

Dr. 16 - Bk. 12

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ COUNTY ROAD "F" _____

From _____ Snelling Ave. To _____ Victoria St. _____

Road Acc't. No. _____ 29 _____

Date Filed _____ 10/26/39 _____

File _____

R. P.
H. W.
A. M.
L. G.
✓39/

Co. Rd "F"

Snelling to Victoria

Alignment

Index.

Alignment - 1 to 4

Topography - 5 to 18

Bench Levels - 19 to 21

Cross sections - 22 to 42.

In to Office 1/31/39

Sta.	Pt.	Lt.	Angle Rt.
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18+99.60 P.I.			0°27'
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Hamline Av.

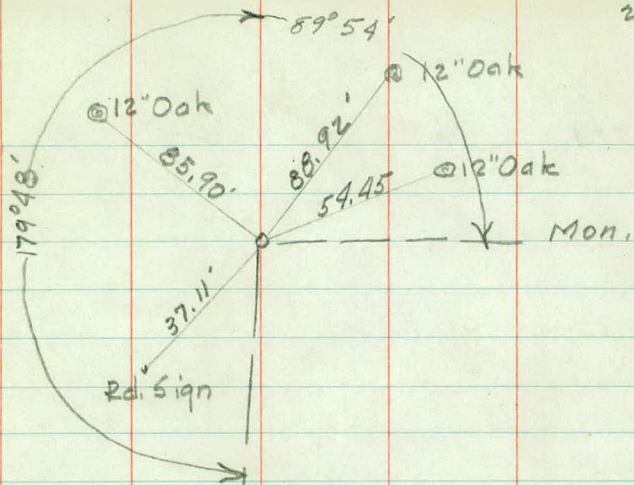
8+30.78 P.O.T.

0+72.3 P.O.T. Co. Rd F = 0+00 P.C. Snelling

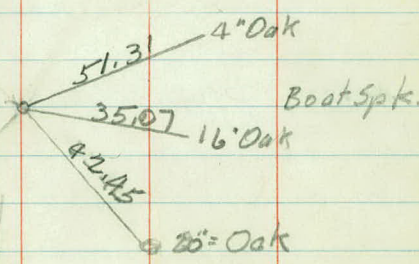
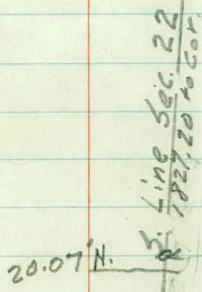
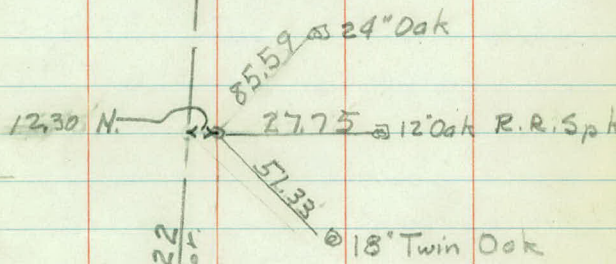
0+41.63 P.I. Snelling 412.

49
179

54 Sec. 22



N



Sta.	Pt.	Lt.	Angle	Rt.
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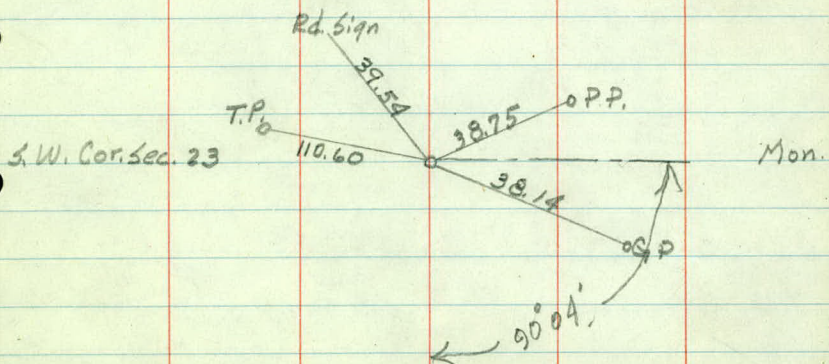
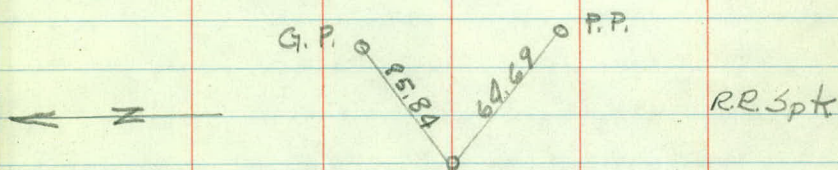
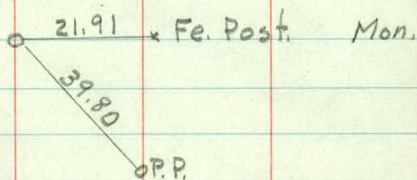
71+69.10	P.O.T.			
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65+00	P.O.T.			
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45+32.65	P.O.T.			
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Lexington Av.

54 Sec. 23

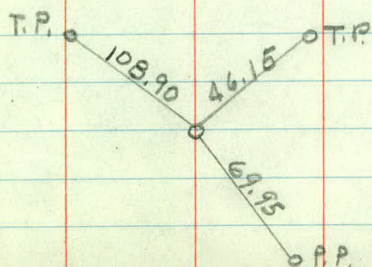
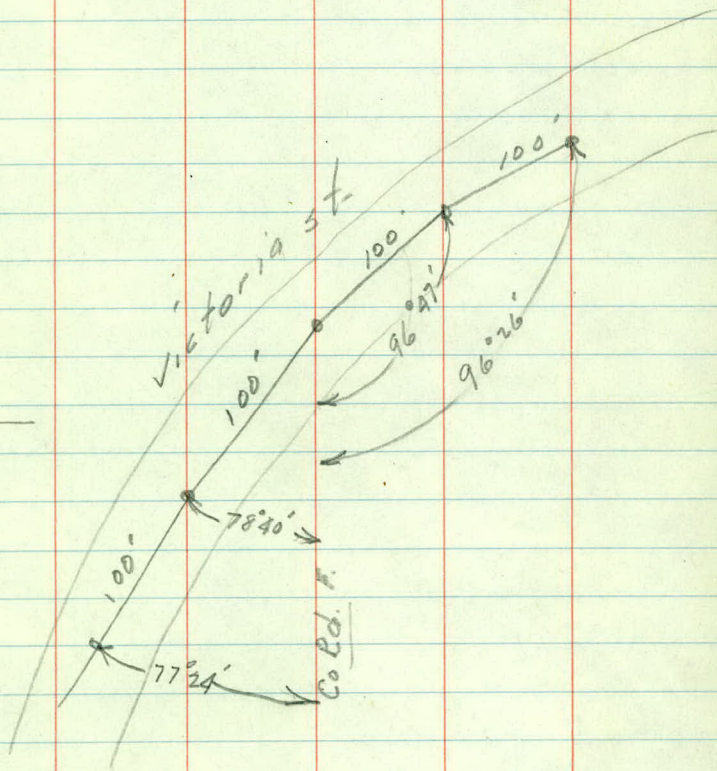


Stg.	Pt.	Lt.	Angle.	Rt.
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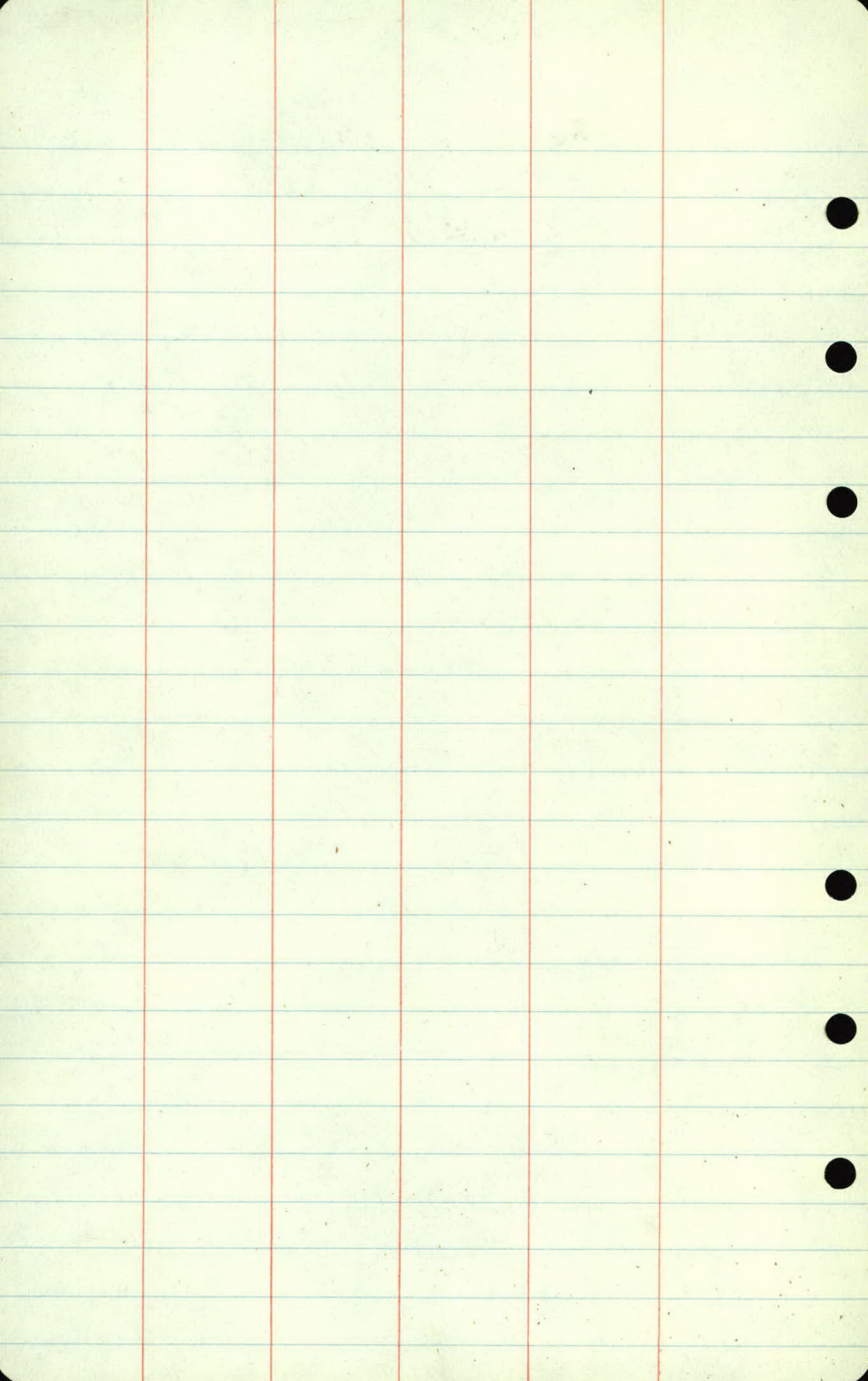
84+95 P.O.T.

Victoria St.

← N →



R.R. Spk.



Topography

Co. Rd "F"

Snelling to Snail Lake Blvd.

9' 13'

5 9' 13'

4 10' 3'

3 11' 13'

2 9' 13'

1 8' 15'

+72.3 6' 16'

* +80 * Fe. Cor. 34'

Fe 27'

+42-4 Willows 26'

Fe 26'

Fe 25'

Fe 26'

+65 Field Ent.

Fe 31'

Fe 31'

Uncultivated

Cultivated

Shedding

12' - 10'

12

13 - 10'

11

14' - 9'

27'

+30 10" x 50' Vit X Drain

23''

10

11' 10'

9

12' 11'

8

12' 11'

7

10' 12'

6

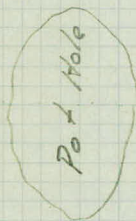
9' 13'

Fe. 30' 7

Uncult.

Fe. 29'

Fe. 27'



2' Ditch

+58 Rgc tie Ditch

+00 Rgc tie Ditch.

Fe. 25'

3' Ditch

Fe. 35'

Cultivated

Wooded - Oaks

Fe. 27

+30 ΔFe. 27'

Fe. 29'

+48-15" Oak 20'

+16-8" Oak 23'
+00-8" Maple 24'

11' - 9'

19

18

11' 13'

17

11' 11'

16

11' 10'

15

13' 10'

14

13' 10'

13

12' - 10'

+55 End Rad-13'

+16 End Rad-46'

Blk top

Hamline Ave.

Note:
No. Radius

+84 12" Oak-28'

+45 12" Oak-29'

+34 8" Oak-29'

+33 End Rad-12'

+16 End Rad-30'

+78 End Rad. 33'

+64 End Fe. 31'

+52 Begin Rad. 15'

+03 36" Oak-24'
Fe. 29'

+86 30" Oak-28'

+68 20" Oak-27'

+32 26" Oak-26'

Fe. 27'

+81 24" Oak-26'

+61 24" Oak-27'

+53 Fe. Cor. 28'

+43 24" Oak-26'

+22 End trees 26'

+11 Ent. 25'

Fe. 26'

Fe. 30'

+81 Begin Row
Trees-30'

Fe. 30'

Cult.

Gravel

Cult.

Uncult.

Uncult.

18' - 3'

26

16' - 4'

25

15' - 5'

24

15' - 6'

23

14' - 7'

22

14' - 8'

21

10' - 10'

20

11' 9'

Scattered
Oaks

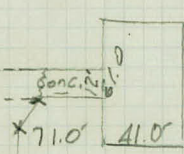
Scattered
Oaks

+79 36" Cot. 6'
+57 30" Cot 34'
+35 40" Cot 35'

+62 20" Elm 34'

+65 24" Oak 48'
+62 24" Oak 22'
+52 End Trees

+46 Ent.



+80 Ent.
+71 End Fe 3
+59 Din Fe 23
+50 Cor. Barn

Scattered Fe 2/
Oaks

+44 Fe. Cor. 20'

+96 24" Bp. 30'
12" Oak 37'

+17 Twin 24" O. 29'

4rd 18

33

5 16

32

6 14

31

10 14

30

23.0'

¹⁰
+94-⁹12'x40'cm

17.0'

29

13 6

+12 Ent

28

17 6

27

18 3

+52 Ent

Scattered
Oaks
& Brush

+68 24" Oak 28"

+34 Ent,
+16 15" Oak - 34
+65 15" Oak - 35

+81-20" Oak - 37

+06-15" Oak - 33
+92 24" Oak 37

+03 Ent
+80 Rge Tie Ent.
Hump

+22 H.P. 38
+23 H.P. 33
Rge Tie Ent +25
+12 P.P. - 26
Ditch 29"

Scattered Oaks

3' Ditch

+21 Δ Ditch - 35

+43 24" Willow 27
+21-24" Willow 33

3^{Kd} 17

11'

+41 $\pm$ 12" O. 17 x 36'

25'

40

0 18'

39

1-22'

38

2-22

37

2-23

36

2-25

35

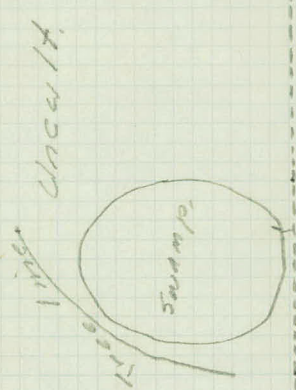
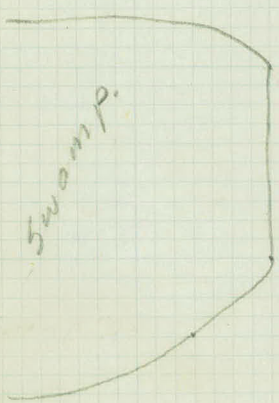
2-22

34

4 18

Scattered Oaks
& Brush

+08 Twin Pop 30'



Scattered
Oaks
&
Brush



①

②

Cult.

2' Ditch

+67 2' Ditch 35'
+54 Rg. Tie Ditch

+53 12' Oak - 33'

10Rd 12

47

9 14

46

11 10

22 +53 - 15" x 42' CM

20

45

44

9 12

43

8 12

42

3 17

41

3 17

+37 - 46" Trees - 32'

+24 P.P. 28
+05 18" Cor. 24
Fe 26

Pasture

+46 Beg. Rad 24'

Lexington Av.

+60 P.P. 27
+58 Fe Cor. 25
+46 Beg. Rad. 30'

+15 End. Rad 42'

+15 End. Rad. 41'
+06 C.P. - 27'

+90 Beg. Rad 12'

+85 Beg. Rad. 15'

Hole

+30 Rgs + 12 Ent
+13 Ent. 25
+17 - 12 Oaks 26' - 33'
+07 10" vit. 42'
+00 32'

Tree line

Cult

10 7

54

10 11

53

9 12

52

8 12

51

9 12

50

8 14

49

24

103-12" x 118" vit
8 12

94

48

10 12

+91 P.P. 28'

Fe. 29

+25 PP 28'

Posture

+48 Fe Cor. 28

Fe 30'

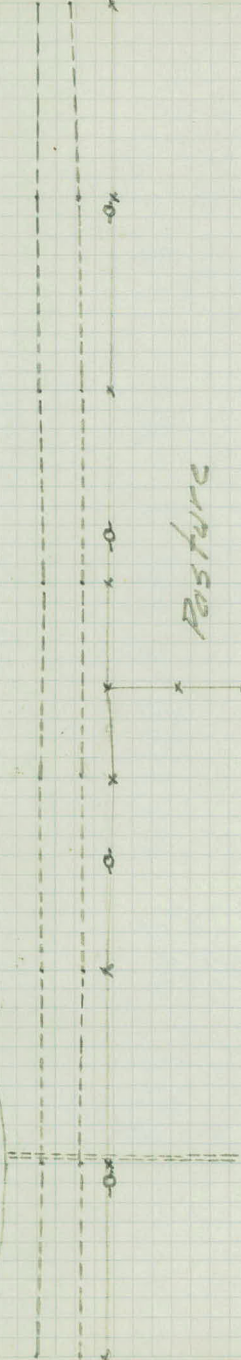
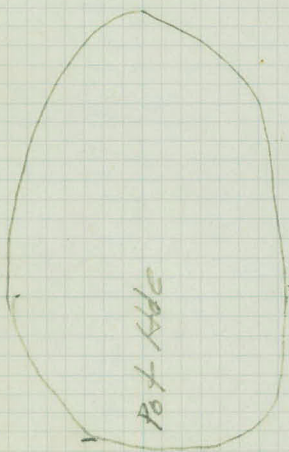
+157 P.P. 27

+90 FS 27
PP 28

Cal 1st

Cal 1st

Posture



10 9

61

10 10

60

23'

10 10

+86 12" x 46' Vif

23'

59

10 10

58

10 10

57

10 10

25'

+30 18" x 48' C.M

23'

56

10 10

55

10 7

6/17

+60 P.P. 29'

+97 Twin Willow 21'

+90 Brush

+89 P.P. Fe. C29'

6/17

+25 P.P. 29'

Fe 29'

Posture

2' Ditch

+20 Rge tie Ditch

A in Ditch 40'

+59 P.P. 28'

10 9

68 32

+03-15² 9 62 G.M.

30'

67

10 8

66

10 7

65

12 9

64

11 8

63

10 8

62

10 9

Uncult.

+53 P.P. 29.

Pot Hole.

+106 P.P. 29.
Fe 29.

+58 ΔFe 18.

+25 Fe Cor 17.
+15 Rge. Tie Drive
+100 Fe. 41.

+90 Ent.

+60 P.P. 29.

+93 P.P. 30.

+26 P.P. & Fe.C. 29.

Uncult.

+81 G.P. 27.

Cult.

Yard

9 10

75

10 10

21

131 - 18" x 42" CM

21

74

9 8

73

9 8

72

10 7

71

11 8

70

11 7

69

10 9

C4/H.

+170 P.P. 28'

φ

+28 P.P. 29'

φ

+84 P.P. 29'

φ

C4/H.

uncult.

+41 P.P. 29'

φ

+98 P.P. 28'

φ

x

x

x

+15 Fe. Cor. 29'

x

9 11

82

9 11

81

9 10

80

9 9

79

8 10

78

9 10

77

9 9

19°

+31-15°34'CM

15°

76

9 10

+86 PP 28.

φ

+43 PP 28.

φ

Hay Field

+00 PP 28.

φ

21/12

20 PP 28

+58 PP 28.

φ

21/12

+14 P.P. 29.

φ

+

85

84

8 11

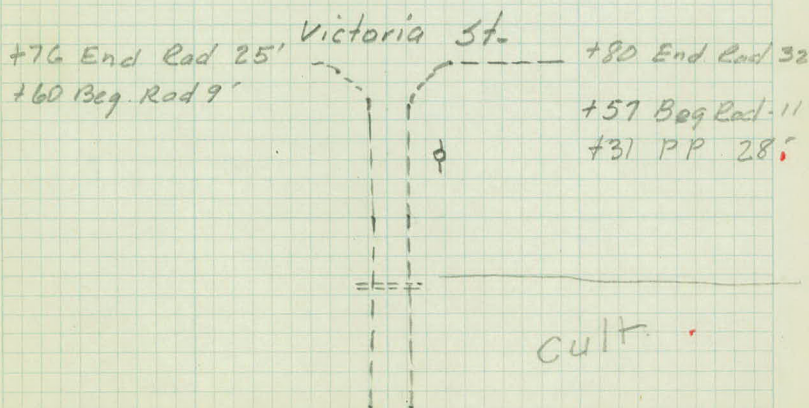
15"

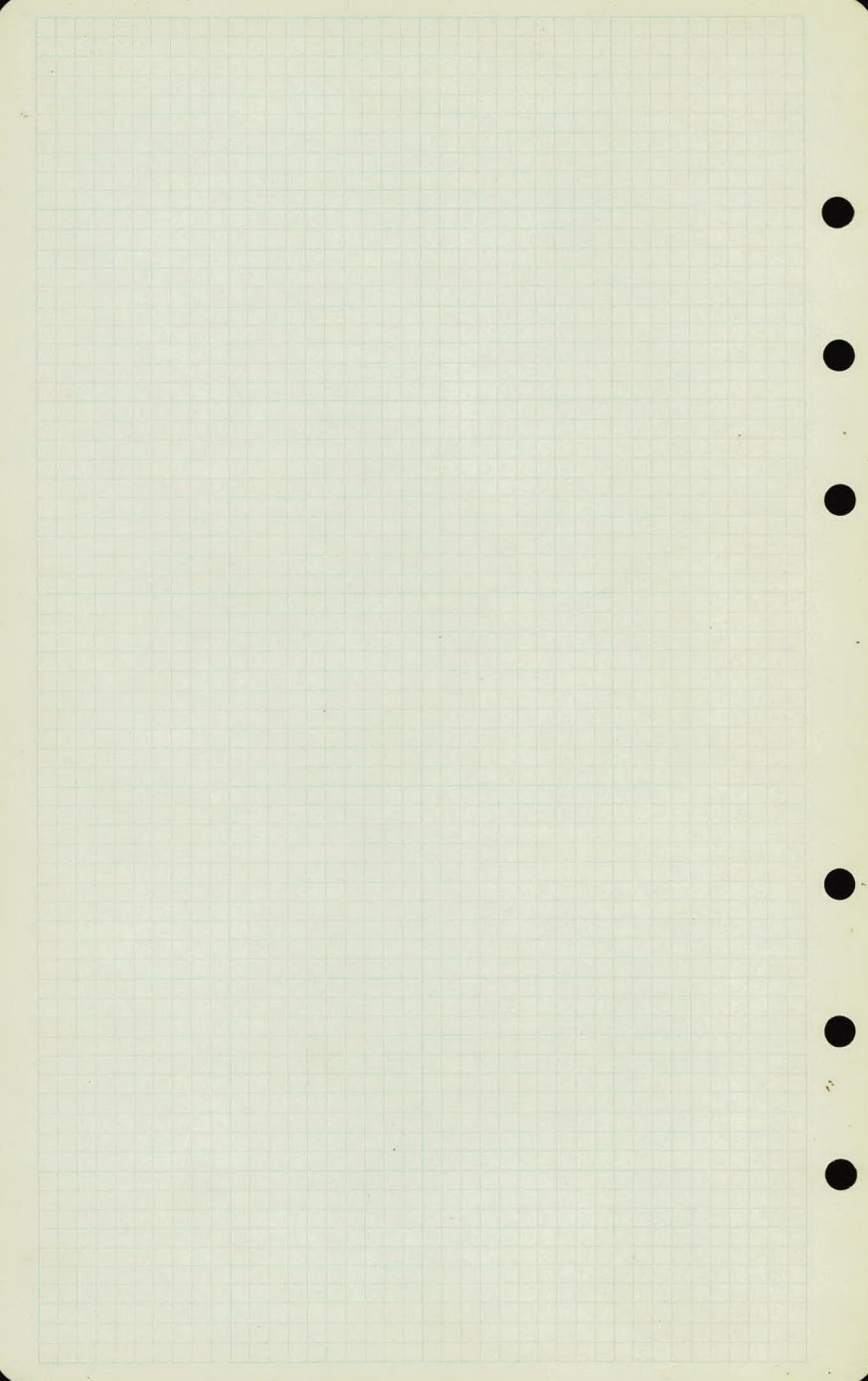
164-12"x34' C.M.

19"

83

9 11





Bench Levels

Co. Rd. "F"

Pt.	+	π	-	Elev.
	6.51	987.43.		980.92
T.P.	2.86	989.53.	0.76	986.67.
B.M.			6.47	983.06.
T.P.	0.93	976.44.	13.52	976.01.
T.P.	0.61	963.34.	13.71	962.73.
T.P.	0.25	956.75.	6.84	956.50.
B.M.			3.03	953.72.
T.P.	0.58	944.39.	12.94	943.81.
T.P.	0.41	932.47.	12.33	932.06.
T.P.	0.89	923.71.	9.65	922.82.
B.M.			4.18	919.53.
B.M.	8.12	991.18.		983.06. ✓
T.P.	0.85	981.64.	10.39	980.79.
T.P.	1.58	969.95.	13.27	968.37.
B.M.			4.13	965.82.
T.P.	8.16	973.15.	4.96	964.99.
T.P.	0.92	964.75.	9.32	963.83.
B.M.			0.53	964.22.
T.P.	8.04	964.65.	8.14	956.61.
T.P.	8.51	970.76.	2.40	962.25.
B.M.			5.46	965.30. ✓
B.M.			6.76	964.00. 963.74
T.P.	10.55	979.08.	2.23	968.53.
T.P.	1.72	977.63.	3.17	975.91.
B.M.			8.72	968.91.

Spike in 30" Oak 120' Rt. 57+59+90 (Hamline Av.)

Top. Mon. at Hamline and Co. Rd. 'F'

Spike in 12" Oak 35' Rt. 7+55

Spike in 24" Oak 25' Rt. 0-60

Top. Mon. at Hamline

Spike in 30" Oak 35' Rt. 30+90

Spike in 30" Oak 100' Rt. 37+30

Top. Mon. Lexington and Co. Rd. 'F'

Spike in P.P. S.E. Cor. Lex. and 'F'

(See Levi Notes)

Spike in P.P. 28' Rt. 57+25

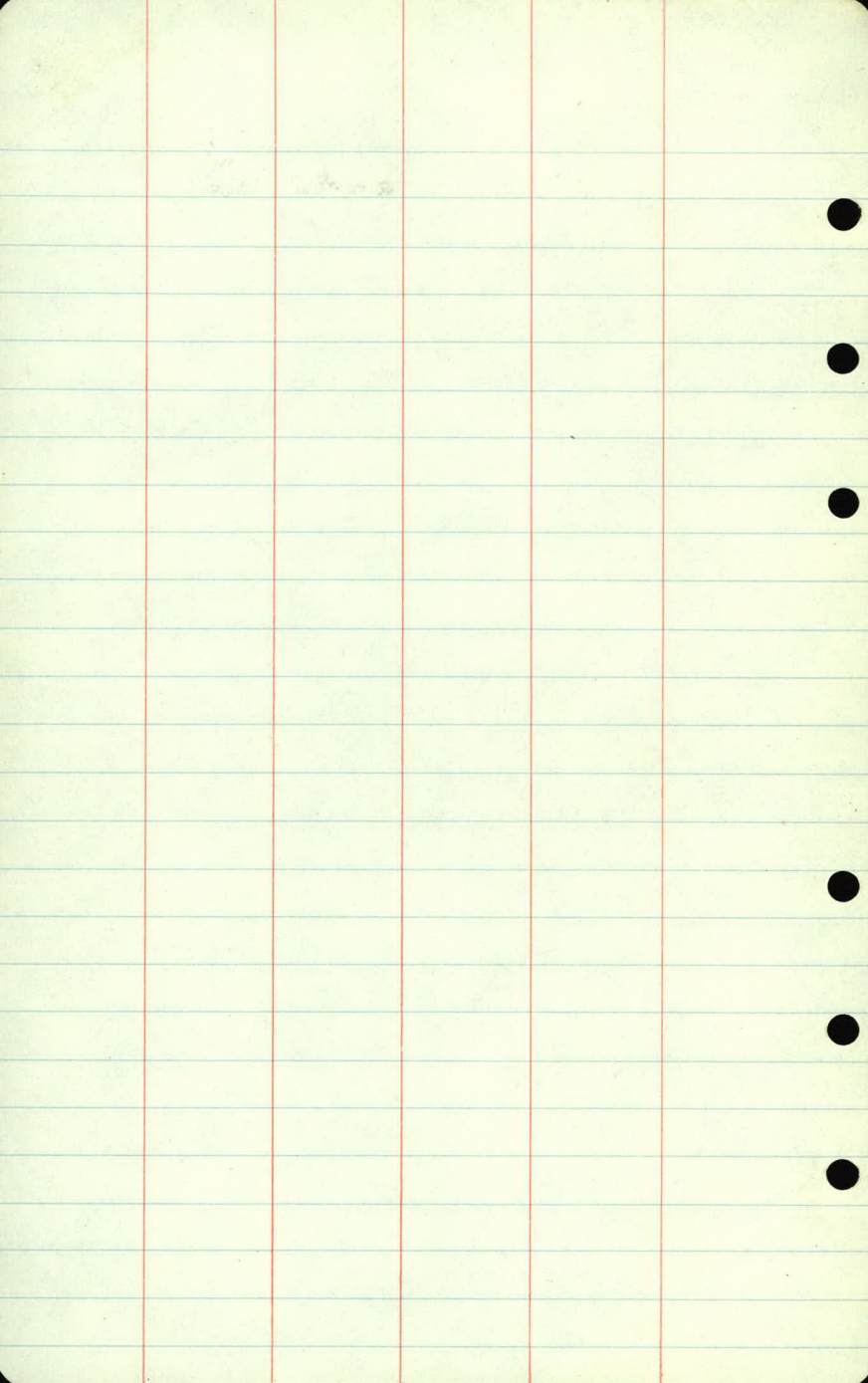
Pt.	+	Σ	-	Elev.
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977.63

T.P.	9.32	982.86	4.09	973.54
T.P.	10.84	993.38	0.32	982.54
T.P.	0.24	986.34	7.28	986.10
B.M.	0.73	984.57	2.50	983.84
T.P.	7.22	980.94	10.85	973.72
T.P.	6.44	986.01	1.37	979.57
B.M.			5.06	980.95

Top Mon. Sta. 71+69.10

Top Spike Sta. 84+95



Cross sections

Co. Rd. "F."

Sta.	+	π	-	Elev.
B.M.	8.57	928.10		919.53
0+72.3			9.1	19.0

1			7.5	20.6
+35			5.8	22.3

2			2.2	25.9
T.P.	11.88	939.46	0.52	927.58
+50			11.1	28.4

3			8.5	31.0
+35			6.6	32.9

4			3.2	31.3	36.3
T.P.	13.52	949.65	3.33	936.13	
+19			12.3	37.4	

+66			9.9	39.8	
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5			2.3	41.4	
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+60			5.5	40.2	44.2
T.P.	13.70	958.79	4.56	945.09	

Spike in 24" Oak - 28' Rt. Sta. 0-60

1.0	+0.5	1.2	2.4	2.8	2.4	2.5	9.0	9.3	9.7	0.3	1.7
100	75	50	29	18	11	9	9.1	10	16	19	30
											50

4.6	3.3	2.7	2.7	7.9	8.3	7.5	7.6	8.0	8.9	4.0	5.4
100	75	50	24	17	9		8	18	20	25	50

5.8	4.2	3.0	6.4	6.2	5.8	5.8	6.3	7.0	4.0	4.5	5.7
75	50	21	15	9		8	14	17	22	34	50

1.5	1.1	13.0	13.5	3.1	2.4	2.4	3.3	11.0	0.3	0.7
100	85	50	23	14	6	9	17	33	34	50

7.8	5.4	3.7	4.9	9.4	11.7	11.7	12.4	7.3	8.0
100	75	50	26	20	16	11	18	24	50

9.0	5.2	2.7	0.6	6.5	9.0	9.0	9.3	2.5	3.8
100	75	50	26	17	14	85	11	20	50

6.6	4.1	0.8	7.1	7.0	13.5	10.5
75	50	24	15	16	24	50

3.8	3.3	1.9	3.7	3.6	0.5	0.0
50	31	19	12	16	21	50

12.9	12.8	11.9	12.9	12.7	13.6	12.1	11.5	11.6
50	24	19	13	12.3	13	17	20	33
								50

0.4	3.0	7.7	9.5	9.2	10.4	16.6	11.5	11.1	12.9	13.5
100	75	50	31	18	14	13	21	34	42	50

13.0	+0.9	1.8	4.8	6.6	9.1	9.4	9.1	9.3	12.9	30
100	75	50	35	17	12	83	16	24	36	50

+6.8	+6.0	+4.0	0.5	4.8	6.2	6.5	6.6	9.1
100	75	50	22	14	14	23	41	50

Sta.	+	Σ	-	Elev.	
		958.79			
5+85			13.5	453.	
6			12.8	420.	
+50			10.2	486.	
7			7.7	511.	
+58			5.0	538.	
B.M.	12.62	966.34	570	953.69	953.72
8			11.4	549.	
+71			9.8	565.	
T.P.	13.25	969.88	9.71	956.63.	
9			13.0	569.	
+50			12.7	572.	
T.P.	6.00	963.44	12.44	957.44.	
10			6.0	574.	
+30		10"x50' Vit Drain			
+50			5.8	576.	
11			5.4	580.	

$\frac{+0.5}{100}$ $\frac{0.6}{75}$ $\frac{2.9}{50}$ $\frac{9.1}{23}$ $\frac{13.6}{15}$ $\frac{13.6}{10}$ 13.5 $\frac{13.9}{12}$ $\frac{16.7}{20}$ $\frac{18.7}{31}$ $\frac{20.2}{50}$

$\frac{0.1}{100}$ $\frac{1.5}{75}$ $\frac{4.2}{50}$ $\frac{6.6}{29}$ $\frac{8.9}{20}$ $\frac{12.1}{15}$ $\frac{13.1}{9}$ 12.8 $\frac{13.4}{14}$ $\frac{16.5}{22}$ $\frac{18.2}{31}$ $\frac{19.7}{50}$

$\frac{+2.5}{100}$ $\frac{+1.8}{75}$ $\frac{2.5}{50}$ $\frac{5.3}{37}$ $\frac{6.5}{25}$ $\frac{9.3}{20}$ $\frac{10.0}{14}$ $\frac{10.7}{10}$ 10.2 $\frac{10.7}{13}$ $\frac{13.4}{21}$ $\frac{14.6}{30}$ $\frac{16.2}{50}$

$\frac{+8.0}{100}$ $\frac{+9.7}{75}$ $\frac{0.0}{50}$ $\frac{1.2}{40}$ $\frac{3.6}{22}$ $\frac{5.2}{17}$ $\frac{7.3}{16}$ $\frac{8.0}{10}$ 7.7 $\frac{8.6}{14}$ $\frac{10.8}{21}$ $\frac{11.8}{29}$ $\frac{13.9}{50}$

$\frac{+11.0}{100}$ $\frac{+9.5}{77}$ $\frac{+8.0}{67}$ $\frac{+5.5}{36}$ $\frac{+4.0}{27}$ $\frac{4.8}{16}$ $\frac{5.5}{12}$ 5.0 $\frac{5.7}{11}$ $\frac{6.6}{15}$ $\frac{2.9}{20}$ $\frac{6.8}{38}$

Spike in 12' Oak 35' Rt. 5' to 7' + 55.

$\frac{+3.3}{100}$ $\frac{+2.5}{75}$ $\frac{+0.6}{50}$ $\frac{0.7}{33}$ $\frac{7.4}{24}$ $\frac{10.5}{19}$ $\frac{11.7}{13}$ 11.4 $\frac{12.0}{11}$ $\frac{12.6}{17}$ $\frac{8.1}{23}$ $\frac{8.1}{27}$ $\frac{10.2}{50}$

+2.5

5

$\frac{+6.8}{100}$ $\frac{+6.5}{77}$ $\frac{+2.5}{50}$ $\frac{+3.1}{36}$ $\frac{10.2}{16}$ $\frac{9.8}{5}$ 9.8 $\frac{10.7}{12}$ $\frac{11.0}{17}$ $\frac{5.1}{26}$ $\frac{7.7}{40}$ $\frac{9.7}{50}$

$\frac{+4.5}{100}$ $\frac{+1.8}{75}$ $\frac{2.9}{50}$ $\frac{3.3}{35}$ $\frac{13.1}{20}$ $\frac{14.0}{16}$ 13.0 $\frac{13.6}{11}$ $\frac{14.4}{17}$ $\frac{9.7}{24}$ $\frac{11.7}{50}$

$\frac{1.8}{100}$ $\frac{5.9}{75}$ $\frac{7.4}{50}$ $\frac{6.5}{29}$ $\frac{12.6}{21}$ $\frac{13.5}{15}$ $\frac{13.0}{12}$ 12.7 $\frac{13.2}{10}$ $\frac{13.6}{15}$ $\frac{9.9}{20}$ $\frac{11.1}{31}$ $\frac{14.0}{50}$

$\frac{4.7}{100}$ $\frac{4.8}{75}$ $\frac{5.0}{50}$ $\frac{4.8}{20}$ $\frac{6.8}{17}$ $\frac{6.3}{11}$ 6.0 $\frac{6.4}{9}$ $\frac{7.5}{16}$ $\frac{9.3}{18}$ $\frac{10.0}{37}$ $\frac{13.2}{50}$

$\frac{13.4}{27}$ 50.0

$\frac{12.6}{23}$ 50.8

$\frac{9.2}{50}$ $\frac{8.6}{33}$ $\frac{8.1}{20}$ $\frac{6.3}{13}$ 5.4 $\frac{6.4}{11}$ $\frac{10.1}{18}$ $\frac{10.8}{21}$ $\frac{8.5}{24}$ $\frac{7.7}{50}$

$\frac{9.3}{50}$ $\frac{9.3}{26}$ $\frac{6.5}{18}$ 5.4 $\frac{6.2}{11}$ $\frac{9.3}{17}$ $\frac{7.5}{20}$ $\frac{6.9}{23}$ $\frac{6.0}{36}$ $\frac{6.0}{50}$

Sta	+	π	-	Elev.
		963.44		
11+50			5.0	58.4
12			4.9	58.5
+50			4.0	59.4
13			3.2	60.2
+50			2.1	61.3
T.P.	12.01	973.43.	2.02	961.42.
14			10.8	62.6
+60			8.6	64.8
15			7.0	66.4
+50			4.8	68.6
+86			3.0	70.4
16			2.4	71.0
T.P.	12.52	985.33.	0.62	972.81.

$$\begin{array}{r} 4.4 \\ 50 \end{array} \quad \begin{array}{r} 9.3 \\ 25 \end{array} \quad \begin{array}{r} 8.7 \\ 22 \end{array} \quad \begin{array}{r} 5.7 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 5.0 \end{array} \quad \begin{array}{r} 5.7 \\ 12 \end{array} \quad \begin{array}{r} 8.3 \\ 19 \end{array} \quad \begin{array}{r} 6.9 \\ 26 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 8.5 \\ 50 \end{array} \quad \begin{array}{r} 8.7 \\ 26 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 4.9 \\ 4.9 \end{array} \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad \begin{array}{r} 8.4 \\ 19 \end{array} \quad \begin{array}{r} 8.7 \\ 26 \end{array} \quad \begin{array}{r} 8.5 \\ 50 \end{array}$$

$$\begin{array}{r} 7.3 \\ 50 \end{array} \quad \begin{array}{r} 7.4 \\ 24 \end{array} \quad \begin{array}{r} 4.4 \\ 13 \end{array} \quad \begin{array}{r} 4.0 \\ 4.0 \end{array} \quad \begin{array}{r} 4.8 \\ 12 \end{array} \quad \begin{array}{r} 9.0 \\ 20 \end{array} \quad \begin{array}{r} 9.1 \\ 30 \end{array} \quad \begin{array}{r} 9.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.5 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 23 \end{array} \quad \begin{array}{r} 3.6 \\ 14 \end{array} \quad \begin{array}{r} 3.2 \\ 3.2 \end{array} \quad \begin{array}{r} 3.9 \\ 11 \end{array} \quad \begin{array}{r} 7.5 \\ 16 \end{array} \quad \begin{array}{r} 8.6 \\ 23 \end{array} \quad \begin{array}{r} 8.8 \\ 30 \end{array} \quad \begin{array}{r} 8.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array} \quad \begin{array}{r} 4.0 \\ 24 \end{array} \quad \begin{array}{r} 3.7 \\ 19 \end{array} \quad \begin{array}{r} 2.4 \\ 13 \end{array} \quad \begin{array}{r} 2.1 \\ 2.1 \end{array} \quad \begin{array}{r} 2.9 \\ 11 \end{array} \quad \begin{array}{r} 6.4 \\ 19 \end{array} \quad \begin{array}{r} 6.8 \\ 25 \end{array} \quad \begin{array}{r} 6.6 \\ 31 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array}$$

$$\begin{array}{r} 12.1 \\ 50 \end{array} \quad \begin{array}{r} 13.1 \\ 24 \end{array} \quad \begin{array}{r} 12.7 \\ 17 \end{array} \quad \begin{array}{r} 11.2 \\ 13 \end{array} \quad \begin{array}{r} 10.8 \\ 10.8 \end{array} \quad \begin{array}{r} 11.4 \\ 11 \end{array} \quad \begin{array}{r} 13.6 \\ 15 \end{array} \quad \begin{array}{r} 14.0 \\ 20 \end{array} \quad \begin{array}{r} 11.7 \\ 26 \end{array} \quad \begin{array}{r} 10.0 \\ 50 \end{array}$$

$$\begin{array}{r} 9.2 \\ 50 \end{array} \quad \begin{array}{r} 9.9 \\ 35 \end{array} \quad \begin{array}{r} 9.9 \\ 22 \end{array} \quad \begin{array}{r} 9.8 \\ 16 \end{array} \quad \begin{array}{r} 9.3 \\ 15 \end{array} \quad \begin{array}{r} 8.6 \\ 8.6 \end{array} \quad \begin{array}{r} 9.3 \\ 9 \end{array} \quad \begin{array}{r} 9.7 \\ 13 \end{array} \quad \begin{array}{r} 7.9 \\ 17 \end{array} \quad \begin{array}{r} 5.3 \\ 22 \end{array} \quad \begin{array}{r} 2.4 \\ 50 \end{array}$$

$$\begin{array}{r} 7.9 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 20 \end{array} \quad \begin{array}{r} 7.7 \\ 14 \end{array} \quad \begin{array}{r} 7.0 \\ 7.0 \end{array} \quad \begin{array}{r} 7.4 \\ 9 \end{array} \quad \begin{array}{r} 8.2 \\ 13 \end{array} \quad \begin{array}{r} 7.0 \\ 18 \end{array} \quad \begin{array}{r} 6.5 \\ 21 \end{array} \quad \begin{array}{r} 6.1 \\ 26 \end{array} \quad \begin{array}{r} 5.3 \\ 39 \end{array} \quad \begin{array}{r} 4.7 \\ 50 \end{array}$$

$$\begin{array}{r} 5.6 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 25 \end{array} \quad \begin{array}{r} 5.3 \\ 17 \end{array} \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad \begin{array}{r} 4.8 \\ 4.8 \end{array} \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 6.1 \\ 13 \end{array} \quad \begin{array}{r} 6.0 \\ 16 \end{array} \quad \begin{array}{r} 4.7 \\ 20 \end{array} \quad \begin{array}{r} 4.5 \\ 27 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 2.8 \\ 50 \end{array} \quad \begin{array}{r} 3.8 \\ 36 \end{array} \quad \begin{array}{r} 3.7 \\ 16 \end{array} \quad \begin{array}{r} 4.2 \\ 15 \end{array} \quad \begin{array}{r} 3.7 \\ 14 \end{array} \quad \begin{array}{r} 3.0 \\ 3.0 \end{array} \quad \begin{array}{r} 4.0 \\ 15 \end{array} \quad \begin{array}{r} 2.6 \\ 18 \end{array} \quad \begin{array}{r} 1.2 \\ 20 \end{array} \quad \begin{array}{r} 0.6 \\ 24 \end{array} \quad \begin{array}{r} 0.2 \\ 50 \end{array}$$

$$\begin{array}{r} 1.5 \\ 50 \end{array} \quad \begin{array}{r} 3.1 \\ 24 \end{array} \quad \begin{array}{r} 2.8 \\ 14 \end{array} \quad \begin{array}{r} 2.4 \\ 2.4 \end{array} \quad \begin{array}{r} 3.1 \\ 13 \end{array} \quad \begin{array}{r} 2.7 \\ 17 \end{array} \quad \begin{array}{r} 1.0 \\ 20 \end{array} \quad \begin{array}{r} 10.3 \\ 50 \end{array}$$

Sta.	+	$\overline{\Delta}$	-	Elev.
		985.33		
16+50			12.4	72.9
17.			11.0	74.3
+50			9.1	76.2
18			7.0	78.3
+50			4.5	80.8
+70			3.3	82.0
+80			2.6	82.7
+86			2.2	83.1
+99			1.8	83.5
B.M.			2.27	83.06
				983.06

$$\begin{array}{r} 10.1 \\ 50 \end{array} \quad \begin{array}{r} 11.7 \\ 33 \end{array} \quad \begin{array}{r} 12.3 \\ 18 \end{array} \quad \begin{array}{r} 12.8 \\ 12 \end{array} \quad 12.4 \quad \begin{array}{r} 13.0 \\ 12 \end{array} \quad \begin{array}{r} 13.8 \\ 18 \end{array} \quad \begin{array}{r} 14.9 \\ 23 \end{array} \quad \begin{array}{r} 13.4 \\ 27 \end{array} \quad \begin{array}{r} 13.4 \\ 50 \end{array}$$

$$\begin{array}{r} 9.9 \\ 50 \end{array} \quad \begin{array}{r} 10.3 \\ 31 \end{array} \quad \begin{array}{r} 10.6 \\ 16 \end{array} \quad \begin{array}{r} 11.2 \\ 12 \end{array} \quad 11.0 \quad \begin{array}{r} 11.8 \\ 14 \end{array} \quad \begin{array}{r} 13.2 \\ 16 \end{array} \quad \begin{array}{r} 14.7 \\ 22 \end{array} \quad \begin{array}{r} 14.9 \\ 26 \end{array} \quad \begin{array}{r} 14.8 \\ 50 \end{array}$$

$$\begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 9.0 \\ 29 \end{array} \quad \begin{array}{r} 9.3 \\ 13 \end{array} \quad 9.1 \quad \begin{array}{r} 10.0 \\ 13 \end{array} \quad \begin{array}{r} 13.8 \\ 19 \end{array} \quad \begin{array}{r} 14.6 \\ 25 \end{array} \quad \begin{array}{r} 14.1 \\ 28 \end{array} \quad \begin{array}{r} 14.8 \\ 50 \end{array}$$

$$\begin{array}{r} 3.0 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 28 \end{array} \quad \begin{array}{r} 7.1 \\ 14 \end{array} \quad 7.0 \quad \begin{array}{r} 7.7 \\ 14 \end{array} \quad \begin{array}{r} 11.8 \\ 20 \end{array} \quad \begin{array}{r} 12.7 \\ 27 \end{array} \quad \begin{array}{r} 14.1 \\ 50 \end{array}$$

$$\begin{array}{r} +1.5 \\ 50 \end{array} \quad \begin{array}{r} 2.1 \\ 21 \end{array} \quad \begin{array}{r} 4.4 \\ 16 \end{array} \quad \begin{array}{r} 5.0 \\ 11 \end{array} \quad 4.5 \quad \begin{array}{r} 4.4 \\ 20 \end{array} \quad \begin{array}{r} 6.3 \\ 25 \end{array} \quad \begin{array}{r} 9.0 \\ 32 \end{array} \quad \begin{array}{r} 10.8 \\ 50 \end{array}$$

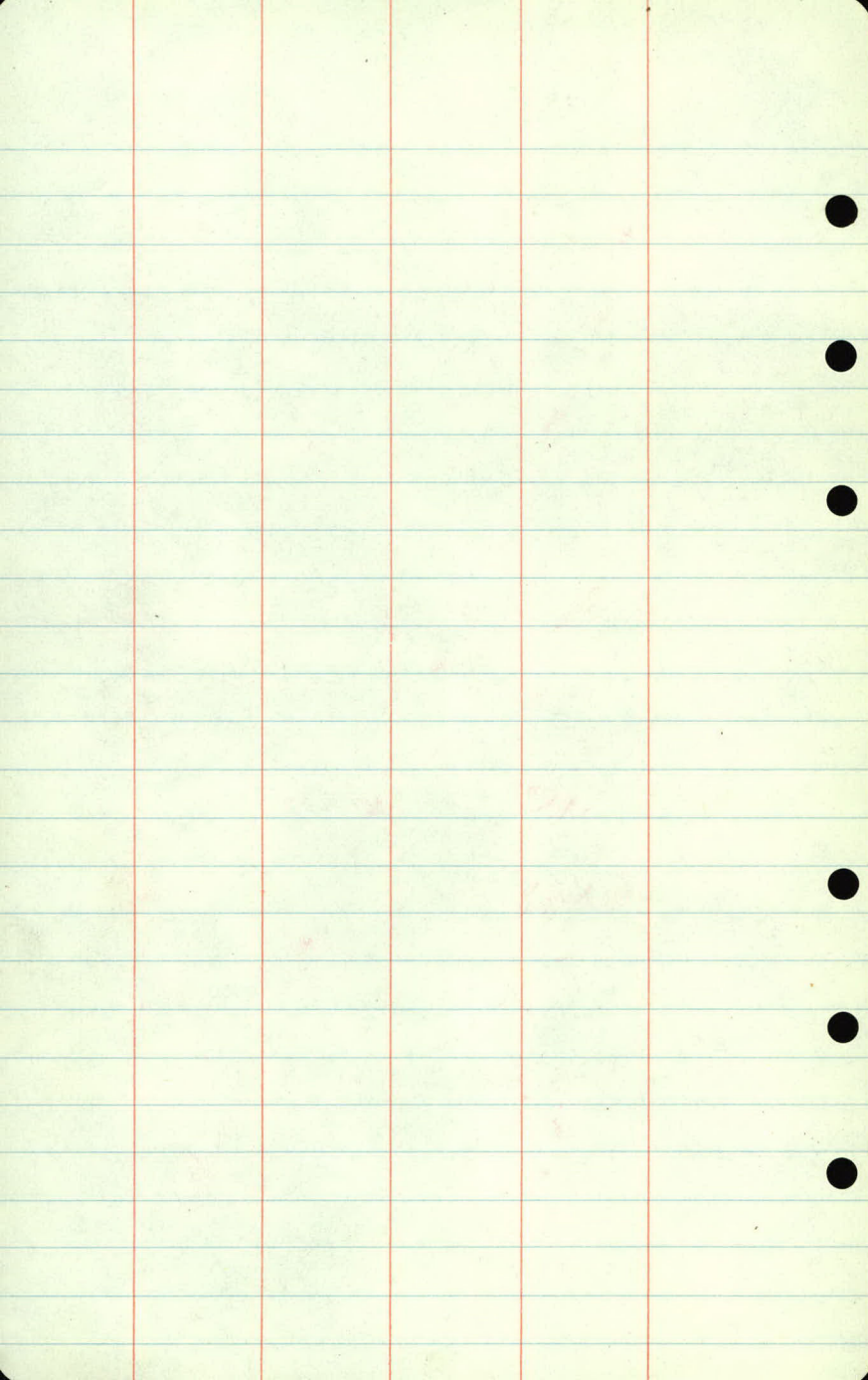
$$\begin{array}{r} +1.5 \\ 50 \end{array} \quad \begin{array}{r} 0.9 \\ 22 \end{array} \quad \begin{array}{r} 4.1 \\ 14 \end{array} \quad \begin{array}{r} 3.4 \\ 9 \end{array} \quad 3.3 \quad \begin{array}{r} 3.1 \\ 28 \end{array} \quad \begin{array}{r} 6.3 \\ 37 \end{array} \quad \begin{array}{r} 8.7 \\ 50 \end{array}$$

$$\begin{array}{r} 2.5 \\ 50 \end{array} \quad \begin{array}{r} 1.7 \\ 27 \end{array} \quad \begin{array}{r} 3.1 \\ 14 \end{array} \quad 2.6 \quad \begin{array}{r} 2.4 \\ 33 \end{array} \quad \begin{array}{r} 3.0 \\ 50 \end{array}$$

$$\begin{array}{r} 1.5 \\ 50 \end{array} \quad \begin{array}{r} 7.5 \\ 25 \end{array} \quad 2.2$$

$$\begin{array}{r} 1.5 \\ 50 \end{array} \quad \begin{array}{r} 2.5 \\ 25 \end{array} \quad 1.8 \quad \begin{array}{r} 2.3 \\ 50 \end{array}$$

Top. Mon. Hamline E "F"



3 now

7.9	7.2	5.3	4.7	5.4	9.1	7.6	6.5		
50	25	17	9	4.8	7	14	20	50	
8.4	8.2	8.1	5.3	4.4	5.2	7.4	8.4	6.7	4.9
50	31	28	18	6	4.7	8	11	15	19
8.4	8.4	7.7	4.7	4.6	7.3	7.4	6.0		
50	32	25	15	4.1	8	5	25	50	
7.4	7.7	4.6	3.7	3.7	4.2	7.5	7.7	7.3	
50	30	18	9		10	16	26	50	
6.3	6.2	3.5	3.0	3.1	3.7	7.5	2.8	7.7	
50	26	17	10		9	15	21	50	
3.4	5.0	2.9	2.8	2.8	6.4	7.0	2.6	7.0	
50	25	17	12	9	14	22	28	50	
12.2	12.1	11.9	10.8	10.3	12.4	14.5	14.2	14.0	
50	39	22	17	10.3	9	13	18	29	50
10.2	11.4	10.7	9.5	8.9	11	11.7	10.6	9.1	8.4
50	34	18	25	9	15	12	21	27	30
9.8	9.2	8.5	7.7	7.1	7.7	9.2	4.0	2.6	0.6
50	35	19	14	9	7.2	7	11	19	25
5.9	6.0	6.0	5.7	5.1	5.4	5.3	3.8	4.0	3.3
50	25	17	14	8	5.1	6	11	20	25
3.4	4.1	3.7	3.4	2.8	3.4	4.1	3.2	2.4	2.0
50	36	17	15	8	9	12	17	7	50
10.5	0.1	1.0	1.2	1.0	0.8	0.9	1.3	1.7	12.6
50	42	27	22	14	0.4	7	10	18	25

Sta + K - Elev

9

100 100 100 100 100

9.5

7.5

5.5

4.7

4.3

4.0

3.7

3.2

3.0

2.8

2.6

B.M. +11.84 994.90 983.06

19+13 994.90 11.2 83.7

+21 11.2 83.7

+31 11.1 83.8

+50 11.1 83.8

07 10 12 15 18 21 24 27 30 33 36 39 42 45 48 51 54 57 60

63 66 69 72 75 78 81 84 87 90 93 96 99 102 105 108 111 114 117 120

123 126 129 132 135 138 141 144 147 150 153 156 159 162 165 168 171 174 177 180

183 186 189 192 195 198 201 204 207 210 213 216 219 222 225 228 231 234 237 240

243 246 249 252 255 258 261 264 267 270 273 276 279 282 285 288 291 294 297 300

303 306 309 312 315 318 321 324 327 330 333 336 339 342 345 348 351 354 357 360

363 366 369 372 375 378 381 384 387 390 393 396 399 402 405 408 411 414 417 420

11.8
50
O.K. 7
50

11.8 11.2 11.2 11.6 11.9
50 50 23 11.2 20 50

11.8 12.0 1.4 11.8 13.3 13.6
50 40 36 11.2 20 37 50

7.7 1.3 1.8 1.3 1.2 11.1 11.5 12.6 12.7 10.3 12.8
50 35 30 36 16 14 18 22 28 34

3.1 7.0 11.5 11.5 11.3 11.1 11.5 13.0 13.0 9.4 9.4 11.7 13.8
50 35 21 19 17 12 14 17 26 27 34 50

Sta + π - Elev.

994.90

20 11.1 83.8

+50 10.9 84.0

21 10.8 84.1

+50 10.7 84.2

22 11.0 83.9

T.P. 0.50 987.86 7.54 987.36

+50 4.5 83.4

23 5.5 82.4

+50 7.2 80.7

24 9.0 78.9

+50 10.9 77.0

+75 12.0 75.9

25 13.2 74.7

T.P. 0.82 975.48 13.20 974.66

$$\frac{3.6}{50} \frac{5.1}{27} \frac{11.4}{17} \frac{11.6}{14} \frac{11.6}{12} \frac{11.3}{8} \frac{11.4}{11} \frac{12.9}{15} \frac{8.1}{17} \frac{10.2}{26} \frac{11.7}{34} \frac{11.7}{50}$$

$$\frac{5.8}{50} \frac{8.5}{25} \frac{10.0}{19} \frac{11.2}{14} \frac{11.1}{10} 10.9 \frac{11.5}{11} \frac{13.5}{15-17} \frac{13.5}{22} \frac{13.9}{50}$$

$$\frac{8.6}{50} \frac{10.2}{17} \frac{11.3}{14-12} \frac{10.9}{8} 10.8 \frac{11.5}{10} \frac{12.8}{16} \frac{13.5}{28} \frac{14.3}{50}$$

$$\frac{6.8}{50} \frac{10.2}{18} \frac{11.3}{13} \frac{11.1}{10} 10.7 \frac{11.1}{9} \frac{11.7}{13} \frac{11.7}{50}$$

$$\frac{8.1}{50} \frac{8.1}{25} \frac{11.9}{16} \frac{11.3}{11} 11.0 \frac{11.4}{7} \frac{11.5}{12} \frac{8.7}{17} \frac{6.7}{50}$$

$$\frac{1.0}{50} \frac{0.5}{27} \frac{5.3}{17} \frac{4.8}{12} 4.5 \frac{4.9}{8} \frac{5.2}{12} \frac{1.3}{19} \frac{2.6}{50}$$

$$\frac{1.7}{50} \frac{1.1}{25} \frac{6.3}{17} \frac{5.8}{11} 5.5 \frac{5.8}{6} \frac{6.1}{11} \frac{2.7}{19} \frac{3.2}{28} \frac{4.9}{50}$$

$$\frac{4.8}{50} \frac{6.1}{21} \frac{7.8}{16} \frac{7.3}{8} 7.2 \frac{7.4}{10} \frac{6.8}{18} \frac{5.9}{50}$$

$$\frac{7.3}{50} \frac{8.5}{23} \frac{9.6}{17} \frac{9.1}{11} 9.0 \frac{9.4}{9} \frac{8.2}{17} \frac{7.6}{29} \frac{6.6}{50}$$

$$\frac{10.2}{50} \frac{9.1}{45} \frac{9.7}{21} \frac{11.4}{17} \frac{10.9}{9} 10.9 \frac{11.5}{8} \frac{9.7}{14} \frac{7.6}{34} \frac{5.7}{50}$$

$$\frac{12.8}{50} \frac{12.9}{40} \frac{13.8}{32} \frac{11.8}{26} \frac{12.8}{20} \frac{12.2}{13} 12.0 \frac{12.4}{8} \frac{10.3}{15} \frac{8.9}{26} \frac{5.5}{50}$$

$$\frac{14.4}{50} \frac{14.4}{41} \frac{15.4}{35} \frac{13.2}{25} \frac{14.1}{20} \frac{13.2}{14} 13.2 \frac{13.7}{8} \frac{11.8}{13} \frac{10.2}{30} \frac{8.0}{50}$$

Sta.	+	π	-	Elev.
		975.48		
25+50			2.8	72.7
26			4.5	71.0
+50			6.5	69.0
27			8.2	67.3
+50			9.5	66.0
28			9.9	65.6
+21	Profile of Ditch on Rt.			
T.P.	4.50	969.49	10.49	964.99
+50			4.5	65.0
29			4.7	64.8
+50			5.1	64.4
+94	Culvert $\frac{1}{2}$ 12' x 40			
30			5.3	64.2
+50			4.8	64.7

$$\begin{array}{r} 3.5 \ 5.2 \ 5.2 \ 4.8 \ 4.9 \ 3.1 \ 2.7 \\ 50 \ 40 \ 28 \ 24 \ 21 \ 16 \ 9 \end{array} \quad \begin{array}{r} 3.2 \ 4.7 \ 4.4 \ 3.7 \ 2.7 \\ 7 \ 10 \ 20 \ 36 \ 50 \end{array}$$

$$\begin{array}{r} 2.6 \ 3.6 \ 5.9 \ 6.6 \ 6.1 \ 4.9 \ 4.5 \\ 50 \ 44 \ 40 \ 30 \ 21 \ 17 \ 12 \end{array} \quad \begin{array}{r} 4.9 \ 7.7 \ 8.2 \ 7.8 \ 7.4 \ 7.0 \\ 4.5 \ 4 \ 12 \ 23 \ 26 \ 40 \ 50 \end{array}$$

$$\begin{array}{r} 4.7 \ 8.1 \ 8.0 \ 7.7 \ 6.5 \ 6.1 \\ 50 \ 37 \ 30 \ 25 \ 18 \ 12 \end{array} \quad \begin{array}{r} 7.0 \ 10.7 \ 11.7 \ 11.3 \\ 6.5 \ 5 \ 12 \ 22 \ 50 \end{array}$$

$$\begin{array}{r} 5.0 \ 5.4 \ 8.8 \ 9.1 \ 8.2 \ 7.9 \\ 50 \ 47 \ 36 \ 26 \ 21 \ 15 \end{array} \quad \begin{array}{r} 8.7 \ 11.7 \ 13.4 \ 14.0 \ 15.0 \\ 8.2 \ 5 \ 9 \ 13 \ 27 \ 50 \end{array}$$

$$\begin{array}{r} 6.8 \ 8.3 \ 10.3 \ 10.3 \ 9.9 \ 9.2 \\ 50 \ 42 \ 31 \ 24 \ 22 \ 12 \end{array} \quad \begin{array}{r} 10.0 \ 14.1 \ 15.6 \\ 9.5 \ 5 \ 13 \ 50 \end{array}$$

$$\begin{array}{r} 8.4 \ 9.4 \ 12.0 \ 11.8 \ 10.6 \ 9.9 \\ 50 \ 43 \ 37 \ 28 \ 23 \ 13 \end{array} \quad \begin{array}{r} 10.5 \ 12.7 \ 13.7 \ 15.4 \ 15.2 \\ 6 \ 12 \ 27 \ 35 \ 50 \end{array}$$

$$\begin{array}{r} 16.7 \ 17.0 \ 17.8 \\ 50 \ 100 \ 150 \end{array}$$

$$\begin{array}{r} 3.2 \ 3.6 \ 6.2 \ 5.8 \ 5.2 \ 4.7 \\ 50 \ 43 \ 37 \ 30 \ 27 \ 19 \end{array} \quad \begin{array}{r} 4.5 \ 4.7 \ 6.0 \ 5.9 \ 6.4 \ 10.5 \ 7.7 \ 7.4 \\ 4.5 \ 7 \ 12 \ 15 \ 23 \ 29 \ 31 \ 36 \ 50 \end{array}$$

$$\begin{array}{r} 4.6 \ 4.3 \ 6.3 \ 6.0 \ 5.6 \ 4.8 \\ 50 \ 40 \ 34 \ 30 \ 22 \ 12 \end{array} \quad \begin{array}{r} 4.7 \ 5.4 \ 7.7 \ 7.5 \ 7.8 \ 10.0 \ 8.4 \ 7.9 \\ 8 \ 14 \ 16 \ 19 \ 25 \ 28 \ 31 \ 34 \ 50 \end{array}$$

$$\begin{array}{r} 8.5 \ 8.6 \ 8.1 \ 6.0 \ 5.4 \\ 50 \ 25 \ 19 \ 15 \ 10 \end{array} \quad \begin{array}{r} 5.7 \ 8.5 \ 8.5 \ 9.8 \ 9.2 \ 9.6 \\ 9 \ 15 \ 21 \ 30 \ 37 \ 50 \end{array}$$

$$\begin{array}{r} 9.3 \ 60.7 \\ 13 \ 17 \end{array} \quad \begin{array}{r} 10.0 \ 59.5 \\ 17 \end{array}$$

$$\begin{array}{r} 8.5 \ 8.7 \ 8.1 \ 5.8 \ 5.4 \\ 50 \ 25 \ 18 \ 11 \ 7 \end{array} \quad \begin{array}{r} 5.9 \ 7.9 \ 9.0 \ 9.9 \\ 11 \ 15 \ 21 \ 50 \end{array}$$

$$\begin{array}{r} 7.7 \ 8.4 \ 5.1 \\ 50 \ 16 \ 9 \end{array} \quad \begin{array}{r} 4.8 \ 5.0 \ 5.6 \ 8.3 \ 9.3 \ 9.1 \\ 8 \ 14 \ 20 \ 38 \ 50 \end{array}$$

Sta	+	+	-	Elev
		969.49		
31			4.1	65.4
B.M.			3.67	(o.k.) B.P. 965.82
+50			3.9	66.2
T.P.	11.62	978.15	2.96	966.53
32			11.4	66.8
+50			10.5	67.7
+75			10.1	68.1
33			9.8	68.4
+50			9.3	68.9
34			10.1	68.1
+50			11.1	67.1
35			12.0	66.2
+50			12.5	65.7
36			13.4	64.8
T.P.	2.91	962.34	13.72	964.43

$$\begin{array}{cccccccccccc} 6.7 & 6.6 & 6.3 & 4.6 & & 4.6 & 6.9 & 7.0 & 4.6 & 3.4 & 3.9 \\ 50 & 27 & 16 & 8 & 4.1 & 15 & 21 & 26 & 30 & 40 & 50 \end{array}$$

Spike in 30' at 35' Rt Sta. 30+90

$$\begin{array}{cccccccccccc} 5.8 & 5.5 & 4.9 & 3.8 & & 3.3 & 3.8 & 5.5 & 1.4 & 0.0 & +0.6 \\ 50 & 21 & 11 & 7 & 3.3 & 9 & 17 & 21.23 & 30 & 38 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 12.3 & 13.5 & 13.2 & 11.7 & & 11.4 & 12.0 & 13.4 & 10.0 & 9.3 & 9.4 \\ 50 & 20 & 11 & 7 & 11.4 & 10 & 17 & 20.23 & 31 & 43 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 12.6 & 12.6 & 11.3 & & & 10.6 & 11.1 & 11.4 & 11.1 & 10.5 \\ 50 & 22 & 9 & 10.5 & 12 & 18 & 22 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 12.2 & 11.1 & 10.8 & 10.3 & & 10.2 & 10.5 & 9.5 & 9.2 & 9.4 \\ 50 & 14 & 9 & 6 & 10.1 & 12 & 16 & 21 & 41 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 10.5 & 10.2 & 8.3 & 10.5 & 10.0 & 9.9 & 10.2 & 7.5 & 8.0 & 7.6 \\ 50 & 43 & 19 & 8 & 6 & 9.8 & 13 & 17 & 25 & 36 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 6.7 & 5.2 & 5.1 & 8.7 & 7.8 & & 9.3 & 9.4 & 5.2 & 5.7 & 6.7 \\ 50 & 30 & 18 & 11 & 7 & 9.3 & 13 & 18 & 25 & 39 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 7.1 & 6.7 & 7.9 & 10.1 & 10.9 & 10.4 & & 10.1 & 10.3 & 6.9 & 7.4 \\ 50 & 21 & 19 & 12 & 8 & 4 & 10.1 & 15 & 19 & 26 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 11.9 & 11.4 & 10.3 & 11.9 & 11.2 & & 10.7 & 11.1 & 11.3 & 10.4 & 9.4 & 9.3 \\ 50 & 38 & 13 & 5 & 2 & 11.1 & 12 & 19 & 23 & 28 & 31 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 17.5 & 16.0 & 15.2 & 13.7 & 12.3 & & 11.7 & 11.4 & 11.6 & 12.1 & 9.8 & 8.5 \\ 50 & 35 & 20 & 8 & 3 & 12.0 & 3 & 4 & 21 & 25 & 30 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 17.8 & 17.2 & 15.2 & 13.2 & & 12.1 & 12.5 & 13.5 & 13.8 & 7.6 & 7.4 \\ 50 & 31 & 16 & 3 & 12.5 & 4 & 25 & 30 & 36 & 45 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 18.0 & 17.0 & 15.2 & & & 13.0 & 13.6 & 14.3 & 14.3 & 10.0 & 9.8 \\ 50 & 33 & 12 & 13.4 & 13 & 26 & 29 & 35 & 42 & 50 \end{array}$$

Sta.	+	π	-	Elev.
		967.34		
B.M.	262	966.84	3.14	964.20
36+68			3.8	63.0
37			4.4	62.4
+62			5.6	61.2
38			6.4	60.4
+71			8.1	58.7
39			8.7	58.1
+25			9.1	57.7
+50			9.6	57.2
40			10.1	56.7
T.P.	8.07	964.73	10.18	956.66
+41-12" Culv. &				
+67	Profile of Ditch Rt.			
+67			7.8	56.9

Spike in 30" Oak 100' RL 37+30

$$\begin{array}{r} 50 \quad 4.0 \quad 7.0 \quad 3.8 \quad 3.4 \quad 3.2 \quad 4.0 \quad 5.5 \quad 5.5 \quad 4.5 \quad 4.5 \\ 50 \quad 20 \quad 6 \quad 5 \quad 5 \quad 13 \quad 24 \quad 28 \quad 35 \quad 46 \quad 50 \end{array}$$

$$\begin{array}{r} 1.5 \quad 3.0 \quad 4.8 \quad 6.8 \quad 4.5 \quad 4.1 \quad 4.0 \quad 4.6 \quad 6.2 \quad 5.7 \quad 5.6 \quad 5.5 \\ 50 \quad 37 \quad 12 \quad 5.7 \quad 5 \quad 4.4 \quad 4 \quad 14 \quad 23 \quad 28 \quad 33 \quad 45 \quad 50 \end{array}$$

$$\begin{array}{r} 4.7 \quad 4.4 \quad 3.8 \quad 7.5 \quad 6.0 \quad 5.2 \quad 5.8 \quad 6.8 \quad 6.7 \quad 6.0 \quad 5.2 \quad 4.8 \\ 50 \quad 26 \quad 11 \quad 7.3 \quad 4 \quad 5.6 \quad 11 \quad 24 \quad 26 \quad 28 \quad 31 \quad 42 \quad 50 \end{array}$$

$$\begin{array}{r} 10.2 \quad 9.7 \quad 8.0 \quad 8.4 \quad 6.7 \quad 6.2 \quad 6.0 \quad 6.7 \quad 7.3 \quad 7.5 \quad 6.1 \quad 5.1 \\ 50 \quad 27 \quad 6 \quad 5 \quad 2 \quad 6.4 \quad 4 \quad 13 \quad 22 \quad 24 \quad 28 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 12.8 \quad 12.5 \quad 11.6 \quad 8.4 \quad 7.7 \quad 8.3 \quad 8.4 \quad 8.1 \\ 50 \quad 20 \quad 8 \quad 2 \quad 8.1 \quad 8 \quad 23 \quad 28 \quad 43 \end{array}$$

$$\begin{array}{r} 12.8 \quad 12.2 \quad 11.4 \quad 11.8 \quad 8.3 \quad 8.7 \quad 9.3 \quad 6.6 \quad 5.2 \\ 50 \quad 25 \quad 11 \quad 8 \quad 3 \quad 8.7 \quad 11 \quad 19 \quad 25 \quad 26 \quad 31 \quad 50 \end{array}$$

$$\begin{array}{r} 11.8 \quad 12.0 \quad 10.5 \quad 10.3 \quad 9.5 \quad 8.8 \quad 9.1 \quad 9.7 \quad 9.7 \quad 4.7 \quad 5.9 \\ 50 \quad 35 \quad 11 \quad 7 \quad 5 \quad 9.1 \quad 8 \quad 18 \quad 24 \quad 33 \quad 43 \quad 50 \end{array}$$

$$\begin{array}{r} 11.2 \quad 11.9 \quad 11.8 \quad 9.8 \quad 9.3 \quad 9.8 \quad 10.1 \quad 6.1 \quad 4.5 \\ 50 \quad 32 \quad 10 \quad 5 \quad 9.6 \quad 9 \quad 17 \quad 23 \quad 35 \quad 50 \end{array}$$

$$\begin{array}{r} 11.9 \quad 13.5 \quad 13.2 \quad 10.4 \quad 9.9 \quad 10.2 \quad 12.4 \quad 11.7 \quad 11.6 \quad 10.7 \\ 50 \quad 77 \quad 10 \quad 3 \quad 10 \quad 12 \quad 21 \quad 28 \quad 35 \quad 41 \quad 50 \end{array}$$

$$\begin{array}{r} 12.4 \\ 11 \end{array} \quad 52.3$$

$$\begin{array}{r} 12.4 \\ 25 \end{array} \quad 52.3$$

$$\begin{array}{r} 14.0 \quad 14.9 \quad 16.4 \\ 50 \quad 100 \quad 150 \end{array}$$

$$\begin{array}{r} 9.2 \quad 10.2 \quad 9.8 \quad 8.0 \quad 7.8 \quad 8.7 \quad 12.6 \quad 13.7 \quad 13.4 \\ 50 \quad 16 \quad 11 \quad 5 \quad 7.8 \quad 7 \quad 18 \quad 26 \quad 38 \quad 50 \end{array}$$

Sta.	+	π	-	Elev
		964.73		
41			7.3	57.4
+24			6.8	57.9
+50			6.3	58.4
42			5.4	59.3
+50			4.2	60.5
43			3.8	60.9
+50			2.9	61.8
44			1.9	62.8
T.P.	8.94	971.42	2.25	962.48
+50			7.6	73.8 63.8
45			6.9	64.5
+15			6.5	64.9
+32.65			6.1	65.3
B.M.			6.11	965.31 965.30

$\frac{5.0}{50}$ $\frac{5.7}{33}$ $\frac{10.7}{24}$ $\frac{11.0}{20}$ $\frac{10.4}{15}$ $\frac{7.6}{7}$ 7.3 $\frac{8.1}{17}$ $\frac{10.4}{24}$ $\frac{11.4}{38}$ $\frac{10.5}{41}$ $\frac{10.8}{50}$

$\frac{2.8}{50}$ $\frac{3.3}{37}$ $\frac{4.5}{36}$ $\frac{10.1}{26}$ $\frac{10.6}{22}$ $\frac{10.2}{15}$ $\frac{7.2}{8}$ 6.8 17 $\frac{7.5}{24}$ $\frac{9.4}{34}$ $\frac{10.1}{39}$ $\frac{8.1}{39}$ $\frac{7.9}{50}$

$\frac{4.4}{50}$ $\frac{4.3}{35}$ $\frac{7.3}{28}$ $\frac{10.3}{19}$ $\frac{6.8}{9}$ 6.3 $\frac{6.9}{17}$ $\frac{8.1}{24}$ $\frac{8.6}{33}$ $\frac{5.2}{41}$ $\frac{5.2}{50}$

$\frac{6.5}{50}$ $\frac{6.5}{43}$ $\frac{6.0}{28}$ $\frac{6.2}{14}$ $\frac{5.7}{8}$ 5.4 $\frac{6.0}{16}$ $\frac{6.7}{22}$ $\frac{6.5}{25}$ $\frac{6.6}{50}$

$\frac{7.6}{50}$ $\frac{6.9}{21}$ $\frac{6.7}{13}$ $\frac{5.3}{10}$ 4.2 $\frac{5.3}{13}$ $\frac{7.0}{17}$ $\frac{7.7}{22}$ $\frac{7.9}{27}$ $\frac{7.9}{34}$ $\frac{8.2}{50}$

$\frac{7.3}{50}$ $\frac{6.5}{22}$ $\frac{6.5}{17}$ $\frac{4.6}{11}$ 3.8 $\frac{4.5}{14}$ $\frac{7.3}{19}$ $\frac{8.0}{28}$ $\frac{8.4}{50}$

$\frac{4.1}{50}$ $\frac{4.4}{32}$ $\frac{5.7}{24}$ $\frac{6.0}{18}$ $\frac{3.5}{12}$ 2.9 $\frac{3.7}{13}$ $\frac{6.3}{17}$ $\frac{8.2}{50}$

$\frac{1.2}{50}$ $\frac{1.7}{39}$ $\frac{3.7}{30}$ $\frac{4.4}{26}$ $\frac{5.1}{22}$ $\frac{2.5}{14}$ $\frac{3.2}{16}$ $\frac{4.1}{26}$ $\frac{5.2}{50}$

$\frac{7.9}{50}$ $\frac{8.2}{33}$ $\frac{2.8}{25}$ $\frac{9.9}{16}$ $\frac{5.0}{13}$ 7.6 $\frac{8.1}{12}$ $\frac{8.2}{14}$ $\frac{6.9}{17}$ $\frac{7.7}{34}$ $\frac{8.6}{50}$

$\frac{6.5}{50}$ $\frac{6.1}{39}$ $\frac{7.8}{26}$ $\frac{7.5}{19}$ $\frac{7.0}{9}$ 6.9 $\frac{7.1}{12}$ $\frac{7.9}{22}$ $\frac{7.8}{28}$ $\frac{9.7}{50}$

$\frac{5.4}{50}$ $\frac{6.1}{21}$ 6.5 $\frac{6.8}{16}$ $\frac{7.9}{50}$

$\frac{4.6}{50}$ 6.1 $\frac{7.7}{50}$

Top Man Lexington E R

Sta	+	π	-	Elev.
		971.42		
45+47			5.9	65.5
+53			5.8	65.6
+59			5.8	65.6
46			5.1	66.3
+50			4.3	67.1
47			3.7	67.7
+50			3.0	68.4
48			2.5	68.9
T.P.	10.48	979.01	2.89	968.53
+50			9.8	69.2
49			9.1	69.9
+03	Cylr. 12" x 118' At $\frac{1}{2}$			
+50			8.2	70.8
50			7.0	72.0

64.8
6.6
6.4

$$\begin{array}{r} 5.2 \ 5.7 \\ 50 \ 21 \ 5.9 \end{array} \quad \begin{array}{r} 6.6 \ 7.2 \ 7.9 \\ 15 \ 27 \ 50 \end{array}$$

$$\begin{array}{r} 6.8 \ 6.9 \ 6.0 \\ 50 \ 21 \ 15 \end{array} \quad \begin{array}{r} 7.4 \ 8.9 \ 8.8 \ 9.1 \\ 5.8 \ 21 \ 21 \ 26 \ 50 \end{array}$$

63.1
6.3
6.0

$$\begin{array}{r} 4.0 \ 4.8 \ 6.6 \ 6.0 \\ 50 \ 29 \ 20 \ 16 \end{array} \quad \begin{array}{r} 5.8 \ 6.5 \ 7.8 \ 8.8 \\ 12 \ 19 \ 50 \end{array}$$

$$\begin{array}{r} 4.2 \ 4.8 \ 5.4 \ 5.2 \\ 50 \ 21 \ 17 \ 12 \end{array} \quad \begin{array}{r} 5.7 \ 6.0 \ 9.0 \\ 7 \ 24 \ 50 \end{array}$$

$$\begin{array}{r} 3.6 \ 3.8 \ 5.0 \ 4.4 \\ 50 \ 22 \ 16 \ 11 \end{array} \quad \begin{array}{r} 4.3 \ 5.0 \ 4.9 \ 8.2 \ 11.4 \\ 7 \ 11 \ 16 \ 25 \ 50 \end{array}$$

$$\begin{array}{r} 2.5 \ 3.4 \ 5.5 \ 4.0 \\ 50 \ 24 \ 19 \ 11 \end{array} \quad \begin{array}{r} 3.7 \ 4.8 \ 6.8 \ 7.7 \ 10.7 \\ 14 \ 17 \ 24 \ 50 \end{array}$$

$$\begin{array}{r} 1.7 \\ 50 \end{array} \quad \begin{array}{r} 1.8 \ 5.4 \ 3.6 \ 3.0 \\ 27 \ 22 \ 20 \ 16 \ 7 \end{array} \quad \begin{array}{r} 3.0 \ 3.9 \ 5.1 \ 7.1 \ 5.7 \ 7.3 \ 8.6 \\ 14 \ 19 \ 22 \ 23 \ 25 \ 43 \ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 3.9 \ 5.5 \ 2.8 \ 2.6 \\ 27 \ 25 \ 23 \ 15 \ 6 \end{array} \quad \begin{array}{r} 2.5 \ 3.2 \ 5.2 \ 6.4 \ 5.4 \ 5.3 \ 7.4 \\ 14 \ 21 \ 24 \ 25 \ 26 \ 32 \ 50 \end{array}$$

$$\begin{array}{r} 16.0 \ 14.8 \ 10.3 \\ 50 \ 24 \ 13 \ 9.8 \end{array} \quad \begin{array}{r} 10.6 \ 13.8 \ 14.0 \ 16.5 \\ 13 \ 19 \ 27 \ 50 \end{array}$$

$$\begin{array}{r} 16.5 \ 15.7 \ 9.6 \\ 50 \ 24 \ 13 \ 9.1 \end{array} \quad \begin{array}{r} 10.0 \ 13.4 \ 14.4 \ 15.8 \\ 13 \ 23 \ 28 \ 50 \end{array}$$

$$\begin{array}{r} 16.9 \\ 24 \end{array} \quad 62.1$$

$$\begin{array}{r} 26.5 \\ 9.4 \end{array} \quad 57.5$$

$$\begin{array}{r} 16.2 \ 14.9 \ 8.9 \\ 50 \ 22 \ 13 \ 8.2 \end{array} \quad \begin{array}{r} 9.0 \ 12.0 \ 10.5 \ 11.8 \\ 16 \ 21 \ 24 \ 26 \ 50 \end{array}$$

$$\begin{array}{r} 15.7 \ 14.0 \ 9.7 \\ 50 \ 23 \ 12 \end{array} \quad \begin{array}{r} 7.3 \ 7.7 \ 7.6 \ 7.2 \ 7.6 \ 8.2 \\ 7.0 \ 8 \ 16 \ 21 \ 24 \ 27 \ 28 \ 50 \end{array}$$

Sta	+	π	-	Elev
		979.01		
50+50			5.7	73.3
+84			4.8	74.2
51			4.3	74.7
T.P.	643	985.03	0.41	978.60
+66			9.2	75.8
52			8.8	76.2
+50			8.3	76.7
+75			8.3	76.7
53			8.3	76.7
+50			8.7	76.3
+68			8.9	76.1
54			9.3	75.7
+63			10.1	74.9

6.

$$\begin{array}{r} 12.7 \\ 50 \end{array} \quad \begin{array}{r} 10.9 \\ 23 \end{array} \quad \begin{array}{r} 6.2 \\ 14 \end{array} \quad 5.7 \quad \begin{array}{r} 6.2 \\ 12 \end{array} \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad \begin{array}{r} 7.1 \\ 18 \end{array} \quad \begin{array}{r} 2.0 \\ 28 \end{array} \quad \begin{array}{r} 2.5 \\ 50 \end{array}$$

$$\begin{array}{r} 10.6 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 18 \end{array} \quad \begin{array}{r} 6.5 \\ 16 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad 4.8 \quad \begin{array}{r} 5.1 \\ 14 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 4.0 \\ 32 \end{array} \quad \begin{array}{r} 0.5 \\ 50 \end{array}$$

$$\begin{array}{r} 9.0 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 33 \end{array} \quad \begin{array}{r} 5.4 \\ 23 \end{array} \quad \begin{array}{r} 5.6 \\ 17 \end{array} \quad \begin{array}{r} 5.7 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 12 \end{array} \quad 4.3 \quad \begin{array}{r} 4.8 \\ 13 \end{array} \quad \begin{array}{r} 5.8 \\ 17 \end{array} \quad \begin{array}{r} 4.0 \\ 26 \end{array} \quad \begin{array}{r} 2.0 \\ 50 \end{array}$$

$$\begin{array}{r} 7.9 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 40 \end{array} \quad \begin{array}{r} 9.1 \\ 19 \end{array} \quad \begin{array}{r} 9.6 \\ 16 \end{array} \quad \begin{array}{r} 9.5 \\ 12 \end{array} \quad 9.2 \quad \begin{array}{r} 9.5 \\ 9 \end{array} \quad \begin{array}{r} 9.8 \\ 14 \end{array} \quad \begin{array}{r} 11.0 \\ 21 \end{array} \quad \begin{array}{r} 11.5 \\ 27 \end{array} \quad \begin{array}{r} 11.8 \\ 37 \end{array} \quad \begin{array}{r} 12.4 \\ 50 \end{array}$$

$$\begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 19 \end{array} \quad \begin{array}{r} 9.0 \\ 15 \end{array} \quad \begin{array}{r} 8.1 \\ 7 \end{array} \quad 8.8 \quad \begin{array}{r} 9.0 \\ 7 \end{array} \quad \begin{array}{r} 9.4 \\ 16 \end{array} \quad \begin{array}{r} 9.5 \\ 22 \end{array} \quad \begin{array}{r} 10.8 \\ 28 \end{array} \quad \begin{array}{r} 13.0 \\ 50 \end{array}$$

$$\begin{array}{r} 7.1 \\ 50 \end{array} \quad \begin{array}{r} 5.1 \\ 29 \end{array} \quad \begin{array}{r} 4.1 \\ 23 \end{array} \quad \begin{array}{r} 9.0 \\ 14 \end{array} \quad \begin{array}{r} 8.2 \\ 9 \end{array} \quad 8.3 \quad \begin{array}{r} 8.5 \\ 12 \end{array} \quad \begin{array}{r} 5.8 \\ 19 \end{array} \quad \begin{array}{r} 5.3 \\ 50 \end{array}$$

$$\begin{array}{r} 5.6 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 27 \end{array} \quad \begin{array}{r} 5.6 \\ 12 \end{array} \quad \begin{array}{r} 8.6 \\ 9 \end{array} \quad \begin{array}{r} 8.9 \\ 13 \end{array} \quad \begin{array}{r} 2.7 \\ 23 \end{array} \quad \begin{array}{r} 3.1 \\ 30 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array}$$

$$\begin{array}{r} 5.5 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 20 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \end{array} \quad 8.3 \quad \begin{array}{r} 8.7 \\ 15 \end{array} \quad \begin{array}{r} 3.6 \\ 22 \end{array} \quad \begin{array}{r} 4.1 \\ 29 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 31 \end{array} \quad \begin{array}{r} 6.4 \\ 28 \end{array} \quad \begin{array}{r} 8.9 \\ 14 \end{array} \quad \begin{array}{r} 8.9 \\ 9 \end{array} \quad 8.7 \quad \begin{array}{r} 9.2 \\ 11 \end{array} \quad \begin{array}{r} 9.3 \\ 15 \end{array} \quad \begin{array}{r} 6.2 \\ 21 \end{array} \quad \begin{array}{r} 6.1 \\ 29 \end{array} \quad \begin{array}{r} 7.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 29 \end{array} \quad \begin{array}{r} 7.0 \\ 19 \end{array} \quad \begin{array}{r} 9.3 \\ 13 \end{array} \quad \begin{array}{r} 9.0 \\ 6 \end{array} \quad 8.9 \quad \begin{array}{r} 9.4 \\ 14 \end{array} \quad \begin{array}{r} 6.4 \\ 22 \end{array} \quad \begin{array}{r} 5.7 \\ 30 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.8 \\ 50 \end{array} \quad \begin{array}{r} 7.5 \\ 29 \end{array} \quad \begin{array}{r} 7.8 \\ 20 \end{array} \quad \begin{array}{r} 9.6 \\ 14 \end{array} \quad \begin{array}{r} 9.4 \\ 6 \end{array} \quad 9.3 \quad \begin{array}{r} 9.6 \\ 7 \end{array} \quad \begin{array}{r} 9.9 \\ 13 \end{array} \quad \begin{array}{r} 8.2 \\ 20 \end{array} \quad \begin{array}{r} 8.3 \\ 29 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 7.0 \\ 39 \end{array} \quad \begin{array}{r} 8.3 \\ 29 \end{array} \quad \begin{array}{r} 7.1 \\ 20 \end{array} \quad \begin{array}{r} 10.4 \\ 15 \end{array} \quad \begin{array}{r} 10.2 \\ 6 \end{array} \quad 10.1 \quad \begin{array}{r} 10.7 \\ 12 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array} \quad \begin{array}{r} 9.9 \\ 29 \end{array} \quad \begin{array}{r} 10.7 \\ 50 \end{array}$$

Sta	+	$\bar{x}$	-	Elev
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985.03

55			10.9	741
T.P.	4.10	978.20	10.93	974.10

+50			5.0	73.2
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56			5.6	72.6
----	--	--	-----	------

+30	18" Culvert			Ditch Lt.
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+50			6.0	72.2
-----	--	--	-----	------

57			6.4	71.8
B.M.		9.28		968.92

+50			6.3	71.9
-----	--	--	-----	------

58			5.8	72.4
----	--	--	-----	------

+31			5.2	73.0
-----	--	--	-----	------

+89			9.0	74.2
-----	--	--	-----	------

59+12			3.1	74.3
-------	--	--	-----	------

+50			3.6	74.6
-----	--	--	-----	------

+86	12" Culvert			
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$$\begin{array}{r} 9.6 \quad 10.7 \quad 11.8 \quad 11.7 \quad 11.5 \quad 11.4 \quad 12.2 \quad 9.9 \quad 9.7 \quad 9.8 \\ 50 \quad 34 \quad 26 \quad 19 \quad 15 \quad 109 \quad 10 \quad 16 \quad 21 \quad 30 \quad 50 \end{array}$$

$$\begin{array}{r} 7.5 \quad 9.0 \quad 9.6 \quad 5.5 \quad 5.7 \quad 9.6 \quad 9.5 \quad 8.6 \quad 6.6 \\ 50 \quad 32 \quad 19 \quad 15 \quad 50 \quad 11 \quad 17 \quad 29 \quad 37 \quad 50 \end{array}$$

$$\begin{array}{r} 9.3 \quad 9.9 \quad 10.4 \quad 6.1 \quad 6.0 \quad 6.3 \quad 12.7 \quad 12.7 \quad 12.9 \\ 50 \quad 44 \quad 22 \quad 12 \quad 12 \quad 5.6 \quad 10 \quad 23 \quad 29 \quad 50 \end{array}$$

$$\begin{array}{r} 9.1 \quad 9.5 \quad 10.6 \quad 12.4 \quad 15.8 \quad 13.0 \quad 65.7 \\ 150 \quad 100 \quad 50 \quad 25 \quad 23 \end{array}$$

$$\begin{array}{r} 10.4 \quad 11.1 \quad 6.6 \quad 6.5 \quad 10.6 \quad 12.0 \quad 12.2 \quad 12.4 \\ 50 \quad 23 \quad 14 \quad 60 \quad 10 \quad 18 \quad 25 \quad 33 \quad 50 \end{array}$$

$$\begin{array}{r} 8.8 \quad 9.7 \quad 9.6 \quad 6.7 \quad 7.1 \quad 10.4 \quad 10.9 \quad 11.7 \quad 11.8 \\ 50 \quad 30 \quad 23 \quad 14 \quad 64 \quad 10 \quad 15 \quad 20 \quad 30 \quad 50 \end{array}$$

Spike in PP 28' Rt. 57 + 25

$$\begin{array}{r} 3.8 \quad 4.1 \quad 4.9 \quad 8.0 \quad 7.4 \quad 6.4 \quad 7.1 \quad 9.0 \quad 9.7 \quad 11.0 \quad 11.3 \quad 11.0 \quad 12.7 \\ 50 \quad 46 \quad 36 \quad 22 \quad 18 \quad 13 \quad 6.3 \quad 11 \quad 17 \quad 20 \quad 29 \quad 30 \quad 34 \quad 50 \end{array}$$

$$\begin{array}{r} 2.3 \quad 3.4 \quad 6.2 \quad 6.6 \quad 6.0 \quad 5.7 \quad 6.0 \quad 6.8 \quad 7.0 \quad 8.6 \quad 9.7 \quad 10.3 \\ 50 \quad 38 \quad 27 \quad 22 \quad 18 \quad 6 \quad 5.8 \quad 6 \quad 15 \quad 20 \quad 30 \quad 40 \quad 50 \end{array}$$

$$\begin{array}{r} 2.4 \quad 2.8 \quad 5.6 \quad 5.8 \quad 5.4 \quad 5.4 \quad 5.7 \quad 4.9 \quad 6.1 \quad 6.7 \quad 7.6 \quad 8.7 \\ 50 \quad 29 \quad 28 \quad 19 \quad 17 \quad 12 \quad 5.2 \quad 13 \quad 17 \quad 24 \quad 27 \quad 44 \quad 50 \end{array}$$

$$\begin{array}{r} 7.5 \quad 5.6 \quad 4.3 \quad 4.7 \quad 4.6 \quad 4.1 \quad 3.6 \quad 4.0 \\ 50 \quad 24 \quad 12 \quad 40 \quad 12 \quad 17 \quad 27 \quad 31 \quad 50 \end{array}$$

$$\begin{array}{r} 9.5 \quad 8.1 \quad 6.5 \quad 4.0 \quad 4.5 \quad 6.2 \quad 6.5 \quad 6.2 \quad 5.4 \\ 50 \quad 30 \quad 21 \quad 13 \quad 3.9 \quad 11 \quad 15 \quad 24 \quad 32 \quad 50 \end{array}$$

$$\begin{array}{r} 9.2 \quad 8.6 \quad 5.8 \quad 3.7 \quad 4.4 \quad 9.5 \quad 9.7 \quad 8.4 \\ 50 \quad 22 \quad 13 \quad 7 \quad 36 \quad 11 \quad 19 \quad 30 \quad 50 \end{array}$$

$$\begin{array}{r} 10.4 \quad 67.8 \quad 11.5 \quad 66.7 \\ 23 \quad 23 \end{array}$$

Sta	+	Δ	-	Elev
60		978.20		
60			2.4	75.8
+50			0.8	77.4
61				79.1
+50				80.9
T.P.	10.85	988.16	0.89	977.31
61			9.1	79.1
+50			7.3	80.9
62			4.9	83.3
+50			2.8	85.4
63			0.7	87.5
T.P.	10.12	997.51	0.77	987.39
63 +50			9.2	88.3
64			8.8	88.7
+50			8.8	88.7

$$\begin{array}{r} 8.8 \\ 50 \end{array} \quad \begin{array}{r} 8.5 \\ 25 \end{array} \quad \begin{array}{r} 2.7 \\ 13 \end{array} \quad \begin{array}{r} 2.4 \\ 6 \end{array} \quad 2.4 \quad \begin{array}{r} 3.0 \\ 10 \end{array} \quad \begin{array}{r} 9.9 \\ 23 \end{array} \quad \begin{array}{r} 10.9 \\ 28 \end{array} \quad \begin{array}{r} 10.7 \\ 50 \end{array}$$

$$\begin{array}{r} 7.4 \\ 50 \end{array} \quad \begin{array}{r} 7.4 \\ 31 \end{array} \quad \begin{array}{r} 6.7 \\ 23 \end{array} \quad \begin{array}{r} 1.2 \\ 15 \end{array} \quad \begin{array}{r} 1.0 \\ 10 \end{array} \quad 0.8 \quad \begin{array}{r} 1.5 \\ 10 \end{array} \quad \begin{array}{r} 9.5 \\ 23 \end{array} \quad \begin{array}{r} 10.2 \\ 28 \end{array} \quad \begin{array}{r} 10.5 \\ 50 \end{array}$$

$$\begin{array}{r} 5.5 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 24 \end{array}$$

$$(40.9)$$

$$\begin{array}{r} 7.5 \\ 24 \end{array} \quad \begin{array}{r} 8.3 \\ 30 \end{array} \quad \begin{array}{r} 8.8 \\ 50 \end{array}$$

$$\begin{array}{r} 2.2 \\ 50 \end{array} \quad \begin{array}{r} 3.0 \\ 25 \end{array}$$

$$(12.7)$$

$$\begin{array}{r} 5.7 \\ 25 \end{array} \quad \begin{array}{r} 6.1 \\ 30 \end{array} \quad \begin{array}{r} 7.4 \\ 50 \end{array}$$

$$\begin{array}{r} 9.6 \\ 16 \end{array} \quad \begin{array}{r} 9.3 \\ 12 \end{array} \quad 9.1 \quad \begin{array}{r} 9.7 \\ 12 \end{array}$$

$$\begin{array}{r} 7.2 \\ 17 \end{array} \quad \begin{array}{r} 7.4 \\ 12 \end{array} \quad 7.3 \quad \begin{array}{r} 8.0 \\ 12 \end{array}$$

$$\begin{array}{r} 4.6 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 24 \end{array} \quad \begin{array}{r} 9.9 \\ 18 \end{array} \quad \begin{array}{r} 5.2 \\ 12 \end{array} \quad 4.9 \quad \begin{array}{r} 5.8 \\ 11 \end{array} \quad \begin{array}{r} 6.0 \\ 16 \end{array} \quad \begin{array}{r} 11.0 \\ 27 \end{array} \quad \begin{array}{r} 12.1 \\ 38 \end{array} \quad \begin{array}{r} 13.0 \\ 50 \end{array}$$

$$\begin{array}{r} 2.9 \\ 15 \end{array} \quad \begin{array}{r} 3.0 \\ 12 \end{array} \quad 2.8 \quad \begin{array}{r} 3.4 \\ 11 \end{array} \quad \begin{array}{r} 2.5 \\ 15 \end{array} \quad \begin{array}{r} 40.5 \\ 18 \end{array} \quad \begin{array}{r} 1.8 \\ 34 \end{array} \quad \begin{array}{r} 4.1 \\ 50 \end{array}$$

$$\begin{array}{r} 1.1 \\ 12 \end{array} \quad 0.7 \quad \begin{array}{r} 1.3 \\ 9 \end{array} \quad \begin{array}{r} 1.3 \\ 11 \end{array} \quad \begin{array}{r} 0.5 \\ 15 \end{array}$$

$$\begin{array}{r} 4.9 \\ 24 \end{array} \quad \begin{array}{r} 7.5 \\ 18 \end{array} \quad \begin{array}{r} 9.3 \\ 12 \end{array} \quad 9.2 \quad \begin{array}{r} 9.6 \\ 9 \end{array} \quad \begin{array}{r} 9.0 \\ 14 \end{array}$$

$$\begin{array}{r} 5.6 \\ 24 \end{array} \quad \begin{array}{r} 6.3 \\ 20 \end{array} \quad \begin{array}{r} 8.9 \\ 13 \end{array} \quad 8.8 \quad \begin{array}{r} 9.1 \\ 10 \end{array} \quad \begin{array}{r} 5.8 \\ 17 \end{array}$$

$$\begin{array}{r} 6.6 \\ 23 \end{array} \quad \begin{array}{r} 9.3 \\ 13 \end{array} \quad 8.8 \quad \begin{array}{r} 9.1 \\ 9 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array}$$

Sta.	+	$\bar{x}$	-	Elev
		997.51		
65			9.7	87.8
T.P.	12.99	1000.82	9.68	987.83
	13.29	1007.97	16.14	994.68
62+50				85.4
63				87.5
+50				88.3
64				88.7
+50				88.7
65				87.8
T.P.	0.33	988.16	1.7129	987.83
+50	9.68		12.19	86.1
66			3.9	84.3
+50			5.9	82.3
67			7.7	80.5

$$\begin{array}{r} 7.5 \quad 9.3 \quad 10.2 \quad 9.8 \\ 24 \quad 19 \quad 13 \quad 9 \end{array} \quad \begin{array}{r} 10.1 \quad 8.8 \\ 9 \quad 18 \end{array}$$

$$\begin{array}{r} 14.5 \\ 50 \end{array} \quad \begin{array}{r} 16.0 \\ 28 \end{array} \quad (22.6)$$

$$\begin{array}{r} 4.5 \\ 75 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array} \quad \begin{array}{r} 7.3 \\ 37 \end{array} \quad \begin{array}{r} 13.6 \\ 23 \end{array} \quad \begin{array}{r} 16.5 \\ 50 \end{array} \quad \begin{array}{r} 20.8 \\ 75 \end{array}$$

$$\begin{array}{r} 1.8 \\ 75 \end{array} \quad \begin{array}{r} 3.8 \\ 50 \end{array} \quad \begin{array}{r} 3.7 \\ 39 \end{array} \quad \begin{array}{r} 10.4 \\ 26 \end{array} \quad \begin{array}{r} 11.2 \\ 50 \end{array} \quad \begin{array}{r} 13.1 \\ 75 \end{array}$$

$$\begin{array}{r} 7.3 \\ 75 \end{array} \quad \begin{array}{r} 8.5 \\ 50 \end{array} \quad \begin{array}{r} 8.3 \\ 33 \end{array} \quad \begin{array}{r} 5.6 \\ 30 \end{array} \quad \begin{array}{r} 7.2 \\ 50 \end{array} \quad \begin{array}{r} 9.8 \\ 75 \end{array}$$

$$\begin{array}{r} 10.5 \\ 75 \end{array} \quad \begin{array}{r} 10.8 \\ 50 \end{array} \quad \begin{array}{r} 10.6 \\ 31 \end{array} \quad \begin{array}{r} 10.3 \\ 25 \end{array} \quad \begin{array}{r} 10.1 \\ 50 \end{array} \quad \begin{array}{r} 12.4 \\ 75 \end{array}$$

$$\begin{array}{r} 11.1 \\ 75 \end{array} \quad \begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 12.1 \\ 30 \end{array} \quad \begin{array}{r} 12.0 \\ 23 \end{array} \quad \begin{array}{r} 13.0 \\ 44 \end{array} \quad \begin{array}{r} 13.8 \\ 50 \end{array} \quad \begin{array}{r} 16.1 \\ 75 \end{array}$$

$$\begin{array}{r} +5.5 \\ 50 \end{array} \quad \begin{array}{r} +5.0 \\ 41 \end{array} \quad \begin{array}{r} +2.8 \\ 29 \end{array} \quad \begin{array}{r} 2.6 \\ 18 \end{array} \quad \begin{array}{r} 2.5 \\ 15 \end{array} \quad \begin{array}{r} 2.1 \\ 2.1 \end{array} \quad \begin{array}{r} 2.6 \\ 9 \end{array} \quad \begin{array}{r} 2.0 \\ 14 \end{array} \quad \begin{array}{r} 0.0 \\ 16 \end{array} \quad \begin{array}{r} 0.0 \\ 25 \end{array} \quad \begin{array}{r} 0.9 \\ 50 \end{array}$$

$$\begin{array}{r} 1.6 \\ 50 \end{array} \quad \begin{array}{r} 2.9 \\ 34 \end{array} \quad \begin{array}{r} 4.4 \\ 29 \end{array} \quad \begin{array}{r} 4.4 \\ 22 \end{array} \quad \begin{array}{r} 4.9 \\ 20 \end{array} \quad \begin{array}{r} 4.6 \\ 15 \end{array} \quad \begin{array}{r} 4.2 \\ 12 \end{array} \quad \begin{array}{r} 3.8 \\ 26 \end{array} \quad \begin{array}{r} 3.6 \\ 41 \end{array} \quad \begin{array}{r} 4.2 \\ 50 \end{array}$$

$$\begin{array}{r} 9.3 \\ 50 \end{array} \quad \begin{array}{r} 10.8 \\ 26 \end{array} \quad \begin{array}{r} 10.8 \\ 24 \end{array} \quad \begin{array}{r} 6.4 \\ 16 \end{array} \quad \begin{array}{r} 5.9 \\ 59 \end{array} \quad \begin{array}{r} 6.2 \\ 70 \end{array} \quad \begin{array}{r} 8.0 \\ 14 \end{array} \quad \begin{array}{r} 8.2 \\ 18 \end{array} \quad \begin{array}{r} 8.6 \\ 39 \end{array} \quad \begin{array}{r} 9.6 \\ 50 \end{array}$$

$$\begin{array}{r} 15.2 \\ 50 \end{array} \quad \begin{array}{r} 15.0 \\ 24 \end{array} \quad \begin{array}{r} 7.8 \\ 13 \end{array} \quad \begin{array}{r} 7.7 \\ 7 \end{array} \quad \begin{array}{r} 9.3 \\ 12 \end{array} \quad \begin{array}{r} 8.5 \\ 21 \end{array} \quad \begin{array}{r} 15.0 \\ 21 \end{array} \quad \begin{array}{r} 17.0 \\ 27 \end{array} \quad \begin{array}{r} 17.5 \\ 50 \end{array}$$

Sta	+	π	-	Elev.
		980.16		
67+50			9.2	79.0
68			10.0	78.2
+03	15" $\pm$ Curb			
+50			10.0	78.2
69			9.2	79.0
T.P.	13.29	992.28	9.17	978.99
+50			12.0	80.3
70			10.5	81.8
+75			8.6	83.7
71			8.2	84.1
+56			8.0	84.3
B.M.			8.40	983.88
72			8.2	84.1
+50			9.4	82.9

983.84.

$$\begin{array}{r} 19.7 \\ 50 \end{array} \quad \begin{array}{r} 19.5 \\ 31 \end{array} \quad \begin{array}{r} 9.5 \\ 14 \end{array} \quad 9.2 \quad \begin{array}{r} 10.0 \\ 11 \end{array} \quad \begin{array}{r} 19.3 \\ 25 \end{array} \quad \begin{array}{r} 20.5 \\ 34 \end{array} \quad \begin{array}{r} 20.5 \\ 50 \end{array}$$

$$\begin{array}{r} 21.0 \\ 50 \end{array} \quad \begin{array}{r} 19.0 \\ 29 \end{array} \quad \begin{array}{r} 17.5 \\ 22 \end{array} \quad \begin{array}{r} 10.4 \\ 13 \end{array} \quad 10.0 \quad \begin{array}{r} 10.8 \\ 11 \end{array} \quad \begin{array}{r} 19.5 \\ 24 \end{array} \quad \begin{array}{r} 21.4 \\ 30 \end{array} \quad \begin{array}{r} 21.5 \\ 50 \end{array}$$

$$\begin{array}{r} 21.7 \\ 200 \end{array} \quad \begin{array}{r} 21.5 \\ 150 \end{array} \quad \begin{array}{r} 21.7 \\ 100 \end{array} \quad \begin{array}{r} 21.5 \\ 50 \end{array} \quad \begin{array}{r} 22.7 \\ 32 \end{array} \quad 65.5$$

$$\begin{array}{r} 22.2 \\ 30 \end{array} \quad 66.0$$

$$\begin{array}{r} 28.0 \\ 50 \end{array} \quad \begin{array}{r} 19.5 \\ 37 \end{array} \quad \begin{array}{r} 18.5 \\ 29 \end{array} \quad \begin{array}{r} 10.3 \\ 13 \end{array} \quad 10.0 \quad \begin{array}{r} 10.6 \\ 12 \end{array} \quad \begin{array}{r} 19.7 \\ 26 \end{array} \quad \begin{array}{r} 21.3 \\ 39 \end{array} \quad 21$$

$$\begin{array}{r} 17.8 \\ 50 \end{array} \quad \begin{array}{r} 17.1 \\ 29 \end{array} \quad \begin{array}{r} 15.4 \\ 23 \end{array} \quad \begin{array}{r} 9.7 \\ 14 \end{array} \quad 9.2 \quad \begin{array}{r} 9.8 \\ 10 \end{array} \quad \begin{array}{r} 15.7 \\ 22 \end{array} \quad \begin{array}{r} 19.5 \\ 29 \end{array} \quad \begin{array}{r} 18.6 \\ 50 \end{array}$$

$$\begin{array}{r} 17.8 \\ 50 \end{array} \quad \begin{array}{r} 15.1 \\ 22 \end{array} \quad \begin{array}{r} 12.8 \\ 16 \end{array} \quad \begin{array}{r} 12.4 \\ 13 \end{array} \quad 12.0 \quad \begin{array}{r} 12.1 \\ 6 \end{array} \quad \begin{array}{r} 12.3 \\ 10 \end{array} \quad \begin{array}{r} 9.7 \\ 16 \end{array} \quad \begin{array}{r} 11.4 \\ 40 \end{array} \quad \begin{array}{r} 11.5 \\ 50 \end{array}$$

$$\begin{array}{r} 13.2 \\ 50 \end{array} \quad \begin{array}{r} 9.7 \\ 22 \end{array} \quad \begin{array}{r} 11.2 \\ 17 \end{array} \quad \begin{array}{r} 11.1 \\ 13 \end{array} \quad 10.5$$

$$\begin{array}{r} 10.7 \\ 12 \end{array} \quad \begin{array}{r} 4.1 \\ 20 \end{array} \quad \begin{array}{r} 5.9 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 4.8 \\ 24 \end{array} \quad \begin{array}{r} 8.6 \\ 17 \end{array} \quad \begin{array}{r} 9.0 \\ 14 \end{array} \quad 8.6 \quad \begin{array}{r} 9.0 \\ 10 \end{array} \quad \begin{array}{r} 9.4 \\ 14 \end{array} \quad \begin{array}{r} 5.7 \\ 19 \end{array} \quad \begin{array}{r} 7.1 \\ 32 \end{array} \quad \begin{array}{r} 7.8 \\ 50 \end{array}$$

$$\begin{array}{r} 3.3 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 25 \end{array} \quad \begin{array}{r} 8.4 \\ 16 \end{array} \quad \begin{array}{r} 8.4 \\ 11 \end{array} \quad 8.2 \quad \begin{array}{r} 8.7 \\ 10 \end{array} \quad \begin{array}{r} 9.0 \\ 13 \end{array} \quad \begin{array}{r} 5.4 \\ 18 \end{array} \quad \begin{array}{r} 5.9 \\ 24 \end{array} \quad \begin{array}{r} 7.0 \\ 50 \end{array}$$

$$\begin{array}{r} 0.0 \\ 50 \end{array} \quad \begin{array}{r} 0.7 \\ 29 \end{array} \quad \begin{array}{r} 6.1 \\ 19 \end{array} \quad \begin{array}{r} 8.2 \\ 13 \end{array} \quad 8.0 \quad \begin{array}{r} 8.2 \\ 8 \end{array} \quad \begin{array}{r} 8.2 \\ 14 \end{array} \quad \begin{array}{r} 3.8 \\ 20 \end{array} \quad \begin{array}{r} 2.9 \\ 29 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array}$$

Top Man Sta. 71 + 69.10

$$\begin{array}{r} 0.7 \\ 50 \end{array} \quad \begin{array}{r} 0.7 \\ 27 \end{array} \quad \begin{array}{r} 7.4 \\ 17 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \end{array} \quad 8.2$$

$$\begin{array}{r} 8.5 \\ 13 \end{array} \quad \begin{array}{r} 5.2 \\ 19 \end{array} \quad \begin{array}{r} 6.9 \\ 50 \end{array}$$

$$\begin{array}{r} 0.5 \\ 50 \end{array} \quad \begin{array}{r} 5.8 \\ 23 \end{array} \quad \begin{array}{r} 7.4 \\ 20 \end{array} \quad \begin{array}{r} 9.8 \\ 16 \end{array} \quad 9.4 \quad \begin{array}{r} 10.1 \\ 12 \end{array} \quad \begin{array}{r} 7.8 \\ 16 \end{array} \quad \begin{array}{r} 7.8 \\ 23 \end{array} \quad \begin{array}{r} 2.1 \\ 50 \end{array}$$

Sta	+	$\bar{K}$ 92.24 992.28	-	Elev
73			16.9	813.
T.P	0.31	979.73	12.82	979.42.
+50			0.5	79.2

74			2.6	77.1
----	--	--	-----	------

+21 18" Cu/v. ϕ

+50			4.0	75.7.
-----	--	--	-----	-------

75			4.8	74.9.
----	--	--	-----	-------

+50			5.5	74.2.
-----	--	--	-----	-------

76			4.0	73.6.
----	--	--	-----	-------

+31 15" Cu/v. ϕ

+50			5.7	74.0
-----	--	--	-----	------

77			5.3	74.4
----	--	--	-----	------

+50			4.7	75.0
-----	--	--	-----	------

$$\frac{9.4}{50} \frac{8.4}{30} \frac{11.1}{14} \quad 10.9 \quad \frac{11.3}{12} \frac{11.1}{16} \quad \frac{12.2}{37} \frac{11.9}{50}$$

$$\frac{3.2}{50} \frac{2.3}{35} \frac{1.4}{18} \quad \frac{2.0}{15.17} \frac{1.0}{73} \frac{0.9}{8} \quad 0.5 \quad \frac{0.8}{8} \frac{1.1}{13} \quad \frac{3.6}{18} \frac{5.4}{50}$$

$$\frac{8.4}{50} \quad \frac{8.2}{23} \quad \frac{3.0}{12} \quad \frac{2.6}{7} \quad 2.6 \quad \frac{2.9}{12} \quad \frac{3.5}{12} \frac{8.1}{21} \frac{7.9}{50}$$

$$\text{Drainage to N.} \quad \frac{10.6}{21} 69.1 \quad \frac{10.2}{21} 69.5$$

$$\frac{8.8}{50} \frac{9.2}{28} \frac{8.6}{18} \frac{4.6}{11} 4.0 \quad \frac{4.7}{12} \frac{7.7}{20} \frac{6.9}{50}$$

$$\frac{8.4}{50} \frac{7.3}{33} \frac{7.0}{15} \frac{5.5}{12.5} \frac{4.9}{4.8} \quad \frac{5.3}{11} \frac{5.4}{18} \frac{5.0}{27} \frac{4.4}{50}$$

$$\frac{10.9}{50} \frac{10.4}{37} \frac{10.0}{26} \frac{9.0}{18} \frac{6.0}{12} 5.5 \quad \frac{6.2}{14} \frac{7.2}{16} \frac{7.1}{25} \frac{6.0}{50}$$

$$\frac{11.8}{50} \frac{11.2}{25} \frac{10.2}{18} \frac{9.4}{13} \frac{6.7}{11} 6.0 \quad \frac{6.9}{13} \frac{8.4}{18} \frac{8.2}{36} \frac{9.4}{50}$$

$$\frac{11.7}{19} 68.0$$

$$\frac{10.4}{15} 69.3$$

$$\frac{11.1}{50} \frac{11.0}{30} \frac{10.7}{21} \frac{9.7}{16} \frac{6.3}{12} 5.7 \quad \frac{6.7}{14} \frac{8.6}{17} \frac{8.5}{32} \frac{7.3}{50}$$

$$\frac{10.1}{50} \quad \frac{9.7}{25} \quad \frac{9.7}{19} \quad \frac{5.8}{11} \quad 5.3 \quad \frac{6.1}{13} \quad \frac{8.4}{20} \frac{7.4}{50}$$

$$\frac{8.3}{50} \frac{7.8}{21} \frac{7.2}{16} \frac{5.1}{12} 4.7 \quad \frac{5.2}{13} \frac{7.3}{18.20} \frac{7.0}{23} \frac{6.1}{27} \frac{6.4}{50}$$

Sta.	+	π	-	Elev
		979.73		
78			3.9	75.8
+50			3.3	76.4
79			2.3	77.4
T.P.	13.03	990.00	2.76	976.97
+50			11.6	78.4
+85			11.0	79.0
80			10.7	79.3
+50			9.5	80.5
81			8.8	81.2
+50			8.5	81.5
82			8.5	81.5
+50			9.0	81.0
83			9.5	80.5
T.P.	4.80	985.18	9.64	980.36

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 5.8 \\ 24 \end{array} \quad \begin{array}{r} 5.8 \\ 17 \end{array} \quad \begin{array}{r} 4.2 \\ 13 \end{array} \quad 3.9 \quad \begin{array}{r} 4.6 \\ 12 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 6.9 \\ 28 \end{array} \quad \begin{array}{r} 6.2 \\ 30 \end{array} \quad \begin{array}{r} 6.5 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 25 \end{array} \quad \begin{array}{r} 5.6 \\ 15 \end{array} \quad \begin{array}{r} 3.8 \\ 11 \end{array} \quad 3.3 \quad \begin{array}{r} 4.1 \\ 13 \end{array} \quad \begin{array}{r} 6.2 \\ 17 \end{array} \quad \begin{array}{r} 6.8 \\ 21 \end{array} \quad \begin{array}{r} 6.9 \\ 50 \end{array}$$

$$\begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 4.2 \\ 21 \end{array} \quad \begin{array}{r} 3.7 \\ 15 \end{array} \quad \begin{array}{r} 2.9 \\ 9 \end{array} \quad 2.3 \quad \begin{array}{r} 3.0 \\ 15 \end{array} \quad \begin{array}{r} 6.5 \\ 20 \end{array} \quad \begin{array}{r} 6.1 \\ 50 \end{array}$$

$$\begin{array}{r} 8.3 \\ 50 \end{array} \quad \begin{array}{r} 9.5 \\ 27 \end{array} \quad \begin{array}{r} 1.5 \\ 18 \end{array} \quad \begin{array}{r} 12.2 \\ 13 \end{array} \quad \begin{array}{r} 11.9 \\ 10 \end{array} \quad 11.6 \quad \begin{array}{r} 11.6 \\ 6 \end{array} \quad \begin{array}{r} 12.0 \\ 13 \end{array} \quad \begin{array}{r} 11.9 \\ 17 \end{array} \quad \begin{array}{r} 11.1 \\ 19 \end{array} \quad \begin{array}{r} 11.7 \\ 23 \end{array} \quad \begin{array}{r} 13.1 \\ 50 \end{array}$$

$$\begin{array}{r} 6.2 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 27 \end{array} \quad \begin{array}{r} 6.0 \\ 22 \end{array} \quad \begin{array}{r} 11.1 \\ 15 \end{array} \quad \begin{array}{r} 11.2 \\ 10 \end{array} \quad 11.0 \quad \begin{array}{r} 11.3 \\ 14 \end{array} \quad \begin{array}{r} 10.3 \\ 17 \end{array} \quad \begin{array}{r} 8.2 \\ 20 \end{array} \quad \begin{array}{r} 8.8 \\ 35 \end{array} \quad \begin{array}{r} 9.8 \\ 50 \end{array}$$

$$\begin{array}{r} 4.6 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 31 \end{array} \quad \begin{array}{r} 5.9 \\ 24 \end{array} \quad \begin{array}{r} 10.9 \\ 15 \end{array} \quad \begin{array}{r} 10.9 \\ 10 \end{array} \quad 10.7 \quad \begin{array}{r} 11.0 \\ 13 \end{array} \quad \begin{array}{r} 10.5 \\ 16 \end{array} \quad \begin{array}{r} 7.7 \\ 20 \end{array} \quad \begin{array}{r} 1.2 \\ 27 \end{array} \quad \begin{array}{r} 8.3 \\ 50 \end{array}$$

$$\begin{array}{r} 2.3 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 24 \end{array} \quad \begin{array}{r} 7.4 \\ 15 \end{array} \quad \begin{array}{r} 9.8 \\ 11 \end{array} \quad 9.5 \quad \begin{array}{r} 9.5 \\ 7 \end{array} \quad \begin{array}{r} 9.9 \\ 15 \end{array} \quad \begin{array}{r} 5.7 \\ 21 \end{array} \quad \begin{array}{r} 5.8 \\ 50 \end{array}$$

$$\begin{array}{r} 3.2 \\ 50 \end{array} \quad \begin{array}{r} 3.9 \\ 24 \end{array} \quad \begin{array}{r} 7.2 \\ 20 \end{array} \quad \begin{array}{r} 7.2 \\ 7 \end{array} \quad 8.8 \quad \begin{array}{r} 7.2 \\ 14 \end{array} \quad \begin{array}{r} 8.7 \\ 16 \end{array} \quad \begin{array}{r} 4.7 \\ 22 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 5.3 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 20 \end{array} \quad \begin{array}{r} 7.4 \\ 17 \end{array} \quad \begin{array}{r} 8.9 \\ 13 \end{array} \quad 8.5 \quad \begin{array}{r} 8.6 \\ 9 \end{array} \quad \begin{array}{r} 9.1 \\ 16 \end{array} \quad \begin{array}{r} 6.2 \\ 21 \end{array} \quad \begin{array}{r} 5.8 \\ 50 \end{array}$$

$$\begin{array}{r} 7.5 \\ 50 \end{array} \quad \begin{array}{r} 7.1 \\ 20 \end{array} \quad \begin{array}{r} 9.0 \\ 17 \end{array} \quad \begin{array}{r} 8.9 \\ 12 \end{array} \quad 8.5 \quad \begin{array}{r} 8.5 \\ 7 \end{array} \quad \begin{array}{r} 9.0 \\ 16 \end{array} \quad \begin{array}{r} 7.4 \\ 20 \end{array} \quad \begin{array}{r} 7.6 \\ 50 \end{array}$$

$$\begin{array}{r} 10.5 \\ 50 \end{array} \quad \begin{array}{r} 9.8 \\ 22 \end{array} \quad \begin{array}{r} 9.5 \\ 17 \end{array} \quad \begin{array}{r} 9.5 \\ 12 \end{array} \quad \begin{array}{r} 9.5 \\ 10 \end{array} \quad 9.0 \quad \begin{array}{r} 9.3 \\ 18 \end{array} \quad \begin{array}{r} 10.2 \\ 22 \end{array} \quad \begin{array}{r} 9.8 \\ 26 \end{array} \quad \begin{array}{r} 9.8 \\ 50 \end{array}$$

$$\begin{array}{r} 12.6 \\ 50 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array} \quad \begin{array}{r} 10.0 \\ 14 \end{array} \quad 9.5 \quad \begin{array}{r} 10.0 \\ 16 \end{array} \quad \begin{array}{r} 11.8 \\ 21 \end{array} \quad \begin{array}{r} 11.8 \\ 23 \end{array} \quad \begin{array}{r} 11.4 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.
		985.16		
83+50			5.4	79.8
+ 64	12' x 34' d	Cal/v.		
84			5.6	79.6
+ 60			4.8	80.4
+ 75			4.6	80.6
+ 80			4.5	80.7
+ 95			4.2	81.0
B. M.			4.22	980.94 980.95

8.3	8.4	8.2	6.1		5.7	8.0	7.0
<u>50</u>	<u>23</u>	<u>17</u>	<u>12</u>	<u>5.4</u>	<u>17</u>	<u>21</u>	<u>50</u>

drainage is No. 8.7 76.5 8.6 76.6.

6.9	7.1	7.5	5.7		5.6	6.7	7.1	6.4	5.7
<u>50</u>	<u>30</u>	<u>17</u>	<u>12</u>	<u>5.6</u>	<u>13</u>	<u>17</u>	<u>25</u>	<u>36</u>	<u>50</u>

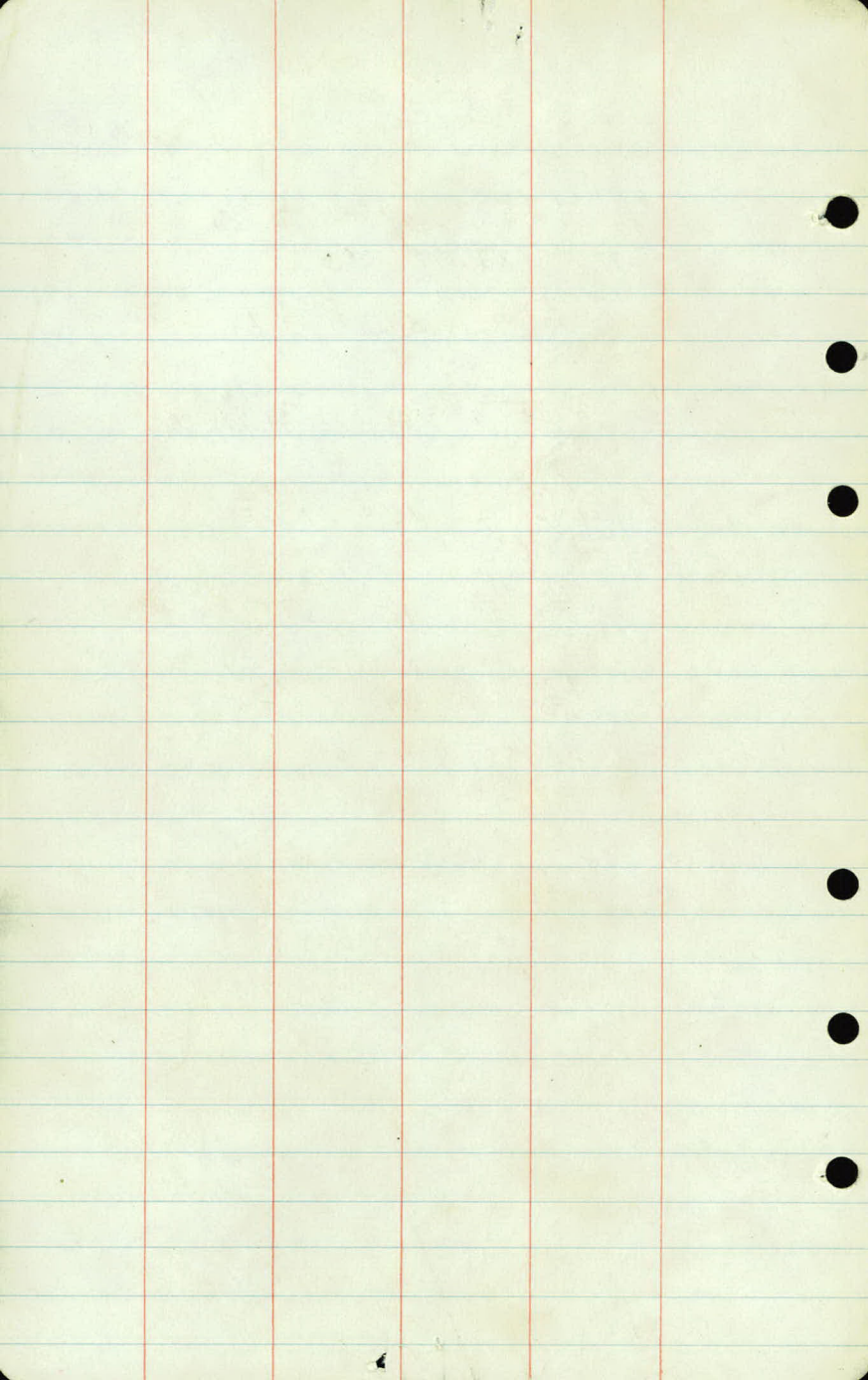
4.0	4.5	<u>6.6</u>	<u>5.6</u>		4.9	<u>5.9</u>	4.3	3.2
<u>50</u>	<u>25</u>	<u>18-15</u>	<u>13</u>	<u>4.8</u>	<u>13</u>	<u>18-24</u>	<u>29</u>	<u>50</u>

6.4	6.4	4.9			4.8	5.8	5.8
<u>50</u>	<u>24</u>	<u>16</u>			<u>4.6</u>	<u>21</u>	<u>27</u>
							<u>50</u>

4.6	4.8		4.5	4.0
<u>50</u>	<u>23</u>	4.5	<u>19</u>	<u>50</u>

4.0		4.2	4.0
<u>50</u>			<u>50</u>

Top spike 84. + 95-



8/39

Slope Stakes

Co Rd "F"

Hamline to Victoria

Sta	+	X	-	Elev	Grade Rod
-----	---	---	---	------	-----------

B.M.	3.75	957.47		953.72	
------	------	--------	--	--------	--

	7.55	964.85	0.17	957.30	
--	------	--------	------	--------	--

	13.15	977.85	0.15	964.70	
--	-------	--------	------	--------	--

	11.34	988.78	0.41	977.44	
--	-------	--------	------	--------	--

B.M	5.26	988.78	5.26	983.52	
-----	------	--------	------	--------	--

19+31				83.4	5.4
-------	--	--	--	------	-----

+50				83.5	5.3
-----	--	--	--	------	-----

T.P	10.91	994.72	4.97	983.81	
-----	-------	--------	------	--------	--

20				83.6	11.1
----	--	--	--	------	------

+50				83.6	11.1
-----	--	--	--	------	------

21				83.4	11.3
----	--	--	--	------	------

+50				83.0	11.7
-----	--	--	--	------	------

T.P	8.25	992.10	10.87	983.85	
-----	------	--------	-------	--------	--

22				82.4	9.7
----	--	--	--	------	-----

+50				81.6	10.5
-----	--	--	--	------	------

23				80.6	11.5
----	--	--	--	------	------

T.P	3.90	985.11	10.89	981.21	
-----	------	--------	-------	--------	--

+50				79.5	5.6
-----	--	--	--	------	-----

Cut 2.1

Ditch
1.6

Fill

3.1

23.5

26.5

Lt

X

Rt

Sph in 12" oak 35' Rt Sta 7465

Top of Mount F&H Hamline

	5.1 C03	4.9 C0.5 77.5
0.7 C4.6 33.0	5.1 C0.2	4.0 C1.3 29.1 9.1
4.7 C6.4 33.0	10.9 C0.2	C2.9 30.5
7.4 C3.7 33	10.8 C03	13.5 F2.4 22.2
9.7 01.6 29.7	10.7 C0.6	13.2 F1.9 20.7
9.5 C2.2 30.9	10.6 C1.1	11.7 C0.0 26.2
5.4 C4.3 33.0	8.2 C1.5	L.0 C3.7 33.0
5.0 C5.5 33.0	8.7 C1.8	6.3 C4.2 33.0
5.5 C6.0 33.0	9.8 C1.7	8.1 C3.4 33.0
7.6 C3.0 32.5	4.4 C1.2	3.4 C2.2 30.9

Sta	+	π	-	Elev	Grade Rid
		985.11			
24				78.1	7.0
+50				76.6	8.5
+75				75.7	9.4
25				74.8	10.3
T.P.	3.19	975.49	12.81	972.30	
+50				73.0	2.5
26				71.1	4.4
+50				69.3	6.2
27				67.6	7.9
T.P.	2.57	968.87	9.19	966.30	
+50				66.4	2.5
28				65.6	3.3
+50				65.3	3.6
29				65.1	3.8

L+

X

A+

$$\begin{array}{r} 5.4 \\ C1.6 \\ \hline 29.7 \end{array}$$

$$\begin{array}{r} L8 \\ C1.7 \\ \hline 29.9 \end{array}$$

$$\begin{array}{r} 9.8 \\ D1.1 \\ \hline 25.7 \end{array}$$

$$\begin{array}{r} 11.5 \\ D0.3 \\ \hline 24.1 \end{array}$$

$$\begin{array}{r} 5.1 \\ F2.6 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ D3.0 \\ \hline 19.9 \end{array}$$

$$\begin{array}{r} 7.6 \\ D0.1 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} 9.0 \\ D0.4 \\ \hline 24.3 \end{array}$$

$$\begin{array}{r} 3.6 \\ D0.4 \\ \hline 24.3 \end{array}$$

$$\begin{array}{r} 4.4 \\ D0.4 \\ \hline 24.3 \end{array}$$

$$\begin{array}{r} 4.4 \\ D0.7 \\ \hline 24.9 \end{array}$$

$$\begin{array}{r} 5.2 \\ D0.1 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} L2 \\ C0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 8.3 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 9.4 \\ C2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 10.5 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 2.8 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ F0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 3.4 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.3 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ C2.0 \\ \hline 30.5 \end{array}$$

$$\begin{array}{r} 5.0 \\ C3.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ C4.0 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 7.5 \\ C2.8 \\ \hline 32.1 \end{array}$$

$$\begin{array}{r} 4.5 \\ F2.0 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 8.4 \\ F4.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 11.9 \\ F5.7 \\ \hline 32.1 \end{array}$$

$$\begin{array}{r} 14.7 \\ F6.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.2 \\ F6.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 7.2 \\ F3.9 \\ \hline 26.9 \end{array}$$

$$\begin{array}{r} 5.6 \\ F2.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 6.9 \\ F3.1 \\ \hline 24.3 \end{array}$$

11.9

D. 4.0

4.4
5.96.2
7.77.9
9.42.5
4.03.3
4.83.6
5.13.8
5.3

Sta	+	π	-	Elev	Grade Rod
		968.87			
29+50				65.0	3.9
30				65.0	3.9
+50				65.2	3.7
B.M	7.50	973.32	3.04	965.83	965.82
31				65.6	7.7
+50				66.3	7.0
32				67.0	6.3
+50				67.7	5.6
T.P	10.05	978.15	5.21	968.11	
+75				67.9	10.3
33				68.0	10.2
+50				68.1	10.1
34				67.8	10.4
+50				67.3	10.9

Lt

R

Rt

3.9
5.48.0
F4.1
2734.6
F0.79.1
F5.2
30.63.9
6.48.3
F4.4
28.24.7
F0.88.2
F4.3
27.93.7
5.27.9
F4.2
27.44.1
F0.48.3
F4.6
28.9

Spk 14 30" Oak 35" Rt 54 30" 190

10.5
F2.8
23.47.9
F0.210.8
F3.1
24.3

8.5

9.9
F2.9
23.74.7
F0.24.7
C2.3
31.19.1
F2.8
23.46.5
F0.38.6
F2.3
21.97.9
F2.3
21.95.8
F0.26.7
C0.4
24.311.6
C0.2
23.910.3
C0.09.5
C0.2
27.99.4
C0.8
27.99.8
C0.47.7
C2.5
21.55.6
C4.5
32.09.4
C0.75.7
C4.4
33.06.7
C3.7
3310.2
C0.26.6
C3.8
3311.2
C1.2
26.911.2
F0.39.5
C1.4
27.3

Sta	+	π	-	Elev	Grade Road
		978.15			

35				66.5	11.7
----	--	--	--	------	------

T.P.	4.23	970.83	11.55	966.60	
------	------	--------	-------	--------	--

+38				65.6	5.2
-----	--	--	--	------	-----

36				64.6	6.2
----	--	--	--	------	-----

+48				63.3	7.5
-----	--	--	--	------	-----

37				62.7	8.1
----	--	--	--	------	-----

B.M	6.63	970.83	6.63	964.22	
-----	------	--------	------	--------	--

+62				61.5	9.3
-----	--	--	--	------	-----

T.P.	5.81	967.15	9.49	961.34	
------	------	--------	------	--------	--

38				60.8	6.4
----	--	--	--	------	-----

+71				59.5	7.7
-----	--	--	--	------	-----

39				58.9	8.3
----	--	--	--	------	-----

+25				58.4	8.8
-----	--	--	--	------	-----

+50				58.0	9.2
-----	--	--	--	------	-----

40				57.2	10.0
----	--	--	--	------	------

T.P	9.15	965.91	10.59	956.56	
-----	------	--------	-------	--------	--

Lt

R

Rt

16.1
F5.4
31.2

12.1
F0.4

9.9
C1.8
30.1

10.4
F5.2
30.6

5.3
F0.1

5.3
D01.4
26.3

9.4
F3.2
24.6

6.2
C0.0

6.4
D01.3
22.7

9.0
9.7
F2.2
21.6

7.8
F0.3

9.0
D00.0
25.3

9.6
9.6
C0.5
22.5

8.4
F0.3

8.9
D00.7
24.9

SpK 17 30' Oak 100' Rf 5/4 37+20

10.8
8.6
C0.7
27.9

9.5
F0.2

10.3
D00.5
24.9

7.9
9.6
F3.2
24.6

6.8
F0.4

7.9
D00.0
24.5

9.7
13.7
F5.2
31.0

8.5
F0.8

9.0
D00.2
23.9

9.8
12.9
F4.6
28.8

9.1
F0.8

9.6
D00.2
23.9

10.3
11.9
F3.1
24.3

9.5
F0.7

9.7
D00.2
24.7

10.7
12.6
F3.4
25.2

10.0
F0.8

10.4
D00.3
24.1

11.5
13.3
F3.3
24.9

10.4
F0.4

11.5
D00.0
24.9

Topog Sta 44 11 Sta 40+00

Sta	+	X	-	Elev	Grade Rod
		965.71			
40+67				57.0	8.7
41				57.2	8.5
+24				57.5	8.4
+50				57.9	7.8
42				58.8	6.5
+50				59.7	6.0
43				60.7	5.0
+50				61.6	4.1
44				62.5	3.2
T.P.	8.20	971.06	2.85	962.86	
+50				63.4	7.7
45				64.3	6.8
+15				64.6	
B.M.	5.80	971.10	5.80	965.26	(965.30)

Lt

L

Rt

8.7
1011.2
F2.4
22.48.8
F0.113.8
F5.1
30.3

8.5

11.5
F3.0
24.38.3
C0.211.4
F2.9
23.78.4
9.911.5
F3.1
24.38.1
C0.39.9
DC0.0
20.17.8
9.311.0
F3.2
24.27.3
C0.59.0
DC0.3
24.16.9
8.48.4
DC0.0
27.46.3
C0.67.7
DC0.7
24.96.0
7.57.5
F1.9
20.75.7
C0.58.9
F2.7
23.15.0
6.57.5
F2.5
22.54.8
C0.29.0
F4.0
27.04.1
5.66.7
F2.6
22.63.9
C0.28.1
F4.0
27.03.2
4.76.0
F2.8
23.42.8
C0.44.8
DC0.1
23.77.7
9.29.9
F2.2
21.67.3
C0.47.2
C0.2
27.56.8
8.37.4
DC0.7
24.96.5
C0.37.8
DC0.5
24.5

Top of Mont Lee LF

Sta	+	π	-	Elev	Grade	Roof
		971.10				

45+53

65.3

+59

65.4

5.7

46

66.1

5.0

+50

66.9

4.2

47

67.7

3.4

T.P. 6.79 974.95 294 968.16

+50

68.5

6.5

48

69.3

5.7

+50

70.1

4.9

49

70.9

4.1

+50

71.7

3.3

50

72.5

2.5

T.P. 10.14 982.79 230 972.65

+50

73.3

Lt

£

Rt

5.7 72	4.5 C1.2 <u>289</u>	5.5 C0.2	7.2 D0.0 <u>27.5</u>
5.0 65	4.7 C0.3 <u>27.1</u>	4.8 C0.2	5.7 D0.8 <u>25.1</u>
4.2 5.7	3.4 C0.8 <u>28.1</u>	4.0 C0.2	8.5 F4.3 <u>27.9</u>
3.4 4.9	3.0 C0.4 <u>27.3</u>	3.3 C0.1	7.2 F4.2 <u>27.6</u>
6.5 8.0	5.1 C1.4 <u>29.3</u>	6.4 C0.1	9.6 F3.1 <u>24.3</u>
5.7 72	8.8 F3.1 <u>24.3</u>	6.0 F0.3	9.2 F3.5 <u>26.5</u>
4.9	11.4 F6.3 <u>33.0</u>	5.9 F0.8	11.1 F6.2 <u>33.0</u>
4.1	12.1 F8.0 <u>33.0</u>	5.1 F4.0	11.1 F7.0 <u>33.0</u>
3.3	11.9 F8.6 <u>33.0</u>	4.1 F0.8	6.5 F3.2 <u>24.6</u>
2.5 4.0	11.4 F8.9 <u>33.0</u>	3.0 F0.5	5.4 F2.2 <u>23.7</u>
Na.1 9.5 11.0	in Fc P0.37 147 F6.2 <u>30.6</u>	9.5 C0.0	5.9 C3.6 <u>33.0</u>

Sta	+	π	-	Elev	
		982.79			

50+84				73.8	
-------	--	--	--	------	--

51				74.1	
----	--	--	--	------	--

+66				75.1	
-----	--	--	--	------	--

52				75.7	
----	--	--	--	------	--

+50				76.4	
-----	--	--	--	------	--

+75				76.6	
-----	--	--	--	------	--

53				76.7	
----	--	--	--	------	--

+50				76.6	
-----	--	--	--	------	--

+68				76.5	
-----	--	--	--	------	--

54				76.1	
----	--	--	--	------	--

+63				74.9	
-----	--	--	--	------	--

55				74.2	
----	--	--	--	------	--

T.P.	3.03	972.02	8.80	973.99	
------	------	--------	------	--------	--

G. Rod

Lt

R

RH

$$\begin{array}{r} 7.0 \\ 10.3 \end{array}$$

$$\begin{array}{r} 10.5 \\ 20.0 \\ 20.1 \end{array}$$

$$\begin{array}{r} 8.5 \\ 00.5 \end{array}$$

$$\begin{array}{r} 3.1 \\ 05.9 \\ 33.0 \end{array}$$

$$\begin{array}{r} 8.7 \\ 10.2 \end{array}$$

$$\begin{array}{r} 9.5 \\ 00.7 \\ 24.9 \end{array}$$

$$\begin{array}{r} 8.1 \\ 00.6 \end{array}$$

$$\begin{array}{r} 2.9 \\ 05.8 \\ 33.0 \end{array}$$

$$\begin{array}{r} 7.7 \\ 9.5 \end{array}$$

$$\begin{array}{r} 6.1 \\ 01.2 \\ 29.7 \end{array}$$

$$\begin{array}{r} 7.0 \\ 00.7 \end{array}$$

$$\begin{array}{r} 8.8 \\ 00.2 \\ 24.9 \end{array}$$

$$\begin{array}{r} 7.1 \\ 8.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ 02.3 \\ 31.1 \end{array}$$

$$\begin{array}{r} 6.6 \\ 00.5 \end{array}$$

$$\begin{array}{r} 8.1 \\ 00.0 \\ 24.5 \end{array}$$

$$\begin{array}{r} 6.4 \\ 7.9 \end{array}$$

$$\begin{array}{r} 2.8 \\ 03.1 \\ 33.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ 00.2 \end{array}$$

$$\begin{array}{r} 3.2 \\ 03.2 \\ 32.9 \end{array}$$

$$\begin{array}{r} 6.2 \\ 7.7 \end{array}$$

$$\begin{array}{r} 2.9 \\ 03.3 \\ 33.0 \end{array}$$

$$\begin{array}{r} 6.1 \\ 00.1 \end{array}$$

$$\begin{array}{r} 1.0 \\ 05.2 \\ 33.0 \end{array}$$

$$\begin{array}{r} 6.1 \\ 7.6 \end{array}$$

$$\begin{array}{r} 3.2 \\ 02.3 \\ 32.3 \end{array}$$

$$\begin{array}{r} 6.1 \\ 00.0 \end{array}$$

$$\begin{array}{r} 1.8 \\ 04.3 \\ 33.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ 7.7 \end{array}$$

$$\begin{array}{r} 3.4 \\ 02.8 \\ 32.1 \end{array}$$

$$\begin{array}{r} 6.6 \\ 00.4 \end{array}$$

$$\begin{array}{r} 4.0 \\ 02.2 \\ 30.9 \end{array}$$

$$\begin{array}{r} 6.3 \\ 7.8 \end{array}$$

$$\begin{array}{r} 4.4 \\ 01.9 \\ 30.3 \end{array}$$

$$\begin{array}{r} 6.7 \\ 00.4 \end{array}$$

$$\begin{array}{r} 3.7 \\ 02.6 \\ 31.7 \end{array}$$

$$\begin{array}{r} 6.7 \\ 8.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ 01.4 \\ 29.3 \end{array}$$

$$\begin{array}{r} 7.1 \\ 00.4 \end{array}$$

$$\begin{array}{r} 5.9 \\ 00.8 \\ 28.1 \end{array}$$

$$\begin{array}{r} 7.9 \\ 9.4 \end{array}$$

$$\begin{array}{r} 5.6 \\ 02.3 \\ 31.1 \end{array}$$

$$\begin{array}{r} 8.0 \\ 00.1 \end{array}$$

$$\begin{array}{r} 7.5 \\ 00.4 \\ 27.3 \end{array}$$

$$\begin{array}{r} 8.4 \\ 10.1 \end{array}$$

$$\begin{array}{r} 9.7 \\ 00.4 \\ 24.3 \end{array}$$

$$\begin{array}{r} 8.8 \\ 00.2 \end{array}$$

$$\begin{array}{r} 8.1 \\ 00.5 \\ 27.5 \end{array}$$

Sta	+	$\bar{A}$	-	Elev	Grade Rod
		977.02			

55+50				73.3	
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56				72.4	
----	--	--	--	------	--

+50				71.8	
-----	--	--	--	------	--

57				71.5	
----	--	--	--	------	--

B.M.	8.03	976.94	8.03	968.99	968.91
+50				71.5	

58				71.9	
----	--	--	--	------	--

+31				72.3	
-----	--	--	--	------	--

+89				73.4	
-----	--	--	--	------	--

T.P.	4.79	980.36	1.37	975.57	
59+12				73.9	

+50				75.0	
-----	--	--	--	------	--

60				76.6	
----	--	--	--	------	--

+50				78.3	
-----	--	--	--	------	--

LT

E

RT

3.5

$$\begin{array}{r} 8.1 \\ F4.6 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 3.8 \\ F0.2 \end{array}$$

$$\begin{array}{r} 7.9 \\ F4.3 \\ \hline 27.9 \end{array}$$

4.5

$$\begin{array}{r} 9.2 \\ F4.7 \\ \hline 29.1 \end{array}$$

$$\begin{array}{r} 4.4 \\ F0.1 \end{array}$$

$$\begin{array}{r} 11.8 \\ F7.3 \\ \hline 33.0 \end{array}$$

5.1

$$\begin{array}{r} 9.4 \\ F0.3 \\ \hline 30.9 \end{array}$$

$$\begin{array}{r} 4.8 \\ C0.3 \end{array}$$

$$\begin{array}{r} 11.2 \\ F6.1 \\ \hline 33.0 \end{array}$$

5.4

$$\begin{array}{r} 8.5 \\ F3.1 \\ \hline 24.3 \end{array}$$

$$\begin{array}{r} 5.2 \\ C0.2 \end{array}$$

$$\begin{array}{r} 10.7 \\ F5.3 \\ \hline 30.9 \end{array}$$

Spk in P.P. 26' RT 54.57 + 2.5

$$\begin{array}{r} 5.4 \\ 6.9 \end{array}$$

$$\begin{array}{r} 6.9 \\ F00.0 \\ \hline 23.5 \end{array}$$

$$\begin{array}{r} 5.1 \\ C0.3 \end{array}$$

$$\begin{array}{r} 9.9 \\ F4.5 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 5.0 \\ 6.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ C0.2 \\ \hline 26.9 \end{array}$$

$$\begin{array}{r} 4.5 \\ C0.5 \end{array}$$

$$\begin{array}{r} 6.5 \\ F00.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ 6.1 \end{array}$$

$$\begin{array}{r} 4.6 \\ F01.5 \\ \hline 26.0 \end{array}$$

$$\begin{array}{r} 3.8 \\ C0.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ F01.4 \\ \hline 26.3 \end{array}$$

$$\begin{array}{r} 3.5 \\ 4.9 \end{array}$$

$$\begin{array}{r} 4.8 \\ F00.1 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} 2.9 \\ C0.6 \end{array}$$

$$\begin{array}{r} 3.1 \\ C0.4 \\ \hline 27.3 \end{array}$$

Nail in T.P

$$\begin{array}{r} 6.5 \\ 8.0 \end{array}$$

$$\begin{array}{r} 9.0 \\ F2.5 \\ \hline 22.9 \end{array}$$

$$\begin{array}{r} 6.1 \\ C0.4 \end{array}$$

$$\begin{array}{r} 8.4 \\ F1.9 \\ \hline 20.7 \end{array}$$

5.4

$$\begin{array}{r} 11.4 \\ F6.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ F0.3 \end{array}$$

$$\begin{array}{r} 12.4 \\ F6.8 \\ \hline 33.0 \end{array}$$

3.8

$$\begin{array}{r} 10.9 \\ F7.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.6 \\ F0.8 \end{array}$$

$$\begin{array}{r} 13.0 \\ F9.2 \\ \hline 33.0 \end{array}$$

2.1

$$\begin{array}{r} 9.6 \\ F7.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 3.0 \\ F0.9 \end{array}$$

$$\begin{array}{r} 12.4 \\ F10.3 \\ \hline 33.0 \end{array}$$

Sta	+	π	-	Elev	Grade Rod
		980.36			

61				80.0	
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+50				81.7	
-----	--	--	--	------	--

T.P.	9.11	989.29	0.18	980.18	
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62				83.4	
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T.P.	11.54	998.26	2.57	986.72	
------	-------	--------	------	--------	--

+50				85.1	
-----	--	--	--	------	--

T.P.	10.39	1007.07	1.58	996.68	
------	-------	---------	------	--------	--

63				86.6	
----	--	--	--	------	--

+50				87.5	
-----	--	--	--	------	--

64				87.9	
----	--	--	--	------	--

+50				87.7	
-----	--	--	--	------	--

65				87.0	
----	--	--	--	------	--

T.P.	0.71	994.92	12.86	994.21	
------	------	--------	-------	--------	--

+50				85.9	
-----	--	--	--	------	--

66				84.1	
----	--	--	--	------	--

T.P.	0.58	984.55	10.95	983.97	
------	------	--------	-------	--------	--

+50				82.1	
-----	--	--	--	------	--

LT

S

RT

00.4

7.6
F0.2
33.0

1.4
F1.0

10.7
F10.3
33.0

+1.3

5.3
F6.4
33

F0.7

8.7
F10.8
33.0

5.9
7.4

7.4
D0.0
26.5

L0
F0.1

12.7
F6.8
33.0

13.2

5.7
C7.5
37.7

12.9
C0.3

11.0
C1.5
29.7

20.5

6.5
C14.0
47.5

C0.7

13.8
C6.7
31.5

19.6

2.9
C16.7
81.0

C0.7

9.5
C10.1
41.7

19.2

43

7.8
C11.4
43.2

C0.7

6.4
C12.8
45.7

19.4

40

10.0
C9.4
40.6

C0.8

10.4
C9.0
40.0

20.1

11.6
C8.5
39.3

19.4
C0.7

12.7
C7.4
37.6

9.0

4.4
C4.6
33.4

8.8
C0.2

7.1
C1.9
30.3

10.8
12.3

10.9
D0.4
26.3

10.7
C0.1

10.6
C0.2
26.9

2.5

7.6
F5.0
30.0

2.4
C0.1

4.8
F2.3
21.9

Sta	+	π	-	Elev	Grade	Part
		984.55				

67				80.2		
----	--	--	--	------	--	--

+50				78.9		
-----	--	--	--	------	--	--

68				78.2		
----	--	--	--	------	--	--

+50				78.3		
-----	--	--	--	------	--	--

69				79.1		
----	--	--	--	------	--	--

+50				80.3		
-----	--	--	--	------	--	--

T.P	9.45	993.30	0.70	983.85		
-----	------	--------	------	--------	--	--

70				81.7		
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+75				83.2		
-----	--	--	--	------	--	--

71				83.5		
----	--	--	--	------	--	--

+56				83.7		
-----	--	--	--	------	--	--

B.M	11.04	994.88	9.45	983.85	983.84	
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72				83.4		
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+50				82.5		
-----	--	--	--	------	--	--

Lt

Z

Rt

4.4

$$\begin{array}{r} 12.5 \\ 8.1 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 13.7 \\ F8.3 \\ \hline 33.0 \end{array}$$

5.7

$$\begin{array}{r} 12.0 \\ F10.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.6 \\ \hline 30.1 \end{array}$$

$$\begin{array}{r} 16.8 \\ F11.1 \\ \hline 33.0 \end{array}$$

6.4

$$\begin{array}{r} 16.9 \\ F10.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 1.5 \\ \hline 30.1 \end{array}$$

$$\begin{array}{r} 18.5 \\ F12.1 \\ \hline 33.0 \end{array}$$

6.3

$$\begin{array}{r} 16.0 \\ F9.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 1.4 \\ \hline 30.1 \end{array}$$

$$\begin{array}{r} 17.5 \\ F11.1 \\ \hline 33.0 \end{array}$$

5.5

$$\begin{array}{r} 13.7 \\ F8.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.6 \\ \hline 30.1 \end{array}$$

$$\begin{array}{r} 14.0 \\ F8.5 \\ \hline 33.0 \end{array}$$
4.3₅₈

$$\begin{array}{r} 7.7 \\ F3.6 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 4.3 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 2.8 \\ C1.9 \\ \hline 33.0 \end{array}$$

11.6

$$\begin{array}{r} 12.0 \\ C6.1 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.5 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 1.0 \\ C5.2 \\ \hline 33.0 \end{array}$$

10.1

$$\begin{array}{r} 6.3 \\ C3.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.7 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 8.1 \\ C2.0 \\ \hline 30.5 \end{array}$$

9.8

$$\begin{array}{r} 4.9 \\ C4.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.4 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 7.2 \\ C2.6 \\ \hline 31.7 \end{array}$$

9.6

$$\begin{array}{r} 2.1 \\ C1.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.1 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 4.3 \\ C5.3 \\ \hline 33.0 \end{array}$$

Top of

Mount 71 + 69.10

11.5

$$\begin{array}{r} 3.8 \\ C7.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 10.9 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 8.5 \\ C3.0 \\ \hline 32.5 \end{array}$$

12.4

$$\begin{array}{r} 8.8 \\ C3.6 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 12.1 \\ \hline 30.3 \end{array}$$

$$\begin{array}{r} 10.8 \\ C1.4 \\ \hline 29.7 \end{array}$$

Sta	+	Σ	-	Elev	Grade Rod
		994.88			

73				81.2	
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T.P.	1.57	982.73	13.72	981.16	
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+50				79.7	
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74				78.1	
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T.P.	4.47	979.00	8.20	974.53	
------	------	--------	------	--------	--

+50				76.6	
-----	--	--	--	------	--

75				75.3	
----	--	--	--	------	--

+50				74.3	
-----	--	--	--	------	--

76				73.8	
----	--	--	--	------	--

+60				73.7	
-----	--	--	--	------	--

77				74.0	
----	--	--	--	------	--

+50				74.8	
-----	--	--	--	------	--

78				75.7	
----	--	--	--	------	--

+50				76.7	
-----	--	--	--	------	--

KT

R

PT

13.7	$\begin{array}{r} 11.5 \\ C22 \\ \hline 30.9 \end{array}$	$\begin{array}{r} 138 \\ F21 \end{array}$	$\begin{array}{r} 145 \\ C207 \\ \hline 249 \end{array}$
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3.045	$\begin{array}{r} 4.6 \\ C209 \\ \hline 23.6 \end{array}$	$\begin{array}{r} 36 \\ F20.6 \end{array}$	$\begin{array}{r} 7.8 \\ F48 \\ \hline 294 \end{array}$
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4.6	$\begin{array}{r} 11.8 \\ F22 \\ \hline 330 \end{array}$	$\begin{array}{r} 56 \\ F1.8 \end{array}$	$\begin{array}{r} 11.6 \\ F2.0 \\ \hline 33.0 \end{array}$
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24	$\begin{array}{r} 8.7 \\ F23 \\ \hline 33.2 \end{array}$	$\begin{array}{r} 33 \\ F0.9 \end{array}$	$\begin{array}{r} 24 \\ F5.0 \\ \hline 300 \end{array}$
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3.75V	$\begin{array}{r} 6.7 \\ F30 \\ \hline 24.0 \end{array}$	$\begin{array}{r} 41 \\ F0.4 \end{array}$	$\begin{array}{r} 47 \\ C207 \\ \hline 245 \end{array}$
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4.7	$\begin{array}{r} 9.7 \\ F5.0 \\ \hline 30.0 \end{array}$	$\begin{array}{r} 4.9 \\ F0.2 \end{array}$	$\begin{array}{r} 6.6 \\ F19 \\ \hline 20.7 \end{array}$
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5.2	$\begin{array}{r} 11.2 \\ F2.0 \\ \hline 32.0 \end{array}$	$\begin{array}{r} 5.3 \\ F0.1 \end{array}$	$\begin{array}{r} 8.1 \\ F2.9 \\ \hline 23.7 \end{array}$
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5.3	$\begin{array}{r} 10.7 \\ F6.4 \\ \hline 31.2 \end{array}$	$\begin{array}{r} 5.1 \\ C0.2 \end{array}$	$\begin{array}{r} 8.4 \\ F31 \\ \hline 243 \end{array}$
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5.0	$\begin{array}{r} 9.1 \\ F4.1 \\ \hline 27.3 \end{array}$	$\begin{array}{r} 4.6 \\ C0.4 \end{array}$	$\begin{array}{r} 8.1 \\ F31 \\ \hline 243 \end{array}$
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4.2	$\begin{array}{r} 7.5 \\ F3.3 \\ \hline 24.5 \end{array}$	$\begin{array}{r} 4.0 \\ C0.2 \end{array}$	$\begin{array}{r} 6.5 \\ F23 \\ \hline 21.9 \end{array}$
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3.3	$\begin{array}{r} 5.2 \\ F1.9 \\ \hline 20.7 \end{array}$	$\begin{array}{r} 3.2 \\ C0.1 \end{array}$	$\begin{array}{r} 6.3 \\ F30 \\ \hline 24.0 \end{array}$
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2.3	$\begin{array}{r} 5.3 \\ F3.0 \\ \hline 24.0 \end{array}$	$\begin{array}{r} 2.6 \\ F0.3 \end{array}$	$\begin{array}{r} 6.6 \\ F43 \\ \hline 27.9 \end{array}$
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Sta	+	π	-	Elev	Grade Rod
		979.00			

79

77.6

T.P.

12.13

989.56

1.57

977.43

+50

78.6

+85

79.3

80

79.5

+50

80.4

81

80.9

+50

81.2

82

81.2

+50

81.1

83

81.0

+50

80.9

84

80.8

LX

X

PX

1.4

$$\begin{array}{r} 3.8 \\ F2.4 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 1.6 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ F4.0 \\ \hline 27.0 \end{array}$$

11.0₁₂₀

$$\begin{array}{r} 8.4 \\ C2.4 \\ \hline 31.3 \end{array}$$

$$\begin{array}{r} 11.1 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 11.6 \\ D0.9 \\ \hline 25.3 \end{array}$$

10.3

$$\begin{array}{r} 5.5 \\ C4.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 10.6 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 9.2 \\ C2.1 \\ \hline 30.7 \end{array}$$

10.1

$$\begin{array}{r} 5.3 \\ C4.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 10.2 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 7.2 \\ C2.9 \\ \hline 32.3 \end{array}$$

9.2

$$\begin{array}{r} 2.8 \\ C6.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.1 \\ C0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ C4.0 \\ \hline 33.0 \end{array}$$

8.7

$$\begin{array}{r} 3.5 \\ C5.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.3 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ C4.8 \\ \hline 33.0 \end{array}$$

8.4

$$\begin{array}{r} 5.0 \\ C3.6 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.1 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ C3.0 \\ \hline 32.6 \end{array}$$

8.4

$$\begin{array}{r} 7.4 \\ C1.0 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} 8.1 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 7.2 \\ C1.2 \\ \hline 28.9 \end{array}$$

8.5_{10.0}

$$\begin{array}{r} 9.8 \\ D0.2 \\ \hline 27.9 \end{array}$$

$$\begin{array}{r} 8.6 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 9.6 \\ D0.4 \\ \hline 24.3 \end{array}$$

8.6_{10.1}

$$\begin{array}{r} 12.1 \\ F3.5 \\ \hline 26.5 \end{array}$$

$$\begin{array}{r} 9.2 \\ F0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 11.5 \\ F2.9 \\ \hline 23.7 \end{array}$$

8.7_{10.2}

$$\begin{array}{r} 13.2 \\ F4.0 \\ \hline 28.5 \end{array}$$

$$\begin{array}{r} 9.9 \\ F1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 12.2 \\ F3.5 \\ \hline 25.5 \end{array}$$

8.8_{10.3}

$$\begin{array}{r} 11.8 \\ F3.0 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 10.0 \\ F1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 11.5 \\ F2.7 \\ \hline 23.1 \end{array}$$

Sta	+	π	-	Elev	Grade Rod
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989.52

84+60

80.7

+75

80.7

+80

80.7

B.M

8.63

980.93

980.95

LT

~~LT~~

RT

8.9

8.9
101.5
26.5

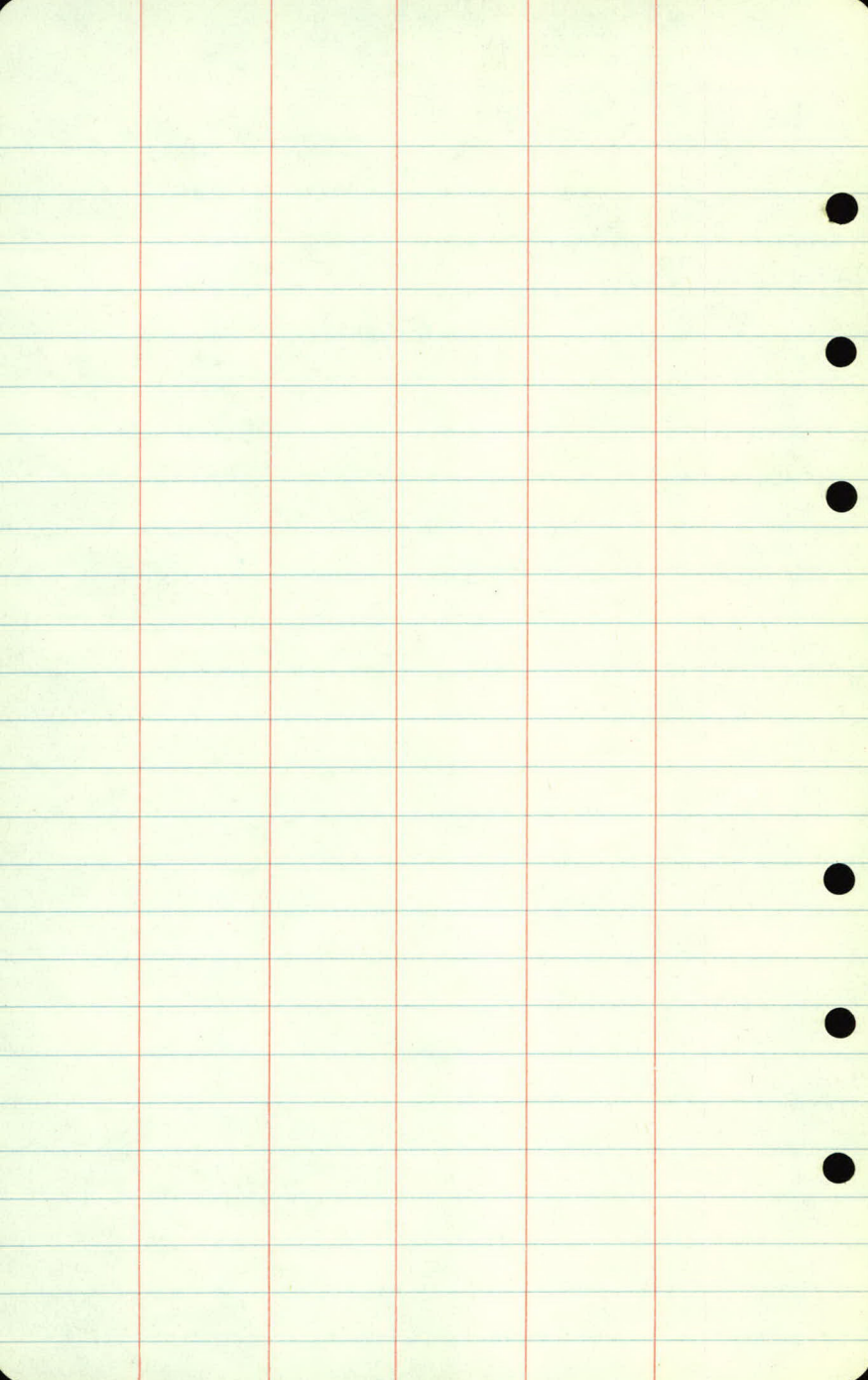
9.2
F0.3

8.9
101.5
26.5

8.9

8.9

Top of Spk. 84+95-

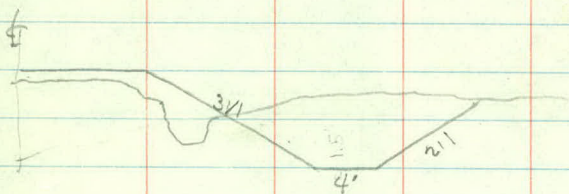


Slope Stakes

Special Ditch

Co. Rd "F"

Sta 76+18 to Sta 78+50 on Rt.



TYPICAL SECTION

Sta

1

G.R.

76+29

9.2

+50

+50

9.0

77

8.5

4.0% Grade

+50

8.0

78

7.5

+50

7.0

79

6.5

$$\begin{array}{r} 8.4 \\ \text{SDC } 0.8 \\ \hline 24.3 \end{array}$$

$$\begin{array}{r} 7.7 \\ \text{SDC } 1.5 \\ \hline 33.7 \end{array}$$

$$\begin{array}{r} 8.4 \\ \text{SDC } 0.6 \\ \hline 24.3 \end{array}$$

$$\begin{array}{r} 7.8 \\ \text{SDC } 1.2 \\ \hline 32.5 \end{array}$$

$$\begin{array}{r} 8.1 \\ \text{SDC } 0.4 \\ \hline 24.3 \end{array}$$

$$\begin{array}{r} 7.6 \\ \text{SDC } 0.9 \\ \hline 31.3 \end{array}$$

$$\begin{array}{r} 6.5 \\ \text{SDC } 1.5 \\ \hline 21.9 \end{array}$$

$$\begin{array}{r} 5.5 \\ \text{SDC } 2.5 \\ \hline 34.4 \end{array}$$

$$\begin{array}{r} 6.3 \\ \text{SDC } 1.2 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 5.5 \\ \text{SDC } 2.0 \\ \hline 35.6 \end{array}$$

$$\begin{array}{r} 6.5 \\ \text{SDC } 0.5 \\ \hline 27.9 \end{array}$$

$$\begin{array}{r} 6.9 \\ \text{SDC } 0.1 \\ \hline 33.6 \end{array}$$

