

BK. 56 Dr. 14

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan.....Survey

Shady Lane, (W.B.C.)

From Lake Ave. To S.T.H. #61

Road Acc't. No.

Date Filed 8-15-49 File

Plan Survey

Shady Lane

Lake Ave to S.T.H. #61

Alignment pages 1-2

Topography " 3-6

X Sections 7-14

5-3-49

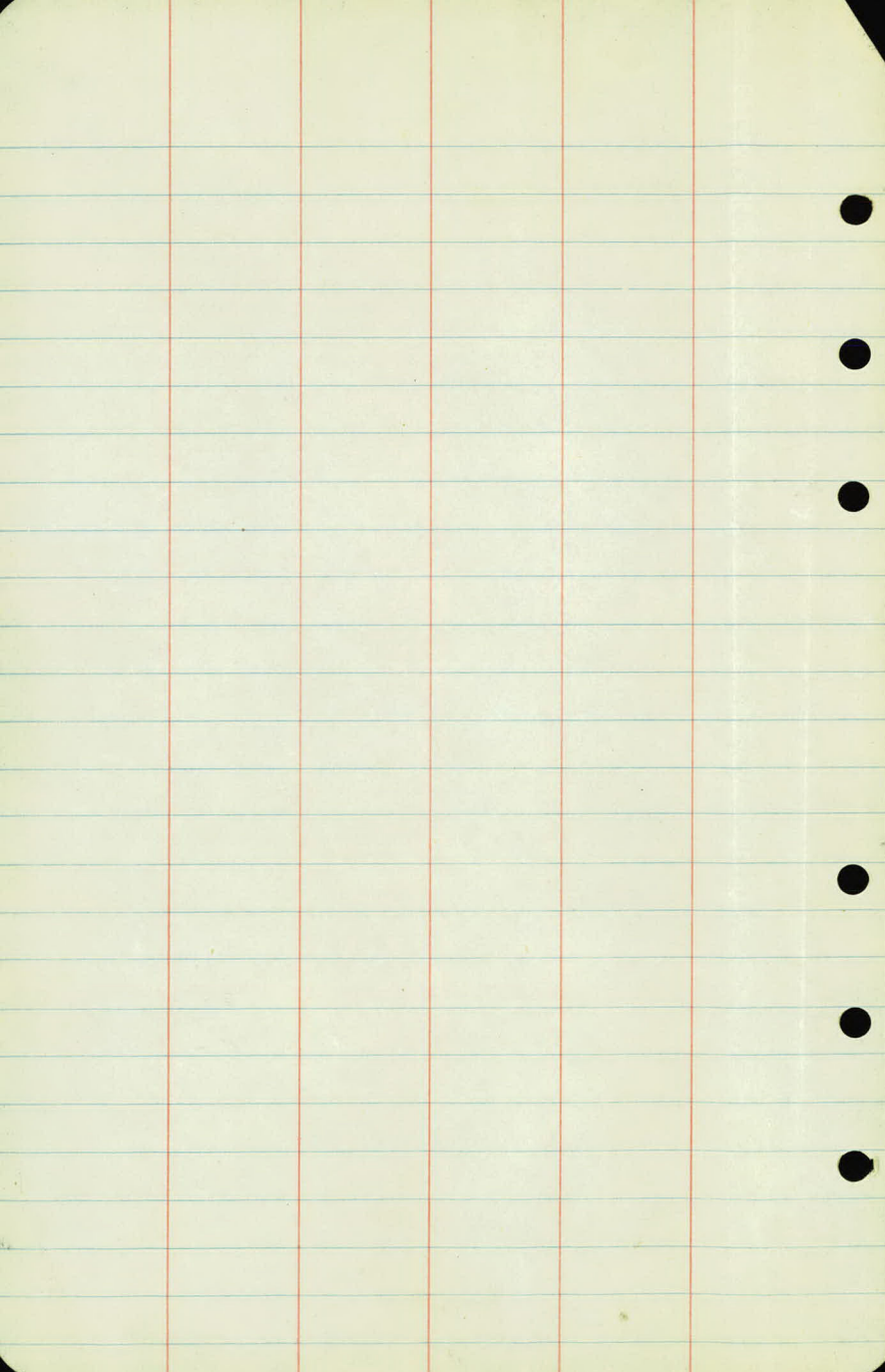
To 5-4-49

G/B A.K.

Rec 5/5/49
L.C.

M/B

B/C



1

Alignment

5-2-49

GB

MB

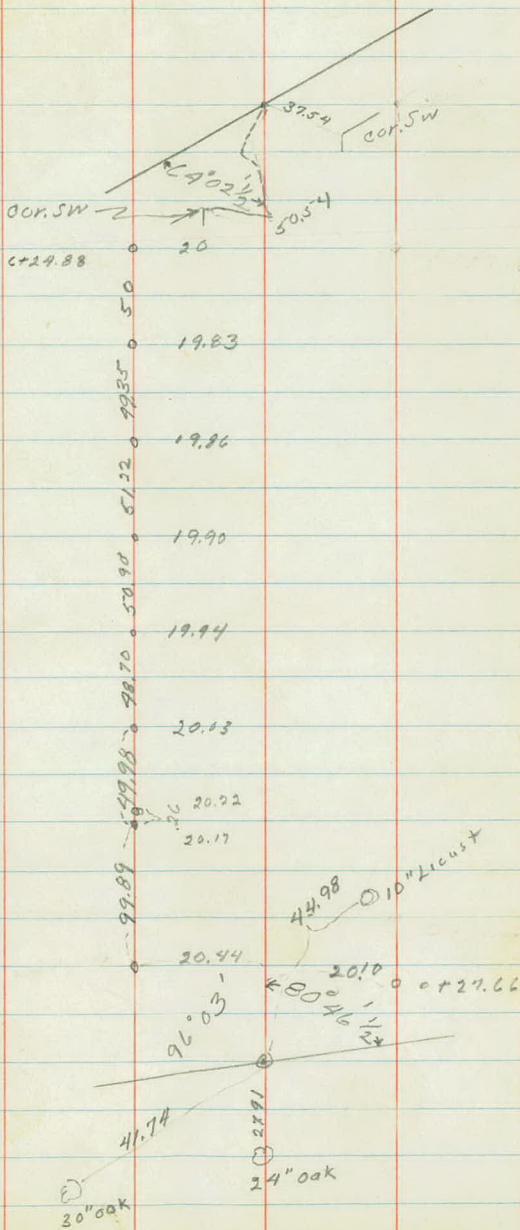
BC

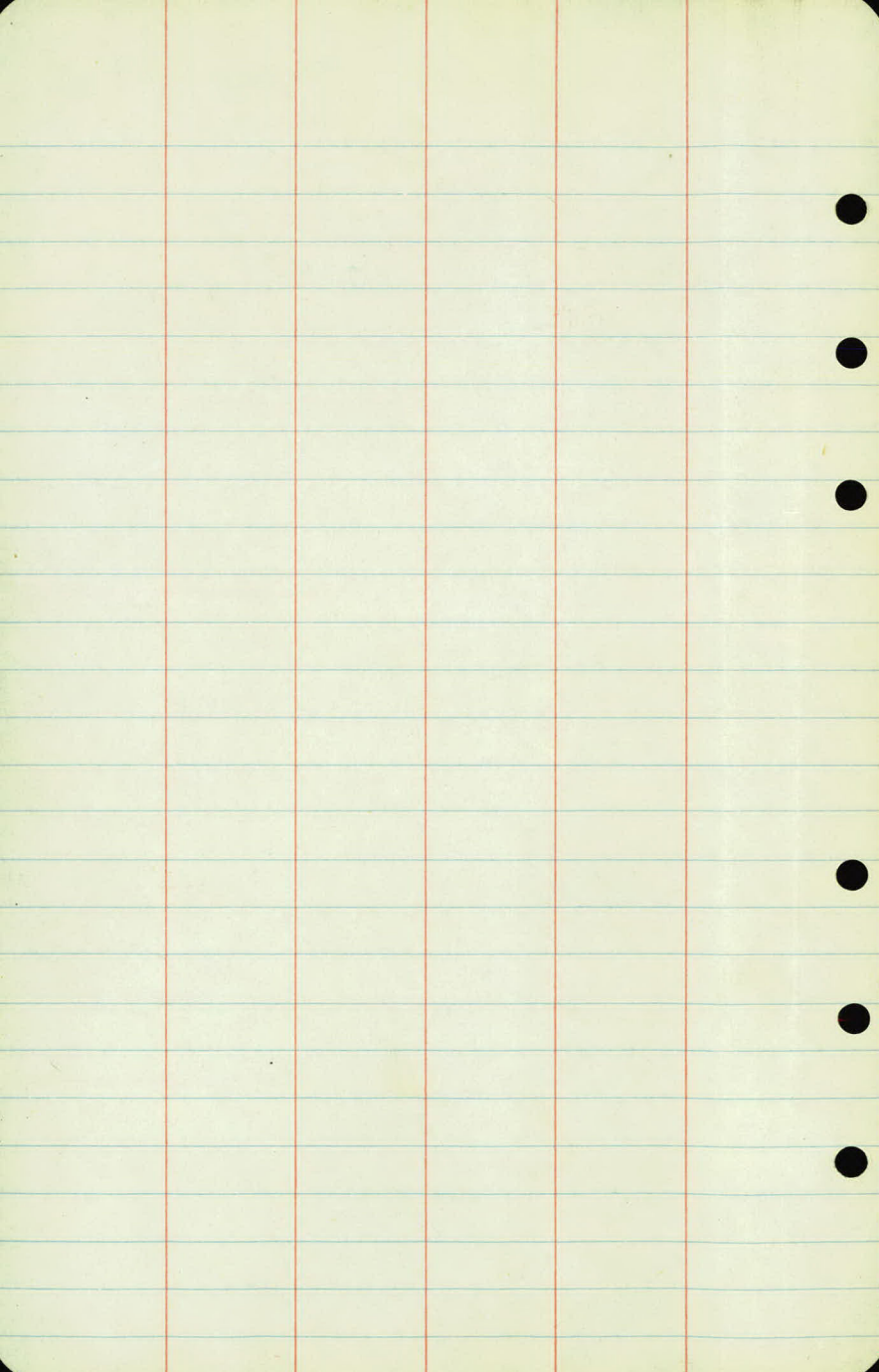
7+51.23

STH # 61
10

0+00

@ Lake Ave





Topography

SHADY LANE
LAKE Ave to S.T.H. #61

5-4-49

G.B.

M.B.

B.C.

end Rod 2' SW 32, SW 20' 10 10

+ 85 SE cor. Ho 37.

+ 90 NW cor. 48

+ 94 end SW - 19

+ 90 2' Conc Drive - 19

+ 86 end Rod 2' Cor. SW - 20.

+ 70 42" Turn Elm - 26

+ 75 2' Elm SW - 20.

+ 59 SW cor. 48 50'

+ 54 15' BE 21'.

+ 63 2' 3' Ent SW

+ 50 15' BE 26

+ 50

+ 26 Hedge W - 25.

+ 25 PP 14'.

+ 25 6" x 15' Ret Wall - 20.5

+ 20 NE cor. Ho 38.

+ 15 2' 9' Ent SW

+ 40 Big SW 4 1/2' - 19'

+ 28 24" Elm - 34'

+ 20 2' Ent

2

SW 20.4 11 11

+ 96 SE cor. Ho 38.

+ 92 2' Ent SW - 20.1

+ 86 30' Elm 22'

+ 71 2' Conc Drive 10' -

+ 69 2' SW - 18.5

+ 37 2' Ent SW

+ 49 2' SW - 18

+ 30

+ 48 20" Oak. 20'

+ 18 2' Elm - 22

+ 15 1' Pine - 38

+ 68 1' Pine - 31

+ 04 1' Pine - 41

+ 15 PP - 15

+ 1

SW 20.7 11 10

+ 96 Stump - 38.

7

+ 94 8" Turn B. Loc. - 29'

+ 93 8" Turn B. Loc. - 25'

+ 50

+ 23 Arc L.P. - 15

+ 21 End Curb 13.5'

+ 18 ins. inside SWs 20.0

+ 20 MH 2 (B. 95 data)

+ 28 W Side B/L

+ 19 end Rod 13'

+ 11 Bay Rod 19'

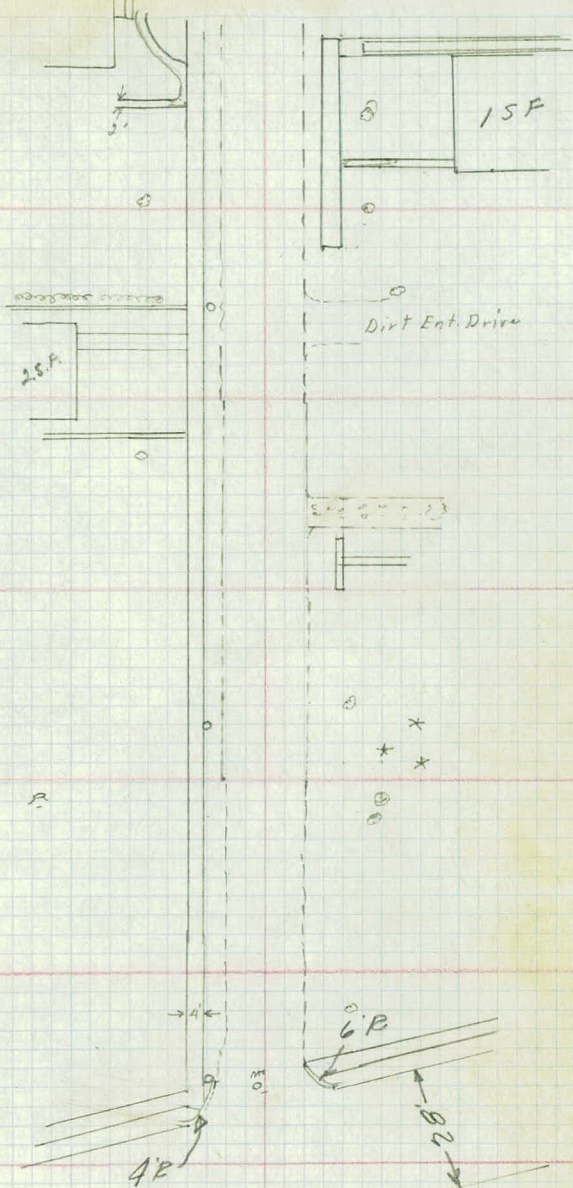
+ 41 8" B. Loc. 27'

+ 28 end Curb 10'

+ 25 end Rod 18' Nodge 6' SW

+ 19 Bay Rod 18'

0+00



Note - Dist. M to Face
of all Trees,
pp - w. Shut. off & M
to E

6 SW 19.7
 +94 SE Cor. Ho 38
 +94 20" Elm - 21
 +68 W. 50 15.5
 +69 Bush - 26
 +66 NE Cor Ho 40
 +57 24" Elm - 20
 +54 2' SW ent

11 SW 20
 +78 18" Elm - 25
 +77 end 4' Hedge - 21
 +91 2' SW ent
 +84 12" Elm - 25
 +73 18" Elm - 25
 +64 20" Elm - 25
 +57 Beg Hedge - 21
 +54 15' BE - 47

+54 2
 +95 SE Cor. Ho - 40
 +26 60' Hedge W - 24
 +26 30' Elm 21
 +26 PP - 14
 +18 NE Cor. Ho - 39
 +15 2' SW Ent

+43 NW Cor. Ho 50
 +43 18" 21
 +32 11' - 3' (10.53' to EL)
 +30 2' SW ent
 +17 SW Cor Ho. 50
 +07 Beg 4' SW - 12.6 - 15.6
 +07 PP - 14
 +04 18" SW Ent 20
 +01 NW Cor Ho - 49

5 SW - 19.7, 11 10

+74 Hedge W - 21
 +69 - NE Cor Ho - 36

+98 2" ? - 37
 +78 1" ? - 27
 +68 SW Cor. Ho 40
 +64 2' Drive
 +56 - 8" Elm - 26

+59 2' SW Ent
 +53 10" Elm - 21

+48 SE Cor. Ho 36
 +38 2' BIA Top Drive
 +23 PP - 15
 +23 Hedge W - 22
 +17 NE Cor Ho 38
 +14 2' SW ent

+43 - 12" Elm - 26
 +15 - 10" Elm - 26
 +06 - 18 Elm - 20

4 SW 19.5

+97 SE Cor. Ho - 38
 +89 - 18" M - 21
 +82 2' Conc ent + 20.14
 +78 39" M - 42
 +68 18" Elm 21
 +66 NE Cor Ho - 39
 +54 Rad 2' SW around t. - 22
 +54 2' SW Back of t.
 +54 21" M - 21

10 10
 +93 20" Elm 20
 +87 2' 3' SW - 19
 +87 2' Conc Slab (6x4) 15
 +79 30" Elm - 20
 +72 SW Cor Ho - 44
 +99 - NW Cor Ho 44

+28 W Shot off 14.5
 +25 11' A - 14
 +24 Hedge W 12
 +18 10' Conc ent 10-12
 +17 W Shot off 15
 +13 NE Cor Ho - 37
 +12 - 18" BE - 22

+48 2' 10' Drive
 +45 NW Cor. Ho 53
 +16 SW Cor Ho 55
 +16 2 1/2' ent + SW - 20

3

+96 NW cor. Ho. 5

+68 SW cor. Ho. 50

25F

0.74

25F

- +99 SE cor. Ho. 39
- +95-18" H-21

25F

145' SHP

Sloped with Blk Top

25F

dirt

15F

15' Conc Drive

- +42 SE cor. Ho. 39
- +41 10" BE 21
- +37 18" M-30
- +29 8 35 & 15' Conc Drive - 20'
- +32 8 10 Conc Ent 16-12'

dirt

- +32 Sedge 6" SW - 60
- +27 Edge Brk. - 0
- +9 end SW E 14.5
- +08 12" Elm - 37
- +08 12" VCR - 29

11 SW 20.5

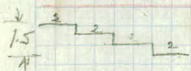
- +93 15" Ent Drain 12'
- +93 M H 13
- +93 20" Elm - 25
- +86 NW cor Ho - 48
- +74 4" SW Ent.
- +66 10" Birch - 36
- +62 SW cor Ho - 48
- +53 20" Elm - 25

- 7
- +85 beg 6' cone steps 20.9-14.9
 - +85 end 4' SW R. 9
 - +16 F. Hd - 14'
 - +7.7 5" SW 50'
 - +71 30" O - 27'

- +26 PP - 14'
- +25 Hedge 4" W - 21
- +15 N.E. cor Ho 38
- +11 4" SW ent.

- +27 24" Oak - 40
- +13 20" Ent dirt.

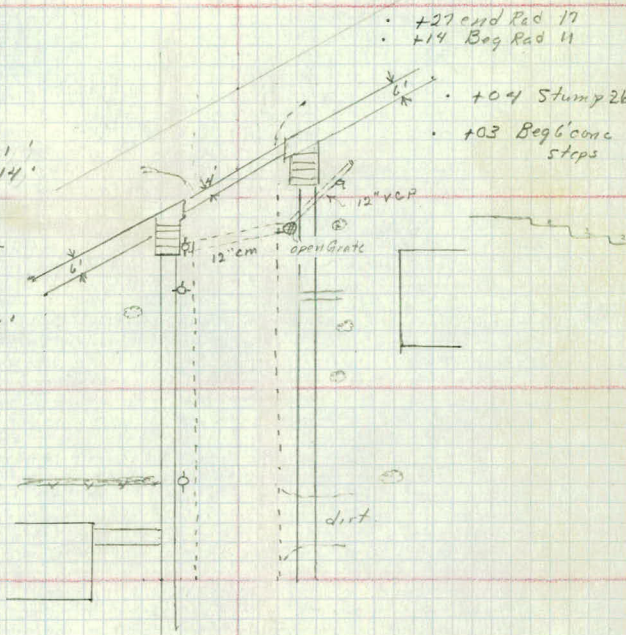
- +09 end Rad 21'
- +02 Beg Rad 14'

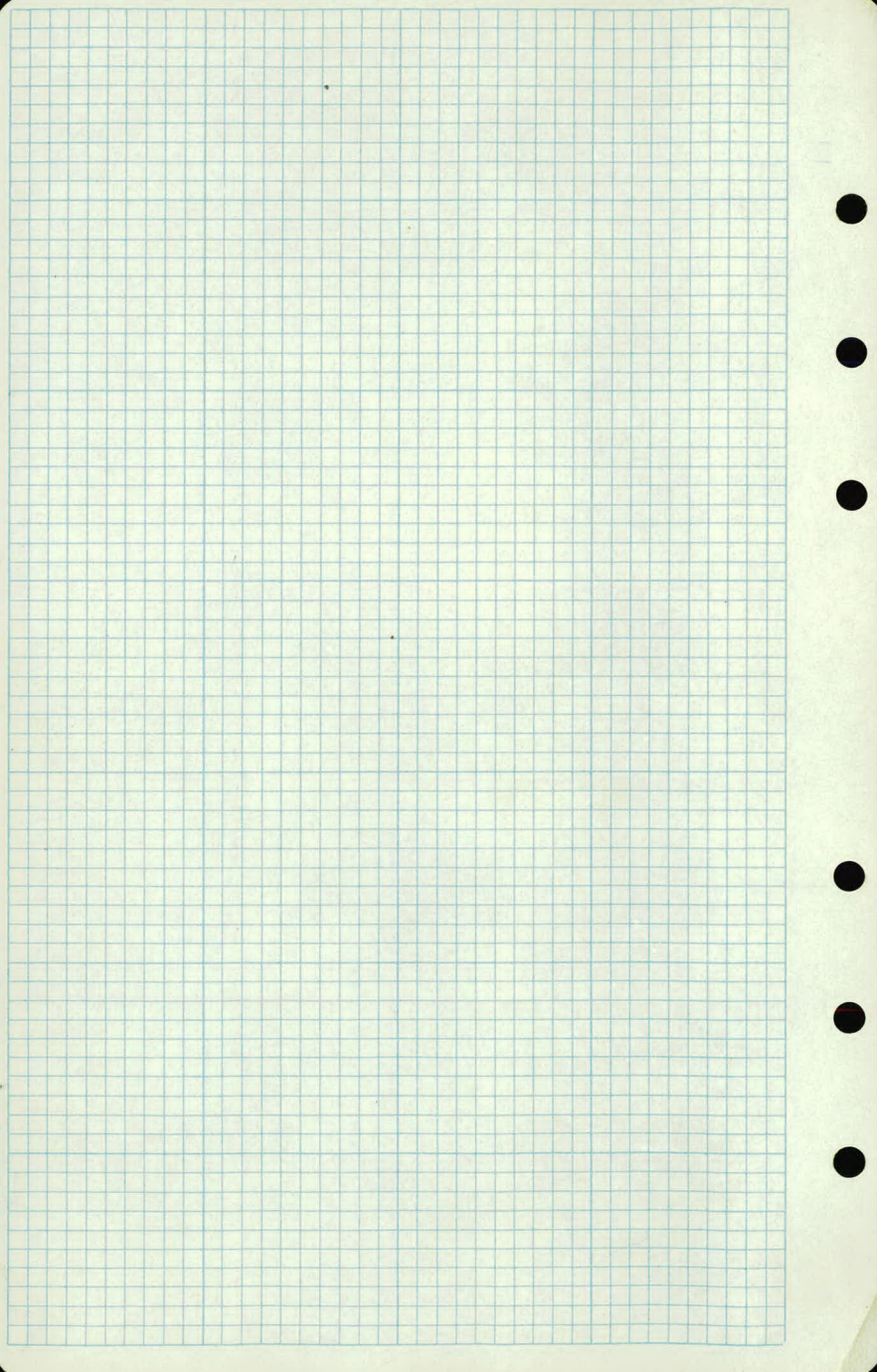


- +95 end SW 14'
- +88 15' SW -11
- +88 PP-19

- +27 end Rad 17
- +14 Beg Rad 11

- +04 Stump 26
- +03 Beg 6' conc steps





X Sections

Sta	+	π	-	Elev	
BM	0.88	943.26		942.38	
check,			4.37	938.89	38.90
New BM	4.42	943.17	4.51	938.75	
old BM			3.82	939.35	"
0+00				37.53	
- 12		Gutter,		37.1	
- 22				37.6	
- 33				30.6	
- 43				26.2	
+14		Gutter		37.5	
+14		Top Curb		37.5	
T.P.	4.22	943.57	3.82	939.35	
+19				37.5	
		Side Walk Profile E & W			
+28				37.1	

Lt

L

Rt

Top Hyd. NE Cor. Burson Ave & 1st St.
 5TH & 1st.

Top Hyd NW Cor. Shady Lane & 5THth 61

RR Spkin PP 105' N & Lake Ave Lt,

$$\frac{5.9}{67} \quad 5.64 \quad \frac{5.6}{50} \quad \frac{5.6}{100} \quad \checkmark$$

6.1

5.6

12.6

17.0

$$\frac{6.3}{50} \quad \frac{6.2}{30} \quad \frac{6.1}{14} \quad 5.7 \quad \frac{5.8}{13.5} \quad \frac{5.9}{18} \quad \frac{5.9}{50} \quad \checkmark$$

$$\frac{5.9}{50} \quad \frac{5.8}{30} \quad \frac{5.6}{14} \quad \frac{6.0}{13} \quad 5.7 \quad \frac{5.8}{13.5} \quad \frac{5.65}{21} \quad \frac{5.5}{50} \quad \checkmark$$

Spk in P.P.

$$\frac{6.0}{50} \quad \frac{5.9}{20} \quad \frac{6.04}{14} \quad \frac{6.5}{13} \quad \frac{6.09}{T/14} \quad 6.1 \quad \frac{6.2}{11} \quad \frac{5.86}{12} \quad \frac{5.9}{21} \quad \frac{5.9}{50} \quad \checkmark$$

$$\frac{5.5}{20} \quad \frac{5.60}{21} \quad \frac{5.63}{17} \quad \frac{5.8}{14} \quad \frac{6.3}{12} \quad 6.5 \quad \frac{6.0}{10} \quad \frac{5.9}{11} \quad \frac{6.0}{20} \quad \frac{5.8}{50} \quad \checkmark$$

SW

1

Sta + π - Elev

943.57

+50

37.7

1.

38.2

+50

38.3

2

38.4

+38

38.5

+40

end S.W.

38.5

+47

38.5

L +

Q

-

38.01

SW

38.01

$$\frac{5.7}{30} \frac{5.4}{24} \frac{5.57}{21}$$

$$\frac{5.56}{17} \frac{5.6}{14}$$

$$\frac{6.2}{12}$$

$$5.9$$

$$\frac{6.0}{8}$$

$$\frac{5.7}{11}$$

$$\frac{5.9}{30}$$

$$6.2$$

✓

38.07

38.02

$$\frac{5.6}{24}$$

$$\frac{5.56}{21}$$

$$\frac{5.95}{17}$$

$$\frac{5.4}{16}$$

$$\frac{5.4}{14}$$

$$\frac{5.8}{11}$$

$$5.4$$

$$5.4$$

$$\frac{5.4}{7}$$

$$\frac{5.7}{10}$$

$$\frac{5.4}{15}$$

$$\frac{5.6}{19}$$

$$\frac{5.8}{21}$$

$$\frac{6.0}{30}$$

$$6.0$$

✓

$$\frac{5.4}{30}$$

38.15

38.16

$$\frac{5.6}{30}$$

$$\frac{5.42}{20.4}$$

$$\frac{5.71}{16.4}$$

$$\frac{5.3}{15.12}$$

$$\frac{5.1}{9}$$

$$5.3$$

$$\frac{5.3}{7}$$

$$\frac{5.1}{11}$$

$$\frac{5.5}{17.5}$$

$$\frac{5.8}{22}$$

$$\frac{6.0}{30}$$

$$6.0$$

$$6.0$$

✓

SW

38.15

SW

5.42

Gar. Floor

$$\frac{4.0}{38}$$

38.42

38.44

$$\frac{4.8}{30}$$

$$\frac{5.15}{20.4}$$

$$\frac{5.13}{16.4}$$

$$\frac{5.4}{14}$$

$$\frac{5.3}{11}$$

$$5.2$$

$$\frac{5.4}{8}$$

$$\frac{5.8}{12}$$

$$\frac{5.4}{17}$$

$$\frac{5.9}{23}$$

$$\frac{6.1}{30}$$

$$6.1$$

$$6.1$$

$$6.1$$

✓

38.47

38.72

$$\frac{3.7}{30}$$

$$\frac{4.0}{25}$$

$$\frac{4.80}{20.4}$$

$$\frac{4.85}{16.4}$$

$$\frac{5.4}{12}$$

$$5.1$$

$$\frac{5.3}{8}$$

$$\frac{5.8}{12}$$

$$\frac{5.6}{22}$$

$$\frac{5.9}{30}$$

$$5.9$$

$$5.9$$

$$5.9$$

$$5.9$$

$$5.9$$

$$5.9$$

✓

38.71

38.27

SW

SW

$$\frac{3.7}{30}$$

$$\frac{4.0}{25}$$

$$\frac{4.80}{20.4}$$

$$\frac{4.85}{16.4}$$

$$\frac{5.4}{12}$$

$$5.1$$

$$\frac{5.3}{8}$$

$$\frac{5.8}{12}$$

$$\frac{5.6}{14.5}$$

$$\frac{5.9}{18.5}$$

$$5.27$$

$$5.27$$

$$5.27$$

$$5.27$$

$$5.27$$

✓

38.77

$$\frac{3.7}{30}$$

$$\frac{4.0}{25}$$

$$\frac{4.80}{20.4}$$

$$\frac{4.85}{16.4}$$

$$\frac{5.4}{12}$$

$$5.1$$

$$\frac{5.3}{8}$$

$$\frac{5.8}{12}$$

$$4.6$$

$$4.5$$

$$4.6$$

$$4.5$$

$$4.6$$

$$4.5$$

$$4.6$$

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

943.51

+70

38.5

3

38.6

+18

Profile Drive way Left.

+18

38.6

+32

38.6

TP.

3.99

942.63

4.93

938.64

50

38.5

82

38.4
Prot. Driveway Lt

Lt

Q

Rt

$$\begin{array}{cccccccccccc}
 \frac{3.5}{30} & \frac{3.6}{25} & \frac{39.06}{45.1} & \frac{38.71}{4.00} & \frac{5.2}{13} & 5.1 & \frac{5.2}{7} & \frac{5.4}{13} & \frac{38.32}{5.20} & \frac{5.19}{14.1} & \frac{4.3}{18.6} & \frac{4.3}{22} \\
 \frac{20.3}{16.3} & & & & & & & & & & & \frac{4.3}{30}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{2.9}{30} & \frac{3.5}{25} & \frac{39.27}{4.31} & \frac{39.22}{4.35} & \frac{5.1}{15} & 5.0 & \frac{5.1}{8} & \frac{5.3}{12} & \frac{5.0}{18} & \frac{4.5}{21} & \frac{4.4}{30}
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{3.3}{29} & \frac{39.57}{4.0} & \frac{4.22}{16.4} & \frac{39.35}{5.0} & \frac{5.1}{14} & \frac{5.1}{10} & 5.0 & \frac{4.7}{5.1} & \frac{5.3}{11} & \frac{4.9}{15} & \frac{4.9}{19} & \frac{4.6}{21} \\
 \text{(Driveway)} & & & & & & & & & & &
 \end{array}$$

$$\begin{array}{cccccccc}
 \frac{3.1}{4.2} & \frac{39.48}{4.09} & \frac{39.32}{4.25} & \frac{5.1}{16.4} & \frac{5.0}{12} & \frac{5.0}{9} & 5.0
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{2.2}{30} & \frac{2.6}{23} & \frac{39.53}{3.1} & \frac{39.43}{3.2} & \frac{4.1}{13} & \frac{4.1}{7} & 4.1 & \frac{4.2}{8} & \frac{4.4}{11} & \frac{3.7}{21} & \frac{3.5}{30} \\
 \text{Ho} & & & & & & & & & &
 \end{array}$$

$$\begin{array}{cccccccccccc}
 \frac{2.0}{46} & \frac{2.9}{20} & \frac{39.73}{3.0} & \frac{39.63}{4.0} & \frac{4.3}{13} & \frac{4.2}{10} & 4.2 & \frac{4.3}{7} & \frac{4.6}{11} & \frac{4.0}{17} & \frac{2.9}{21} & \frac{2.8}{35} \\
 \text{Ho} & & & & & & & & & &
 \end{array}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

942.63

4				38.3
---	--	--	--	------

+16

+12

38.1

+38

driveway Lt. 38.0^{ok}

+70

37.6

5

37.5

07

end SW K+

+25

37.3

+50

37.1

L+

L

R+

$$\begin{array}{cccccccccccc}
 H_0 & 39.83 & 39.5 & 39.63 & & & & & & & & \\
 \frac{2.1}{35} & \frac{2.8}{20} & \frac{3.0}{16} & \frac{4.1}{13} & \frac{4.3}{8} & 4.3 & \frac{4.6}{11} & \frac{4.1}{19} & \frac{3.0}{22} & \frac{3.0}{30} & & \checkmark
 \end{array}$$

$$\begin{array}{cccccccccccc}
 39.83 & 39.63 & & & & & & & & & & \checkmark \\
 \frac{2.5}{30} & \frac{2.8}{19.9} & \frac{3.0}{15.9} & \frac{4.3}{14} & 4.5 & \frac{4.7}{11} & \frac{4.5}{19} & \frac{4.1}{22} & \frac{4.2}{30} & & &
 \end{array}$$

$$\begin{array}{cccccccccccc}
 39.73 & 39.43 & & & & & & & & & & \checkmark \\
 \frac{2.7}{48} & \frac{2.9}{20} & \frac{3.2}{16} & \frac{4.7}{10} & 4.6 & \frac{4.9}{11} & \frac{4.1}{25} & \frac{4.3}{30} & & & &
 \end{array}$$

$$\begin{array}{cccccccccccc}
 H_0 & 38.93 & 38.93 & & & & & & & & & \checkmark \\
 \frac{3.1}{34} & \frac{3.7}{20} & \frac{3.7}{16} & \frac{5.1}{12} & 5.0 & \frac{5.1}{12} & \frac{4.7}{22} & \frac{4.6}{30} & & & &
 \end{array}$$

$$\begin{array}{cccccccccccc}
 38.27 & 38.23 & & & & & & & & & & \checkmark \\
 \frac{4.1}{40} & \frac{4.36}{20} & \frac{4.4}{16} & \frac{5.4}{12} & \frac{5.2}{8} & 5.1 & \frac{5.4}{12} & \frac{4.9}{22} & \frac{4.5}{48} & & &
 \end{array}$$

$$\begin{array}{cc}
 37.61 & \\
 \frac{5.02}{15.5} & \frac{5.05}{19.5}
 \end{array}$$

$$\begin{array}{cccccccccccccccc}
 37.93 & 37.73 & & & & & & & & & & & & & & \checkmark \\
 \frac{4.7}{30} & \frac{4.7}{20} & \frac{4.9}{16} & \frac{5.9}{12} & \frac{5.6}{9} & 5.3 & \frac{5.4}{8} & \frac{5.7}{13} & \frac{5.98}{15.5} & \frac{5.09}{19.5} & 5.0 & 5.0 & & & &
 \end{array}$$

$$\begin{array}{c}
 TMH \\
 37.28 \\
 \frac{5.35}{138}
 \end{array}$$

$$\begin{array}{cccccccccccccccc}
 H_0 & 37.20 & 37.10 & & & & & & & & & & & & & \checkmark \\
 \frac{4.8}{39} & \frac{5.43}{20} & \frac{5.53}{16} & \frac{6.0}{14} & \frac{5.8}{9} & 5.5 & \frac{5.7}{9} & \frac{6.0}{13} & \frac{5.43}{16} & \frac{5.5}{20} & \frac{5.5}{30} & & & & &
 \end{array}$$

Sta	+	π	-	Elev
		942.63		
TP	4.03	940.83	5.83	936.80
				36.8

5 +75



6

36.5

+25

36.3

+50

36.2

+75

36.6

L+

L

R+

$\frac{4.3}{30}$ $\frac{4.20}{20}$ $\frac{4.21}{16}$ $\frac{4.5}{13}$ $\frac{4.3}{9}$ 4.0 $\frac{4.2}{9}$ $\frac{4.4}{13}$ $\frac{4.2}{16}$ $\frac{4.28}{20}$

$\frac{4.4}{50}$
 $\frac{50}{100}$

$\frac{4.8}{38}$ $\frac{4.72}{20}$ $\frac{4.47}{16}$ $\frac{4.6}{11}$ $\frac{4.3}{9}$ $\frac{4.4}{9}$ $\frac{4.7}{13}$ $\frac{4.62}{16}$ $\frac{4.72}{20}$

$\frac{4.5}{30}$

$\frac{4.8}{30}$ $\frac{4.65}{20}$ $\frac{4.66}{16}$ $\frac{4.7}{10}$ 4.5

$\frac{4.5}{8}$ $\frac{4.87}{16}$ $\frac{4.88}{20}$ $\frac{4.7}{22}$ $\frac{4.8}{30}$

$\frac{4.6}{22}$ $\frac{4.60}{20}$ $\frac{4.67}{16}$ $\frac{4.6}{14}$ $\frac{5.2}{12}$ $\frac{4.7}{10}$ 4.6 $\frac{4.7}{9}$ $\frac{5.2}{15}$ $\frac{4.88}{16}$ $\frac{4.89}{20}$ $\frac{4.9}{30}$

$\frac{5.0}{35}$ $\frac{4.9}{35}$

$\frac{4.4}{31}$ $\frac{4.50}{20}$ $\frac{4.51}{16}$ $\frac{5.2}{12}$ $\frac{4.6}{10}$ 4.2 $\frac{4.5}{16}$ $\frac{5.3}{14}$ $\frac{4.9}{16.2}$ $\frac{4.93}{20.2}$ $\frac{4.94}{44}$

123
4.3

Sta + π - Elev

940.83

6 +85 37.0

+88

37.3

+93.7

Note on Open Grate NH.

To NE 2.6' to incoming ^{12"} FL From top
To NW 4.0 to out Fall 12" FL " "

7 +03 37.5

+08

+11 37.5

+29

S. edge Pavement 38.3

7 +51.27 ϕ STH # C1 38.11

BM @ 451 943.25 2.09 938.74

L+

E

R+

36.46
SW 16.36

$\frac{2.9}{31}$	$\frac{7.37}{21}$	$\frac{4.17}{15}$	$\frac{4.6}{14}$	$\frac{5.2}{13}$	$\frac{5.2}{11}$	$\frac{4.1}{10}$	3.8	$\frac{4.2}{16}$	$\frac{5.4}{14}$	$\frac{7.92}{11.4}$	48.9	$\frac{4.7}{21}$	$\frac{4.9}{30}$
------------------	-------------------	-------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	---------------------	------	------------------	------------------

 $\frac{2.9}{50}$

 FL
 $\frac{5.53}{\text{end } 15'' \text{ CM}}$

$\frac{2.88}{33}$	$\frac{2.85}{15}$	$\frac{3.7}{11}$	3.5	$\frac{3.9}{10}$	4.48	$\frac{5.52}{12.5/41}$	$\frac{4.9}{16.4}$	35.93 SW
-------------------	-------------------	------------------	-----	------------------	------	------------------------	--------------------	-------------

$\frac{2.5}{32}$	$\frac{2.9}{27}$	$\frac{3.77}{13.8}$	$\frac{3.5}{13.8}$	3.3	$\frac{3.4}{12}$	$\frac{4.77}{16.4}$	$\frac{4.81}{20.4}$	$\frac{4.7}{30}$	✓
------------------	------------------	---------------------	--------------------	-----	------------------	---------------------	---------------------	------------------	---

 FL. 12" V.C.P.
 6.38

$\frac{3.3}{50}$	$\frac{3.4}{26}$	3.3	3.3	$\frac{3.2}{8}$	$\frac{3.0}{15.2}$	$\frac{2.7}{15.2}$	$\frac{2.75}{21.2}$	$\frac{5.8}{29}$
------------------	------------------	----------------	-----	-----------------	--------------------	--------------------	---------------------	------------------

 $\frac{4.8}{41}$ $\frac{5.4}{36}$
 $\frac{2.53}{3.53}$

2.72

Top Hyd NW cor Shady Lane & SFH, # 61

Sta	+	π	-	Elev
		943.25		
B.M.	4.10		0.88	942.37
				942.38

B.M.	4.10	42.85		938.75
------	------	-------	--	--------

Top M.H.			5.57	37.28
----------	--	--	------	-------

4+80 Rt Ho. Elev.			4.53	38.32
-------------------	--	--	------	-------

3+87 Top sw. rt	Ho. =	3.01	39.84	✓
		4.21	38.64	

2+90 sw. 16' Rt		4.48	38.37	
-----------------	--	------	-------	--

3+25 Ho. rt.		3.28	39.58	✓
--------------	--	------	-------	---

2+75 Ho. rt.		3.41	39.44	✓
--------------	--	------	-------	---

B.M.	3.11	942.45		939.35
------	------	--------	--	--------

Top curb 25' rt		4.83	37.62	
-----------------	--	------	-------	--

" " 25' Lt.		5.02	37.43	
-------------	--	------	-------	--

" end curb Lt		4.94	37.51	
---------------	--	------	-------	--

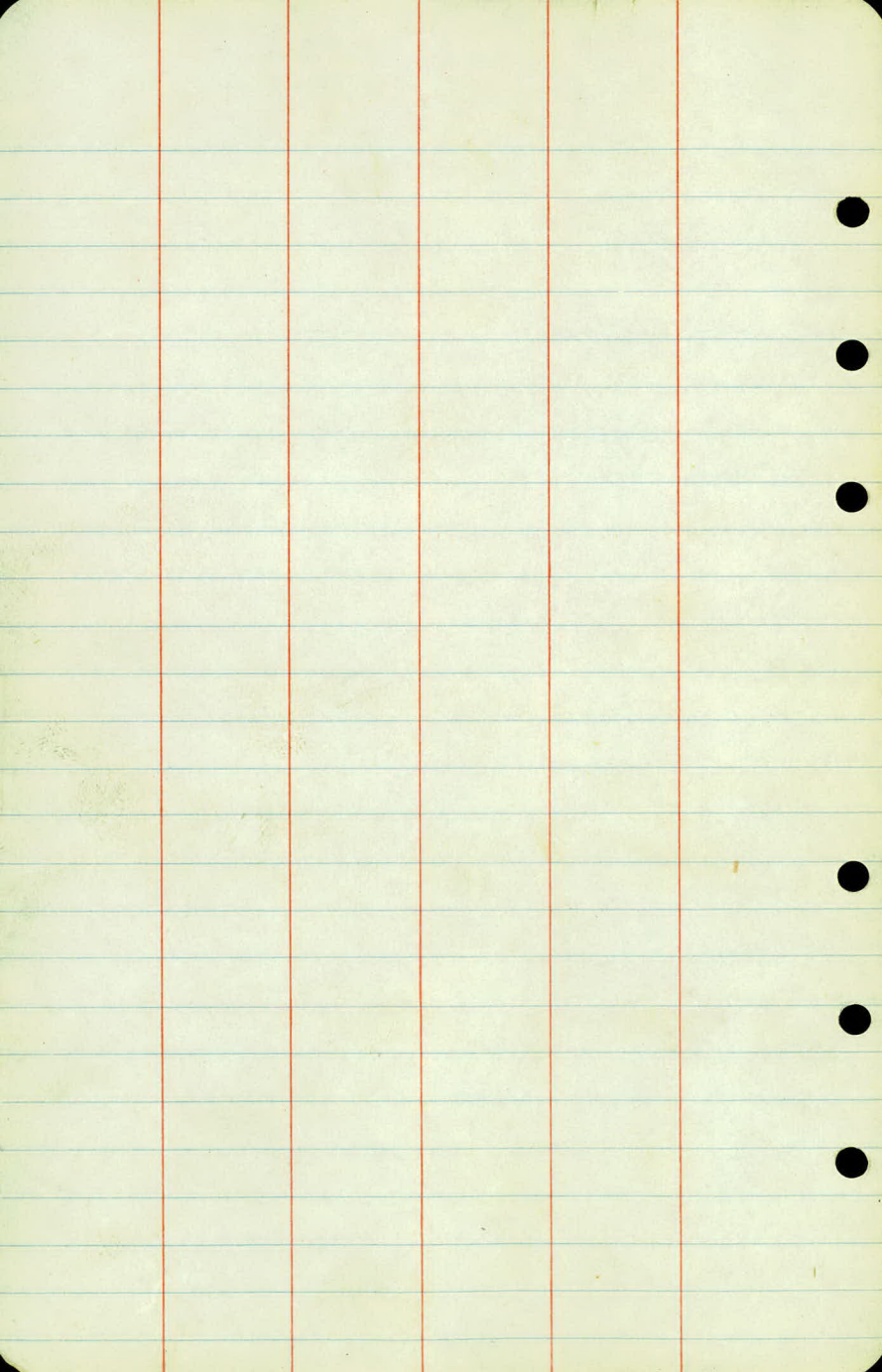
" " " rt		4.63	37.82	
----------	--	------	-------	--

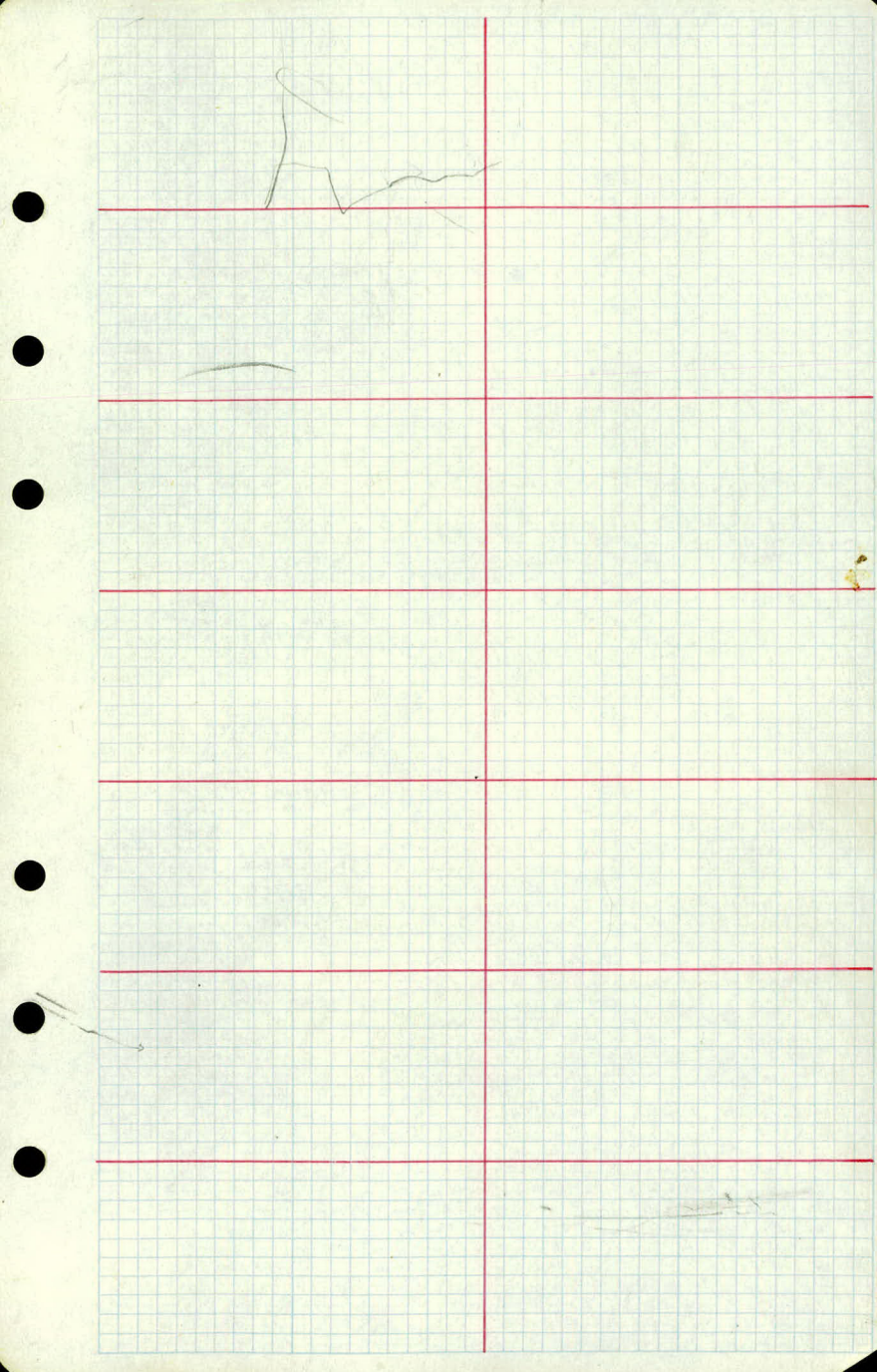
Lt

C

Rt

Top Hyd NE Cer. Burson & Ist.





Location of 6' steps

Shady Lane - STH # 61

+ 9.25 Top Step outside 21.5

+ 9.15 Top Steps inside 15.5

+ 3.16 Bot Step inside 15.6

+ 3.14 Bot. Step outside 21.6

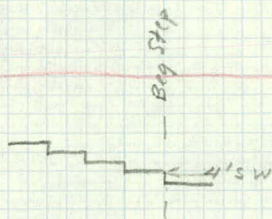
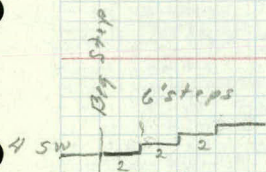
7

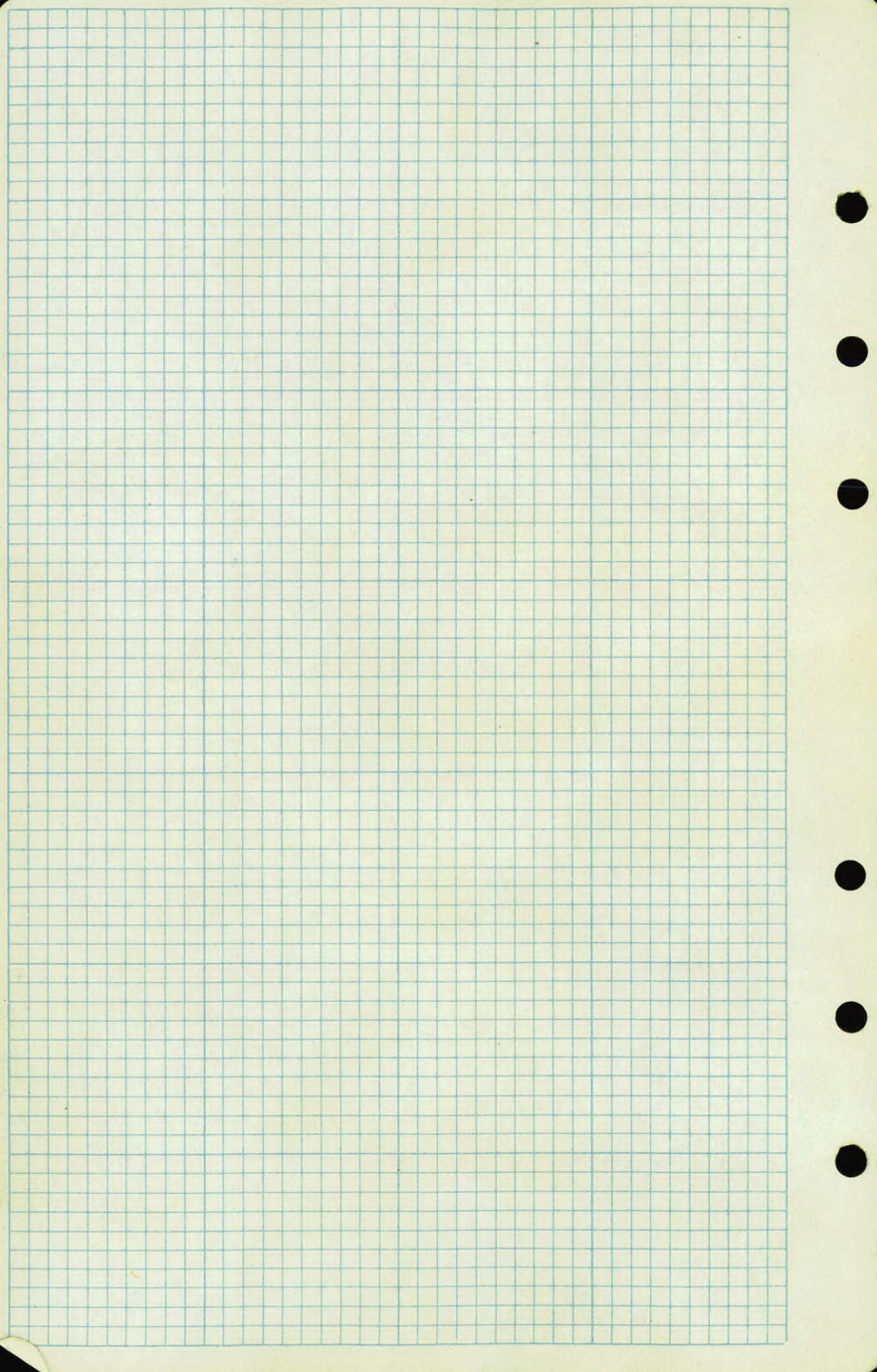
+ 91.75 Top Steps inside 15'

+ 91.74 " " outside 21'

+ 85.25 Bot. Step. outside - 21'

+ 85.29 " " inside 15'





Shady Lane.

Sta	+	π	-	Elev
-----	---	-------	---	------

B.M.	2.80	941.55		938.75
------	------	--------	--	--------

Top MH			3.56	37.99
--------	--	--	------	-------

~~-12.3~~

~~938.75~~

$$\begin{array}{r} 30 \\ 37.7 \\ \hline 12.3 \end{array}$$

12.3 To inv. 23.69

~~~~~

|      |      |        |  |        |
|------|------|--------|--|--------|
| B.M. | 1.37 | 940.72 |  | 939.35 |
|------|------|--------|--|--------|

$$\begin{array}{r} 12.12 \\ 3.90 \\ \hline 16.02 \end{array}$$

Inv.

16.02 924.70

1.8  
12  
3-  
18  
216

Top F/Hyd. SE cor. Shady lane + #41

4 1/2' Lt @ 7+60



Spk in PP Lt @ 1+20 (approx)

outlet @ Lake (1.8' dia)  
0-42 - 7' Lt.

