

Bk. 11 - Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

EAGLE ST.

From Park Ave To Bald Eagle Blvd. E.

Road Acc't. No.

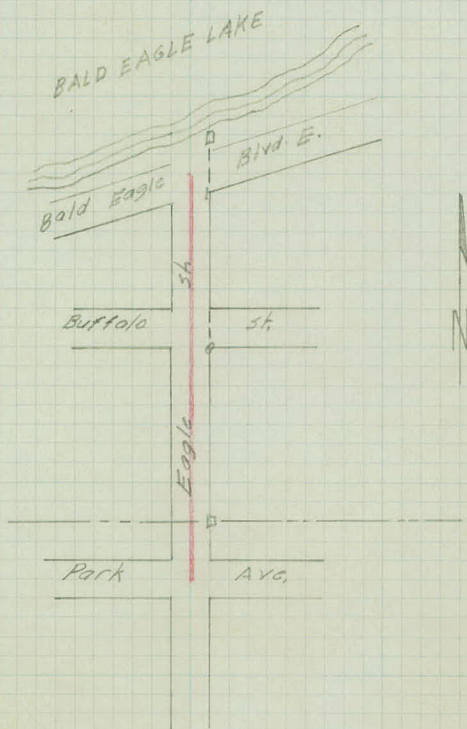
Date Filed 10/24/29

File

PLAN SURVEY

EAGLE AVE.

Park Ave to Bald Eagle Blvd. E.

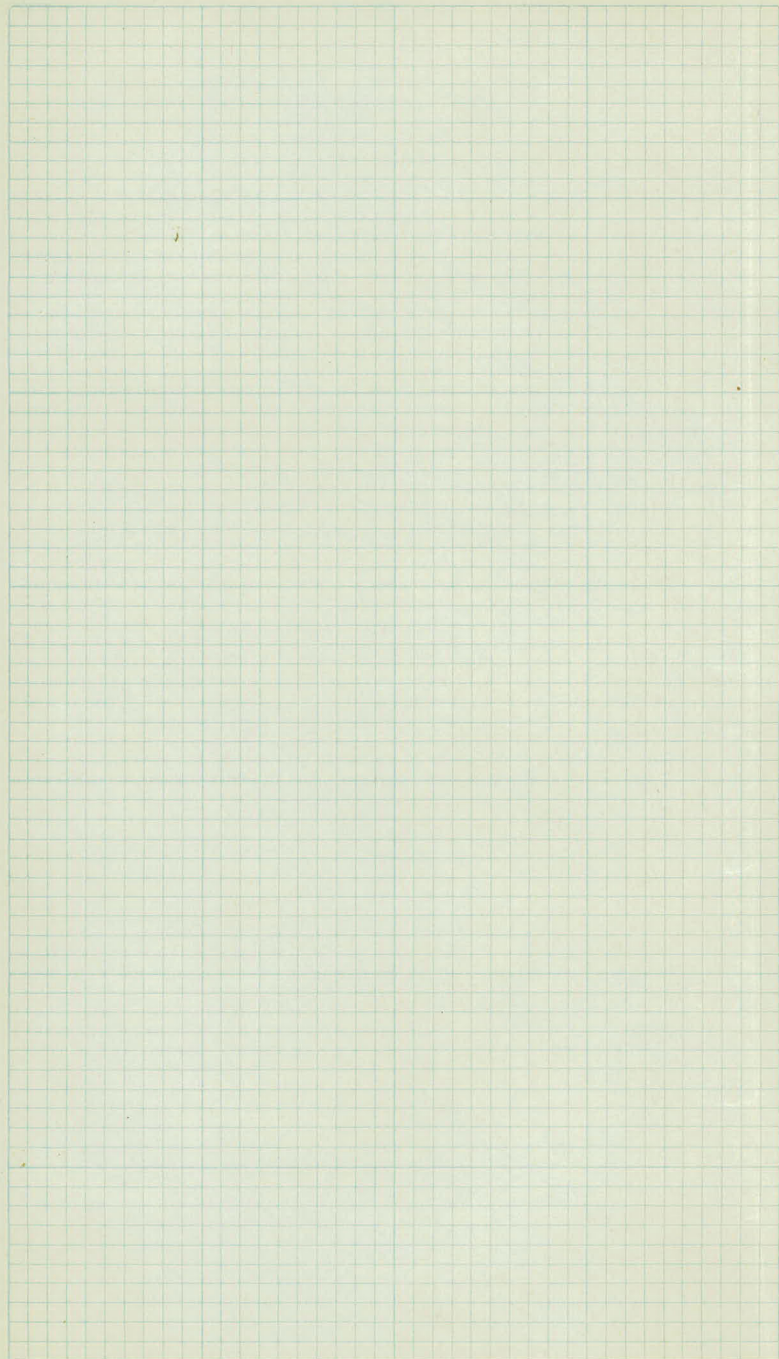


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Align. - 1-2

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Alignment.

Sta.	Point	ΔL	ΔR
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21	+05.57	P.O.T. = E. Black Top Bald Eagle Blvd. E.	
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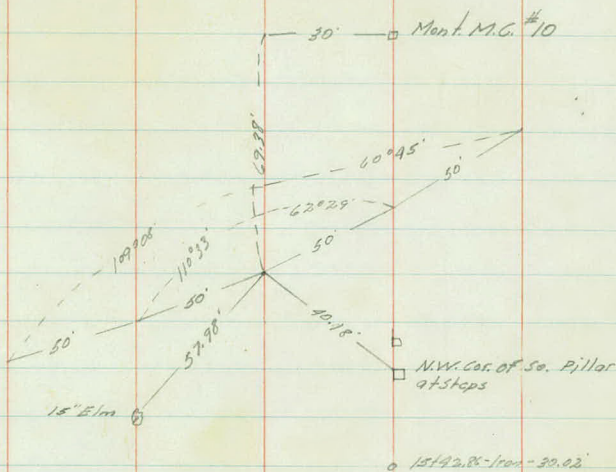
1A	+83.50	P.I.	$0^{\circ}01'30''$
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1	+63.38	P.I.	$0^{\circ}05'$
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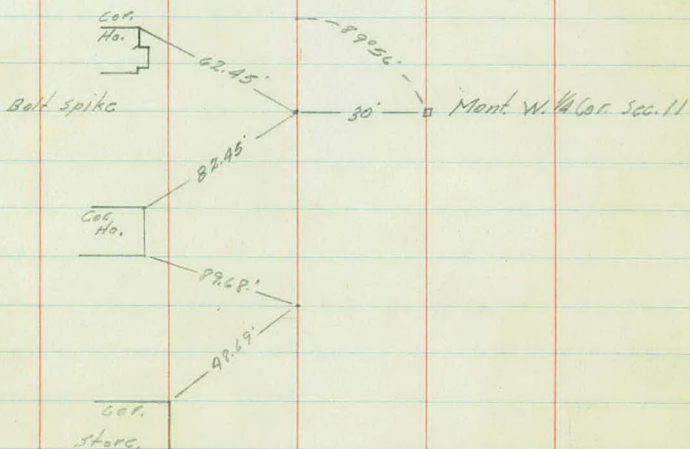
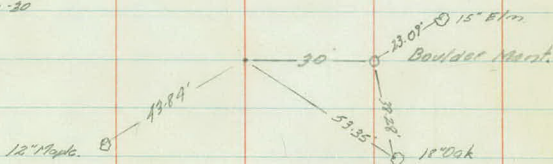
0	+00	P.O.T. = E. Por. Park Ave.	
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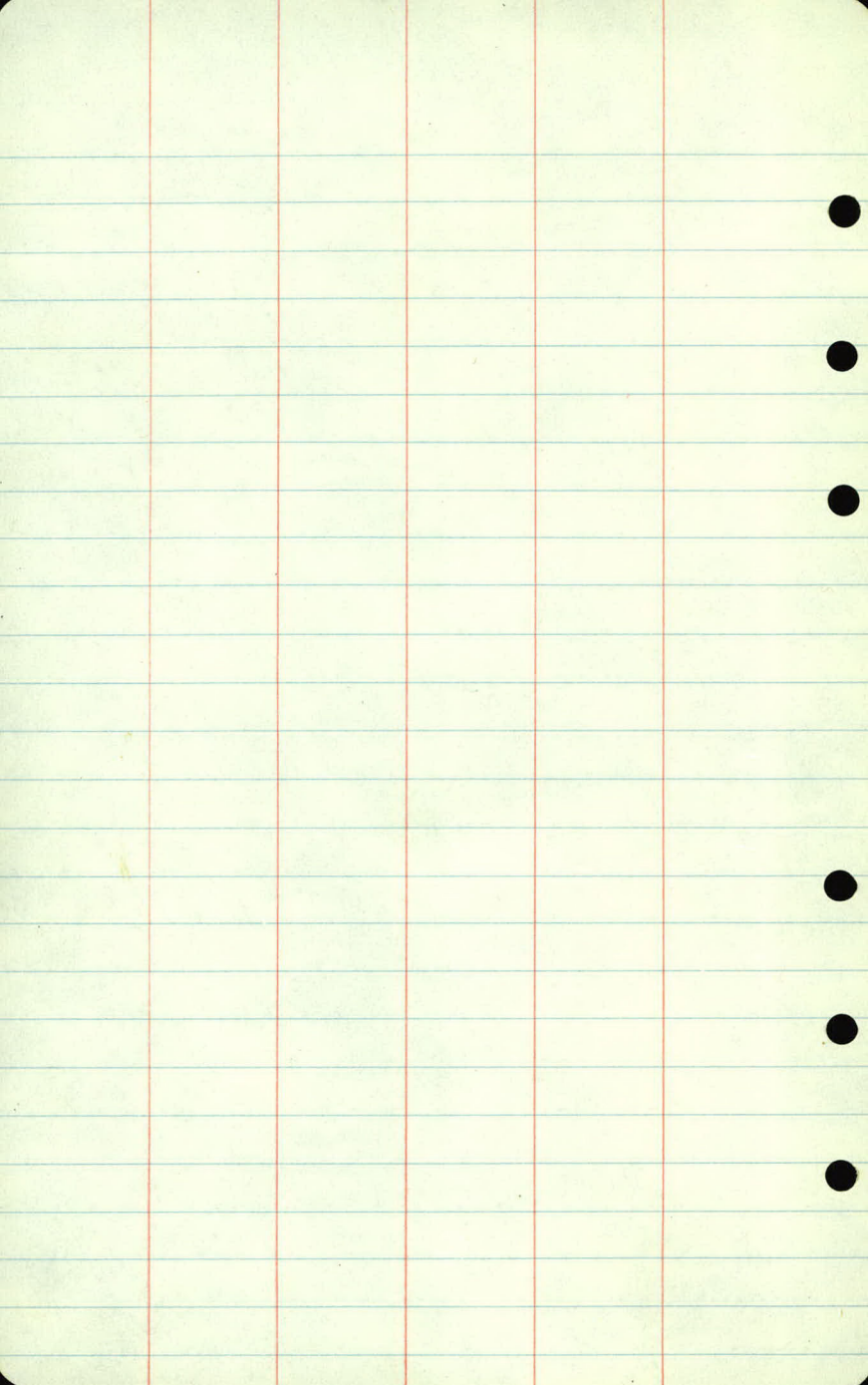
312137
K.H.
L.B.H.
L.C.
A.B.

2



$14486.94 - \text{Iron} - 30'$
Belt spike





Topography

Ent.
+92-End Brush-36'

+85-P.P.-

5
+32-Beg. Brush-34'
+05-Grow 6-6" Elder-27'
+90-Ditch

8' 9'

+01-Fe. Cor.-30'

+66-Light P.-28'

+25-Ent.

1
9' 9'

+35-P.P.-28'

3
9' 10'

+73-30" Willow-38'
+65-2 15" X 39 C.M.
17' 10'

2
8' 10' P.P.-27'

+90-42" Willow-31'
+73-6" Apple-31'
+70-10" Elm-30'

+41-Cor. Ho.-63'
+21-15" Elder-20'
Ent.

9' 10'

Ent.

+90-Shrub-22'
+85-Shrub-18'
+80-Shrub-18'
+70-Cor. Ho.-55'

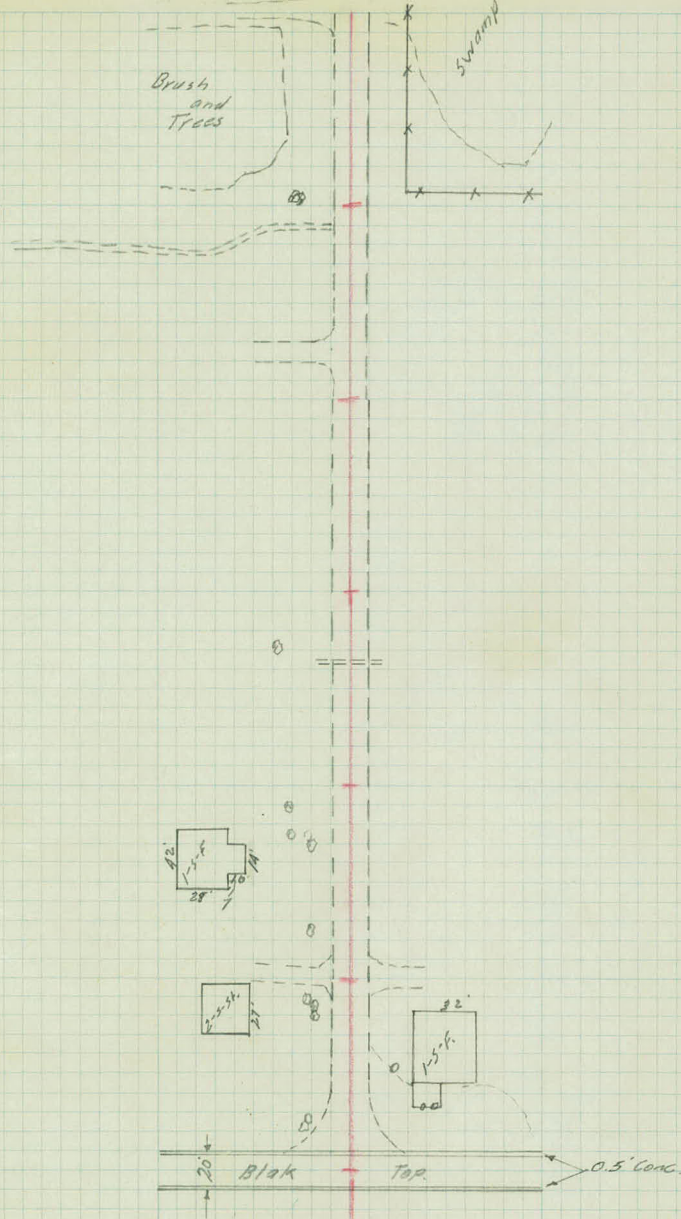
+82-Cor. Gar.-32'
+70-P.P.-27'
+51-Air Pump-23'
+45-Cor. Gar.-22'

+40- 10'

+26-Shrub-23'
+23-Shrub-22'
+19-T.P.-25'

+34-Shrub-32' -50'
Pump-39'-46'

0+00



+95-15" B. Elder - 15"

+72-Cor Ho - 62

469-5hrub-20

766-5 shrub - 2.7'

42-3" Type - 20

453-15 Elm - 19

137-Ent-12"X15"6. N7-13'

+29-24" Elm - 19' + End Brush

403-15" Oak-24'

490-RP-28

784-Cor. H-26-29

477-Encl - 12" X 16" C.M. - 15"

122-Cor Ho. - 62'

195- Bcg. 41/400 Hcd/90 32'

174 Ent - 10" x 20' C 17 - 19'

42-PP-28

438'-8' August - 19'

4-15 Locust - 32'

105-8" Tw. Locust - 30'

402-Ent-10" x 16" C. 19-19'

181-End. Hedge-32.

489-18" X Elm - 33'

467-15° Birch - 34'

420 Bes. H. 190-31

115-Enl-10" x 14" C. 12-18

405-PP-28' 8" East - 31'

Aug. 8th 1905

+73-6" Locust - 29'

193-12" Locust - 32'

479-6 'Locust-87'

+ 74.5" locust - 27'

467-3' E/42-22'

73J-E10A-12" x 20' C.M. - 17

HC 2-8 Dec. 28

145. P.D. - 28

138-Ent.

+ 26.14924-19.

 $+20.6^{\circ} \text{ Oct } 30^{\circ}$

106-Fe. Cor. - 30'

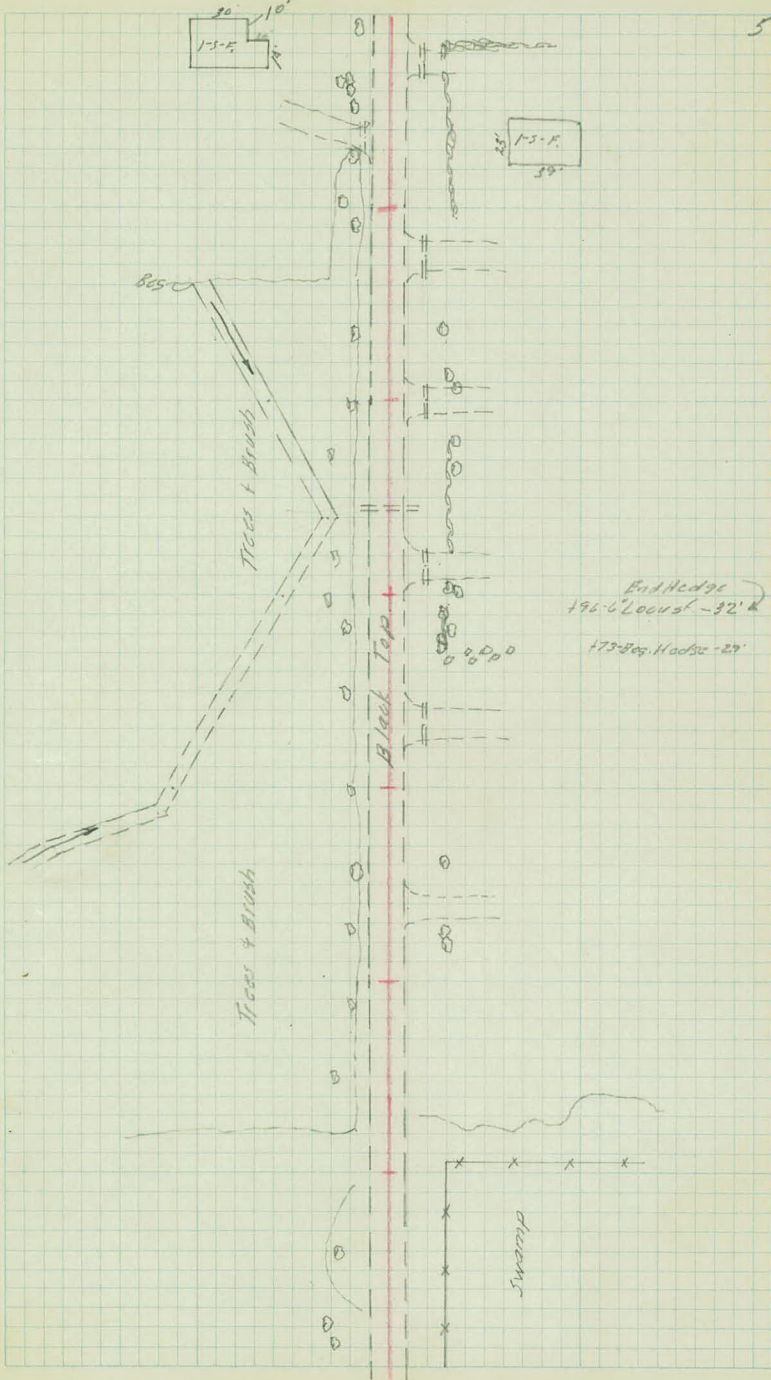
103-PP

+21-Box Road - A140013-17

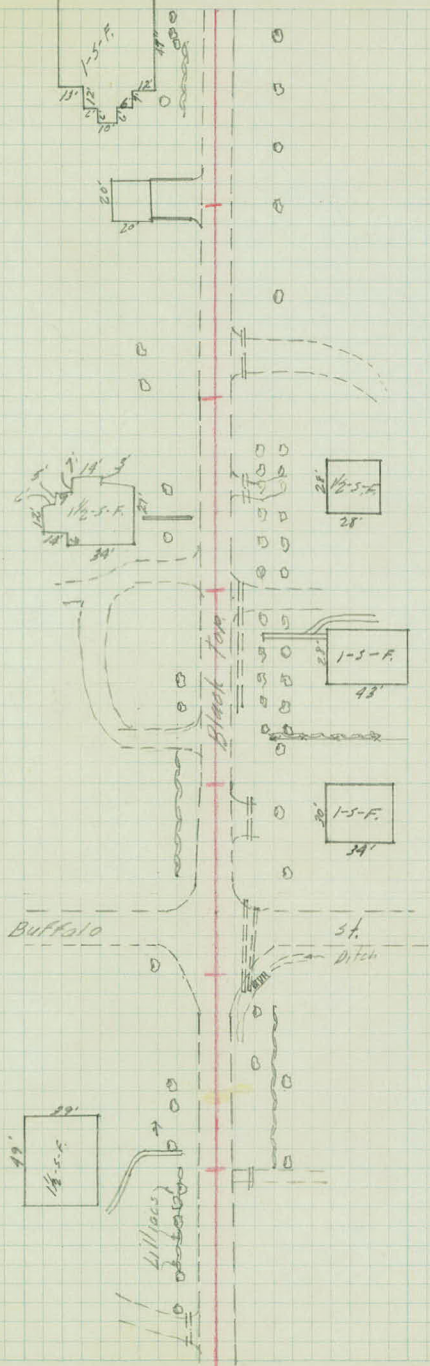
460-1st Spruce-27'

$+24-13^{\circ}00' - 31'$

113-1" SURFACE - 28"



- 198-6" Pine - 22'
 188-6" Pine - 22'
 188-End Hedge - 16' 3" Pine - 20'
 159-Cor Ho. - 31'
 153-30" Oak - 28'
 145-Beg Hedge - 16'
 141-Conc. Wall - 13'
 191-Conc. Wall 13.4' Cor Cor - 58'
- 187-P.R. - 27'
 153-18" Oak - 33'
 136-P.R. - 27'
 122-Ent - 12" x 22" C.M. - 15'
 178-End Row Elm - 22' 35'
 153-S.W. Ent - 10" x 10" C.M. - 15'
 140-Cor Ho. - 57'
 120-P.R. - 28'
 102-N End 10" C.M. - 14'
 193-Ent -
 197-8.3' Walk - 23'
 152-Cor Ho. - 57'
 190-3 End 12" C.M. - 14'
 128-Beg Row Elm - 25' - 30'
 129-Hedge - 27'
 123-End Fe - 29'
 119-12" Oak - 34'
 187-28" Oak - 34'
 181-Ent - 15" x 20" C.M. - 15'
 170-Cor Ho. - 57'
 153-10 Oak - 30'
 149-P.R. - 28'
 139-End 12" C.M. - 16'
 135-Ent 12" C.M. - 22'
 132-N Edge 81' Tree
 119-S Edge 81' Tree
 180-9' Board Walk - 22'
 149-4-9' Board Walk - 20'
 171-5 End 12" C.M. - 15-17'
 183-Ent Hedge - 31'
 180-18" Oak - 21'
 159-12" Oak - 20'
 146-18" Oak - 34'
 105-P.R. - 28' 108-150' 35'
 85 Hedge - 30'
 190-24" Oak - 18'
 152-6" Mossy Ash - 20'
 172-Pine - 20'
 144-18" Elm - 15'
 126-18" Elm - 20' Redwood Hedge
 117-Ent - 10" x 16" C.M. - 13'
- 191-Long Wall 13.4' Cor Cor - 58'
 125-8" Apple - 38'
 108-6" Apple - 37'
 153-18" Oak - 26'
 138-8-16" Board Walk - 12'
 128-8" B. Elm - 25'
 124-Cor Ho. - 42'
 109-Ent -
 154-Shrub - 18'
 140-Shrub - 18'
 123-Ent -
 114-End Hedge - 18'
 152-Beg Hedge - 20'
 140-G.R. - 21'
 106-18" Elm - 31'
 143-18" Maple - 24'
 128-Cor Ho. - 61'
 132-15 Ash - 22'
 117-Pump - 30.5'
 111-15" Red Oak - 28'
 107-8-16" Walk - 18'
 End Hedge - 18'
 190-24" Oak - 18'
 152-6" Mossy Ash - 20'
 172-Pine - 20'
 144-18" Elm - 15'
 126-18" Elm - 20' Redwood Hedge
 117-Ent - 10" x 16" C.M. - 13'
- 7' 9' Beg Row 24" Oak - 32'
 8' 8'
 8' 9'
 8' 8'
 8' 9'
 8' 8'
 10' 9'
 7' 17'
 9' 8'
 9' 8'
 9' 10'



21

122-6.0 X 6

27'

H. End 12" C. A. 2. 40' 40. D. in Wall 41'

24'

D. in Wall 33'

167-15" Elm - 41'

180- 21'

185- 4' SW - 32.6'

166-3" Pine - 23'

+79- 5' 1" Conc. Wall - 32'

+62-12" Birch - 24'

12" 167' 402- 4" B. Elder - 32'

+87-2" Pine - 24'

158- 6'

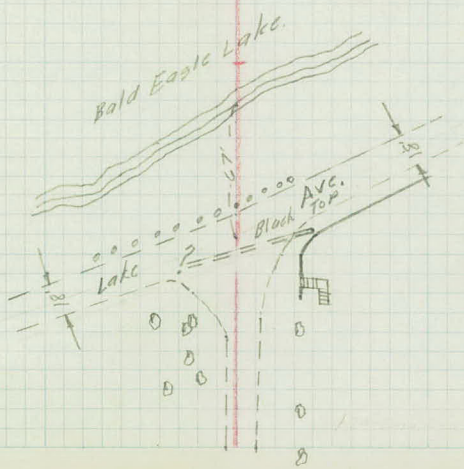
+25-36" Oak - 18'

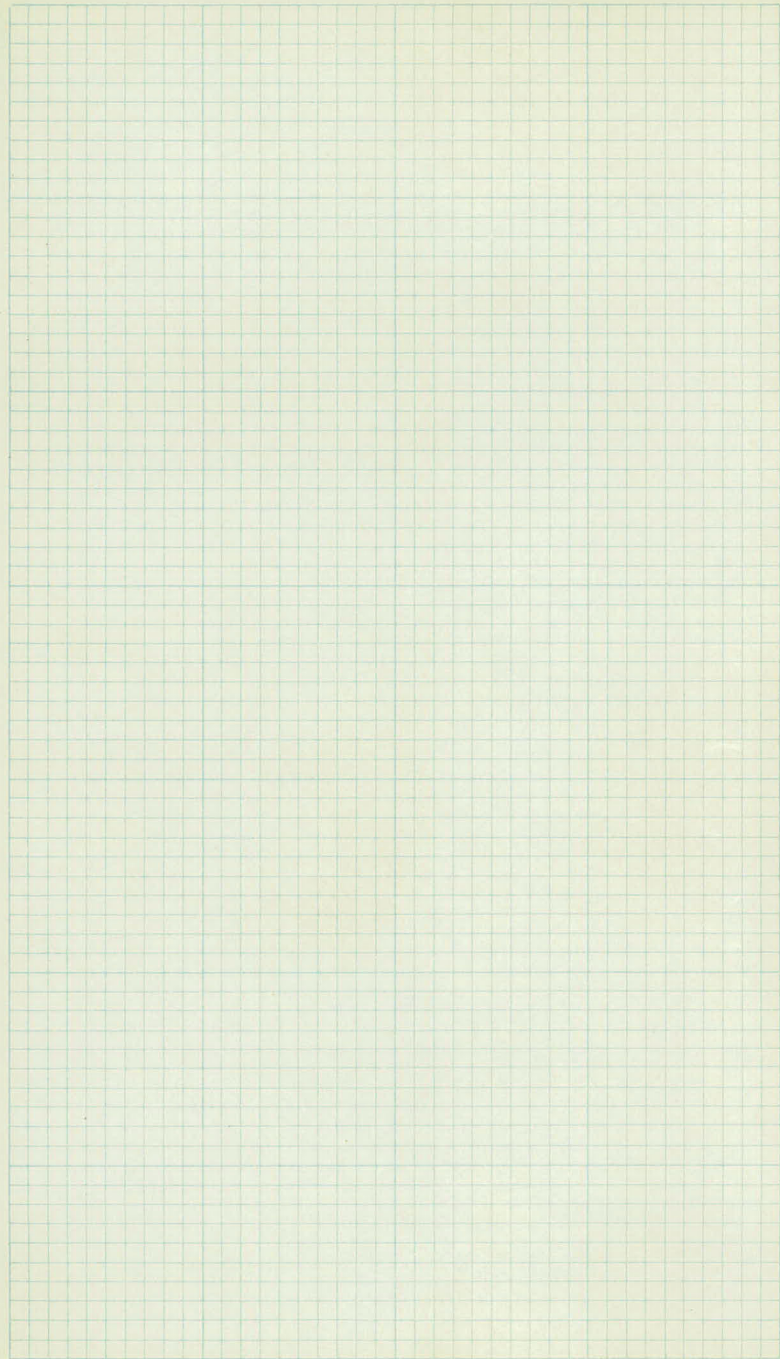
+32-36" Oak - 36'

+20- End Rev. Traces - 33'

20

6' 10'





8

x sections

Sta	+	-	Elev.
B.M.	4.29	926.79	(922.50)
I.P.	6.55	927.79	5.55 921.24
I.P.	7.77	931.68	3.88 923.91
B.M.		5.16	926.52
I.P.	7.75	935.50	3.93 927.75
B.M.		2.19	933.21
B.M.	5.36	927.86	(922.50)
0	+00		24.8
+10			924.71 ⁶¹
+28			24.2
+50			23.6
1			23.7
+50			23.0
2			22.7
+60			22.1

44

2

RF

Top Mont. W. $\frac{1}{4}$ Cor. Sec. 11

Top of Boulder Mant. 30' Bt. 19+83.5

Top N.W. Cor. Bottom Step 33' Rt. 20186

Top Mont. w. $\frac{1}{4}$ Cor. Sec. 11

[illegible]

Sta T A - E/cv

927.86

2 465 2 Culv.

3 22.1

450 22.2

T.R. 5.20 927.12 593 921.93

480 22.2

4 22.1

450 21.8

490 ditch Lt. 21.8

5 21.8

450 22.1

6 22.1

450 21.9

Lt

\$

Rt

17.07

17.89

10.79
Flow Line

9.97
Flow Line

19.9 19.3 19.3 20.9 21.5 20.0
 $\frac{80}{50} \frac{86}{30} \frac{86}{16} \frac{10}{11} \frac{64}{8} \frac{59}{9} \frac{63}{11} \frac{66}{14} \frac{79}{17} \frac{76}{19} \frac{73}{50}$

19.9 19.3 19.9 21.5 21.8 2.20 21.7 20.6 21.7
 $\frac{80}{50} \frac{86}{41} \frac{86}{16} \frac{10}{10} \frac{64}{7} \frac{61}{7} \frac{57}{9} \frac{59}{12} \frac{62}{15} \frac{73}{17} \frac{73}{19} \frac{65}{34} \frac{60}{50} \frac{6.2}{50}$

19.3

20.4

20.6

$\frac{78}{50} \frac{77}{33} \frac{67}{14} \frac{55}{11} \frac{52}{8} \frac{49}{9} \frac{52}{12} \frac{54}{15} \frac{65}{16} \frac{65}{19} \frac{59}{29} \frac{55}{32} \frac{51}{50} \frac{53}{50}$

19.1 19.7

20.1

$\frac{89}{50} \frac{80}{36} \frac{74}{15} \frac{60}{11} \frac{54}{8} \frac{50}{8} \frac{54}{12} \frac{57}{14} \frac{70}{18} \frac{70}{19} \frac{60}{27} \frac{63}{27} \frac{54}{33} \frac{53}{50}$

19.3

20.1

$\frac{78}{50} \frac{78}{15} \frac{62}{12} \frac{57}{8} \frac{53}{7} \frac{55}{12} \frac{59}{15} \frac{70}{18} \frac{70}{20} \frac{65}{30} \frac{64}{50} \frac{58}{50}$

18.6 18.4

18.2

19.3

19.9

End of 85 87 89 88 82 63 59 53
 Ditch 205 150 100 50 72 72 8

18.8 18.9 19.4

20.0

$\frac{83}{50} \frac{82}{40} \frac{77}{15} \frac{60}{11} \frac{57}{8} \frac{53}{8} \frac{56}{12} \frac{59}{14} \frac{69}{19} \frac{71}{20} \frac{66}{20} \frac{68}{50}$

19.7

20.2

$\frac{66}{50} \frac{68}{37} \frac{74}{22} \frac{70}{15} \frac{61}{12} \frac{55}{8} \frac{50}{8} \frac{53}{13} \frac{57}{16} \frac{69}{19} \frac{60}{20} \frac{63}{41} \frac{69}{50}$

20.4

20.7

21.6

21.3

20.3

20.5

20.0

19.4

$\frac{64}{50} \frac{67}{34} \frac{69}{17} \frac{56}{10} \frac{52}{8} \frac{50}{9} \frac{55}{12} \frac{58}{15} \frac{68}{21} \frac{66}{29} \frac{71}{50} \frac{77}{50}$

20.2

21.8

20.9

19.4

18.4

18.2

18.5

$\frac{63}{50} \frac{64}{33} \frac{69}{22} \frac{68}{15} \frac{58}{11} \frac{54}{8} \frac{52}{8} \frac{57}{11} \frac{62}{15} \frac{87}{30} \frac{89}{39} \frac{86}{50}$

Top Water 5/13/39

Sta + A - E/cv.

927.13

7

21.9

+25

22.1

T.P

4.76

927.31 ✓

4.52

922.61

+35

22.3

8

22.6

+50

22.8

9

22.7

+50

22.8

+77

22.8

10

22.7

+40

22.5

11

23.0

LT

2

LT

199

21.2

196 200 195 196

$\frac{68}{50} \frac{71}{28} \frac{72}{15} \frac{60}{12} \frac{55}{8} \frac{52}{5}$

$\frac{59}{9} \frac{75}{15} \frac{71}{23} \frac{76}{31} \frac{75}{50}$

204

209

216

214

201

208

199

$\frac{67}{50} \frac{69}{34} \frac{62}{16} \frac{55}{11} \frac{52}{8} \frac{50}{5}$

$\frac{55}{7} \frac{57}{11} \frac{68}{14} \frac{70}{19} \frac{66}{20} \frac{72}{50}$

2 sks 8

207

205

207

220

218

206

205

216

209

$\frac{72}{50} \frac{69}{36} \frac{63}{19} \frac{67}{16} \frac{67}{15} \frac{58}{12} \frac{53}{9} \frac{51}{5}$

$\frac{54}{8} \frac{56}{16} \frac{69}{14} \frac{69}{16} \frac{58}{19} \frac{65}{50}$

217

218

219

224

222

212

211

226

226

231

$\frac{67}{50} \frac{66}{44} \frac{54}{16} \frac{60}{15} \frac{60}{14} \frac{54}{12} \frac{50}{9} \frac{48}{5}$

$\frac{50}{7} \frac{52}{11} \frac{62}{13} \frac{63}{16} \frac{48}{19} \frac{48}{24} \frac{41}{26} \frac{46}{50}$

214

218

227

224

216

216

232

237

240

$\frac{60}{50} \frac{56}{31} \frac{56}{13} \frac{52}{11} \frac{49}{9} \frac{46}{5}$

$\frac{47}{7} \frac{50}{11} \frac{58}{15} \frac{58}{19} \frac{42}{21} \frac{37}{25} \frac{34}{50}$

181

200

205

225

221

210

207

224

221

231

Flings 93
Ditch 114

$\frac{74}{50} \frac{72}{53} \frac{69}{16} \frac{53}{11} \frac{51}{9} \frac{47}{5}$

$\frac{49}{8} \frac{53}{10} \frac{64}{14} \frac{67}{17} \frac{50}{21} \frac{53}{26} \frac{43}{50}$

211

227

222

212

207

219

219

227

$\frac{62}{50} \frac{60}{36} \frac{63}{14} \frac{52}{10} \frac{50}{9} \frac{46}{5}$

$\frac{47}{8} \frac{52}{11} \frac{62}{13} \frac{67}{16} \frac{55}{21} \frac{55}{24} \frac{47}{50}$

196

209

226

222

209

221

219

224

224

$\frac{78}{50} \frac{66}{26} \frac{54}{14} \frac{51}{11} \frac{49}{8} \frac{46}{5}$

$\frac{48}{8} \frac{52}{11} \frac{65}{16} \frac{65}{18} \frac{53}{21} \frac{53}{26} \frac{50}{50}$

191

197

207

226

223

209

207

221

220

224

$\frac{83}{50} \frac{83}{55} \frac{77}{25} \frac{67}{16} \frac{55}{12} \frac{51}{9} \frac{47}{5}$

$\frac{48}{8} \frac{51}{11} \frac{66}{15} \frac{67}{17} \frac{53}{21} \frac{54}{24} \frac{50}{50}$

188

198

224

221

205

203

214

212

218

$\frac{74}{50} \frac{72}{36} \frac{86}{23} \frac{86}{22} \frac{76}{30} \frac{75}{16} \frac{59}{11} \frac{54}{7} \frac{49}{5}$

$\frac{50}{8} \frac{53}{10} \frac{69}{14} \frac{71}{17} \frac{60}{20} \frac{62}{29} \frac{56}{41} \frac{52}{50}$

Ditch

200

201

207

210

209

$\frac{71}{63} \frac{84}{61} \frac{84}{60} \frac{84}{50} \frac{67}{32} \frac{64}{16} \frac{53}{11} \frac{48}{8} \frac{44}{9} \frac{47}{12} \frac{60}{14} \frac{65}{17} \frac{50}{22} \frac{51}{27} \frac{46}{50}$

203 194

Sta	+	π	-	Elev.
		92737		
11	+50			23.6
12				23.9
	+50			24.3
I.P.	7.57	932.17	2.77	929.60
13				24.6
	+50			25.2
14				25.9
	+50			26.3
B.M.			5.63	926.54
15				26.9
	+0.6			27.0
	+11			27.7
122				27.0

(926.52)

Lt.

L

Rt.

21.5

22.0

22.5

59	51	49	54	54	45	41	38	41	51	52	46	41	35
50	50	18	16	14	11	8		9	14	18	21	26	50

22.1

22.6

50	48	36	34	47	47	40	38	35	37	39	48	45	37	37	19	18	21
50	34	31	18	15	12	10	8		9	12	16	18	21	27	31	44	50

22.8

22.9

34	37	39	46	46	37	34	31	34	37	45	45	32	34	19	19
50	38	18	14	15	10	8		10	12	15	18	20	25	30	50

23.0

22.7

70	81	91	92	79	76	79	83	92	95	90	85	77
50	29	19	12	9		9	12	15	18	20	35	50

24.0

22.9

76	75	76	83	82	76	73	70	75	86	91	93	87	87	73	88
50	37	16	14	12	10	8		8	11	15	18	19	24	26	50

25.1

23.8

72	71	68	71	70	65	63	65	70	80	59	78	81	79
50	35	19	14	11	8		7	12	16	18	19	27	50

25.0

24.8

60	61	66	72	72	64	63	59	62	65	73	74	67	66	67
50	33	19	17	14	11	9		8	11	15	17	19	32	50

Top of Boulder Mouth 30' at 14182.5

25.7

62	64	65	64	58	53	56	60	57	65	65	57	56
50	33	23	17	11		12	18	21	23	26	27	50

24.7

65	63	61		55	52		53		57	61	57
50	33	19		9			11		26	29	50

68		61		57		50			53		51
50		30		19					25		50

61		52		46
50				50

sta	+	Δ	-	Elev.
		932.17		
15	+34			27.2
	+36			27.2
	+39			27.2
	+74			27.4
16				27.6
	+40			27.6
	+45			27.4
	+85			27.7
17				27.8
	+02			27.8
	+60			28.4
T.P.	5.89	934.66	3.40	928.77

Lt.

R.

Rt.

$$\frac{64}{50} \quad \frac{55}{16}$$

$$\frac{50}{13} \quad \frac{5.2}{13} \quad \frac{54}{25} \quad \frac{6.8}{21} \quad \frac{5.0}{50}$$

$$\frac{67}{50} \quad \frac{65}{33} \quad \frac{58}{16}$$

$$\frac{50}{13} \quad \frac{5.3}{13} \quad \frac{6.2}{50}$$

$$\frac{61}{50} \quad \frac{61}{32} \quad \frac{59}{16} \quad \frac{52}{7} \quad \frac{50}{7}$$

$$\frac{55}{12} \quad \frac{66}{16} \quad \frac{58}{19} \quad \frac{55}{31} \quad \frac{55}{50}$$

$$\frac{51}{30} \quad \frac{51}{29} \quad \frac{46}{19} \quad \frac{57}{16} \quad \frac{57}{12} \quad \frac{51}{10} \quad \frac{50}{8} \quad \frac{48}{8} \quad \frac{53}{11} \quad \frac{55}{15} \quad \frac{6.5}{16} \quad \frac{6.5}{19} \quad \frac{54}{19} \quad \frac{4.9}{50}$$

$$\frac{66}{30} \quad \frac{62}{27} \quad \frac{55}{19} \quad \frac{62}{16} \quad \frac{60}{12} \quad \frac{50}{9} \quad \frac{48}{8} \quad \frac{46}{8} \quad \frac{50}{8} \quad \frac{53}{10} \quad \frac{6.1}{12} \quad \frac{6.8}{15} \quad \frac{5.5}{18} \quad \frac{50}{50}$$

Culv.

$$\frac{37}{50} \quad \frac{75}{21} \quad \frac{46}{15} \quad \frac{53}{10} \quad \frac{51}{8} \quad \frac{46}{8} \quad \frac{49}{8} \quad \frac{52}{11} \quad \frac{6.7}{14} \quad \frac{5.7}{16} \quad \frac{52}{30} \quad \frac{4.4}{50}$$

$$\frac{76}{50} \quad \frac{74}{33} \quad \frac{75}{19} \quad \frac{67}{16} \quad \frac{51}{9}$$

$$\frac{46}{8} \quad \frac{49}{12} \quad \frac{51}{17} \quad \frac{55}{31} \quad \frac{51}{31} \quad \frac{4.4}{50}$$

$$\frac{76}{50} \quad \frac{75}{35} \quad \frac{73}{21} \quad \frac{51}{11} \quad \frac{48}{8} \quad \frac{45}{8} \quad \frac{48}{8} \quad \frac{4.9}{16} \quad \frac{4.4}{31} \quad \frac{3.5}{50}$$

$$\frac{75}{30} \quad \frac{6.9}{30} \quad \frac{6.2}{19} \quad \frac{51}{10} \quad \frac{4.7}{8} \quad \frac{4.4}{8} \quad \frac{4.8}{8} \quad \frac{4.9}{16} \quad \frac{4.2}{32} \quad \frac{3.2}{50}$$

Culv.

$$\frac{4.4}{8} \quad \frac{4.8}{12} \quad \frac{5.3}{13} \quad \frac{6.6}{16} \quad \frac{5.0}{16} \quad \frac{4.4}{25} \quad \frac{3.0}{50}$$

$$\frac{82}{50} \quad \frac{75}{30} \quad \frac{61}{19} \quad \frac{4.4}{10} \quad \frac{4.1}{7} \quad \frac{3.8}{8} \quad \frac{4.0}{8} \quad \frac{4.1}{11} \quad \frac{4.1}{15} \quad \frac{2.3}{18} \quad \frac{1.1}{34} \quad \frac{0.6}{50}$$

Sta	+	π	-	Elev
		934.66.		
18				28.7
	+50			28.8
	+91			29.3
	+91			29.3
19				29.5'
	+50			30.1
20				30.4
F.P.	6.70	937.61.	3.75	930.91
	+50			31.0
	+82			31.0
	+93	Bottom Wall Perpendicular to Rd.		31.0
21				31.1
				31.2
B.M.			4.26	933.35. (933.31)

Lt.

R.

Rt.

$$\frac{113}{50} \quad \frac{121}{29} \quad \frac{89}{16} \quad \frac{65}{10} \quad \frac{62}{8} \quad \frac{60}{7} \quad \frac{61}{10} \quad \frac{67}{12} \quad \frac{65}{15} \quad \frac{47}{18} \quad \frac{37}{31} \quad \frac{34}{50}$$

$$\frac{102}{50} \quad \frac{97}{31} \quad \frac{93}{16} \quad \frac{66}{9} \quad \frac{65}{7} \quad \frac{59}{9} \quad \frac{58}{11} \quad \frac{61}{12} \quad \frac{65}{17} \quad \frac{66}{18} \quad \frac{61}{26} \quad \frac{61}{40} \quad \frac{57}{50}$$

$$\frac{81}{50} \quad \frac{78}{39} \quad \frac{77}{15} \quad \frac{62}{10} \quad \frac{58}{7} \quad \frac{59}{9} \quad \frac{56}{11} \quad \frac{58}{14} \quad \frac{63}{17} \quad \frac{63}{19} \quad \frac{56}{31} \quad \frac{40}{50}$$

$$\frac{625}{32} \quad \frac{691}{13} \quad \frac{58}{7} \quad \frac{54}{7}$$

$$\frac{624}{33} \quad \frac{645}{29} \quad \frac{62}{16} \quad \frac{54}{7} \quad \frac{52}{8} \quad \frac{54}{11} \quad \frac{58}{14} \quad \frac{63}{16} \quad \frac{62}{19} \quad \frac{53}{27} \quad \frac{43}{36} \quad \frac{34}{50}$$

$$\frac{74}{47} \quad \frac{72}{35} \quad \frac{72}{23} \quad \frac{67}{12} \quad \frac{50}{6} \quad \frac{46}{9} \quad \frac{50}{11} \quad \frac{51}{13} \quad \frac{56}{16} \quad \frac{55}{19} \quad \frac{44}{22} \quad \frac{42}{26} \quad \frac{32}{38} \quad \frac{27}{50}$$

$$\frac{74}{32} \quad \frac{75}{16} \quad \frac{52}{8} \quad \frac{47}{5} \quad \frac{43}{9} \quad \frac{47}{11} \quad \frac{47}{13} \quad \frac{50}{16} \quad \frac{47}{18} \quad \frac{37}{24} \quad \frac{38}{36} \quad \frac{17}{50}$$

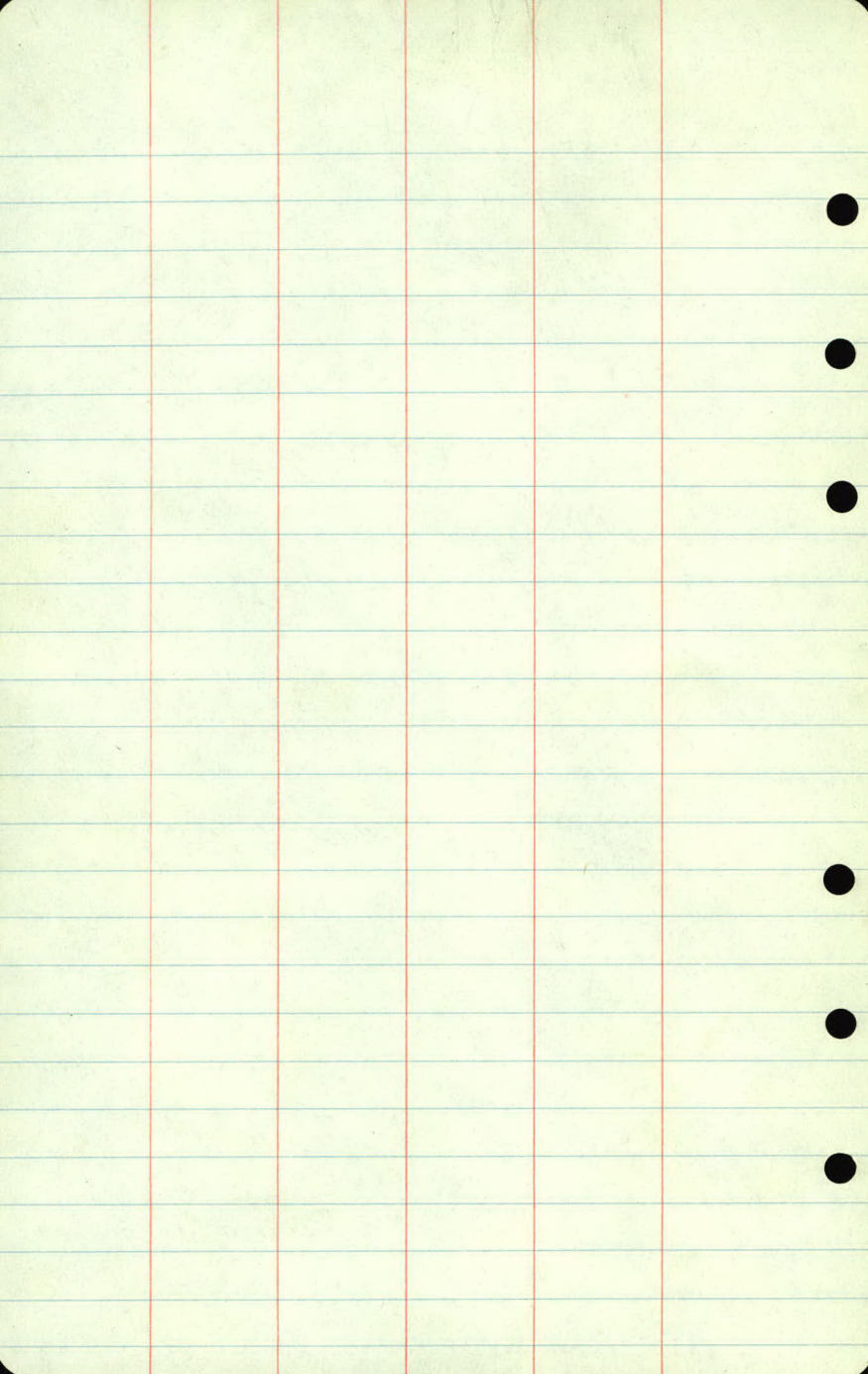
$$\frac{116}{50} \quad \frac{102}{29} \quad \frac{93}{14} \quad \frac{75}{8} \quad \frac{70}{4} \quad \frac{66}{9} \quad \frac{65}{9} \quad \frac{67}{13} \quad \frac{68}{16} \quad \frac{70}{18} \quad \frac{70}{20} \quad \frac{59}{23} \quad \frac{57}{34} \quad \frac{20}{50}$$

$$\frac{101}{50} \quad \frac{99}{34} \quad \frac{72}{7} \quad \frac{66}{6} \quad \frac{63}{14} \quad \frac{64}{19} \quad \frac{64}{23} \quad \frac{51}{28} \quad \frac{48}{40} \quad \frac{00}{50}$$

$$\frac{66}{12} \quad \frac{60}{26} \quad \frac{58}{28} \quad \frac{59}{32} \quad \frac{51}{44} \quad \frac{47}{50} \quad \frac{45}{100}$$

$$\frac{65}{14} \quad \frac{58}{23} \quad \frac{58}{24} \quad \frac{60}{28} \quad \frac{50}{33} \quad \frac{48}{93} \quad \frac{215}{50}$$

$$\frac{7.4}{50} \quad \frac{6.9}{50} \quad \frac{4.0}{50}$$





storm sewer

4 Levels

Eagle Ave.

Sta.	+	π	-	Elev.
3.35	3.35	925.85		922.50

$1+25 =$
 $0+00$

4.0 21.9

+08

4.5 21.4

+27

6.0 19.9

+42

6.5 19.4

+60

6.1 19.8

+85

6.2 19.7

1

6.0 19.9

+50

5.9 20.0

+75

5.4 20.5

2

6.2 19.7

+05

6.1 19.8

Top Mont. E 1/4 Cor. Sec. 11

Mantle/c 0127

2.45' Deep

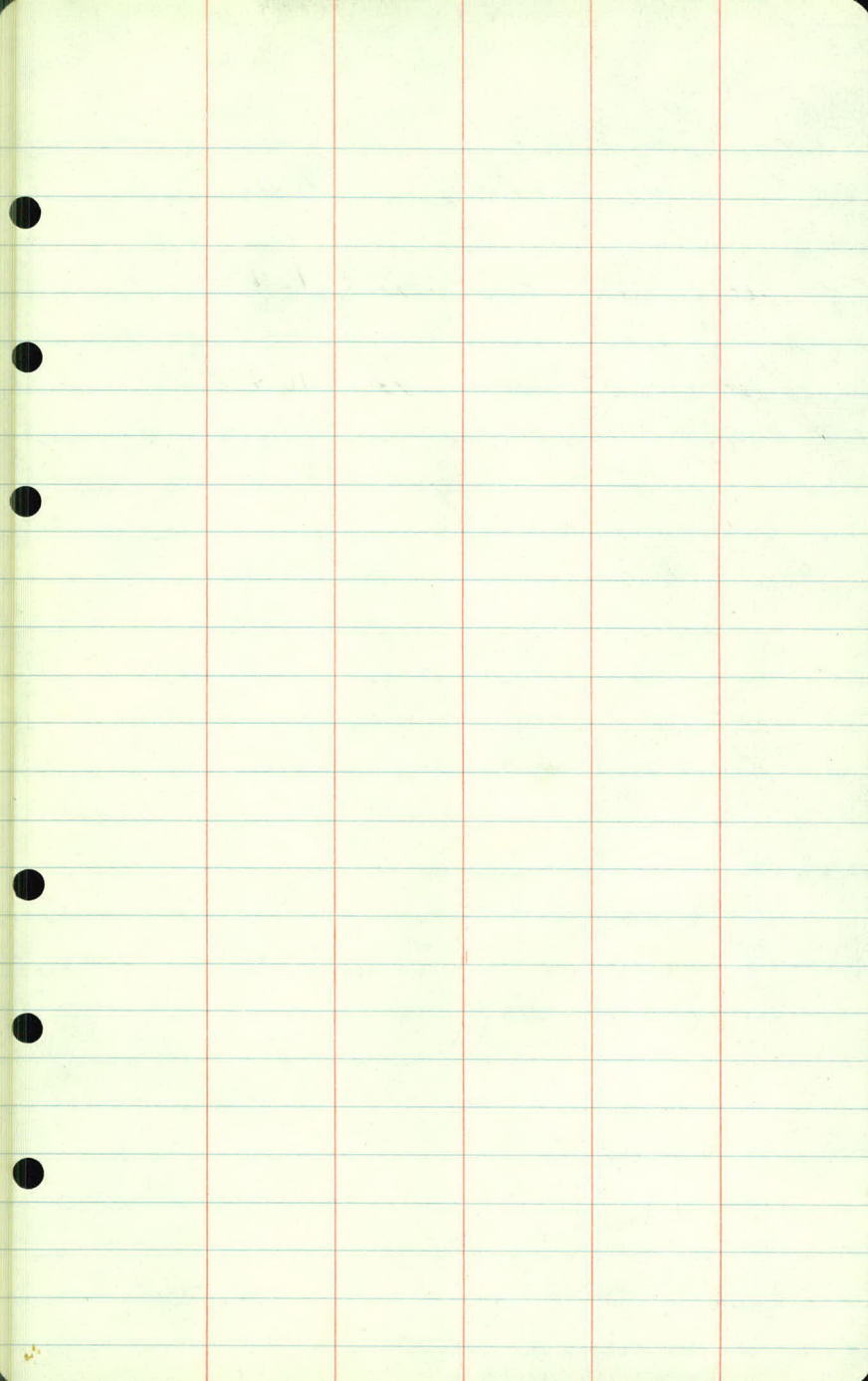
" 1429

2.80' "

" 2133

3.25' "

Sta.	+	π	-	Elev.
		925.85		
2	+07		7.7	18.2
	+09		7.7	18.2
	+10		6.4	19.5
	+29		6.2	19.7
	+39		5.6	20.3
	+50		4.0	21.9
	+66		4.0	21.9
	+71		4.7	21.2
3			6.1	19.8
	+22		6.4	19.5
	+30		7.0	18.9



Sta	+	π	-	Elev.
-----	---	-------	---	-------

		925.85		
--	--	--------	--	--

3	+35			
---	-----	--	--	--

			9.5	
--	--	--	-----	--

				16.4
--	--	--	--	------

	+38			
--	-----	--	--	--

			9.5	
--	--	--	-----	--

				16.4
--	--	--	--	------

B.M.				
------	--	--	--	--

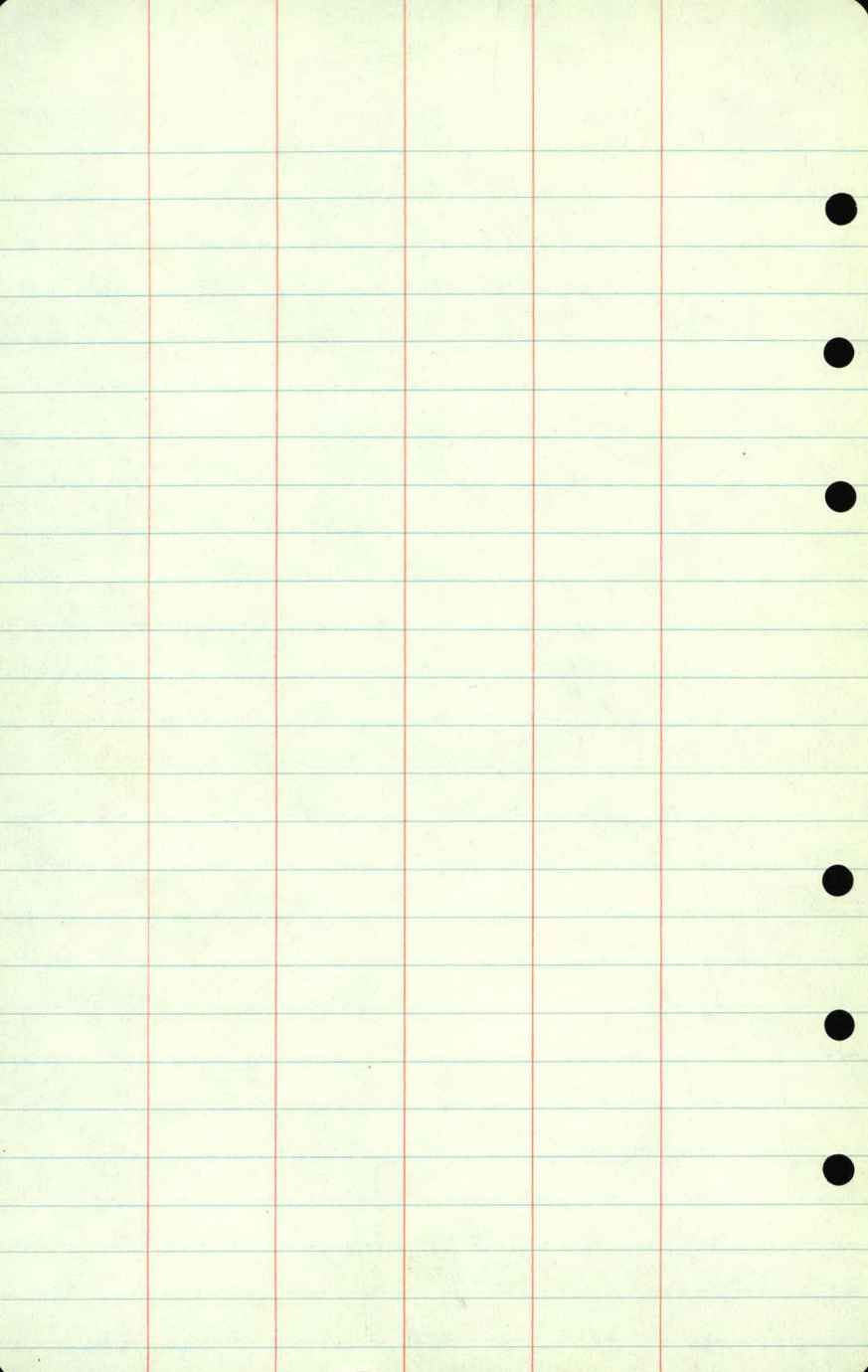
			3.33	
--	--	--	------	--

				922.52
--	--	--	--	--------

				922.50
--	--	--	--	--------

L. Ditch

Top Mont E. $\frac{1}{4}$ Cor. Sec. 11



Eagle Ave
Drainage stakes.

Sta.	+	x	-	Elev
B.M.	5.07	927.57		922.50

22.3

+50

23.0

2 100

22.7

4

pt.

917.9

9.7

4.3

$\frac{58}{205/29.0}$

4.6

47

$\frac{62}{202/29.8}$

4.9

47

$\frac{63}{202/29.2}$

Sta	+	-	Ditch Grade Bl.
B.M.	4.37	926.87	922.50

2	7.00		921.0
---	------	--	-------

	4.65		18.0
--	------	--	------

3			17.93
---	--	--	-------

	4.50		17.83
--	------	--	-------

	4.80		17.79
--	------	--	-------

4			17.73
---	--	--	-------

	4.25		17.7
--	------	--	------

	4.50		17.77
--	------	--	-------

I.P.	4.99	926.83	503	921.84
------	------	--------	-----	--------

5			17.87
---	--	--	-------

	4.50		17.97
--	------	--	-------

6			18.07
---	--	--	-------

C 115/39
K.R.
L.B.H.
L.C.
A.B.

21.0

Gr. Rod.

4

RT.

Top Mont. E. 1/4 Cor. sec. 11 - 30' RT 1163.38

5.9 4.2 54
K.205/25.4

8.9 4.9 76
K.1.3/20.0

9.0 4.9 68
K.2.2/30.0

9.1 4.7 53
K.3.0/30.0

9.1

9.2 4.8 58
K.3.4/30.0

9.2 5.0 60
K.3.7/30.0

9.1 5.0 62
K.3.9/30.0

Nail in T.P.

8.9 5.0 65
K.2.4/30.0

8.8 4.8 59
K.2.7/30.0

8.7 4.7 65
K.2.2/30.0

5/2	+	T	-	inlets broad ft.
		926.83		
6	+30			18.2
T.P.	5.68	927.52		926.89
7				18.8
	+25			19.1
	+55			19.46
8				20.0
	+30			20.3
	+50			20.55
		927.52		
9				20.65
	+50			20.75
	+77			20.8
10				20.85
	+40			20.95
T.P.	205	929.21	5.36	922.16
11				21.05

Toe Rock
slope.

R

Rt.

86

49

81
R.05/30.0

27'

Nail in T.P.

8.7

42

79
R.08/27.8

26.2'

8.4

75
R.07/27.6

25.8

8.0

5

62
R.18/25.9

25.3

7.5

49

44
R.21/30.0

24.4'

7.2

47

39
R.33/30.0

23.8'

6.9

48
22.7

44
R.25/28.0

23.1

6.8

48

54
R.14/25.8

25.1

6.7

47

56
R.11/25.2

25.5

6.7

X

6.6

48

55
R.11/25.2

6.5

50

60
R.05/24.0

8.1

62

71
R.10/25.0

Fig. 1. Soil profile at toe of rock slope.

Sta	+	Σ	-	Grade
-----	---	----------	---	-------

		929.21		
--	--	--------	--	--

11	+50			
----	-----	--	--	--

12				
----	--	--	--	--

	+50			
--	-----	--	--	--

13				
----	--	--	--	--

	+50			
--	-----	--	--	--

14				
----	--	--	--	--

	+50			
--	-----	--	--	--

B.M.				
------	--	--	--	--

		2.65		
--	--	------	--	--

			926.56	
--	--	--	--------	--

				956.52
--	--	--	--	--------

£

Gr. Rod.

Rt.

5.6

$\frac{64}{R.12/25.4}$

5.3

$\frac{54}{R.19/26.8}$

4.9

$\frac{44}{R.22/27.0}$

4.6

$\frac{5.9}{R.27/29.4}$

4.1

$\frac{55}{R.06/24.2}$

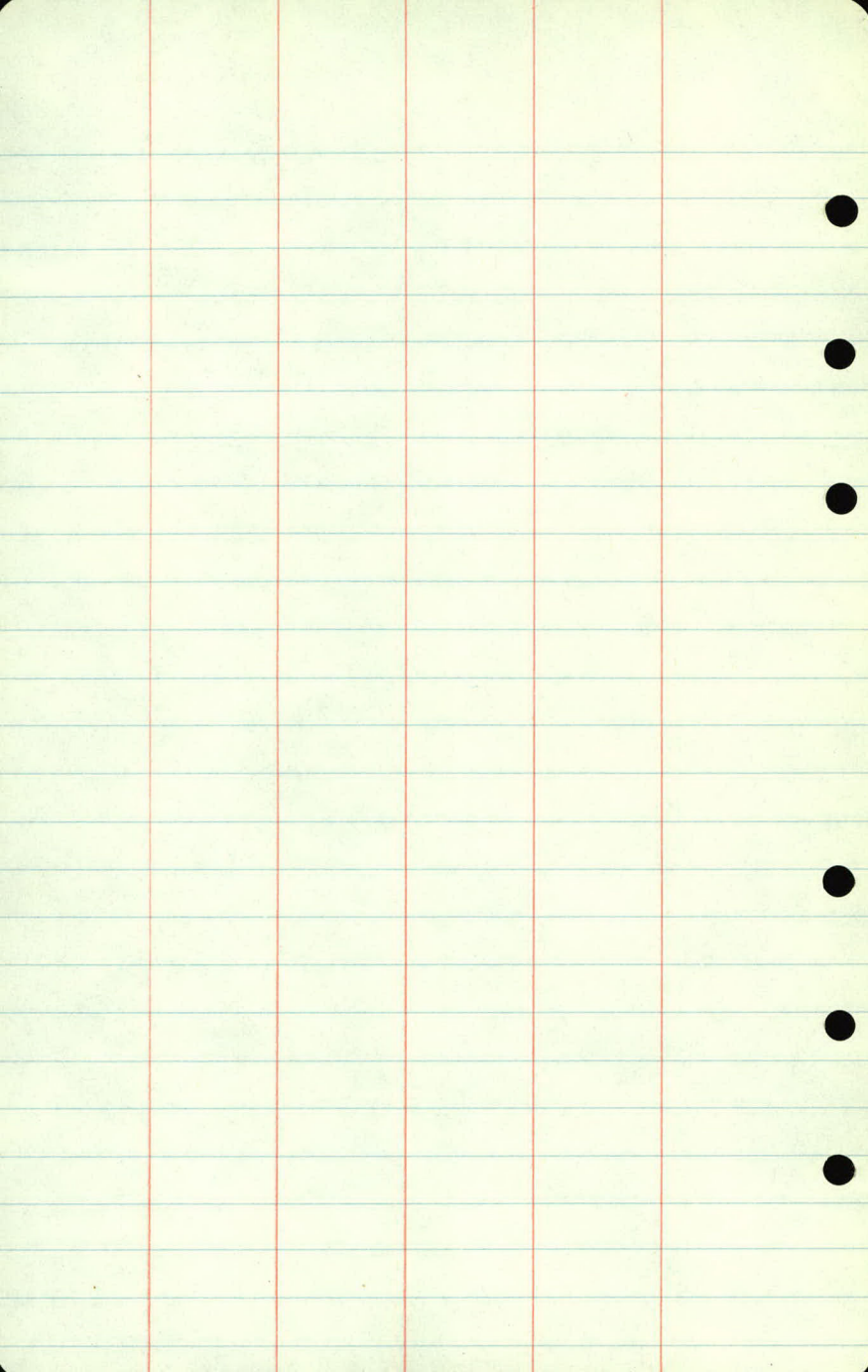
3.3

$\frac{51}{R.02/23.4}$

2.9

$\frac{38}{R.11/25.2}$

Top Boulder Mant 30' L. 14' R. 5'



Grade stakes

Eagle Ave storm sewer

B.M.	4.15	926.65	922.50
------	------	--------	--------

0	-22		917.6
---	-----	--	-------

0	+27		917.45
---	-----	--	--------

	+60		17.35
--	-----	--	-------

1			17.25
---	--	--	-------

	+50	8.62	17.10
--	-----	------	-------

B.M.	322	925.72	-0.3%	922.50
------	-----	--------	-------	--------

2			16.95
---	--	--	-------

	+50		16.80
--	-----	--	-------

3			16.65
---	--	--	-------

	+38		16.50
--	-----	--	-------

Top Mont. E. M. Cor. 500 11

9.05 ✓

9.2 ✓

9.3 ✓

9.4 ✓

9.55 ✓

Top Gr. Stoko 1450 ✓

8.77 ✓

8.92 ✓

9.07 ✓

9.22 ✓

