

Bk. 115 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

Ditch No. 5

From Co. Rd. "C" To N. of Co. Rd. "E"

Road Acc't. No.

Date Filed 3-22-44

File

Plan Survey

Ditch # 5

From Co Rd C To Jones Lake

2-22-43

HAW

LC

AM

L.L

C.F

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Align 1 to 21

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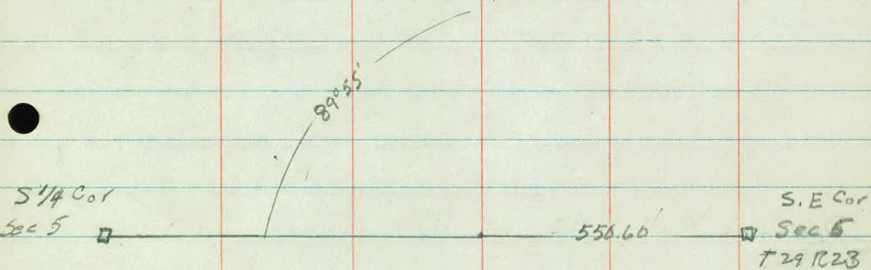
Completed 2/2/43

Sta	Pt	ΔL	ΔR	True Bearing
-----	----	------------	------------	--------------

0+47.30	P.1		14°11'	
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0+00				
------	--	--	--	--

Description



S. 1/4 Sec 5
T 29 R 23

Sta	Pt	ΔL	ΔR	True Bearing
-----	----	------------	------------	--------------

20+35 ¹⁰	P.1	8° 19'		
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17+44.85	P.1	11° 59'		
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16+88 ⁰⁰	P.1		8° 21'	
---------------------	-----	--	--------	--

Description

End Title Line

Ref Pipe Line

Sta	Pt.	Alt	Δ Rt	True Bearing
-----	-----	-----	------	--------------

22+31 ⁶⁵	P.1	64° 34'		
---------------------	-----	---------	--	--

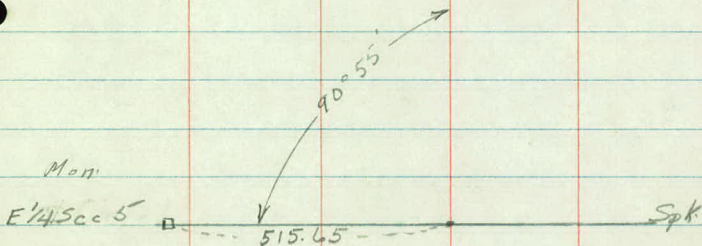
22+06 48	P.O.T.	Δ Cleveland		
----------	--------	-------------	--	--

21+81 ¹⁵	P.1	87° 24'		
---------------------	-----	---------	--	--

Description

End 24" CM

1X2 Hub



Reg 24" x 50' CM

1X2 Hub

Sta	Pt.	Alt	Δ Rt	True Bearing
-----	-----	-----	------	--------------

28+25 ²²	P.I.	3° 51'		
---------------------	------	--------	--	--

28+00.93	POT	Δ Cord "0.2"		
----------	-----	--------------	--	--

27+76 ²⁵	P.I.	23° 22'		
---------------------	------	---------	--	--

Description

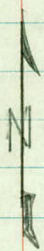
End 36" C.M

E 1/4 Cor
Sec 5

265.35

Nail

92°07'



Beq 36" X 48' CM

Sta

Pt.

ΔL

ΔR

43+01.75

P.I.

$32^{\circ}11'$

39+78.26

P.I.

$22^{\circ}38'$

35+80.45

P.I.

$13^{\circ}17'$

Description

Ctr. M.H.

Ctr. M.H.

Beg 20" Vit. Sewer

C 2' NW

Sta

Pt.

$\Delta Lt.$

$\Delta Rt.$

47+153.1

P.O.T.

$\pm$ Cleveland

46+72.79

P.1

$9^{\circ} 06'$

45+29.93

P.1

$10^{\circ} 46'$

Mon
N.E. Cor
Sec 5

Description

$\angle 43^{\circ}34'$
1069.22

E line Sec 5

Nail

Hub

Hub

Sta	Pt	ΔL	ΔR	True Bearing
-----	----	------------	------------	--------------

60+74.82	P.O.T.	$\pm$	Co Rd "D"	
----------	--------	-------	-----------	--

58+84.68	P.I.		$3^{\circ} 23'$	
----------	------	--	-----------------	--

52+67.89	P.I.		$12^{\circ} 09'$	
----------	------	--	------------------	--

Description

N. Line Sec 5

125°45'

Nail

810.39

N.E. Cor
Sec 5

Mon

1x2 Hub

Gen. M H

549

PL

ΔL

ΔR

79+55⁷²

P. I.

91°25'

73+56⁰⁰

POT

66+21⁹²

P. I.

48°46'

Description

Hub

End Sewer

ctr. MH

Sta	Pt.	ΔL	ΔR
-----	-----	------------	------------

83+51 ⁰⁹	P.1	2°39'	
---------------------	-----	-------	--

80+19 ³⁰	P.1		12°17'
---------------------	-----	--	--------

79+96 ⁹⁵	P.O.T	$\pm$	M.T.R. Tr.
---------------------	-------	-------	------------

Description

Hub 1.1

End 24" Iron Pipe

 Nail

Sta

Pt.

ΔLT

ΔRT

88+19.60

P.1

13°00'

86+81.18

P.1

✓30°30'

85+09.89

P.1

✓31°30'

Description

Sta

Pt.

$\Delta L+$

$\Delta R+$

P.O.T.

70+62.35

P. 1

$16^{\circ}00'$

89+62.45

P. 1

$2^{\circ}30'$

Description

Hub

Nail

Sta

Pt.

Δ Lt

Δ Rt

112+54.80

P. 1

$34^{\circ}15'$

108+57.95

P. 1

$13^{\circ}30'$

93+63.25

P. 1

$13^{\circ}41'$

Description

Bay Pitch #2

Edge Jones Lake

Sta	Pt.	ΔL	ΔR
-----	-----	------------	------------

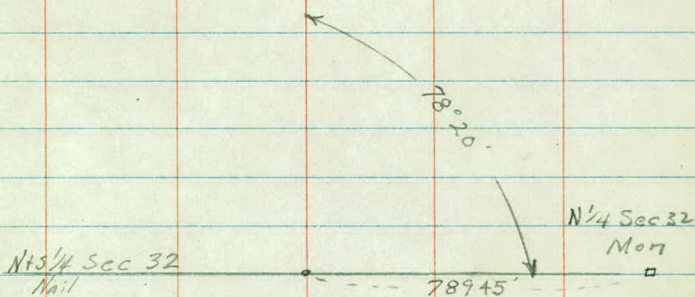
115+62 ¹⁵	P1		38°32'
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115+47 ³⁵	P.O.T	End 30" CM	
----------------------	-------	------------	--

115+07 ⁵⁵	P.O.T	Long Lake Rd	
----------------------	-------	--------------	--

114+07 ⁴⁸	P1	5°00'	
----------------------	----	-------	--

Description



Be 30" C.M.

Sta

Pl

ΔLt

ΔRt

121+16.62

P.1

$89^{\circ}52'$

118+29.60

P.1

$90^{\circ}12'$

117+02.90

P.1

$71^{\circ}08'$

190

Description

End 36" Conc Pipe

Beg 36" Conc Pipe

Sta

Pt.

ΔL

ΔR

122+46.21

P1

90°03'

121+57.06

P.O.T

Begin 39" Iron R.R. Culvert

121+42.84

P1

76°02'

Description

End RRCu/v

Sta.

Pt

ΔL

ΔR

129+46.84

P.I

$13^{\circ}23'$

127+72.18

P.I

$11^{\circ}55'$

124+91.40

P.I

$2^{\circ}09'$

Description

Beg 36 CM

Sta	Pt.	ΔLt	ΔRt
-----	-----	-------------	-------------

131+51.28	P.1	14° 04'	
-----------	-----	---------	--

130+21.28	P.1		18° 28'
-----------	-----	--	---------

P.O.T. $\frac{1}{2}$ Co Rd E

Description

End 36" Culv

Sta

Pt.

ΔL

ΔR

137+67⁴³

P1

7°05'

137+05⁶³

P1

49°29'

132+35⁴⁶

P1

33°53'

Description

Sta

Pt.

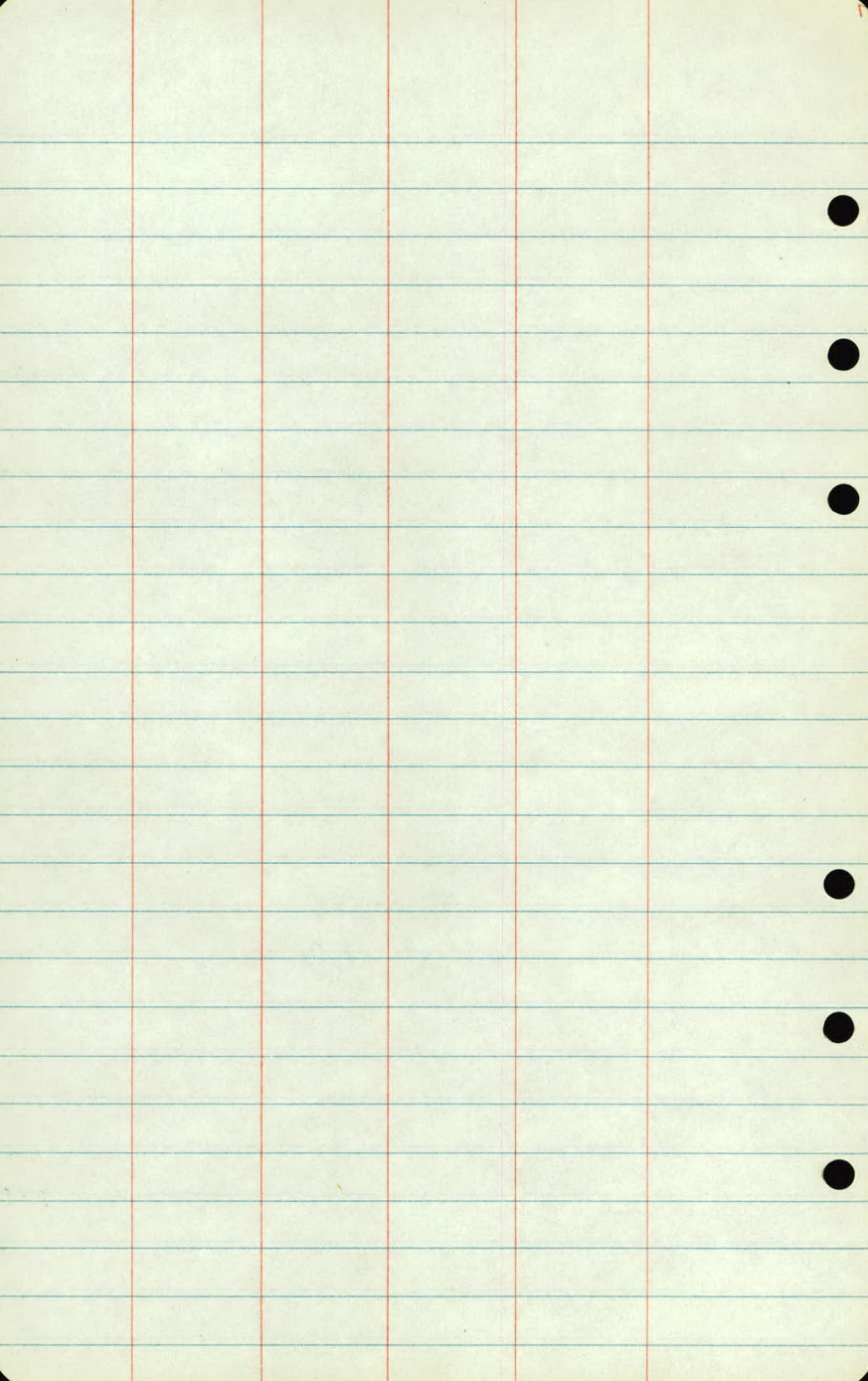
$\Delta L+$

$\Delta R+$

139497⁰⁰

P.1

Description



Topography
Ditch # 5

5
4
3
2
1
0
+47 End 24" Conc Pipe
+19 Edge Shoulder
+11 Edge Pave.
± Co Rd "C"
0-11 Edge Pave
0-19 " Shoulder
0-42 End 24" Conc

Lake 300'

Lake 360

Lake 200'

Lake 275'

+47 Edge Lake 130'

+47 Lake 250

+27 PP 5'

22' ICC Parc

12 400 Island 63'

400 End Island

11

410 Bog Island

10

9

8

7

6

5

Ditch 66

23

high ground

+50 Edge Island 100

+50 Ed Island 20

Ditch 83

Ditch 100

Edge Lake 325

Ed. Lake 279

Edge Lake 250

Ed Lake 310

Ed. Lake 315

Ed. Lake 325

19

18

+ 72 Fox R.

17

+ 88 Bag 20" Vit Tile Line

+ 45 Bag Ditch to End Lake

16

15

14

13

12

Fe 27' 24

+150 Fe 37'

+11 Oak 20'
+08 Oak 34'

+99 Fe Cor 52' 55'

+45 Fe 63'

Scattered Oaks
Pasture

+145 Fe 54'

+100 End Lake 30'

+188 Lake 30' 4 175'

Edge Lake 230'
Ditch 13'

Edge Lake 70'

Edge Lake 350'
Ditch 26'

Edge Lake 93'

Edge Lake 400'
Ditch 40'

Edge Lake 110'

Ditch 55'

Edge Lake 81'

Edge Lake 375'
Ditch 11'

Edge Lake 100'

26 Edge Lake 165'

25 +100 Edge Lake 119' 184' +474'
+100 & Cleve 154'

24

23

22

+31.65 End 24" CM
+06.68 & Cleve

+81.15 Beg 24" X 50" CM

21

+35.15 End 20" V. & Tile Line Beg Ditch
1' X 6" Headwall +35 Beg G.R. 23' & 45"
+28 Fc X & Cor.

20

19

Edge Lake 261
25

Edge Lake 228

Lake 154

Lake 207

+00 Edge Lake 73, 132, 525'
+00 & Cleve 106'

+00 Edge Lake 25, 88, 438'
+00 & Cleve 60'

Match

Match

+81 Lake 200'

+81 Lake 50' & 207

Edge Lake 190'

+00 Lake 56' & 150
+00 & Cleve. 31'

+35 Bag Lake 0' & 50'

+35 Edge Lake 60' & 100
+35 & Cleve 34' 22'
Top

+00 Fe 94'

100 Fe 06'

Pasture

+50 Fe 16'

Fe 27'

33

32

31

30

29

28

27

+25.27 End 36" CM Beg Ditch

+01 & "C 2"

+76.75 Beg 36" X 48" CM

26 Edge Lake 165'

Edge Lake 192

Edge Lake 167
26

Edge Lake 215'

Edge Lake 250'

Edge Lake 150

Note Approx.
4' Btm Ditch
Tru Lake

Edge Lake 281

Edge Lake 110'

Edge Lake 348'

Edge Lake 81

Edge Lake 300

+25 Cor Lake 100

+25 Cor Lake 285

26' 0" Treated Top

+77 Cor Lake 225'
(For Tan)

+77 Cor Lake 261'
(Note Taken From Fern Tan)

Lake 148'

Edge Lake 288'

Lake

Edge Lake 261

40

+78.26 C M H

+22 1' Ditch X 2

39

38

37

36

+15 Rd X 2

+11 Beg Open Ditch 42'
 +11 End 12" Vif 42'
 +00 Rd 20'

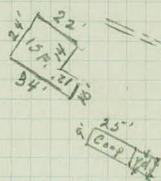
+80.45 Beg 20" Vif 2' Hd Wall
 End open Ditch

35

34

33

34
 +07 Cor Ho
 +07 Septic Tank 1'
 +00 SE Cor Ho 60'



+75 Cor Bldg 26'
 +70 Fe Cor 14'
 +66 Cor Ch. Coop 27'
 +61 Fe Cor 16'

+07 1' Ditch 42'

Gardens

Gardens

+100 Ditch 93'

+35 Group 4 Cot/25'

+20 Edge Rd
 +12 Beg Row Will 16'
 +10 Edge Rd
 +96 Beg Row Will 10'
 +83 Beg 12" Vit 24'
 +77 Δ in Ditch 18'
 +68 Beg 2' Off Take Ditch 5'

+100 End Lake 10' + 35'

+35 End Lake 10' + 46'

Edge Lake 193'

Edge Lake 95'

4' Btm Ditch 7'

Edge Lake 192'

Edge Lake 167'

47

+73 Fe X R

46

45

+77 Fe X R

44

+23 Fe + Edge Wd. Pile
+11 Edge Wood Pile
+0175 Cen MH

43

42

+39 Fe X R

+035 WCor Barn

41

40

#43 PP 03'

Fe 34

#17 Fe Cor 90'

Pasture

#40 Fe 82'

Cult

#44 End Fe 41'
#31 PP 14'

Wood Pile

#18 Fe Cor 18'
#00 Fe 14'#150 Lt Pole 5'
#48 NW Cor Coop 7'
#34 SW Cor Coop 9'

Barn Yd

#39 Fe Cor 2'

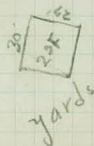
#20 NW Cor Gar 6'
#18 NW Cor Barn 02'

#98 SE Cor Gar 2'

#65 NE Cor Ho 57'

#38 SE Cor Ho 52'

#43 Fe Cor 22'



yards

yards

54

53

+68 Can Broken M.H.

+41 Fe X 2

52

51

50

+106 Fe X 2

+94 Rd X 2

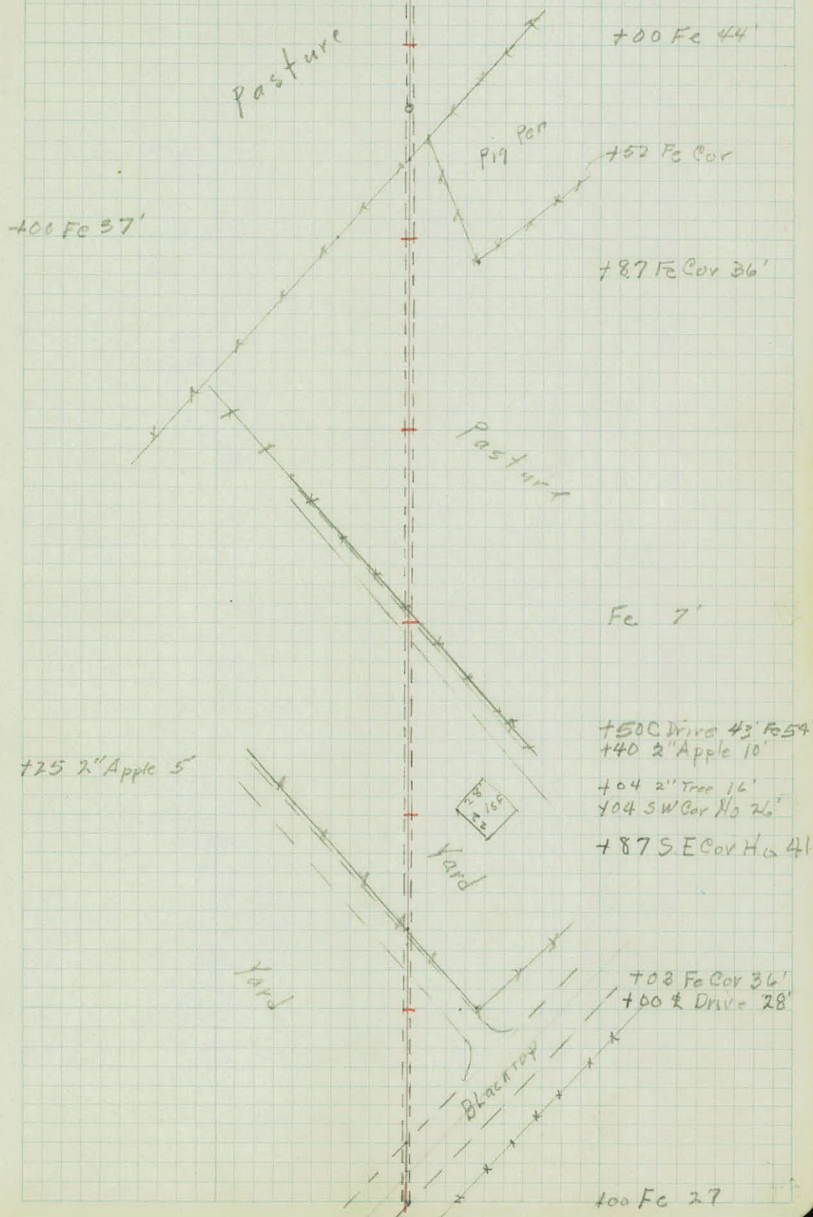
49

48

+40 Fe X 2
+27 Drive X 2

47

+30 Edge Blacktop
+15.31 R Glove
+100 Edge Blacktop



61

+85 Edge Blacktop

60

+59 Edge Blacktop

59

+75 Fe & R

+27 Fe & R

58

+60 Fe & R

57

56

+28 Hi Line & R Steel Towers

55

+09 Tel Line & R

+92 Power Line & R

54

+100 Fe 7' 30

+77 12" CM 27'
+75 Fe 40' 12" X 36" CM
+47 12" CM 4'

+19 Fe Cor 81'
+100 Fe 19'
+78 Fe Cor 53'

+100 Fe 18' + 54'

+75 Fe 35'

+12 Fe Cor 74'

+44 Fe Cor 24'

+28 Fe Cor 13'
+106 Fe Cor 39'

+100 Fe 84'

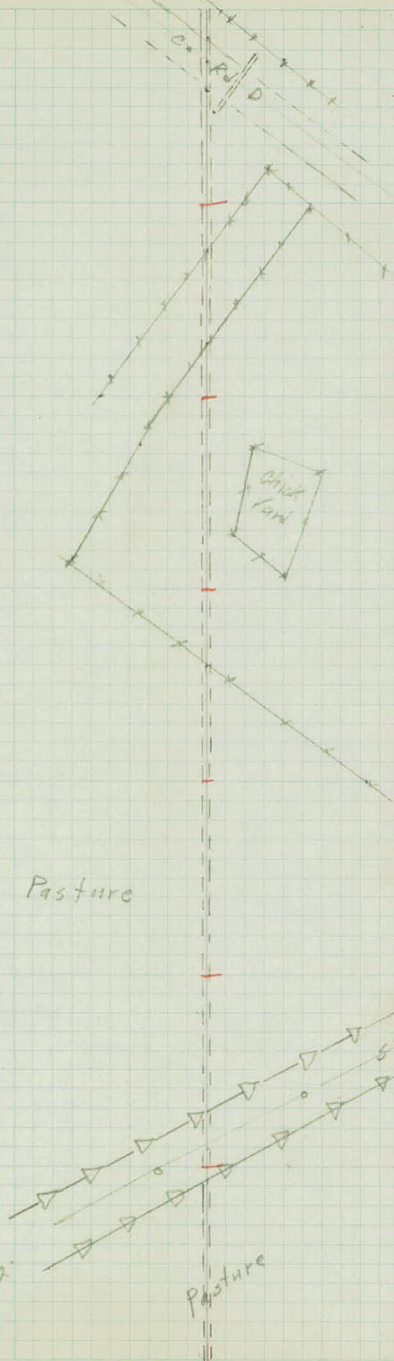
Pasture

+97 T.P. 25'

+47 Cen H Tower 87'

Pasture

57 Croix Falls Imp Co



68

67

+21.92 Com M. H

66

+26 Spur Tr X ♀

65

64

+69 Spur Tr X ♀

63

62

61

+65 Fo X ♀

Tracks 44

Fe 6'

31

Tracks 44

Fe 6'

+66 T.P. 7'

Note Parallel
To Tracks

+23 & Main Tr. 44

+23 Fe 6'

+95 Beg Spur Tr. 39'

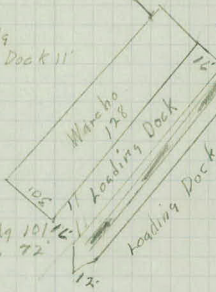
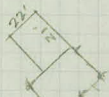
+52 NW Cor Coop 7'

+32 N.E. Cor Chicken Coop. 52'

+18 Fe Cor 3L'

+71 N.E. Cor Bldg

+62 Cor Loading Dock 11'



+77 S.E. Cor Bldg 101' x 12'

+77 & Spur Tr. 72'

& Spur Tr. 100' x 117'

+52 P.P. 23'

+46 Beg Spur Tr 6'

+48 Fe 49'

+48 & Ent 49'

400 Fe 7'

75

74

+56 End Sewer Beg open Ditch
1x6 Hd wall

73

+58 Spur X E

72

71

70

69

68

Main Tr 42

Fe 07

32

Main Tr. 42' Spur 30'

Fe 08'

+54 T.P. 05'

PASTURE

Main Tr 42' Spur Tr. 7.5'

+29' Breather Pipe Not
Gns Line 8
(T.C.P.)

+97 Fe Cor 8'
+96 Rgc Tie Fe

Tr. 42'

+85 T.P. 07'

Spur 13.5' Fe

+89 Fe Cor. 27'
+83 Fe Cor 07'

K.C. Gate

Tr. 42'

Main Spur 38' Fe 06'

+08 T.P. 07'
Tr. 43

Spur Tr 43 61' 69'
Fe 07'

+60 24' Pop 13'

Tracks 43'

Spur Tr. 51' 84' 99'
Fe 06'

+48 T.P. 07'

+74 Fe Cor 6' 37'

Tracks 44'

+25 Fe Cor 6' 44'

Fe 06'
Spur Tr. 54'

82

81

+48 Fe x 2 Parallel to Tracks

80

+1930 End 24" Conc Pipe

+9695 2 Tracks

+7430 Beg 24 x 46" Conc Pipe

79

78

77

76

75

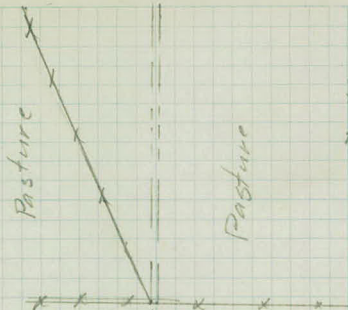
Fe 48'

33

+44 8" B.E.L'

Fe 26'

+48 Fe Cor 04'



+71 24" CoH 4

+67 30" CoH 5

+38 24" CoH 04'

2

+03 T.P 04'
Tracks 40

Fe 8

Fe 7'

Tracks 41

+88 T.P 04'

Fe 7'

Fe 7'

+26 Pl of Switch 42'

+10 T.P 4'
Main Tr. 42

+06 Fe Cor 08'
+04 R.e.T. i.e Fe
Fe 6 7'

89

88

87

^{53}Fe K α

86

85

84

83

82

Fe 18'

34

+1960 Fe 7'

Fe 7'

Cull

Pasture

Fe 14'

+71 Fe Cor 26'

X X X

Pasture

Pasture

+1412 Tw. Coll 3'

+40 30" Cor 7'

+20 24" Cor 8'

96

95

94

+63.25 Edge Lake

93

+26 Fe x 8

92

91

90

+64 End Conc Box
+56 2 Drive
+50 Reg Box Cntr

89

Jones Lake

Lake 700'

- +56 18" Stn 2'
- +42 15" Will 22'
- +37 12" Will 3'
- +27 15" Will 14'
- +18 12" Will 17'
- +18 Cor 3 12" Will 7'
- +12 12" Will 12'
- +05 24" Will 5'

Lake 500'

- +67 12" Will 6'
- +56 12" Will 2'
- +44 16" Will 2'

+96 12" Will 2'

- +35 15" Will 5'
- +33 10" Will 2'

+00 Lake 300'

Fe 58'

+29 24" Tw. Cott 6'

- +53 Rgc Tie
- +50 Fe Cor 17'

Fe 15'

- +66 Rgc Tie Fe
- +64 Fe Cor 14'
- +60 Fe Cor 27'

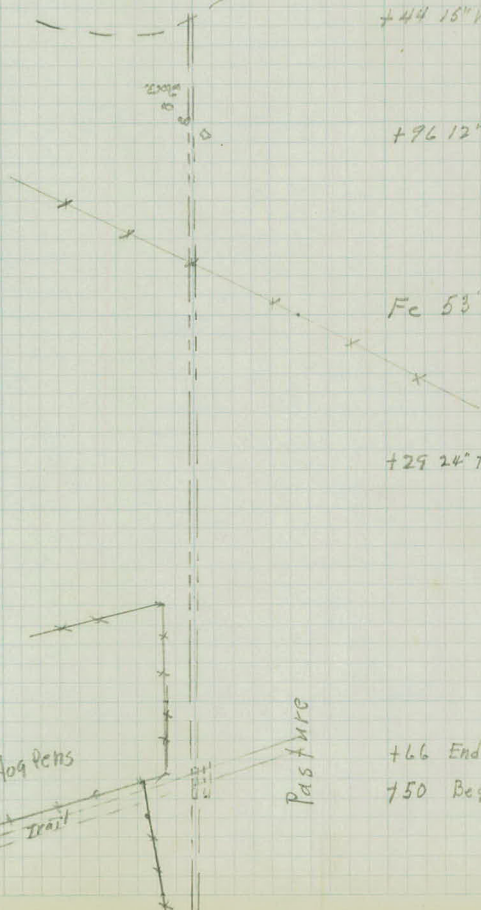
Hog Pens

Pasture

- +66 End 24" Cone 5'
- +50 Beg 24" Cone 5'

Fe 18'

Trail



103

102

101

100

99

99

97

96

Approx 300'

Approx 500'

36

Approx 500'

Approx 700'

Approx 500'

Approx 700'

Jones Lake

110

109

+ 57.95 Beg Ditch #2
Edge Lake

108

107

106

105

104

103

+81 15" Tw. Will 2'

UnCultivated

UnCultivated

+36 12" Tw. Will 1'

Lake 50

Lake 200'

Lake 150'

Approx 400'

Approx 250'

Jones Lake

Approx 450'

117

116

+47.35 End 30" CM
+20 Edge Rd
+107.55 * Long Lake Rd

115

+96 Edge Rd
+75 Fe K²
+6748 Bos 30" CM

114

113

112

111

110

+62 Triple 8" W.I. 0

+06 24" C.H. 02'

UnCult

UnCult.

+72 15" Tr W.I. 12'

+33 15" BE 5'

+64 12" BE 13'

+53 24" W.I. 6'

UnCult

UnCult

124

123

+ 41 Fe. & S

122

+ 10.28 Con No Tr

+ 95 Con So Tr

+ 57.06 Beg 39" Iron RL Cnly

121

120

119

+ 29.60 End 36" Conc P

+ 15 Shld. Rd

+ 09.5 Edge Parc

+ 96 R STH # 8

+ 82.5 Edge Parc

+ 76 Shld. Rd

+ 62.90 Beg 36" Conc Pip. L7

118

117

Fe 52'

+84 18" W. 11' 11"
+73 Group 6 18" W. 11' 10"

+54 Fe Cor 47'

500 Line R.R.

+27 NW Cor Br. 43'

+71 S.W. Cor Bridge 44'

+47 Fe Cor 15'

+43 Fe 13'

End Brush 15 + 40

Shld Pave
+10.62 12-57 22-49

+67 Fe Cor 7'

+58 Rge Tie Fe.

Fe 5
Brush 15 40

Shld Pave
12-57 22-49

+40 Brush 15-30'

Fe 6'

Shld Pave
13-56 21-48

+30 Fe 05'

Uncult.

Uncult.

Pasture

Brush & Scattered Trees

27100 R.R.

U.S. #8

131

+ 91 Twin 12" W, 11"

130

+ 2128 End 36" CM

+ 94 Shld + G.R

74'
36" x (54") CM

+ 69 Shld. Co Ed E + G.R

+ 4684 Beg 36" CM

129

128

127

126

+ 86 Fe X R

125

124

Pasture

Pasture

+30 8" W.H 10'
+21 Be g Fe 2'

+75 Rd 8 G.R 3'

+47 Edge Rd 53'
+ G.R

Black Top

Cult.

UnCult

+75 36" C.H 11'

UnCult

+21 Fe Cor 95'

+91 Fe 74'

Fe 60

138

137

136

135

134

+83 Fe x 2

133

132

131

+23 Tw 15" W 11' 00

+11 Tw 12" W 11' 2'

+88 12" Oak 13'

+18 20" Oak 13'

+80 10" Oak 7'

+20 12" Oak 5'

Pasture

Pasture

+22 24" Co H 3'

+63 30" Co H 4'

+25 12" Oak 12'

+19 Tw 15" Oak 15'

+15 12" Oak 8'

+00 18" W 11' 4'

+68 6" Co H 3'

+56 Stu 6'

+46 Stu 4'

+15 6" W 11' 2'

+13 8" Tw Co H 3'

+12 8" Co H 8'

+02 8" W 11' 2'

Fe 55

+58 24" Co H 2'

+68 10" Tw W 11' 4'

+52 12" W 11' 5'

+35.46 Fe 68'

+26 Tw in 18" Co H 6'

Pasture

Pasture

+53 48" Co H 6'

+51 Fe 27

Fe 26

140

139

138

+97 Fe 20'

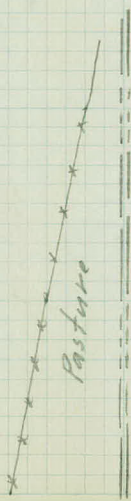
Fe 41'

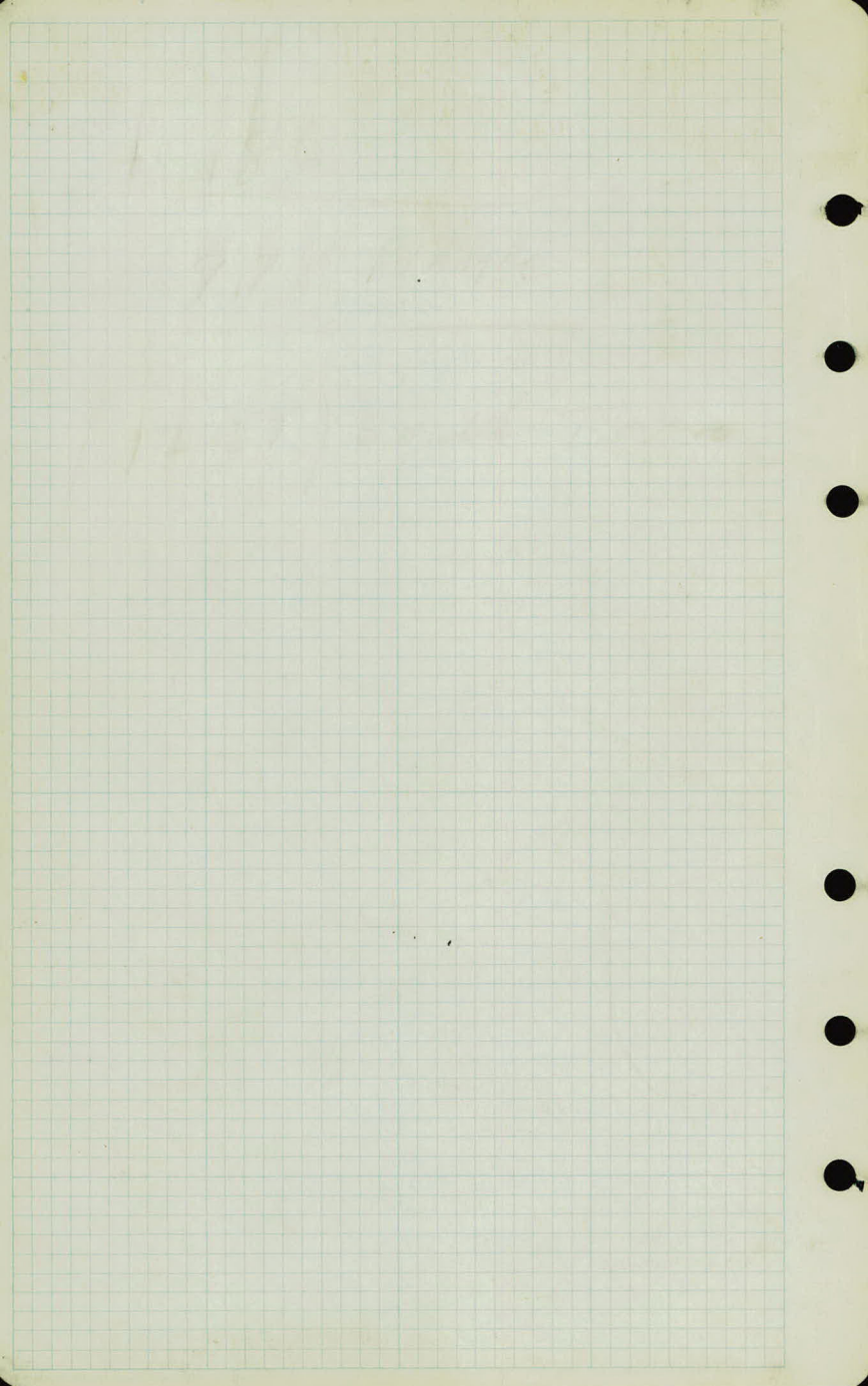
Fe 59

Uncult

Pasture

Pasture





Bench Levels

Ditch #5

Sta	+	π	-	Elev	
B.M	2.72	928.61			925.894
	1.90	921.27	9.24	919.37	
B.M	6.92	921.27	6.92	914.35	914.55
B.M	2.21	916.78	6.70	914.57	
	2.83	912.95	6.66	910.12	
	6.85	911.02	8.78	904.17	
B.M	2.29	910.63	2.68	908.34	✓
	4.34	909.11	5.86	904.77	
B.M	5.52	908.86	5.77	903.34	
	6.65	912.27	3.24	905.62	
	5.09	913.35	4.01	908.26	
B.M	7.14	913.13	7.36	905.99	
	8.37	919.57	1.93	911.20	
B.M	2.91	919.91	2.57	917.00	
	3.95	915.58	8.28	911.63	
B.M	0.32	915.58	0.32	915.26	
	3.13	912.58	6.13	909.45	
	4.71	911.60	5.69	906.89	
	5.59	912.15	5.04	906.56	
B.M	5.42	912.15	5.42	906.73	
T.P.	6.57	906.37	12.35	899.80	
	1.83	904.64	3.56	902.81	
B.M	4.62	904.64	4.62	900.02	
	3.53	898.90	9.27	895.37	
	1.20	898.92	1.18	897.72	

Description

Top of U.S.G.S #G13 36' East & Clove + 350' So of "C"

Spk in 12" Oak 125' Rt Sta 52+65 (Co Rd @ Proj)

Top Mon Clove & Co Rd @

Top Conc. Tel. Marker 60' Rt Sta 17+44

6th Post

Spk in Arc Lt Pole So Ea Cor Clove & C2

Spk in P.P. 5' Lt Sta 46+73

Top Mon D* + Clove

Top No. West Cor Btm Step 70' Lt Sta 60+00

Top of N.E Bolt of Switch 35' Lt Sta

Nail in Co. Fe Post 6' Lt Sta 88+46

Top Mon ~~the~~ Sec 35 S $\frac{1}{4}$ Cor. N.E $\frac{1}{4}$ Sec 32

Sta	+	Σ	-	Elev
		898.92		
	1.28	898.88	1.32	897.60
B.M	4.62	901.22	2.28	896.60
	8.43	908.80	0.85	900.37
	5.17	902.14	11.83	896.97
B.M	5.62	902.14	5.62	896.52
	3.75	899.06	6.83	895.31
	7.84	905.29	1.61	897.45
	2.34	900.17	7.46	897.83
B.M			6.88	893.29

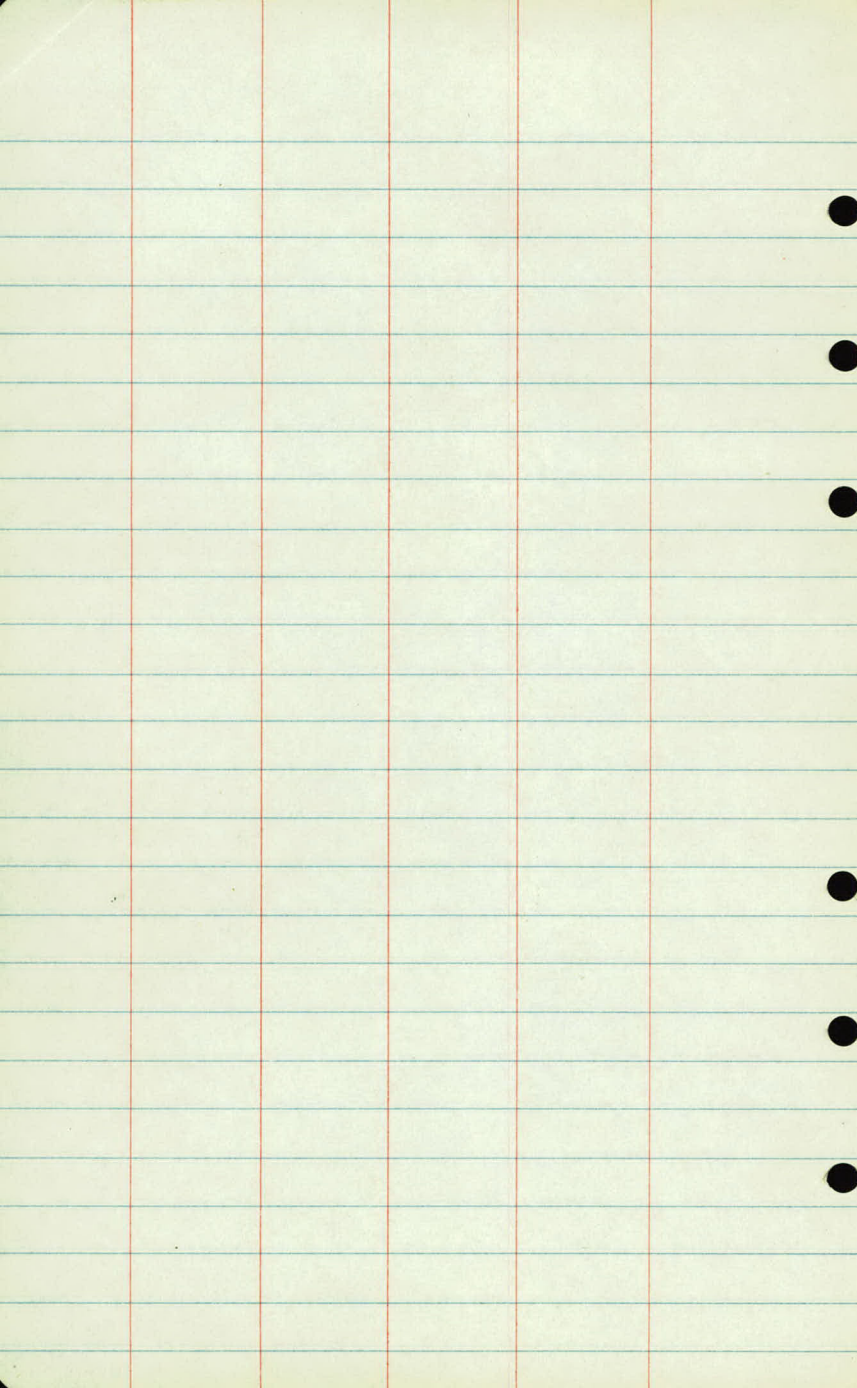
Description

SpK in 12" Twin Willow 10' Rt Sta 109+30

Near Fe Post Lt of Culv Longlake Rd.

SpK in 24" CoH. 10' Lt Sta 124+90

SpK. in 15" Oak 15' Rt Sta 136+75



Profile Levels



Sta	+	Δ	-	Elev
BM	2.51	917.08		914.57
	3.22	911.68	8.62	908.46
				899.08
0+42		So Inv 24" x 97' Conc P.P.		
0+00		Σ C.P.C		906.75
+11		Edge Pavc		906.60
+20		Shld C.P.C		906.50
+37				902.90
+47				899.80
+47		No Inv 24" Conc		897.41
T.P	5.19	904.84	12.03	899.65
1+00				898.7
2+00				898.3
3+00				898.1
4+00				897.3

Lt

R

Rt

Top Mon Cleve + Co Rd C

12.60

493

508

52

88

11.9

1427

6.1

W.S
5.70 899.14

65

6.7

68 78.0
100

W.S
5.72 899.12

7.5

97.6 97.5
7.2 7.30
100 138

Sta	+	Δ	-	Elev
		904.84		
5+00				898.9.
6+00				898.9.
T.P.	2.08	905.59	1.33	903.51
7+00				898.9.
8+00				899.0.
9+00				899.2.
T.P.	5.75	910.59	1.25	904.34.
10+00				899.8.
11+00				901.4.
+50				902.0.
12+00				901.6.
13+00				899.6.
14+00				899.4.
15+00				899.4.

Lt

R

Rt

97.9

98.0

59

$\frac{69}{100}$

$\frac{68}{200}$

98.1

98.6

59

$\frac{67}{100}$

$\frac{62}{200}$

- 67

$\frac{7.0}{100}$

$\frac{69}{150}$

$\frac{66}{100}$

$\frac{67}{50}$

66

$\frac{55}{100}$

$\frac{63}{200}$

$\frac{61}{250}$

$\frac{64}{100}$

64

$\frac{61}{50}$

$\frac{59}{100}$

$\frac{10.2}{200}$

$\frac{10.8}{100}$

$\frac{11.3}{95}$

10.3

$\frac{10.6}{50}$

$\frac{10.6}{100}$

$\frac{8.2}{85}$

$\frac{11.0}{82}$

$\frac{8.7}{78}$

8.7

$\frac{10.2}{100}$

8.1

$\frac{11.2}{61}$

8.5

$\frac{12.2}{55}$

10.5

$\frac{12.9}{40}$

10.7

$\frac{12.6}{26}$

10.7

Sta	+	X	-	Elev
		918.09		
16 +00				901.4
B.M.	5.72	914.07	1.74	908.35
16 + 87.6		beg. 20" Tile line		897.13
17 +00				900.7
+ 44				902.3
18 +00				907.6
19 +00				905.7
20 +00				903.3
I.P.	6.47	908.98	14.56	902.51
20 +35		End 20" Tile line		896.38
21 +00				898.7
21 +81		beg. 24" X Drain		895.80
22 + 32		End 24" X Drain		895.83
23 +00				896.9

Lt.

£

Rt.

$\frac{12.2}{13} \quad 8.7$

Top Conc. Tel. Marker 60' R1 17+44

16.94 F.I.

13.4

11.8

6.5

8.4

10.8

12.60 F.I.

10.3

897.08

$\frac{11.9}{\text{Low spot}}$

13.18 F.I.

13.15 F.I.

12.1

Sta	+	π	-	Elev
		908.98		
24 + 00				896.9.
25 + 00				896.7.
26 + 00				896.7.
B.M.	471	908.05	5.60	903.38 903.34
27 + 00				897.0.
27 + 77		36" X Drain		897.12.
+ 86				901.6.
28 + 13				901.8.
+ 25 ²⁷		End 36" Drain		897.05.
+ 50				897.1.
29				897.2.
+ 50				896.9.
36				897.3

Lt

¢

RT

$$\frac{12.1}{5} \quad 121$$

$$\frac{12.3}{5} \quad 123$$

W.S. 899.26

972

$$\frac{12.3}{5} \quad 123$$

SPK in Light Pole S.E. Cor. "C 2" + Cleveland Ave

111

$$\frac{113}{50}$$

10.93

6.5

$$\frac{08.05}{11.20} = 96.75$$

6.3

11.0

11.0

899.27

10.9

$$\frac{10.8}{50}$$

W.S.
8.78

11.2

10.8

$$\frac{11.6}{5}$$

Sta	+	π	-	Elev
		908.05		
31+00				896.8.
32+00				896.7.
33+00				896.8.
TP	5.98	910.43	360	904.45
34				897.1.
35				897.4.
+80 ⁴⁵				896.07.
		Beg 21" Vit Sewer Line		
+85				901.9.
+95				902.8.
36				904.6.
+09				908.0.
+20				908.2.
+31				903.4

Lt

Z

Rt

899.37

113

 $\frac{11.5}{4}$ $\frac{113}{50}$ 45
968

114

113

13.3

130

14.36

8.5

7.6

5.8

2.4

2.2

7.0

Sta	+	Δ	-	Elev
		910.43.		
36	+50			902.8.
37				903.5.
	+50			904.5.
38				905.1.
	+50			904.3.
39				904.6.
T.P.	7.39	913.45	4.37	906.06.
	+18			904.7.
	+22			902.2.
	+41			900.6.
	+58			904.7.
	+79 ²⁶	Ben M. H		905.03
40				905.1.

2

7.6

6.9

5.9

5.3

6.1

5.8

8.8

11.3

12.9

8.8

Top M.H.

8.42

896.02

Inv

1717.43

8.4

Sta	+	$\bar{X}$	-	Elev
		913.45.		
40+50				905.1.
41				907.5.
T.P.	494	910.09	8.30	905.15.
+50				905.8.
42				905.0.
+50				904.4.
43				903.7.
401.75		Cor M.H.		904.09.
+50				903.1.
44				903.1.
+50				902.6.
45				902.0.
+50				901.7.

2

3

84

6.0

43

51

5.7

L4

895.49

Top M.H

Inv

6.00

14.60

40

70

75

8.1

8.4

Sta	+	π	-	Elev
		910.09		
46				901.9.
BM	3.70	909.69	414	905.95 905.99
+52				903.99.
		(Note Elev of Sewer was obtained where Co open hole above sewer)		
+73				902.8.
+93				906.9.
47				907.6.
+36				907.0.
+50				903.1.
48				902.4.
+50				902.5.
49				902.8.
+50				903.7.
50				903.9.
T.P	3.54	910.66	2.57	907.12

2

82

SpK in R.P. Blt Sta 46+73

5.70 $\frac{1414}{Inv}$ 895.55

6.8

28

2.1

2.7

6.6

7.3

7.2

6.9

6.0

5.8

Top Fe Post Sta 50+00

Sta + X - Elev

910.66

50+50 902.1

51 902.1

+50 903.7

52 903.1

+50 902.4

+67.89 MH 902.2

53 902.2

+50 902.8

54 902.8

+50 902.5

55 903.7

+50 902.2

T.P. 5.91 911.93 4.64 906.02

2

8.6

8.6

7.0

7.6

8.3

895.03

8.5

15.63
Inv

8.5

7.9

7.9

8.2

7.0

8.5

Sta	+	Δ	-	Elev
		911.93		
56				902.0
+50				901.8
57				902.0
+50				902.4
58				903.6
+50				904.6
59				905.4
+50				906.7
60				907.0
+50				907.6
+52				907.9
+58				909.8
T.P	5.10	915.54	1.49	910.44

$\frac{1}{2}$

9.9

10.1

9.9

9.5

8.3

7.3

6.5

5.2

4.9

4.3

4.0

2.1

Sta	+	Δ	-	Elev	
		915.54			
B.M	0.34	915.60. 915.50	0.34	915.20	915.26
60+90				909.9	
+95				908.4	
61				908.0	
+50				909.8	
62				909.6	
+50				909.3	
63				909.0	
+50				908.6	
+52				908.5	
+60				905.62	
64				905.4	
T.R	2.52	96. 911.86	6.16	944. 909.34	
+50				905.1	

Σ

Top N.W. Cor Btm Step at Ho 70' Lt Sta 60400

5.7

7.2

7.6

5.8

6.0

6.3

6.6

7.0

7.1

798
 Top East Rail

10.2

6.9

Sta	+	Σ ⁹⁶ 911.86	-	Elev
65				904.4
+24				904.87
+50				904.0
66				903.6
T.P.	783	⁸¹ 911.71	798	⁹⁸ 903.88
+21.92				903.83
+50				902.8
67				902.6
+50				902.6
68				902.7
+50				901.6
69				902.2
+50				902.6

$\frac{1}{2}$

7.6

 $\frac{7.09}{\text{East Rail}}$

8.0

8.4

894.91

 $\frac{7.98}{7.74 \text{ M.N.}}$
 $\frac{\text{Int}}{1690}$

9.0

9.2

9.2

9.1

10.2

9.6

9.2

Sta	+	π	-	Elev
		911.71 ⁸¹		
70				900.6
+50				900.1
T.P.	2.30	908.83 ⁹³	5.18	906.53 ⁶³
71				899.2
+50				899.7
+90				900.4
72				902.3
+12				903.1
+48				904.49
+70				904.67
73				903.9
+08				904.2
+45				901.1
+56				894.62

2

112

11.7

97

92

8.5

6.6

5.8

444
Top Rail426
Top Rail

5.0

4.7

78

~~14.7~~ 3.0

Sta	+	Δ	-	Elev
		908.83 ⁹³		
B.M	2.16	908.89	2.15	906.78 ⁷⁸
73+56		(End Sewer)	93.98	97.71
+56		(X Sect.)		95.7
				97.9
74				96.5
+50				95.4
75				95.1
+50				95.5
76				95.1
+50				95.3
77				95.0
+50				95.2
B.M	3.13	909.86	2.16	906.73
78				95.3
+50				95.2

Lt

♀

Rt

Top Bolt N.E. Bolt of Switch 33' Lt Sta

897.71
11.18
1491
Inv 893.98

$\frac{48}{17} \frac{40}{13} \frac{61}{9} \frac{77}{7} \frac{101}{5} \frac{132}{3} 132 \frac{132}{3} \frac{64}{7} \frac{67}{15} \frac{72}{25} \checkmark$

$\frac{36}{25} \frac{47}{20} \frac{61}{13} \frac{91}{8} \frac{103}{5} \frac{123}{3} \frac{137}{3-1} \frac{110}{1} 110 \frac{63}{9} \frac{62}{13} \frac{72}{18} \frac{78}{25} \checkmark$

$\frac{41}{27} \frac{48}{18} \frac{50}{10} \frac{67}{10} \frac{80}{8} \frac{91}{6} \frac{113}{3-2} \frac{135}{2} 135 \frac{111}{6-1} \frac{64}{7} \frac{63}{13} \frac{72}{25} \checkmark$

$\frac{26}{35} \frac{54}{27} \frac{74}{21} \frac{75}{12} \frac{90}{7} \frac{103}{5} \frac{112}{3-2} \frac{138}{2} 138 \frac{112}{142} \frac{77}{8} \frac{74}{12} \frac{83}{25} \checkmark$

$\frac{32}{21} \frac{75}{18} \frac{102}{15} \frac{92}{13} \frac{83}{9} \frac{92}{5} \frac{107}{3} \frac{134}{1} 134 \frac{134}{3} \frac{91}{9} \frac{86}{11} \frac{90}{20} \frac{94}{25} \checkmark$

$\frac{52}{27} \frac{113}{1612} \frac{98}{9} \frac{106}{4} \frac{124}{2} 138 \frac{128}{3} \frac{106}{6} \frac{102}{8} \frac{97}{12} \frac{107}{25} \checkmark$

$\frac{29}{31} \frac{99}{22} \frac{120}{15} \frac{109}{11} \frac{105}{97} \frac{111}{4} \frac{122}{2} 136 \frac{128}{4} \frac{110}{6} \frac{103}{15} \frac{117}{19} \frac{119}{25} \checkmark$

$\frac{82}{25} \frac{113}{78} \frac{118}{13} \frac{108}{11} \frac{107}{6} \frac{121}{3} \frac{131}{2} 139 \frac{133}{4} \frac{112}{6} \frac{108}{14} \frac{121}{20} \frac{121}{25} \checkmark$

$\frac{30}{29} \frac{92}{24} \frac{121}{19} \frac{127}{14} \frac{111}{9} \frac{115}{3} \frac{132}{2} 137 \frac{135}{5} \frac{116}{7} \frac{113}{14} \frac{125}{17} \frac{127}{25} \checkmark$

Top Bolt N.E. Cor. of Switch

$\frac{122}{18} \frac{135}{15} \frac{121}{11} \frac{119}{6} \frac{134}{4} 146 \frac{145}{3} \frac{130}{5} \frac{118}{8} \frac{117}{16} \frac{124}{22} \checkmark$

$\frac{130}{16} \frac{133}{14} \frac{123}{11} \frac{122}{6} \frac{135}{3} 147 \frac{138}{4} \frac{127}{7} \frac{115}{9} \frac{119}{24}$

Stg	+	X	-	Elev
		909.86		
79				95.2
+50				95.1
+66				94.3
+72		Toe RR Slope	945	Note Cannot obtain East Inv due to Fill + cribbing
+80				07.1 at East End
+94		East Rail		08.12
+99. ⁵⁰		West Rail		08.12
80+06				07.0
T.P.	5.12	90492	10.06	899.80
+19 ³⁰				93.60
		West End 24' Conc		
+50				95.0
81				94.9
+50				95.0

Lt

R

Rt

$$\frac{12.3}{17} \quad \frac{12.7}{13} \quad \frac{12.5}{10} \quad \frac{12.0}{5} \quad \frac{12.2}{3} \quad 14.7 \quad \frac{13.6}{5} \quad \frac{12.6}{7} \quad \frac{11.3}{9} \quad \frac{11.4}{2.5} \quad \checkmark$$

$$\frac{10.3}{21} \quad \frac{11.0}{16} \quad \frac{12.0}{11} \quad \frac{12.4}{7} \quad \frac{13.3}{5} \quad 14.8 \quad \frac{13.9}{3} \quad \frac{11.5}{6} \quad \frac{11.0}{17} \quad \frac{10.8}{2.5} \quad \checkmark$$

$$\frac{11.0}{20} \quad \frac{12.3}{18} \quad \frac{13.7}{4} \quad 15.6 \quad \frac{13.9}{3} \quad \frac{12.2}{5} \quad \frac{12.4}{14} \quad \frac{12.3}{2.7} \quad \checkmark$$

$$\frac{11.2}{2.5} \quad \frac{11.7}{7} \quad \frac{16.5}{2} \quad 15.0 \quad \frac{14.7}{2} \quad \frac{11.7}{5} \quad \frac{10.8}{12} \quad \frac{11.2}{2.5} \quad \checkmark$$

$$\frac{3.0}{2.5} \quad 2.8 \quad \frac{2.5}{2.5} \quad \checkmark$$

$$1.74 \quad \checkmark$$

$$1.74 \quad \checkmark$$

$$\frac{3.0}{2.5} \quad 2.9 \quad \frac{2.5}{2.5} \quad \checkmark$$

Na:1 14 Cor Fe Root

$$\frac{6.6}{18} \quad \frac{7.2}{4} \quad \frac{11.3}{2} \quad 11.32 \quad \frac{11.3}{2} \quad \frac{7.4}{4} \quad \frac{5.3}{8} \quad \frac{5.0}{2.5} \quad \checkmark$$

$$\frac{7.0}{2.5} \quad \frac{6.7}{6} \quad 9.7 \quad \frac{9.2}{5} \quad \frac{5.9}{11} \quad \frac{5.4}{2.5} \quad \checkmark$$

$$\frac{6.9}{2.5} \quad \frac{6.1}{5} \quad \frac{8.9}{3} \quad 10.0 \quad \frac{8.9}{4} \quad \frac{6.4}{8} \quad \frac{5.2}{12} \quad \frac{5.3}{2.5} \quad \checkmark$$

$$\frac{6.0}{2.5} \quad \frac{5.9}{8} \quad \frac{8.9}{4} \quad 9.9 \quad \frac{8.8}{4} \quad \frac{5.0}{12} \quad \frac{5.1}{2.5} \quad \checkmark$$

Sta	+	π	-	Elev
-----	---	-------	---	------

904.92

82				94.9
----	--	--	--	------

+50				94.8
-----	--	--	--	------

83				95.0
----	--	--	--	------

+50				95.0
-----	--	--	--	------

84				95.2
----	--	--	--	------

T.P	5.69	906.81	3.80	901.12
-----	------	--------	------	--------

+50				95.0
-----	--	--	--	------

85				95.1
----	--	--	--	------

+50				95.0
-----	--	--	--	------

86				94.9
----	--	--	--	------

+50				94.9
-----	--	--	--	------

+81				95.3
-----	--	--	--	------

87				96.1
----	--	--	--	------

Lt

2

Rt

$$\frac{5.7}{25} \quad \frac{5.3}{10} \quad \frac{8.9}{3} \quad 10.0 \quad \frac{9.0}{4} \quad \frac{7.9}{12} \quad \frac{4.9}{25} \quad \checkmark$$

$$\frac{5.6}{25} \quad \frac{5.9}{11} \quad \frac{8.7}{3} \quad 10.1 \quad \frac{8.6}{4} \quad \frac{5.4}{12} \quad \frac{5.1}{25} \quad \checkmark$$

$$\frac{4.0}{25} \quad \frac{4.2}{10} \quad \frac{9.0}{4} \quad 9.9 \quad \frac{8.9}{4} \quad \frac{6.3}{9} \quad \frac{4.0}{14} \quad \frac{4.1}{25} \quad \checkmark$$

$$\frac{2.8}{25} \quad \frac{3.0}{12} \quad \frac{6.1}{5} \quad \frac{8.3}{3} \quad 9.9 \quad \frac{9.1}{4} \quad \frac{8.0}{6} \quad \frac{3.8}{15} \quad \frac{3.6}{25} \quad \checkmark$$

$$\frac{2.9}{25} \quad \frac{3.5}{13} \quad \frac{7.0}{10} \quad \frac{8.7}{5} \quad 9.9 \quad \frac{8.3}{4} \quad \frac{5.9}{11} \quad \frac{4.0}{13} \quad \frac{3.9}{25} \quad \checkmark$$

$$\frac{5.3}{25} \quad \frac{5.4}{15} \quad \frac{6.8}{10} \quad \frac{10.7}{5} \quad 11.8 \quad \frac{10.2}{5} \quad \frac{8.7}{7} \quad \frac{5.3}{12} \quad \frac{3.9}{25} \quad \checkmark$$

$$\frac{5.5}{25} \quad \frac{6.2}{12} \quad \frac{8.4}{8} \quad \frac{11.0}{3} \quad 11.7 \quad \frac{10.3}{6} \quad \frac{8.4}{8} \quad \frac{5.1}{16} \quad \frac{4.3}{25} \quad \checkmark$$

$$\frac{4.9}{25} \quad \frac{5.4}{16} \quad \frac{8.8}{7} \quad \frac{11.4}{3} \quad 11.8 \quad \frac{10.4}{5} \quad \frac{7.6}{8} \quad \frac{4.7}{12} \quad \frac{3.3}{25} \quad \checkmark$$

$$\frac{4.9}{25} \quad \frac{6.1}{13} \quad \frac{8.2}{5} \quad \frac{11.3}{4} \quad 11.9 \quad \frac{9.9}{3} \quad \frac{8.1}{7} \quad \frac{5.0}{12} \quad \frac{4.1}{25} \quad \checkmark$$

$$\frac{4.6}{25} \quad \frac{5.6}{16} \quad \frac{9.2}{6} \quad \frac{10.7}{3} \quad 11.9 \quad \frac{10.8}{6} \quad \frac{9.0}{8} \quad \frac{9.4}{14} \quad \frac{5.3}{16} \quad \frac{4.0}{25} \quad \checkmark$$

Ditch

$$\frac{7.0}{25} \quad \frac{7.4}{14} \quad \frac{11.7}{7} \quad \frac{12.8}{4} \quad 11.5 \quad \frac{10.8}{4} \quad \frac{8.9}{7} \quad \frac{7.5}{15} \quad \frac{6.2}{17} \quad \frac{5.0}{25} \quad \checkmark$$

Ditch

$$\frac{5.2}{25} \quad \frac{5.6}{14} \quad \frac{8.0}{10} \quad \frac{12.1}{7} \quad \frac{12.4}{4} \quad 10.7 \quad \frac{10.7}{4} \quad \frac{8.8}{11} \quad \frac{6.3}{16} \quad \frac{5.4}{25} \quad \checkmark$$

Sta	+	π	-	Elev
-----	---	-------	---	------

906.81.

87+50

92.1.

T.P.

248

903.39

5.90

900.91.

88

92.8.

+50

95.6
96.6.

89

94.7.

B.M.

303

903.05

3.39

900.00

900.02

+48

94.6.

+50

98.6.

+63

98.6.

+64

94.4.

90

94.6.

+50

95.0.

91

94.6.

+50

94.8.

LX

2

RX

Ditch

$$\frac{5.9}{25} \frac{5.7}{17} \frac{11.6}{10} \frac{12.1}{4} \frac{12.0}{4} 9.7 \frac{8.7}{3} \frac{6.3}{10} \frac{6.0}{25}$$

Ditch

$$\frac{3.2}{25} \frac{3.5}{17} \frac{5.5}{13} \frac{7.3}{7} \frac{8.6}{4} \frac{7.4}{2} 5.6 \frac{3.0}{8} \frac{3.3}{17} \frac{2.7}{25}$$

Ditch

$$\frac{3.6}{25} \frac{3.9}{17} \frac{6.4}{11} \frac{8.2}{8} \frac{8.8}{5} 7.8 \frac{5.9}{4} \frac{4.1}{9} \frac{3.6}{25}$$

$$\frac{4.0}{25} \frac{4.5}{19} \frac{5.5}{10} \frac{8.5}{5} 8.7 \frac{7.3}{5} \frac{4.3}{12} \frac{4.3}{25}$$

Top Men $\frac{1}{2}$ sec 35 95.21 $5\frac{1}{4}$ Cor NE $\frac{1}{4}$ sec 32

$$\frac{2.6}{25} \frac{5.2}{10} \frac{6.1}{6} 8.5 \frac{7.8}{4} \frac{8.9}{4} \frac{4.8}{7} \frac{4.4}{18} \frac{4.2}{25}$$

$$\frac{2.6}{25} \frac{3.2}{14} \frac{3.7}{7} 4.5 \frac{4.1}{25}$$

$$\frac{2.6}{25} \frac{3.2}{14} \frac{3.7}{7} 4.5 \frac{4.1}{25}$$

$$\frac{2.6}{25} \frac{3.2}{14} \frac{6.4}{4} 8.7 \frac{7.9}{4} \frac{6.5}{7} \frac{5.1}{10} \frac{4.1}{25}$$

$$\frac{3.9}{10} \frac{6.0}{6} \frac{7.2}{5} \frac{8.5}{2} 8.5 \frac{8.5}{2} \frac{6.7}{5} \frac{4.7}{12} \frac{4.9}{25}$$

$$\frac{7.3}{25} \frac{7.3}{13} \frac{7.7}{9} \frac{8.4}{6} \frac{8.4}{3} 8.1 \frac{8.1}{1} \frac{7.6}{2} \frac{5.5}{6} \frac{5.3}{25}$$

$$\frac{5.9}{25} \frac{6.0}{11} \frac{7.7}{6} \frac{7.8}{2} \frac{8.5}{1} 8.5 \frac{8.5}{2} \frac{6.9}{6} \frac{5.3}{10} \frac{4.9}{25}$$

$$\frac{6.7}{25} \frac{6.4}{11} \frac{8.2}{7} \frac{8.5}{2} 8.3 \frac{7.8}{6} \frac{5.6}{11} \frac{5.4}{25}$$

Sta	+	Δ	-	Elev
-----	---	----------	---	------

90305

92				94.3
----	--	--	--	------

+50		End Ditch		95.7
-----	--	-----------	--	------

93				93.9
----	--	--	--	------

T.P.	3.81	899.19	7.67	895.38
------	------	--------	------	--------

94				92.8
----	--	--	--	------

95				92.0
----	--	--	--	------

96				91.1
----	--	--	--	------

97				92.5
----	--	--	--	------

98				90.9
----	--	--	--	------

99				89.7
----	--	--	--	------

100				91.6
-----	--	--	--	------

T.P.	5.06	899.08	5.17	894.02
------	------	--------	------	--------

101				90.9
-----	--	--	--	------

102				92.1
-----	--	--	--	------

Lt

Z

Rt

$$\frac{79}{25} \quad \frac{79}{18} \quad \frac{69}{10} \quad \frac{81}{6} \quad \frac{81}{3} \quad \frac{88}{2} \quad 8.8 \quad \frac{88}{2} \quad \frac{75}{5} \quad \frac{79}{25}$$

$$\frac{84}{25} \quad \frac{81}{6} \quad 74 \quad \frac{82}{25}$$

9.2

64

7.2

8.1

93.76
W.S.
5.43

67

8.3

95

7.1

8.2

70

Sta	+	Δ	-	Elev
		899.08		
103				92.7.
104				91.6.
105				90.9.
106				91.9.
T.P.	407	900.36 900.26	2.79	896.19
107				92.2.
108				91.7.
157 ⁹⁵		Bcg Pitch #2		92.3.
109				92.3.
B.M.	3.63	900.23	3.63	896.63
+50				93.2.
110				92.9.
+50				92.7.
111				92.6.

Lt

Rt

Rt

64

75

82

72

82

6.7

8.1

8.1

SpK in Twin 12" Oak 10 Rt Sta 109+30

70

7.3

76

76

Sta	+	π	-	Elev
		900.23		
111+50				92.4
112				92.7
+50				92.9
T.P.	7.62	902.26	5.59	894.64
113				92.7
+50				92.6
114				92.9
+50				93.2
T.P.	6.87	907.25	1.88	900.38
+67 ⁴⁸		Beq 30" CM X Drain		91.38
+76				96.3
+93				05.7
115				05.7
+20				05.6

L+

Σ

R+

7.8

7.5

7.3

9.6

9.7

9.4

9.1

15.87

11.0

1.6

1.6

1.7

Sta	+	π	-	Elev
		907.25		
115+30				98.6
+38				95.5
+44				95.7
+47 ³⁵		End	30" CM	90.79
116				92.6
+50				93.0
T.P.	5.83	901.62	1146	895.79
117				92.0
+50				92.0
+62 ⁹⁰		Beg	36" Conc Pipe	91.34
+77				99.9
183				00.06
+83 ⁵⁰				99.8

LT

~~R~~

RY

8.7

11.8

716

16.46

147

143

96

96

10.28

1.7

1.56

1.80

Sta	+	π	-	Elev
		901.62		
117	+97			99.99.
118	+07			99.81.
	+08			99.94.
	+15			99.7
+29 ⁶⁰		End 36" Core Pipe		91.07.
	+50			91.9.
119				91.6.
	+50			91.5.
120				91.8.
	+50			91.4.
121				91.5.
	+16			91.5.

Lt

R

Rt

1.63

1.81

1.68

1.9

10.55

9.7

10.0

10.1

9.8

10.2

10.1

10.1

Sta	+	π	-	Elev
		901.62		
121+42.84				91.4
+57		Beq 39" Iron	R.R. P.c (So End 39")	90.32
T.P.	1122	912.84	0.00	901.62
+88				10.5
122				11.6
+18				11.3
T.P.	0.27	899.53	1358	899.26
+46.71		R.R. Culv. (No End 43")		90.26
123				90.9
+50				90.7
124				90.7
+50				90.4
125				90.4
B.M.	696	903.38	3.04	896.49 896.52
+50				90.6

Lt

2

Rt

10.2

11.30

2.3

1.2

1.5

9.27

86

88

88

91

9.1

Spk in 24" G.H. 10' Lt 5t9 124t 91

12.8

Sta	+	π	-	Elev
		903.38		
126				90.6
+50				90.7
127				90.6
+50				90.4
128				90.1
+50				90.1
129				89.8
+46.34		Bag 36" CM		89.98
+50				93.5
+69				02.4
+95				02.2
+12				92.9
T.P	8.5L	901-20	10.74	892.64

Lt

L

Rt

12.8

127

12.8

130

133

133

136

13.40

9.9

1.0

1.2

10.5

Sta	+	X	-	Elev
		901.20		
130+21 ¹⁸		End 36" CM		89.60
+50				89.7
131				89.7
+50				89.2
132				88.9
+50				88.2
133				87.8
T.P	3.47	894.44	10.23	890.97
+50				87.9
134				87.4
+50				87.1
135				86.5
+50				86.3

~~£~~

1160

115

11.5

120

12.3

130

134

6.5

70

73

79

8.1

Sta + Δ - Elev

894.44

136

86.1

+50

85.9

B.M

1.17

894.44

1.17

893.27

893.27

137

85.6

+50

85.4

138

84.8

+50

84.4

139

84.0

+50

83.4

140

83.8

B.M

1.17

893.24

893.29

Z

8.3

8.5

SpK in 12" Oak 10' RT 136+90

8.8

9.0

9.6

10.0

10.4

11.0

10.6

SpK in 12" Oak 10' RT Sta 136+90

