

Book 100 Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

BIRCH LAKE BLVD. So

From Centerville To Otter Lake Rd

Road Acc't. No. 31

Date Filed. 1-30-43

File.

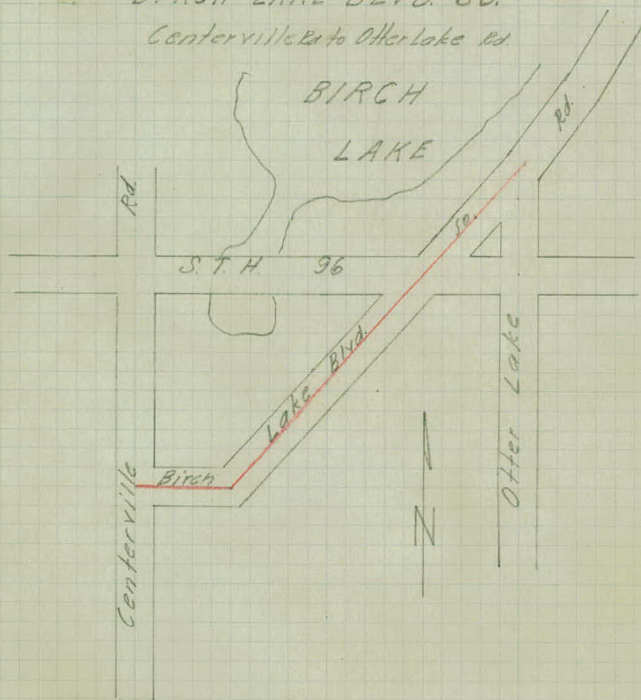
7456
4837
157.7
60

177-2
120 35
1925

PLAN SURVEY

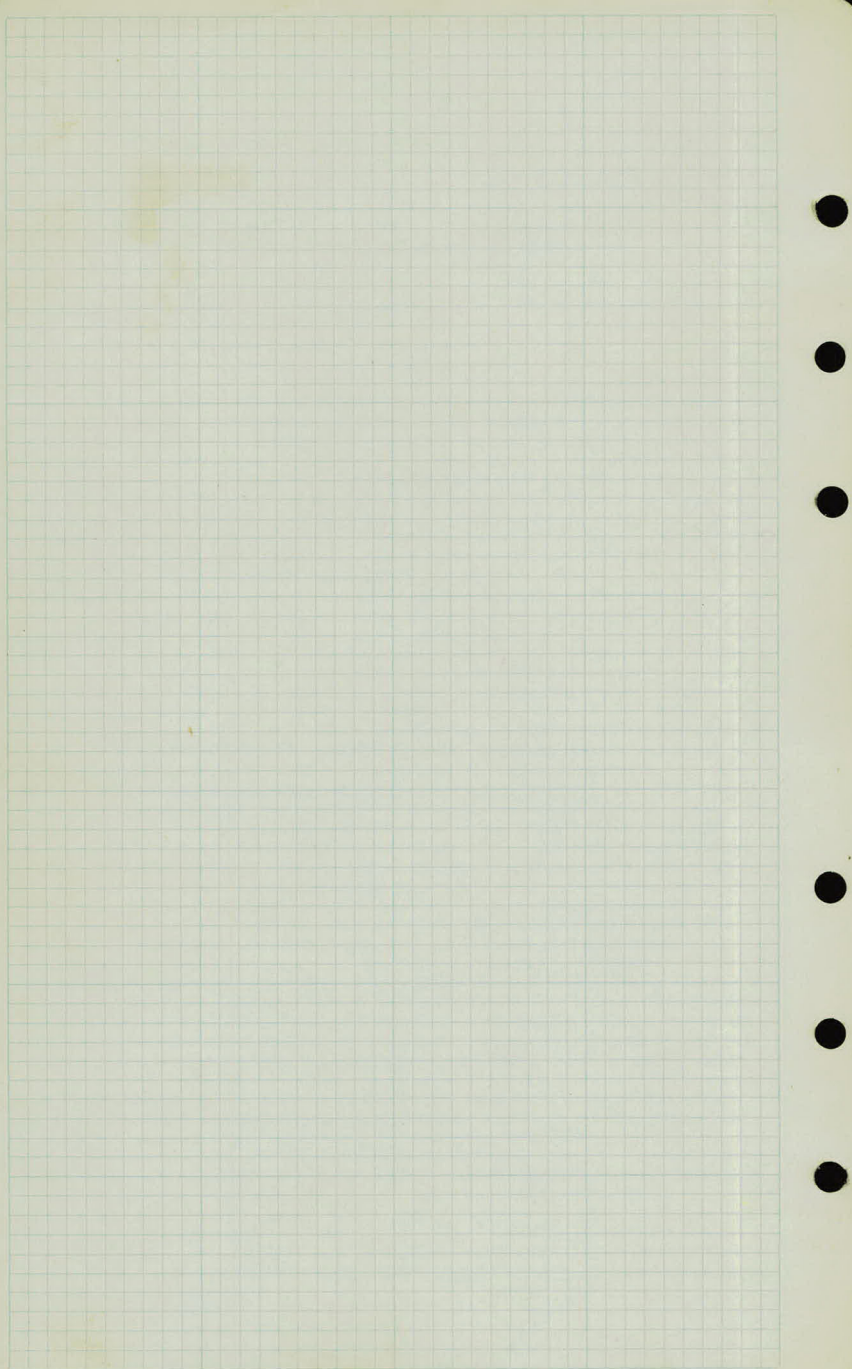
BIRCH LAKE BLVD. SO.

Centerville Rd to Otter Lake Rd



INDEX

Align	1-7
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1

Alignment

Sta	Point	ΔLt	ΔRt
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+76.88	P.T.	$27^{\circ}14'$	
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+50		$22^{\circ}07.5'$	
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			$\Delta-54^{\circ}28'$
--	--	--	------------------------

+25		$17^{\circ}22.5'$	
-----	--	-------------------	--

			$D-38^{\circ}-$
--	--	--	-----------------

12	+12.59	P.I.	
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			$T-79.04'$
--	--	--	------------

12		$12^{\circ}37.5'$	
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			$L-143.33'$
--	--	--	-------------

+75		$7^{\circ}52.5'$	
-----	--	------------------	--

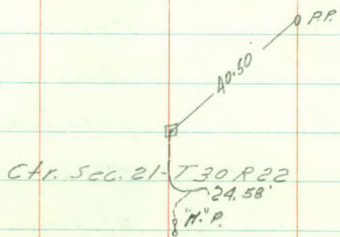
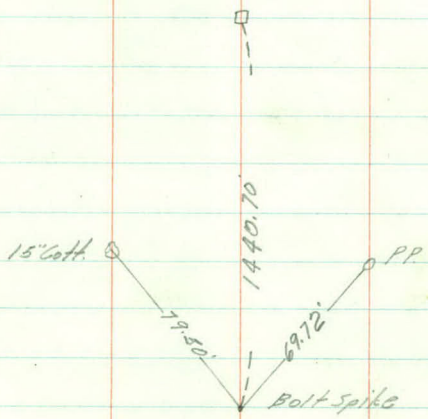
			$R-153.58'$
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+50		$3^{\circ}07.5'$	
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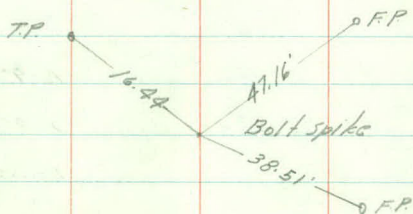
11	+33.55	P.C.	$0^{\circ}00'$
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0	+00	= & Centerville Rd.	
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E. 1/4 Cor. Sec. 21



Sta	Point	ΔL	ΔR
	+17.90 P.T.		$2^{\circ} 37'$
20			$2^{\circ} 26.3'$
	+50		$1^{\circ} 56.3' \Delta - 5^{\circ} 14'$
19			$1^{\circ} 26.3' D - 2^{\circ} 00'$
18	+87.19 P.I.		$T - 130.96'$
	+50		$0^{\circ} 56.3' L - 261.67'$
18			$0^{\circ} 26.3' R - 2864.93'$
17	+56.23 P.C.		$0^{\circ} 00'$
	+42.89 P.T.		$8^{\circ} 20.5'$
17			$7^{\circ} 22.6'$
	+50		$6^{\circ} 15.1' \Delta - 16^{\circ} 41'$
16			$5^{\circ} 07.6' D - 4^{\circ} 30'$
15	+58.88 P.I.		$T - 186.73'$
	+50		$4^{\circ} 00.1' L - 370.74'$
15			$2^{\circ} 52.6' R - 1273.57'$
	+50		$1^{\circ} 45.1'$
14			$0^{\circ} 37.6'$
13	+72.15 P.C.		$0^{\circ} 00'$



Sta	Point	ΔL	ΔP
-----	-------	------------	------------

31 +20.55 P.O.T.

40.28	PT.	4°38.5'
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25	4.528
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150	3047.8
-----	--------

 $\Delta = 9^{\circ}17'$

24	3002.8
----	--------

p. 30 -

23 451.93 P1.

T-155.09'

750	2017.8
-----	--------

1.309.44'

23	1032.8'
----	---------

P-1910.08

150	0°47.8'
-----	---------

22	0°02.8'
----	---------

21	+96.89	P.C.	0°00'
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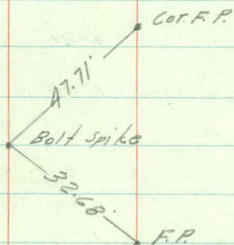
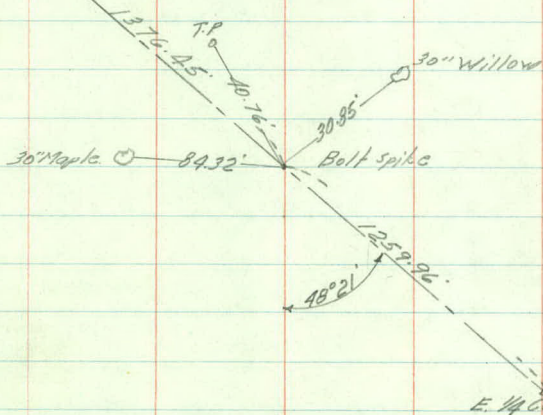
+ 75°

G-25-41
K.A.
M.B.
C.N.

4

N.E. Cor. B

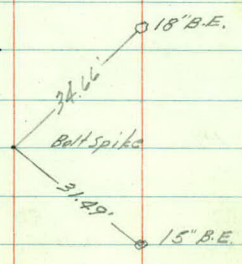
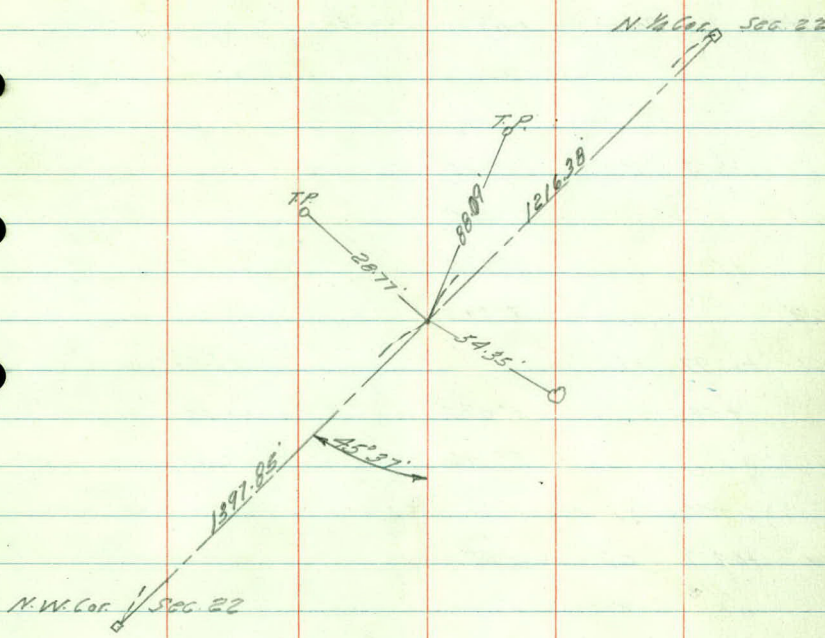
Sec. 21



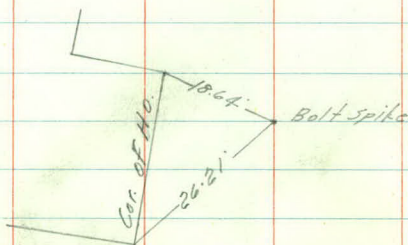
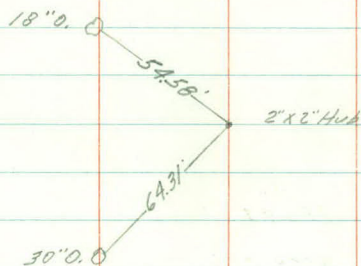
Sta	Point	ΔL	ΔE
-----	-------	------------	------------

50 + 78.20 P.O.T. = E.S.T.H. #96

497.81	P.T.	1°50.5'	
+50		1°36'	
37		1°21'	$\Delta \cdot 3^{\circ}41'$
+50		1°06'	D-1°00'
36 + 13.68	P.I.		T-184.20'
36		0°51'	L-368.33'
+50		0°36'	R-5729.65'
35		0°21'	
+50		0°06.2'	
34 + 29.48	P.C.	0°00'	



Sta	Point	ΔL	ΔR
	116.27 P.T.	12°48.5'	
63	+50	11°49.5'	
	+50	9°49.5'	$\Delta - 24°57'$
62	+50	7°49.5'	$D - 8° -$
61	+62.97 P.I.		$T - 158.58$
	+50	5°49.5'	$L - 311.88$
61	+50	3°49.5'	$R - 716.78$
	+50	1°49.5'	
60	+04.39 P.C.	0°00'	
	+84.30 P.T.		13°31'
	+50		11°57.8' $\Delta - 27°02'$
55			8°52.8' $D - 11° -$
54	+63.94 P.I.		$T - 125.90$
	+50		6°07.8' $L - 245.76$
54		06'	3°22.8' $R - 521.67$
	+50		0°37.8'
53	+38.34 P.C.		0°00'



Sta	Point	ΔLt	ΔRt
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46.63	P.T.	7° 59.7'	
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+50		7° 29.8'	
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66		5° 59.8'	
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			A - 15° 59'
--	--	--	-------------

+50		4° 29.8'	
-----	--	----------	--

			D - 60 -
--	--	--	----------

65	+34.23 = P.I. = M. 58 + 29.07	after Lake Rd.	
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			T - 134.13'
--	--	--	-------------

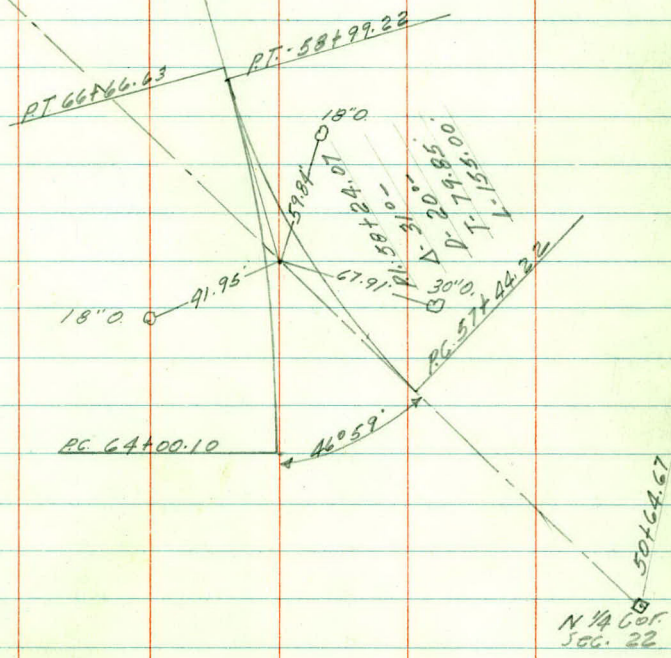
65		20.59.8'	
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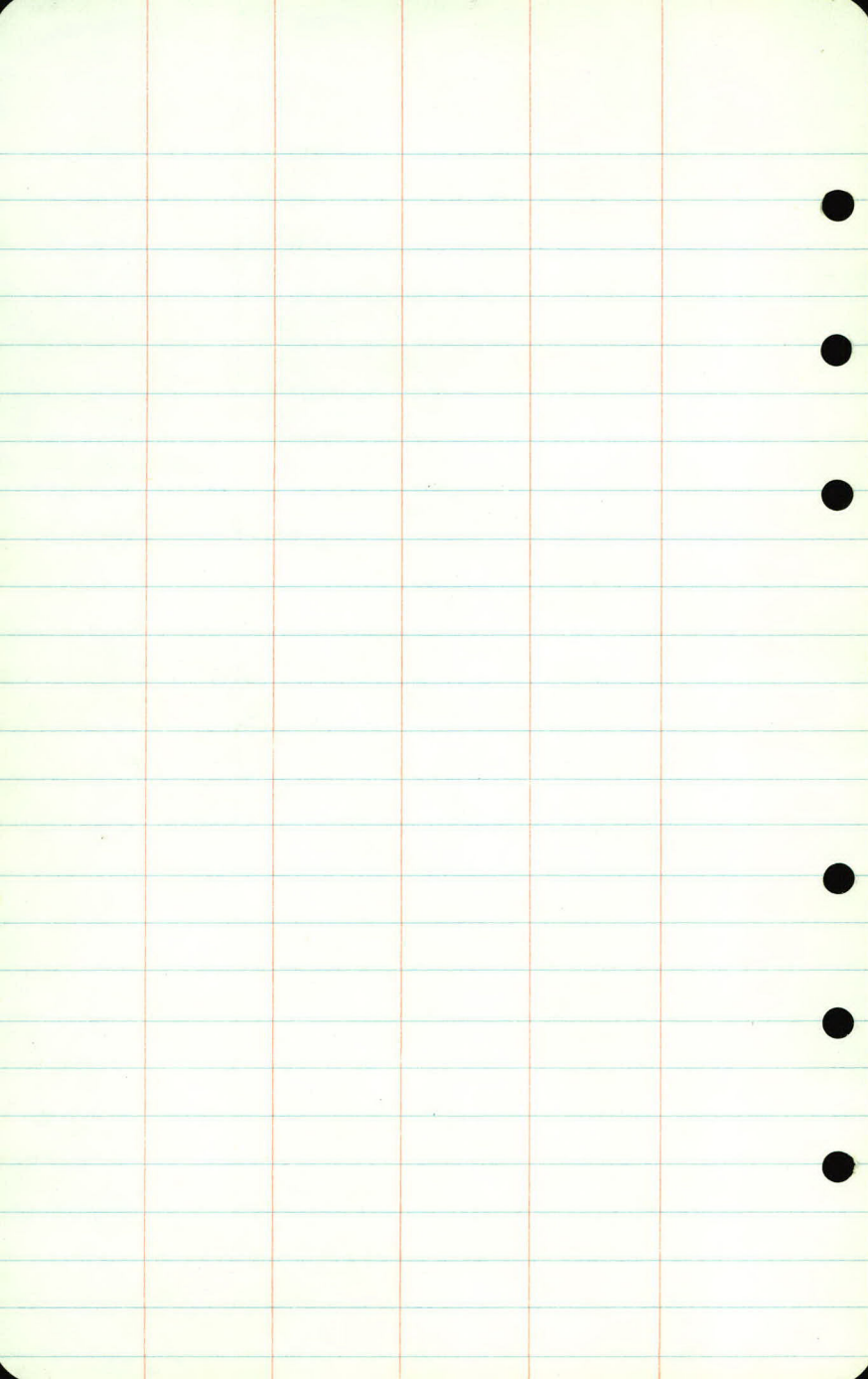
			L - 266.53'
--	--	--	-------------

+50		1° 29.8'	
-----	--	----------	--

			E - 955.37'
--	--	--	-------------

64	+00.10	P.C.	0° 00'
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Topography

5 12' 12'

+85-T.P.-19- End Brush- 28-18'

4 12' 12'

+75-Beg Brush- 23'-17'

+91-T.P.-16'

+30-Rd Sign-15'

+25-PP-30'

3 11' 13'

2 11' 13'

+95-T.P.-16'

1 11' 12'

+66-T.P.-16'

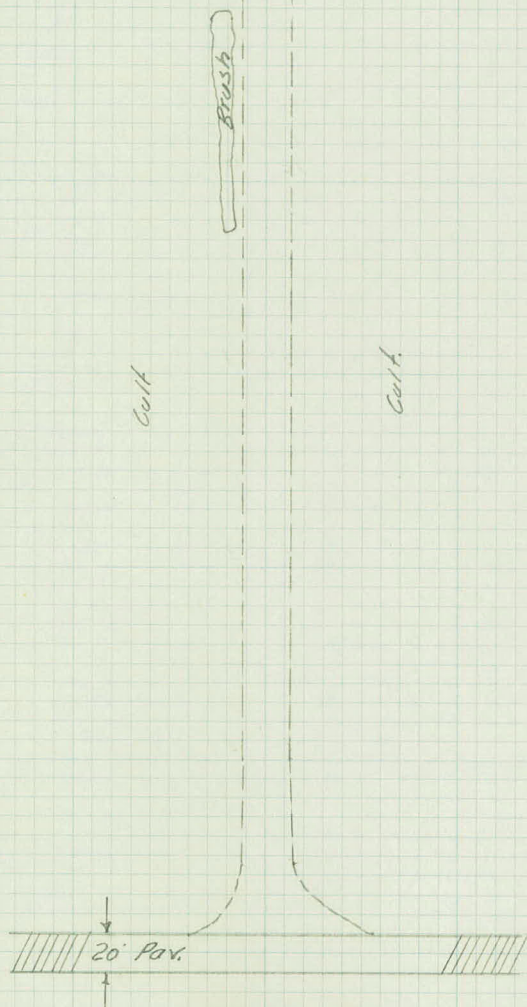
+49-Rd Sign-15'

+45-12' 15' +45'

0+00

+10-Cor- 40'

+27-PP-30'
54' Cal



+50- 13'-12' 168-15' Pop-48'
15" X 34 CM.
19:45 +43-End 15" CM-20'

+38-End 15" CM.-14'

12 10' 25'

+50- 12' 13'

+35-T.P.-24'

11 +01-T.P.-24' 12' 13'

10 +10-X Drains 12" X 32' CM. 15' 17'
12' 12'

+77-Ed. Signs-15'

+56-T.P.-20'

+32-PP-28'

9 12' 12'

8 12' 12'

+85-T.P.-19'

7 11' 13'

+30-T.P.-10'

+25-PP-28'

6 12' 13'

Cult.

Cult.

Cult.

Cult.

Road

13' 13' +57-Range Tie
+37-Fc Cor - 28' 2

19 13' 13' Fe-29'

+77-T.P.-35'

+29-Rd Sign-18'

18 12 12' Fe-27'

13' 13'

17 +17-T.P.-26' 14' 13' Fe-25'

15' 12'

16 15 12' Fe-24'

+71-T.P.-23'

14' 12'

15 14' 11' Fe-22'

13' 13'

+33-T.P.-31'

14 11' 14' Fe-26'

+90-Range Tie to Fc.

+46-Fc Cor-22'

13 12' 13'

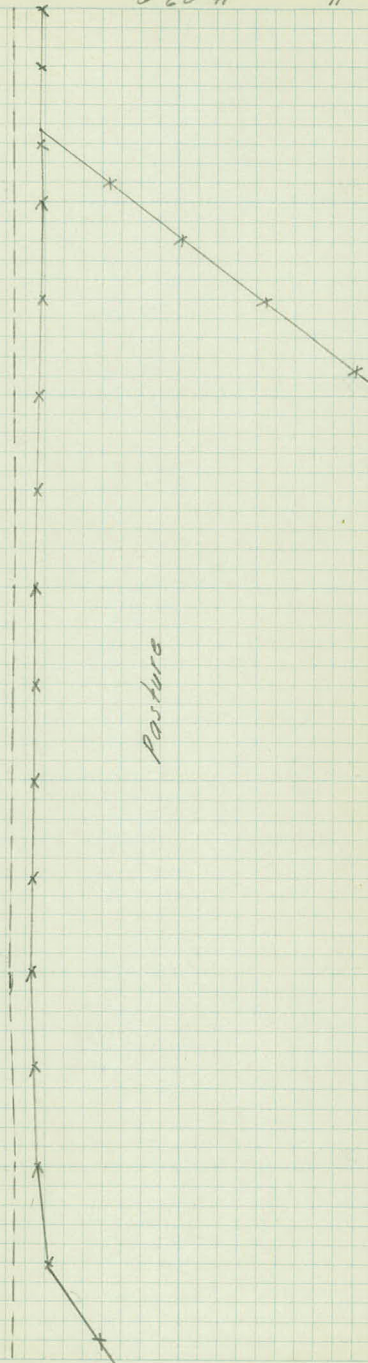
6-28-41

11

Uncult.

Pasture

Cult.



+92-5tp-23'
+84-5tp-32'
+70-5tp-24'
+65-12"BF-33'

+25-T.P.-26'

26

12' 12'

+30-12"BF-32'
+17-8"BF-34'
+06-6"TwBF-34'
+85-Group 6-3'BF-36'
+93-Range Tie
+75-End Brush-22'

25

11' 12' Brush-22'-38'

+80-TP-33'

+70-BES Lulluws

24

12' 13'

+30-Red Brush-23-43'
+17-Range Tie to FC.
+89-FC Cor-36'

+29-TP-39'

23

12' 12' FC-37'

12' 13'

22

13' 14'

+22-6"tp-30'
+07-5"tp-25'
FC-38'

+57-TP-33'

+53-Range Tie to Ho
+50-FC-40'

+27-NW Cor. Ho-79'

21

13' 13'

B-End-58'

+83-BES FC-35'
+65-End
+47-FC Cor-33'
+40-Range Tie

20

+01-TP-33'

13' 13'

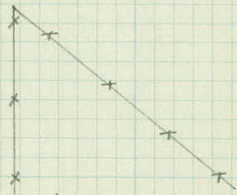
FC-69

Bay. Cult.

7
11
11
D
D
D
D
D

Cult.

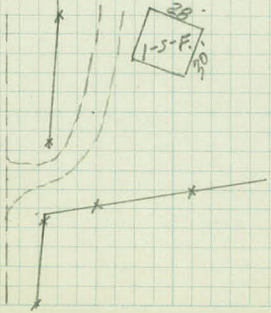
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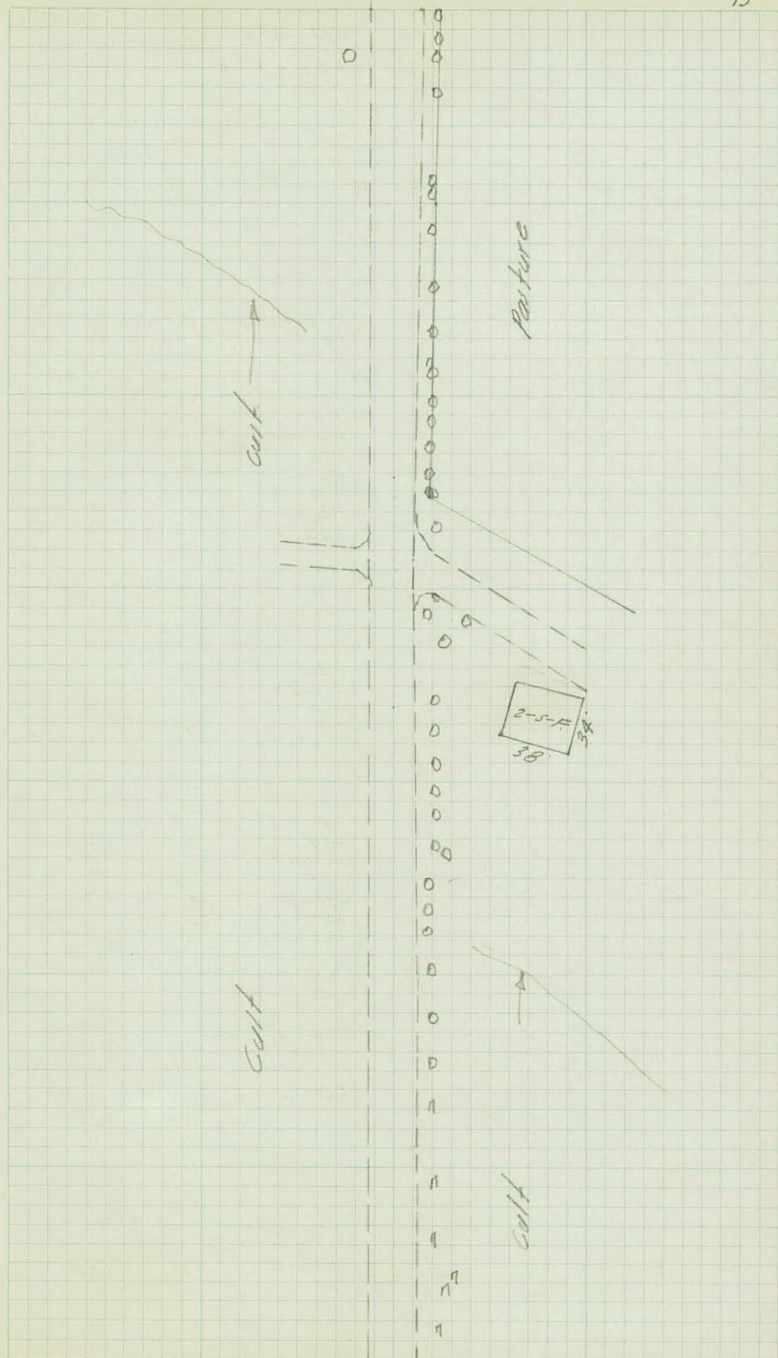


Cult.

Uncult.

28.
1-5-F.
190





+89-T.P.-20'

+98-30" B.E.-30'

+83-PP-18'

40

11' 12'

+36-T.P.-18'

+16-Range Tie

+10-Dio FC-42'

+02-24" B.E. + FC-23'

39

12' 11'

+87-20 -22'

+83-PP-18'

+75-20 -22'

+63-18" -23'

+51-18" -23'

+38-20 -24'

+25-20 -23'

38

12' 12'

FC-24'

+92-T.P.-18'

+90-30" -22'

+76-12" -23'

+62-18" -23'

+50-20" -23'

+36-10" -24'

+12-15" -22'

37

13' 12'

FC-24'

+56-T.P.-21'

+99-10" -23'

+87-12" -23'

+84-PP-19'

+74-15" -23'

+53-24" -24'

+41-12" -25'

+28-15" B.E.-24'

36

13' 13'

FC-26'

+90-12" -25'

+76-24" -26'

+47-12" B.E.-25'

+35-PP-24'

+03-T.P.-23'

35

13' 13'

FC-25'

+84-20" B.E.-25' PP-20'

+71-20" B.E.-24'

+56-20" E/PP-24'

+41-12" B.E.-23'

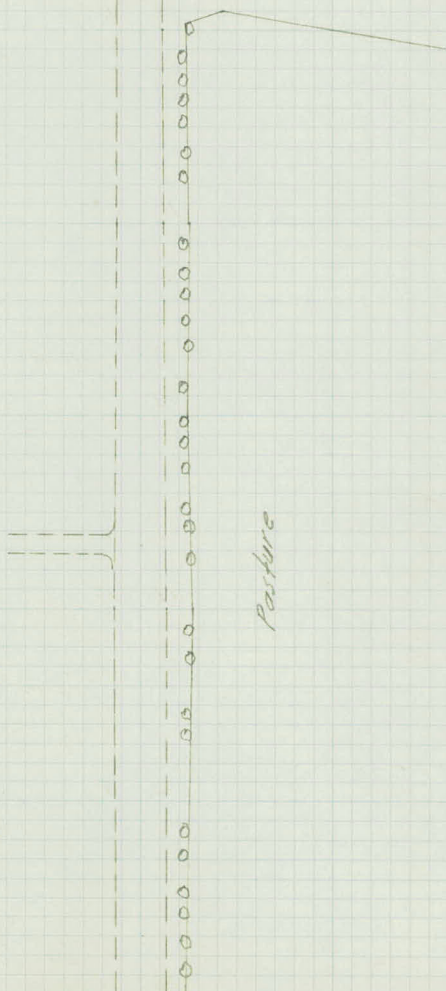
+27-15" B.E.-23'

+13-12" E/PP-23'

34

12' 13'

FC-24'



+91-12" B.E-25

+92-FC-19'

47

+07-Kd. Sig. 15-19'
11' 12'

+05-T.P-18'

+33-PP-19'

46

11' 12'

45 +18-T.P-17'

11' 12'

+33-PP-18'

44

12' 11'

+72-T.P-18'

43

12' 12'

+56-PP-18'

+33-Ent.
42 +17-T.P-18'

12' 12'

41

+20-24" B.E-31'
+10-Ent.
12' 12'

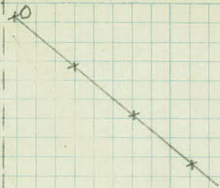
uncult

uncult

uncult

uncult

Eastward →



+55-Range tie to Ho.
 +51-2" Plum - 25' +60-2" Plum - 25'
 +41-2" Tw. Plum - 28'
 +39-Gar Gar - 30'
 +38-2" Myrm Tr. - 28' 14' 11"
 +30-Ent.
 +20-Rd. Sign - 20'
 +17-PP-R.P. - 22'
 +107-Range tie to Gar.
 54 Range tie to Ent. 14' 11"

13' 11"
 +175-B Ent. - 26'
 +164-Lind Brush - 25'
 +132-Bush - 20'
 +104-4" Plum Tr. - 24'
 53 12' 11"

1
 +190-2" Plum Tr. - 25'
 +179-Gar Ho - 58'
 +167-4" - 24'
 +152-4" - 23'
 +136-4" Plum Tr. - 30'
 +121-Range tie to Ho.
 52 2 Ent. - 34' 11' 11" +118-PP - 19'

+87-Bee Hedge - 33'
 +65-Range tie to Ent.
 +54-T.P. - 40'
 +41-15' X 98' Cove. - 29' (Under Highway)
 +37-Rad. - 12'
 +30-Rad. - 36'
 +109-Rd. Sign - 15'
 51 +102-T.P. - 19' +107-Rad. - 11'

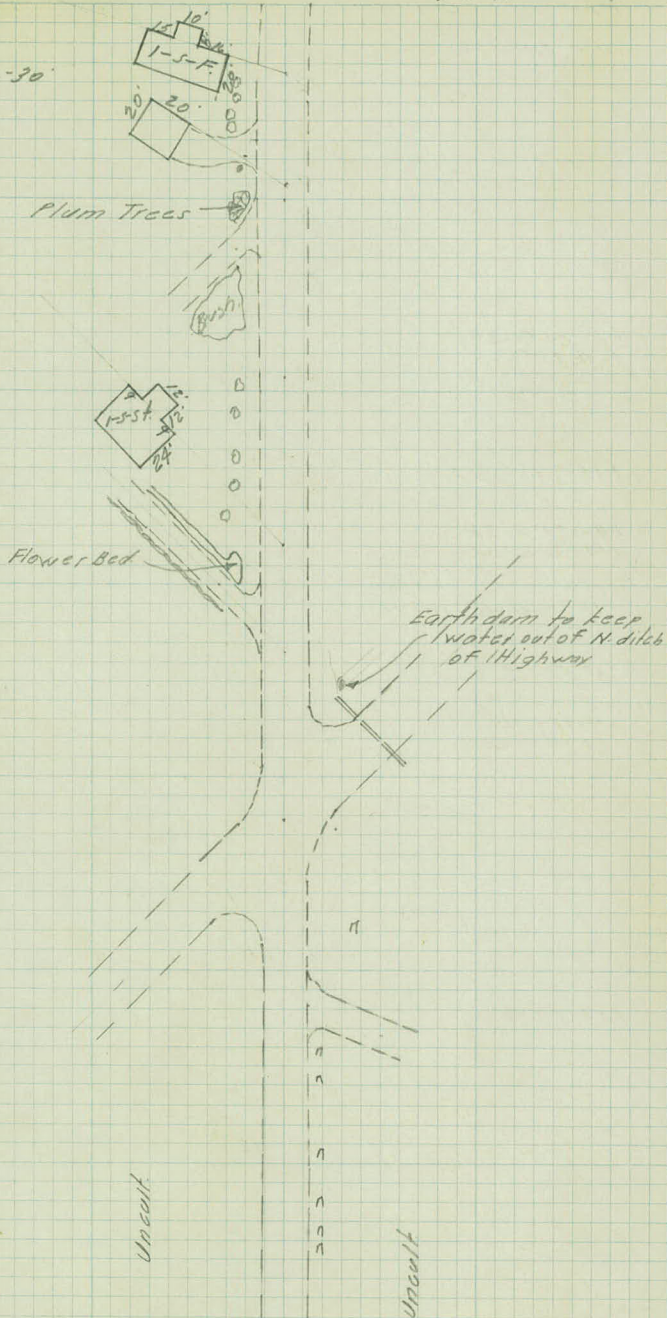
+183-Rad. - 27'
 +147-Rad. - 11'
 +145-Rd. Sign - 18'
 +122-Ste - 36'
 +118-PP - 19'
 +176-Rad. - 20'
 +123-Rad. - 39'
 +113-Rad. - 17'
 50 11' 11'

+93-T.P. - 19' +181-Ent.
 +167-R Ent. - 30'

+158-Ste - 19'
 +144-Ste - 18'
 +105-Ste - 18'
 49 +103-T.P. - 18' 11' 12'

+180-Ste - 18'
 +165-Ste - 18'
 +155-Ste - 19'
 +133-PP - 19'
 +11-Range tie to Fe.
 48 +102-T.P. - 17' 12' 12'

123 Cor. Ho. - 30'



+96-24°O.-26'

+71-10°B.W.65-34

+69-Rd Sign-18'
12' 12'

61 +02-30°O.-12'
Lake-63' 10' 13'

+73-15°O.-20'
+69-18°O.-21'
+76-P.P.-19'
11' 12'

+25-24°O.-24'
+04-20°O.-25'
60 Lake-70' 13' 12'
+92-10°O.-31'

+78-12°O.-35'

+47-End Coll N.W.S.
+30-P.P.-13'

+46-50°O.-24'
+07-12°O.-26'
59 Lake 67' 13' 10'
+76-12°O.-25' +92-15°O.-30'
+71-12°O.-31' +82-15°O.-23'
+47-15°O.-22'
+43-15°O.-35'
+35-8°O.-32'
+25-10°O.-36'
+18-12°O.-34'
+14-18°O.-38'
+08-18°O.-23'
58 Lake-65' 13' 11'

+83-Rd Sign-16'

+62-18°O.-32'
+70-P.P.-19'
+37-15°O.-32'
+28-8°O.-25'
+46-10°Tw B.W.65-33'
+10-18°O.-24'
57 Lake-71' 13' 11'

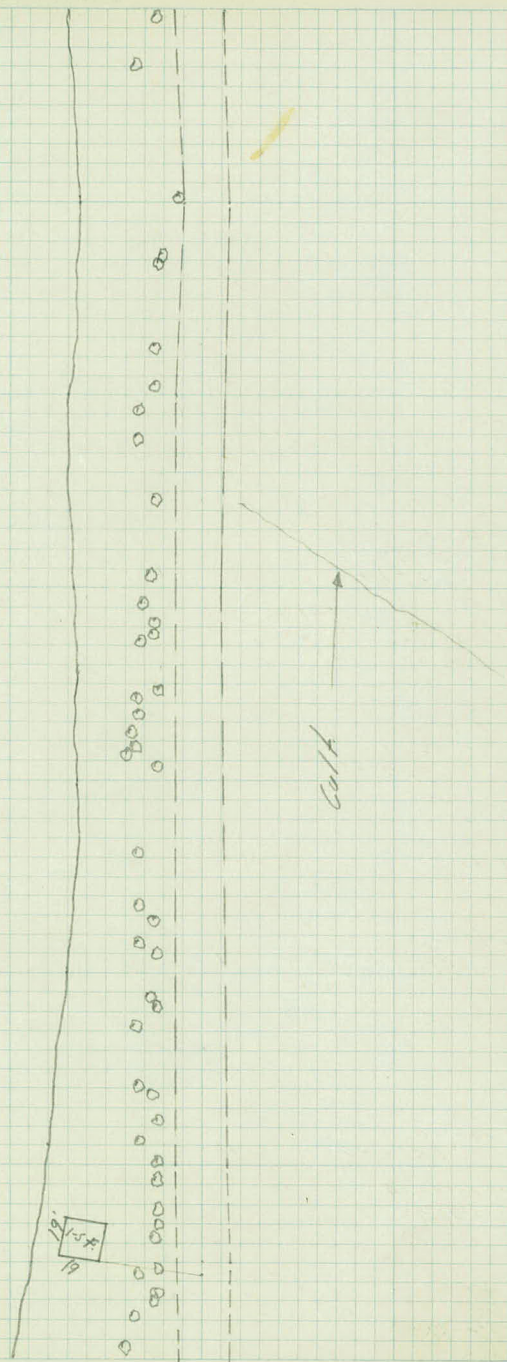
+30-P.P.-19'

+89-15°O.-27'
+84-12°O.-22'
+74-10°O.-33'
+42-15°O.-31'
+37-18°O.-22'
+23-15°O.-21'
+13-12°O.-35'
+02-15°O.-21'
56 Lake-80' 13' 12'

+64-15°O.-20'
+51-Com Ho-54' +88-P.P.-19'
+49-15°O.-21' +73-18°O.-23'
+43-Comp +10 ft Ho +81-G.P.-15'
+24-20°O.-35' +80-12°O.-21' 12' 14'
+33-15°O.-22' +70-12°O.-22'
+30-10°O.-24'
+22-12°O.-35'
+08-12°O.-20'

55 12' 12'

Birch Lake



67 Lake-13' 9' 12'

+66-PP-14'

+65-CP-26'
8' 13'

End Ditch - 50'

+102-End 24" C.M. - 20'

66 Lake-74'

+103-End 24" C.M. - 26'
10' 17'

+85-B1 top - 9'

13' (B1 top - 9'-30')

+18-18" O - 31'

+117-PP-29'

+115-SP-30'

65 Lake-13'

16' (B1 top - 32'-58')

+86-18" O - 39'

+85-SP-28'

+70-SP-30'

+59-SP-27'

48' 71'
8' 46' 159
16' +52-PP-37'

+102-18" O - 23'

64 Lake-67' Sp 21' 17' 7'

+190-24" O - 24'

+176-12" P100 - 34'

+172-PP-22'

17' 7'

+20-24" O - 32'

+104-SP-12" X 306-M.

63 Lake-69'

18' 12'
17' 7'

+95-24" O - 24'

+192-SP-34'

17' 7'

+133-24" O - 24'

+123-18" O - 37'

+101-SP-29-23'

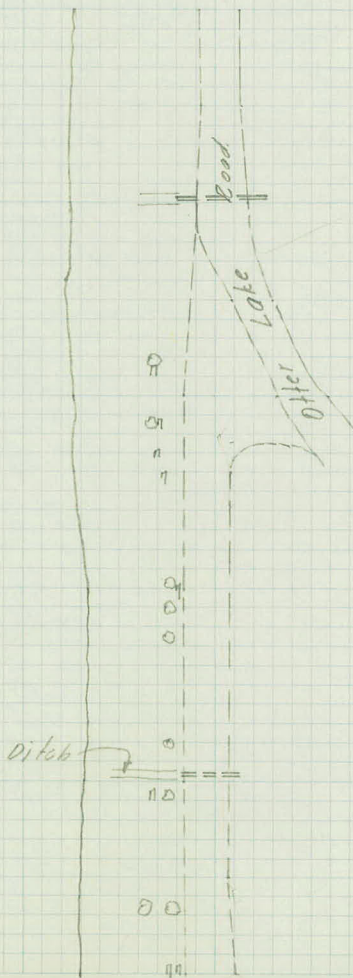
62 Lake-70'

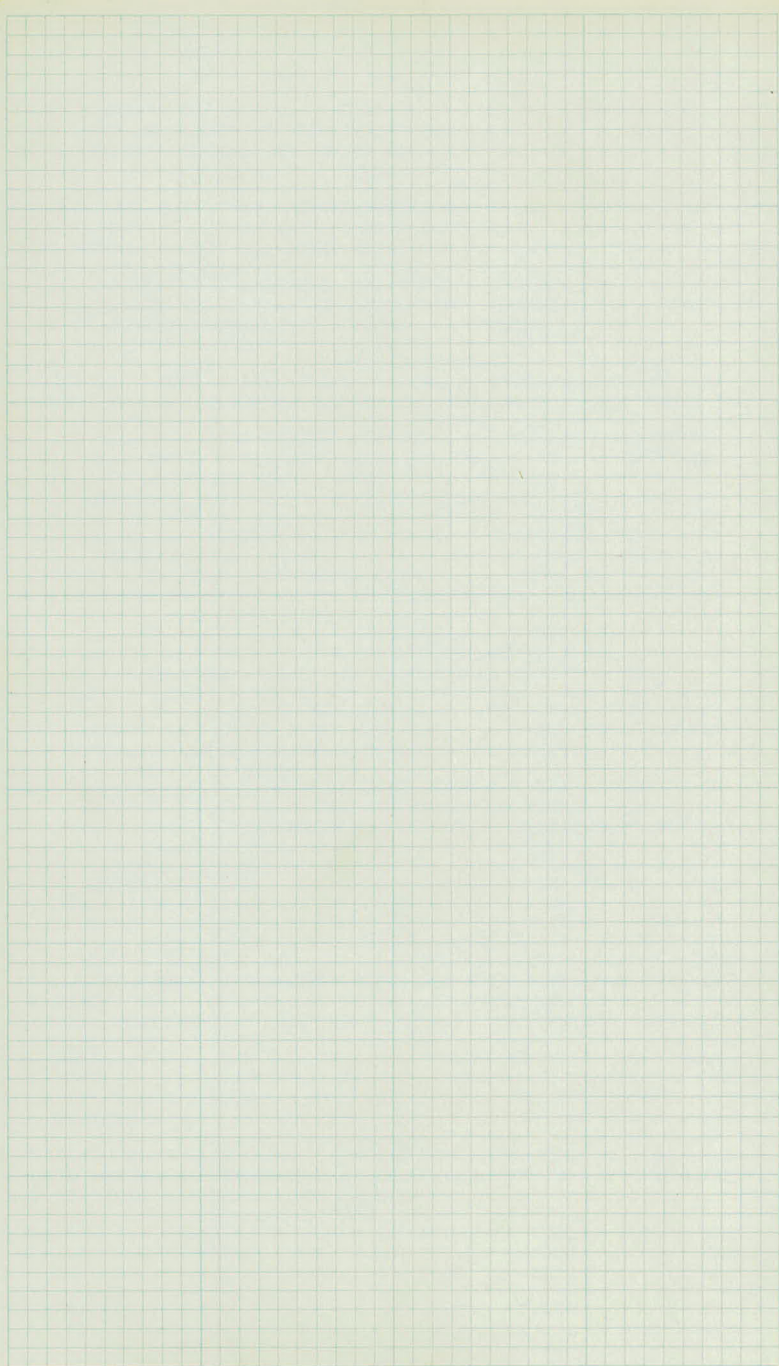
+125-PP-15'
15' 11'

7-7-41

16

Birch Lake





Xsections

Sta	I	T	-	Elev
B.M.	6.64	954.63		(947.99)

0 +00

+10

+19

+50

1

+35

+75

2

+50

3

+50

LT

K

RT

Top Mont. Centerville Rd to Birch Lake Blvd. S.

657

$\frac{6.28}{50}$ $\frac{6.61}{50}$ $\frac{7.08}{50}$

$\frac{7.9}{100}$ $\frac{7.6}{86}$ $\frac{8.3}{50}$ $\frac{7.6}{32}$ $\frac{6.7}{28}$ $\frac{6.4}{16}$ $\frac{6.4}{15}$ $\frac{6.6}{37}$ $\frac{7.5}{30}$ $\frac{7.4}{50}$

$\frac{5.9}{50}$ $\frac{5.8}{30}$ $\frac{5.5}{15}$ $\frac{6.3}{12}$ $\frac{6.1}{14}$ $\frac{6.8}{15}$ $\frac{6.4}{29}$ $\frac{5.7}{50}$ $\frac{5.7}{50}$

$\frac{7.2}{50}$ $\frac{6.9}{36}$ $\frac{6.4}{18}$ $\frac{6.0}{11}$ $\frac{5.7}{12}$ $\frac{6.2}{13}$ $\frac{5.8}{29}$ $\frac{5.6}{50}$ $\frac{5.5}{50}$

$\frac{8.6}{50}$ $\frac{8.1}{33}$ $\frac{7.2}{17}$ $\frac{5.9}{11}$ $\frac{5.6}{13}$ $\frac{6.0}{14}$ $\frac{5.8}{31}$ $\frac{5.6}{50}$ $\frac{5.4}{50}$

$\frac{9.0}{50}$ $\frac{8.7}{31}$ $\frac{8.0}{17}$ $\frac{5.9}{11}$ $\frac{5.5}{13}$ $\frac{5.8}{22}$ $\frac{6.1}{35}$ $\frac{5.8}{50}$ $\frac{5.7}{50}$

$\frac{8.6}{50}$ $\frac{8.5}{35}$ $\frac{8.4}{19}$ $\frac{7.5}{14}$ $\frac{6.0}{11}$ $\frac{5.4}{13}$ $\frac{5.7}{22}$ $\frac{6.1}{35}$ $\frac{5.3}{50}$ $\frac{5.2}{50}$

$\frac{6.6}{50}$ $\frac{6.1}{33}$ $\frac{5.9}{18}$ $\frac{5.4}{12}$ $\frac{5.1}{13}$ $\frac{5.4}{14}$ $\frac{5.2}{30}$ $\frac{4.8}{50}$ $\frac{5.2}{50}$

$\frac{7.3}{50}$ $\frac{6.8}{33}$ $\frac{6.7}{21}$ $\frac{6.4}{15}$ $\frac{5.3}{11}$ $\frac{5.0}{13}$ $\frac{5.3}{21}$ $\frac{6.0}{30}$ $\frac{5.3}{50}$ $\frac{4.7}{50}$

$\frac{8.5}{50}$ $\frac{8.3}{35}$ $\frac{8.0}{24}$ $\frac{7.8}{17}$ $\frac{5.3}{12}$ $\frac{5.0}{13}$ $\frac{5.4}{16}$ $\frac{7.0}{32}$ $\frac{7.0}{28}$ $\frac{7.0}{50}$

Sta	+	π	-	Elev
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		954.63		
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4

+50

5

T.P.	5.57	956.09	4.11	950.52
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+50

6

+50

+73

7

T.P.	4.17	953.51	4.75	951.34
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+50

8

+30

lt

r

rt

$$\frac{74}{50} \frac{72}{30} \frac{94}{26} \frac{82}{17} \frac{50}{12} \frac{47}{13} \frac{53}{16} \frac{67}{21} \frac{74}{34} \frac{85}{50}$$

$$\frac{62}{50} \frac{75}{31} \frac{84}{29} \frac{88}{24} \frac{80}{19} \frac{48}{13} \frac{46}{13} \frac{50}{15} \frac{60}{20} \frac{74}{32} \frac{78}{30} \frac{92}{50}$$

$$\frac{67}{50} \frac{70}{29} \frac{83}{26} \frac{77}{18} \frac{49}{13} \frac{45}{13} \frac{50}{16} \frac{70}{20} \frac{79}{32} \frac{82}{32} \frac{92}{50}$$

$$\frac{74}{50} \frac{78}{38} \frac{85}{26} \frac{93}{23} \frac{83}{17} \frac{62}{13} \frac{57}{13} \frac{62}{16} \frac{74}{21} \frac{83}{32} \frac{77}{32} \frac{80}{50}$$

$$\frac{69}{50} \frac{72}{35} \frac{81}{24} \frac{82}{17} \frac{58}{13} \frac{53}{14} \frac{60}{14} \frac{68}{19} \frac{71}{33} \frac{76}{50}$$

$$\frac{41}{50} \frac{50}{36} \frac{65}{23} \frac{76}{20} \frac{75}{16} \frac{51}{12} \frac{49}{14} \frac{54}{20} \frac{58}{32} \frac{52}{32} \frac{66}{50}$$

$$\frac{27}{50} \frac{36}{37} \frac{59}{23} \frac{71}{19} \frac{74}{15} \frac{51}{11} \frac{47}{19} \frac{53}{20} \frac{58}{28} \frac{56}{28} \frac{74}{50}$$

$$\frac{36}{50} \frac{41}{37} \frac{61}{23} \frac{70}{21} \frac{75}{15} \frac{51}{12} \frac{47}{14} \frac{53}{17} \frac{65}{29} \frac{68}{29} \frac{88}{50}$$

$$\frac{42}{50} \frac{43}{36} \frac{56}{23} \frac{63}{21} \frac{68}{16} \frac{45}{12} \frac{40}{13} \frac{45}{16} \frac{51}{29} \frac{60}{29} \frac{77}{50}$$

$$\frac{49}{50} \frac{53}{36} \frac{59}{23} \frac{63}{16} \frac{43}{14} \frac{41}{14} \frac{48}{15} \frac{55}{26} \frac{56}{26} \frac{69}{50}$$

$$\frac{47}{50} \frac{48}{40} \frac{61}{23} \frac{66}{21} \frac{67}{16} \frac{44}{12} \frac{40}{13} \frac{44}{14} \frac{54}{26} \frac{53}{26} \frac{82}{50}$$

Sta.	t	π	-	Elev	
		955.51			
8	+62				
9					
	+23				
	+73				
10	+10				
	+46				
	+71				
11					
	+19				
	+50				
12					
BM	7.71	955.26	2.94	947.57	(947.55)

Lt.

E

Rt.

$\frac{35}{50} \frac{49}{39} \frac{63}{23} \frac{71}{21} \frac{72}{17} \frac{82}{12} \frac{87}{14} \frac{46}{16} \frac{42}{22} \frac{38}{22} \frac{50}{37} \frac{66}{50}$

$\frac{41}{50} \frac{49}{41} \frac{65}{24} \frac{75}{23} \frac{75}{18} \frac{47}{12} \frac{43}{13} \frac{48}{14} \frac{53}{24} \frac{43}{24} \frac{45}{37} \frac{53}{50}$

$\frac{46}{50} \frac{56}{41} \frac{75}{23} \frac{71}{22} \frac{78}{17} \frac{50}{12} \frac{45}{12} \frac{50}{14} \frac{60}{27} \frac{43}{27} \frac{52}{50}$

$\frac{76}{50} \frac{81}{45} \frac{82}{24} \frac{85}{23} \frac{87}{17} \frac{56}{12} \frac{51}{11} \frac{57}{16} \frac{88}{27} \frac{96}{41} \frac{98}{50} \frac{104}{50}$

(Colv)

(Colv)

$\frac{82}{50} \frac{86}{43} \frac{83}{25} \frac{97}{22} \frac{97}{19} \frac{90}{17} \frac{99}{16} \frac{58}{13} \frac{54}{12} \frac{59}{17} \frac{106}{19} \frac{106}{25} \frac{109}{36} \frac{113}{50}$

$\frac{72}{50} \frac{84}{26} \frac{93}{25} \frac{96}{19} \frac{63}{13} \frac{55}{12} \frac{60}{17} \frac{79}{19} \frac{88}{30} \frac{86}{30} \frac{88}{50}$

$\frac{65}{50} \frac{82}{26} \frac{91}{21} \frac{91}{18} \frac{62}{13} \frac{58}{14} \frac{64}{15} \frac{71}{22} \frac{77}{22} \frac{75}{29} \frac{84}{50}$

$\frac{70}{50} \frac{74}{36} \frac{74}{22} \frac{84}{20} \frac{85}{17} \frac{65}{13} \frac{62}{13} \frac{68}{17} \frac{88}{21} \frac{94}{33} \frac{97}{50} \frac{105}{50}$

$\frac{88}{100} \frac{88}{75} \frac{85}{50} \frac{88}{34} \frac{87}{19} \frac{67}{14} \frac{64}{14}$

$\frac{68}{50} \frac{70}{36} \frac{90}{23} \frac{91}{16} \frac{76}{13} \frac{68}{12} \frac{71}{15} \frac{85}{21} \frac{91}{32} \frac{89}{32} \frac{94}{50}$

$\frac{59}{50} \frac{82}{27} \frac{90}{16} \frac{90}{13} \frac{75}{5} \frac{71}{15} \frac{68}{25} \frac{75}{28} \frac{81}{35} \frac{93}{35} \frac{80}{50}$

Sph in 12" Pap 40' Pt. 12+68

Sta	+	π	-	Elev.
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955.26

12+25

138

+76.88

13

+38

+72

14

+50

15

+50

16

+50

T.P.

12.73

966.87

1.12

954.14

LF E EF

6.1	7.5	8.3	8.9	7.6	6.8	8.0	8.5
50	29	16	14	11	6.9	14	29
							50

$\frac{5.9}{50}$ $\frac{7.2}{31}$ $\frac{8.3}{17}$ $\frac{9.0}{15}$ $\frac{9.5}{15}$ $\frac{7.4}{12}$ $\frac{7.0}{4}$ $\frac{7.0}{12}$ $\frac{7.8}{20}$ $\frac{8.5}{38}$ $\frac{8.4}{50}$

55 6.0 7.3 7.1 7.1 8.4 8.6 8.8
50 36 20 13 6 7 13 17 27 50

5.4 5.8 2.0 6.9 6.9 7.6 7.9 7.9 8.3
50 36 20 12 65 14 16 31 39 50

5.4 5.6 6.3 6.5 6.7 8.1 8.0 8.4 8.0
50 34 19 9 6 2 14 16 25 40 50

<u>5.0</u>	<u>5.2</u>	<u>5.9</u>	<u>6.2</u>	<u>6.4</u>	<u>6.6</u>	<u>7.7</u>	<u>9.3</u>
50	36	22	10	5.8	14	21	28

$\begin{array}{r} 4.5 \\ 50 \end{array}$
 $\begin{array}{r} 6.2 \\ 23 \end{array}$
 $\begin{array}{r} 6.6 \\ 15 \end{array}$
 $\begin{array}{r} 5.9 \\ 12 \end{array}$
 $\begin{array}{r} 5.6 \\ 5.6 \end{array}$
 $\begin{array}{r} 6.3 \\ 15 \end{array}$
 $\begin{array}{r} 7.9 \\ 18 \end{array}$
 $\begin{array}{r} 9.1 \\ 27 \end{array}$
 $\begin{array}{r} 9.5 \\ 50 \end{array}$

4.5 5.2 6.1 6.1 6.7 6.2 5.4 6.2 7.2 8.8 9.9 10.8
5.0 3.8 3.5 2.6 2.4 1.8 1.6 5.3 1.3 1.4 2.4 3.8 5.0

<u>4/1</u>	<u>4/2</u>	<u>6/2</u>	<u>6/2</u>	<u>5/0</u>	<u>5/8</u>	<u>5/1</u>	<u>6/1</u>	<u>7/5</u>	<u>8/5</u>	<u>9/1</u>	<u>9/9</u>
5/0	3/8	3/6	2/7	2/1	2/0	1/8	5/2	1/1	1/4	1/9	3/6

$\frac{3.5}{5.0}$	$\frac{3.3}{3.8}$	$\frac{4.0}{2.0}$	$\frac{4.7}{1.8}$	$\frac{4.6}{1.4}$	$\frac{5.6}{1.2}$	$\frac{6.3}{1.4}$	$\frac{7.4}{2.2}$	$\frac{8.3}{3.5}$	$\frac{9.0}{5.0}$
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$\frac{3.1}{50}$
 $\frac{3.2}{29}$
 $\frac{3.6}{15}$
 $\frac{4.0}{13}$
 $\frac{4.8}{19}$
 $\frac{5.2}{25}$
 $\frac{6.1}{50}$

$\frac{1.1}{50}$	$\frac{1.7}{28}$	$\frac{2.7}{20}$	$\frac{2.8}{18}$	$\frac{2.3}{16}$	2.3	$\frac{2.9}{14}$	$\frac{3.8}{16}$	$\frac{4.9}{25}$	$\frac{6.0}{50}$
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Sta	+	T	-	Elev
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		966.87		
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17				
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	+50			
--	-----	--	--	--

18				
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	+50			
--	-----	--	--	--

19				
----	--	--	--	--

	+50			
--	-----	--	--	--

20				
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	+50			
--	-----	--	--	--

21				
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	+25			
--	-----	--	--	--

	+62			
--	-----	--	--	--

22				
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T.P	6.71	963.61	9.97	956.70
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Lt.

E

Et

$\frac{11.6}{50}$ $\frac{11.8}{36}$ $\frac{12.8}{21}$ $\frac{13.3}{20-17}$ $\frac{12.7}{16}$ 12.7 $\frac{13.4}{74}$ $\frac{14.4}{17}$ $\frac{15.5}{26}$ $\frac{16.3}{50}$

$\frac{10.4}{50}$ $\frac{10.4}{34}$ $\frac{11.7}{19}$ $\frac{12.0}{17-15}$ $\frac{11.6}{14}$ 11.4 $\frac{12.2}{14}$ $\frac{13.2}{24}$ $\frac{15.2}{50}$

$\frac{9.1}{50}$ $\frac{9.3}{38}$ $\frac{9.1}{20}$ $\frac{10.4}{16}$ $\frac{10.4}{13}$ 10.2 $\frac{10.9}{14}$ $\frac{11.6}{16}$ $\frac{11.4}{20}$ $\frac{12.8}{32}$ $\frac{14.6}{50}$

$\frac{6.5}{50}$ $\frac{6.4}{28}$ $\frac{9.5}{20}$ $\frac{9.5}{16}$ $\frac{8.9}{13}$ 8.7 $\frac{9.2}{14}$ $\frac{9.8}{17}$ $\frac{7.9}{22}$ $\frac{10.0}{28}$ $\frac{12.6}{50}$

$\frac{2.9}{50}$ $\frac{2.6}{32}$ $\frac{8.0}{22}$ $\frac{8.4}{17}$ $\frac{7.5}{14}$ 7.3 $\frac{7.9}{13}$ $\frac{8.1}{19}$ $\frac{6.7}{21}$ $\frac{8.6}{31}$ $\frac{10.9}{50}$

$\frac{2.1}{50}$ $\frac{2.2}{26}$ $\frac{6.8}{23}$ $\frac{7.1}{16}$ $\frac{6.8}{14}$ 6.6 $\frac{7.2}{13}$ $\frac{6.4}{20}$ $\frac{8.2}{27}$ $\frac{10.2}{43}$ $\frac{10.8}{50}$

$\frac{3.7}{50}$ $\frac{3.4}{29}$ $\frac{6.7}{23}$ $\frac{6.6}{16}$ $\frac{6.5}{14}$ 6.3 $\frac{6.9}{13}$ $\frac{6.5}{19}$ $\frac{7.7}{28}$ $\frac{9.2}{50}$

$\frac{2.2}{50}$ $\frac{2.4}{29}$ $\frac{6.7}{25}$ $\frac{7.0}{16}$ $\frac{6.8}{13}$ 6.2 $\frac{6.4}{13}$ $\frac{6.1}{28}$ $\frac{8.1}{36}$ $\frac{9.2}{50}$

$\frac{1.1}{50}$ $\frac{0.8}{34}$ $\frac{6.9}{26}$ $\frac{7.4}{17}$ $\frac{2.0}{14}$ 6.5 $\frac{6.9}{13}$ $\frac{7.3}{28}$ $\frac{2.5}{35}$ $\frac{3.1}{50}$

$\frac{1.6}{50}$ $\frac{0.8}{33}$ $\frac{7.7}{25}$ $\frac{8.0}{17}$ $\frac{7.4}{13}$ 7.0 $\frac{7.5}{13}$ $\frac{8.0}{17}$ $\frac{7.8}{29}$ $\frac{1.3}{38}$ $\frac{1.5}{50}$

$\frac{3.8}{50}$ $\frac{3.7}{30}$ $\frac{8.4}{23}$ $\frac{9.0}{15}$ $\frac{8.5}{13}$ 7.9 $\frac{8.6}{14}$ $\frac{9.4}{18}$ $\frac{9.4}{21}$ $\frac{2.9}{38}$ $\frac{2.5}{50}$

$\frac{7.6}{50}$ $\frac{7.1}{31}$ $\frac{8.0}{24}$ $\frac{9.7}{20}$ $\frac{10.2}{15}$ $\frac{10.0}{13}$ 9.2 $\frac{10.0}{15}$ $\frac{10.5}{17}$ $\frac{10.2}{26}$ $\frac{5.4}{33}$ $\frac{4.0}{50}$

Sta	t	π	-	ELEV
		963.61		

22 + 50

23

+ 50

24

T.P.	7.65	957.58	13.68	949.93
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+ 50

25

T.P.	1.70	945.70	13.58	944.00
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+ 50

26

+ 50

27

T.P.	2.07	936.57	11.20	934.50
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+ 50

L1

2

R1

6.6 6.2 5.9 8.5 8.6 8.3 9.6 8.7 4.6 4.2
 50 38 24 19 12 7.8 14 16 25 31 50

6.1 5.2 4.8 10.5 10.1 9.9 10.6 11.2 10.5 4.6 3.7 3.7
 50 42 29 23 12 9.5 13 16 22 28 34 39 50

3.4 3.1 3.4 9.9 11.7 12.6 11.9 11.8 13.1 13.0 6.7 5.9 6.4
 50 39 33 26 21 15 13 11.3 13 16 24 31 38 50

8.6 8.2 7.4 13.0 13.9 14.7 13.8 14.0 14.7 11.4 10.1 10.3
 50 38 34 26 20 15 12 13.4 14 22 27 41 50

8.1 8.1 7.7 9.6 10.6 10.4 10.2 11.2 11.1 8.2 6.2 5.6
 50 36 22 20 16 12 9.7 13 15 22 26 35 50

14.2 13.9 12.2 13.1 12.8 12.6 12.8 7.5 7.7
 50 35 18 15 11 12.3 13 26 34 50

8.8 8.1 4.6 3.5 3.4 3.5 4.1 5.0 5.2 7.3
 50 33 21 16 11 3.0 15 21 26 36 50

11.5 10.7 7.8 5.6 5.8 10.4 11.6 12.6
 50 29 19 12 5.1 15 23 32 50

13.2 13.2 12.5 7.8 2.8 12.0 12.9 13.1
 50 31 21 15 7.3 12 19 30 50

14.1 13.7 13.0 9.6 9.9 13.3 14.1 14.2
 50 27 20 14 9.1 12 19 35 50

P.P. L1 27+25

5.5 5.4 4.8 2.2 1.7 2.4 5.3 5.7 6.2
 50 24 19 12 11 17 31 50

Sta	+	π	-	Elev.
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		936.57		
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28

+50

29

+50

30

+50

B.M.

509

931.48

931.50

31

+50

T.P.

612

937.78

491

931.66

32

+50

33

LH

R

RH

$$\frac{60}{50} \frac{61}{52} \frac{55}{17} \frac{34}{13} \frac{29}{12} \frac{36}{19} \frac{55}{30} \frac{62}{50} \frac{68}{50}$$

$$\frac{65}{50} \frac{67}{33} \frac{63}{17} \frac{43}{13} \frac{37}{13} \frac{45}{15} \frac{58}{28} \frac{65}{50} \frac{66}{50}$$

$$\frac{68}{50} \frac{68}{34} \frac{66}{17} \frac{48}{13} \frac{43}{12} \frac{50}{14} \frac{65}{30} \frac{68}{50} \frac{72}{50}$$

$$\frac{67}{50} \frac{70}{34} \frac{73}{18} \frac{54}{13} \frac{48}{12} \frac{55}{15} \frac{65}{35} \frac{69}{50} \frac{62}{50}$$

$$\frac{67}{50} \frac{70}{30} \frac{72}{16} \frac{56}{13} \frac{51}{12} \frac{55}{14} \frac{67}{18} \frac{68}{22} \frac{64}{36} \frac{60}{50} \frac{56}{50}$$

$$\frac{65}{50} \frac{69}{33} \frac{70}{16} \frac{56}{13} \frac{51}{11} \frac{55}{14} \frac{67}{18} \frac{68}{25} \frac{62}{50} \frac{57}{50}$$

Top N.W. Cor. Lower Conc. Step Front Ho. Rt. 5/6 30t

$$\frac{63}{50} \frac{66}{34} \frac{63}{16} \frac{54}{13} \frac{49}{11} \frac{55}{14} \frac{60}{20} \frac{58}{50} \frac{59}{50}$$

$$\frac{63}{50} \frac{64}{29} \frac{66}{17} \frac{50}{13} \frac{48}{11} \frac{52}{13} \frac{64}{16} \frac{62}{32} \frac{64}{50} \frac{63}{50}$$

$$\frac{81}{50} \frac{82}{25} \frac{85}{18} \frac{67}{13} \frac{62}{11} \frac{68}{13} \frac{79}{17} \frac{79}{50} \frac{82}{50}$$

$$\frac{90}{50} \frac{88}{34} \frac{88}{17} \frac{68}{13} \frac{62}{12} \frac{66}{14} \frac{71}{22} \frac{72}{50} \frac{68}{50}$$

$$\frac{88}{50} \frac{82}{32} \frac{83}{16} \frac{66}{14} \frac{59}{12} \frac{63}{14} \frac{74}{15} \frac{74}{18} \frac{67}{27} \frac{63}{50} \frac{63}{50}$$

Sta.	+	π	-	Elev.
		937.78		
33	+50			
34				
	+50			
35				
	+50			
36				
	+50			
T.P.	4.88	938.26	4.40	933.38
37				
	+50			
38				
	+50			

LH

R

LH

$$\frac{75}{50} \frac{70}{30} \frac{78}{21} \frac{76}{16} \frac{62}{13} \frac{56}{13} \frac{61}{13} \frac{63}{19} \frac{54}{22} \frac{56}{39} \frac{57}{50}$$

$$\frac{63}{50} \frac{64}{37} \frac{58}{21} \frac{61}{16} \frac{56}{12} \frac{51}{15} \frac{59}{19} \frac{64}{27} \frac{54}{26} \frac{50}{50} \frac{58}{50}$$

$$\frac{60}{50} \frac{55}{24} \frac{53}{19} \frac{48}{14} \frac{55}{14} \frac{57}{20} \frac{50}{23} \frac{51}{31} \frac{59}{50}$$

$$\frac{57}{50} \frac{52}{32} \frac{52}{13} \frac{46}{14} \frac{53}{20} \frac{57}{23} \frac{49}{36} \frac{52}{50} \frac{58}{50}$$

$$\frac{58}{50} \frac{53}{31} \frac{48}{14} \frac{52}{13} \frac{46}{15} \frac{52}{21} \frac{60}{23} \frac{51}{36} \frac{51}{50} \frac{56}{50}$$

$$\frac{57}{50} \frac{52}{33} \frac{48}{15} \frac{51}{14} \frac{45}{14} \frac{52}{17} \frac{57}{24} \frac{50}{50} \frac{54}{50}$$

$$\frac{52}{50} \frac{48}{25} \frac{55}{16} \frac{50}{14} \frac{45}{14} \frac{51}{17} \frac{55}{23} \frac{47}{29} \frac{51}{50} \frac{52}{50}$$

Nail in P.P. at 36+

$$\frac{65}{50} \frac{62}{26} \frac{55}{14} \frac{49}{13} \frac{54}{14} \frac{59}{20} \frac{58}{22} \frac{53}{32} \frac{57}{50} \frac{57}{50}$$

$$\frac{64}{50} \frac{62}{23} \frac{54}{14} \frac{49}{12} \frac{53}{14} \frac{63}{19} \frac{61}{22} \frac{52}{50} \frac{55}{50}$$

$$\frac{63}{50} \frac{60}{32} \frac{57}{21} \frac{53}{14} \frac{48}{12} \frac{53}{14} \frac{65}{19} \frac{60}{22} \frac{52}{50} \frac{59}{50}$$

$$\frac{64}{50} \frac{58}{32} \frac{58}{19} \frac{52}{13} \frac{47}{12} \frac{53}{14} \frac{62}{17} \frac{62}{21} \frac{52}{38} \frac{58}{50} \frac{60}{50}$$

Sta + - Elev

938.26

39

+50

40

+50

B.M.

5.44

932.82

932.82

41

+50

42

+50

43

T.P.

4.78

938.05

4.99

933.27

+50

44

Lt.

2

Rt.

$$\begin{array}{cccccccccccc} \frac{6.1}{50} & \frac{6.3}{33} & \frac{6.2}{20} & \frac{5.2}{13} & \frac{4.1}{11} & \frac{5.2}{14} & \frac{6.7}{18} & \frac{6.8}{20} & \frac{5.5}{35} & \frac{5.9}{50} & \frac{5.9}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{6.0}{50} & \frac{6.0}{36} & \frac{5.8}{21} & \frac{5.3}{13} & \frac{5.0}{12} & \frac{5.4}{14} & \frac{6.3}{14} & \frac{6.2}{33} & \frac{6.3}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{6.2}{50} & \frac{6.3}{33} & \frac{6.1}{17} & \frac{5.4}{12} & \frac{5.0}{13} & \frac{5.5}{16} & \frac{6.0}{16} & \frac{6.4}{31} & \frac{6.6}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{6.5}{50} & \frac{6.3}{33} & \frac{6.3}{18} & \frac{5.6}{14} & \frac{5.0}{13} & \frac{5.6}{16} & \frac{6.1}{16} & \frac{6.4}{32} & \frac{6.6}{50} \end{array}$$

Spt. in 30" R.E. pt. sta. 40 + 98

$$\begin{array}{cccccccccccc} \frac{6.0}{50} & \frac{6.4}{33} & \frac{6.4}{18} & \frac{5.6}{14} & \frac{4.9}{13} & \frac{5.4}{16} & \frac{6.0}{16} & \frac{5.9}{36} & \frac{5.8}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{6.1}{50} & \frac{6.1}{31} & \frac{6.3}{17} & \frac{5.4}{13} & \frac{5.0}{13} & \frac{5.4}{15} & \frac{6.0}{15} & \frac{6.1}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{6.1}{50} & \frac{5.8}{29} & \frac{6.4}{16} & \frac{5.3}{13} & \frac{5.0}{13} & \frac{5.5}{15} & \frac{6.0}{15} & \frac{6.2}{30} & \frac{6.3}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{6.1}{50} & \frac{6.6}{32} & \frac{6.5}{16} & \frac{5.3}{12} & \frac{5.1}{13} & \frac{5.7}{16} & \frac{6.1}{16} & \frac{6.1}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{6.4}{50} & \frac{6.1}{32} & \frac{6.1}{16} & \frac{5.5}{13} & \frac{5.0}{13} & \frac{5.6}{14} & \frac{6.0}{14} & \frac{5.9}{32} & \frac{5.9}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{5.8}{50} & \frac{6.1}{33} & \frac{6.1}{16} & \frac{5.3}{13} & \frac{4.8}{12} & \frac{5.3}{12} & \frac{5.9}{14} & \frac{5.9}{27} & \frac{5.8}{50} \end{array}$$

$$\begin{array}{cccccccccccc} \frac{5.9}{50} & \frac{5.8}{36} & \frac{6.1}{16} & \frac{5.3}{14} & \frac{4.8}{12} & \frac{5.3}{14} & \frac{5.8}{14} & \frac{5.2}{23} & \frac{5.7}{36} & \frac{5.5}{50} \end{array}$$

Sta	+	π	-	Elev.
		938.05		

44 +50

45

+50

46

+50

47

+50

I.P.	4.51	938.00	4.56	933.49
------	------	--------	------	--------

48

B.M.	5.03	937.90	5.15	932.85	(932.87)
------	------	--------	------	--------	----------

+50

49

+50

Lt.

x

Rt.

$$\begin{array}{r} 59 \quad 59 \quad 52 \quad 47 \quad 52 \quad 57 \quad 59 \\ 50 \quad 17 \quad 14 \quad 12 \quad 27 \quad 50 \end{array}$$

$$\begin{array}{r} 60 \quad 58 \quad 59 \quad 51 \quad 47 \quad 52 \quad 50 \quad 56 \quad 57 \\ 50 \quad 34 \quad 18 \quad 13 \quad 12 \quad 22 \quad 38 \quad 50 \end{array}$$

$$\begin{array}{r} 61 \quad 61 \quad 58 \quad 51 \quad 47 \quad 50 \quad 61 \quad 54 \quad 56 \\ 50 \quad 34 \quad 16 \quad 13 \quad 12 \quad 15 \quad 22 \quad 50 \end{array}$$

$$\begin{array}{r} 59 \quad 57 \quad 59 \quad 52 \quad 47 \quad 52 \quad 58 \quad 58 \quad 55 \quad 55 \quad 56 \\ 50 \quad 36 \quad 16 \quad 13 \quad 12 \quad 15 \quad 19 \quad 21 \quad 36 \quad 50 \end{array}$$

$$\begin{array}{r} 63 \quad 63 \quad 57 \quad 52 \quad 49 \quad 54 \quad 65 \quad 66 \quad 56 \quad 56 \quad 53 \\ 50 \quad 32 \quad 16 \quad 12 \quad 13 \quad 16 \quad 18 \quad 21 \quad 36 \quad 50 \end{array}$$

$$\begin{array}{r} 59 \quad 63 \quad 65 \quad 62 \quad 54 \quad 49 \quad 56 \quad 64 \quad 64 \quad 58 \quad 58 \\ 50 \quad 34 \quad 27 \quad 14 \quad 12 \quad 13 \quad 15 \quad 17 \quad 26 \quad 50 \end{array}$$

$$\begin{array}{r} 64 \quad 66 \quad 60 \quad 54 \quad 48 \quad 53 \quad 63 \quad 63 \quad 52 \quad 60 \quad 54 \\ 50 \quad 26 \quad 15 \quad 13 \quad 12 \quad 15 \quad 19 \quad 22 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 62 \quad 57 \quad 54 \quad 47 \quad 57 \quad 59 \quad 57 \\ 50 \quad 15 \quad 13 \quad 12 \quad 15 \quad 50 \end{array}$$

Spl. in 36" O. SE Cor. S.T.H. 96 * Birch Lake Blva S.

$$\begin{array}{r} 62 \quad 56 \quad 61 \quad 53 \quad 48 \quad 65 \quad 65 \quad 58 \quad 58 \quad 58 \\ 50 \quad 36 \quad 17 \quad 14 \quad 12 \quad 17 \quad 19 \quad 23 \quad 40 \quad 50 \end{array}$$

$$\begin{array}{r} 67 \quad 62 \quad 56 \quad 52 \quad 46 \quad 51 \quad 69 \quad 69 \quad 55 \quad 55 \\ 50 \quad 37 \quad 19 \quad 13 \quad 12 \quad 16 \quad 18 \quad 20 \quad 50 \end{array}$$

$$\begin{array}{r} 61 \quad 63 \quad 53 \quad 53 \quad 48 \quad 45 \quad 51 \quad 21 \quad 71 \quad 57 \quad 47 \quad 49 \\ 50 \quad 27 \quad 21 \quad 14 \quad 11 \quad 12 \quad 17 \quad 19 \quad 22 \quad 42 \quad 50 \end{array}$$

Sta + π - Elev

937.90

50

+22

+50

+78.2 Kt. Δ

+78.2 Profile S.T.H 96

51 Lt only

+33

+41

+50

52

+50

Lt.

4

Rt.

$$\begin{array}{r} 73 \\ 50 \end{array} \frac{82}{46} \frac{84}{41} \frac{61}{53} \frac{59}{13} \quad \frac{50}{11} \quad \frac{45}{13} \frac{49}{18} \frac{69}{20} \frac{59}{24} \frac{53}{50}$$

$$\frac{58}{50} \frac{60}{24} \frac{49}{9} \frac{46}{9} \quad \frac{49}{12} \frac{75}{18} \frac{75}{22} \frac{57}{26} \frac{56}{50}$$

$$\frac{64}{50} \frac{58}{44} \frac{53}{30} \quad \frac{45}{13} \frac{52}{18} \frac{76}{22} \frac{76}{25} \frac{61}{25} \frac{56}{50}$$

$$\frac{66}{50} \frac{67}{42} \frac{78}{36} \frac{74}{32} \frac{57}{27} \frac{48}{19} \frac{44}{19} \quad \frac{48}{13} \frac{55}{23} \quad \frac{77}{32} \frac{77}{38} \frac{60}{42} \frac{60}{50}$$

$$\frac{63}{150} \frac{60}{100} \frac{55}{50} \quad \frac{44}{50} \frac{52}{50} \frac{58}{100} \frac{63}{150}$$

$$\frac{64}{50} \frac{63}{32} \frac{58}{23} \frac{61}{21} \frac{60}{18} \frac{52}{14} \frac{45}{14}$$

$$\frac{66}{50} \frac{64}{29} \frac{65}{15} \frac{53}{11} \quad \frac{47}{13} \frac{52}{29} \frac{56}{29} \frac{57}{50}$$

(w/v.)

$$\frac{65}{50} \frac{65}{15} \frac{53}{11} \quad \frac{47}{12} \frac{53}{18} \frac{76}{29} \frac{79}{29} \frac{810}{29} \frac{58}{33} \frac{58}{50}$$

$$\frac{68}{50} \frac{36}{24} \frac{65}{18} \frac{66}{15} \frac{51}{11} \quad \frac{47}{11} \frac{53}{19} \frac{80}{23} \frac{80}{23} \frac{65}{27} \frac{67}{34} \frac{82}{18} \frac{82}{42} \frac{65}{50}$$

$$\frac{58}{50} \frac{58}{49} \frac{58}{21} \frac{65}{19} \frac{65}{16} \frac{50}{10} \quad \frac{46}{12} \frac{53}{17} \frac{80}{20} \frac{80}{25} \frac{65}{25} \frac{63}{50}$$

$$\frac{55}{50} \frac{56}{24} \frac{65}{20} \frac{65}{16} \quad \frac{50}{12} \quad \frac{46}{17} \frac{53}{16} \frac{82}{20} \frac{82}{29} \frac{61}{29} \frac{64}{50}$$

Sta.	+	π	-	Elev.
		937.90		

53

I.P.

4.82 933.08

Lt.

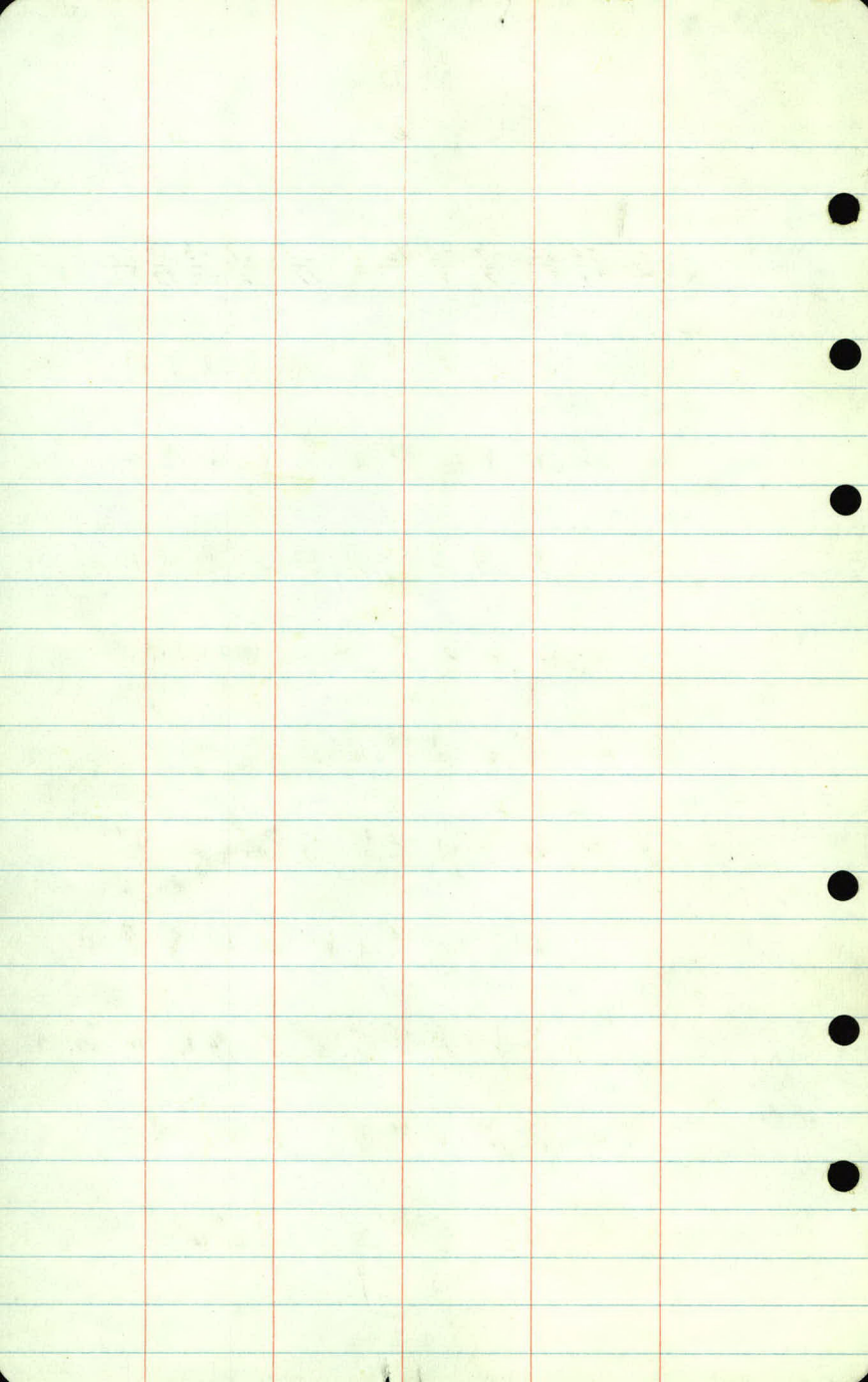
K

Rt.

$$\begin{array}{r} 55 \ 56 \ 65 \ 67 \ 52 \ 46 \\ 50 \ 29 \ 23 \ 17 \ 13 \end{array}$$

$$\begin{array}{r} 53 \ 81 \ 88 \ 62 \ 64 \\ 11 \ 16 \ 22 \ 33 \ 50 \end{array}$$

Nail in RR Pt. sta. 53+



Bench Levels

Sta.	+	π	-	Elev.
B.M.	12.88	932.34		(919.46)
T.P.	7.98	939.02	1.30	931.04
T.P.	7.51	942.20	4.53	934.69
T.P.	8.91	949.03	2.08	940.12
B.M.	6.71	954.70	1.04	947.99
T.P.	6.42	956.54	4.58	950.12
T.P.	3.34	953.59	6.29	950.25
B.M.			6.04	947.55
T.P.	11.94	963.39	2.14	951.45
T.P.	0.31	959.59	4.11	959.28
T.P.	0.48	947.42	12.65	946.94
T.P.	1.40	936.57	12.45	934.97
B.M.	5.25	936.75	4.87	931.50
T.P.	5.58	938.72	3.61	933.14
B.M.	5.47	938.29	5.90	932.82
T.P.	4.55	937.92	4.92	933.37
B.M.	5.57	938.44	5.05	932.87
T.P.	1.30	933.97	5.17	932.67
T.P.	4.23	928.64	9.56	924.41
B.M.			4.94	923.70
T.P.	7.88	934.85	1.67	926.97
B.M.			4.41	930.49 (930.97)

Description

High point Mont. at Centerville Rd. + Co. Rd. "F"

Top Mont. Centerville Rd. + Birch Lake Blvd. Sta.

Spt. in 12" Pop. 48' Bl. Sta. 12768

Top N.W. Cor. Lower C. Conc. stop front of Ho. Sta 304

Spt. in 30" R.E. 30' Bl. Sta 40498

Spt. in 36" O.S.E. Cor. S.T.H. #96 + Birch Lake Blvd. S.

Top N. End. C.M. X drain 20' ft. Sta 66402

923.80 { from Lake Imp.
Data.

Top Mont. S.T.H. 96 + Otter Lake Rd.

