

K 117

DR. 16

OF

UNTY ENGINEER

SE. CO. MINN.

PLAN

Survey

SAR 'EN TEUR AVENUE

From WEST-COUNTY, MINN. TO HAMLINE AV.

Road Acc't. No. 14

Date Filed 1-31-45

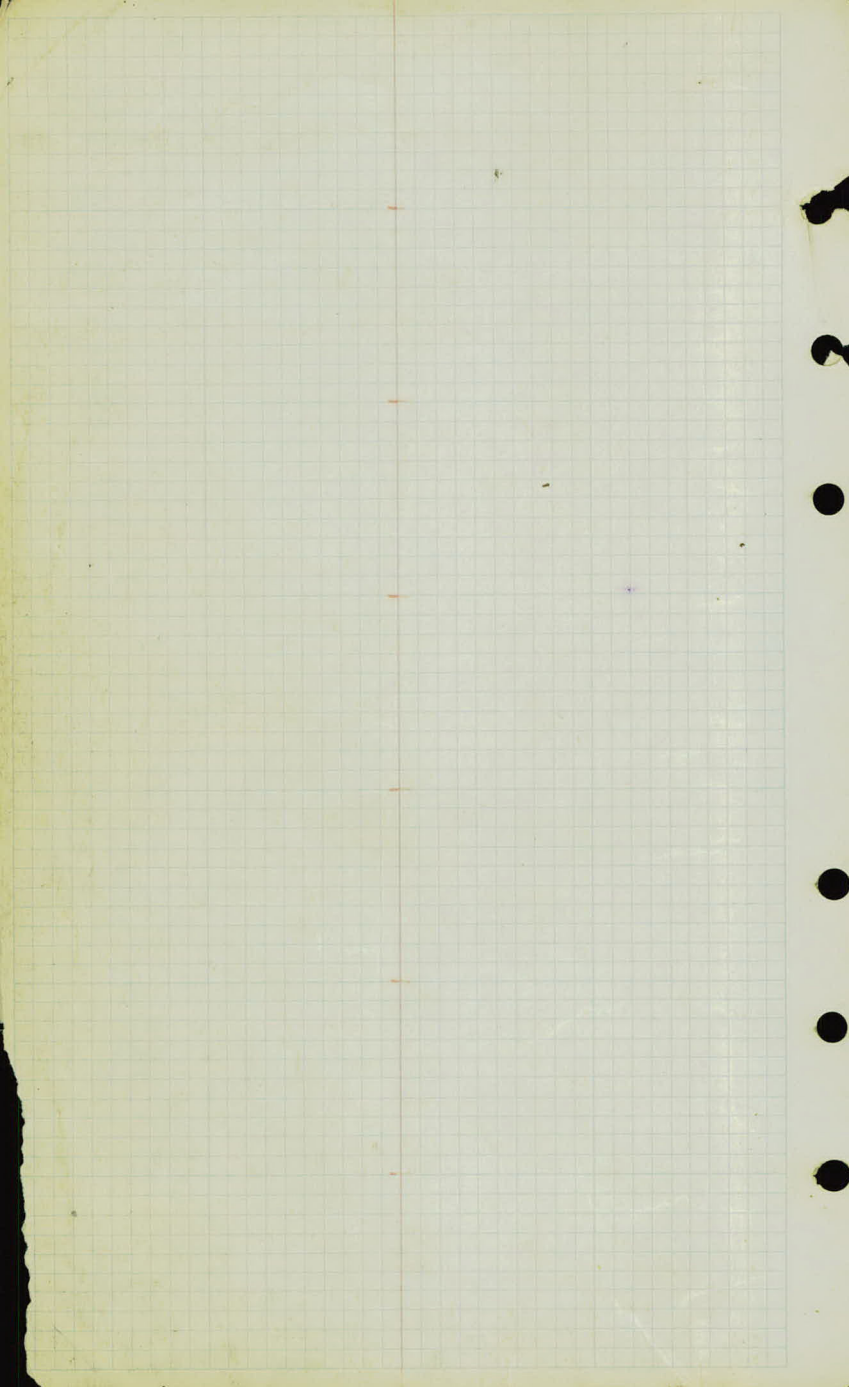
File

PLAN SURVEY
LARPENTEUR AVE.

West County Line to Hamline Ave.

INDEX

Align. - 1-3
Topog. - 4-25
X Sections - 26-87
Bench Levels - 88-91
Borings Sta. 22-92-99
Drainage Levels. 100-164



1
Alignment

Larpenleur Ave
(West Co. Line To Hamline)

Sta	Point	ΔLt	ΔRt
13 + 21.22	P.O.T = E Eustis St. So.		

13 + 11.00	P.O.T = E Eustis St. No.		
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3 + 54.67	P.O.T = E Minn. Transfer Track		
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0 + 00	P.I.		1° 07'
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5-1-44
K.H.
L.C.
C.N.

70°+

Found hole .57' so.
Does not look like
drill hole

Drill Hole

Found drill hole .66' so.

83.34'

49.26'

Found drill .67' so.

13+11.18

Drill
Hole

Found drill hole .67' so.

76.82'

43.25'

Base

Cor.
Fill
Sta.

□ Pumps □

Cor. Bld'g

85° 26'

Mont

Sta	Point	ΔL	ΔR
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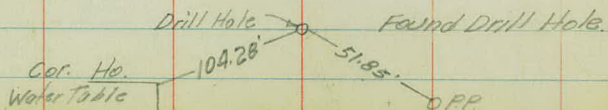
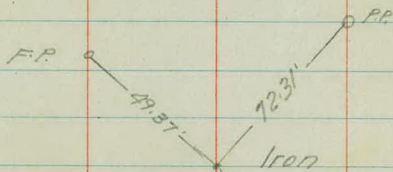
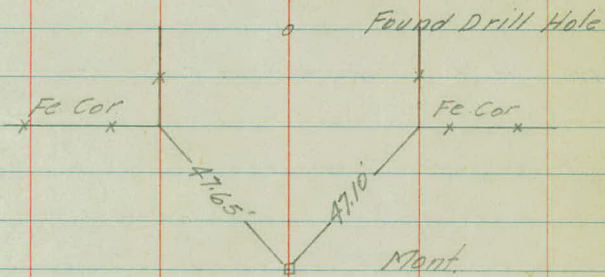
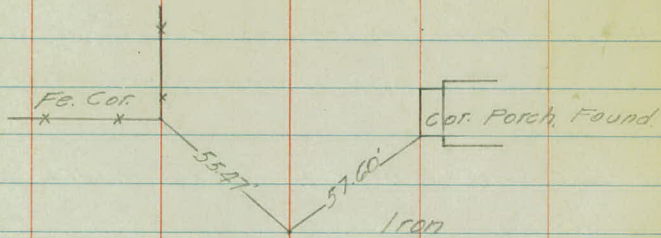
79+07.91	P.I.	0°07'	E New Brighton Rd.
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52+81.83	P.I.	0°09'	E Cleveland Ave
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26+41.78	P.I.	0°01'	E Fulham St.
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¹⁹ 6+19.72	P.O.T.		E Pleasant Ave.
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5-1-94
K.A.
L.C.
C.N.



Sta	Point	ΔL	ΔR
131 + 96.10	P.I.	$0^{\circ}29\frac{1}{2}'$	= $\angle$ Hamline Ave.

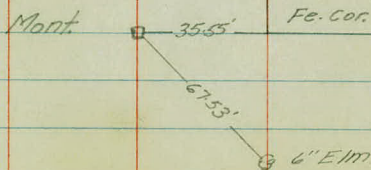
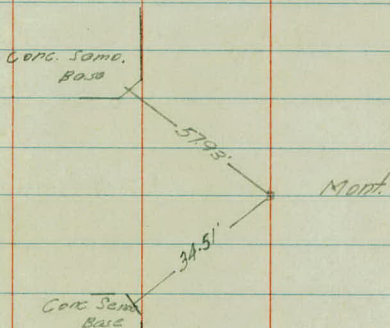
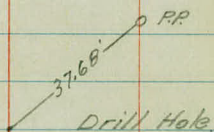
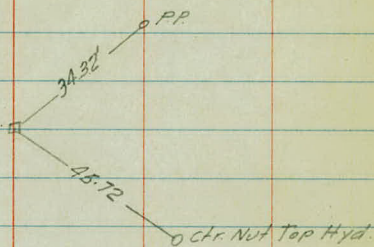
118 + 64.98	P.O.T.	= $\angle$ Pascal Ave.	
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105 + 34.21	P.I.	$0^{\circ}17\frac{1}{2}''$	= $\angle$ Snelling Ave.
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92 + 21.16	P.O.T.		
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S-2-44 70°4
K.H.
L.C.
G.N.

3



Sta.

+

π

-

Elev

Topography

+70-Ent.

+35 M.G.E. M.H. - 34' Cor Bldg 2-77'
+38 Cor. + Face Retain Wall - 35.5'
+20 M.G.E. M.H. - 28.3'

+39 P.R. - 32'
+20 Tol. - M.H. - 26'

1 M.G.E. M.H. - 9'

+87 M.G.E. M.H. - 4'
+57.5 Bdg. + Face / Cong. Wall - 35.8'
+30 PAV - 10' 10'

+52 Cr II Cong. Walk - 33'
+05 M.G.E. Co. M.H. - 2' - 10.5 - 22''
+08 End Curb - 26.5'

+03 M.G.E. Co. M.H. - 14.5'
+06 Edge Pav. - 18'

+01 Cor Pav. - 18.7'

+01 Edge Cong.

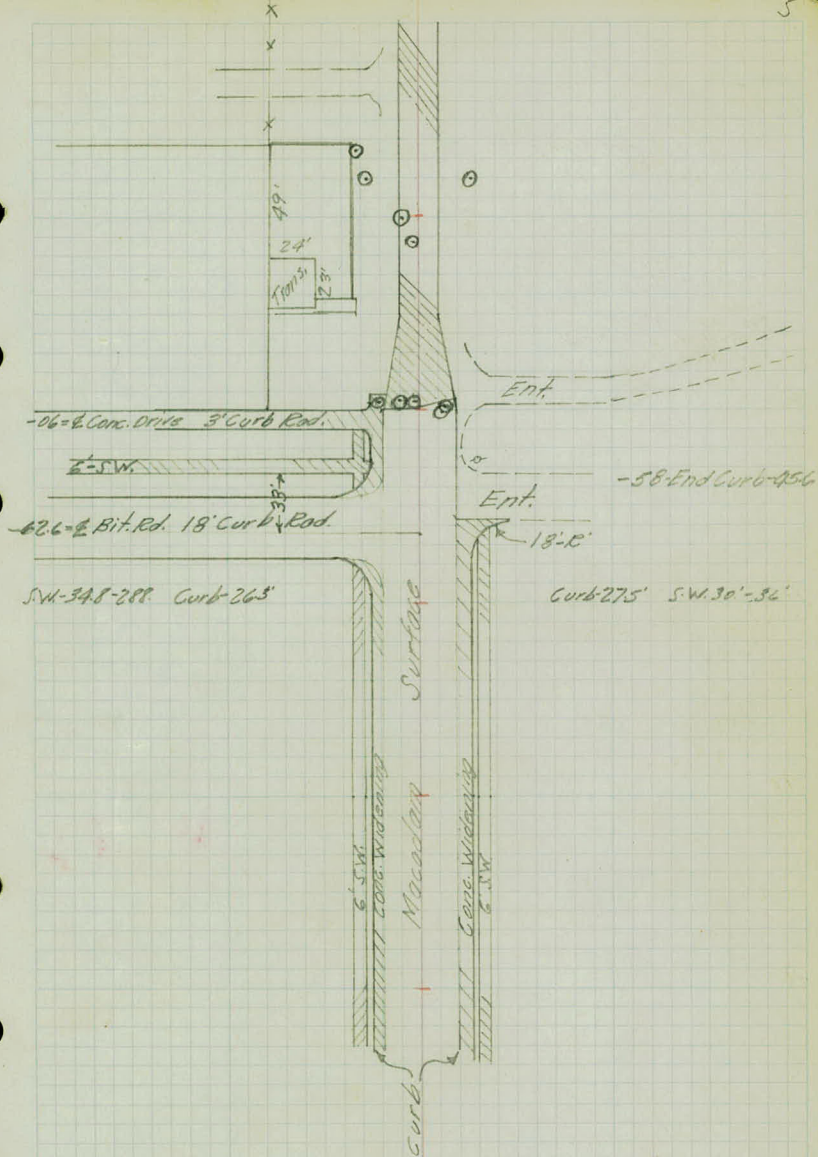
0 +00 Cor Bldg. - 78'

-01 M.G.E. Co. M.H. - 11'

-26 P.R. - 30'

-1-00

-2-00



+84-SW Cor. Poiny Store-45

+57-Cor. Parking Lot-28'

+52-6' Pop-31'-46'

+32-Ctr 4' Conc Walk-23.5

+25-SW Cor. Ho-56'

7 +103-18' Pop-30'

9.7 10.3'

+90-Rd-18'

+81-EN 15' C.M-41'

+75-Rd-45'

+81-PP-32'

+48-Rd-50'

+39-EN 18' C.M-41'

+20-Rd-20'

6

+85-15' O-48'
+80-10' O-45'

+47-PP-32'

5

+25-MGE-M.H.-95' +47-End Widening

+14-T.P.-46'

+25-PP-32'

+12-T.P.-30'-40'

4

184- +97.7-Beg. Pav.-196'
+97.7-Cor Bridge-256 26.8'

+04-T.P.-60'

18.5- +13.3-End Pav.-196'

3 T.P.-46'

+13.3-Cor Bridge-257 26.8'

PP-33'

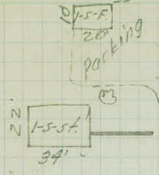
+96-T.P.-39' +93-T.P.-43'

+74-MGE-M.H.-10.5'

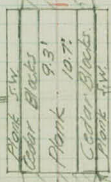
+64-Beg. Widening

2

Walnut St



Curb-18.6'



4' High iron hand rail Rt + Lt.

2' Apr 1' high on curb Rt + Lt.

Curb-19.9'

10' Timber Curb

Cor Nursery - 43'

+83 - Pine Shrub - 27'
 +16 - Pine Shrub - 30'
 +75 - 35
 +73 - Pine Shrub - 39'
 +66 - Cor Nursery - 63'
 +56.5 = 67 Pav - 102.3'
 +38 - End - 18' M - 94
 23/102 34. From E & W of (red)
 +21.22E 24' Buck Rd -

+59 - SW Cor Bldg - 57' Cor SW - 49'
 +45 - Sign Post - 34'
 +43 - 3' Wedge - 59'
 +38 - Ctr 2' S.D. - 32.5'

13 -66 97

+93 - End S.W. 27' = End Slab
 + End Curb - 98' +87 - Cor SW - 26.8'
 +81 - Curb - 177' Cor SW - 33.27'
 +41.5 - Curb - 18' Conc. Slab - 10-17'
 +39 - 800' Curb + SW - 33' +50 - Curb - 379'
 +15 - P.P. - 33' +38 - 800' Curb - 27'
 +103 - N Edge S.W. Slab - 32.5'
 +101 - Slab - 172' - 96'

12 96

+60 - S.W. Cor Taper - 57'
 +56 - Cor Parking Lot - 32'

+30 - SW Cor Ho - 57.5'

+11 - Fe. Cor - 32.5'
 +106 - P' Elm - 36' 9.5
 +13 - 2.3' Conc. Walk - 33'
 +70 - S.W. Cor Ho - 57'
 +68 - Row 144 - 34'
 +67 - Cor Fe - 32.5'
 +65 - End Conc SW - 27.7337'
 +21 - S.W. Cor Bldg - 51'
 +17 - End 12' C.M. - 17' Rod - 14'
 +16 - S.W. Cor G Conc S.W. - 33'
 +100 - Rod - 35' 9.4

10 9.4 10.7

+80 - Cor Slab - 33.6
 +69 - Ctr Gas Pump - 50' Slab - 38.4'
 +53 - Ctr Gas Pump - 46'
 +51 - Cor Slab - 30.7' Slab - 60.3

+27 - N.W. Cor Slab - 30.5'
 +23 - Light Pole - 50' 10.6

+89 - NW Cor Store - 65'
 +71 - P.P. - 32'

+26 - 6 Drive Way - 20'
 +18 - E Edge Drive Way

+84 - 32'
 +70 - Ear - 16'
 +78 - Ctr 4' Conc. Walk - 33'
 +61 - NW Cor Bldg - 70'
 +47 - P.P. - 32'
 +45 - Cor Parking Lot - 20'
 +77 - End 12' C.M. - 21' P. 16'
 +60 - SW Cor 18' P. 16' - 34'
 +39 - S.W. Cor 18' Pillar - 33' } 5' wide Conc. SW
 +14 - 6' Apple Tree - 37'
 +27 - S.W. Cor 18' Pillar - 33'
 +66 - 6' Plum Tree - 50'
 +102 - S.W. Cor 18' Pillar - 33' 9.4 10.7

+39 - Gate Valve - 27'
 +38 - 4' Square Well - 40'

8 Pav 9.3 10.8

Frank -

Locate surface
Drain on corner of
Jarp & Eustis running
N. + S. on East side of
Eustis.

+57 Rd-20

+30 Rd-50

Eustis

Nursery

St

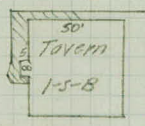
+49 Gas Pst 48.5x50.25
+49 Cor Bldg 61.5'

+1A Slab-61.5'
+01 Wood FC-40'

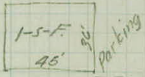
+00 Gate Valve-24.8'

+90 2.3' Walk-31'

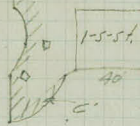
+18 S.W. Cor. Ho.-51'



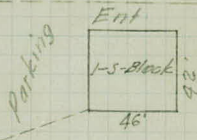
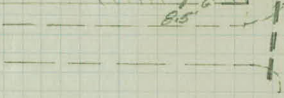
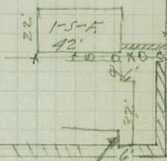
+90 Cor S.W.-23.8'
+67 S.W.-28.8'
+59 S.W.-26.5'
+56 S.W.-29-37.5'



Parking

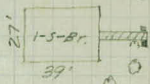


+88 Cir Gas Pump-96'
+69 Light Pole-32'
+54 NW Cor Bldg-65.2'



Parking

Ent



+82-PP-32

+45-End 24" Conc Culv.-25' +99.2-Beg. Pav. +45-End 24" Conc Culv.-30'
 +24-Cor Nursery-48' +99.5-End Pav. +35-E. Masonry Ditch-35'
 +17-End 12" C.M.-29' 18 Long
 +11-End 12" C.M.-46'
 20 9.7 103'
 +98-Rd-43'
 +13-Rd-43'

+51-PP-32'

+34-18" D-40'
 +24-18" D-40' +37-Rd-17'
 +17-8" Pine-23'
 +104-Pine Shrub-22'
 19 9.8 102
 +94-Pine Shrub-22'
 +87-S.W. Cor. Ho-51'
 +84-C Pine-20'
 +113-30" D-38'
 +54-End Hedge-23'
 +38-Cor Hedge-23'
 +07-E 3' Conc Walk-23.5'
 +05-S.W. Cor. Ho.-66'
 +03-E 2' Hedge-23'
 18 9.8 102
 +105-E Masonry Ditch-35'
 Nursery-41'
 +95-Road Ditch Line
 +54-PP-32'

+50-5" Tw Tie-23'
 +12-E 4' Conc Walk-22.2'
 +05-S.W. Cor. Ho.-58'
 +54-E 2' Walk-21.8'
 +36-12" Maple-35'
 +31-12" Maple-36' S.W. Cor. Ho.-51'
 +12-8" Pine-40'
 +05-E 3' Conc Walk-20.6'
 17 9.8 101
 +93-S.W. Cor. Ho.-51'
 +57-PP-32'
 +50-S.W. Post-31'
 +41-Pine Shrub-41'
 +31-Ent
 +20-2 Pine Shrub-42'
 +08-Cor Shrub-23'-30'

186-9' Elm-36'
 +34-4' Tw Elm-34'
 16 9.9 101
 +60-Beg. Row Shrub-23'
 +52-End Hedge-26'
 +23-15' Linden Tr.-22'
 +06-9' Pine-40'
 +95-3' Pine-38' +97-8' Pine-50'
 +80-PP-31' 5' Pines-46'-55'
 +01-Beg. Hedge-25'

+41-15" Tw B.E.-29'
 +20-S.W. Cor. Ho-54'
 +17-2' -31'
 +12-E 2' Conc Drive Lane -31'
 15 9.7 103'

+57-15' Linden Tr.-21'
 +40-Ent-20'
 +39-Range Tie to Ent
 +20-Cor Rose Bush-21'-32'

+82-E 3.5' Conc Walk-34.2'
 +70-S.W. Cor. Ho-57'
 +61-Ent
 +32-Shrub-31'
 +5 on Top Wall
 +31-E 1' Conc Wall-31'
 14 9.7 102
 +61-12' Pop-37'
 +54-18' PP-18' +57-12' Pop-26'
 +46-Cor Nursery-46'
 +36-Cor Rose Bush-22'-30'
 +32-6" Pine-24'
 +31-PP-31'

Nursery

+07-12" Maple - 42'

26' 1 1/2 - 5 ft 36'

1-5-F

28' 1-5-F 34'

1-5-F 34'

1-5-F 35'

+22-Rd-16'
Rd-43'
+90-Range 112'

Road

+78-Rd-35'
+60-Rd-19'

24' 1-5-F 34'

+07-18" BE - 30'

22' 1-5-F 34'

10' R.

2 1/2 Bottom

10' R.

Nursery

+55-End Hedge - 23'
+53-End Hedge - 22'
+46-Bog Hedge - 42'
+44-Bog Hedge - 41'

+73-8" Pine - 42-55'
+70-8" Pine - 34'
+65-10" Pine - 48'
+62-8" Pine - 39'
+57-8" Pine - 31'

Stubs

Nursery

2.7

+75-FC-37' Shrub-50'-37'
+69-End 24' Conc Culv-22'
+175-Ed-20'
+34-Ed-43'
+129-Ed-28'
+14-End 24' Conc Culv-23'
+102-Cor Nursery-45'
+104-Ed-17'

2.6

+52-End 6" Drain Tile-77'

2.5

Nursery-45'

2.4

Nursery-46'

+51-Ent.

2.3

Nursery-45'

10' 10'

Nursery-35'

2.2

Nursery-46'

9.8 10.2

+119-PP-32'
Nursery-37'

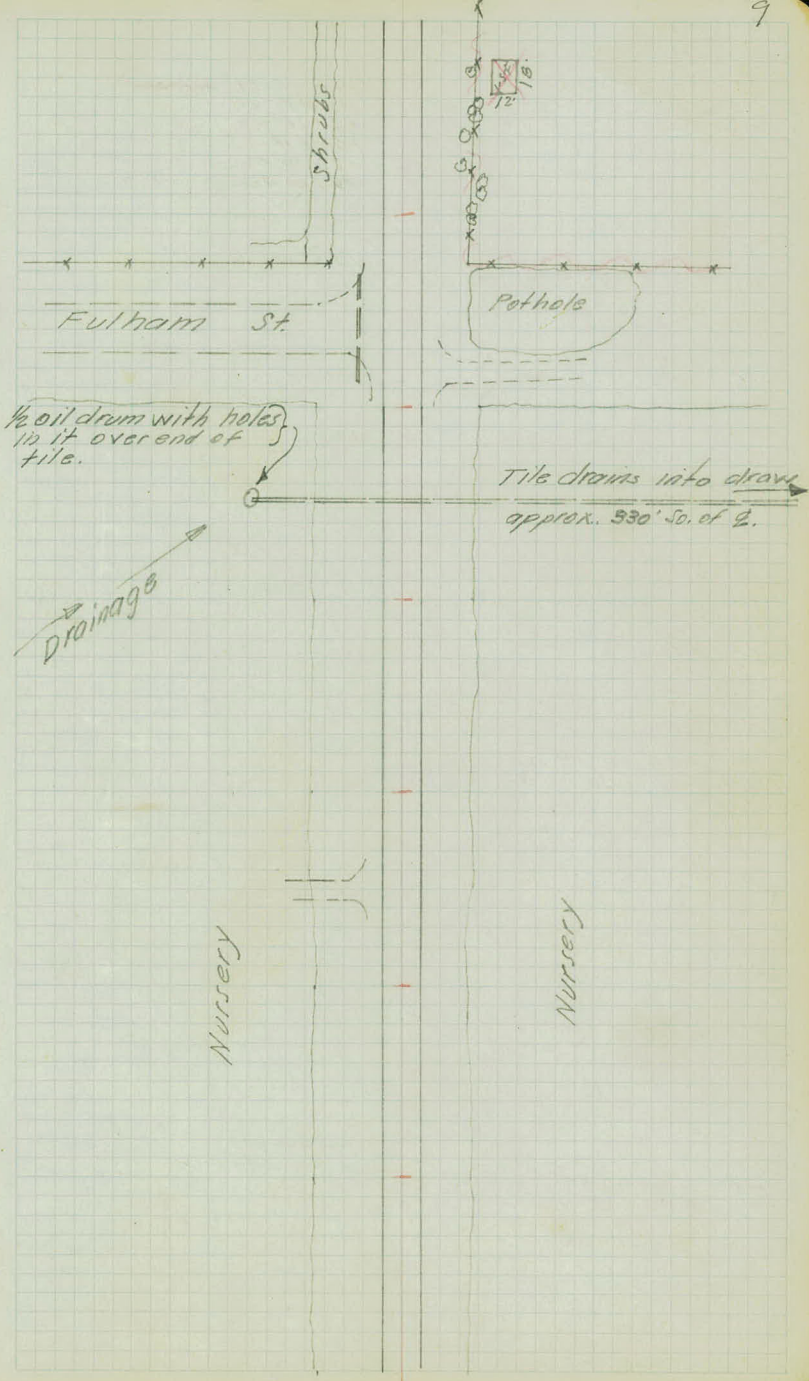
2.1

Nursery-44'

9.7 10.3

Nursery-35'

+73-12'-35'
+62-NW Cor. Caddy Ho-45'
~~+59-12'-32'~~
~~+58-10'-32'~~ +55-10'-34'
~~+57-12'-31'~~ +42-12'-33'
+107-PP-32' +17-10'-43'
+104-15'-0.36' +10-8'-41'
+99-15'-0.36'
+75-FC Cor-33'
+119-Ent.
Cor Nursery-40'
+60-PP-32'



+58-Beg. Fe-33'
+53-Cor Cable Fe-33'
+49-Range Tie 3

FC-41
~~177-8"0-31-44-39~~
~~166-10"0-47'~~
~~+43-12"0-46'~~
~~+40-PP-~~
~~+26-10"0-60'~~
~~125-11"42'~~
~~FC-43'~~

+88-Ent.

+97-12"0-60'
+94-12"0-51'
+73-12"0-99'

+43-10"0-37'

+01-Cable Fe-34'-73'

+22-PP-32'
~~FC-45~~

+80-15% Conc. X Drain
286' 29.8'

+115-Range Tie to Fe.

~~116-18"0-57'~~
~~109-6"0-56'~~
~~+04-PP-~~
~~FC-45'~~

+02-Hyd.-40'

10' 10'

+97-S.E. Cor. 2 1/2 X 2 1/2' Pillar-33'
+68-S.W. Cor. 2 1/2 X 2 1/2' Pillar-33'
+65-Cor. Shrubs-31-50'
+50-Shrubs-48'-66'
+43-6" Pine-52' 6" Pine-66'
+24-6" Pine-53' +32-6" Pine-45'
~~+18-3/4" Birch-72'~~
~~+10-10" Tw. Birch-60'~~
~~+05-3/8" Birch-75'~~

152-10"0-36' 20"0-99'

+10-Cor. Shrubs-32'-44'

102 98 ~~FC-46'~~

~~+94-4-8 Birch-45'~~
~~+96-Forest-55'~~
~~+77-6 Birch-46'~~ +85-6 Birch-62'
~~+74-8 Birch-46'~~ 6 Birch-48'

+80-PP-

10' 10' +15-12"0-51'

+90-Beg. Pav. +95-12"0-Beg. Fe-45'

+113-36"0-70'

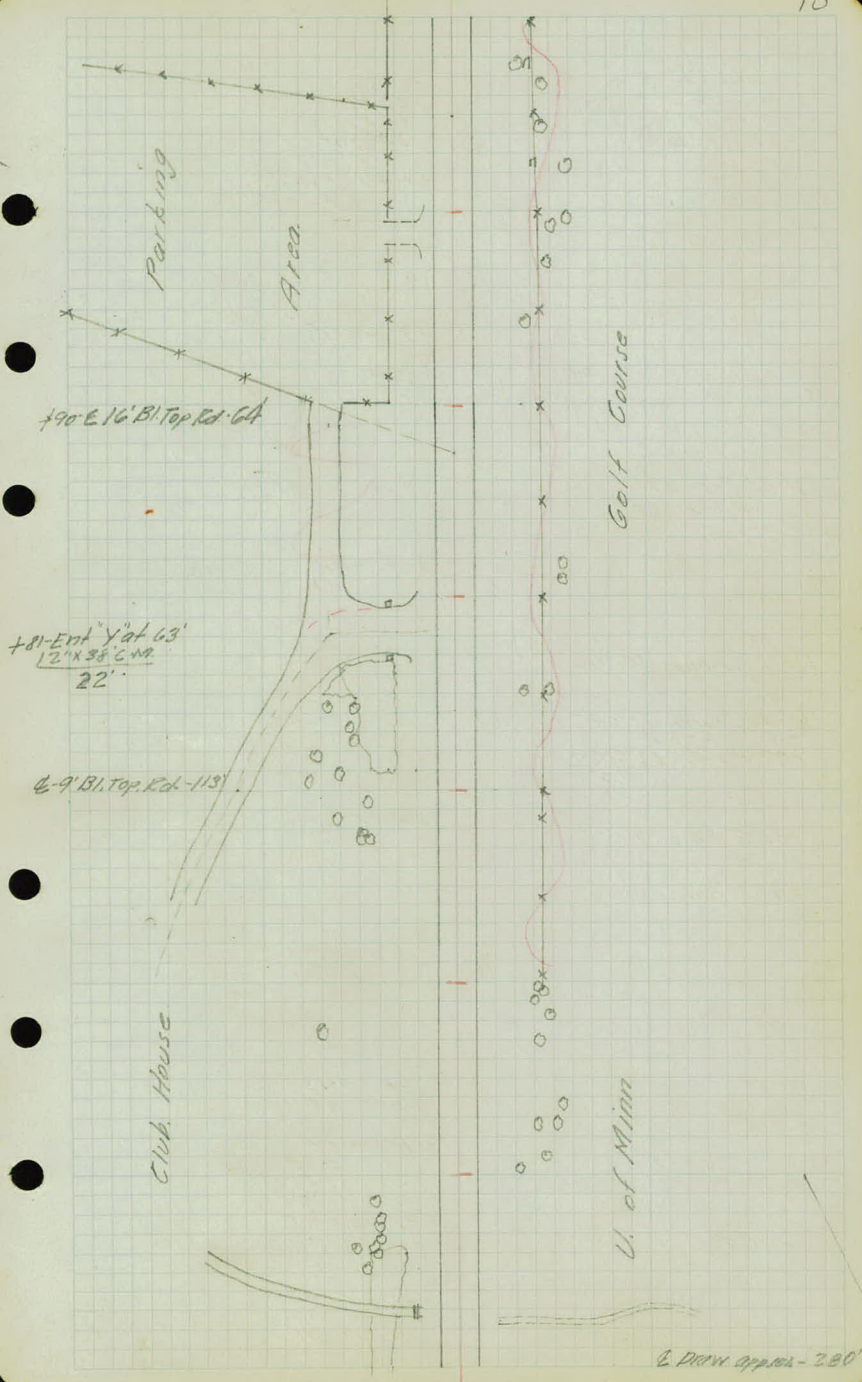
~~198-40-8"0-43'~~
~~194-10"0-45'~~
+93-12"0-89' +91-10"0-40'
+50-PP-32' +70-8"0-42'
+36-12"0-55'
+28-10"0-41' 15"0-53'
~~104-12"0-32'~~ +10-8"0-46'
Beg. Driv. 180'

+74-10" Birch-40' +87-10" Birch-44'
+67-12" Birch-40' +69-6" Birch-40'
+65-15" Birch-62' +62-6" Birch-54' +75-End Pav.
~~+52-8" Birch-48'~~ +60-10" Birch-42'
+60-40-End Shrubs-27'-45'

Top Steps-40.5'
Bulb. Flans-30.5'
+29-2 G. Meadows Walk-12' X 7' Long
23'

+95-PP-32'
+114-6" Dirt Walk-
+10-End Pav-40'

Shrubs-42'-95'



+74-Ent.

+32-18" RE - 34'

41

+50-PP-

+34-Ent.

+03-6" Trip Willow - 47'
SWAMP - 40-200'

+35-PP-32'

+09-24" Conc. X Drain
+32' 35'

40

~~+61-Fc Cor 33'~~
~~Lowland - 60'~~~~+61-Fc Cor 33' - Bog Swamp~~

+19-PP

~~FC 34~~

39

+90-18" 0 - 39'

+66-20" 0 - 54'

+43-Path-

+73-Lowland - 30-100'

+30-Bog Lowland - 34-46'
+18-18" 0 - 39'+07-Path - 12" CM X 10'
26'

38

~~+80-3" Pine 39'~~

+90-PP-

+41-3" Pine - 41'

37

10' 10' ~~FC 38'~~

+80-PP-32'

+39-8" 0 - 43'
~~+33-8" 0 - 54'~~

36 FC - 33'

+07-15" 0 - 32'

~~FC 34~~

+96-8" 0 - 32'

+75-8" 0 - 33'

+72-12" 0 - 40'

+64-Ent -

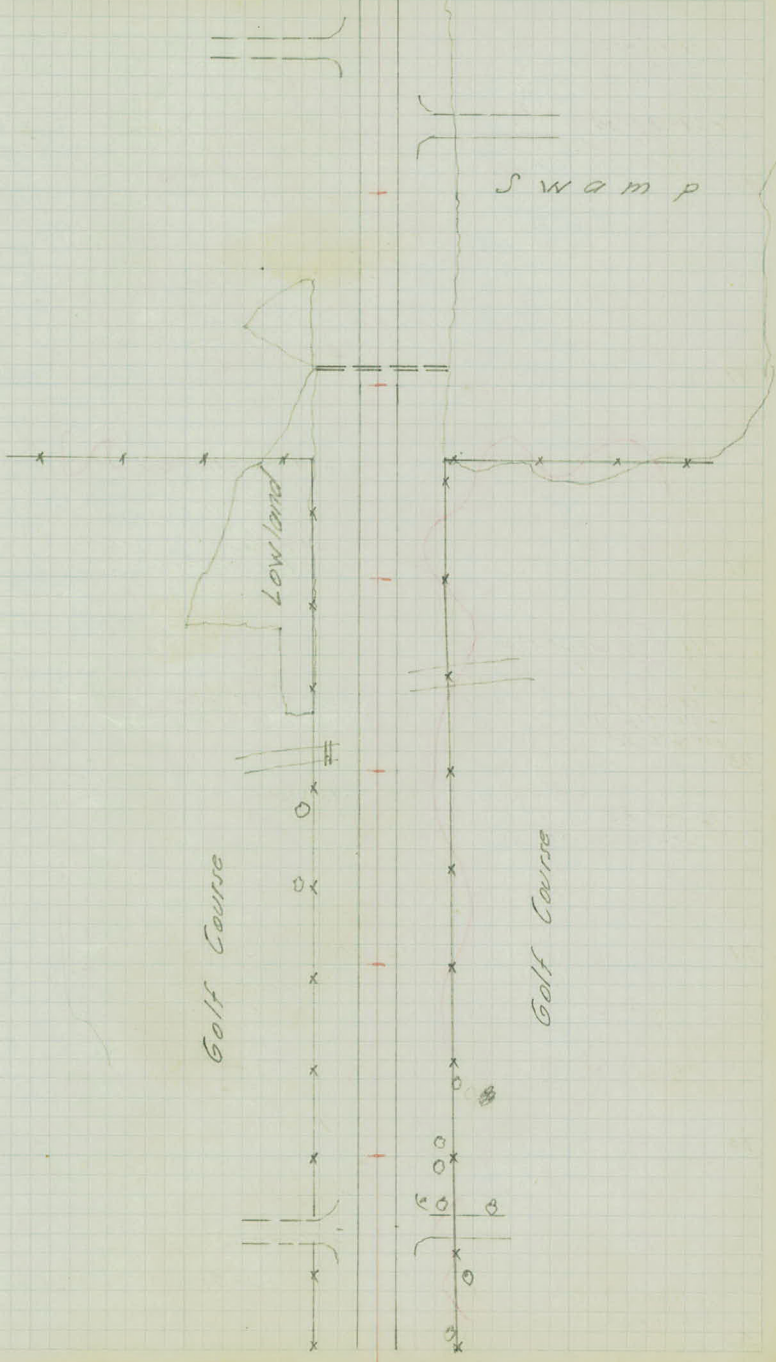
+54-PP-32'

+62-Ent.

+38-15" 0 - 47'

+10-12" 0 - 37'

35



Golf Course

Golf Course

+86-8" Elm-35'
 +50-PP-30' +61-4" Elm-31'
 +48-1/2 Cor-34' 12" X 20' C.M.
 +39-Ent. 26'
 +29-Step-34'
 +15-T.P. + FC Cor-32'
 +11-Row of Shrub-23'
 48 Ent.
 +92-End Plant Fc-27'

+60-12" Elm-37'
 +43-PP-33'
 T.P.
 +92-CP-33'
 +75-Ent-

Arc II 32
 +28-PP

47

+59-8-4" Elm-40'
 +22-12" X 8' Cor-24'
 +14-24" Maple 40'
 +105-PP-32'
 NW Cor Porch-71'

46

+71-Fc-33'
 +71-Beg Wood Plant-Fc-28'
~~+54-15-4-34'~~
 +46-Ent-12" X 20' C.M.-25'
~~+33-Step-31'~~
~~+22-Step-21'~~
 +10-6'0-31'

+89-Row 8' Wide Lillies-35'
 +73-15'0-35'
 +37-End 3' Cor Walk-33'
 18" X 8' C.M.
 27'

45

+95-12'0-32' +97-Step-37'
 +92-Step-32'
 +10-Step-36' 6' BE-41'-44'-46'

+93-NW Cor Ho-70'
 +71-PP-32' 12" X 20' C.M.
 +62-Ent-26'
 +38-15'0-38' ~~Step-34'~~
 +29-6' BE-30' 12' BE-45'
 +25-12'0-32' 15' BE-45'
 +18-6'0-31'
~~+11-15' BE-34'~~

44

102

+35 Low land-35

98 Swamp-60'
 +98-6'0-26'
 +96-15' BE-40'
 +86-12'0-27'
 +64-12' BE-33'
 +56-PP-32'
 +35-6'0-25' +38-8' BE-34'
 +33-10'0-25' ~~Step-34'~~
 +18-5'0-25'
 +10-Ent-

43

~~+90-10'0-32'~~ +95 Low land-35

+92 E.R. 42'
 +68 B.R. 19
 +57-PP-32'

42

~~+19-10'0-35'~~
~~+106-Step-23'~~

+18.5" Elm-27'
+15.4" Elm-24'

Shrubs

2-5-F
45'

1/2-5-F
35'

Pothole

Swamp

0001

n

+67-PP-32

55

+45-PP-32

54

+15-Cor. Water main - 35'±
 +26-
 +15-Fc Cor - 34'
 +19-PP-44
 +26-Rd-20'
 +97-Fd-50'

+44-Por-10.3-11.4'

+15-PP-32 Fc Cor - 33.5'

53

+68-Tel. M.H.-15' +69-Rd-50' +55-12"CM-42' 12"X20"CM
 +50-Fc Cor-33' +40-Fc-34' +51-Fc-42'
 +41-15"Elm-40' +39-12"CM-29'
 +40-Rd-17' +20-Por-10.2-11.2'
 +09-2.2' High X 9' Wide Mono. X Drom
 End Barrel-192 21.3'
 " Floor = 251 26.5' +04-PP-33'

52

+26-Por-12"X8"CM
28

+35-15"Elm-32'

+17-Fc Cor-33

51

+82-Stop-37'
 +59-Stop-35'
 +50-10"Elm-34'
 +47-Stop-37'
 +44-Stop-34'
 +32-Stop-34'
 +28-Stop-34'

+92-10" B.E.-33'
 +82-PP-32'
 +62-12" B.E.-36'
 +50-15" B.E.-35' Stop
 +36-6" B.-36'
 +35-42-37' Stop

50

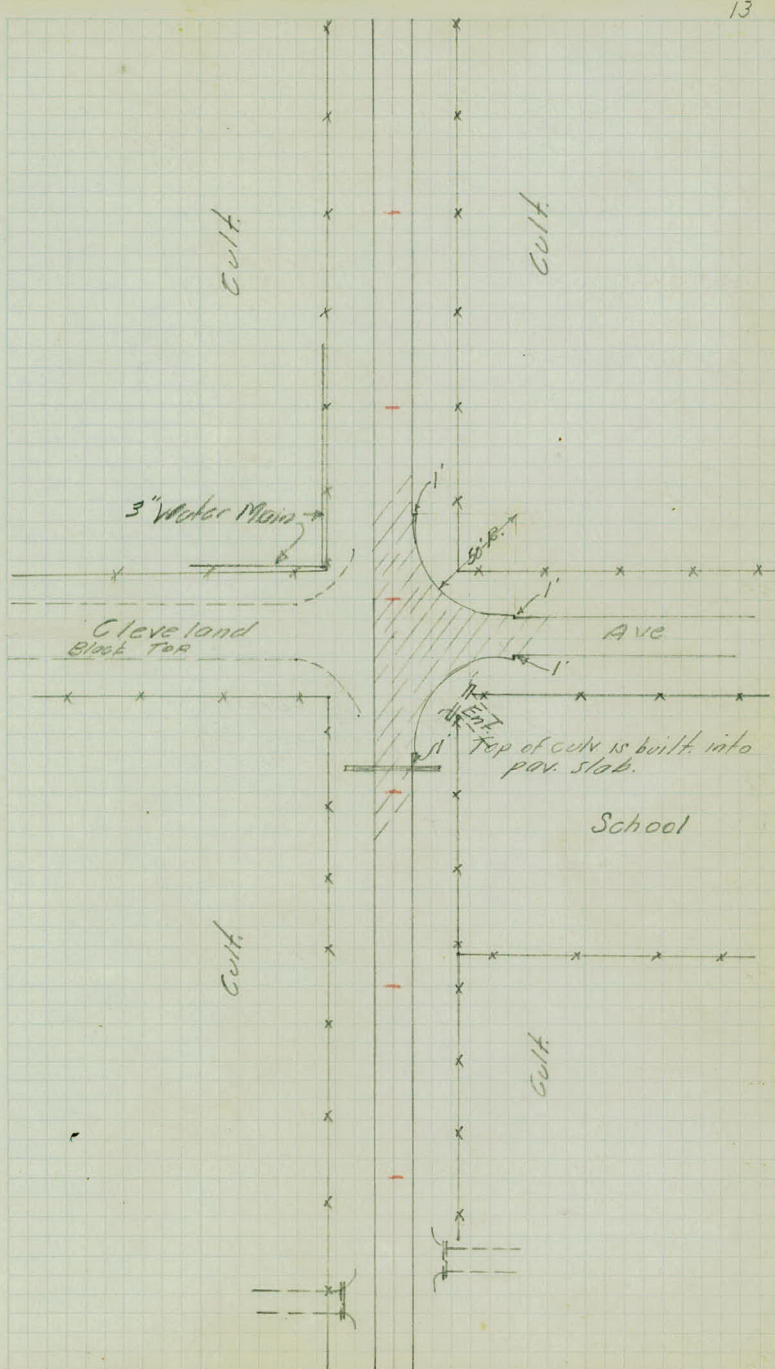
Fc-34'

+95-18" Mono-35'
 +67-PP-Box Fc-33'
 +57-Ent-15"X20"CM
27'

+35-Ent-12"X14"CM
27'

49

10' 10'



+91-PP-33'
Arc Lt.

+45-Beg FC-33'

+36-End - $\frac{12' \times 20' \text{ C.M.}}{27'}$

+21-2" Water main 33' - M.H.

62

+71-PP-

+65-Cor Pines - 40'

+28-Cor Pines - 40'

61

10.2 9.8

FC-33'

+52-PP-

60

+95-End $\frac{12' \times 20' \text{ C.M.}}{27'}$

+87-End FC-34'

+58-22' High 4' Wide Mono. X Drain
End Barrel 20.5' 20.8'
" Floor 23.8' 25.1'

+33-PP-

59

+11-PP-Arc Lt 32

58

57

+88-PP-32

+15-Water main - 35

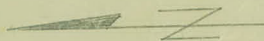
+ = Water main 2

+13-Off 2 Dia. M.H. - 33'

56

Full of Water

file with Page 14 - Bk 117 - Dr 16



r & Carpenter Ave

35'±

3" Water Main R

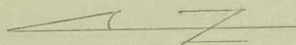
{ 3" Water Main X's
at sta 56+15

Top of main is
3.5' below ℓ

36'±

ℓ Cleveland

Ave R



5.0' below pav.

M.H.

2" Water Pipe.

7.7' below pav.

33'

62+21

E Carpenter Ave

5-10-44

K.A.

L.G.

C.N.

Wood Rail →

2" Pipe

5' below par. M.H.

NURSERY
Pines

Top of culv. built into
par. slab

Cult.

Cult.

3" Water Main

3.5' below par.

69 +15 Ent. - 12" X 20" CM
28'

+99-6" Birdi - 48'
+88-S.E. Cor. Ho. - 88'

+58-8" Mt. Ash - 48'
+50-Ent. -

~~+158~~

+96-PP - 32.5'

68 +04-S.W. Cor. Ho. - 88'

Fe - 33'

+60-E. Edge Driveway
+51-S.E. Cor. Greenho. -

+76-PP -

67

+43-S.W. Cor. Greenho. - 89'
+31-PP - 61'

+58-PP -

+21-Ent. -

66

+33-PP

65

10.3 9.5

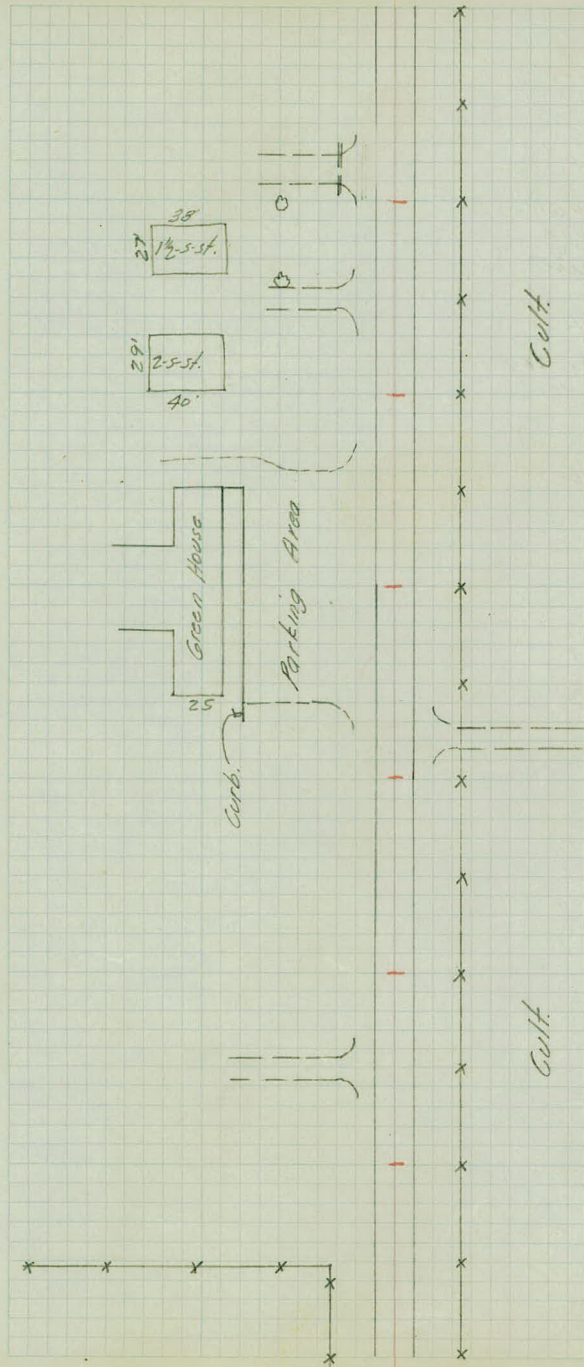
+59-Ent. -

+13-PP -

64

+49-F.C. Cor. - 33'

63



Cult.

Cult.

~~159-24°BE-36'~~

+49-Ent. - $\frac{12" \times 20' \text{ C.M.}}{29'}$

~~+31-Shrub-41'~~

+31-PP-

76 +04-Shrub-55'

+94-SW Cor Ho-126'

+87-Ent. - $\frac{15" \times 20' \text{ Conc.}}{28'}$

+67-Ent. - $\frac{15" \times 20' \text{ C.M.}}{29'}$

+33-24°BE-41'

75 +16-SW Cor Ho-104'

10' 10' +09-PP-32.5'
FB-33'

~~+40-20°BE-40'~~

~~+17-16°BE-36'~~

+26-Ent. - $\frac{12" \times 14' \text{ C.M.}}{28'}$

74 +05-Ent. -

+82-PP-

+80-4°Pine-52'

+76-10°Pine-44'

+62-4°Pine-52'

~~+37-13°BE-41'~~

+36-SW Cor Ho-100'

73

+93-Ent. - $\frac{12" \times 20' \text{ C.M.}}{28'}$

+89-E 2 1/4 Conc Walk-35.3'

~~+16-4°Pine-39'~~

+13-15°Ash-39'

+50-15°BE-39'

+49-SW Cor Ho-104'

~~+32-Cor Hedge-50'~~

+27-Ent. - $\frac{12" \times 20' \text{ C.M.}}{28'}$

+45-PP-

72

+46-Cor Hedge-

+43-PP-

+20-E 1/4 Conc Walk-40.2'

71

+98-SW Cor Ho-86'

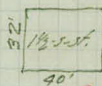
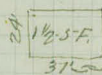
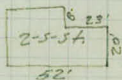
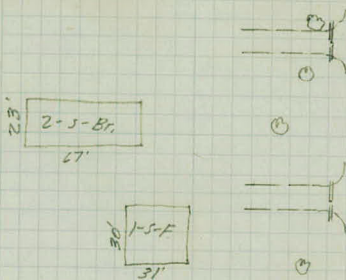
+87-~~Cor~~ Hedge-52'

Big in

+61.95 = E Toadum St - $\frac{18" \times 37' \text{ Conc. Walk}}{28.5'}$
26' Top

70

Orchard



Tatum St.

~~+68-5' Ash-34'~~
~~+50-5' Ash-33'~~
~~+30-5' Tw. Ash-33'~~
~~+11-5' Tw. Ash-33'~~
~~+10-5' Ash-33'~~
~~+99-5' Ash-33'~~
~~+95-6' Ash-33'~~

Cult.

Cult.

+99-6" Elm - 38
+97-N.W. Cor. Ho. - 82'

+12-PP-^{Age} Lt

83

+80-Ent - $\frac{12" \times 20' \text{ C.M.}}{28'}$

82

Fe - 34'

+95-Ent $\frac{15" \times 20' \text{ C.M.}}{28'}$

+69-PP-315'

+36-1.5' High X 4' Wide Maple X Drains
End Barrel - 21.3' 21.1'
End Floor - 26.3' 26.1'
10' 10'

81

+25-6" Elm - 51'
+23-PP-32'

80

+76-15' Elm - 53'

+51-FC Cor - 345' +47-Ed - 19'
+41-End 18" Conc. Culv. - 30'

+22-Ed - 45'

+32-N.W. Cor. Ho. - 52'
+21-Ent - $\frac{15" \times 20' \text{ C.M.}}{28'}$
+06-8' Wide Lvl. Ho. - 36'

79

+75-Ent 18" Conc. Culv. - 30' +95-Ent - 41'
+15-Ed - 24'

+81-PP-32'
+80-Shrub - 34'

+69-15' Ash - 40'

78

10' 10'

+42-PP-32'

~~+43-FC Cor - 32.6'~~
~~+41-PP-32'~~

77

2-5-F 26'
35'

17

Cult.

Cult.

Cult.

New Brighton Rd.

Cult.

Cult.

2-5-F 24'

40'

+136' BE-33'
+07-57' per A56-3A'

+88-10" Elm - 36'

+51-10" Elm - 36'

+28-PP-32'

+28-E-Ent 15" Cornc Cdrk - 28'

+27-100% Masonry Wall - 23'

90 Fe - 33'

10' 10'

+75-W-Ent Cornc Cdrk - 28'

+38-5" Pine - 49'

89

+85-PP-32'

+57-Ent - $\frac{15" \times 26" \times 17}{28}$

+20-NW Cor H.C. - 83'

88

+35-PP-32'

+29-Rdw 15" Elms - 46'

+16-Ent - $\frac{15" \times 20" \times 17}{28}$

~~+23-15" Ash - 40'~~

87

O.K.

+77-NW Cor H.C. - 82'

~~+76-15" Ash - 40'~~

86

+97-PP-32'

~~+38-Ent - $\frac{15" \times 30" \times 17}{28}$~~

85

Fe - 34'

+54-PP-32'

+43-18" Elm - 39'

+34-Ent - $\frac{15" \times 20" \times 17}{28}$

+28-E 2" Wdk - 33'

84

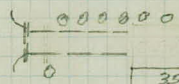
Nursery

Driveway and
Parking Area

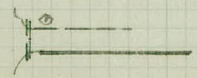
Office



25' x 18'
34'



35' x 24'



+99-30" Maple -

+78-30" Maple -

~~+60-24" Maple~~

~~+40-30" Maple~~

~~+20-30" Maple~~

97

~~+98-30" Maple 40~~

~~+76-Ent -~~

~~+87-End 15' C.M. 29'~~

~~+68-End 15' C.M. 38'~~

~~+56-Ent -~~

~~+92-End 15' C.M. 28'~~

~~+39-Hedge - 34'~~

96

Avg Lt.
+106-PP-32

+57-25' X 4" Wide Mono. X Draw

21"

26"

~~+97-Fc. Cor~~

~~+40-Fc. Cor. 34'~~

+36-PP-32

95

+79-Cor. Fruit stand - 37'

~~+71-Ent. 12' X 7' C.M.~~

29

+23-Ent -

+10-End Hedge - 35'

+13-PP-23'

94

+86-12" Linden - 37'

+72-12" Linden - 37'

+58-Cor. Hedge - 35'

+39-Fc. Cor. - 33'

+67-PP-92

+31-2.6' High X 4" Wide Mono. Culv.

End Barrel 20.8' 21.2'

" Floor. 25.0' 25.9'

93

+23-Fc. Cor - 35.5'

+21-PP-32'

92

+01 10' Elm - 36'

+63-10' Elm -

91

+28-10' Elm -

15'X32'CM
15'X18'CM
15'X14'CM

23

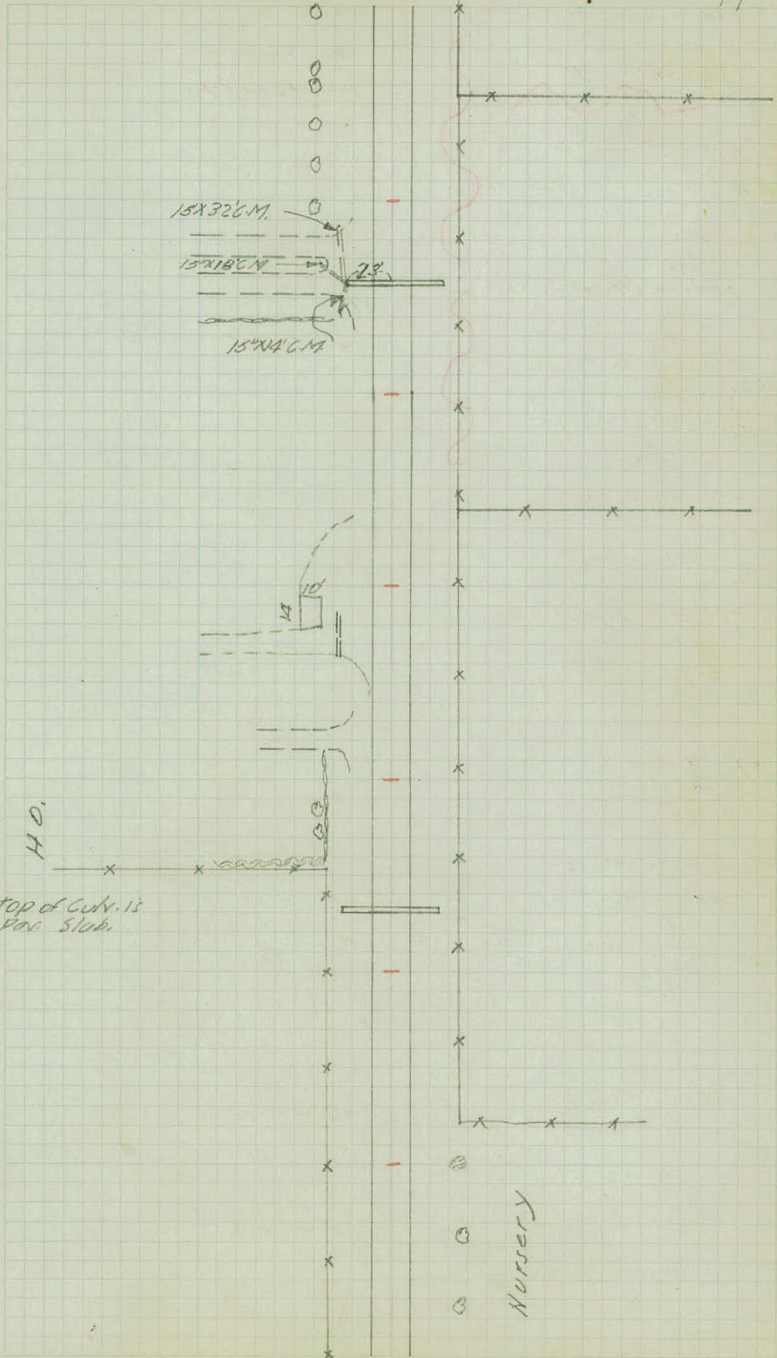
14

10'

H.O.

top of Culv. is
Pave. Slope

Nursery



~~+98-30" Maple-36'~~

~~+85-Curb-2.45'~~
~~+16-Bcg. Pav. Ext.-10'~~
~~+63-SE Cor. Bldg.-87'~~

~~+21-18" Tree-36'~~

104 Parking Area-70

~~+64-36" Maple-36'~~

103

~~+89-36" Maple-37'~~

~~+63-Ent.~~

~~+52-24" Maple-~~

102

~~+18-18" Maple-~~

~~+90-24" Maple-~~

~~+52-24" Maple-~~

101

10' 10'

~~+55-30" Maple-~~

~~+35-18" Maple-38'~~

100

~~+35-Cor-20'~~
~~+12-Ed.-33'~~
~~+15x36 CM.-28'~~
~~+98-Ed.-35'~~
~~+57-Ed.-19'~~

~~+38-30" Maple-~~

99 ~~+18-18" Maple-~~

~~+99-30" Maple-~~

~~+58-30" Maple-~~

~~+18-Ent.-15" Azalea~~

~~+38-24" Maple-~~

98

~~+92-Δ in Hedge-81'~~

~~+87-Bcg. Curb-15.5'~~
~~+79-Pav.-10.2-11.2' P.P.-30'~~
~~+67-15 CM-52'~~

~~+44-Δ in Hedge-45'~~

~~+15-30" Maple-36'~~

~~+59-Automatic Signal Change-0.9'~~

~~+44-P.P.-28'~~

~~+18-N.E. Cor. 3'x3' Pillar-45'~~

~~+99-N.W. Cor. 3'x3' Pillar-45'~~
~~+88-Δ in FC-39'~~
~~+95-P.P.-28'~~

~~+58-24" Maple-35'~~

~~+44-24" Maple-25'~~

~~+30-P.P.-28'~~
~~+18-Δ in FC-38'~~
~~+08-N.E. Cor. 3'x3' Pillar-45'~~

~~+89-N.W. Cor. 3'x3' Pillar-45'~~

~~+81-Δ in FC-38'~~

~~+62-30" Maple-34'~~

~~+21-18" Maple-34'~~

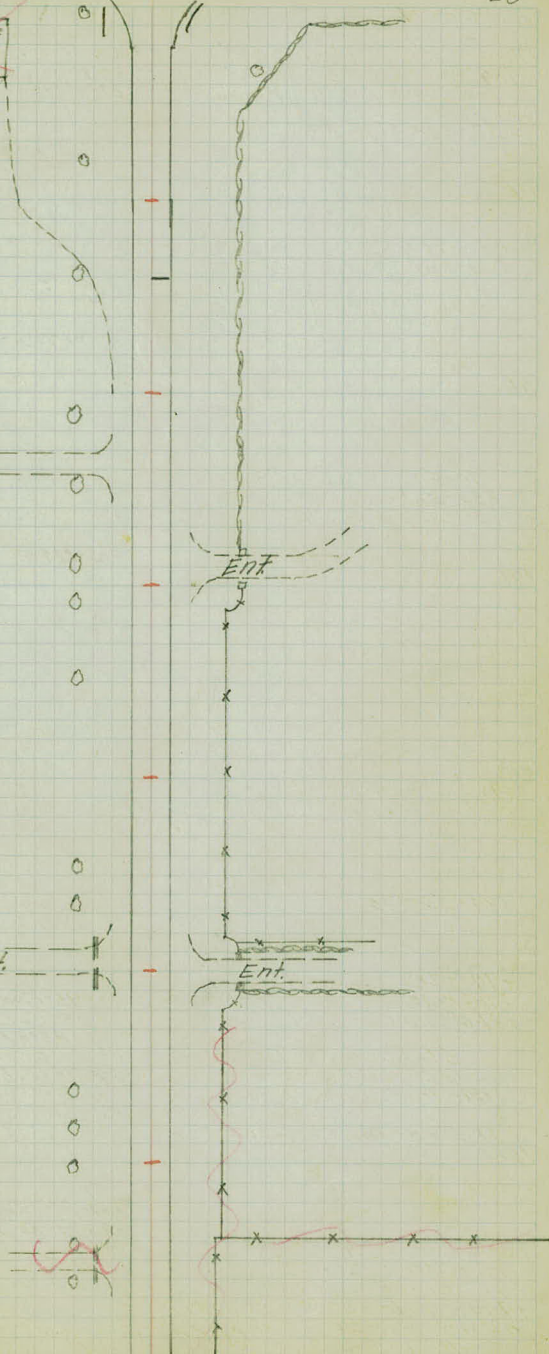
~~+76-P.P.-28'~~
~~+65-30" Maple-34'~~
~~+66-FC Cor.-39.5-37.5'~~

~~store~~
~~15-16~~
 34'

St. Marys St.

Ent.

Ent.



194-CB-94
 171-M.H.-35' 4x4
 171-1.8' High x 4' Wide Mono. X Drive -
 End Barrel
 " Floor
 193-Rd.-32'
 180-Rd.-19'
 184-PP-32'
 20.8
 27'
 153-Cor. Sko.-82'

111

188-Fc.-52'
 131-End 24" Conc. Culv.-35'
 156-PP-

110

10' 10'

140-End 15' Sewer-35'
 135-Ent-
 130-Con Bldg.-59.5'
 137-PP-32'

109

115-PP
 103-Ent

108

198-S.W. Cor. Store-67.5'
 184.5-Semisphere Signal change-10.9'

134-S.D.-35'

107

197-24"x24" S.D.-45'
 196-P-40'
 187-6' Curb Rad-45-31'
 188 Pavement
 183 Pavement
 172-Rd.-10 10'
 50' Pav. Rad. + 45' Pavement
 End Curb-51' 2' + 35' Pavement
 144-Ctr 10' Curb Rad-34'
 124-Pav. Rad.-59'
 124-End 50' Pav. Rad.-60' = joint
 195-End Curb-18.4'
 180-Face Curb-33.3'-61'
 185-PP-32'
 180-50' Pav Rad.-7'
 144-Ctr Curb Rad-32.5'
 137-Semisphere 28"
 56'
 124-End 50' Pav Rad-60'

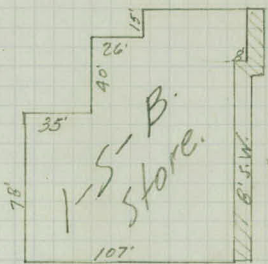
106

185-Semisphere-29'
 174-Ctr 28' Curb Rad-52'
 160-PP-33'
 117-Face Curb-32'-56' 7' Curb Rad.
 112-Semisphere-29'
 105-140-End 12" Conc.-37' 50' Pav Rad
 105-End 12" Conc.-57'
 147-Cul. Vile-46'
 178-PP-32' Switch Box-37'
 171-Ctr-25' Curb Rad-49'
 168-Semisphere-29' 157-Hydr-65'
 163-M.H.-27.5 Telco
 114-Face Curb-48.3-74'
 112-Pav. Rad-33'
 108-12" CM-60 Approx 26' Curb R.

5-11-4

K.A.
L.C.
C.M.

1-5-F

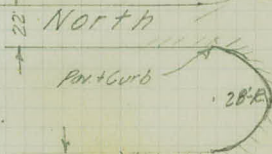


Parking

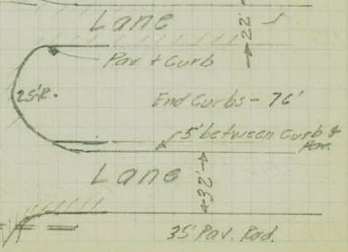


Entr.

+53-End Signal Changer - 27'
+41-End Signal Changer - 21'



+26-End Pav. Rad - 60'



+88-Rd-18'
 +70-Rd-34'
 15' x 20' CM
 34'
 +51-Rd-31'

+92-Rd-19'
 18' PP-32'
 +76-Rd-35'
 +51-Rd-37'

118
 +11-Walk 12' x 8' Conc. Walk
 24'
 +92-Gate Valve-45'

+34-Rd-18'

+45-PP-32'

117
 +67-Gate Valve-43.5'

116
 +41-2' C' Conc. Walk-49.5'
 +11-Gate Valve-43'

+45-PP-32'

115
 +36-Gate Valve-44'
 +25-2' C' Conc. Walk-49.5'
 +95-Gate Valve-44'

114
 +46-2' C' Conc. Walk-49.5' 12' x 8' Conc.
 35'
 +24-Gate Valve-44.5'

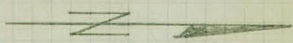
+66-PP-32'

+25-PP-32'

113
 +47-Hyd-21.6'
 +35-End 24' CM-35'
 +41-Rd-17'
 +22-Rd-40'

+39-Rd-17'
 +17-Rd-36'

112



Ave

35' Pav. Rd.

Curb

3.2' Molochan Surface

South

50' Pav. R.

Curb

3' Curb R.

21.5'

Long

20' Bl. Top over Pav.

21'

Curb

28.4'

Snelling

Curb

North

Long

22' Pav.

22' Pav.

(106 +24.7 Joint)

43.9'

Curb

+35'

+46'

28'

50' Pav. R.

28'

Curb

63.5'

18'

Curb

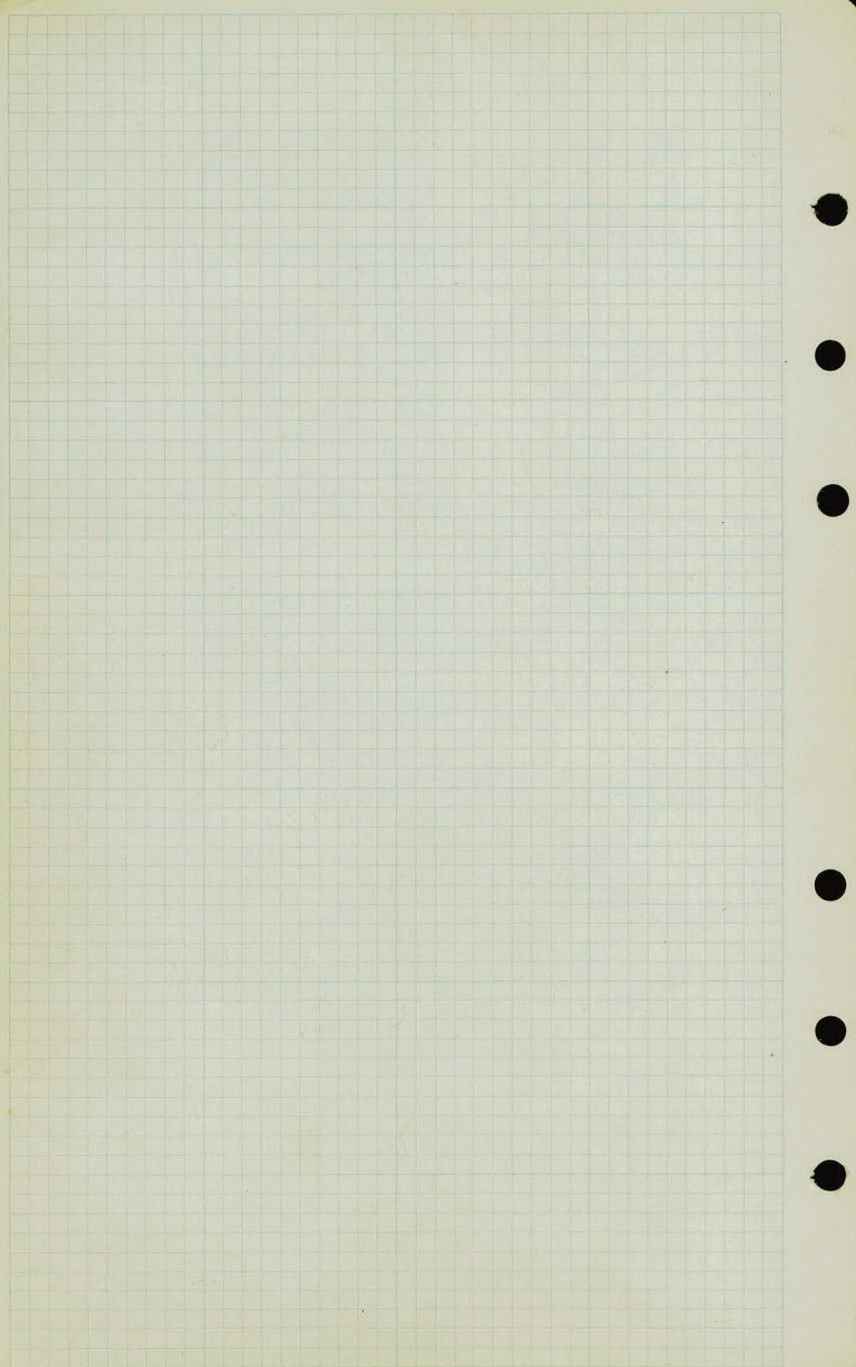
17.4'

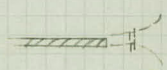
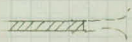
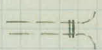
50' Pav. R.

Curb

788'

Pav





+95-B Comp. Walk-50' 18" X 6" Conc. Culv.
34'

+66-Hydr-23' +71-Rd-18'

+60-End 18" Conc. Culv-34'

+59-G.P.-33'

+48-18" C.M.-55'

+45-Rd-40'

+58-Rd-18'

+48-Rd-32'

+42-Rd-30'

18" X 30" C.M.-35'

+18-Rd-20'

Rd-19'

+14-12" C.M.-53'

+18-Rd-50'

125

+67-Gr. 3' X 17' Conc. Pump. Base-68'

+68-Base-18" Conc. Culv-34'

+64-End 18" Conc-34'

+15-5" Galv. Steel-90'

124 +64-End 18" Conc. Culv-34'

+19-Ent.- 15" X 30" C.M.
34'

123

+92-P.P.-

+30-Rd-18'

+18-End 18" Conc. Culv-34'

+11-Rd-39'

122

+88-Rd-42'

+73-P.P.-

+77-End 18" Conc. Culv-34'

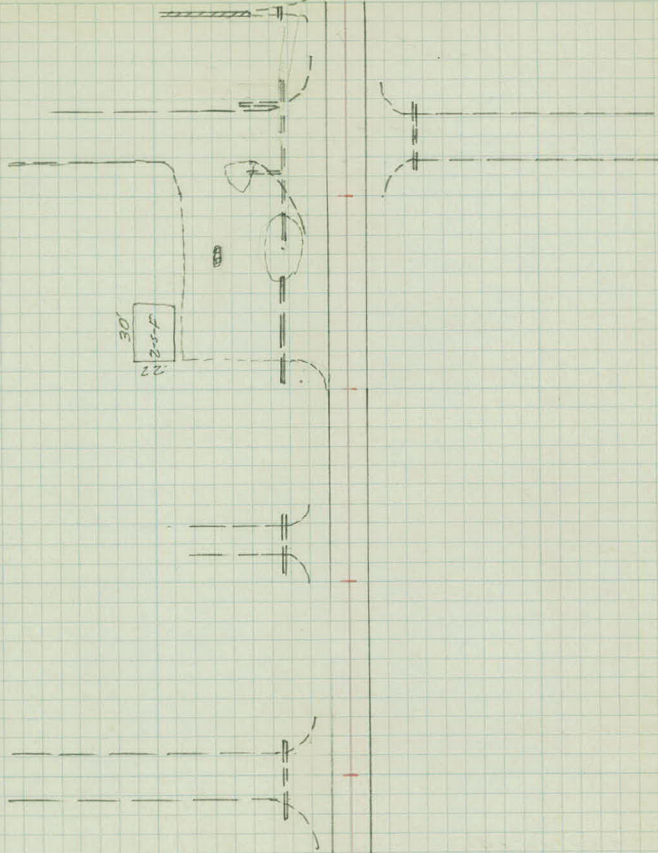
+Hyd-55'

121

+28-P.P.-

120

119



Cont. next page.

+118-Black Top-50

+58-Beg-24" C.M. - 35'

+52-T.P.-32'

+30-Black Top-10'

131

+178-Black Top-50'

+174-Hyd-39'

+30-Black Top-10'

+12-PP-32'

+55-Ent-15" X 20" C.M.
37'

+108-PP-32'

130 +01

+96 } 2' Conc. Drive - 43'

+96 } 18" X 20" Conc. Culv - 35'

+59 - Hedge - 48'

+50 - } 2' Conc. Drive - 49'

+45 - } 18" X 20" Conc. Culv - 35'

+24-Gate Valve - 42'

+109-PP-32'

129

+85 - Ent. - 18" X 20" Conc. 7' Conc. Slab
35' 49.5'

+79 - End Hedge - 49'

+25 - Beg Hedge - 49'

+23 - }

+18 - } 2' Conc. Drive - 49.5'

+18 - } 18" X 20" Conc. Culv - 35'

+12 - End Hedge - 49'

128

+53 - PP -

+64 - Beg Hedge - 48'

+63 - End 24" Conc. Culv - 35'

+56 - }

+51 - } 2' Conc. Drive - 46.5'

+51 - }

+102 - End 18" Conc. Culv - 35'

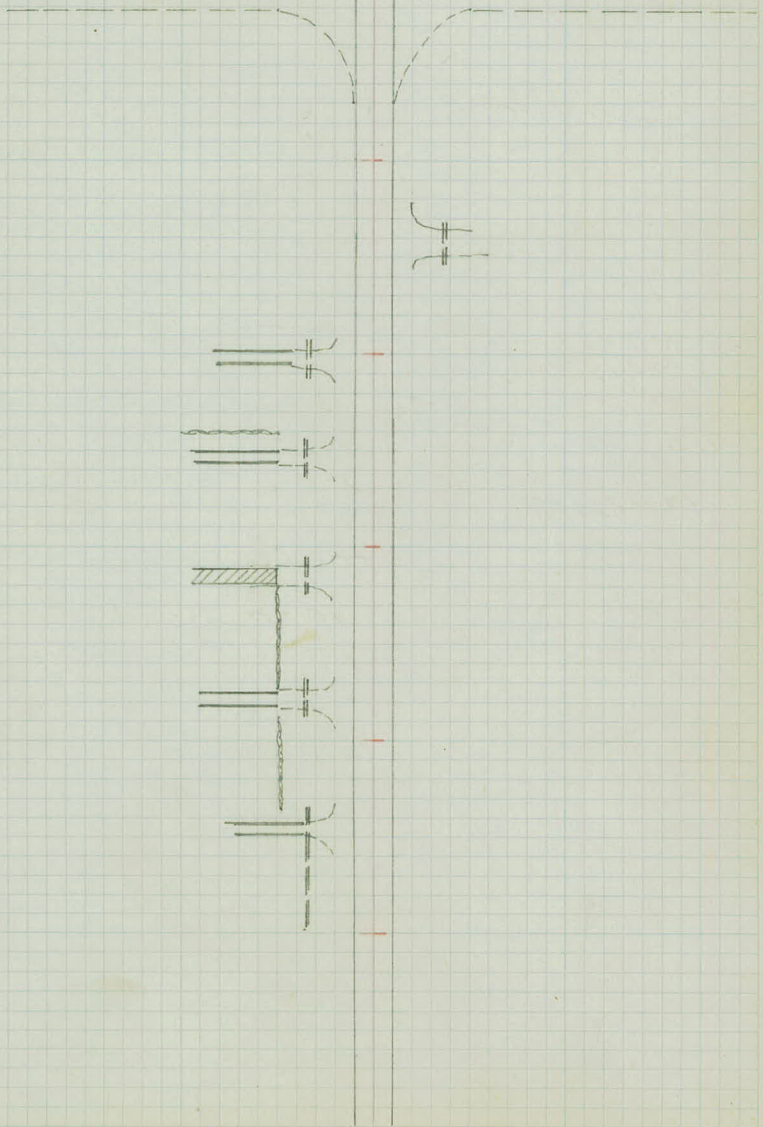
127

PP-32'

126

Hamline

Ave.



134

+67-5 E Cor Ho. - 51'

133. Gutter - 22'
Stone slope - 32'

+063-End Curb-10.4'

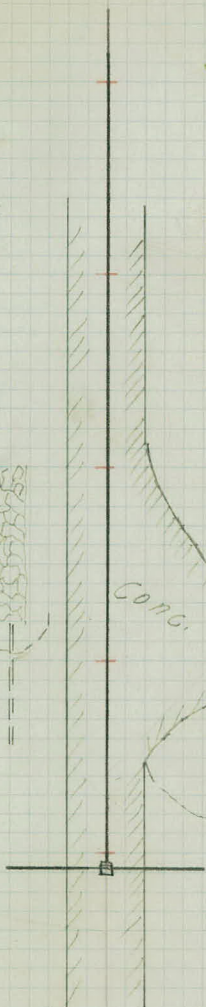
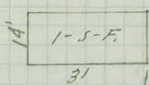
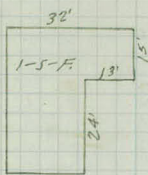
+89-5 E Cor Pop. stand - 39'

+59-8a Right Gutter + slope 22'
+59-End 24 CM - 20' 31.4'

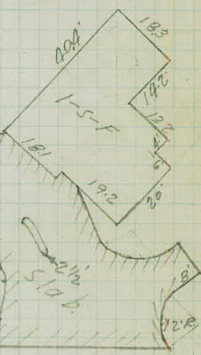
+90-Curb-23.0' +85-Curb-18.9'
+70-Curb-35.5' +75-Curb-27.8'
+21-Range TIC to Bldg.
+69E-N.W. Cor Bldg-4.4'
+59-Curb + Bldg-6.85'
+46-End Conc. Pump Base-51.3'
+40.3-Cor Curb-91.5'
+37-End Conc. Pump Base-57.3'
+32.2-Cor Curb-97.6' +30-Curb-78'
+41-Curb-3.5' +40-Curb-71'
+30-Curb-15.40.2' +35-Curb-196-43.7'
+23.2-End Curb + Pop-10'
+20-Curb-44.9' 114-PP-30'
+11-End Curb + Slab-88.8'
+0.7-End Curb + Slab-37.2'

132

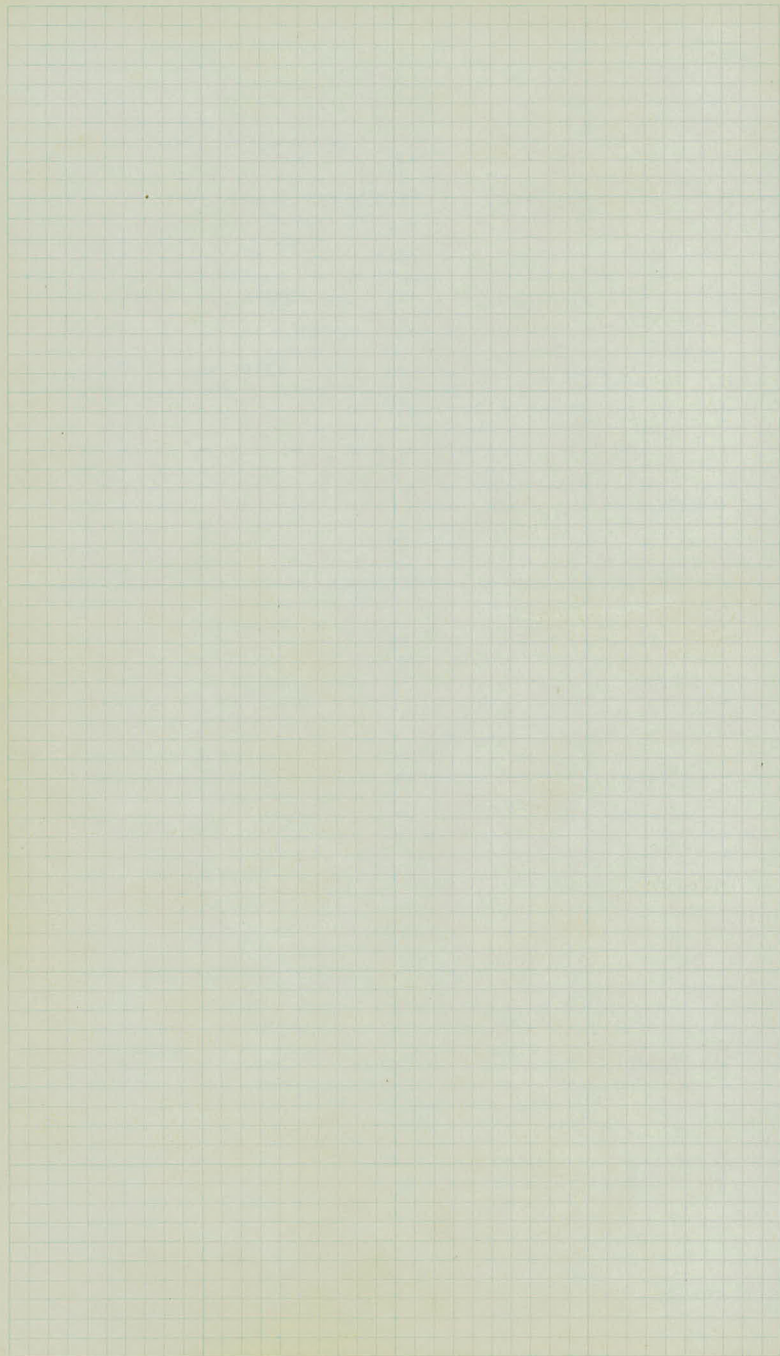
131



CONC.



200' 1/2
Slab



Topography
Larpentour Ave.

138 Fe-47'

+11-P.P.-28'

137 Fe-50

+65-P.P.-

+40-Fe-61'

136 End Mason. Slope-28-22'
+96-Fe Cor.-61'

+13-Ent-

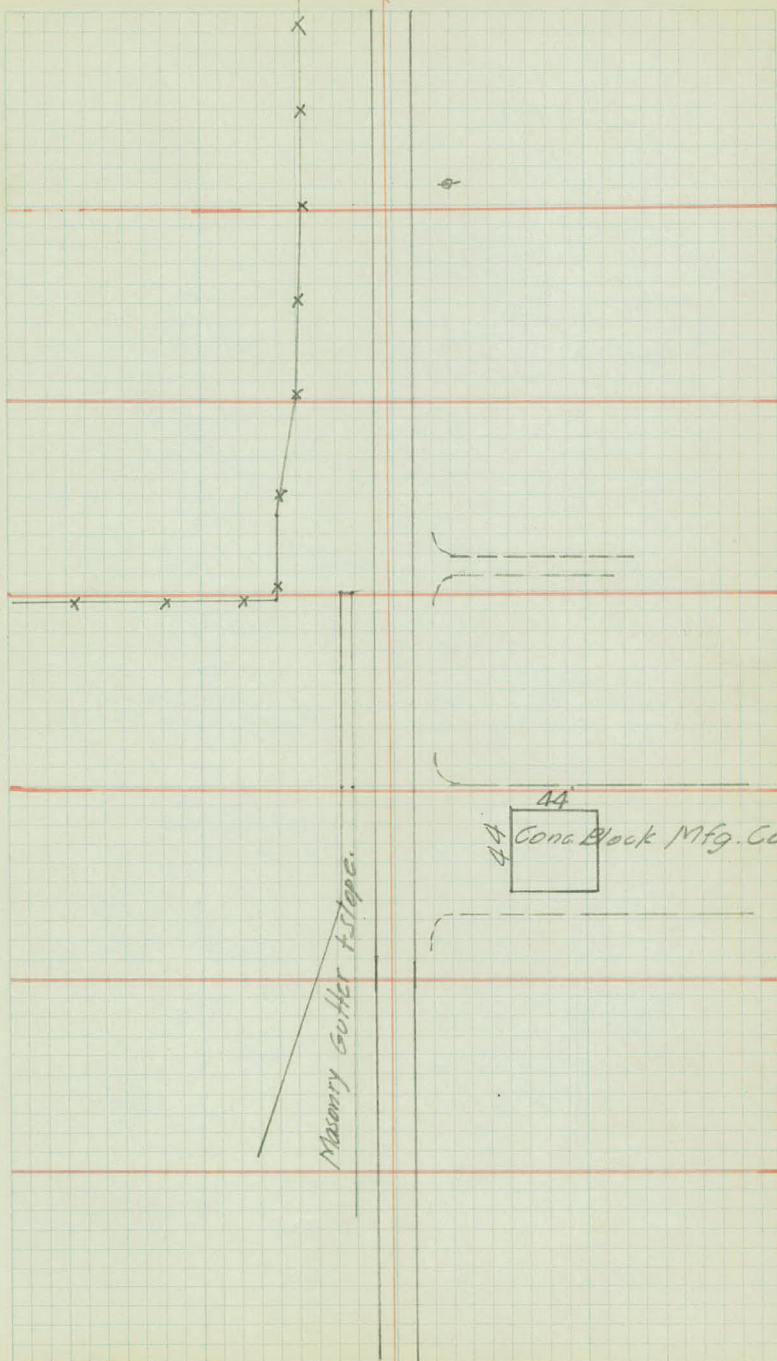
+75-Group 5-8' Willows-36'

135 Mason. Slope-28-22'

+16-P.P.-28'
Edge Ent

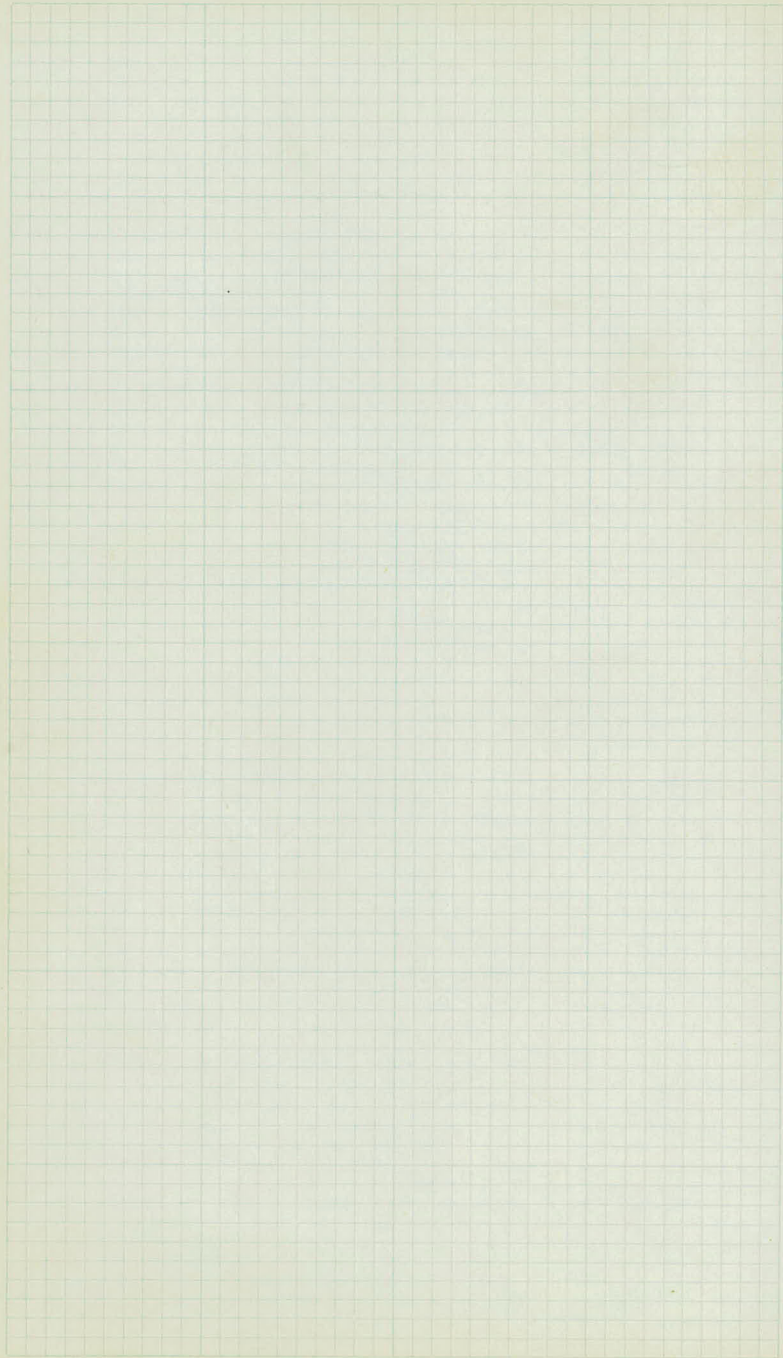
+39-Δ in Mason. Slope-29' +44-N.W. Cor. Plant-60'
+33-W. Edge Ent-

134



Masonry gutter + slope.

44'
44' Cong Block Mfg. Co.



Profile Levels Under Minn. Transfer Tracks.

Sta.	+	π	-	Elev.
B.M.	0.25	936.11.		(935.86)

3	+13.8		6.7	29.4
---	-------	--	-----	------

	+17		7.0	29.1
--	-----	--	-----	------

	+23.6		10.5	25.6
--	-------	--	------	------

	+96.9		4.9	31.2
--	-------	--	-----	------

	+89.4		7.3	29.8
--	-------	--	-----	------

	+86.6		8.9	29.2
--	-------	--	-----	------

	+83.3		11.8	24.2
--	-------	--	------	------

I.P.	0.86	923.42.	13.55	922.56.
------	------	---------	-------	---------

	+38.7		5.7	17.7
--	-------	--	-----	------

5-16-44
K.A.
L.C.
C.N.

27

Description

Spk in P.P. Rt. Sta. 6+47

Approx. W End of Bridge

Top Tie Wall

Approx. E. End of Bridge

Top of Tie Wall

Angle in Tie Wall

S/g	t	π	-	Elev.
-----	---	-------	---	-------

		923.42		
--	--	--------	--	--

3	+39.2			
---	-------	--	--	--

			11.4	
--	--	--	------	--

				12.0
--	--	--	--	------

	+44.5			
--	-------	--	--	--

			11.5	
--	--	--	------	--

				11.9
--	--	--	--	------

	+44.5			
--	-------	--	--	--

			10.6	
--	--	--	------	--

				12.8
--	--	--	--	------

	+52.25			
--	--------	--	--	--

			9.52	
--	--	--	------	--

				13.90
--	--	--	--	-------

	+57.07			
--	--------	--	--	--

			9.50	
--	--	--	------	--

				13.92
--	--	--	--	-------

	+64			
--	-----	--	--	--

			9.9	
--	--	--	-----	--

				13.5
--	--	--	--	------

	+64			
--	-----	--	--	--

			10.8	
--	--	--	------	--

				12.6
--	--	--	--	------

	+70			
--	-----	--	--	--

			11.4	
--	--	--	------	--

				12.0
--	--	--	--	------

Description

& Top West Rail

& Top East Rail

Bottom of Wall

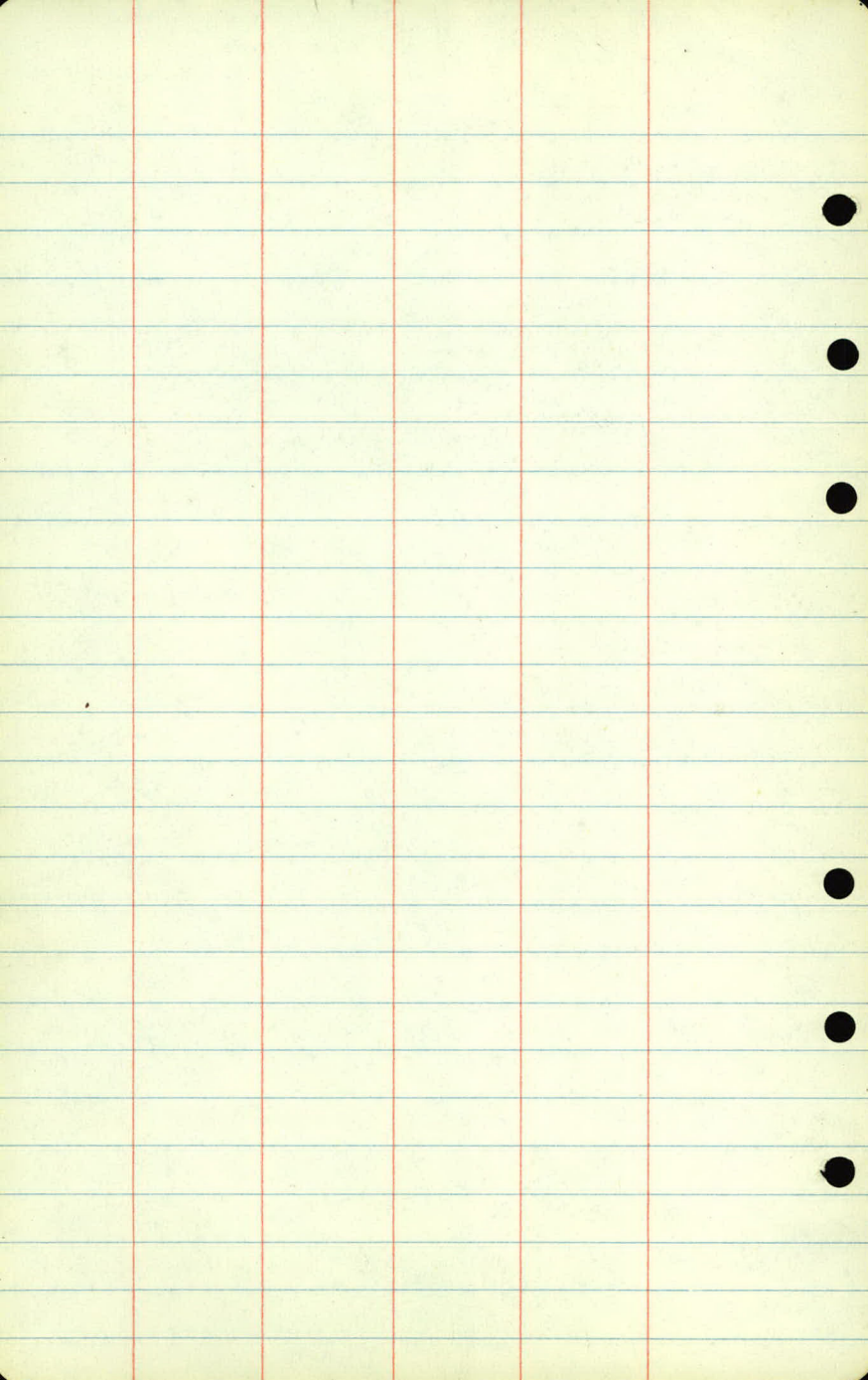
Sta.	+	π	-	Elev.
		923.42		
3 +70.5			6.4	17.0
+81.7				
T.P.	13.61	936.79	0.24	923.18
B.M.			0.93	935.86 - (935.86)

Description

Top of Wall

Bottom of Wall

Spk. in R.R. Rt. Sta. 5147

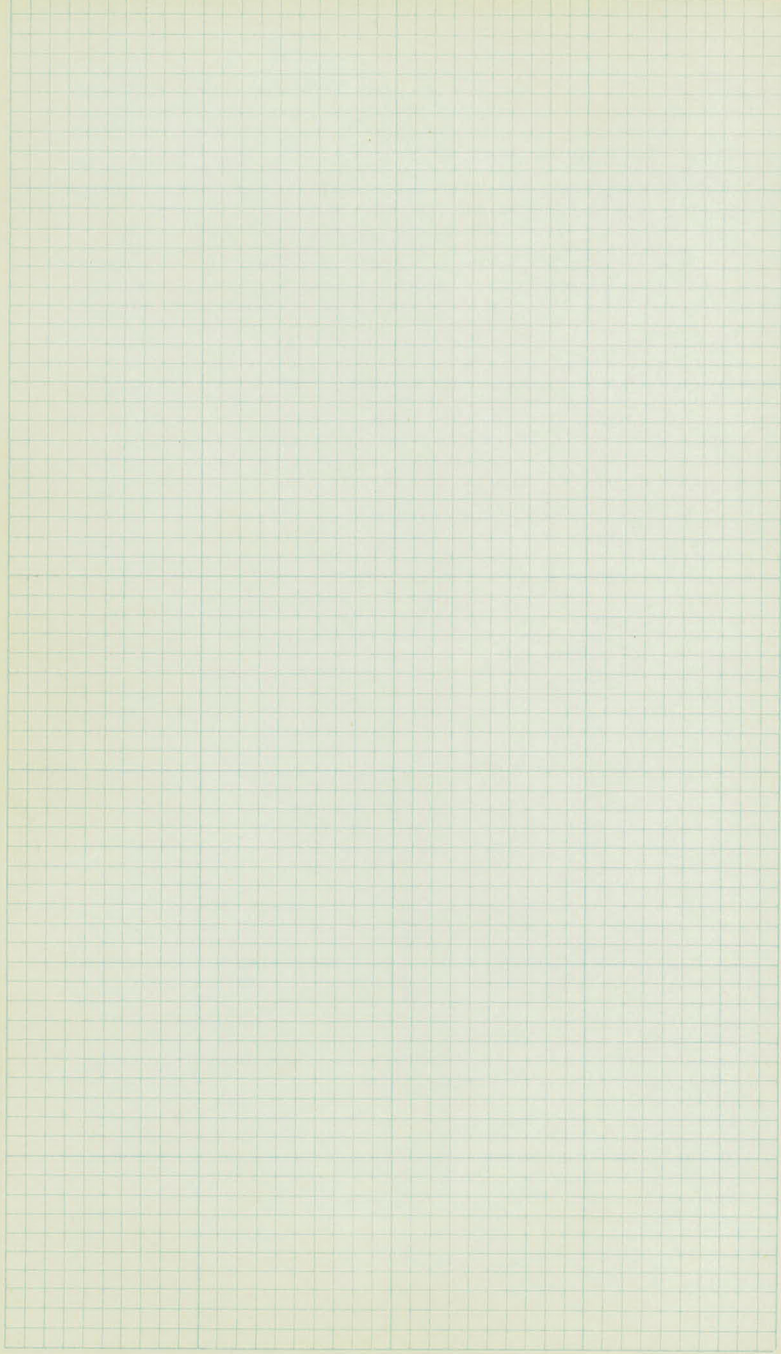


~~Pleasant St. Stone Gutter~~

Finish Topog. E. of Hamline

~~Depth of Bldg. @ Snelling~~

~~Culverts @ Fry St.~~



5-11-44

A.M

C.F

L.L

X SECTION

LARPENTUER AVE

WEST CO-LINE TO HAMLINE AVE

STA	+	π	-	ELEV	
B.M	2.95	938.81		935.86	936.21
	0.99	926.99	12.81	926.00	
B.M	2.51	924.01	5.49	921.50	921.86
T.P.	0.34	912.05	12.30	911.71	
T.P.	3.54	903.56	12.03	900.02	
T.P.	7.65	910.95	0.26	903.30	
- 4+00				895.7	
- +75				96.7	
- +50				97.8	
- +25				98.6	
- 3+00				899.7	
- +75				901.1	
- +50				02.7	
- +25				04.4	
- 2+00				06.0	
- +75				07.6	
- +50				09.3	
- +25				11.0	
T.P.	10.46	920.79	0.62	910.33	
- 1+00				12.6	
0 +76				14.1	
- +62.6	E 51			14.8	

LT

4

RT

SPIKE IN P. POLE 32 RT STA 5+47

Top IRON TOP S.W. COR STEP ENT. TO N.S.P BLDG

15.3

14.3

13.2

12.4

11.3

9.9

8.3

6.6

5.0

3.4

1.7

0.0

8.2

13.97
CURB

$\frac{6.3}{50}$	$\frac{6.8}{30}$	$\frac{6.9}{27}$	$\frac{7.0}{18}$	$\frac{6.7}{18}$	$\frac{7.3}{20}$	$\frac{7.4}{28}$	$\frac{6.82}{28}$	$\frac{6.9}{30}$	$\frac{6.9}{36}$	$\frac{7.3}{46}$	$\frac{8.3}{60}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

14.49
CURB

$\frac{6.0}{50}$	$\frac{6.4}{22}$	$\frac{6.3}{18}$	$\frac{6.0}{21}$	$\frac{6.6}{21}$	$\frac{6.8}{34}$	$\frac{6.3}{34}$	$\frac{7.0}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

STA	+	Δ	-	ELEV	
		920.79			
-0+58				15.0	
-0+50				15.2	
-0+25				16.3	
-0+10				17.1	
B.M.				916.28	916.284
0+00				17.6	
+25				18.9	
+33				19.4	
+50				20.5	
T.P	8.12	928.60	0.31	920.48	
+75				22.0	
+100				23.5	
+36				25.6	
+38				25.7	

LT

X

RT

CURB

5.7	6.1	6.1		6.4	6.5	7.0	6.55	7.3
50	30	19	5.8	21	28	46	46	50

5.4	5.8	5.9		6.1	6.2	7.2
50	30	19	5.6	20	30	50

3.3	3.6	3.7	3.1	4.4	4.7		5.0	4.7	5.2	6.9
50	35	29	26	26	19	4.5	20	25	34	50

2.5	3.0	3.2	3.2	3.8	3.9		4.2	4.0	5.0	5.9
50	35	29	26	26	19	3.7	20	22	38	50

Top of Mont. 0.00

1.3' Below Surface

1.8	3.6	3.3	3.4		3.6	3.9	5.7	7.2
50	27	27	19	3.2	18	33	50	60

0.7	1.6		1.8		2.0	2.9	3.5	5.2	7.3	9.2
50	27		13	1.9	12	21	28	39	50	60

0.4	1.1	1.3		1.5	2.2	8.9	9.8	10.3
50	22	12	1.4	13	23	40	50	60

0.0	0.1	0.3		0.4	0.8	5.9	10.3	11.0	11.2
50	20	10	0.3	10	22	33	41	50	60

7.3	7.5	6.8	6.7	6.7	6.7	7.0	7.0	11.6	15.0	15.6
50	37	37	36	19	10	6.6	10	16	21	32

Floor
B106 - N.S.P

7.1	6.4	6.2	5.4	5.4	5.2	5.2	4.9	5.2	8.4	9.3
78	50	37	37	36	33	16	10	19	22	29

4.3	4.2	3.1	3.4	2.9	3.1	3.0	3.2	3.4	2.8	2.7	4.1	4.3
50	37	37	36	32	18	10	3.0	10	19	21	31	50

3.0	3.4	2.8	2.9		3.0	3.4	2.8	2.7	4.1	4.3
50	32	18	10	2.9	10	19	21	21	50	60

STA	+	π	-	ELEV
		928.60		
1+50				26.4
B.M	7.10	928.60	7.10	921.50
				921.50
T.P	10.28	938.51	0.37	928.23
2+00				29.5
+50				32.5
+85				34.5
3+00				35.3
+13				35.9
+30				36.8
+46				37.5
+55	* BRIDGE			37.7
+63				37.9
+80				37.6
+98				37.3

LT

E

R

✓ $\frac{2.7}{50}$ $\frac{3.0}{44}$ $\frac{2.9}{30}$ $\frac{2.2}{21}$ $\frac{2.2}{15}$ $\frac{2.3}{10}$ $\frac{2.2}{10}$ $\frac{2.3}{10}$ $\frac{2.4}{16}$ $\frac{2.7}{24}$ $\frac{2.0}{32}$ $\frac{2.7}{50}$

Top JORN Top S.W. COR STEP ENT TO N.S.P. BLDG

✓ $\frac{11.5}{50}$ $\frac{12.0}{41}$ $\frac{11.2}{26}$ $\frac{9.3}{20}$ $\frac{9.0}{10}$ $\frac{9.0}{10}$ $\frac{9.1}{10}$ $\frac{9.5}{20}$ $\frac{8.2}{23}$ $\frac{9.5}{38}$ $\frac{10.1}{50}$

✓ $\frac{9.9}{50}$ $\frac{7.7}{35}$ $\frac{7.4}{30}$ $\frac{5.8}{24}$ $\frac{6.0}{16}$ $\frac{6.0}{10}$ $\frac{6.0}{10}$ $\frac{6.1}{10}$ $\frac{6.1}{16}$ $\frac{6.4}{27}$ $\frac{7.5}{36}$ $\frac{8.0}{43}$ $\frac{7.7}{50}$

✓ $\frac{3.8}{50}$ $\frac{3.2}{41}$ $\frac{5.0}{27-34}$ $\frac{3.4}{26}$ $\frac{3.3}{22}$ $\frac{4.0}{12}$ $\frac{4.0}{40}$ $\frac{4.1}{18}$ $\frac{3.9}{22}$ $\frac{4.8}{34}$ $\frac{6.8}{50}$

✓ $\frac{0.0}{50}$ $\frac{1.8}{33}$ $\frac{2.6}{24}$ $\frac{3.1}{16}$ $\frac{3.2}{10}$ $\frac{3.3}{17}$ $\frac{3.2}{22}$ $\frac{4.0}{35}$ $\frac{5.4}{50}$

✓ $\frac{6.3}{50}$ $\frac{6.2}{26}$ $\frac{2.6}{25}$ $\frac{2.5}{18}$ $\frac{2.6}{20}$ $\frac{2.7}{27}$ $\frac{5.2}{31}$ $\frac{5.9}{39}$ $\frac{7.0}{50}$

✓ $\frac{1.6}{26}$ $\frac{1.6}{20}$ $\frac{1.5}{19}$ $\frac{1.7}{10}$ $\frac{1.5}{20}$ $\frac{1.8}{21}$ $\frac{1.8}{26}$

✓ $\frac{1.1}{26}$ $\frac{1.1}{20}$ $\frac{0.9}{19}$ $\frac{1.0}{10}$ $\frac{1.0}{20}$ $\frac{1.2}{21}$ $\frac{1.2}{26}$

TOP
RAILTOP
RAIL

✓ $\frac{2.54}{26}$ $\frac{1.9}{26}$ $\frac{0.9}{20}$ $\frac{0.7}{19}$ $\frac{0.8}{10}$ $\frac{0.8}{20}$ $\frac{1.0}{21}$ $\frac{1.0}{26}$ $\frac{2.48}{26}$

✓ $\frac{0.7}{26}$ $\frac{0.7}{20}$ $\frac{0.5}{19}$ $\frac{0.6}{10}$ $\frac{0.6}{20}$ $\frac{0.7}{21}$ $\frac{0.7}{26}$

✓ $\frac{0.9}{26}$ $\frac{1.0}{20}$ $\frac{0.8}{19}$ $\frac{0.9}{10}$ $\frac{0.8}{20}$ $\frac{1.0}{21}$ $\frac{0.9}{26}$

✓ $\frac{1.2}{26}$ $\frac{1.2}{20}$ $\frac{1.1}{19}$ $\frac{1.2}{10}$ $\frac{1.2}{20}$ $\frac{1.5}{21}$ $\frac{1.5}{26}$ ✓

STA	+	∇	-	ELEV
		938.51		
T.P.	11.54	943.53	6.52	931.99
4+00				37.4
+05				37.4
+50				37.7
+75				
5				38.0
+25				
+50				38.5
+75				
+73				38.7
B.M	7.66	943.52	7.66	935.87
6+00				39.3
+22				39.7
+35				40.0
+45				40.3
+52				
		WALNUT ST	LT	40.7
+76				41.1

LT

d

RT

✓ $\frac{4.2}{50} \frac{5.3}{35} \frac{6.1}{25} \frac{6.1}{10} \frac{6.1}{10} \frac{6.3}{10} \frac{6.3}{15} \frac{6.8}{20} \frac{7.2}{28} \frac{11.4}{28} \frac{13.8}{43} \frac{14.2}{50} \frac{10.9}{58}$

✓ $\frac{4.2}{50} \frac{4.5}{44} \frac{6.1}{26} \frac{5.9}{17} \frac{6.1}{10} \frac{6.2}{10} \frac{6.2}{16} \frac{5.9}{19} \frac{7.2}{27} \frac{10.0}{33} \frac{10.2}{50}$

✓ $\frac{5.0}{50} \frac{5.5}{3.6} \frac{7.0}{30-27} \frac{6.0}{23} \frac{5.6}{19} \frac{5.8}{10} \frac{6.0}{10} \frac{5.8}{16} \frac{6.2}{22} \frac{8.0}{30} \frac{9.3}{50}$

✓ $\frac{6.8}{50} \frac{7.2}{29} \frac{5.6}{22} \frac{5.3}{17} \frac{5.6}{10} \frac{5.5}{10} \frac{5.7}{10} \frac{5.7}{13} \frac{6.0}{19} \frac{6.8}{24} \frac{8.9}{32} \frac{10.2}{50}$

✓ $\frac{7.3}{50} \frac{7.4}{28} \frac{5.1}{21} \frac{4.9}{14} \frac{5.1}{10} \frac{5.3}{5.0} \frac{5.7}{10} \frac{6.5}{18} \frac{9.9}{23} \frac{11.2}{33} \frac{12.0}{39} \frac{12.0}{50}$

✓ $\frac{7.2}{50} \frac{7.1}{39} \frac{4.8}{21} \frac{4.7}{14} \frac{4.8}{10} \frac{5.2}{4.8} \frac{5.1}{10} \frac{5.6}{14} \frac{6.7}{20} \frac{9.3}{24} \frac{11.8}{33} \frac{12.5}{41} \frac{15.2}{47} \frac{17.3}{50}$

SPIKE P.P. RT STA 54 50

✓ $\frac{6.3}{50} \frac{6.2}{28} \frac{4.2}{22} \frac{4.3}{17} \frac{4.3}{10} \frac{4.5}{4.2} \frac{4.7}{10} \frac{5.4}{18} \frac{7.7}{22} \frac{11.5}{27} \frac{14.3}{40} \frac{14.8}{60} \frac{13.6}{63} \frac{13.6}{70}$

✓ $\frac{5.1}{50} \frac{4.1}{28} \frac{3.8}{22} \frac{4.0}{15} \frac{3.8}{10} \frac{3.8}{3.8} \frac{4.1}{10} \frac{4.7}{20} \frac{7.3}{29} \frac{10.9}{33} \frac{12.6}{47} \frac{12.7}{70} \frac{11.4}{75}$

✓ $\frac{4.2}{50} \frac{4.3}{44} \frac{4.0}{34} \frac{3.6}{29} \frac{3.6}{20} \frac{3.5}{10} \frac{3.5}{3.5} \frac{3.8}{10} \frac{4.1}{20} \frac{6.6}{28} \frac{10.1}{41} \frac{11.9}{53} \frac{11.3}{61} \frac{11.7}{74}$

✓ $\frac{2.4}{50} \frac{3.2}{32} \frac{3.1}{18} \frac{3.2}{10} \frac{3.2}{3.2} \frac{3.5}{10} \frac{3.7}{21} \frac{4.9}{31} \frac{9.6}{42} \frac{11.1}{52} \frac{11.8}{56} \frac{11.7}{66} \frac{11.0}{76}$

✓ $\frac{0.8}{75} \frac{1.8}{50} \frac{2.3}{26} \frac{2.8}{10} \frac{2.8}{2.8} \frac{3.3}{10} \frac{3.4}{19} \frac{6.4}{21} \frac{9.0}{41} \frac{12.2}{53} \frac{11.0}{64} \frac{10.8}{70}$

✓ $\frac{1.9}{50} \frac{2.3}{32} \frac{2.2}{15} \frac{2.4}{10} \frac{2.4}{2.4} \frac{2.6}{10} \frac{2.9}{17} \frac{3.6}{23} \frac{6.6}{33} \frac{8.9}{47} \frac{9.5}{56} \frac{10.3}{63} \frac{10.1}{70}$

STA + π - ELEV
943.52

6+85 41.4

+94 41.7

7+00 41.8

+50 43.2

+80 44.0

8+00 11.95 44.6

T.P. 7.95 955.32 0.15 943.37

7+80 44.0

8+00 44.6

+15 45.0

+50 46.1

9+00 47.7

+50 49.1

LT

±

RT

$$\checkmark \quad \frac{2.8}{50} \quad \frac{3.3}{41} \quad \frac{2.2}{31} \quad \frac{2.2}{20} \quad \frac{2.1}{13} \quad \frac{2.2}{10} \quad 2.1 \quad \frac{2.3}{10} \quad \frac{2.3}{14} \quad \frac{3.1}{22} \quad \frac{5.6}{30} \quad \frac{7.5}{39} \quad \frac{7.5}{43} \quad \frac{9.8}{52} \quad \frac{9.8}{78}$$

$$\checkmark \quad \frac{1.2}{50} \quad \frac{1.4}{36} \quad \frac{2.0}{25} \quad \frac{2.1}{14} \quad \frac{2.0}{10} \quad 1.8 \quad \frac{2.1}{10} \quad \frac{2.2}{14} \quad \frac{2.7}{20} \quad \frac{5.6}{31} \quad \frac{7.3}{39} \quad \frac{9.2}{43} \quad \frac{9.6}{54} \quad \frac{9.5}{77}$$

$$\checkmark \quad \frac{0.9}{50} \quad \frac{1.5}{24} \quad \frac{2.0}{16} \quad \frac{1.8}{10} \quad 1.7 \quad \frac{1.9}{10} \quad \frac{2.2}{16} \quad \frac{2.7}{21} \quad \frac{4.8}{29} \quad \frac{6.9}{36} \quad \frac{8.6}{42} \quad \frac{9.3}{55} \quad \frac{9.3}{74}$$

$$\checkmark \quad \frac{4.02}{50} \quad \frac{0.3}{15} \quad \frac{0.4}{14} \quad \frac{0.4}{10} \quad \frac{0.89}{30} \quad \frac{1.2}{15} \quad \frac{3.1}{20} \quad \frac{5.7}{28} \quad \frac{7.8}{38} \quad \frac{8.0}{44} \quad \frac{8.1}{59} \quad \frac{8.1}{70}$$

$$\checkmark \quad \textcircled{+0.5} \quad \frac{0.6}{24} \quad \frac{3.2}{32} \quad \frac{4.4}{38} \quad \frac{6.0}{42} \quad \frac{6.1}{55} \quad \frac{6.0}{67}$$

$$\checkmark \quad \textcircled{+1.1} \quad \frac{1.2}{27} \quad \frac{2.6}{34} \quad \frac{4.8}{40} \quad \frac{4.7}{48} \quad \frac{4.2}{61} \quad \frac{3.0}{70}$$

$$\checkmark \quad \frac{10.8}{50} \quad \frac{11.2}{31} \quad \frac{11.4}{16} \quad \frac{11.4}{10} \quad 11.3 \quad \frac{11.5}{10} \quad \frac{12.0}{20}$$

$$\checkmark \quad \frac{10.5}{50} \quad \frac{10.6}{32} \quad \frac{10.8}{21} \quad \frac{10.8}{10} \quad 10.7 \quad \frac{10.9}{10} \quad \frac{11.3}{15} \quad \frac{11.5}{20}$$

$$\checkmark \quad \frac{10.8}{50} \quad \frac{10.5}{28} \quad \frac{10.4}{16} \quad \frac{10.3}{10} \quad 10.3 \quad \frac{10.4}{10} \quad \frac{10.8}{16} \quad \frac{11.3}{23} \quad \frac{12.5}{30} \quad \frac{12.6}{50}$$

$$\checkmark \quad \frac{9.7}{50} \quad \frac{9.4}{22} \quad \frac{9.4}{15} \quad \frac{9.2}{10} \quad 9.2 \quad \frac{9.2}{10} \quad \frac{10.5}{14} \quad \frac{9.8}{20} \quad \frac{10.2}{32} \quad \frac{8.8}{39} \quad \frac{7.6}{50}$$

$$\checkmark \quad \frac{6.8}{50} \quad \frac{7.0}{36} \quad \frac{7.6}{21} \quad \frac{7.8}{15} \quad \frac{7.6}{10} \quad 7.6 \quad \frac{8.0}{10} \quad \frac{8.3}{18} \quad \frac{8.6}{22} \quad \frac{8.5}{27} \quad \frac{7.5}{36} \quad \frac{6.4}{50}$$

$$\checkmark \quad \frac{5.9}{50} \quad \frac{6.3}{22} \quad \frac{7.0}{20} \quad \frac{6.2}{14} \quad \frac{6.3}{10} \quad 6.2 \quad \frac{6.4}{10} \quad \frac{6.6}{15} \quad \frac{6.8}{24} \quad \frac{5.0}{50}$$

STA	+	π	-	ELEV
		955.32		
9+77				49.8.
+95	$\angle$	MALVERN ST		LT 50.4.
10				50.5.
T.P.	9.78	962.88	2.22	953.10
+12				50.9.
+16				51.0.
+20				51.1.
+25				51.2.
+50				51.9.
11				53.5.
+50				54.8.
12				56.1.
+36				57.0.

L7

4

RT

$$\checkmark \quad \frac{5.8}{50} \quad \frac{5.9}{31} \quad \frac{5.6}{25} \quad \frac{6.1}{22} \quad \frac{5.7}{16} \quad \frac{5.6}{10} \quad \frac{5.6}{55} \quad \frac{5.7}{10} \quad \frac{5.7}{15} \quad \frac{5.7}{22} \quad \frac{4.0}{50}$$

$$\checkmark \quad \frac{3.8}{100} \quad \frac{4.6}{60} \quad \frac{4.6}{33} \quad \frac{4.7}{18} \quad \frac{4.9}{10} \quad \frac{4.9}{49} \quad \frac{5.2}{10} \quad \frac{5.4}{18} \quad \frac{5.2}{25} \quad \frac{4.1}{39} \quad \frac{3.6}{50}$$

$$\checkmark \quad \frac{4.5}{50} \quad \frac{4.5}{27} \quad \frac{4.6}{15} \quad \frac{4.8}{10} \quad \frac{4.8}{48} \quad \frac{5.0}{10} \quad \frac{5.3}{20} \quad \frac{4.5}{32} \quad \frac{3.6}{50}$$

$$\checkmark \quad \frac{12.4}{50} \quad \frac{12.6}{42} \quad \frac{12.8}{28} \quad \frac{12.8}{26} \quad \frac{12.0}{15} \quad \frac{12.0}{10} \quad \frac{12.0}{12.0} \quad \frac{12.2}{10} \quad \frac{12.3}{16} \quad \frac{12.3}{34} \quad \frac{11.0}{50}$$

$$\checkmark \quad \text{WALK} \quad \frac{11.9}{50} \quad \frac{12.1}{41} \quad \frac{12.1}{28} \quad \frac{12.0}{25} \quad \frac{12.9}{23} \quad \frac{12.1}{24} \quad \frac{11.9}{21} \quad \frac{11.9}{15} \quad \frac{11.9}{10} \quad \frac{11.9}{11.9} \quad \frac{12.2}{10} \quad \frac{12.3}{16} \quad \frac{12.3}{34} \quad \frac{11.0}{50}$$

$$\checkmark \quad \text{WALK} \quad \frac{12.0}{50} \quad \frac{12.0}{28} \quad \frac{12.0}{23} \quad \frac{12.9}{21} \quad \frac{12.2}{20} \quad \frac{11.8}{18} \quad \frac{11.8}{10} \quad \frac{11.8}{11.8} \quad \frac{11.9}{10} \quad \frac{12.1}{15} \quad \frac{12.2}{21} \quad \frac{11.7}{32} \quad \frac{10.9}{58}$$

$$\checkmark \quad \text{WALK} \quad \frac{10.4}{50} \quad \frac{10.5}{37} \quad \frac{11.8}{38} \quad \frac{11.9}{28} \quad \frac{11.8}{23} \quad \frac{12.5}{20} \quad \frac{11.9}{19} \quad \frac{11.7}{16} \quad \frac{11.7}{10} \quad \frac{11.7}{11.7} \quad \frac{11.8}{10} \quad \frac{11.8}{15} \quad \frac{12.0}{20} \quad \frac{11.3}{30} \quad \frac{9.3}{50}$$

$$\checkmark \quad \text{WALK} \quad \frac{9.4}{50} \quad \frac{9.9}{38} \quad \frac{11.0}{33} \quad \frac{11.0}{28} \quad \frac{11.3}{32} \quad \frac{11.5}{20} \quad \frac{11.0}{19} \quad \frac{11.0}{17} \quad \frac{11.0}{10} \quad \frac{11.0}{11.0} \quad \frac{11.1}{10} \quad \frac{11.2}{15} \quad \frac{11.2}{25} \quad \frac{10.1}{30} \quad \frac{9.1}{50}$$

$$\checkmark \quad \frac{8.2}{50} \quad \frac{9.0}{31} \quad \frac{9.5}{23} \quad \frac{9.8}{20} \quad \frac{9.8}{19} \quad \frac{9.6}{18} \quad \frac{9.4}{10} \quad \frac{9.4}{9.4} \quad \frac{9.6}{10} \quad \frac{9.5}{18} \quad \frac{9.6}{25} \quad \frac{7.7}{40} \quad \frac{7.6}{50}$$

$$\checkmark \quad \frac{7.7}{50} \quad \frac{7.7}{33} \quad \frac{8.1}{22} \quad \frac{8.3}{17} \quad \frac{8.1}{16} \quad \frac{8.1}{15} \quad \frac{8.1}{10} \quad \frac{8.1}{8.1} \quad \frac{8.3}{10} \quad \frac{8.2}{15} \quad \frac{8.2}{21} \quad \frac{7.4}{31} \quad \frac{6.7}{50}$$

CONC
DRIVECONC
DRIVE

$$\checkmark \quad \frac{6.2}{50} \quad \frac{6.0}{33} \quad \frac{6.8}{21} \quad \frac{7.1}{17} \quad \frac{6.9}{16} \quad \frac{6.8}{14} \quad \frac{6.8}{10} \quad \frac{6.8}{6.8} \quad \frac{6.9}{10} \quad \frac{7.0}{21} \quad \frac{6.5}{33} \quad \frac{6.2}{50}$$

CONC
DRIVE CURB

$$\checkmark \quad \frac{4.7}{50} \quad \frac{5.1}{33} \quad \frac{5.3}{27} \quad \frac{6.1}{18} \quad \frac{5.9}{10} \quad \frac{5.9}{5.9} \quad \frac{6.0}{10} \quad \frac{6.3}{15} \quad \frac{5.9}{26} \quad \frac{5.6}{38}$$

STA	+	Δ	-	ELEV
		962.88		
12+42				57.2 .
+50				57.3 .
+82				58.1 .
+94				58.3 .
13				58.6 .
T.P	8.21	965.34	5.75	957.13.
B.M	487	965.25	4.95	960.39 960.38
+11	⊕	EUSTIS ST LT		58.9 .
				*
+22	⊕	EUSTIS ST. RT		59.2 .
+38	SECTION 18" X 126' C.M. X DRAIN			59.5 .
+50				59.8 .
+85				60.5 .
14				60.7 .
+30				61.2 .

	LT				♀				RT			
	CONE DRIVE				WALK CURB							
✓	4.5	5.0	5.1	5.5	6.0	5.8	5.7	5.9	6.1	5.7	5.6	
	50	38	27	18	18	10	5.7	10	15	26	37	
✓	WALK CURB											
	4.3	4.4	4.0	4.2	4.7	4.9	5.2	5.8	5.6	5.6		
	50	38	34	33	27	18	18	15	10	5.6	5.7	5.6
										10	15	26
												37
	WALK CURB								WALK			
✓	3.7	3.8	3.9	4.1	4.4	5.0	4.7	4.8	4.9	4.9	4.6	4.3
	50	38	33	27	18	18	10	4.8	10	17	29	37
												3.85
												37
	WALK CURB								WALK			
✓	3.9	4.0	3.9	3.9	4.1	4.5	4.5	4.6	4.6	5.2	4.7	4.6
	50	38	33	27	22	22	10	4.6	10	12	23	29
												37
												5.0
												5.0
✓	3.6	3.9	4.2	4.3				4.3	4.4	4.5	5.0	5.6
	50	34	17	10				4.3	10	15	23	30
												4.3
												5.0

TOP HYDRANT S.W. COR. CARPENTEUR ⁵⁰⁵ ST. ¹⁸

✓	3.6	4.2	5.0	5.6	6.2	6.4	6.4	6.6	7.0	8.3	9.0	
	200	150	100	50	18	10	4.4	10	18	32	50	

✓	5.6	5.7	6.0	6.2	6.1	6.3	7.2	8.6	10.1	11.7	13.2	15.0
	50	24	18	10	6.1	10	25	50	75	100	125	150

54.262

FL C.B.

FL 52.26

✓	5.6	5.9	10.99	6.4	6.0	5.8	6.0	7.0	9.1	12.97		
	50	40	32	32	27	10	5.8	10	23	50	94	

✓	4.6	5.0	5.7	5.8	5.6	5.5	5.7	5.8	6.0	5.6	5.5	6.0
	50	36	27	23-24	18	10	5.5	10	12	18	20	32
												50

60.95 FLOOR TAVERN

✓	4.3	4.4	4.9	5.2	5.1	4.9	4.8	5.0	5.1	5.3	6.9	
	57	50	34	27-25	18	10	4.8	10	17	35	50	

✓	4.5	4.8	5.0	4.8	4.6	4.6	4.7	4.9	5.5	6.9	7.8	
	50	36	19-17	19	10	4.6	10	20	10	41	50	
												30

✓	4.0	4.5	4.5	4.3	4.1	4.1	4.2	4.5	6.7	8.3	9.8	10.2
	50	23	21	15	10	4.1	10	21	30	36	50	60

STA	+	Δ	-	ELEV
		965.25.		

14+32				61.3 . .
-------	--	--	--	----------

+50				61.5 . .
-----	--	--	--	----------

T.P.	6.91	969.40	2.76	962.49.
------	------	--------	------	---------

15	+17			62.1 .
----	-----	--	--	--------

	+17			62.4 .
--	-----	--	--	--------

	+44			62.7 .
--	-----	--	--	--------

	+69			63.0 .
--	-----	--	--	--------

16				63.4 .
----	--	--	--	--------

	+17			63.7 .
--	-----	--	--	--------

LT

F

RT

✓ $\frac{2.7}{50}$ $\frac{3.0}{36}$ $\frac{4.0}{25}$ $\frac{4.5}{23-21}$ $\frac{4.3}{75}$ $\frac{4.0}{10}$ $\frac{4.0}{10}$ $\frac{4.1}{10}$ $\frac{4.5}{20}$ $\frac{6.7}{30}$ $\frac{8.3}{36}$ $\frac{9.8}{50}$ $\frac{10.2}{60}$

✓ $\frac{2.0}{50}$ $\frac{3.1}{34}$ $\frac{3.7}{24}$ $\frac{4.1}{21-19}$ $\frac{4.0}{17}$ $\frac{3.8}{10}$ $\frac{3.8}{10}$ $\frac{4.8}{10}$ $\frac{4.4}{19}$ $\frac{6.4}{25}$ $\frac{10.1}{34}$ $\frac{11.5}{50}$ $\frac{12.3}{60}$

✓ $\frac{6.5}{50}$ $\frac{6.9}{38}$ $\frac{7.8}{27}$ $\frac{7.6}{21}$ $\frac{7.3}{10}$ $\frac{7.3}{10}$ $\frac{7.6}{10}$ $\frac{8.2}{19}$ $\frac{14.8}{32}$ $\frac{15.5}{50}$ $\frac{15.5}{60}$

✓ $\frac{6.2}{50}$ $\frac{7.0}{31}$ $\frac{7.0}{10}$ $\frac{7.0}{10}$ $\frac{7.3}{10}$ $\frac{7.8}{18}$ $\frac{13.1}{22}$ $\frac{13.9}{36}$ $\frac{13.4}{50}$ $\frac{13.0}{60}$

(Drive)

✓ $\frac{6.4}{53}$ $\frac{7.1}{27}$ $\frac{6.7}{10}$ $\frac{6.7}{10}$ $\frac{6.8}{10}$ $\frac{6.9}{17}$ $\frac{7.7}{46}$ $\frac{8.1}{60}$

✓ $\frac{7.7}{60}$ $\frac{7.4}{42}$ $\frac{6.7}{27}$ $\frac{7.1}{25}$ $\frac{6.4}{10}$ $\frac{6.4}{10}$ $\frac{6.6}{20}$ $\frac{6.7}{22}$ $\frac{7.3}{33}$ $\frac{7.2}{60}$ $\frac{6.7}{60}$

✓ $\frac{9.4}{200}$ $\frac{9.7}{150}$ $\frac{9.3}{100}$ $\frac{8.2}{60}$ $\frac{7.3}{36}$ $\frac{6.1}{19}$ $\frac{6.0}{10}$ $\frac{6.0}{10}$ $\frac{6.2}{10}$ $\frac{6.4}{20}$ $\frac{7.1}{23}$ $\frac{6.7}{31}$ $\frac{6.7}{60}$

Profile Carl St. →

✓ $\frac{7.7}{60}$ $\frac{7.2}{50}$ $\frac{6.5}{34}$ $\frac{6.0}{19}$ $\frac{6.3}{18}$ $\frac{5.8}{10}$ $\frac{5.7}{10}$ $\frac{5.9}{10}$ $\frac{6.0}{20}$ $\frac{6.5}{22}$ $\frac{6.4}{34}$ $\frac{6.6}{60}$

Sta	+	π	-	Elev
		969.40		
16	+36			64.0
	+67			64.4
T.P	9.24	971.73	6.91	962.49
17				64.8
	+43			65.3
	+59			65.5
18				66.0
	+38			66.5
	+44			66.6

Lt.

L

Rt.

✓ 5.8 5.1 4.4 6.0 5.5 5.5 5.3 5.4 5.6 5.7 6.6 6.6 6.5 6.5
60 50 36 26 23 18 10 10 19 23 29 50 60

✓ 3.9 3.2 3.2 3.6 5.2 4.9 4.9 5.0 5.2 5.5 6.1 6.4 6.8 6.7
60 50 40 34 24 20 10 10 19 21 26 50 60

✓ 5.5 5.8 6.8 6.8 6.9 7.2 7.4 8.2 8.6 9.3 9.5
50 43 22 10 10 20 22 31 50 60

✓ 5.8 6.6 6.4 6.4 6.7 7.2 7.7 9.3 10.5 10.8
50 21 10 10 17 26 45 51 60

✓ 5.8 6.0 6.2 6.2 6.5 6.9 7.0 9.6 10.4 11.1
50 20 10 10 11 21 31 40 60

✓ 5.4 5.7 5.7 5.7 6.0 6.3 6.4 11.1 11.4 11.8 12.0
50 22 10 10 11 20 32 39 50 60

✓ 5.1 5.2 5.2 5.2 5.5 5.7 6.1 10.6 10.7 11.5
50 20 10 10 11 21 35 43 60

✓ 7.4 6.2 5.0 5.1 5.1 5.4 Duplicate + 38
50 32 20 10 10

Sta	+	π	-	Elev
		971.73		

18	+18			67.0
----	-----	--	--	------

	+84			67.1
--	-----	--	--	------

+95 Profile of Ditch Rt

19				67.3
----	--	--	--	------

	+35			67.6
--	-----	--	--	------

	+62			67.9
--	-----	--	--	------

	+91.72 = Pleasant St			68.5
--	----------------------	--	--	------

20				68.6
----	--	--	--	------

Lt.

E

Rt.

✓

7.3 7.5 6.9 4.9 4.7 4.7 4.9 5.2 5.3 9.0 10.0 10.7
60 43 31 20 10 10 11 21 34 50 60

✓

4.9 5.1 4.6 4.6 4.6 4.8 Duplicate + 78
50 23 19 10 10

(No Seed)

112 121 140 159
43 60 100 150

✓

4.7 4.7 4.4 4.5 4.4 4.6 4.8 5.1 7.4 8.5 10.7 10.8 9.0 10.3
53 22 18 10 10 11 21 29 32 34 32 39 60
Ditch

✓

4.6 4.8 3.9 4.2 4.1 4.3 4.7 4.9 8.2 9.5 9.5 8.3 7.9 8.1 10.0
50 22 18 10 10 22 29 33 33 34 38 40 41 60
Ditch

✓

3.7 4.4 3.7 3.4 3.9 3.8 3.9 4.1 6.0 8.6 8.6 7.4 7.1 7.6 9.0
60 34 30 12 10 10 29 31 33 36 38 40 48 60

Make Left hand side X

✓

3.2 3.2 3.0 2.5 1.9 1.4 1.2
10 11 50 100 150 200

Sta	+	π	-	Elev	
		971.73			
20 +06				68.7	
+09				68.7	*
+12				68.8	
+17				68.9	
+45 X Drain		24" cone		69.3	
T.P.	8.77	977.53	2.97	968.76	
+50				69.3	
+78				69.6	
21				69.9	

L f.

 $\mathbb{Z}$

23

✓

2.6 2.3 2.7 2.8 3.0 3.0 3.2 3.5 4.8 5.6 7.6 7.6 6.6 6.4 8.5
6.0 3.7 2.7 1.4 1.0 1.0 2.2 2.7 3.1 3.3 3.6 1.3 1.7 3.9 6.0

✓

40 41 21 24 28 30 30 32 Duplicate + 06
60 48 43 26 21 10 10

✓

40	41	20	25	28	29	29	32	35	52	54	75	75	65	64	85
60	48	43	22	18	10		10	22	28	31	33	35	37	39	60

✓

15 20 40 4025 28 28 28 30 34 47 52 74 74 64 62 71 83
60 33 30 25 21 16 10 10 32 36 30 33 36 37 39 50 60

✓

14	19	13	20	51	52	22	25	24	26	30	42	67	68	55	78
60	44	39	34	29	24	22	10	10	22	29	30	34	36	60	
					CUV					HV		CUV			



6.9	7.5	7.0	8.0	10.3	10.3	8.2	8.2	8.2	8.4	8.6	9.8	11.6	13.1	14.0
6.0	4.4	3.9	3.3	2.9	2.6	2.1	1.0		1.0	2.1	2.6	3.5	5.2	6.0

✓

6.4	6.8	6.3	6.5	9.9	9.8	8.2	7.9	7.9	8.0	8.5	9.6	11.2	12.5	13.5
6.0	4.8	4.2	3.5	3.0	2.5	2.1	1.0		1.0	2.0	2.6	3.7	5.1	6.0

✓

47	50	59	56	54	97	97	80	77	76	77	79	94	108	136
75	60	49	44	35	29	24	21	10		10	21	27	34	60

Sta	+	π	-	Elev.
		977.53		
21	+28			70.3
	+57			70.5
	+78			70.7
22				70.9
	+50			71.3
23				71.8
I.P.	5.73	977.90	5.36	972.17
	+50			72.2
24				72.4

Lt.

E

Rt.

✓
 2.6 37 44 44 36 24 24 94 95 7.7 7.3 7.2 7.4 7.6 108 124 138
 70 55 51 46 43 42 39 30 25 22 10 10 22 34 45 50

✓
 06 13 18 27 98 08 88 90 74 7.0 70 7.0 7.5 114 125 136
 70 60 53 45 44 40 28 24 21 10 10 21 33 45 60

✓
 0.7 1.0 16 15 1.7 5.6 5.9 8.6 8.6 7.2 6.9 6.8 6.9 7.4 11.3 13.7
 70 60 50 46 41 36 33 29 24 21 10 10 22 34 60

✓
 14 1.7 23 23 25 8.6 8.6 7.0 6.7 6.6 6.7 7.4 11.6 12.8 13.5
 70 60 49 44 36 28 24 21 10 10 23 34 49 60

✓
 2.3 2.6 3.2 3.2 3.4 8.0 8.0 6.7 6.2 6.2 6.3 6.9 11.9 13.9
 70 60 46 40 34 28 24 21 10 10 22 35 60

✓
 3.7 3.9 3.8 7.6 7.6 6.2 5.8 5.7 6.2 6.7 11.8 12.9
 60 45 34 28 24 21 10 19 22 35 60

✓
 5.0 4.6 5.2 7.8 7.8 5.7 5.7 5.7 5.9 6.2 6.8 11.7 12.4
 60 41 33 28 24 20 10 10 18 22 36 60

✓
 4.2 4.1 3.9 7.9 7.9 5.7 5.6 5.5 5.7 5.9 6.3 10.2 11.4
 60 41 33 27 24 20 10 10 20 24 37 60

Sta.	+	π	-	Elev
		977.90		

24 + 31				72.6
---------	--	--	--	------

+63				72.9
-----	--	--	--	------

25				73.1
----	--	--	--	------

+31				73.4
-----	--	--	--	------

25 +53 Profile of low land

+75				73.8
-----	--	--	--	------

26				74.0
----	--	--	--	------

+11				74.1
-----	--	--	--	------

Lt

E

Pt

✓ 3.2 29 27 79 79 55 53 53 54 56 60 95 101 108
60 43 33 27 24 20 10 10 18 22 36 50 60

✓ 48 48 50 45 78 78 52 51 50 52 54 56 91 100
60 50 41 32 28 25 21 10 10 17 23 37 60

✓ 76 71 64 82 82 52 48 48 49 52 54 88 92 90
60 43 32 28 25 21 10 10 18 22 36 51 60

✓ 82 82 79 74 80 80 55 50 46 45 46 48 53 71 80 84
60 44 37 30 28 25 21 18 10 10 19 23 30 35 60

No

75 84 84 82 100
150 100 78 50
75
FL.
6" Tile

Tile drains into draw

approx. 300' so. of E.

✓ 78 75 75 44 68 68 53 46 43 41 42 44 48 71 83 86 85
60 44 35 30 28 24 21 17 10 10 18 22 31 40 50 60

✓ 60 55 40 40 58 59 42 40 39 40 42 45 84 87
60 54 37 34 29 24 19 10 10 18 24 32 60

✓ 43 37 34 56 57 41 39 38 39 41 47 57 65
60 52 32 29 23 20 10 10 19 33 48 60

Sta	+	π	-	Elev
		977.90		
26 + 16				74.2
+22				74.2
+26				74.2
+41.78	Profile of Fulham St. Lt.			74.4
B.M.	575	980.25	3.47	974.53 ⁴³ 43
				(974.50)
+57				74.7
+66				74.8
+72				74.8
+78				74.9

5-9-44
F.P.
L.C.
C.N.
C.F.
C.L.

44

Lt.

E

Rt.

✓

5.2 55 40 39 37 39 41 47 55 64
60 30 24 10 10 18 31 44 60

✓

5.0 50 36 36 38 37 Duplicate +16
60 44 33 11 10

✓

34 33 34 37 37 41 46 52 61
60 38 12 10 18 26 40 60

✓

18 23 26 29 33 36 37 36 40 58 88 113 112
200 150 100 50 11 10 10 18 25 33 46 60

4 Pavement Top from S 1/4 Cor Sec. 17

✓

5.5 56 55 58 56 57 63 67 111 128 132
60 35 11 10 10 18 22 34 48 60

✓

67 70 69 58 57 57 55 56 63 67 111 121 133
60 39 34 26 15 10 10 18 22 34 42 60

✓

42 42 63 70 58 57 55 55 63 66 109 118 128
60 36 30 24 21 10 10 18 22 33 41 60

✓

39 39 67 67 58 56 54 55 60 66 104 106 106
60 36 26 24 22 10 10 18 23 33 44 60

Sta	+	π	-	Elev
		980.25		
27				75.0
				*
+35				75.3
+75				75.5
28				75.6
+90				75.8
+75				75.9
29.				76.0

Lt.

E

Rt.

✓ 3.0 3.4 3.3 6.4 6.9 5.6 5.5 5.3 5.4 5.7 6.5 10.4 10.3
75 56 35 25 23 20 10 10 18 24 36 60

✓ 1.6 2.4 2.7 3.5 6.0 6.0 5.4 5.2 5.0 5.1 5.5 6.2 9.9 10.3 10.2
75 52 36 33 25 23 20 10 10 19 24 36 48 60

✓ 1.1 1.3 2.0 5.8 5.8 5.2 4.9 4.8 5.0 5.5 6.1 10.2 10.9 10.8
75 46 36 25 23 20 10 10 19 23 34 39 60

✓ H.2 0.1 1.8 5.6 5.6 4.9 4.8 4.7 4.8 5.1 5.5 10.3 10.6 10.7
75 42 35 25 23 20 10 10 11 20 36 47 60

✓ 12.8 12.0 11.5 0.5 2.2 5.0 5.0 4.5 4.7 4.5 4.5 5.3 8.6 10.0 10.7
75 62 55 40 33 25 23 20 10 10 20 33 44 60

✓ 14.6 12.4 0.0 0.9 5.3 5.3 4.6 4.4 4.4 4.4 4.8 5.3 8.8 10.3 14.4
75 53 40 37 25 23 20 10 10 19 22 35 46 100

Drain SW. 23.6 21.6 18.0
250 200 150

✓ 14.6 13.6 11.8 1.0 5.3 5.3 4.7 4.5 4.3 4.4 4.6 5.0 7.2 8.3 11.1
75 62 49 37 25 23 20 10 10 19 22 30 41 60

Sta	+	π	-	Elev
		980.25		

29 +50				76.1
--------	--	--	--	------

+82				76.0
-----	--	--	--	------

30				76.0
----	--	--	--	------

+37				75.8
-----	--	--	--	------

+70				75.7
-----	--	--	--	------

31				75.8
----	--	--	--	------

T.P.	4.28	979.90	4.63	975.62
------	------	--------	------	--------

+50				75.7
-----	--	--	--	------

32				75.4
----	--	--	--	------

Lt.

Z

Rt.

✓

+4.5 +4.0 +3.9 +1.2 0.0 5.2 5.2 4.5 4.3 4.2 4.3 4.6 6.3 6.4 5.2 5.0 9.1
 100 75 60 45 41 25 23 20 20 10 19 22 29 34 35 60

✓

+6.3 +3.4 +2.7 +1.0 1.8 5.1 5.1 4.6 4.4 4.3 4.5 4.7 4.5 6.9 5.7 6.8 9.2
 100 70 55 44 35 25 23 20 10 10 21 26 30 33 43 60

✓

+4.3 +3.8 +2.4 +1.0 1.3 5.3 5.3 4.6 4.4 4.3 4.4 4.6 5.0 7.2 6.6 10.0
 100 75 60 45 37 25 23 20 10 10 18 22 29 38 60

✓

+4.0 +4.2 +1.7 1.1 4.3 5.6 4.8 4.5 4.5 4.6 5.1 7.5 11.4 12.4 12.8
 100 74 49 38 28 23 20 10 10 18 26 36 47 60

✓

+3.5 +2.0 0.0 3.5 5.7 5.7 5.0 4.7 4.6 4.8 5.5 8.2 12.1 13.0 13.3
 75 60 45 32 25 23 19 10 10 18 27 29 50 60

✓

+2.9 0.4 1.1 2.5 3.8 5.9 5.9 5.0 4.6 4.5 4.8 5.1 5.5 6.3 11.2 12.3 13.0
 75 60 50 40 34 25 23 19 10 10 11 18 22 27 36 60

✓

3.2 3.6 4.2 5.1 5.2 4.6 4.4 4.2 4.4 4.6 4.9 5.8 8.8 9.8 11.2
 70 50 40 28 23 20 10 10 11 18 23 32 41 60

✓

4.0 4.7 5.2 4.6 4.4 4.5 4.6 4.9 5.0 5.8 8.1 9.4 10.3
 60 27 21 19 10 10 12 19 24 30 45 60

Sta	+	π	-	Elev	
		979.90			
B.M.			6.49	973.41	978.35
32 + 33				75.5	.
+80				75.3	.
33				75.5	.
+50				75.7	.
34				76.0	.
+50				76.6	.
35				77.4	.
I.P.	6.27	984.18	1.99	977.91	.
+50				78.0	.

5-9-44
K.A.
L.C.
C.N.
L.L.
C.F.

47

Lt

E

Rt.

Top Hyd Lt sta 32+02

✓ 53 53 64 66 48 45 44 47 49 54 86 92 102
60 55 31 26 21 10 10 12 21 30 45 60

✓ 9.20 6.8 6.9 8.9 8.7 4.7 4.6 4.6 5.0 5.3 5.9 8.4 8.9 8.6 10.35
FL 15" Culv. 28.6 60 53 34 32 20 10 10 19 24 31 45 60 FL 15" Culv. 28.6

✓ 7.4 7.3 8.1 8.3 4.8 4.5 4.4 4.8 5.1 5.8 8.5 8.5 7.6
60 55 42 32 21 10 10 19 23 32 41 60

✓ 7.7 7.5 7.1 4.7 4.2 4.2 4.5 4.7 4.9 5.5 7.4 7.1 6.3
60 36 29 21 10 10 11 18 23 30 43 60

✓ 7.3 6.6 4.6 4.1 4.0 3.9 4.1 4.3 4.4 4.8 5.9 6.3 6.3 5.6 5.1 4.2
60 30 24 21 10 10 11 18 22 25 28 32 34 33 60 43

✓ 6.9 6.4 6.2 3.7 3.4 3.3 3.5 3.8 4.2 5.7 5.7 5.1 4.4
60 31 29 21 10 10 11 22 29 31 35 60

✓ 4.3 3.7 4.7 4.7 2.8 2.8 2.5 2.7 3.0 3.1 3.7 5.3 5.3 4.8 3.9
60 33 30 27 22 10 10 11 18 23 19 23 35 60
29 33

✓ 2.5 7.1 6.3 7.8 2.6 6.5 6.2 6.3 6.3 6.2 6.5 6.6 7.1 8.1 8.1 7.5 8.0
60 36 33 30 26 22 19 15 10 6.2 10 11 19 22 25 31 33 60

Sta	+	π	-	Elev
		984.18		
36+00				78.6
+50				79.1
37				79.3
+50				79.5
+70				79.5
38				79.5
+50				79.4
39				79.3
+50				79.1
40				78.9
+09	SECTION 24"X67' CONC X DRAIN			78.9
+50				78.9

L.A.

2

Ref.

✓ $\frac{6.4}{60} \frac{6.0}{36} \frac{5.6}{33} \frac{7.4}{29} \frac{7.5}{76} \frac{6.4}{23} \frac{5.8}{17} \frac{5.6}{10} \frac{5.7}{5.6} \frac{5.8}{10} \frac{5.9}{11} \frac{6.7}{20} \frac{9.9}{28} \frac{11.3}{40} \frac{11.3}{53}$

✓ 2.5 5.4 5.5 1.8 3.7 6.8 6.0 5.5 5.2 5.2 5.6 6.1 8.1 2.8 7.3 6.8 7.0
66 60 54 48 33 28-25 22 19 10 51 10 20 26 37 40 57 53 60

✓ $\frac{3.7}{60}$ $\frac{3.0}{34}$ $\frac{7.0}{29-26}$ $\frac{5.1}{20}$ $\frac{4.9}{10}$

4.9 5.1 5.4 6.0 8.1 8.7 7.6 7.0 4.1 4.7
4.9 10 11 21 25 32 33 36 38 48 59 65

✓ $\frac{6.0}{60}$ $\frac{5.5}{47}$ $\frac{5.0}{33}$ $\frac{4.5}{30.77}$ $\frac{5.1}{28}$ $\frac{4.9}{19}$ $\frac{4.8}{10}$ $\frac{4.8}{47}$ $\frac{5.0}{10}$ $\frac{5.1}{19}$ $\frac{5.5}{25}$ $\frac{7.9}{34}$ $\frac{8.7}{36}$ $\frac{8.3}{44}$ $\frac{7.8}{52}$ $\frac{5.8}{60}$ $\frac{5.1}{65}$

$\frac{7.1}{60} \quad \frac{6.4}{33} \quad \frac{6.8}{32-28} \quad \frac{5.3}{21} \quad \frac{4.9}{19} \quad \frac{4.8}{10} \quad 4.7 \quad \frac{4.8}{10} \quad \frac{5.0}{11} \quad \frac{5.1}{21} \quad \frac{5.5}{24} \quad \frac{8.5}{36-39} \quad \frac{8.1}{40} \quad \frac{8.4}{56} \quad \frac{8.1}{57} \quad \frac{5.3}{70}$

✓ $\begin{array}{cccccccccccccccccccc} \underline{6.2} & \underline{8.0} & \underline{7.9} & \underline{7.2} & \underline{5.2} & \underline{4.9} & \underline{4.8} & \underline{4.9} & \underline{5.2} & \underline{5.5} & \underline{7.4} & \underline{7.6} & \underline{8.1} & \underline{7.9} & \underline{8.0} & \underline{8.2} & \underline{8.0} & \underline{4.6} \\ 60-58 & 56 & 36 & 28 & 22 & 19 & 10 & 4 & 7 & 10 & 20 & 24 & 32 & 35 & 37-39 & 41 & 50 & 58 & 60 & 76 \end{array}$

✓ $\frac{6.4}{60} \frac{6.6}{57} \frac{10.0}{56} \frac{9.6}{34} \frac{5.8}{22} \frac{5.0}{17} \frac{4.9}{10} \frac{5.1}{48} \frac{5.1}{10} \frac{5.1}{11} \frac{5.5}{20} \frac{6.9}{23} \frac{6.7}{32} \frac{6.7}{60}$

✓

10.7	10.6	10.4	9.9	6.4	5.3	5.0	4.9	5.1	5.4	5.5	5.9	7.7	8.6	9.3
60	46	36	33	28	19	10	4.9	10	11	20	24	31	36	60

✓	10.2	9.5	9.4	5.8	5.3	5.1	6.3	5.5	5.7	7.0	10.5	11.0	11.4	
	60	33	31	22	19	10	5.1	10	11	20	27	37	41	60

✓ $\frac{9.6}{60} \frac{9.8}{40} \frac{9.7}{35} \frac{5.6}{24} \frac{5.1}{18} \frac{5.4}{10} \frac{5.3}{5.3} \frac{5.6}{10} \frac{5.7}{19} \frac{5.9}{27} \frac{10.9}{38} \frac{11.6}{43} \frac{11.9}{60}$

74.38 - F.L.

FL 73.18

✓ $\frac{9.5}{60} \frac{10.1}{36} \frac{7.8}{32} \frac{7.4}{30} \frac{5.7}{24} \frac{5.3}{17} \frac{5.3}{10} 5.3 \frac{5.6}{10} \frac{5.7}{17} \frac{5.8}{29} \frac{8.9}{34} \frac{11.0}{35} \frac{11.2}{39} \frac{11.6}{60}$

✓ $\frac{9.6}{60} \frac{9.7}{43} \frac{10.3}{37} \frac{9.8}{33} \frac{5.7}{22} \frac{5.3}{18} \frac{5.3}{10} 5.3 \quad \frac{5.7}{10} \frac{5.9}{19} \frac{5.8}{28} \frac{10.3}{37} \frac{11.0}{43} \frac{12.1}{60}$

Sta	+	π	-	Elev
		984.18		
41				78.9 .
	+18			78.9 .
B.M.	6.05	984.64	5.59	978.59 . 978.57
	+27			78.9 .
	+44			78.9 .
	+50			78.9 .
42				79.1 .
	+50			79.1 .
	+95			79.3 .
43				79.3 .
	+16			79.4 .
	+31			79.5 .
	+50			79.6 .

Lt.

E

Rt.

✓ $\frac{7.7}{60} \frac{8.6}{40} \frac{8.2}{32} \frac{6.0}{23} \frac{5.5}{18} \frac{5.4}{10} \quad \frac{5.4}{10} \frac{5.9}{18} \frac{6.3}{27} \frac{10.7}{37} \frac{12.2}{60}$

✓ $\frac{7.2}{60} \frac{8.0}{30} \frac{6.1}{22} \frac{5.7}{19} \frac{5.4}{10} \quad \frac{5.3}{10} \frac{5.7}{20} \frac{6.0}{30} \frac{10.8}{39} \frac{11.4}{44} \frac{12.2}{60}$

Spk. in P.P. 32' Lt. Sta 41+51

✓ $\frac{7.4}{60} \frac{7.6}{45} \frac{8.2}{28} \frac{6.2}{22} \frac{6.0}{19} \frac{5.9}{10} \quad \frac{5.9}{10} \frac{6.1}{11} \frac{6.1}{20} \frac{6.3}{32} \frac{7.0}{45} \frac{6.9}{60}$

✓ $\frac{6.9}{60} \frac{7.6}{43} \frac{7.9}{29} \frac{6.0}{20} \frac{5.8}{10} \quad \frac{5.9}{10} \frac{6.1}{11} \frac{5.8}{18} \frac{6.3}{30} \frac{7.0}{60}$

✓ $\frac{7.0}{60} \frac{7.3}{48} \frac{7.8}{28} \frac{5.9}{20} \frac{5.8}{10} \quad \frac{5.9}{10} \frac{6.0}{11} \frac{5.9}{19} \frac{6.4}{30} \frac{10.0}{37} \frac{10.7}{60}$

✓ $\frac{8.5}{60} \frac{8.5}{46} \frac{7.8}{39} \frac{7.8}{29} \frac{5.9}{20} \frac{5.6}{10} \quad \frac{5.7}{10} \frac{5.8}{18} \frac{6.3}{29} \frac{8.6}{35} \frac{9.3}{60}$

✓ $\frac{9.7}{60} \frac{9.5}{34} \frac{6.7}{22} \frac{5.8}{16} \frac{5.6}{10} \quad \frac{5.7}{10} \frac{5.8}{11} \frac{5.9}{17} \frac{5.8}{30} \frac{8.9}{41} \frac{8.8}{60}$

✓ $\frac{11.1}{60} \frac{10.5}{36} \frac{8.0}{23} \frac{5.9}{19} \frac{5.5}{10} \quad \frac{5.5}{10} \frac{5.5}{17} \frac{5.6}{28} \frac{4.6}{32} \frac{9.5}{50} \frac{10.1}{60}$

✓ $\frac{11.3}{60} \frac{10.6}{34} \frac{5.9}{26} \frac{5.6}{16} \frac{5.5}{10} \quad \frac{5.5}{10} \frac{5.4}{18} \frac{5.2}{30} \frac{4.2}{35} \frac{3.1}{48} \frac{3.7}{60}$

✓ $\frac{11.7}{60} \frac{10.7}{36} \frac{5.8}{20} \frac{5.5}{16} \frac{5.4}{10} \quad \frac{5.3}{10} \frac{5.3}{17} \frac{5.1}{38} \frac{4.0}{37} \frac{4.2}{60}$

✓ $\frac{11.4}{60} \frac{11.0}{42} \frac{9.8}{33} \frac{5.5}{21} \frac{5.4}{16} \frac{5.3}{10} \quad \frac{5.1}{10} \frac{5.2}{18} \frac{5.2}{30} \frac{9.7}{43} \frac{10.7}{60}$

✓ $\frac{10.2}{60} \frac{10.3}{45} \frac{9.8}{36} \frac{5.7}{22} \frac{5.2}{15} \frac{5.2}{10} \quad \frac{5.0}{10} \frac{5.3}{17} \frac{5.6}{28} \frac{8.3}{35} \frac{10.3}{60}$

Sta	+	π	-	Elev.
		984.64		
44+00				80.2
+41				80.7
+54				80.9
+78				81.3
45				81.7
+34				82.3
+59				82.6
T.P.	9.04	991.72	1.96	982.68
+67				82.7
+90				82.9
46				83.1
+50				83.3
+88				83.7

Lt.

4

et.

$$\checkmark \frac{8.6}{60} \frac{8.3}{42} \frac{7.8}{30} \frac{5.3}{26} \frac{4.8}{18} \frac{4.6}{10} \frac{4.4}{10} \frac{4.5}{10} \frac{4.8}{18} \frac{5.2}{26} \frac{8.1}{34} \frac{9.5}{46} \frac{10.5}{60}$$

$$\checkmark \frac{10.0}{60} \frac{10.3}{35} \frac{10.0}{32} \frac{5.2}{21} \frac{4.6}{17} \frac{4.2}{10} \frac{3.9}{10} \frac{4.0}{10} \frac{4.3}{18} \frac{5.1}{27} \frac{7.5}{32} \frac{8.3}{48} \frac{8.3}{60}$$

$$\checkmark \frac{10.4}{60} \frac{10.8}{47} \frac{11.2}{34} \frac{9.2}{31} \frac{5.0}{21} \frac{4.4}{18} \frac{4.0}{10} \frac{3.7}{10} \frac{4.0}{19} \frac{5.0}{24} \frac{5.0}{29} \frac{3.9}{45} \frac{4.3}{60}$$

$$\checkmark \frac{9.9}{60} \frac{9.8}{49} \frac{9.2}{41} \frac{9.4}{35} \frac{4.5}{21} \frac{4.0}{17} \frac{3.6}{10} \frac{3.2}{10} \frac{3.3}{17} \frac{3.6}{20} \frac{5.1}{25} \frac{5.2}{29} \frac{4.0}{33} \frac{3.5}{60}$$

$$\checkmark \frac{8.6}{60} \frac{8.3}{42} \frac{7.6}{36} \frac{3.9}{21} \frac{3.5}{19} \frac{3.3}{10} \frac{2.9}{10} \frac{3.0}{17} \frac{3.4}{21} \frac{4.7}{25} \frac{4.8}{29} \frac{3.6}{33} \frac{2.9}{60}$$

$$\checkmark \frac{5.9}{60} \frac{4.8}{44} \frac{4.5}{36} \frac{3.7}{29} \frac{4.3}{25} \frac{2.7}{21} \frac{2.6}{10} \frac{2.4}{10} \frac{2.4}{18} \frac{2.5}{21} \frac{3.7}{24} \frac{3.7}{29} \frac{2.5}{33} \frac{2.2}{60}$$

$$\checkmark \frac{2.4}{60} \frac{1.8}{32} \frac{3.0}{27} \frac{3.0}{23} \frac{2.2}{22} \frac{2.1}{16} \frac{2.1}{10} \frac{2.1}{10} \frac{2.1}{10} \frac{2.1}{20} \frac{2.9}{23} \frac{2.8}{30} \frac{1.9}{34} \frac{1.6}{60}$$

$$\checkmark \frac{9.6}{60} \frac{8.1}{32} \frac{9.9}{26} \frac{9.2}{24} \frac{9.1}{14} \frac{8.1}{10} \frac{9.0}{10} \frac{9.1}{17} \frac{9.1}{21} \frac{9.9}{24} \frac{6.6}{26} \frac{6.3}{34} \frac{6.3}{60}$$

$$\checkmark \frac{8.2}{60} \frac{6.7}{33} \frac{8.9}{27} \frac{9.9}{23} \frac{9.0}{21} \frac{8.8}{14} \frac{9.0}{10} \frac{8.8}{10} \frac{8.9}{19} \frac{9.4}{24} \frac{9.1}{26} \frac{4.1}{34} \frac{3.1}{60}$$

$$\checkmark \frac{7.9}{60} \frac{6.7}{34} \frac{6.8}{32} \frac{8.7}{28} \frac{9.5}{23} \frac{8.9}{21} \frac{8.7}{14} \frac{8.8}{10} \frac{8.6}{10} \frac{8.6}{10} \frac{9.2}{18} \frac{8.9}{23} \frac{3.4}{26} \frac{2.4}{34} \frac{2.4}{60}$$

$$\checkmark \frac{7.4}{60} \frac{6.3}{34} \frac{8.6}{29} \frac{9.5}{25} \frac{8.6}{24} \frac{8.5}{20} \frac{9.5}{12} \frac{8.4}{10} \frac{8.4}{10} \frac{8.6}{18} \frac{9.3}{21} \frac{8.7}{24} \frac{2.7}{26} \frac{2.3}{34} \frac{2.3}{60}$$

$$\checkmark \frac{5.2}{60} \frac{5.3}{34} \frac{8.3}{28} \frac{8.8}{23} \frac{8.3}{20} \frac{8.1}{10} \frac{8.0}{10} \frac{9.1}{10} \frac{8.0}{17} \frac{8.0}{19} \frac{9.0}{23} \frac{4.2}{25} \frac{4.6}{34} \frac{5.2}{60}$$

Sta	+	π	-	Elev
		791.72		
47+00				83.8
+50				84.1
+88				84.1
48				84.1
+50				83.9
49				83.7
+50				83.6
T.P	2.44	986.18	7.98	983.74
50				83.5
+50				83.1
51				82.5
+50				81.9
52				81.3

Lt

F

Pt

$$\checkmark \begin{array}{cccccccccccc} 4.9 & 5.1 & 8.4 & 8.7 & 8.1 & 8.0 & 7.9 & 7.8 & 7.7 & 8.0 & 5.6 & 6.1 \\ 60 & 34 & 27 & 22 & 18 & 10 & 7.9 & 7.0 & 11 & 19 & 23-26 & 33 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 5.0 & 5.3 & 7.8 & 8.6 & 7.9 & 7.7 & 7.6 & 7.7 & 7.7 & 8.9 & 8.5 & 8.6 \\ 60 & 34 & 28 & 24 & 18 & 10 & 7.6 & 10 & 16 & 20 & 26-29 & 32 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 5.9 & 6.0 & 7.9 & 8.3 & 7.5 & 7.7 & 7.7 & 7.5 & 7.5 & 8.4 & 7.6 & 7.4 & 10.3 & 9.7 \\ 60 & 31 & 26 & 22 & 20 & 10 & 7.6 & 10 & 12 & 20 & 26 & 32 & 40 & 46 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 6.7 & 6.9 & 8.2 & 7.3 & 7.7 & & 7.7 & 7.9 & 7.8 & 8.4 & 9.7 & 9.2 & 7.5 & 10.4 & 11.4 \\ 60 & 29 & 26 & 24 & 19 & 10 & 7.6 & 10 & 18 & 21 & 26 & 31 & 36 & 40 & 45 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 8.0 & 7.7 & 9.6 & 9.6 & 8.6 & 7.9 & 7.8 & 8.1 & 8.8 & 7.9 & 10.0 & 9.8 & 7.8 & 11.0 & 10.5 \\ 60 & 32 & 29 & 25 & 23 & 19 & 10 & 7.8 & 7.9 & 10 & 19 & 22 & 27 & 31 & 34 & 40 & 57 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 7.8 & 7.8 & 7.7 & 8.5 & 8.2 & 8.0 & 8.0 & 8.1 & 8.8 & 10.1 & 9.7 & 9.7 & 10.7 & 10.8 \\ 60 & 33 & 30 & 25 & 21 & 18 & 10 & 8.0 & 11 & 19 & 24 & 27 & 32 & 35 & 40 & 46 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 7.6 & 7.9 & 10.2 & 8.8 & 8.3 & 8.2 & 8.2 & & & & 8.2 & 8.3 & 10.1 & 9.2 & 10.1 \\ 60 & 33 & 29 & 26 & 22 & 19 & 15 & 10 & & & 8.1 & 10 & 21 & 24 & 27 & 32 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 2.0 & 1.7 & 4.2 & 4.7 & 3.2 & 3.0 & 2.8 & & & & 2.8 & 2.8 & 3.3 & 4.6 & 4.6 & 2.3 & 4.1 & 4.3 \\ 60 & 34 & 30 & 28 & 25 & 22 & 19 & 10 & 2.7 & & 10 & 18 & 21 & 26 & 29 & 33 & 44 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 2.5 & 2.6 & 2.1 & 5.0 & 5.2 & 3.8 & 3.4 & 3.2 & & & 3.3 & 3.4 & 3.9 & 5.4 & 3.2 & 4.1 & 4.3 \\ 60 & 40 & 34 & 29 & 28 & 25 & 21 & 17 & 10 & 3.1 & 10 & 18 & 23 & 26 & 30 & 33 & 46 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 3.3 & 3.0 & 5.7 & 4.4 & 4.0 & 3.8 & 3.7 & & & & 3.8 & 4.0 & 5.2 & 5.8 & 3.6 & 4.4 & 5.0 \\ 60 & 34 & 28 & 25 & 22 & 20 & 16 & 10 & 3.7 & & 10 & 20 & 24 & 27 & 29 & 30 & 47 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 3.7 & 3.8 & 6.2 & 4.8 & 4.6 & 4.4 & & & & & 4.4 & 4.4 & 4.5 & 4.8 & 6.4 & 4.5 & 5.7 \\ 60 & 34 & 29 & 26 & 21 & 18 & 10 & & & & 4.3 & 10 & 14 & 19 & 22 & 26 & 30 & 33 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 4.9 & 4.6 & 7.1 & 4.8 & 4.8 & 4.8 & 4.9 & & & & 4.9 & 4.8 & 4.9 & 6.5 & 5.3 & 6.3 \\ 60 & 31 & 28 & 26 & 20 & 15 & 10 & 4.9 & & & 10 & 16 & 21 & 27 & 30 & 33 & 60 \end{array}$$

Sta	+	π	-	Elev	
		986.18			
52+09	SECTION	¢ MONOLITHIC CHLV		81.3	
+35				81.1	
+50				80.9	
+57	¢	DITCH WEST ON CLEVELAND		80.8	
+67				80.7	
+81.8	¢	CLEVELAND		80.5	
B.M.	5.72	986.18	5.72	980.46	980.46
B.M.	365	983.34	6.42	979.69	
53				80.1	
+03	¢	DITCH EAST ON CLEVELAND	RT	80.0	
+08	¢	DITCH EAST ON CLEVELAND LT.		79.9	
+20				79.8	
+50				79.3	
54				78.7	

Sta	+	π	-	Elev
		983.34.		
		5.9		
54+50		977.4		78.2.

55				77.8.
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+50				77.4.
-----	--	--	--	-------

56				77.1.
----	--	--	--	-------

+50				76.9.
-----	--	--	--	-------

57				76.8.
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T.P.	3.69	980.83	6.20	977.14.
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+50				76.8.
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58				76.8.
----	--	--	--	-------

+50				76.7.
-----	--	--	--	-------

59				76.5.
----	--	--	--	-------

+50				76.1.
-----	--	--	--	-------

+53	SECTION MONOLITHIC CURV			76.1.
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+53	SOUTH EAST. DRAWL			
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Lt

E

Rt

$$\checkmark \frac{5.9 \ 6.5}{60 \ 36}$$

$$\frac{6.6 \ 7.1 \ 7.1 \ 5.8 \ 5.1}{34 \ 33 \ 25 \ 22 \ 10} \quad \frac{5.2 \ 5.6 \ 6.1 \ 7.2 \ 7.8 \ 7.6 \ 7.2 \ 7.6}{5.10 \ 18 \ 21 \ 26 \ 33 \ 35 \ 47 \ 60}$$

$$\checkmark \frac{6.4 \ 7.0}{60 \ 36}$$

$$\frac{6.9 \ 7.5 \ 6.0 \ 5.6}{34 \ 32 \ 25 \ 22 \ 10} \quad \frac{5.6 \ 5.8 \ 6.1 \ 6.6 \ 7.7 \ 7.6 \ 9.1 \ 7.8 \ 8.1}{5.5 \ 10 \ 11 \ 19 \ 22 \ 26 \ 33 \ 36 \ 39 \ 60}$$

$$\checkmark \frac{7.0 \ 7.4 \ 7.5 \ 7.7 \ 7.9 \ 6.7 \ 6.2 \ 6.0}{60 \ 38 \ 34 \ 32 \ 25 \ 22 \ 17 \ 10}$$

$$\frac{6.1 \ 6.2 \ 6.3 \ 6.8 \ 8.2 \ 7.9 \ 8.6 \ 8.9 \ 8.4}{5.9 \ 10 \ 11 \ 18 \ 22 \ 26 \ 32 \ 33 \ 39 \ 60}$$

$$\checkmark \frac{7.2 \ 7.5 \ 7.7 \ 7.9 \ 7.9 \ 6.9 \ 6.5 \ 6.3}{60 \ 36 \ 34 \ 33 \ 26 \ 23 \ 18 \ 10}$$

$$\frac{6.3 \ 6.4 \ 6.5 \ 6.7 \ 8.3 \ 8.2 \ 8.6 \ 8.0 \ 8.8}{6.2 \ 10 \ 11 \ 19 \ 22 \ 26 \ 33 \ 35 \ 44 \ 60}$$

$$\checkmark \frac{7.4 \ 7.2}{60 \ 36}$$

$$\frac{7.6 \ 8.1 \ 8.2 \ 6.9 \ 6.6 \ 6.4}{34 \ 32 \ 26 \ 22 \ 17 \ 10}$$

$$\frac{6.5 \ 6.7 \ 6.9 \ 7.3 \ 8.4 \ 8.0 \ 8.5 \ 8.6 \ 7.0}{6.4 \ 10 \ 11 \ 18 \ 23 \ 26 \ 33 \ 34 \ 47 \ 60}$$

$$\checkmark \frac{7.6 \ 7.6 \ 8.0 \ 7.6 \ 7.7 \ 8.1 \ 8.1 \ 6.8 \ 6.7 \ 6.5}{60 \ 37 \ 36 \ 35 \ 34 \ 32 \ 25 \ 22 \ 17 \ 10}$$

$$\frac{6.6 \ 6.7 \ 7.1 \ 8.5 \ 8.4 \ 8.9 \ 8.6 \ 7.2}{6.5 \ 10 \ 19 \ 22 \ 25 \ 32 \ 34 \ 43 \ 60}$$

$$\checkmark \frac{5.0 \ 5.3 \ 5.1 \ 5.1 \ 5.8 \ 5.7 \ 4.5 \ 4.2 \ 4.0}{60 \ 37 \ 35 \ 34 \ 32 \ 25 \ 22 \ 18 \ 10}$$

$$\frac{4.1 \ 4.3 \ 4.3 \ 4.6 \ 6.0 \ 5.8 \ 6.2 \ 5.9 \ 6.7}{4.0 \ 10 \ 11 \ 18 \ 22 \ 26 \ 33 \ 35 \ 43 \ 60}$$

$$\checkmark \frac{4.9 \ 5.2 \ 6.0 \ 5.4 \ 6.0 \ 6.0 \ 4.5 \ 4.2 \ 4.1}{60 \ 36 \ 35 \ 33 \ 32 \ 25 \ 21 \ 15 \ 10}$$

$$\frac{4.1 \ 4.5 \ 4.4 \ 4.7 \ 5.8 \ 5.9 \ 5.3 \ 5.9 \ 6.4}{4.0 \ 10 \ 11 \ 18 \ 23 \ 25 \ 32 \ 33 \ 44 \ 60}$$

$$\checkmark \frac{5.0 \ 5.3 \ 4.9 \ 5.2 \ 6.3 \ 6.3 \ 4.5 \ 4.4 \ 4.2}{60 \ 37 \ 35 \ 34 \ 31 \ 25 \ 21 \ 16 \ 10}$$

$$\frac{4.3 \ 4.4 \ 4.5 \ 4.6 \ 6.1 \ 6.0 \ 5.2 \ 6.1 \ 5.6 \ 6.1}{4.1 \ 10 \ 11 \ 17 \ 22 \ 26 \ 31 \ 33 \ 34 \ 44 \ 60}$$

$$\checkmark \frac{5.3 \ 5.5 \ 5.4 \ 5.6 \ 6.7 \ 6.6 \ 4.9 \ 4.6 \ 4.4}{60 \ 38 \ 35 \ 33 \ 31 \ 25 \ 21 \ 15 \ 10}$$

$$\frac{4.5 \ 4.6 \ 4.8 \ 5.1 \ 6.2 \ 6.5 \ 6.1 \ 6.4 \ 6.8}{4.3 \ 10 \ 11 \ 17 \ 22 \ 25 \ 31 \ 32 \ 34 \ 47 \ 60}$$

$$\checkmark \frac{6.5 \ 6.1 \ 6.0 \ 5.5 \ 5.5 \ 6.8 \ 6.9 \ 5.2 \ 5.0 \ 4.8}{60 \ 38 \ 37 \ 36 \ 34 \ 31 \ 24 \ 19 \ 15 \ 10}$$

$$\frac{4.8 \ 4.9 \ 5.3 \ 7.1 \ 7.3 \ 6.6 \ 8.7 \ 8.3}{4.7 \ 10 \ 15 \ 21 \ 27 \ 30 \ 33 \ 47 \ 60}$$

FL

FL

$$\checkmark \frac{5.5 \ 5.7 \ 6.0 \ 5.5 \ 5.5 \ 6.8 \ 7.7 \ 7.2 \ 4.9}{60 \ 38 \ 37 \ 36 \ 34 \ 31 \ 24 \ 24 \ 10}$$

$$\frac{4.8 \ 5.1 \ 7.1 \ 7.3 \ 7.5 \ 6.8 \ 8.3 \ 8.7 \ 8.3}{4.7 \ 10 \ 21 \ 25 \ 25 \ 31 \ 34 \ 35 \ 47 \ 60}$$

$$\frac{9.2 \ 9.4 \ 9.6 \ 9.7 \ 10.0 \ 11.0}{4.0 \ 100 \ 150 \ 200 \ 250 \ 300}$$

11.6
350

STA	+	π	-	ELEV
-----	---	-------	---	------

		980.83.		
--	--	---------	--	--

60+00				
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				75.9.
--	--	--	--	-------

+50				
-----	--	--	--	--

				75.7.
--	--	--	--	-------

61				
----	--	--	--	--

				75.6.
--	--	--	--	-------

+50				
-----	--	--	--	--

				75.6.
--	--	--	--	-------

62				
----	--	--	--	--

				75.6.
--	--	--	--	-------

+50				
-----	--	--	--	--

				75.8.
--	--	--	--	-------

63				
----	--	--	--	--

				75.8.
--	--	--	--	-------

+50				
-----	--	--	--	--

				75.9.
--	--	--	--	-------

T.P.	5.68	981.46.	5.05	975.78.
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LT

♀

RT

✓ $\frac{5.2}{60} \frac{5.4}{33} \frac{6.9}{31} \frac{7.1}{24} \frac{5.0}{20} \frac{4.9}{10} \underline{4.9} \frac{5.0}{10} \frac{5.2}{19} \frac{5.4}{22} \frac{6.8}{25} \frac{6.9}{33} \frac{8.1}{35} \frac{7.9}{47} \frac{8.3}{60}$

✓ $\frac{5.6}{60} \frac{5.6}{33} \frac{7.1}{30} \frac{7.1}{24} \frac{5.2}{20} \frac{5.1}{10} \underline{5.1} \frac{5.1}{10} \frac{5.4}{20} \frac{5.9}{23} \frac{7.0}{26} \frac{7.0}{31} \frac{6.6}{33} \frac{7.5}{35} \frac{7.1}{42} \frac{8.0}{60}$

✓ $\frac{5.5}{60} \frac{5.6}{33} \frac{7.0}{30} \frac{6.9}{24} \frac{5.6}{21} \frac{5.2}{18} \frac{5.3}{10} \underline{5.2} \frac{5.3}{10} \frac{5.6}{17} \frac{6.1}{23} \frac{7.1}{27} \frac{7.1}{33} \frac{6.8}{35} \frac{7.6}{35} \frac{7.4}{48} \frac{7.8}{60}$

✓ $\frac{5.6}{60} \frac{5.7}{33} \frac{6.9}{30} \frac{6.9}{24} \frac{5.5}{21} \frac{5.3}{18} \frac{5.3}{10} \underline{5.2} \frac{5.3}{10} \frac{5.6}{19} \frac{6.1}{23} \frac{7.3}{26} \frac{7.2}{32} \frac{6.9}{34} \frac{7.8}{36} \frac{7.5}{42} \frac{8.0}{60}$

✓ $\frac{5.7}{60} \frac{5.6}{34} \frac{6.5}{31} \frac{6.8}{24} \frac{5.7}{21} \frac{5.3}{18} \frac{5.2}{10} \underline{5.2} \frac{5.3}{10} \frac{5.5}{18} \frac{5.9}{23} \frac{7.1}{27} \frac{7.1}{31} \frac{6.5}{34} \frac{7.2}{37} \frac{7.0}{46} \frac{7.6}{60}$

✓ $\frac{5.6}{60} \frac{6.0}{33} \frac{6.6}{30} \frac{5.1}{26} \frac{5.1}{23} \frac{5.1}{10} \underline{5.0} \frac{5.2}{10} \frac{5.4}{20} \frac{7.1}{26} \frac{6.4}{32} \frac{6.5}{34} \frac{7.0}{36} \frac{6.7}{46} \frac{7.3}{60}$

✓ $\frac{6.0}{60} \frac{6.6}{33} \frac{6.9}{31} \frac{7.0}{26} \frac{5.6}{22} \frac{5.1}{18} \frac{5.1}{10} \underline{5.0} \frac{5.2}{10} \frac{5.5}{20} \frac{5.8}{25} \frac{6.8}{27} \frac{7.0}{32} \frac{6.9}{33} \frac{6.7}{35} \frac{7.3}{36} \frac{7.0}{39} \frac{7.3}{60}$

✓ $\frac{5.9}{60} \frac{6.6}{33} \frac{6.8}{31} \frac{6.8}{26} \frac{5.5}{22} \frac{5.0}{18} \frac{5.0}{10} \underline{4.9} \frac{5.0}{10} \frac{5.4}{18} \frac{5.8}{23} \frac{7.0}{26} \frac{7.0}{33} \frac{6.8}{35} \frac{7.4}{36} \frac{7.0}{46} \frac{7.5}{60}$

STA	+	$\bar{\Delta}$	-	ELEV	
		981.46			
B.M.	2.43	980.93	2.96	978.50	978.48
64+00				76.1	
+50				76.3	
65				76.5	
+50				76.7	
66				76.7	
+30				76.8	
+38				76.8	
+50				76.7	

LT

E

RT

TOP. S.W. COR LOWER STEP FRONT OF OFFICE 67400 LT

✓ $\frac{5.5}{60}$ $\frac{5.6}{33}$ $\frac{6.8}{29}$ $\frac{4.7}{26}$ $\frac{5.4}{22}$ $\frac{5.0}{17}$ $\frac{4.9}{11}$ $\frac{4.8}{4.8}$ $\frac{4.9}{10}$ $\frac{5.2}{18}$ $\frac{5.1}{21}$ $\frac{5.7}{22}$ $\frac{6.9}{28}$ $\frac{7.0}{32}$ $\frac{6.6}{33}$ $\frac{6.8}{35}$ $\frac{7.2}{36}$ $\frac{7.2}{60}$

✓ $\frac{4.7}{60}$ $\frac{5.1}{33}$ $\frac{6.1}{30}$ $\frac{6.3}{27}$ $\frac{4.9}{22}$ $\frac{4.7}{18}$ $\frac{4.6}{10}$ $\frac{4.7}{4.6}$ $\frac{4.9}{10}$ $\frac{4.9}{18}$ $\frac{5.3}{20}$ $\frac{6.7}{22}$ $\frac{6.7}{27}$ $\frac{5.6}{31}$ $\frac{5.9}{33}$ $\frac{6.5}{35}$ $\frac{6.3}{49}$ $\frac{6.3}{60}$

✓ $\frac{5.6}{60}$ $\frac{6.1}{26}$ $\frac{4.9}{22}$ $\frac{4.5}{20}$ $\frac{4.4}{10}$ $\frac{4.4}{4.4}$ $\frac{4.5}{10}$ $\frac{4.8}{18}$ $\frac{5.4}{24}$ $\frac{6.2}{27}$ $\frac{6.5}{32}$ $\frac{5.3}{33}$ $\frac{6.0}{35}$ $\frac{6.3}{36}$ $\frac{6.3}{60}$

✓ $\frac{6.0}{60}$ $\frac{6.1}{26}$ $\frac{4.6}{22}$ $\frac{4.4}{19}$ $\frac{4.3}{10}$ $\frac{4.2}{4.2}$ $\frac{4.3}{10}$ $\frac{4.6}{20}$ $\frac{5.0}{23}$ $\frac{5.9}{26}$ $\frac{6.1}{32}$ $\frac{5.4}{33}$ $\frac{6.1}{36}$ $\frac{5.8}{46}$ $\frac{6.1}{60}$

✓ $\frac{5.6}{60}$ $\frac{5.9}{26}$ $\frac{4.8}{22}$ $\frac{4.5}{19}$ $\frac{4.5}{15}$ $\frac{4.2}{10}$ $\frac{4.2}{4.2}$ $\frac{4.2}{10}$ $\frac{4.2}{19}$ $\frac{4.5}{21}$ $\frac{6.2}{26}$ $\frac{6.2}{31}$ $\frac{5.2}{33}$ $\frac{5.5}{37}$ $\frac{5.8}{38}$ $\frac{6.8}{60}$

✓ $\frac{5.4}{60}$ $\frac{5.7}{39}$ $\frac{5.3}{26}$ $\frac{4.7}{21}$ $\frac{4.2}{10}$ $\frac{4.1}{4.1}$ $\frac{4.2}{10}$ $\frac{4.6}{19}$ $\frac{5.7}{22}$ $\frac{5.9}{26}$ $\frac{4.9}{32}$ $\frac{5.1}{33}$ $\frac{5.6}{37}$ $\frac{6.6}{38}$ $\frac{6.6}{60}$

✓ $\frac{4.0}{60}$ $\frac{4.5}{27}$ $\frac{4.7}{22}$ $\frac{4.2}{10}$ $\frac{4.1}{4.1}$ $\frac{4.2}{10}$ $\frac{4.2}{19}$ $\frac{4.6}{22}$ $\frac{5.7}{26}$ $\frac{5.9}{32}$ $\frac{4.7}{33}$ $\frac{5.1}{37}$ $\frac{5.1}{38}$ $\frac{6.6}{60}$

✓ $\frac{4.0}{60}$ $\frac{4.6}{29}$ $\frac{4.3}{18}$ $\frac{4.2}{10}$ $\frac{4.2}{4.2}$ $\frac{4.3}{10}$ $\frac{4.3}{19}$ $\frac{4.7}{23}$ $\frac{6.1}{26}$ $\frac{6.1}{31}$ $\frac{5.2}{33}$ $\frac{5.4}{35}$ $\frac{6.2}{37}$ $\frac{6.1}{45}$ $\frac{6.3}{60}$

STA	+	π	-	ELEV
		780.73.		
67+00				76.4 .
+50				76.3 .
+60				76.2 .
+15				76.2 .
68				76.1 .
+50				75.8 .
69				75.4 .
+21				75.1 .

LT

✱

RT

$$\checkmark \quad \begin{array}{ccccccc} 3.9 & 4.2 & 4.2 & 4.5 & & 4.6 & 4.8 & 5.2 & 6.4 & 6.5 & 5.7 & 6.0 & 6.4 & 6.9 \\ 6.0 & 3.6 & 1.8 & 1.0 & 4.5 & 1.0 & 2.0 & 2.2 & 2.6 & 3.1 & 3.3 & 3.5 & 3.6 & 5.0 & 6.0 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccc} 4.2 & 4.4 & 4.4 & 4.6 & & 4.8 & 5.1 & 5.3 & 6.6 & 6.6 & 5.8 & 5.9 & 6.8 & 6.8 & 7.6 \\ 6.0 & 4.2 & 1.9 & 1.0 & 4.6 & 1.0 & 1.8 & 2.2 & 2.6 & 3.1 & 3.3 & 3.5 & 3.6 & 5.1 & 6.0 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccc} 4.4 & 4.7 & 4.8 & 4.6 & & 4.9 & 5.1 & 5.8 & 6.6 & 6.6 & 5.8 & 6.0 & 6.8 & 6.6 & 7.3 \\ 6.0 & 3.3 & 1.9 & 1.0 & 4.7 & 1.0 & 1.9 & 2.5 & 2.7 & 3.1 & 3.3 & 3.5 & 3.6 & 4.3 & 6.0 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccc} 4.4 & 4.8 & 5.2 & 4.8 & 4.7 & & 4.7 & 4.9 & 5.4 & 6.7 & 6.6 & 5.8 & 6.6 & 7.3 \\ 6.0 & 3.2 & 2.8 & 2.6 & 1.9 & 1.0 & 4.7 & 1.0 & 1.8 & 2.3 & 3.2 & 3.3 & 3.5 & 6.4 & 6.0 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccc} 4.2 & 4.4 & 4.9 & 5.8 & 5.9 & 5.1 & 5.1 & 4.9 & 4.8 & & 4.9 & 5.2 & 5.6 & 5.6 & 6.2 & 6.6 & 5.7 & 5.8 & 6.7 & 6.8 & 7.1 \\ 6.0 & 3.8 & 3.3 & 2.9 & 2.7 & 2.4 & 2.2 & 1.8 & 1.0 & 4.8 & 1.0 & 1.9 & 2.4 & 2.7 & 2.9 & 3.2 & 3.3 & 3.5 & 3.6 & 4.4 & 6.0 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccc} 4.6 & 4.7 & 5.2 & 5.8 & 6.0 & 5.9 & 5.1 & 5.2 & 5.1 & & 5.2 & 5.6 & 5.8 & 6.7 & 7.0 & 6.0 & 6.2 & 6.8 & 6.5 & 7.0 \\ 6.0 & 3.7 & 3.2 & 3.0 & 2.8 & 2.4 & 2.1 & 1.7 & 1.0 & 5.1 & 1.0 & 2.0 & 2.4 & 2.6 & 2.9 & 3.3 & 3.5 & 3.6 & 4.6 & 6.0 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccc} 5.3 & 5.7 & 7.3 & 7.3 & 6.9 & 5.6 & 5.5 & 5.5 & & 5.8 & 5.5 & 5.9 & 7.6 & 7.6 & 7.6 & 6.3 & 6.5 & 7.0 & 6.7 & 7.3 \\ 6.0 & 3.4 & 2.9 & 2.8 & 2.5 & 2.2 & 1.8 & 1.0 & 5.5 & 1.0 & 1.9 & 2.2 & 2.6 & 2.8 & 3.1 & 3.3 & 3.5 & 3.6 & 4.6 & 6.0 \end{array}$$

$$\checkmark \quad \begin{array}{ccccccc} 5.5 & 5.9 & 7.2 & 7.6 & 7.6 & 5.9 & 6.0 & 5.8 & & 5.9 & 5.8 & 6.5 & 7.4 & 7.8 & 7.8 & 6.4 & 6.7 & 6.9 & 7.7 \\ 6.0 & 3.4 & 3.1 & 2.8 & 2.6 & 2.1 & 1.7 & 1.0 & 5.8 & 1.0 & 1.8 & 2.2 & 2.5 & 2.8 & 3.0 & 3.3 & 3.5 & 3.6 & 4.5 & 6.0 \end{array}$$

STA	+	π	-	ELEV
		980.93.		
69+25				75.1 .
+50				74.9 .
				X
70				74.4 .
+35				74.0 .
+44				74.0 .
+50				73.9 .
+62	£	TATUM ST	LT	73.9 .
+75				73.7 .

LT

L

RT

$$\checkmark \quad \frac{6.6}{60} \frac{7.3}{34} \frac{7.5}{28} \frac{7.5}{26} \frac{6.1}{21} \frac{5.9}{19} \frac{5.9}{10} \quad \frac{6.0}{58} \frac{5.9}{10} \frac{6.0}{18} \frac{7.8}{22} \frac{7.9}{27} \frac{7.8}{29} \frac{6.4}{31} \frac{6.6}{33} \frac{7.1}{35} \frac{6.9}{36} \frac{7.7}{45} \frac{7.7}{60}$$

$$\checkmark \quad \frac{6.6}{60} \frac{6.7}{45} \frac{7.6}{25} \frac{6.4}{22} \frac{6.2}{18} \quad \frac{6.0}{10} \quad \frac{6.2}{60} \frac{6.3}{10} \frac{6.5}{19} \frac{7.9}{23} \frac{8.1}{25} \frac{8.1}{28} \frac{6.9}{31} \frac{6.9}{33} \frac{7.6}{35} \frac{7.6}{36} \frac{7.7}{45} \frac{7.7}{60}$$

$$\checkmark \quad \frac{7.4}{60} \frac{7.5}{40} \frac{7.6}{31} \frac{8.2}{28} \frac{8.1}{26} \frac{6.8}{21} \frac{6.7}{17} \frac{6.6}{10} \quad \frac{6.5}{65} \quad \frac{6.7}{10} \frac{6.9}{18} \frac{7.0}{22} \frac{6.4}{26} \frac{8.5}{28} \frac{8.5}{31} \frac{7.5}{33} \frac{7.6}{34} \frac{8.0}{36} \frac{8.6}{40}$$

$$\checkmark \quad \frac{7.6}{60} \frac{7.7}{45} \frac{8.2}{31} \frac{8.2}{28} \frac{8.2}{26} \frac{7.0}{24} \frac{6.9}{20} \frac{6.9}{10} \quad \frac{6.9}{69} \quad \frac{7.0}{10} \frac{7.2}{18} \frac{7.7}{24} \frac{8.7}{26} \frac{8.9}{29} \frac{8.9}{31} \frac{7.9}{33} \frac{7.8}{34} \frac{8.2}{36} \frac{8.4}{45} \frac{8.8}{60}$$

$$\checkmark \quad \frac{8.3}{60} \frac{8.4}{41} \frac{8.5}{30} \frac{8.5}{28} \frac{8.3}{27} \frac{7.2}{25} \frac{7.1}{18} \frac{6.9}{10} \quad \frac{6.9}{69} \quad \frac{7.1}{10} \frac{7.3}{18} \frac{7.7}{23} \frac{8.8}{26} \frac{9.0}{29} \frac{8.9}{32} \frac{8.0}{33} \frac{8.7}{34} \frac{8.4}{36} \frac{8.7}{45} \frac{8.7}{60}$$

$$\checkmark \quad \frac{7.4}{60} \frac{7.3}{29} \frac{7.1}{19} \frac{6.9}{10} \quad \frac{7.0}{70} \quad \frac{7.2}{10} \frac{7.3}{18} \frac{7.7}{23} \frac{8.1}{26} \frac{8.9}{29} \frac{8.5}{32} \frac{8.1}{33} \frac{8.0}{35} \frac{8.8}{36} \frac{8.6}{45} \frac{7.2}{60}$$

$$\checkmark \quad \frac{6.9}{200} \frac{7.0}{150} \frac{7.0}{100} \frac{7.2}{50} \frac{7.0}{25} \frac{7.0}{18} \frac{7.0}{10} \quad \frac{7.0}{70} \quad \frac{7.2}{10} \frac{7.4}{18} \frac{7.8}{24} \frac{8.8}{26} \frac{9.0}{29} \frac{8.9}{31} \frac{8.1}{33} \frac{8.4}{34} \frac{8.6}{36} \frac{9.2}{45} \frac{9.2}{60}$$

$$\checkmark \quad \frac{7.4}{60} \frac{7.4}{43} \frac{7.3}{24} \frac{7.2}{18} \frac{7.1}{10} \quad \frac{7.2}{72} \quad \frac{7.5}{10} \frac{7.5}{19} \frac{7.9}{23} \frac{8.1}{27} \frac{8.1}{30} \frac{9.0}{32} \frac{8.7}{33} \frac{8.5}{35} \frac{9.0}{36} \frac{8.8}{46} \frac{9.3}{60}$$

STA	+	Δ	-	ELEV
-----	---	---	---	------

980.93.

70+80				73.6 .
-------	--	--	--	--------

+81				73.6 .
-----	--	--	--	--------

71				73.6 .
----	--	--	--	--------

+50				73.3 .
-----	--	--	--	--------

T.P.	2.79	976.30	7.42	973.51.
------	------	--------	------	---------

72				73.1 .
----	--	--	--	--------

+50				72.9 .
-----	--	--	--	--------

73				72.6 .
----	--	--	--	--------

+50				72.0 .
-----	--	--	--	--------

LT

9

RT

✓ $\frac{8.7}{60} \frac{8.6}{46} \frac{8.8}{32} \frac{8.8}{29} \frac{8.6}{26} \frac{7.6}{23} \frac{7.3}{18} \frac{7.2}{10} \frac{7.4}{10} \frac{7.6}{18} \frac{8.0}{23} \frac{9.0}{26} \frac{9.2}{29} \frac{9.1}{31} \frac{8.2}{33} \frac{8.6}{35} \frac{7.1}{36} \frac{9.1}{46} \frac{9.7}{60}$

✓ $\frac{7.5}{60} \frac{7.4}{50} \frac{7.5}{34} \frac{8.8}{30} \frac{8.7}{28} \frac{8.5}{26} \frac{7.1}{22} \frac{7.3}{19} \frac{7.3}{10} \frac{7.3}{10} \frac{7.5}{10} \frac{7.6}{18} \frac{8.0}{23} \frac{9.2}{27} \frac{9.3}{29} \frac{7.2}{32} \frac{8.4}{33} \frac{8.6}{35} \frac{9.1}{36} \frac{9.7}{46} \frac{9.7}{60}$

✓ $\frac{7.2}{60} \frac{7.5}{50} \frac{7.8}{33} \frac{9.0}{30} \frac{9.0}{28} \frac{8.9}{26} \frac{7.4}{22} \frac{7.3}{17} \frac{7.3}{10} \frac{7.3}{10} \frac{7.5}{10} \frac{7.6}{18} \frac{7.9}{23} \frac{9.2}{26} \frac{9.3}{29} \frac{9.3}{31} \frac{8.4}{33} \frac{8.6}{35} \frac{9.1}{36} \frac{9.7}{46} \frac{9.7}{60}$

✓ $\frac{7.9}{60} \frac{8.0}{38} \frac{8.2}{34} \frac{9.3}{30} \frac{9.5}{27} \frac{9.3}{25} \frac{8.1}{22} \frac{7.8}{18} \frac{7.6}{10} \frac{7.6}{10} \frac{7.8}{10} \frac{7.9}{18} \frac{8.4}{24} \frac{9.5}{27} \frac{9.6}{29} \frac{9.5}{31} \frac{8.8}{33} \frac{9.1}{35} \frac{7.4}{36} \frac{9.2}{46} \frac{9.4}{60}$

✓ $\frac{3.9}{60} \frac{3.7}{50} \frac{3.7}{34} \frac{5.1}{30} \frac{5.1}{27} \frac{3.6}{25} \frac{3.4}{21} \frac{3.2}{19} \frac{3.2}{10} \frac{3.2}{10} \frac{3.3}{10} \frac{3.6}{20} \frac{4.2}{24} \frac{4.9}{26} \frac{5.1}{28} \frac{5.1}{31} \frac{4.4}{33} \frac{4.6}{35} \frac{5.0}{36} \frac{4.7}{46} \frac{5.0}{60}$

✓ $\frac{3.9}{60} \frac{4.0}{34} \frac{5.6}{30} \frac{5.5}{27} \frac{3.8}{22} \frac{3.5}{18} \frac{3.4}{10} \frac{3.4}{10} \frac{3.6}{10} \frac{3.8}{20} \frac{4.3}{24} \frac{5.4}{27} \frac{5.5}{28} \frac{5.5}{31} \frac{5.5}{33} \frac{5.5}{35} \frac{5.1}{36} \frac{4.8}{46} \frac{5.2}{60}$

✓ $\frac{3.9}{60} \frac{4.7}{38} \frac{5.5}{31} \frac{5.6}{28} \frac{5.4}{26} \frac{3.9}{21} \frac{3.9}{10} \frac{3.9}{10} \frac{3.9}{10} \frac{4.1}{20} \frac{4.5}{23} \frac{5.8}{26} \frac{5.8}{31} \frac{4.7}{33} \frac{4.8}{35} \frac{5.5}{36} \frac{5.0}{46} \frac{5.3}{60}$

✓ $\frac{4.5}{60} \frac{4.7}{43} \frac{5.3}{35} \frac{6.0}{30} \frac{6.1}{28} \frac{6.0}{26} \frac{4.5}{21} \frac{4.4}{18} \frac{4.4}{10} \frac{4.4}{10} \frac{4.7}{20} \frac{5.3}{23} \frac{6.2}{26} \frac{6.2}{31} \frac{5.2}{33} \frac{5.5}{35} \frac{5.5}{36} \frac{5.4}{46} \frac{5.7}{60}$

STA	+	⌒	-	ELEV
		976.30		
		5.2		
74+00		70.20		71.3 .
+50				70.8 .
75				70.4 .
+50				69.8 .
76				69.5 .
+50				69.0 .
T.P.	2.27	970.46 .	8.11	968.19 .
77				68.7 .
+42				68.2 .
+50				68.1 .

LT

Z

RT

$$\checkmark \begin{array}{cccccccccccc} \frac{5.0}{60} & \frac{5.2}{34} & \frac{6.1}{36} & \frac{6.4}{27} & \frac{6.3}{26} & \frac{5.0}{21} & \frac{5.0}{10} & \frac{5.0}{50} & \frac{5.1}{10} & \frac{5.3}{19} & \frac{5.5}{22} & \frac{6.7}{26} & \frac{6.9}{30} & \frac{5.6}{33} & \frac{5.6}{34} & \frac{6.2}{35} & \frac{5.9}{38} & \frac{6.1}{60} \end{array}$$

69.4

$$\checkmark \begin{array}{cccccccccccc} \frac{6.1}{60} & \frac{6.2}{36} & \frac{6.9}{29} & \frac{6.9}{25} & \frac{5.8}{21} & \frac{5.6}{19} & \frac{5.6}{10} & \frac{5.5}{50} & \frac{5.7}{10} & \frac{5.8}{20} & \frac{6.2}{22} & \frac{7.5}{26} & \frac{7.5}{31} & \frac{6.1}{33} & \frac{6.4}{35} & \frac{7.6}{36} & \frac{6.2}{38} & \frac{6.5}{60} \end{array}$$

68.8

$$\checkmark \begin{array}{cccccccccccc} \frac{6.7}{60} & \frac{7.5}{27} & \frac{7.4}{25} & \frac{6.4}{21} & \frac{6.1}{18} & \frac{6.1}{10} & \frac{6.1}{5.9} & \frac{6.0}{10} & \frac{6.2}{19} & \frac{6.5}{22} & \frac{7.9}{26} & \frac{8.0}{30} & \frac{6.6}{33} & \frac{6.9}{35} & \frac{7.1}{36} & \frac{6.8}{38} & \frac{6.6}{46} & \frac{7.0}{60} \end{array}$$

68.1

$$\checkmark \begin{array}{cccccccccccc} \frac{6.8}{60} & \frac{7.3}{39} & \frac{8.1}{30} & \frac{8.2}{26} & \frac{6.9}{22} & \frac{6.7}{18} & \frac{6.5}{10} & \frac{6.7}{65} & \frac{6.6}{10} & \frac{7.0}{19} & \frac{8.3}{22} & \frac{8.3}{27} & \frac{7.2}{30} & \frac{7.2}{33} & \frac{7.5}{34} & \frac{7.3}{35} & \frac{7.3}{38} & \frac{7.4}{45} & \frac{7.4}{60} \end{array}$$

67.7

$$\checkmark \begin{array}{cccccccccccc} \frac{7.6}{60} & \frac{7.6}{34} & \frac{8.6}{31} & \frac{8.6}{26} & \frac{7.5}{22} & \frac{7.1}{19} & \frac{6.9}{10} & \frac{6.9}{68} & \frac{6.9}{10} & \frac{7.1}{20} & \frac{7.3}{24} & \frac{8.7}{26} & \frac{8.8}{30} & \frac{7.4}{33} & \frac{7.3}{34} & \frac{7.3}{35} & \frac{7.3}{38} & \frac{8.1}{45} & \frac{8.1}{60} \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} \frac{8.2}{60} & \frac{8.0}{33} & \frac{9.0}{31} & \frac{9.0}{28} & \frac{8.7}{25} & \frac{7.5}{20} & \frac{7.3}{10} & \frac{7.3}{7.3} & \frac{7.4}{10} & \frac{7.4}{18} & \frac{7.5}{22} & \frac{9.0}{26} & \frac{9.2}{28} & \frac{9.2}{30} & \frac{8.1}{31} & \frac{7.8}{38} & \frac{8.4}{40} & \frac{8.4}{60} \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} \frac{2.6}{60} & \frac{2.9}{33} & \frac{3.6}{31} & \frac{3.5}{26} & \frac{2.4}{23} & \frac{2.1}{19} & \frac{1.9}{10} & \frac{1.8}{1.8} & \frac{1.9}{10} & \frac{2.0}{18} & \frac{2.3}{23} & \frac{3.7}{26} & \frac{3.7}{30} & \frac{2.3}{32} & \frac{2.1}{33} & \frac{2.1}{40} & \frac{2.1}{60} \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} \frac{2.7}{60} & \frac{2.7}{33} & \frac{3.9}{30} & \frac{3.7}{26} & \frac{2.6}{22} & \frac{2.4}{20} & \frac{2.3}{10} & \frac{2.3}{2.3} & \frac{2.4}{10} & \frac{2.5}{18} & \frac{2.7}{22} & \frac{3.9}{26} & \frac{4.1}{28} & \frac{3.9}{30} & \frac{2.4}{33} & \frac{2.6}{44} & \frac{2.6}{60} \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} \frac{2.7}{60} & \frac{2.7}{33} & \frac{3.9}{30} & \frac{3.7}{26} & \frac{2.6}{22} & \frac{2.4}{20} & \frac{2.4}{10} & \frac{2.4}{2.4} & \frac{2.5}{10} & \frac{2.6}{19} & \frac{2.7}{21} & \frac{4.1}{26} & \frac{3.3}{28} & \frac{3.3}{33} & \frac{2.9}{48} & \frac{3.0}{60} \end{array}$$

STA	+	π	-	ELEV
-----	---	-------	---	------

		970.46.		
--	--	---------	--	--

78				67.6 .
----	--	--	--	--------

+50				66.9 .
-----	--	--	--	--------

+75				66.6 .
-----	--	--	--	--------

+81				66.5 .
-----	--	--	--	--------

+90				66.3 .
-----	--	--	--	--------

79				66.2 .
----	--	--	--	--------

+08	NEW BRIGHTON RD LT			66.1 .
-----	--------------------	--	--	--------

X

+26				65.9 .
-----	--	--	--	--------

LT

Z

RT

$$\checkmark \begin{array}{cccccccc} 3.1 & 3.2 & 4.5 & 4.2 & 4.5 & 3.1 & 3.1 & 2.9 \\ 60 & 38 & 30 & 28 & 25 & 21 & 18 & 10 \end{array} \quad \begin{array}{cccc} 3.0 & 3.2 & 3.3 & 4.4 \\ 10 & 18 & 21 & 25 \end{array} \quad \begin{array}{cccc} 4.0 & 3.7 & 3.6 & \\ 33 & 47 & 60 & \end{array}$$

$$\checkmark \begin{array}{cccccccc} 3.1 & 3.9 & 5.3 & 5.5 & 5.4 & 3.9 & 3.9 & 3.7 \\ 60 & 34 & 31 & 29 & 26 & 21 & 18 & 10 \end{array} \quad \begin{array}{cccc} 3.7 & 3.8 & 4.2 & 5.4 \\ 10 & 18 & 22 & 26 \end{array} \quad \begin{array}{cccc} 5.4 & 4.4 & 4.2 & 4.1 \\ 29 & 33 & 40 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccc} 3.9 & 4.4 & 6.3 & 6.3 & 6.5 & 4.4 & 4.3 & 4.0 \\ 60 & 40 & 36 & 32 & 28 & 25 & 20 & 10 \end{array} \quad \begin{array}{cc} 4.1 & 4.1 \\ 10 & 18 \end{array} \quad \begin{array}{cccc} 4.4 & 5.8 & 5.9 & 5.7 \\ 22 & 26 & 28 & 29 \end{array} \quad \begin{array}{cc} 4.8 & 4.5 \\ 33 & 60 \end{array}$$

$$\checkmark \begin{array}{cccc} 5.8 & 6.1 & 4.4 & 4.4 \\ 60 & 41 & 34 & 22 \end{array} \quad \begin{array}{c} 4.1 \\ 10 \end{array} \quad \begin{array}{cccc} 4.1 & 4.2 & 4.6 & 5.8 \\ 10 & 18 & 22 & 26 \end{array} \quad \begin{array}{cc} 6.0 & 4.9 \\ 28 & 32 \end{array} \quad \begin{array}{c} 4.5 \\ 60 \end{array}$$

$$\checkmark \begin{array}{cccc} 4.5 & 4.4 & 4.3 & 4.2 \\ 60 & 42 & 21 & 10 \end{array} \quad \begin{array}{cccc} 4.2 & 4.4 & 4.2 & 6.0 \\ 10 & 18 & 21 & 26 \end{array} \quad \begin{array}{cc} 6.1 & 6.0 \\ 28 & 30 \end{array} \quad \begin{array}{cc} 4.9 & 4.5 \\ 33 & 60 \end{array}$$

$$\checkmark \begin{array}{cccc} 4.4 & 4.4 & 4.3 & 4.4 \\ 60 & 39 & 22 & 10 \end{array} \quad \begin{array}{cc} 4.4 & 4.4 \\ 10 & 18 \end{array} \quad \begin{array}{cccc} 4.1 & 6.0 & 6.2 & 6.0 \\ 22 & 26 & 28 & 31 \end{array} \quad \begin{array}{cc} 4.9 & 4.4 \\ 33 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccc} 3.9 & 4.2 & 4.3 & 4.4 & 4.3 & 4.4 \\ 200 & 150 & 100 & 50 & 33 & 13 \end{array} \quad \begin{array}{cc} 4.5 & 4.4 \\ 10 & 18 \end{array} \quad \begin{array}{cccc} 4.4 & 4.6 & 4.7 & 6.2 \\ 10 & 18 & 23 & 26 \end{array} \quad \begin{array}{cccc} 6.4 & 6.1 & 5.0 & 4.3 \\ 28 & 30 & 33 & 60 \end{array}$$

$$\checkmark \begin{array}{cccc} 4.6 & 4.8 & 4.9 & 4.2 \\ 60 & 40 & 26 & 14 \end{array} \quad \begin{array}{c} 4.1 \\ 10 \end{array} \quad \begin{array}{cccc} 4.1 & 4.2 & 4.8 & 6.3 \\ 10 & 18 & 21 & 26 \end{array} \quad \begin{array}{cc} 6.4 & 6.1 \\ 28 & 31 \end{array} \quad \begin{array}{cc} 4.8 & 4.3 \\ 33 & 60 \end{array}$$

STA	+	π	-	ELEV
		970.46.		
79+34				65.7 .
+42				65.6 .
+50				65.5 .
B.M	4.37	970.46.	4.37	96.609 . 966.13
B.M	3.98	970.46.	3.98	966.48 .
80				64.9 .
+50				64.4 .
81				63.9 .
+36	SECTION	MONOLITHIC CULV		63.6 .
+50				63.5 .

LT

L

RT

FLOOR
HOUSE

✓ 5.7 6.0 6.1 5.0 5.0 4.9 4.7 4.9 5.0 6.6 6.6 6.5 4.9 4.3 1.9
6.0 5.4 4.3 3.1 2.0 1.0 1.8 1.8 2.2 2.6 2.8 3.1 3.3 4.2 4.2

✓ 4.5 4.9 6.1 6.7 6.5 6.2 5.1 5.2 5.0 4.9 4.9 5.0 6.6 6.6 6.5 4.9 4.8
6.0 4.7 3.9 3.5 3.0 2.6 2.3 1.8 1.0 4.9 1.6 1.8 2.2 2.6 2.8 3.1 3.3 4.2

✓ 4.5 4.7 5.1 6.7 6.7 6.5 5.1 5.2 5.1 5.1 5.2 5.2 6.8 6.9 6.7 5.1 4.4
6.0 4.3 3.4 3.1 2.8 2.5 2.2 1.9 1.0 5.0 1.0 1.8 2.2 2.6 2.8 3.0 3.3 4.2

Top SEC COR IRON NEW-BRIGHTON RD + LARPENTUER

Top N.W. COR BOTTOM STEP RT 79+40

✓ 5.1 5.7 5.9 6.0 7.4 7.7 7.5 6.1 5.6 5.6 5.7 5.9 6.0 7.4 7.7 7.6 6.4 6.2
6.0 5.2 3.7 3.4 3.1 2.8 2.6 2.2 2.0 1.0 5.6 1.0 1.9 2.2 2.6 2.8 3.1 3.3 6.0

✓ 6.2 6.6 7.1 6.6 6.6 8.2 7.8 6.7 6.1 6.2 6.3 6.4 6.7 8.4 8.2 8.0
6.0 5.0 4.3 4.1 3.7 3.4 3.1 2.8 2.6 2.2 2.0 1.0 6.1 1.0 2.0 2.2 2.6 2.8 3.1 3.3 6.0

✓ 7.3 7.8 7.4 7.5 8.5 8.0 6.8 6.7 6.7 6.8 6.8 6.9 9.1 8.6 8.3 8.5
6.0 5.3 3.8 3.6 3.4 3.1 2.6 2.4 2.2 2.0 1.0 6.6 1.0 2.0 2.2 2.6 2.8 3.1 3.3 6.0

F.L

F.L

✓ 8.1 8.2 8.1 8.0 9.2 9.2 9.6 9.6 7.0 7.0 6.9 7.2 9.8 9.8 9.5 8.7 8.7
6.0 4.2 3.9 3.4 3.2 2.6 2.6 2.1 2.1 1.0 6.9 1.0 2.1 2.1 2.6 2.6 3.1 3.1 6.0

✓ 8.2 8.4 8.1 8.2 9.2 8.9 7.4 6.9 7.0 7.3 7.3 7.7 9.6 9.3 9.1 9.1
6.0 4.2 3.8 3.4 3.1 2.8 2.4 2.1 1.0 7.0 1.0 1.9 2.1 2.6 2.6 3.1 3.1 6.0

STA	+	Δ	-	ELEV
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		970.46		
--	--	--------	--	--

82+00				63.3
-------	--	--	--	------

+50				63.1
-----	--	--	--	------

T.P	3.44	966.12	7.78	962.68
-----	------	--------	------	--------

83				63.2
----	--	--	--	------

+50				63.0
-----	--	--	--	------

84				62.8
----	--	--	--	------

+45				62.5
-----	--	--	--	------

+50				62.5
-----	--	--	--	------

85				62.0
----	--	--	--	------

LT

♀

RT

$\frac{8.0}{60}$ $\frac{8.6}{40}$ $\frac{8.1}{36}$ $\frac{8.3}{34}$ $\frac{8.8}{32}$ $\frac{8.8}{27}$ $\frac{7.6}{25}$ $\frac{7.2}{20}$ $\frac{7.2}{10}$ $\frac{7.2}{7.2}$ $\frac{7.5}{10}$ $\frac{7.4}{21}$ $\frac{7.9}{23}$ $\frac{9.9}{27-29}$ $\frac{9.5}{31}$ $\frac{9.2}{37}$ $\frac{9.6}{60}$

$\frac{8.1}{60}$ $\frac{8.3}{42}$ $\frac{8.3}{34}$ $\frac{8.9}{31}$ $\frac{9.6}{30-29}$ $\frac{8.8}{28}$ $\frac{7.7}{24}$ $\frac{7.5}{22}$ $\frac{7.4}{10}$ $\frac{7.4}{7.4}$ $\frac{7.7}{10}$ $\frac{7.6}{20}$ $\frac{7.9}{22}$ $\frac{7.9}{27}$ $\frac{10.2}{27-31}$ $\frac{9.5}{37}$ $\frac{9.8}{60}$

$\frac{4.0}{60}$ $\frac{4.3}{46}$ $\frac{3.9}{34}$ $\frac{4.9}{31-30}$ $\frac{5.5}{30-28}$ $\frac{3.6}{25}$ $\frac{3.2}{18}$ $\frac{3.1}{10}$ $\frac{2.9}{2.9}$ $\frac{3.1}{10}$ $\frac{3.3}{18}$ $\frac{3.7}{23}$ $\frac{5.8}{27}$ $\frac{5.5}{32}$ $\frac{5.3}{60}$

$\frac{4.0}{60}$ $\frac{4.4}{45}$ $\frac{4.0}{34}$ $\frac{4.9}{30-27}$ $\frac{3.8}{24}$ $\frac{3.4}{18}$ $\frac{3.2}{10}$ $\frac{3.2}{3.1}$ $\frac{3.4}{10}$ $\frac{3.6}{18}$ $\frac{3.6}{23}$ $\frac{5.7}{27-29}$ $\frac{5.2}{31}$ $\frac{5.0}{38}$ $\frac{4.8}{60}$

$\frac{3.7}{60}$ $\frac{4.0}{50}$ $\frac{4.8}{38}$ $\frac{4.2}{34}$ $\frac{5.3}{31-27}$ $\frac{4.0}{24}$ $\frac{3.6}{18}$ $\frac{3.5}{10}$ $\frac{3.3}{3.3}$ $\frac{3.4}{10}$ $\frac{3.4}{18}$ $\frac{3.6}{22}$ $\frac{6.2}{28-30}$ $\frac{4.4}{33}$ $\frac{4.2}{60}$

$\frac{4.0}{60}$ $\frac{4.5}{50}$ $\frac{5.0}{46}$ $\frac{5.2}{36}$ $\frac{4.6}{34}$ $\frac{5.5}{31}$ $\frac{5.4}{26}$ $\frac{4.1}{23}$ $\frac{3.8}{18}$ $\frac{3.7}{10}$ $\frac{3.6}{3.6}$ $\frac{3.7}{10}$ $\frac{3.8}{18}$ $\frac{3.9}{21}$ $\frac{6.6}{28-31}$ $\frac{4.6}{33}$ $\frac{5.0}{60}$

$\frac{4.0}{60}$ $\frac{4.5}{50}$ $\frac{5.0}{46}$ $\frac{5.2}{36}$ $\frac{4.6}{34}$ $\frac{5.6}{31}$ $\frac{5.5}{28}$ $\frac{4.2}{24}$ $\frac{3.9}{18}$ $\frac{3.7}{10}$ $\frac{3.6}{3.6}$ $\frac{3.7}{10}$ $\frac{3.8}{18}$ $\frac{4.0}{22}$ $\frac{6.7}{27-30}$ $\frac{6.0}{32}$ $\frac{6.3}{60}$

$\frac{4.8}{60}$ $\frac{5.0}{57}$ $\frac{5.5}{47}$ $\frac{5.4}{38}$ $\frac{5.2}{34}$ $\frac{6.1}{32}$ $\frac{5.9}{26}$ $\frac{4.7}{22}$ $\frac{4.3}{18}$ $\frac{4.2}{10}$ $\frac{4.1}{4.1}$ $\frac{4.2}{10}$ $\frac{4.4}{18}$ $\frac{4.6}{22}$ $\frac{6.7}{27}$ $\frac{6.7}{35}$ $\frac{6.7}{60}$

STA	+	↑	-	ELEV
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		966.12.		
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85+50				61.6 .
-------	--	--	--	--------

86				61.3 .
----	--	--	--	--------

+50				61.2 .
-----	--	--	--	--------

+67				61.2 .
-----	--	--	--	--------

+73				61.2 .
-----	--	--	--	--------

87				61.1 .
----	--	--	--	--------

+50				60.8 .
-----	--	--	--	--------

88				60.6 .
----	--	--	--	--------

LT

Q

RT

$\frac{5.5}{60}$ $\frac{5.6}{38}$ $\frac{5.7}{34}$ $\frac{6.3}{32}$ $\frac{6.3}{26}$ $\frac{5.2}{23}$ $\frac{4.7}{18}$ $\frac{4.5}{10}$ $\frac{4.7}{10}$ $\frac{4.9}{18}$ $\frac{5.1}{22}$ $\frac{7.3}{27}$ $\frac{7.1}{31}$ $\frac{7.0}{41}$ $\frac{7.0}{60}$

$\frac{5.6}{60}$ $\frac{5.8}{37}$ $\frac{5.9}{34}$ $\frac{6.4}{32}$ $\frac{6.5}{27}$ $\frac{5.3}{24}$ $\frac{4.9}{18}$ $\frac{4.8}{10}$ $\frac{4.8}{10}$ $\frac{5.1}{10}$ $\frac{5.4}{20}$ $\frac{7.7}{28}$ $\frac{7.5}{60}$

$\frac{5.3}{60}$ $\frac{5.8}{47}$ $\frac{5.8}{36}$ $\frac{5.9}{31}$ $\frac{6.5}{32}$ $\frac{6.7}{27}$ $\frac{5.3}{21}$ $\frac{5.0}{18}$ $\frac{4.9}{10}$ $\frac{4.9}{10}$ $\frac{5.1}{18}$ $\frac{5.4}{21}$ $\frac{5.6}{28}$ $\frac{8.0}{34}$ $\frac{7.8}{60}$

$\frac{4.8}{60}$ $\frac{5.3}{50}$ $\frac{5.6}{36}$ $\frac{5.9}{34}$ $\frac{6.6}{32}$ $\frac{6.7}{27}$ $\frac{5.6}{24}$ $\frac{5.1}{18}$ $\frac{4.9}{10}$ $\frac{4.9}{10}$ $\frac{5.1}{18}$ $\frac{5.3}{18}$ $\frac{5.4}{20}$ $\frac{8.0}{28}$ $\frac{7.6}{30}$ $\frac{7.7}{32}$ $\frac{7.7}{60}$

$\frac{4.8}{60}$ $\frac{5.3}{50}$ $\frac{5.6}{36}$ $\frac{5.9}{34}$ $\frac{6.6}{32}$ $\frac{6.7}{27}$ $\frac{5.6}{24}$ $\frac{5.1}{18}$ $\frac{5.0}{10}$ $\frac{4.9}{10}$ $\frac{5.1}{18}$ $\frac{5.3}{18}$ $\frac{5.8}{22}$ $\frac{8.3}{28}$ $\frac{6.6}{30}$ $\frac{6.5}{34}$ $\frac{6.5}{60}$

$\frac{4.5}{60}$ $\frac{5.3}{45}$ $\frac{5.5}{37}$ $\frac{5.7}{34}$ $\frac{6.8}{31}$ $\frac{6.9}{26}$ $\frac{5.7}{23}$ $\frac{5.2}{18}$ $\frac{5.0}{10}$ $\frac{5.0}{10}$ $\frac{5.2}{10}$ $\frac{5.5}{19}$ $\frac{5.9}{22}$ $\frac{8.1}{28}$ $\frac{6.5}{30}$ $\frac{6.2}{34}$ $\frac{6.2}{60}$

$\frac{4.9}{60}$ $\frac{5.6}{38}$ $\frac{5.3}{37}$ $\frac{5.7}{34}$ $\frac{6.8}{31}$ $\frac{7.0}{27}$ $\frac{5.8}{21}$ $\frac{5.6}{18}$ $\frac{5.4}{10}$ $\frac{5.3}{10}$ $\frac{5.4}{10}$ $\frac{5.6}{18}$ $\frac{5.7}{21}$ $\frac{8.2}{27}$ $\frac{7.1}{30}$ $\frac{7.1}{33}$ $\frac{7.0}{60}$

$\frac{5.8}{60}$ $\frac{6.5}{37}$ $\frac{6.1}{36}$ $\frac{6.5}{34}$ $\frac{7.5}{31}$ $\frac{7.5}{25}$ $\frac{6.0}{22}$ $\frac{5.7}{18}$ $\frac{5.6}{10}$ $\frac{5.5}{10}$ $\frac{5.6}{10}$ $\frac{5.8}{18}$ $\frac{6.1}{21}$ $\frac{8.4}{28}$ $\frac{6.7}{30}$ $\frac{7.2}{34}$ $\frac{7.2}{60}$

STA	+	π	-	ELEV
-----	---	-------	---	------

		966.12.		
--	--	---------	--	--

88+50				60.3
-------	--	--	--	------

89				60.1
----	--	--	--	------

+50				59.8
-----	--	--	--	------

T.P.	4.51	96420.	6.43	959.69.
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+72				59.8
-----	--	--	--	------

+75				59.8
-----	--	--	--	------

				X
--	--	--	--	---

90				59.6
----	--	--	--	------

+27				59.5
-----	--	--	--	------

+28				59.5
-----	--	--	--	------

B.M	5.14	96420.	5.14	959.06.	959.10
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B.M	1.13	96243.	2.90	961.30.	
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LT

2

RT

✓ $\frac{6.8}{60} \frac{7.3}{37} \frac{6.9}{36} \frac{7.2}{34} \frac{7.7}{32} \frac{7.7}{26} \frac{6.0}{21} \frac{5.8}{18} \frac{5.8}{10} \frac{5.8}{10} \frac{5.9}{10} \frac{5.9}{18} \frac{5.9}{21} \frac{8.6}{27-30} \frac{6.9}{33} \frac{7.2}{60}$

✓ $\frac{7.4}{60} \frac{7.8}{36} \frac{7.9}{34} \frac{8.4}{31} \frac{8.4}{26} \frac{6.7}{21} \frac{6.3}{18} \frac{6.1}{10} \frac{6.0}{10} \frac{6.2}{18} \frac{6.4}{21} \frac{8.8}{27-30} \frac{7.4}{33} \frac{7.7}{60}$

✓ $\frac{7.7}{60} \frac{7.7}{35} \frac{8.0}{34} \frac{8.6}{31} \frac{8.8}{26} \frac{7.0}{20} \frac{6.6}{18} \frac{6.4}{10} \frac{6.3}{10} \frac{6.3}{10} \frac{6.5}{18} \frac{6.9}{21} \frac{9.2}{26-30} \frac{8.2}{35} \frac{7.7}{39} \frac{7.8}{60}$

✓ $\frac{5.8}{60} \frac{6.1}{48} \frac{6.0}{35} \frac{6.2}{34} \frac{6.8}{32} \frac{6.5}{25} \frac{5.2}{22} \frac{4.7}{18} \frac{4.6}{10} \frac{4.4}{10} \frac{4.5}{10} \frac{4.8}{18} \frac{5.0}{22} \frac{7.3}{27-30} \frac{6.1}{35} \frac{6.1}{60}$

✓ $\frac{5.8}{60} \frac{6.1}{48} \frac{6.0}{35} \frac{6.2}{34} \frac{6.8}{32} \frac{6.5}{25} \frac{5.2}{22} \frac{4.7}{18} \frac{4.6}{10} \frac{4.4}{10} \frac{4.5}{10} \frac{4.8}{18} \frac{4.8}{21} \frac{5.2}{35} \frac{5.2}{60}$

✓ $\frac{5.9}{60} \frac{6.0}{45} \frac{6.0}{36} \frac{6.1}{34} \frac{6.6}{32} \frac{6.7}{27} \frac{5.3}{22} \frac{4.9}{18} \frac{4.7}{10} \frac{4.6}{10} \frac{4.4}{18} \frac{4.7}{32} \frac{5.1}{40} \frac{5.2}{60}$

✓ $\frac{5.8}{60} \frac{6.1}{45} \frac{5.9}{36} \frac{6.2}{34} \frac{6.7}{32} \frac{6.5}{25} \frac{5.1}{20} \frac{4.7}{10} \frac{4.7}{10} \frac{4.8}{10} \frac{5.2}{18} \frac{5.1}{33} \frac{4.7}{60}$

✓ $\frac{5.8}{60} \frac{6.1}{45} \frac{5.9}{36} \frac{6.2}{34} \frac{6.7}{32} \frac{6.5}{25} \frac{5.1}{20} \frac{4.7}{10} \frac{4.7}{10} \frac{4.8}{10} \frac{5.2}{18} \frac{5.6}{22} \frac{7.5}{26} \frac{7.4}{30} \frac{6.7}{33} \frac{6.8}{60}$

TOP MONT

STA

92+

S.W. COR LOWER STEP

LT STA 93+70

STA	+	π	-	ELEV
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		962.43.		
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90+50				
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			59.4	.
--	--	--	------	---

91				
----	--	--	--	--

			59.3	.
--	--	--	------	---

+50				
-----	--	--	--	--

			59.2	.
--	--	--	------	---

92				
----	--	--	--	--

			59.1	.
--	--	--	------	---

+20				
-----	--	--	--	--

			59.0	.
--	--	--	------	---

+23				
-----	--	--	--	--

			59.0	.
--	--	--	------	---

+50				
-----	--	--	--	--

			59.0	.
--	--	--	------	---

93				
----	--	--	--	--

			58.6	.
--	--	--	------	---

LT

E

PT

$$\checkmark \begin{array}{ccccccc} \frac{4.2}{60} & \frac{4.1}{37} & \frac{4.0}{34} & \frac{4.9}{30} & \frac{4.9}{27} & \frac{3.9}{26} & \frac{3.4}{23} & \frac{3.0}{18} & \frac{3.0}{10} & \frac{3.1}{10} & \frac{3.5}{18} & \frac{3.9}{22} & \frac{5.9}{27} & \frac{5.8}{35} & \frac{5.8}{60} \end{array}$$

$$\checkmark \begin{array}{ccccccc} \frac{4.1}{60} & \frac{4.3}{37} & \frac{3.9}{36} & \frac{3.9}{35} & \frac{4.9}{32} & \frac{4.9}{26} & \frac{3.8}{23} & \frac{3.5}{19} & \frac{3.2}{10} & \frac{3.2}{10} & \frac{3.7}{19} & \frac{4.2}{22} & \frac{5.9}{27} & \frac{6.1}{30} & \frac{5.8}{31} & \frac{5.1}{37} & \frac{5.2}{60} \end{array}$$

$$\checkmark \begin{array}{ccccccc} \frac{4.1}{60} & \frac{4.4}{36} & \frac{4.2}{35} & \frac{5.1}{32} & \frac{4.9}{27} & \frac{3.7}{24} & \frac{3.4}{18} & \frac{3.3}{10} & \frac{3.2}{32} & \frac{3.3}{10} & \frac{3.6}{20} & \frac{4.1}{23} & \frac{6.0}{27-30} & \frac{4.9}{33} & \frac{5.5}{60} \end{array}$$

$$\checkmark \begin{array}{ccccccc} \frac{4.1}{60} & \frac{4.6}{36} & \frac{4.2}{35} & \frac{5.0}{33} & \frac{4.9}{26} & \frac{4.0}{24} & \frac{3.6}{20} & \frac{3.4}{10} & \frac{3.3}{33} & \frac{3.4}{10} & \frac{3.5}{19} & \frac{3.8}{23} & \frac{5.9}{27-30} & \frac{4.8}{32} & \frac{5.1}{60} \end{array}$$

$$\checkmark \begin{array}{ccccccc} \frac{4.2}{60} & \frac{4.6}{36} & \frac{4.1}{35} & \frac{4.4}{38} & \frac{5.0}{31} & \frac{5.1}{27} & \frac{3.9}{23} & \frac{3.6}{18} & \frac{3.4}{10} & \frac{3.4}{10} & \frac{3.6}{20} & \frac{4.0}{23} & \frac{6.1}{27-29} & \frac{4.8}{33} & \frac{5.0}{60} \end{array}$$

$$\checkmark \begin{array}{ccccccc} \frac{4.2}{60} & \frac{4.6}{36} & \frac{4.1}{35} & \frac{4.4}{38} & \frac{5.0}{31} & \frac{5.1}{27} & \frac{3.9}{23} & \frac{3.6}{18} & \frac{3.4}{10} & \frac{3.4}{10} & \frac{3.7}{20} & \frac{4.2}{23} & \frac{6.1}{27-29} & \frac{3.7}{32} & \frac{4.3}{60} \end{array}$$

$$\checkmark \begin{array}{ccccccc} \frac{4.1}{60} & \frac{4.5}{36} & \frac{4.0}{35} & \frac{5.2}{38} & \frac{5.2}{27} & \frac{3.8}{23} & \frac{3.6}{17} & \frac{3.6}{10} & \frac{3.4}{10} & \frac{3.5}{10} & \frac{3.8}{18} & \frac{4.1}{22} & \frac{6.3}{26-28} & \frac{3.8}{31} & \frac{3.9}{37} & \frac{4.7}{60} \end{array}$$

$$\checkmark \begin{array}{ccccccc} \frac{4.2}{60} & \frac{4.5}{36} & \frac{4.1}{35} & \frac{5.2}{30} & \frac{5.6}{27} & \frac{5.3}{26} & \frac{4.1}{23} & \frac{3.8}{18} & \frac{3.9}{10} & \frac{3.9}{10} & \frac{3.9}{18} & \frac{4.1}{22} & \frac{6.3}{26-28} & \frac{3.9}{31} & \frac{4.2}{37} & \frac{4.9}{60} \end{array}$$

STA	+	↑	-	ELEV
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962.43 .

93+31	SECTION	MONOLITHIC CURV	58.3	.
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+50

58.1 .

+54

58.1 .

94

57.5 .

+13

57.4 .

+15

57.4 .

+50

56.9 .

+60

56.8 .

LT

F

RT

F.L

F.L

✓ $\frac{4.1}{60} \frac{4.5}{35} \frac{4.1}{33} \frac{5.4}{31} \frac{6.2}{30} \frac{7.2}{26} \frac{7.2}{21} \frac{8.4}{21} \frac{4.2}{10} \frac{4.2}{10} \frac{7.3}{21} \frac{7.4}{26} \frac{6.5}{26} \frac{4.3}{28} \frac{3.9}{31} \frac{4.5}{34} \frac{5.3}{38} \frac{5.3}{60}$

✓ $\frac{4.1}{60} \frac{4.2}{33} \frac{5.1}{31} \frac{5.9}{30} \frac{5.8}{26} \frac{4.4}{23} \frac{4.2}{21} \frac{4.4}{10} \frac{4.4}{10} \frac{4.5}{19} \frac{4.8}{22} \frac{6.5}{25} \frac{6.6}{27} \frac{4.8}{30} \frac{4.0}{34} \frac{4.4}{37} \frac{5.0}{42} \frac{5.7}{60}$

✓ $\frac{3.3}{60} \frac{3.5}{37} \frac{3.9}{34} \frac{5.5}{31} \frac{5.7}{26} \frac{4.4}{22} \frac{4.3}{20} \frac{4.4}{10} \frac{4.4}{10} \frac{4.5}{19} \frac{4.8}{22} \frac{6.5}{25} \frac{6.7}{27} \frac{4.8}{30} \frac{3.9}{34} \frac{4.4}{37} \frac{5.0}{42} \frac{5.8}{60}$

✓ $\frac{3.7}{60} \frac{4.2}{38} \frac{4.7}{34} \frac{6.1}{31} \frac{6.0}{25} \frac{4.7}{21} \frac{4.9}{10} \frac{5.0}{10} \frac{4.9}{20} \frac{5.3}{22} \frac{7.5}{26} \frac{5.1}{28} \frac{4.9}{31} \frac{5.0}{34} \frac{6.1}{38} \frac{6.1}{60}$

✓ $\frac{3.8}{60} \frac{4.4}{37} \frac{4.9}{33} \frac{5.9}{31} \frac{6.1}{27} \frac{4.7}{22} \frac{5.0}{10} \frac{5.1}{5.0} \frac{5.2}{10} \frac{5.4}{19} \frac{8.0}{23} \frac{5.2}{26} \frac{5.3}{28} \frac{5.8}{32} \frac{5.8}{44} \frac{5.8}{60}$

✓ $\frac{5.0}{60} \frac{4.8}{34} \frac{4.9}{33} \frac{6.0}{31} \frac{6.1}{27} \frac{4.9}{23} \frac{5.1}{10} \frac{5.1}{5.0} \frac{5.2}{10} \frac{5.4}{19} \frac{8.0}{23} \frac{5.2}{26} \frac{5.3}{28} \frac{5.8}{32} \frac{5.8}{44} \frac{5.8}{60}$

✓ $\frac{5.6}{60} \frac{5.6}{34} \frac{7.0}{31} \frac{7.1}{26} \frac{5.5}{21} \frac{5.4}{18} \frac{5.5}{10} \frac{5.5}{5.5} \frac{5.7}{10} \frac{5.5}{21} \frac{8.2}{26} \frac{8.4}{28} \frac{5.6}{34} \frac{5.7}{38} \frac{6.4}{60}$

✓ $\frac{5.9}{60} \frac{5.8}{34} \frac{6.9}{32} \frac{7.1}{30} \frac{6.9}{26} \frac{5.5}{22} \frac{5.6}{18} \frac{5.6}{10} \frac{5.7}{5.6} \frac{5.8}{10} \frac{6.0}{19} \frac{8.4}{22} \frac{6.6}{28} \frac{6.0}{30} \frac{5.7}{34} \frac{6.4}{38} \frac{6.4}{60}$

STA + π - ELEV

962.43

95+00

5.6

56.8

56.83

+30

56.4

+50

56.1

96

55.5

+41

55.3

+46

55.3

T.P

4.63

959.82

7.24

95 519

+50

DRAWL RT

55.3

+51

MONO CULV RT & FRY LT

55.2

LT

E

RT

✓ $\frac{5.8}{60}$ $\frac{5.8}{34}$ $\frac{5.5}{32}$ $\frac{5.7}{18}$ $\frac{5.6}{10}$ $\frac{5.6}{10}$ $\frac{5.7}{10}$ $\frac{5.8}{19}$ $\frac{6.0}{22}$ $\frac{8.4}{28}$ $\frac{6.6}{32}$ $\frac{6.0}{34}$ $\frac{7.0}{44}$ $\frac{7.4}{60}$

✓ $\frac{8.0}{60}$ $\frac{8.0}{44}$ $\frac{5.3}{43}$ $\frac{5.8}{34}$ $\frac{6.1}{18}$ $\frac{6.0}{10}$ $\frac{6.0}{10}$ $\frac{6.2}{10}$ $\frac{6.3}{18}$ $\frac{6.6}{28}$ $\frac{9.0}{27}$ $\frac{7.5}{31}$ $\frac{7.2}{34}$ $\frac{7.7}{44}$ $\frac{8.3}{60}$

✓ $\frac{7.1}{60}$ $\frac{7.8}{37}$ $\frac{6.3}{33}$ $\frac{6.3}{10}$ $\frac{6.5}{10}$ $\frac{6.6}{18}$ $\frac{6.7}{22}$ $\frac{9.2}{26}$ $\frac{7.5}{29}$ $\frac{7.5}{31}$ $\frac{8.0}{34}$ $\frac{8.6}{41}$ $\frac{8.6}{60}$

✓ $\frac{7.8}{60}$ $\frac{8.1}{40}$ $\frac{8.3}{25}$ $\frac{7.0}{21}$ $\frac{7.0}{10}$ $\frac{6.9}{10}$ $\frac{7.0}{10}$ $\frac{7.0}{18}$ $\frac{7.3}{21}$ $\frac{10.0}{28}$ $\frac{8.8}{30}$ $\frac{9.5}{32}$ $\frac{9.1}{42}$ $\frac{9.1}{60}$

✓ $\frac{8.2}{60}$ $\frac{8.7}{33}$ $\frac{9.0}{28}$ $\frac{7.4}{24}$ $\frac{7.1}{18}$ $\frac{7.1}{10}$ $\frac{7.1}{10}$ $\frac{7.3}{10}$ $\frac{7.3}{18}$ $\frac{7.5}{20}$ $\frac{9.9}{27}$ $\frac{10.2}{29}$ $\frac{9.7}{32}$ $\frac{9.9}{39}$ $\frac{10.7}{60}$

✓ $\frac{8.0}{60}$ $\frac{7.6}{31}$ $\frac{7.0}{19}$ $\frac{7.1}{10}$ $\frac{7.1}{10}$ $\frac{7.2}{10}$ $\frac{7.2}{15}$ $\frac{7.2}{19}$ $\frac{7.4}{27}$ $\frac{9.9}{34}$ $\frac{10.1}{39}$ $\frac{10.2}{150}$ $\frac{10.5}{200}$

TOP SO HEDWALL N.W COR

✓ $\frac{5.4}{60}$ $\frac{5.2}{42}$ $\frac{4.5}{23}$ $\frac{4.3}{15}$ $\frac{4.6}{18}$ $\frac{4.5}{10}$ $\frac{4.6}{10}$ $\frac{4.7}{18}$ $\frac{7.2}{25}$ $\frac{7.3}{28}$ $\frac{7.5}{32}$ $\frac{8.4}{53}$ $\frac{8.8}{100}$ $\frac{9.1}{150}$ $\frac{9.4}{200}$ $\frac{9.4}{250}$

52.0
K.H.

$\frac{4.3}{200}$ $\frac{4.7}{150}$ $\frac{5.1}{100}$ $\frac{5.3}{56}$ $\frac{4.7}{34}$ $\frac{4.4}{16}$ $\frac{4.6}{10}$ $\frac{4.6}{10}$ $\frac{4.6}{10}$ $\frac{4.6}{11}$ $\frac{4.7}{11}$ $\frac{7.8}{21}$ $\frac{7.4}{30}$ $\frac{7.6}{34}$ $\frac{8.0}{50}$ $\frac{8.2}{60}$

STA	+	⌞	-	ELEV
		959.82		
96+65				55.2
+68	NEAR 15" C M CULV	LT		55.2
+73				55.2
				X
+84				55.2
+88				55.1
97	DRAWL	RT		55.1
+50				54.9
98				54.9
+50				54.9

LT

Z

RT

✓ $\frac{5.3}{60} \frac{5.3}{50} \frac{5.0}{37} \frac{4.3}{20} \frac{4.7}{10} \frac{4.7}{46} \frac{4.6}{10} \frac{7.3}{19} \frac{7.8}{26} \frac{7.2}{31} \frac{7.5}{33} \frac{7.9}{35} \frac{2.6}{36} \frac{8.1}{41} \frac{8.1}{60}$

FL

✓ $\frac{5.8}{60} \frac{6.0}{45} \frac{6.3}{39} \frac{6.8}{38} \frac{6.8}{34} \frac{4.8}{30} \frac{4.3}{15} \frac{4.7}{10} \frac{4.7}{46} \frac{4.5}{10} \frac{7.6}{19} \frac{7.8}{26} \frac{7.2}{29} \frac{7.4}{30} \frac{7.5}{31} \frac{7.9}{33} \frac{7.6}{35} \frac{8.1}{36} \frac{8.1}{41} \frac{8.1}{60}$

✓ $\frac{5.4}{60} \frac{5.3}{43} \frac{4.7}{30} \frac{4.4}{16} \frac{4.7}{10} \frac{4.7}{46} \frac{4.6}{10} \frac{7.2}{19} \frac{7.6}{26} \frac{7.9}{31} \frac{7.4}{33} \frac{7.7}{34} \frac{8.0}{36} \frac{7.7}{37} \frac{7.8}{47} \frac{8.2}{60}$

✓ $\frac{5.1}{60} \frac{5.2}{39} \frac{4.5}{24} \frac{4.6}{15} \frac{4.7}{10} \frac{4.7}{46} \frac{4.7}{10} \frac{7.5}{19} \frac{7.8}{26} \frac{8.0}{27} \frac{7.8}{34} \frac{8.2}{38} \frac{8.4}{50} \frac{8.4}{60}$

✓ $\frac{5.8}{60} \frac{5.5}{38} \frac{6.8}{29} \frac{4.7}{24} \frac{4.6}{16} \frac{4.7}{10} \frac{4.8}{47} \frac{4.8}{10} \frac{7.3}{20} \frac{7.9}{25} \frac{7.8}{26} \frac{7.7}{29} \frac{7.1}{31} \frac{7.1}{34} \frac{8.0}{36} \frac{8.0}{45} \frac{8.3}{60}$

✓ $\frac{6.1}{60} \frac{5.9}{33} \frac{6.6}{30} \frac{6.6}{26} \frac{4.9}{22} \frac{4.7}{19} \frac{4.8}{10} \frac{4.8}{47} \frac{4.9}{10} \frac{7.6}{19} \frac{7.7}{26} \frac{8.0}{30} \frac{8.1}{34} \frac{8.4}{36} \frac{8.4}{44} \frac{9.7}{100} \frac{9.7}{150} \frac{9.7}{200}$
 $\frac{10.1}{250} \frac{10.2}{300} \frac{10.2}{350} \frac{10.2}{400}$

✓ $\frac{6.2}{60} \frac{5.9}{33} \frac{6.6}{31} \frac{6.6}{27} \frac{6.3}{25} \frac{5.6}{23} \frac{5.1}{18} \frac{5.0}{10} \frac{5.0}{49} \frac{5.0}{10} \frac{5.0}{20} \frac{7.9}{26} \frac{7.0}{30} \frac{7.1}{33} \frac{7.3}{34} \frac{7.8}{40} \frac{8.7}{43} \frac{8.7}{60}$

✓ $\frac{5.8}{60} \frac{5.7}{34} \frac{6.8}{31} \frac{6.7}{26} \frac{5.8}{23} \frac{5.1}{13} \frac{5.0}{10} \frac{5.0}{49} \frac{5.0}{10} \frac{7.4}{20} \frac{6.5}{26} \frac{6.3}{30} \frac{6.4}{31} \frac{6.4}{34} \frac{6.2}{40} \frac{6.6}{44} \frac{7.5}{60}$

✓ $\frac{4.9}{60} \frac{5.5}{34} \frac{6.7}{31} \frac{6.9}{26} \frac{4.9}{22} \frac{4.8}{16} \frac{5.0}{10} \frac{4.9}{49} \frac{5.0}{10} \frac{5.3}{20} \frac{7.2}{26} \frac{7.3}{29} \frac{6.0}{32} \frac{5.9}{34} \frac{6.1}{44} \frac{6.5}{60}$

STA	+	Δ	-	ELEV
		959.82.		
99+00				55.1
+50				55.4
+89				55.9
+93				56.0
100+00				56.0
+04	ST. MARYS AVE LT.			56.1
+20				56.3
+23				56.3
T. P	3.65	962.73.	0.74	959.08.

LT

♀

RT

$$\begin{array}{cccccccc} \checkmark & 4.3 & 4.2 & 4.8 & 6.2 & 6.9 & 6.5 & 6.2 & 4.9 & 4.8 \\ 60 & 45 & 34 & 30 & 26 & 21 & 22 & 17 & 10 & 4.7 \end{array}$$

$$\begin{array}{ccccccc} 4.7 & 4.9 & 5.2 & 4.8 & 5.5 & 6.3 \\ 10 & 19 & 23 & 27 & 31 & 33 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccc} 3.6 & 3.7 & 4.4 & 6.2 & 6.4 & 5.0 & 4.5 & 4.5 \\ 60 & 46 & 34 & 30 & 26 & 22 & 16 & 10 & 4.4 \end{array}$$

$$\begin{array}{ccccccc} 4.4 & 4.6 & 5.1 & 6.4 & 6.4 & 5.0 & 5.0 & 5.8 \\ 10 & 20 & 23 & 26 & 31 & 33 & 43 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccc} 3.1 & 4.0 & 5.5 & 5.1 & 4.3 & 4.8 & 4.0 \\ 60 & 33 & 30 & 26 & 22 & 16 & 10 & 3.9 \end{array}$$

$$\begin{array}{ccccccc} 3.9 & 4.0 & 5.9 & 5.6 & 5.2 & 5.1 \\ 10 & 21 & 26 & 32 & 34 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccc} 3.6 & 3.9 & 4.1 & 4.3 & 3.9 & 3.9 & 3.8 \\ 60 & 43 & 33 & 25 & 15 & 10 & 3.8 \end{array}$$

$$\begin{array}{ccccccc} 3.9 & 4.0 & 5.9 & 5.6 & 5.2 & 5.1 \\ 10 & 21 & 26 & 32 & 34 & 60 \end{array}$$

$$\checkmark \begin{array}{ccccccc} 3.2 & 3.7 & 3.8 & 3.8 & 3.8 \\ 60 & 39 & 18 & 10 & 3.8 \end{array}$$

$$\begin{array}{ccccccc} 3.8 & 3.9 & 4.0 & 5.9 & 5.6 & 5.2 & 5.1 \\ 10 & 20 & 21 & 26 & 32 & 34 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccc} 1.0 & 1.4 & 2.2 & 3.3 & 3.6 & 3.6 & 3.8 \\ 200 & 150 & 100 & 50 & 26 & 18 & 10 & 3.7 \end{array}$$

$$\begin{array}{ccccccc} 3.8 & 3.8 & 4.0 & 5.1 & 5.8 & 4.8 & 4.5 & 5.2 \\ 10 & 16 & 22 & 26 & 31 & 33 & 37 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccc} 3.5 & 3.9 & 3.9 & 3.8 & 3.7 & 3.6 & 3.5 \\ 60 & 38 & 26 & 22 & 17 & 10 & 3.5 \end{array}$$

$$\begin{array}{ccccccc} 3.6 & 3.8 & 4.1 & 5.6 & 5.5 & 4.6 & 5.2 \\ 10 & 19 & 21 & 26 & 31 & 33 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccc} 2.8 & 2.8 & 3.5 & 5.1 & 5.2 & 4.2 & 3.7 & 3.6 \\ 60 & 47 & 33 & 30 & 26 & 23 & 19 & 10 & 3.5 \end{array}$$

$$\begin{array}{ccccccc} 3.5 & 3.8 & 4.1 & 5.6 & 5.5 & 4.6 & 5.2 \\ 10 & 19 & 21 & 26 & 31 & 33 & 60 \end{array}$$

STA	+	π	-	ELEV
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962.73

100+50

56.7

101

57.2

+50

57.7

102

58.0

+50

58.0

103

58.0

+50

57.9

104

57.7

LT

Q

RT

✓ $\frac{5.3}{60}$ $\frac{5.5}{43}$ $\frac{6.1}{34}$ $\frac{7.6}{30}$ $\frac{7.6}{26}$ $\frac{6.4}{22}$ $\frac{6.1}{17}$ $\frac{6.1}{10}$ $\frac{6.0}{10}$ $\frac{6.1}{10}$ $\frac{6.5}{18}$ $\frac{7.0}{22}$ $\frac{7.9}{25}$ $\frac{8.0}{30}$ $\frac{6.8}{33}$ $\frac{6.8}{38}$ $\frac{7.6}{60}$

✓ $\frac{4.9}{60}$ $\frac{5.0}{48}$ $\frac{5.5}{33}$ $\frac{6.8}{30}$ $\frac{6.9}{25}$ $\frac{6.0}{22}$ $\frac{5.7}{17}$ $\frac{5.6}{10}$ $\frac{5.5}{10}$ $\frac{5.7}{10}$ $\frac{5.8}{17}$ $\frac{6.1}{20}$ $\frac{7.1}{25}$ $\frac{7.5}{30}$ $\frac{5.9}{34}$ $\frac{6.5}{47}$ $\frac{6.7}{60}$

✓ $\frac{4.8}{60}$ $\frac{4.5}{38}$ $\frac{5.2}{33}$ $\frac{6.6}{30}$ $\frac{7.0}{25}$ $\frac{5.6}{22}$ $\frac{5.2}{17}$ $\frac{5.1}{10}$ $\frac{5.0}{10}$ $\frac{5.1}{10}$ $\frac{5.3}{18}$ $\frac{5.8}{22}$ $\frac{6.8}{25}$ $\frac{6.7}{30}$ $\frac{5.3}{33}$ $\frac{5.5}{40}$ $\frac{6.2}{60}$

✓ $\frac{5.0}{60}$ $\frac{4.8}{48}$ $\frac{5.1}{35}$ $\frac{6.5}{30}$ $\frac{6.6}{25}$ $\frac{5.4}{22}$ $\frac{5.0}{18}$ $\frac{4.9}{10}$ $\frac{4.7}{10}$ $\frac{4.8}{10}$ $\frac{4.9}{17}$ $\frac{5.1}{22}$ $\frac{6.8}{25}$ $\frac{6.7}{30}$ $\frac{5.5}{33}$ $\frac{5.9}{46}$ $\frac{6.0}{60}$

✓ $\frac{5.2}{60}$ $\frac{4.8}{36}$ $\frac{5.1}{33}$ $\frac{6.5}{30}$ $\frac{6.3}{25}$ $\frac{5.3}{22}$ $\frac{4.9}{17}$ $\frac{4.8}{10}$ $\frac{4.7}{10}$ $\frac{4.8}{10}$ $\frac{5.1}{18}$ $\frac{5.7}{22}$ $\frac{6.9}{23}$ $\frac{6.7}{31}$ $\frac{5.4}{33}$ $\frac{5.7}{43}$ $\frac{5.7}{60}$

✓ $\frac{5.6}{60}$ $\frac{5.8}{35}$ $\frac{5.6}{26}$ $\frac{5.1}{18}$ $\frac{4.9}{10}$ $\frac{4.7}{10}$ $\frac{4.8}{10}$ $\frac{5.1}{18}$ $\frac{5.6}{22}$ $\frac{6.5}{25}$ $\frac{6.7}{30}$ $\frac{5.6}{33}$ $\frac{6.0}{60}$

✓ $\frac{5.6}{60}$ $\frac{5.3}{50}$ $\frac{5.5}{33}$ $\frac{5.4}{25}$ $\frac{5.2}{18}$ $\frac{4.9}{10}$ $\frac{4.8}{10}$ $\frac{4.9}{10}$ $\frac{5.3}{19}$ $\frac{5.8}{22}$ $\frac{7.0}{27}$ $\frac{6.7}{31}$ $\frac{5.6}{33}$ $\frac{5.6}{39}$ $\frac{5.9}{60}$

✓ $\frac{5.5}{60}$ $\frac{5.3}{35}$ $\frac{5.3}{24}$ $\frac{5.2}{18}$ $\frac{5.0}{10}$ $\frac{5.0}{50}$ $\frac{5.1}{10}$ $\frac{5.2}{18}$ $\frac{5.6}{21}$ $\frac{6.6}{25}$ $\frac{6.8}{30}$ $\frac{5.5}{33}$ $\frac{5.4}{45}$ $\frac{5.8}{60}$

STA	+	IN	-	ELEV
		962.73		
104	+50			57.3
	+87			56.8
	105			56.7
	+06			56.6
	+09	CONC. 12" X 97' c.m. RT	X DRAIN	56.6
B.M	3.24	961.28	4.69	958.04
				958.05
	+14			56.6
	+17			56.5
	+34	SOUTH BOUND 1 SNELLING LANE		56.3
				X
	+50			56.2

LT

E

RT

✓ $\frac{5.8}{60} \frac{5.8}{32} \frac{5.6}{18} \frac{5.5}{10} \frac{5.4}{5.4} \frac{5.5}{10} \frac{5.5}{18} \frac{6.6}{22} \frac{6.9}{26} \frac{7.0}{30} \frac{5.7}{33} \frac{5.9}{60}$

CURB GUTTER

GUTTER CURB

✓ $\frac{6.4}{60} \frac{6.3}{35} \frac{5.8}{25} \frac{6.4}{24} \frac{6.2}{18} \frac{6.0}{11} \frac{5.9}{5.9} \frac{6.1}{12} \frac{6.4}{18} \frac{5.9}{19} \frac{6.3}{22} \frac{7.4}{26} \frac{7.8}{30} \frac{6.2}{33} \frac{6.5}{44} \frac{6.4}{50}$

CURB GUTTER

GUTTER CURB

✓ $\frac{6.5}{50} \frac{6.3}{39} \frac{5.9}{31} \frac{5.9}{26} \frac{6.6}{25} \frac{6.2}{15} \frac{6.0}{6.0} \frac{6.6}{18} \frac{6.9}{22} \frac{6.4}{23} \frac{6.4}{27} \frac{7.4}{32} \frac{6.7}{33} \frac{6.7}{50}$

CURB GUT

GUT. CURB

✓ $\frac{6.3}{50} \frac{6.4}{40} \frac{5.9}{31} \frac{5.9}{25} \frac{6.5}{24} \frac{6.3}{17} \frac{6.1}{6.1} \frac{6.8}{72} \frac{7.0}{24} \frac{6.5}{25} \frac{6.6}{29} \frac{6.3}{33} \frac{7.1}{35} \frac{6.8}{37} \frac{6.8}{50}$

F.L

F.L

CURB GUT

GUT CURB

F.L

✓ $\frac{8.3}{56} \frac{8.1}{50} \frac{8.2}{37} \frac{6.0}{33} \frac{6.0}{25} \frac{6.5}{24} \frac{6.4}{22} \frac{6.1}{6.1} \frac{6.9}{26} \frac{7.0}{27} \frac{6.6}{28} \frac{6.6}{34} \frac{7.2}{38} \frac{8.0}{45} \frac{8.1}{60} \frac{7.2}{60}$

Top HYDRANT RT STA 105+75 SNEELING + LARPENTIER

CURB GUTTER

GUTTER CURB GUTTER CURB

✓ $\frac{4.6}{50} \frac{4.5}{32} \frac{4.5}{28} \frac{5.0}{27} \frac{4.8}{10} \frac{4.7}{4.7} \frac{5.2}{15} \frac{5.7}{35} \frac{5.2}{35} \frac{5.9}{50} \frac{5.3}{50}$

CURB GUTTER CURB GUTTER

✓ $\frac{4.5}{50} \frac{5.1}{50} \frac{4.5}{34} \frac{5.0}{34} \frac{4.9}{24} \frac{4.8}{10} \frac{5.0}{10} \frac{5.4}{24} \frac{5.6}{33} \frac{5.7}{50}$

✓ $\frac{3.2}{250} \frac{3.7}{200} \frac{4.1}{150} \frac{4.4}{100} \frac{4.5}{75} \frac{4.7}{50} \frac{4.7}{25} \frac{5.0}{5.0} \frac{5.3}{25} \frac{5.6}{50} \frac{5.9}{75} \frac{6.1}{100} \frac{6.6}{150} \frac{7.2}{200} \frac{7.8}{250}$

5.1

STA + ∇ - ELEV

961.28

106

55.9

+13 ∇ NORTH BOUND
EAST SNELLING LANE

55.8

+50

55.3

+66 ∇ EAST SERVICE DRIVE

55.0

+80

54.7

+85

54.5

+91

54.4

+97 ∇ 15" CONC
C.B. DRAIN EAST

LT 54.3

LT

4

RT

5.4

<u>4.1</u>	<u>4.3</u>	<u>4.5</u>	<u>4.8</u>	<u>4.9</u>	<u>5.1</u>	<u>5.3</u>		<u>5.8</u>	<u>6.0</u>	<u>6.3</u>	<u>6.6</u>	<u>7.1</u>	<u>7.8</u>	<u>8.5</u>
250	200	150	100	75	50	25	55	25	50	75	100	150	200	250

6.0

✓ 6.0	6.1	6.3	6.7	6.9	6.7	6.5	6.4	6.4	6.6	6.8	7.4	7.6	8.5	9.4	10.4	
280	200	150	100	75	50	25	10	63	10	35	50	75	100	150	200	250

GUTTER CURB				CURB GUTTER				GUTTER CURB				CURB GUTTER			
7.0	6.7	6.5	6.5	6.9	6.7	6.9	6.9	6.6	7.1	7.3	6.9	7.0	7.0	7.0	7.0
50	45	45	31	31	18	10	6.6	10	24	33	33	50	50	50	50

GUTTER CURB		CURB GUTTER		GUTTER CURB		CURB GUTTER	
✓ 12	67	65	64	65	71	69	68
50	48	47	27	26	25	16	10
						68	10
						72	22
						68	23
						68	24
						71	50

CNRB-GUT ₇ GUT ₁₂ CNRB										GUT ₇ CNRB					
✓	72	67	26	24	68	74	20	69	70	21	68	69	69	83	83
	60	44	44	31	31	27	17	10	69	10	19	20	20	24	30

C.B.

F.L

$\frac{7.6}{60}$	$\frac{8.0}{48}$	$\frac{8.2}{45}$	$\frac{9.7}{43}$	$\frac{7.9}{41}$	$\frac{7.6}{27}$	$\frac{7.1}{18}$	$\frac{7.0}{10}$	$\frac{7.0}{10}$	$\frac{7.0}{18}$	$\frac{7.4}{22}$	$\frac{8.5}{26}$	$\frac{8.6}{31}$	$\frac{8.0}{33}$	$\frac{8.3}{60}$
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STA	+	+	-	ELEV
-----	---	---	---	------

96.28

107				54.3
-----	--	--	--	------

+34	C.B. 15" CONC DRAIN EAST LT.			54.0
-----	------------------------------	--	--	------

+50				53.8
-----	--	--	--	------

108				53.2
-----	--	--	--	------

T.P.	3.24	956.36	8.16	953.12
------	------	--------	------	--------

+50				52.7
-----	--	--	--	------

109				52.4
-----	--	--	--	------

+38				52.1
-----	--	--	--	------

+41	EAST END 15' CONC CULV			52.1
-----	------------------------	--	--	------

LT

E

RT

✓ $\frac{7.8}{60} \frac{7.7}{56} \frac{7.3}{17} \frac{7.1}{10} \frac{7.0}{10} \frac{7.1}{18} \frac{7.2}{22} \frac{8.6}{26} \frac{8.7}{32} \frac{7.9}{34} \frac{8.4}{60}$

WEST EAST

FL FL

✓ $\frac{7.7}{60} \frac{8.0}{35} \frac{9.15}{35} \frac{9.55}{35} \frac{7.7}{24} \frac{7.4}{7.3} \frac{7.6}{10} \frac{8.0}{19} \frac{8.8}{22} \frac{9.2}{25} \frac{8.3}{31} \frac{8.7}{33} \frac{8.9}{45} \frac{8.9}{60}$

✓ $\frac{7.5}{60} \frac{7.7}{32} \frac{7.7}{17} \frac{7.6}{10} \frac{7.5}{10} \frac{7.6}{10} \frac{7.9}{17} \frac{8.0}{22} \frac{9.2}{25} \frac{9.4}{32} \frac{8.5}{33} \frac{8.9}{47} \frac{9.3}{60}$

✓ WALK $\frac{7.4}{60} \frac{7.8}{45} \frac{8.1}{23} \frac{8.1}{17} \frac{8.2}{10} \frac{8.2}{8.1} \frac{8.2}{10} \frac{8.2}{17} \frac{8.1}{23} \frac{9.5}{26} \frac{9.7}{32} \frac{9.0}{34} \frac{9.7}{60}$

✓ WALK $\frac{2.6}{60} \frac{2.9}{50} \frac{3.7}{29} \frac{3.6}{18} \frac{3.8}{10} \frac{3.7}{3.7} \frac{3.8}{10} \frac{4.2}{20} \frac{4.6}{28} \frac{5.6}{36} \frac{5.2}{42} \frac{5.2}{49} \frac{5.4}{60}$

STORE
FLOOR WALK

✓ $\frac{2.4}{60} \frac{2.8}{51} \frac{3.8}{38} \frac{4.0}{20} \frac{4.1}{17} \frac{4.1}{10} \frac{4.0}{4.0} \frac{4.4}{10} \frac{4.5}{21} \frac{5.9}{25} \frac{6.1}{28} \frac{6.1}{32} \frac{5.4}{33} \frac{5.2}{46} \frac{5.6}{60}$

✓ $\frac{3.4}{60} \frac{3.3}{49} \frac{4.2}{32} \frac{4.3}{18} \frac{4.4}{10} \frac{4.3}{4.3} \frac{4.4}{10} \frac{4.6}{21} \frac{6.3}{26} \frac{6.4}{32} \frac{5.6}{34} \frac{5.4}{36} \frac{5.7}{60}$

F.L

✓ $\frac{4.8}{60} \frac{5.1}{49} \frac{6.0}{42} \frac{6.5}{35} \frac{5.9}{31} \frac{4.1}{25} \frac{4.4}{18} \frac{4.4}{10} \frac{4.3}{4.3} \frac{4.4}{10} \frac{4.6}{15} \frac{4.7}{21} \frac{6.4}{27} \frac{6.4}{32} \frac{5.6}{33} \frac{5.5}{39} \frac{6.0}{60}$

STA	+	↑	-	ELEV
				956.36 .
109+50				52.1 .
110				51.8 .
+50				51.6 .
+66				51.6 .
+80	24" C.M		EAST DRAIN LT	51.5 .
+88	"			51.5 .
111				51.5 .
+50				51.4 .

LT

Z

RT

$$\checkmark \begin{array}{cccccccccccccccc} 4.9 & 5.4 & 5.1 & 6.1 & 5.9 & 4.6 & 4.5 & & 4.4 & 4.7 & 4.8 & 5.3 & 6.4 & 6.5 & 5.6 & 5.7 & 6.0 \\ 60 & 50 & 45 & 37 & 31 & 25 & 17 & 10 & 10 & 15 & 21 & 24 & 27 & 32 & 34 & 48 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccccccc} 5.6 & 5.2 & 5.5 & 6.3 & 6.6 & 6.4 & 5.0 & 4.8 & 4.7 & & 4.7 & 5.0 & 5.2 & 5.6 & 6.8 & 6.6 & 5.8 & 5.9 & 6.3 \\ 60 & 51 & 47 & 43 & 35 & 27 & 23 & 17 & 10 & 4 & 10 & 16 & 21 & 24 & 28 & 32 & 33 & 46 & 60 \end{array}$$

$$\begin{array}{cccccccccccccccc} 6.0 & 5.5 & 6.6 & 6.8 & 6.8 & 4.9 & 4.9 & 4.9 & & 4.9 & 5.1 & 5.3 & 5.8 & 6.8 & 7.0 & 6.4 & 6.5 & 7.0 \\ 60 & 48 & 44 & 37 & 28 & 23 & 17 & 10 & 4 & 10 & 15 & 21 & 23 & 26 & 31 & 33 & 45 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccccccc} 6.2 & 6.1 & 7.0 & 6.9 & 6.6 & 5.2 & 5.0 & 4.9 & & 4.9 & 5.1 & 5.3 & 5.8 & 6.8 & 7.0 & 6.4 & 6.5 & 7.0 \\ 60 & 47 & 40 & 33 & 26 & 23 & 18 & 10 & 4 & 10 & 15 & 21 & 23 & 26 & 31 & 33 & 45 & 60 \end{array}$$

F.L

$$\checkmark \begin{array}{cccccccccccccccc} 6.1 & 5.6 & 6.5 & 7.2 & 6.8 & 4.9 & 5.0 & 5.0 & & 5.0 & 5.2 & 5.6 & 6.1 & 7.0 & 7.0 & 7.5 \\ 60 & 53 & 43 & 35 & 35 & 30 & 20 & 10 & 4 & 10 & 21 & 23 & 25 & 31 & 42 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 4.1 & 4.0 & 4.5 & 4.9 & 5.0 & & 5.0 & & 5.1 & 5.3 & 6.5 & 7.0 & 7.6 \\ 60 & 50 & 42 & 24 & 10 & 4 & 10 & & 19 & 21 & 26 & 40 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 3.9 & 4.1 & 4.7 & 4.8 & 5.1 & & 5.1 & 5.1 & 5.5 & 6.8 & 6.9 & 7.2 & 7.7 \\ 60 & 50 & 23 & 16 & 10 & 4 & 10 & 19 & 22 & 26 & 32 & 46 & 60 \end{array}$$

$$\checkmark \begin{array}{cccccccccccc} 4.1 & 4.5 & 4.9 & 5.0 & 5.1 & 5.0 & & 5.1 & 5.1 & 5.5 & 7.1 & 7.2 & 7.7 \\ 60 & 46 & 31 & 18 & 10 & 5 & & 10 & 18 & 22 & 27 & 42 & 60 \end{array}$$

STA + π - ELEV

956.36.

111+71 24" C.M. LT MONOLITHIC RT C.B. + EAST DRAIN LT 51.4

+75 51.4

+80 51.4

+95 51.4

112 51.4

+07 ϕ ARONA 51.4

+20 51.4

+23 51.4

X

49.03
 $\downarrow$
 T

2

PT 41.86

TOP
C.A

F.L

F.L F.L

✓ $\frac{4.3}{60}$ $\frac{4.5}{37}$ $\frac{1.32}{35}$ $\frac{5.0}{30}$ $\frac{5.1}{19}$ $\frac{5.1}{10}$ $\frac{5.0}{5.0}$ $\frac{5.1}{10}$ $\frac{5.2}{21}$ $\frac{7.6}{21}$ $\frac{7.5}{26}$ $\frac{7.1}{31}$ $\frac{7.3}{47}$ $\frac{7.7}{60}$

✓ $\frac{4.4}{60}$ $\frac{4.3}{54}$ $\frac{4.9}{33}$ $\frac{5.0}{21}$ $\frac{5.1}{10}$ $\frac{5.0}{5.0}$

$\frac{5.1}{10}$ $\frac{5.3}{21}$ $\frac{6.1}{26}$ $\frac{7.0}{32}$ $\frac{6.9}{42}$ $\frac{7.4}{60}$

✓ $\frac{4.6}{60}$ $\frac{5.0}{38}$ $\frac{5.1}{23}$ $\frac{5.1}{10}$

$\frac{5.0}{5.0}$ $\frac{5.1}{10}$ $\frac{5.3}{18}$ $\frac{5.2}{23}$ $\frac{5.7}{39}$ $\frac{6.0}{60}$

✓ $\frac{5.0}{60}$ $\frac{5.0}{45}$ $\frac{5.2}{24}$ $\frac{5.1}{10}$ $\frac{5.0}{5.0}$

$\frac{5.1}{10}$ $\frac{5.2}{19}$ $\frac{5.8}{33}$ $\frac{6.1}{60}$

✓ $\frac{5.0}{60}$ $\frac{5.0}{45}$ $\frac{5.2}{24}$ $\frac{5.1}{10}$ $\frac{5.0}{5.0}$

$\frac{5.1}{10}$ $\frac{5.1}{19}$ $\frac{5.4}{33}$ $\frac{5.9}{60}$

✓ $\frac{4.0}{200}$ $\frac{4.5}{150}$ $\frac{5.0}{100}$ $\frac{5.1}{50}$ $\frac{5.2}{25}$ $\frac{5.1}{10}$ $\frac{5.0}{5.0}$ $\frac{5.1}{10}$ $\frac{5.1}{19}$ $\frac{5.2}{25}$ $\frac{5.6}{50}$ $\frac{6.0}{100}$ $\frac{6.4}{150}$ $\frac{6.9}{200}$

✓ $\frac{5.4}{60}$ $\frac{5.5}{36}$ $\frac{5.2}{20}$ $\frac{5.1}{10}$ $\frac{5.0}{5.0}$

$\frac{5.1}{10}$ $\frac{5.1}{15}$ $\frac{5.5}{26}$ $\frac{6.0}{41}$ $\frac{6.3}{60}$

60 46 24 10 10 5.0

✓ $\frac{5.7}{60}$ $\frac{5.6}{46}$ $\frac{5.6}{34}$ $\frac{5.2}{20}$ $\frac{5.1}{10}$ $\frac{5.0}{5.0}$ $\frac{5.1}{10}$ $\frac{5.3}{19}$ $\frac{5.7}{28}$ $\frac{5.6}{33}$ $\frac{6.0}{60}$

STA + π - ELEV

956.36

112+24

51.4

+26

51.4

+38 24" C.M. EAST DRAIN LT 51.3

+43

51.3

+50

51.3

113

51.3

+50

51.3

114

51.2

B.M. 1.62 956.36 1.62 954.74 954.72

B.M. 2.30 953.55 3.11 953.25

LT

C

RT

✓ $\frac{6.3}{60} \frac{5.9}{45} \frac{5.6}{32} \frac{5.3}{30} \frac{5.2}{19} \frac{5.1}{10} \frac{5.0}{5.0} \frac{5.1}{10} \frac{5.4}{18} \frac{5.7}{29} \frac{5.6}{33} \frac{6.0}{60}$

✓ $\frac{5.6}{60} \frac{5.6}{48} \frac{6.1}{44} \frac{5.1}{32} \frac{5.3}{20} \frac{5.2}{19} \frac{5.1}{10} \frac{5.0}{5.0} \frac{5.1}{10} \frac{5.4}{18} \frac{5.5}{29} \frac{5.6}{33} \frac{6.0}{60}$

F.L.

✓ $\frac{5.3}{60} \frac{5.8}{46} \frac{6.9}{41} \frac{7.0}{34} \frac{7.4}{35} \frac{6.7}{32} \frac{5.9}{27} \frac{5.0}{22} \frac{5.1}{10} \frac{5.1}{5.1} \frac{5.2}{10} \frac{5.3}{20} \frac{5.7}{33} \frac{6.1}{50} \frac{6.1}{60}$

✓ $\frac{6.3}{60} \frac{6.2}{47} \frac{6.8}{40} \frac{6.7}{39} \frac{6.0}{36} \frac{5.8}{23} \frac{5.3}{17} \frac{5.1}{10} \frac{5.1}{5.1} \frac{5.2}{10} \frac{5.2}{18} \frac{5.6}{21} \frac{7.2}{27} \frac{7.3}{39} \frac{7.5}{60}$

✓ $\frac{6.0}{60} \frac{6.1}{48} \frac{6.8}{45} \frac{6.7}{37} \frac{6.6}{28} \frac{5.3}{21} \frac{5.3}{17} \frac{5.1}{10} \frac{5.1}{5.1} \frac{5.2}{10} \frac{5.2}{18} \frac{5.6}{22} \frac{7.4}{26} \frac{7.6}{32} \frac{6.7}{34} \frac{7.4}{60}$

✓ $\frac{5.5}{60} \frac{5.5}{49} \frac{6.0}{45} \frac{6.1}{34} \frac{6.1}{25} \frac{5.6}{32} \frac{5.3}{18} \frac{5.2}{10} \frac{5.1}{5.1} \frac{5.2}{10} \frac{5.4}{18} \frac{5.7}{22} \frac{7.3}{27} \frac{7.3}{32} \frac{6.4}{34} \frac{6.9}{51} \frac{7.1}{60}$

✓ $\frac{5.4}{60} \frac{5.3}{47} \frac{6.3}{44} \frac{6.2}{26} \frac{5.5}{22} \frac{5.2}{19} \frac{5.2}{10} \frac{5.1}{5.1} \frac{5.2}{10} \frac{5.4}{19} \frac{5.6}{22} \frac{7.0}{26} \frac{7.2}{30} \frac{6.0}{33} \frac{6.2}{47} \frac{6.6}{60}$

✓ $\frac{5.1}{60} \frac{5.4}{49} \frac{6.5}{44} \frac{6.3}{33} \frac{5.3}{20} \frac{5.2}{10} \frac{5.2}{5.2} \frac{5.3}{10} \frac{5.4}{18} \frac{5.7}{21} \frac{7.1}{26} \frac{7.0}{31} \frac{5.9}{33} \frac{5.8}{49} \frac{6.4}{60}$

TOP HYDRANT NE COR ARONA + LARPENTUER

(1499 Larp Ave) S.W. COR LOWER STEP LT STA 114+45

Sta.	+	π	-	Elev
------	---	-------	---	------

965.55.

114 +50

51.2

115

51.1

+50

51.0

116

51.0

+50

50.9

117

50.9

+50

50.8

118

50.8

5-17-44

K.A.
L.C.
C.N.
C.F.
L.L.

77

Lt.

E

Rt.

✓ 37 40 52 56 56 46 45 44 45 48 51 62 62 51 48
60 51 38 34 24 18 10 10 18 23 26 31 34 50

✓ 41 45 53 55 55 48 46 45 46 47 50 60 62 49 47
60 44 39 31 25 20 10 10 18 22 25 30 33 50

✓ 41 45 53 53 53 48 47 46 46 47 49 62 62 45 44
60 44 38 30 23 19 10 10 19 23 26 30 33 50

✓ 40 46 49 52 52 47 47 46 47 48 41 62 65 47 47
60 44 39 33 25 19 10 10 19 22 25 30 34 50

✓ 43 47 52 53 55 49 47 47 48 49 50 62 62 48 47
60 48 43 32 25 19 10 10 19 22 25 30 34 50

✓ 43 48 55 53 54 50 48 47 48 49 51 65 68 55 55
50 48 46 34 25 19 10 10 19 22 25 31 34 50

✓ 58 58 58 55 55 50 48 48 48 49 51 52 66 68 57 56
60 58 44 34 26 23 18 10 10 19 22 26 31 34 50

✓ 44 49 56 57 56 50 49 48 49 51 53 69 71 57 58
60 47 45 34 23 19 10 10 19 21 26 34 37 50

Sta.	+	π	-	Elev.
		955.55.		
118 + 46				50.8
+50				50.8
+64.9	E Percol Ave.			50.7
+78				50.7
119				50.7
T.P.	3.65	954.32.	4.88	950.67.
+50				50.6
120				50.6
+50				50.5

Lt.

2

Bt.

✓ 48 49 59 59 58 50 49 48 50 53 53 69 73 62 60
60 48 45 33 25 19 10 10 19 21 26 34 37 50

✓ 53 51 50 48 50 59 66 67
60 26 10 10 29 38 50

5105

✓ 45 46 52 50 50 49 50 54 59 61 54 42
120 100 50 20 10 10 20 50 100 150 200

✓ 61 62 60 54 50 49 50 57 62 66 65
60 44 28 24 10 10 19 29 42 60

✓ 64 61 65 65 49 50 49 51 53 58 70 70 48 62 62
60 44 42 26 21 10 10 19 23 27 36 46 48 60
250 19

✓ 47 46 55 56 55 43 41 38 37 39 39 40 58 60 61 49 47
60 45 42 35 26 23 19 10 10 19 22 26 34 43 47 60

✓ 46 40 58 58 57 41 41 41 37 40 41 43 57 58 57 43 33 36
60 45 41 32 27 22 19 10 10 19 22 26 32 40 47 55 60

✓ 45 43 35 57 57 55 41 40 38 40 39 39 56 57 55 23 24
60 50 45 41 34 26 21 10 10 19 23 27 33 38 48 60

Sta	+	π	-	Elev
		95432.		

121				50.3
-----	--	--	--	------

+50				50.0
-----	--	--	--	------

+70				49.9
-----	--	--	--	------

+80				49.9
-----	--	--	--	------

122	ϕ HOLTEN LT			49.7
-----	------------------	--	--	------

+15				49.5
-----	--	--	--	------

+19				49.5
-----	--	--	--	------

+27				49.4
-----	--	--	--	------

X

Lh

E

Dh

✓ 44 44 38 58 60 60 44 41 40 41 41 58 60 56 17 16 60
60 50 44 41 32 26 21 10 10 22 26 31 37 49 55

✓ 48 48 44 64 66 64 49 43 4.3 4.4 44 64 64 59 20 18
60 50 44 41 33 26 22 10 10 22 27 32 37 48 60

✓ 50 50 60 64 65 46 45 44 45 46 65 66 61 22 18 21
60 50 40 34 48 22 10 10 21 26 31 37 48 54 60

✓ 5.5 48 47 45 44 45 46 66 66 61 23 21 22
60 37 30 10 10 22 27 32 37 48 55 60

49.9

49.8

✓ 44 45 48 47 46 47 46 47 48 67 68 65 27 25 26
200 150 100 50 25 10 10 21 27 31 37 48 55 60

✓ 5.3 49 49 48 49 51 68 71 48 31 28 31
60 31 10 10 21 26 33 37 48 55 60

✓ 6.2 6.2 7.0 7.1 48 4.9 48 49 Duplicate + 15
60 51 42 32 26 10 10

✓ 48 50 67 72 71 49 50 49 50 53 70 72 70 35 32 35
60 47 43 35 26 22 10 10 21 26 32 37 48 55 60

Sta + π -

954.32.

122 +50

49.1

123

48.6

+50

48.0

124

47.6

+08

47.5

+11

47.5

+50

47.2

125

46.9

T.P.

1.89

950.81.

5.40

948.92.

Lt

E

Pt

✓ 52 52 71 77 75 55 52 52 53 54 70 73 69 91 90 91
60 48 43 24 25 21 10 10 22 26 31 38 48 56 60

✓ 51 53 74 82 78 55 58 57 58 57 77 75 47 45 45
60 47 42 34 26 21 10 10 21 27 40 49 55 60

✓ 70 70 76 89 89 80 78 58 63 63 63 64 80 82 79 54 53 54
60 46 39 36 33 31 27 21 10 10 22 25 33 40 49 56 60

✓ 78 78 81 93 93 87 85 70 68 67 68 69 86 87 83 64 62 64
60 45 40 36 33 31 26 21 10 10 21 26 35 42 48 55 60

✓ 80 76 82 95 95 87 73 69 68 69 70 85 87 86 65 66
60 44 38 36 33 31 22 10 10 21 25 33 41 48 60

✓ 71 71 73 69 68 69 Duplicate + 08
60 41 28 10 10

✓ 78 80 77 78 76 72 71 72 73 74 89 90 89 80 76 77
60 50 48 33 20 10 10 18 22 26 33 43 47 54 60

✓ 85 86 84 75 74
60 49 23 10

75 77 94 98 87 85 85
10 23 27 30 46 50 60

Top Hyd N.E. Cor. Albert & Larpenleur

Sta	+	π	-	Elev
		950.81		
125+10				46.8
+17				46.7
+30.4 = g Albert St				46.8
+45				46.7
+57				46.7
+63				46.6
126				46.5
+25				46.4

Lt.

C.

Ct.

✓ 51 52 48 40 40 41 46 54 58 58 44 47
60 33 30 10 10 22 27 35 44 49 60

✓ 58 52 47 41 41 41 46 48 50
60 45 30 10 10 25 40 50

✓ 55 53 48 42 41 40 41 44 48 52 53 55
132 100 50 25 10 10 25 50 100 150 200

✓ 56 55 44 42 41 42 46 47 51 53
60 40 24 10 10 22 32 48 60

✓ 50 49 47 42 41 43 46 59 61 61 46 48
60 40 24 10 10 21 26 35 45 49 60

✓ 48 50 41 61 45 43 42 43 45 49 59 61 62 51 49
60 47 37 33 22 10 10 19 22 26 32 46 50 60

✓ 45 47 61 62 48 45 44 43 45 45 47 62 62 62 52 52
60 49 37 33 22 19 10 10 18 22 28 40 53 55 60

✓ 73 68 50 54 64 51 48 45 44 45 48 63 64 64 64 58
150 180 50 46 35 23 19 10 10 23 26 36 47 56 60

Sta + π - Elev

950.81 .

126 +60

46.3 .

127

46.3 .

+05

46.3 .

+09

46.2 .

+60

46.1 .

+64

46.0 .

128

46.0 .

+50

45.9 .

Lt.

E

Rt.

✓ 59 59 53 62 66 61 52 49 45 45 46 47 50 65 66 65 56
60 50 47 43 35 28 22 19 10 10 18 23 27 40 55 60

✓ 56 54 63 67 61 49 46 45 47 49 53 66 68 68 62 62 52
60 48 42 35 28 20 10 10 18 22 25 35 46 48 54 60

✓ 5.5 59 63 68 61 49 46 45 47 Duplicate station 127
60 48 42 34 28 20 10 10

✓ 45 46 46 47 46 47 50 59 66 69 68 62 53
60 40 19 10 10 18 23 26 36 46 49 60

✓ 43 43 45 47 47 48 52 67 67 63 51 48
60 38 20 10 10 22 27 40 54 56 60

✓ 45 48 61 65 47 49 48 49 51 53 67 68 67 60 52
60 47 43 36 28 22 10 10 18 22 26 35 45 49 60

✓ 45 48 67 65 47 49 48 50 53 67 68 67 60 52 50
60 47 35 27 20 10 10 22 26 36 47 53 55 60

✓ 45 48 53 49 74 66 65 51 50 49 50 50 67 68 68 58 58 48 48
60 51 47 41 35 32 22 21 10 10 21 26 35 40 48 54 56 60

Sta	+	π	-	Elev
		950.81		
129				45.8
I.P	4.42	950.01	5.22	945.59
+50				45.7
130				45.5
+50				45.3
				X
131				45.2
+50				45.0
+65				45.0
+72				45.0

Lt.

4

Rth

✓ 45 45 68 70 68 57 53 51 50 51 59 56 68 69 68 56 57
 50 50 43 34 25 22 18 10 10 18 23 27 35 44 48 60

✓ 44 47 62 65 42 47 44 43 45 49 51 62 64 62 50 46
 60 49 44 36 25 20 10 10 18 22 26 34 44 48 60

✓ 50 53 65 65 59 45 46 45 47 49 52 66 66 65 56 57
 60 47 44 37 25 20 10 10 18 22 27 37 45 48 60

✓ 56 56 67 66 66 53 50 48 47 48 51 54 64 70 70 61 61
 60 49 44 35 26 22 18 10 10 18 23 26 35 45 49 60

✓ 57 57 65 67 66 55 51 48 50 52 55 68 70 67 61 60
 60 49 45 35 26 22 18 10 18 23 26 35 46 49 60

✓ 54 56 67 70 67 54 50 50 50 53 57 68 70 69 56 57
 60 48 45 28 26 22 10 10 20 25 28 37 45 50 60

✓ 47 47 50 52 50 50 50 53 55 56 67 67 52
 60 46 28 25 10 10 21 30 39 42 48 60

✓ 51 49 48 51 51 50 50 53 53 54 64 65 69
 60 42 35 31 10 10 22 35 43 45 60 110

Sta	+	π	-	Elev
		950.01		
131	+76			45.0
+96.10	E Homing Ave.			44.9
B.M.	1.36	946.34	5.07	944.94 (944.98)
132			1.5	44.8
+41				43.4
+65				42.1
133			6.0	40.3
+50			8.5	37.8
134			11.1	35.2

4-17-49
K.A.
L.G.
C.N.
C.F.
L.L.

84

Lt

E

Cl

✓ 5.0 3.0 5.0 5.1 5.0 5.0 5.2 5.4 5.5 5.5
6.0 4.8 2.7 1.0 1.0 2.2 3.5 4.7 6.0

✓ 2.7 3.4 4.4 5.0 5.0 5.2 5.1 5.2 5.1 5.2 5.1 4.8 4.5
200 150 100 50 25 10 10 25 50 100 150 200
Top Mast. Ham line + Lorpenteur Aves

2.9 3.2 1.8 1.3 1.1
1.0 3.3 4.5 5.6

4.2 4.4 3.0 1.5 1.2
1.0 2.6 4.5 5.3

Sta	+	π ✓	-	Elev
		946.34		
134 + 50			13.6	32.7 ✓
T.P.	0.17	933.06 ✓	13.45	932.89
135			2.8	30.3
+50			5.3	27.8
136			2.8	25.3
+50			10.3	22.8
137			12.8	20.3 ✓
T.P.	0.12	919.68 ✓	13.50	919.56
+50			2.0	17.7
138			4.6	15.1

X Sections

Larpenteur Ave.

Sta	+	π	-	Elev
B.M.	4.23	949.21		944.98
132 +23				44.2

+59

42.5

+59

42.5

+89

40.9

133

40.4

+06

40.0

+57

37.5

-3-44
K.A.
L.C.
C.F.
C.N.
L.L.

Lt. 9 Rt.

Top Mont of Hamline + Carpenter Ave.

40 43 53 53 50 53 47 39 44 43
60 47 28 10 10 15 46 46 60

Dup. from 28' Lt. 57 62 68 70 67 70 63 49 42
26 21 19 10 10 20 34 46

25 29 39 70 92 83 68 70 67
55 34 31 28 26 23 19 10
* Gutter *

15 15 18 37 97 93 88 85 85 83 85 80 75 43 48 31
60 50 35 32 25 22 21 18 10 10 18 18 29 43 60
* Gutter *

14 14 34 101 96 91 90 91 88 90 85 83 101 100 65 92 34
60 37 32 25 22 20 15 10 13 13 20 24 28 33 50 60
* Gutter *

+ 03-5" Tile 30' from stand

11 10 10 33 103 100 94 94 92 94 92 88 89 93 110 110 97
60 50 35 33 25 22 20 10 103 104 14 17 20 23 26 29
* Gutter *

36 41 65
60 50 34

03 04 31 129 126 120 120 117 119 122 130 130 73 45 33
50 39 36 25 22 20 10 10 20 23 26 34 43 60
* Gutter *

Sta.	+	π	-	Elev.
------	---	-------	---	-------

949.21

133 +76

36.6

134

35.4

+40

33.4

B.M.

4.23 744.98

Lt

C

Rt

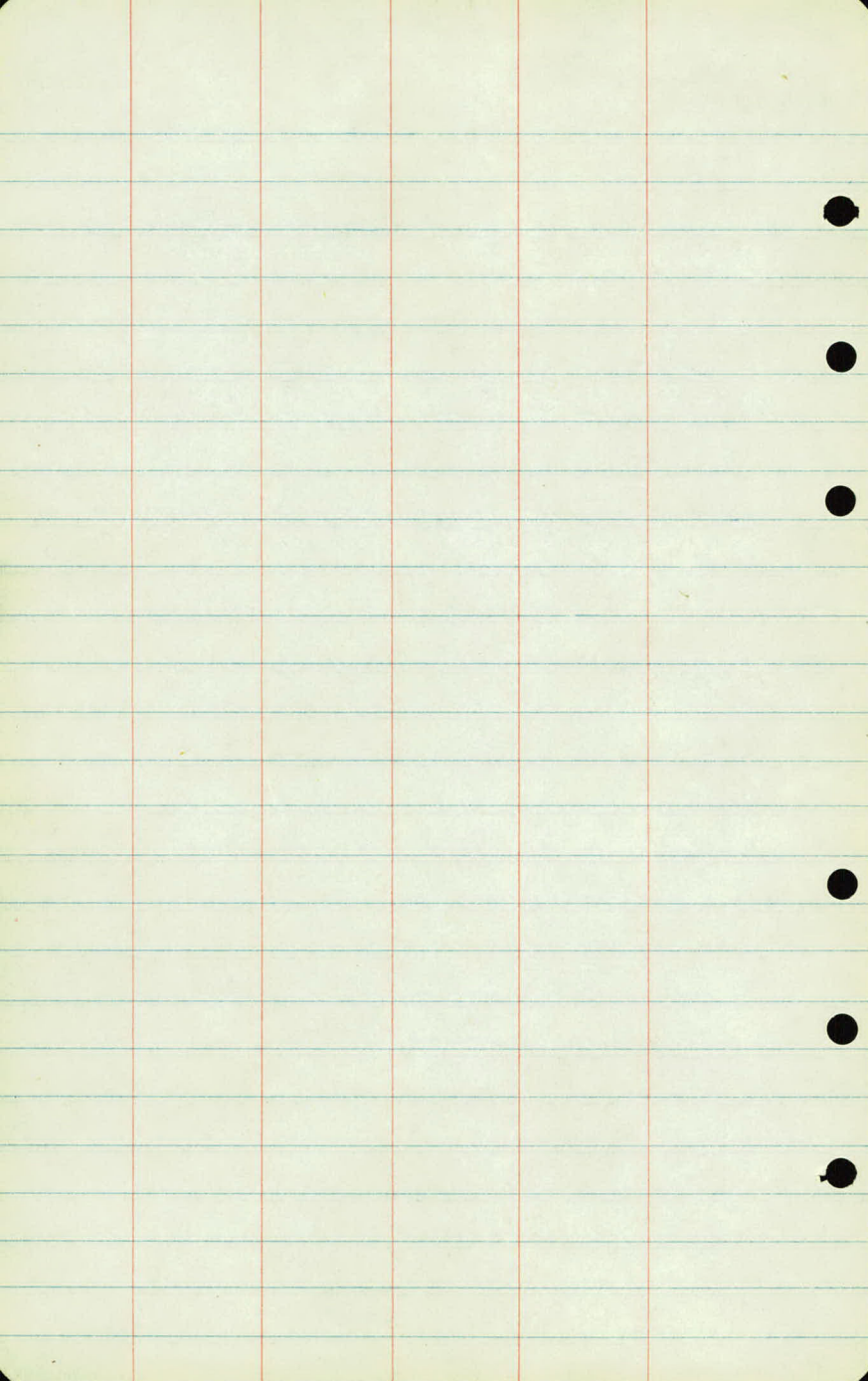
L.O. 0.2 0.2 3.2 13.8 13.7 12.9 12.9 12.6 12.9 13.2 14.5 14.7 6.2 7.0
 50 40 36 25 22 19 10 10 21 22 30 47 60
 ← Gutter →

L.O. 0.3 0.4 5.3 15.0 14.6 13.9 14.1 13.8 14.0 14.5 15.0 17.3 18.7 18.7
 49 42 36 25 22 20 10 10 20 27 36 53 60
 ← Gutter →

3.6 13.7 17.1 16.7 16.4 16.1 16.1 15.8 16.0 16.4 17.4 19.7 19.9
 42 29 25 22 21 16 10 10 19 27 52 60
 ← Gutter →

0.7 0.6 L.O.
 43 50

Top Mont Loce + Hamline Ave's.



Lt.

£

Rt.

Sta	+	T ✓	-	Elev
-----	---	-----	---	------

919.68

138 + 50			7.0	12.7.
----------	--	--	-----	-------

139			9.5	10.2.
-----	--	--	-----	-------

+ 50			11.7	08.0.
------	--	--	------	-------

140			13.5	06.2.
T.P.	3.81	✓ 910.09	13.40	906.28

+ 50			5.1	05.0.
------	--	--	-----	-------

141			6.0	04.1.
-----	--	--	-----	-------

+ 50			6.4	03.7.
------	--	--	-----	-------

142			6.3	03.8.
-----	--	--	-----	-------

Lt.

E

Rt.

9.9.19

Sta.	+	✓ 910.09	-	Elev.
------	---	-------------	---	-------

142 +50			6.0	04.1
---------	--	--	-----	------

143			5.2	04.9
-----	--	--	-----	------

+50			4.0	06.1
-----	--	--	-----	------

144			2.8	07.3
-----	--	--	-----	------

+50			1.5	08.6
-----	--	--	-----	------

B.M.			0.42	909.67 ✓ <u>909.58</u>
------	--	--	------	---------------------------

5-23-44
K.A.
L.G.

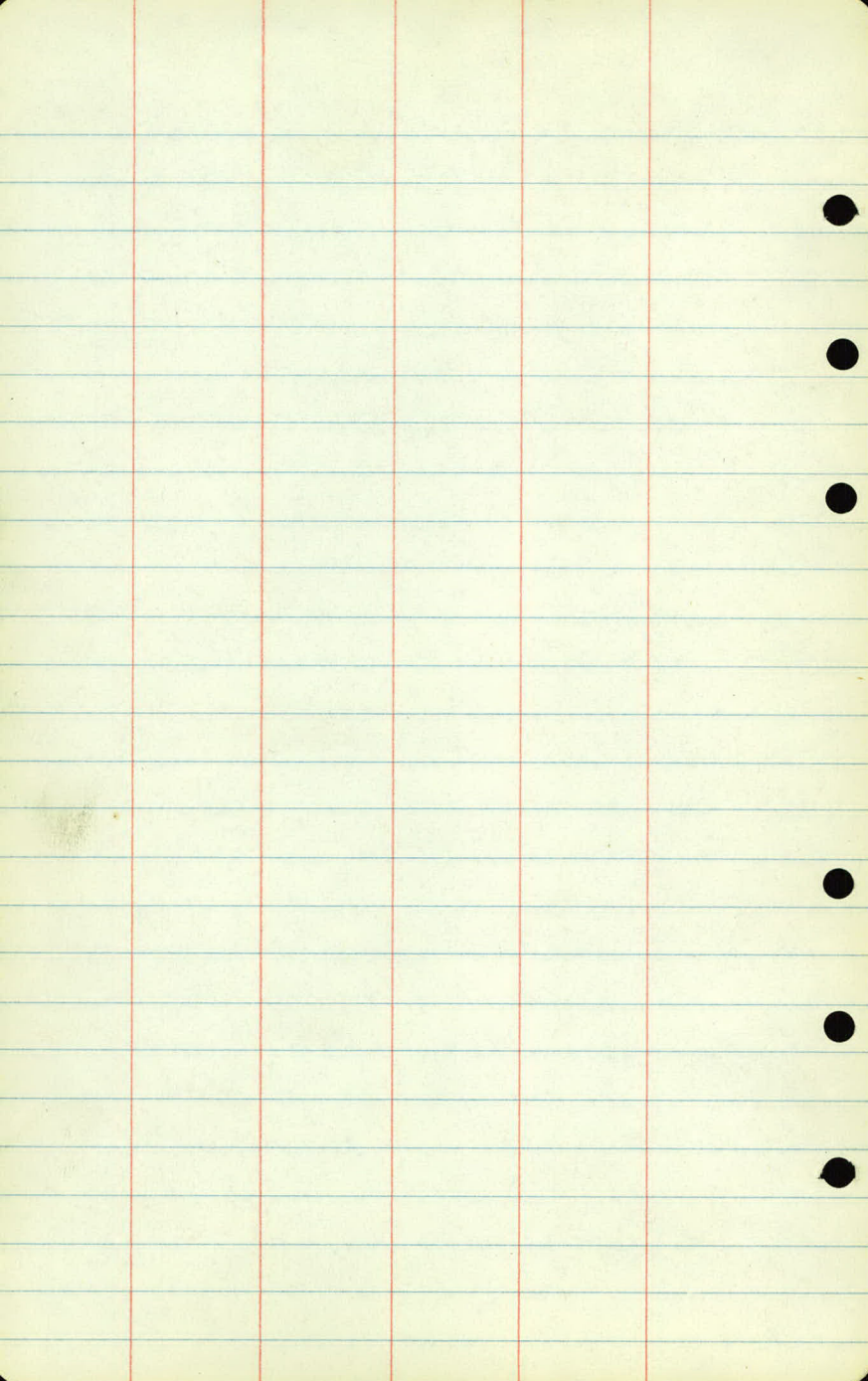
87

Lt.

\$

Rt.

Top Mon. 1/4 Mi. E. of Hamline.



7-7-44

A.B.
L.C.
C.F.
D. G.
D.S.

4 Levels

Larp. Ave - Fernwood To Let.

Rec'd in office 7/8/44
Photo'd 7/8/44

Sta.	+	H.I.	-	Elev.
------	---	------	---	-------

B.M.	6.82	916.40.		909.58
------	------	---------	--	--------

145

+34	± Ferwood St. (Approx)	10.7
-----	------------------------	------

146		12.1
-----	--	------

+50		13.6
-----	--	------

147		15.2
-----	--	------

T.P.	10.24	925.68.	0.96	915.44.
------	-------	---------	------	---------

+50		16.1
-----	--	------

148		16.8
-----	--	------

+50		17.7
-----	--	------

149		18.8
-----	--	------

+50		19.8
-----	--	------

150		21.0
-----	--	------

Top Of Mont. 145+02.85 - High Point.

$$5.7 \quad \frac{5.9}{10} \quad \frac{5.4}{22} \quad \frac{4.0}{50} \quad \frac{0.7}{100} \quad \frac{+2.9}{150} \quad \frac{+6.5}{200}$$

4.3

2.8

1.3

9.6

8.9

8.0

6.9

5.9

4.7

Sta.	+	H.I.	-	Elev.
		925.68		
150+07.5	± Dunlap St. (North)			21.2
+50				22.5
151				24.0
+50				25.7
T.P.	7.75	933.37	0.06	925.62
152+01	± Dunlap St. (South)			27.4
B.M.			1.15	932.22
				932.21
+50				29.2
153				31.0
+50				32.3
154				33.4
T.P.	10.15	943.51	0.01	933.36
+50				34.1
155				35.1
+50				36.3

<u>1.1</u>	<u>2.8</u>	<u>4.4</u>	<u>5.6</u>	<u>6.3</u>	<u>6.5</u>	<u>6.7</u>	<u>5.6</u>	<u>4.7</u>
400	350	300	250	200	150	100	50	10

3.2

1.7

0.0

<u>6.2</u>	<u>5.1</u>	<u>4.2</u>	<u>3.4</u>	<u>2.2</u>	<u>0.9</u>	<u>+0.1</u>
6.0	10	50	100	150	200	250

Top of Hyd. S.E. Cor. Dunlap + Larp.

4.2

2.4

1.1

0.0

9.4

8.4

7.2

Sta.	+	H.I.	-	Elev.
------	---	------	---	-------

		943.51.		
--	--	---------	--	--

156				37.6
-----	--	--	--	------

+50				38.9
-----	--	--	--	------

157				40.0
-----	--	--	--	------

+50				40.7
-----	--	--	--	------

158				41.3
-----	--	--	--	------

+08	4 Lex. Ave			41.4
-----	------------	--	--	------

B.M.		2.12	941.39.	941.35
------	--	------	---------	--------

R

5.9

4.6

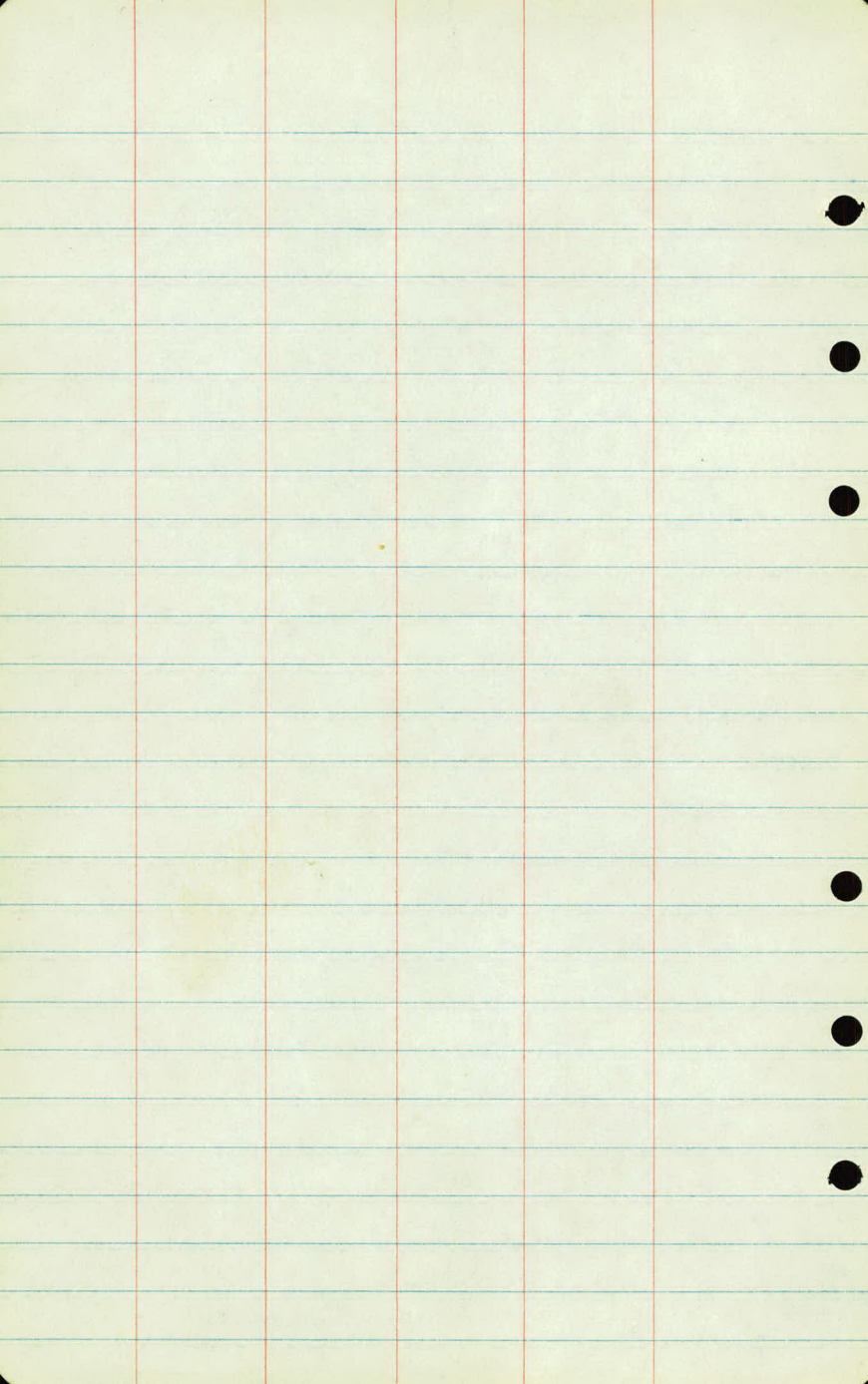
3.5

2.8

2.2

2.1

Top of Sec. Cor. Pipe Lex. + Larp.



BENCH LEVELS

USC + GS NO. 611 CO. RD 'B' + HAMLINE

TO

LARPENTEURE + WEST CO. LINE

	+	π	-	ELEV
B. M	9.22	959.77.		950.552
B. M	293	959.77.	2.93	956.84.
	363	962.34.	1.06	958.71.
	348	957.07.	8.75	953.59.
B. M	175	957.07.	175	955.32.
	5.91	957.37.	5.61	951.46.
	7.69	964.21.	0.85	956.52.
B. M	1.86	956.62.	9.45	954.76.
	111	951.62.	6.11	950.51.
	375	947.95.	7.42	944.20.
B. M	247	947.95.	2.47	945.48.
	5.11	947.41.	5.65	942.30.
	8.65	953.67.	239	945.02.
B. M	8.69	953.67.	8.69	944.98. 945.35
B. M.			3.70	949.97.

U.S.C + G.S No G.11 Co. RD. "B" + HAMLINE
 Top S.E. COR. 2ND STEP ROSE TOWN HALL

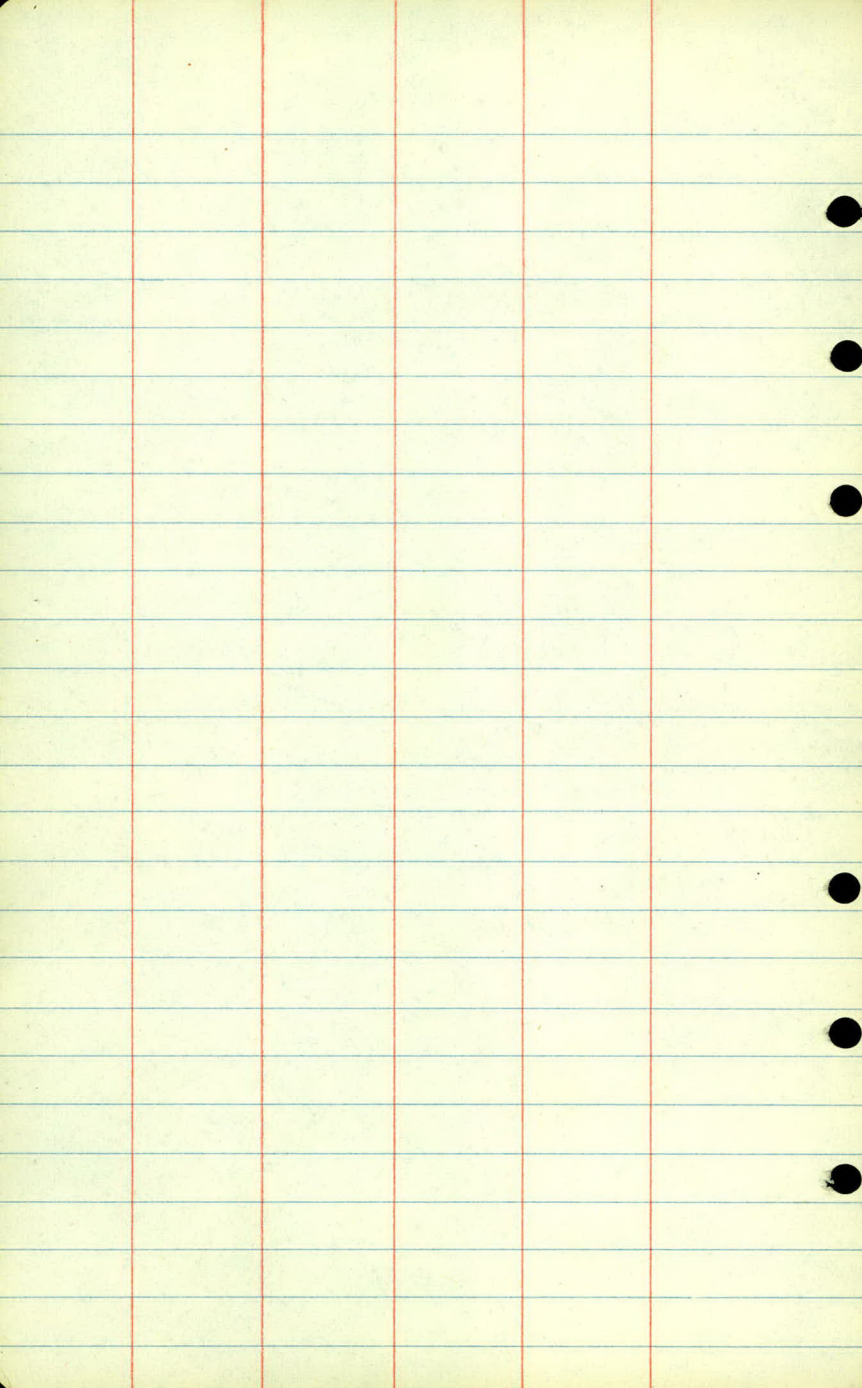
Top BOTTOM So. STEPS S.W. COR ST. ROSA LIMA SCHOOL

R.R. SPIKE P. POLE N.W. COR HAMLINE + ROSELAWN

Top HYDRANT S.W. COR GARDEN + HAMLINE

Top MONT HAMLINE + LARPENTUER

BOTTOM STEP S.E COR STUCCO HOUSE 1707 HAMLINE

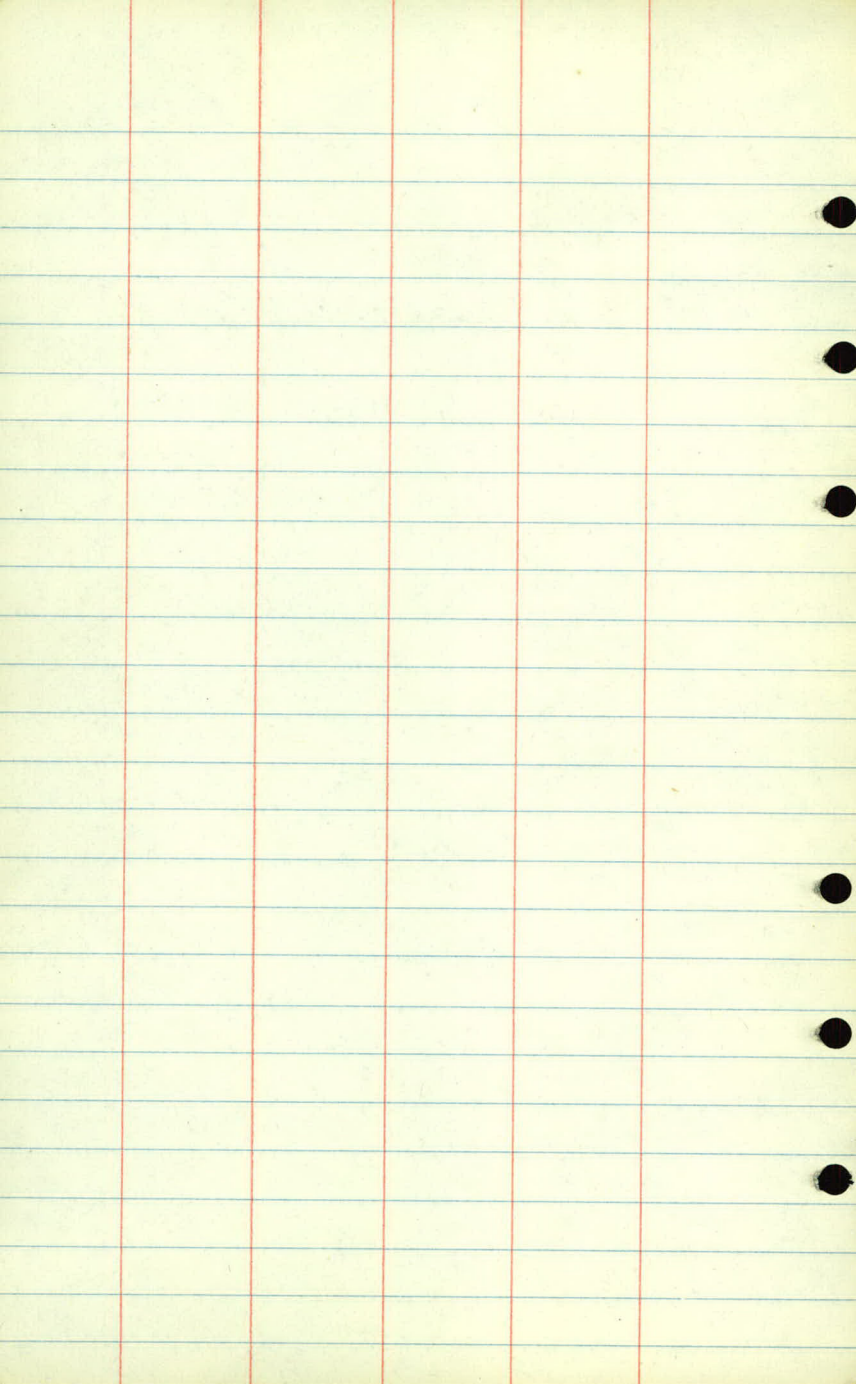


STA	+	π	-	ELEV
B.M	138	961.76.		960.38 960.75
	0.05	950.52.	11.29	950.47.
	5.89	947.74.	8.67	941.85.
	11.88	947.74.	11.88	935.86. 936.21
	10.52	952.37.	5.89	941.85.
	9.63	961.55.	0.45	951.92.
	6.16	961.50.	6.21	955.34.
	3.28	959.57.	5.21	956.29.
	1.33	957.89.	3.01	956.56.
	0.32	952.67.	5.54	952.35.
	1.72	941.83.	12.56	940.11.
	2.60	934.61.	9.82	932.01.
	4.29	932.02.	6.88	927.73.
	7.27	937.90.	1.39	930.63.
	10.04	946.55.	1.39	936.51.
	4.39	944.67.	6.27	940.28.
B.M			6.18	938.49. 938.37 ?

TOP HYDRANT S.W. COR. LARRENTUEN + EUSTIS

SPIKE IN P. POLE RT STA 5+47 113' WEST WALNUT

TOP MONT CO. RD "B" + WEST CO LINE



Larpenteur Ave
Borings

Sta. 28 to 46+50

Fulham = 26+41
Cleveland = 52+81

5-19-44

Sta. 28+00 12' Lt.

Feet

Material

0'-1'

Fill Material

1-3

Clay

3-5

Mixture Clay, Sand, some pebbles
and quite a few larger stones

No water

5-19-44

93

Sta. 28+00 12' Bt.

Feet	Material
0'-1'	Fill Material
1'-5.5'	White + Yellow Clay
5.5'-9'	Hard Red Clay

No water

5-19-44

Sta 28+50 12' Lt

Feet

Material

0'-1'

Fill Material

1'-4'

White Clay

4' - -

* Pebbles
Sand - Water washes

material off auger.

4' Hit water

5-19-44

94

Sta 28+50 12' Bt

Feet	Material
0' - 2'	Fill Material
2 - 6'	clay
6.0 - 7.5	Sandy clay
7.5 - —	+ pebbles Sand - water washes material off auger

6' Hit water

5-1844

Sta 29 12' L+

Feet

Material

0'-1'

Fill Material

1'-6'

Clay Yellow

6'-

Sand

Water washes material
off auger.

4.5' Hit water

Sta 29 12' Bl.

Feet

Material

0'-2'

Mixture of fill material

2'-5'

Clay Yellow

5'-5.5'

Sand & water

5.5'-down

Hard red clay

5' hit water

5-19-44
Antert party

Sta 29+50 12 ft

Feet

Material

Fill Material

0-1

= Mixture sand, gravel & clay

1'-8

clay

3.5' water seeps into hole

Sta 29+50 12' Bl.

Feet	Material
0 - 1'	Fill Material
1' - 8	Clay

Hit Water at 60' below surface

5-19-44

Sta. 30+00 12' Lt.

Feet

Material

0-1

Fill Material

1-6'

Hard Red Clay

No water

5-19-44

97

Sta 30+00 12' Bt

Feet

Material

0'-1'

Fill Material

1'-7.5

Clay

7.5 - -

Hard Red Clay

7'

Hit water

5-19-24

Sta. 30 +50 12' Lt.

Feet

0. - 1.5

1.5 - 8'

Material

Fill Material

clay

No water

Sta. 46 12' E

Feet	Material
0' - 1'	Fill Material
1 - 3.5	Hard Red Clay
3.5 - 4'	Sandy Clay
4' - down	Sandy Material.
	Auger cannot penetrate because of stones

No Water

5-20-44

Sta 44+50 12' R.H.

Feet

Material

0-0.5'

Fill Material

0.5-2'

Sandy Clay & Stones

Sandy Material

No Water

Sta. 45+50

Feet

0 - 1'

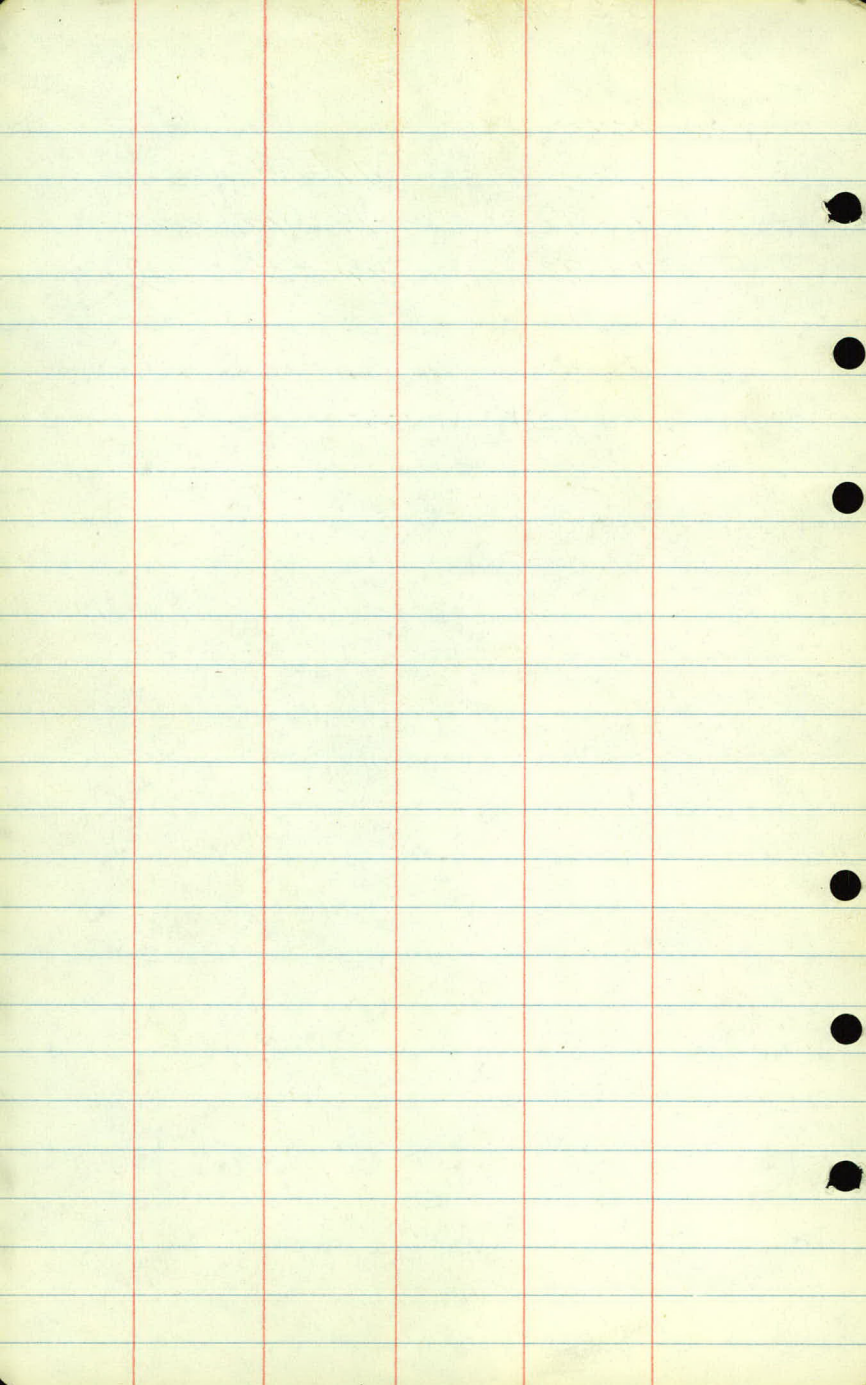
1 - 9

Material

Fill Material

Hard Red Clay

No water



Pavement Levels
at
Snelling Ave.
and
Larpentour Ave.

sta	+	π	-	Elev.
B.M.	2.49	960.54		(958.05)

105 +14			4.00	956.54
---------	--	--	------	--------

+15			4.02	956.52
-----	--	--	------	--------

+26			4.19	956.35
-----	--	--	------	--------

+26			4.37	956.17
-----	--	--	------	--------

106 +29			4.85	955.69
---------	--	--	------	--------

13886

lt

z

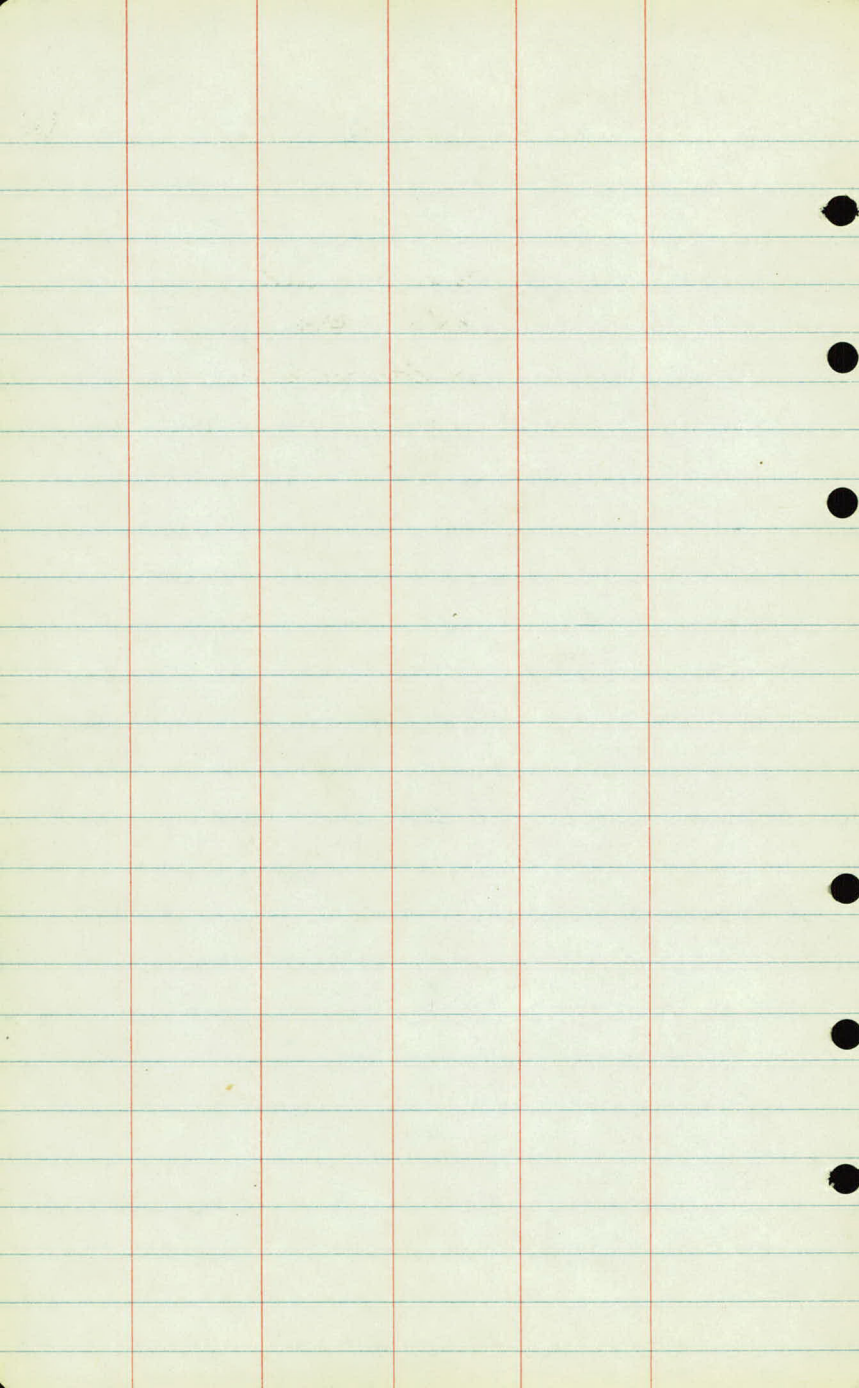
pt

Top Hyd at Snelling Ave.

Top Black Top

Top old Conc.

East Edge of North Lane



Larpenteur Ave

Profile Levels

Sta	+	π	-	Elev.
B.M.	2.90	944.35	4.51	939.84

158 +50

159

+50

160

+50

161

+50

162

+50

163

+50

164

T.P.	839	948.23
------	-----	--------

Lt.

£

RA.

Top Sec. Cer. pipe - Larp. & Lexington Aves.

32

38

40

42

45

49

51

52

52

53

51

48

Sta	+	π	-	Elev
-----	---	-------	---	------

948.23

164 + 50

165

+50

166

+50

167

+50

168

+50

169

B.M.

2.81

945.42

+50

170

T.P.

2.28

943.09

2.42

940.81

Lt

#

Rt

8.1

7.3

6.3

5.3

4.6

4.4

4.6

4.9

5.3

5.8

Top Hyd. Pt. Sta. 169+

6.3

6.6

Sta	+	π	-	Elev
-----	---	-------	---	------

943.09

170	+50			
-----	-----	--	--	--

171

+50

172

+50

173

+50

174

+50

175

+50

176

B.M.

868

934.11

Lt.

£

Rt.

2.0

2.4

2.9

3.4

3.9

4.4

4.9

5.2

5.7

6.1

6.8

7.7

Drill Hole £ Pav. Victoria + Harp. Ave

Sta	+	Δ	-	Elev
-----	---	----------	---	------

943.09

176 +50

177

J.P.	0.18	932.58	10.69	932.40
------	------	--------	-------	--------

+50

178

+50

179

+50

180

+50

181

+50

182

T.P.	2.98	924.20	11.36	921.22
------	------	--------	-------	--------

Lt.

±

Rt.

9.0

10.3

1.5

3.5

5.5

7.2

8.8

9.9

10.6

10.8

11.0

11.1

Sta.	+	π	-	Elev
------	---	-------	---	------

		924.20		
--	--	--------	--	--

182 +50				
---------	--	--	--	--

183				
-----	--	--	--	--

+50				
-----	--	--	--	--

184				
-----	--	--	--	--

+50				
-----	--	--	--	--

185				
-----	--	--	--	--

+50				
-----	--	--	--	--

B.M.				
------	--	--	--	--

3.14				
------	--	--	--	--

921.06				
--------	--	--	--	--

920.97				
--------	--	--	--	--

186				
-----	--	--	--	--

+50				
-----	--	--	--	--

187				
-----	--	--	--	--

+50				
-----	--	--	--	--

188				
-----	--	--	--	--

Lt.

4

Rt.

2.8

3.0

3.4

4.0

4.5

5.2

5.8

Top of Hyd. Rt. Sta. 1854

6.4

6.9

7.5

8.2

8.5

Sta.	+	H.I.	-	Elev.
------	---	------	---	-------

924.20

188+50

189

T.P.	6.12	921.17	9.15	915.05
------	------	--------	------	--------

+50

190

+50

191

+50

192

B.M.			1.51	919.66	919.57
------	--	--	------	--------	--------

+50

193

+50

194

8.7

8.9

5.8

5.8

5.6

5.4

5.3

5.0

Top of Hyd Rt. Sta. 192+

4.6

4.0

3.2

2.5

Sta.	T	H.I.	-	Elev.
------	---	------	---	-------

921.17

194+50

195

+50

T.P.	5.17	925.80	0.54	920.63
------	------	--------	------	--------

196

+50

197

+50

198

+50

199

+50

200

1.7

1.0

0.5

4.7

4.3

4.2

4.1

4.0

4.0

4.2

4.4

4.6

Sta	+	H.I.	-	Elev
-----	---	------	---	------

925.80

200+50

201

+50

202

+50

203

+50

B.M.	0.78	923.62	2.96	922.84
------	------	--------	------	--------

204

+50

205

+50

206

4.7

4.9

5.1

5.2

5.3

5.5

5.7

Top of Hyd. Rt. Sta. 203+

3.6

3.8

3.9

4.0

4.0

Sta.	f	H.I.	-	Elev
------	---	------	---	------

		923.62		
--	--	--------	--	--

206	+50			
-----	-----	--	--	--

207				
-----	--	--	--	--

	+50			
--	-----	--	--	--

208				
-----	--	--	--	--

	+50			
--	-----	--	--	--

209				
-----	--	--	--	--

	+50			
--	-----	--	--	--

210				
-----	--	--	--	--

	+50			
--	-----	--	--	--

+78	4 Dale St. So.			
-----	----------------	--	--	--

B.M.				
------	--	--	--	--

		2.16		
--	--	------	--	--

			921.46	
--	--	--	--------	--

				921.46
--	--	--	--	--------

4.3

4.5

4.6

4.8

5.0

5.2

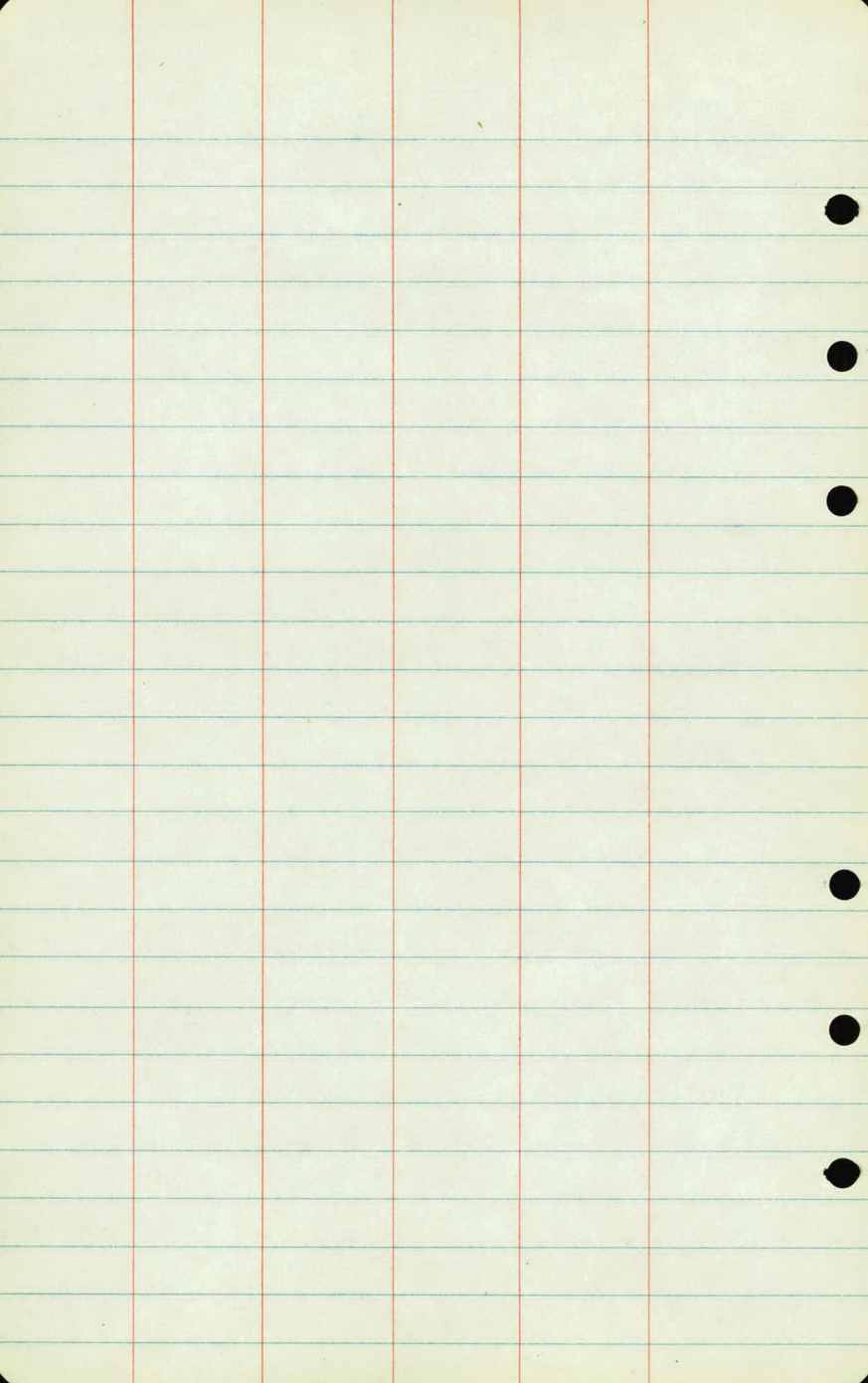
5.2

5.1

5.0

4.9

Top Hyd S.W. Cor. Dale & Larp.



Profile Levels

Walnut Street

Sta	+	π	-	Elev
B.M.	13.47	949.33.		935.86

0	+00		8.6	40.7
---	-----	--	-----	------

	+30		8.0	41.3
--	-----	--	-----	------

	+60		7.1	42.2
--	-----	--	-----	------

1			5.4	43.9
---	--	--	-----	------

	+50		2.3	47.0
--	-----	--	-----	------

T.P	12.17	961.28.	0.22	949.11
-----	-------	---------	------	--------

2			11.6	49.7
---	--	--	------	------

	+50		9.2	52.1
--	-----	--	-----	------

3			7.3	54.0
---	--	--	-----	------

	+50		6.0	55.3
--	-----	--	-----	------

4			5.4	55.9
---	--	--	-----	------

	+50		4.9	56.4
--	-----	--	-----	------

5			4.4	56.9
---	--	--	-----	------

5-23-44

K.A.
L.C.
L.N.
C.F.
L.L.

101

Lt

L

101

Spt. in PR Rt sta. 5147 (Larp. Ave.)

E Larpentaur Ave.

48.70 51.0

55.20



126 103
100 50

61
50

Sta	+	π	-	Elev
		961.28		
5	+50		4.4	56.9
6			4.5	56.8
	+50		4.8	56.5
7			5.5	55.8
T.P.				
	+50		6.2	55.1
8			7.2	54.1
T.P.	3.15	958.24	6.19	955.09
	+50		4.9	53.3
	+60	X Drain		
9			5.1	53.1
	+50		4.9	53.3
10			4.9	53.3
	+50		5.0	53.2
11			4.9	53.3

Lt.

4

Rt.

41.5 442 46.5 488

5140


 14.7 14.0 11.7 9.4

200 150 100 50

6.8

50

Sta	+	π	-	Elev	
		95824			
11	+50		43	53.9	.
12			32	55.0	.
		764.46		955.28	
T.P.	9.18	964.56	2.96	955.38	
	+50		7.6	55.9	56.9.
13			5.8	58.7	.
+17 = Approx 2 Spring Sta					
B.M.			3.90	960.66	
	+50		5.3	59.2	.
14			5.6	58.9	.
	+50		6.2	58.3	.
15			6.8	57.7	.
	+50		7.7	56.8	.
16			8.7	55.8	.
	+50		9.8	54.7	.

Lt

E

Rt

Nail in PP N.E. Cor. Spring + Malvern
 59 45 44 45 44 47 46 4.3
 31 50 100 150 200 250 300
 4.1 60 4
 327 Malvern

Sta.	+	π	-	Elev.
		764.46		

17			11.2	53.3
----	--	--	------	------

+50			12.6	51.9
-----	--	--	------	------

18			13.7	50.8
----	--	--	------	------

LH

E

RH

46.1

49.7

51.90

18A

14.8

12.6

100

50

Sta.	$\pm$	π	-	Elev.
------	-------	-------	---	-------

7

 π

1

Elev.

Lt

C

Rt

Profile Levels

Melvern Street

Sta.	+	π	-	Elev.
T.P.	12.68	963.08		950.4

0	+00		12.68	50.4
---	-----	--	-------	------

	+50		11.4	51.7
--	-----	--	------	------

1			11.6	51.5
---	--	--	------	------

	+50		9.7	53.4
--	-----	--	-----	------

2			7.2	55.9
---	--	--	-----	------

	+50		4.5	58.6
--	-----	--	-----	------

3			2.1	61.0
---	--	--	-----	------

	+50		0.1	63.0
--	-----	--	-----	------

T.P.	646	969.14	0.40	962.68
------	-----	--------	------	--------

4			4.2	64.9
---	--	--	-----	------

	+50		3.7	65.4
--	-----	--	-----	------

5			4.3	64.8
---	--	--	-----	------

	+50		5.1	64.0
--	-----	--	-----	------

Lt.

E

Bt.

E. Prov. Sta. 9195

St _g	±	π	-	F/ev	
		969.14			
6			5.8	63.3	.
+50			6.1	63.0	.
+58	= Approx ± 1 one St. 6.1			63.0	.
7			6.2	62.9	.
+50			6.7	62.4	.
8			7.0	62.1	.
+50			6.9	62.2	.
T.P.	4.86	966.74	7.26	961.88	.
9			4.6	62.1	.
+50			4.6	62.1	.
10			4.5	62.2	.
+50			4.7	62.0	.
11			5.0	61.7	.

Lt.

\$

Rt

61.1

80 61

69

Sta	+	π 966.74 966.76	-	Elev	
11	+50		5.2	61.5	.
12			5.1	61.6	.
	+50		5.4	61.3	.
13			6.1	60.6	.
+17	Approx. $\pm$ Spring St. ^{6A}			60.3	.
	+50		7.0	59.7	.
14			7.6	59.1	.
	+50		7.9	58.8	.
15			8.7	58.0	.
+55	X Drain drains W			57.2	.
T.P.	6.18	962.77 962.79	10.15	956.59 956.61	
16			5.2	57.6	.
	+50		5.2	57.6	.

Lt.

E

Rt.

52.7

54.5

56.0

Drois

14.0

12.22

10.22

Wast.

50

25

30

Ho.

to pot hole

Sta	+	π	-	Elev	
		962.77			
		962.79			
17			5.7	57.1	.
	+50		6.4	56.4	.
18			7.5	55.3	.
	+50		9.2	53.6	.
19			10.8	52.0	.
	+50		11.7	51.1	.
+75 A ₁			11.6	51.2	.
B.M.			2.17	960.60	960.56
				960.68	960.66

5-23-44
K.A.
L.C.
C.F.
C.N.
C.L.
Lt

109

£

Et.

Chr. Pot hole Lt. sta 17

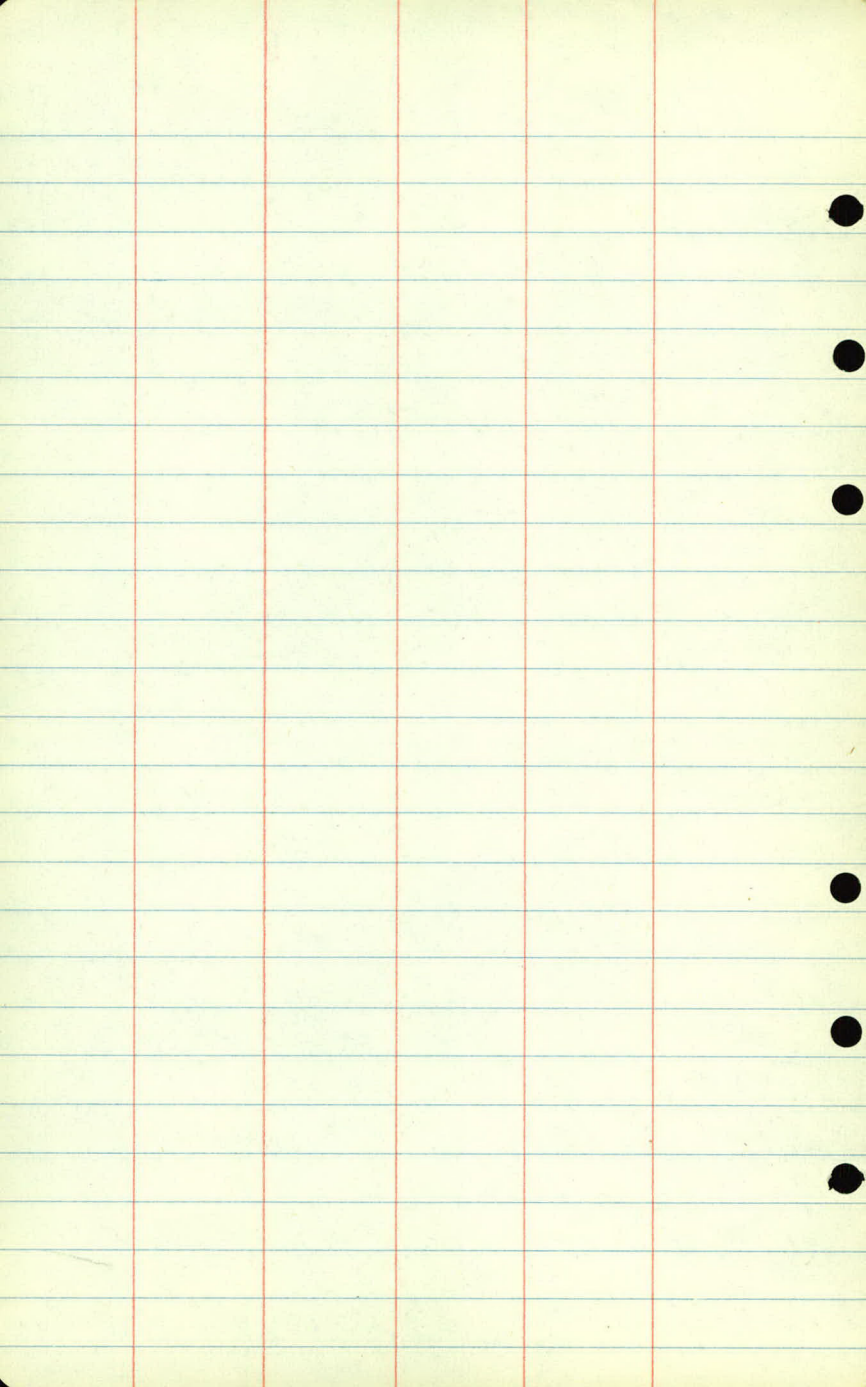
457 46.6 488 51.8

171 16.2 140 11.0

150 133 100 50

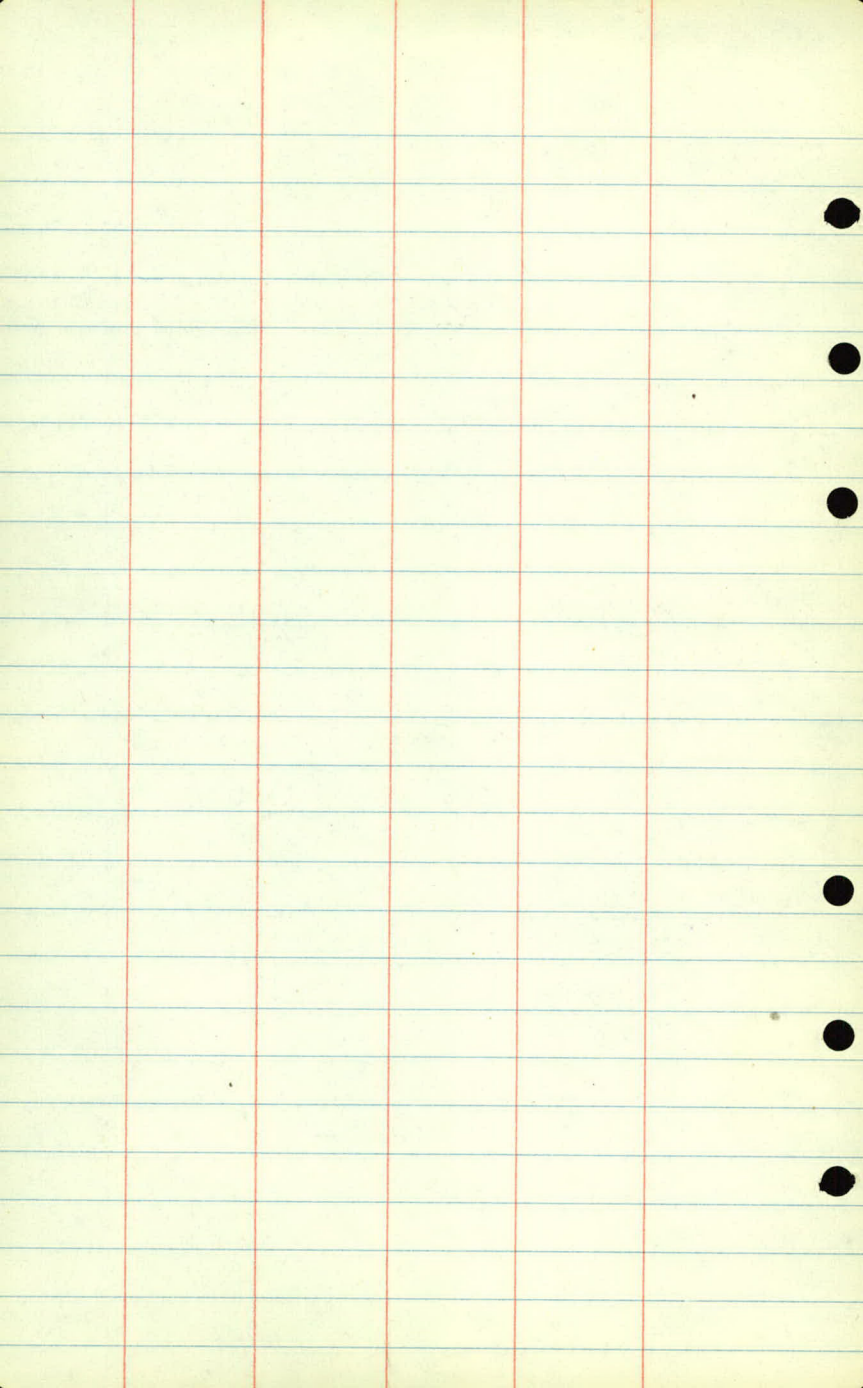
Approx. £ Summer St.

Nail in P.P.N.E. Cor. Spring & Melvern



Profile Levels

Eustis Street.



Profile Levels
Eustis St.
So. of Carpenter Ave.

Sta.	+	π	-	Elev.
B.M.	0.12	960.50		(960.38)
0	+00		1.3	59.2
	+10		1.5	59.0
	+50		3.8	56.7
1			2.0	53.5
	+50		10.1	50.4
2			13.2	47.3
	+50		16.5	44.0
3			20.2	40.3
	+50		24.6	35.9

5-23-44

K.A.

L.C.

C.F.

C.N.

L.L.

Lt.

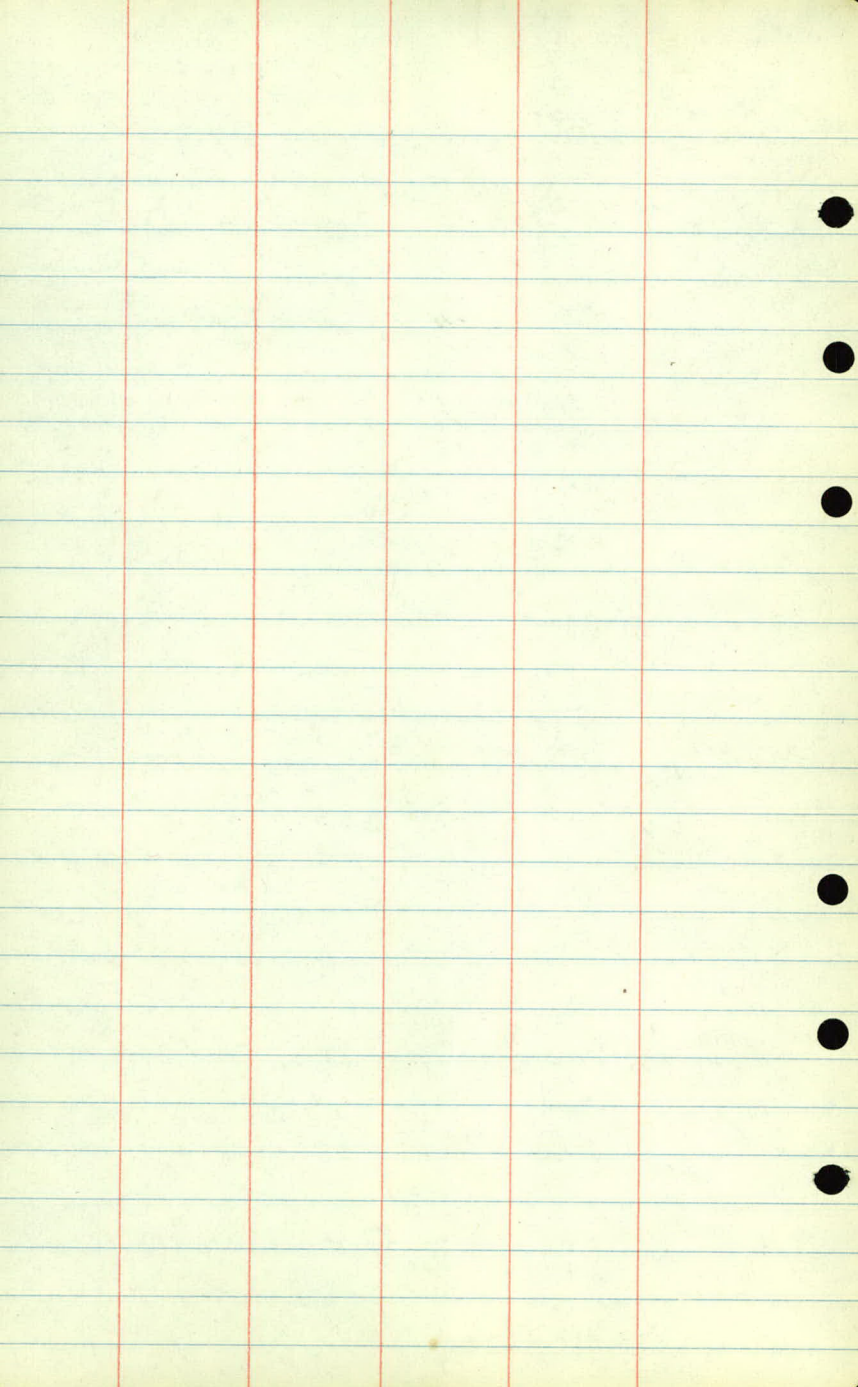
4

Cl.

112

Top Hyd. SW. Cor. Larp. & Eustis.

= E. Larpeur Ave.



Profile Levels
Eustis Street

No. of Larpenfour Ave

Sta	+	π	-	Elev
B.M.	472	965.10		960.38
0	+50		5.5	59.6
1			4.9	60.2
	+50		4.0	61.1
	+68			
2			3.4	61.7
	+50		2.6	62.5
3			1.8	63.30
T.P.	9.57	972.92	1.75	963.35
	+50		9.0	63.9
4			8.4	64.5
	+50		7.7	65.2
5			6.9	66.0
	+50		6.1	66.8

K.A.
L.C.
C.N.
L.L.

114

Lt.

£

et.

Top Hyd. SW. Cor Larp + Eustis

55.9

9.2 = 30' Rt.

FL. M.H. From E goes So.

Sta	+	π	-	Elev
		972.92.		
6			5.6	67.3
+60	Approx $\pm$ 1000 ft.		5.0	67.9
7			4.7	68.2
+50			4.2	68.7
8			3.9	69.0
+50			3.6	69.3
9			3.6	69.3
+50			3.5	69.4
10			3.8	69.1
+50			4.0	68.9
T.P.	2.85	971.57	4.20	968.72
11			3.3	68.3
+50			3.9	67.7

Lt.

E

Rt.

64°

65.2

65.9

66.7

67.1

67.8

68.0

68.4

89 7.7 7.0 6.2
200 150 100 50

5.3 5.1 4.9 4.5
50 100 150 200

Sta.	+	π	-	Elev.
		971.57		
12			4.4	67.2
+50			5.0	66.6
13			5.0	66.6
+19	Approx & Spring St.		6.1	66.5
B.M.			11.0	960.57
14			6.2	65.4
15			7.2	64.4
16			8.5	63.1
I.P.	0.90	963.05	9.42	962.15
17			1.5	61.6
18			2.8	60.3
19			4.4	58.7
+58	Approx. & Summer St. Lt.			
B.M.			5.38	957.67
+75	Approx. & Summer St. Lt.			

Lt.

E

Et.

62 ⁰	63 ⁴	64 ⁴	65 ⁶	66 ⁹	68 ¹	69 ²	69 ⁰	67 ³
9.6	8.2	7.2	6.0	4.7	3.5	2.4	2.6	4.3
200	150	100	50	50	100	150	200	250

Nail in P.P. N.E. Cor. Melvern & Spring

8 ²	57 ⁵	56 ⁹	56 ⁹
4.9	5.6	6.2	6.2
	100	200	300

Nail in P.P. at Summit & Cardus

54 ³	55 ⁸	58 ¹	57 ⁹
8.8	7.3	5.0	5.2
200	100	22	

Sta.	+	π	-	Elev
		963.05		
20			5.7	57.4
21			7.0	56.1
22			8.5	54.6
23			9.9	53.2
T.P.	0.60	953.63	10.02	953.03
24			2.0	51.6
25			3.4	50.2
26			4.6	49.0
+ 36 Approx @ Roselaw Ave			5.0	48.6
B.M.		948.93	3.11	950.52
T.P.	4.15	948.92	8.85	944.78 942.41
T.P.	3.14	945.55	6.52	942.40
B.M.			9.00	936.55

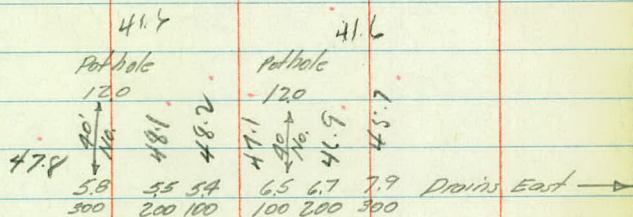
5-24-44

117

Lt.

E

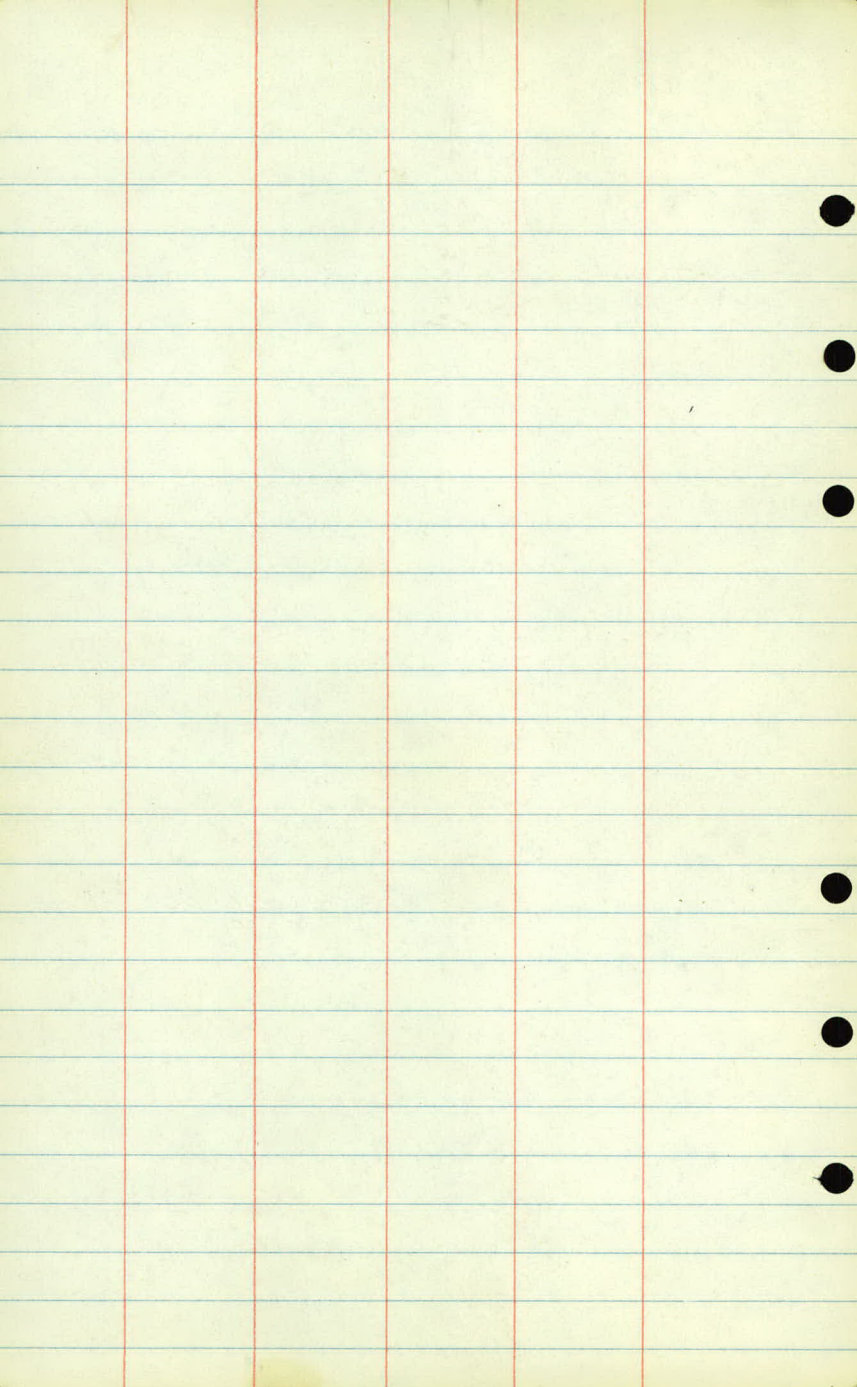
Rt.



Top N.E. Cor. Bottom Stop on H. 1917 Eustis St.

Drainage continues north

Spt in Arc Light Pole at Rose/own + Fulham



Profile Levels

Carl Street

Sta.	+	π	-	Elev.
------	---	-------	---	-------

BM.	2.12	965.52		63.4
-----	------	--------	--	------

0 +00			2.4	63.1
-------	--	--	-----	------

+18			2.4	63.1
-----	--	--	-----	------

+50			3.7	61.8
-----	--	--	-----	------

1			5.3	60.2
---	--	--	-----	------

+50			5.9	59.6
-----	--	--	-----	------

+57	C.B. Lt.			
-----	----------	--	--	--

+	C.B. Rt.			
---	----------	--	--	--

2			5.6	59.9
---	--	--	-----	------

3			4.8	60.7
---	--	--	-----	------

4			4.1	61.4
---	--	--	-----	------

T.P.	11.50	973.21	3.81	961.71
------	-------	--------	------	--------

5			9.7	63.5
---	--	--	-----	------

6			6.6	66.6
---	--	--	-----	------

lt.

¢

rt.

Esto 16400 Lorr Ave.

56.90

58.5

8.6
7.77.0
inlet

58.8

57.5

6.7
inlet8.0
F.L. = Beg. Sewer

Sta.	+	π	-	Elev.
		973.21		
6	+88	Approx. E. lane st.	4.3	68.9
7			4.3	68.9
8			5.2	68.0
9			5.9	67.3
10			6.5	66.7
T.P.	2.83	970.07	5.97	967.24
11			4.2	65.9
12			5.0	65.1
13			5.3	64.8
+31	C.B. Rt. & Lt.			
+54	Approx E. spring st.			
			4.8	65.3
+79	C.B. Rt. & Lt.			
14			5.1	65.0

Lt.

E

Et.

45
10042
100

61.60

63.7

63.5

60.3

8.5
F.L.6.4
inlet6.6
inlet9.8
F.L.

65.4

4.7
100

63.1

64.4

63.5

59.8

7.0
F.L.5.7
inlet6.6
inlet10.3
F.L.Drains
East.

Sta	+	π	-	Elev
		970.07		
15			3.5	66.6
16			2.0	68.1
17			2.8	67.3
T.P.	0.47	967.33	3.21	966.86
18			4.0	63.3
19			8.7	58.6
+ 97	Approx. @ Summer St.		10.5	56.8
B.M.			9.65	957.68. (951.67)

K.A.
L.G.
C.N.
L.L.

121

L.A.

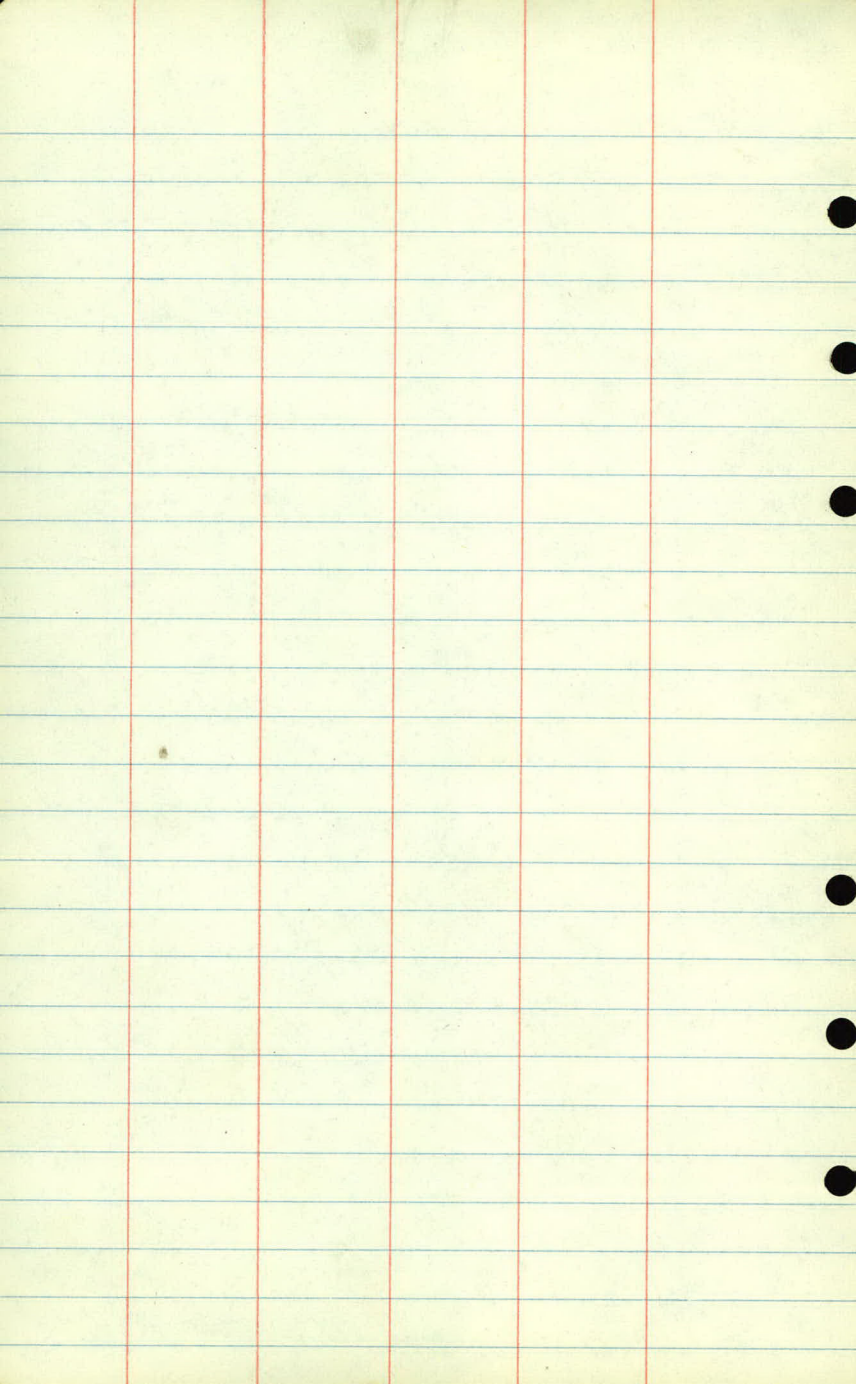
L

Et.

5-63

11.0
100

Nail in P.R. Summit + Corl



Profile Levels
Pleasant Street

Sta.	+	π	-	Elev.
B.M.	652	975.02		968.5
0 +50			5.9	69.1
1			5.2	69.8
2			4.8	70.2
3			5.0	70.0
4			4.8	70.2
T.P.	426	975.09	4.19	970.88
5			4.5	70.6
6			4.4	70.7
+59 Approx & lone st.			4.9	70.2
7			5.4	69.7
8			6.8	68.3
9			7.6	67.5
10			7.9	67.2
T.P.	425	971.57	7.77	967.32

5-24-44

123

Lt

E

Rt

E Pav 19+91.72 (Lamp. Ave.)

69.0 69.2

61 59
200 100

643 63.7 61.7

N.E. thru low land

108 114 134 NE
50 100 200

Sta	+	π	-	Elev
-----	---	-------	---	------

971.57

11			3.9	67.7
----	--	--	-----	------

12			3.9	67.7
----	--	--	-----	------

13			4.8	66.8
----	--	--	-----	------

+21 Approx. & Spring St.

+40 M.H. Lt.

14			6.6	65.0
----	--	--	-----	------

15			9.4	62.2
----	--	--	-----	------

16			13.0	58.6
----	--	--	------	------

T.P.	0.06	958.48	13.15	958.42
------	------	--------	-------	--------

+85

16			3.2	55.3
----	--	--	-----	------

17			4.9	53.6
----	--	--	-----	------

+64 Approx. & Summer St

B.M.	6.98	960.43	5.03	953.45
------	------	--------	------	--------

			2.77	957.66
--	--	--	------	--------

967.67

R.A.
L.G.
C.N.
G.F.

124

Lt.

E

Rt.

66.0 62.6 60.4 58.9 58.9
56 9.0 11.2 12.7 12.7 Drains North on
100 100 200 300 323 = E Lake St

584

132 = F.L.

F.L. from West goes north

547

3.8

12" C.M. = maybe end of sewer

55.4 53.6 50.4 47.5 43.4 41.7

33 49 8.1 11.0 15.1 16.8
200 100 100 200 300 400

Nail in PP. at Summit Pleasant

Nail in PP. Carl + Summer

Sta.

+

π

-

Elev.

Profile Levels

Fulham Street

Sta.	+	π	-	Elev.
B.M	8.67	983.10		(974.43)
1 +00			7.8	75.3
2			7.0	76.1
3			6.2	76.9
4			5.2	77.90
5			4.8	78.3
6			4.6	78.5
7			4.7	78.4
8			4.9	78.2
T.P.	2.16	980.69	4.57	978.53
9			2.7	78.0
10			3.5	77.2
11			4.5	76.2

Ho X Drain

LT

E

EL

Top Iron Fulham + Larpentour Ave.

Spt. Light Pole LT 8100

59.0 64.4

Drains along
Lake St.

21.7	163
200	100

Sta	+	π	-	Elev
		980.69		
12			6.0	74.7
13			8.0	72.7
+31	Approx & Summer St.		8.3	72.4
14			10.2	70.5
15			13.0	67.7
T.P.	0.11	968.31	12.49	968.20
16			3.9	64.4
17			7.6	60.7
18			11.3	57.0
T.P.	0.70	955.43	13.58	954.73
19			2.4	53.0
+77	Approx & Summer St.		5.2	50.2
20			6.1	49.3
21			10.2	45.2

K.A.
L.C.
C.N.
C.L.

127

Lt

2

rt.

65.2

15.5
125

Sta	+	π	-	Elev
		955.43		
21 + 23 =	Int. of Ditches Lt.			
22			13.6	41.8
T.P.	0.52	943.14	12.81	942.62
23			4.3	38.8
24			7.1	36.0
25			8.0	35.1
+50			8.4	34.7
26			7.3	35.8
+10				
+25			5.5	37.6
+37	Approx E Roadway		5.3	37.8
B.M.			6.66	936.48
				(936.52)

L.A.

E

R.A.

36.5

18.9

29

32.8

10.9

26

12.9

30

26.9

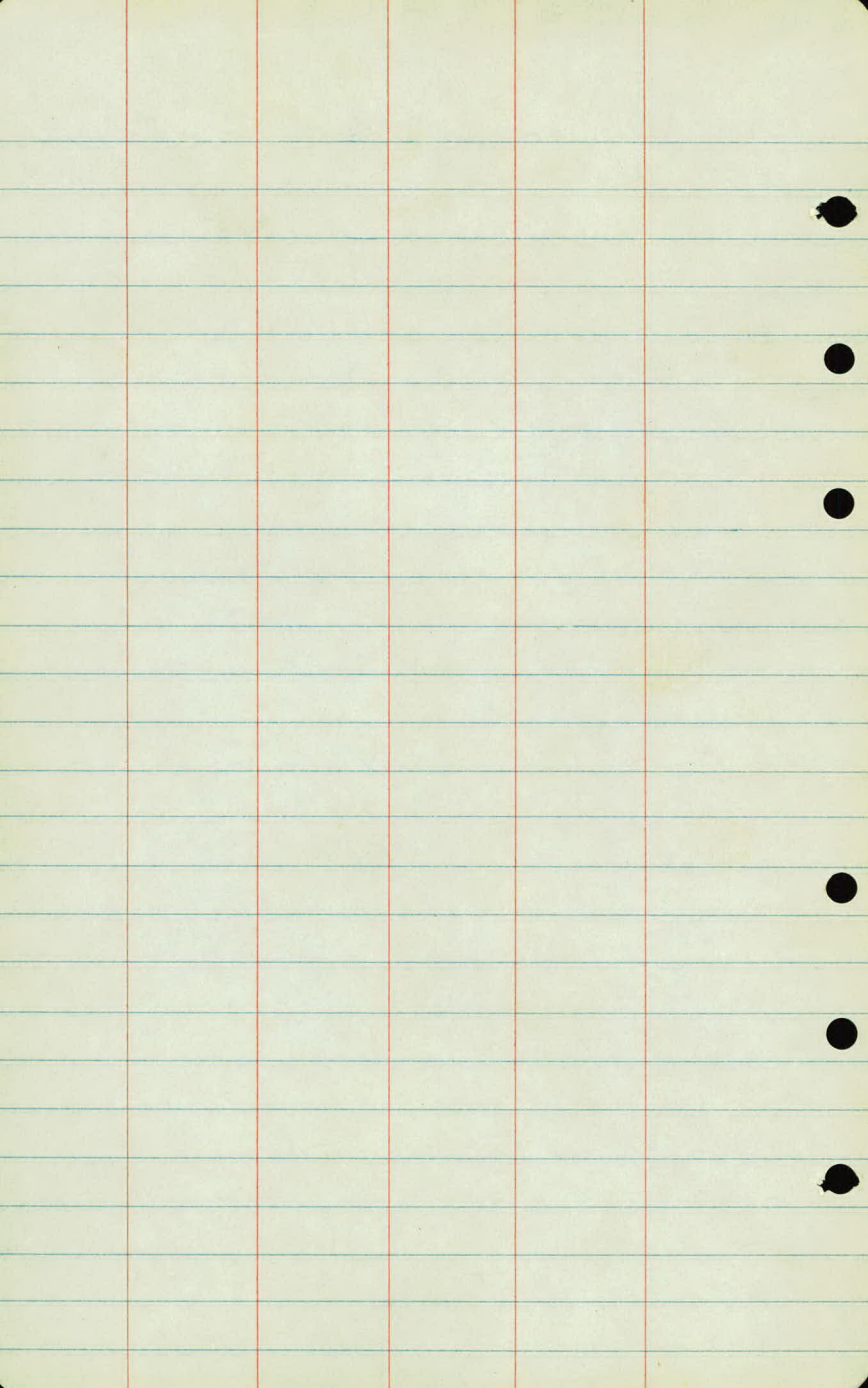
16.2

F.L. Weir Box Runs N.W.

36'

Spt in Light Pole at Rose lawn + Fulham

See 1942 Survey for Drainage



Profile Levels

Cleveland Ave.

No. of Carpenter

Sta	+	π	-	Elev.
B.M.	6.69	986.38		(979.69)
0	+50		5.3	981.1
1			5.1	81.3
2			5.1	81.3
3			5.0	81.4
	+50			
4			4.7	81.7
5			4.1	82.3
6			4.0	82.4
7			4.0	82.4
T.P.	4.62	986.81	4.19	982.19
8			4.6	82.2
9			5.0	81.8
10			5.0	81.8

5-24-44
K.A.
L.C.
C.N.
L.L.

130

Lt. E et.

Top N.W. Cor. Bottom Step on School Ho.

		79.3°	
		71	
		35	
79.9°			
6.5			
35			
	78.3°		
	78.1°		
	77.8°		
	77.5°		
	81	8.3	8.6
	35	100	200
			300

Top N.H. Lt. 6190

Sta.	+	π	-	Elev
		986.81 ✓		
11			5.1	81.7 ·
12			6.0	80.8 ·
13			7.2	79.6 ·
14			8.3	78.5 ·
15			9.6	77.2 ·
T.P.	5.18	986.86 ✓	10.13	976.68 ✓
+25 Pocket Et + Lt.				
16			5.5	76.4 ·
17			5.7	76.2 ·
18			5.5	76.4 ·
19			5.3	76.6 ·
20			5.1	76.8 ·
21			4.0	77.9 ·

Lt

Z

Rt

70.1

11.8
50

72.9

9.0
33

72.9

9.0
44

71.7

10.2
35

70.6

11.3
90 = packet

Sta	+	π	-	Elev.
		981.86 ✓		
22			2.9	79.0 ✓
23			0.9	81.0 ✓
T.P.	6.20	986.96 ✓	1.10	980.76 ✓
24			5.3	81.7 ✓

+64 X Drain Drains West

25			5.2	81.8 ✓
26			4.5	82.5 ✓

+34 E Barclay Ave.			4.2	82.8 ✓
B.M.			4.42	982.54 ✓
				(982.45)

5-25-44
L.A.
L.C.
C.N.
L.L.

132

Lt.

£

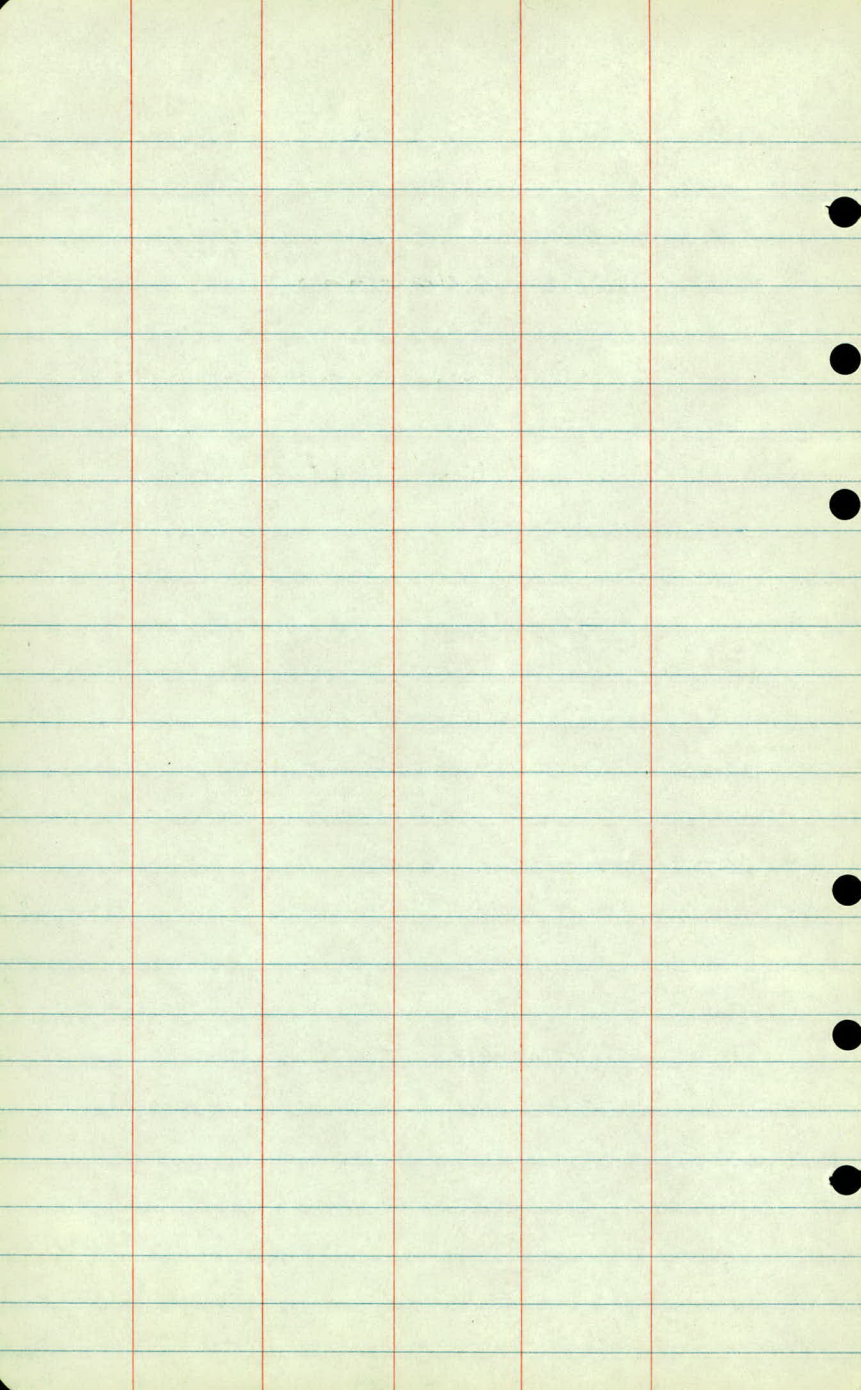
Rt.

760. . .
739. . .

59 80
90 100 = Pocket

Top Mart Roselawn + Cleveland

Pond at S.W. + N.W. Cor. Roselawn + Cleveland



Drainage

Lorpenfeur Ave.

Lt. sta. 57+00

Object Azimuth Dist Rod Elev

H.I. = 982.15

At 57+00 H.I. = 535 above 57+00 El. = 976.8

90°00' = to New Brighton Rd + Carpenter Ave

Ground	55°30'	340'	6.0	976.2	✓
"	32°30'	570'	4.6	77.6	✓
"	270-	301'	5.0	77.2	✓
"	23030	525'	4.8	77.4	✓
"	160-	330'	4.5	77.7	✓
"	130-	492'	4.8	77.4	✓
"	351°30'	303'	4.2	78.0	✓
"	10-	478'	4.3	77.9	✓
"	327°-	360'	4.6	77.6	✓
"	349°-	485'	4.7	77.5	✓
"	338°30'	518'	3.8	78.4	✓
"	328°30'	553'	2.3	79.9	✓
"	314°30'	418'	4.1	78.1	✓
"	343°30'	950'	3.2	79.0	✓
"	347°-	725'	4.3	77.9	✓
"	350°-	935'	4.6	77.6	✓
"	0°00	705'	2.8	79.4	✓
"	356°-	890'	2.8	79.4	✓
"	130-	720 520'	1.6	80.6	✓
"	363°-	904	0.8	81.4	✓
"	23°30'	770'	1.0	81.2	✓
"	10°-	930'	+0.3	82.5	✓
"	17°30'	960	+1.1	83.3	✓

5-25-44

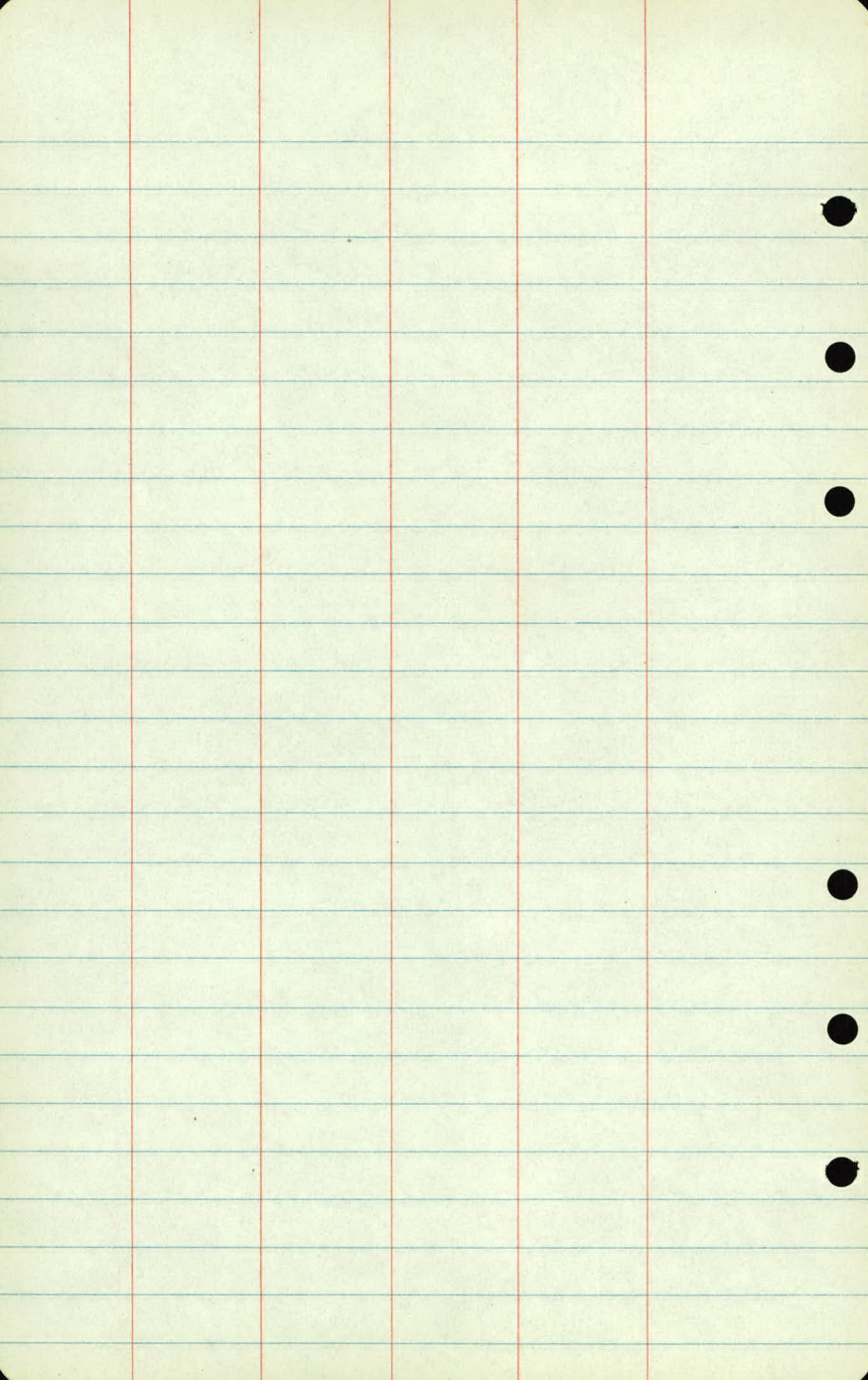
K.A.

L.C.

C.N.

L.L.

134



Profile Levels

Tatum street

Sta	+	π ✓	-	Elev
B.M.	4.95	978.85		(973.9)
0 +50			5.1	973.8
1 +00			4.9	74.0
2			4.8	74.1
+50				
3			4.7	74.2
4			4.6	74.3
5			4.9	74.0
6			4.8	74.1
7			4.5	74.4
8			4.3	74.6
9			4.2	74.7
10			4.2	74.7
T.P.	7.63	981.45 ✓	5.03	973.82 ✓

Lt.

E

Rt.

E. Pav. 70+62

74.0

7.9
50

72.9

6.0
50

73.3

56
100

75.5

34
100

Sta	+	π ✓	-	Elev.
		981.45		
10				
11			6.2	75.3
12			5.5	76.0
13			4.9	76.6
14			4.5	77.0
15			4.2	77.3
16			3.7	77.8
T.P.	665	983.56 ✓	4.54	976.91 ✓
17			5.5	78.1
18			5.0	78.6
19			4.8	78.8
20			4.1	79.5
21			3.0	80.6
T.P.	743	988.28 ✓	2.71	980.85 ✓

Lt

73.8.

7.7
100

E

71.8.

97
50

Rt

71.5.

97
100

71.1.

109
200water drains south
in road ditch

71.7.

59
25

73.8.

9.8
100

69.5.

141
200

66.6.

17.0
300

= Lowland

Sta	+	π ✓	—	Elev.
		988.28		
22			7.0	81.3
+30				
23			5.9	82.4
24			5.0	83.3
25			5.3	83.0
26			7.4	80.9
+34 & Barclay Ave.			7.6	80.7 ✓
I.P.			7.53	980.75

5-25-44
K.A.
L.C.
C.N.
L.L.

138

Lt.

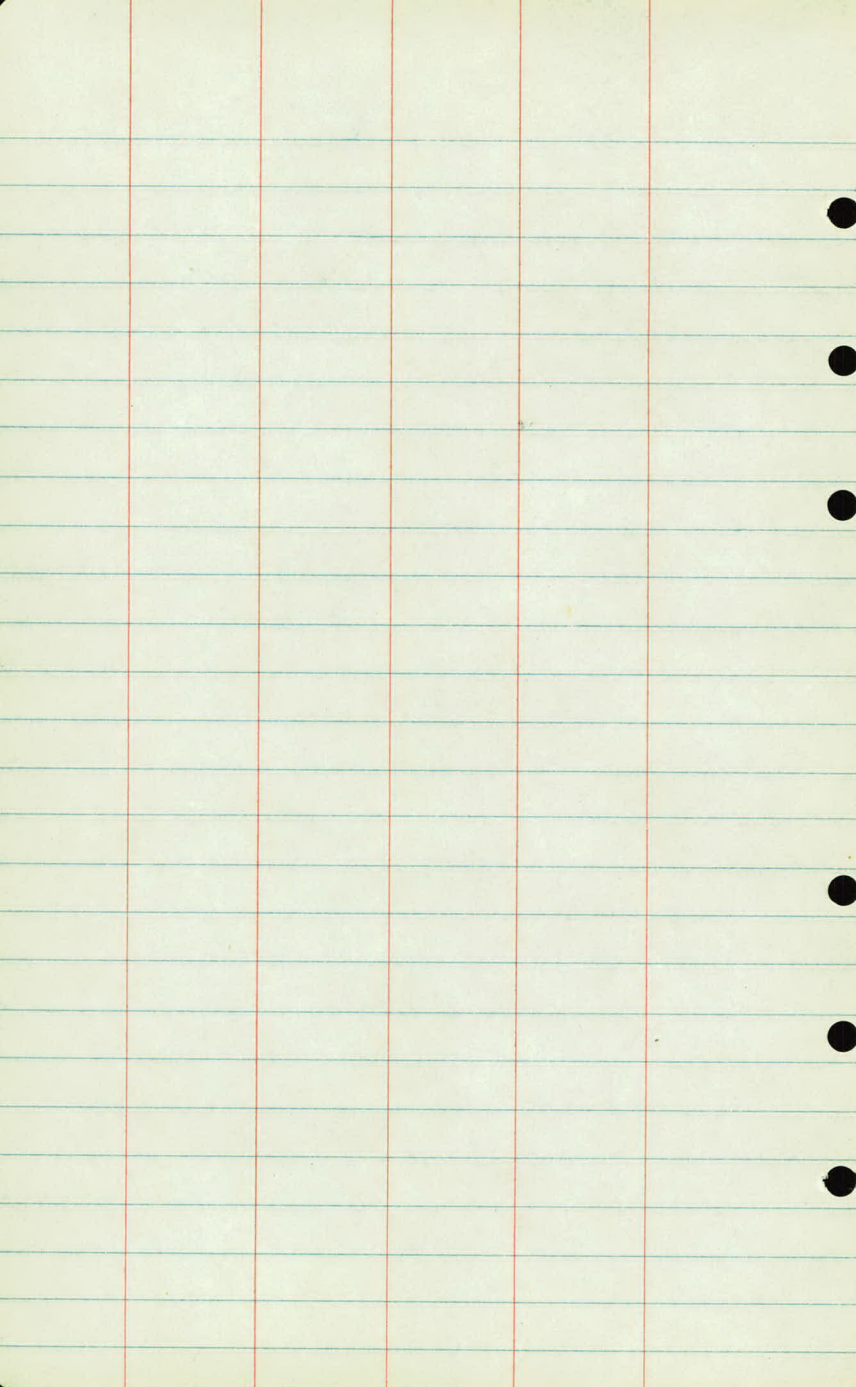
£

Rt.

79.9	79.5	77.8	
84	88	10.5	water drains
50	100	200	South into low land.

Boat Spk at Tatum & Basclawm

Pond at north side of Tatum & Basclawm



Profile Levels

New Brighton Road

Sta	+	π	-	Elev
B.M.	5.68	972.16		(966.48)
0 +00			6.1	966.1.
+50			6.1	66.1.
1			6.0	66.2.
2			5.6	66.6.
3			5.0	67.2.
4			4.4	67.8.
5			4.2	68.0.
6			3.8	68.4.
7			3.0	69.2.
T.P.	8.82	978.18	2.80	969.36
8			8.3	69.9.
9			7.4	70.8.
10			6.8	71.4.

Lt.

E

Et.

Top N.W. Cor. Bottom step Et. 79+40

67.1.
5.1
100

67.0.
5.2
33

67.4.
4.8
45

66.7.
5.5
100

67.8.
10.4
200

67.9.
10.3
100

Sta.	+	π	-	Elev
		978.18		
11			6.0	72.2
12			5.1	73.1
13			4.1	74.1
14			3.1	75.1
15			1.8	76.4
16			0.6	77.6
T.P.	1075	988.31	0.62	977.56
17			9.5	78.8
18			7.9	80.4
19			6.1	82.2
20			4.2	84.1
21			3.3	85.0
22			2.9	85.4

5-25-24

K.A.
L.C.
C.N.
L.L.

141

Lt.

2

PL

71.5

70.4

Drains west

6.7

7.8

200

100

71.9

74.0

Drains N.W.

6.3

4.2

200

100

Sta	+	π ✓	-	Elev.
		988.31		
23		✓	3.8	84.5 ✓
I.P.	1.43	986.01	3.73	984.58
24			3.1	82.9
25			4.8	81.2
26			5.4	80.6
+33			5.6	80.4 ✓
B.M.		✓	6.77	979.24 ✓
I.P.	3.88	986.62	3.27	982.71 (980.75) ✓
I.P.			5.81	980.81 ✓
ok. Rough Check				

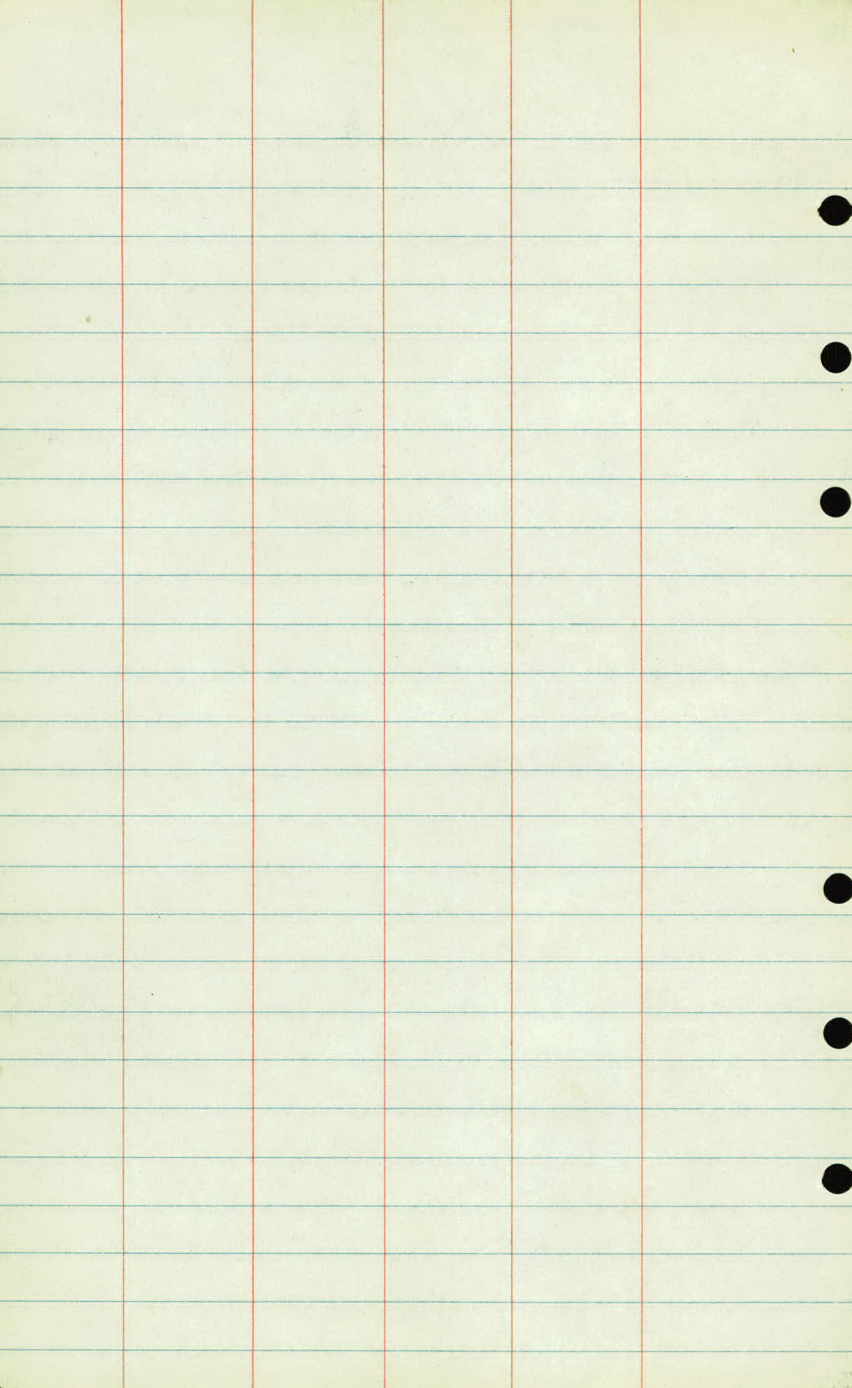
Lt

Q

Rt

Top Conc. Footing End of Fe. S.E. Cor. New Brighton Rd + "A2"

Boat Spk at Totumt Rose lawn.



Profile Levels

Arona Ave.

Larpenteur Ave. No.

Sta	+	π	-	Elev
B.M.	2.78	957.50		(954.72)
0 +00			6.2	951.3
+50			6.3	51.2
1			6.2	51.3
2			5.2	52.3
3			5.0	52.5
+ 82 Approx. Crawford			4.7	52.8
TP			4.62	952.88
4			4.7	52.8
5			4.8	52.7
6			4.1	53.4
T.P.	7.18	961.18	3.50	954.00
7			7.0	54.2
8			6.6	54.6
9			6.2	55.0

5-25-44
K.A.
L.C.
C.N.
L.L.

144.

lt

¢

ret

Top Hyd N.E. Cor Arona + Larp Ave.
= ¢ Larpenteur Ave.

Nail in PPMW Cor Crawford + Arona

Sta	+	π ✓ 961.18	-	Elev.
10			6.1	55.1
11			5.5	55.7
12			5.3	55.9
T.P.			1.46	959.72
13			4.7	56.5
+18			4.7	56.5
14			5.8	55.4
15			7.2	54.0
16			8.1	53.1
17			9.0	52.2
18			10.6	50.6
19			10.9	50.3
+75			10.4	50.8
T.P.			7.43	953.75

lt

c

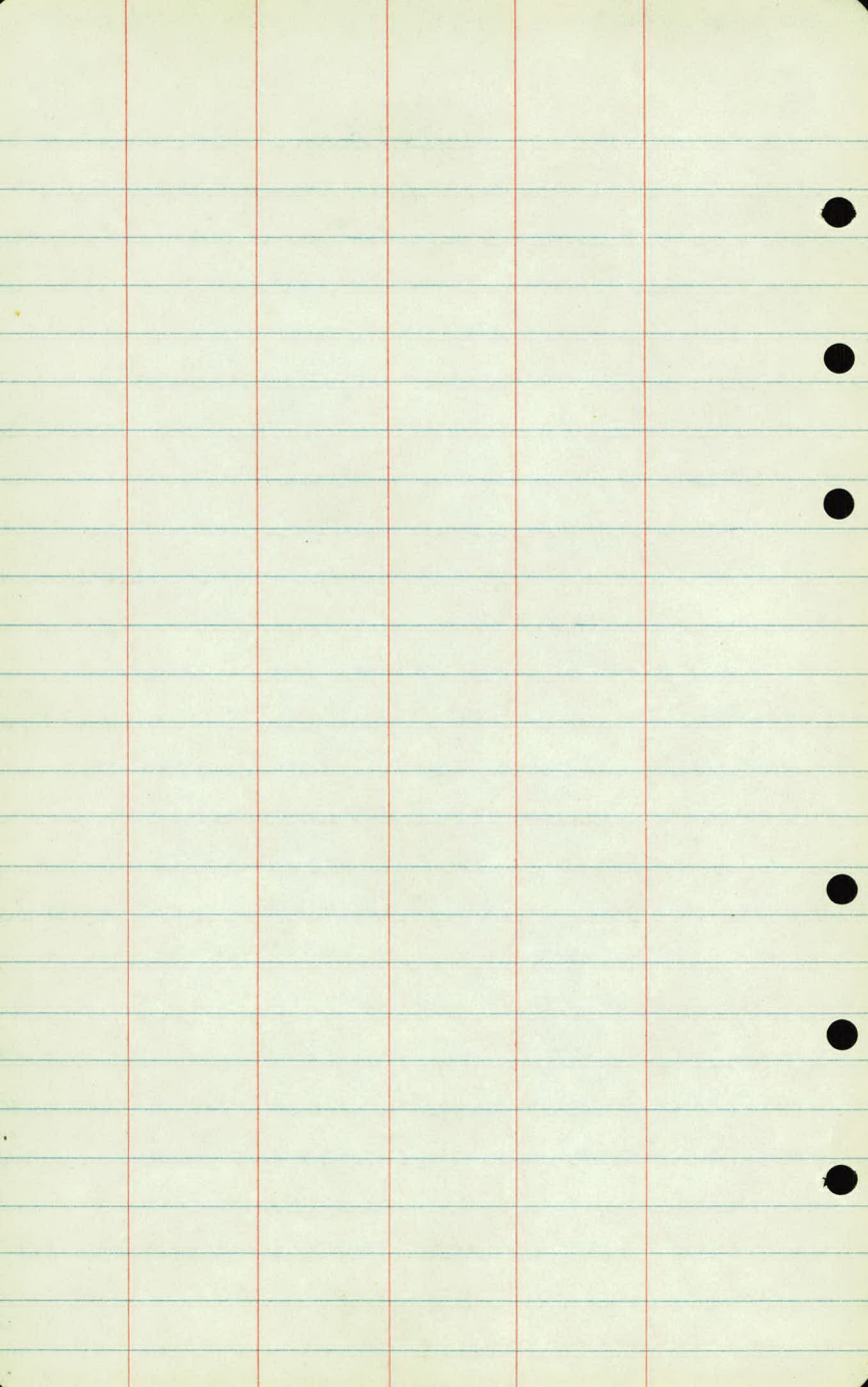
rt

Top Hyd S.W. Cor. Garden + Arona

Approx. c Garden Ave.

Approx. c. Buggles St.

Top Hyd Buggles + Arona



Profile Levels

Simpson St.

Sta	+	π	-	Elev
T.P.	4.73	957.61		952.88
0 +00			4.7	52.9
+15			4.5	53.1
+60			5.0	52.6
1			4.8	52.8
2			4.7	52.9
3			4.6	53.0
4			4.5	53.1
+50			4.1	53.5
5			3.5	54.1
T.P.	4.08	958.72	2.97	954.64
+50			3.9	54.8
6			2.8	55.9
+50			1.9	56.8

5-25-44

K.P.

L.G.

C.N.

L.L.

147

Lt.

2

Rt.

Nail in P.P. N.W. Cor Crawfordt Arena.

Approx. 2 Simpson & Crawford

Sta	+	π ✓	-	Elev.
-----	---	---------	---	-------

95872

7			1.6	57.1
---	--	--	-----	------

+50			2.0	56.7
-----	--	--	-----	------

8			3.2	55.5
---	--	--	-----	------

9			5.9	52.8
---	--	--	-----	------

+16 = gutter			6.2	52.5
--------------	--	--	-----	------

+34			5.8	52.9
-----	--	--	-----	------

10			6.0	52.7
----	--	--	-----	------

11			6.8	51.9
----	--	--	-----	------

12			6.9	51.8
----	--	--	-----	------

13			7.2	51.5
----	--	--	-----	------

T.P.	304	95516 ✓	6.60	952.12 ✓
------	-----	---------	------	----------

14			4.3	50.9
----	--	--	-----	------

15			4.8	50.4
----	--	--	-----	------

+91			5.1	50.1
-----	--	--	-----	------

T.P.			1.44	953.72 ✓
------	--	--	------	----------

95375

lt.

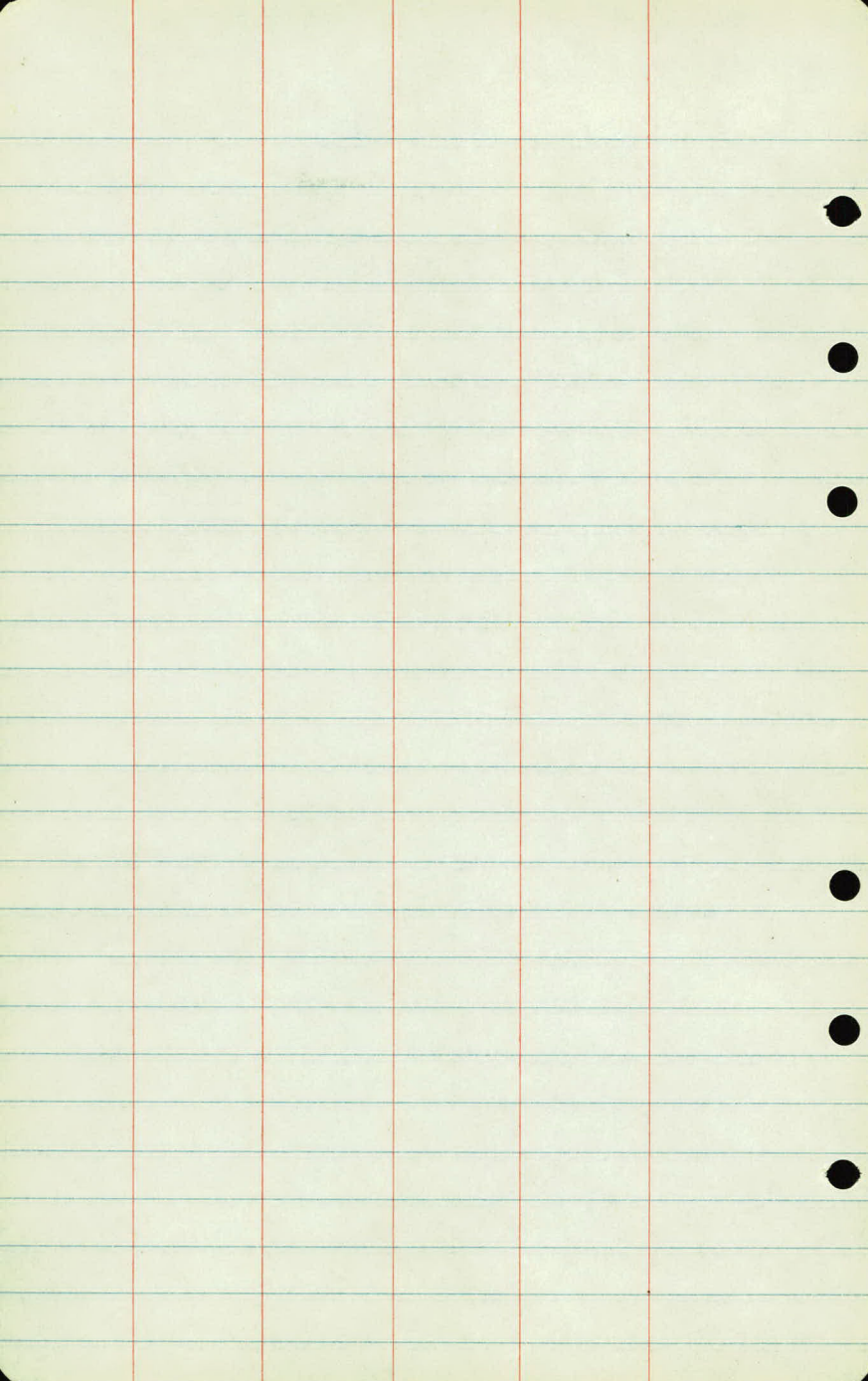
e

rt

Approx. E Garden Ave.

Approx. E Ruggles St.

Top Blvd S.W. Cor. Ruggles + Arona



Profile Levels

Pascal Ave

Sta	+	π	-	Elev
B.M.	2.37	955.62		955.25
B.M.			2.77	952.85
0 +00			4.9	50.7
+50			5.3	50.3
1			4.8	50.8
2			4.0	51.6
3			3.8	51.8
+80			3.3	52.3
4			3.2	52.4
5			2.2	53.4
T.P.	12.36	965.51	2.47	953.15
6			2.8	56.7
7			5.8	59.7
8			4.4	61.1

Lt

E

Rt

SW Cor. Lower step of H₆ at 1499 Corp AveTop S.E. Cor Lower Step Front of H₆ at 1463 Corp Ave

50.5	50.9	48.3	49.6	50.6
51	47	73	60	50
27	30	100	150	200

Approx. E Crawford Ave

Sta.	+	π ✓	-	Elev.
		965.51		
9			2.6	62.9.
	+50		1.9	63.6.
10			2.3	63.2.
	+50		5.0	60.5.
11		✓	9.1	56.4.;
T.P.	0.25	956.92	8.84	956.67.
12			3.1	53.8.
	+70		5.3	51.6.
13			5.5	51.4.
	+18		5.6	51.3.
	+60		5.9	51.0.
14		✓	6.6	50.3.;
T.P.	2.68	952.35.	7.25	949.67.
15			40	48.4.

5-26-44
K.A.
L.G.
C.N.
C.F.

151

Lt.

2

Bl.

50.9	48.5	46.4	47.2	49.1	
6.0	8.4	10.5	9.7	7.8	Church
30	50	100	150	167	Yard.

46.7	46.0	45.1	49.2	
102	119	118	77	Church
35	100	153	170	Yard

= Approx. 2 Garden Ave.

46.2	45.2	46.9
107	117	10.0
40	100	200

Sta.	+	π	-	Elev.
		952.35		
15	150		4.8	47.6
16			5.2	47.2
17			5.0	47.4
18			4.5	47.9
19			3.8	48.6
	+76		3.2	49.2
20	Approx. X Drain		3.0	49.4
21			2.7	49.7
T.P.	6.09	955.87	2.57	949.78
22			5.6	50.3
23			5.9	50.5
24			5.0	50.9
25			4.5	51.4

Lt

E

Et

Londoni betve Pascal + Holten

42.9.	40.9.	40.8.
9.5	11.5	11.6
30	100	200

44.6.	48.4.	48.4.	49.3.
7.8	4.0	4.0	3.1
20	28	100	200

E
Ditch

Approx E Ruggles St.

Water Drains From

West to south

46.7.	46.4.
5.7	6.0
33	18
FL 18' Long Culv.	FL 18' Long culv

49.4.	49.4.	49.1.
3.0	3.0	3.3
100	100	200

52.1.	49.4.	48.9.
3.8	6.5	7.0
100	100	200

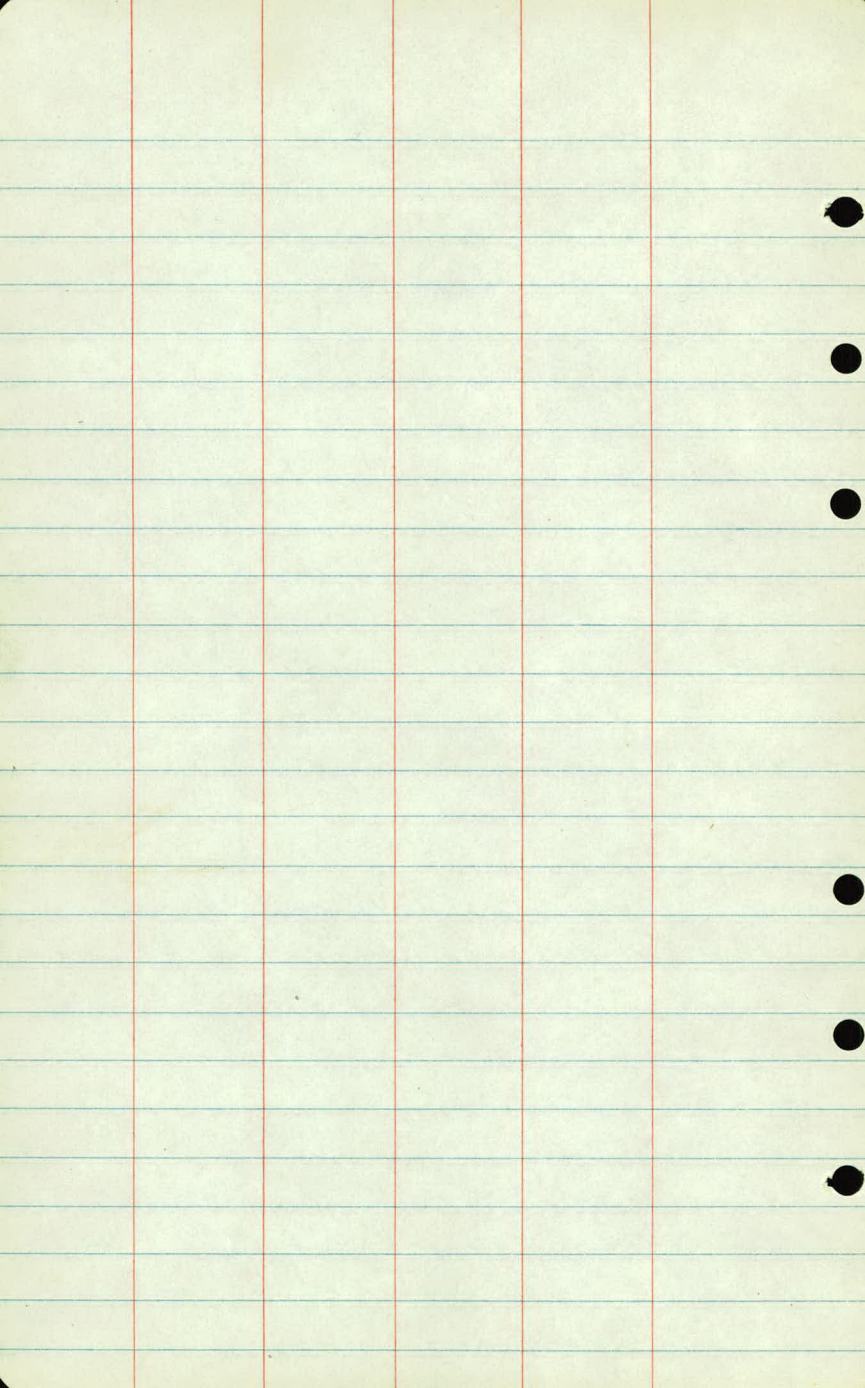
Sta	+	π	-	Elev
		955.87		
26			3.4	52.5
T.P	5.20	957.72	3.35	952.52
+36			45	53.2
B.M.			4.64	953.08
				953.15

Lt

E

Rt

Top S.W. Cor Lower step on Ho. at 1451 Rose lawn Ave.



Profile Levels

Holton Ave

Sta	+	Σ	-	Elev
B.M.	2.10	954.95 ✓		(95283)
0 +00			5.3	49.7 ✓
1			5.4	49.6 ✓
2			5.0	50.0 ✓
3			5.1	49.9 ✓
4			4.7	50.3 ✓
5			4.6	50.4 ✓
6			4.5	50.5 ✓
7			4.3	50.7 ✓
I.P.	2.46	953.36 ✓	4.05	950.90 ✓
8			3.0	50.4 ✓
9			3.6	49.8 ✓
10			4.4	49.0 ✓
11			4.8	48.6 ✓

5-26-44
K.A.
L.C.
C.N.
L.L.

155

Lt

E

Rt

Top S.E. Cor Lower Step Front of Hb at 1463 Corp. Ave
= E Corp Ave.

48.5' 50.2'
65 48
100 50

47.0' 46.4' 44.2'
80 86 10.8
50 100 200

SLOPES S.E.

49.3' 49.0' 49.5'
57 60 5.5
50 100 175

53.6'
40.2
100

53.4'
0.0
100

48.8' 47.7' 47.1'
46 57 63
200 100 50

46.5' 47.6' 51.2'
69 58 22
50 100 175

Sta	+	π ✓	-	Elev.
		953.36		
12			4.9	48.5
13			5.2	48.2
+21			5.2	48.2
14			5.3	48.1
15			5.3	48.1
16			5.8	47.6
+20 X Drain Drains West ✓				
T.P.	5.94	953.55	5.75	947.61
17			5.7	47.9
18			5.1	48.5
+50				
19			5.0	48.6
20			4.6	49.0

Lt

E

Rt

50.5.
29
100

47.0.
47.5.
64 59
50 100

Approx. 4. Garden Ave.

47.1.
45.9.
6.3 7.5
200 100

Lowland

41.1.
42.3.
40.0.
41.0.
50.0.
12.3 11.1 13.4 12.9 3.4
200 65 62 30 100

48.3.
5.3
100

47.8.
5.8
250

49.6.
40
35

48.8.
48
100

47.6.
47.0.
47.0.
47.1.
60 6.6 6.6 6.5
100 200 300 400

Sta	+	Σ	-	Elev
-----	---	----------	---	------

953.55

21			4.5	49.1
----	--	--	-----	------

22			4.4	49.2
----	--	--	-----	------

23			4.0	49.6
----	--	--	-----	------

T.P.	6.58	954.42	3.71	949.84
------	------	--------	------	--------

24			6.2	50.2
----	--	--	-----	------

25			5.6	50.8
----	--	--	-----	------

26			4.9	51.5
----	--	--	-----	------

+37			4.5	51.9
-----	--	--	-----	------

B.M.			3.36	953.06
------	--	--	------	--------

953.15

T.P.	3.17	955.28	4.31	952.11
------	------	--------	------	--------

			0.61	954.67
--	--	--	------	--------

954.76

131

Lt

E

Rt.

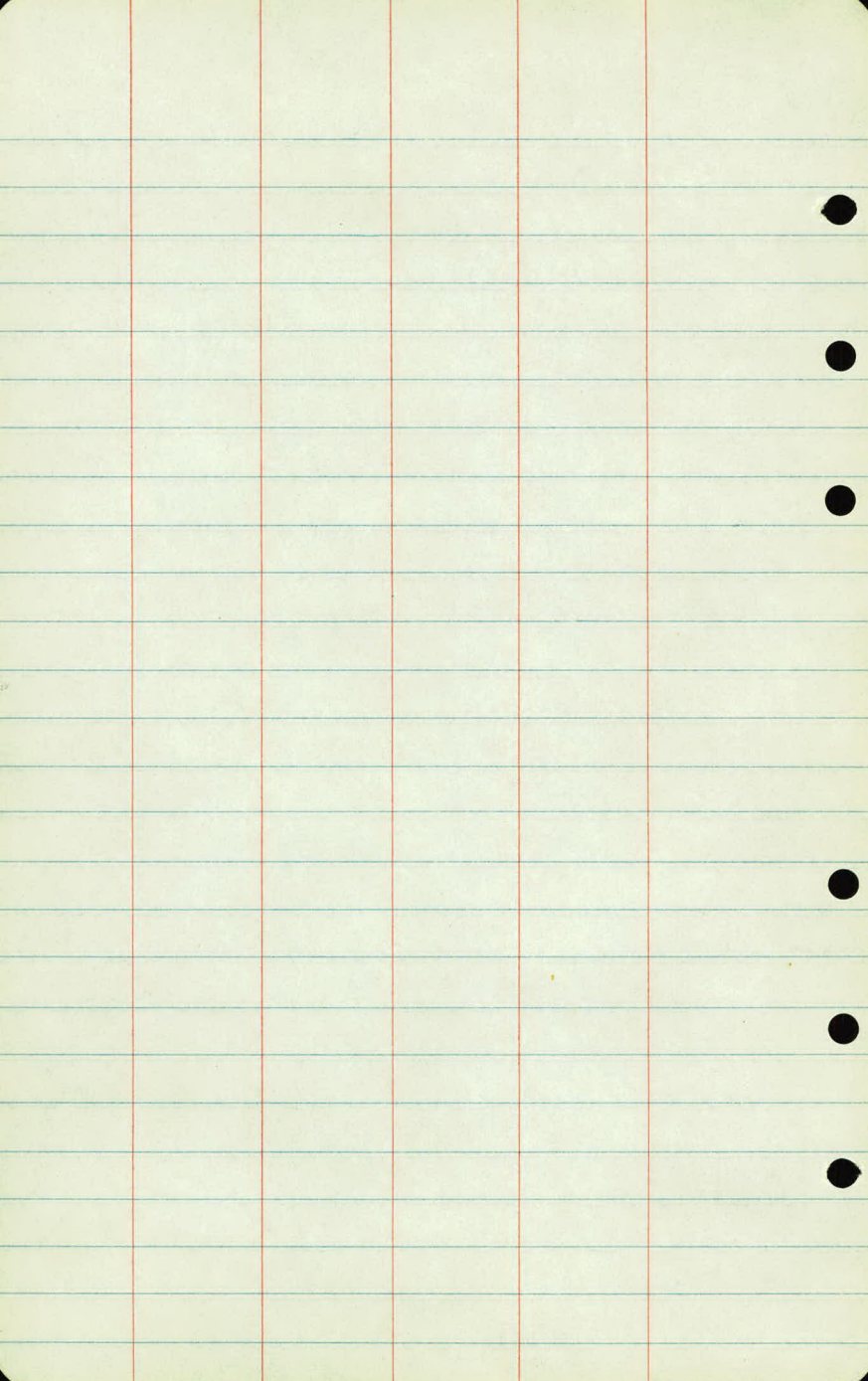
493.	481.	480.	490.	496.
4.3	5.5	5.6	4.6	4.0
200	100	50	100	200

49.6.	49.7.
6.8	7.7
100	200

Top S.W. Cor Lower step on Ho at 1451 Roselawn Ave.

RR Spk in P.P.N.W. Cor. Roselawn & Harding

959.76
<u>0.61</u>
955.37
<u>3.17</u>
952.20
<u>4.31</u>
956.51
<u>3.36</u>
953.15



Profile Levels

Albert Ave.

Sta	+	π	-	Elev
B.M.	3.51	950.31		946.8

0 +00

+50			4.3	46.0
-----	--	--	-----	------

1			5.3	45.0
---	--	--	-----	------

2			5.0	45.3
---	--	--	-----	------

+30

3			4.8	45.5
---	--	--	-----	------

+20

+32

4			4.4	45.9
---	--	--	-----	------

5			3.1	47.2
---	--	--	-----	------

I.P.	8.83	956.22	2.92	947.39
------	------	--------	------	--------

6			7.3	48.9
---	--	--	-----	------

7			5.9	50.3
---	--	--	-----	------

5-26-44
 J.C.A.
 L.C.
 C.N.
 C.F.
 L.L.
 Lt.

159

Q

Et

Q Pav Lorp Albert.
 = Q Lorp Ave.

43.7.	44.2.
66	91
175	50

Lowland

	42.9.	42.7.
	74	76
	100	50
46.9.	46.9.	46.1.
34	34	42
170	100	50

High ground on both
 sides of road

Sta	+	π ✓ 956.22	-	Elev.
8			5.2	51.0 .
9			4.9	51.3 .
10			5.2	51.0 .
11			6.3	49.9 .
12			7.3	48.9 .
+50			7.8	48.4 .
13			8.3	47.9 .
+20			8.6	47.6 . ✓
T.P.	0.33	951.42 ✓	5.13	951.09 ✓
B.M.			6.02	945.40 (945.43)

Lt.

E

Rt.

High ground both
sides of road.

46.6.	46.4.
96	98
50	100

Top Hyd Garden + Albert

Top Hyd S.W. Cor. Garden + Homline

Sta	+	π	-	Elev.
B.M	2.83	952.80		<u>949.97</u>
0 +00			7.9	
1			7.2	
2			5.6	
3			4.5	
4			4.6	
5			6.4	
6			8.5	
7			9.8	
I.P.	6.73	950.12	9.91	943.39
8			7.8	
9			8.4	
10			9.0	
11			8.0	

Profile Levels

Hamline Ave.

Larpenteur Ave. No.

Sta.	+	π	-	E/cv.
B.M.	2.83	952.80		(949.97)
0 +00			7.9	44.9
1			7.2	45.6
2			5.6	47.2
3			4.5	48.3
4			4.6	48.2
5			6.4	46.4
6			8.5	44.3
7			9.8	43.0
T.P.	6.73	950.12	9.41	943.39
8			7.8	42.3
9			8.4	41.7
10			9.0	41.1
11			8.0	42.1

5-26-44

162

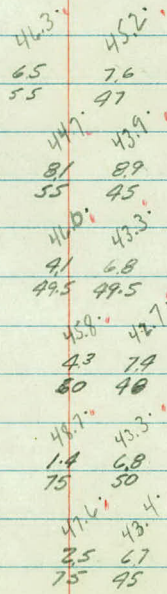
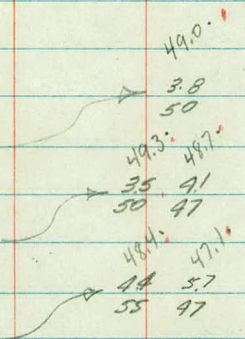
Lt.

E

Rt.

Top S.E. Cor Bottom Step Front Ho. 1707 Hamling Ave.

= E Larp. Ave.



Sta	+	π ✓	-	Elev
		950.12 ✓		
12			7.7	42.4 ✓
13			7.9	42.2 ✓
+ 21			7.8	42.3 ✓
B.M.	3.65	949.13 ✓	4.75	945.37 ✓
14			6.4	42.7 ✓
15			5.5	43.6 ✓
16			5.1	44.0 ✓
17			4.9	44.2 ✓
18			4.5	44.6 ✓
19			3.5	45.6 ✓
20			2.1	47.0 ✓
21			0.6	48.5 ✓
T.P.	8.05	956.38 ✓	0.80	948.33 ✓
22			6.1	50.3 ✓

(945.48)

LH

E

RH

486.	44.0.
1.5	6.1
75	45
460.	43.5.
91	6.6
60	45

Top Hyd. SW Cor. Garden of Hemlock

sta + π ✓
956.39

23 5.3 51.1 !

24 5.0 51.4 !

25 4.9 51.5 !

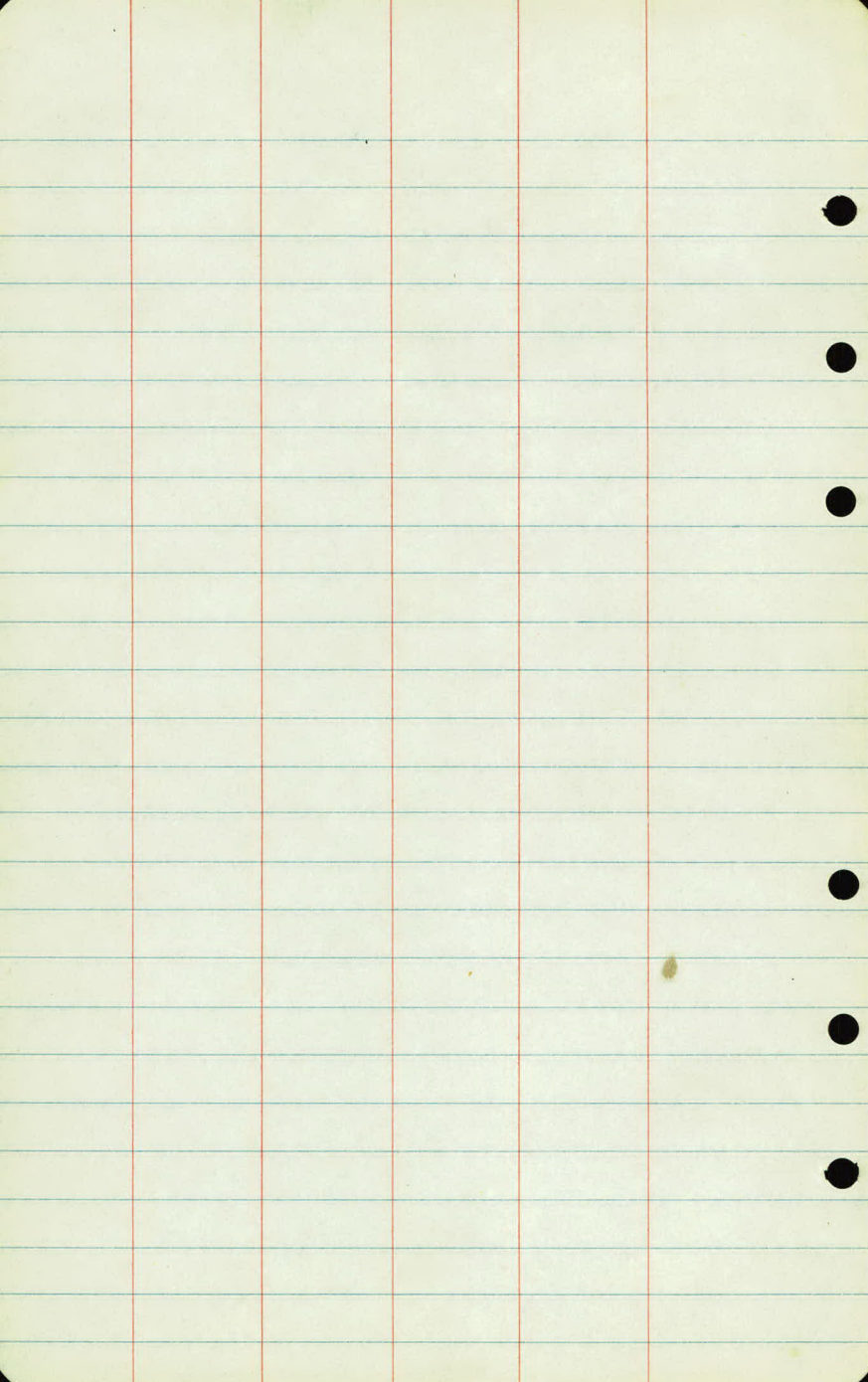
26 4.2 52.2 !

+44 3.4 53.0 ! ✓

B.M. 1.64 954.74 (954.76)

51.1	51.1
5.3	5.3
100	30

R.R. Spc in P.R. N.W. Co. Rosebud + Hamline



Profile Levels

Fry St

Sta	+	-	Elev
B.M.	467		955.1
0	+00 = 96+44	4.6	55.2
	+10	4.6	55.2
	+20	4.4	55.4
	+40	5.4	54.4
1		5.2	54.6
	+50	4.7	55.1
2		4.9	55.4
3		2.9	56.9
4		1.1	58.7
5			
6	Cont. to raise going north		

6-2-44
K.A.
L.C.
C.F.
C.N.
C.L.
Lt.

4

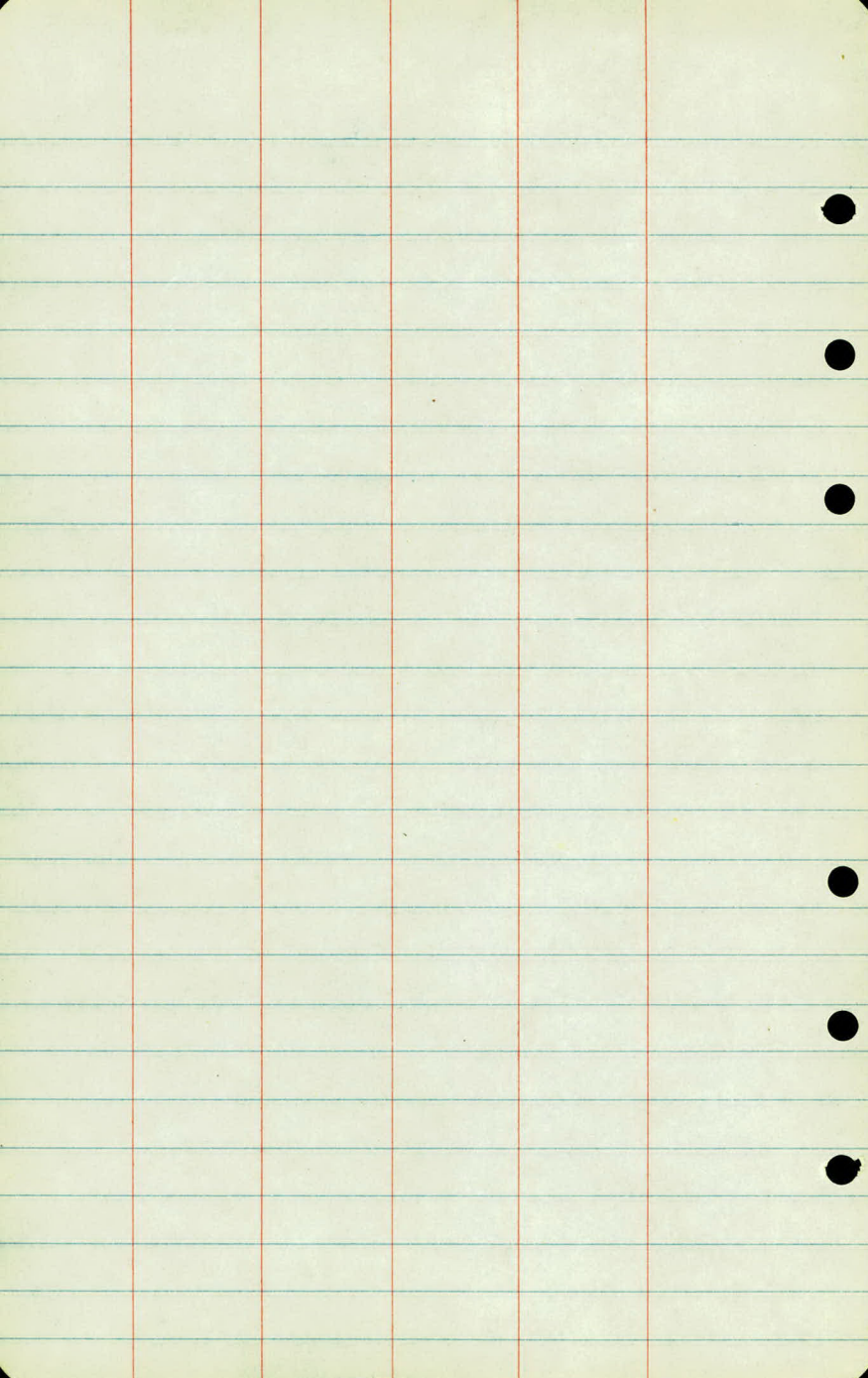
104

6 Pav sta 97+00

6.0
50

5.8
50

5.2
50



Profile Levels

St Mary St.

Sta	+	-	Elev.
B.M.	5.00		956.0
0+00 = 100+05		4.9	561
+10		5.0	56.0
+45		4.8	56.2
1		3.5	57.5
2		2.4	58.6
3		0.9	60.1
4		1.06	61.6
5			

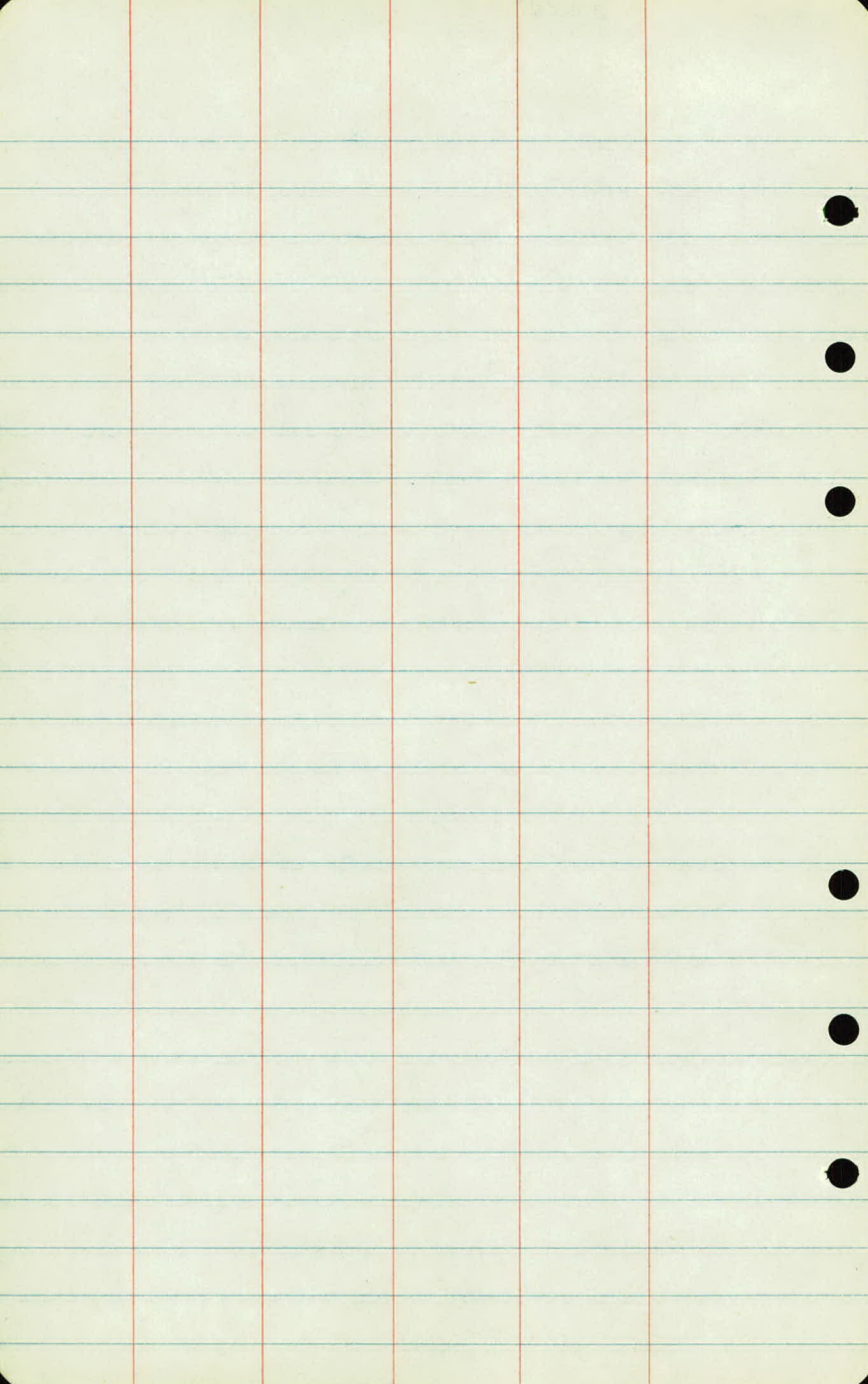
G-2-44
K.A.
L.C.
C.N.
C.F.
L.L.

Lt.

2

Et.

E. Pav sta 100+00



Profile Levels

Aroma Ave.

So. of Larpenbur.

Sta.	+	π	-	Elev
B.M.	3.63	955.03		951.40
0 100			3.63	51.40
110			3.7	51.3
150			4.2	50.8
1			4.6	50.4
2 120			5.4	49.6
3			6.1	48.9
140			6.2	48.9
4			6.3	48.7
5			6.9	48.1
6			7.5	47.5
160			8.4	46.6
7			8.1	

1-2-44
K.A.
L.G.
C.F.
C.N.
C.C.

Lt.

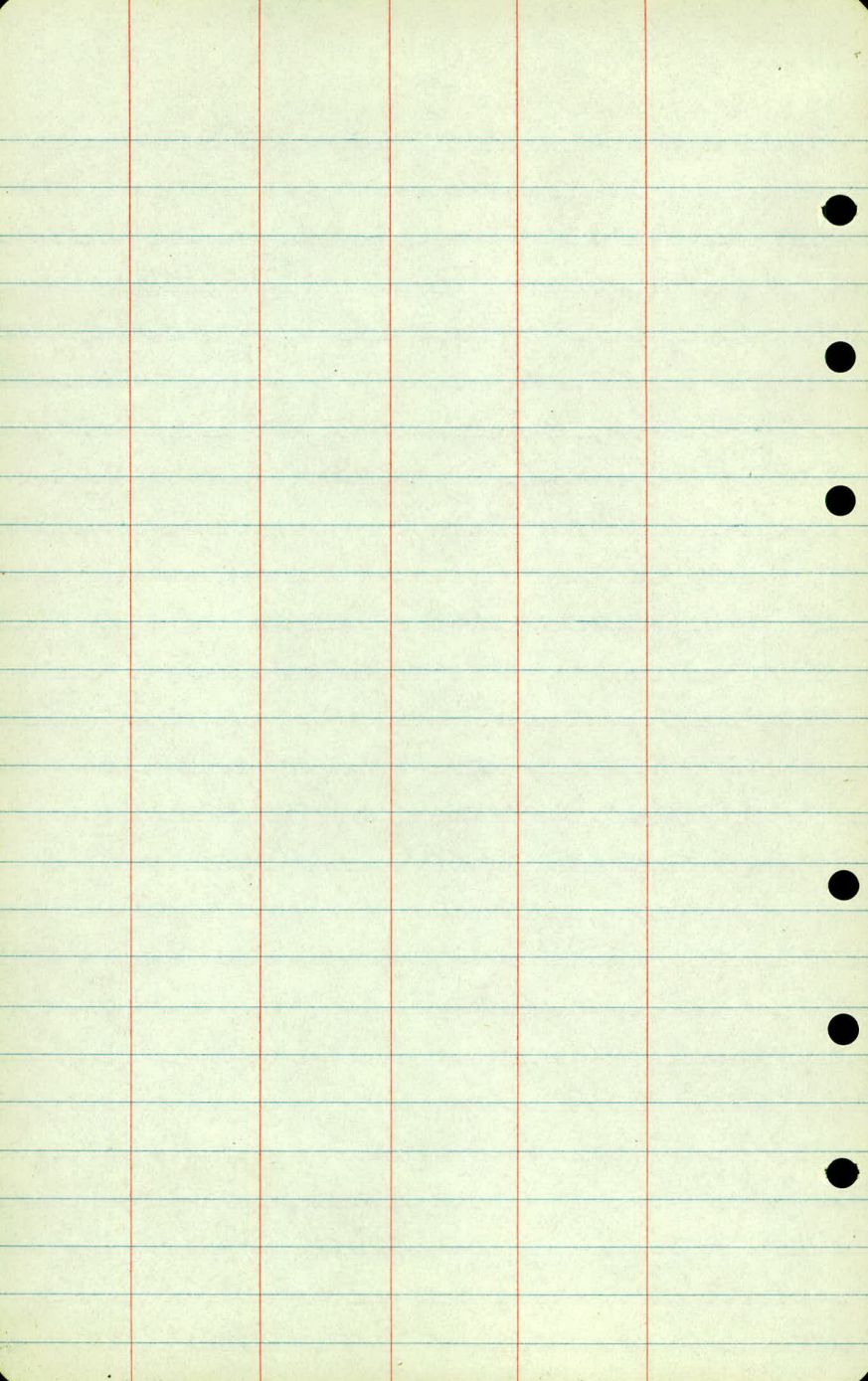
E

Pl.

E. Pav. Arona + Larpenteur Aves

Approx. E California Ave.

Approx. E Idaho Ave. Drains West



Profile Levels

Pascal Ave.

So. of L'Orpenteur

Sta	+	π	-	Elev
B.M.	4.08			956.7
0	+00		4.08	50.7
	+10		4.2	50.6
	+50		5.1	49.7
1			5.3	49.5
	+80 Approx & Alley		3.9	50.9
2			3.4	51.4
3			1.2	53.6
	+38		0.7	54.1
4			0.8	54.0
5			1.6	52.2
6			2.1	52.7

G.E-44
K.A.
L.C.
C.F.
C.N.
L.L.

Lt

E

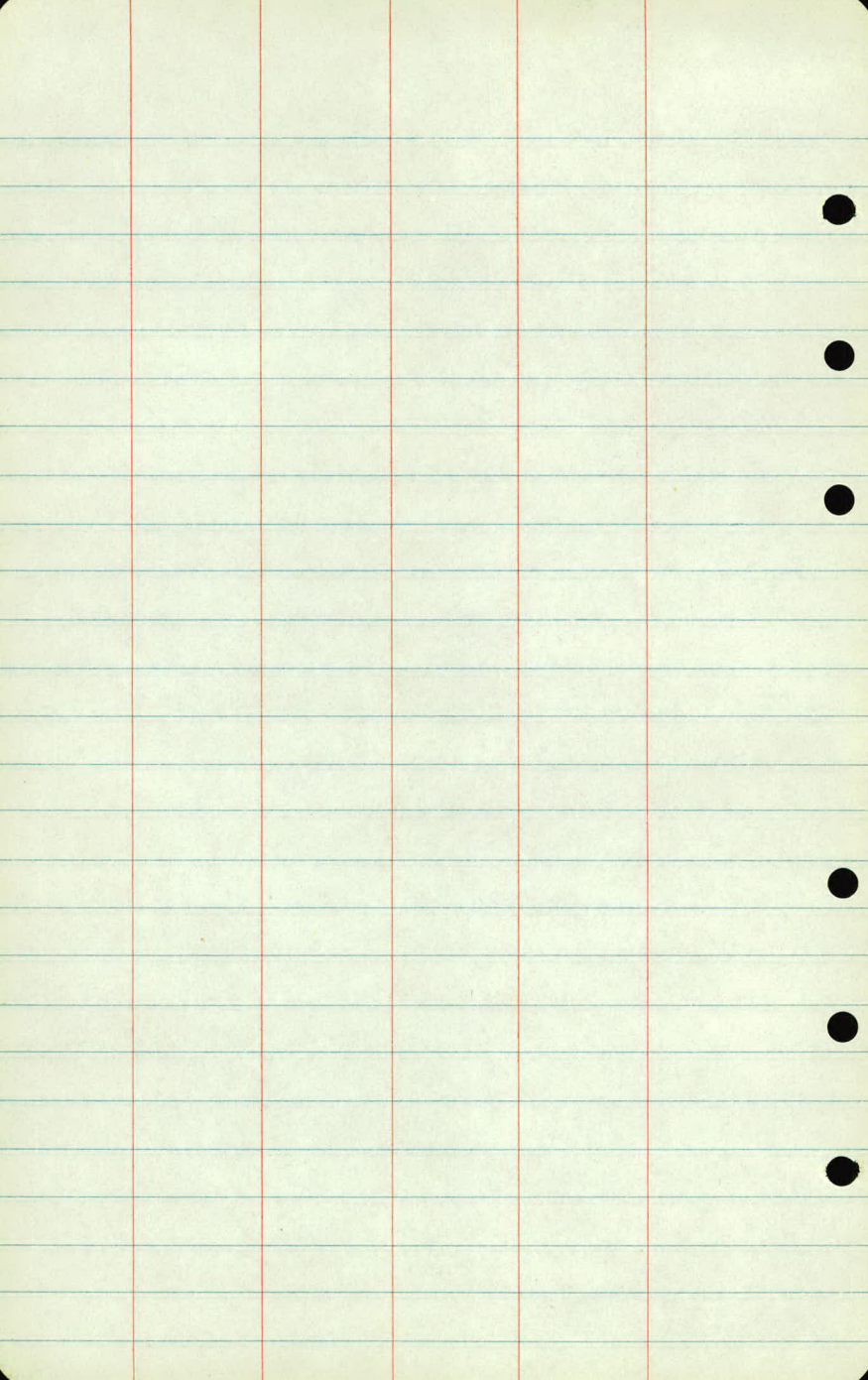
Et

& Pav. Pascal + Larpenteur Ave's.

Drains East

1.3	1.5	3.1
250	200	100

Approx & California Ave.



Profile Levels

Albert St.

So. of Larpenfeur

Sta	+	π	-	Elev
B.M.	3.65			946.8
0 100			3.65	468
110			3.7	468
150			4.4	461
1			4.8	45.7
180 Approx. E. Alley			5.1	45.4
2			5.2	45.3
3			5.5	45.0
138 Approx. E. California			5.6	44.9
4			5.1	45.4
5			3.9	46.6
6			2.6	47.9

6-2-44
K.A.
L.C.
C.F.
C.M.
L.L.

Lt.

2

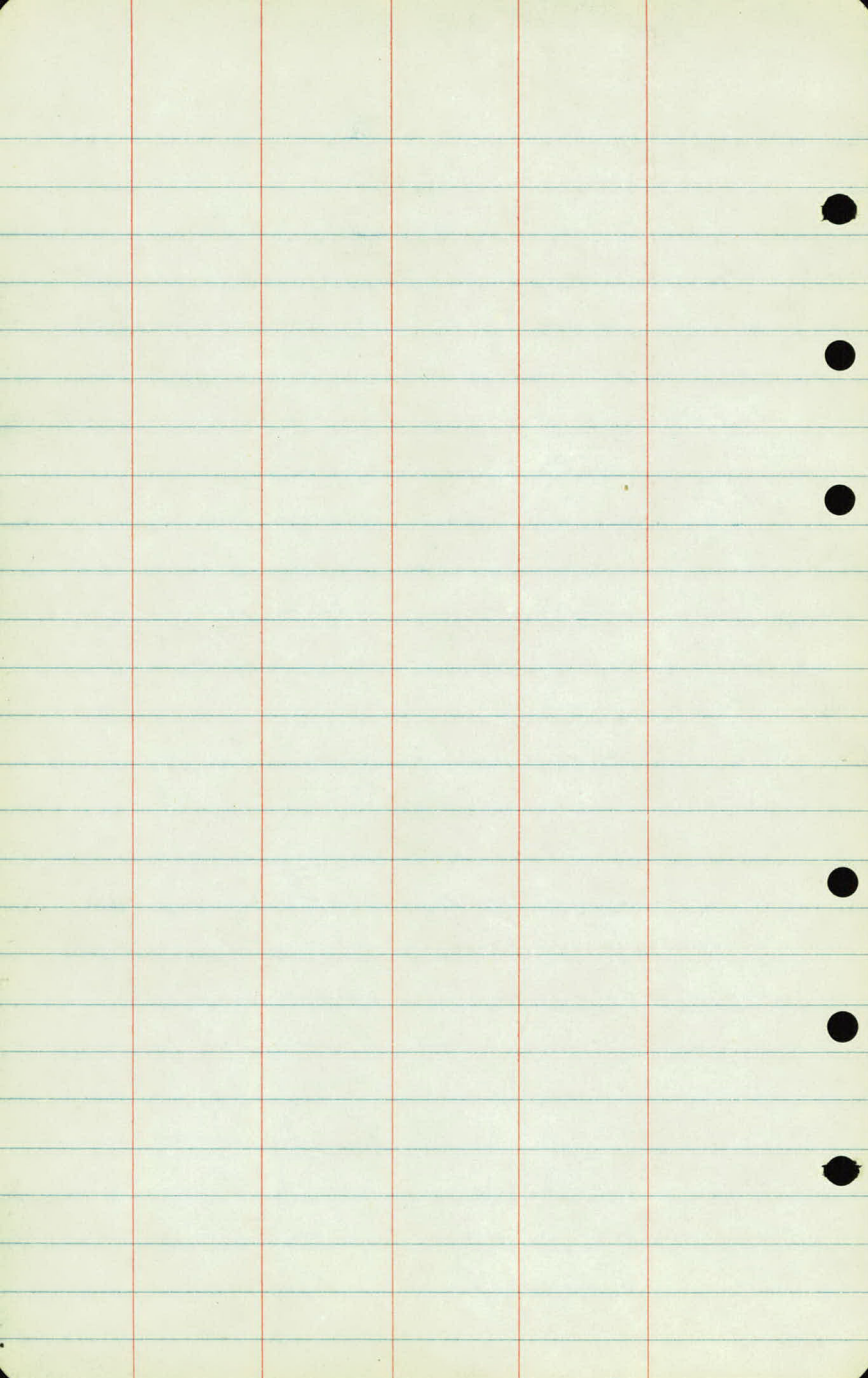
Et.

2 Pav. Abert + Larpenteur-Aves

52	56	64	62	33	1.2	0.0	Drainage
400	300	200	100	100	200	275	From East.

Drains East. 59 56
200 50

Drainage From West.



Profile Levels

Hamling Ave.

So. of Carpenter

Sta.	+	π	-	Elev.
B.M.	496			944.95
0 +00			4.96	45.0
+10			5.2	44.9
+50			5.1	44.8
1			5.0	44.9
+80 Approx. to Alley			4.4	45.5
2			4.5	45.4
3			5.3	44.6
+38			5.9	44.5
4			6.8	43.1
5			7.9	42.0
6			10.0	39.9

62-44
K.A.
L.C.
C.F.
C.H.
L.L.

Lt.

E

Rt.

Top Meat Hamling + Larp Area

4.09
S.W. 30'

4.4 52 50
36 100 200

3.78
S.W. 30'

4.69
S.W. 30'

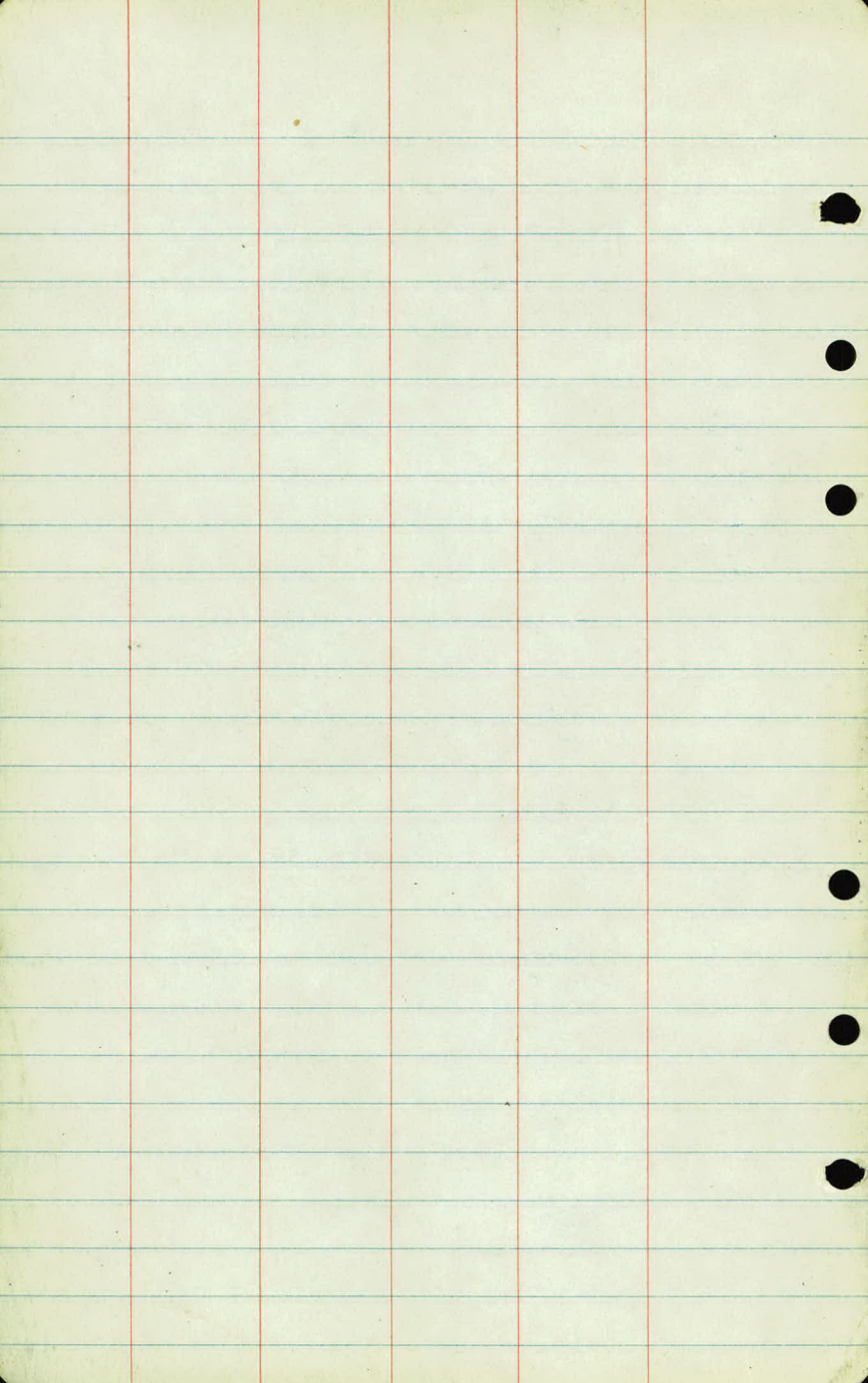
Approx 2 California

6.1 58
100 200

6.30
S.W. 30'

7.72
S.W. 30'

10.0
S.W. 30'



6-2-44

Elev. of water in Pothole

B.M. Top Mark at Fernwood + Lorpenbur Arc.

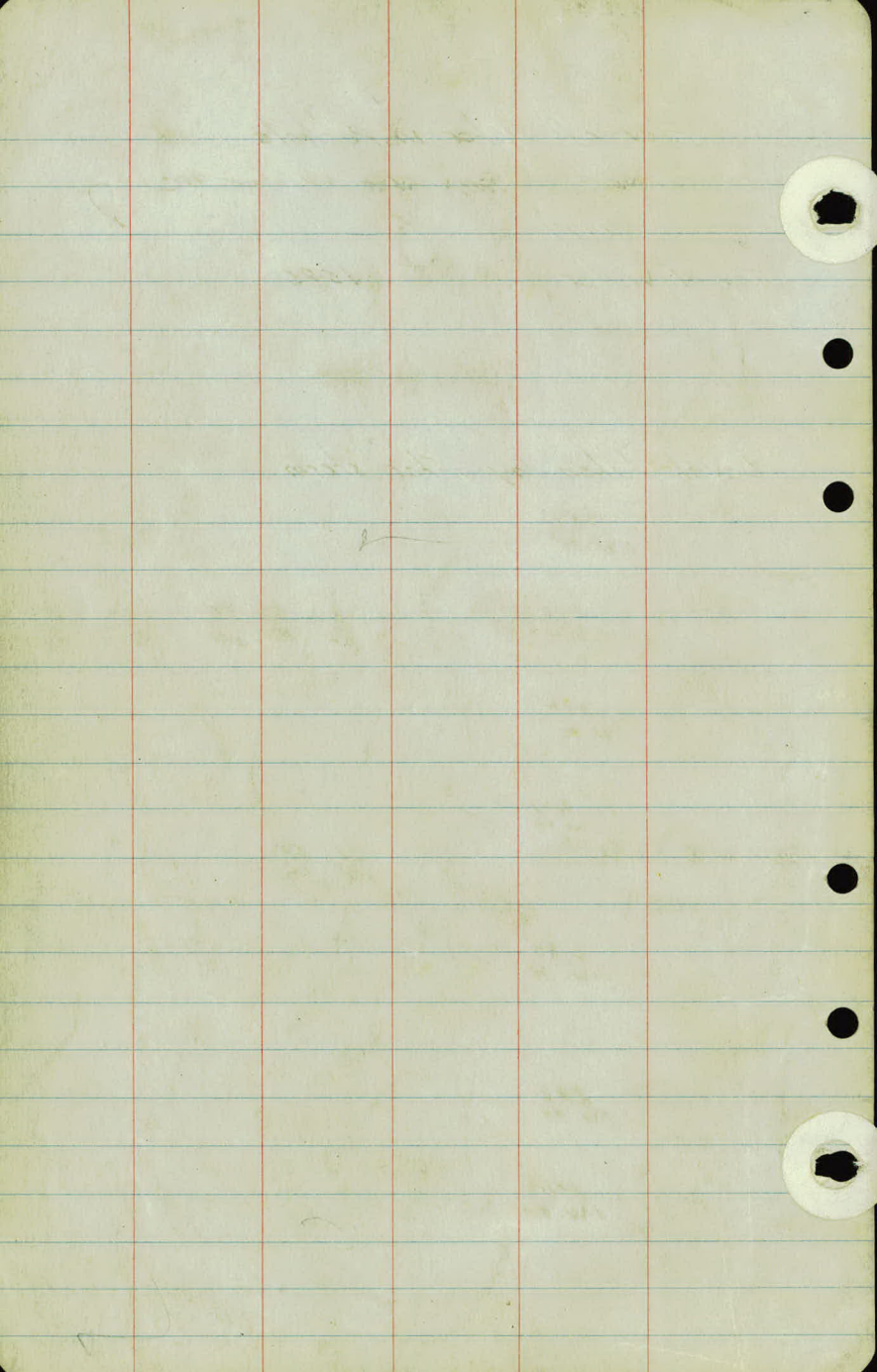
0.77

2

Top of water

15.85

Levels taken day after storm



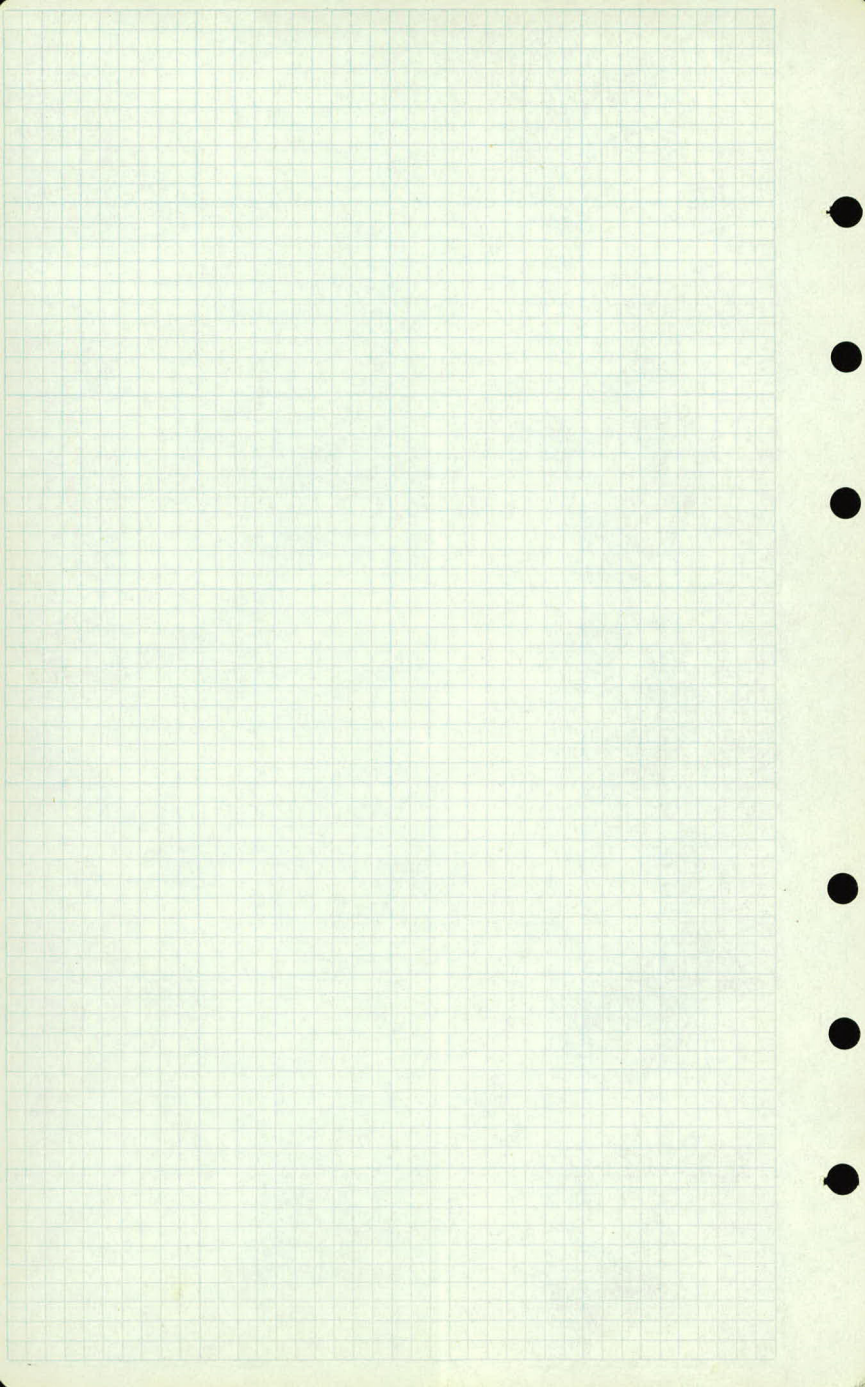
House Locations

Larpenters Ave

West of Tatum St

Dec 11 1950

HAW
AM
LC
MB
ES



+00 SW Cor Gar. 2

Ga
+70 SE Cor Gar

+67 SW Cor Green H.

Larpenteur

Harmes Floral

Green House

+19 S.W Cor Green Ho

+10 S.E Cor Green Ho

+59 SW Cor Ho

+30 SE Cor Ho

+05 SW Cor Ho

+73 SE Cor Ho

+50 Green Ho

+36 SW Cor Ho

+81 SE Cor Ho

Approx & Tatum





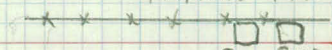
7



+95 SW Cor Ho

+65 SE Cor Ho

Prophine +12



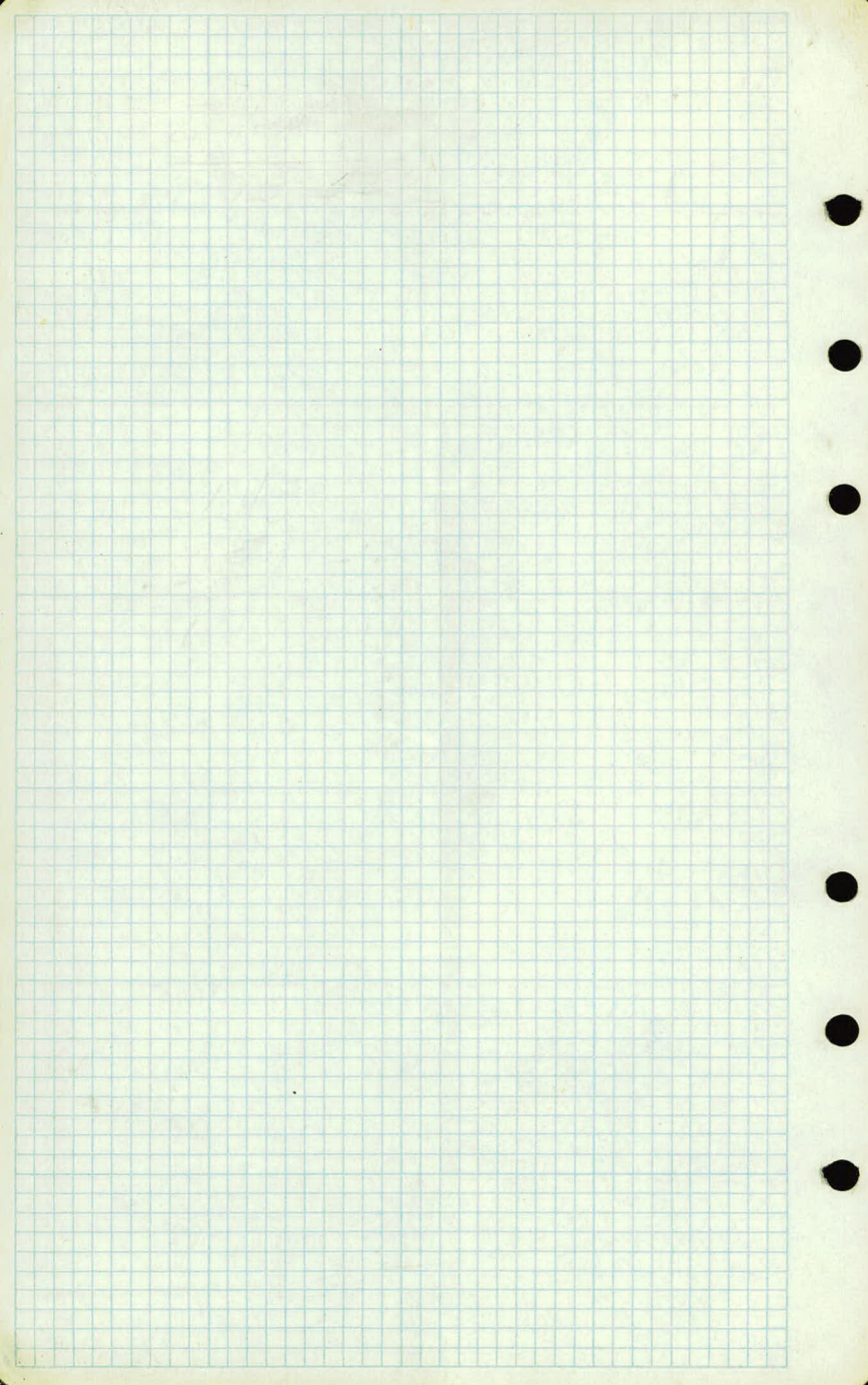
Ga. CoSp

+70 SW Cor Ho



+38 SE Cor Ho

+21 SE Cor Bldg



Elevations

Pt 330' East of ~~X~~ Tatum

Roselawn South

0+00

=

Roselawn

5+00

10+00

15+00

330' Egg +

2

5.1

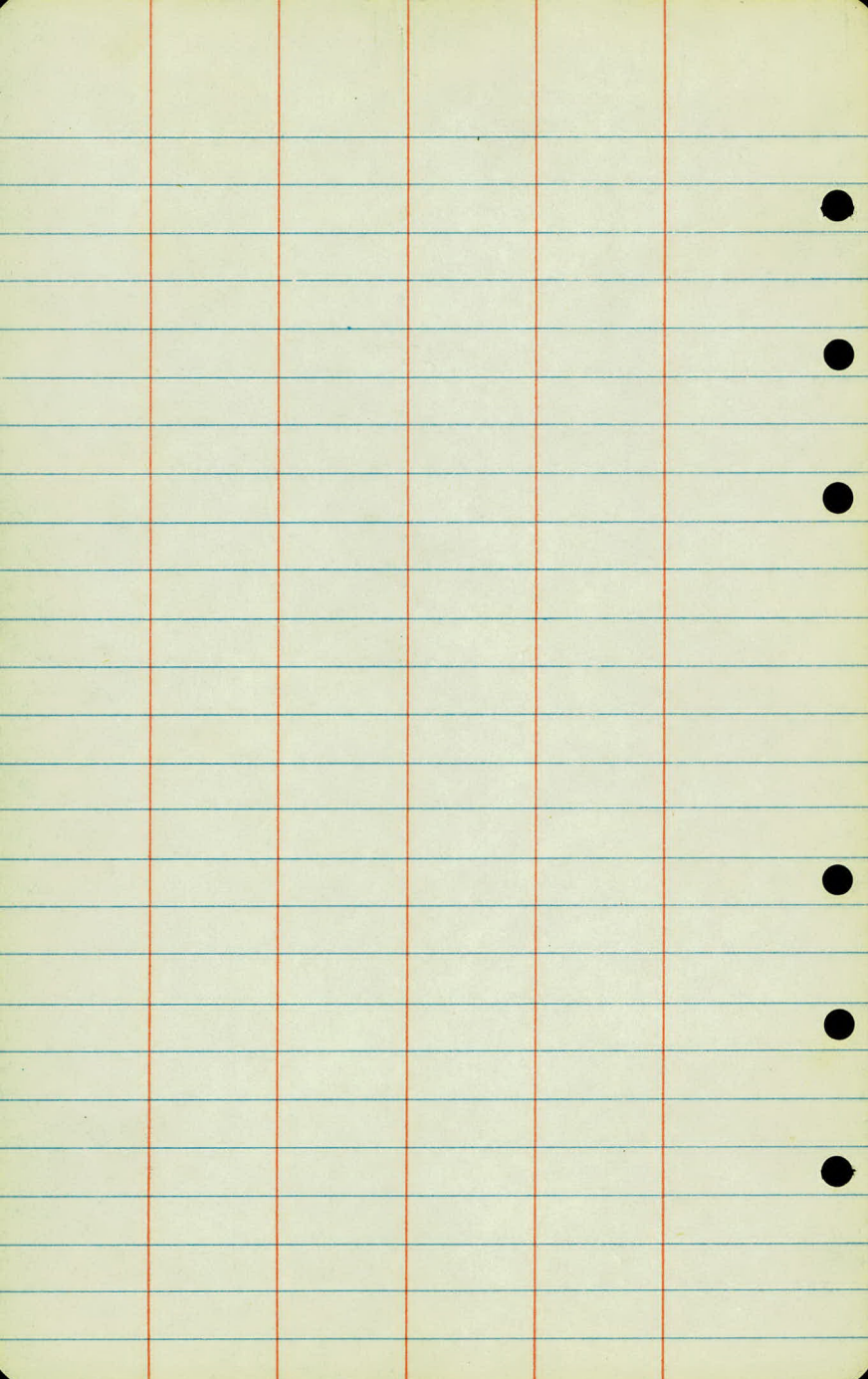
9.9

5.2

15.5

5.5

9.8



10/9
50
A.M.
K.R.
E.J.

House Locations

Tatum St. from Larpenteur Ave.
to Roselawn Ave.
pages 1 to 5

Fairview Ave. from Larpenteur Ave.
to Roselawn Ave.
pages 6 to 10

Larpenteur Ave. from Fairview Ave.
to Tatum St.
pages 11 to 13

Roselawn Ave. from Fairview Ave.
to Tatum St.
page 14

Spotted on Map

6

+92 END-GREEN-HOUSE -160

5

4

3

2

+100 BEG GREEN-HOUSES/60

+05' GHR. 52

+73 GHR-52

+23. HQ-90

+60 HQ. 36

1

+85 HQ-90

+95 HQ.-36

0+00 = ♀ - LAR PENTEUR

GREEN — HOUSES

20
STUCO

7.5
STUCO

GAR

+80-Ho-60

+67-Ho-60

+19-Ho-60 13.43

+37-Ho-60 13.42

13

+96-Ho-60

+66-Ho-60 12.90

+60-Ho-60

12

+18-Ho-60

+34-Ho-60 12.59

+85-Ho-60 12.08 v

+56-Ho-60'

11

+04-Ho-60' +25

10

+93-Ho-60'

+60-Ho-60'

+20-Ho-60'

+09-Ho-45'

9

+88-Ho-60'

+47-BASMT-Ho-60'

+77-Ho-45'

+14-BASMT-Ho-60'

8

+96-GAR-90'

+84-GAR-90'

+80-Ho-60'

+57-Ho-60'

7+00

$1\frac{1}{2}$ -S
 $1\frac{1}{2}$
 F

$1\frac{1}{2}$ -S
 F

$1\frac{1}{2}$ -S
 F

1-S
 STUC

$1\frac{1}{2}$ -S
 F

$1\frac{1}{2}$ -S
 $1\frac{1}{2}$
 F

2-S
 STUC

2-S
 F

1-S
 F

BASNT
 HB

GPR

2-S
 STUC

778-Ho-6 21108

+64 GAR-90'

+49-GAR-90'

+49-Ho-60

+13-Ho-60' 20192

+44-GAR-90'

+24-GAR-90'

+42-Ho-60'

+66 Ho-60 17101

+25 BASMT-FOUND-60'

+93 BASMT FOUND. - 60' 18130

+91-Ho-60 2133

+84 GAR-90'

+70 GAR-90' 2110

+62-Ho-60

+30-Ho-60' 2070

+87-Ho-60'

+50 Ho-60' 1988

+17-Ho-60'

+75 Ho-60' 1911

+34 Ho-60'

+72 Ho-60' 1708

NO

+58 Ho-60' +85 Ho-60'

+38-GAR-90' 1690

+25-GAR-90' 1667

+11-Ho-60'

+70 Ho-60' 1601

+27-Ho-60'

+22-Ho-60

+71-Ho-60' 1500

+92-Ho-60' 15110

+51-Ho-60'

+49-Ho-60'

+19-Ho-60' 1447

+23-Ho-60' 14151

GAR

 $1\frac{1}{2}$ S
F $1\frac{1}{2}$ S
BRICK $1\frac{1}{2}$ S
F $1\frac{1}{2}$ S
STUCCO1.5
F

GAR

 $1\frac{1}{2}$ S
STUCCO2.5
F $1\frac{1}{2}$ S
STUCCO $1\frac{1}{2}$ S
F

GAR

 $1\frac{1}{2}$ S
F

GAR

 $1\frac{1}{2}$ S
FBASEMENT
FOUND $1\frac{1}{2}$ S
STUCCO2.5
F

+35-Ho-60'

+26-Ho-60'

+98-Ho-60' 2442

+73-Ho-60' 24+08

+75-Ho

+42-Ho-60' 22+85

+36 GAR-90'

+24 GAR-90'

+12-Ho-60'

+04-Ho-60'

+72-Ho-60' 22+08

+60 GAR-90'

+57-Ho-60' 2200

+18-GAR-90'

+22-Ho-60'

+0.6-Ho-60'

$1\frac{1}{2}-5$
F

 $1\frac{1}{2}-5$
F

 1ST
BRICK

GAR

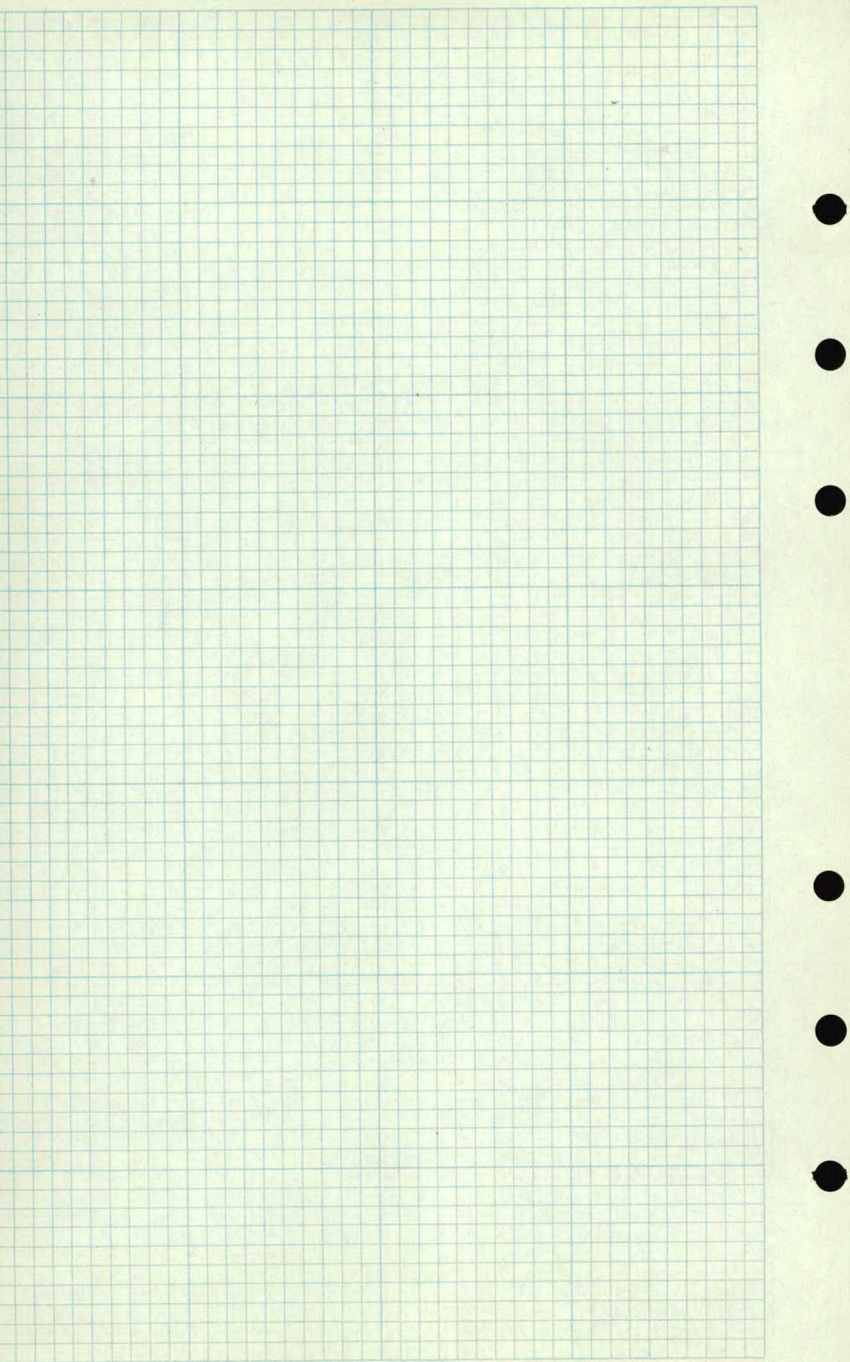
 $1\frac{1}{2}-5$
F

 $1\frac{1}{2}-5$
F

GAR

 $1\frac{1}{2}-5$
F

 $1\frac{1}{2}-5$
F



10/9/50

R.M.
H.R.
E.J.

HOUSE - LOCATION
FAIRVIEW - AVE
LARPENTEUR - TO - ROSELAWN

+45-HO-100°.

6.

5

4

3

2

1

0+00 = \$ L'ARPENTIER

2-5
F

13

 $+75-H_0-100'$ $+30-H_0-100'$

12

 $+74-H_0-100'$ $+43-H_0-100'$

11

 $+86-H_0-130'$ $+50-H_0-130'$

10

9

 $+95-H_0-100'$ $+56-H_0-100'$

8

 $+14-H_0-100'$

7

$$\begin{array}{|c|} \hline 1.5 \\ \hline F \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 1.5 \\ \hline F \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 1.5 \\ \hline F \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 2.5 \\ \hline F \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 2.5 \\ \hline F \\ \hline \end{array}$$

21
+89-Ho.-90

+44 Ho.-90

20

+92 GAR-120'

+79-GAR-120'

+68-Ho-90'

+36-Ho-90'

19

+88-Ho-90'

+40-Ho-90'

18

+71-Ho-90'

+39-Ho-90'

17

+72-Ho-100'

+17-Ho-100'

16

+72-Ho-100'

+24-Ho-100'

15

+73-Ho-100'

+20-Ho-100'

14

$$\begin{array}{|c|} \hline 2-5 \\ \hline F \\ \hline \end{array}$$

GAR

$$\begin{array}{|c|} \hline 2-5 \\ \hline F \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 2-5 \\ \hline F \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 2-5 \\ \hline STUC \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 1\frac{1}{2}-5 \\ \hline F \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 1-5 \\ \hline F \\ \hline \end{array}$$

$$\begin{array}{|c|} \hline 1-5 \\ \hline F \\ \hline \end{array}$$

25

+15 Ho-90'

24

+54 Ho-90'

+03 Ho-90'

23

+56 Ho-90'

22

22+05 Ho-90'

+46 Ho-90'

21

1-5
BRICK

1-5
BRICK

1-5
BRICK



11/24/50 (1)

A.M
M.B
E.J
K.R

HOUSE - LOCATION

LARPELVEUR - AVE

FROM - FAIRVIEW-AVE TO TATUM-ST

ROSELAWN - AVE

FROM - FAIRVIEW-AVE - TO - TATUM-ST

+59 Ho - 100'

+34 Ho 100'

+21 Ho - 100'

+40 Ho - 100'

+92 Ho - 100'

+61 Ho - 100'

+13 Ho 100'

+89 Ho 100'

2 ST
STUCCO

2 ST
STUCCO

2 ST
FRANK

2 ST
STUCCO

LARPENTEUR - AVE

FARVIEW - AVE

+09-H0-100

+77 H0-100

LARPERN T'FUR

2-57
STUC 6

EARNVIEW

+47-Ho-110'

6

+93-Ho-110'

+60-Ho-140'

+22-Ho-140'

5

4

+60-Ho-130'

3

+89-Ho-130'

2

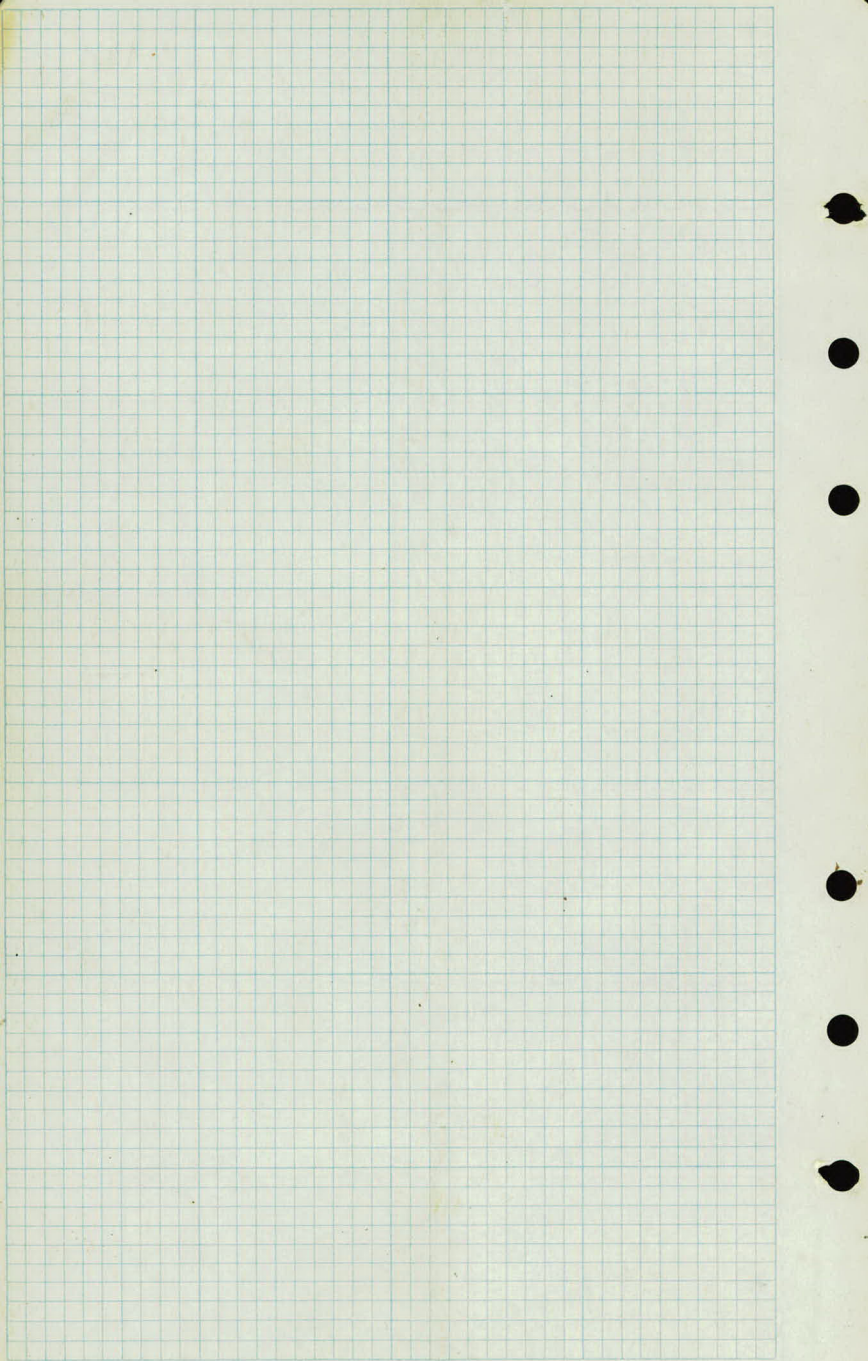
1

2.57
FRAME

1.57
FRAME

1-1/2 ST
FRAME

ROSE LAWN - AVE



Topog.

Cleve Y. Larp

1/19/53

HAW

LQ

AM

NB

FR

+53 Nov 8th 1923 PC M-H 123

+13' PP 44'

+15 Apr 4 32'

53

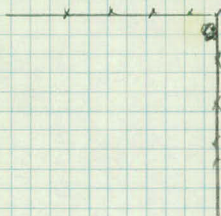
+43 24" BE 38'

+05 PP 23'

62

+1

51



⊙

Underground Duct Line
46" Below Profile Grade To Top of Road

⊙

24' 100%

