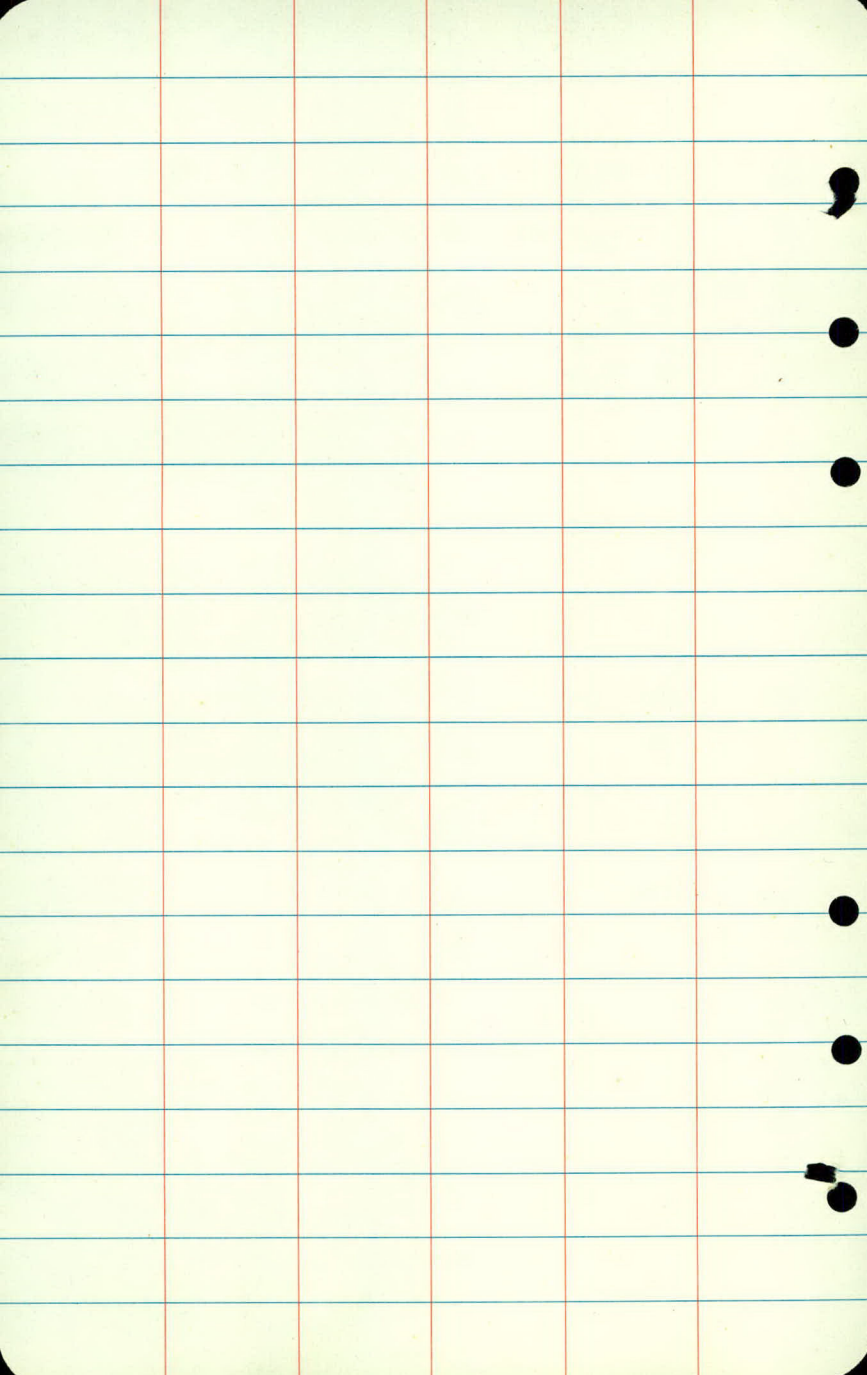
File

KP
DS
RJ
TV

24 MAR 1976 1,
SUNNY 50°



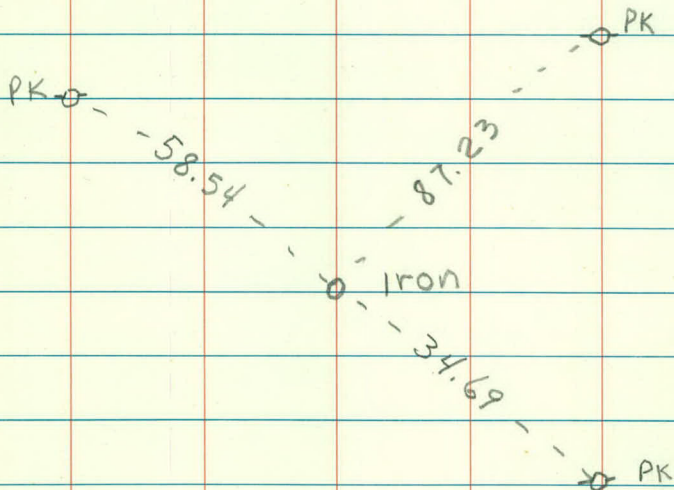
Keller Pkwy



KP
DS
RV
TV

24 MAR 1976 2.

W¹/₄ Cor Sec. 4 - T28 - R23



£ Arcade

curve

STA	POINT	LT	Δ	RT	DATA
-----	-------	----	----------	----	------

6+79⁵⁹

0+00 = KELLER PKWY STA 41+13⁴⁸ P.O.S.T.

KP
DS
RV
TJ

LT

E

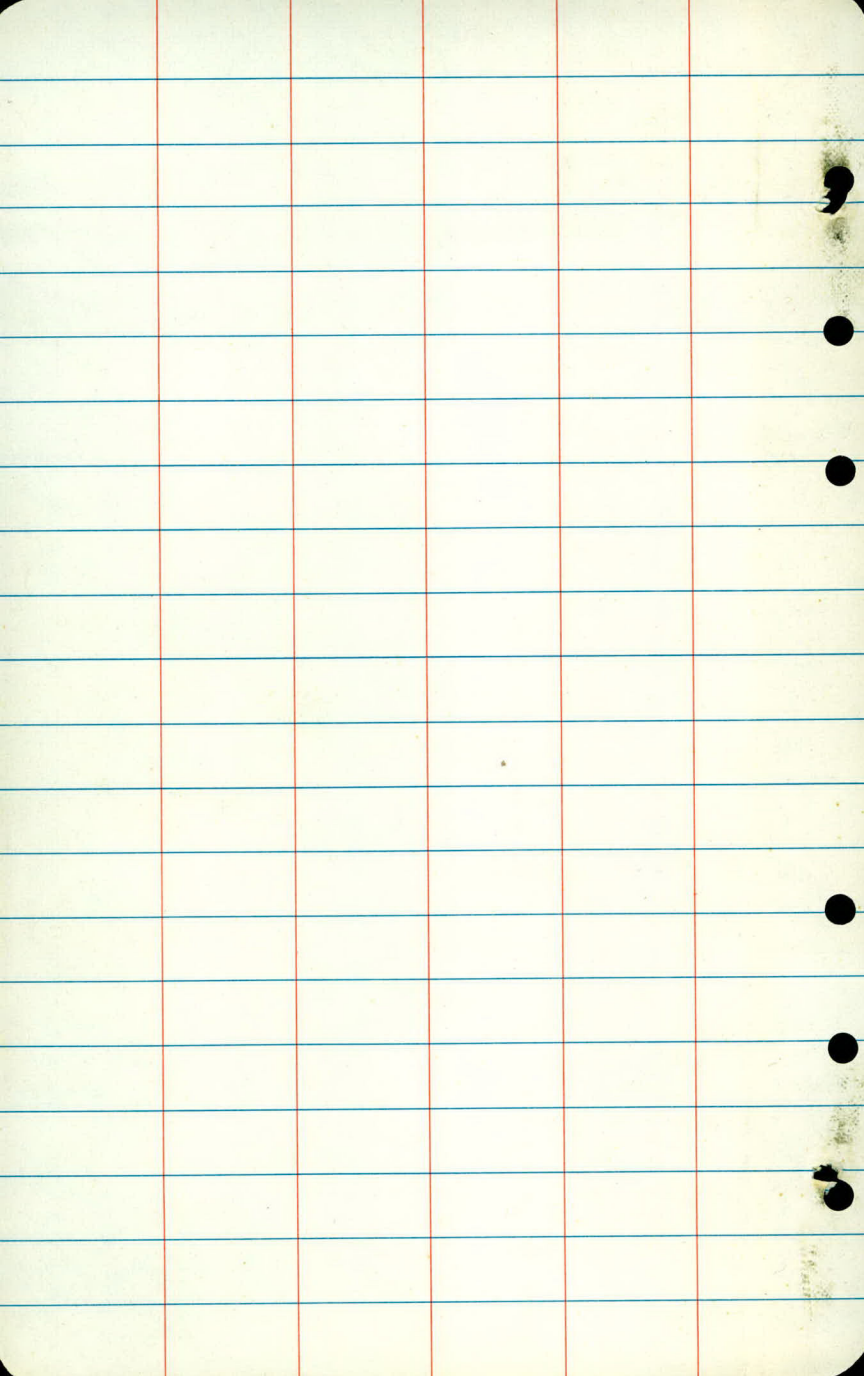
24 MAR 1976

R

3.

W/4 Sec 4-28-23

BOAT SPIKE



Plan Survey
Keller Pky.
From Edgerton to Co Rd C

3-20-44

Index	Pages	ALB	HAW
Align	1 to 12		AM
Topography	13 to 23		LC
Bench Levels	24 to 25		LC
X Sections	26 to 49		CF

Sta	Pt	Def	ALT	ART
-----	----	-----	-----	-----

2+55.37	PT			
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+50				
-----	--	--	--	--

+25				
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2				
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1+84.63	P.I.			
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+75				
-----	--	--	--	--

+50				
-----	--	--	--	--

+25				
-----	--	--	--	--

1				
---	--	--	--	--

0+87.87	PC			
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		67°00'		
--	--	--------	--	--

		D° 40°		
--	--	--------	--	--

		T. 9676		
--	--	---------	--	--

		L 167.50		
--	--	----------	--	--

		R 146.19		
--	--	----------	--	--

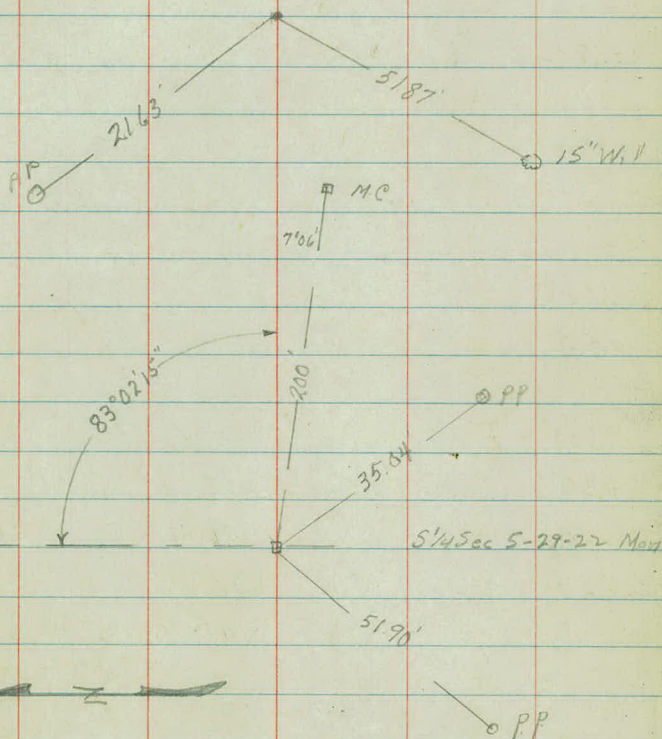
(184.63)

0+00	P.I.			
------	------	--	--	--

		7°06'	£ Edgerton Str	
--	--	-------	----------------	--

Description

Boat Spl



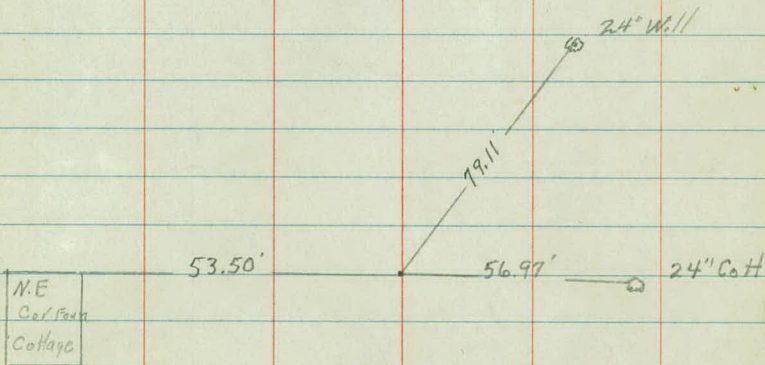
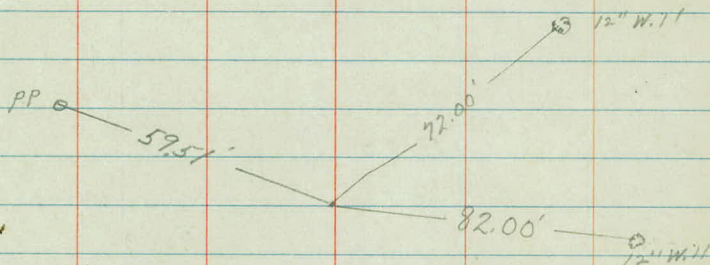
Sta	Pt	Def	ΔL	Air
+6204	P.T	18° 10'		
+50		17° 07' 30"		
8		12° 37' 30"		
7+64.90	P. 1			36° 21'
+50		8° 07' 30"		D 18°
7		3° 37' 30"		T 105.08
6+59.82	P.C	0° 00'		L 202.22
				R 319.623

387.17

+64.23	P.T	10° 15'		
+50		9° 24'		
4		6° 24'		
3+79.90	P. 1		20° 30'	
+50		3° 24'	D 12°	
3		0° 24'	T. 86.50	
2+93.40	P.C	0° 00'	L. 170.83	
			R. 478.339	

221.29

Description



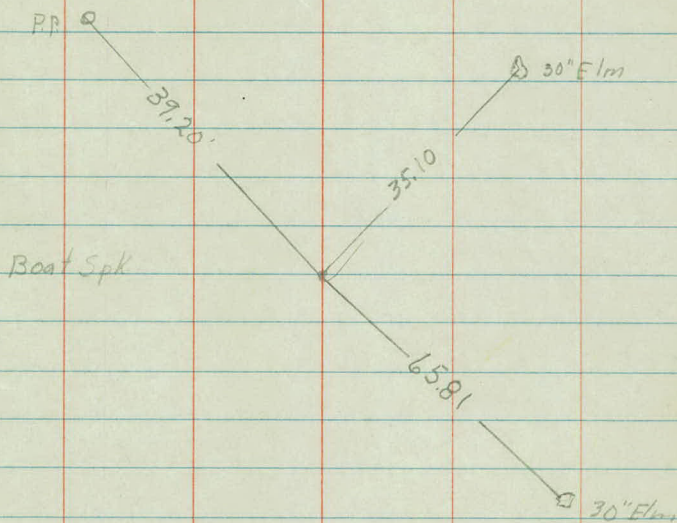
Sta	Pt.	Def	$\Delta Lt.$	ΔRl
+11.26	PT	$4^{\circ}30'$		
21		$4^{\circ}13'30''$		
+50		$2^{\circ}58'30'$		
20+21.47	P1			$9^{\circ}00'$
20		$1^{\circ}43'30'$		$D-5^{\circ}$
+50		$0^{\circ}28'30'$		$T 90.21'$
19+31.26	P.C	$0^{\circ}00'$		$L 180.00$
				$R 1146.28$

736.17'

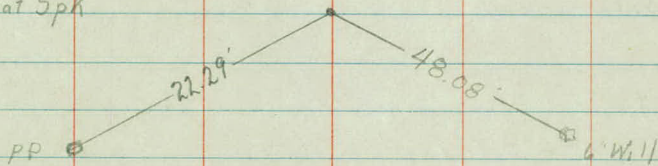
12+85.30 P1 $1^{\circ}30'$

528.34'

Description



Boat Spk



Sta	Pt	Def	Δ L	Δ R
-----	----	-----	-----	-----

24+90.48	P.T	4°00'		
+50		2°23'		

24+40.66	P.I			Δ 8°00'
24		0°23'		D 8°

23+90.48	P.C	0°00'		T 50.12
				L 100.00
				R 716.779

+84.58	P.T	3°58'		
+50		2°36'		

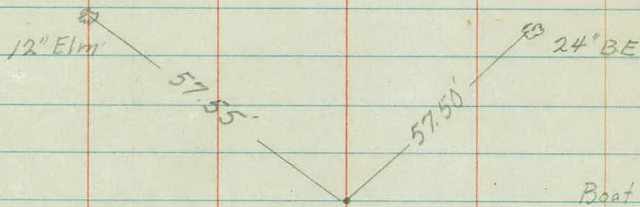
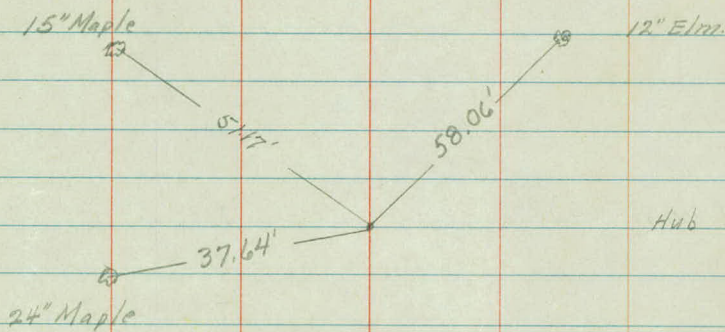
23+35.12	P.I		7°56'	
23		0°36'	D 8°	

22+85.42	P.C	0°00'	T 49.70	
			L 99.16	
			R 716.779	

105.72

314.07

Description



Sta	PT	Def	ΔL	ΔR
+6339	P.T	$15^{\circ}15'$		
+50		$14^{\circ}23'$		
29		$11^{\circ}08'$		
+50		$7^{\circ}53'$		
28+49.19	P.I			$\Delta 30^{\circ}30'$
28		$4^{\circ}38'$		$D 13^{\circ}$
+50		$1^{\circ}23'$		$T 12042$
27+28.77	P.C	$0^{\circ}00'$		$L 234615$
				$R 44168$
+19.51	P.T	$10^{\circ}15'$		
27		$9^{\circ}05'$		
+50		$6^{\circ}05'$		
26+35.18	P.I			$\Delta 20^{\circ}30'$
26		$3^{\circ}05'$		$D 12^{\circ}$
+50		$0^{\circ}05'$		$T 8656'$
25+48.68	P.C	$0^{\circ}00'$		$L 17083$
				$R 478.34$

20482

Description

24" Elm

64.21'

20.52'

Boat Spk

12" Maple

43.16'

R.R. Spk

33.03'

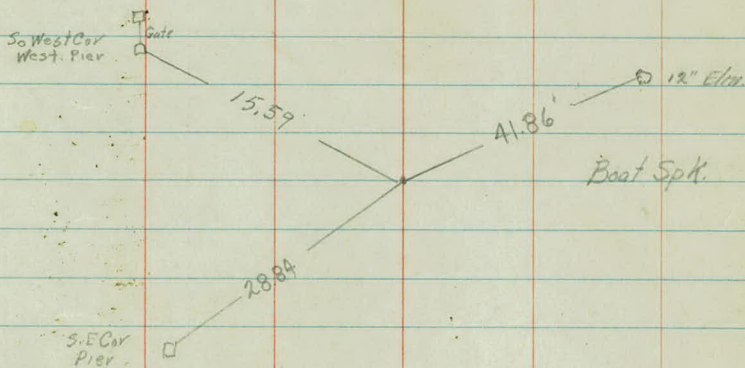
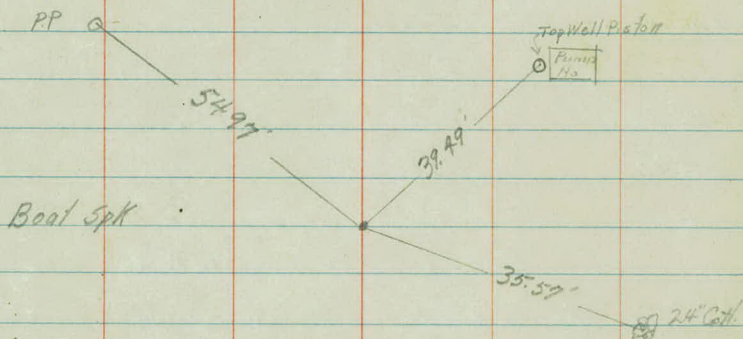
36.26'

20" Maple

24" Catt

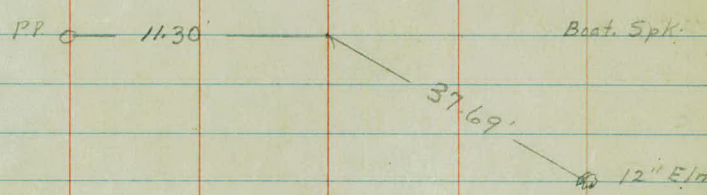
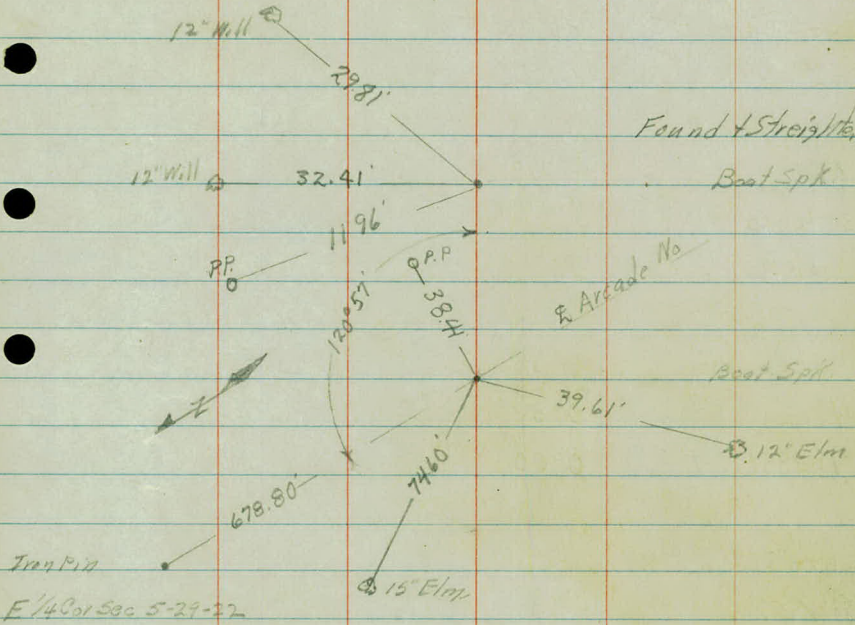
Sta	Rt	Def	ΔL	ΔR
+7170	P.T.	2° 57'		
+50		2° 44'		
35		2° 14'		
+50		1° 44'		
34+24.33	P.I.			$\Delta 5^{\circ} 54'$
34		1° 14'		D 2°
+50		0° 44'		T 142.63
33		0° 14'		L 295.00
32+76.70	P.C.	0° 00'		R 286.93
+46.81	P.T.	6° 00'		
32		4° 57'		
+50		3° 49' 30"		
31+14.00	P.I.			$\Delta 12^{\circ} 00'$
31		2° 42'		D 4° 30'
+50		1° 34' 30"		T 133.86
30		0° 27'		L 266.607
29+80.14	P.C.	0° 00'		R 1273.57

Description



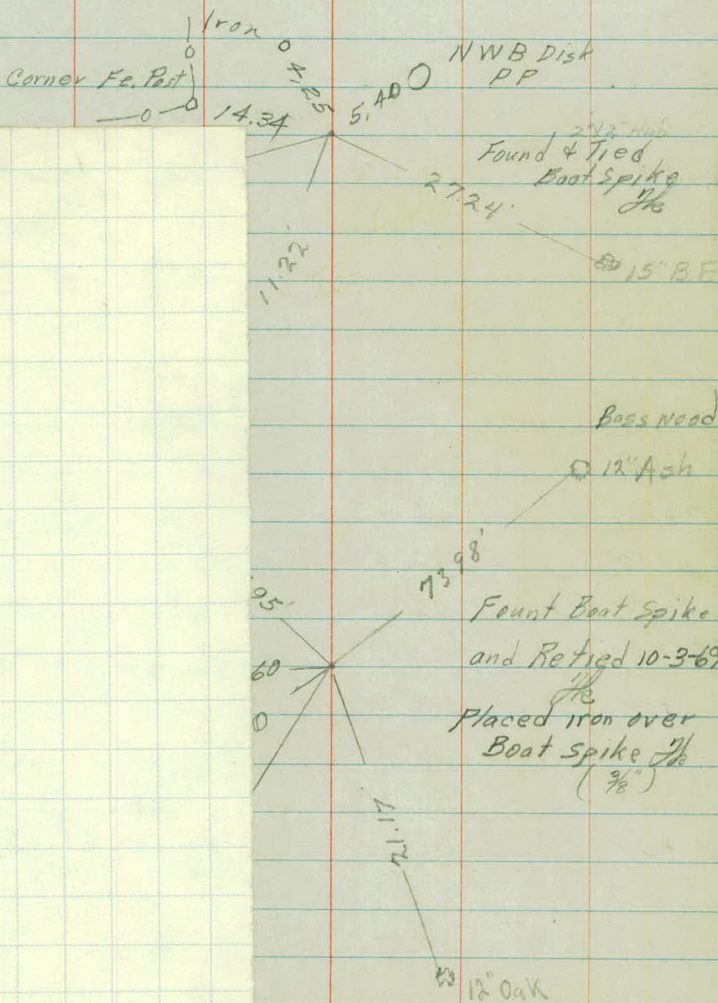
Sta	PT.	Def.	ΔL	ΔR
+16.83	P.T	$19^{\circ}22'$		
42+00		$16^{\circ}58'30''$		
+75		$13^{\circ}24'30''$		
41+52.32	P.I.			$\Delta 38^{\circ}44'$
+50		$9^{\circ}50'30''$		$D 28^{\circ}30'$
+25		$6^{\circ}17'$		$T 71.40'$
				$L 135.91$
41+13.48	POST.			$R 203.125$
41		$2^{\circ}43'$		
40+80.92	P.C	$0^{\circ}00'$		
46				
+34.46	P.T	$6^{\circ}06'$		
39		$4^{\circ}43'$		
38+58.56	P.I			$\Delta 12^{\circ}12'$
+50		$2^{\circ}43'$		$D 8^{\circ}00'$
38		$0^{\circ}43'$		$T 76.60$
37+18.96	P.C	$0^{\circ}00'$		$L 152.50$
				$R 716.779$

Description



Sta	Pt	Def	ΔL	ΔRt
+21.56	P.T	$20^{\circ}43'$		
52		$19^{\circ}23'$		
+50		$16^{\circ}18'$		
51		$13^{\circ}13'$		
50+61.65	P.I			$\Delta 41.26'$
+50		$10^{\circ}08'$		$D^{\circ}12^{\circ}20'$
50		$7^{\circ}03'$		$T 176.04$
+50		$3^{\circ}58'$		$L 335.95'$
49		$0^{\circ}53'$		$R. 465.459$
48+85.61	P.C	$0^{\circ}00'$		
+32.02	P.T.	$18^{\circ}25'$		
+25		$17^{\circ}44'$		
46		$15^{\circ}19'$		
+75		$12^{\circ}54'$		
+50		$10^{\circ}29'$		
45+46.65	P.I		$\Delta 36^{\circ}50'$	
+25		$8^{\circ}04'$	$D^{\circ}19^{\circ}20'$	
45		$5^{\circ}39'$	$T 99.15'$	
+75		$3^{\circ}14'$	$L 190.52'$	
+50		$0^{\circ}49'$	$R 297.768$	
44+41.58	P.C	$0^{\circ}00'$		

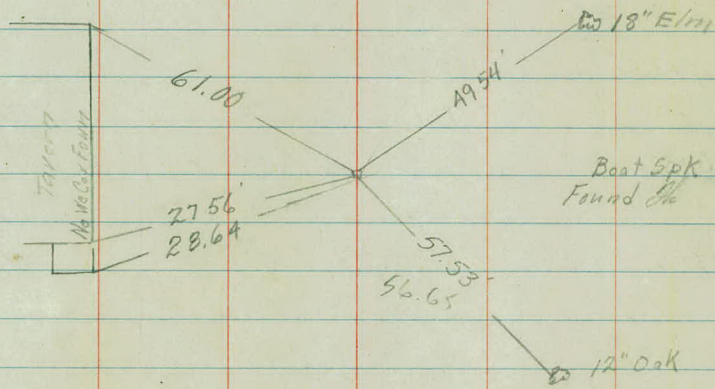
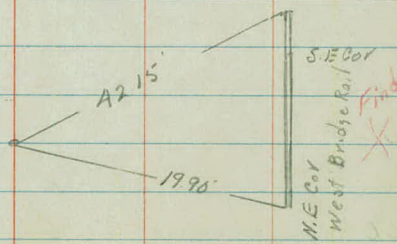
Description



Sta	Pt	Def.	ΔL	ΔR
+40.84	P.T	$7^{\circ}21'$		
57		$5^{\circ}12'30''$		
56+71.32	P.I		$\Delta 14^{\circ}42'$	
+50		$2^{\circ}35'$	$D 10^{\circ}30'$	
56+00.84	P.C P.T	$0^{\circ}00'$	T.70.48	
			L 140.00	
			R 546.438	
+35.80	P.T	$22^{\circ}20'$		
55		$19^{\circ}39'$		
+50		$15^{\circ}54'$		
54		$12^{\circ}09'$		
53+95.39	P.I		$\Delta 44^{\circ}40'$	
+50		$8^{\circ}24'$	D 15°	
53		$4^{\circ}39'$	T 157.37	
+50		$0^{\circ}54'$	L 297.78	
52+38.02	P.C	$0^{\circ}00'$	R 383.065	

Description

Boat Spk



Sta	Pt	Def	ΔL	ΔR
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+39.86	P.T	6°29'		
63		4°53'		

2+59.23	P.I		$\Delta 12^{\circ}58'$	
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+50		2°53'	D 8°00'	
-----	--	-------	---------	--

2		0°53'	T 81.45'	
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1+77.78	P.C	0°00'	L 162.08'	
			R 716.779'	

+93.83	P.T.	3°41'		
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+50		2°22'		
-----	--	-------	--	--

60+32.55	P.I		$\Delta 7^{\circ}22'$	
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60		0°52'	D 6°00'	
----	--	-------	---------	--

59+71.05	P.C	0°00'	T 61.497'	✓
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			L 122.778'	
--	--	--	------------	--

			R 955.366'	7/16
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Description

Boat Spk.

35.34' 12" Elm

20.65' 8" Elm

same

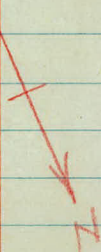
56.57' 56.53' 12" Oak

Boat Spk.

45.29' 45.21' 21.42' 21.34' 12" Elm

same P.I.

PP



Sta

pt

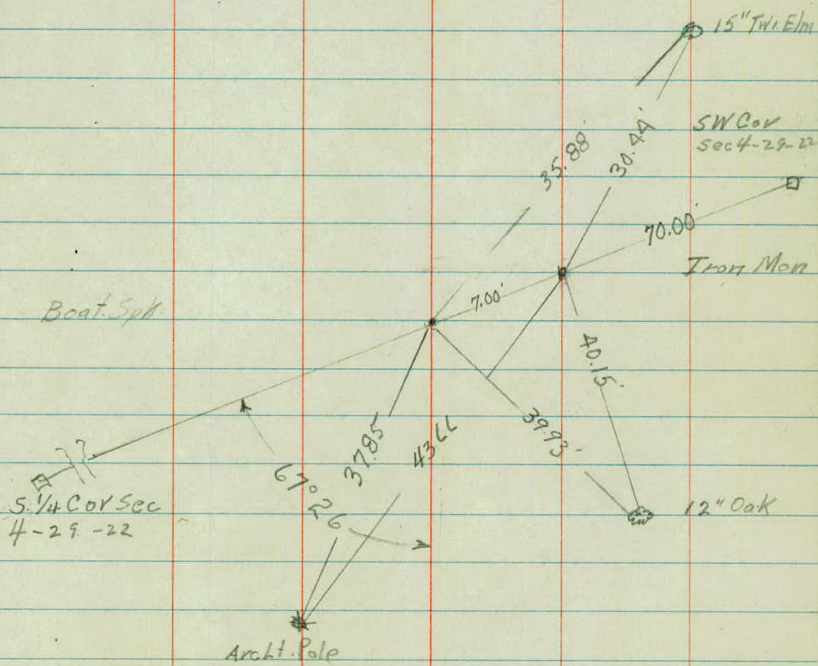
ΔL

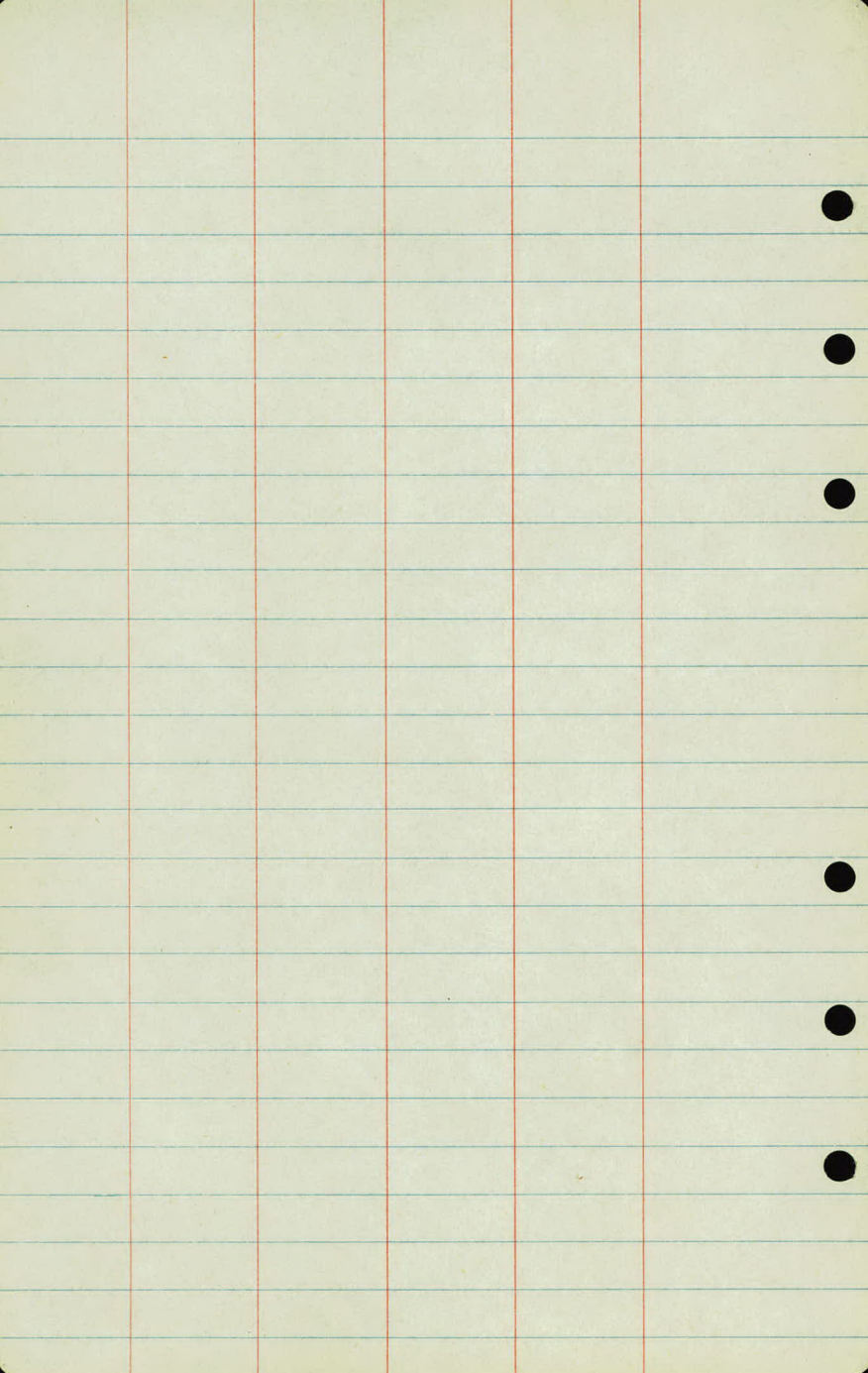
ΔR

65+27.20- P.1

0+00 Co Rd "C"

Description





Topograph
Keller Parkway

Rd Rd LK
10' 10' 70'

+32 Tr. 15" W. 11' 51'

5 10' 10' 70'

10' 10' 72' +50

4
+97 * Ent 10' 11' 81'

+90 Tr. 24" Co H 55'

9' 11' 72' +50

3 10' 11' 55'

27' +42 x Drain 13' 8' 15' 70' CM +50 43'
14' 9' 45' +25

2 13' 10' 50'

12' 14' 71' +75

10' 16' 100' +50

11' 15' +25

1 9' 15'

+50 12' 14'

+093 Edge Pav

+0110.7 West Edge Pav

+18 Arch Pole 15'

+00 End Yard
+84 PP 18'
+73 18" CoH 38'
+69 Rgetie Ho.
+67 SE Cor Ho 45'
+50 Bag Yard.

+135 End Swp 22'

Swp 20'

+50 Swp 27'

+25 Swp 25'

+00 Swp 24'

+75 Swp 22'

+50 Swp 23'

+25 Swp 24'

+80 Swp 25'

+78 Bag Swp 30'

+58 End Rad 12'

+50 QP 20'

+31 TP 68'

+09.3 Bag Rad 45'

Uncult

Uncultivated

Lake

CoH 26'

CoH 26'

CoH 26'

+96 15" W.I. 68'

+73 PP 19'

+66 N.W. Cor CoH Age 36'

+50 S.W. Cor CoH Age 36'

+16 N.W. Cor CoH Age 37'

+05 10" W.I. 27'

+00 S.W. Cor CoH Age 37'

+66 12" W.I. 51u 72'

+39 24" CoH 60'

+34 Ent 11'

+22 Rgetie Ent

+86 51u 81'

+84 24" CoH 66'

+67 10" W.I. 78'

+00 6" W.I. 55'

+88 15" W.I. 49'

+66 PP 15'

+38 TH 10" W.I. 45'

+27 2" W.I. 45'

+90 10" W.I. 75'

+52 PP 23'

+39 End Rad 14'

+28 PP 22'

+09.3 Bag Rad 60'

20'

100 Feet

13

Rd Rd, LK
10 9

15'

+57 60" X 30" CM X Drain 15'
(Note Helwall West End) Conc Helwall East End
Lower Half only

12

10' 9'

11

9' 9'

10

9' 9'

9

8' 9'

8' 10'

+50

8 +00 Bes Ditch 32'

9' 9'

10' 10'

110' 150

7

10' 10'

81'

10' 10'

72' +50

6

10' 10'

70'

Swp 19'

+80 Rge tie Ditch
+72 Arch Pole 17.

+51 A in Ditch 47'

Swp 20'

VII

VII

Gerrard's Creek

1x8x8'

Brush
+ Scattered
Trees

+57 Ditch 50'
+45 Rge tie Ditch

Fe 25'

+90 Beg Brush
35'

+17 PP 14'

Swp 19'

VII

VII

Fe 25'

Swp 16'

VII

VII

Low Area

+19 24' CoH 18'

Fe 25'

+55 PP 11'

VII

Φ

Swp 19 + 150'

Fe 26'

+54 Ditch 90'
+50 Swp 19

+02 PP 13

+00 Beg Swp 24 + 90'

Btm

Uncultivated

+70 Rge tie Edge Woods

+87 Beg Fe & Woods 34'
+56 Woods 29'

Woods 29'

Low Area
Scattered Willows

Woods 50'

Woods 50

+70 PP 12'

+88 Edge Woods 42'
+50 Beg Woods 55'

28'
2 CoH

+22 NW Cor Cottage 36,
+02 SW Cor Cottage 35

20 Rd 10' Rd 8' LK 52'

19 11' 7' 39'

18 11' 8' 34'

+87 24 BE 41' 33' +50

17 11' 8' 31'

38' +50

16 11' 10' 56'

83' +50

15 10' 11' 150'

14 10' 10'

13 10' 9'

+56 15" Oak 36'
+31 12" Oak 29'
+19 Fe Cor 31'
+08 Arc. H. Pole 14'
Fe 32

+80 12" BE 29'
+66 Rye tie Fe
+35 Gr. Lila Bushes 40'

Fe 34.5'
+89 Ent 11'
+78 Rye tie Ent
+54 24" Will 30'

+47 PP 14.5'
+41 Fe Cor 35'
+41 End Swp 17'

Swp 19

Swp 17'

+75 PP 16'

Swp 17'

+22 PP 16'

Swp 18

Swp 19

+60 Stn 16'
+57 30" Elm 14'

+57 12" BE 18'

+66 End Fe 29'
+54 Gr. P. BE 33'
+32 Tr. 6" BE 30'
+30 Tr. 6" BE 37'

+00 End Woods 49'
Fe 29'

+50 Woods 40'
+42 Rye tie Woods

Fe 29'

+80 Beg Woods 60'

Fe 28'

+50 End Brush

Fe 25'

Scattered
Trees

Yard

LAKE

Low Area

Brush

27

Rd 11' Rd 9' LK 47'

20' 190 12" X 38 V.7 X Drain 18'

11' 11' 34' +50

26

11' 10' 31'

95 24" Maple 38'

9' 9' 27' +50

69 Ben 5' Step 21' +30'
54 Rge tie Wood Steps

25

10' 10' 30'

8' 11' 30'

4

9' 11' 30'

86 12" Elm 26'
74 6" BE 40'

+ 67 X Drain 24 X 41' - 30" X 8"
8 9 34' +50

60 Tr 12" B.E 45'

48 Ent 9'
38 Rge tie Ent

3

8 11 34

8' 134 10" X 33' C.M. X Drain 25'

2

5' 14' 47'

21

6' 12' 50'

52' +50

0

10 9 52'

+91 Stu 38'
+90 6" Drain tile 22'

+66 10" Maple 36'
+42 P.P. 16'
+42 18" Maple 42'

+16 24" Maple 37'

+81 6" B.E. 41'
+75 6" B.E. 28'
+66 1" B.E. 33'
+63 6" B.E. 25'
+55 Bush 28'
+48 24" Maple 39'

+25 10" Maple 40'

+01 24" Maple 41'

+85 P.P. 15'
+75 15" Maple 40'

+52 12" Maple 40'

+28 24" Maple 29'
+04 10" Elm 41'

+80 End 24" 14.5'
+57 End Wall 45'
+39 Rot Wall 45'
+57 Rge Tie Steps
+44 Con 3" Brick Step 33'
+42 Arch 19'
+33 Tri. 10" B.E. 31'
+28 10" B.E. 33'

+04 6" B.E. 24'

+03 P.P. 16'

+57 Tri 6" Will 18'

+59 P.P. 12'

Yard

Scattered Maples & Elms

Yard
Scattered Oaks & Elms

Germis Lake

+49 8" CoH 18'

+05 24" CoH 17'

+69 14" B.E. 15'

+52 12" B.E. 15'

+34 20" CoH 15'

+97 15" Elm 16'

+57 Stu 15'

+91 24" B.E. 17'
+59 End G.R. 13'
+54 End 24" Q.M. Dog 30' 11"
+52 End 30" Q.M. 26'

+00 Dog G.R. 16 G.Pst.

+26 Tri Will 46'

+03 Stu 26'

+51 24" Elm 18'

	Rd	Fd	LK
344	9'	11'	41
+83 4" Spruce 33'			
+78 4" Spruce 54'			
+68 4" Spruce 39'			
+59 2" Spruce 52'	9' 11'		41' + 50
+21 P.P. 13	14'	+31 15" x 40' C.M.	26'
33	9' 9'		41

32	9' 10'		45'
+98 Cen 4' Flagstone Steps 16'			
+59 2 1/4" Oak 30'			
+42 Stu 41'	8' 11'		50' 150
+40 Stu 37'			

31	10' 10'		60'
+76 P.P. 17'			
+72 Stu 34'			
+70 S.E. Cor Masonry Wall 43'			
+57 Face 18" Pier 24'			
+54 S.W. Cor Masonry Wall 43'	10' 10"		
+55 Cen 4 Masonry Step 20'			64' + 50
+51 Face 18" Pier 22'			
+36 Stu 34'			

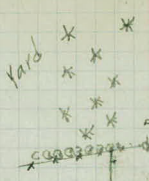
30	11' 10'		65'
+90 Stu 37'			
+84 Stu 50'	16'	+77 12" x 69' C.M. + Dredge Pipe	53'
		9' 10'	65'

29	9' 11'		70'
+94 1/2" Fe 34'			
+89 Hedge 29'			
+85 Rye tie Hedge			
+82 Cen 18" Rubble Drive 23'			
+78 Rye tie End	10' 10'		65' + 50'

28	10' 10'		54'
	9' 10'		46' + 50

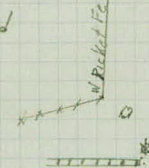
27	11' 9'		47'
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- +53 6" Spruce 30'
- +42 6" Spruce 40'
- +37 6" Spruce 51'
- +31 6" Spruce 32'
- +25 4" Spruce 46'
- +25 Rye Fir Hedge
- +19 End Fe 19 Hedge 25'
- +18 Fe Cor 32'
- +03 6" Tw Elm 18'
- Fe 32'



- +72 18" Elm 24'
- +54 Stu 24'
- +39 4" Lom Pop 21'
- +32 4" Lom Pop 21'
- +31 PP 38'
- +22 GP 18'

- +38 Rye Fir Fe
- +32 Fe Cor 37'
- +23 24" Oak 23'
- +08 Arc Lt Pole 15'
- +48 Cor Hedge 22'
- +48 Face Pier 20'
- +48 End Wall 17' 20'



- 176 12" Ash 26'
- +74 Tw 8" Ash 29'
- +59 12" BE 24'
- +42 24" C. H 24'
- +13 12" Oak 17'
- +84 10" BE 33'

- +28 Face 18" Pier 24'
- +25 Cor 4" Gate 1 Steps 21'
- +22 Face 18" Pier 24'
- +21 Stu 26'
- Hedge 22 Wall 17' 20'



- +34 12" Elm 31'
- +31 Tw 6" W. H 48'
- +20 Gr. 6-6" Will 48'
- +05 8" Ash 33'

- +88 Face 18" Pier 22'
- +33 Top Masonry Wall 18'
- +33 Beg Hedge 24'
- +32 Rye Fir Fe
- +31 X Fe 24'
- +31 Face 18" Cor Pier 22'
- +17 Tri 15" Elm 35'
- +08 Stu 34'
- +00 Tw 24" C. H 32'

- +22 12" BE 33'
- +05 End Area 18'

- +98 End 12" x 20" CM 17'
- +78 Beg 12" x 20" " 17'
- +79 24" C. B. 17'
- +76 End 12" CM 17'
- +56 Ent

- +92 Δ in Parking Lot 33'
- +73 NE Cor Tavern 34'

- +46 Beg 12" x 36" CM 16'
- +29 P.P 15'
- +08 24" Elm 25'

- +39 NW Cor Tavern 24'
- +06 Δ in Parking Lot 31'
- +02 NW Cor Out Ho 37'
- +00 Beg Parking Area 19'

- +67 2" Tree 23'
- +52 24" Coll 39'
- +48 18" " 39'

- +75 End Gr. R 15'
- +57 Beg Gr. R 15' 6" P.

- +17 Ent 11'
- +14 Rye Fir Ent
- +12 Hedge 25'
- +01 Rye Fir Hedge
- +86 12" B.E 38'
- +82 Arc Lt P 18'
- +67 2" Tree 39'

- +98 End 4" Iron Pipe 40'

- +37 12" Ash 38'
- +35 24" Coll 51'

- +55 4" Tree 22'
- +41 4" Tree 28'
- +12 24" Coll 20'



44	Rd	Rd	LK
+81 End Rad 58'	54'	14'	86'
+73 Rad 175'			+71 30" Oak 33'
+59 12" Elm 58'	375 + 74 X Drain 84'	465'	+60 18" Elm 16'
+57 Beg Rad 10	30"	24"	
	+48 X Drain ?	73 + 50	
40	10' 9	63'	100 Gr 6-6" Willb 58'
+63 12" Birch 50'			+81 Rye tie Fe
+65 Bush 32'			
+60 PP 12'			
+56 2" Elm 47'			
+56 6" Elm 49'	+80' Gr 6 Bush 32'	60' + 50	
+46 6" Elm 37'			
+24 6" Elm 37'			
+08 6" Elm 37'			
37	11' 10	62'	
+28 5 1/2" 18'	+89 8" Elm 38'		
+24 1" Plum 17'	+62 Gr 6 Plum 21		
+17 3" Spruce 44'	+39 2" Plum 13'		
	+33 2 Plum 1/2 20-32		
+16 2" Pine 34'			
+05 2" Pine 31'	11' 10'	58' + 50	
+03 1" Plum 21'			
38	11' 11	58'	
+97 2" Plum 24			
37	10' 9'	50'	
+93 Rye tie Hedge			
+83 X Hedge 33			
+70 End Hedge 24			
H3 PP 12'			
36	8' 8'	45'	
+81 2" Pine 38'			
+79 2" " 32'			
+77 2" Pine 46'			
+73 4" " 38'			
+60 4" " 30'			
+59 4" " 41'	9' 10	43' + 50	
+48 4" " 34'			
+42 4" Spruce 45			
35	9' 10"	42'	
+81 4" Spruce 30'			
+78 4" Spruce 52			
+70 4" " 32'			
+63 4" " 44'			
+55 4" " 30'			
+49 2" " 49'			
+41 6" " 35'		42 + 50	
+37 6" " 57'			
+33 4" " 42			
34	9 11	41	

+74 Beg 30" CM 32'
 +61 Shrubbery 29'
 +58 P.P. 12'
 +54 Shrubbery 17'
 +40 Cen Rock Garden 34'
 +40 Shrub 14'-53
 +22 Shrub 14'
 +16 Beg Shrub 22
 +00 Ent.

+90 Rgt tie Fe
 +84 S.E. Cor Rock 42'
 +84 Beg 15" CM 21'
 +79 L in Hdm 13' 22"
 +68 S.W. Cor Granite P.T. 34'
 +68 Beg Masonry Hdw 32
 +56 1 Fe 52'
 +76 Ent 11' +81 Rgt tie Ent
 +68 Rgt tie Fe
 +60 P.P. 16'
 +60 Fe Cor 21'

+52 Rgt tie Ent
 +44 Ent 11'

Fe 22'
 +99 4" Spruce 39'
 +94 Rgt tie Fe
 +87 Fe Cor 22

+41 P.P. 15'

+87 Rgt tie Ent
 +82 Ent 13'

+46 Rgt tie Hedge
 +39 Cor Hedge 24'

+19 Rgt tie Hedge
 +12 Hedge 20'
 +08 End CM 16
 +04 Rgt tie Ent

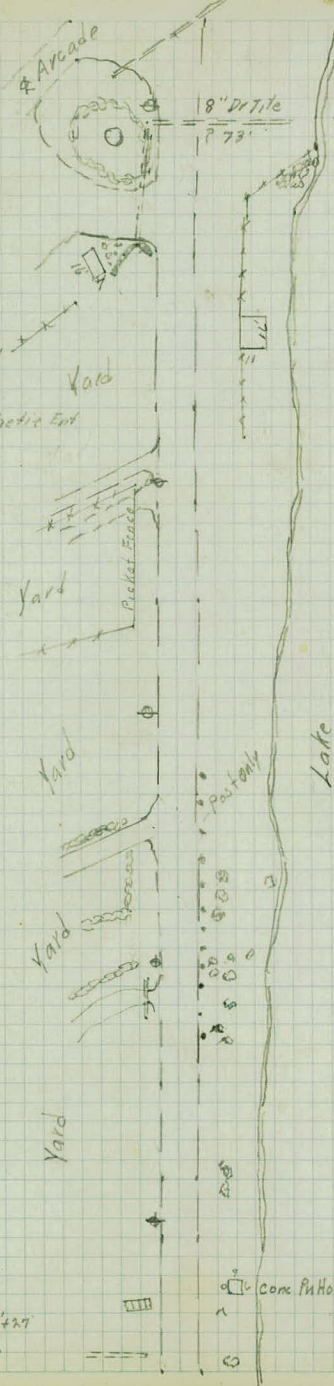
+96 Ent 8'

+82 Beg 15" x 26" CM 16.5'

+79 P.P. 12'

+34 Cen 7" Stone Steps 16' 29"

+09 4" Drain Tile 17'
 Sewer



+92 10" Elm 32' 19
 +48 End CM 15?
 +34 End Fe 73'
 +26 Gr 4'-6" W 11 70'
 +23 Gr 7'-4" W 11 60'
 +15 Gr 7'-6" W 11 55'
 +09 Fe Cor 37'
 +00 Stu 24
 Fe 37
 +85 Stu 27'
 +68 30" Elm 23'

+48 N.E. Cor Boat Hdw 34'
 +40 4" Ash 30'
 +34 2" Tr. 20'
 +32 N.W. Cor Boat Hdw 33'
 +21 2" Tr 24'
 +12 2" Tr 25'
 +04 Stu 24'

+85 Beg Fe 35'

+41 12" Elm 31'
 +41 24" Oak 22'

+86 12" Elm 26'
 +82 10" Elm 25'

+49 12" Oak 18'
 +49 Gr 6" W 11 57'
 +36 Tr. 6" W 11 48'

+22 24" Boh 24'
 +06 End Gr 11'
 +00 Tr 6" W 11 46
 +55 Stu 48
 +57 15" Elm 24
 +47 24" Elm 22
 +38 Tr 12" Elm 20'
 +17 4" Lom Pop 34'
 +14 " " 28'
 +11 " " 17'
 +04 Stu 18'
 +02 4" Lom Pop 24
 G.R 11' Root only

+90 4" Lom Pop 27'

+78 Stu 19'

+74 Beg G.R 13
 +72 4" Lom Pop 22
 +06 2" Lom Pop 24
 +04 2" " " 26'

+97 4" Lom Pop 27'

+56 N.E. Cor P.H. 25'
 +50 N.W. Cor P.H. 25'

+33 Stu 21

+03 24" Opt 27'

48
 +97 5" 25'
 +87 5" 20'
 +83 5" 27'
 +31 12" Tree 37'
 +29 12" Tree 42'

Rd Rd
 11 9

LK
 29

47 11' 11' 36'

46 10' 12' 42' +86" 12" E/m 33'

+97 10" Oak 39' 78 +75 LK
 +60 L" Tr 40'
 9 13' 55 150

45 11' 11 37'

+47 L" Oak 35' 12' 11 35'
 +16 Rgctic Fe

44 11' 12' 37'

43 11' 10 34'

+90 PP(TP 15'

+77 End Fe 28
 +69 Tw 15" E/m 29

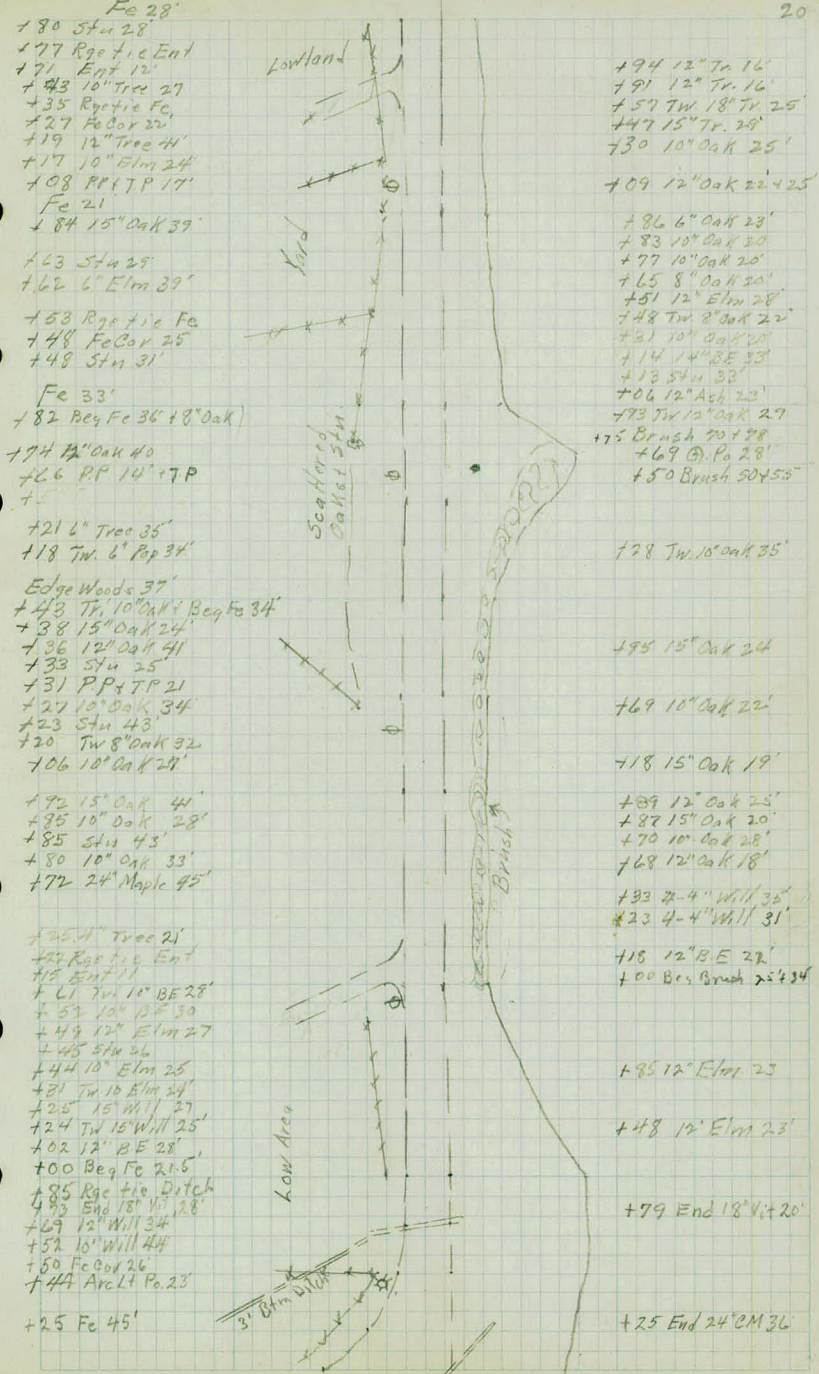
42 9' 14' 83'

28' +77 18" x 48" V.4 x Dr. 20'
 +75 9' 14 92'

+48 Rgctic Fe 150 15' 14' 94'

+25 30 14' 88'

41 54' 86'



56	RD 8	RD 11	LK 44	+99 18" Tr. 28'	+78 4" Tr. 44
	10'	10'	46'	+50	
54	10	10	52'	+	
+83 NW Cor. Twp 58'				+91 8" Oak 17	
		10'	55'		
				+61 12" Oak 20'	
53	10	11'	48'		
	16"	+91 X Drain 12" X 32' CM		+95 End 12" CM 15'	
+85 End 15" CM 15'			16'		
	10'	11	47'	+50	
52	9	10'	42'		
	10'	10'	39'	+50	
51	12'	10'	45'		
+93 15" Maple 43'				+98 Cor Foundation 37'	
+85 PP 23				+60 Cor Foundation 35'	
+52 12" Tr. 46					
+44 Rd 12'					
+31 Rgetie Rd	12'	11	38'	+50	
50	11'	12'	39'		
	9	12'	35'	+50	
49	9	11'	31		
+31 End 12" Vit 38'					
+21 Rgetie Ditch	34'	+23 X Drain 12" X 52'		18'	
48	11'	9'	29'	+19 End 12" Vit 18'	

+59 SW Cor Shed 60'
+40 SW Cor Tr 56'

+65 Rd 21'
+37 Rd 32'
+37 15" Oak 18'
+32 Adult Po 16'
+93 12" Tr 21'
+27 12" Oak 20'
+20 12" Tr 20'
+11 Rd 44'

+98 Stn 20
+91 15" Oak 21'
+85 15" Oak 42'
+79 10" Tr 26'
+42 12" Tr 24'
+37 TP 21'
+06 PP 17'

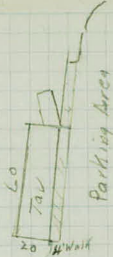
+11 TP 21'
+51 10" BE 43'
+50 End Fe 45'
+47 18" Tr 36'

+39 18" BE 33'
+29 15" BE 28'
+11 15" BE 27'

Fe 33'
+89 15" BE 29'
+24 PP TP 18'
+50 Fe 27'
+42 Fe Cor 27'
+36 Rge tie Fe

+34 12" BE 26'
+25 Stn 24'
Fe 25' Woods 26'

+66 Stn 23'
+53 Stn 27'
+47 TP PR 15'
+47 Stn 23'
+30 Beg Woods 30'
+21 Stn 24'
+10 5' Elm 36'
Fe 18'



Parking Area

Uncultivated

Woods

Lowland

Post only



33'

Lake Corral

GK 14
+75 4" Tr 25 21
+72 Beg Cor 14'
+52 24" Tr 19'
+40 12" Tr 21'
+24 4" Tr 28'
+23 6" Tr 18'
+15 6" Tr 28'
+10 12" Tr 21'
+08 15" Tr 17'
+00 18" Tr 18'

+39 20" Tr 48'
+32 8" Tr 50'
+32 10" Tr 47'
+32 SE Cor Boat Ho 28'
+32 12" Tr 20'
+20 10" Tr 23'
+19 15" Tr 15'
+08 N.E. Cor Boat Ho 25'
+06 Tr 7" Tr 30'
+97 24" Tr 43'
+80 Quad 12" Tr 18'
+69 10" Oak 24'
+60 10" Oak 21'
+51 10" Oak 21'
+39 2" Tr 28'
+32 2" Tr 27'
+19 4" Tr 25'

+04 12" Oak 14'
+62 4" Tr 33'

+48 18" Tr 18'
+30 8" Tr 15'
+29 8" Tr 15'
+27 12" Tr 25'
+09 12" Oak 28'
+08 10" Oak 27'

+57 10" Tr 20'
+50 10" Tr 24'
+36 8" Tr 24'
+28 10" Oak 25'
+17 12" Oak 17'
+04 10" Oak 16'

+96 12" Elm 28'
+81 12" Oak 16'

+54 24" Elm 24'
+44 12" Elm 23'
+37 6" Oak 18'
+31 8" Oak 31'
+07 Tr 10" Oak 17'

+83 10" Tr Oak 15'
+71 12" Oak 17'
+53 15" Tr Elm 19'
+08 24" Tr 28'
+07 24" Stn 21'
+03 12" Tr Tr 20'

62

Rd Ld
10' 10'

LK
50'

61

10' 11'

44'

10' 11'

43' 150

60

10' 10'

43'

+90 PP. 14
+90 12" Tr. 41'
+87 Stn 43'

+98 10" Tr. 25'
+88 Stn 22'

+58 12" x 36' CM

+17 2 Stn 33'

59

9' 10'

36'

+97 Stn 40'

+43 30" Tr. 17'
+40 15" Tr. 30'
+36 15" Tr. 23'
58
+87 Tw. Tr. 31'
+83 24" Elm. 31'
+60 Rsp. tie Fe.
+56 10" Tr. 28' + Fe Cor
+47 15" Tr. 28'
+39 2" Tr. 29'
+33 15" Tr. 31'
+31 8" Tr. 40'
+10 4" Tr. 20'

9' 9'

35

+96 4-12" Tr. 24'

57

10' 10'

+64 12" Tr. 24'
+59 10" Tr. 24'
+57 10" Tr. 37'
+55 Stn 16'
+46 Tw. 12 Tr. 45'

+67 Cor Bridge 148-148'

8 9'

36' Lk

+53 End GR 13
+28 Beg. GR 12' +69 Tw. 15 Tr. 29

56

9' 10'

37'

+50

55

9 11

44

+07 P.P. 19'

+88 8" Oak 29'
+77 Birch 29'
+73 Birch 28'
+63 End 12" GM 14'
+42 Ent
+37 Rye 10 Fe
+27 Fe Cor 30'
+22 End GR 22'
+17 GR 13
GR 12' Fe 28'
+94 6" Tr 33'
+94 12" Tr 50'
+69 Tr 6" Tr 42'
+64 10" Tr 44'
+59 4" Tr 41'
+52 P.P. 12.5'

+04 10" Tr 27'
GR 12' Fe 29'

+96 15" Tr 26'

+09 3-15" Tr 45'
+16 GR 12'
+13 Fe Cor 29'
+08 P.P. 10'

+077 Cor Bridge 14.
+40 15" Tr 40'
+34 Stu 29'
+34 6" Tr 36'
+34 15" Tr 50'
+28 Tr 31'
+24 Stu 13'
+17 10" Tr 42'
+11 4" Tr 36'
+08 15" Tr 27'

+36 P.P. 14' End Parking Area

+15 12" Tr 60' Δ Parking Area

Scattered Oak 15th

Hard

Woods
Lowland

Mohican
Creek

Woods

Post only

Post only

GR 13' 22'
+99 3-8" Tr 27'
+87 8" Tr 23'
+70 6" Tr 30'
+49 10" Tr 30'
+47 10" Tr 30'
+42 8" Tr 31'

+05 Tr 10" Tr 37'
G.R. 15'

+85 10" Tr 23'

+51 10" Tr 31'
+50 GR 15'
+27-2-12" Tr 24'
+19 10" Tr 20
GR 13'
+77 15" Tr 39'
+74 10" Elm 27'
+66 5-10" Tr 25'
+52 End 12" GM 21'
+52 8" Tr 17'
+39 Tr 8" Tr 25'
+34 8" Tr 29'
+26 4-12" Tr 25'

GR 12'

+95 10" Tr 36'

+70 10" Tr 20'
+64 10" Tr 21'

+00 15" Tr 27'
GR 13'
+89 12" Tr 25'
+67 Stu 27'
+63 18" Tr 16'
+52 Tr 15" Tr 21'
+46 Tr 24" Tr 27'
+36 Tr 12" Tr 27'
+32 15" Tr 29'
+19 15" Tr 16'
+09 Bay GR 11'
+077 Cor Br 158

+67 End GR 10'
+63 18" Tr 16'
+56 12" Tr 21'
+50 8" Tr 23'
+46 12" Tr 21'
+41 12" Tr 20'
+20 15" Tr 22'
+09 12" Tr 21'
+00 24" Tr 24'
GR 12'
+85 Stu 22'
+79 8" Tr 25'
+42 12" Elm 22'
+23 12" Tr 23'
+17 8" Tr 20'
+08 10" Tr 26'
+06 Stu 23'

GR 14' Post only

16

11' 11' 60'

+75 Rad 12'

+50 Rad 23'

+48 Rgetre Shoulder

58' +27

+29 End Rad 48'

+5

11 53'

+90 Beg Rad 13'

+90 Beg Cable G.R.

14

11' 10' 57

+98 4" Tr. 28

+90 Tw 4" Elm 30'

+84 4" Elm 34'

3

11 11 67

+95 10" Tr 25

+89 Tw 12" Tr +54w 25'

+69 Tw 6" Tr 39

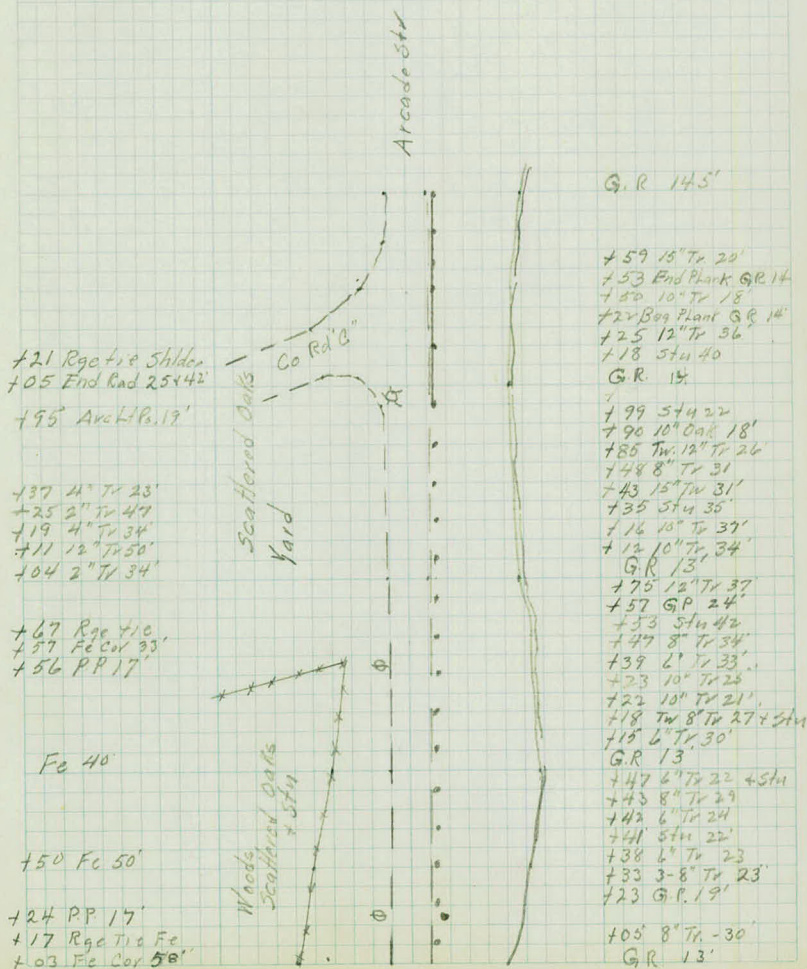
+67 6" Tr 28'

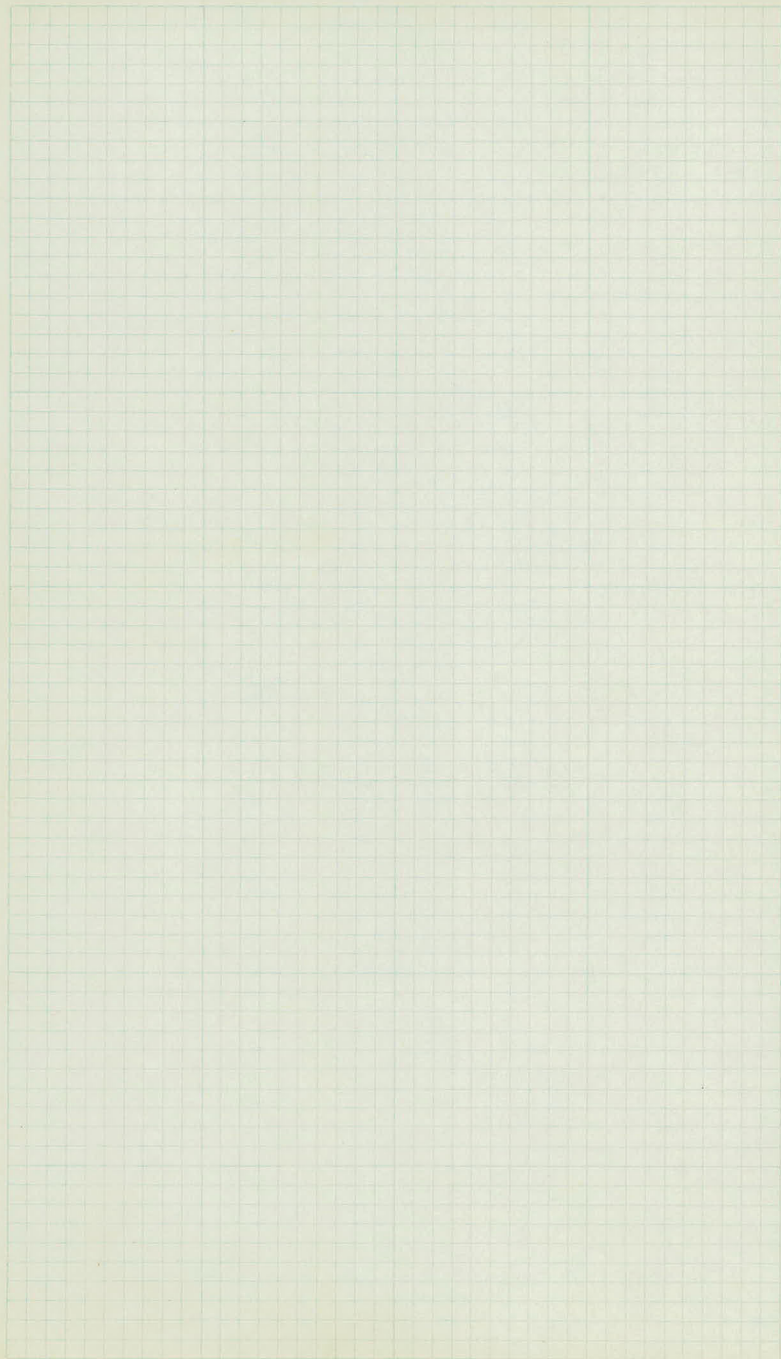
10' 10'

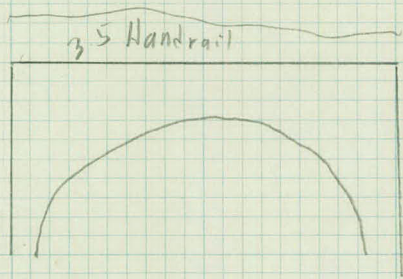
62' +50 G.R. 15'

2

10 10 50









Bench Levels
Keller Parkway

Sta	+ -	π	-	Elev	
B.M.	8.51	880.98		872.47	✓
	1.75	880.74	1.99	878.99	
T.P.	2.26	872.55	10.45	870.29	
B.M.	6.76	873.40	5.91	866.64	
	9.31	875.42	7.29	866.11	
	3.74	869.82	9.34	866.08	
B.M.	4.74	869.82	4.74	865.08	
	5.62	872.40	3.04	866.78	
B.M.	6.04	871.37	7.07	865.33	
	6.96	874.57	3.76	867.61	
B.M.	3.52	869.86	8.23	866.34	
	6.58	871.16	5.28	864.58	
	4.45	873.47	2.14	869.02	
B.M.			0.63	872.84	✓
	70.24		69.87		

Description

SpK in 15" Tw. Elm. 15' Rt St 65+68

Top Boat SpK

Top N.W Cor Con Stop 50' ^{at} East of Sta 54+00

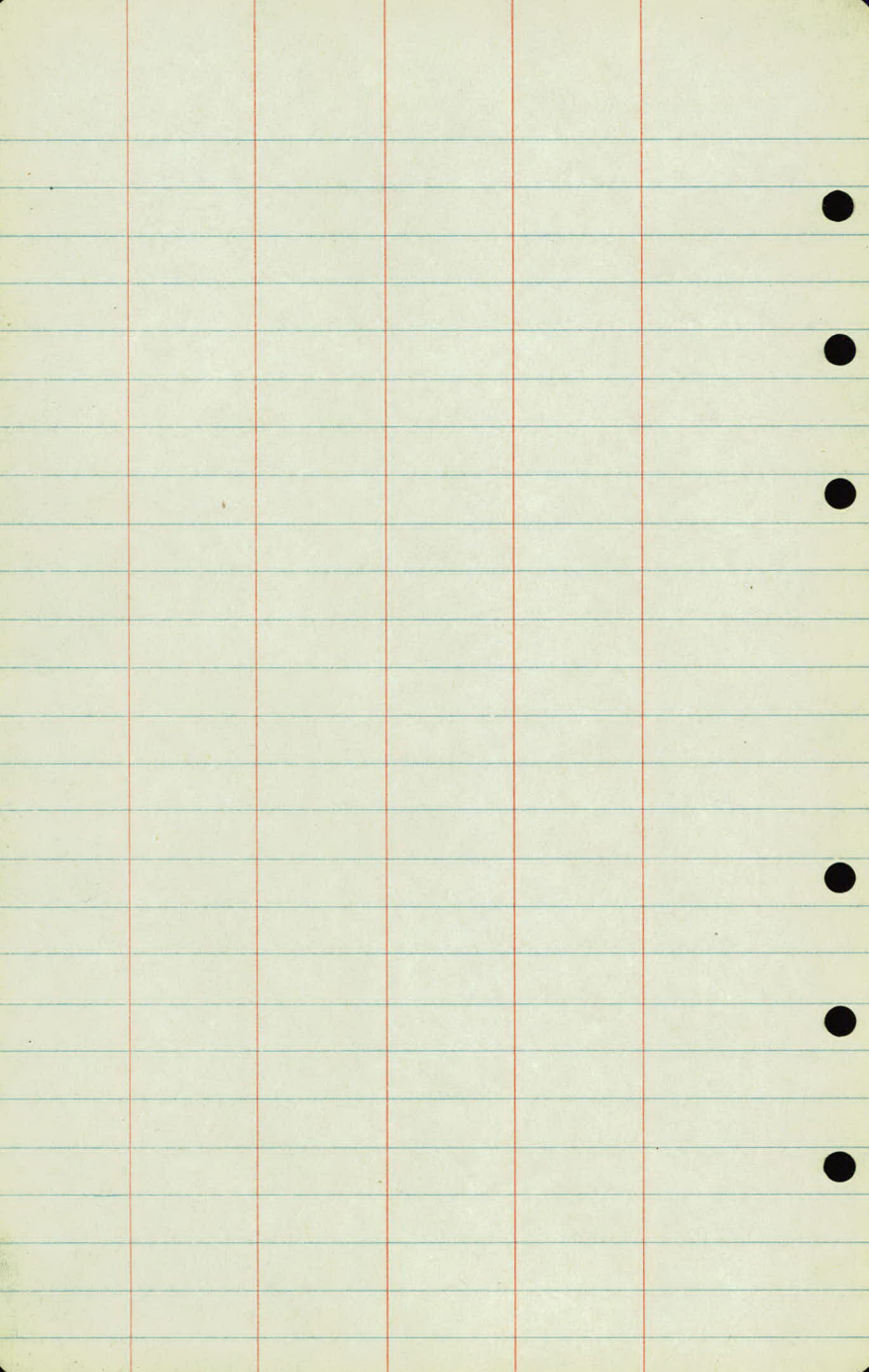
Top 28" Elm. 25' Rt Sta 32+47

SpK in 15" Elm. N.W Cor Keller Pkwy & Arcade Str

SpK in 28" Cott 25' Rt Sta 32+47

SpK 28" Elm. 14' Rt Sta 19+60

Top Stone Man & Edgerton & Co Rd "C"



X Sections

Keller Parkway

Sta	+	Δ	-	Elev	
B.M.	0.60	873.44		872.84	✓

0+00				72.8	
------	--	--	--	------	--

0+093				72.7	
-------	--	--	--	------	--

+16				72.6	
-----	--	--	--	------	--

+37				71.8	
-----	--	--	--	------	--

+60				70.7	
-----	--	--	--	------	--

+80				69.9	
-----	--	--	--	------	--

1+00				68.9	
------	--	--	--	------	--

1+25				68.2	
------	--	--	--	------	--

+50				67.7	
-----	--	--	--	------	--

+75				67.6	
-----	--	--	--	------	--

2+00				67.4	
------	--	--	--	------	--

+25				67.3	
-----	--	--	--	------	--

Lt.

R

Rt

Top Stone Men Co Rd C + Edgerton 0400

$$\begin{array}{r} 4.0x \\ 50 \end{array} \quad \begin{array}{r} 0.2 \\ 25 \end{array} \quad \begin{array}{r} 0.60 \\ 25 \end{array} \quad \begin{array}{r} 0.9 \\ 25 \end{array} \quad \begin{array}{r} 1.1 \\ 50 \end{array}$$

$$\begin{array}{r} 1.01 \\ 50 \end{array} \quad \begin{array}{r} 0.3 \\ 25 \end{array} \quad \begin{array}{r} 0.2 \\ 25 \end{array} \quad \begin{array}{r} 1.0 \\ 25 \end{array} \quad \begin{array}{r} 1.2 \\ 50 \end{array}$$

$$\begin{array}{r} 0.3 \\ 50 \end{array} \quad \begin{array}{r} 0.5 \\ 20 \end{array} \quad \begin{array}{r} 0.6 \\ 17 \end{array} \quad \begin{array}{r} 0.8 \\ 20 \end{array} \quad \begin{array}{r} 1.2 \\ 20 \end{array} \quad \begin{array}{r} 1.4 \\ 42 \end{array} \quad \begin{array}{r} 1.2 \\ 50 \end{array}$$

$$\begin{array}{r} 3.1 \\ 50 \end{array} \quad \begin{array}{r} 1.8 \\ 44 \end{array} \quad \begin{array}{r} 1.2 \\ 29 \end{array} \quad \begin{array}{r} 2.2 \\ 23 \end{array} \quad \begin{array}{r} 1.8 \\ 13 \end{array} \quad \begin{array}{r} 1.6 \\ 15 \end{array} \quad \begin{array}{r} 2.0 \\ 25 \end{array} \quad \begin{array}{r} 2.0 \\ 39 \end{array} \quad \begin{array}{r} 8.1 \\ 50 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 8.6 \\ 55 \end{array} \quad \begin{array}{r} 6.3 \\ 45 \end{array} \quad \begin{array}{r} 2.5 \\ 42 \end{array} \quad \begin{array}{r} 2.4 \\ 33 \end{array} \quad \begin{array}{r} 3.0 \\ 12 \end{array} \quad \begin{array}{r} 2.8 \\ 8 \end{array} \quad \begin{array}{r} 2.7 \\ 14 \end{array} \quad \begin{array}{r} 3.0 \\ 21 \end{array} \quad \begin{array}{r} 3.4 \\ 33 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array} \quad \begin{array}{r} 10.8 \\ 50 \end{array}$$

$$\begin{array}{r} 9.4 \\ 50 \end{array} \quad \begin{array}{r} 8.6 \\ 28 \end{array} \quad \begin{array}{r} 3.2 \\ 14 \end{array} \quad \begin{array}{r} 3.8 \\ 9 \end{array} \quad \begin{array}{r} 3.5 \\ 15 \end{array} \quad \begin{array}{r} 3.7 \\ 20 \end{array} \quad \begin{array}{r} 3.9 \\ 34 \end{array} \quad \begin{array}{r} 10.3 \\ 50 \end{array} \quad \begin{array}{r} 11.5 \\ 50 \end{array}$$

$$\begin{array}{r} 11.2 \\ 50 \end{array} \quad \begin{array}{r} 10.3 \\ 28 \end{array} \quad \begin{array}{r} 8.3 \\ 22 \end{array} \quad \begin{array}{r} 5.1 \\ 13 \end{array} \quad \begin{array}{r} 4.5 \\ 20 \end{array} \quad \begin{array}{r} 4.4 \\ 35 \end{array} \quad \begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 12.0 \\ 50 \end{array}$$

$$\begin{array}{r} 11.3 \\ 50 \end{array} \quad \begin{array}{r} 10.8 \\ 26 \end{array} \quad \begin{array}{r} 9.5 \\ 21 \end{array} \quad \begin{array}{r} 5.9 \\ 13 \end{array} \quad \begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 4.6 \\ 23 \end{array} \quad \begin{array}{r} 5.1 \\ 30 \end{array} \quad \begin{array}{r} 8.7 \\ 39 \end{array} \quad \begin{array}{r} 11.8 \\ 50 \end{array} \quad \begin{array}{r} 12.2 \\ 50 \end{array}$$

$$\begin{array}{r} 11.1 \\ 50 \end{array} \quad \begin{array}{r} 11.6 \\ 31 \end{array} \quad \begin{array}{r} 9.3 \\ 20 \end{array} \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad \begin{array}{r} 5.7 \\ 16 \end{array} \quad \begin{array}{r} 5.1 \\ 21 \end{array} \quad \begin{array}{r} 5.3 \\ 30 \end{array} \quad \begin{array}{r} 9.4 \\ 40 \end{array} \quad \begin{array}{r} 11.3 \\ 50 \end{array} \quad \begin{array}{r} 11.8 \\ 50 \end{array}$$

$$\begin{array}{r} 11.3 \\ 50 \end{array} \quad \begin{array}{r} 11.2 \\ 27 \end{array} \quad \begin{array}{r} 9.7 \\ 20 \end{array} \quad \begin{array}{r} 7.3 \\ 15 \end{array} \quad \begin{array}{r} 6.2 \\ 6 \end{array} \quad \begin{array}{r} 5.8 \\ 17 \end{array} \quad \begin{array}{r} 5.5 \\ 28 \end{array} \quad \begin{array}{r} 10.3 \\ 45 \end{array} \quad \begin{array}{r} 11.3 \\ 50 \end{array} \quad \begin{array}{r} 11.3 \\ 50 \end{array}$$

$$\begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 11.0 \\ 29 \end{array} \quad \begin{array}{r} 9.6 \\ 21 \end{array} \quad \begin{array}{r} 7.2 \\ 14 \end{array} \quad \begin{array}{r} 6.9 \\ 11 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 5.6 \\ 11 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 10.2 \\ 23 \end{array} \quad \begin{array}{r} 11.0 \\ 46 \end{array} \quad \begin{array}{r} 13.2 \\ 50 \end{array} \quad \begin{array}{r} 14.4 \\ 55 \end{array}$$

$$\begin{array}{r} 11.4 \\ 50 \end{array} \quad \begin{array}{r} 10.9 \\ 25 \end{array} \quad \begin{array}{r} 7.1 \\ 16 \end{array} \quad \begin{array}{r} 7.1 \\ 14 \end{array} \quad \begin{array}{r} 6.1 \\ 17 \end{array} \quad \begin{array}{r} 5.9 \\ 20 \end{array} \quad \begin{array}{r} 9.9 \\ 43 \end{array} \quad \begin{array}{r} 10.7 \\ 45 \end{array} \quad \begin{array}{r} 14.4 \\ 50 \end{array}$$

STA	+	π	-	ELEV
		873.44.		

2+42		15" CROSS-DRAIN		67.2.
------	--	-----------------	--	-------

+75				67.5.
-----	--	--	--	-------

3+00				67.7.
------	--	--	--	-------

+42				68.2.
-----	--	--	--	-------

+50				68.3.
-----	--	--	--	-------

4+00				68.9.
------	--	--	--	-------

+08				69.0.
-----	--	--	--	-------

T. P	3.79	87320.	4.03	86941.
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+50				69.4.
-----	--	--	--	-------

5+00				69.5.
------	--	--	--	-------

+50				69.2.
-----	--	--	--	-------

6+00				68.3.
------	--	--	--	-------

LT

E

RT

CNLU

CNLU

$$\begin{array}{r} 11.4 \quad 11.9 \quad 12.4 \quad 7.8 \quad 7.0 \\ 50 \quad 30 \quad 27.5 \quad 15 \quad 6.2 \end{array} \quad \begin{array}{r} 6.1 \quad 9.1 \quad 10.6 \quad 13.5 \quad 14.4 \\ 10 \quad 20 \quad 40 \quad 42 \quad 44 \end{array}$$

$$\begin{array}{r} 11.3 \quad 10.7 \quad 7.4 \quad 6.6 \quad 5.9 \quad 5.9 \quad 9.4 \quad 11.3 \quad 14.4 \\ 50 \quad 24 \quad 17 \quad 11 \quad 5.2 \quad 11 \quad 21 \quad 44 \quad 48 \end{array}$$

$$\begin{array}{r} 10.7 \quad 10.1 \quad 7.2 \quad 6.3 \quad 5.7 \quad 9.5 \quad 10.8 \quad 14.4 \\ 50 \quad 24 \quad 17 \quad 10 \quad 5.2 \quad 12 \quad 24 \quad 50 \quad 55 \end{array}$$

$$\begin{array}{r} 7.7 \quad 7.7 \quad 6.4 \quad 5.9 \quad 5.3 \quad 6.6 \quad 8.2 \quad 9.9 \\ 50 \quad 24 \quad 18 \quad 10 \quad 5.2 \quad 13 \quad 19 \quad 24 \quad 50 \end{array}$$

$$\begin{array}{r} 6.7 \quad 5.0 \quad 5.0 \quad 6.6 \quad 6.2 \quad 6.5 \quad 5.1 \quad 5.3 \quad 6.6 \quad 8.9 \quad 10.3 \\ 50 \quad 40 \quad 25 \quad 16 \quad 12 \quad 11 \quad 13 \quad 20 \quad 26 \quad 50 \end{array}$$

$$\begin{array}{r} 4.0 \quad 3.7 \quad 4.8 \quad 5.2 \quad 4.9 \quad 4.5 \quad 5.0 \quad 8.0 \quad 9.9 \quad 10.8 \\ \text{FLOOR HOUSE} \quad 50 \quad 31 \quad 15 \quad 9 \quad 14 \quad 21 \quad 29 \quad 50 \end{array}$$

$$\begin{array}{r} 2.9 \quad 1.8 \quad 2.6 \quad 5.5 \quad 5.1 \quad 4.7 \quad 4.4 \quad 4.9 \quad 7.9 \quad 9.7 \quad 10.8 \quad 10.6 \\ 50 \quad 40 \quad 27 \quad 20 \quad 14 \quad 10 \quad 4.4 \quad 13 \quad 23 \quad 30 \quad 44 \quad 50 \end{array}$$

$$\begin{array}{r} 4.9 \quad 4.1 \quad 3.8 \quad 4.4 \quad 6.8 \quad 8.0 \quad 9.6 \\ 21 \quad 18 \quad 12 \quad 12 \quad 20 \quad 25 \quad 50 \end{array}$$

$$\begin{array}{r} 4.0 \quad 4.7 \quad 4.5 \quad 4.1 \quad 3.7 \quad 4.3 \quad 6.6 \quad 7.6 \quad 9.6 \\ 24 \quad 19 \quad 14 \quad 9 \quad 3.7 \quad 14 \quad 22 \quad 33 \quad 50 \end{array}$$

$$\begin{array}{r} 4.0 \quad 3.1 \quad 4.6 \quad 4.4 \quad 4.0 \quad 4.1 \quad 4.5 \quad 8.9 \quad 10.0 \\ 33 \quad 23 \quad 11 \quad 10 \quad 4.0 \quad 12 \quad 15 \quad 27 \quad 50 \end{array}$$

$$\begin{array}{r} 2.0 \quad 5.0 \quad 6.4 \quad 5.7 \quad 5.3 \quad 4.9 \quad 5.2 \quad 9.5 \quad 10.5 \quad 10.8 \\ 41 \quad 39 \quad 30 \quad 19 \quad 9 \quad 4.9 \quad 14 \quad 27 \quad 36 \quad 50 \end{array}$$

STA	+	$\nearrow$	-	ELEV
		873.20.		
6+50				67.5.
7+00				66.6.
T.P.			6.83	866.37.
	13.08	885.92.	0.36	872.84.
4+50				(69.4)
5+00				(69.5)
T.P.	8.91	892.94.	1.89	884.03.
+50				(69.2)
6+00				(68.3)
+50				(67.5)
T.P.	0.93	880.17.	13.70	879.24.
7+00				(66.6)
T.P.	3.16	869.55.	13.78	866.39.
7+50				66.2.
8+00				65.6.
+50				65.0.

LT

L

RT

$$\frac{7.0}{22} \frac{7.2}{15} \frac{6.2}{12} \frac{6.0}{9} \frac{5.7}{5.7} \frac{6.0}{11} \frac{6.9}{17} \frac{10.6}{26} \frac{11.3}{50}$$

$$\frac{3.1}{31} \frac{4.4}{25} \frac{7.7}{18} \frac{7.1}{16} \frac{6.6}{14} \frac{6.6}{9} \frac{7.2}{14} \frac{11.6}{23} \frac{12.5}{50}$$

$$\frac{9.1}{100} \frac{9.7}{86} \frac{8.8}{50} \frac{11.3}{32} \quad (16.5)$$

$$\frac{4.00}{100} \frac{2.4}{75} \frac{4.5}{53} \frac{8.2}{35} \quad (16.4)$$

$$\frac{4.6}{100} \frac{6.1}{85} \frac{7.8}{61} \quad (23.7)$$

$$\frac{1.9}{100} \frac{4.3}{86} \frac{7.3}{65} \quad (24.6)$$

$$\frac{3.7}{100} \frac{6.3}{88} \frac{10.7}{68} \frac{15.4}{52} \frac{18.6}{31} \quad (25.4)$$

$$\frac{72.0}{100} \frac{00}{88} \frac{5.1}{89} \frac{8.6}{50} \frac{9.7}{37} \quad (13.6)$$

$$\frac{3.8}{50} \frac{4.5}{46} \frac{5.2}{47} \frac{5.3}{17} \frac{9.3}{14} \frac{3.4}{34} \frac{4.3}{12} \frac{7.7}{15} \frac{8.9}{50}$$

$$\frac{7.6}{50} \frac{7.1}{37} \frac{8.0}{33} \frac{7.6}{21} \frac{5.4}{13} \frac{4.1}{9} \frac{4.8}{13} \frac{8.6}{21} \frac{9.1}{50}$$

$$\frac{8.0}{50} \frac{7.6}{40} \frac{8.1}{19} \frac{4.9}{10} \frac{4.6}{10} \frac{5.2}{10} \frac{5.8}{13} \frac{9.1}{20} \frac{9.4}{35} \frac{9.4}{50}$$

STA	+	↑	-	ELEV
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869.55.

9+00

64.5.

+50

64.3.

10+00

64.4.

+50

64.6.

11+00

64.6.

+50

64.6.

12+00

64.7.

+50

64.8.

+57

SECTION & 60" C.M X DRAIN

64.9.

13+00

64.3.

+50

64.5.

14+00

64.4.

LT

L

RT

$$\begin{array}{cccccccccccc} 7.8 & 7.6 & 8.2 & 5.6 & 5.3 & & 5.4 & 6.1 & 8.9 & 9.2 & 9.6 \\ 50 & 33 & 27 & 11 & 8 & 5.1 & 9 & 12 & 19 & 25 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 8.3 & 7.7 & 7.4 & 7.8 & 7.6 & 5.6 & 5.3 & 5.6 & 6.2 & 9.0 & 9.6 & 9.6 \\ 50 & 41 & 30 & 24 & 18 & 10 & 5.3 & 8 & 11 & 20 & 32 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 7.3 & 7.7 & 6.9 & 7.0 & 6.0 & 5.3 & 5.2 & 5.5 & 6.3 & 8.9 & 9.2 \\ 50 & 40 & 28 & 17 & 14 & 9 & 9 & 9 & 12 & 20 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 8.3 & 7.6 & 7.5 & 5.6 & 5.2 & 5.0 & 5.2 & 5.5 & 7.2 & 7.2 & 7.2 \\ 50 & 31 & 17 & 11 & 9 & 5.0 & 9 & 11 & 17-19 & 23 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 8.5 & 8.3 & 8.0 & 5.8 & 5.4 & 5.0 & 5.2 & 5.6 & 7.2 & 7.6 & 8.2 \\ 50 & 26 & 18 & 11 & 9 & 5.0 & 9 & 12 & 18-20 & 23 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 8.5 & 8.3 & 5.8 & 5.4 & 5.0 & 5.3 & 6.1 & 8.4 & 7.9 & 7.8 & 8.1 & 9.1 \\ 50 & 20 & 12 & 10 & 5.0 & 9 & 13 & 19-20 & 22 & 34 & 41 & 50 \end{array}$$

$$\text{DITCH } \begin{array}{cccccccccccc} 10.6 & 8.3 & 5.5 & 5.9 & 5.4 & 4.9 & 5.2 & 6.0 & 8.2 & 8.5 \\ 12.5 & 50 & 21 & 13 & 9 & 4.9 & 9 & 11 & 18 & 50 \end{array}$$

DITCH

$$\begin{array}{cccccccccccc} 8.6 & 10.2 & 8.3 & 8.5 & 5.7 & 5.2 & 4.8 & 5.3 & 5.1 & 5.9 & 5.8 & 8.2 \\ 50 & 47 & 44 & 41 & 20 & 12 & 9 & 4.8 & 9 & 11 & 19 & 40-50 \end{array}$$

FL

FL

$$\begin{array}{cccccccc} 4.7 & 10.7 & 11.2 & 5.7 & 5.0 & 4.7 & 5.0 & 5.7 \\ 50 & 15 & 15 & 13 & 10 & 9 & 15 & 15 \end{array}$$

$$\begin{array}{cccccccc} 8.1 & 8.2 & 5.5 & 5.2 & 5.3 & 6.3 & 8.4 & 7.9 & 7.8 \\ 50 & 18 & 13 & 10 & 13 & 13 & 18 & 25 & 50 \end{array}$$

$$\begin{array}{cccccccc} 7.9 & 8.0 & 6.2 & 5.6 & 5.1 & 5.3 & 5.9 & 8.5 & 8.5 & 9.0 \\ 50 & 18 & 14 & 10 & 10 & 10 & 13 & 21 & 40 & 50 \end{array}$$

$$\begin{array}{cccccccc} 7.9 & 8.1 & 6.0 & 5.5 & 5.2 & 5.5 & 6.8 & 7.9 & 8.2 & 8.0 & 7.0 \\ 50 & 17 & 13 & 9 & 5.2 & 10 & 14 & 20 & 24 & 29 & 43-50 \end{array}$$

STA	+	π	-	ELEV
		869.55.		
14+50				64.8.
T.P.	5.93	870.03.	5.45	864.10.
15+00				64.8.
+50				64.9.
16+00				65.1.
+50				65.0.
17+00				65.3.
+50				65.7.
18+00				65.8.
+15				65.9.
+50				66.0.
19+00				66.4.
+50				66.5.

LT

L

RT

$$\begin{array}{r} 8.0 \quad 7.7 \quad 5.4 \quad 4.8 \quad 5.2 \quad 6.0 \quad 8.6 \quad 7.6 \\ 50-32 \quad 17 \quad 12 \quad 4 \quad 11 \quad 15 \quad 22-29 \quad 34-50 \end{array}$$

NAIK IN P.P. LT STA. 14+25

$$\begin{array}{r} 8.5 \quad 8.4 \quad 6.4 \quad 5.9 \quad 5.4 \quad 5.2 \quad 5.3 \quad 6.4 \quad 8.5 \quad 8.5 \quad 7.8 \quad 8.6 \\ 50 \quad 17 \quad 13 \quad 9 \quad 4 \quad 5 \quad 9 \quad 11 \quad 16 \quad 21 \quad 24 \quad 28 \quad 50 \end{array}$$

$$\begin{array}{r} 8.3 \quad 8.0 \quad 6.2 \quad 5.6 \quad 5.3 \quad 5.1 \quad 5.1 \quad 5.3 \quad 5.9 \quad 8.4 \quad 8.4 \quad 7.9 \quad 8.4 \\ 50 \quad 19 \quad 13 \quad 10 \quad 6 \quad 5 \quad 6 \quad 11 \quad 15 \quad 21 \quad 24 \quad 26 \quad 41-50 \end{array}$$

$$\begin{array}{r} 8.2 \quad 8.0 \quad 6.3 \quad 5.6 \quad 5.3 \quad 4.9 \quad 5.0 \quad 5.5 \quad 8.0 \quad 8.3 \quad 8.5 \quad 8.6 \quad 7.7 \quad 5.1 \quad 8. \\ 50 \quad 19 \quad 14 \quad 11 \quad 8 \quad 4 \quad 10 \quad 13 \quad 21 \quad 27 \quad 31 \quad 36 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 8.0 \quad 7.5 \quad 6.2 \quad 5.5 \quad 5.0 \quad 5.0 \quad 5.6 \quad 7.0 \quad 6.5 \quad 4.4 \quad 4.0 \quad 9.6 \quad 11.2 \quad 12.4 \\ 50 \quad 19 \quad 14 \quad 10 \quad 5 \quad 8 \quad 12 \quad 16 \quad 19 \quad 25 \quad 32 \quad 36 \quad 41 \quad 50 \end{array}$$

$$\begin{array}{r} 7.7 \quad 7.7 \quad 7.3 \quad 6.2 \quad 5.3 \quad 4.9 \quad 4.9 \quad 5.3 \quad 5.3 \quad 4.2 \quad 4.3 \quad 6.6 \quad 9.8 \quad 11.0 \quad 13.1 \\ 50 \quad 27 \quad 18 \quad 15 \quad 11 \quad 6 \quad 4 \quad 9 \quad 12 \quad 14 \quad 18 \quad 23 \quad 28 \quad 30 \quad 35 \quad 50 \end{array}$$

$$\begin{array}{r} 6.8 \quad 6.1 \quad 6.1 \quad 5.1 \quad 4.8 \quad 4.5 \quad 4.8 \quad 5.4 \quad 5.2 \quad 4.2 \quad 4.1 \quad 6.4 \quad 11.4 \quad 13.3 \\ 50 \quad 28 \quad 19 \quad 15 \quad 12 \quad 7 \quad 4 \quad 8 \quad 12 \quad 15 \quad 19 \quad 22 \quad 27 \quad 34 \quad 50 \end{array}$$

$$\begin{array}{r} 4.6 \quad 4.6 \quad 4.4 \quad 4.3 \quad 4.3 \quad 4.2 \quad 4.5 \quad 5.1 \quad 6.1 \quad 6.4 \quad 6.3 \quad 10.0 \quad 11.2 \quad 13.0 \\ 50 \quad 32 \quad 30 \quad 18 \quad 8 \quad 4 \quad 6 \quad 10 \quad 16 \quad 22 \quad 28 \quad 32 \quad 36 \quad 50 \end{array}$$

$$\begin{array}{r} 4.0 \quad 3.6 \quad 3.3 \quad 4.0 \quad 6.4 \quad 6.4 \quad 4.5 \quad 4.2 \quad 4.1 \quad 4.3 \quad 4.8 \quad 6.4 \quad 6.6 \quad 6.0 \quad 9.7 \quad 11.2 \quad 12.7 \\ 50 \quad 46 \quad 40 \quad 31 \quad 24 \quad 19 \quad 14 \quad 8 \quad 4 \quad 5 \quad 10 \quad 15 \quad 21 \quad 28 \quad 31 \quad 36 \quad 50 \end{array}$$

$$\begin{array}{r} 3.0 \quad 4.0 \quad 6.2 \quad 6.2 \quad 4.3 \quad 4.0 \quad 4.0 \quad 4.2 \quad 4.6 \quad 5.7 \quad 6.8 \quad 6.3 \quad 10.1 \quad 11.3 \quad 12.4 \\ 50 \quad 30 \quad 25 \quad 18 \quad 14 \quad 5 \quad 6 \quad 10 \quad 14 \quad 22 \quad 32 \quad 35 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 1.3 \quad 2.8 \quad 5.5 \quad 5.3 \quad 3.7 \quad 3.6 \quad 3.9 \quad 4.5 \quad 5.7 \quad 6.6 \quad 6.9 \quad 6.2 \quad 10.1 \quad 11.0 \quad 11.9 \\ 50 \quad 31 \quad 24 \quad 18 \quad 13 \quad 5 \quad 3 \quad 6 \quad 9 \quad 13 \quad 16 \quad 28 \quad 35 \quad 38 \quad 43 \quad 50 \end{array}$$

$$\begin{array}{r} +2.3 \quad 0.2 \quad 1.1 \quad 4.8 \quad 4.6 \quad 3.6 \quad 3.6 \quad 3.5 \quad 3.8 \quad 4.4 \quad 7.3 \quad 7.2 \quad 6.7 \quad 9.9 \quad 11.2 \quad 11.5 \\ 50 \quad 33 \quad 27 \quad 20 \quad 17 \quad 13 \quad 9 \quad 7 \quad 11 \quad 17 \quad 30 \quad 38 \quad 44 \quad 47 \quad 50 \end{array}$$

STA	+	π	-	ELEV
		870.03.		
B.M	6.78	873.12.	3.70	866.33. 866.34
20+00				66.9.

	+50			67.4.
--	-----	--	--	-------

21+00				67.9.
-------	--	--	--	-------

	+50			68.4.
--	-----	--	--	-------

22+00				68.8.
-------	--	--	--	-------

	+34	SECTION 10" X 32' C. M X DRAIN		
--	-----	--------------------------------	--	--

	+50			69.2.
--	-----	--	--	-------

23+00				69.6.
-------	--	--	--	-------

	+50			70.0.
--	-----	--	--	-------

T.P	12.52	884.77.	0.87	872.25.
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T.P	13.41	896.78.	1.40	883.37.
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20+00				(66.9)
-------	--	--	--	--------

	+50			(67.4)
--	-----	--	--	--------

LT

L

RT

SPIKE 28" ELM 14 RT STA 19+60

$$\begin{array}{cccccccccccccccc} \frac{4.3}{21} & \frac{7.1}{16} & \frac{6.6}{13} & \frac{6.3}{7} & \frac{6.2}{6} & \frac{6.5}{8} & \frac{7.0}{11} & \frac{10.4}{18} & \frac{10.3}{32} & \frac{10.2}{40} & \frac{9.7}{47} & \frac{13.6}{58} & \frac{15.1}{60} \end{array}$$

$$\begin{array}{cccccccccccccccc} \frac{2.7}{22} & \frac{6.4}{13} & \frac{5.8}{11} & \frac{5.8}{6} & \frac{5.7}{5} & \frac{6.3}{11} & \frac{6.8}{14} & \frac{10.2}{22} & \frac{10.2}{30} & \frac{10.4}{41} & \frac{9.6}{44} & \frac{13.0}{48} & \frac{14.5}{58} \end{array}$$

15.0/61

$$\begin{array}{cccccccccccccccc} \frac{0.9}{19} & \frac{5.7}{13} & \frac{5.2}{11} & \frac{5.2}{6} & \frac{5.2}{5} & \frac{5.6}{29} & \frac{6.3}{20} & \frac{10.4}{22} & \frac{10.5}{31} & \frac{10.7}{40} & \frac{9.6}{45} & \frac{13.4}{47} & \frac{14.5}{52} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{4.9}{12} & \frac{4.9}{6} & \frac{4.7}{5} & \frac{4.7}{15} & \frac{5.6}{24} & \frac{10.4}{38} & \frac{10.4}{41} & \frac{9.3}{44} & \frac{13.3}{44} & \frac{14.9}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{4.8}{14} & \frac{4.5}{7} & \frac{4.3}{7} & \frac{4.5}{7} & \frac{4.9}{16} & \frac{9.4}{26} & \frac{8.4}{38} & \frac{9.8}{42} & \frac{13.1}{44} & \frac{14.9}{52} \end{array}$$

F.L

F.L

$$\begin{array}{cccccccccccccccc} \frac{2.9}{17} & \frac{6.0}{11} & \frac{4.3}{6} & \frac{4.1}{4} & \frac{4.2}{7} & \frac{4.5}{17} & \frac{8.4}{25} & \frac{9.5}{32} & \frac{9.3}{36} & \frac{13.1}{39} & \frac{14.0}{43} & \frac{14.6}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{1.6}{18} & \frac{4.4}{11} & \frac{4.0}{8} & \frac{3.9}{7} & \frac{4.0}{7} & \frac{4.4}{16} & \frac{4.5}{21} & \frac{8.8}{30} & \frac{12.5}{34} & \frac{14.5}{40} & \frac{15.1}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{0.8}{20} & \frac{3.8}{15} & \frac{3.5}{12} & \frac{3.6}{7} & \frac{3.5}{5} & \frac{3.7}{5} & \frac{4.0}{14} & \frac{5.1}{19} & \frac{6.3}{27} & \frac{14.5}{35} & \frac{16.2}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{2.5}{16} & \frac{2.9}{9} & \frac{3.1}{3} & \frac{3.4}{13} & \frac{4.9}{20} & \frac{14.3}{32} & \frac{16.5}{50} \end{array}$$

$$\begin{array}{cccc} \frac{11.6}{98} & \frac{14.0}{70} & \frac{11.7}{50} & \frac{22.1}{29} \end{array}$$

(29.9)

$$\begin{array}{cccc} \frac{5.1}{100} & \frac{8.7}{80} & \frac{10.6}{65} & \frac{12.3}{56} & \frac{14.3}{45} & \frac{18.6}{34} \end{array}$$

(29.4)

STA	+	π	-	ELEV
-----	---	-------	---	------

896.78.

21+00

(67.9)

+50

(68.4)

22+00

(68.8)

+50

(69.2)

23+00

(69.6)

T.P.

0.03

883.71.

13.10

883.68.

+50

(70.0)

+50

Profile Ent Lt.

70.0.

+68

X Drain

T.P.

T.P.

8.83

881.08.

1146

872.25.

24

69.9

+50

69.4.

T.P.

411

872.44.

1275

868.33.

25

68.6.

+50

67.8.

LT.

L

RT

✓

$$\frac{1.9}{100} \frac{4.8}{80} \frac{6.1}{74} \frac{7.1}{67} \frac{8.7}{58} \frac{24.3}{33} \frac{22.3}{23} \quad (28.9)$$

✓

$$\frac{0.2}{100} \frac{2.7}{82} \frac{5.7}{65} \frac{14.8}{43} \frac{20.3}{26} \quad (28.4)$$

✓

$$\frac{+1.0}{100} \frac{0.0}{96} \frac{10.5}{78} \frac{12.0}{62} \frac{14.0}{58} \frac{15.4}{48} \frac{17.0}{44} \frac{19.4}{30} \quad (28.0)$$

✓

$$\frac{10.6}{0.0} \frac{11.8}{76} \frac{14.0}{64} \frac{14.5}{58} \frac{17.5}{51} \frac{18.3}{46} \frac{20.6}{37} \frac{22.5}{31} \quad (27.6)$$

$\frac{98.94}{+1.5/01}$

✓

$$\frac{2.4}{100} \frac{4.6}{83} \frac{7.3}{60} \frac{12.1}{57} \frac{16.9}{39} \frac{16.9}{33} \quad (27.2)$$

✓

$$\frac{+7.7}{100} \frac{+6.7}{90} \frac{+3.2}{70} \frac{+1.5}{46} \frac{1.5}{46} \frac{7.2}{34} \quad (13.7)$$

✓

$$\frac{4.8}{100} \frac{7.1}{75} \frac{10.2}{50} \frac{12.8}{21} \frac{13.5}{1.2} \quad 137$$

$$\frac{86.69}{17.02} \quad \text{INV}$$

$$\frac{86.65}{21.06} \quad \text{INV}$$

✓

$$\frac{77.7}{75} \frac{3.7}{62} \frac{4.7}{50} \frac{6.0}{40} \frac{8.4}{25} \frac{11.9}{16} \frac{11.1}{14} \frac{11.2}{11} \frac{11.6}{9} \frac{11.9}{15} \frac{20.8}{27} \frac{22.3}{34} \frac{23.3}{50}$$

✓

$$\frac{0.0}{75} \frac{4.3}{50} \frac{7.8}{29} \frac{12.5}{18} \frac{12.5}{15} \frac{11.6}{11} \frac{11.7}{11} \frac{12.3}{11} \frac{13.0}{15} \frac{13.5}{20} \frac{21.0}{28} \frac{22.2}{40} \frac{23.9}{50}$$

✓

$$\frac{77.7}{75} \frac{+3.2}{46} \frac{0.0}{27} \frac{4.6}{17} \frac{4.0}{15} \frac{3.8}{11} \frac{3.8}{38} \frac{4.4}{10} \frac{4.8}{13} \frac{5.7}{20} \frac{12.4}{28} \frac{14.3}{38} \frac{14.7}{50}$$

✓

$$\frac{48.7}{75} \frac{+4.0}{50} \frac{0.0}{34} \frac{3.5}{22} \frac{5.1}{20} \frac{4.4}{18} \frac{4.6}{14} \frac{5.0}{9} \frac{5.6}{16} \frac{6.9}{20} \frac{12.3}{25} \frac{13.3}{32} \frac{15.1}{50}$$

STA + π - ELEV

872.44.

26 67.5.

+50 67.3.

+90 12" V.I. x Drain 67.0.

27 67.0.

+50 66.9.

28 66.8.

TP 1287 879.73. 558 866.86.

26 (67.5).

+50 (67.3).

27 (67.0).

+50 (66.9).

28 (66.8).

+14 Profile End Lt 66.9.

LT

L

RT

15.2

50

$$\checkmark \quad \frac{0.4}{29} \quad \frac{33}{22} \quad \frac{5.2}{18-16} \quad \frac{47}{12} \quad 49 \quad \frac{5.3}{9} \quad \frac{5.6}{13} \quad \frac{6.3}{20} \quad \frac{8.2}{25} \quad \frac{12.7}{30} \quad \frac{13.4}{34}$$

$$\checkmark \quad \frac{0.0}{36} \quad \frac{4.4}{23} \quad \frac{6.2}{20} \quad \frac{6.2}{18} \quad \frac{5.4}{16} \quad \frac{5.0}{12} \quad 51 \quad \frac{5.9}{10} \quad \frac{6.5}{14} \quad \frac{8.2}{26} \quad \frac{13.0}{31} \quad \frac{13.8}{38} \quad \frac{14.7}{50}$$

$$\checkmark \quad \begin{array}{c} \text{Inv} \\ \frac{0.4}{35} \end{array} \quad \frac{8.2}{21} \quad \frac{8.45}{21} \quad \frac{5.6}{16} \quad \frac{5.2}{12} \quad 54 \quad \frac{6.0}{8} \quad \frac{6.6}{12} \quad \begin{array}{c} \text{Inv} \\ \frac{11.62}{19} \end{array} \quad \frac{12.4}{33} \quad \frac{11.0}{36} \quad \frac{12.5}{38} \quad \frac{13.7}{45}$$

$$\checkmark \quad \frac{0.0}{35} \quad \frac{4.0}{25} \quad \frac{6.7}{20-18} \quad \frac{5.6}{15} \quad \frac{5.2}{12} \quad 54 \quad \frac{6.3}{10} \quad \frac{7.2}{13} \quad \frac{9.1}{33} \quad \frac{12.9}{42} \quad \frac{13.4}{50}$$

$$\checkmark \quad \frac{0.5}{38} \quad \frac{3.7}{22} \quad \frac{5.8}{17-15} \quad \frac{5.5}{13} \quad \frac{5.4}{10} \quad 55 \quad \frac{6.0}{8} \quad \frac{6.6}{13} \quad \frac{8.4}{19} \quad \frac{9.7}{35} \quad \frac{11.6}{39} \quad \frac{13.9}{50}$$

12.7
50

$$\checkmark \quad \frac{0.7}{36} \quad \frac{3.7}{21} \quad \frac{5.7}{17} \quad \frac{5.3}{15} \quad \frac{5.2}{12} \quad 56 \quad \frac{6.1}{9} \quad \frac{6.4}{14} \quad \frac{8.6}{21} \quad \frac{9.3}{32} \quad \frac{10.4}{39} \quad \frac{11.7}{42}$$

$$\checkmark \quad \frac{0.0}{62} \quad \frac{2.8}{50} \quad \frac{5.2}{38} \quad (12.2)$$

$$\checkmark \quad \frac{0.0}{60} \quad \frac{3.9}{46} \quad (12.4)$$

$$\checkmark \quad \frac{0.2}{60} \quad \frac{3.1}{53} \quad \frac{5.8}{42} \quad (12.7)$$

$$\checkmark \quad \frac{0.0}{68} \quad \frac{4.7}{50} \quad \frac{6.6}{45} \quad (12.8)$$

$$\checkmark \quad \frac{0.9}{65} \quad \frac{4.4}{50} \quad (12.9)$$

$$\checkmark \quad \frac{+1.3}{100} \quad \frac{3.4}{75} \quad \frac{7.4}{50} \quad \frac{11.6}{25} \quad 12.8$$

Sta	+	π	-	Elev
		87973.		
28+50				66.7.
+80	Profile Ent Lt.			66.6.
29				66.6.
+11				66.4.
+50				66.4.
T.P.	3.50	87192.	1131	868.42.
+57	Profile Ent Lt.			66.3.
+63				66.3.
+76	12" x 70' CM			66.3.
30				66.4.
+50				66.7.
31				67.0.
+50				66.9.
32				67.3.
B.M.			660	865.32. 865.33.

Lt

Rt

Rt

$$\begin{array}{cccccccccccccccc} \checkmark & 1.5 & & & & & & & & & & & & & & & & & & & 20.5 \\ & (0.5) & 41 & 65 & 82 & 112 & 128 & 128 & & 133 & 136 & 164 & 180 & 190 & 190 & & & & & 65 \\ & 75 & 63 & 50 & 35 & 21 & 16 & 10 & 130 & 8 & 15 & 22 & 38 & 46 & 50 & & & & & \\ \checkmark & & 44 & & 63 & & 125 & & 131 & & & & & & & & & & & 21 \\ & & 72 & & 62 & & 25 & & & & & & & & & & & & & 70 \\ \checkmark & & 44 & 63 & 85 & 123 & 131 & 130 & & 136 & 139 & 157 & 178 & 186 & 183 & & & & & \\ & & 76 & 52 & 47 & 22 & 18 & 72 & 131 & 11 & 15 & 22 & 37 & 50 & 62 & & & & & \\ & & & & & & & & & & & & & & & & & & & 21 \\ & & & & & & & & & & & & & & & & & & & 71 \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & 44 & 44 & 92 & 126 & 139 & 135 & & 133 & 139 & 138 & 138 & \text{Tar} & & & & & & \\ & & 88 & 65 & 50 & 22 & 13 & 9 & 133 & 6 & 11 & 26 & 33 & - & & & & & & \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & & & 30 & 36 & 5.2 & 5.4 & & 6.2 & 6.2 & \text{Tar} & & & & & & & & \\ & & & & 50 & 39 & 21 & 12 & 56 & 10 & 38 & & & & & & & & & \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & & & 19 & 34 & 5.4 & 5.5 & & 6.2 & 6.1 & \text{Tar} & & & & & & & & \\ & & & & 40 & 25 & 20 & 13 & 56 & 10 & 33 & & & & & & & & & \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & & & \text{Inv} & & & & & & & & & & \text{Inv} & & & & & \\ & & 18 & 36 & 63 & 864 & 63 & 56 & & 60 & 63 & 63 & 72 & 101 & 122 & 132 & & & & \\ & & 35 & 25 & 19 & 17 & 17 & 10 & 56 & 8 & 11 & 33 & 34 & 50 & 53 & 67 & & & & \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & 1.1 & & 2.6 & 6.7 & 5.9 & 5.6 & & 6.1 & 6.6 & 6.4 & 6.8 & 10.7 & 11.4 & 11.7 & & & & \\ & & 38 & & 23 & 17 & 15 & 9 & 5.5 & 8 & 11 & 14 & 24 & 35 & 50 & 58 & & & & \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & & & 1.8 & 2.0 & 5.5 & 5.4 & & 5.9 & 6.8 & 9.2 & 11.0 & 11.0 & 10.0 & 12.2 & 12.2 & & & \\ & & & & 29 & 22 & 18 & 12 & 5.2 & 9 & 15 & 20 & 31 & 41 & 45 & 47 & 57 & & & \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & 1.1 & & 2.1 & 5.1 & 4.9 & & & 5.5 & 6.0 & 10.1 & 10.9 & 11.6 & 12.3 & 13.3 & & & & \\ & & 30 & & 21 & 17-14 & 12 & 4.9 & & 10 & 13 & 24 & 29 & 46 & 50 & 60 & & & & \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & 1.8 & 38 & 43 & 45 & & & & 5.4 & 6.1 & 9.5 & 11.5 & 9.9 & 11.5 & 11.7 & 12.8 & & & \\ & & 20 & 16 & 13 & 10 & 50 & & & 9 & 16 & 23 & 38 & 40 & 41 & 47 & 50 & & & \end{array}$$

$$\begin{array}{cccccccccccccccc} \checkmark & & & & 0.2 & 3.9 & 4.0 & & & 5.3 & 5.7 & 10.0 & 11.3 & 10.5 & 13.2 & & & & \\ & & & & 21 & 16 & 9 & 46 & & 10 & 14 & 23 & 32 & 34 & 50 & & & & \end{array}$$

Sph in 28' Cotl 25' Rt St 32+47

Sta	+	X	-	Elev
	17.18	882.51.		
29+57				(66.3)
+63				(66.3)
+76				(66.3)
30+00				(66.4)
+50				(66.7)
31+06				(67.0)
+50				(66.9)
32+00				(67.3)
T.P.	7.82	873.15.	17.18	865.33.
+50				67.5
33+00				67.7
+20				67.6

+31 SECTION 15" X 40' X DRAIN
67.7

Lt

Rt

Rt

$$\checkmark \quad \frac{4.7}{100} \quad \frac{10.1}{75} \quad (16.2)$$

$$\checkmark \quad \frac{4.6}{100} \quad \frac{7.8}{75} \quad \frac{11.3}{50} \quad (16.2)$$

$$\checkmark \quad \frac{3.3}{100} \quad \frac{6.2}{75} \quad \frac{10.7}{50} \quad (16.2)$$

$$\checkmark \quad \frac{1.9}{100} \quad \frac{5.3}{75} \quad \frac{8.7}{57} \quad (16.1)$$

$$\checkmark \quad \frac{7.0}{100} \quad \frac{0.8}{70} \quad \frac{4.0}{55} \quad \frac{5.2}{43} \quad (15.8)$$

$$\checkmark \quad \frac{7.0}{100} \quad \frac{0.0}{75} \quad \frac{1.1}{55} \quad (15.5)$$

$$\checkmark \quad \frac{7.0}{100} \quad \frac{0.8}{58} \quad \frac{5.6}{36} \quad (15.6)$$

$$\checkmark \quad \frac{7.0}{100} \quad \frac{4.3}{61} \quad \frac{6.6}{32} \quad (15.2)$$

$$\checkmark \quad \frac{5.2}{16} \quad \frac{5.6}{7} \quad \frac{5.7}{9} \quad \frac{6.2}{12} \quad \frac{6.5}{28} \quad \frac{12.3}{45} \quad \frac{14.0}{50} \quad \frac{15.3}{50}$$

$$\checkmark \quad \frac{4.5}{17} \quad \frac{5.4}{8} \quad \frac{5.5}{10} \quad \frac{6.1}{13} \quad \frac{6.3}{29} \quad \frac{11.8}{42} \quad \frac{13.9}{50} \quad \frac{15.1}{50}$$

$$\checkmark \quad \frac{5.2}{17} \quad \frac{5.4}{9} \quad \frac{5.6}{10} \quad \frac{6.0}{13} \quad \frac{6.3}{30} \quad \frac{12.3}{43} \quad \frac{14.0}{50} \quad \frac{15.2}{50}$$

$$\checkmark \quad \begin{array}{cccccccc} & & \text{F.L.} & & & & & & \text{F.L.} \\ \frac{0.7}{25} & \frac{10.2}{16} & \frac{10.0}{15} & \frac{5.4}{13} & \frac{5.3}{8} & \frac{5.5}{55} & \frac{6.0}{11} & \frac{6.5}{16} & \frac{11.4}{26} & \frac{12.7}{40} & \frac{13.9}{43} & \frac{15.5}{50} \end{array}$$

STA + ∇ - ELEV
873.15.

33+50 67.8.

34+00 67.9.

+50 67.7.

35+00 67.3.

+50 67.4.

36+00 67.3.

36+00 Ent Profile Left (67.3).

T. P. 18.73 888.45. 343 869.72.

32+50 (67.5).

33+00 (67.7).

+20 (67.6).

+31 (67.7).

+50 (67.8).

LT

Q

RT

$$\checkmark \quad \frac{1.1}{25} \frac{6.3}{15} \frac{5.3}{12} \frac{5.2}{9} \frac{5.4}{5} \frac{5.8}{10} \frac{6.2}{14} \frac{12.4}{31} \frac{14.0}{43} \frac{15.9}{55}$$

$$\checkmark \quad \frac{0.9}{26} \frac{5.7}{17} \frac{5.2}{13} \frac{5.2}{11-9} \frac{5.3}{5} \frac{5.8}{11} \frac{6.3}{14} \frac{12.6}{32} \frac{13.9}{41} \frac{15.3}{50}$$

$$\checkmark \quad \frac{2.7}{25} \frac{5.7}{16-14} \frac{5.5}{10} \frac{5.5}{5} \frac{6.0}{10} \frac{6.3}{13} \frac{11.8}{29} \frac{14.6}{43} \frac{15.6}{64}$$

$$\checkmark \quad \frac{2.6}{23} \frac{6.3}{15-13} \frac{5.8}{10-8} \frac{5.9}{5} \frac{6.3}{11} \frac{6.5}{13} \frac{12.2}{33} \frac{14.6}{45} \frac{15.4}{60}$$

$$\checkmark \quad \frac{2.4}{25} \frac{6.3}{16-14} \frac{5.8}{11} \frac{5.7}{8} \frac{5.8}{5} \frac{6.3}{10} \frac{6.5}{11} \frac{12.6}{31} \frac{14.6}{47} \frac{15.6}{63}$$

$$\checkmark \quad \frac{2.6}{26} \frac{6.3}{18-16} \frac{5.5}{11} \frac{5.9}{5} \frac{6.1}{10} \frac{6.2}{12} \frac{12.6}{33} \frac{14.6}{47} \frac{15.5}{63}$$

$$\frac{37}{28} \frac{5.2}{10} 5.9$$

$$\checkmark \quad \frac{1.3}{80} \frac{3.9}{66} \frac{9.8}{34} \quad (21.0)$$

$$\checkmark \quad \frac{2.9}{84} \frac{6.2}{60} \frac{11.1}{37} \frac{13.4}{31} \quad (20.8)$$

$$\checkmark \quad \frac{0.8}{90} \frac{3.5}{76} \frac{7.2}{54} \frac{13.9}{32} \quad (20.9)$$

$$\checkmark \quad \frac{1.5}{89} \frac{5.9}{62} \frac{12.9}{40} \quad (20.8)$$

$$\checkmark \quad \frac{6.7}{87} \frac{4.7}{62} \frac{12.6}{40} \quad (20.7)$$

STA	+	π	-	ELEV
		888.45		

34+00				67.9
-------	--	--	--	------

+50				67.7
-----	--	--	--	------

35+00				67.3
-------	--	--	--	------

+50				67.4
-----	--	--	--	------

36+00				67.3
-------	--	--	--	------

36+00	ENT. PROFILE LEFT			
-------	-------------------	--	--	--

T.P	1.55	871.27	18.73	869.72
-----	------	--------	-------	--------

+35				67.3
-----	--	--	--	------

+50				67.2
-----	--	--	--	------

37+00				67.0
-------	--	--	--	------

+50				66.9
-----	--	--	--	------

38+00				66.7
-------	--	--	--	------

+50				66.8
-----	--	--	--	------

Lt

R

Rt

✓

(2.2)

$$\begin{array}{r} 198 \quad 205 \quad 222 \\ \hline 42 \quad 65 \quad 76 \end{array}$$

✓

(1.7)

$$\begin{array}{r} 178 \quad 198 \quad 222 \\ \hline 40 \quad 51 \quad 85 \end{array}$$

✓

(1.8)

$$\begin{array}{r} 180 \quad 199 \quad 223 \\ \hline 46 \quad 58 \quad 85 \end{array}$$

✓

(2.3)

$$\begin{array}{r} 188 \quad 195 \quad 224 \\ \hline 42 \quad 56 \quad 80 \end{array}$$

✓

(3.1)

$$\begin{array}{r} 185 \quad 205 \quad 225 \\ \hline 39 \quad 56 \quad 90 \end{array}$$

✓

(4.2)

$$\begin{array}{r} 178 \quad 207 \quad 225 \\ \hline 36 \quad 60 \quad 90 \end{array}$$

✓

$$\begin{array}{r} 68 \quad 96 \quad 120 \\ \hline 100 \quad 74 \quad 50 \end{array}$$

(15.6)

✓

$$\begin{array}{r} 32 \quad 49 \quad 86 \quad 109 \\ \hline 98 \quad 72 \quad 46 \quad 24 \end{array}$$

(15.3)

✓

$$\begin{array}{r} 67 \quad 95 \quad 122 \quad 154 \\ \hline 100 \quad 68 \quad 50 \quad 32 \end{array}$$

(27.4)

✓

$$\begin{array}{r} 09 \quad 20 \quad 38 \quad 64 \quad 76 \\ \hline 100 \quad 83 \quad 68 \quad 50 \quad 40 \end{array}$$

(26.6)

Elev. at
No 60480

✓

$$\begin{array}{r} 80 \quad 81 \quad 95 \quad 119 \\ \hline 100 \quad 89 \quad 72 \quad 49 \end{array}$$

(34.3)

✓

$$\begin{array}{r} 27 \quad 32 \quad 49 \quad 81 \\ \hline 100 \quad 90 \quad 78 \quad 49 \end{array}$$

(33.7)

Sta	+	Δ	-	Elev
		910.56		
62				(77.6)
+50				(78.1)
63				(78.0)
T.P.	378	901.14 ³	13.21	897.39 ⁵
+50				(77.5)
64				(76.7)
T.P.	0.13	887.78 ^W	13.52	887.65 ⁵
+50				(75.6)
+70				75.3
T.P.	1.34	879.07 ⁰³	10.05	877.73 ⁶⁹
+90				74.8
65				74.6
+127 ²⁰		$\times$ CORD C		74.2
+50				73.5
66				71.8 _u
T.P.	0.87	866.45	13.49	865.58
66 + 70				

Lt

L

Rt

$$\checkmark \quad \frac{2.0}{100} \quad \frac{2.1}{92} \quad \frac{3.9}{73} \quad \frac{7.3}{53} \quad \frac{8.8}{47}$$

(33.0)

$$\checkmark \quad \frac{4.1}{100} \quad \frac{4.7}{77} \quad \frac{6.2}{66} \quad \frac{9.2}{46}$$

(32.5)

$$\checkmark \quad \frac{9.8}{100} \quad \frac{10.3}{80} \quad \frac{10.9}{60} \quad \frac{11.7}{38}$$

(32.6)

$$\checkmark \quad \frac{1.7}{100} \quad \frac{2.9}{87} \quad \frac{4.0}{70} \quad \frac{5.8}{58} \quad \frac{8.4}{33}$$

(23.7)

$$\checkmark \quad \frac{12.8}{100} \quad \frac{13.0}{82} \quad \frac{14.2}{50} \quad \frac{16.4}{28}$$

(24.5)

$$\checkmark \quad \frac{4.0}{100} \quad \frac{4.3}{83} \quad \frac{4.2}{58} \quad \frac{5.4}{50} \quad \frac{7.7}{29} \quad \frac{8.7}{24}$$

(12.2)

$$\checkmark \quad \frac{8.2}{100} \quad \frac{5.8}{75} \quad \frac{7.3}{50} \quad \frac{8.6}{42} \quad \frac{10.1}{25} \quad \frac{12.7}{19} \quad \frac{12.8}{12} \quad \frac{12.5}{9} \quad \frac{12.7}{9} \quad \frac{13.2}{12}$$

$$\checkmark \quad \frac{5.3}{60} \quad \frac{5.1}{50} \quad \frac{3.0}{31} \quad \frac{3.2}{23} \quad \frac{4.6}{18} \quad \frac{4.5}{13} \quad 4.3 \quad \frac{4.4}{8} \quad \frac{4.8}{13}$$

$$\checkmark \quad \frac{4.9}{50} \quad \frac{5.2}{32} \quad \frac{5.0}{19} \quad \frac{4.6}{9} \quad 4.5 \quad \frac{4.9}{10} \quad \frac{5.2}{13}$$

$$\checkmark \quad \frac{4.9}{35} \quad \frac{5.0}{16} \quad 4.9 \quad \frac{5.2}{10} \quad \frac{5.4}{13}$$

5.6

7.3

Sta + π - Elev

866.45

64+70

75.3

+90

74.8

65

74.6

127²⁰

74.2

T.P

11.00

876.58^x

0.87

865.58^x

B.M

4.10

872.48^x

872.47 ✓

LT

Q

RT

$$1 \quad \frac{9.9}{100} \quad \frac{5.0}{74} \quad \frac{10.7}{50} \quad (20.6)$$

$$1 \quad \frac{1.0}{99} \quad \frac{4.1}{68} \quad \frac{13.6}{40} \quad (20.8)$$

$$\checkmark \quad \frac{3.8}{99} \quad \frac{6.3}{79} \quad \frac{14.9}{40} \quad (21.2)$$

$$\checkmark \quad \frac{5.1}{100} \quad \frac{10.4}{87} \quad \frac{11.2}{75} \quad \frac{11.0}{71} \quad \frac{13.9}{50} \quad (21.1)$$

$$\checkmark \quad \frac{7.2}{100} \quad \frac{10.9}{76} \quad \frac{16.0}{50} \quad (21.2)$$

$$\frac{7.6}{120} \quad \frac{10.7}{100} \quad \frac{13.5}{75} \quad \frac{16.0}{50}$$

$$\checkmark \quad \frac{73.0}{75} \quad \frac{1.2}{32} \quad \frac{3.6}{17} \quad \frac{7.3}{13} \quad \frac{7.8}{10} \quad \frac{4.0}{4.0} \quad \frac{4.2}{8} \quad \frac{4.3}{9} \quad \frac{7.4}{78} \quad \frac{8.3}{24} \quad \frac{9.9}{27} \quad \frac{10.9}{36} \quad \frac{10.3}{38} \quad \frac{12.5}{47} \quad \frac{14.0}{65}$$

$$\checkmark \quad \frac{72.3}{70} \quad \frac{2.0}{50} \quad \frac{1.7}{23} \quad \frac{4.1}{17} \quad \frac{3.9}{16} \quad \frac{4.0}{13} \quad \frac{4.0}{10} \quad \frac{4.1}{4.1} \quad \frac{4.2}{8} \quad \frac{4.3}{10} \quad \frac{8.1}{21} \quad \frac{11.3}{38} \quad \frac{11.3}{45} \quad \frac{12.5}{53} \quad \frac{14.1}{70}$$

$$\checkmark \quad \frac{2.3}{50} \quad \frac{3.5}{39} \quad \frac{2.8}{26} \quad \frac{4.5}{17} \quad \frac{4.0}{15} \quad \frac{4.4}{12} \quad \frac{4.4}{8} \quad \frac{4.3}{4.3} \quad \frac{4.5}{7} \quad \frac{4.7}{10} \quad \frac{8.3}{20} \quad \frac{11.2}{43} \quad \frac{12.3}{52} \quad \frac{14.3}{79}$$

$$\checkmark \quad \frac{4.0}{50} \quad \frac{4.6}{22} \quad \frac{5.2}{16} \quad \frac{4.6}{14} \quad \frac{4.6}{12} \quad \frac{4.6}{9} \quad \frac{4.4}{4.4} \quad \frac{4.7}{8} \quad \frac{5.0}{12} \quad \frac{10.4}{33} \quad \frac{12.6}{54} \quad \frac{14.3}{81}$$

$$\checkmark \quad \frac{5.0}{50} \quad \frac{5.2}{21} \quad \frac{5.4}{16} \quad \frac{5.1}{14} \quad \frac{5.0}{13} \quad \frac{5.0}{9} \quad \frac{4.6}{4.6} \quad \frac{4.9}{11} \quad \frac{5.1}{13} \quad \frac{10.9}{38} \quad \frac{12.4}{55} \quad \frac{13.9}{81}$$

$$\checkmark \quad \frac{5.5}{63} \quad \frac{5.7}{40} \quad \frac{5.5}{18} \quad \frac{4.9}{10} \quad \frac{4.5}{4.5} \quad \frac{4.9}{10} \quad \frac{5.2}{12} \quad \frac{6.0}{20} \quad \frac{9.2}{34} \quad \frac{12.4}{60}$$

STA	+	π	-	ELEV
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871.27.

39+00

66.7.

+50

66.5.

+66

66.4.

+81

66.2.

+82

66.2.

40+00

65.8.

+50

65.2.

B.M 5.86 870.94. 6.20

865.07. (865.08)

+67

65.0.

+75

65.0.

+94 SECTION 30" X 84 C.M X DRAIN

65.0.

41+00

64.8.

+25

64.7.

LT

E

RT

$$\checkmark \quad \frac{6.5}{50} \quad \frac{6.9}{27} \quad \frac{5.1}{14} \quad \frac{5.0}{10} \quad \frac{4.6}{9} \quad \frac{5.1}{12} \quad \frac{5.4}{24} \quad \frac{8.1}{29} \quad \frac{9.7}{40} \quad \frac{10.8}{57} \quad \frac{12.1}{57}$$

$$\checkmark \quad \frac{5.4}{58} \quad \frac{5.6}{52} \quad \frac{7.3}{45} \quad \frac{7.6}{32} \quad \frac{7.1}{19} \quad \frac{5.0}{11} \quad \frac{4.8}{9} \quad \frac{5.2}{12} \quad \frac{5.7}{25} \quad \frac{8.7}{34} \quad \frac{10.2}{46} \quad \frac{11.3}{58} \quad \frac{12.1}{58}$$

$$\checkmark \quad \frac{4.8}{60} \quad \frac{5.0}{46} \quad \frac{5.2}{41} \quad \frac{7.6}{31} \quad \frac{7.5}{21} \quad \frac{5.3}{11} \quad \frac{5.2}{8} \quad \frac{4.9}{9} \quad \frac{5.2}{12} \quad \frac{5.7}{31} \quad \frac{9.8}{48} \quad \frac{11.0}{54} \quad \frac{11.1}{60} \quad \frac{12.2}{60}$$

$$\checkmark \quad \frac{4.9}{60} \quad \frac{5.1}{40} \quad \frac{5.7}{24} \quad \frac{8.1}{24} \quad \frac{7.1}{21} \quad \frac{5.9}{17} \quad \frac{5.4}{16} \quad \frac{5.1}{9} \quad \frac{5.5}{9} \quad \frac{5.7}{11} \quad \frac{7.9}{23} \quad \frac{10.0}{34} \quad \frac{11.0}{48} \quad \frac{12.1}{60}$$

$$\checkmark \quad \frac{4.9}{60} \quad \frac{5.1}{40} \quad \frac{5.9}{16} \quad \frac{5.1}{9} \quad \frac{5.5}{9} \quad \frac{5.7}{11} \quad \frac{7.9}{23} \quad \frac{10.0}{34} \quad \frac{11.0}{48} \quad \frac{12.1}{60}$$

$$\checkmark \quad \frac{5.2}{50} \quad \frac{5.5}{14} \quad \frac{5.5}{8} \quad \frac{5.5}{6.5} \quad \frac{5.7}{9} \quad \frac{6.1}{12} \quad \frac{8.1}{23} \quad \frac{10.0}{35} \quad \frac{10.9}{45} \quad \frac{10.9}{57}$$

$$\checkmark \quad \frac{6.9}{75} \quad \frac{10.1}{12.8} \quad \frac{7.0}{56} \quad \frac{6.2}{35} \quad \frac{6.8}{16} \quad \frac{6.4}{8} \quad \frac{6.1}{10} \quad \frac{6.4}{14} \quad \frac{6.7}{24} \quad \frac{9.0}{60} \quad \frac{10.9}{76} \quad \frac{13.4}{76}$$

SPIKE-IN-15' ELM N.W. COR KELLER PKY + ARCADE

$$\checkmark \quad \frac{6.2}{85} \quad \frac{7.5}{46} \quad \frac{9.6}{40-36} \quad \frac{7.4}{28} \quad \frac{7.2}{16} \quad \frac{6.2}{7} \quad \frac{5.9}{5.9} \quad \frac{6.3}{11} \quad \frac{6.6}{20} \quad \frac{10.2}{56} \quad \frac{11.7}{81}$$

$$\checkmark \quad \frac{6.4}{77} \quad \frac{6.9}{49} \quad \frac{7.8}{32} \quad \frac{7.2}{22} \quad \frac{6.3}{7} \quad \frac{5.9}{5.9} \quad \frac{6.3}{11} \quad \frac{6.6}{20} \quad \frac{10.2}{56} \quad \frac{11.7}{81}$$

$$\frac{10.32}{38}$$

$$\frac{5.9}{5.9}$$

$$\frac{11.60}{46}$$

$$\checkmark \quad \frac{7.3}{70} \quad \frac{6.8}{44} \quad \frac{6.3}{78} \quad \frac{6.9}{6.1} \quad \frac{7.1}{13} \quad \frac{7.3}{17} \quad \frac{10.3}{31} \quad \frac{10.3}{72}$$

$$\checkmark \quad \frac{9.5}{63} \quad \frac{9.0}{47} \quad \frac{7.7}{36} \quad \frac{7.4}{30} \quad \frac{6.6}{12} \quad \frac{6.2}{6.2} \quad \frac{2.5}{14} \quad \frac{7.9}{23} \quad \frac{9.0}{34} \quad \frac{11.6}{38-42} \quad \frac{9.3}{50} \quad \frac{10.5}{77}$$

STA	+	π	-	ELEV
		870.94.		

41+50				64.6.
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+77	SECTION-18"X48 VIT X DRAIN			64.5.
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42+00				64.6.
-------	--	--	--	-------

+50				65.3.
-----	--	--	--	-------

43+00				65.9.
-------	--	--	--	-------

+50				66.3.
-----	--	--	--	-------

44+00				67.3.
-------	--	--	--	-------

+39				68.1.
-----	--	--	--	-------

+50				68.3.
-----	--	--	--	-------

+75				68.9.
-----	--	--	--	-------

T.P	4.96	875.36	0.54	870.40.
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45				69.6.
----	--	--	--	-------

+25				70.1.
-----	--	--	--	-------

LI

E

RT

$$\checkmark \quad \frac{9.3}{60} \quad \frac{9.3}{44} \quad \frac{9.3}{35} \quad \frac{7.2}{20} \quad \frac{6.9}{15} \quad 6.3 \quad \frac{7.5}{13} \quad \frac{7.8}{20} \quad \frac{9.0}{50} \quad \frac{11.4}{61-67} \quad \frac{10.0}{69} \quad \frac{10.6}{81}$$

FL

F.L

$$\checkmark \quad \frac{9.8}{50-32} \quad \frac{9.8}{28} \quad \frac{10.6}{27} \quad \frac{9.8}{20} \quad \frac{9.8}{19} \quad \frac{6.8}{10} \quad 6.4 \quad \frac{7.4}{13} \quad \frac{7.8}{18} \quad \frac{11.75}{20} \quad \frac{11.0}{38} \quad \frac{9.5}{43} \quad \frac{10.6}{54}$$

$$\checkmark \quad \frac{9.9}{50-40} \quad \frac{9.5}{24} \quad \frac{6.9}{14} \quad \frac{6.5}{8} \quad 6.3 \quad \frac{7.0}{13} \quad \frac{7.4}{22} \quad \frac{9.6}{32} \quad \frac{10.3}{49} \quad \frac{11.3}{53-56} \quad \frac{10.3}{68} \quad \frac{10.9}{71}$$

$$\checkmark \quad \frac{9.5}{75} \quad \frac{9.0}{50} \quad \frac{9.2}{29} \quad \frac{6.3}{19} \quad \frac{5.8}{11} \quad 5.6 \quad \frac{6.2}{11} \quad \frac{6.7}{20} \quad \frac{10.2}{30} \quad \frac{10.8}{31} \quad \frac{11.8}{57} \quad \frac{13.1}{75}$$

$$\checkmark \quad \frac{7.2}{71} \quad \frac{7.9}{50} \quad \frac{7.8}{26} \quad \frac{5.4}{17} \quad \frac{5.2}{11} \quad 5.0 \quad \frac{5.6}{11} \quad \frac{6.1}{16} \quad \frac{12.2}{38} \quad \frac{13.2}{66}$$

ELEV 1ST FLOOR

$$\checkmark \quad \frac{3.30}{66} \quad \frac{6.6}{55} \quad \frac{6.6}{26} \quad \frac{5.4}{15} \quad \frac{4.8}{11} \quad 4.6 \quad \frac{5.0}{11} \quad \frac{5.6}{19} \quad \frac{11.4}{33} \quad \frac{13.9}{113} \quad \frac{14.4}{60}$$

$$\checkmark \quad \frac{0.2}{50} \quad \frac{1.0}{47} \quad \frac{4.8}{29} \quad \frac{4.8}{23} \quad \frac{4.2}{17} \quad \frac{4.0}{11} \quad 3.6 \quad \frac{4.1}{12} \quad \frac{4.8}{22} \quad \frac{10.7}{33} \quad \frac{11.8}{36} \quad \frac{14.5}{71}$$

$$\checkmark \quad \frac{3.3}{17} \quad \frac{3.2}{11} \quad 2.8 \quad \frac{3.2}{11} \quad \frac{3.8}{23} \quad \frac{9.2}{30} \quad \frac{12.4}{36} \quad \frac{14.2}{75}$$

$$\checkmark \quad \frac{3.2}{24} \quad \frac{3.0}{12} \quad 2.6 \quad \frac{2.8}{10} \quad \frac{3.5}{20} \quad \frac{9.4}{27} \quad \frac{12.4}{37} \quad \frac{14.2}{75}$$

$$\checkmark \quad \frac{2.8}{40} \quad \frac{2.8}{27} \quad \frac{2.5}{13} \quad 2.0 \quad \frac{2.3}{10} \quad \frac{2.6}{22} \quad \frac{9.8}{32} \quad \frac{12.2}{37} \quad \frac{14.7}{76}$$

$$\checkmark \quad \frac{1.6}{33} \quad \frac{5.0}{25} \quad \frac{6.0}{15} \quad \frac{6.3}{11} \quad 5.8 \quad \frac{6.0}{9} \quad \frac{6.4}{14} \quad \frac{6.4}{19} \quad \frac{5.4}{25} \quad \frac{13.8}{32} \quad \frac{16.4}{40} \quad \frac{18.0}{60}$$

$$\checkmark \quad \frac{0.0}{29} \quad \frac{3.4}{20} \quad \frac{5.9}{11} \quad 5.3 \quad \frac{5.6}{13} \quad \frac{6.3}{23} \quad \frac{5.5}{26} \quad \frac{15.2}{40} \quad \frac{17.0}{47} \quad \frac{18.0}{64}$$

Sta + π - Elev

875.36.

45450 70.4 .

+75 70.7 .

46 70.9 .

+25 70.6 .

+45 70.3 .

+75 69.8 .

47 69.1 .

+50 67.8 .

48+00 66.5 .

T.P. 9.40 875.36. 9.40 865.96 .

13.18 888.38. 0.16 875.20 .

44 (67.3) .

+39 (68.1) .

+50 (68.3) .

L+

R

R+

$$\checkmark \quad \frac{23}{25} \quad \frac{43}{17} \quad \frac{55}{10} \quad 50 \quad \frac{5.3}{15} \quad \frac{5.7}{28} \quad \frac{137}{39} \quad \frac{15.3}{50} \quad \frac{163}{60}$$

$$\checkmark \quad \frac{34}{19} \quad \frac{5.1}{10} \quad 47 \quad \frac{5.0}{11} \quad \frac{5.0}{25} \quad \frac{12.0}{33} \quad \frac{142}{47} \quad \frac{15.8}{60} \quad \frac{164}{75}$$

$$\checkmark \quad \frac{1.3}{23} \quad \frac{46}{15} \quad \frac{49}{11} \quad 45 \quad \frac{49}{13} \quad \frac{45}{23} \quad \frac{105}{33} \quad \frac{111}{36} \quad \frac{148}{41} \quad \frac{169}{47} \quad \frac{177}{68}$$

$$\checkmark \quad \frac{24}{22} \quad \frac{5.3}{18} \quad \frac{5.1}{11} \quad 48 \quad \frac{5.3}{12} \quad \frac{5.9}{17} \quad \frac{92}{23} \quad \frac{150}{32} \quad \frac{166}{39} \quad \frac{180}{70}$$

$$\checkmark \quad \frac{0.7}{25} \quad \frac{61}{18} \quad \frac{5.6}{13} \quad \frac{5.4}{10} \quad 51 \quad \frac{5.6}{11} \quad \frac{60}{13} \quad \frac{69}{19} \quad \frac{113}{28} \quad \frac{149}{31} \quad \frac{163}{36} \quad \frac{180}{66}$$

$$\checkmark \quad \frac{0.0}{50} \quad \frac{24}{22} \quad \frac{6.5}{16} \quad \frac{62}{13} \quad \frac{60}{8} \quad 56 \quad \frac{61}{11} \quad \frac{62}{14} \quad \frac{61}{18} \quad \frac{112}{22} \quad \frac{148}{30} \quad \frac{167}{38} \quad \frac{178}{59}$$

$$\checkmark \quad \frac{48}{50} \quad \frac{43}{20} \quad \frac{70}{16} \quad \frac{68}{12} \quad \frac{66}{10} \quad 63 \quad \frac{67}{11} \quad \frac{69}{14} \quad \frac{73}{20} \quad \frac{149}{29} \quad \frac{165}{38} \quad \frac{179}{65}$$

$$\checkmark \quad \frac{106}{62} \quad \frac{105}{51} \quad \frac{103}{42} \quad \frac{92}{20} \quad \frac{80}{10} \quad 76 \quad \frac{79}{9} \quad \frac{82}{13} \quad \frac{86}{18} \quad \frac{93}{21} \quad \frac{101}{26} \quad \frac{151}{32} \quad \frac{160}{37} \quad \frac{180}{62}$$

$$\checkmark \quad \frac{139}{54} \quad \frac{132}{25} \quad \frac{114}{17} \quad \frac{95}{12} \quad \frac{92}{10} \quad 89 \quad \frac{90}{9} \quad \frac{96}{12} \quad \frac{110}{19} \quad \frac{147}{24} \quad \frac{173}{32} \quad \frac{181}{60}$$

$$\checkmark \quad \frac{72}{100} \quad \frac{137}{72}$$

(21.1)

$$\checkmark \quad \frac{0.4}{88} \quad \frac{3.5}{78} \quad \frac{94}{50} \quad \frac{156}{24}$$

(20.3)

$$\checkmark \quad \frac{0.3}{80} \quad \frac{89}{45}$$

(20.1)

Sta	+	Δ	-	Elev
		88838.		
44475				(68.9)
454				(69.6)
T.P	15.56	903.72.	0.22	888.96
44				(67.3)
+39				(68.1)
+50				(68.3)
+75				(68.9)
45				(69.6)
+25				(70.1)
+50				(70.4)
+75				(70.7)
46				(70.9)
T.P	0.19	890.78.	13.73	889.99.
+25				(70.6)

L+

R

R+

✓

$$\frac{138}{50}$$

(19.5)

✓

$$\frac{5.9}{50} \quad \frac{13.9}{34}$$

(18.8)

$$\frac{78}{200} \quad \frac{96}{176} \quad \frac{17.0}{132}$$

(36.4)

✓

$$\frac{5.8}{170} \quad \frac{5.3}{147} \quad \frac{8.6}{120}$$

(35.6)

✓ x

$$\frac{98}{188} \quad \frac{68}{167} \quad \frac{5.1}{147} \quad \frac{6.6}{122}$$

(35.4)

✓ x

$$\frac{77}{170} \quad \frac{37}{140} \quad \frac{36}{120} \quad \frac{94}{76}$$

(34.8)

✓ x

$$\frac{74}{160} \quad \frac{41}{140} \quad \frac{2.5}{120} \quad \frac{1.8}{100} \quad \frac{2.6}{85}$$

(34.1)

✓ +

$$\frac{63}{152} \quad \frac{46}{144} \quad \frac{1.8}{119} \quad \frac{1.4}{101} \quad \frac{0.8}{95} \quad \frac{1.2}{77} \quad \frac{3.7}{52}$$

(33.6)

✓ +

$$\frac{91}{149} \quad \frac{53}{128} \quad \frac{22}{102} \quad \frac{2.8}{78} \quad \frac{5.6}{58} \quad \frac{80}{42}$$

(33.3)

✓ x

$$\frac{11.6}{150} \quad \frac{70}{121} \quad \frac{4.9}{100} \quad \frac{5.5}{83} \quad \frac{9.6}{59} \quad \frac{13.7}{37}$$

(33.0)

✓ x

$$\frac{12.3}{136} \quad \frac{103}{117} \quad \frac{9.6}{98} \quad \frac{11.3}{93} \quad \frac{16.6}{50} \quad \frac{20.0}{34}$$

(32.8)

✓ x

$$\frac{5.0}{100} \quad \frac{5.9}{76} \quad \frac{9.8}{58} \quad \frac{13.7}{28}$$

(19.6)

✓

Sta	+	π	-	Elev
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890.18.

45
46+25

(70.3)

T.P	0.16	875.36.	1498	875.20.
-----	------	---------	------	---------

T.P	6.52	872.48.	940	865.96.
-----	------	---------	-----	---------

48+23		12" X 52' K.T X Drain		66.0.
-------	--	-----------------------	--	-------

+50				65.7
-----	--	--	--	------

T.P	764	873.60.	652	865.96.
-----	-----	---------	-----	---------

49				66.4
----	--	--	--	------

+50				67.2
-----	--	--	--	------

+56				67.2
-----	--	--	--	------

50				68.1
----	--	--	--	------

+50				69.0
-----	--	--	--	------

+68				69.1
-----	--	--	--	------

+85				69.1
-----	--	--	--	------

51				69.1
----	--	--	--	------

+50				68.6
-----	--	--	--	------

Lt

X

Rt

$$\frac{16.4}{75} \quad \frac{16.4}{65} \quad \frac{131}{53} \quad \frac{132}{50}$$

$$(19.9)$$

✓

Inv

Inv

$$\checkmark \quad \frac{126}{63} \quad \frac{133}{33} \quad \frac{109}{28} \quad \frac{91}{17} \quad \frac{73}{13} \quad \frac{69}{10} \quad 65 \quad \frac{65}{8} \quad \frac{66}{11} \quad \frac{102}{17} \quad \frac{130}{19} \quad \frac{136}{28} \quad \frac{149}{72}$$

$$\checkmark \quad \frac{11.3}{60} \quad \frac{11.2}{26} \quad \frac{9.4}{78} \quad \frac{7.4}{14} \quad \frac{71}{6} \quad 68 \quad \frac{6.8}{9} \quad \frac{7.4}{13} \quad \frac{11.2}{18} \quad \frac{136}{31} \quad \frac{15.9}{74}$$

$$\checkmark \quad \frac{12.2}{66} \quad \frac{12.3}{40} \quad \frac{11.2}{20} \quad \frac{8.1}{12} \quad \frac{7.7}{10} \quad 7.2 \quad \frac{7.5}{10} \quad \frac{7.8}{13} \quad \frac{13.1}{23} \quad \frac{14.4}{29} \quad \frac{16.3}{64}$$

$$\checkmark \quad \frac{11.4}{64} \quad \frac{11.5}{46} \quad \frac{10.6}{27} \quad \frac{9.2}{18} \quad \frac{7.1}{13} \quad \frac{6.7}{9} \quad 64 \quad \frac{7.0}{11} \quad \frac{7.5}{15} \quad \frac{8.9}{21} \quad \frac{13.2}{28} \quad \frac{14.4}{35} \quad \frac{16.4}{60}$$

$$\checkmark \quad \frac{8.0}{61} \quad \frac{7.6}{34} \quad \frac{9.6}{29} \quad \frac{9.1}{21} \quad \frac{8.1}{16} \quad \frac{6.9}{14} \quad \frac{6.5}{9} \quad 64 \quad \frac{6.8}{11} \quad \frac{7.3}{15} \quad \frac{8.1}{18} \quad \frac{12.4}{27} \quad \frac{14.4}{37} \quad \frac{16.1}{60}$$

$$\checkmark \quad \frac{7.1}{50} \quad \frac{6.8}{34} \quad \frac{5.6}{27} \quad \frac{5.3}{20} \quad \frac{6.1}{17} \quad \frac{5.8}{15} \quad \frac{5.6}{11} \quad 5.5 \quad \frac{6.0}{11} \quad \frac{6.4}{14} \quad \frac{8.8}{20} \quad \frac{10.2}{26} \quad \frac{13.6}{32} \quad \frac{15.0}{41} \quad \frac{16.1}{65}$$

$$\checkmark \quad \frac{6.3}{55} \quad \frac{7.0}{58} \quad \frac{4.5}{38} \quad \frac{5.2}{31} \quad \frac{5.7}{29} \quad \frac{5.2}{17} \quad \frac{4.6}{11} \quad 46 \quad \frac{5.4}{11} \quad \frac{6.0}{14} \quad \frac{13.1}{29} \quad \frac{14.8}{37} \quad \frac{16.3}{59}$$

$$\checkmark \quad \frac{6.5}{58} \quad \frac{6.1}{42} \quad \frac{5.7}{28} \quad \frac{4.9}{17} \quad \frac{4.6}{12} \quad 45 \quad \frac{5.2}{9} \quad \frac{5.7}{14} \quad \frac{13.1}{28} \quad \frac{14.6}{39} \quad \frac{16.3}{60}$$

$$\checkmark \quad \frac{6.7}{68} \quad \frac{5.9}{60} \quad \frac{0.9}{41} \quad \frac{0.8}{28} \quad \frac{4.6}{23} \quad \frac{5.2}{20} \quad \frac{4.8}{17} \quad \frac{4.6}{12} \quad 45 \quad \frac{5.2}{9} \quad \frac{5.6}{13} \quad \frac{12.9}{27} \quad \frac{14.7}{40} \quad \frac{16.3}{60}$$

$$\checkmark \quad \frac{0.4}{50} \quad \frac{0.5}{41} \quad \frac{5.0}{19} \quad \frac{4.8}{11} \quad 45 \quad \frac{5.3}{10} \quad \frac{5.7}{14} \quad \frac{8.4}{19} \quad \frac{12.0}{27} \quad \frac{13.7}{32} \quad \frac{14.3}{40} \quad \frac{16.1}{60}$$

$$\checkmark \quad \frac{1.1}{50} \quad \frac{1.2}{23} \quad \frac{5.5}{16} \quad \frac{5.2}{10} \quad 5.0 \quad \frac{5.5}{8} \quad \frac{5.9}{12} \quad \frac{8.6}{18} \quad \frac{12.7}{26} \quad \frac{14.4}{39} \quad \frac{15.7}{63}$$

Sta + π - Elev

873.60.

52 67.7.

+50 66.7.

+84 12" x 32' Drain Lt In 66.2.

53 12 x 32' Drain Rt In 66.0.

B.M 5.10 871.74. 7.00 866.60. 866.64

+50 65.4.

54 65.0.

+50 65.5.

55 66.5.

+50 67.4.

+62 67.6.

56 68.3.

+50 69.6.

Lt.

X

Rt

$$\checkmark \quad \frac{21}{50} \quad \frac{21}{48} \quad \frac{25}{20} \quad \frac{58}{14} \quad \frac{58}{10} \quad 5.9 \quad \frac{64}{10} \quad \frac{67}{13} \quad \frac{86}{17} \quad \frac{9.5}{21} \quad \frac{125}{25} \quad \frac{137}{35} \quad \frac{156}{61}$$

$$\checkmark \quad \frac{35}{64} \quad \frac{35}{45} \quad \frac{39}{23} \quad \frac{70}{19} \quad \frac{71}{12} \quad 6.9 \quad \frac{77}{12} \quad \frac{94}{20} \quad \frac{131}{28} \quad \frac{140}{39} \quad \frac{156}{65} \quad \frac{154}{78}$$

$$\checkmark \quad \frac{75}{54} \quad \frac{71}{43} \quad \frac{62}{32} \quad \frac{60}{21} \quad \frac{87}{20} \quad \frac{82.5}{15} \quad \frac{77}{13} \quad 7.4 \quad \frac{8.2}{12} \quad \frac{8.8}{17} \quad \frac{10.3}{22} \quad \frac{126}{27} \quad \frac{137}{37} \quad \frac{147}{51}$$

$$\checkmark \quad \frac{78}{50} \quad \frac{77}{35} \quad \frac{68}{30} \quad \frac{68}{24} \quad \frac{7.5}{20} \quad \frac{77}{12} \quad 7.6 \quad \frac{8.3}{11} \quad \frac{10.7}{16} \quad \frac{106}{24} \quad \frac{122}{27} \quad \frac{137}{38} \quad \frac{149}{54} \quad \frac{156}{74}$$

Top N.W. Cor Conc. Step 20 East Sta. 54

$$\checkmark \quad \frac{6.7}{50} \quad \frac{6.4}{28} \quad \frac{6.3}{17} \quad 6.3 \quad \frac{6.9}{10} \quad \frac{7.6}{13} \quad \frac{9.3}{20} \quad \frac{11.4}{39} \quad \frac{12.4}{55} \quad \frac{13.2}{65}$$

$$\checkmark \quad \frac{5.5}{53} \quad \frac{6.2}{36} \quad \frac{6.5}{10} \quad 6.7 \quad \frac{7.6}{12} \quad \frac{8.9}{17} \quad \frac{10.4}{23} \quad \frac{11.4}{40} \quad \frac{12.3}{48} \quad \frac{13.1}{60}$$

$$\checkmark \quad \frac{6.7}{55} \quad \frac{6.4}{31} \quad \frac{6.4}{11} \quad 6.2 \quad \frac{6.7}{10} \quad \frac{7.7}{16} \quad \frac{10.4}{23} \quad \frac{11.8}{33} \quad \frac{12.0}{44} \quad \frac{13.0}{56}$$

$$\checkmark \quad - \quad \frac{7.6}{50} \quad \frac{6.7}{28} \quad \frac{5.7}{9} \quad \frac{5.4}{8} \quad 5.2 \quad \frac{5.6}{13} \quad \frac{7.5}{17} \quad \frac{10.0}{23} \quad \frac{11.4}{27} \quad \frac{12.0}{32} \quad \frac{12.4}{52}$$

$$\checkmark \quad \frac{7.6}{55} \quad \frac{6.8}{37} \quad \frac{6.1}{27} \quad \frac{4.5}{10} \quad 4.3 \quad \frac{4.5}{11} \quad \frac{11.1}{21} \quad \frac{11.9}{31} \quad \frac{13.1}{50}$$

$$\checkmark \quad \frac{11.3}{53} \quad \frac{12.2}{40} \quad \frac{10.4}{31} \quad \frac{5.5}{24} \quad \frac{4.5}{13} \quad 4.1 \quad \frac{4.3}{11} \quad \frac{10.9}{23} \quad \frac{12.4}{35} \quad \frac{13.2}{50}$$

$$\checkmark \quad \frac{12.5}{50} \quad \frac{12.2}{27} \quad \frac{4.7}{19} \quad \frac{3.7}{13} \quad 3.4 \quad \frac{3.4}{11} \quad \frac{10.4}{23} \quad \frac{12.5}{36} \quad \frac{13.4}{50}$$

$$\checkmark \quad \frac{10.6}{50} \quad \frac{10.4}{37} \quad \frac{9.6}{26} \quad \frac{2.2}{11} \quad 2.1 \quad \frac{2.4}{10} \quad \frac{10.5}{27} \quad \frac{12.5}{37} \quad \frac{13.6}{64}$$

Sta	+	Σ	-	Elev
		871.74		
56+67		O.O Sec End Bridge		70.1.
+67		Under Bridge		58.5.
T.P	5.91	876.20	1.43	870.31 870.29
57+08		under Bridge		58.6.
+08		O.O Sec End Bridge		70.7.
+19				70.3.
+50				70.8.
58				71.3.
+50				71.6.
59				72.3.
+30				73.2.
+50		12" x 32' X Drain Rt In/		73.6.
+43		12" x 32' X Drain Lt In/		73.9.

Lt

✱

Rt

$$\checkmark \begin{array}{cccccccc} 10.4 & 9.5 & 11.4 & 13.2 & 1.5 & 1.6 & & \\ \hline 60 & 47 & 31 & 16 & 16 & 11 & 1.6 & \end{array} \quad \begin{array}{cccccc} 1.9 & 1.7 & 13.2 & 12.5 & 13.6 & \\ \hline 10 & 17 & 17 & 37 & 64 & \end{array}$$

$$\checkmark \begin{array}{cccccc} 10.4 & 9.5 & 11.4 & 13.2 & & \\ \hline 60 & 47 & 31 & 16 & 13.2 & \end{array} \quad \begin{array}{ccc} 13.2 & 12.5 & 13.6 \\ \hline 17 & 37 & 64 \end{array}$$

Top Boat Spk.

$$\checkmark \begin{array}{cccccc} 14.5 & 16.2 & 17.7 & 17.6 & 17.6 & 15.5 & 17.4 & 17.9 \\ \hline 50 & 26 & 17 & 17 & 17 & 18 & 26 & 40 & 50 \end{array}$$

$$\checkmark \begin{array}{cccccccc} 14.5 & 16.2 & 17.7 & 5.4 & 5.4 & 5.7 & & \\ \hline 50 & 26 & 17 & 16 & 14 & 9 & 5.5 & \end{array} \quad \begin{array}{cccccc} 5.7 & 5.8 & 5.6 & 17.6 & 15.5 & 17.4 & 17.9 \\ \hline 9 & 12 & 16 & 18 & 26 & 40 & 50 \end{array}$$

$$\checkmark \begin{array}{cccccc} 14.7 & 13.0 & 6.2 & 5.8 & & \\ \hline 50 & 26 & 13 & 8 & 5.9 & \end{array} \quad \begin{array}{cccccc} 5.7 & 6.1 & 15.5 & 17.6 & 17.9 & 18.8 \\ \hline 8 & 12 & 26 & 40 & 50 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccc} 15.7 & 14.7 & 13.4 & 5.8 & 5.5 & & \\ \hline 55 & 39 & 26 & 13 & 8 & 5.4 & \end{array} \quad \begin{array}{cccccc} 5.6 & 5.7 & 14.9 & 17.2 & 18.2 & \\ \hline 8 & 12 & 26 & 38 & 60 & \end{array}$$

$$\checkmark \begin{array}{cccccc} 15.7 & 14.7 & 13.2 & 5.2 & 5.0 & & \\ \hline 60 & 35 & 27 & 13 & 7 & 4.9 & \end{array} \quad \begin{array}{cccccc} 5.1 & 5.4 & 16.8 & 15.7 & 17.2 & 18.8 \\ \hline 7 & 12 & 26 & 28 & 40 & 64 \end{array}$$

$$\checkmark \begin{array}{cccccc} 14.7 & 14.1 & 13.1 & 5.0 & 4.8 & & \\ \hline 36 & 35 & 27 & 13 & 7 & 4.6 & \end{array} \quad \begin{array}{cccccc} 4.9 & 5.2 & 15.3 & 17.0 & 18.8 & \\ \hline 9 & 12 & 28 & 36 & 64 & \end{array}$$

$$\checkmark \begin{array}{cccccc} 8.5 & 9.6 & 9.7 & 7.9 & 3.8 & 4.0 & & \\ \hline 36 & 45 & 31 & 21 & 12 & 6 & 3.9 & \end{array} \quad \begin{array}{cccccc} 4.2 & 4.4 & 15.3 & 16.5 & 18.9 & \\ \hline 9 & 13 & 32 & 39 & 66 & \end{array}$$

$$\checkmark \begin{array}{cccccc} 1.2 & 1.6 & 2.5 & 3.0 & & \\ \hline 62 & 29 & 17 & 7 & 3.0 & \end{array} \quad \begin{array}{cccccc} 3.3 & 4.1 & 15.7 & 17.0 & 18.8 & \\ \hline 10 & 14 & 40 & 47 & 66 & \end{array}$$

$$\checkmark \begin{array}{cccccc} & & 1.0 & 2.0 & 2.4 & & \\ & & \hline 34 & 16 & 9 & 2.6 & 2.8 & 3.3 & \end{array} \quad \begin{array}{cccccc} & & 5.4 & 15.7 & 17.0 & 18.8 \\ & & \hline 21 & 40 & 47 & 70 \end{array}$$

$$\checkmark \begin{array}{cccccc} & & 2.8 & 3.8 & 2.2 & 2.2 & & \\ & & \hline 17 & 16 & 13 & 10 & 2.3 & 2.6 & 3.1 & \end{array} \quad \begin{array}{cccccc} & & 15.6 & 16.7 & 18.8 & \\ & & \hline 40 & 46 & 66 & \end{array}$$

Sta	+	Σ	-	Elev	
		876.20			
60				74.7	
+50				75.5	
T.P	7.04	882.65	0.59	875.61	
61				76.3	
+50				76.9	
62				77.6	
+50				78.1	
63				78.0	
+50				77.5	
64				76.7	
+50				75.6	
B.M	10.18	882.65	10.18	872.47	872.47
T.P	4.22	879.83	7.04	875.61	
61				(76.3)	
+50				(76.9)	

Lt

R

Rt

$$\checkmark \quad \frac{1.9}{18} \quad \frac{1.7}{13} \quad \frac{1.6}{9} \quad 1.5 \quad \frac{1.8}{10} \quad \frac{2.2}{14} \quad \frac{1.6}{40} \quad \frac{1.7}{47} \quad \frac{1.88}{70}$$

$$\checkmark \quad \frac{0.9}{17} \quad \frac{1.0}{10} \quad 0.7 \quad \frac{1.0}{10} \quad \frac{1.5}{17} \quad \frac{15.7}{40} \quad \frac{16.6}{51} \quad \frac{18.8}{70}$$

$$\checkmark \quad \frac{0.6}{25} \quad \frac{6.0}{18} \quad \frac{6.5}{9} \quad 6.4 \quad \frac{6.8}{10} \quad \frac{7.5}{16}$$

$$\checkmark \quad \frac{1.0}{27} \quad \frac{5.7}{20} \quad \frac{6.0}{11} \quad 5.8 \quad \frac{6.3}{10} \quad \frac{6.7}{15}$$

$$\checkmark \quad \frac{0.3}{27} \quad \frac{3.8}{19} \quad \frac{5.2}{12} \quad 5.1 \quad \frac{5.6}{10} \quad \frac{5.9}{15}$$

$$\checkmark \quad \frac{0.2}{23} \quad \frac{5.4}{16} \quad \frac{4.7}{11} \quad 4.6 \quad \frac{5.2}{11} \quad \frac{5.8}{18}$$

$$\checkmark \quad \frac{1.0}{21} \quad \frac{4.8}{14} \quad \frac{4.8}{11} \quad 4.7 \quad \frac{5.1}{11} \quad \frac{5.5}{20}$$

$$\checkmark \quad \frac{0.5}{21} \quad \frac{5.6}{15} \quad \frac{5.6}{12} \quad 5.2 \quad \frac{5.4}{10} \quad \frac{6.6}{21}$$

$$\checkmark \quad \frac{0.9}{22} \quad \frac{6.1}{16} \quad \frac{6.4}{11} \quad 6.0 \quad \frac{6.3}{9} \quad \frac{6.9}{16}$$

$$\checkmark \quad \frac{3.5}{24} \quad \frac{7.3}{18} \quad \frac{7.4}{12} \quad 7.1 \quad \frac{7.3}{11} \quad \frac{7.8}{14}$$

SpK in 15' Tw Elm 15' Rt Sta 65+48

$$\checkmark \quad \textcircled{3.5} \quad \frac{1.96}{38} \quad \frac{20.0}{50} \quad \frac{21.1}{82}$$

$$\checkmark \quad \textcircled{2.9} \quad \frac{18.6}{36} \quad \frac{20.2}{54} \quad \frac{21.1}{80}$$

Sta + π - Elev

879.83

62

(77.6)

+50

(78.1)

63

(78.0)

+50

(77.5)

64

(76.7)

+50

(75.6)

T.P. 13.54 889.15 4.22

875.61

59+50

(73.6)

+63

(73.9)

T.P. 13.54 902.09 0.60

888.55

60

(74.7)

+50

(75.5)

T.P. 11.15 910.56 2.68

899.41

61

(76.3)

+50

(76.9)

Lt R Rt

$$\checkmark \quad + (8.8) \quad \frac{1.8}{30} \quad \frac{5.6}{41} \quad \frac{6.9}{48} \quad \frac{8.6}{66}$$

$$\checkmark \quad + (8.3) \quad \frac{2.5}{29} \quad \frac{5.2}{38} \quad \frac{6.8}{48} \quad \frac{8.5}{70}$$

$$\checkmark \quad + (8.1) \quad \frac{3.7}{34} \quad \frac{6.6}{45} \quad \frac{8.6}{70}$$

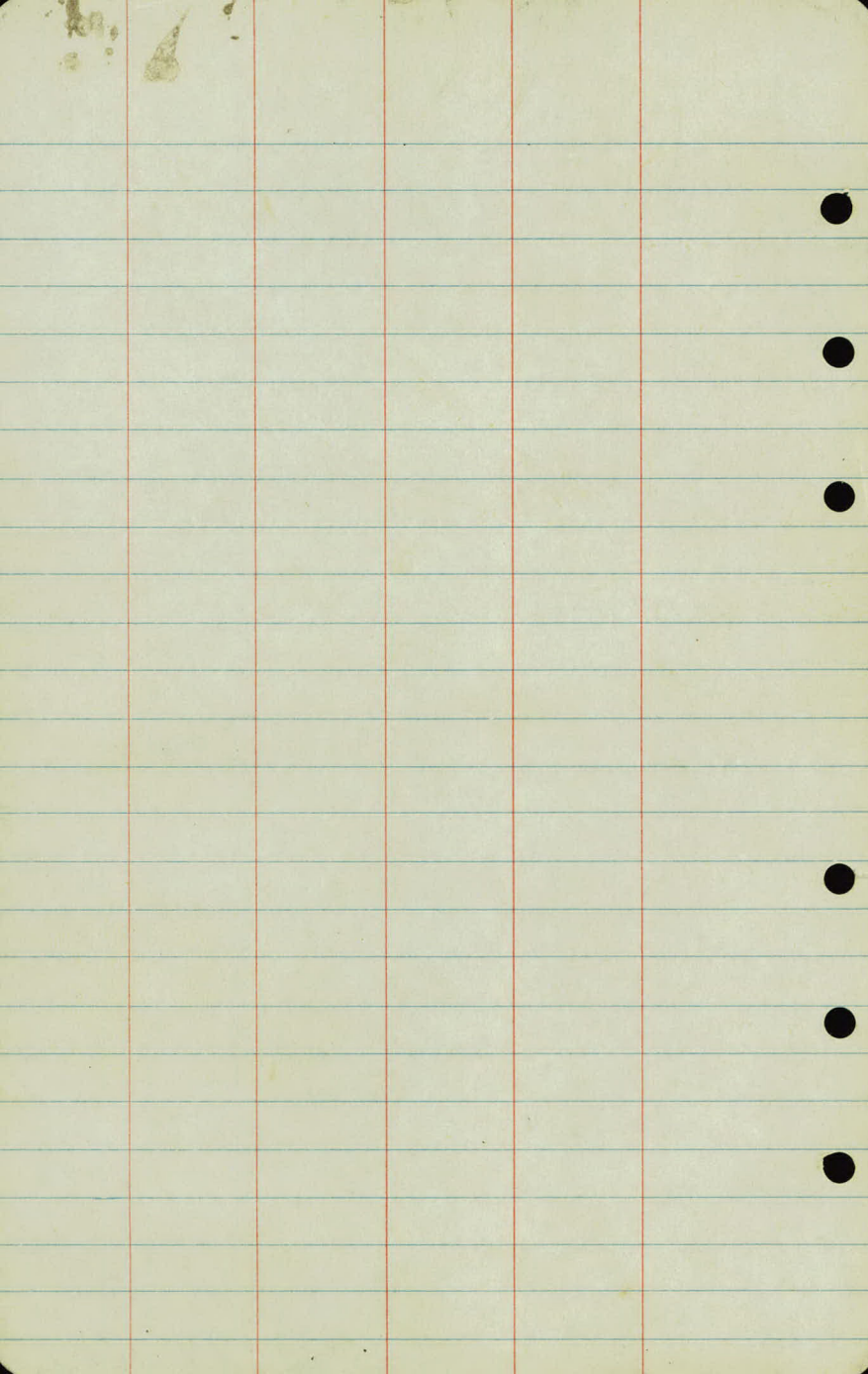
$$\checkmark \quad + (7.7) \quad \frac{3.8}{35} \quad \frac{6.0}{40} \quad \frac{6.8}{52} \quad \frac{8.8}{70}$$

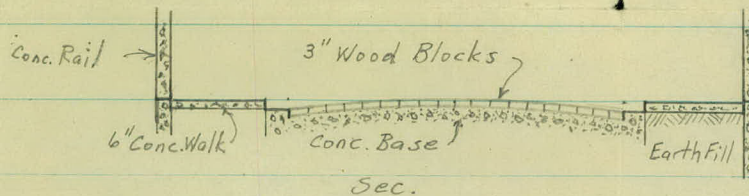
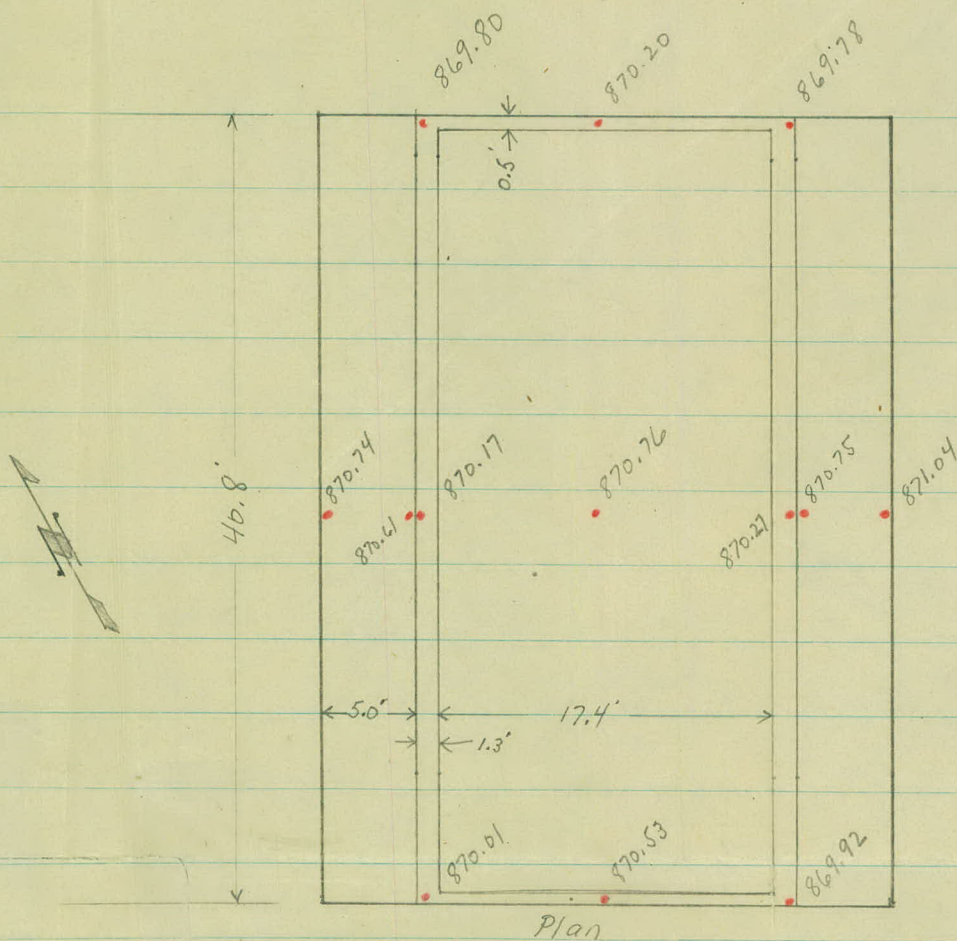
WS 3/30/44

7.20

859.15

SpK in 15" TW Oak AS RT Stg 65 + 68





Elevations On Bridge Between Kohlman's + Gervais Lakes

4-22-44

A. L. B.