

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

WHITE BEAR AVE

From FROST To Co. Rd. "C"

Road Acc't. No. 65

ate Filed DR 14 File BK 64A



FK
FS
BB

Dec. 5, 1963

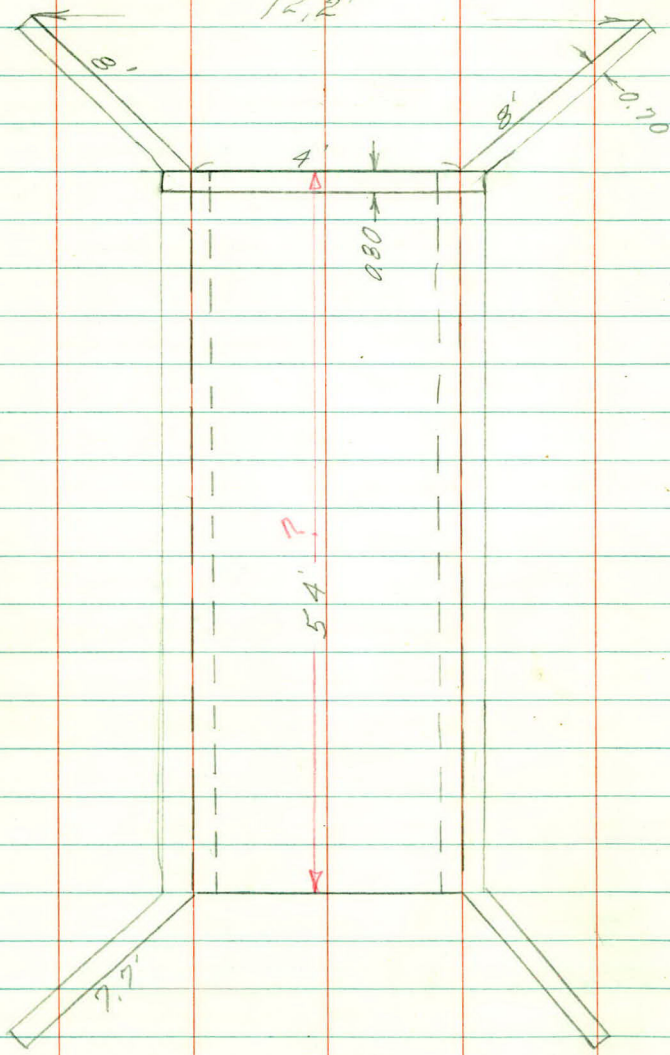
1

Box Culvert

Measurements

STA. 102+60 ~~E~~

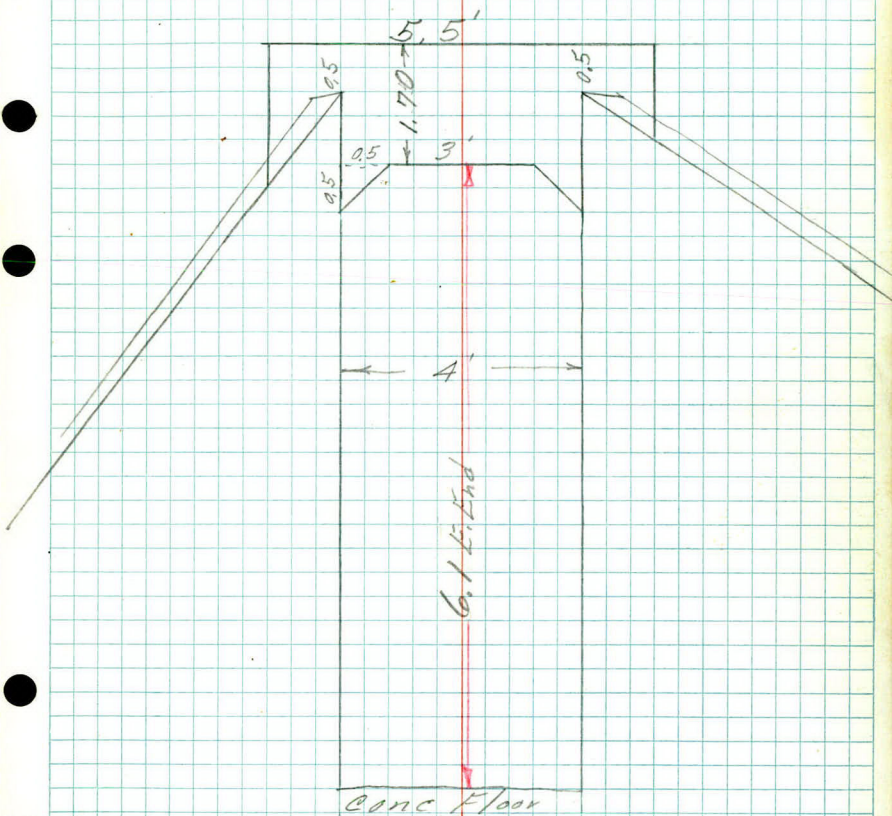
West End
12.2'

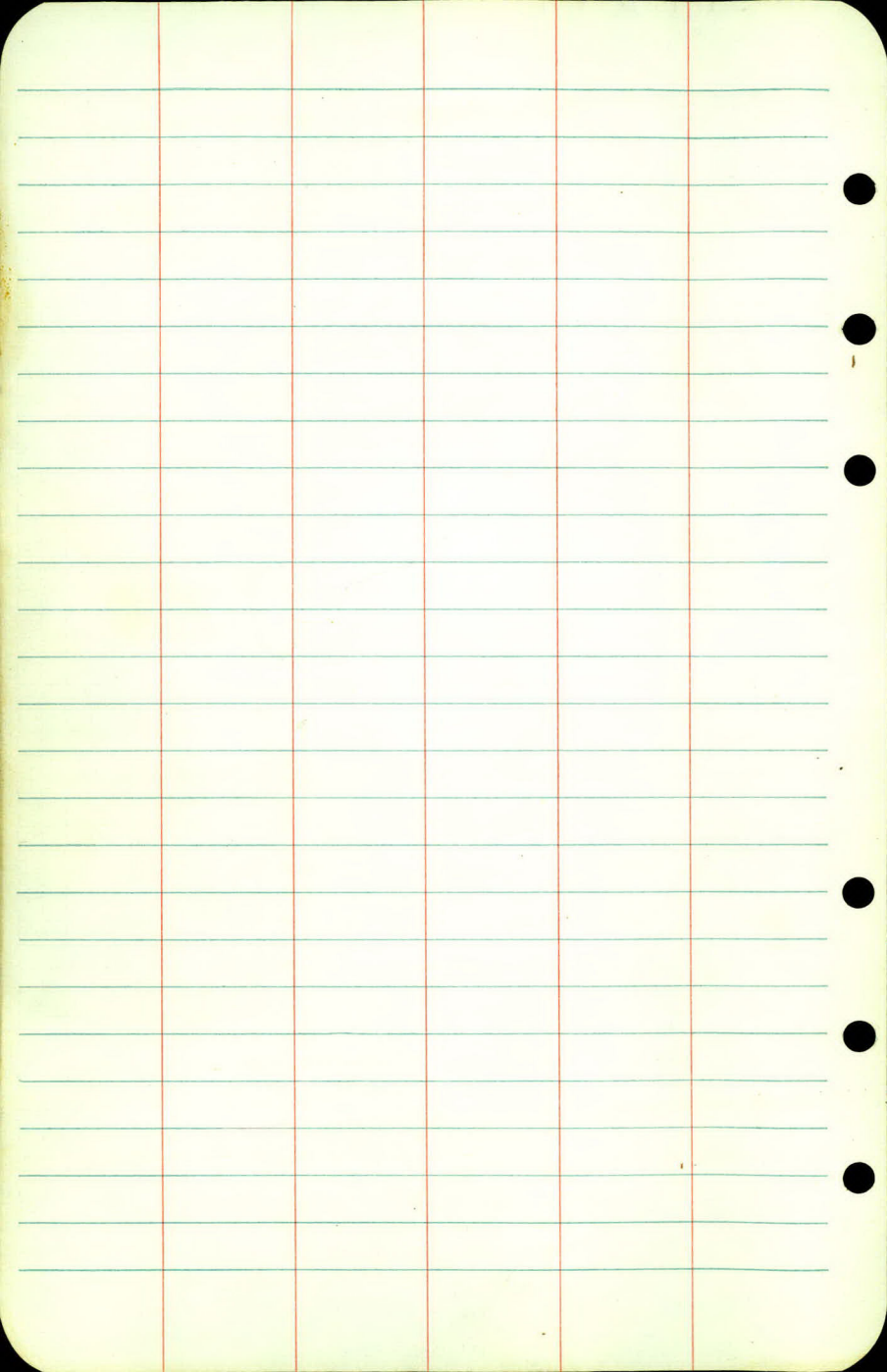


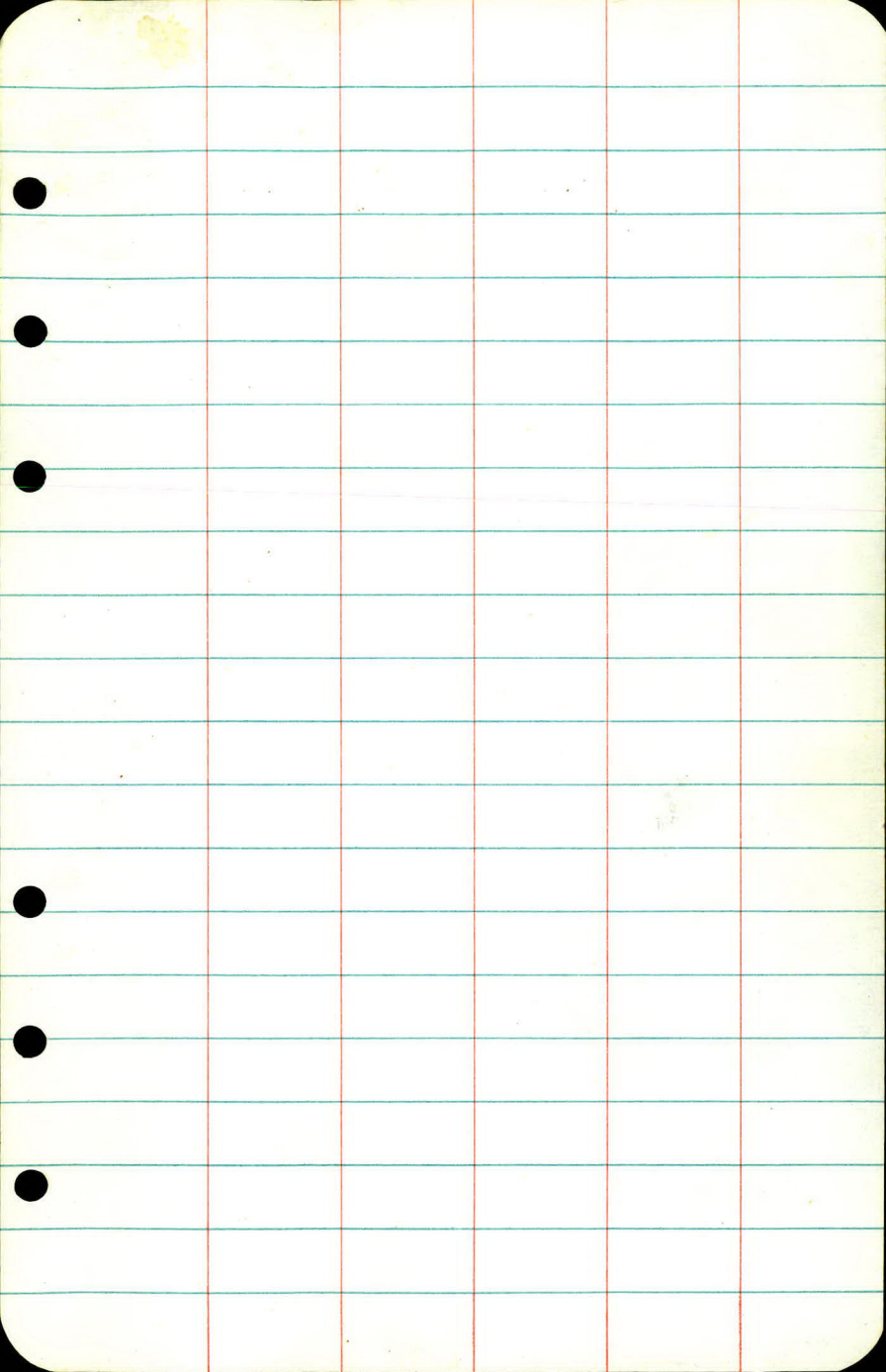
East End

Dec 5, 1963

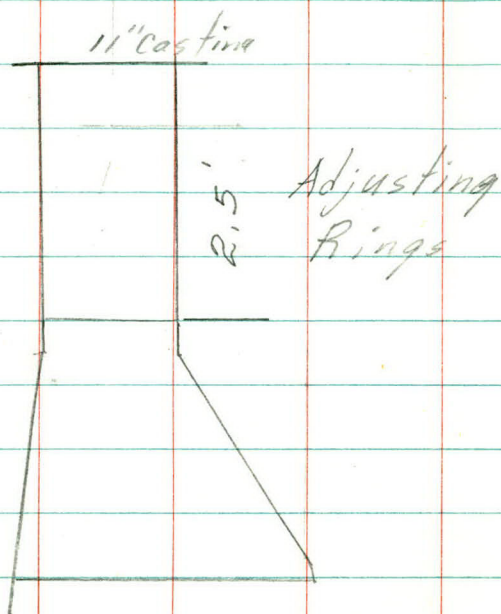
2



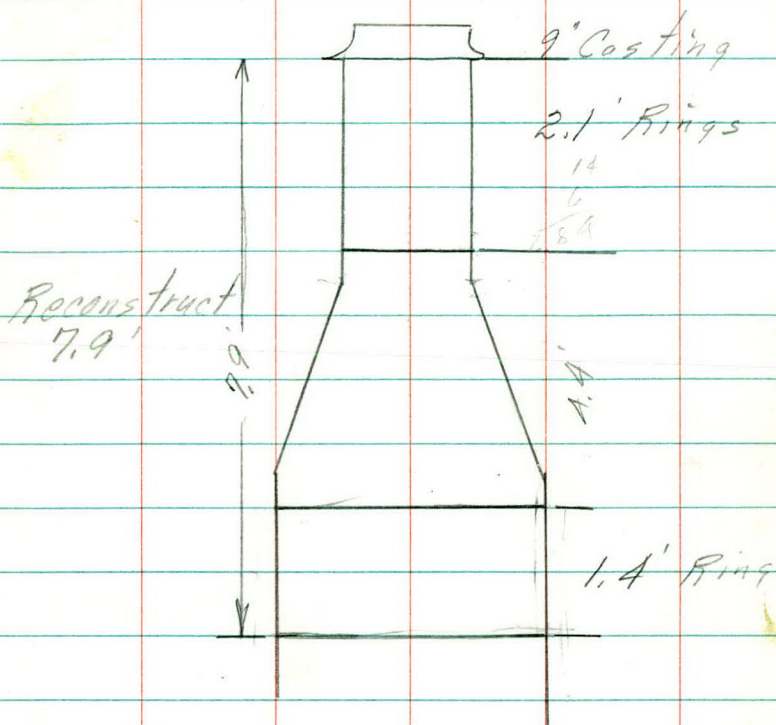




99+76



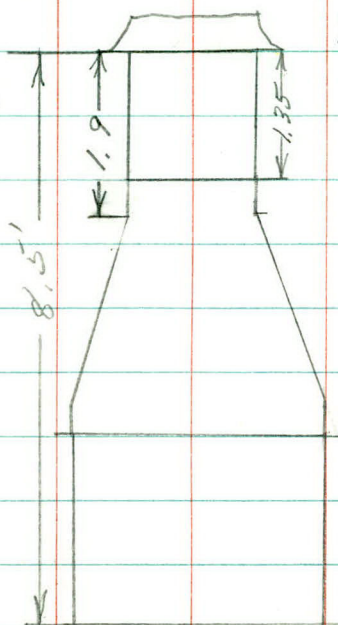
$$100 + 86$$



$$14.2 = \text{Height of M.H.}$$

$$\begin{array}{r} 1.4 \\ 2.1 \\ \hline 3.5 \end{array} \quad \begin{array}{r} 7.9 \\ 3.5 \\ \hline 11.4 \end{array}$$

103 + 86



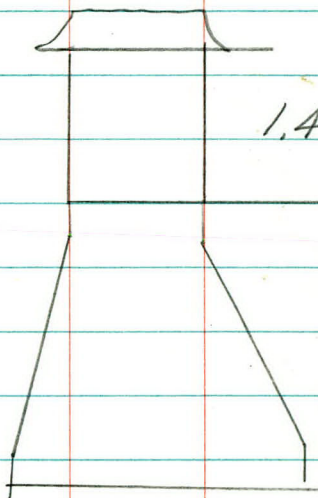
9" Casting

1.35 Rings

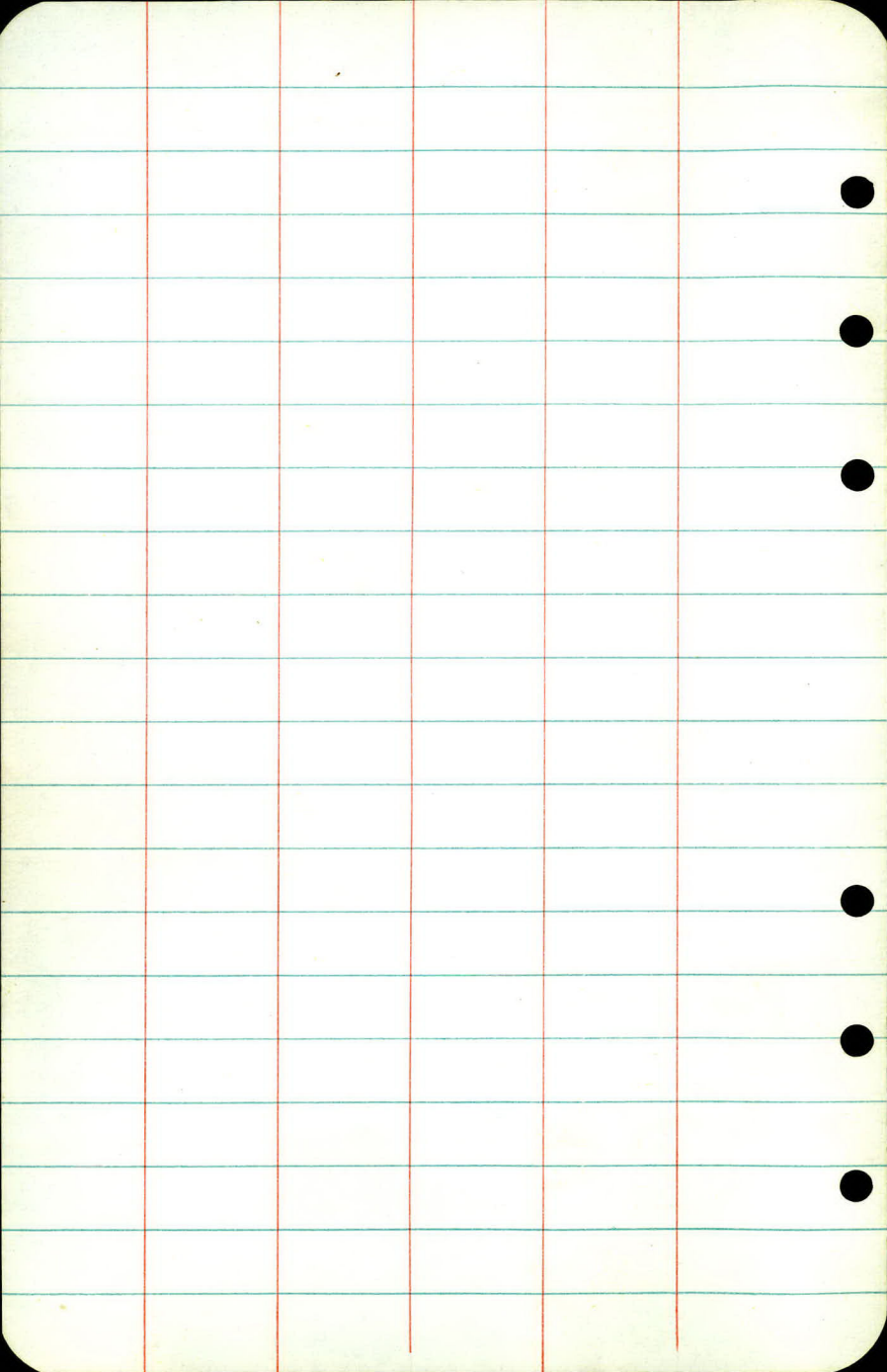
Cone

2.7 Ring

106+87



1.4' Rings



June 18, 1963

21

Bench Levels

Sta	+	π	-	ele	
B.M.	0.14	922.95			922.81
B.M.	0.49	916.12	7.32	915.63	
T.P.	3.94	912.88	7.18	908.94	
T.P.	5.96	914.58	4.26	908.62	908.61
B.M.	7.72	920.36	1.94	912.64	912.63
T.P.	7.33	926.91	0.78	919.58	
B.M.			1.57	925.34	925.32
B.M.			4.76	922.15	
B.B.	4.89	930.23			925.34
B.M.	2.11	928.88	3.46	926.77	
B.M.	4.01	929.32	3.57	925.31	925.28
B.M.	3.19	929.43	3.08	926.24	926.21
T.P.	2.43	926.14	5.72	923.71	923.68
T.P.	13.04	938.11	1.07	925.07	
T.P.	10.38	947.72	0.77	937.34	937.30
T.P.	0.65	937.06	11.31	936.41	
T.P.	3.79	932.54	8.31	928.75	Bent
T.P.			7.76	924.78	924.23 Raised

June 18, 1963 21

Top N.W. Cor Conc Foundation Central Structure

Box SE Cor RR tracks

S.W. Cor Slab Monette Const Co.

Top P.K. nail Station 42+00

Top P.K. nail sta 47+00

S.E. corner lower step Ho. # 2125

Top of rock 28' left Sta 51+50

Spike in transformer pole 88' left 52+50

Top of monument Co Rd B + White Bear Ave

Spike in transformer pole 88' left 52+50

S.W. corner lower step Ho. # 2200

Top E. corner base light std. 51' left Sta 60+38

Top N.W. corner metal base light std. Sta 64+60, 45' R

Top of base light std. W. approach HW 36 + White Bear Ave

Top of N. end curb So bound lane, HW 36 underpass

Top N. end 24" SCP E approach lane HW 36 + W Bear Ave

Top N. end 15" GMC Ho. # 2416

Top N. end 15" GMC Ho. # 2462

Top E rim manhole

Sta	+	π	-	Elev.
T.P.	4.25	929.03	7.76	924.78
T.P.	7.93	932.01	4.95	924.08
BM			1.40	930.61
				930.55

FK
JS
EZ
FK
JM

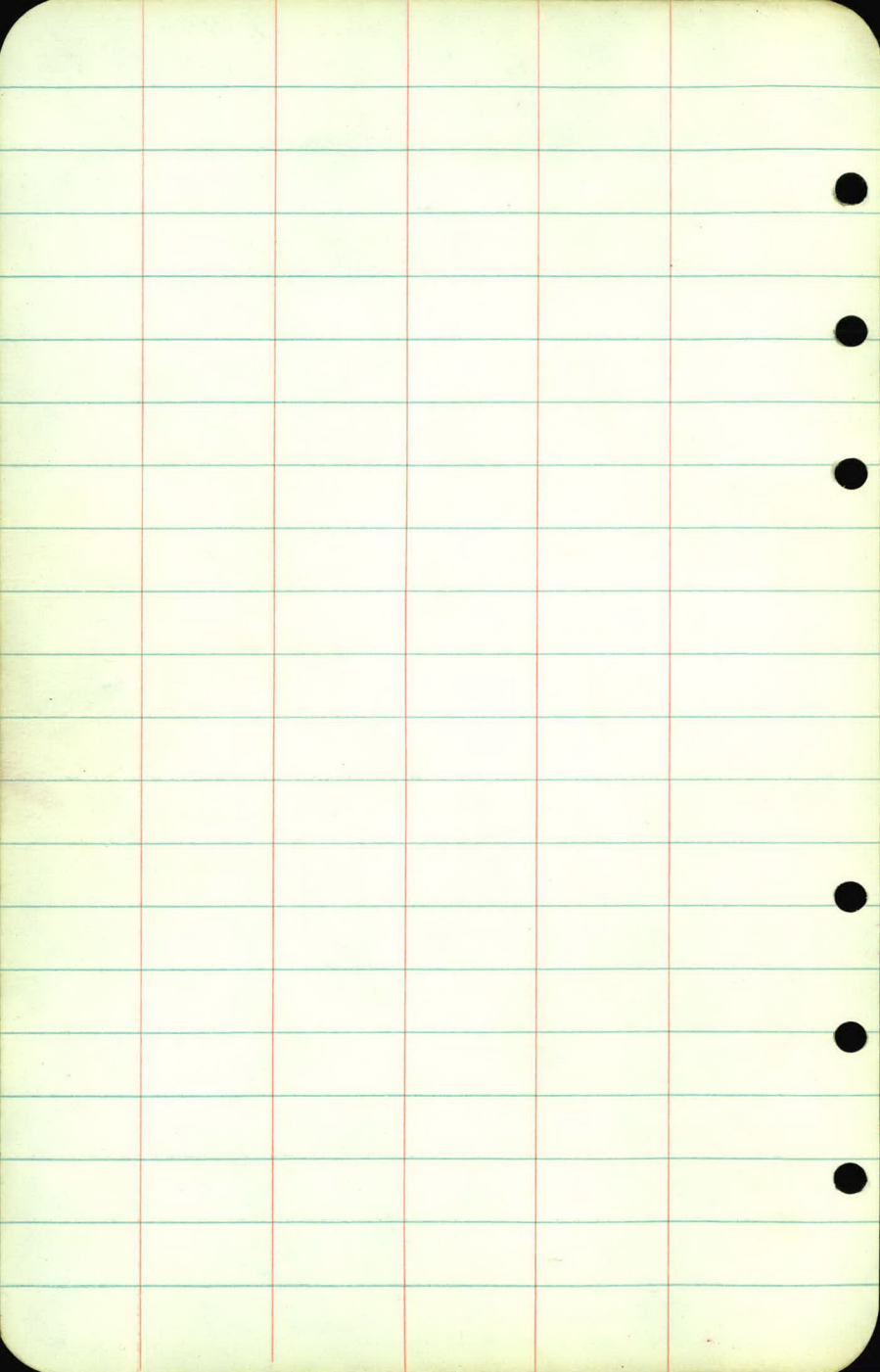
June 19, 1963

22

Top E. Rim manhole

Edge of pavement

Top USGS Co. Rd C + White Bear Ave



June 19, 1963

23

X-Sections

Sta	+	π	-	Elev
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BM	0.54	974.04		
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				(973.50)
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27				
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✓				
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+50				
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✓				
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+67				
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✓				
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June 19, 1963

24

Lt

Rt

Top Hyd 100'± East Sta 27+25

67.5	65.5	65.32	64.93	65.16	64.88	65.44	65.4	70.4
6.5	8.5	8.72	9.11	8.88	9.16	8.60	8.6	3.6
45	34	C	G		G	C	33	34
		<u>25.5</u>			<u>25.5</u>			Wall

68.6
5.4
55

69.4
4.6
75

✓

66.8	65.2	63.79	63.38	63.55	63.21	63.79	63.6
7.2	8.8	10.25	10.66	10.49	10.73	10.25	10.4
42	32	C	G		G	C	33
		<u>25.5</u>			<u>25.5</u>		

67.9
6.1
54

68.4
5.6
75

✓

66.9
7.1
34
Wall

66.7	63.15	62.76	62.96	62.68	63.11	63.0
7.3	10.89	11.28	11.08	11.36	10.93	11.0
39	C	G		G	C	33
	<u>25.5</u>			<u>25.5</u>		

69.6
4.4
53

70.4
3.6
75

✓

66.4
7.8
34

Sta + π - Elev

974.04

28

✓

+21

✓

T.P. 6.73 969.73 11.04 963.00

+26

+45

11

June 19, 1963 RT 25

64.0	61.94	61.48	61.74	61.56	61.95	61.9
10.0	12.10	12.56	12.30	12.48	12.09	12.1
34		G		G	C	33
	25.5			25.5		

68.7
→ 5.8
54

69.1
4.9
75

65.0
9.0
34
Wall

65.9	63.4	60.6	60.93	60.80	61.26	61.1
8.1	10.6	13.4	13.11	13.24	12.78	12.9
49	36	25		G	C	33
				25.5		

67.1
→ 6.9
58

67.8
6.2
75

64.3
9.7
34

61.18	61.1	60.8	60.48	58.74	60.74	60.62	61.09	60.9	64.1
8.55	8.6	8.9	9.25	10.99	9.11	8.64	8.8	5.6	✓
81	75	35	24	8.99	G	G	33	34	
Apron					25.5			Wall	

61.18	60.9	60.2	59.6	60.03	59.9	60.3	60.2	63.5
8.55	8.8	9.5	10.1	9.7	9.8	9.4	9.5	6.2
81	60	35	20		G	C	33	34
Apron					25.5			✓

Sta	+	π	-	Elev.
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		969.73		
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28+50				
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✓				
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+80				
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✓				
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29				
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June 19, 1963

26

LT

E

RT

64.1	60.3	59.8	59.4	58.83	59.7	60.1	60.1	63.2
5.6	9.4	9.9	10.3	9.9	10.0	9.6	9.6	6.5
45	26	20	19		G	C	33	34
					25.5			

66.7	67.3	64.19	64.15	69.16
30	2.4	5.56	5.58	0.57
61	68	69	75	82
Ho				

63.1	59.5	59.0	58.5	58.83	58.6	58.9	58.8	62.3
6.6	10.2	10.7	11.2	10.9	11.1	10.8	10.9	7.4
48	25	19.5	19		25.5	26	33	34

65.7	66.3
4.0	3.4
65	75

66.8	66.1	65.6
2.9	3.6	4.1
75	54	46

62.1	60.5	58.4	57.9	58.06	57.9	58.2	58.2
7.6	9.2	11.3	11.8	11.67	11.8	11.5	11.5
50	33	19.5	19		25	25.5	33

65.4	65.9
4.3	3.8
69	75

66.2	65.2	64.29	64.19
3.5	4.5	5.44	5.56
75	52	46.5	43

Top step

Sta	+	π	-	Elev.
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		969.73		
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29+22				
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✓				
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+29				
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+39				
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+46				
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BM	6.63	964.15	12.21	957.52
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+65	Lt. - south edge Concrete drive			
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June 19, 1963

27

Lt.

Rt.

60.8	58.9	57.5	57.0	57.28	57.3	57.2	61.3	64.6
89	10.8	12.2	12.7	12.45	12.4	12.5	8.4	5.1
50	33	19.5	19		15	31	41	52

64.1
5.6
70
70-75
Step

64.80
4.93
70-75
Step

65.8
3.9
75

✓

60.3	60.0	58.7	56.7	57.0	57.0	56.9	61.8	64.7	65.1
9.4	9.7	11.0	13.0	12.7	12.7	12.8	7.9	5.0	4.0
91	66	38	19		15	31	44	56	75

Apron

60.3	59.6	58.3	56.4	56.7	56.7	56.5	61.0	64.4	65.6
9.4	10.2	11.4	13.3	13.0	13.0	13.2	8.7	5.3	4.1
91	55	25	19		15	31	44	58	75

✓

62.7	61.7	58.3	56.7	56.1	56.4	56.4	56.1	61.3	64.0	65.3
7.0	8.0	11.4	13.0	13.6	13.3	13.3	13.6	8.4	5.7	4.4
75	61	34	19.5	19		15	31	46	57	75

Spike in PP Rt Sta 29+37

✓

61.00	59.93	55.5	55.9	55.5	56.1	60.3	63.4	64.8
3.15	4.42	8.40	8.4	8.3	8.7	8.1	3.9	0.8
75	51	19		15	20.5	24	45	55

✓

sta + π - elev

964.15

29+23 Lt North edge Concrete drive

30

+30 M.H. 24'2" 10.42 53.73

+32

+49

+70

✓

June 19, 1963

28

Lt

L

Pt

61.01	59.74	55.29	55.5	55.6	55.1	60.0	63.3	64.3
2.14	4.41	8.86	8.7	8.6	9.1	4.2	0.9	10.1
75	51	19		15	31	45	56	75

✓

60.8	58.7	55.4	54.83	54.33	54.6	54.49	54.17	54.4	62.0	62.6
3.4	5.5	8.8	9.32	9.82	9.55	9.66	9.98	6.8	2.2	1.6
75	45	25	19.5	19		15	31	41	55	75

✓

59.1	57.5	55.8	54.0	53.1	52.2	52.6	53.5	53.0	52.9	61.4
5.1	6.7	8.4	10.2	10.5	11.0	10.6	10.7	11.2	4.3	2.8
75	55	34	25	20	19.5		15	31	52	75

✓

59.5	58.2	56.1	53.6	53.1	52.6	53.0	52.9	52.4	53.7	59.1	60.6
4.7	6.0	8.1	10.6	11.1	11.6	11.2	11.3	11.8	10.5	5.1	3.6
75	58	37	27	20	19.5		20	30	32	50	75

✓

54.0	52.9	52.5	52.0	52.2	52.1	51.8	54.3	57.8	59.0	59.9
10.2	11.3	11.7	12.2	12.0	12.1	12.4	9.9	6.4	5.2	4.3
33	28	20	19.5		20	28	32	42	60	75

56.6	54.0	53.9
2.6	2.2	5.3
52	58	75

✓

Sta	+	π	-	Elev
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		964.15		
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30+81				
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✓				
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+82				
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✓				
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+94				
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✓				
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June 19, 1963

29

LH

BK

53.5	53.1	52.0	51.5	51.8	51.7	51.4	51.6	51.4	51.3
10.7	11.1	12.2	12.7	12.4	12.5	12.8	9.6	6.8	4.9
53	41	28	21		20	28	32	40	63

53.44	53.25	56.5	51.3
10.71	10.90	7.7	6.9
54	59	64	75

on step

✓

59.9
4.3
75

52.83	52.64	52.38	51.60	51.4	51.8	51.7	51.4	51.6	51.4
11.32	11.51	11.77	12.55	12.8	12.4	12.5	12.8	9.6	6.8
91	75	52	28	21		20	28	32	40

APren Conc

✓

59.9	59.3
4.3	4.9
75	63

52.14	51.31	50.8	51.2	51.4	51.1	51.0	51.3	51.1
12.01	12.84	13.4	13.0	12.8	13.1	13.2	9.9	7.1
50	28	22	12		20	27	31	37

Conc

52.50	52.75
11.65	11.40
75	91

✓

59.0	58.4
5.5	5.2
65	56

Sta	+	π	-	Elev
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		964.15		
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31			13.04	51.11
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T.P.	6.36	959.60	10.91	953.24
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+07	Top of Wall			
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✓				
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+07	Bottom of Wall			
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✓				
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+17				
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✓				
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Lt

June 19, 1963 Rt 30

51.7	50.9	50.4	50.7	50.80	50.7	50.5	52.7	53.1	56.6
7.9	8.7	9.2	8.9	8.8	8.9	9.1	6.9	6.5	3.0
32	20	19.5	13		15	27	31	34	40

52.05 52.54
 → 7.55 7.06
 50 91
 Conc Conc

V

		54.6	58.1
55	0.0	1.5	
	71	55	
50.7	50.5	52.6	53.0
8.9	9.1	7.0	6.6
15	27	31	35

57.4
 2.2
 75

51.7	51.5	50.5	50.0	50.3	50.50	50.4	50.2	50.8	51.6
7.9	8.1	9.1	9.6	9.3	9.1	9.2	9.4	8.8	8.0
51	32	20	19.5	13		15	25	32	34

51.9
 → 7.7
 75

V

55.8 52.7
 3.8 6.9
 75 47

Sta	+	π	-	Elev
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		959.60		
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31+41				
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✓				
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+48				
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✓				
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+58.5 Walk 51' Lt				
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	8.74	50.86		
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+60				
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✓				
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June 19, 1963 31

LT

ST

51.4	50.9	49.9	49.2	49.4	49.60	49.5	49.5	51.5	54.2
8.2	8.7	9.9	10.4	10.2	10.0	10.1	10.1	8.1	5.4
53	32	20	19.5	12		16	24	40	61

51.8
7.8
75

55.7
3.9
75

✓

50.7	49.4	48.9	49.1	49.3	49.2	49.0	50.5	51.6
8.9	10.2	10.7	10.5	10.3	10.4	10.6	9.1	8.0
31	20	19.5	14		15	24	26	36

51.0 51.7
8.6 7.9
54 75

55.8 54.5 52.9
3.8 5.1 6.7
75 65 50

✓

50.86	50.5	49.0	48.5	48.6	48.80	48.7	49.9	48.6	48.9
8.74	9.1	10.6	11.1	11.0	10.8	10.9	11.7	11.0	10.7
51	33	20	19.5	15		15	24	26	29

51.49 51.89
8.11 7.71
66 75

54.3 52.9 50.5 49.9 50.8 50.4
5.3 6.7 9.1 9.7 8.8 9.2
75 61 48 41 36 31

✓

Sta + π - Elev.

959.60

31480

✓

✓

BM 0.23 953.32 4.52 953.08 (953.09)

32

✓

+30

Lt

June 19, 1963
BX 32

48.6	48.2	47.9	47.8	48.00	47.9	47.1	47.8	48.0
11.0	11.4	11.9	11.8	11.6	11.7	12.5	11.8	11.6
26	20	19.5	15		17	24	26	29

49.6	50.1	51.8
10.0	9.5	7.8
34	51	75

45.9	46.8	49.4	50.2
13.7	12.8	10.2	9.4
58	48	37	32

45.2	44.8
14.4	14.8
66	75

Top N.E. Cor. Lower Step Ho #1975 W.B. Ave.

49.3	49.1	47.4	46.9	47.22	47.0	46.6	47.2	47.3
4.0	4.2	5.9	6.4	6.10	6.3	6.7	6.1	6.0
51	32	20	19.5		18	21	26	29

49.7
3.6
75

Edge Drive

43.6	44.5	46.4	48.5
9.7	8.8	6.9	4.8
75	62	47	36

48.6	48.5	46.3	46.2	45.7	46.0	45.8	45.1	45.5	45.8	47.9
4.7	4.8	7.0	7.1	7.6	7.3	7.5	8.2	7.8	7.5	5.4
54	33	22	20	19.5		18	24	25	29	34

48.7	48.2	48.4
4.6	5.1	4.9
66	67	75

Drive

43.2	44.9	46.5
10.1	8.4	6.8
75	60	45

Sta	+	π	-	Elev.
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		953.32		
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32+46				
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✓				
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+62				
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✓				
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+79				
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✓				
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		90		
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FK
JS
BZ
FK
JM

Lt.

June 20, 1963
Rt. 33

47.7	47.4	45.4	45.0	45.3	45.4	45.1	44.2	44.5	44.6	48.0
56	59	79	83	8.0	7.9	8.2	9.1	8.8	8.7	53
52	34	20	19.5	12		19	24	26	28	34

46.3	46.1	46.8	47.5
70	72	65	5.8
58	61	71	75

Drive

43.0	43.3	45.6	47.9
10.3	10.0	7.7	54
75	68	53	37

44.9	44.6	44.5	44.2	44.3	44.7	44.7	44.7	44.4	43.7
8.4	8.7	8.8	9.1	9.0	8.6	8.6	8.6	8.9	9.6
75	60	38	24	20	10	7	18	21	24

Ent

42.9	42.8	43.3	47.2	47.9	43.8
104	105	100	6.1	5.4	9.5
75	66	54	41	36	29

44.6	44.4	43.98	43.6	44.0	44.1	44.0	44.0	43.0	43.3
8.7	8.9	9.54	9.7	9.3	9.2	9.3	9.3	10.3	10.0
55	41	23.6	20	10		8	19	24	29

Ch. MH

44.8	43.2
8.5	8.1
75	100

42.8	42.8	46.3	46.4
10.5	10.5	7.0	6.9
75	49	37	35

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		953.32		
--	--	--------	--	--

32+95				
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33				
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		9.99		
--	--	------	--	--

			43.33	
--	--	--	-------	--

+08				
-----	--	--	--	--

✓				
---	--	--	--	--

+28				
-----	--	--	--	--

June 20, 1963 34

LT

RT

44.1	43.9	43.4	43.0	43.4	43.5	43.4	43.4	42.1	42.8	44.8
9.2	9.4	9.9	10.3	9.9	9.8	9.9	9.9	11.2	10.5	8.5
60	41	32	21	10		8	19	23	28	32

Corbarkins

44.3

9.0

75

Corbarkins

✓

42.7	42.7	42.8	43.8
10.6	10.6	10.5	9.5
75	62	44	37

45.4	44.7	43.1	42.6	42.9	43.0	42.9	42.9	41.6	43.3
7.9	8.6	14.2	10.7	10.4	10.3	10.4	10.4	11.7	10.0
55	35	29.5	20	10		8	18	24	31

EP

45.6

45.8

7.7

7.5

69

75

EP

✓

42.7	42.7	42.5	42.3
10.6	10.6	10.8	11.0
75	60	43	36

46.1	45.8	42.5	42.0	42.1	42.2	42.2	42.3	41.1	42.4
7.2	9.5	10.8	11.3	11.2	11.1	11.1	11.0	12.2	10.9
50	31	20	19.5	10		8	19	32	37

48.0

48.5

5.3

4.8

67

75

✓

42.9	42.7
10.4	10.6
75	55

Sta	+	π	-	Elev.
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		953.32		
--	--	--------	--	--

33+42				
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✓				
---	--	--	--	--

+54				
-----	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

TP	4.59	946.29	11.62	941.70
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+73				
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LT

June 20, 1963
RT 35

43.0	42.0	41.5	41.6	41.7	41.6	41.8	41.4	42.4	42.5
10.3	11.3	11.8	11.7	11.6	11.7	11.5	11.9	10.9	10.8
31	20	19.5	10		8	19	35	50	75

46.0	46.02	48.24	48.65
2.3	7.30	5.08	4.67
54	58	63	75

Walk

41.62	41.35	41.23	41.0	41.1	41.2	41.1	41.2	41.0	39.7
11.70	11.97	12.09	12.3	12.2	12.1	12.2	12.1	12.3	13.6
51	32	19.5	19.5	10		8	18	20	25

C. Ent 3

41.64
11.68
61

42.0	42.4	41.9	39.8	39.2
11.3	10.9	11.4	13.5	14.1
60	53	41	37	32

42.8	42.7
10.5	10.6
70	75

41.50	41.22	40.43	40.3	40.4	40.5	40.4	40.2	38.8	38.5	40.7
4.79	5.07	5.86	6.0	5.9	5.8	5.9	6.1	25	28	5.6
49	34	20	20	10		8	18	22	30	37

Circ

41.67
4.62
56

44.3	43.9	42.5	42.1
20	24	38	42
75	64	55	49

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		946.29		
--	--	--------	--	--

34				
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✓				
---	--	--	--	--

+25				
-----	--	--	--	--

✓				
---	--	--	--	--

+43				
-----	--	--	--	--

✓				
---	--	--	--	--

June 20, 1963

36

LT

BT

41.5	40.5	39.6	39.1	39.3	39.45	39.45	39.4	39.1	37.4	37.3	40.5
4.8	5.8	6.7	7.2	7.0	6.84	6.9	7.2	8.9	9.0	5.8	
52	36	20.5	20	10		7	18	22	27	32	

42.6	42.7	44.2	45.7
37	36	21	0.6
53	55	56	62

44.8	44.0	42.3	41.2
1.5	2.3	4.0	5.1
75	63	49	37

✓

40.1	39.2	38.6	38.1	38.3	38.5	38.4	38.2	37.7	36.2	36.2
6.2	7.1	7.7	8.2	8.0	7.8	7.9	8.1	8.6	10.1	10.1
42	31	20.5	20	10		8	17	19	22	27

Cor Park

40.8	42.3	43.0	46.1
5.5	4.0	3.3	9.2
53	54	58	75

43.1	42.9	43.0	42.3
3.2	3.4	3.3	4.0
75	61	51	36

✓

40.3	39.2	39.9	39.4	39.7	37.8	39.7	37.5	35.5	35.6	40.9
6.0	7.1	8.4	8.9	8.6	8.5	8.6	8.8	10.8	10.7	5.4
55	41	20.5	20	10		10	18	22	27	35

Park

41.3	41.31	45.13
5.0	4.98	1.16
56	61	75

Steps

42.0	42.0	42.2
4.3	4.3	4.1
75	60	43

✓

Sta	+	π	-	Elev
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		946.29		
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34+48				
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✓				
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+68				
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✓				
---	--	--	--	--

+78				
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✓				
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June 20, 1963

37

Lt

Rt

11.0	10.1	36.2	37.1	37.5	37.6	37.5	37.3	35.4	35.5
5.3	6.2	8.1	9.2	8.8	8.7	8.8	9.0	10.9	10.8
72	55	34	22	10		8	18	23	27

11.75

4.54
86

Apron



11.3	11.8	11.8	11.4
5.0	4.5	4.5	4.9
75	60	49	38

10.0	37.8	36.7	36.4	36.6	36.8	36.8	36.4	34.5	34.4	37.9
6.3	8.5	9.6	9.9	9.7	9.5	9.5	9.9	11.8	11.9	8.4
55	34	23	21	10		10	18.5	22	27	38

10.9

11.76

5.4 4.53
72 86

Apron



39.7	39.2	38.4
6.6	7.1	7.9
75	61	45

37.3	36.80	36.5	36.0	36.3	4.95	36.3	36.0	37.8	37.9
9.0	9.49	9.8	10.3	10.0	9.9	10.0	10.3	12.5	12.4
29	22	20.5	20	10		10	18	22	27

MH

10.2

11.7

11.9

11.6

6.1 4.6 2.4 + 0.03
39 55 57 62

Conc



37.6	36.9	35.5
8.7	9.4	10.8
75	54	39

Sta + π - Elev.

946.29

35

✓

+30

✓

TP 1.37 938.17 9.49 936.80

6.51 31.66 931.42

+30

+55

✓

June 20, 1963

38

Lt

£

36.1	35.7	35.2	35.5	35.51	35.2	32.5	32.3	31.2
9.6	10.6	11.1	10.8	10.78	11.1	13.8	14.0	15.1
30	20.5	20	10		17	24	31	48

40.1	42.2	44.9	46.3
6.2	4.1	1.4	0.0
38	56	57	64

✓

33.7	32.7
12.6	13.6
75	64

41.7	39.0	35.4	34.5	34.1	34.4
4.6	7.3	10.9	11.8	12.2	11.9
57	39	28	20.5	20	

✓

43.4	43.9
2.9	2.4
64	75

✓

34.1	31.8	30.7	29.7	29.4	29.1
4.1	6.4	7.5	8.5	8.8	9.1
17	23	33	49	62	75

34.6	34.4	33.7	33.7	33.2	33.4
3.6	3.8	4.5	4.5	5.0	4.8
64	49	29	20	19.5	

33.0	31.4	31.2	30.1
5.2	6.8	7.0	5.5
17	21	23	27

✓

34.6

3.6 Under Const
75

28.9	29.7	32.2	33.1
9.3	8.5	6.0	5.1
75	62	48	30

Sta	+	x	-	Elev
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		938.17		
--	--	--------	--	--

35+85				
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✓				
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TP	10.59	942.72	6.04	932.13
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36				
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✓				
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+30				
-----	--	--	--	--

Lt

June 20, 1963

39
Rt

30.9	30.9	32.0	32.5	32.0	32.3	31.8	30.7	32.3	32.8	33.1
73	73	62	57	62	59	64	75	59	54	51
75	65	43	24	20		18	23	28	39	52

Under Construction



29.7	31.7	32.2
8.5	6.5	6.0
75	67	63

Curb Lt.

30.3	30.6	31.5	31.7	31.4	31.66	31.5	31.3	30.4	31.9
12.4	12.1	11.2	11.0	11.3	11.06	11.2	11.4	12.3	10.8
75	57	42	21	20.5		10	18	24	30

Under Const.

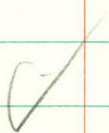


31.4	33.7	36.1	33.5
11.3	9.0	6.6	9.2
75	65	54	46

30.4	30.6	30.2	30.1	30.5	30.1	29.1	32.3	35.0
12.3	12.1	12.5	12.6	12.2	12.6	13.6	10.4	7.7
46	23	20	19		17	23	31	40

Under Const.

26.4	28.2
16.3	14.5
50	75



37.8	39.6	40.5
4.9	3.1	2.2
75	66	52

Sta + π - Elev.

942.72

36+50

✓
T.P. 3.61 933.23 13.10 929.62

10.36 922.87 922.81

+75

✓
37

✓
BM 4.04 926.85 10.36 922.87 (922.81)

Lt

June 20, 1963

Rt

40

25.6	30.1	29.5	29.3	29.7	29.2	28.7	27.9	32.2
17.1	12.6	13.2	13.4	13.0	13.5	14.0	14.8	10.5
39	31	19.5	19		17	21	22	31

Under Const.

37.1	37.1	35.4	32.6
5.6	5.6	7.3	10.1
25	64	47	37



21.0	21.6	28.5	28.2	28.6	28.1	27.8	24.1	23.4
12.2	5.6	4.7	5.0	4.6	5.1	5.4	9.1	9.8
55	44	33	20	19	17	27	32	38

60' Under Const



31.7	30.2	26.0
1.5	3.0	7.2
75	67	51

21.3	24.8	27.6	27.2	27.4	27.56	27.1	26.5	26.7	21.0
11.9	8.4	5.6	6.0	5.8	5.67	4.1	6.7	6.5	12.2
37	24	21	18	7		15	20	25	38

20.0

13.2

42

Under Const.

24.4	22.9	19.4
88	10.3	13.8
75	69	55



N.W. Cor Signal Control Structure

Sta	+	π	-	Elev.
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		926.85		
--	--	--------	--	--

37+30				
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✓				
---	--	--	--	--

+70				
-----	--	--	--	--

✓				
---	--	--	--	--

38				
----	--	--	--	--

✓				
---	--	--	--	--

June 20, 1963 41
RH

21.

23.1	25.7	26.6	26.0	26.3	26.5	26.1	25.7	19.4	18.5
3.8	1.2	0.3	0.9	0.6	0.4	0.8	1.2	7.5	8.4
33	22	19.5	17	10		15	28	37	45

Under Const

18.3

8.6
43

17.3

9.6
75

17.3

9.6
57

✓

22.0	24.6	25.3	24.5	24.6	24.8	24.7	24.2	17.8	15.9
4.9	2.4	1.6	2.4	2.3	2.1	2.2	2.7	9.1	11.0
35	21	19	16	9		14	24	35	46

13.8

13.1
47

09.5

17.4
56

07.1

19.8
75

14.6

12.3
75

15.1

11.8
57

✓

11.7	16.5	23.5	23.3	23.4	23.4	23.4	23.2	16.4	15.3
15.2	10.4	3.4	3.6	3.5	3.39	3.5	3.7	10.5	11.6
37	26	17	15	13		12	20	33	46

14.9

17.0
51

08.1

18.8
75

15.7

11.2
75

15.2

11.7
61

✓

Sta

926.85

38+20

✓

+32

✓

+38

✓

June 20, 1963

42

LT

♀

RT

22.3	22.9	22.5	22.6	22.8	22.8	22.8	16.7	15.3
4.6	4.0	4.4	4.3	4.1	4.1	4.1	10.2	11.6
18	16.5	15	10		13	19	29	44

21.5	16.7	12.3	10.2	09.2	✓	18.1	17.5	16.1
5.4	10.2	14.6	16.7	17.7		8.8	9.4	10.8
25	34	42	58	75		25	65	53

20.9	21.5	22.3	22.1	22.5	22.4	22.2	19.4	16.96
6.0	5.4	4.6	4.8	4.4	4.5	4.7	2.5	9.89
35	23	18	15		12	21	28	33

Inv. Calc

16.8	12.3	10.6	10.2	✓	21.3	20.6	19.8	19.8
10.1	14.6	16.3	16.7		5.6	6.3	7.1	7.1
41	49	65	75		75	59	46	37

15.0	16.4	20.6	22.0	22.3	22.2	21.6	21.2	22.38
11.9	10.5	6.3	4.9	4.6	4.7	5.3	5.7	4.47
41	36	33	15		12	27	50	Rail 69

13.0	10.6	10.3		✓	21.9
13.9	16.3	16.6			5.0
45	63	75			75

Sta	+	π	-	Elev.
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		926.85		
--	--	--------	--	--

38+50				
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✓				
---	--	--	--	--

+60				
-----	--	--	--	--

+72				
-----	--	--	--	--

o				
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✓				
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+66	NE Culv	38' RT (Inv.)	11.03	15.82
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BM	0.14	922.95	4.04	922.81
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				(922.81)
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+89				
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June 20, 1963 Rt 43

Lt

16.4	17.7	20.8	21.7	21.6	21.8	21.8	21.80	21.5	22.08
10.5	9.2	6.1	5.2	5.3	5.1	5.1	5.05	5.4	4.77
58	44	26	18	13		11	S Rail 20	33	N Rail 47

15.5

11.4
75

21.4 21.5
5.5 5.4
75 62

✓

19.4	20.3	21.4	20.8	21.4	21.44	21.6	21.7	21.4	19.9	20.1	20.4
7.5	6.6	5.71	6.1	5.5	5.4	5.3	5.2	5.5	7.0	6.8	6.5
75	57	32	19	13	7		12	26	38	52	75
S Rail & Track				N Rail		✓					

20.3	20.78	20.0	20.7	21.2	21.3	21.2	21.0	17.2	16.7
6.6	6.07	6.9	6.2	5.7	5.6	5.7	5.9	9.7	10.2
77	N Rail 69	44	22	10		10	18	26	35

✓

19.2 18.0 16.9
7.7 8.9 10.0
75 57 43

N.W. Cor Signal Base

14.8	13.0	13.3	20.5	20.7	20.8	20.7	20.4	14.9	13.6	13.2
8.2	10.0	7.7	2.5	2.3	2.2	2.3	2.6	8.1	9.4	9.8
50	42	27	17	11		10	18	27	33	45

15.3
17.5 17.4
5.5 5.6
66 75

✓

16.0 14.8
7.0 8.2
75 61

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		922.95		
--	--	--------	--	--

39				
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✓				
---	--	--	--	--

BM	5.66	921.29	7.32	915.63 ✓
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+11				
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✓				
---	--	--	--	--

+22				
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✓				
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FK
JS
BZ
FK
JM

Lt

June 20, 1963 44
June 21, 1963

11.4	12.5	19.8	20.2	20.24	20.2	19.8	12.5	11.8
11.6	10.5	3.2	2.8	2.71	2.8	3.2	10.5	11.2
47	31	17	10		10	17	31	40

12.9 14.2
10.1 8.8
64 75

11.4 11.0 11.7
11.6 12.0 11.3
75 67 51

Top S.W. Cor Ent. Slab Monette Const. Co.

13.9	15.2	18.8	19.6	19.7	19.6	19.2	10.9	11.9
7.4	6.1	2.5	1.7	1.6	1.7	2.1	10.4	9.4
29	23	19	10		11	18	34	39

14.3 12.6 13.6 15.0
7.0 8.7 7.7 6.3
37 47 68 75

9.8 10.0 10.1
11.5 11.3 11.2
75 63 45

17.4 17.6 18.5 19.0 19.1
3.9 3.7 2.8 2.3 2.2
41 26 16 11

19.0 18.8 10.4 9.9
2.3 2.5 10.9 11.4
11 18 33 37

16.7 16.1
4.6 5.2
63 75

9.1 9.8
12.2 11.5
75 54

Sta	+	π	-	Elev.
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		921.29		
--	--	--------	--	--

39+52				
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✓				
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+70				
-----	--	--	--	--

✓				
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40				
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T.P.	3.86	916.05	9.10	912.19
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+38				
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June 21, 1963

45

Lt

Rt

Rt

16.0	16.3	16.4	16.8	17.1	17.7	17.6	17.5	17.5	17.1
5.3	5.0	4.4	4.5	3.6	3.6	3.7	3.8	10.8	10.6
75	56	32	19	10		11	19	30	55

✓

9.8	10.4
11.5	10.9
75	66

15.6	16.2	16.2	16.8	17.0	16.8	16.6	15.6	16.1
5.7	5.1	5.1	4.5	4.3	4.5	4.7	5.7	5.2
55	30	19	12		11	18	21	35

✓

14.5
6.8
75

11.2	14.1	16.1	14.7
10.1	7.2	5.2	6.6
75	65	55	47

13.9	14.5	15.6	15.2	15.7	15.83	15.5	15.0	14.8	15.0
7.4	6.8	5.7	6.1	5.6	5.46	5.8	6.3	6.5	6.3
75	56	30	18	11		13	22	39	57 8 1/2

✓

07.53	07.53	8.6	13.9	14.4	14.7	14.1	13.7	14.3	14.9
8.52	8.52	7.5	2.2	1.7	1.7	2.0	2.4	1.8	1.2
52	42	31	20	11		11	20	37	60 Bldg

(Headwall)

11.2	05.1
8.9	11.0
56	75

✓

Sta	+	π	-	Elev.
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		916.05		
--	--	--------	--	--

40+66				
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✓				
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+87	Ent	Rt		
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✓				
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41	N. Edge	Ent Rt		
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✓				
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June 21, 1963 46

11

5

899.5	04.9	06.9	12.1	13.3	13.30	13.3	13.0	13.6	14.2
16.6	11.2	9.2	3.4	2.8	2.75	2.8	3.1	2.5	1.9 Under
43	37	29	19	11		11	20	34	53 Const

898.8	03.8	05.5	04.6	03.4
17.3	12.3	10.6	11.5	12.7
51	56	60	61	75

✓

899.2	04.6	07.2	12.1	12.6	12.7	12.4	12.9	12.0	10.8
16.9	11.5	8.9	4.0	3.5	3.4	3.7	3.2	3.1	5.3
41	37	26	17	11		15	31	48	67

899.5	899.7	02.5	02.1
16.6	16.4	13.6	14.0
46	52	55	75

✓

05.7	08.2
10.4	7.9
100	84

898.7	04.0	05.8	11.7	12.1	12.34	12.2	11.9	12.5	12.7
17.4	12.1	10.3	4.4	4.0	3.71	3.9	4.2	3.6	3.4
41	37	27	18	11		11	18	32	47

898.4	898.6	02.7	01.7
12.7	12.5	13.4	14.4
47	53	55	75

✓

06.0	04.8	11.9
10.1	6.3	4.2
100	73	58

Sta	+	π	-	Elev.
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		916.05		
--	--	--------	--	--

41+22				
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✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	2.96	912.86	6.15	909.90
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42				
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✓				
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21

June 21, 1963 47

02.1	05.0	11.2	11.5	11.8	11.4	11.2	11.4	10.4
13.4	11.1	4.9	4.6	4.3	4.7	4.9	4.7	5.7
37	28	17	11		12	23	28	33

898.7	898.2	898.3	01.2	00.3	✓	01.0	10.3	10.7	10.9
17.4	17.9	17.8	14.9	15.8	✓	9.1	5.8	5.4	5.2
41	46	51	54	75		75	66	53	42

02.1	02.5	10.6	10.9	11.0	10.7	10.3	03.2	01.9
14.0	13.6	5.5	5.2	5.1	5.4	5.8	12.9	14.2
35	32	17	11		11	21	32	38

897.9	897.5	898.2	00.1	899.8	✓	00.4	00.4	00.8
18.2	18.6	17.9	16.0	16.3	✓	15.7	15.7	15.3
39	46	51	54	75		75	71	55

897.9	899.7	01.2	09.6	09.9	09.9	09.8	09.0	00.2	899.1	899.0
15.0	13.2	11.7	3.3	3.0	2.96	3.1	3.9	12.7	13.8	13.9
39	36	30	17	11		11	21	38	54	75

897.1	897.8	899.7	899.6
15.8	15.1	13.2	13.3
43	48	51	75

Sta	+	π	-	Elev
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		912.86		
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42+50				
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✓				
---	--	--	--	--

		53		
--	--	----	--	--

+62				
-----	--	--	--	--

✓				
---	--	--	--	--

+77				
-----	--	--	--	--

✓				
---	--	--	--	--

June 21, 1963

48

Lt

E

Rt

898.7	899.9	01.5	08.7	09.2	09.4	09.3	08.4	899.8	898.9
14.2	13.0	11.4	4.2	3.7	3.5	3.6	4.5	13.1	14.0
35	33	28	17	11		11	21	38	57

897.4	897.7	899.3	899.5
15.5	15.2	13.6	13.4
41	44	48	75

898.8
14.1
75

✓

898.2	00.07	01.3	08.5	04.1	09.2	09.0	08.3	00.8	00.1
14.7	12.79	11.6	4.4	3.8	3.65	3.9	4.6	12.1	12.8
34	33	28	17	11		11	22	33	36
Top Culvert						Culv Buried			

897.9	898.0	899.4	899.5
15.0	14.9	13.5	13.4
40	45	51	75

898.8	898.9
14.1	14.0
75	59

✓

08.5	09.0	09.2	09.0	08.5	01.8	00.2
4.4	3.9	3.7	3.9	4.4	11.1	12.7
17	11		11	20	30	36

05.1	899.3	899.4	899.4
7.8	13.6	13.5	13.5
31	40	51	75

898.6	898.9
14.3	14.0
75	55

✓

Sta	+	π	-	Elev.
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		912.86		
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43				
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✓				
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T.P.	8.55	912.62	8.79	904.07
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+50				
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✓				
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44				
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FK
FS
LB
BZ

LT

June 26, 1963
Sept 4, 1963 R+ 49

00.0	01.9	08.4	08.8	08.74	08.8	08.2	00.3
12.9	11.0	4.5	4.1	3.92	4.1	4.7	12.6
34	25	17	11		11	21	34

899.4	899.1	899.4	898.5	898.8	899.6
13.5	13.8	13.5	14.4	14.1	13.3
49	62	75	75	59	37

Nail in PPLT.

01.1	03.8	07.9	08.5	08.7	08.6	07.6	02.1	00.3
11.5	8.8	4.7	4.1	3.9	4.0	5.0	10.5	12.3
33	24	18	11		12	19	26	33

99.9	99.4	99.4	98.3	98.6	98.7
12.7	13.2	13.2	14.3	14.0	13.9
44	60	75	75	63	47

00.1	02.8	08.2	08.5	08.68	08.5	07.8	04.3	00.6
12.5	9.8	4.4	4.1	3.94	4.1	4.8	8.3	12.0
37	26	17	11		11	18	27	33

00.5	00.3	00.6	998.5	998.6	999.0
12.1	12.3	12.0	14.1	14.0	13.6
41	56	75	75	59	43

Sta + π

912.62

44+50

✓

45

✓

+50

✓

Sept. 4, 1963 50
 Rt

11

02.6

10.0
20

07.9

4.7
18

08.4

4.2
11

08.6

4.0

08.3

4.3
11

07.5

5.1
18

02.3

10.3
26

04.7

11.9
32

00.6

12.0
36

01.5

11.1
39

01.5

11.1
49

01.7

10.9
75

98.6

14.0
75

98.8

13.8
57

99.2

13.4
42

02.5

10.1
32

04.2

8.4
24

08.0

4.6
18

08.3

4.3
11

08.44

4.18

08.2

4.4
11

07.6

5.0
17

02.2

10.4
27

00.9

11.7
33

00.8

11.8
36

01.5

11.1
40

01.6

11.0
57

02.2

10.4
75

98.7

13.9
75

99.1

13.5
57

99.2

13.4
43

01.2

11.4
33

03.0

9.6
26

07.7

4.9
18

08.1

4.5
11

08.17

4.45

07.9

4.7
11

07.1

5.5
19

01.2

11.4
28

00.0

12.6
36

00.9

11.7
40

00.8

11.8
57

01.2

11.4
25

99.5

13.1
75

99.7

12.9
66

99.4

13.2
44

00.1

12.5
34

Sta	+	π	-	Elev.
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9/12.62

46

✓

+50 Feels like Peat Bog as cars
Hit crack in Pavement

✓

47

✓

Sept. 4, 1963 51

LT

RT

02.4	07.0	07.8	08.04	07.9	07.6	02.3
10.2	5.6	4.8	4.58	4.7	5.0	10.3
27	19	11		11	19	26

00.9	00.1	00.2	00.4	99.9	99.3	99.8
11.7	12.5	12.4	12.2	12.7	13.3	12.8
38	42	59	75	75	55	35

03.5	07.8	08.1	08.2	08.1	07.6	02.2
9.1	4.8	4.5	4.4	4.5	5.0	10.4
25	19	11		11	19	29

01.6	00.5	00.1	00.1	01.4	00.8	00.6	00.9
11.0	12.1	12.5	12.5	11.2	11.8	12.0	11.7
32	39	57	75	75	64	51	38

01.3	02.8	08.0	08.4	08.60	08.6	08.2	04.6
11.3	9.8	4.6	4.2	4.02	4.0	4.4	8.0
38	28	19	11		11	21	25

00.5	00.4	00.6	02.9	02.5	02.3	03.2
12.1	12.2	12.0	9.7	10.1	10.3	9.4
52	65	75	75	56	43	31

Sta	+	π	-	Elev.
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		912.62		
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47+50				
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✓				
---	--	--	--	--

48				
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✓				
---	--	--	--	--

+30				
-----	--	--	--	--

✓				
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B.M	665	919.27	0.00	912.62 (912.62)
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Sept. 4, 1963 52
 Lt Rt

08.2	08.9	09.1	09.1	08.7	08.9	02.7
4.4	3.7	3.5	3.5	3.9	8.7	9.9
19	11		11	21	29	39

03.5	02.2	01.7	01.2	03.5	02.8
9.1	10.4	10.9	11.4	9.1	9.8
29	39	57	75	75	56

04.7	06.0	09.2	09.8	09.96	09.8	09.5	05.5
7.9	6.6	3.4	2.8	2.66	2.8	3.1	7.1
36	28	21	11		11	20	29

04.1	04.0	03.3	04.2	04.1	04.8
8.5	8.6	9.3	8.4	8.5	7.8
48	60	75	75	54	35

06.5	07.4	10.2	10.3	10.5	10.4	10.2	06.7	05.5
6.1	5.2	2.4	2.3	2.1	2.2	2.4	5.9	7.1
37	27	19	11		11	20	27	38

05.6	04.9	04.9	05.0	05.1
7.0	7.7	7.7	7.6	7.5
55	70	75	75	56

Top S. E. Cor Lower Step Ho #2125

Sta + π - Elev

919.27

48+55

✓

+80

✓

49

✓

Sept. 4, 1963 53
Rt

Lt

09.3	10.7	10.9	11.0	11.2	10.9	10.9	08.3	07.0
10.0	8.6	8.4	8.3	8.1	8.4	8.4	11.0	12.3
26	21	18	11		11	21	26	35

10.5	11.1	11.4	11.7		05.9	06.1	06.6
8.8	8.2	7.9	7.6	✓	13.4	13.2	12.7
32	47	61	75		75	66	51

11.2	10.6	11.5	11.6	11.8	11.5	11.5	10.5
8.1	8.7	7.8	7.7	7.5	7.8	7.8	8.8
29	24	20	10		11	22	28

11.9	12.2	12.3	11.97	06.9	07.2	08.1	09.1
7.4	7.1	7.0	7.30	12.4	12.1	11.2	10.2
46	60	75	Wakot H. 85	75	58	45	34

11.4	11.8	12.1	12.3	12.2	12.3	12.2	11.2
7.9	7.5	7.2	7.0	7.1	7.0	7.1	8.1
24	20	10		10	15	20	24

11.9	12.3	12.3	12.3	07.4	07.9	08.4	09.6	10.2
7.4	7.0	7.0	7.0	11.9	11.4	10.9	9.7	9.1
31	44	60	75	75	63	51	37	27

✓

Sta + π - Elev

9/19.27

49+23

✓

+41

✓

+53

✓

Sept. 4, 1963 54
R1

LT

12.6	12.4	12.7	12.7	12.92	12.9	12.9	13.0	11.8
6.7	6.9	6.6	6.6	6.35	6.4	6.4	6.3	7.5
25	23	20	10		10	16	20	26

12.4	12.4	12.6	12.7	12.57	08.2	08.7	09.4	10.9
6.9	6.9	6.7	6.6	6.70	11.1	10.6	9.9	8.4
29	45	60	75	Apron 89	75	58	44	36

13.3	13.1	13.3	13.5	13.42	13.3	14.1	14.3
6.0	6.2	6.0	5.8	5.85	6.0	5.2	5.0
23	22	10		10	19	31	45

13.1	13.3	13.3	13.6	14.6	14.5
6.2	6.0	6.0	5.7	4.7	4.8
36	50	61	75	75	59

14.2	13.9	13.3	13.6	13.8	13.8	13.8	14.1	14.5
5.1	5.4	6.0	5.7	5.5	5.5	5.5	5.2	4.8
31	25	22	10		10	20	29	43

14.6	13.8	14.0	14.5	15.2	14.9
4.7	5.5	5.3	4.8	4.1	4.4
50	55	62	66	75	59

14.8
4.5
75

Sta	+	π	-	Elev
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9/9.27

49+58	Berm	Left		
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✓

+62	Gn Her	Left		
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✓

+77	± Batke St			
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✓

£ Sept. 4, 1963 55

Lt

Rt

13.9	13.3		13.4	13.8	14.0	13.9	13.8	13.2	13.7
54	60	59	55	53	54	55	61	56	
29	25	22	10		10	19	21	22	

14.5	14.5	14.1	14.2	14.7	14.7	✓ 16.2	16.2	15.8	15.2	14.6
48	48	52	51	46	46	31	31	35	41	47
39	51	54	63	66	75	75	56	44	32	26

13.7	13.5	13.5	13.9	14.1		14.0		13.7	13.9
56	58	58	54	52		53		56	54
48	33	22	10			10		20	23

13.9	14.0	✓	16.2	16.4	16.0	15.2
54	53		31	29	33	41
66	75		75	64	44	30

14.1	13.9	13.8	14.0	14.3	14.5	14.5	14.0	14.4	14.6
52	54	55	53	50	48	48	53	49	47
60	46	32	22	10		10	20	23	26

14.2	14.7	15.7	17.3	✓ 16.8	16.7	16.2	15.4
51	46	36	20	25	26	31	39
75	100	125	150	61	51	40	31

19.1
02
175

16.9
2.4
75

227
Walkat H.
76

Sta + π - Elev.

919.27

49+92 Gutter Line

✓

50

✓

TP 9.30 926.96 1.61 917.66 (917.66)

+10

✓

Sept. 4, 19

56

11

2

Rt

14.2	14.2	14.8	14.9	14.8	14.5	14.8
5.1	5.1	4.5	4.4	4.5	4.8	4.5
37	24	10		10	20	22

14.2	14.2	14.3	17.1	17.0	16.4	15.4
5.1	5.1	5.0	2.2	2.3	2.9	3.9
54	66	75	75	57	41	29

14.9	14.5	15.0	15.12	15.1	14.9	15.1
4.4	4.8	4.3	4.15	4.2	4.4	4.2
24	22	10		10	19	23

14.9	15.0	14.9	14.8	17.3	17.2	17.0	16.5	15.6	15.1
4.4	4.3	4.4	4.5	2.0	2.1	2.3	2.8	3.7	4.2
32	43	59	75	75	63	54	42	30	27
S.W. Cor		Lower	Stop Ho #				Rt Sta	50	

16.2	15.3	14.7	15.3	15.4	15.4	16.3	15.5
10.8	11.7	12.3	11.7	11.6	11.6	11.7	11.5
28	24	22	10		10	20	23

16.7	16.8	16.1	15.8	17.1	17.0	16.9	16.3
10.3	10.2	10.9	11.2	9.9	10.0	10.1	10.7
38	53	68	75	75	65	51	36

Sta	+	π	-	Elev.
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		926.96		
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50+27				
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✓				
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+48				
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✓				
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+71				
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T.P.	7.51	930.07	4.40	922.56
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Sept. 4, 1963

57

14

4

RT

116.0	115.6	115.2	115.7	115.9	115.8	115.4	116.8
110	114	118	113	111	112	116	102
26	23	22	10		10	19	23
18.7	21.0	21.9	21.3	20.2	18.2	18.3	18.3
8.3	6.0	5.1	5.7	6.8	7.7	8.8	8.7
29	33	37	48	60	75	75	68
						55	40
							30

16.6	16.4	15.9	16.3	16.5	16.4	16.2	18.6
10.4	10.6	11.1	10.7	10.5	10.6	10.8	8.4
25	23	22	10		10	19	24
20.1	23.6	22.8	22.5	21.6	21.3	22.4	22.2
6.9	3.4	4.2	4.5	5.4	5.7	4.6	4.8
29	33	44	54	66	75	75	68
							52
							39

20.3	18.0	17.3	16.8	17.0	17.1	17.0	16.9
6.7	9.0	9.7	10.2	10.0	9.9	10.0	10.1
31	29	23	22	10		10	19
21.8	22.2	22.5	22.6	23.3	25.2	25.6	25.0
5.2	4.8	4.5	4.4	3.7	1.8	1.4	2.0
34	39	52	62	75	75	65	56
							40

Nail in PP RT Sta 51+05

Sta	+	π	-	Elev.
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		930.07		
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50+86				
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✓				
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51				
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✓				
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+24				
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Sept. 4, 1963

58

lt.

rt.

18.6	17.9	17.2	17.5	17.6	17.5	17.4	18.7
11.5	12.2	12.9	12.6	12.5	12.6	12.7	11.4
31	23	20	10		10	19	24

20.2	21.7	22.4	23.1	24.0	24.9	25.0	24.7	24.0	22.7	20.7
9.9	8.4	7.7	7.0	6.1	5.2	5.1	5.4	6.1	7.4	9.4
33	37	51	62	75	75	64	55	41	29	27

19.1	18.0	17.5	17.8	17.92	17.9	17.6	19.1	22.7
11.0	12.1	12.6	12.3	12.15	12.2	12.5	11.0	7.4
32	24	22	10		10	19	24	31

21.3	22.3	23.3	24.3	25.4	24.7	24.0
8.8	7.8	6.8	5.8	4.7	5.4	6.1
46	59	68	75	75	58	47

20.1	18.7	18.3	18.5	18.6	18.5	18.2	18.8	20.5
10.0	11.4	11.8	11.6	11.5	11.6	11.9	11.3	9.6
31	24	23	10		10	20	23	26

22.2	22.7	23.1	24.4	26.6	25.5	24.2	23.3	22.2
7.9	7.4	7.0	5.7	3.5	4.6	5.9	6.8	7.9
39	50	59	75	75	62	47	34	28

Sta	+	π	-	Elev.
		930.07		

51+54

✓

+75

✓

TP	9.48	929.02	10.53	919.54
----	------	--------	-------	--------

BM			3.70	925.32 (925.32)
----	--	--	------	-----------------

52				L.D.G.
----	--	--	--	--------

✓

Lt

Sept. 4, 1963 59

Rt

19.6	19.3	19.0	19.4	19.5	19.32	19.1	19.4	20.9
10.5	10.8	11.1	10.7	10.6	10.75	11.0	10.7	9.2
32	24	23	10		10	19	24	27

22.1	22.7	23.4	24.3
8.0	7.4	6.7	5.8
36	54	66	75

25.8	25.1	23.7	22.4	21.9
4.3	5.0	6.4	7.7	8.2
75	65	51	39	30

22.6	21.2	19.8	19.5	19.9	20.0	19.9	19.3	21.2	22.3
75	8.9	10.3	10.6	10.2	10.1	10.2	10.8	8.9	7.8
34	30	24	23	10		10	22	32	45

22.9	23.7	25.0
7.2	6.4	5.1
48	60	75

23.6	23.0
6.5	7.1
75	60

22.5	21.4	20.8	20.3	20.5	20.59	20.5	20.0	21.2	24.3
6.5	7.6	8.2	8.7	8.5	8.43	8.5	9.0	7.8	4.7
31	28	23	22	10		10	21	32	34

24.1	24.7	25.1
4.9	4.3	3.9
36	44	53

22.6	23.2	23.5	23.8
6.4	5.8	5.5	5.2
75	61	49	40

Sta	+	π	-	Elev
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		929.02		
--	--	--------	--	--

52+19				
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✓				
---	--	--	--	--

+40				
-----	--	--	--	--

✓				
---	--	--	--	--

BM	4.88	930.20	3.70	925.32 (925.32)
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+46				
-----	--	--	--	--

✓				
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FK
JS
FS
LB
BZ

Sept. 4, 1963 60
Sept 5, 1963 Rt.

1.

21.5	21.1	20.5	20.9	21.1	21.0	20.4	20.5	21.0
7.5	7.9	8.5	8.1	7.9	8.0	8.6	8.5	8.0
29	25	22	10		10	21	24	29

25.0	25.4	25.7	26.2	26.3	23.8	24.5	25.3	25.8	21.3
4.0	3.6	3.3	2.8	2.7	5.2	4.5	3.7	3.2	7.7
35	46	60	71	75	75	63	54	44	37

21.0	20.7	21.1	21.4	21.6	21.5	20.7	21.0	22.3
8.0	8.3	7.9	7.6	7.4	7.5	8.3	8.0	6.7
24	23	20	10		10	22	24	29

25.4	25.8	26.5	27.5	24.7	25.2	25.9	22.8	22.4
3.6	3.2	2.5	1.5	4.3	3.8	3.1	6.2	6.6
34	46	56	75	75	64	57	48	40

Spike in Transformer Pole 88 Lt Sta 52+50

21.9	21.0	21.3	21.6	21.8	21.7	21.1	20.5	20.2
8.3	9.2	8.9	8.6	8.4	8.5	9.1	9.7	10.0
28	26	23	10		10	26	35	52

21.8	23.6	23.9	24.4	20.3	20.2
8.4	6.6	6.3	5.8	9.9	10.0
34	52	66	75	75	66

Sta + π - Elev.

930.20

52+52

+72.95 $\pm$ B

v

+85

+94

v

Sept. 5, 1963

11

£

RT 61

i3.0	i2.5	i2.1	i2.5	i2.9	i2.9	i2.8	i2.5	i2.8	i2.0
7.2	7.7	8.1	8.7	8.3	8.3	8.4	8.7	8.4	8.2
75	56	43	22	10	✓	10	25	57	75

i2.6	i2.5	i2.9	i2.3	i2.3	i2.3	i2.5	i2.6	i2.9
6.6	7.7	8.3	7.9	7.81	7.9	7.7	7.6	7.5
61	38	21	10	✓	10	29	47	64

i3.0	i2.9	i2.3	i2.5	i2.4	i2.5	i2.6	i2.6
7.2	5.3	3.9	2.7	7.8	2.7	7.6	7.6
75	100	150	200	200	150	100	75

i2.8	i2.2	i2.6	i2.1	i2.5	i2.6	i2.5	i2.5	i2.5	i2.6
6.4	7.0	7.6	8.1	7.7	7.6	7.7	7.7	7.7	7.6
75	58	39	23	10	✓	10	25	40	55

i2.9	i2.8	i2.5	i2.1	i2.8	i2.7	i2.4	i2.2	i2.0
7.3	7.4	7.7	7.5	7.4	7.5	7.8	8.0	8.2
61	47	27	10		10	25	33	45

i3.3
6.9
75

✓

i2.7 i2.8
8.5 8.4
75 60

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		930.20		
--	--	--------	--	--

53				
----	--	--	--	--

✓				
---	--	--	--	--

+10				
-----	--	--	--	--

✓				
---	--	--	--	--

+33				
-----	--	--	--	--

✓				
---	--	--	--	--

Sept. 5, 1963 62

21

RT

24.4	23.5	22.5	22.9	22.95	22.8	22.4	22.1	21.7
5.8	6.7	7.7	7.3	11.25	7.4	7.8	8.1	8.5
50	37	24	10	10	10	20	28	39

16.95
7.25 ✓

24.3	24.6
5.9	5.6
63	75

21.1	21.4
9.1	8.8
75	60

24.3	22.9	22.1	23.1	23.2	23.0	22.6	22.7	22.9
5.9	7.3	7.5	7.1	7.0	7.2	7.6	7.5	7.3
40	28	19	10		10	19	22	28

25.0	25.2	25.5
5.2	5.0	4.7
52	66	75

22.1	22.4	23.0
8.1	7.8	7.2
75	65	46

24.0	22.8	23.4	23.5	23.6	23.5	22.9	22.8	24.0
6.2	7.4	6.8	6.7	6.6	6.7	7.3	7.4	6.2
30	24	14	10		10	19	21	27

24.7	25.7	25.8	26.0
5.5	4.5	4.4	4.2
38	54	65	75

23.5	23.4	24.3
6.7	6.8	5.9
75	55	37

Sta + π - Elev.

930.20

53+50

✓

54

✓

+50

14

Sept 5, 1963 63
BT

24.2	23.2	23.7	23.7	23.84	23.8	23.3	23.1	24.2
6.0	7.0	6.5	6.5	6.36	6.4	6.9	7.1	6.0
30	23	12	10		10	18	22	29

25.1	25.5	25.9	26.2
5.1	4.7	4.3	4.0
37	44	59	75

23.7	24.1	24.1
6.5	6.1	6.1
75	65	45

25.5	25.0	23.7	24.4	24.54	24.4	23.9	23.8	24.7
4.7	5.2	6.5	5.8	5.66	5.8	6.3	6.4	5.5
38	31	22	11		10	18	21	28

25.8	26.0	26.1
4.4	4.2	4.1
54	67	75

24.2	24.4	24.0
6.0	5.8	6.2
75	57	40

24.1	23.8	24.6	25.0	25.1	24.9	24.8	24.0	24.1
5.5	6.4	5.6	5.2	5.1	5.3	5.4	6.2	5.5
30	22	17	10		10	12	20	23

25.7	26.0	26.1	26.2
4.5	4.2	4.1	4.0
42	56	65	75

24.0	24.7	24.6
6.2	5.5	5.6
75	50	32

Sta	+	π	-	Elev.
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		930.20		
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55				
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✓				
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TP	4.96	930.76	4.40	925.80
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Iron

+40				
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✓				
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+71				
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Lt

Sept 5, 1963 64

Rt

25.0	25.8	25.1	25.4	25.56	25.4	25.3	24.8	25.8
5.2	6.4	5.1	4.8	4.69	4.8	4.9	5.4	4.4
30	23	15	10		10	12	18	24

25.6	25.6	25.9	26.2
4.6	4.6	4.3	4.0
35	50	63	75

✓

24.7	24.8	25.4
5.5	5.4	4.8
75	61	44

25.2	24.1	24.9	25.5	25.7	25.9	25.9	25.4	25.0	25.8
5.6	6.7	5.9	5.3	5.1	4.9	5.1	5.4	5.8	5.0
30	23	18	13	11		10	16	21	25

26.2	26.2	26.2
4.6	4.6	4.6
48	64	75

✓

25.2	25.8	25.9
5.6	5.0	4.9
75	59	40

25.9	24.2	25.7	25.8	26.0	25.9	25.6	25.8	25.6
4.9	6.6	5.1	5.0	4.8	4.9	5.2	5.0	5.2
34	23	15	11		10	16	23	40

26.4	25.9	25.8
4.4	4.9	5.0
43	62	75

✓

25.2	25.4
5.6	5.4
75	60

Sta + Δ - Elev

930.76

55+86

✓

56 Aprox $\pm$ St. Rth

✓

+16

✓

11

Sept 5, 1963

Rt 65

25.7	24.1	25.7	25.9	26.1	26.0	25.3	24.8	24.5
5.1	6.7	5.1	4.9	4.7	4.8	5.5	6.0	6.3
32	23	14	11		10	24	38	55

26.5	25.7	25.4
4.3	5.1	5.4
43	59	75

24.3
6.5
75

26.0	24.3	25.7	25.9	26.05	25.9	25.4	24.9	24.5
4.8	6.5	5.1	4.9	4.71	4.9	5.4	5.9	6.3
34	23	14	10		11	24	40	55

26.0	25.8	25.5
4.7	5.0	5.3
46	61	75

22.8	22.6	23.77	24.2
8.0	8.2	6.99	6.6
200	150	104	75

MH

26.2	24.2	25.7	26.0	26.1	25.8	25.2	24.9	24.4
4.6	6.6	5.1	4.8	4.7	5.0	5.6	5.9	6.4
36	23	13	10		11	23	32	50

25.7	25.6	25.4
5.1	5.2	5.4
53	68	75

24.1
6.7
75

Sta + π - Elev.

930.76

56+20

✓

+31

✓

+79 on Edge Ent Rt

✓

LT

✓

RT

26.2	24.3	25.1	25.9	26.1	25.9	25.3	25.1	25.4
4.6	6.5	5.1	4.9	4.7	4.9	5.5	5.7	5.4
35	23	14	10		10	20	34	41

25.1	25.8	25.5
5.1	5.0	5.3
50	63	75

✓

24.1	25.1
6.1	5.7
75	50

26.0	24.2	25.1	26.0	26.1	25.9	25.4	25.1	25.6
4.8	6.6	5.1	4.8	4.7	4.9	5.4	5.7	5.2
46	23	14	10		11	19	21	24

25.8	25.1	25.5
5.0	5.1	5.3
51	65	75

✓

24.8	24.9	25.3
6.0	5.9	5.5
75	63	40

25.6	25.1	24.2	25.1	25.8	26.0	25.1	25.5	25.6	25.6
5.2	5.1	6.6	5.1	5.0	4.8	5.1	5.3	5.3	5.2
56	38	24	14	10		11	17	28	45

25.6
5.4
75

✓

25.6	25.6
5.2	5.2
75	60

Sta + π - Elev.

930.76

56+95 N. side Ent Rt.

✓

57

✓

+42

Sept 5, 1963 67

11

51

25.1	24.3	25.6	25.8	25.91	25.7	25.4	25.5	25.6
5.1	6.5	5.2	5.0	4.85	5.1	5.4	5.3	5.2
34	23	13	10		12	21	28	50

26.2	25.4	25.6
4.6	5.4	5.2
47	64	75

25.8
50
75

✓

26.0	25.8	24.2	25.6	25.8	25.90	25.61	25.5	24.2	25.3
4.8	5.0	6.6	5.2	5.0	4.86	5.15	5.3	5.6	5.5
50	34	24	13	10		12	18	23	27

✓

25.4	25.5
5.4	5.3
63	75

25.8	25.86	25.1	25.6
5.0	4.90	5.1	5.2
75	Walk	60	45
	63		

25.9	24.1	25.2	25.6	25.7	25.5	25.2	24.6	24.5
4.9	6.7	5.6	5.2	5.1	5.3	5.6	6.2	6.3
34	23	15	10		11	17	22	27

26.0	25.9	25.8
4.8	4.9	5.0
46	59	75

✓

25.8	25.6	25.5	24.9
5.0	5.2	5.3	5.9
75	69	59	35

Sta	+	π	-	Elev
-----	---	-------	---	------

		930.76		
--	--	--------	--	--

57+75				
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✓				
---	--	--	--	--

+93				
-----	--	--	--	--

✓				
---	--	--	--	--

58				
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Sept. 5, 1963

68

LT

£

BT

25.1	23.9	24.8	25.3	25.4	25.2	25.0	22.7	22.2
5.7	6.9	6.0	5.5	5.4	5.6	5.8	8.1	8.6
31	23	17	10		11	15	25	37

24.9	24.9	25.3
5.9	5.9	5.5
44	58	75

✓

22.2	22.9
8.6	8.4
75	59

25.0	23.6	24.5	25.1	25.3	25.1	24.8	22.6	22.1
5.8	7.2	6.3	5.7	5.5	5.7	6.0	8.2	8.7
34	24	18	10		12	16	28	40

24.7	24.9	24.8
6.1	5.9	6.0
45	59	75

✓

21.7	21.8
9.2	9.0
75	60

24.9	23.6	24.2	25.1	25.22	25.0	24.6	25.3	22.8
5.9	7.2	6.6	5.7	5.54	5.8	6.2	7.5	8.0
35	24	19	10		12	17	26	45

24.9	24.7	24.8
5.9	6.1	6.0
46	59	75

✓

21.5	22.4
9.3	8.4
75	64

Sta	+	π	-	Elev
-----	---	-------	---	------

		930.76		
--	--	--------	--	--

58+32				
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✓				
---	--	--	--	--

+60				
-----	--	--	--	--

✓				
---	--	--	--	--

59				
----	--	--	--	--

✓				
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T.P.	1.29	927.22	4.83	925.93
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B.M.	1.95	927.22	1.95	925.27
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Lt

Sept. 5, 1963 69
BT

25.2	23.9	24.2	24.8	24.91	24.7	24.4	23.8	25.4
5.6	6.9	6.6	6.0	5.85	6.1	6.4	7.0	5.4
32	22	19	10		11	17	21	27

24.8	24.5	24.8
6.0	6.3	6.0
48	62	75

✓

26.0	26.0	26.0
4.8	4.8	4.8
75	60	45

24.9	25.2	23.7	24.0	24.4	24.6	24.4	24.1	23.7	25.5
5.9	5.6	7.1	6.8	6.4	6.2	6.4	6.7	7.1	5.3
50	31	22	19	10		12	16	20	27

✓

24.6	24.6
6.2	6.2
67	75

26.3	26.2	26.0
4.5	4.6	4.8
75	55	38

24.4	24.0	23.5	24.0	24.17	24.0	23.9	23.5	24.9
6.4	6.8	7.3	6.8	6.59	6.8	6.9	7.3	5.9
36	28	20	10		12	19	23	27

24.6	24.9	25.0
6.2	5.9	5.8
52	65	75

✓

25.9	25.6	25.3
4.9	5.2	5.5
70	55	37
40		

Sta	+	π	-	Elev.
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		927.22		
--	--	--------	--	--

59+16	±	Ent	Rt	
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✓				
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+25	on	Ent/Lt.		
-----	----	---------	--	--

✓				
---	--	--	--	--

+35				
-----	--	--	--	--

✓				
---	--	--	--	--

Sept. 5, 1963 70
BT

1f

24.6	24.4	24.2	23.8	24.0	23.9	24.2	24.3	24.9
2.6	2.8	3.0	3.4	3.2	3.3	3.0	2.9	2.3
56	43	30	10		12	21	36	55

BT
Ent

24.9
2.3
67

25.4
1.81
67.5

Sen. sta walk

✓

25.4
1.8
75

24.8	24.7	24.3	23.8	23.95	23.8	23.6	24.5	25.1
2.4	2.5	2.9	3.4	3.27	3.4	3.6	2.7	2.1
59	47	31	10		11	21	30	46

Edge BT

✓

24.9
2.3
68

25.40
1.82
68.5

Walk

25.4
1.8
75

25.2
2.0
62

24.9	24.9	24.7	24.3	23.8	23.8	23.6	23.4	22.3	22.7
2.3	2.3	2.5	2.9	3.4	3.4	3.6	3.8	4.9	4.5
75	66	50	29	10		10	18	23	28

✓

22.5
4.7
75

22.7
4.5
60

22.7
4.5
45

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		927.22		
--	--	--------	--	--

59+56				
-------	--	--	--	--

✓				
---	--	--	--	--

+80				
-----	--	--	--	--

✓				
---	--	--	--	--

BM	2.95	928.22	1.95	925.27
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60				
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✓				
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Sept. 5, 1963

71

14

R4

24.4	22.6	23.3	23.6	23.6	23.4	23.0	22.6	22.0
2.8	4.6	3.9	3.6	3.6	3.8	4.2	4.6	5.2
29	20	16	10		10	15	18	22

24.40	24.64	24.73	24.7	21.2	21.3	21.8	22.2
282	268	249	25	6.0	5.9	5.4	5.0
32	45	61	75	75	60	42	28

concrete

22.5	22.5	23.4	23.6	23.50	23.19	22.4	21.9	22.2
4.7	4.7	3.8	3.6	3.72	4.03	4.8	5.3	5.0
21	19	16	10		10	18	21	27

23.0	24.3	24.30	24.43	24.61	24.59
4.2	2.9	2.92	2.79	2.61	2.63
24	30	concrete			
32	48	61	75		

20.9	21.1	21.7
6.3	6.1	5.5
75	60	41

24.5	24.5	24.4	24.1	23.6	23.42	23.0	22.5	21.5	22.6
3.7	3.7	3.8	4.1	4.6	4.80	5.2	5.7	6.7	5.6
75	58	44	33	10		10	18	23	27

21.4	21.8	21.9
6.8	6.4	6.3
75	55	40

Sta + π - Elev

928.22

60+27.89

✓

+50

✓

+85

✓

FL 24" SCP RT 11.20 917.02

14

Sept. 5, 1963 72
BT

22.6	22.6	23.5	23.5	23.3	22.8	22.7	20.8	22.1
5.6	5.6	4.7	4.7	4.9	5.4	5.5	7.4	6.1
22	20	16	11		12	18	25	32

23.5	23.9	23.9	24.1	24.1
4.7	4.3	4.3	4.1	4.1
26	39	54	62	75

21.6	21.8
6.6	6.4
75	50

23.5	22.3	22.3	23.8	23.7	23.30	22.7	22.5	20.3	20.6	20.9
4.7	5.9	5.9	4.4	4.5	4.92	5.5	5.7	7.9	7.6	7.3
25	20	18	16	10		12	19	26	31	51

23.8	23.7	23.5	22.6	22.8
4.4	4.5	4.7	5.6	5.4
38	52	61	71	75

21.2
7.0
75

21.2	20.1	19.64	23.5	23.7	23.2	22.4	22.2	18.4	17.8
7.0	8.1	8.58	4.7	4.5	5.0	5.8	6.0	9.8	10.4
23	22	FL24"	16	10		11	19	31	42
		18.5							

22.7	21.8	21.9	22.9
5.5	6.4	6.3	5.3
29	37	42	49

17.6	17.8	17.8
10.6	10.9	10.4
75	65	55

23.8	23.3
4.4	4.9
71	55

Sta + π - Elev

928.22

61

✓

+30

✓

TP 5.25 928.81 4.66 923.56

+50

✓

FK
JS
LB
BZ

LT

Sept. 5, 1963
Sept. 6, 1963 RY

73

23.7	22.9	23.4	23.6	23.15	22.3	22.2	18.2	17.8
4.5	5.3	4.8	4.6	5.07	5.9	6.0	10.0	10.4
31	23	18	10		12	18	25	40

23.4	23.7	23.3
4.8	4.5	4.9
41	58	75

✓

17.7	17.7
10.5	10.5
75	55

23.4	23.8	23.9	23.8	23.2	22.5	22.4	18.6	21.9
4.8	4.4	4.3	4.4	5.0	5.7	5.8	9.6	6.3
51	36	23	10		11	18	29	38

22.9	22.5	23.0	23.2
5.3	5.7	5.2	5.0
56	63	69	75

MH West Edge

✓

22.1	22.3	22.3
6.1	5.9	5.9
75	67	53

23.6	24.0	24.1	24.0	23.41	22.7	22.4	18.8	21.0
5.2	4.8	4.7	4.8	5.40	6.1	6.4	10.0	7.8
40	27	13	10		11	18	27	32

4

23.3	22.3	22.8	23.4
5.5	6.5	6.0	5.4
48	54	58	70

✓

23.0	23.3	22.9
5.8	5.5	5.9
63	50	39

23.6
5.2
75

23.2
5.6
75

Sta	+	π	-	Elev.
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		928.81		
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61+77				
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✓				
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62				
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✓				
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		1.25		
		6.15		
		5.32		

+33				
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Lt

£

Rt

74

23.4	23.8	24.0	24.1	23.6	22.9	22.3	21.4	19.0
5.4	5.0	4.8	4.7	5.2	5.9	6.5	7.4	9.8
39	34	20	10		12	19	24	28

22.3	21.4	21.5
6.5	7.4	7.3
47	63	75

✓

23.5	23.7	23.3	19.5
5.3	5.1	5.5	9.3
75	58	40	30

23.6	23.8	24.1	24.2	23.65	22.9	22.5	22.0	20.0
5.2	5.0	4.7	4.6	5.16	5.9	6.3	6.8	8.8
54	44	23	10		12	20	23	28

23.2	21.44	23.3
5.6	7.37	5.5
64	FL 15 CM	75
	68	

✓

25.9	26.4	26.4	26.0	23.2	19.4
2.9	2.4	2.4	2.8	5.6	8.9
75	69	59	45	39	32

22.8	23.1	23.8	24.2	23.16	22.9	22.6	21.3	20.50
6.0	5.7	5.0	4.6	5.05	5.9	6.2	6.5	8.31
45	28	20	10		12	17	22	26

FLC 1/4

23.2	23.2
5.6	5.6
66	75

✓

25.5	24.3	22.9	21.5
3.3	4.5	5.9	7.3
75	54	38	27

Sta + π - Elev

928.81

62+50

✓

+ 71.88 P.T.

✓

+ 76

8.20 920.61

63

✓

Sept. 6, 1963

75

LT

RT

22.5	23.4	23.9	24.2	23.83	23.1	22.8	23.4	24.3
6.3	5.4	4.9	4.6	4.98	5.7	6.0	5.4	4.5
37	24	17	10		11	19	35	54

in Ent

22.1	22.3	22.4
6.7	6.5	6.4
49	58	75

25.2
3.6
75

22.4	23.5	23.9	24.2	23.91	23.3	23.1	23.5	24.2
6.4	5.3	4.9	4.6	4.90	5.5	5.7	5.3	4.6
29	21	17	10		12	19	29	38

in Ent

21.5	21.6	22.0	22.0
7.3	7.2	6.8	4.8
43	55	68	75

FL Calc. RT

25.1	25.2
3.1	3.6
75	56

21.8	23.2	23.8	24.1	23.46	23.46	23.1	20.1	20.1
7.0	5.6	5.0	4.7	4.85	5.35	5.7	8.7	8.7
32	24	19	10		11	20	25	28

20.8	21.2	21.6
8.0	7.6	7.2
50	59	75

26.4	26.1	25.7	21.6
24	2.7	3.1	7.2
61	45	41	32

26.8
2.0
75

Sta	+	x	-	Elev
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		928.81		
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63+11				
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			2.35	
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				926.46
--	--	--	--	--------

+36				
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			2.28	
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				926.53
--	--	--	--	--------

+50				
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✓				
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64				
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✓				
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✓				
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BM				
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			2.62	
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				926.19
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Lt

Sept. 6, 1963

BT 76

Concrete Pump

1.44
88

Area

1.49
88

21.5	23.3	23.9	24.06	24.12	23.9	23.4	20.7	20.7
7.3	5.5	4.9	4.75	4.69	4.9	5.4	8.1	8.1
35	25	17	10		10	20	26	29

20.1	20.7	21.0	21.0	✓	21.0	26.8	26.5	25.5	21.9
8.7	8.1	7.8	7.8		1.8	2.0	2.3	3.3	6.9
52	59	70	75		75	63	47	40	32

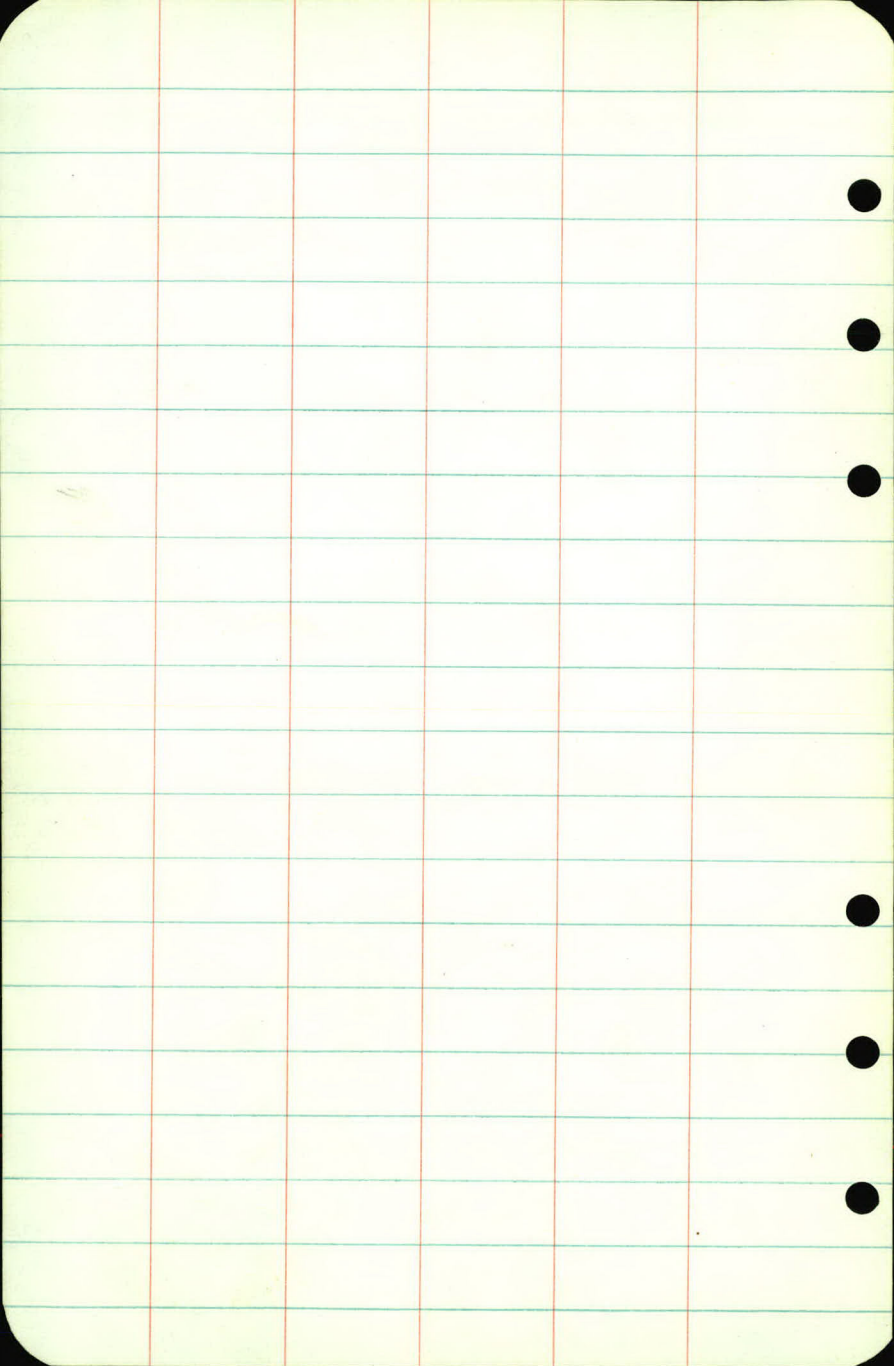
21.4	23.2	23.6	23.88	24.05	23.95	23.5	22.3
7.4	5.6	5.2	4.93	4.76	4.86	5.3	6.5
34	24	20	10		10.5	20	20

19.9	20.8	20.9
8.9	8.0	7.9
52	61	75

25.3	22.7	20.9	20.9
3.5	6.1	7.9	7.9
41	33	30	26

25.9	26.4	26.8
2.9	2.4	2.0
48	63	75

Top N.W. Cor Metal Base Sign 45' BT Sta 64+60



64400 is x-sectioned 926,19

X-Sections

Sta	+	π	-	Elev.
BM	8.71	934.90		926.19

64+25

✓

✓

+38

✓

+64

Sept. 10, 1963

L1

E

BT

19.7	21.4	23.1	23.5	23.97	23.9	23.5	23.0	22.4
152	135	11.8	11.4	10.93	11.0	11.4	11.9	12.5
52	31	23	19		10	19	23	27

20.7	20.8	20.9
14.2	14.1	14.0
59	63	75

25.6	26.9	22.8	21.1	19.9
9.3	8.0	12.1	13.8	15.0
48	41	35	33	FL 30" CH 31

26.1	26.9
8.8	8.0
60	75

19.7	21.3	22.8	23.4	24.0	23.8	23.7	24.2	25.5
152	136	12.1	11.5	10.9	11.1	11.2	10.7	9.4
54	32	25	20		10	18	29	50

20.7	20.8
14.2	14.1
59	75

27.8	26.6
7.1	8.3
75	68

19.4	20.8	22.8	23.5	24.1	24.0	23.8	24.0	25.1
155	141	12.1	11.4	10.8	10.9	11.1	10.9	9.8
54	38	25	20		12	20	31	45

20.5	20.8
14.4	14.1
59	75

30.9	26.6
4.0	8.3
75	60

Sta	+	π	-	Elev
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C		934.90		
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64+73				
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✓				
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65				
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✓				
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T.P.	7.52	930.42	12.00	922.90
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+34				
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Sept. 10, 1963

Lt

Rt

19.7	21.1	22.7	23.5	24.1	24.0	23.7	22.8	21.12
15.2	12.8	12.2	11.4	10.8	10.9	11.2	12.1	13.78
54	34	25	19		11	19	28	32
								FL 30" OM

20.6	20.7		34.2	33.6	31.5	27.3	26.2	24.9	22.8
14.3	14.2		0.7	1.3	3.4	7.6	8.7	10.0	12.1
59	75		House 101	80	75	63	54	41	35

19.6	21.3	22.9	23.6	24.28	24.2	23.9	22.3	21.1
15.3	13.6	12.0	11.3	10.62	10.7	11.0	12.6	13.8
50	33	26	19		12	21	29	31

19.7	20.5	20.6	32.5	32.1	27.3	26.2	22.2	21.1
15.2	14.4	14.3	24	2.8	7.6	8.7	12.7	13.8
54	59	75	75	72	60	44	35	34

19.5	20.2	22.9	23.6	24.4	24.5	24.5	22.4	20.8
10.9	10.2	7.5	6.8	6.0	5.9	5.9	8.0	9.6
52	42	27	20		12	22	29	33

20.4	20.7		30.2	27.5	26.0	22.4	20.8
10.0	9.7		0.2	2.9	4.4	8.0	9.6
58	75		63	57	44	37	36

30.4
0.0
70

30.8
+ 0.5
75

Sta	+	π	-	Elev.
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		930.42		
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65+56				
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✓				
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+63				
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✓				
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+79				
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Sept, 10, 1963

Lt

Rt

19.9	21.0	23.0	23.6	24.5	24.5	24.3	22.8	22.23
10.5	9.4	7.4	6.8	5.9	5.9	6.1	7.6	8.19
48	38	27	21		12	24	32	FL 30" CM
								34
19.7	20.4	20.6		29.4		28.9	26.0	24.7
10.7	10.0	9.8		1.0	1.5	4.4	5.7	7.5
52	58	75		75	60	52	41	38

19.6	20.3	22.7	23.7	24.6	24.6	24.4	24.5	25.3	26.2
10.8	10.1	7.7	6.7	5.8	5.8	6.0	5.9	5.1	4.2
52	45	30	21		12	23	34	50	65

20.3	20.6							27.0	
10.1	9.8							3.4	
58	75							75	

19.6	20.2	23.1	23.7	24.6	24.7	24.5	24.7	25.8
10.8	10.2	7.3	6.7	5.8	5.7	5.9	5.7	4.6
52	48	28	21		12	22	36	60

20.3	20.5							26.9
10.1	9.9							3.5
58	75							75

Sta + π - Elev.

930.42

65+84

✓

66

✓

+20

Sept. 10, 1963

BT ?

11

19.6	20.1	23.0	23.7	24.7	24.6	24.5	23.0	21.40
10.8	10.3	7.4	6.7	5.7	5.8	5.9	7.4	9.02
53	45	28	22		12	21	32	35

FL 30' CM

20.2	20.5
10.2	9.9
58	75

26.6	26.3	25.4	23.2
3.8	4.1	5.0	7.2
75	67	51	38

19.4	20.4	22.9	23.8	24.68	24.7	24.2	22.6	20.9
11.0	10.0	7.5	6.6	5.74	5.7	6.2	7.8	9.5
53	43	29	22		12	23	32	34

20.2	20.4
10.2	10.0
58	75

25.3	25.7	25.3	22.3	20.9
5.1	4.7	5.1	8.1	9.5
75	64	50	39	37

19.9	22.5	23.7	24.3	24.8	24.6	24.2	23.2	21.0
10.5	7.9	6.7	6.1	5.6	5.8	6.2	7.2	9.4
45	31	25	15		12	21	30	34

19.2	20.1	20.4
11.2	10.3	10.0
52	58	75

24.9	25.2	25.0	22.3	21.0
5.5	5.2	5.4	8.1	9.4
75	66	51	39	37

Sta	+	π	-	Elev.
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		930.42		
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66+60				
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	✓			
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TP	4.59	927.71	7.30	923.12
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67				
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	✓			
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+03				
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FK
JS
FS

11

Sept. 10, 1963
Oct. 2, 1963 RT 6

19.6	23.0	23.8	24.4	24.8	24.5	24.6	23.2	21.47
10.8	7.4	6.6	6.0	5.6	5.9	5.8	7.2	8.95
35	31	25	16		12	31	34	36

FL

19.2	20.1	20.4	25.3	25.1	24.7	23.4
11.2	10.3	10.0	5.1	5.3	5.7	7.0
52	58	75	75	65	50	40

Top W.F. SCP Cn/n

20.6	23.0	23.8	24.5	24.80	25.1	25.1	24.8	24.5
7.1	4.7	3.9	3.2	2.91	2.6	2.6	2.9	3.2
43	33	26	14		15	23	32	40

19.1	19.9	20.2	20.5	26.2	26.0	25.6	25.1
8.6	7.8	7.5	7.2	1.5	1.7	2.1	2.6
52	56	61	81	94	75	58	46

20.6	23.0	23.8	24.3	25.35	24.9	25.1	24.9	23.2	21.88
7.1	4.7	3.9	3.2	2.36	2.8	2.6	2.8	4.5	5.83
43	33	26	14	Median 2		16	25	34	FL Cn/n 37

19.1	19.9	20.2	20.5	26.0	25.3	24.1
8.6	7.8	7.5	7.2	1.7	2.4	3.6
52	56	61	81	75	50	46

Sta	+	π	-	Elev.
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		927.71		
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67+50				
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✓				
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+66 ⁺				
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68 -				
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✓				
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✓				
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Oct. 7, 1963

LH

♀

RY

c

23.7	24.3	24.6	25.15	25.33	24.7	25.0	24.5	22.5
4.0	3.4	3.1	2.56	2.38	3.0	2.7	3.2	5.2
28	18	5	4		1	16	27	35

22.3	20.0	18.6	18.8	20.1	20.0	25.0	24.5	22.8
5.4	7.7	9.1	8.9	7.6	7.7	2.7	3.2	4.9
36	44	49	51	57	75	75	63	50

16.84

18.00

10.87

9.71

Plugged Pipe (CM)

23.4	24.1	24.5	25.07	25.20	25.23	24.8	25.1	24.7
4.3	3.6	3.2	2.64	2.51	2.48	2.9	2.6	3.0
28	21	5	4		1	2	18	29

22.2	19.7	19.5	19.5	24.4	23.0	22.5	22.9
5.5	8.0	9.2	9.2	3.3	4.7	5.2	4.8
36	44	51	52	75	61	43	37

19.8	20.1
7.9	7.6
75	59

Sta	+	π	-	Elev.
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		927.71		
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68+50				
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✓				
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✓				
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69				
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✓				
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✓				
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Oct. 7, 1963

£

d

23.1	23.7	24.4	24.91	25.11	25.18	24.6	25.1
4.6	4.0	3.3	2.80	2.60	2.53	3.1	2.6
30	22	6	5		2	3	20

22.2	20.5	19.3	18.8	18.8	23.7	23.1	22.6	23.5	24.7
5.5	7.2	8.4	8.9	8.9	4.0	4.6	5.1	4.2	3.0
36	43	48	52	53	75	58	44	36	31

19.6	20.3	19.2
8.1	7.4	8.5
75	61	55

23.0	23.6	24.1	24.75	24.85	24.89	24.4	25.0	24.5
4.7	4.1	3.6	2.96	2.86	2.82	3.3	2.7	3.2
31	21	6	5		3	4	22	32

21.4	19.2	18.4	18.4	23.9	23.2	22.7	23.3
6.3	8.5	9.3	9.3	3.8	4.5	5.0	4.4
41	50	56	57	75	62	47	39

19.4	19.8	18.8
8.3	7.9	8.9
75	66	61

Sta + π - Elev.

927.71

69+50

✓

T.P. 1.49 926.42 2.78 924.93

70

✓

+50

✓

Oct. 31 1963

LT

RT

E

22.8	23.3	24.0	24.53	24.9	24.90	24.3	24.8	24.4
4.9	4.4	3.7	3.18	2.8	2.81	3.4	2.9	3.3
32	26	7	6		4	5	24	36

21.4	18.2	17.3	17.6	✓	24.1	23.8	23.1
6.3	9.5	10.4	10.1		3.6	3.9	4.6
42	56	67	75		75	61	44

22.9	23.2	23.7	24.42	24.8	24.68	24.2	24.8	24.6
3.5	3.2	2.7	2.00	1.6	1.74	2.2	1.6	1.8
33	23	7	6		5	6	27	40

21.7	19.6	18.2	17.1	✓	23.7	23.1	23.2
4.7	6.8	8.2	9.3		2.7	3.3	3.2
44	53	60	75		75	51	47

22.3	22.6	23.1	23.5	24.00	24.5	24.43	23.9	24.3	24.7
4.1	3.8	3.3	2.9	2.42	1.9	1.99	2.5	2.1	1.7
37	33	22	8	7		6	7	24	37

21.0	19.0	16.4	16.0	✓	23.5	23.8	23.5	24.3
5.4	7.4	10.0	10.4		2.9	2.6	2.9	2.1
45	55	69	75		75	59	53	48

Sta	+	π	-	Elev.
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		926.42		
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70+63				
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✓				
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✓				
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+68				
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		9.54		
--	--	------	--	--

			16.88	
--	--	--	-------	--

+83				
-----	--	--	--	--

✓				
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BM				
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	4.46			
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		928.10		
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			2.78	
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				923.64
--	--	--	--	--------

+93				
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			4.17	
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				23.93
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+94				
-----	--	--	--	--

			4.8	
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				23.3
--	--	--	--	------

Oct. 7, 1963

Lt

£

BT

F

22.5	23.0	23.4	23.98	24.4	24.31	23.8	24.3	24.7
3.9	3.4	3.0	2.54	2.0	2.11	2.6	2.1	1.7
34	21	8	7		6	7	26	42

22.0	20.7	18.4	16.88	23.8	24.0	23.7	24.3
4.4	5.7	8.0	9.56	2.6	2.4	2.7	2.1
40	49	56	62	75	63	57	53

Top Apron

14.8	15.2	15.9
11.6	11.2	10.5
75	72	68

Top 15" CM 65 ± Lt

22.3	22.8	23.2	23.78	24.3	24.24	23.7	24.2	23.5
4.1	3.6	3.2	2.64	2.1	2.18	2.7	2.2	2.9
37	24	8	7		7	8	30	43

✓

21.7	20.65	21.5	20.5	19.16	19.4	24.0	24.2	24.4	24.7
4.7	5.77	4.9	5.9	6.8	7.0	2.4	2.2	2.0	1.7
50	Apron	56	61	70	75	75	72	60	50

53

£ cut 6

£

Sta + π - Elev

928.10

71

✓

+25

+35

+36

+45

6.15 21.95 $\neq$ Gutter

4.58 23.52 $\neq$ Carb

✓

+65

Oct. 7/1963

1+

2

RT

9

21.7	22.0	22.3	22.8	23.36	23.8	24.3	24.8	24.1
6.4	6.1	5.8	5.3	4.74	4.3	3.8	3.3	4.0
75	48	33	20		21	38	58	69

✓

24.3

3.8

75

35	22.0	21.3	22.0	22.5	23.1	23.4	24.0	24.6	24.9	24.6
26	6.1	6.8	6.1	5.6	5.0	4.7	4.1	3.5	3.2	3.5
	75	56	37	20		11	33	54	69	75

✓

22.0	22.3	22.7	23.14	23.8	23.75	23.3	23.6	24.1
6.1	5.8	5.4	4.96	4.3	4.35	4.8	4.5	4.0
33	22	8	7		7	8	26	40

✓

21.4	18.7	18.2	18.5
6.7	9.4	9.9	9.6
43	57	65	75

25.1

25.1

3.0

3.0

75

56

20.9	21.8	22.2	22.5	24.12	23.7	23.57	23.1	23.7	23.7
72	63	59	56	398	4.4	4.53	5.0	4.4	4.4
45	34	21	8	7		7	8	32	42

16.8 15.6

✓

25.6 25.2 23.2

11.3 12.5
63 752.5 2.9 4.9
75 62 47

Sta + π - Elev

928.10

72

✓

+50

✓

+82

13.89 14.21 Top Apron

73

✓

Oct. 7, 1963

14

2

81

1

20.5	21.6	22.3	22.83	23.1	23.30	22.8	23.4	23.1
7.6	6.5	5.8	5.27	5.0	4.80	5.3	4.7	5.0
45	34	8	7		7	8	33	41

17.0	15.2
11.1	12.9
58	75

26.8	26.7	26.4	22.7	22.4
1.3	1.4	1.7	5.4	5.7
75	69	66	50	47

20.7	21.3	21.7	21.8	22.48	22.9	22.81	22.3	22.5	22.7
7.4	6.8	6.4	6.3	5.62	5.2	5.29	5.8	5.6	5.4
45	33	21	8	7		7	8	21	33

17.2	15.2	14.6
10.9	12.9	13.5
57	66	75

20.1	27.2	25.6	21.8	20.8	22.5
0.0	0.9	2.5	6.3	7.3	5.6
71	69	65	53	49	43

20.3	21.1	21.5	21.6	22.16	22.6	22.32	21.8	22.0	22.2
7.8	7.0	6.6	6.5	5.94	5.5	5.78	6.3	6.1	5.9
45	34	21	8	7		7	8	20	33

16.8	14.5	14.1
11.3	13.6	14.0
59	71	75

27.7	25.6	20.4	19.7	21.6
0.4	2.5	7.7	8.4	6.5
75	70	58	51	44

Sta	+	x.	-	Elev.
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		928.10		
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73+42				
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✓				
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+49				
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		10.44	17.66	
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+77				
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✓				
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74				
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Oct. 7, 1963

Lt

£

Rt

20.3	21.0	21.4	21.4	21.99	22.4	22.1	21.5	21.7	21.1
7.8	7.1	6.7	6.7	6.11	5.7	6.00	6.6	6.4	7.0
44	33	21	8	7		7	8	33	44

17.3	15.05	14.5	13.5	✓	26.1	23.0	19.3	18.9
10.8	13.05	13.6	14.6		2.0	5.1	8.8	9.2
55	FL Apron	64	75		75	68	57	51
FL Apron 47 Rt								

20.2	21.1	21.4	21.5	22.04	22.5	22.08	21.5	21.4	21.4
7.9	7.0	6.7	6.6	6.06	5.6	6.02	6.6	6.7	6.7
46	33	21	8	7		7	8	22	33

18.0	16.6	16.5	✓	25.8	23.3	19.7	19.6	20.8
10.1	11.5	11.6		2.3	4.8	8.4	8.5	7.3
54	67	75		75	69	57	49	44

21.2	21.5	21.6	22.15	22.3	22.16	21.6	21.5	21.4
6.9	6.6	6.5	5.95	5.8	5.94	6.5	6.6	6.7
33	20	8	7		7	8	22	33

20.3	20.7	20.3	23.3	26.3	25.0	22.7	19.9	19.9	20.9
7.8	7.4	7.8	4.8	1.8	3.1	5.4	8.2	8.2	7.2
42	43	54	66	75	75	69	58	52	42

Sta	+	x	-	Elev.
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		928.10		
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74+29				
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29 ✓				
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53				
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87				
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+53				
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✓				
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+87				
-----	--	--	--	--

✓				
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T.P.				
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6.78				
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931.77				
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3.11				
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924.99				
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925.07				
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75				
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7.7				
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24.07 (24.1)				
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Oct. 7, 1963

LT

£

RT

22.16	21.3	21.7	21.9	22.41	22.8	22.42	21.9	21.7	21.5
5.94	6.8	6.4	6.2	5.69	5.3	5.68	6.2	6.4	6.6
C	G	20	8	7		7	8	22	34
40									

22.0	21.7
6.1	0.4
46	60

✓

24.0	21.4	20.3	20.3	21.2
4.1	6.7	7.8	7.8	6.9
78	66	53	48	43

21.7	22.0	22.2	22.75	23.3	22.74	22.3	22.0	21.9
6.4	6.1	5.9	5.35	4.8	5.36	5.8	6.1	6.2
32	20	8	7		7	8	23	34

21.6	22.49	23.09	28.00
6.5	5.61	5.01	0.10
G	C	48	59
40			

✓

23.8	22.2	20.8	21.6
4.3	5.9	7.3	6.5
75	68	57	43

22.4	22.7	22.8	23.43	23.9	23.37	22.8	22.7	22.5
5.7	5.4	5.3	4.67	4.2	4.73	5.3	5.4	5.6
32	21	8	7		7	8	22	33

22.2	23.07	23.0	28.1
5.9	5.03	5.1	0.0
G	C	49	60
40			

✓

27.9	22.8	23.15	22.3
0.2	5.3	4.95	5.8
63	48	C	G
40			

£

Sta	+	X	-	Elev.
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		931.77		
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75+32				
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✓				
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+55				
-----	--	--	--	--

✓				
---	--	--	--	--

+87				
-----	--	--	--	--

✓				
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26				
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	4.7	27.07	(27.1)	
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Oct. 7, 1963

24.94	23.3	24.20	24.4	24.7	24.8	23.1	31.72	25.5	25.8	25.1	25.2
683	8.5	7.57	74	71	70	8.7	005	6.3	6.0	6.7	6.6
41	32	48	22	43	43	52	62	51	47	C	C
40	40	40	40	40	40	40	40	40	40	40	40
24.0	23.5	23.5	24.2	23.0	25.3	21.7	25.5	25.5	25.4	25.1	25.2
76	8.0	8.3	76	8.8	6.5	10.1	6.0	6.0	5.8	5.8	6.6
32	21	21	32	50	32	75	8	22	8	22	33
24.4	23.8	23.5	24.4	24.1	25.7	26.29	26.32	25.5	25.8	25.1	25.2
74	7.8	7.57	74	7.7	6.1	5.48	5.45	6.3	6.0	5.8	6.6
22	8	48	22	57	8	7	7	51	47	C	C
8	7	58	8	68	75	7	7	7	8	22	33
24.6	24.0	27.5	24.6	26.0	25.7	26.6	26.32	25.5	25.8	25.1	25.2
72	7.8	4.3	72	5.8	6.1	5.2	5.45	6.3	6.0	5.8	6.6
8	7	64	8	75	75	7	7	7	8	22	33
25.18	24.53	30.0	25.18	25.1	26.29	26.6	26.32	25.5	25.8	25.1	25.2
6.59	7.24	1.8	6.59	6.7	5.48	5.2	5.45	6.3	6.0	5.8	6.6
6.3	6.9	1.8	6.3	7.5	7	7	7	7	8	22	33
25.5	24.9	30.0	25.5	25.1	26.29	26.6	26.32	25.5	25.8	25.1	25.2
7	7	1.8	7	7.5	5.48	5.2	5.45	6.3	6.0	5.8	6.6
3	9	1.8	3	7.5	7	7	7	7	8	22	33
6.59	7.24	1.8	6.59	6.7	5.48	5.2	5.45	6.3	6.0	5.8	6.6
7	7	1.8	7	7.5	7	7	7	7	8	22	33
25.18	24.53	30.0	25.18	25.1	26.29	26.6	26.32	25.5	25.8	25.1	25.2
6.59	7.24	1.8	6.59	6.7	5.48	5.2	5.45	6.3	6.0	5.8	6.6
6.3	6.9	1.8	6.3	7.5	7	7	7	7	8	22	33
25.5	24.9	30.0	25.5	25.1	26.29	26.6	26.32	25.5	25.8	25.1	25.2
7	7	1.8	7	7.5	5.48	5.2	5.45	6.3	6.0	5.8	6.6
3	9	1.8	3	7.5	7	7	7	7	8	22	33
6.59	7.24	1.8	6.59	6.7	5.48	5.2	5.45	6.3	6.0	5.8	6.6
7	7	1.8	7	7.5	7	7	7	7	8	22	33
25.18	24.53	30.0	25.18	25.1	26.29	26.6	26.32	25.5	25.8	25.1	25.2
6.59	7.24	1.8	6.59	6.7	5.48	5.2	5.45	6.3	6.0	5.8	6.6
6.3	6.9	1.8	6.3	7.5	7	7	7	7	8	22	33
25.5	24.9	30.0	25.5	25.1	26.29	26.6	26.32	25.5	25.8	25.1	25.2
7	7	1.8	7	7.5	5.48	5.2	5.45	6.3	6.0	5.8	6.6
3	9	1.8	3	7.5	7	7	7	7	8	22	33
6.59	7.24	1.8	6.59	6.7	5.48	5.2	5.45	6.3	6.0	5.8	6.6
7	7	1.8	7	7.5	7	7	7	7	8	22	33

Sta + π - Elev

931.77

76+11

✓

TP 7.01 934.69 4.09 927.68

10.47 938.17 5.25 32.82
For check only 0.87 937.30 (937.30)

+55

✓

+92

77

3.8 30.89

KK
FS
RB

Oct. 7, 1963
Oct 31, 1963

26.1	26.3	26.6	27.23	27.6	27.25	26.7	26.4	26.1
5.7	5.5	5.2	4.54	4.2	4.52	5.1	5.4	5.7
32	20	8	7		7	8	21	33

25.5	23.6	22.3
6.3	8.2	9.5
43	53	75

31.7	26.7	26.97	26.0
0.1	5.1	4.80	58
60	50	C	G

Top W. E Culvert Apron

40

B.M. Top N. End 24" SCP E. Approach TH#364 W.B.A.

24.9	26.8	27.8	28.4	29.03	29.2	29.0	28.4	27.7	27.1
9.8	7.9	6.9	6.3	5.66	5.5	5.69	6.3	7.0	7.6
53	44	33	8	7		7	8	33	43

24.2

10.5
75

29.10

5.7
75

27.8

6.9
61

25.43

28.5

29.2

29.8

30.48

30.6

30.36

29.8

29.0

28.6

9.26	6.2	5.5	4.9	4.21	4.1	4.33	4.9	5.7	6.1
49	43	33	8	7		7	8	34	44

FL Culv

25.6

25.4

27.4

26.9

26.09

9.1
55

9.3
75

7.3
75

7.8
52

8.60
49

FL Culvert

Sta + π - Elev.

934.69

77+40

✓

+80

✓

78

T.P. 3.45 938.55 0.09 934.60

Oct. 31, 1963

11

84 m

43	36	30.0	2.32	2.4	2.44	2.0	3.5	4.2
44	33	8	7	7	7	8	33	44
30.4	31.1	31.7	32.37	32.3	32.25	31.7	31.2	30.5

6.4	6.5					6.3	6.6	
54	75					75	58	
28.3	28.2					28.4	28.1	

2.8	2.0	1.5	0.86	0.6	0.82	1.4	1.9	2.6
44	33	8	7	7	7	8	34	45
31.9	32.7	33.2	33.83	34.1	33.87	33.3	32.8	32.1

4.0	3.9	3.0	1.7			4.6	5.1	
53	58	68	75			75	58	
30.5	30.8	31.7	33.0			30.1	29.6	

1.1	0.7	0.12	+ 0.2	0.0	0.5	1.1	1.4
32	8	7		7	8	33	44
33.6	34.0	34.57	34.9	34.7	34.2	33.6	33.3

1.4	0.9	0.8				3.6	3.8
46	63	75				75	55
33.3	33.8	33.9				31.1	30.9

Sta + π - Elev

938.55

78+27

✓

+55

✓

+61

5.64 32.91

+68

✓

± Oct. 31, 1963

11

RT

2

34.2	34.5	34.7	35.1	35.0	34.9	34.8	34.3	31.8
44	41	39	35	36	37	38	43	68
75	53	36	20		20	34	43	57

32.4
6.2
75

34.4	34.8	35.5	36.0	36.1	36.1	35.9	35.4	33.0
42	38	31	26	25	25	27	32	56
66	61	37	19		20	33	42	55

33.3
5.3
69

32.9
5.7
75

FL Culv 53' RT 24" S, End

33.8
4.8
75

35.2	35.8	36.3	36.5	36.7	36.8	36.6	36.6	36.4
34	28	23	21	19	18	20	20	22
55	44	32	20		20	31	43	55

33.8
4.8
61

33.3
5.3
67

34.1
4.5
75

37.0
1.6
75

36.6
2.0
69

Sta + π - Elev

938.55

79

✓

TP 5.36 943.83 0.08 938.47

+22

✓

+50

✓

+80

7.32 36.50

RF 8

14

41	2.1	36.5
30	1.3	37.3
20	1.0	37.6
8	0.7	37.9
0	0.7	37.9
20	0.4	38.2
33	0.6	38.0
54	0.7	37.9
67	0.5	37.8

36.3	34.5	34.1	35.1	36.7
23	41	45	35	19
44	51	58	67	75
SEAd 1/2 land				

38.5
0.1
75

75	65	56	52	470	43	458	50	50	52
36.3	37.3	38.2	38.6	39.13	39.5	39.25	38.8	38.8	38.6
44	38	21	7	6		7	8	21	39

34.9	34.4	36.0	37.1
8.9	9.4	7.8	6.1
49	56	67	75

76	36.2
75	35.9
70	35.8
59	35.18
56	37.9
48	59
FL 24" 50"	

FL 24¹¹ SCP

60	53	48	44	388	37	370	42	41	50
40	32	20	7	6	9	7	8	31	42
37.8	38.5	39.0	39.4	39.95	40.1	40.13	39.6	39.7	38.8

35.6	35.2	36.5	38.7
8.2	8.6	7.3	5.1
50	55	64	75
F.L. Calvert 29.44			

36.3	36.4
2.5	7.4
75	55

Sta	+	π	-	Elev.
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		943.83		
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80				
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✓				
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+50				
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✓				
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81				
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✓				
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Oct. 31, 1963

14

B1

P

39.3	40.0	40.3	40.7	41.20	41.5	41.33	40.8	41.0	41.2
45	38	35	31	263	23	250	30	28	26
36	26	15	5	4		7	8	20	30

37.4	35.9	36.2	38.6	40.1	37.4	37.0	37.5	38.6	40.5
64	29	76	52	37	64	68	63	52	33
44	52	58	69	75	75	63	55	49	41

39.9	40.9	41.1	41.4	42.05	42.3	42.41	41.8	42.1	42.3
3.9	2.9	2.7	2.4	1.78	1.5	1.42	2.0	1.7	1.5
36	24	15	4	3		7	8	20	28

37.7	36.6	36.3	36.8	39.1	40.5	38.3	37.8	38.3	39.7	41.9
61	72	75	70	47	33	55	60	55	41	19
43	48	52	59	69	75	75	68	61	49	38

40.4	41.5	41.8	42.1	42.65	42.72	42.90	42.4	42.6	42.8
34	23	20	1.7	1.18	1.11	0.93	14	1.2	10
33	22	13	3	2		7	8	15	26

37.7	36.4	36.6	38.4	41.0	38.9	38.0	39.0	39.0	42.5
61	74	72	54	28	49	48	38	13	
43	49	56	66	75	75	63	49	37	

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		943.83		
--	--	--------	--	--

81+50				
-------	--	--	--	--

✓				
---	--	--	--	--

82				
----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	0.81	943.31	1.33	942.50
----	------	--------	------	--------

Oct. 31, 1963

14

84

9

2.0	1.8	1.4	0.85	0.81	0.69	1.1	1.1	0.9
19	11	2	1		6	7	16	24

3.0	5.8	7.1	7.6	7.0	3.1	4.7	4.1	3.2	1.2
31	40	45	51	58	75	75	63	49	37

5.3	2.8	2.1	1.9	1.5	0.95	0.80	1.3	1.2	1.0
37	28	17	9	1		5	6	14	22

6.8	7.1	6.6	4.2	4.0		3.9	3.1	2.7	1.2
44	50	55	69	75		75	59	46	35

6.8	6.0	3.6	2.5	2.3	2.0	1.33	1.25	1.7	1.6
43	35	28	16	8		1	5	6	13

6.3	5.5	5.7				3.2	3.2	3.0	1.7	1.5
50	59	75				75	69	45	32	20

on Median By +50

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		943.31		
--	--	--------	--	--

82+93				
-------	--	--	--	--

✓				
---	--	--	--	--

83				
----	--	--	--	--

✓				
---	--	--	--	--

+30				
-----	--	--	--	--

+33		Profile of Gervias		
-----	--	--------------------	--	--

FK
FS
DS
WS

Nov. 5, 1963

14

14

1

37.0	37.10	39.7	40.8	41.2	41.3	41.91	41.90	41.3
6.3	6.21	3.6	2.5	2.1	2.0	1.40	1.41	2.0
39	FL	27	15		1	2	5	6
32								

38.5	38.0			41.2	40.8	41.4	41.8
4.8	5.3			2.1	2.5	1.9	1.5
53	75			75	50	35	20

38.6	39.2	39.9	40.5	41.1	41.2	41.7	41.3	41.6	41.1
4.7	4.1	3.4	2.8	2.2	2.1	1.6	2.0	1.7	2.2
75	50	30	20		1	3	5	19	35

41.7	41.1
1.6	2.2
75	57

37.9	38.1	39.3	39.8	40.2	40.5	41.0	41.4	42.0	42.3
5.4	5.2	4.0	3.5	3.1	2.8	2.3	1.9	1.3	1.0
75	60	41	26	14		19	35	57	75

35.0	36.3	38.0	39.4	40.5	40.8	41.6	42.5	42.6
8.3	7.0	5.3	3.9	2.8	2.5	1.7	1.06	0.7
200	150	100	50		18	45	66	100

43.3
133

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		943.31		
--	--	--------	--	--

83+50				
-------	--	--	--	--

✓				
---	--	--	--	--

+65				
-----	--	--	--	--

✓				
---	--	--	--	--

+85				
-----	--	--	--	--

Nov. 5, 1963

1+

R1

S

37.5	38.0	39.4	39.7	40.12	40.5	41.4	42.1	42.2
5.8	5.3	3.9	3.6	3.19	2.8	1.9	1.2	1.1
43	39	23	14		18	43	70	75

40.2
3.1
57

40.8
2.5
75

✓

37.1	37.2	38.5	39.3	39.8	40.0	40.7	41.4	41.8
6.2	6.1	4.8	4.0	3.5	3.3	2.6	1.9	1.5
40	32	24	13		15	40	63	75

37.6
3.7
55

40.6
2.7
75

✓

38.0	36.0	36.5	37.6	38.7	39.14	39.5	39.6	39.2	38.5
5.3	7.3	6.8	5.7	4.6	4.17	3.8	3.7	4.1	4.8
59	40	32	25	12		16	22	33	38

38.9
44
75

40.1
3.2
75

39.3
4.0
59

✓

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		943.31		
--	--	--------	--	--

84				
----	--	--	--	--

✓				
---	--	--	--	--

T.P.	4.10	941.46	5.95	937.36
------	------	--------	------	--------

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+72				
-----	--	--	--	--

✓				
---	--	--	--	--

Nov. 5, 1963

11.

R/ 1

35.3	35.8	37.1	38.3	38.70	39.1	38.7	37.7	37.9
8.0	7.5	6.2	5.0	4.61	4.2	4.6	5.6	5.4
40	32	25	13		16	28	35	52

36.6	37.2	36.8
6.7	6.1	6.5
48	63	75
84 + 50		

✓

38.5
48
75

38.7	34.4	36.0	37.1	37.4	37.9	37.5	36.1	36.6
7.8	7.1	5.5	4.4	4.1	3.6	4.0	5.4	4.9
40	32	25	12		15	25	35	57

✓

37.0
4.5
75

35.2	27.7
6.3	13.8
59	75

34.1	33.1	33.6	35.4	36.5	36.8	37.3	37.2	35.31	36.1
7.4	8.4	7.9	6.1	5.0	4.7	4.2	4.3	6.15	5.4
52	41	32	25	12		15	25	FLC _{Ch} 35	39

35.0	26.1
6.5	15.4
62	75

✓

37.1	36.7
4.4	4.8
75	58

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		941.46		
--	--	--------	--	--

84+75				
-------	--	--	--	--

✓				
---	--	--	--	--

+94				
-----	--	--	--	--

✓				
---	--	--	--	--

85				
----	--	--	--	--

✓				
---	--	--	--	--

T.P.	1.41	937.54	5.33	936.13
------	------	--------	------	--------

Nov. 5, 1963

R1 m

11

8.3	79	6.1	5.1	48	42	4.3	4.5	4.6
42	32	25	12		15	25	43	55

7.2	6.7	16.4
55	61	75

✓

37.0
4.5
75

9.1	8.7	6.8	5.7	5.3	4.7	4.9	4.9	4.7
41	33	25	12		15	25	46	58

8.8	13.6	12.6
50	58	75

✓

37.1
4.4
75

9.2	9.1	8.7	7.0	5.8	5.4	4.9	5.0	6.4	6.52
51	44	32	24	12		14	22	34	36

FLCulV.

128.0	123.9
59	75

✓

37.29	37.21	36.8	36.3	35.4
417	425	4.7	5.2	6.1
75	71	61	51	42

Walk Walk

Sta	+	x	-	Elev.
-----	---	---	---	-------

				937.54
--	--	--	--	--------

85+20				
-------	--	--	--	--

✓				
---	--	--	--	--

+35				
-----	--	--	--	--

✓				
---	--	--	--	--

+39				
-----	--	--	--	--

✓				
---	--	--	--	--

Sta + π - Elev.

937.54

85+58

✓

6+63

✓

+85

✓

Nov. 5, 1963

11

11

31.0	31.0	32.8	33.9	34.4	34.9	34.6	34.7	34.7
6.5	6.5	4.7	3.6	3.1	2.6	2.9	2.8	2.8
41	33	25	13		14	23	27	35

31.5	31.0	30.3
6.0	6.5	7.2
49	65	75

✓

35.3	35.2
2.2	2.3
75	59

31.0	30.7	32.7	33.7	34.2	34.7	34.4	34.7	32.9
6.5	6.8	4.8	3.8	3.3	2.8	3.1	2.8	4.6
42	34	25	13		14	22	25	33

31.4	30.7	30.0
6.1	6.8	7.5
53	66	75

✓

36.1	35.5	33.9	32.9	32.73
1.4	2.0	3.6	4.6	4.81
75	53	42	37	35

FLC_{calc}

31.2	30.1	30.2	32.2	33.1	33.6	34.1	33.7	33.8	32.0
6.3	7.4	7.3	5.3	4.4	3.9	3.4	3.8	3.7	5.5
48	41	35	25	13		14	23	24	32

30.4	29.7
7.1	7.8
61	75

✓

36.1	35.2	32.1
1.4	2.3	5.4
75	50	37

Sta + π - Elev.

937.54

86

✓

+15 $\pm$ E₀ + R₁

✓

+32

✓

Nov. 5, 1963

14

81 x

7.7	7.8	5.6	4.7	4.20	3.8	4.0	3.8	5.5
43	35	25	13		14	23	25	32
29.8	29.7	31.9	32.8	33.34	33.7	33.5	33.7	32.0

6.8	7.4	8.0		36.1	1.4	1.8	2.5	5.6
50	64	75	✓	75	60	49	37	
30.7	30.1	29.5			35.7	35.0	31.9	

8.1	7.4	6.1	5.0	4.5	4.1	4.2	3.4	2.65
43	32	25	13		14	23	40	Conc 61
29.4	30.1	31.4	32.5	33.0	33.4	33.3	34.1	34.89

7.1	8.1							2.35.20
53	75							75 Conc
30.4	29.4							

9.1	8.4	6.3	5.4	5.0	4.5	4.8	6.1	6.2
43	37	25	13		14	23	33	37
28.4	29.1	31.2	32.1	32.5	33.0	32.7	31.4	31.3

7.4	8.3				2.35.3	2.2	2.8	3.3
56	75				75	60	47	
30.1	29.2					34.7	34.2	

Sta + π ~ Elev.

937.54

86+50

✓

+59

7.13 30.41

+69

✓

+85 $\pm$ Ent R1

✓

Nov. 5, 1963

14

R/ 2

28.3	28.8	30.8	31.7	32.2	32.6	32.4	30.8	31.0
9.2	8.9	6.7	5.8	5.3	4.9	5.1	6.7	6.5
43	36	26	13		14	25	33	38

28.3
8.2
53
M.H. 32 RT

28.7
7.8
62
32 RT

29.1
8.4
75

32.1
2.4
75

34.8
2.7
63

34.1
3.4
48

28.1	28.1	30.4	31.3	31.8	32.2	32.0	30.3	30.2
9.4	9.4	7.1	6.2	5.7	5.3	5.5	7.2	7.3
43	37	25	12		13	23	31	34

28.9
8.6
51

29.2
8.3
60

28.9
8.6
75

35.0
2.5
75

34.4
3.1
58

33.6
3.9
47

31.9
5.6
40

27.7	28.0	30.2	31.0	31.4	31.8	32.0	32.4	33.0
9.8	9.5	7.3	6.5	6.1	5.7	5.5	5.1	4.5
42	34	24	12		14	32	54	75

28.3
9.2
50

28.6
8.9
60

28.1
9.4
75

35.0
2.5
75

34.4
3.1
58

33.6
3.9
47

31.9
5.6
40

Sta	+	π	-	Elev
-----	---	-------	---	------

		937.54		
--	--	--------	--	--

87				
----	--	--	--	--

✓				
---	--	--	--	--

T.P.	3.68	934.01	7.21	930.33
------	------	--------	------	--------

+31				
-----	--	--	--	--

✓				
---	--	--	--	--

+48				
-----	--	--	--	--

✓				
---	--	--	--	--

Nov. 5, 1963

81

9

11

27.1	27.4							
10.4	10.1	7.6	6.8	6.4	6.0	6.0	7.9	8.1
43	37	24	12		13	21	28	31

27.8	28.0	27.1
9.7	9.5	10.4
53	61	75

33.59	33.08	32	34
3.95	4.46	5.20	6.6
75	Conc	45	38
Conc	59	Conc	

26.1	26.8	29.4	30.2	30.6	31.0	30.8	29.0	29.1
7.9	7.2	4.6	3.8	3.4	3.0	3.2	5.0	4.9
44	36	24	12		13	21	28	33

25.9	25.6	24.7
8.1	8.4	9.3
56	66	75

33.6	33.2	31.7
0.4	0.8	5.5
75	63	53

22.8	25.4	26.1	28.1	30.0	30.4	30.8	30.8	31.0	31.1
11.2	8.6	7.9	5.9	4.0	3.6	3.2	3.2	3.0	2.5
54	48	39	24	14		12	28	43	57

24.9	23.2
9.1	10.8
59	75

32.4
1.6
75

Sta + π - Elev

934.01

87+65

✓

+95

✓

88

4.21 929.80

109 E Ent Rt

✓

Nov. 5, 1963

RT 100

Lt

8.7	8.1	5.3	4.3	3.9	3.4	3.6	5.1	4.9
46	37	24	14		13	20	27	31

10.0	12.2
61	75

32.5	31.8	30.9
75	56	39

9.7	8.8	8.7	5.5	4.6	4.2	3.7	3.9	5.2	5.1
52	43	40	24	13		12	22	29	33

11.3	12.8
65	75

32.4	31.5	30.7
75	55	41

8.9	8.8	5.7	4.7	4.3	3.8	3.6	3.2	2.8
46	39	24	14		12	30	53	58

10.0	12.8
54	75

31.62
239
75
conc

Sta + π - Elev.

934.01

88+25

✓

+58

✓

+75

✓

Nov. 5, 1963

11.

RT. 1-1

9.0	8.5	5.9	4.9	4.5	4.0	4.1	5.6	5.5
42	36	24	13		11	19	27	31

10.1	11.6	12.6
55	67	75

22	33	37
75	50	38

8.9	8.5	6.2	5.2	4.7	4.7	4.8	5.7	5.7
42	37	25	13		10	17	24	26

9.8	11.4	12.1
53	66	75

23	32	39	46
75	57	40	33

10.0	9.4	8.6	5.7	5.2	4.8	4.8	5.0	5.7	5.6
75	54	38	24	13		10	19	24	27

37	40	42	46
75	60	44	31

Sta + N - Elev

93401

89.

✓

+11 Abandon Ent Rt

✓

+25

✓

± Nov. 5, 1963

BT cc

lt.

8.3	76	58	5.2	4.91	5.0	4.8	5.6	4.6
25.7	26.4	28.2	28.8	29.10	29.0	29.2	28.4	29.4
36	31	24	12	10	18	23	27	

7.4	7.9	7.8
26.6	26.1	26.2
46	59	75

3.6	4.0	4.2
30.4	30.0	29.8
75	52	39

7.5	7.4	5.9	5.2	4.9	5.0	4.5	4.2	3.8
26.5	26.6	28.1	28.8	29.1	29.0	29.5	29.8	30.2
36	31	23	12	9	18	28	48	

6.6	6.0	6.9	7.0
27.4	28.0	27.1	27.0
43	47	61	75

3.4	3.4
30.6	30.6
75	68

7.3	7.2	6.0	5.1	4.9	5.0	4.9	5.6	5.7
26.7	26.8	28.0	28.9	29.1	29.0	29.1	28.4	28.3
35	31	23	12	9	18	21	23	

6.9	5.7	6.4	6.5
27.1	28.3	27.6	27.5
39	43	55	75

3.0	3.33	3.9	4.6
31.0	30.68	30.1	29.4
75	66	47	26

walk

Sta + x - Elev

934.01

89+45

✓

T.P. 4.77 933.44 5.34 928.67 ~~924.75~~

+ 69 ± Ent Rt

✓

+ 74

✓

#K
DS
FS

lt.

Nov. 5, 1963
Nov. 7, 1963

id

28.0	26.9	28.0	28.8	29.0	29.0	29.2	27.9	27.9
6.0	7.1	6.0	5.2	5.0	5.0	4.8	6.1	6.1
36	30	23	11	9	17	22	24	24
28.7	28.3	27.7	27.6	30.7	30.6	30.0	29.4	29.4
5.3	5.7	6.3	6.4	4.3	3.4	4.0	4.6	4.6
42	53	64	75	62	57	44	27	27
Top N End 15 " GMC Ho #2462								

27.8	27.0	27.1	27.8	28.8	29.0	28.9	29.3	29.56	30.29
5.6	6.4	6.3	5.6	4.6	4.4	4.5	4.1	3.88	3.15
36	31	29	22	11	9	18	23	42	42
28.6	27.7	27.4							
4.8	5.7	6.0							
40	69	75							
Conc.									
						30.97	247	265	30.79
						68	52		
Conc.									

28.3	27.0	27.0	27.9	28.8	28.9	28.9	29.1	28.1	28.7
5.1	6.4	6.4	5.5	4.6	4.5	4.5	4.3	5.3	4.7
36	31	29	22	11	9	19	23	27	27
28.9	28.2	27.6							
4.5	5.2	5.8							
41	65	75							
Conc.									
						30.9	30.6	30.1	29.6
						2.5	2.8	3.3	3.8
						75	54	41	30

Sta + π - Elev.

933.44

90

✓

+47

✓

+78

FK
DS
FS

Lt

Nov. 2, 1963.

Bt ee

27.2

27.2

27.8

28.7

28.88

28.8

28.4

28.0

28.4

6.2

6.2

5.6

4.7

4.56

4.6

5.0

5.4

5.0

29

26

22

11

9

19

23

28

28.5

29.4

29.0

27.4

31.5

31.8

31.3

4.9

4.0

4.4

6.0

1.9

1.6

2.1

34

40

54

75

75

55

32

31.3

27.3

27.2

28.1

28.5

28.7

28.6

28.3

27.7

27.7

2.1

6.1

6.2

5.3

4.9

4.7

4.8

5.1

5.7

5.7

33

26

23

18

12

10

18

22

24

32.0

31.5

29.9

30.2

30.5

31.0

29.8

29.4

1.4

1.9

3.5

3.2

2.9

2.4

3.6

4.0

46

55

75

75

52

42

38

30

30.6

26.8

26.7

28.1

28.5

28.7

28.6

28.3

27.4

27.4

2.8

6.6

6.7

5.3

4.9

4.7

4.8

5.1

6.0

6.0

33

26

22

17

11

10

17

22

24

30.9

30.3

29.7

29.0

29.0

29.1

29.1

2.5

3.1

3.7

4.4

4.4

4.3

4.3

50

61

75

75

56

41

29

Sta	+	π	-	Elev.
-----	---	-------	---	-------

Sta	+	π	-	Elev.
-----	---	-------	---	-------

933.44

Sta	+	π	-	Elev.
-----	---	-------	---	-------

90 + 90

✓

91

✓

+30

BM

1.43 932.01

Nov. 7, 1963

Lt.

84 ff

6.7	6.7	5.5	4.9	4.8	4.8	4.8	4.4	4.0
27	24	18	11		9	15	28	37

3.5	3.0	3.5	4.2				3.8	3.9
32	48	62	75				75	62

3.6	6.8	6.7	5.4	4.9	4.77	4.8	4.8	6.2	5.9
32	27	23	18	11		9	17	21	27

3.8	4.1	4.6				4.3	4.6	4.9
48	63	75				75	48	33

5.6	7.1	7.0	5.6	5.0	4.8	5.0	5.4	6.3	6.4
33	27	23	18	11		10	17	22	25

5.1	5.5	5.9				4.3	4.5	4.8	5.0	5.9
52	64	75				75	64	53	37	29

Top N.W. Cor lower step Ho # 2470

Sta + π - Elev.

933.44

91+60

✓

+80 $\pm$ Elev Rt

✓

92

✓

Nov. 7, 1963

14

14

99

27.9 26.0 26.0 27.7 28.2 28.4 28.3 27.7 26.7 26.7
5.5 7.4 7.4 5.7 5.2 5.0 5.1 5.7 6.7 6.7
32 26 23 16 10 10 10 18 23 20 5

28.6 28.3 28.2 28.2 28.3 28.0 27.8 28.2 27.7 27.7
4.8 5.1 5.2 5.2 5.1 5.4 5.6 5.2 5.7 5.7
50 60 75 75 75 63 47 37 31 31

28.6 25.8 25.9 27.4 28.2 28.4 28.2 28.2 28.2 28.4
4.8 7.6 7.5 6.0 5.2 5.0 5.2 5.2 5.2 5.0
33 26 23 17 10 10 10 18 32 48

28.5 28.4 28.2 28.2 28.7 28.6
4.9 5.0 5.2 5.2 4.7 4.8
44 60 75 75 75 64

28.7 25.8 25.8 27.4 28.0 28.2 28.1 27.7 26.4 26.4 27.0
4.7 7.6 7.6 6.0 5.4 5.2 5.3 5.7 7.0 7.0 6.4
33 25 23 17 11 10 10 18 20 22 24

28.8 28.4 27.9 28.2 28.3 28.4 29.3 29.4 29.9 29.9
4.6 5.0 5.5 5.1 5.0 4.1 4.0 3.5 3.5 3.5
48 61 75 75 69 50 40 30 30 30

Sta + π - Elev.

933.44

92+20

✓

+45

✓

TP 4.08 931.68 5.84 927.60

+70

✓

Nov. 7, 1963

11.

2

At. h.h

5.1	7.7	7.7	6.2	5.5	5.2	5.4	5.7	6.2	6.6
28.3	25.7	25.7	27.2	27.9	28.2	28.0	27.7	27.2	26.8
34	26	22	17	11		10	15	18	21

5.8	6.1
27.6	27.3
59	75

4.5	3.9	3.8	3.1	6.6
28.9	29.5	29.6	30.3	26.8
75	56	43	30	23

6.0	8.3	8.3	6.5	5.6	5.4	5.5	5.8	6.1	7.1	7.1
27.4	25.1	25.1	26.9	27.8	28.0	27.9	27.6	27.3	26.3	26.3
33	26	23	18	11		10	15	18	22	24

6.7	7.4	8.1
26.7	26.0	25.3
45	55	75
93		

3.4	3.3	3.4
30.0	30.1	30.0
70	56	33
40		

7.0	5.7	5.3	4.5	4.0	3.8	3.9	4.3	5.9	5.9	2.8
24.7	26.0	26.4	27.2	27.7	27.9	27.8	27.4	25.8	25.8	28.9
50	39	26	18	11		10	18	22	24	30

7.6	8.2
24.1	23.4
63	75

2.1	2.7	2.8
29.6	29.0	28.9
75	58	35

Sta + T - Elev.

931.68

927.83

✓

93

✓

TP 5.42 932.00 5.10 926.58

+13

✓

FK
DS
FS

Lt.

Nov. 7, 1963
Nov. 12, 1963

RT

ii

25.3	26.2	26.9	27.6	27.8	27.7	27.6	28.1	28.1
6.4	5.5	4.8	4.1	3.9	4.0	4.1	3.6	3.6
44	30	19	11		9	17	24	43

24.3	23.5
7.4	8.2
60	75

29.3	28.6
2.4	3.1
75	59

24.1	24.8	26.9	27.4	27.6	27.5	27.4	25.4	25.4
7.6	6.9	4.8	4.3	4.1	4.2	4.3	6.3	6.3
28	22	18	11		10	18	23	25

22.6	23.0	23.1	22.6
9.1	8.7	8.6	9.1
34	45	57	75

Sta 94

28.0	26.9	26.2	26.2	26.2
3.7	4.8	5.5	5.5	5.5
75	64	55	43	31

22.1	23.9	27.0	27.3	27.5	27.3	27.00	25.2	25.4
9.9	8.1	5.0	4.7	4.5	4.7	5.00	6.8	6.6
36	22	16	10		9	18	23	47

24 MH

22.5	22.5
9.5	9.5
56	75

27.7	26.1
4.3	5.9
75	62

Sta	+	π	-	Elev.
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Sta	+	π	-	Elev.
		932.00		

Sta	+	π	-	Elev.
93+37				

Sta	+	π	-	Elev.
✓				

Sta	+	π	-	Elev.
+58				

Sta	+	π	-	Elev.
✓				

Sta	+	π	-	Elev.
+80				

Sta	+	π	-	Elev.
✓				

Nov. 12, 1963

14

At. 10

21.7	22.9	26.7	27.1	27.2	27.1	26.5	24.3	24.1
10.3	9.1	5.3	4.9	4.8	4.9	5.5	7.7	7.9
35	24	17	11		10	18	26	37

21.6	21.6	32.4	27.6	28.3	27.0	25.6	25.0	24.1
10.4	10.4	10.4	2.4	3.7	5.0	6.4	7.0	7.9
54	75	123	100	90	80	75	70	52

21.4	22.4	26.0	26.8	27.0	26.8	26.7	26.9
10.6	9.6	6.0	5.2	5.0	5.2	5.3	5.1
36	27	18	11		10	20	36

20.6	20.9
11.4	11.1
57	75

✓

28.70	27.2	27.0
3.30	4.8	5.0
116	75	55

Gar. Apron

21.2	22.3	26.0	26.5	26.8	26.6	26.0	22.6	22.5
10.8	9.7	6.0	5.5	5.2	5.4	6.0	9.4	9.5
43	25	16	11		10	19	28	30

20.8	21.4
11.2	10.6
63	75

✓

26.5	26.5	26.7
5.5	5.5	5.3
75	59	40

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		932.00		
--	--	--------	--	--

94				
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✓				
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+30				
-----	--	--	--	--

✓				
---	--	--	--	--

+66				
-----	--	--	--	--

✓				
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T.P.	5.13	930.88	6.25	925.75
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Oct. 12, 1963

Lt

Rt k k

21.4	22.1	25.5	26.3	26.58	26.4	25.7	22.6	22.3
10.6	9.9	6.5	5.7	5.42	5.6	6.3	9.4	9.7
50	27	18	11		10	18	24	31

21.7

10.3
75

25.0

27.2

25.0

24.4

7.0 48 7.0 7.6
75 61 52 36

23.1

22.4

25.5

26.0

26.3

26.1

25.3

21.9

22.0

8.9	9.6	6.5	6.0	5.7	5.9	6.7	10.1	10.0
38	26	18	11		10	18	28	32

23.1

23.4

22.2

21.6

21.5

8.9 8.6
62 75

9.8 10.4 10.5
75 61 44

22.8

22.8

25.2

25.7

26.0

25.8

25.4

21.6

20.5

9.2	9.2	6.8	6.3	6.0	6.2	6.6	10.4	11.5
25	23	18	11		10	17	25	30

23.5

24.3

24.5

24.4

21.0

20.4

8.5 2.7 2.5 7.6
28 35 56 75

11.0 11.6
75 50

Sta 9.5

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		930.88		
--	--	--------	--	--

95				
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✓				
---	--	--	--	--

+35				
-----	--	--	--	--

✓				
---	--	--	--	--

+63				
-----	--	--	--	--

✓				
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FF
WS
FS
DS

Nov. 19, 1963

11.

FF. 11

25.3	24.1	23.6	24.8	25.6	25.75	25.7	25.1	25.1	20.8
5.6	6.8	7.3	6.1	5.3	5.13	5.2	5.8	5.8	10.1
35	28	23	19	10		9	19	23	31

24.4	23.6	23.4
6.5	7.3	7.5
48	65	75

20.7	20.2
10.2	10.7
75	64

22.7	23.0	24.6	25.4	25.6	25.5	25.2	24.1	22.2
8.2	7.9	6.3	5.5	5.3	5.4	5.7	6.8	8.7
28	23	19	11		9	18	23	31

23.5	24.2	23.2	23.4
7.4	6.7	7.7	7.5
32	39	50	75

20.7	20.4	20.8
10.2	10.5	10.1
75	58	48

23.8	22.4	22.8	24.7	25.2	25.5	25.4	25.1	24.0	23.3
7.1	8.5	8.1	6.2	5.7	5.4	5.5	5.8	6.9	7.6
39	30	24	19	11		10	18	23	36

23.8	24.0
7.1	6.9
58	75

21.0	21.4
9.9	9.5
75	56

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		930.88		
--	--	--------	--	--

96				
----	--	--	--	--

✓				
---	--	--	--	--

+20				
-----	--	--	--	--

✓				
---	--	--	--	--

+41				
-----	--	--	--	--

		6.14	24.74	
--	--	------	-------	--

+53				
-----	--	--	--	--

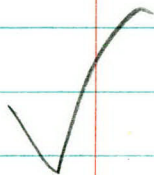
✓				
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Nov. 18, 1963

11.

FL mm

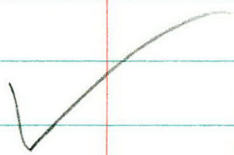
25.0	22.6	22.9	24.4	25.2	25.32	25.3	24.8	23.6
5.9	8.3	8.0	6.5	5.7	5.56	5.6	6.1	7.3
35	30	23	20	11		10	19	26



22.2	22.0	22.7
8.7	8.9	8.2
75	59	43

26.6	25.7	26.3
4.3	5.2	4.6
45	59	75

26.5	23.0	23.0	24.6	25.1	25.3	25.2	24.8	22.7	21.4
4.4	7.9	7.9	6.3	5.8	5.6	5.7	6.1	8.2	9.5
34	29	23	19	11		10	19	29	61



21.6
9.3
75

28.3	27.8	28.0
2.6	3.1	2.9
43	56	75
MH 19.5'81		

24.9	22.9	23.0	24.5	25.0	25.2	25.1	24.7	23.2	22.0
6.0	8.0	7.9	6.4	5.9	5.7	5.8	6.2	7.7	8.9
31	26	24	19	11		10	18	25	37



20.7	21.1
10.2	9.8
75	54

28.2	29.4	29.0	28.8
2.7	1.5	1.9	2.1
35	43	65	75

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		930.88		
--	--	--------	--	--

96+62				
-------	--	--	--	--

✓				
---	--	--	--	--

97				
----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

Nov. 19, 1963

Rt nn

11

25.3	23.0	22.9	24.5	25.0	25.2	25.1	24.6	23.4	23.9
5.6	7.9	8.0	6.4	5.9	5.7	5.8	6.3	7.5	7.0
32	26	24	19	11		10	18	23	26

27.9	29.2	29.1	28.6
3.0	1.7	1.8	2.3
36	46	60	75

24.6	24.4	24.7
6.4	6.5	6.2
75	54	34

24.7	22.6	22.0	24.5	24.9	25.12	25.0	24.5	23.6	23.6
6.2	8.3	8.1	6.4	6.0	5.76	5.9	6.4	7.3	7.3
34	31	25	20	11		10	19	22	23

26.3	26.3	25.4
4.6	4.6	5.5
38	59	75

25.0	25.2	25.3	24.5
5.9	5.7	5.6	6.4
75	59	40	30

24.4	22.5	22.7	24.2	24.8	25.06	25.0	24.5	23.6	23.6
6.5	8.4	8.2	6.7	6.1	5.82	5.9	6.4	7.3	7.3
35	31	27	20	11		10	18	23	25

26.5	25.6	25.4
4.4	5.3	5.5
39	61	75

25.0	25.0	25.0	24.5
5.9	5.9	5.9	6.4
75	57	45	32

Sta	+	π	-	Elev
-----	---	-------	---	------

		930.88		
--	--	--------	--	--

98				
----	--	--	--	--

✓				
---	--	--	--	--

+30				
-----	--	--	--	--

✓				
---	--	--	--	--

+74				
-----	--	--	--	--

✓				
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2 Nov. 19, 1963

RT 00

22.5	22.9	24.1	24.8	24.96	24.8	24.2	23.8	23.2
8.4	8.0	6.8	6.1	5.92	6.1	6.7	7.1	7.7
33	25	21	11		10	18	21	25

24.9	25.3	24.9	24.6	✓	25.1	24.8	24.5	23.9
6.0	5.6	6.0	6.3		5.8	6.1	6.4	7.0
39	47	62	75		75	56	38	28

24.0	22.3	23.1	24.4	24.8	24.83	24.8	24.3	23.7	23.6
6.9	8.6	7.8	6.5	6.1	6.05	6.1	6.6	7.2	7.3
37	32	24	19	11		10	18	21	23

24.4	23.8	23.2	✓	24.7	24.9	24.6	24.2
6.5	7.1	7.7		6.2	6.0	6.3	6.7
43	58	75		75	59	42	27

23.7	22.2	23.0	24.1	24.9	24.84	24.7	24.2	23.9	23.9
7.2	8.7	7.9	6.8	6.0	6.04	6.2	6.7	7.0	7.0
37	32	23	19	11		10	16	22	24

23.0	21.7	21.7	✓	24.6	24.4	24.5	24.3
7.9	9.2	9.2		6.3	6.5	6.4	6.6
49	64	75		75	59	48	29

Sta + π - Elev.

930.88

99

✓

T.P. 6.65 931.43 6.10 924.78

+50

✓

+77

7.38 24.05

100

✓

Nov. 19, 1963

11

Rt

pp

22.4	22.8	24.3	24.9	24.81	24.6	24.1	23.9	24.3
8.5	8.1	6.6	6.0	6.07	6.3	6.8	7.0	6.6
30	22	19	11		10	18	21	28

24.3	22.8	21.6	20.6	24.6	24.7	24.6
6.6	8.1	9.3	10.3	6.3	6.2	6.3
35	48	58	75	75	66	53

P.C. E

25.5	22.5	23.1	24.6	25.1	24.7	24.3	23.9	23.7	24.4
5.9	8.9	8.3	6.8	6.3	6.7	7.1	7.5	7.7	7.0
35	31	22	18	11		10	18	22	30

25.5	26.1	26.0	24.7	24.8	24.5
5.9	5.3	5.4	6.7	6.6	6.9
50	61	75	75	60	45

MH 20' Rt

21.8	22.7	24.6	25.1	24.73	24.2	24.0	24.3	24.9
9.6	8.7	6.8	6.3	6.70	7.2	7.4	7.1	6.5
31	22	18	11		10	17	25	33

23.8	24.3	24.3	25.0	25.3	24.7	24.8	24.7
7.6	7.1	7.1	6.4	6.1	6.7	6.6	6.7
35	42	55	66	75	75	66	52

Sta + π - Elev.

931.43

100+50

✓

+85

2.36 24.07

101

✓

T.P. 1.99 926.63 6.79 924.64

+31

✓

Lt.

Nov. 19, 1963

Rt. 29

22.9	21.2	21.9	24.6	25.0	24.69	24.1	23.9	23.6	23.9
8.5	10.2	9.5	6.8	6.4	6.74	7.3	7.5	7.8	7.5
36	31	23	18	11		10	18	23	29

23.0	22.4	23.2	23.9
8.4	9.0	8.2	7.5
43	58	69	75

MH 18.5 Rt.

24.1	24.2	24.2
7.3	7.2	7.2
75	63	39

19.4	19.3	21.0	24.0	24.8	24.62	24.3	24.0	24.2	24.2
12.0	12.1	10.4	7.4	6.6	6.81	7.1	7.4	7.2	7.2
33	31	26	19	11		10	18	29	47

19.7	20.4	21.2	21.0
11.7	11.0	10.2	10.4
36	45	56	75

P.T. 2

23.9
75
75

15.5	16.4	23.7	24.5	24.57	24.3	23.8	23.5	24.0
11.1	10.2	2.9	2.1	2.06	2.3	2.8	3.1	2.6
41	31	20	11		10	17	21	23

16.4	17.5	18.1
10.2	9.1	8.5
53	66	75

23.9	24.0	23.9	24.4
2.7	2.6	2.7	2.2
75	65	48	32

Sta + π - Elev

926.63

101+67

✓

102

✓

+25

✓

11.

Nov. 19, 1963

Rt.

rr

13.1	14.0	23.5	24.2	24.49	24.4	22.8	23.5	23.8
13.5	12.6	3.1	2.4	2.14	2.2	17.8	3.1	2.8
51	34	20	11		10	19	23	31

12.5

14.1

75

23.9

23.8

2.7

2.8

75 59



12.6	13.5	17.1	23.1	24.0	24.37	24.3	23.7	23.2	20.9
14.0	13.1	9.5	3.5	2.6	2.26	2.3	2.9	3.4	5.7
52	38	28	20	11		10	17	24	30

12.6

14.0

75

24.3

23.9

23.6

21.0

2.3

2.7

3.0

5.6

75 56 35 32



13.0	14.1	17.4	23.1	23.9	24.29	24.2	23.6	23.6	18.2
13.6	12.5	9.2	3.5	2.7	2.34	2.4	3.0	3.0	8.4
46	34	27	19	11		10	18	23	32

11.5

11.3

15.1

15.3

59

75

22.9

22.7

22.0

18.2

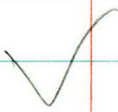
3.7

3.9

4.6

8.4

75 57 41 35



Sta + π - Elev

926.63

102+46

✓

TP 0.55 924.87 2.31 924.32

✓OK

+60

✓

+71

FK
FS
WS
DS
RB

Lt.

Nov. 19, 1963
Nov. 21, 1963 Rt

11.6	13.1	15.4	23.0	23.9	24.26	24.2	23.8	19.1	16.8
15.0	13.5	11.2	3.6	2.7	2.37	2.4	2.8	7.5	9.8
47	45	31	20	11		10	19	29	35

11.5	11.9	11.3				16.6	16.1	15.9
15.1	14.7	15.3				10.0	10.5	10.7
55	59	75				75	61	47
103	£							

10.33	20.5	23.2	24.0	24.2	24.2	23.9	20.9	19.01
6.54	4.4	1.7	0.9	0.7	0.7	1.0	4.0	5.86
Top Cattle Pass	24	19	10		10	18	24	27
28								Top Cattle Pass

11.2	12.4	13.2	13.0	12.9	11.3	11.7	11.2	11.6	11.3
13.7	12.5	11.7	11.9	12.0	13.6	13.2	13.7	13.3	13.6
28	48	53	72	75	100	84	77	49	27

13.0	10.0	23.1	24.1	24.3	24.2	24.0	14.7	16.2	16.6
11.1	6.9	1.8	0.8	0.6	0.7	0.9	5.2	8.7	8.3
38	27	19	10		10	18	28	38	53

14.6	14.8	12.8	12.7			13.9	14.8
10.3	10.1	12.1	12.2			11.0	10.1
45	58	66	75			75	68

Sta	+	' π	-	Elev.
-----	---	---------	---	-------

		924.87		
--	--	--------	--	--

103				
-----	--	--	--	--

✓				
---	--	--	--	--

+22				
-----	--	--	--	--

✓				
---	--	--	--	--

+60				
-----	--	--	--	--

✓				
---	--	--	--	--

+89				
-----	--	--	--	--

		1.19	23.68	
--	--	------	-------	--

Nov. 23, 1963

1+

RT 11

14.8	18.9	23.3	24.0	24.4	24.2	24.0	18.5	14.4
10.1	6.0	1.6	0.9	0.5	0.7	0.9	6.4	10.5
36	25	20	11		10	18	30	39

14.0	13.6	14.3
10.9	11.3	10.6
49	62	75

14.5	14.0
10.4	10.9
75	58

16.0	18.9	23.2	24.1	24.3	24.2	23.6	20.0	15.9
8.9	6.0	1.7	0.8	0.6	0.7	1.3	4.9	9.0
32	24	19	11		10	23	30	38

16.0	15.8	16.3
8.9	9.1	8.6
48	62	75

14.5	14.7
10.4	10.2
75	52

18.3	20.4	23.4	24.2	24.4	24.2	23.8	19.9	17.7
6.6	4.5	1.5	0.7	0.5	0.7	1.1	5.0	7.2
28	23	20	11		10	21	30	39

19.0	18.6	18.0	18.0
5.9	6.3	6.9	6.9
34	48	63	75

15.8	15.8
9.1	9.1
75	54

Top MH 19' RT

Sta + π - Elev

924.87

104

✓

+50

✓

+79

✓

Lt.

Nov. 21, 1963

RH an

19.0	21.0	23.6	24.3	24.39	24.3	23.7	19.8	17.4
5.9	3.9	1.3	0.6	0.48	0.6	1.2	5.1	7.5
28	22	19	11		10	22	31	37

20.0	20.1	20.0	19.7
4.9	4.8	4.9	5.2
36	50	63	75

✓

16.9	16.7
8.0	8.2
75	57

19.9	21.9	23.9	24.3	24.5	24.3	23.7	19.9	18.4
5.0	3.0	1.0	0.6	0.4	0.6	1.2	5.0	6.5
29	23	18	10		9	21	28	37

18.9	18.7	19.1
6.0	6.2	5.8
42	58	75

✓

18.0	17.4
6.9	7.5
75	56

19.7	21.8	23.90	24.5	24.7	24.5	24.2	21.1	19.1
5.2	3.1	0.97	0.4	0.2	0.4	0.7	3.8	5.8
27	23	MH 19	10		10	23	28	38

✓

19.5	19.3	18.7	19.0
5.4	5.6	6.2	5.9
38	51	64	75

18.7	18.5	18.2
6.2	6.4	6.7
75	67	55

Sta + π - Elev

924.87

105

✓

TP 5.56 930.35 0.08 924.79

+20

✓

+33

✓

± Nov. 21, 1963

RT vv

11

19.9	21.0	22.4	24.2	24.6	24.8	24.6	24.4	21.5	20.3
50	3.9	2.5	0.7	0.3	0.08	0.3	0.5	3.4	46
39	24	21	18	10		10	21	28	36

19.6	19.7
5.3	5.2
58	75
105	

19.6	19.3
5.3	5.6
75	54

21.5	21.7	23.1	24.5	24.9	24.99	24.9	24.4	22.3	21.1
8.9	8.7	7.3	5.9	5.5	5.36	5.5	6.0	8.1	9.3
47	34	21	18	10		10	21	27	47

21.1	21.3
9.3	9.1
60	75

21.0	21.2
9.4	9.2
75	61

26.2	25.4	24.8	24.9	25.0	25.1	25.0	24.5	23.0	23.3
4.2	5.0	5.6	5.5	5.4	5.25	5.4	5.9	7.4	7.1
62	50	34	20	10		10	18	22	25

26.7
3.7
75

21.7	21.8	21.8	22.1
8.7	8.6	8.6	8.3
75	65	51	36

Sta + π - Elev.

930.35

105+55

✓

+75 $\neq$ Ent Lt.

✓

106

Lt

Nov. 21, 1963

Rt w w w

26.1	25.6	24.8	25.3	25.2	25.27	25.1	24.7	23.5	23.6
4.3	4.8	5.6	5.1	5.2	5.08	5.3	5.7	6.9	6.8
73	58	34	18	10		10	22	30	46

26.51

3.84
walk
80

22.9	23.7
7.5	6.7
75	57

25.3	25.4	25.4	25.3	25.6	25.3	25.4	24.6	24.8
5.1	5.0	5.0	5.1	4.8	5.1	5.0	5.8	5.6
49	35	19	10		10	20	27	39

25.4	25.5
5.0	4.9
62	75

27.0	27.9	27.2
3.4	2.5	3.2
75	63	51

25.5	25.3	25.2	25.4	25.56	25.5	25.5	25.3	26.7
4.9	5.1	5.2	5.0	4.79	4.9	4.9	5.1	3.7
50	35	20	10		10	17	26	40

26.0	26.55
4.4	3.80
65	70
	Walk

26.3	26.9	27.0
4.1	3.5	3.4
75	67	57

Sta	+	π	-	Elev.
		930.35		

106+30

✓

BM	4.48	932.08	2.75	927.60
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+60

✓

+87

5.45 26.63

107

✓

+27

5.68 26.40

Nov. 21, 1963

LT

RT

26.1	25.7	25.4	25.7	25.75	25.7	25.8	26.0	27.0
4.3	4.7	5.0	4.7	4.60	4.7	4.6	4.4	3.4
53	35	20	10		10	16	27	32

26.6	26.9		28.7	29.2	29.5	28.5
3.8	3.5		1.7	1.2	0.9	1.9
66	75		75	68	53	47

SE Cor Lower Step H. #2623

26.0	25.7	25.6	25.8	26.00	25.9	26.1	27.0	28.7
6.1	6.4	6.5	6.3	6.08	6.2	6.0	5.1	3.4
59	40	20	11		10	18	31	48

26.2		29.5
5.9		2.6
75		75

MH 19.5' RT

26.83	26.8	26.4	26.1	26.2	26.30	26.3	26.5	27.1	28.0
5.25	5.3	5.7	6.0	5.9	5.78	5.8	5.6	5.0	4.1
Walk 65	55	37	20	10		10	18	38	48

28.7	28.8
3A	3.3
75	60

MH 19' LT

Sta	+	π	-	Elev.
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		932.08		
--	--	--------	--	--

107+30	Edge B.T. Lt.			
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✓				
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+65				
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✓				
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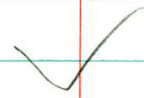
108				
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Nov. 26, 1963

Lt.

RT yy

26.8	26.6	26.5	26.5	26.53	26.4	26.5	27.1	27.6
5.3	5.5	5.6	5.6	5.55	5.7	5.6	5.0	4.5
45	28	20	10		10	15	35	52

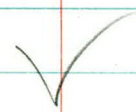


26.9
5.2
62

27.1
5.0
75

28.05
4.03
Walk
64

27.1	27.0	26.8	26.7	27.7 26.7	26.70	26.7	26.7	26.9	27.6
5.0	5.1	5.3	5.4	4.4	5.38	5.4	5.4	5.2	4.5
62	45	28	20	10		10	16	29	50



27.2
4.9
75

28.3
3.8
72

27.3	27.1	26.9	26.7	27.0	27.10	27.1	26.9	27.3	27.6
4.8	5.0	5.2	5.4	5.1	4.98	5.0	5.2	4.8	4.5
62	45	29	20	10		10	17	34	50



27.3
4.8
75

27.6
4.5
75

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		932.08		
--	--	--------	--	--

108+26				
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✓				
---	--	--	--	--

+66				
-----	--	--	--	--

✓				
---	--	--	--	--

109				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	5.67	932.72	5.03	927.05
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Nov. 21, 1963

RT 77

27.33	27.18	26.9	27.1	27.20	27.2	27.1	27.3	27.9
4.75	4.90	5.2	5.0	4.88	4.9	5.0	4.8	4.2
45	33	20	12		10	17	35	50
CONC.								

27.46
4.62
CONC.
65

29.07 28.3
301 38
Walk 68
68

27.47	27.37	27.3	27.2	27.3	27.3	27.4	27.3	27.7	28.3
4.61	4.71	4.8	4.9	4.8	4.6	4.7	4.8	4.4	3.8
48	33	33	20	12		10	16	29	53
CONC.									

27.77
4.31
64
CONC.

29.26 28.8
282 33
68 68
CONC

27.54	27.50	27.3	27.4	27.63	27.6	27.7	28.1	28.4
4.54	4.58	4.8	4.7	4.45	4.5	4.4	4.0	3.7
48	35	25	12		10	22	36	51
CONC								

27.55
4.53
65
CONC

28.6 28.7
3.5 3.4
75 65

Sta

+

A

-

ELEV.

932.72

109+33

+54

+78

+81.?? Profile Co Rd "C"

✓

+84

4.77 27.95

110

+08

4.21

28.51

MH 28' RT

Nov. 21 1963

14

PH 999

26.8	27.0	27.1	27.1	27.6	27.75	27.7	27.8	28.5	28.8
59	57	56	56	51	4.97	50	49	4.2	3.9
75	50	33	21	10	✓	10	19	50	75

25.9	26.3	26.6	26.9	27.6	27.75	27.8	27.7	28.5	29.0
6.8	6.4	6.1	5.8	5.1	4.97	4.9	5.0	4.2	3.737
75	59	37	22	10	✓	10	17	44	6775

26.1	26.5	27.1	27.37	27.5	27.75	27.8	28.1	28.2	28.9
6.6	6.2	5.6	5.35	5.2	4.97	4.9	4.6	4.5	3.836
75	56	31	MH	10	✓	10	32	40	6075
			19						

25.9	26.2	26.7	27.3	27.5	27.77	27.9	28.8	29.3	29.6
6.8	6.5	6.0	5.4	5.2	4.95	4.8	3.9	3.4	3.1
100	75	50	25	10	✓	10	50	75	100

25.6	25.2	24.9	24.5	30.9	30.6	30.2	29.9
7.1	7.5	7.8	8.2	1.8	2.1	2.5	2.8
125	150	175	200	200	175	150	125
MH	19	81					

26.2	26.1	26.5	26.9	27.7	28.00	28.0	28.0	28.4	28.9
65	66	62	58	50	4.75	4.7	4.7	4.3	3.8
69	53	33	25	10	✓	10	16	25	50
									75

26.5

6.2
75

Sta + π - Elev

932.72

110+19

+50

✓

111

✓

BM

2.09 930.63

(930.61)

Nov. 21, 1963

Lt.

RT 666

27.5	27.0	27.0	27.4	27.8	28.07	28.1	29.2	28.7	29.1
5.2	5.7	5.7	5.3	4.9	4.65	4.6	3.5	4.0	3.6
75	56	34	19	10	✓	10	30	55	75

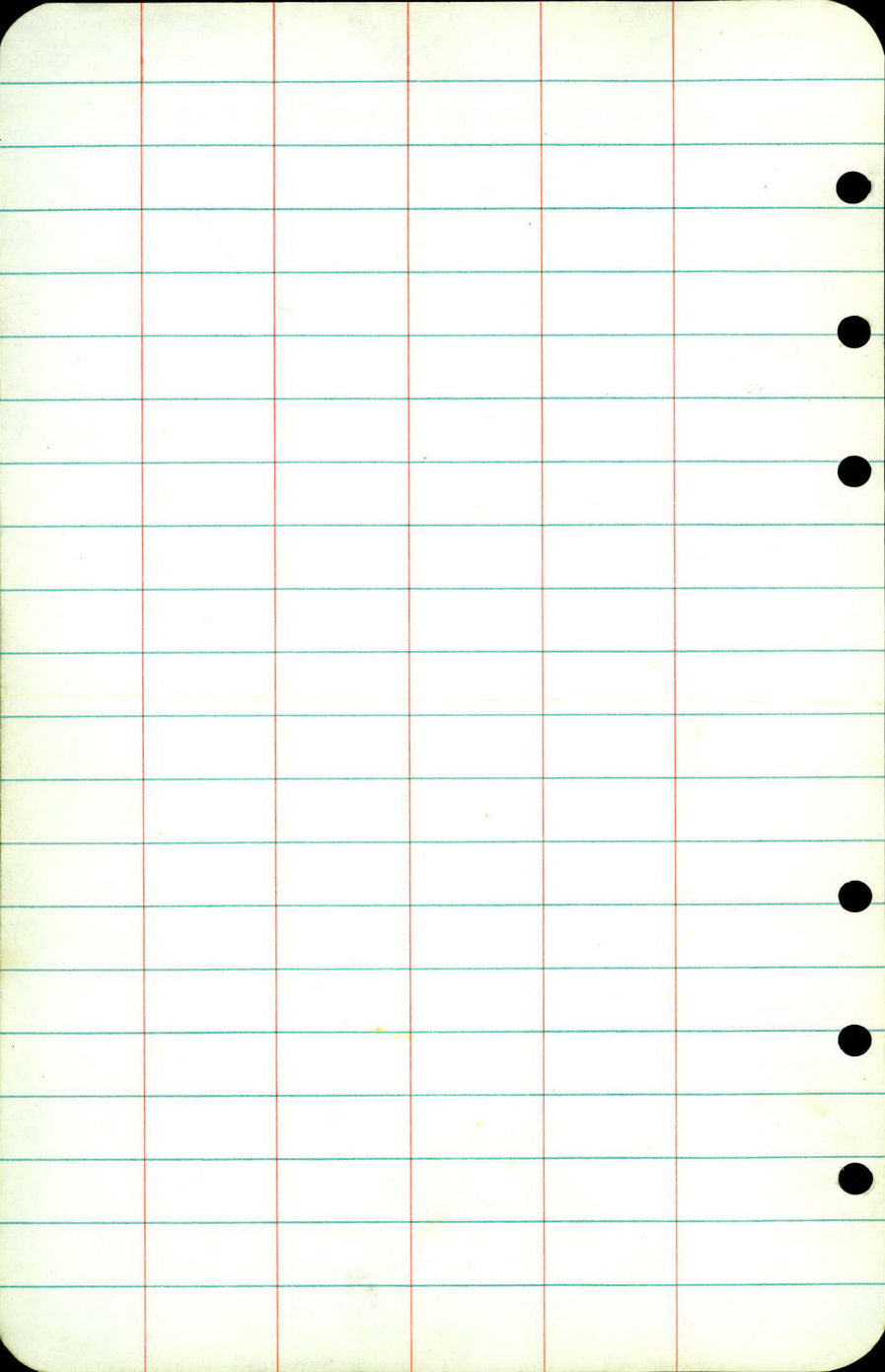
27.4	27.7	27.9	27.7	27.9	28.13	28.1	27.9	27.9	30.2
5.3	5.0	4.8	5.0	4.8	4.59	4.6	4.8	4.8	2.5
75	52	34	20	10	✓	10	18	24	33

32.7	31.8
0.0	0.9
75	40

27.4	27.6	27.8	28.0	28.19	28.0	27.9	27.5	29.0
5.3	5.1	4.9	4.7	4.53	4.7	4.8	5.2	3.7
75	50	25	10	✓	12	17	22	29

32.5	32.0	29.6
0.2	0.7	3.1
64	41	33

USGS NEC₂₂ C & W.B.A.



Dec 4, 1963

1

New Alignment Differences
for x-sections

1 page

Sta.

New Line
x' Lt of old Line

63	0.00
+75	0.00
+50	0.7 ✓
62	2.15 ✓
+50	3.65 ✓
61	4.95 ✓
+50	6.20 ✓
+25	6.40 ✓
60	6.46 ✓
59	5.55 ✓
58	4.67 ✓
57	3.79 ✓
56	2.90 ✓
55	2.01 ✓
54	1.12 ✓
53	0.23 ✓
52+72.95 ± Co R/B	0.00 ✓

Plotted 12/14/63

Nov. 15, 1963

1

Additional Info.

Sta + π - Elev

BM 1.27 924.08

922.81

36+50

+75

37

+30

T.P. 2.25 915.15 11.18 912.90

40+38

41 $\angle$ 2.82 912.33

FK
FS
WS
DS
RB

Nov 19, 1963

Lt

± 2

Top N.W. Cor. Conc. Foundation Control

Structure S.E. Cor. RR Tracks

13.2	16.8	17.9	19.9	22.8
10.9	7.3	6.2	4.2	1.3
100	88	75	59	47

✓

10.1	12.2	13.6	19.7
14.0	11.9	10.5	4.4
100	76	57	46

✓

09.0	10.2	10.9	12.0	20.9
15.1	13.9	13.2	12.1	3.2
100	84	69	57	41

✓

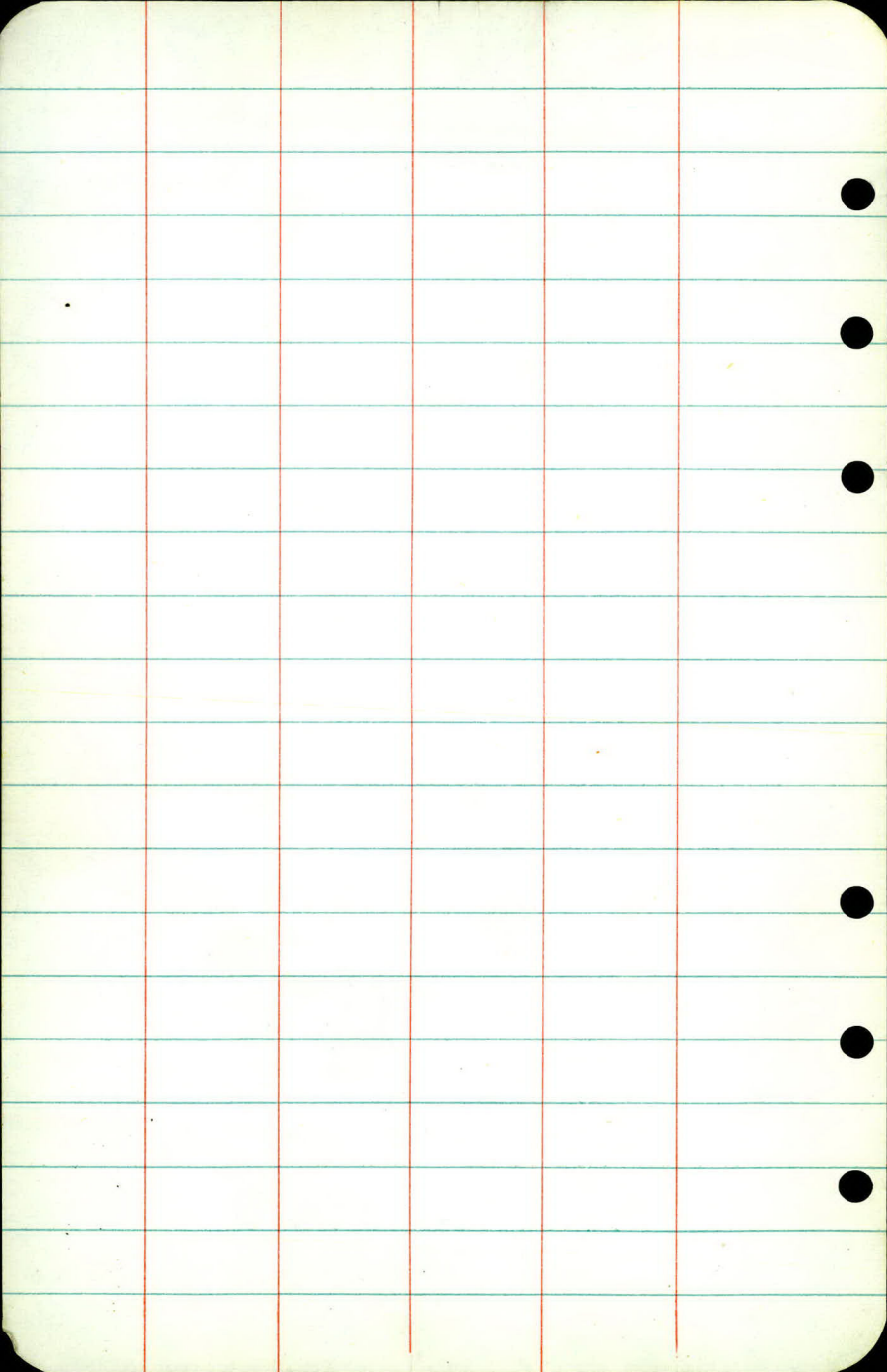
05.9	07.9	10.5	11.7	16.5
18.2	16.2	13.6	12.4	7.6
100	94	76	52	44

✓

07.52	09.7	98.5	01.9	07.51	08.8	13.7	14.4	14.4
7.63	15.5	16.7	12.3	7.64	6.4	1.5	0.8	0.8
Conc 52	52	48	43	Conc 42	29	20	10	

✓

03.6	04.6	07.96
11.6	10.6	17.19
62	100	FL Culv. 48' 24"



MH Location

Sta + π - Elev.

BM 2.67 927.99

(925.32) Spike in

Top MH

5.92 922.07

Transformer
Pole SW corner
of W.B.A.

M.H. $\pm$ W.B.A. 5.3' So. of $\pm$ Cor'd "B"

2 Adjustment Rings

8" Casting

Nov. 28, 1963

1

Prosperity Ave

x-sections

4 pages

Sta	+	π	-	Elev
BM	3.10	928.38		925.28
3+50			4.75	923.63
3+70			6.86	921.52
4+00			4.60	923.78
+05			7.14	921.24
+50			4.54	923.84
+73			6.35	922.03
5				
+10			6.14	922.24
+27				
✓				

FK
DS
FS
RB

Nov. 27, 1963

2

Top E. Cor. Lite standard $60^{\pm}'$ Lt sta $62^{\pm}$

F.L. Culv. 23' Rt 15" x 40' CM

F.L. NE Culv. 25' Rt 15" x 40' CM $\frac{5.89}{1.4}$

F.L. 15" CM 25' Rt

24.1	23.5	23.0	22.1	23.4	23.6	23.86	23.6	23.6	24.1	24.4
4.34	4.95	4.63	5.0	4.8	4.52	4.8	4.8	4.3	4.0	
50	44	36	22	19	13	11	19	35	50	

F.L. NE 15" x 37' CM 24' Rt

23.4	23.1	22.3	23.3	23.6	23.85	23.5	23.0	22.9	22.3
5.0	5.3	6.1	5.1	4.8	4.53	4.9	5.4	5.5	6.1
43	35	22	19	14	11	17	21	25	

24.4
40
50

23.9 23.9 23.3
45 45 5.1
50 40 30

Sta	+	π	-	Elev.
-----	---	-------	---	-------

Sta	+	π	-	Elev.
-----	---	-------	---	-------

928.38

Sta	+	π	-	Elev.
-----	---	-------	---	-------

5+52

Sta	+	π	-	Elev.
-----	---	-------	---	-------

✓

Sta	+	π	-	Elev.
-----	---	-------	---	-------

+70

Sta	+	π	-	Elev.
-----	---	-------	---	-------

✓

Sta	+	π	-	Elev.
-----	---	-------	---	-------

+84

Sta	+	π	-	Elev.
-----	---	-------	---	-------

✓

Nov. 27, 1963

3

22.8	22.4	23.3	23.5	23.76	23.4	22.9	21.7	22.7
56	60	51	49	4.62	50	5.5	6.7	57
32	23	19	14		11	17	24	28



23.5	24.7
49	3.7
43	50

23.8	23.5
46	49
50	33

22.8	22.1	23.2	23.4	23.72	23.5	23.1	22.0	21.4
56	6.3	5.2	5.0	4.66	4.9	5.3	6.4	7.0
28	23	18	14		12	18	22	25



23.2	23.8	25.1
5.2	4.6	3.3
36	44	50

23.6	23.7	22.3
4.8	4.7	6.1
50	38	28

22.8	22.3	23.1	23.4	23.74	23.6	23.4	23.5	23.1
56	6.1	5.3	5.0	4.64	4.8	5.0	4.9	5.3
29	24	18	14		12	17	29	34

23.5	25.4
4.9	3.0
41	50



19.65	21.6
8.73	6.8
FL 24 SCP	36
39	

Sta + π - Elev.

928.38

6

✓

+27

✓

+52

4.31 24.07

7

4.27 24.11

62 WBAZ

4.70 923.68

Nov. 23, 1963

RT

4

LT

23.4	23.6	23.3	23.4	23.71	23.7	23.5	23.4	23.6
50	4.8	5.1	5.0	4.67	4.7	4.9	5.0	4.8
33	22	19	13		12	20	28	35

23.7 24.3

4.7 4.1
47 50

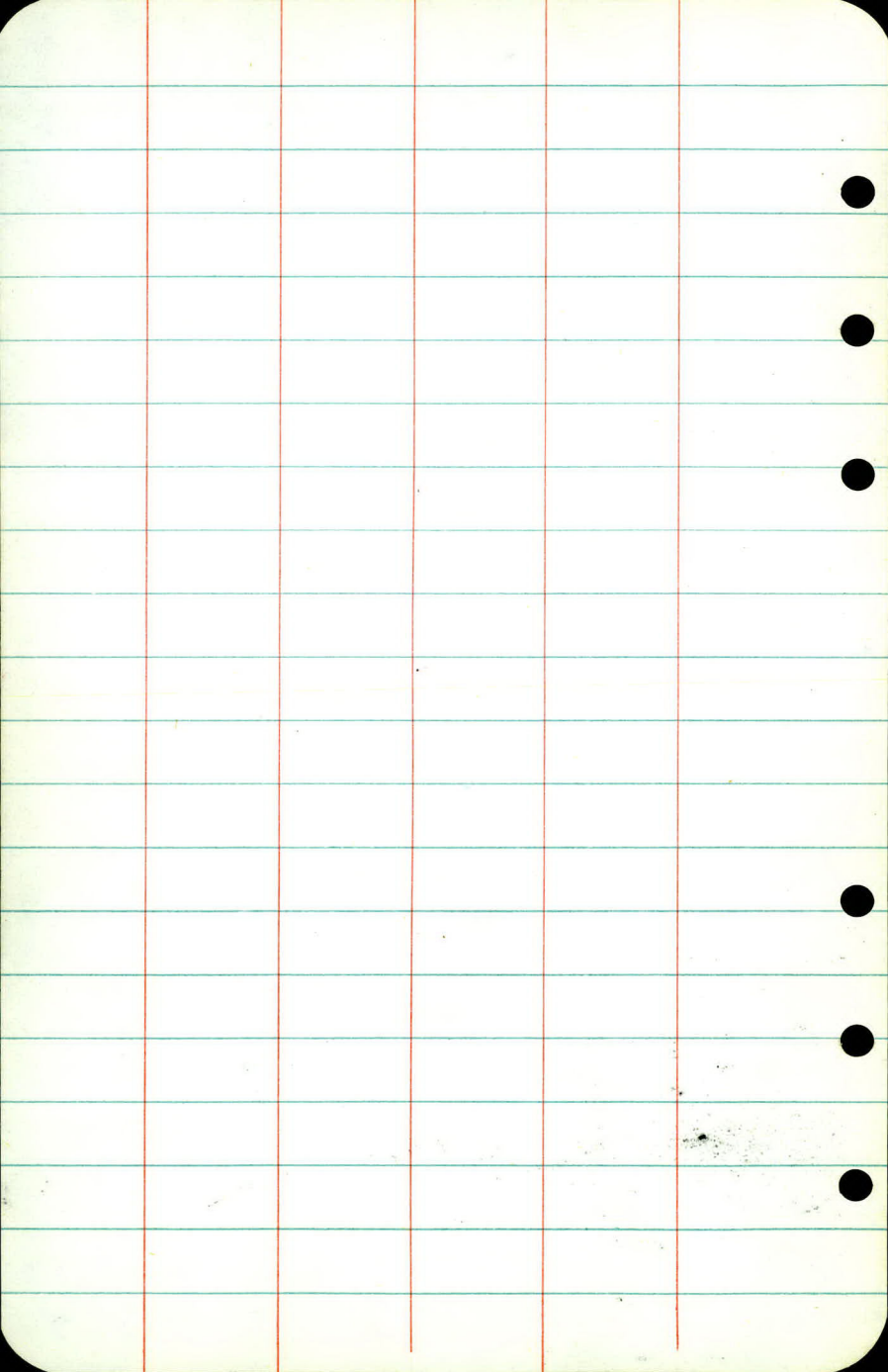
23.2 23.7

5.2 4.7
50 39
LWBA

23.3	23.0	22.4	23.4	23.6	23.88	24.0	23.8	23.3	22.5
5.1	5.4	6.0	5.0	4.8	4.50	4.4	4.6	5.1	5.9
40	30	25	22	13		12	24	33	46

23.7
4.7
50

22.6
5.8
50



FK
JS

Dec. 13, 1963

DS
RB

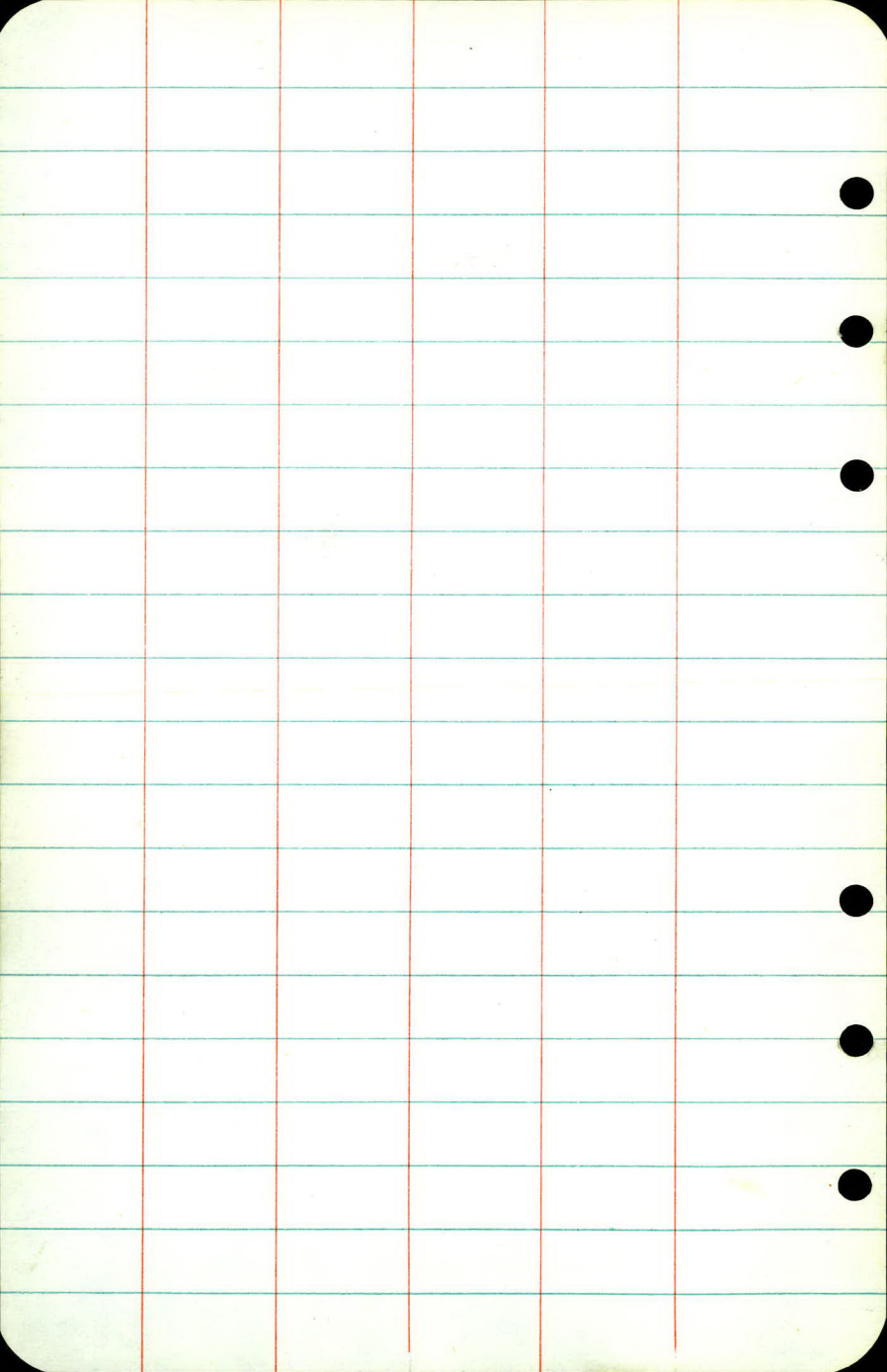
Section Line →

PROSPERITY 33'

WHITE BEAR AVE

33'

33'



B. T. Elevations



pages

Sta + π - Elev.

BM 6.34 930.02

¹
(923.68)

68+50 ± 4.88 925.14

67+05

+50

68

+50

69

+50

FK
FS
RB

Lt.

Median Dec. 4, 1963
Gutter

Rt.

2

S.E. Cr. Life Standard W. Side W. B.A. At TH 36
Approach

23.96	24.43	24.62	24.72	24.88	24.93	25.07	25.15
6.06	5.59	5.40	5.30	5.14	5.09	4.95	4.87
21	12	5			5	12	14



23.99	24.43	24.55	24.64	24.73	24.87	25.07	25.08
6.03	5.59	5.47	5.38	5.29	5.15	4.95	4.94
21	12	5			5	12	14



23.66 23.76	24.25	24.42	24.54	24.80	24.86	25.04	25.13 24.13
6.36	5.77	5.60	5.48	5.22	5.16	4.98	4.89
21	12	5			5	12	15



23.30	23.92	24.25	24.39	24.69	24.76	24.98	25.12
6.72	6.10	5.77	5.63	5.33	5.26	5.04	4.90
23	12	5			5	12	17



23.11	23.77	24.01	24.14	24.44	24.60	24.84	25.05
6.91	6.25	6.01	5.88	5.58	5.42	5.18	4.99
24	12	5		6	5	12	18



22.86	23.62	23.86	24.01	24.38	24.43	24.61	24.84
7.16	6.40	6.16	6.01	5.64	5.59	5.41	5.18
24	12	5			5	12	19



Sta	+	π	-	Elev.
-----	---	-------	---	-------

		930.02		
--	--	--------	--	--

70				
----	--	--	--	--

+50				
-----	--	--	--	--

	927.81	927.81	4.15	923.68
BM	4.13	934.15	6.34	930.02

71		in Intersection		
----	--	-----------------	--	--

+50				
-----	--	--	--	--

72				
----	--	--	--	--

+50				
-----	--	--	--	--

+85				
-----	--	--	--	--

		5.83	921.98	Gutter Rt at C.B.
--	--	------	--------	----------------------

73				
----	--	--	--	--

Median Dec. 4, 1963

Gutter

RT

3

Lt

22.99	23.39	23.65	23.79	24.17	24.33	24.55	24.81
703	6.63	6.37	6.23	5.85	5.69	5.47	5.21
25	12	5		✓	5	12	21

Gutter

22.62	23.23	23.42	23.50	23.94	24.03	24.23	24.55
7.40	6.79	6.60	6.52	6.08	5.99	5.79	5.47
24	12	5		✓	5	12	21

SE. Cor Life Standard W. Side W.B.A. at TH#36 App.

22.02	22.33	22.51	22.64	23.25	23.31	23.45	23.88
5.79	5.48	5.30	5.17	4.56	4.50	4.36	3.93
24	12	5		Gutter ✓	5	12	24

21.61	22.01	22.20	22.28	22.78	22.85	23.00	23.39
6.20	5.80	5.61	5.53	5.03	4.96	4.81	4.42
24	12	5		✓	5	12	24

21.39	21.72	21.84	21.86	22.36	22.41	22.54	22.71
6.42	6.09	5.97	5.95	5.45	5.40	5.27	5.04
25				✓			25

21.16	21.53	21.60	21.60	21.83	21.94	22.02	22.23
6.65	6.28	6.21	6.21	5.98	5.87	5.79	5.58
25	12	5		✓	5	12	25

Sta + π - Elev

927.81
934.15

73+50

74

+50

75

4.12 923.69
930.03 Curb R+8'

73+70

Median Dec. 4, 1963

Lt

Gutter

Rt.

4

21.09	21.44	21.50	21.48	21.50	21.66	21.64	21.69
6.72	6.37	6.31	6.33	6.31	6.15	6.17	6.12
24	12	5			5	12	25

✓

21.25	21.49	21.64	21.68	21.65	21.59	21.50	21.44
6.56	6.32	6.17	6.13	6.16	6.22	6.31	6.37
					5	12	24

✓

21.78	22.02	22.13	22.20	22.23	22.14	22.07	21.89
6.03	5.79	5.68	5.61	5.58	5.67	5.74	5.92
							24

✓

22.76	23.02	23.11	23.14	23.16	23.16	23.07	22.76
5.05	4.79	4.70	4.67	4.65	4.65	4.74	5.05
24							

✓

21.50	21.55
6.31	6.26

Sta + π - Elev. 937.30

BM 1324 938.28 (925.04)

75+50

76

+50

77

+50

78

BM 0.93 937.35 937.30

Lt.

Median Dec. 4, 1963

Gutter

R1

5

Top N. End Curb S.B. Lane WBA at TH 36

24.1	24.37	24.42	24.52	24.57	24.50	24.39	24.1
14.2	13.91	13.86	13.76	13.71	13.78	13.89	14.2
							24



25.82	25.97	26.10	26.19	26.30	26.12	25.87	25.78
12.46	12.31	12.18	12.09	11.98	12.16	12.31	12.50



27.66	27.85	28.01	28.09	28.21	27.99	27.76	27.55
10.62	10.43	10.27	10.19	10.07	10.29	10.52	10.73



29.59	29.94	30.12	30.20	30.18	29.97	29.76	29.60
8.69	8.34	8.16	8.08	8.10	8.31	8.52	8.68



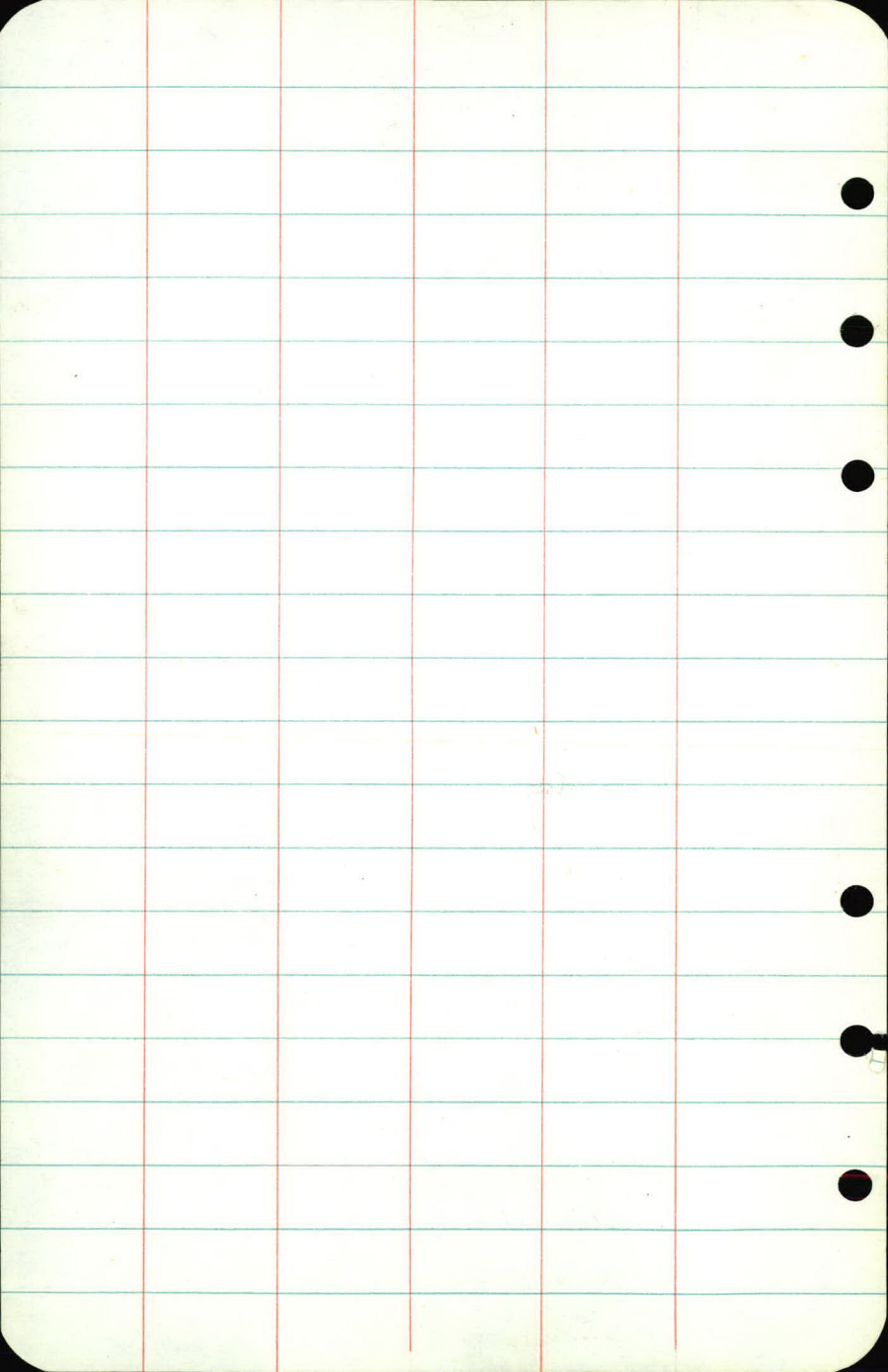
31.62	31.86	32.00	32.07	32.10	31.92	31.83	31.72
6.66	6.42	6.28	6.21	6.18	6.36	6.45	6.56



33.70	33.93	34.01	34.06	34.15	33.92	33.68	33.53
4.58	4.35	4.27	4.22	4.13	4.36	4.60	4.75



Top N End 24"SCP L. Approach Lane TH #36



Additional Info

67+50

Typical Median



Sta + π - Elev.

38+49.8 Cor. Conc Rt.

+58.0 " " Rt.

38+54.1 Cor Conc. Lt.

+62.0 Cor Conc. Lt.

BM 0.79 913.42

(912.63)

46 Conc^{10'} Rt. 6.06 07.36

46 $\pm$ 5.39 08.03

BM 2.47 927.75

Top & Cor Light
Std. 51' Lt 60+38
(925.28)

61+50

9.70

Rt 130'
18.05 End Apron

62+48 Inv

7.52

20.23 89' Lt.

BM

1.53

926.22

N.W. Gr Metal/
Base Lt Std
45' Rt Sta 64160

Nov. 19, 1963

3

SE Cor Lower step Ho # 2125

62+50

144.6

Culvert

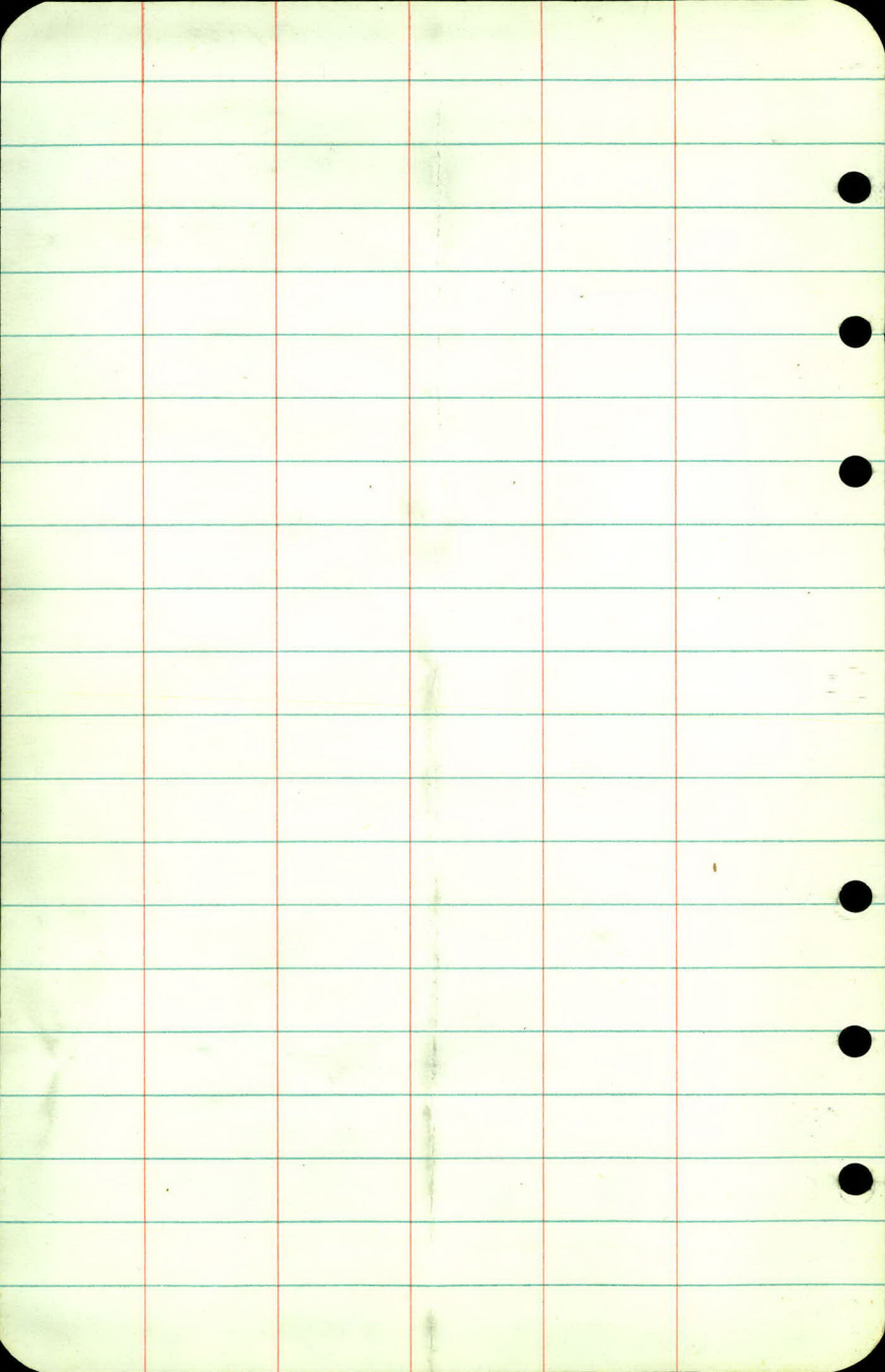
102.4

Apron

24" sewer

60+00

168.7



Borrow Pit

WHITE BEAR AVE

Sta + π - c/cu

B.M. 1.22 824.03

822.81

T.P. 3.57 819.85 7.75 816.28

+50

+100

V

+50

✓

J.S
F.S
D.S
R.B

1-14.64
15.64

\$

Rt

1

N. W. Coy Control structure

Top Log 0+75 Rt 60'

811.6	10.4	10.0	10.1	12.5	17.1	821.3	821.6
8.3	9.5	9.9	9.8	7.4	2.8	+1.4	+1.7
00	7	27	41	59	77	9.5	100
							Base Track

808.5	808.7	809.3	11.1	15.3	8.6	19.0	18.6
11.4	11.2	10.6	8.8	4.6	1.3	0.9	1.4
00	15	39	56	64	66	74	82
				90			

822.3	821.8
+2.4	+1.9
110	105
Base Track	

807.1	808.5	809.4	10.9	14.6	16.2	15.2
12.2	11.4	10.5	9.0	5.3	3.7	4.7
00	26	37	48	55	67	78

822.9	822.4	19.6	14.3	13.7
+3.0	+2.5	0.3	5.6	6.2
122	118	111	100	94
Base				

Sta + π - elev

819.85

R+00

✓

+12

✓

+49

VS
FS
DS
PB

R

Rt

2

807.8	808.2	809.0	11.5	14.6	15.1	14.8	FENCE
121	117	109	8.4	5.3	4.8	5.1	
00	16	31	42	53	62	77 81	

23.3	22.5	18.5	14.0	13.7	13.4
+ 34	+ 26	1.4	5.9	6.2	6.5
130	124	116	107	100	89

807.6	08.3	09.3	11.9	14.3	15.5	14.9
123	11.6	106	80	56	44	50
	19	33	43	54	64	76

822.3	822.7	19.1	15.1	13.8	14.0
+ 34	+ 28	0.8	4.8	6.1	5.9
132	128	120	113	96	85

806.8	08.0	08.7	10.8	13.6	15.9	16.4	17.9
131	11.9	11.2	9.1	6.3	4.0	3.5	2.0
	19	32	45	56	67	90	100

823.9	23.3	21.7	21.1
+ 4.0	+ 3.4	1.8	+ 1.2
136	132	122	111

Sta + π - elev
819.85

3+00

✓

B.M.

8.19 811.66

B.M.

14.08 836.89

822.81

+50

✓

4+00

Minnesota Highway Department
Division of Materials & Research

IDENTIFICATION CARD — CONCRETE TEST CYLINDER

S. P. Br. NO. or
Culv. Sta.

Field Identification No. Date Made

Part of Structure

Concrete Mix No. (1A6 etc.)

Remarks

Source of Ready Mix

Job Mix — ☐

.....
PROJECT ENGINEER

(See reverse side of instructions)

INSTRUCTIONS

1. Fill in front of card completely.
2. If early break is desired request under "Remarks."
3. Place this card in envelope (Form 2407).
4. Remove cardboard from the test cylinder.
5. Attach envelope to the cylinder.
6. Ship cylinders for early breaks in wood crates to prevent damage. Wrap cylinders in wet newspaper.
7. For normal 28 day breaks wrap cylinder in wet newspaper and ship in waterproof sample bag. Do not ship before 14 days.

JS
DS
FS
RB

14.95
11.5

1-11-63

4

RT

3

805.4 06.9 08.7 10.7 12.5 16.3 17.9 21.4
14.5 13.0 11.2 9.2 7.4 3.6 2.9 +1.5
10 43 60 66 79 100 99 108

24.5 24.0 23.2 24.9 24.0
+4.6 14.1 +3.3 +5.0 +4.1
14.4 138 135 131 119
Base

SPIKE IN TWIN COTONWOOD STA 5+27 RT 60'

N. W. COR CONTROL STRUCTURE

805.4 06.9 08.9 13.7 18.7 23.4 28.3
31.5 30.0 28.0 23.2 18.2 13.5 8.6
27 60 79 89 100 109 115

257.3 25.3 24.5 23.7 28.2
11.6 11.6 12.4 13.2 8.7
153.5 153 149 145 135
Top Rail - Base

805.0 806.9 09.3 16.6 24.3 30.1 29.5
31.9 30.0 27.6 20.3 12.6 6.7 7.4
33 70 89 100 112 113 136

267.1 25.7 25.0 24.3
10.68 11.2 11.9 12.6
155.5 155 151 147
Top Rail - Base

Sta + π - elev

836.89

4+25

✓

+60

✓

5+00

✓ B.M. 2.05 829.52 9.42 827.47

670

822.82

(822.81) →

25
FS
DS

1-14-64

L

RT

4

805.4	06.8	09.1	10.6	16.2	21.4	25.7	FENCE
31.5	30.1	27.8	26.3	20.7	15.5	11.2	
	32	69	81	91	100	107	

26.48	25.9	25.4	24.5	30.2	30.0	FENCE
10.41	11.0	11.5	12.4	6.7	6.9	
156.5	156	153	149	137	117	

Top Rail Base

805.2	07.2	09.0	10.4	12.5	16.7	22.9	FENCE
31.7	29.7	27.9	26.5	24.4	20.2	14.0	
	33	57	76	83	90	100	

76.83	26.4	25.8	24.6	30.9	31.1	32.2	25.6	FENCE
10.06	10.5	11.1	12.3	6.0	5.8	4.7	11.3	
157.5	157	154	149	137	121	116	104	

Top Rail Base

805.9	805.0	09.5	13.9	18.7	23.6	29.2	FENCE
31.0	29.9	27.4	23.0	18.2	13.3	7.7	
	30	61	71	79	89	100	

27.4	26.6	26.2	25.4	31.4	32.0	33.6	FENCE
9.75	10.3	10.7	11.5	5.4	4.9	2.3	
153.5	155	152	148	136	123	115	

TOP S.W. NUT S. RAIL Sta 5+06 RT+160'

S+A + T - elev

B. M. 8.81 \$36.28

837.17

5+33

✓

+88

✓

6+00

✓

NS
FS
DS

13.0
1
120

1-16-64
30°

4

RT

5

TOP S.W. NOT S. RAIL 5406 RT 160

806.4	08.0	095	13.0	21.1	27.7	33.5	40.0
29.9	28.3	26.8	23.3	15.2	8.6	2.8	2.3
	30	44	62	78	88	100	110

2743	27.0	26.3	25.7	34.3
88.5	9.3	10.0	10.6	2.0
155.5	155	151	147	131
Top N. Rail	Base			

07A	10.3	12.6	16.7	24.1	27.7	33.2
28.9	26.0	23.7	19.6	12.2	8.6	3.1
	24	34	46	58	61	69

2777	27.4	26.7	25.8	34.6	35.1	35.2
8.51	8.9	9.6	10.5	1.7	1.2	1.1
Top N. Rail	143	139	135	117	95	83
143.5	Base					

08.0	10.6	13.5	18.0	23.0	31.1	34.9	35.2
28.3	25.8	22.8	18.3	13.3	5.2	1.4	1.1
	18	30	37	44	56	68	94

27.90	27.4	25.9	26.1	33.4	34.9
8.38	8.9	9.4	10.2	2.9	1.4
140.5	140	137	132	122	113
Top N. Rail	Base				

STA + π - elev
836.28

6+50

✓

7+00

✓

+17.24

✓

E

27

6

11.9	15.3	18.1	25.0	31.2	34.4	34.0
244	210	18.2	11.3	5.1	1.9	2.3
	7	15	27	40	50	77

28.22	27.6	27.0	26.3	27.5	27.7	32.5
8.06	8.7	9.3	10.0	8.8	6.6	3.8
134.5	134	130	126	117	100	85

TOP N. Rail

24.9	26.3	29.8	26.4	22.1	22.4	23.3
11.4	10.0	6.5	9.9	14.2	13.9	13.0
	8	23	46	22	90	100

28.52	27.9	27.4	26.6
7.76	8.4	8.9	9.7
122.5	122	119	113

TOP N. Rail

30.7	28.4	25.2	22.6	20.4	20.9	26.8
5.6	7.9	11.1	13.7	15.9	15.4	9.5
	23	37	47	69	89	108

28.70	28.2	27.5
7.58	8.1	8.8
116.5	116	113

TOP N. Rail

Sta + π - elev

836.28

7+67

✓

8+00

11

T.P. 0.08 819.93 16.43 819.85

B.M.

8.29 811.64 (811.66)

J.S.
F.S.
D.S.

2

R1

1-16-64

7

27.1	24.0	20.6	18.7	18.8	27.1
9.2	12.3	15.7	17.6	17.5	9.2
	17	26	34	76	95

29.0	28.6	28.0
7.22	7.7	8.3
109.5	109	100

Top N Rail

25.2	24.1	21.3	20.6	20.3	21.3	21.3
11.1	12.2	15.0	15.7	16.0	9.0	8.0
	14	30	40	65	82	88

29.38	28.7
6.90	7.6
90.5	90

Top N Rail

ROCK

SPIKE IN TWIN COTTONWOOD 5495 R160

Sta + π - elev

B.M. 5.00 827.47

827.47

8+50

9+00

5.00 827.47 827.47

J.S.
F.S.
DS

1-17-64
20° 64

RT

8

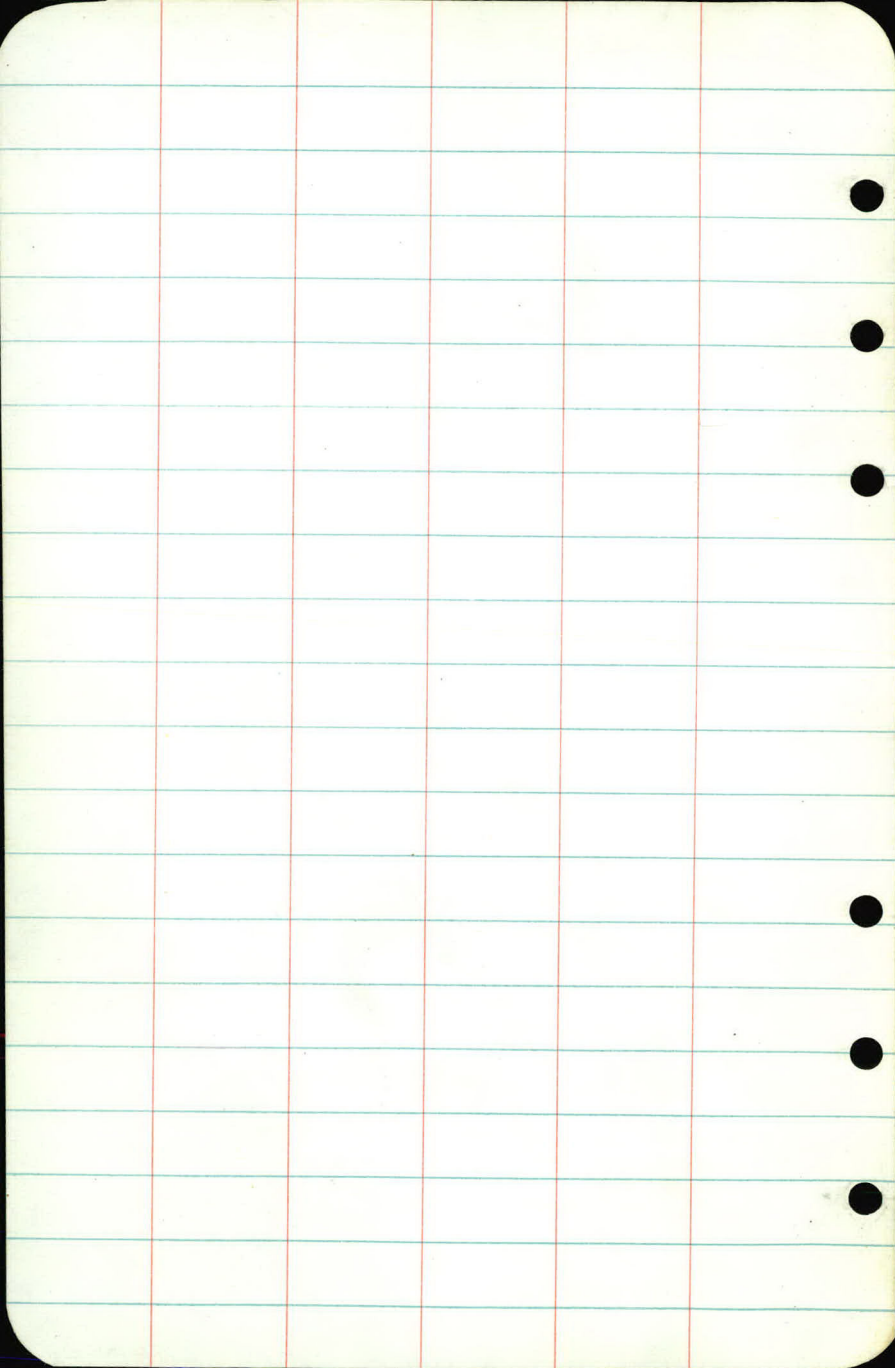
TOP S.W. NUT S. RAIL STA 5+06 RT 160'

25.2	25.1	24.9	27.5	28.7	29.3	29.8
7.3	7.4	8.1	5.0	3.8	3.2	2.66
	23	52	62	66	71	71.5

Top N. Rail

27.9	29.2	30.1	28.2	29.3	29.9	30.35
4.5	3.3	2.4	4.3	3.2	2.6	2.12
	11	31	38	43	47	47.5

TOP S.W. NUT S. RAIL STA 5+06 RT 160' Top N. Rail



1
WHITE BEAR AVE

Alignment

62-665-05

N.B.L. Revision

Sta Point ΔL ΔR

+85.42

+85.74 P.T.

24°41'

+75

23°46.2'

+50

21°38.7'

Chord

+25

19°31.2' P.I. = ~~61+50.82~~

61+51.50

62

17°23.7' $\Delta = 49°22'$

+75

15°16.2' $\frac{1}{2}\Delta = 24°41'$

+50

13°08.7' $D = 17°$

+25

11°01.2' $T = 155.47$

134.90 Arc

61

8°53.7' $L = 290.39$

+75

6°46.2' $R =$

+50

4°38.7'

+25

2°31.2'

60

0°23.7'

+95.03

59+95.35 P.C.

0°00'

County Rider #2

Jones St. & Park St.

11

$$\begin{array}{r} 61+49.10 \\ 1 \quad 31.67 \\ \hline 60+17.43 \\ 23.8 \\ \hline 59+93.63 \end{array}$$

P.C. 60+19.15

23.8

$$\begin{array}{r} P=20 \\ T=121.6 \\ L=243.2 \end{array}$$

Survey Line D=207

D=179

$$\begin{array}{r} P=17 \\ T=155.47 \\ L=240.39 \end{array}$$

Base Line for inside curve

P.C. 58+93.63

23.8

20+48+10 = 179

Sta. 62+

Locate sign on new line (fill sta. sign) (Face and back of sign)

$$\begin{array}{r} 155.4 \\ 131.61 \\ \hline 23.80 \end{array}$$

17'

80/100 = .8

480

30

510/100 = 5.1'

60+19.15

23.8

59+95.35 ✓

60+19.15

2 46.83 ✓

62 65.98

60+19.15

1 31.67

61 50.82

61 49.10

1.72 Diff.

60+19.15

23.8

59 95.35

290.99

62 85.74

58 93.63

290.39

61 84.02

155,47
4,65

154,90

FK
JS
FS
DS

Feb 4, 1964
2

2

$$\begin{array}{r} 62 + 87.42 \\ \hline 62 + 85.42 \end{array}$$

$$\begin{array}{r} 62 + 38.5 \\ \hline 32.5 \end{array}$$

Hex Bolt.

$$\begin{array}{r} 61 + 96 \\ \hline 47.3 \end{array}$$

$$\begin{array}{r} 61 + 92 \\ \hline 43.6 \end{array}$$

14645

362

506

FK
JS
DS
WS

Feb 5, 1964

3

16955

9170

33750

16955

33750

306 45 168 55 62400±

P.T.

33'

99°25'

79.15'

168°55'

71.65'

40'

54'

20'

48'

20.85'

89.47'

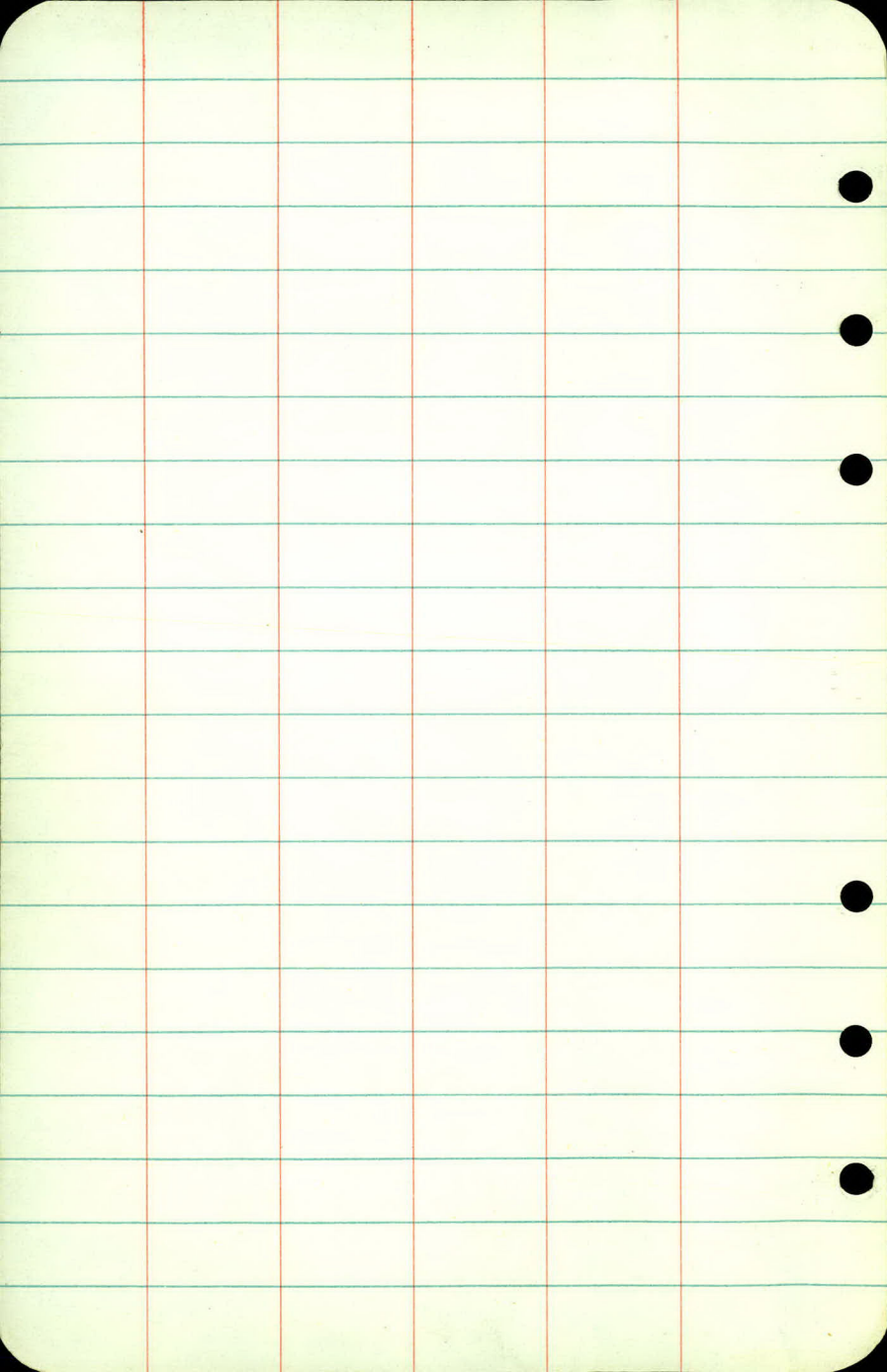
80°25'

33'

P.C.

PI

7

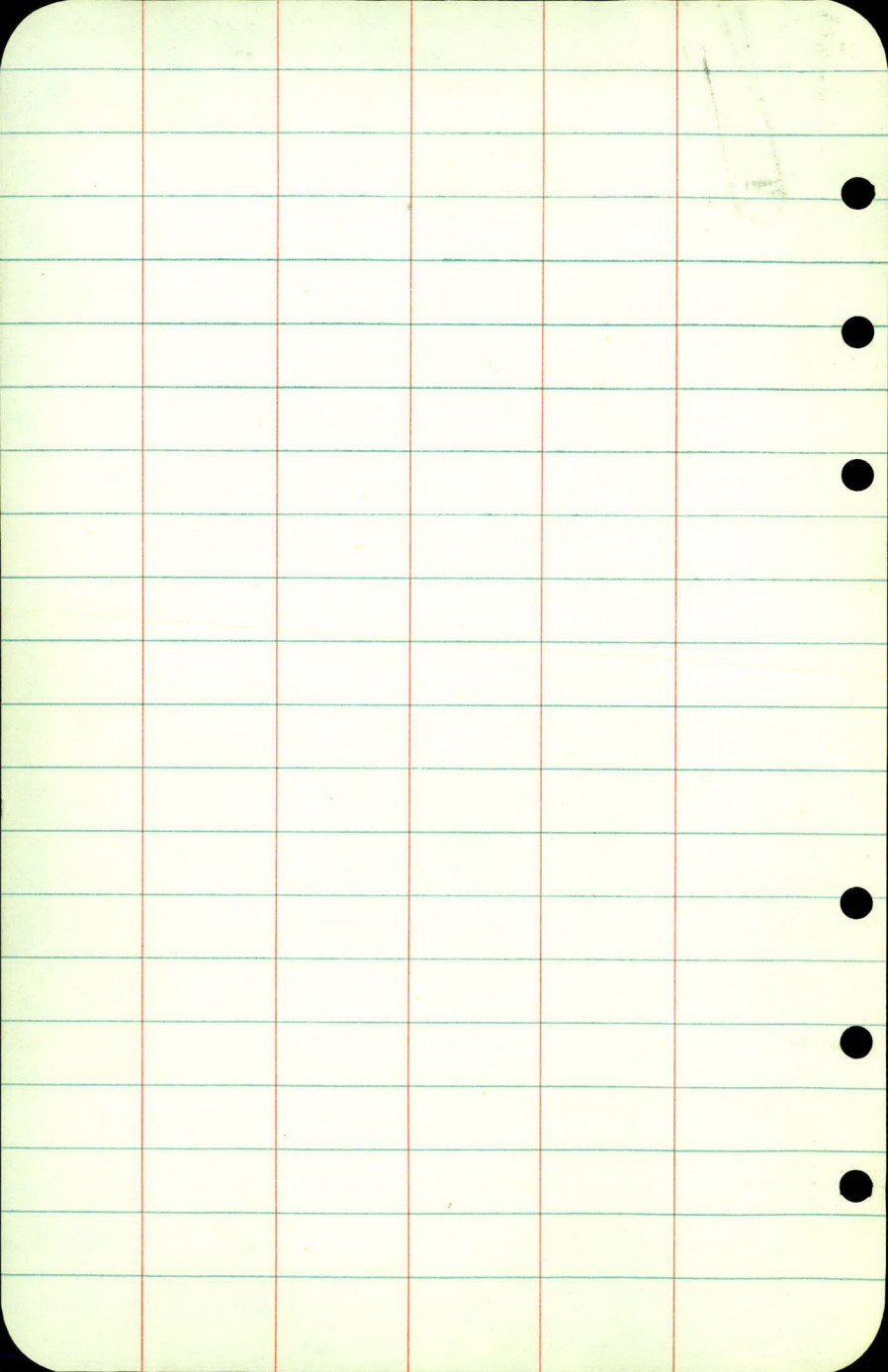


Jan 31, 1964

1

White Bear Ave.

Right of Way at Prosperity



954.31 Top hyd
by Ho #1178 "B"

$17 + 77 = \text{last}$
first X-sec = 18 + 00

22 + 00 has been taken

951.42 - Top Hyd By School

955.10 Top hyd SE
Cor fernwood

Fernwood

x sec thru S.O.⁵ from E

11-10-65

White Bear Ave.

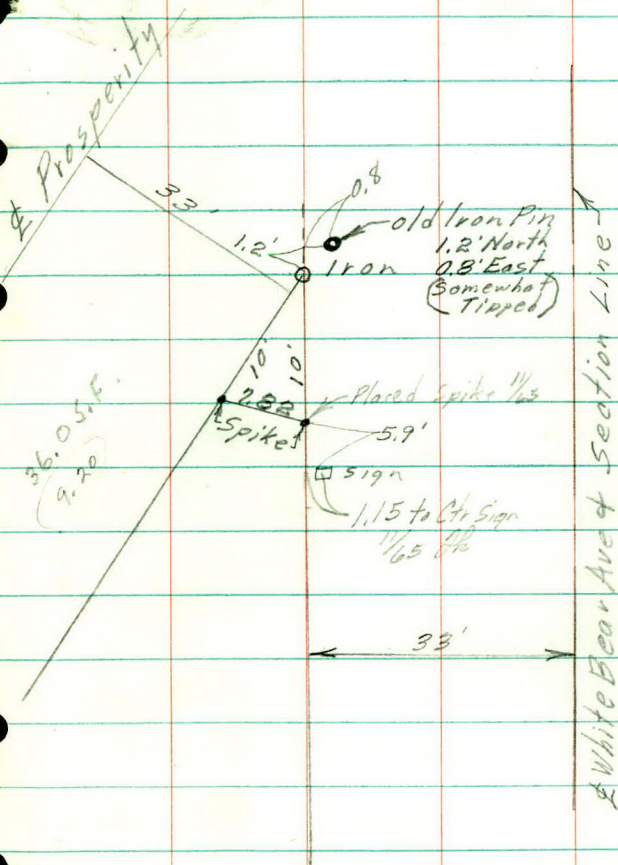
Get dist. to P X sta. ^{sign} from

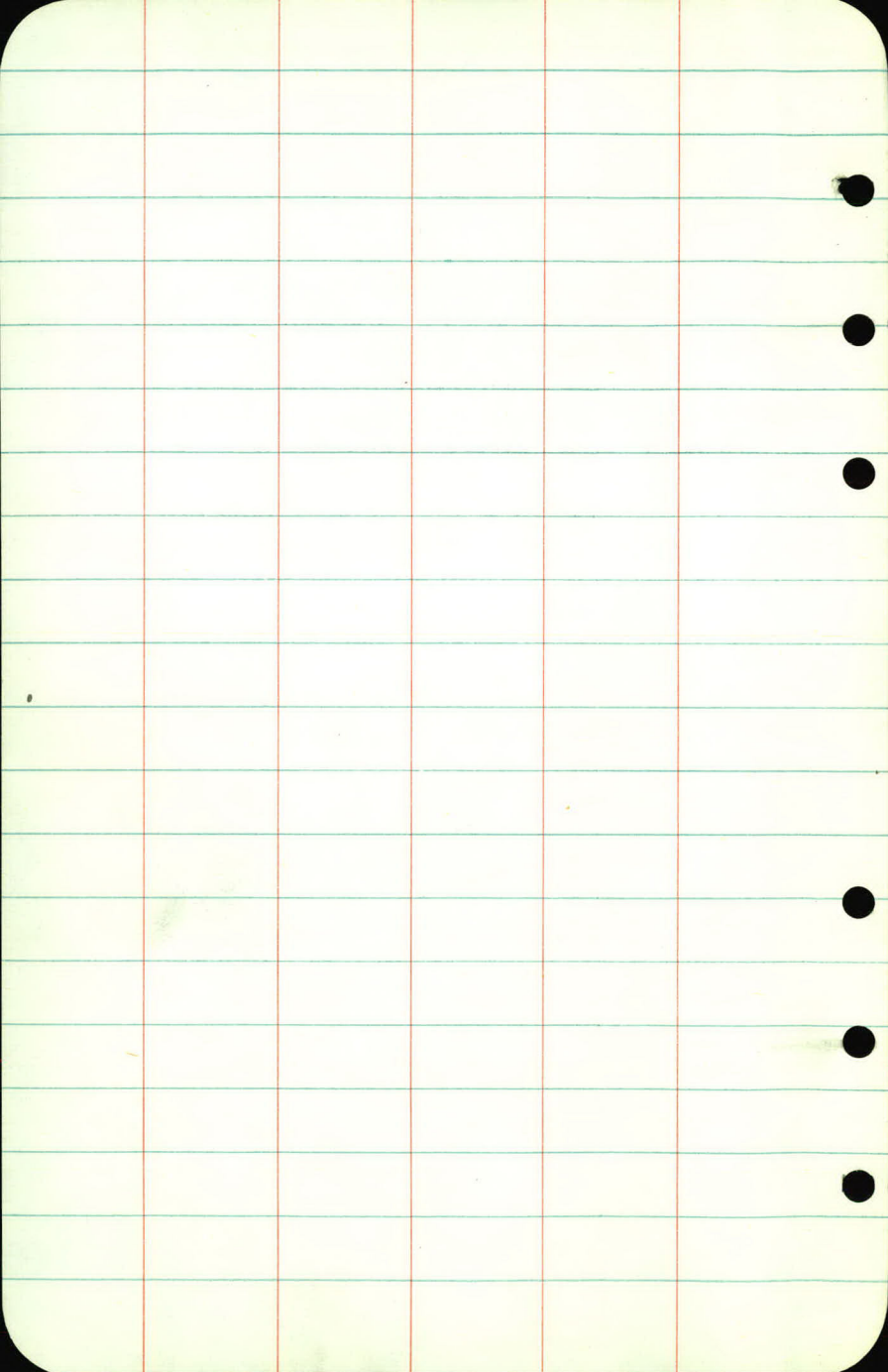
Sec. Line.

FK
JS
FS
DS

Jan. 31, 1964
Clear Fair 25°

2





WHITE BEAR AVE

N.H. ELEVATION

StH + π - elev

B.M. 1.65° 933.66

932.01

19.H.

5.12 928.54

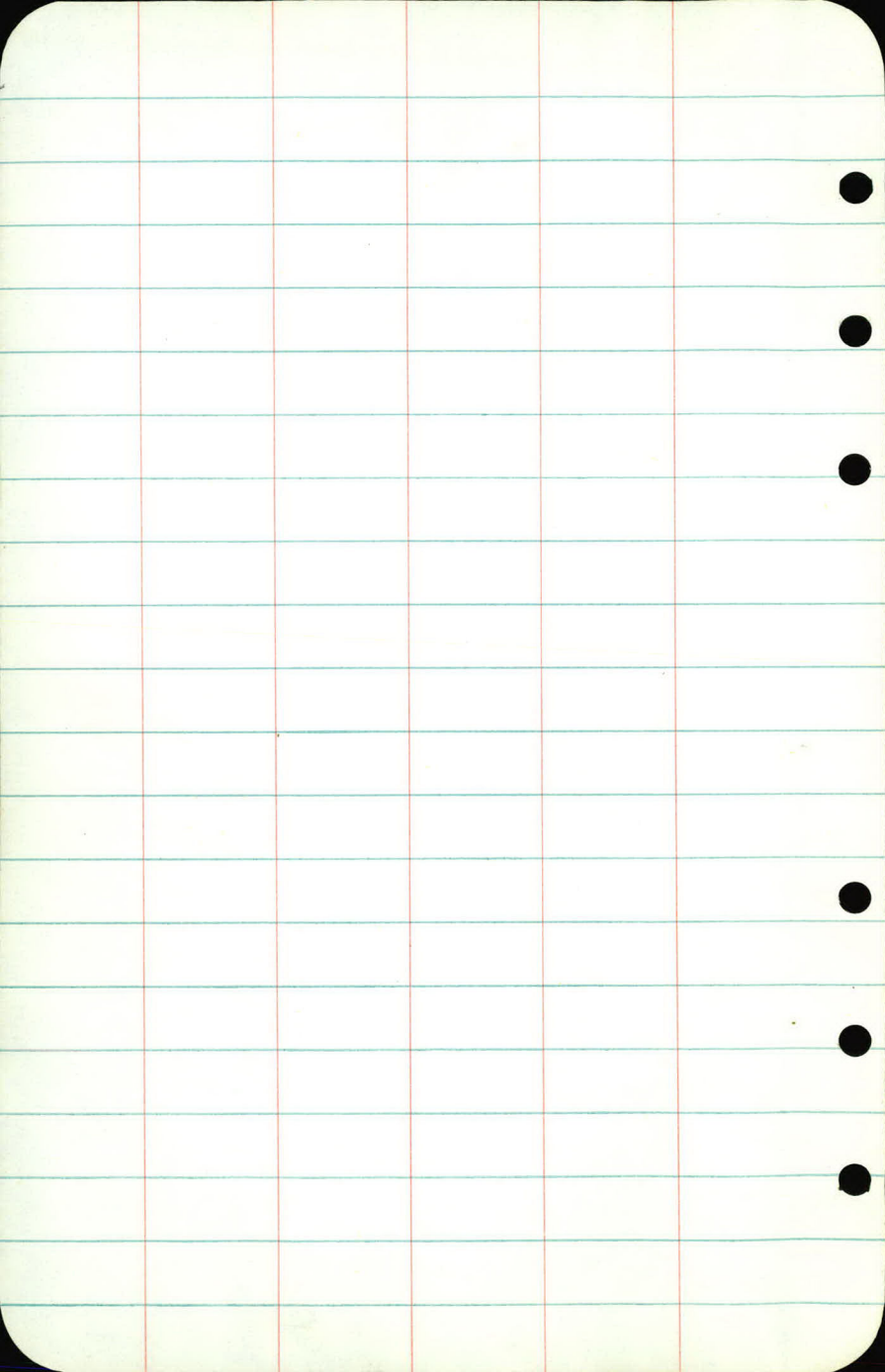
91+00

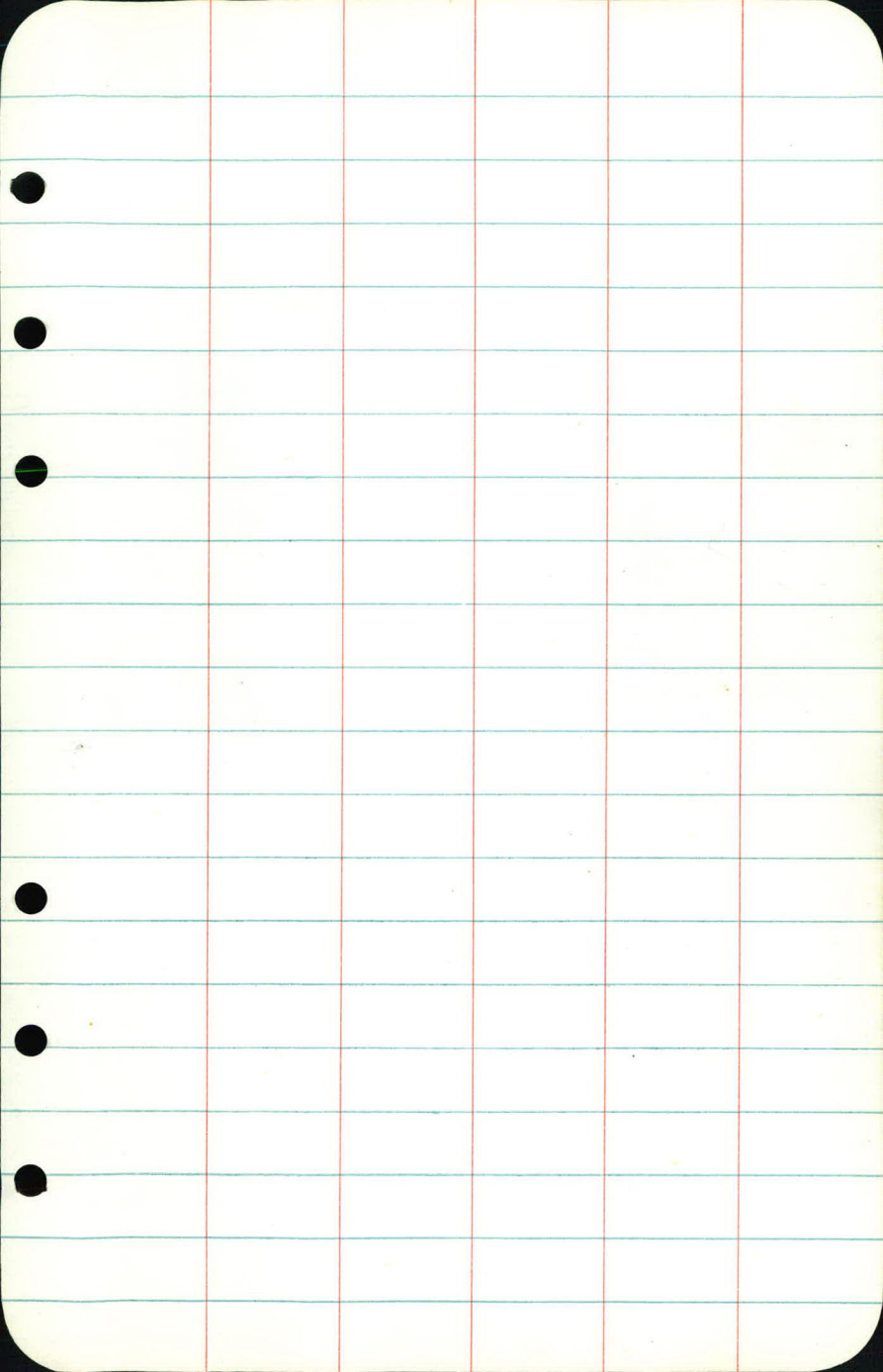
4.98 928.68 928.67

TOP N.W. COR. LOWER STEP HQ. # 2470

89+85 RT 19' - N. RIM.

~~£~~





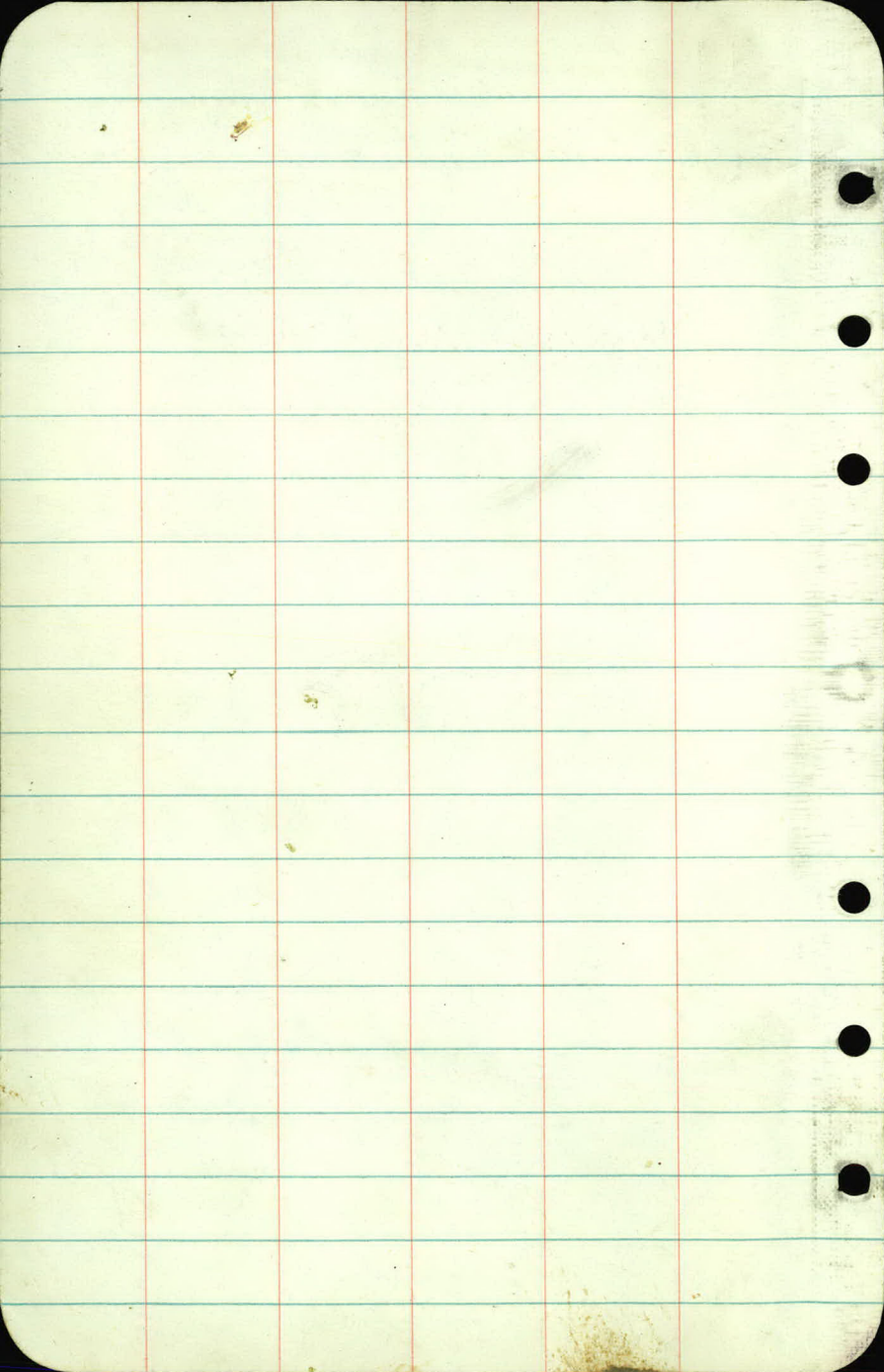
Sta	+	π	-	Hev.
BM	0.19	973.69		973.50

29+70				12.36961.33
-------	--	--	--	-------------

28+00	$\pm$			11.95 961.74
-------	-------	--	--	--------------

Top Hyd at Ramsey County home ^{NE Cor} First & WBA

Garage 90' Lt



White Bear Ave

Sta + X - Elev.

5' x 112.1' C.M. Culvert

Top Culv. 10.08 S. End.

Top Culv. 11.81 N. End

BM 1.14 923.95

(922.81)

21.7

23.3

61.00

41.00

39+78.3

FK
JS
DS
TL

Feb. 20, 1964

Lt.

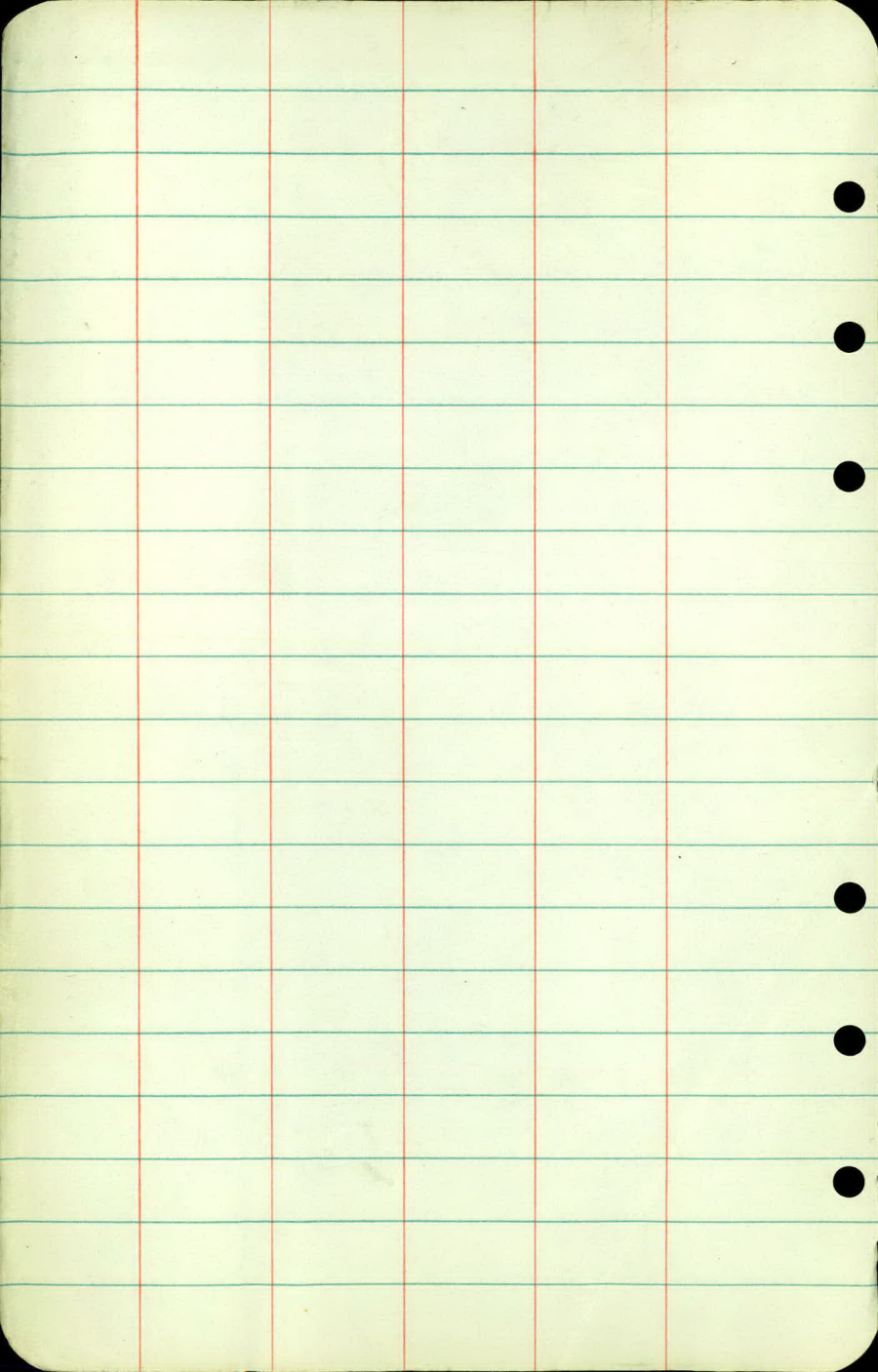
£

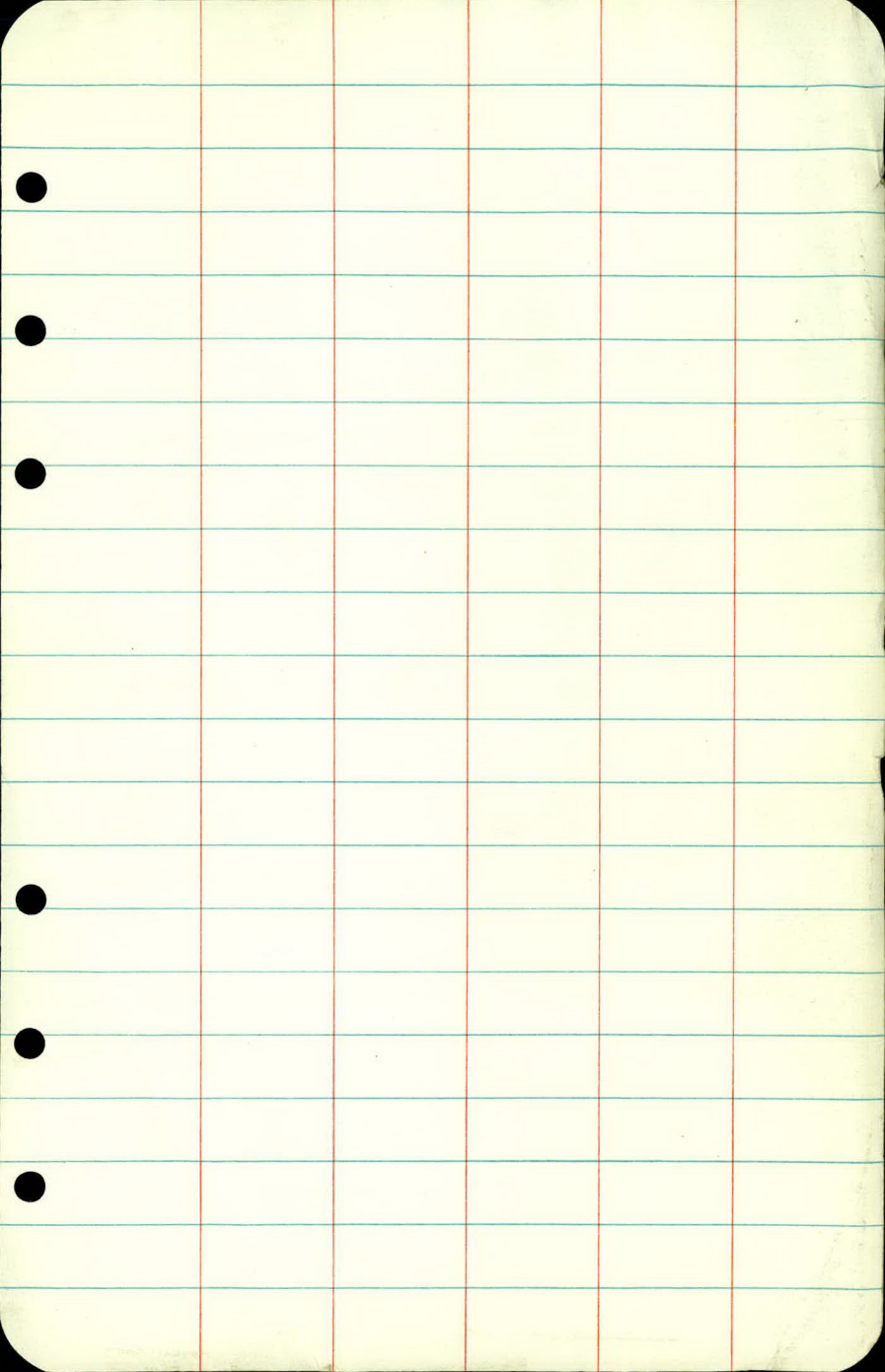
Rt. 2

Top N.W. Cor Conc Base Control Structure

94	8.8	8.3	7.8	8.1	7.4	11.3	7.5	7.8	8.1	90	93
75	67	50	35	19	10		10	16	17	28	50

9.8
75





Sta	+	π	-	Elev
BM	3.23	947.70		944.47
BM			0.78	946.92
TP	4.44	945.04	7.10	940.60
BM			6.81	938.23
Inv Elev. in M.H.			10.23	929.21
			<u>5.62</u>	
			15.83	939.21
TP	3.69	947.89	0.84	944.20
BM			0.97	946.92
BM			3.42	944.47
				944.47

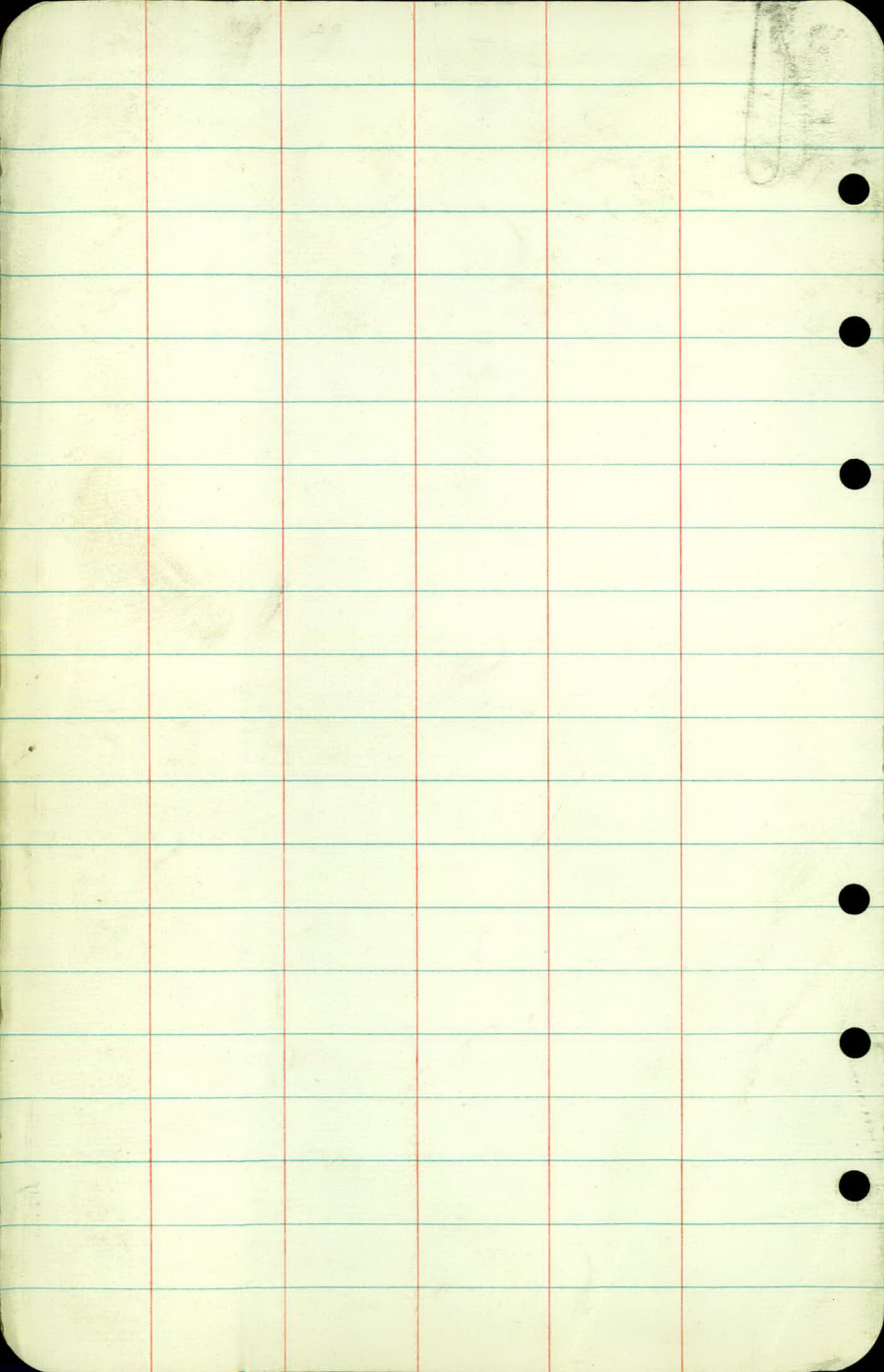
FK
HL
GB

August 31, 1964

● Top Hyd N.W. Cor Orchard Lane & WBA

● Top Hyd S.W. Cor Belland & WBA
West Side White Bear Ave.

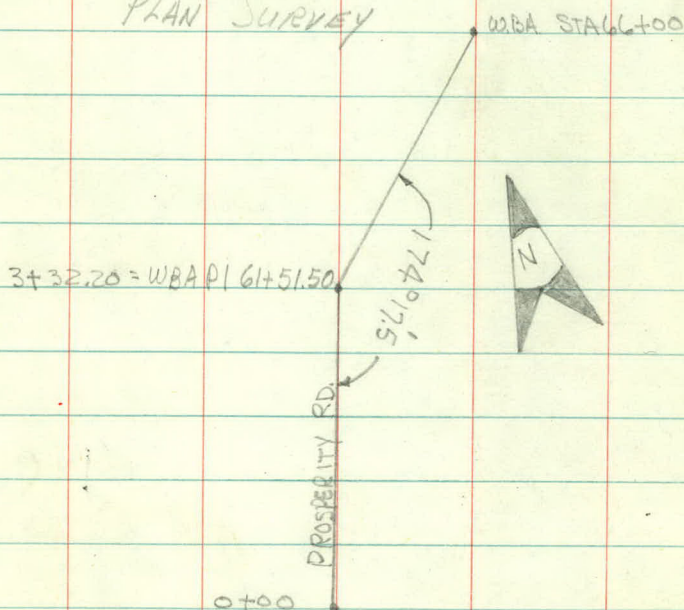
● Top Hyd N.W. Cor Orchard Lane & WBA



15 July 1964 1.

PROSPERITY RD
CO. RD B TO WHITE BEAR AVE

PLAN SURVEY



STA.	POINT	ΔL	ΔR
------	-------	------------	------------

$$3+32.20 = \text{W.B.A. PI STA } 61+51.50$$

0400

PROSPERITY RD.

1740/75

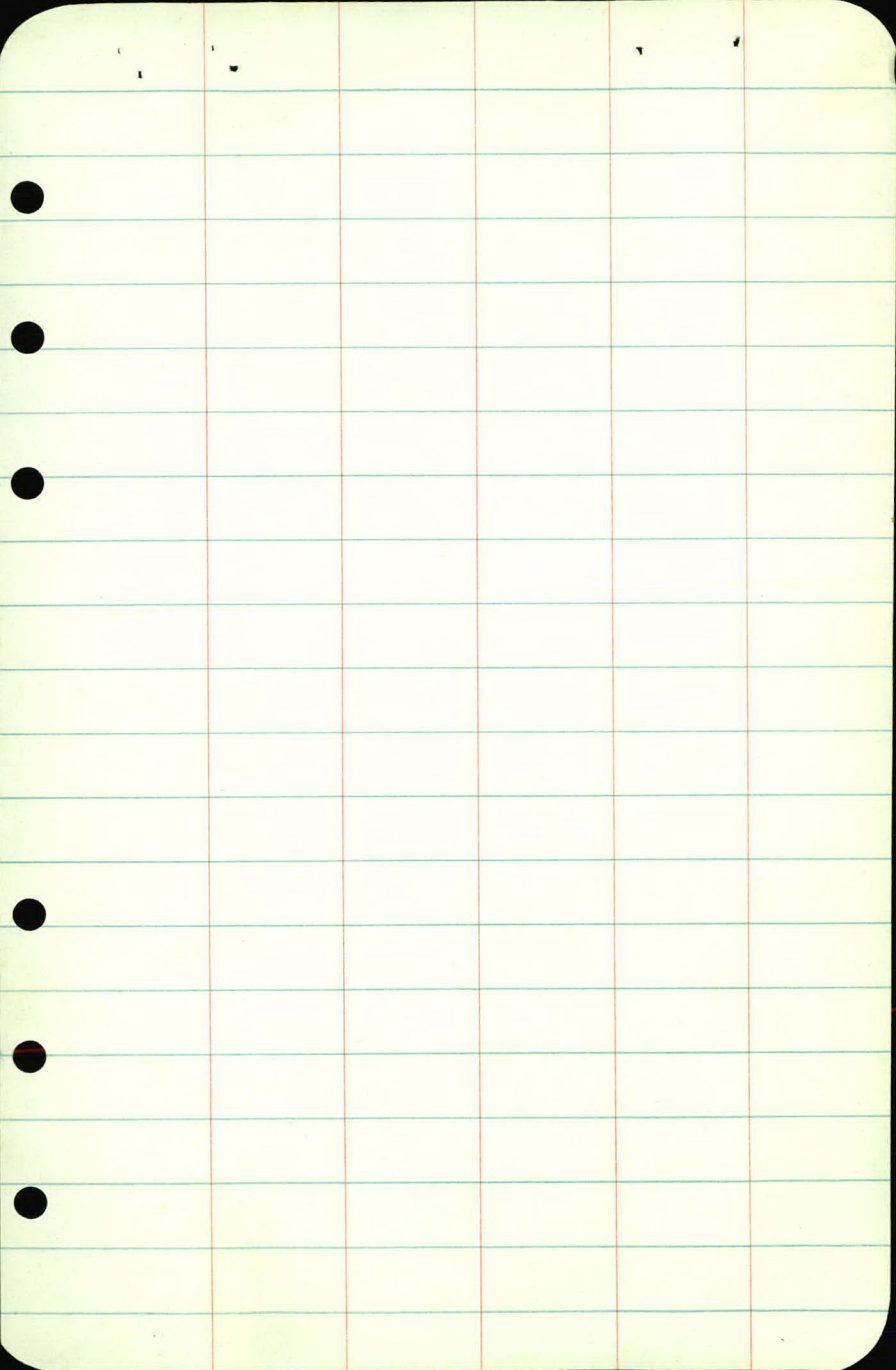
50425

17

4

17

2



15 JULY 1964 3.

PROSPERITY RD.
TOPOGRAPHY

+50

FE
35

BT BT
12 8

+30 W. END 24" STD
27

+25 FE COR
34
+08 PP
57

+14 ER
11
+16 LITE STD
38
+06 POR
18
+06
BR
27

2+00

BT BT
11

+75 ER
28
+70 S. END 18" X 37.0 CM
24
+59 BR
11
+66 POR
14
+55 COR CONC.
40

+50

BT BT
10

+49 LITE STD
40
+34 S. END PUMP 15 (2.5 X 9.0)
56
+16 COR CONC.
40
+14 COR CONC.
55
+19 RT CONC.

1+00

BT BT
10 13

+04 ER
12
+100 POR
15
+75 NW COR BLDG
76
+68 S. END 18" X 36.0 CM
24
+60 LIGHT STD
20
+58 BR
14
+64 RT CONC.

0+50

BT BT
8 15

+49 RT CURB
+35 ER
21
+27 BR
23
+30 POR
22
+23 MH
7

+23 RT STATION

0+00

LAURIERD
33

BT
15

15 July 1964

4

LT

RT

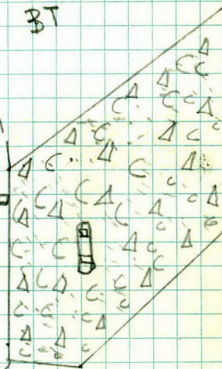
NEW
CYCLONE
FENCE



PROSPERITY RD

GRASS

BT



BT

A.T.O
D-X
STA.
290

E LAURIE RD

MO

GRASS

LT

±

RT

+50

+32.2 = P1

+12.5 RTFE

+08 FE_{cor}

34

3+00

FE
34

+52 RTFE

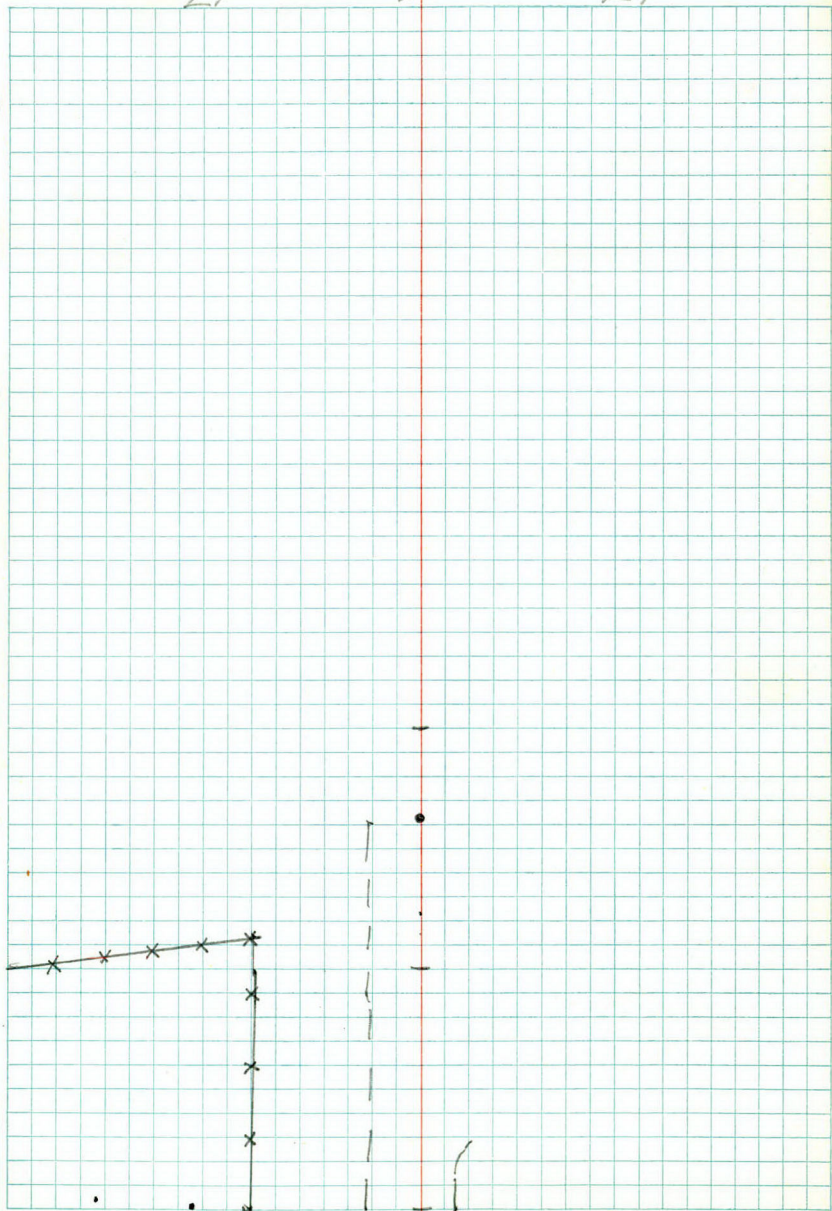
2+50

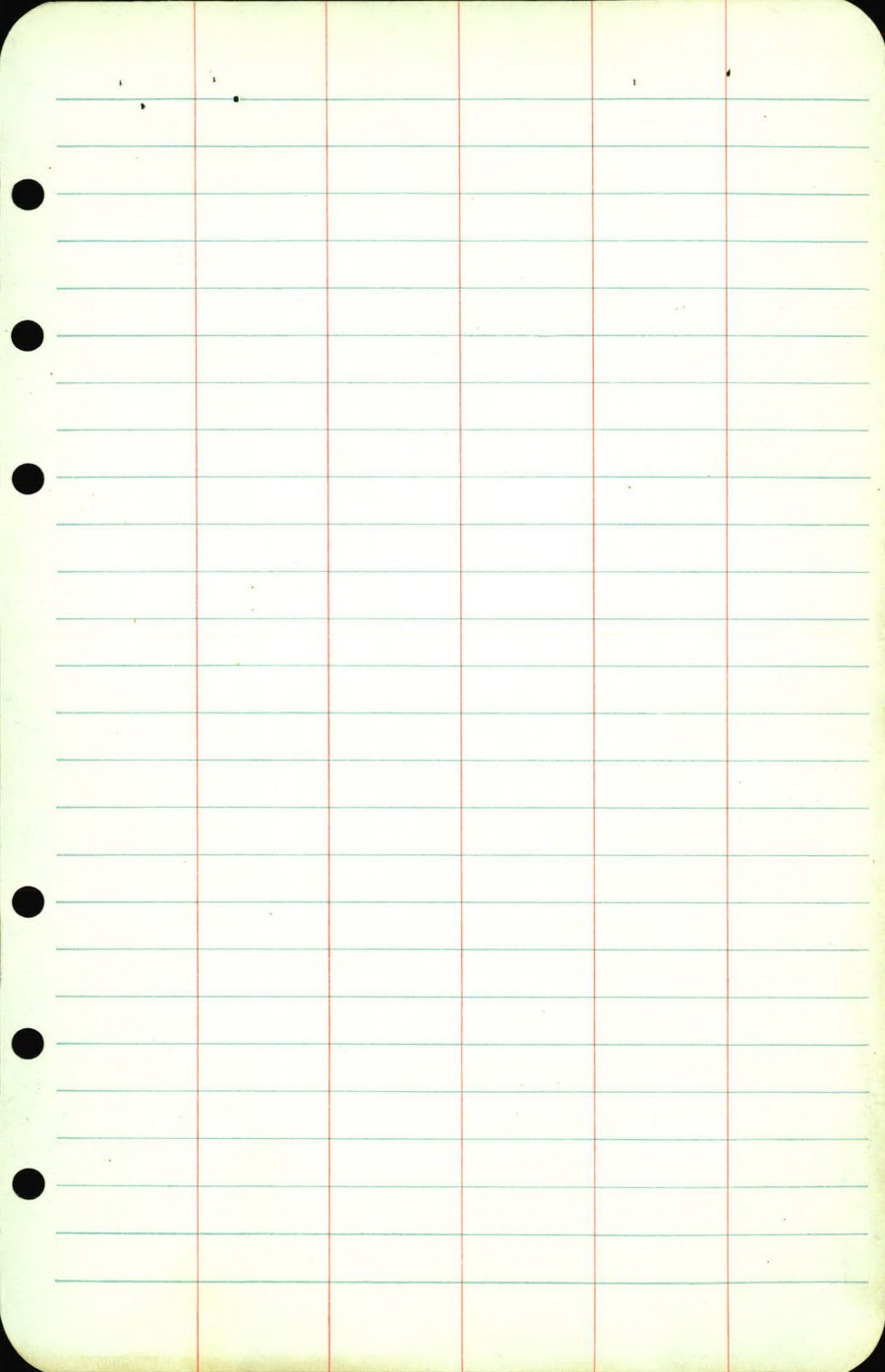
15 JULY 1964 5.

LT

E

RT





15 JULY 1964

6.

PROSPERITY RD.

CO. RD 13 TO WHITE BEAR AVE

X- SECTIONS

STA	+	π	-	ELEV.
-----	---	-------	---	-------

BM	2.52	927.80		
----	------	--------	--	--

(925.28)

0+00

v

+23

4.03

23.77

+50

✓

+68

6.52

21.28

LT

15 JULY 1964 RT

7.

E. EDGE LITE STD 45.0 LT WBA STA 60+38

25.1	25.1	24.4	24.0	23.84	23.6	23.2	22.7	23.6
2.4	2.7	3.4	3.8	3.96	4.2	4.5	5.1	4.2
50	39	20	6		15	20	24-28	33

DITCH

24.3	24.4
3.5	3.4
50	43

TOP MH 7.0 LT

23.6	23.1	23.4	23.5	23.6	23.7	23.2	22.7	24.0
4.2	4.7	4.4	4.3	4.2	4.1	4.6	5.6	3.8
23	21	15	8		13	20	24-28	35

DITCH

24.4	25.4	25.9	24.4
3.4	2.4	1.9	3.4
34	46	50	50

FL SEND 18" CM 24.0 RT

STA

+

 π

-

ELEV.

927.80

0+85 = ~~E~~ ENTRANCE RT.

✓

1+00

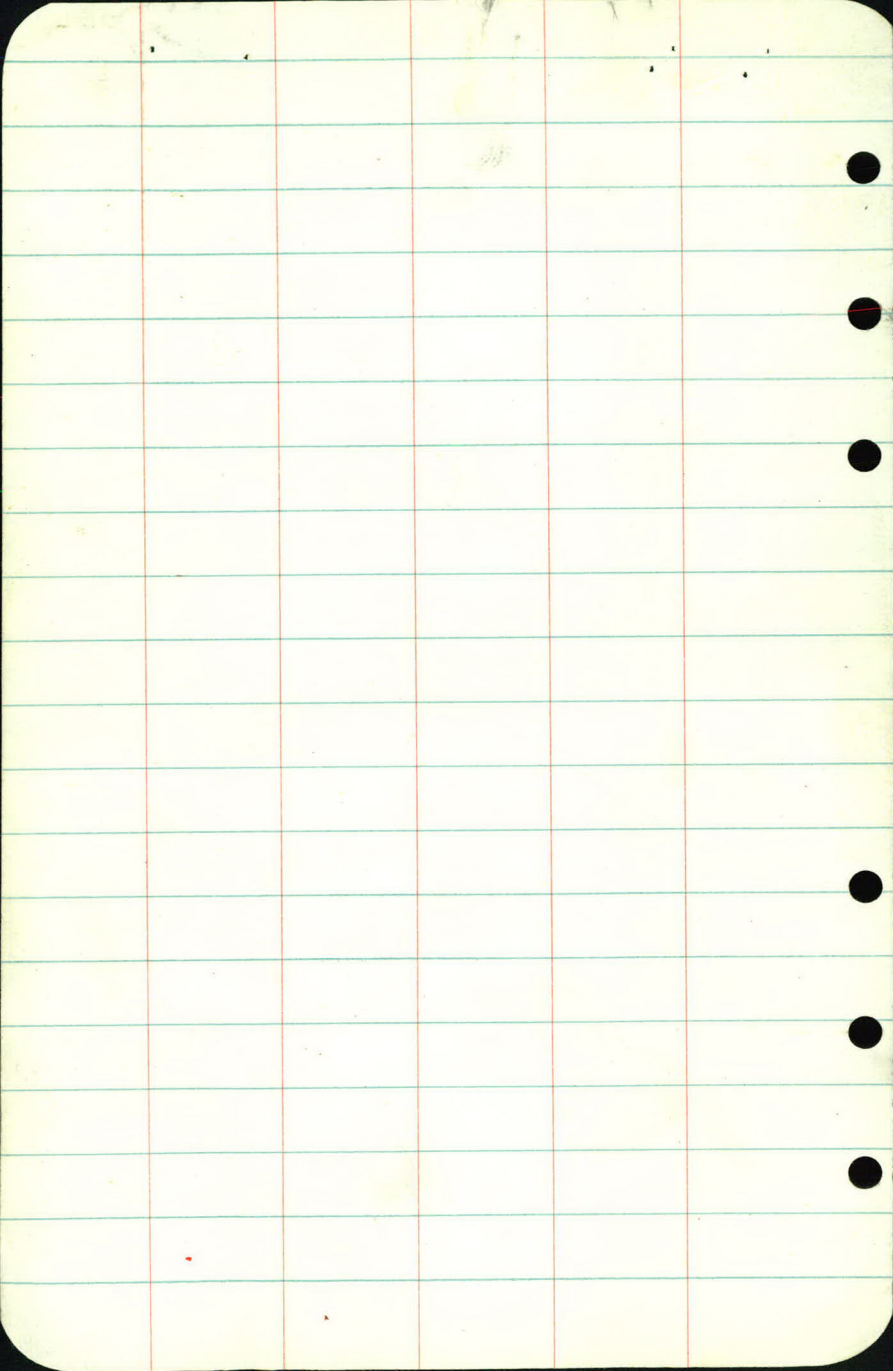
✓

+04

6.76

21.04

+50



LT

15 JULY 1964

RT

10.

FL 24" SCP 270 RT

23.1	22.8	23.3	23.6	23.8	23.7	23.5	23.6
5.8	6.5	5.6	5.3	5.1	5.2	5.4	5.3
35	22-24	18	11		6	16	24
FE	DITCH						

22.6	23.2	23.8	23.6
6.3	5.7	5.1	5.6
50	42	35	30

23.3	22.9	23.2	23.4	23.4	23.3	22.8	22.6
5.6	6.0	5.7	5.5	5.5	5.6	6.1	6.3
26	23-25	22	10		6	12	26
	DITCH						

23.6
5.3
35
FB

E. END LITE STD, 45.0 Lt W. BA STA 60+38

LT

15 July 1964

RT

8.

22.8	23.1	23.4	23.7	23.7	23.6	24.0	24.4
5.0	4.7	4.4	4.1	4.1	4.2	3.8	3.4
21	18	10		10	20	34	50

22.9	24.2	24.7
4.9	3.6	3.1
33	41	50

24.5
2.65
80
6A Floor
3.0
67

22.9	22.7	23.1	23.5	23.77	23.6	23.4	23.5	24.1
4.9	5.2	4.7	4.3	4.03	4.2	4.4	4.3	3.7
24	22	18	10		10	19	26	35

23.4	22.4	25.8
4.4	3.4	2.0
36	43	50

24.9
3.4
50

FL N. END 18" CM 24'0 RT

25.5	23.6	22.2	21.9	23.3	23.6	23.8	23.6	23.1	22.4	23.4
23.42	5.6	5.9	4.5	4.2	4.0	4.2	4.7	5.4	4.4	3.58
50	40	31	22-26	18	11	11	17	22-26	33	40
			DITCH					DITCH		CONC

STA.	+	π	-	ELEV.
------	---	-------	---	-------

		927.80		
--	--	--------	--	--

1470				
------	--	--	--	--

			5.77	22.03
--	--	--	------	-------

+89 = $\angle$ ENTRANCE RT

TP	5.01	928.86	3.95	923.85
----	------	--------	------	--------

2400.

✓

107				
-----	--	--	--	--

			6.86	22.00
--	--	--	------	-------

STA

+

π

-

ELEV

928.86

2+30

8.45

20.41

+50

✓

3+00

✓

BM

3.59

925.27

(925.28)

LT

15 JULY 1964
RT

9.

FL 18" X 37.0 CM 24.0 RT

24.3	23.4	22.0	23.3	23.7	23.9	23.8	23.6	23.8	24.4
3.5	4.4	5.8	4.5	4.1	3.9	4.0	4.2	4.0	3.4
50	42	22-26	19	11		8	16	23	50

DITCH

TOP PK & STA 2+00

22.7	22.2	23.9	23.7	23.9	23.8	23.6	23.5	23.7
6.2	6.7	5.5	5.2	5.0	5.1	5.3	5.4	5.2
29	22-26	16	11		7	11	13	20

DITCH

23.2
5.2
50

24.3
4.6
50

24.0
4.9
34

FL N END 18" CM 24.0 RT