

Bk. 1 - Dr. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

RAMSEY CO. ASPHALT PLANT.
~~From~~ Co. Rd "E" & Lexington

Road Acc't. No.

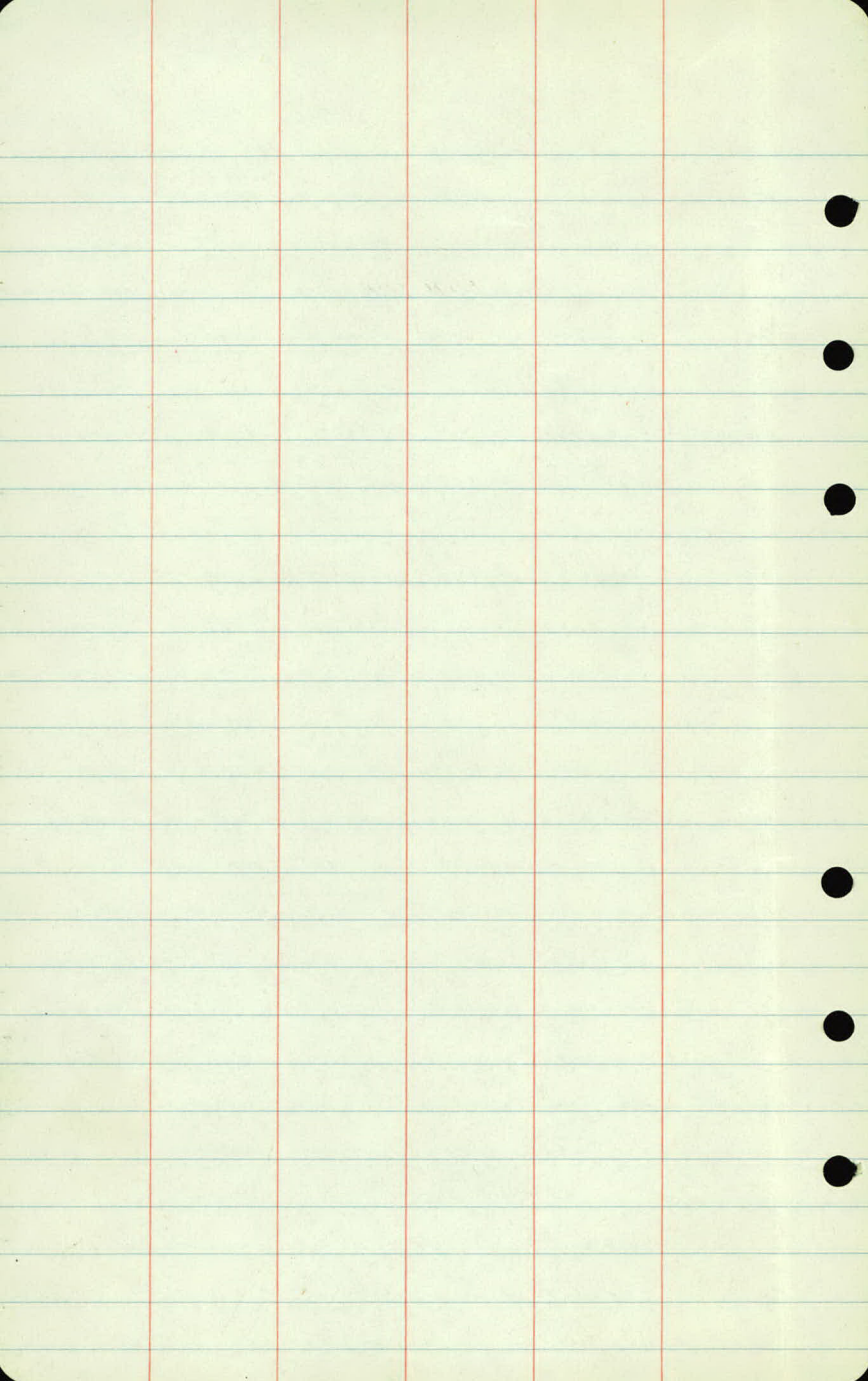
Date Filed 7/26/29

File

PLAN SURVEY
Ramsey Co. Asphalt Plant.

INDEX.

Align -	1-2
Topog. Co. Rd. E.	3-5
" Lex. Ave.	6-7
" "A" Line	8-9
" "B" Line	10-11
" "C" Line	12-13
" "D" Line	14-16
X Sections -	17-37

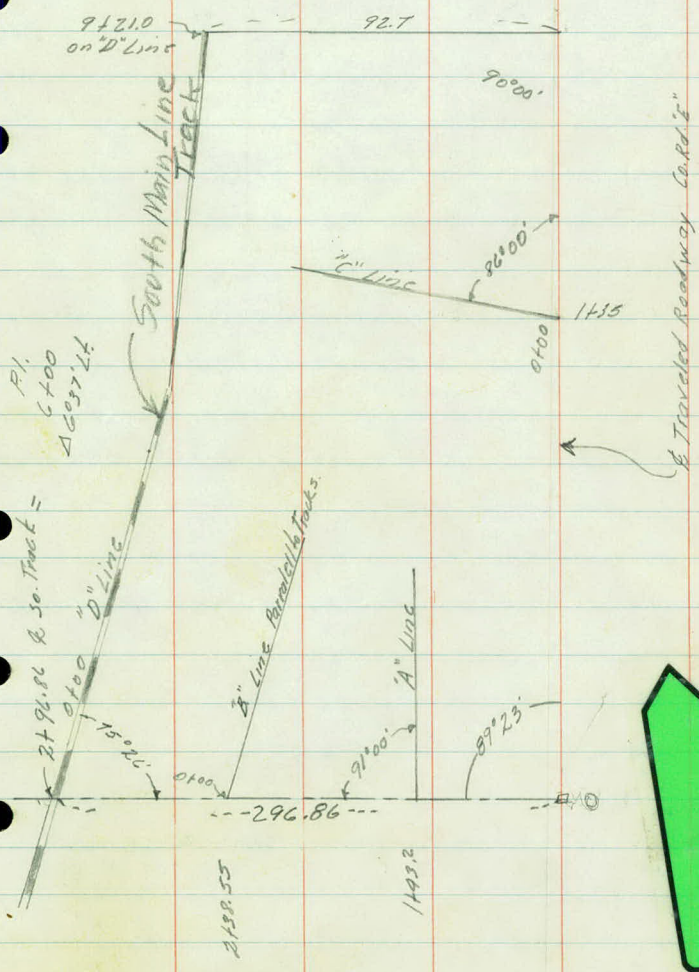


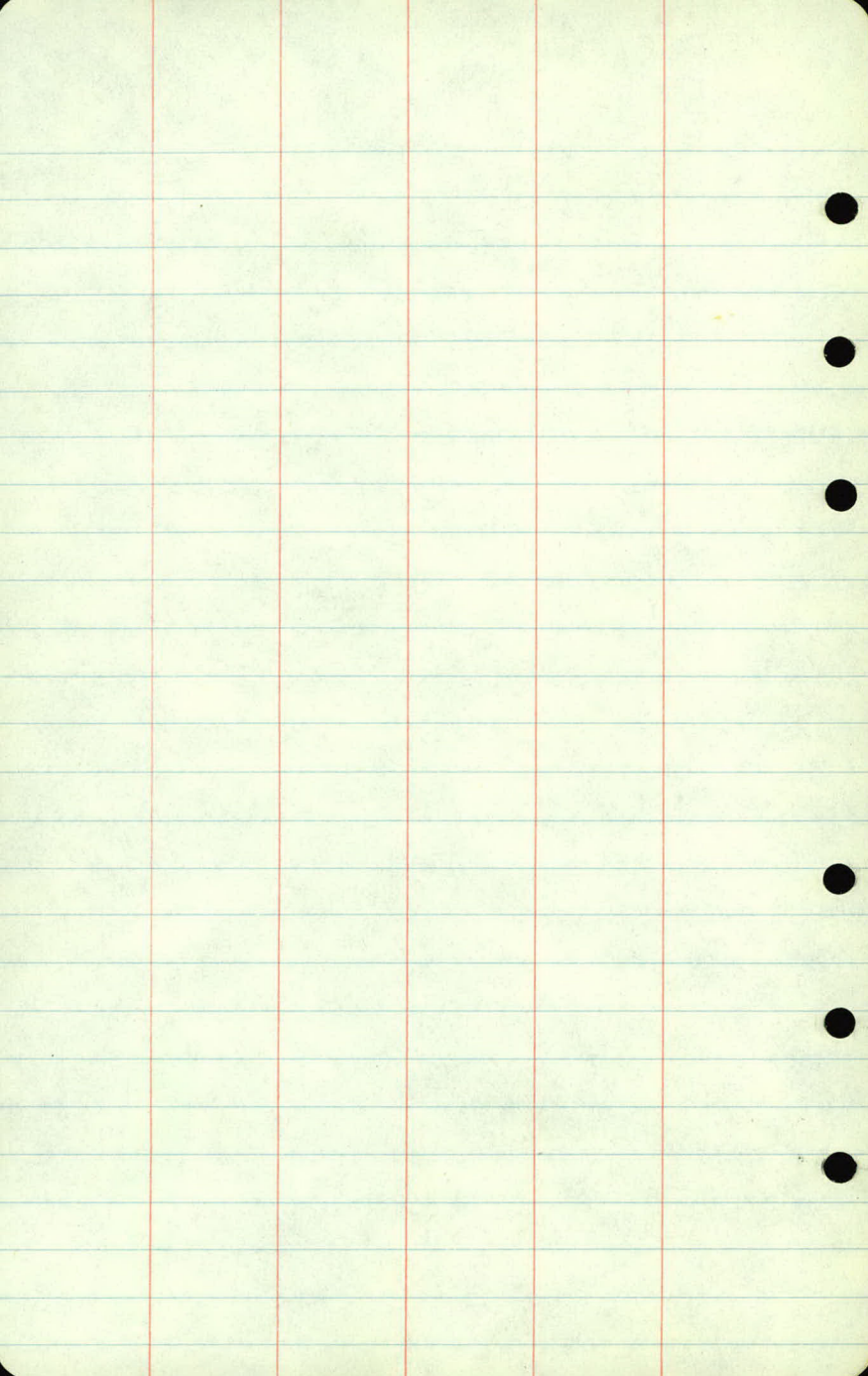
Alignment

9 100

0 100 Mont Co Rd E² Lexington Ave

6-20-39
K.A.
L.C.
A.B.





Topography
G. R. E.

11' 7'

5

11' 7'

11' 7'

4

11' 7'

11' 7'

3

10' 7'

+60-Light Pale-25'

12' 8'

2

11' 9'

12' 9'

1

+67-End G.R-26'

14' 8'

+61-G.R-26'

19'

0400

9 T.R. - 55'

7' 9'

9' 9'

8

9' 9'

7' 8'

7

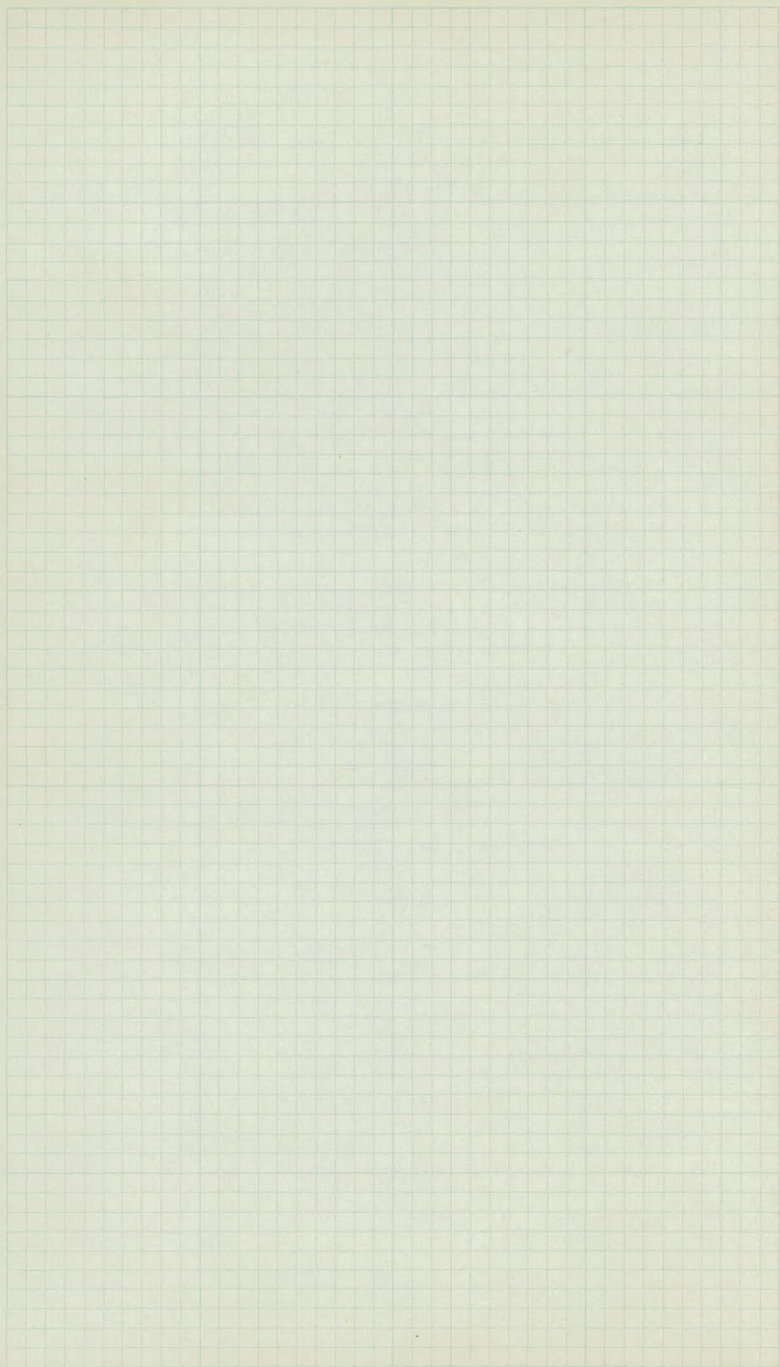
10' 8'

10' 7'

6

10' 7'





Topography
Lexington Arc

+28.86 Plank King 13.5 11'

+73.61 End Spur Track - 18'

9' 10'

+50
+97.76 L.M.H. - 14.8'

2. 8' 12'

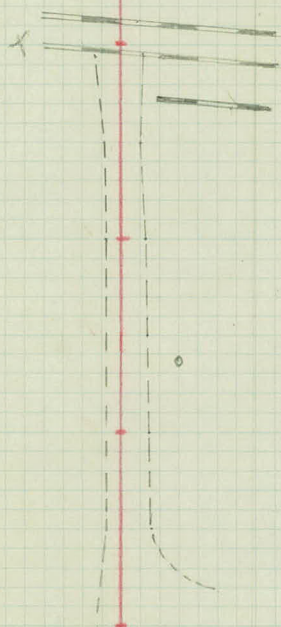
8' 13' +50

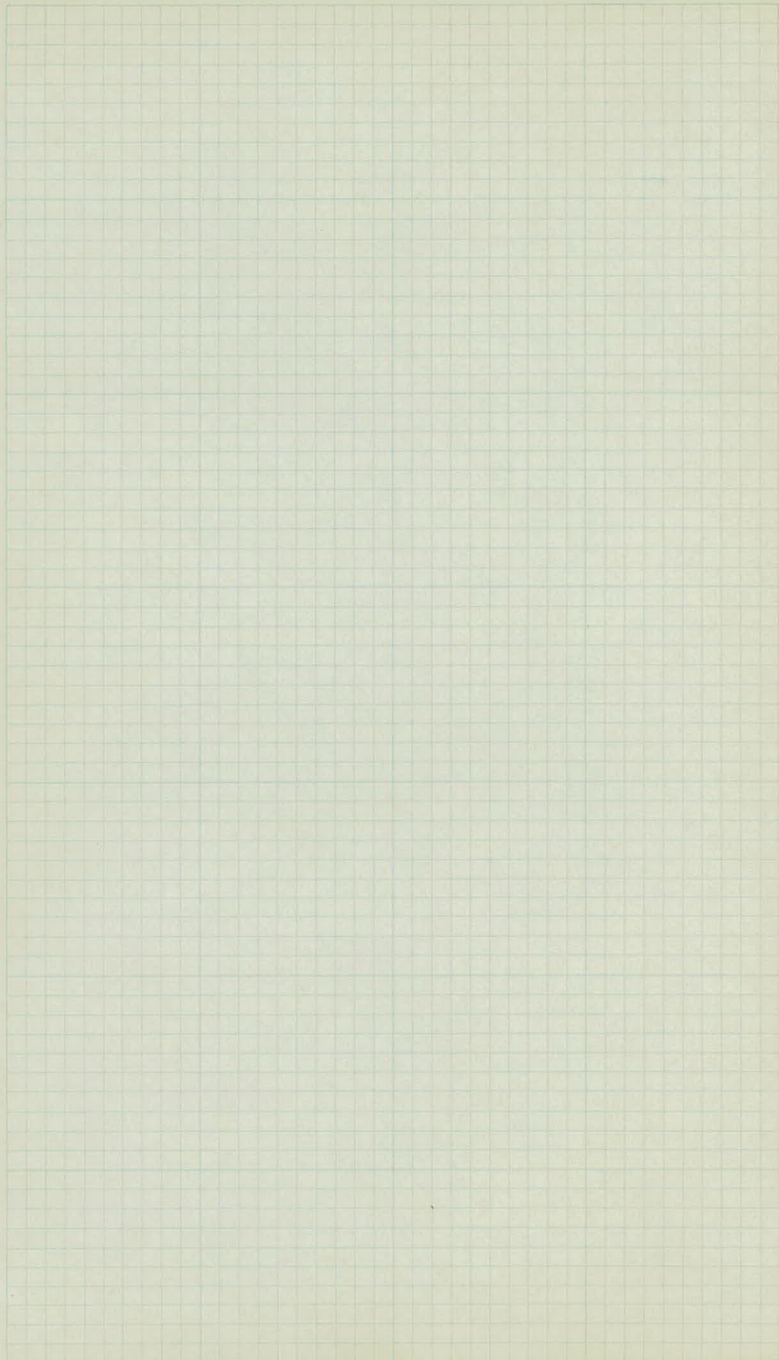
+37-PP - 30'

1 8' 14'

8' 15' +50

0700



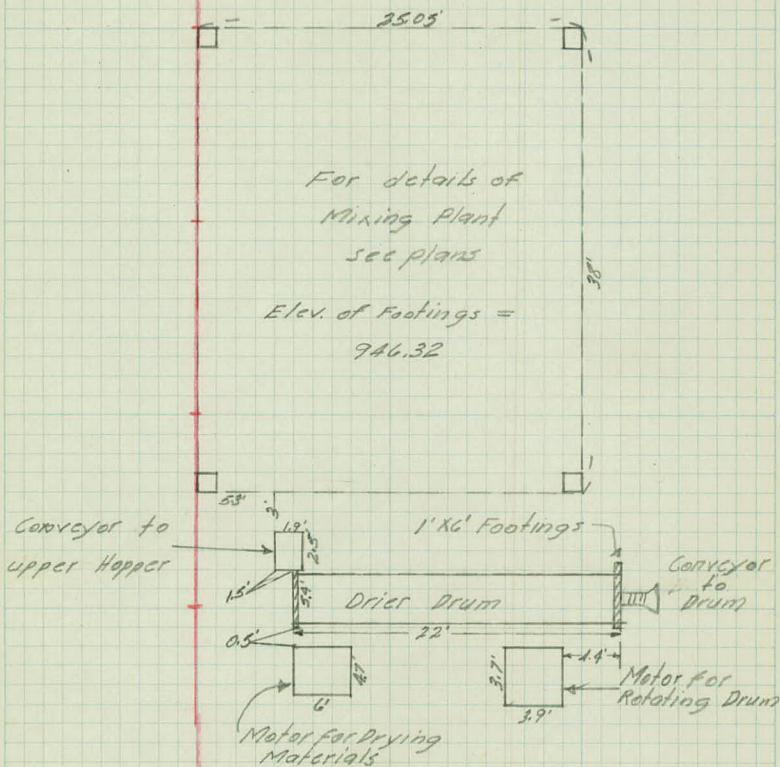


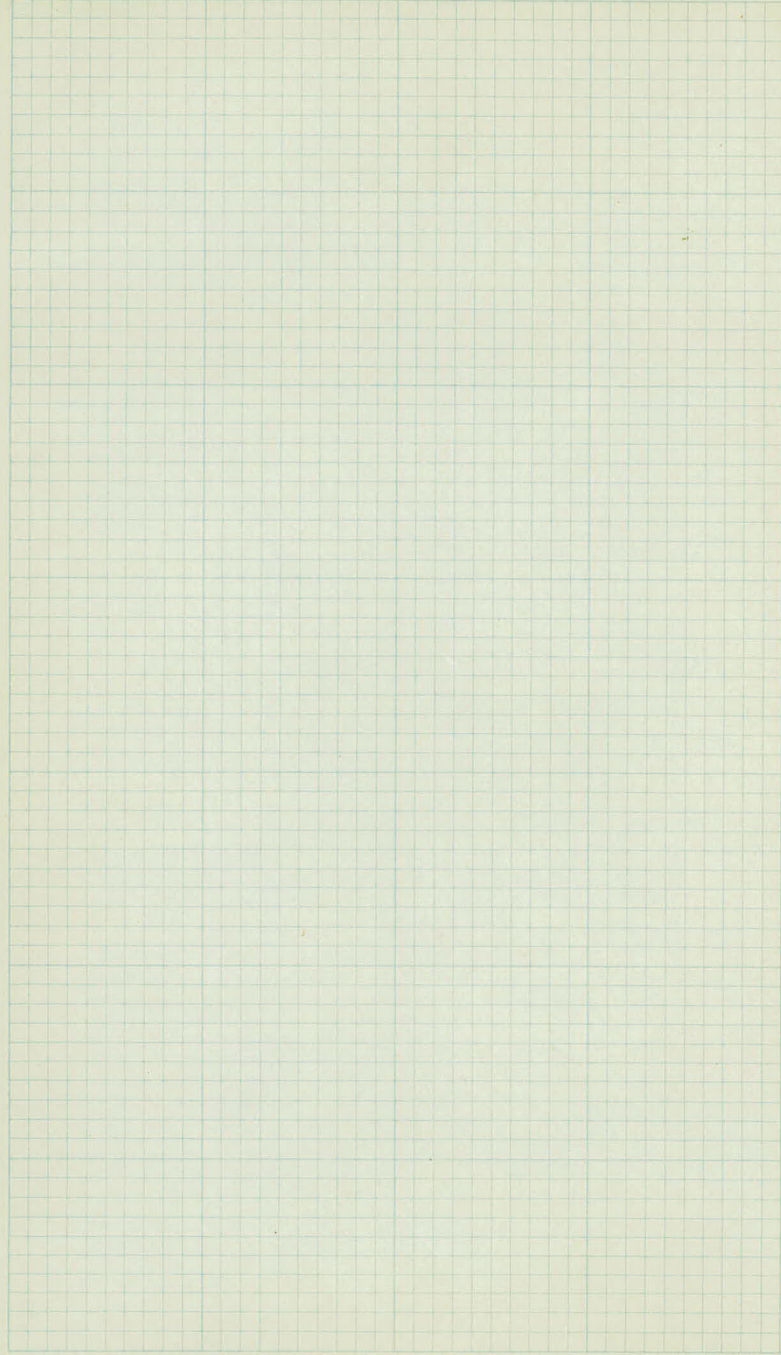
Topography

"A" Line

161.5 = N.W. Cor. of N.W. Footing of Mixing Plant - 0.0

1
(0) ?





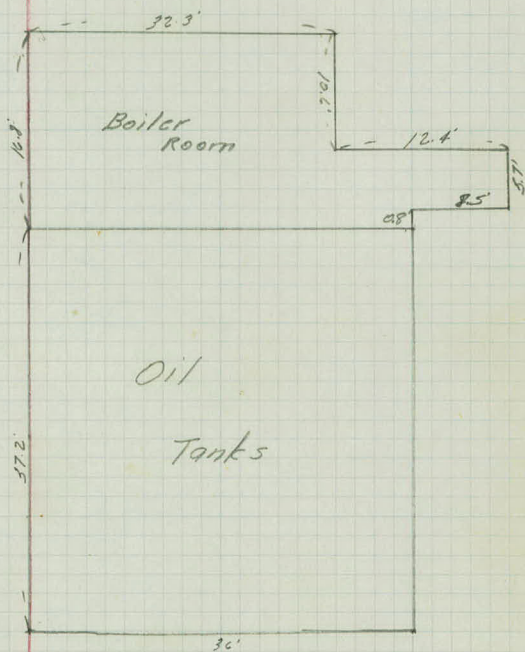
Topography
"B" Line

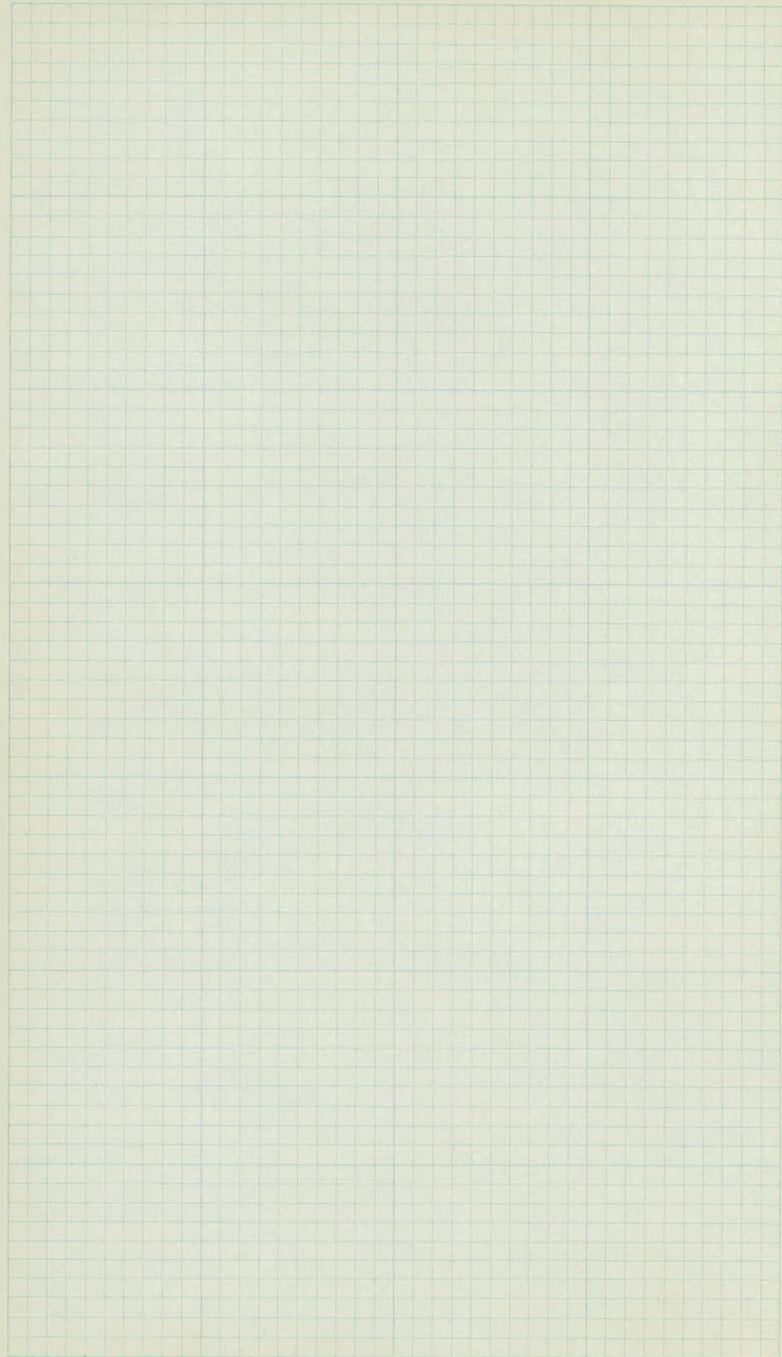
+23-Garage 15' 5'

1

+10-N.W. Cor. Conc. Base of Oil Tanks -0.0

0/100





Topography

"C" Line

2

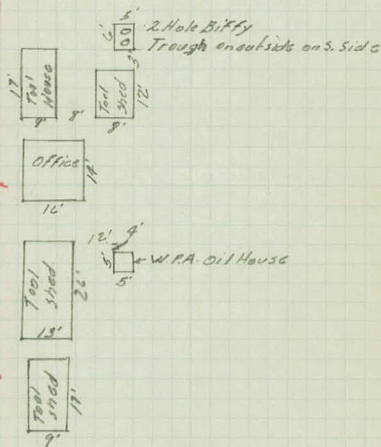
+67-Cor. County Tool House-6'

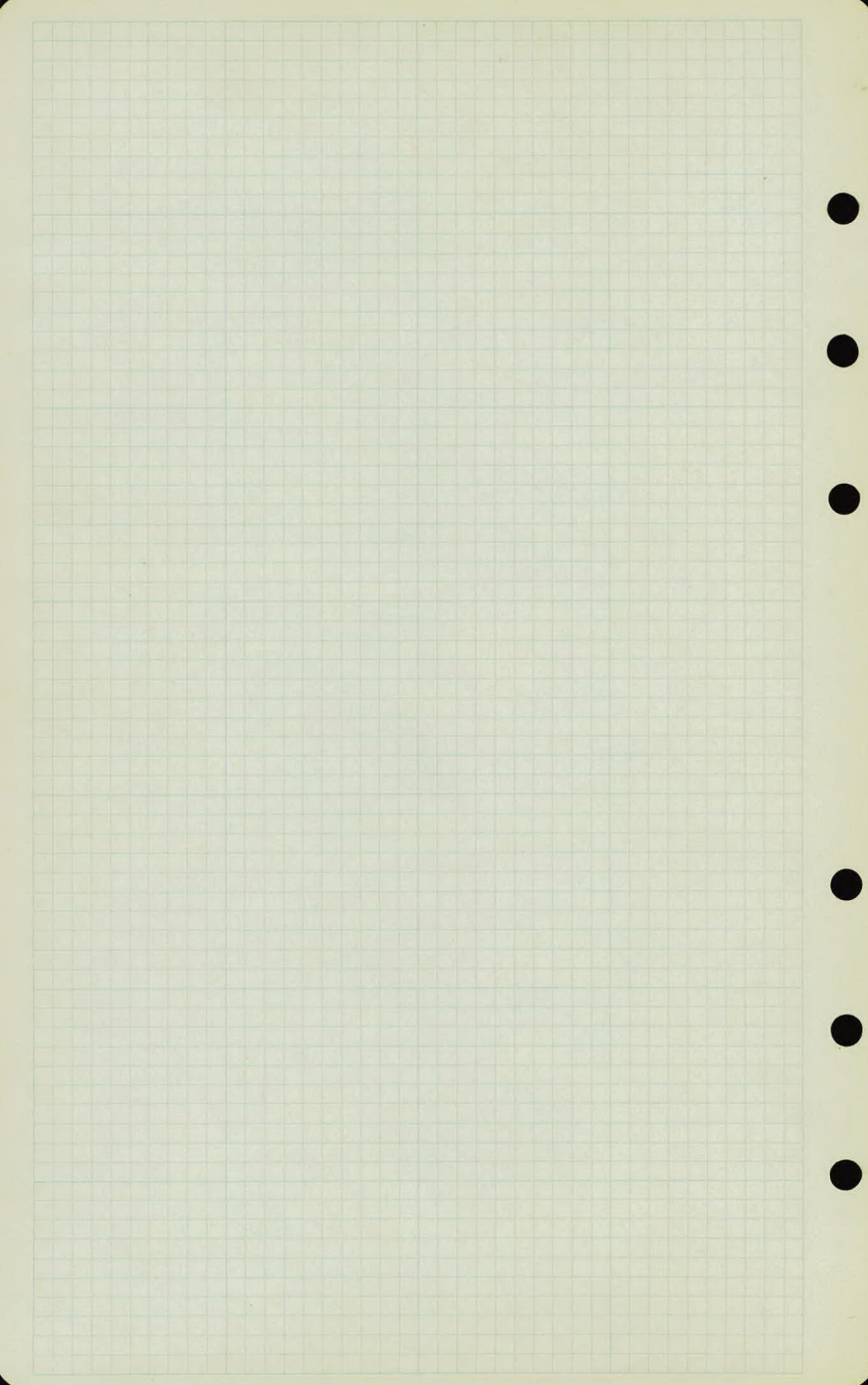
+46-Cor. Ramsey Co. Office-6'

+09-Cor. W.P.A. Tool House-6'

+87-Cor. W.P.A. Tool House-7'

0400





Topography

"D" Line

Track - 5'

5 Track - 3'

+11-T.P. - 38'

Track - 1.3'

4 Track - 0.6'

+24 Kc. - 15' End Plank Gutter - 53'

+08-T.P. - 39'

+77-6 24" X 59' Iron Culv. 39' 20'

+68-15' C.M. 45'-55'

+47.5-Point of Switch -
+33-12" C.M. 45'-53'

3

T.P. - 40' Plank Gutter - 50'

Track - 7'

+21-Beg. Plank Gutter - 38'

2

Track - 12'

+90-T.P. - 40'

+40-Unloading Valve - 20.5' Tr. 14.8'

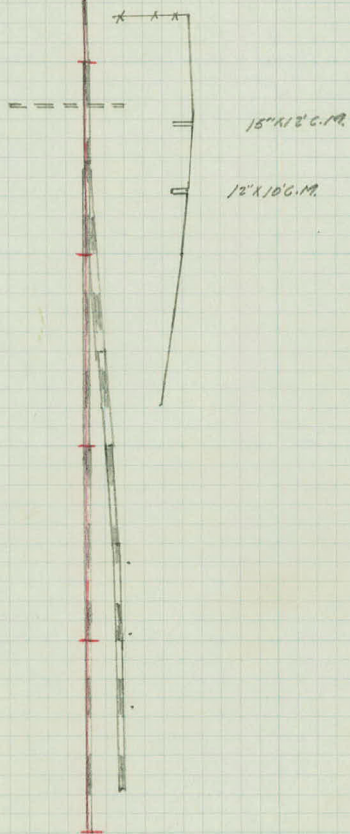
+02-Unloading Valve - 23'
Track - 16.4'

1

+64-C4 Unloading Valve - 23.5
+63-T.P. - 40'

+23-End Spur Tr. 18.5'

0100



+21. Track-3.1'

9 Track-2.7'

Track-1.8'

8 Track-1.7'

+19-T.P.-

Track-2.0'

7 Track-3.3'

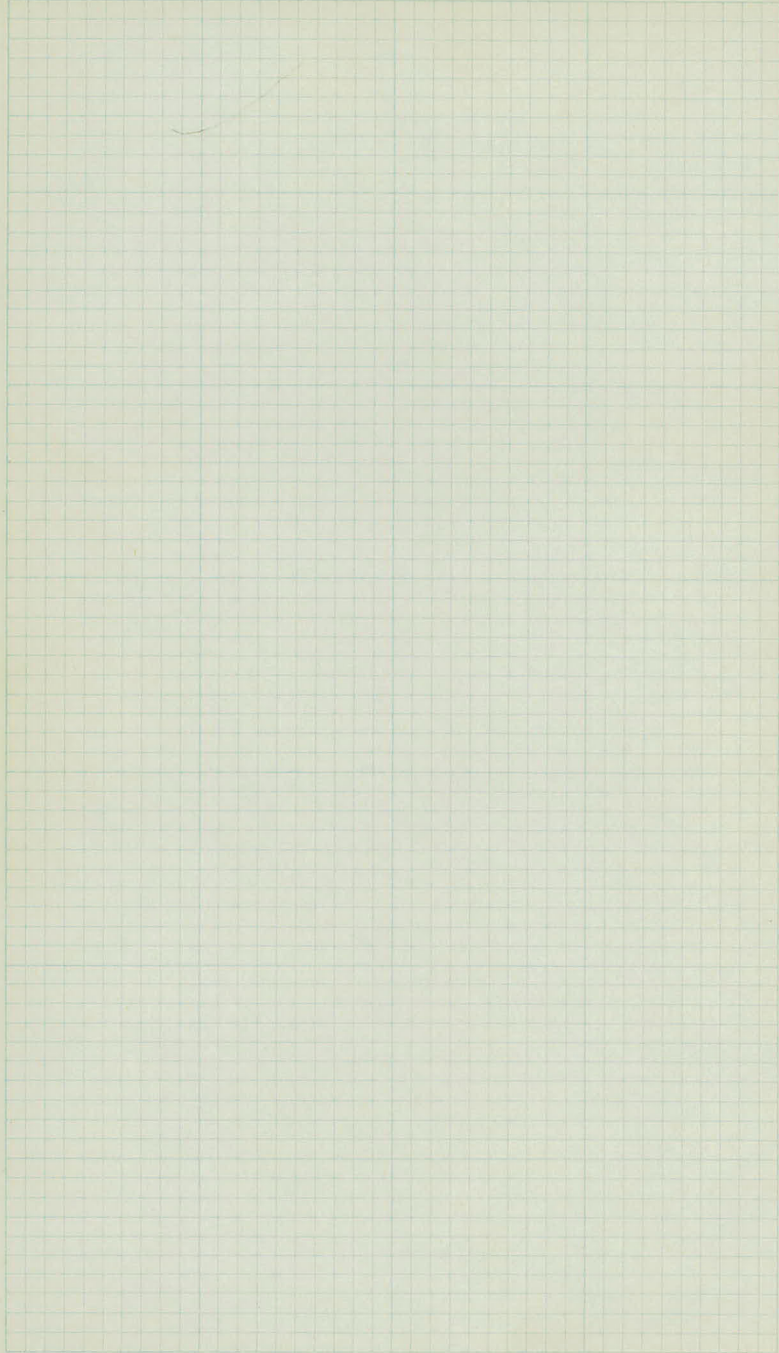
+107-T.P.-

Track-5'

6 Track-7.6'

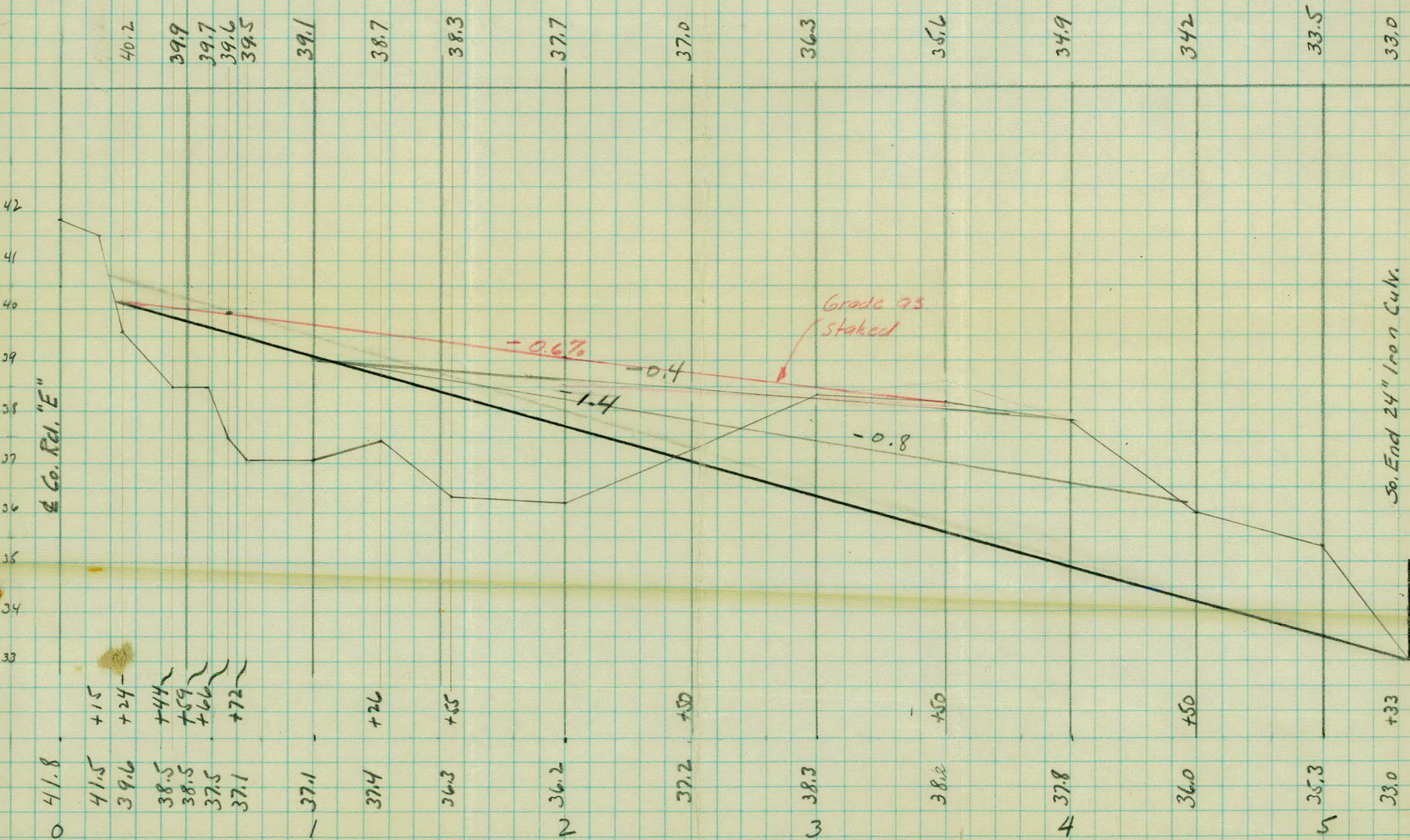
+107-T.P.-34'





Drainage @ Oil Tanks

B.M. Top Mont. "E" & Lex.
Elev. 946.31



xsections

(NOTE) All xsections are at Rt A to Co. Rd. E"

Sta	+	π	-	E/cv
B.M.	3.36	949.67		

946.31

0 +0.0

+15

+30

+40

see page 20

+50

page 20

I.P.	5.20	949.10	5.17	943.90
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+60

page 21

+10

page 21

sta.	+	π	-	Elev.
------	---	-------	---	-------

		94910		
--	--	-------	--	--

0	+80			
---	-----	--	--	--

	+90			
--	-----	--	--	--

1	+00			
---	-----	--	--	--

	+10			
--	-----	--	--	--

L.

2

44.0	44.1	44.5	44.5	44.4	44.3	44.4	44.3	44.3	44.5	44.5	44.6	44.2	45.9	46.8	47.1	20
$\frac{51}{150}$	$\frac{50}{140}$	$\frac{46}{130}$	$\frac{46}{120}$	$\frac{47}{110}$	$\frac{48}{100}$	$\frac{47}{90}$	$\frac{48}{80}$	$\frac{48}{70}$	$\frac{46}{60}$	$\frac{46}{50}$	$\frac{45}{40}$	$\frac{39}{30}$	$\frac{32}{20}$	$\frac{23}{10}$		

44.0	43.8	43.5	43.3	page 21
$\frac{51}{160}$	$\frac{53}{170}$	$\frac{56}{171}$	$\frac{58}{180}$	

44.6	44.7	44.5	44.4	44.2	44.4	44.4	44.5	44.5	44.7	45.3	46.1	46.9	47.2	19
$\frac{45}{140}$	$\frac{44}{130}$	$\frac{46}{120}$	$\frac{47}{110}$	$\frac{48}{100}$	$\frac{48}{90}$	$\frac{47}{80}$	$\frac{47}{70}$	$\frac{46}{60}$	$\frac{46}{50}$	$\frac{44}{40}$	$\frac{38}{30}$	$\frac{30}{20}$	$\frac{22}{10}$	

44.3	44.1	43.8	43.5	43.3	43.0	43.3	page 21
$\frac{48}{150}$	$\frac{50}{160}$	$\frac{53}{170}$	$\frac{56}{180}$	$\frac{58}{190}$	$\frac{61}{200}$	$\frac{58}{210}$	

44.3	44.4	44.6	44.5	44.4	44.4	44.3	44.4	44.4	44.4	44.5	44.7	45.4	46.3	47.1	47.4	17
$\frac{48}{150}$	$\frac{47}{140}$	$\frac{45}{130}$	$\frac{46}{120}$	$\frac{47}{110}$	$\frac{47}{100}$	$\frac{48}{90}$	$\frac{47}{80}$	$\frac{47}{70}$	$\frac{47}{60}$	$\frac{46}{50}$	$\frac{44}{40}$	$\frac{37}{30}$	$\frac{28}{20}$	$\frac{20}{10}$		

44.3	44.1	43.8	43.3	43.3	page 21
$\frac{48}{160}$	$\frac{50}{170}$	$\frac{53}{180}$	$\frac{58}{200}$	$\frac{58}{210}$	

44.2	44.2	44.2	44.1	44.2	44.1	44.2	44.3	44.4	44.5	44.8	45.4	46.3	47.2	47.5	16
$\frac{49}{150}$	$\frac{49}{140}$	$\frac{48}{130}$	$\frac{50}{120}$	$\frac{49}{110}$	$\frac{50}{100}$	$\frac{50}{90}$	$\frac{49}{80}$	$\frac{48}{70}$	$\frac{47}{60}$	$\frac{46}{50}$	$\frac{43}{40}$	$\frac{37}{30}$	$\frac{28}{20}$	$\frac{19}{10}$	

44.5	44.1	43.8	43.7	43.5	page 21
$\frac{46}{160}$	$\frac{50}{170}$	$\frac{53}{190}$	$\frac{54}{200}$	$\frac{56}{210}$	

Sta. + x - Elev.

949.10

1 +20

+30

+40

B.M.

2.06

948.31

2.78

946.32

946.31

0 +40

+50

14

2

44.0	44.1	44.0	44.0	43.9	44.0	44.1	44.2	44.3	44.2	44.8	45.6	46.5	47.3	47.6
$\frac{51}{140}$	$\frac{50}{130}$	$\frac{51}{120}$	$\frac{51}{110}$	$\frac{52}{100}$	$\frac{51}{90}$	$\frac{50}{80}$	$\frac{49}{70}$	$\frac{48}{60}$	$\frac{46}{50}$	$\frac{43}{40}$	$\frac{35}{30}$	$\frac{26}{20}$	$\frac{18}{10}$	$\frac{15}{1}$
44.2	44.3	44.2	44.0	43.8	43.8	43.6	Page 21							
$\frac{49}{150}$	$\frac{48}{160}$	$\frac{49}{170}$	$\frac{51}{180}$	$\frac{53}{190}$	$\frac{53}{200}$	$\frac{55}{210}$								

44.1	44.0	43.9	43.9	43.9	43.8	43.9	44.1	44.1	44.3	44.6	45.0	45.7	46.7	47.5	47.7
$\frac{50}{150}$	$\frac{51}{140}$	$\frac{52}{130}$	$\frac{52}{120}$	$\frac{52}{110}$	$\frac{53}{100}$	$\frac{52}{90}$	$\frac{50}{80}$	$\frac{50}{70}$	$\frac{48}{60}$	$\frac{45}{50}$	$\frac{41}{40}$	$\frac{34}{30}$	$\frac{29}{20}$	$\frac{16}{10}$	$\frac{14}{1}$
44.2	44.1	43.9	43.9	43.9	43.9	Page 21									
$\frac{49}{160}$	$\frac{50}{170}$	$\frac{52}{180}$	$\frac{52}{190}$	$\frac{52}{197}$											

43.9	43.9	43.9	44.0	43.9	44.0	44.0	44.1	44.3	44.4	44.7	45.1	45.9	46.7	47.5	47.8
$\frac{52}{150}$	$\frac{52}{140}$	$\frac{52}{130}$	$\frac{51}{120}$	$\frac{52}{110}$	$\frac{51}{100}$	$\frac{51}{90}$	$\frac{50}{80}$	$\frac{48}{70}$	$\frac{47}{60}$	$\frac{44}{50}$	$\frac{40}{40}$	$\frac{32}{30}$	$\frac{24}{20}$	$\frac{16}{10}$	$\frac{13}{1}$
44.0	44.1	44.0	Page 22												
$\frac{51}{160}$	$\frac{50}{170}$	$\frac{51}{180}$													

Top Mont.

43.2	43.1	43.1	43.1	43.2	43.2	43.2	43.3
$\frac{52}{284}$	$\frac{53}{280}$	$\frac{53}{270}$	$\frac{53}{260}$	$\frac{53}{250}$	$\frac{52}{240}$	$\frac{52}{230}$	$\frac{51}{220}$

43.2	43.1	43.3	43.2	43.2	43.2
$\frac{51}{291}$	$\frac{53}{270}$	$\frac{51}{260}$	$\frac{52}{250}$	$\frac{52}{240}$	$\frac{52}{230}$

Sta

+

x

-

Elev

948.37

0 +60

+70

+80

+90

1 +100

+110

+

+120

+130

T.P.

4.94

948.76

4.55

948.82

lt.

4

43.4
 $\frac{50}{278}$
 43.0
 $\frac{51}{270}$
 43.4
 $\frac{50}{260}$
 43.3
 $\frac{51}{250}$
 42.2
 $\frac{52}{240}$
 43.2
 $\frac{52}{230}$
 42.4
 $\frac{50}{223}$

42.4
 $\frac{50}{275}$
 42.2
 $\frac{52}{270}$
 42.4
 $\frac{50}{260}$
 42.4
 $\frac{50}{250}$
 42.4
 $\frac{50}{240}$
 42.3
 $\frac{51}{230}$
 42.5
 $\frac{49}{220}$

43.5
 $\frac{49}{273}$
 42.5
 $\frac{49}{270}$
 43.4
 $\frac{50}{260}$
 42.4
 $\frac{50}{250}$
 42.3
 $\frac{51}{240}$
 42.4
 $\frac{50}{230}$
 43.5
 $\frac{49}{220}$

43.5
 $\frac{49}{270}$
 43.2
 $\frac{52}{260}$
 43.5
 $\frac{49}{250}$
 43.3
 $\frac{51}{240}$
 43.2
 $\frac{52}{230}$
 43.3
 $\frac{51}{220}$

43.5
 $\frac{49}{267}$
 43.3
 $\frac{51}{260}$
 43.5
 $\frac{49}{250}$
 43.2
 $\frac{52}{240}$
 43.1
 $\frac{53}{230}$
 43.3
 $\frac{51}{220}$

43.6
 $\frac{48}{265}$
 43.5
 $\frac{49}{260}$
 43.6
 $\frac{48}{250}$
 43.3
 $\frac{51}{240}$
 43.1
 $\frac{53}{230}$
 43.3
 $\frac{51}{220}$

43.7
 $\frac{47}{262}$
 43.8
 $\frac{46}{260}$
 43.6
 $\frac{48}{250}$
 43.3
 $\frac{51}{240}$
 43.0
 $\frac{54}{230}$
 43.4
 $\frac{50}{220}$

43.7
 $\frac{47}{260}$
 43.6
 $\frac{48}{250}$
 43.3
 $\frac{51}{240}$
 42.8
 $\frac{56}{230}$
 42.8
 $\frac{56}{220}$

Sta + T - Elev

948.76

1 +40

+50

+60

+70
I.P. 1

470

944.06

B.M.

638

952.69

(946.31)

1 +50

+60

+70

43.8	43.7	43.0	42.4	42.5	43.2	43.6	43.9	43.9	44.0	43.9	44.1
$\frac{50}{254}$	$\frac{51}{238}$	$\frac{58}{250}$	$\frac{64}{223}$	$\frac{67}{220}$	$\frac{56}{210}$	$\frac{52}{200}$	$\frac{49}{190}$	$\frac{49}{180}$	$\frac{48}{170}$	$\frac{49}{160}$	$\frac{47}{150}$
43.7	43.6	43.6	43.0	42.6	43.4	43.8	43.9	44.0	43.9	44.0	44.1
$\frac{51}{257}$	$\frac{52}{250}$	$\frac{52}{240}$	$\frac{58}{230}$	$\frac{62}{220}$	$\frac{54}{210}$	$\frac{50}{200}$	$\frac{49}{190}$	$\frac{48}{180}$	$\frac{47}{170}$	$\frac{46}{160}$	$\frac{45}{150}$

page 22

43.8	43.8	43.5	42.2	43.0	43.6	44.0	43.9	44.0	44.0	44.0	44.0
$\frac{50}{251}$	$\frac{50}{237}$	$\frac{53}{230}$	$\frac{66}{220}$	$\frac{58}{210}$	$\frac{52}{200}$	$\frac{48}{190}$	$\frac{49}{180}$	$\frac{48}{170}$	$\frac{47}{160}$	$\frac{46}{150}$	$\frac{45}{140}$

page 22

43.8	43.6	43.5	42.7	42.1	42.9	43.0	43.3	43.9	43.9	43.9	43.9
$\frac{40}{249}$	$\frac{52}{240}$	$\frac{53}{230}$	$\frac{61}{220}$	$\frac{67}{216}$	$\frac{59}{214}$	$\frac{58}{210}$	$\frac{55}{200}$	$\frac{49}{190}$	$\frac{49}{180}$	$\frac{49}{170}$	$\frac{49}{160}$

page 22

ok see check on page 47

Top Mont.	43.9	44.0	44.1	44.2	44.3	44.5	44.7	45.2	46.0	46.8	47.7	47.9
$\frac{88}{110}$	$\frac{87}{100}$	$\frac{86}{90}$	$\frac{85}{80}$	$\frac{84}{70}$	$\frac{83}{60}$	$\frac{80}{50}$	$\frac{75}{40}$	$\frac{67}{30}$	$\frac{59}{20}$	$\frac{50}{10}$	$\frac{48}{1}$	$\frac{47}{1}$

43.8	43.7	44.1	44.4	44.5	44.6	45.2	46.1	46.9	47.8	48.0	48.0	48.0
$\frac{89}{100}$	$\frac{90}{90}$	$\frac{86}{80}$	$\frac{83}{70}$	$\frac{82}{60}$	$\frac{81}{50}$	$\frac{75}{40}$	$\frac{66}{30}$	$\frac{58}{20}$	$\frac{49}{10}$	$\frac{47}{1}$	$\frac{46}{1}$	$\frac{45}{1}$

43.8	43.7	43.7	44.1	44.4	44.6	44.6	45.2	46.1	47.0	47.9	48.1	48.1
$\frac{89}{120}$	$\frac{90}{110}$	$\frac{90}{100}$	$\frac{86}{90}$	$\frac{83}{80}$	$\frac{81}{70}$	$\frac{81}{60}$	$\frac{75}{50}$	$\frac{66}{40}$	$\frac{57}{30}$	$\frac{48}{20}$	$\frac{46}{10}$	$\frac{45}{1}$

44.0	44.1	43.9	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0
$\frac{87}{130}$	$\frac{86}{140}$	$\frac{88}{150}$	$\frac{87}{160}$	$\frac{87}{170}$	$\frac{87}{180}$	$\frac{87}{190}$	$\frac{87}{200}$	$\frac{87}{210}$	$\frac{87}{220}$	$\frac{87}{230}$	$\frac{87}{240}$	$\frac{87}{250}$

Sta

+

π

-

Elev.

952.69

1 +80

1 +90

B.M.

6.24

952.55

6.88

946.31

2

+10

Sta.	+	π	-	Elev.
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		952.55		
--	--	--------	--	--

2	+20			
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	+30			
--	-----	--	--	--

T.P.	4.65	953.13	407	948.48
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	+40			
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	+50			
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Page 27

	+60			
--	-----	--	--	--

L.

R

$\frac{93}{150}$	$\frac{94}{140}$	$\frac{91}{150}$	$\frac{95}{126}$	$\frac{93}{120}$	$\frac{91}{110}$	$\frac{90}{100}$	$\frac{90}{90}$	$\frac{88}{80}$	$\frac{85}{70}$	$\frac{85}{12}$	$\frac{85}{10}$	$\frac{84}{10}$	$\frac{89}{10}$
43.3	43.2	43.5	43.1	43.3	43.5	43.6	43.6	43.8	44.1	48.1	48.3	48.7	

$\frac{95}{160}$	$\frac{97}{170}$	$\frac{98}{150}$	$\frac{100}{194}$	$\frac{93}{195}$	$\frac{116}{200}$	$\frac{115}{201}$	$\frac{96}{204}$	$\frac{92}{216}$	$\frac{85}{233}$				
43.1	42.9	42.8	42.6	43.3	41.1	41.1	43.0	43.4	44.1				

$\frac{108}{191}$	$\frac{104}{190}$	$\frac{101}{170}$	$\frac{97}{160}$	$\frac{95}{150}$	$\frac{98}{190}$	$\frac{95}{130}$	$\frac{92}{120}$	$\frac{92}{110}$	$\frac{92}{100}$	$\frac{90}{90}$	$\frac{87}{80}$	$\frac{90}{70}$	$\frac{89}{10}$	$\frac{89}{10}$
41.8	42.2	42.5	42.9	43.1	43.1	43.4	43.4	43.4	43.6	43.9	43.6	48.3	48.7	
40.3	40.4	42.3	44.2	44.2										
$\frac{123}{196}$	$\frac{122}{198}$	$\frac{107}{202}$	$\frac{84}{220}$	$\frac{84}{231}$										

$\frac{108}{186}$	$\frac{113}{185}$	$\frac{108}{160}$	$\frac{102}{190}$	$\frac{101}{130}$	$\frac{101}{120}$	$\frac{98}{110}$	$\frac{97}{100}$	$\frac{96}{90}$	$\frac{96}{80}$	$\frac{98}{70}$	$\frac{90}{60}$	$\frac{98}{10}$	$\frac{45}{10}$	
42.3	41.8	42.3	42.9	43.0	43.0	43.3	43.4	43.5	43.5	43.3	44.1	48.3	48.6	

$\frac{110}{182}$	$\frac{116}{181}$	$\frac{108}{160}$	$\frac{106}{150}$	$\frac{104}{140}$	$\frac{103}{130}$	$\frac{103}{120}$	$\frac{98}{110}$	$\frac{95}{90}$	$\frac{94}{80}$	$\frac{89}{70}$	$\frac{86}{60}$	$\frac{83}{50}$	$\frac{48}{16}$	$\frac{45}{10}$
42.1	41.5	42.3	42.5	42.7	42.8	42.8	43.3	43.3	43.6	43.7	44.2	44.5	47.8	48.3

$\frac{112}{160}$	$\frac{107}{150}$	$\frac{106}{140}$	$\frac{106}{130}$	$\frac{105}{120}$	$\frac{98}{80}$	$\frac{94}{70}$	$\frac{89}{60}$	$\frac{87}{50}$	$\frac{80}{40}$	$\frac{73}{30}$	$\frac{58}{20}$	$\frac{48}{10}$	$\frac{45}{10}$	
41.9	42.4	42.5	42.5	42.6	43.3	43.7	44.2	44.4	45.1	45.7	47.3	48.3	48.6	

$\frac{114}{170}$	$\frac{119}{177}$	$\frac{112}{178}$												
41.4	41.2	41.9												

Page 21

Sta

+

π

-

Elev.

953.13

2 +70

+80

+90

3 +00

Sta + π - Elev

953.13

3 +10

+20

B.M.

6.37

952.68

6.82

946.31

946.31

+30

Page 28

+40

Page 28

+50

Page 28

+60

+70

+80

14

R

Page 28

$\frac{110}{120}$	$\frac{102}{90}$	$\frac{99}{80}$	$\frac{96}{70}$	$\frac{94}{60}$	$\frac{89}{50}$	$\frac{82}{40}$	$\frac{70}{30}$	$\frac{55}{20}$	$\frac{49}{10}$	$\frac{45}{1}$
42.1	42.9	43.2	43.5	43.7	44.2	44.9	46.1	47.6	48.2	48.4

$\frac{110}{130}$	$\frac{109}{120}$	$\frac{104}{90}$	$\frac{102}{80}$	$\frac{99}{70}$	$\frac{97}{60}$	$\frac{90}{50}$	$\frac{82}{40}$	$\frac{70}{30}$	$\frac{57}{20}$	$\frac{48}{10}$	$\frac{45}{1}$
42.1	42.2	42.7	42.9	43.2	43.4	44.1	44.9	46.1	47.4	48.3	48.6

Top Mont.
42.2
41.6
41.8
42.1

$\frac{105}{152}$	$\frac{111}{150}$	$\frac{109}{140}$	$\frac{106}{130}$	$\frac{105}{120}$	$\frac{99}{90}$	$\frac{96}{80}$	$\frac{93}{70}$	$\frac{90}{60}$	$\frac{83}{50}$	$\frac{77}{40}$	$\frac{66}{30}$	$\frac{52}{20}$	$\frac{44}{10}$	$\frac{41}{1}$
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42.4	41.6	41.7	42.0	42.3	42.9	43.3	43.7	43.9	44.3	45.2	46.2	47.5	48.4	48.6
$\frac{103}{148}$	$\frac{111}{146}$	$\frac{110}{140}$	$\frac{107}{130}$	$\frac{104}{120}$	$\frac{95}{90}$	$\frac{94}{80}$	$\frac{90}{70}$	$\frac{88}{60}$	$\frac{84}{50}$	$\frac{75}{40}$	$\frac{65}{30}$	$\frac{52}{20}$	$\frac{43}{10}$	$\frac{41}{1}$

42.5	41.8	41.8	42.0	42.1	43.2	43.5	43.8	44.0	44.4	45.1	46.3	47.4	48.1	48.4	48.6	48.6
$\frac{102}{145}$	$\frac{109}{144}$	$\frac{109}{140}$	$\frac{107}{130}$	$\frac{106}{120}$	$\frac{95}{90}$	$\frac{92}{80}$	$\frac{89}{70}$	$\frac{87}{60}$	$\frac{83}{50}$	$\frac{76}{40}$	$\frac{64}{30}$	$\frac{53}{20}$	$\frac{46}{16}$	$\frac{43}{10}$	$\frac{41}{1}$	$\frac{41}{1}$

	42.7	42.1	42.1	42.3	43.7	43.9	44.1	44.4	45.0	46.4	47.9	48.4	48.6
Page 29	$\frac{100}{142}$	$\frac{106}{140}$	$\frac{106}{130}$	$\frac{104}{120}$	$\frac{90}{80}$	$\frac{88}{70}$	$\frac{86}{60}$	$\frac{83}{50}$	$\frac{77}{40}$	$\frac{63}{30}$	$\frac{48}{20}$	$\frac{43}{10}$	$\frac{41}{1}$

Page 29

43.0	42.4	42.4	42.7	48.2	48.4	48.5
$\frac{97}{140}$	$\frac{103}{138}$	$\frac{103}{130}$	$\frac{100}{120}$	$\frac{45}{16}$	$\frac{43}{10}$	$\frac{42}{1}$

Page 29

43.1	42.6	42.9	43.1	43.4	48.2	48.3	48.5
$\frac{96}{139}$	$\frac{101}{137}$	$\frac{98}{130}$	$\frac{96}{120}$	$\frac{93}{110}$	$\frac{45}{16}$	$\frac{44}{10}$	$\frac{42}{1}$

Sta. + 1 - Elev.

952.68

3 +90

4

+10

T.P. 2.22 946.63 8.27 944.41

T.P. 2.55 949.08 944.06

2 +90

+50

+60

+70

Lt

4

	43.4						
Page 29	$\frac{93}{136}$	$\frac{96}{135}$	$\frac{99}{130}$	$\frac{92}{120}$	$\frac{92}{110}$	$\frac{45}{15}$	$\frac{45}{10}$
						$\frac{45}{4}$	$\frac{43}{1}$

	43.4	43.8	43.5	43.6	48.1	48.2	48.4
Page 29	$\frac{93}{130}$	$\frac{89}{120}$	$\frac{92}{110}$	$\frac{91}{100}$	$\frac{46}{15}$	$\frac{45}{10}$	$\frac{43}{1}$

	43.2	43.8	43.7	43.9	44.0	44.2	47.6	48.1	48.3	48.3
Page 29	$\frac{96}{133}$	$\frac{89}{130}$	$\frac{90}{120}$	$\frac{88}{110}$	$\frac{87}{100}$	$\frac{85}{90}$	$\frac{51}{20}$	$\frac{46}{10}$	$\frac{44}{7}$	$\frac{44}{1}$

Check on T.P.#1 page 22

44.2	44.2	43.1	42.7	42.1	40.0	39.6
$\frac{24}{227}$	$\frac{24}{220}$	$\frac{35}{215}$	$\frac{39}{209}$	$\frac{43}{200}$	$\frac{66}{197}$	$\frac{70}{192}$

44.3	44.3	41.9	41.6	41.7	39.3	39.2
$\frac{23}{226}$	$\frac{23}{217}$	$\frac{47}{211}$	$\frac{50}{203}$	$\frac{49}{195}$	$\frac{73}{191}$	$\frac{74}{188}$

44.4	44.4	41.6	41.3	41.4	38.9	39.0
$\frac{22}{224}$	$\frac{22}{213}$	$\frac{50}{208}$	$\frac{53}{201}$	$\frac{52}{192}$	$\frac{77}{180}$	$\frac{76}{185}$

44.5	44.6	43.9	41.2	41.3	37.6	38.0
$\frac{21}{220}$	$\frac{20}{213}$	$\frac{27}{210}$	$\frac{54}{204}$	$\frac{53}{199}$	$\frac{90}{186}$	$\frac{86}{179}$

Sta.

+

π

-

Elev.

946.63

2 +80

+90

3

+10

+30

+40

+50

13.7

Sta. + X - E/G.

946.63

3 +60

+70

+80

+90

4

+10

T.P. 4.33 950.28 0.68 945.95

+20

LH

R

37.3	130	96	55	48
40.7	156	176	174	180
45.0				
45.5				
36.3	140	136	68	62
36.7	150	141	120	110
43.8				
44.1				
44.2				
44.2				
44.5				
44.6				
45.0				
46.1				
47.4				
48.0				
48.2				

45.2	187	181	179	163	157	151	147	135
45.4	184	179	170	157	151	144		
45.1	190	184	175	164	157	147		
44.4								
38.8								
35.7								
36.0								
42.6								
40.1								
36.6								
35.7								
40.7								
37.8								
35.4								
45.1								
44.7								
44.9								

45.0	195	190	179	173	165	152		
44.6								
37.7								
35.2								
34.5								
35.1								
44.9								
44.7								
37.7								
34.7								
34.8								
35.4								

1.7	197	192	182	175	166	154		
1.9								
8.9								
11.5								
11.8								
11.2								

Sta.

+

π

-

Elek

950.28

9

+30

+40

+50

+60

LH

K

43.6	43.9	44.1	44.1	44.2	44.3	44.5	44.6	44.9	46.0	47.0	47.9	48.1
$\frac{67}{130}$	$\frac{64}{110}$	$\frac{62}{100}$	$\frac{63}{90}$	$\frac{61}{80}$	$\frac{60}{70}$	$\frac{58}{60}$	$\frac{57}{50}$	$\frac{54}{40}$	$\frac{43}{30}$	$\frac{29}{20}$	$\frac{29}{10}$	$\frac{22}{1}$
37.3	36.5	37.1	39.4	41.8	44.9	44.6						
$\frac{130}{141}$	$\frac{138}{147}$	$\frac{132}{153}$	$\frac{109}{160}$	$\frac{85}{167}$	$\frac{34}{173}$	$\frac{47}{178}$						

43.8	44.1	44.0	44.1	44.1	44.1	44.2	44.5	44.6	44.8	45.9	47.2	47.8	48.0
$\frac{65}{130}$	$\frac{62}{120}$	$\frac{63}{110}$	$\frac{62}{100}$	$\frac{63}{90}$	$\frac{62}{80}$	$\frac{61}{70}$	$\frac{58}{60}$	$\frac{57}{50}$	$\frac{55}{40}$	$\frac{44}{30}$	$\frac{31}{20}$	$\frac{28}{10}$	$\frac{23}{1}$
38.5	37.3	37.3	39.9	42.4	45.3	45.6							
$\frac{118}{138}$	$\frac{130}{143}$	$\frac{130}{148}$	$\frac{104}{154}$	$\frac{79}{164}$	$\frac{50}{171}$	$\frac{47}{176}$							

44.1	44.2	44.1	44.0	44.1	44.2	44.5	44.4	44.9	45.9	47.0	47.6	47.8
$\frac{62}{120}$	$\frac{61}{110}$	$\frac{62}{100}$	$\frac{63}{90}$	$\frac{62}{80}$	$\frac{61}{70}$	$\frac{58}{60}$	$\frac{59}{50}$	$\frac{54}{40}$	$\frac{44}{30}$	$\frac{33}{20}$	$\frac{27}{10}$	$\frac{25}{1}$
43.7	38.6	37.4	38.2	40.9	45.2	45.7						
$\frac{66}{130}$	$\frac{117}{138}$	$\frac{129}{144}$	$\frac{121}{148}$	$\frac{99}{156}$	$\frac{51}{170}$	$\frac{46}{174}$						

43.7	44.0	43.9	43.8	43.8	44.0	44.2	44.3	44.5	44.8	45.7	46.8	47.4	47.6
$\frac{66}{129}$	$\frac{63}{120}$	$\frac{64}{110}$	$\frac{65}{100}$	$\frac{65}{90}$	$\frac{63}{80}$	$\frac{61}{70}$	$\frac{60}{60}$	$\frac{58}{50}$	$\frac{55}{40}$	$\frac{46}{30}$	$\frac{35}{20}$	$\frac{29}{10}$	$\frac{27}{1}$
38.8	37.7	38.9	42.6	45.4	45.8								
$\frac{115}{136}$	$\frac{120}{142}$	$\frac{114}{146}$	$\frac{27}{151}$	$\frac{49}{166}$	$\frac{45}{172}$								

Sta.	+	π	-	Elev
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950.28

4	+70			
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+80

+90

5

Sta.	+	X	-	Elev.
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		950.28		
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5	110			
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	120			
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	130			
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	140			
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T.P.	2.20	948.19	1.29	945.99
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42.9 43.5 43.6 43.7 43.8 43.8 43.9 44.2 44.5 44.8 45.8 46.6 46.7

$\frac{74}{119}$ $\frac{68}{110}$ $\frac{67}{100}$ $\frac{66}{90}$ $\frac{65}{80}$ $\frac{65}{70}$ $\frac{64}{60}$ $\frac{61}{50}$ $\frac{58}{40}$ $\frac{55}{30}$ $\frac{45}{20}$ $\frac{37}{10}$ $\frac{36}{1}$

39.0 38.7 42.7 45.0 45.9 46.2

$\frac{113}{127}$ $\frac{116}{135}$ $\frac{76}{144}$ $\frac{53}{150}$ $\frac{44}{153}$ $\frac{41}{159}$

39.1 42.8 43.3 43.7 43.7 43.7 43.9 44.0 44.1 44.7 45.6 46.4 46.6

$\frac{112}{123}$ $\frac{75}{117}$ $\frac{70}{110}$ $\frac{66}{100}$ $\frac{66}{90}$ $\frac{66}{80}$ $\frac{69}{70}$ $\frac{69}{60}$ $\frac{63}{50}$ $\frac{62}{40}$ $\frac{56}{30}$ $\frac{47}{20}$ $\frac{39}{10}$ $\frac{37}{1}$

38.8 39.1 42.2 46.1 46.2

$\frac{115}{129}$ $\frac{112}{136}$ $\frac{81}{140}$ $\frac{42}{151}$ $\frac{41}{157}$

40.0 42.8 43.0 43.4 43.6 43.7 43.8 43.7 43.8 44.3 44.8 45.6 46.2 46.4

$\frac{103}{120}$ $\frac{75}{116}$ $\frac{73}{110}$ $\frac{69}{100}$ $\frac{67}{90}$ $\frac{66}{80}$ $\frac{65}{70}$ $\frac{66}{60}$ $\frac{65}{50}$ $\frac{60}{40}$ $\frac{53}{30}$ $\frac{47}{20}$ $\frac{41}{10}$ $\frac{39}{1}$

39.6 38.9 39.9 40.1 45.6 46.3

$\frac{107}{127}$ $\frac{114}{130}$ $\frac{104}{132}$ $\frac{102}{139}$ $\frac{47}{149}$ $\frac{40}{156}$

40.8 40.4 42.7 43.0 43.4 43.3 43.4 43.5 44.0 44.0 44.6 45.3 46.0 46.2

$\frac{95}{121}$ $\frac{99}{116}$ $\frac{76}{112}$ $\frac{73}{100}$ $\frac{69}{90}$ $\frac{70}{80}$ $\frac{69}{70}$ $\frac{68}{60}$ $\frac{63}{50}$ $\frac{63}{40}$ $\frac{57}{30}$ $\frac{50}{20}$ $\frac{43}{10}$ $\frac{41}{1}$

38.8 40.4 45.4 46.3

$\frac{115}{123}$ $\frac{99}{136}$ $\frac{99}{144}$ $\frac{40}{153}$

Sta + π - E/c

948.19

5 +50

+60

+70

+10

Sta.	+	π	-	Elev.
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		948.17		
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5	+90			
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6				
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	+10			
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	+20			
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	+30			
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	+40			
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	+50			
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T.P.				
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	5.37			
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		949.36		
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			4.20	
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				943.99
--	--	--	--	--------

	+60			
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41

4

46.7	46.3	40.4	40.2	39.3	40.3	41.8	42.4	42.5	42.7	42.7	42.9	43.6	44.0	44.8	45.2
$\frac{15}{192}$	$\frac{19}{137}$	$\frac{78}{126}$	$\frac{80}{117}$	$\frac{89}{109}$	$\frac{79}{103}$	$\frac{64}{98}$	$\frac{58}{90}$	$\frac{57}{80}$	$\frac{57}{70}$	$\frac{55}{60}$	$\frac{55}{50}$	$\frac{53}{40}$	$\frac{46}{30}$	$\frac{42}{20}$	$\frac{39}{10}$
46.7	46.2	40.5	39.1	39.2	40.6	41.7	41.9	42.1	42.4	42.8	42.6	42.6	43.2	43.9	44.6
$\frac{15}{190}$	$\frac{20}{135}$	$\frac{77}{129}$	$\frac{81}{113}$	$\frac{90}{108}$	$\frac{76}{96}$	$\frac{63}{93}$	$\frac{68}{90}$	$\frac{61}{80}$	$\frac{57}{70}$	$\frac{54}{60}$	$\frac{56}{50}$	$\frac{56}{40}$	$\frac{50}{30}$	$\frac{43}{20}$	$\frac{36}{10}$
46.7	46.1	40.7	39.9	39.2	39.2	40.6	41.5	41.8	42.1	42.2	42.6	42.8	43.0	43.8	44.5
$\frac{15}{138}$	$\frac{21}{132}$	$\frac{75}{123}$	$\frac{83}{110}$	$\frac{90}{103}$	$\frac{90}{100}$	$\frac{76}{92}$	$\frac{67}{90}$	$\frac{64}{80}$	$\frac{61}{70}$	$\frac{60}{60}$	$\frac{56}{50}$	$\frac{54}{40}$	$\frac{52}{30}$	$\frac{49}{20}$	$\frac{37}{10}$
46.8	46.1	40.9	40.3	39.3	39.4	39.7	41.5	41.8	42.0	42.3	42.5	42.5	42.9	43.6	44.3
$\frac{14}{137}$	$\frac{21}{131}$	$\frac{73}{122}$	$\frac{79}{111}$	$\frac{89}{105}$	$\frac{88}{100}$	$\frac{85}{89}$	$\frac{67}{86}$	$\frac{69}{80}$	$\frac{62}{70}$	$\frac{59}{60}$	$\frac{57}{50}$	$\frac{57}{40}$	$\frac{53}{30}$	$\frac{46}{20}$	$\frac{39}{10}$
46.9	46.1	40.8	39.6	49.1	39.0	41.1	41.8	42.0	42.1	42.2	42.5	42.8	43.5	44.1	44.5
$\frac{13}{135}$	$\frac{21}{128}$	$\frac{74}{117}$	$\frac{86}{105}$	$\frac{91}{97}$	$\frac{92}{87}$	$\frac{71}{84}$	$\frac{69}{80}$	$\frac{69}{70}$	$\frac{62}{60}$	$\frac{61}{50}$	$\frac{57}{40}$	$\frac{54}{30}$	$\frac{47}{20}$	$\frac{41}{10}$	$\frac{37}{10}$
47.0	46.1	41.1	40.0	39.3	39.2	39.6	41.0	41.5	41.7	41.9	42.0	42.5	42.6	43.2	43.9
$\frac{12}{134}$	$\frac{21}{128}$	$\frac{71}{120}$	$\frac{82}{109}$	$\frac{89}{105}$	$\frac{90}{97}$	$\frac{86}{85}$	$\frac{72}{82}$	$\frac{67}{80}$	$\frac{65}{70}$	$\frac{63}{60}$	$\frac{62}{50}$	$\frac{57}{40}$	$\frac{56}{30}$	$\frac{50}{20}$	$\frac{41}{10}$
46.9	46.2	40.9	40.0	39.1	39.1	40.3	41.3	41.4	41.8	42.0	42.1	42.6	42.9	43.7	44.0
$\frac{13}{132}$	$\frac{20}{126}$	$\frac{73}{117}$	$\frac{82}{108}$	$\frac{91}{100}$	$\frac{91}{95}$	$\frac{79}{81}$	$\frac{69}{78}$	$\frac{68}{70}$	$\frac{64}{60}$	$\frac{62}{50}$	$\frac{61}{40}$	$\frac{54}{30}$	$\frac{53}{20}$	$\frac{45}{10}$	$\frac{42}{10}$
47.0	46.2	41.5	40.4	39.1	39.0	39.0	40.1	40.8	41.2	41.3	41.9	42.3	42.5	42.7	43.5
$\frac{24}{130}$	$\frac{32}{125}$	$\frac{79}{117}$	$\frac{90}{110}$	$\frac{103}{100}$	$\frac{104}{95}$	$\frac{104}{85}$	$\frac{93}{78}$	$\frac{86}{76}$	$\frac{86}{70}$	$\frac{81}{60}$	$\frac{78}{50}$	$\frac{71}{40}$	$\frac{69}{30}$	$\frac{67}{20}$	$\frac{59}{10}$

Sta + π - Elev.

949.36

6 +70

+80

+90

7

+10

+20

+30

+40

L

L

47.1	46.2	40.9	39.6	39.2	38.8	39.7	40.6	40.9	41.2	41.2	41.3	42.3	42.6	43.3	43.5
$\frac{2.3}{127}$	$\frac{3.2}{122}$	$\frac{8.5}{114}$	$\frac{9.8}{104}$	$\frac{10.2}{98}$	$\frac{10.6}{84}$	$\frac{9.7}{75}$	$\frac{8.8}{73}$	$\frac{8.5}{70}$	$\frac{8.2}{60}$	$\frac{8.2}{50}$	$\frac{8.1}{40}$	$\frac{7.1}{30}$	$\frac{6.8}{20}$	$\frac{6.1}{10}$	$\frac{5.9}{1}$

47.0	46.6	40.5	39.5	39.1	39.6	40.6	40.8	40.9	41.2	41.8	42.2	43.0	43.3
$\frac{2.4}{126}$	$\frac{2.8}{121}$	$\frac{8.9}{110}$	$\frac{8.9}{100}$	$\frac{10.3}{90}$	$\frac{9.8}{80}$	$\frac{8.8}{70}$	$\frac{8.6}{60}$	$\frac{8.5}{50}$	$\frac{8.2}{40}$	$\frac{7.6}{30}$	$\frac{7.2}{20}$	$\frac{6.4}{10}$	$\frac{6.1}{1}$

47.1	46.5	40.6	39.0	39.1	38.9	40.0	40.6	40.6	41.1	41.5	42.2	42.8	43.0
$\frac{2.3}{124}$	$\frac{2.9}{120}$	$\frac{8.8}{110}$	$\frac{10.4}{100}$	$\frac{10.3}{90}$	$\frac{10.5}{80}$	$\frac{9.4}{70}$	$\frac{8.8}{60}$	$\frac{8.5}{50}$	$\frac{8.3}{40}$	$\frac{7.9}{30}$	$\frac{7.2}{20}$	$\frac{6.6}{10}$	$\frac{6.4}{1}$

47.1	46.4	40.8	39.7	39.3	39.3	39.5	40.3	40.4	40.5	41.0	41.9	42.5	42.8
$\frac{2.3}{122}$	$\frac{3.0}{117}$	$\frac{8.6}{107}$	$\frac{9.7}{100}$	$\frac{10.1}{90}$	$\frac{10.1}{80}$	$\frac{9.7}{70}$	$\frac{9.1}{60}$	$\frac{9.0}{50}$	$\frac{8.9}{40}$	$\frac{8.9}{30}$	$\frac{7.5}{20}$	$\frac{6.9}{10}$	$\frac{6.6}{1}$

47.3	46.5	40.7	39.9	39.5	39.5	39.6	40.1	40.2	40.3	40.6	41.3	42.2	42.5
$\frac{2.1}{120}$	$\frac{2.9}{115}$	$\frac{8.7}{106}$	$\frac{9.5}{100}$	$\frac{9.9}{90}$	$\frac{9.8}{80}$	$\frac{9.8}{70}$	$\frac{9.3}{60}$	$\frac{9.2}{50}$	$\frac{9.1}{40}$	$\frac{8.8}{30}$	$\frac{8.1}{20}$	$\frac{7.2}{10}$	$\frac{6.9}{1}$

47.3	46.6	40.7	40.5	39.8	39.6	39.2	40.3	40.5	40.6	40.9	41.1	42.1	42.3
$\frac{2.1}{118}$	$\frac{2.8}{113}$	$\frac{8.7}{104}$	$\frac{8.9}{100}$	$\frac{9.6}{90}$	$\frac{9.8}{80}$	$\frac{10.2}{70}$	$\frac{9.1}{60}$	$\frac{8.9}{50}$	$\frac{8.8}{40}$	$\frac{8.5}{30}$	$\frac{8.3}{20}$	$\frac{7.3}{10}$	$\frac{7.1}{1}$

47.3	46.7	40.8	39.8	40.0	38.9	40.3	40.5	40.8	41.0	41.1	41.9	42.1
$\frac{2.1}{117}$	$\frac{2.7}{112}$	$\frac{8.6}{100}$	$\frac{9.6}{90}$	$\frac{9.4}{80}$	$\frac{10.5}{70}$	$\frac{9.1}{60}$	$\frac{8.9}{50}$	$\frac{8.6}{40}$	$\frac{8.4}{30}$	$\frac{8.3}{20}$	$\frac{7.5}{10}$	$\frac{7.3}{1}$

47.4	46.9	41.0	40.2	39.1	39.1	40.4	40.9	40.9	42.1	41.9	41.6	42.0
$\frac{2.0}{115}$	$\frac{2.5}{110}$	$\frac{8.4}{100}$	$\frac{9.2}{90}$	$\frac{10.1}{80}$	$\frac{10.3}{70}$	$\frac{9.0}{60}$	$\frac{4.5}{50}$	$\frac{4.5}{40}$	$\frac{7.0}{30}$	$\frac{7.5}{20}$	$\frac{7.8}{10}$	$\frac{7.9}{1}$

shock pile

clay + peat

562

+

π

-

Elv.

949.36

7

+50

+60

+70

+80

+90

8

+10

+20

47.5	47.4	47.6	47.7	47.7	47.8	48.0	47.6	40.5	40.5	40.0	39.1	39.8	46.2	44.3	43.7	41.4	41.5	41.9
$\frac{1.9}{13}$	$\frac{2.0}{11}$	$\frac{1.8}{10}$	$\frac{1.7}{109}$	$\frac{1.7}{107}$	$\frac{1.6}{106}$	$\frac{1.4}{103}$	$\frac{1.9}{98}$	$\frac{8.9}{85}$	$\frac{8.9}{90}$	$\frac{9.9}{80}$	$\frac{10.3}{70}$	$\frac{9.6}{60}$	$\frac{3.2}{50}$	$\frac{3.1}{40}$	$\frac{5.7}{30}$	$\frac{8.0}{20}$	$\frac{7.9}{10}$	$\frac{7.6}{1}$
46.9	46.8	46.9	47.7	47.2	47.3	48.0	47.8	47.5	40.4	40.3	39.8	40.0	46.2	44.3	43.7	41.4	41.5	41.9
$\frac{2.5}{108}$	$\frac{2.6}{106}$	$\frac{2.5}{105}$	$\frac{2.2}{104}$	$\frac{2.2}{102}$	$\frac{2.1}{100}$	$\frac{2.0}{98}$	$\frac{1.8}{95}$	$\frac{1.9}{100}$	$\frac{8.9}{90}$	$\frac{9.1}{80}$	$\frac{9.6}{70}$	$\frac{9.6}{80}$	$\frac{3.2}{50}$	$\frac{3.1}{40}$	$\frac{5.7}{30}$	$\frac{8.0}{20}$	$\frac{7.9}{10}$	$\frac{7.6}{1}$
41.0	40.8	40.9	47.2	47.2	47.3	48.0	47.8	47.5	40.4	40.3	39.8	40.0	46.2	44.3	43.7	41.4	41.5	41.9
$\frac{8.9}{97}$	$\frac{8.6}{95}$	$\frac{8.5}{95}$	$\frac{8.9}{90}$	$\frac{8.9}{89}$	$\frac{9.0}{88}$	$\frac{8.9}{85}$	$\frac{8.8}{90}$	$\frac{8.9}{100}$	$\frac{8.9}{90}$	$\frac{9.1}{80}$	$\frac{9.6}{70}$	$\frac{9.6}{80}$	$\frac{3.2}{50}$	$\frac{3.1}{40}$	$\frac{5.7}{30}$	$\frac{8.0}{20}$	$\frac{7.9}{10}$	$\frac{7.6}{1}$
40.5	40.5	40.6	40.5	40.4	40.4	40.5	40.4	40.5	40.4	40.3	39.8	40.0	46.2	44.3	43.7	41.4	41.5	41.9
$\frac{8.9}{90}$	$\frac{8.9}{90}$	$\frac{8.8}{90}$	$\frac{8.9}{90}$	$\frac{9.0}{89}$	$\frac{9.0}{88}$	$\frac{8.9}{85}$	$\frac{8.8}{90}$	$\frac{8.9}{100}$	$\frac{8.9}{90}$	$\frac{9.1}{80}$	$\frac{9.6}{70}$	$\frac{9.6}{80}$	$\frac{3.2}{50}$	$\frac{3.1}{40}$	$\frac{5.7}{30}$	$\frac{8.0}{20}$	$\frac{7.9}{10}$	$\frac{7.6}{1}$
39.1	39.0	39.3	39.4	39.8	39.8	40.0	40.4	40.0	39.8	40.3	39.8	40.0	46.2	44.3	43.7	41.4	41.5	41.9
$\frac{10.3}{70}$	$\frac{1.4}{70}$	$\frac{10.1}{70}$	$\frac{100}{70}$	$\frac{96}{70}$	$\frac{96}{70}$	$\frac{9.6}{60}$	$\frac{9.6}{60}$	$\frac{9.6}{60}$	$\frac{9.6}{60}$	$\frac{9.6}{60}$	$\frac{9.6}{60}$	$\frac{9.6}{60}$	$\frac{3.2}{50}$	$\frac{3.1}{40}$	$\frac{5.7}{30}$	$\frac{8.0}{20}$	$\frac{7.9}{10}$	$\frac{7.6}{1}$
39.8	39.9	40.2	40.1	40.4	40.4	40.5	40.6	41.1	42.2	41.3	41.7	41.9	46.2	44.3	43.7	41.4	41.5	41.9
$\frac{9.6}{60}$	$\frac{9.5}{60}$	$\frac{9.2}{60}$	$\frac{90}{50}$	$\frac{90}{50}$	$\frac{90}{50}$	$\frac{90}{50}$	$\frac{8.8}{40}$	$\frac{8.8}{30}$	$\frac{7.2}{20}$	$\frac{7.2}{20}$	$\frac{7.2}{10}$	$\frac{7.2}{10}$	$\frac{3.2}{50}$	$\frac{3.1}{40}$	$\frac{5.7}{30}$	$\frac{8.0}{20}$	$\frac{7.9}{10}$	$\frac{7.6}{1}$
46.2	45.7	45.3	40.5	40.5	40.7	41.0	40.7	41.1	41.3	41.7	41.9	42.1	46.2	44.3	43.7	41.4	41.5	41.9
$\frac{46.2}{40}$	$\frac{45.7}{40}$	$\frac{45.3}{40}$	$\frac{40.5}{40}$	$\frac{40.5}{40}$	$\frac{40.7}{40}$	$\frac{41.0}{40}$	$\frac{40.7}{40}$	$\frac{41.1}{40}$	$\frac{41.3}{40}$	$\frac{41.7}{40}$	$\frac{41.9}{40}$	$\frac{42.1}{40}$	$\frac{46.2}{40}$	$\frac{44.3}{40}$	$\frac{43.7}{40}$	$\frac{41.4}{40}$	$\frac{41.5}{40}$	$\frac{41.9}{40}$
44.3	44.2	43.5	42.9	42.2	41.0	40.9	40.9	41.1	41.3	41.7	41.9	42.1	46.2	44.3	43.7	41.4	41.5	41.9
$\frac{44.3}{30}$	$\frac{44.2}{30}$	$\frac{43.5}{30}$	$\frac{42.9}{30}$	$\frac{42.2}{30}$	$\frac{41.0}{30}$	$\frac{40.9}{30}$	$\frac{40.9}{30}$	$\frac{41.1}{30}$	$\frac{41.3}{30}$	$\frac{41.7}{30}$	$\frac{41.9}{30}$	$\frac{42.1}{30}$	$\frac{46.2}{30}$	$\frac{44.3}{30}$	$\frac{43.7}{30}$	$\frac{41.4}{30}$	$\frac{41.5}{30}$	$\frac{41.9}{30}$

sta	+	π	-	Elev
		949.36		

8	+40
---	-----

+60

+80

9

+50

T.P.	7.53	953.32	3.37	945.99
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B.M.			6.99	946.33
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946.31

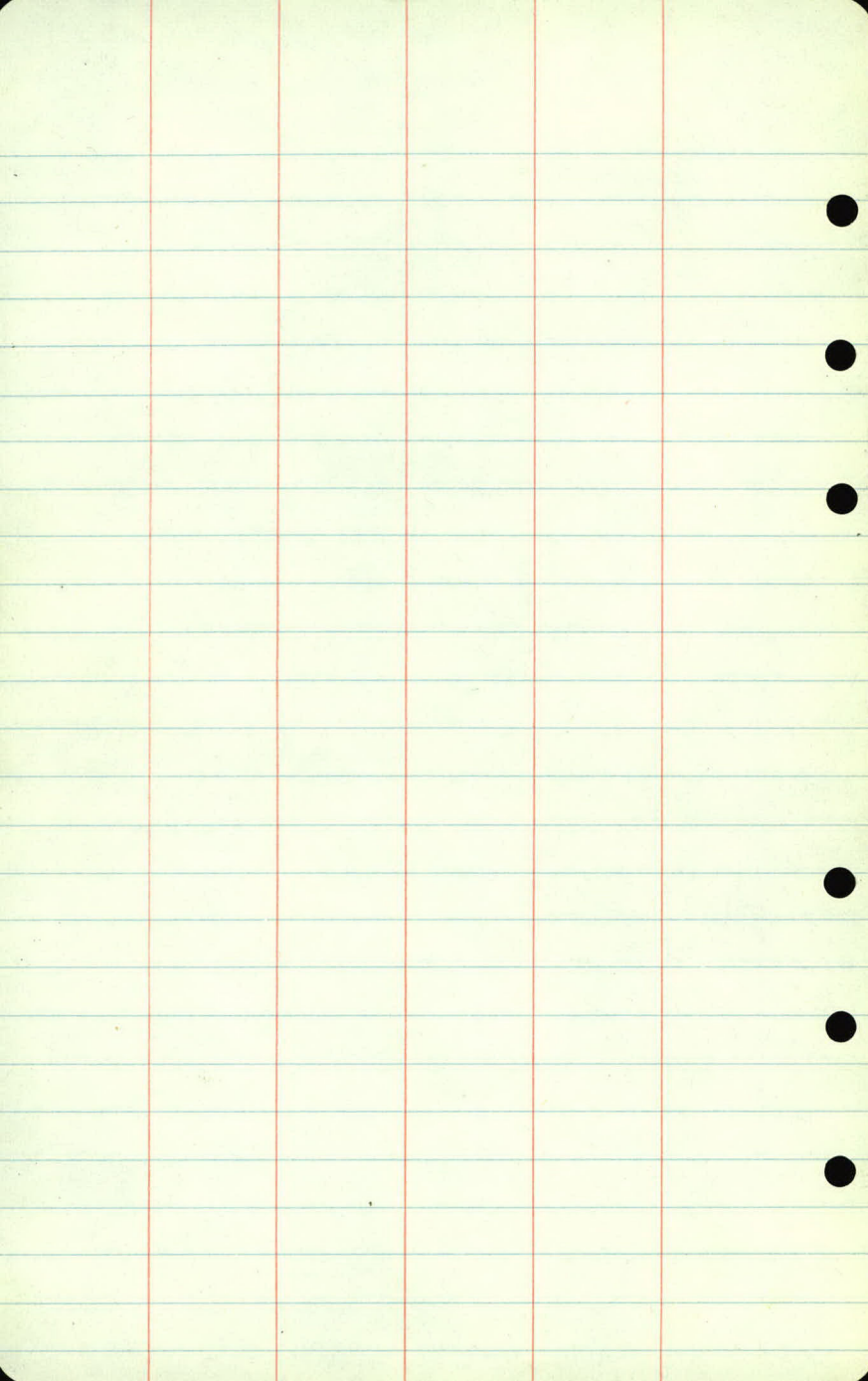
7-1-39
K.A.
L.C.
A.B.

Lt.

A

48.1	13	100	48.0	14	98	48.2	12	95	48.3	11	93	48.6	9	87
47.8	16	96	47.7	17	93	47.8	16	90	47.8	16	87	48.4	10	82
41.0	89	84	41.4	80	81	42.0	74	80	42.3	71	77	43.0	69	72
40.8	86	80	41.1	83	70	41.8	76	70	42.1	73	70	42.4	69	62
40.6	88	70	41.3	81	60	41.8	76	60	41.9	75	60	42.9	65	50
41.0	84	50	41.5	79	50	41.8	76	50	41.9	75	50	42.9	65	38
41.1	83	40	41.7	77	40	41.8	74	40	42.1	73	40	42.9	65	20
41.3	81	30	41.7	77	30	42.0	74	30	42.2	72	30	44.2	52	19
41.5	79	20	41.8	76	20	42.2	72	20	42.4	70	20	44.1	53	7
42.0	74	10	42.4	70	10	42.9	65	10	43.3	61	10	44.1	53	7
42.3	71	1	42.6	68	1	43.0	64	1	43.4	60	1	44.4	50	1

Top Mount Lexington Ave & Co. Rd. "E"



Drainage of Oil Tanks.

3 Pages

Sta	+	-	Elcv
B.M.	7.27	753.58	
T.P.	2.73	745.29	1102
1st 60 Co. 12th E. 2. 90° Lt			942.56
0+00 at top of grade		3.5	941.8

946.31

+15 3.8 41.5

+24 5.7 39.6

+44 6.8 38.5

+59 6.8 38.5

+66 7.8 37.5

+72 Δ Rt. 2 $\left\{ \begin{array}{l} 40' \text{ from } E \\ 50' \text{ from } S. \text{ Track} \end{array} \right.$ 8.2 37.1

1 +00 8.2 37.1

+26 7.7 37.4

+55 9.0 36.3

2 9.1 36.2

2/6/39
K.H.
L.C.
L.B.H.
19.2.6

1

Top Man/ Cold "E" & Lexington Ave

Lexington Ave.

Cold "E"

5105-P1. = 33'
from S. side Trk.

3100-L170 =
33' from S. side Trk.

0172
40' from S. side Trk.

0100 =
48760

N

Sta	I	π	-	Elev.
		945.89		

2	+50		8.1	37.2
---	-----	--	-----	------

3			7.0	38.3
---	--	--	-----	------

T.P.	4.64	946.01	3.92	941.37
------	------	--------	------	--------

	+50		7.4	38.6
--	-----	--	-----	------

4			8.2	37.8
---	--	--	-----	------

	+50		10.0	36.0
--	-----	--	------	------

5			10.7	35.3
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+05 Δ 90° Rt

+17	Sa. End 24" Iron Culv.		13.0	33.0
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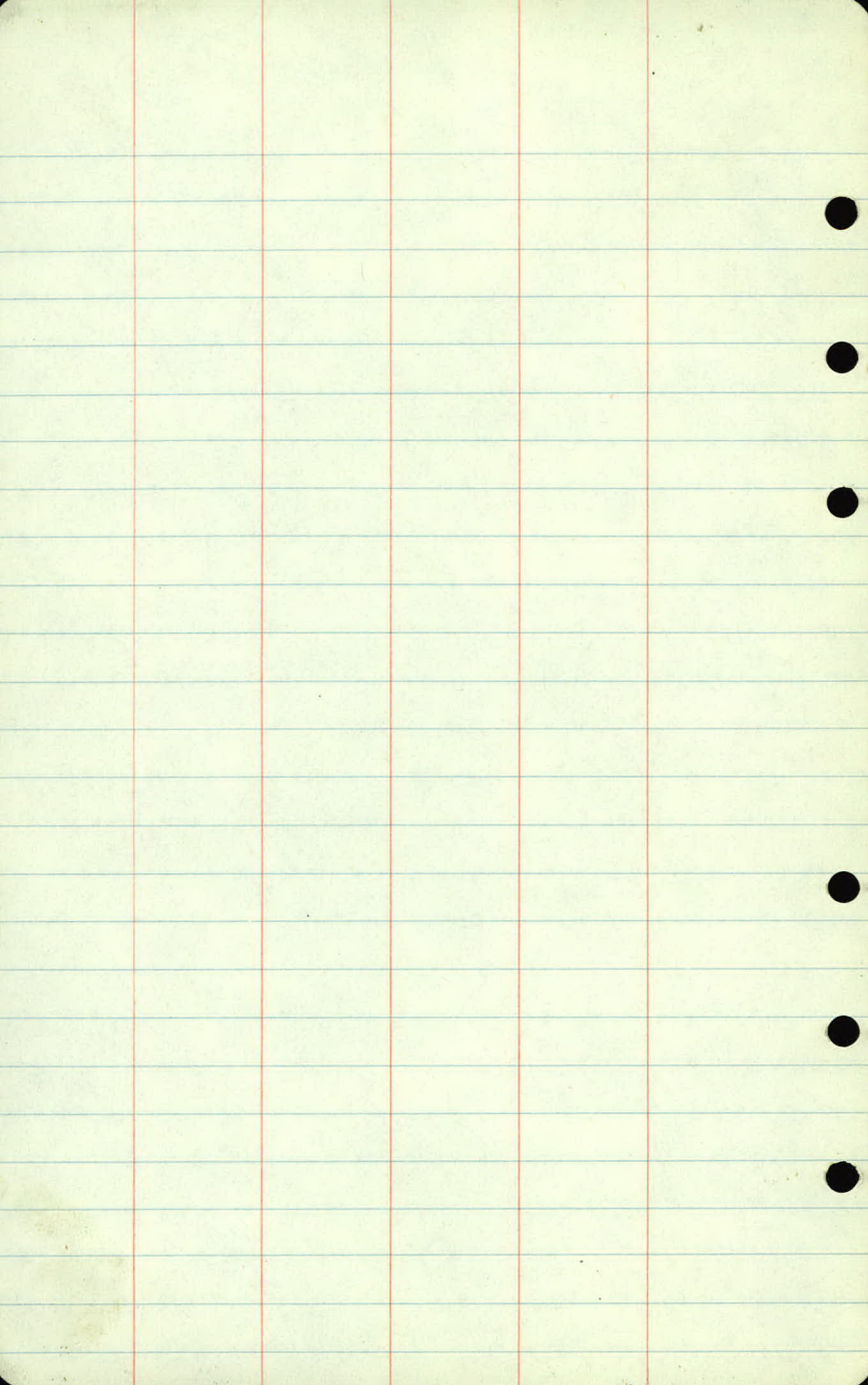
+77	N. End 30" Concrete Culv.		13.5	32.5
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T.P.	7.28	952.38	0.91	946.10
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B.M.			6.06	946.32
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(946.31)

Top Mont LCA + CARLE



Staking Notes
Drainage of Oil Tanks

2 Pages

Sta	+	X	-	Grade
B.M.	1.40	943.2		941.8

0	1.00			41.8
---	------	--	--	------

	1.25		40.2	
--	------	--	------	--

	1.72		39.9	
--	------	--	------	--

1			39.7	
---	--	--	------	--

	1.50		39.4	
--	------	--	------	--

2			39.1	
---	--	--	------	--

	1.50		38.8	
--	------	--	------	--

3			38.5	
---	--	--	------	--

	1.50		38.2	
--	------	--	------	--

Gr. Road

A

to Sta 0+00

3.0

 $\frac{37}{-97}$

3.3

3.5

3.8

4.1

4.4

4.7

5.0

